Heterogeneous Catalysts for Conversion of Biodiesel-Waste Glycerol into High-Added-Value Chemicals

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Abstract: The valuable products produced from glycerol transformation have become a research route that attracted considerable benefits owing to their huge volumes in recent decades (as a result of biodiesel production as a byproduct) as well as a myriad of chemical and biological techniques for transforming glycerol into high-value compounds, such as fuel additives, biofuels, precursors and other useful chemicals, etc. Biodiesel has presented another challenge in the considerable increase in its byproduct (glycerol). This review provides a recent update on the transformation of glycerol with an exclusive focus on the various catalysts’ performance in designing reaction operation conditions. The different products observed and cataloged in this review involved hydrogen, acetol, acrolein, ethylene glycol, and propylene glycol (1,3-propanediol and 1,2-propanediol) from reforming and dehydration and hydrogenolysis reactions of glycerol conversions. The future prospects and critical challenges are finally presented.

Keywords: glycerol; biodiesel-biowaste; value-added products; hydrogen energy; lignocellulosic biomass valorization; fuels; catalysts

1. Introduction

Petroleum fuels became the primary energy source for transport requirements during the twentieth century. Since the beginning of the twenty-first century, primarily all vehicles run with diesel, gasoline, or natural gas [1]. Around the world, the population is increasing, thereby increasing energy requirements simultaneously, and nowadays, the origin of energy is mostly fossil fuels such as oil, coal, or natural gas [2–4]. Generally, fossil fuel-based carbon dioxide emissions are unaltered and grant the so-called “greenhouse effect”, which intensively affects the climate changes [5,6]. Furthermore, with the rise in pollution and crude oil prices, oil, coal, and gas burn not only to fulfills energy demands, but also contribute to the global warming crisis. The burning of fossil fuels produces a substantial amount of carbon dioxide, which traps heat in the atmosphere and contributes to global
warming [7,8]. Wind, water, biomass, and solar energy are primary alternative energy sources to stop using fossil fuels.

Biomass is currently achieving a significant focus in terms of providing the world’s energy needs [9–11]. Due to its eco-friendly nature and low sulfur production, it is estimated that by 2050, biomass will contribute 50% of the total energy demand. The demand for energy worldwide is expected to increase up to 48% by 2040 [10]. Thus, bio-derived fossil fuels are crucial for reducing the carbon footprint [9–11].

Biodiesel is commonly manufactured from animal fat or vegetable oil, and through the transesterification technique, glycerol is produced as a waste product (Equation (1)) [12]. Biodiesel production is growing continuously due to the growing fossil fuel demand for transportation and industries. The biodiesel trend enhanced glycerol production as a byproduct [11]. Glycerol contains higher hydrogen moles compared to ethanol and methanol [13]. Each 1 ton of biodiesel production from plants produces 110 kg of glycerol. Worldglycerol production was increased fivefold to reach 36 billion liters between 2006–2018 [14]. It is pretty clear that glycerol availability is not in doubt; it is believed that generally, glycerol production will continue to increase due to an upsurge in biodiesel production. Glycerol was raised as an exciting biomass feedstock for high-value-added product conversion due to its modest price and high availability in the market [15]. Hence, glycerol transformation into other useful products is the essence of overall improvement in biodiesel production economics [16].

\[
\text{C}_3\text{H}_5(\text{OOC})_3(\text{R}_n)_3 + 3\text{R}'\text{OH} \rightarrow 3\text{R}_n\text{COOR} + \text{C}_3\text{H}_5(\text{OH})_3
\]  
(1)

Glycerol is crucial for feedstocks in food, pharmaceutical, and other industries and is produced through microbial or biodiesel. Semkiv et al. explained glycerol production by microbes (Saccharomyces cerevisiae, Osmotolerant yeasts, Microalgae, and cyanobacteria). High-added value chemicals produced from glycerol follow different paths such as oxidation, reforming, carboxylation, acetalization, esterification, hydrogenolysis, dehydration, etc., as shown in Table 1 [16–21]. Glycerol-based additives have been used for blending agents in gasoline, diesel fuel, and biodiesel [22].

**Table 1.** Derivatives of glycerol.

| Chemical Derivative | Chemical Structure | Route from Glycerol |
|---------------------|-------------------|---------------------|
| Syngas              | H2 + CO           | Reforming           |
| 1,2 Propanediol     |                   | hydrogenolysis      |
| 1,3 Propanediol     |                   | hydrogenolysis      |
| Acrolein            |                   | Dehydration         |
| Ethylene oxide      |                   | Via 1,2 propanediol |
| Propylene oxide     |                   | Via 1,3 propanediol |
Table 1. Cont.

| Chemical Derivative      | Chemical Structure | Route from Glycerol |
|--------------------------|--------------------|---------------------|
| Epichlorohydrin          | ![Epichlorohydrin](image1) | Cyclization         |
| Polyglycerol             | ![Polyglycerol](image2) | Oligomerization     |

Martin and Richter presented a review for glycerol oligomerization to diglycerol and triglycerol, focusing on utilizing acidic and basic heterogeneous catalysts. Pure glycerol was replaced through its oligomers for numerous uses in the cosmetics and food industries [23]. Razali and Abdullah presented a review for catalyzing glycerol to lactic acid, where mixed metal oxides and bimetallic catalysts were found to be promising candidates [24]. Most of the published reviews have summarized the chemo, as well as biochemocatalytic transesterification and economic aspects of various transformation routes discussed [25,26]. A few comprehensive reviews have been published on the catalytic conversion of glycerol via reforming, dehydration, and hydrogenolysis. Since glycerol transformation is rapidly developing and its critical features are not clear, it is important to gather information on recent developments. Consequently, the objective of this review is to provide an update on the transformation of glycerol derived from biodiesel plants using heterogeneous catalysts into different products (chemicals, fuel additives, fuels). The review is organized well into three sections, dedicated to three major types of reactions (reforming, dehydration, and hydrogenolysis), with an emphasis on the performance of catalysts in designing reaction conditions. The different products observed and cataloged in this review involved hydrogen, acetol, acrolein, ethylene glycol, 1,3-propanediol (1,3-PDO), and 1,2-propanediol (1,2-PDO) from reforming, dehydration and hydrogenolysis reactions of glycerol conversions.

The production of chemical products from the catalytic transformation of glycerol is shown in Figure 1. Glycerol is produced from the transesterification of biodiesel and vegetable oils and animal fats, and the fermentation of carbohydrates. Syngas produced from glycerol yield liquid hydrocarbons, methanol, and other value-added products from the Fischer–Tropsch process. Syngas through the water–gas shift reaction produces liquid hydrocarbons, which include diesel, liquid naphtha, etc. Furthermore, through the methanol synthesis process, syngas produces methanol, and further methanol is used for the transesterification process and to produce chemicals [27].
2. Glycerol Reforming

The glycerol transformation carried out through combustion in the past was unsafe, uneconomic, and technically deficient due to the high temperature employed, unwanted gas emission, and complex product [27,28]. Reforming techniques have gained acceptance by industrialists and researchers in view of their efficiencies. Steam, aqueous, and autothermal reforming processes have been primarily investigated in glycerol reforming. The steam reforming reaction is one of the most common reactions used in hydrogen synthesis. Low pressure and very endothermic reactions promote hydrogen selectivity. The aqueous phase reforming (APR) method is regarded as an inexpensive method for producing H\textsubscript{2} due to its lower temperature and lack of vaporizing water and fuels [29,30]. Glycerol has a wide product distribution due to its complexity compared to low-chain hydrocarbons or alcohols and to the numerous reactions associated with the reforming process (Figure 2). However, this technique creates H\textsubscript{2} without vaporizing the feedstock, resulting in significant energy savings [31]. Supercritical water gasification (SCWG) is a cost-effective method of turning biomass (such as food waste, paper industrial waste, sewage sludge, agricultural waste, and forestry residue) into hydrogen-rich syngas [32]. Chemical looping steam reforming (CLSR), which uses oxygen carriers (OCs) as a catalyst, has been widely recognized as a highly effective method for generating hydrogen from catalytic steam reforming [33].

Bio-derived liquids steam reforming produces hydrogen and becomes interested due to the environment and raises hydrogen demand, specifically in proton-exchange membrane fuel cells (PEMFC) [34]. The low temperature and high-pressure process conditions, concentrated feed, and acidic catalysts are used for the supercritical water reforming process. High temperature and low pressure, diluted feed, and alkali catalyst are used for gasification [35].
The glycerol reforming and endothermic reactions took place. Hence, the heat needed for the decomposition of glycerol (Equation (2)) is significantly larger than the water–gas shift (WGS) reaction (Equation (3)), where heat is produced as energy. As operated under atmospheric pressure, glycerol steam reforming (Equation (4)) becomes desirable with less fear of protection. Considerably, 1 mol of glycerol converts to produce 7 mol of hydrogen (Equation (3)). Vast amounts of steam and elevated temperature shift a reaction forward to equilibrium, and hence much more H$_2$ is generated [36].

\[
\text{C}_3\text{H}_8\text{O}_3 \leftrightarrow 4\text{H}_2 + 3\text{CO} \quad \text{Decomposition Reaction} \quad (2)
\]

\[
\text{CO} + \text{H}_2\text{O} \leftrightarrow \text{H}_2 + \text{CO}_2 \quad \text{Water Gas Shift Reaction} \quad (3)
\]

\[
\text{C}_3\text{H}_8\text{O}_3 + 3\text{H}_2\text{O} \leftrightarrow 7\text{H}_2 + 3\text{CO}_2 \quad \text{Steam Reforming Reaction} \quad (4)
\]

The mentioned noble metal catalysts, Pt [37,38], Ir [39], Ru [40], and Rh [41,42], have shown good resistance to coke and catalytic activity. Vaidya and Rodrigues studied Ni, Pt, and Ru catalysts that promote hydrogen production but cause deactivation by dehydration [43].

### 2.1. Platinum Catalysts for Glycerol Reforming

Doukkali et al. investigated Pt and/or Ni supported over γ-alumina catalyst for the generation of hydrogen by a method of APR through three preparation methods of catalyst: impregnation method, and sol-gel in acidic and basic medium. Total glycerol transformation occurred with maximum hydrogen production by sol-gel in basic method over PtNiAl (T = 250 °C, P = 30 bar, and WHSV = 2.6 hr$^{-1}$). The acidity of the superficial hydroxyl groups on the -AlOOH surface could be to blame for the lower glycerol conversion into gaseous products, favoring dehydration processes and resulting in more OHCs in the liquid phase. In fact, by blocking surface hydroxyl sites on -Al$_2$O$_3$, structural alterations in hydrothermal settings were explored to create efficient alumina catalysts for APR pro-
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The drop in H₂ production could be explained by Ni particle aggregation and reoxidation of Ni particles. These behaviors combined with the adsorption of carbonaceous molecules/organic compounds identified on several of the catalysts could be the primary causes of their deactivation [37].

Pompeo et al. investigated SiO₂ catalyst supported with Pt and Ni through the ion-exchange method for steam reforming to produce hydrogen. The experiment for the steam reforming reaction of glycerol has demonstrated that using 1 Pt and 2 Pt catalysts. The more active and stable catalyst was Pt compared to Ni catalyst. At 350 °C, a complete conversion to gas was achieved with a space-time of 1.66 and 0.88 min, respectively. Due to the fact that the Ni catalyzed the WGS reaction to remove the CO adsorbed on the surface and turn it into CO₂, the selectivity of gas products was significantly different. Only 3% CO was obtained using the 5 Ni catalyst at 450 °C for 1.66 min. During 40 hr activity test on stream at 350 °C, the 2 Pt catalyst allowed entire conversion to gas without deactivation. It was also suggested that bimetallic catalyst research is required to obtain a system with high selectivity for H₂ and good stability [38].

2.2. Ruthenium Catalysts for Glycerol Reforming

Ru catalyst supported over core-shell metal-ceramic micro composites, created at low temperature and 1 atm pressure through microwave-induced hydrothermal oxidation technique (MW-HTO) of aluminum (Al) metal particles. The highest glycerol turnover ratio was achieved over Al, and Ru-modified Al₂O₃ at Al compared with Ru-modified MgAl₂O₄ and Ru-modified Al₃O₅ catalysts, suggesting that Al metal particles seem to be more effective in preparing MgAl₂O₄ at Al and Al₂O₅ at Al composite structure. The highest selectivity of hydrogen was 70% at Ru/MgAl₂O₄ at Al catalyst at 823 K reaction temperature, 1 atm pressure with 870 mmgcat⁻¹ h⁻¹ feed flow rate. The Ru/MgAl₂O₄@Al and Ru/Al₂O₅@Al catalysts have 2–3 times the glycerol conversion rates of their Ru/MgAl₂O₄ and Ru/Al₂O₅ counterparts, owing to enhanced heat transfer via the metal-ceramic composite catalytic architectures [40]. Glycerol steam reforming process over Ru doped Al₂O₃ catalyst. In total, 89.1% glycerol transformed to produce 0.49 (mol/mol) yield of hydrogen at T = 500 °C, P = 0.1 MPa and 1.98 W/FA₀. This research has aided in developing reactor systems for producing hydrogen from glycerol steam reforming [41].

2.3. Rhodium Catalysts for Glycerol Reforming

Martinez et al. studied hydrogen production from glycerol reforming using fluorite-type oxides CeZr-CoRh prepared by the sol-gel method. 100% glycerol was transformed to produce 86% hydrogen yield at 650 °C. The activity data showed that the catalysts’ ability to activate H₂O under reaction circumstances was connected to selective H₂ generation. This process guarantees that the by-products are steam reformed to H₂. As this capacity deteriorates, H₂ generation decreases, steam reforming capability reduces, and glycerol decomposition takes over. In this scenario, the creation of condensable compounds, such as hydroxyacetone, acetaldehyde, and acrolein, was aided by the production of CO, CH₄, and C₂H₄ [44].

Lee and Doohwan synthesized Core–shell MgAl₂O₄ metal–ceramic composites at Al catalyst by hydrothermal method, and Rh (1, 3, and 5 wt.% loading) modified MeAl₂O₄ catalysts were synthesized by incipient wetness impregnation method. Then, 100% glycerol transformed to produce Rh/MgAl₂O₄ at Al catalyst [T = 450 °C, and WHSV = 34,000 mL g⁻¹ h⁻¹]. The high surface area and complex surface morphological properties of MeAl₂O₄@Al as a catalyst enhance increased Rh cluster dispersion while hindering their thermal sintering during glycerol steam reforming processes at high temperatures. Rh/MeAl₂O₄@Al had a 20–30% greater glycerol conversion turnover rate than Rh/MeAl₂O₄ (both Rh cluster sizes are similar), indicating that the facilitated heat and mass transfer through the unique MeAl₂O₄@Al microstructures cooperated constructively for the reactions. These are being explored as future research topics [45]. Baca et al. studied Rh, Ni, and Co metal-doped over Al₂O₃–ZrO₂–TiO₂ (AZT) for syngas production through carbon dioxide reforming.
of glycerol. Then, 1 wt.% Rh doped AZT, 5 wt.% Ni-doped AZT, and 5 wt.% Co-doped AZT catalysts were synthesized through the incipient impregnation method. The glycerol transformation was 80% achieved with 24% maximum hydrogen yield on Rh doped AZT catalyst at 750 °C. Glycerol Conversion reduced in the given sequence: 1% Rh doped AZT > 5% Ni doped AZT > 5% Co-doped AZT. Rh doped AZT catalyst remained stable due to fewer coke formations and a shortage of sintering. During the 72-h testing, the decrease in CO₂ conversions was less than 13%, indicating the remarkable stability of Rh/AZT and Ni/AZT [42]. Delparish et al. produced syngas from glycerol by oxidative steam reforming. The impregnation technique was used to prepare 2 wt.% of Rh doped Al₂O₃ catalysts. The glycerol was completely converted at 550 °C, and maximum hydrogen yield was achieved at 700 °C. Temperature influenced product distribution by increasing the amount of combustible species in the product mixture that were oxidized. The effect became more severe when C/O was lowered from 1.125 to 0.75. The promotion of WGS in the presence of steam was confirmed by reducing S/C from 5 to 4 and then from 4 to 3, which resulted in monotonically decreased H₂ and CO₂ yields and an increase in CO yield [46]. Danga et al. studied glycerol and ethanol for dry reforming with CaCO₃ to produce syngas. A series of metal components, such as nickel, iron, copper, platinum, palladium, ruthenium, and rhodium, were used to promote dry reforming. In these series of metals, nickel became a promising candidate due to its outstanding performance, as well as its low price. Here, 100% glycerol conversion along with approximate 92% syngas selectivity achieved on 10 wt.% Ni contained in CaCO₃ catalyst [T = 550 °C, and P = 1 atm.]. The CO₂ released from the CaCO₃ catalyst eliminated cokes and attained stability. The direct use of CaCO₃ in this process was discovered viable, and the CO₂ generated from CaCO₃ decomposition may be used to modify the H₂/CO ratio. Ni was the most promising contender among the active metals, including Ni, Co, Fe, Cu, Rh, Ru, Pt, and Pd, due to its great performance and low price. Over the 10 Ni–CaCO₃ catalyst, 100% conversion of glycerol and ethanol, 92% summed H₂ and CO selectivity, and an H₂/CO ratio of 1.2 could be reached under ideal conditions. Meanwhile, the robustness of this integrated technique was proved over five dry reforming–regeneration cycles. The findings suggest a novel way to use CO₂ in the form of carbonates [47].

2.4. Nickel Catalysts for Glycerol Reforming

The catalyst based on Ni becomes a choice for the reason that the metallic sites of Ni work well enough in water gas shift reaction as well as C–H and C–O cleavage. Nevertheless, the tremendous challenge is how to control catalysts’ deactivation triggered by sintering and deposition of carbon at catalyst active sites under optimum operating conditions [13]. Hence, various protocols [40,48] and supports like Al₂O₃ [49–51], ZrO₂ [52–54], CeO₂ [55,56] were generated. Yancheshmeh et al. suggested a new and simple method for preparing Ni-modified Al₂O₃ spinel catalyst from the steam reforming technique of glycerol for the production of hydrogen. Solvothermal preparation method was used for catalyst represented as NiAl-G1, and the coprecipitation preparation method was used for catalyst described as NiAl-G2 as well as NiAl-C (NiAl₂O₄ catalyst synthesized via the coprecipitation method was designated as NiAl-C). The maximum hydrogen yield was 76.38% achieved with 95.42% maximum glycerol transformation on NiAl-G2 catalyst 630 °C, 1 atm, and 19,600 cm³/gcat/h space velocity reaction conditions. By creating an oxidative environment surrounding nickel active sites, the creation of a well-dispersed CeAlO₃ phase slowed the growth of filamentous carbon on the nickel surface and aided the gasification of carbon deposits. During the 16-h SRG process, the catalytic activity was maintained, and the rate of coke generation was as low as 0.0004 gcoke/gcatal·h⁻¹. These findings support Ce/NiAl-G2’s potential as a catalyst for the SRG reaction [56]. Ni added to CaO-modified attapulgite (CaO–ATP) catalyst from reforming of glycerol for hydrogen manufacturing. Using the impregnation technique, NiAl₂O₃, Ni-ATP, and Ni-CaO-ATP catalysts can be synthesized. A maximum hydrogen yield of 85.3% was achieved on Ni-CeO-ATP catalyst with 93.71%
glycerol conversion at $T = 600 \, ^\circ\text{C}$ and GHSV = 1 h$^{-1}$ reaction condition. The stability of catalyst showed that ATP had better resistance for deposition of carbon compared to alumina and CaO addition further reduced the production of carbon. Due to its unusual intermediate structure, ATP outperformed Al$_2$O$_3$ as a carrier. When CaO was utilized as an ATP modifier, it promoted the water gas shift reaction, resulting in increased hydrogen yield, hydrogen selectivity, and a reduction in CO production. The stability results revealed that ATP is more resistant to carbon deposition than Al$_2$O$_3$, and the addition of CaO lowered carbon formation even more. As a result, a Ni-based catalyst supported on a CaO-modified attapulgite could be a potential material for efficient glycerin steam reforming to create H$_2$ [57].

Wu et al. explored the mesoporous Ni-Cu/CeO$_2$ for the production of renewable hydrogen via APR of glycerol. The C-C breakage of glycerol benefits from Ni, but Cu can amplify the WGS reaction. Cu metal’s surface is amenable to adsorption Carbonyl radical following glycerol’s decarbonylation and hydroxyl free radical in the solution, which facilitates the reaction. Consequently, the addition of Cu element enhanced the proportion of H$_2$ and CO$_2$ in the overall gas. It was discovered that increasing the catalyst’s Cu concentration improved hydrogen production (125.08 to 195.57 $\mu$mol min$^{-1}$ g$^{-1}$ cat). Additionally, the CO$_2$ in overall gas was absorbed by the addition of CaO and it lowers the activation energy. Hence, 1Ni2Cu/CeO$_2$ + 0.2gCaO catalyst shows H$_2$ production rate increased from 168.97 to 301.92 $\mu$mol min$^{-1}$ g$^{-1}$ cat. Therefore, improved H$_2$ production as a result of the inclusion of Cu and CaO [29].

Liu et al. studied MgO supported Ni-Co bimetallic catalyst prepared by sol-gel method followed by calcination. The resulted catalyst examined the APR of glycerol for hydrogen production. After addition MgO support, H$_2$ production activity improves by 1.5 times compared to pure Ni-Co bimetallic catalyst. Due to the in-situ adsorption and removal of CO$_2$, the WGS reaction was further stimulated with the addition of CaO, and the methanation reaction was inhibited, resulting in the catalyst having a high activity of hydrogen production. The stability test also shown that the gelatinous MgO supports had an impact on the catalyst’s activity and stability [30].

Veiga et al. studied crude glycerol steam reforming with oxalic acid to synthesize Ni-doped La-Zr catalysts. Ni-doped La-Zr catalyst was prepared with the coprecipitation method at different calcination temperatures. Ni-doped La-Zr catalysts calcined at 850 $^\circ$C achieved 90% hydrogen yield and 99.9% glycerol conversion. The catalyst prepared at 850 $^\circ$C calcination and operated at 650 $^\circ$C reaction showed higher catalytic stability, activity, and better resistance to carbon formation. The greatest performance seen for Ni-850 catalysts is mostly due to the development of oxygen vacancies caused by nickel substitution into the La-Zr lattice during calcination, favoring the oxidation of carbon deposits throughout the process [58].

Charisiou et al. investigated Ni supported over Y$_2$O$_3$–ZrO$_2$ catalyst for the glycerol steam reforming. The catalyst synthesized through the impregnation technique was Ni modified Zr and Ni modified YZr. The maximum transformation was 90% achieved at 700 $^\circ$C, and the maximum H$_2$ selectivity was 82% achieved at 450 $^\circ$C over Ni modified YZr catalyst. The research on spent catalyst revealed the less carbon deposition on Ni/Zr (Ni modified Zr) catalyst as it was more graphitic in nature and higher carbon deposition on Ni/YZr spent catalyst. The addition of Y$_2$O$_3$ stabilized the ZrO$_2$ tetragonal phase, resulted in more easily reducible NiO nanoparticles, increased the O$_2$ storage capacity of the support and the medium strength acid sides of the catalyst, and, despite having a higher concentration of basic sites, the Ni/YZr presented more stable monodentate carbonates. Allyl alcohol, acetaldehyde, acetone, acrolein, acetic acid, and acetol were the primary liquid products detected for both catalysts. Although higher amounts of carbon were deposited on the Ni/YZr spent catalytic sample (0.70 g$_{\text{coke}}$/g$_{\text{catal}}$ compared to 0.51 g$_{\text{coke}}$/g$_{\text{catal}}$ for the Ni/Zr catalyst), the addition of Y$_2$O$_3$ on to the ZrO$_2$ support resulted in structures with lower crystallinity (amorphous carbon) that are more easily oxidized during the reaction. The coke deposits found on spent Ni/Zr catalysts, on the
other hand, were graphitic structures with little flaws, resulting in the deadly encapsulation of Ni particles [54].

2.5. Cobalt Catalysts for Glycerol Reforming

Cobalt (Co) played an extensive role in the synthesis of hydrogen as many researchers represented this glycerol steam reforming. Ghungrud and Vaidya studied the synthesis of hydrogen by sorption–enhanced steam reforming technique (SESGR) on a Co-promoted hydrotalcites catalyst. 92.8% maximum glycerol conversion and 89.7% hydrogen yield were achieved over Co-Ca-HTlc catalyst represented as HM2 at T = 823 K, GHSV = 5600 mL g \(^{-1}\) h \(^{-1}\). Ca, Co, and Zn promoted hydrotalcite catalysts were manufactured through the precipitation method. HM2 contained Cu showed the best performance for the dehydrogenation process, and it was known that basic sites promoted the dehydrogenation process. At 550 °C, Cu-bearing materials showed a long pre-breakthrough duration (40 min) and high H\(_2\) purity (93.1 mol%). They were also better adsorbents, removing 1.1 mol CO\(_2\)/kg sorbent at 550 °C. Over 20 cycles of adsorption and regeneration, the cyclic stability of materials was examined. The potential of customized HTlc-materials for better H\(_2\) production from the SESGR process is explored in this work [59].

A feasible reaction pathway for the SESGR process was provided based on the product composition (Figure 3). Glycerol undergoes dehydorination reactions upon adsorption, resulting in acetaldehyde. The adsorbed acetaldehyde was then further hydration-dehydrogenated into acetic acid. Over Co metal, acetic acid undergoes C-C bond breakage, yielding H\(_2\), CO\(_2\), CO, and CH\(_4\). The basic catalyst promotes rapid dehydrogenation, which prevents the generation of olefins and carbon deposition. CO and CH\(_4\) are converted to H\(_2\) and CO\(_2\) by WGS reaction and steam reforming processes, with trace amounts of CO remaining [59].

![Figure 3. Plausible reaction mechanism for SESGR.](image)

Zhou et al. investigated NiCo modified CNTs bimetallic catalysts with an appropriate distribution of Ni, as well as Co, metal for synthesizing hydrogen through the impregnation technique in which metal precursors were injected into the cave of CNTs by ultra-radiations. At 450 °C and 1 atm, 100% glycerol transformation was achieved with 91.4% H\(_2\) selectivity over Ni(i)Co(i)/CNTs catalyst. Ni(i)Co(i)/CNTs exhibited the best stability and catalyst performance. Although the Ni and Co oxides were only partially reduced, the location of metal species had a significant impact on reducibility. The synergetic effect between Ni and Co species was found in Ni(i)Co(i)/CNTs and Ni(o)Co(o)/CNTs, where they had the same distribution on the internal or external wall. Sintering of active sites was markedly simpler on the external wall of CNTs, causing the catalyst to deactivate quickly and become less reactive for the water gas shift process. The result of this study revealed that there is a new and straightforward method for assembling bimetallic catalyst systems. The Ni-based bimetallic catalysts might be used to reform mono/multi-alcohols such as ethanol, ethylene
glycol, sorbitol, and other organic wastes from second-generation biorefineries, as well as biogas and other organic wastes [37].

Al-Salihi et al. investigated Co-Ni-MgO-based SBA-15 nano-catalysts for the glycerol steam reforming for hydrogen manufacturing. The one pot hydrothermal method was used to create different mesoporous catalysts, such as Co-SBA-15, Ni-SBA-15, Co-MgO-SBA-15, Ni-MgO-SBA-15, and Co-Ni-SBA-15 and bimetallic 10 wt.% Co-5 wt.% Ni modified SBA-15 catalyst synthesized by the impregnation method. A glycerol conversion rate of 100% along with 82.8% hydrogen selectivity was achieved over 10 wt.% Co-5 wt.% Ni modified SBA-15 catalyst at 650 °C. At a low temperature (450 °C), the one-pot catalysts showed 50% glycerol conversion compared to 70% for the impregnated catalyst, while both yielded 62% H₂ selectivity. Cobalt-based SBA-15 catalysts have superior GSR activity and stability than nickel-based catalysts in monometallic catalysts. The addition of MgO to Co-SBA-15 improved glycerol conversion (up to 99%) and catalyst stability. The addition of MgO to Ni-SBA-15 reduced the quantity of carbon deposition on the catalysts by as much as 66%, according to TGA-TPO analyses of spent catalysts. It’s worth noting that under our experimental conditions, all of the catalysts examined at the optimum temperature of 650 °C demonstrated a remarkable hydrogen selectivity of 70% [36].

Duo et al. developed chemical looping steam reforming process for glycerol conversion to hydrogen over Al-MCM-41 and SBA-15 well-order mesoporous OCs containing NiO and CeO₂ nanoparticles [33]. It was discovered that the NiO and CeO₂ in the OCs were reduced by glycerol, and the reduced OCs were in charge of producing hydrogen. It was shown remarkable stability in 60 redox cycles (180 h), and the carbon conversion and hydrogen selectivity were both over 60% and 85%, respectively. Oxygen transport was enhanced by heavily loading mesoporous MCM-41 and SBA-15 with NiO and CeO₂, which also produced outstanding redox CLSR cycles and long-term stability [33].

The summary of some more reported literature related to glycerol reforming over various catalysts to produce hydrogen is represented in Table 2. Noble metal catalysts, such as Pd, Ru, Ir, Rh, and Pt, are known for their high catalytic activity, which results in good performance and coke resistance. Other catalysts, such as Ni, Co, and Cu, on the other hand, are less expensive and more readily available and have a desirable catalytic activity for boosting hydrogen production. Their stability, on the other hand, is undesirable since the coking process frequently deactivates them. As a result, developing a highly active and stable catalyst requires the employment of metals as catalysts in combination with the proper selection of support (based on porosity, redox characteristics, and thermal stability, among other factors). Alumina and silica are the most common catalytic supports in research, but some catalysts can also be supported on active carbon, nanotubes, mesoporous carbon, nanoparticles, and other materials. Due to its high specific surface and thermal stability, alumina is the preferred and most used support for this purpose. However, carbon deposition tends to render it inactive. The optimal bimetallic catalyst must possess excellent thermal strength, mechanical resistance, and redox characteristics to produce H₂ with high selectivity.

Table 2. Hydrogen production from glycerol reforming using various catalytic systems under optimal reaction conditions.

| S. No. | Catalyst | Reaction Condition/Reactor | X (%) | S (%) | Y (%) | References |
|--------|----------|-----------------------------|-------|-------|-------|------------|
| 1      | Co-Ni-MgO-based SBA-15 (one-pot hydrothermal and impregnation method) | T = 650 °C P = 1 atm (Fixed bed reactor) | 100   | 82.8  | 82.8  | [36]       |
| 2      | Pt and/or Ni supported over γ-alumina (Sol-gel method) | T = 250 °C P = 30 bar WHSV = 2.6 h⁻¹ | 100   | -     | -     | [37]       |
Table 2. Cont.

| S. No. | Catalyst | Reaction Condition/Reactor | X (%) | S (%) | Y (%) | References |
|--------|----------|-----------------------------|-------|-------|-------|------------|
| 3      | Pt and Ni supported SiO₂ (Ion exchange method) | T = 350 °C  
Feed flowrate = 0.5 cm³ h⁻¹  
(Fixed bed reactor) | 100   | 70    | 70    | [38]       |
| 4      | Ru doped Al₂O₃ | T = 500 °C,  
P = 0.1 MPa  
Cat. Wt. = 0.1 g  
W/FA0 = 1.98 | 89.1  | -     | -     | [41]       |
| 5      | CeZr-CoRh | T = 650 °C,  
P = 0.1 MPa  
Cat. Wt. = 55 mg  
WHSV = 8.4 g₉₅₉₅cat⁻¹ | 100   | 86    | 86    | [44]       |
| 6      | Rh modified MeAl₂O₄ at Al | T = 723 K  
WHSV = 34,000 mL g⁻¹ h⁻¹ | 100   | -     | -     | [45]       |
| 7      | Rh/Al₂O₃ (Impregnation technique) | T = 823 K  
WHSV = 4.8 × 10³ N mL/gcat⁻¹ min | 100   | -     | -     | [46]       |
| 8      | Ni/CaCO₃ | T = 550 °C  
P = 1 atm | 100   | 92    | 92    | [47]       |
| 9      | Rh/γ—Al₂O₃@CeO₂, MgO, La₂O₃ (Co-precipitation method) | T = 600 °C  
P = 1 atm  
GHSV = 5000 N mL g⁻¹ h⁻¹  
(Fixed bed reactor) | 90    | 78    | 78    | [49]       |
| 10     | Ni supported over Y₂O₃–ZrO₂ (Impregnation technique) | T = 700 °C | 90    | 91    | 82    | [54]       |
| 11     | Ni modified Al₂O₄ (Coprecipitation method) | T = 630 °C  
P = 1 atm press., WHSV = 19,600 cm³/gcat/h | 95.42 | 80    | 76.4  | [56]       |
| 12     | Ni added to CaO—modified attapulgite (Impregnation method) | T = 600 °C  
Cat. Wt. = 0.5 g  
GHSV = 1 h⁻¹ | 93.7  | 91    | 85.3  | [57]       |
| 13     | Co promoted hydrotalcite (Precipitation method) | T = 550 °C  
GHSV = 5600 mL g⁻¹ h⁻¹ | 92.8  | 96.7  | 89.7  | [59]       |
| 14     | NiCo modified CNFs bimetallic catalysts (Impregnation method) | T = 450 °C  
P = 1 atm  
(Fixed bed reactor) | 100   | 91.4  | 91.4  | [60]       |
| 15     | Pt/Al₂O₃ | T = 200–240 °C  
P = 16–33.5 bar  
(Batch reactor) | 84    | 16.8  | 14.1  | [61]       |
| 16     | Pt/Al₂O₃ | T = 240 °C  
P = 42 bar  
(Batch reactor) | 34    | 36.8  | 12.5  | [62]       |
| 17     | Pt/SiO₂ (Sol—gel method) | T = 300–400 °C  
P = 1 atm  
(Microchannel reactor) | 96.8  | 90    | 89.7  | [63]       |
| S. No. | Catalyst | Reaction Condition/Reactor | X (%) | S (%) | Y (%) | References |
|--------|----------|----------------------------|-------|-------|-------|------------|
| 18     | Pt/γ—Al₂O₃, SiO₂ & silica—alumina (Impregnation method) | T = 225 °C P = 29 bar WHSV = 4.2 h⁻¹ (Fixed bed reactor) | 11.9  | 73    | 8.9   | [64]       |
| 19     | Pt/ZrO₂ (Impregnation method) | T = 350 °C P = 29 bar (Fixed bed reactor) | 100   | 69    | 6.9   | [65]       |
| 20     | Pt/Al₂O₃, Puralox, Catapal B (Impregnation method) | T = 250 °C Cat. Wt. = 300 mg Feed flowrate = 0.5 mL/min (Fixed bed reactor) | 57    | -     | 85    | [66]       |
| 21     | Pt—Re/C (Impregnation method) | T = 225 °C P = 420 psi WHSV = 5 hr⁻¹ (Fixed bed reactor) | 89.4  | 26.1  | 23    | [67]       |
| 22     | 10 Ni/Al₂O₃/5 CeO₂ (Impregnation method) | T = 550–800 °C P = 1 atm WHSV = 10 hr⁻¹ (Fixed bed reactor) | 100   | 88.6  | 86    | [68]       |
| 23     | Ru-Mg-Al hydrotalcite- mixed oxides (Impregnation method) | T = 400–700 °C P = 1 atm GHSV = 69,000 h⁻¹ (Fixed bed reactor) | 45    | 90    | 40.5  | [69]       |
| 24     | Ru/Al₂O₃ (Wet co-impregnation method) | T = 400–600 °C P = 1 atm Cat. Wt. = 200 g W/F = 1.05 mg min mL⁻¹ (Fixed bed reactor) | 100   | 80    | 80    | [70]       |
| 25     | Ru/C (Impregnation method) | T = 773 K P = 1 atm (Fixed bed reactor) | 94.6  | 99.8  | 94.5  | [71]       |
| 26     | Mg(Al)₂O₃/Ru (Impregnation method) | T = 450–650 °C P = 1 atm (Fixed bed reactor) | 97    | 96    | 90    | [72]       |
| 27     | C/Pt and Pt/Ru (Impregnation method) | T = 225 °C P = 1 bar (Fixed bed reactor) | 24    | -     | -     | [73]       |
| 28     | Rh/ZrO₂, Rh/CeO₂ (Impregnation method) | T = 650–750 °C Cat. Wt. = 20 mg (Fixed bed reactor) | 79    | 30.6  | 24.2  | [74]       |
| 29     | Rh/Al₂O₃ (Impregnation method) | T = 250 °C P = 50 bar Cat. Wt. = 250 mg WHSV = 2.45 h⁻¹ (Fixed bed reactor) | 82    | 85.2  | 69.9  | [75]       |
| 30     | Pt and Pt-Rh/α-Al₂O₃ (Impregnation method) | T = 503 K Cat. Wt. = 300 mg (Batch reactor) | 67    | 1.67  | 1.12  | [76]       |
### Table 2. Cont.

| S. No. | Catalyst | Reaction Condition/Reactor | X (%) | S (%) | Y (%) | References |
|--------|----------|-----------------------------|-------|-------|-------|------------|
| 31     | Rh and Ni/γ—Al₂O₃ (Impregnation method) | T = 723 to 1073 K  
                     P = 1 atm  
                     GHSV = 5000 to 30,000 mL_gly h⁻¹ mL_cat⁻¹ | 69    | 50    | 34.5  | [77]       |
| 32     | Ni-La-Ti oxide (Coprecipitation method) | T = 500–650 °C  
                     P = 1 bar  
                     Cat. Wt. = 0.1 gm  
                     WHSV = 3 h⁻¹  
                     (Fixed bed reactor) | 99.7  | 90.3  | 90    | [78]       |
| 33     | NiAl₂O₄ (Impregnation method) | T = 600 °C  
                     Feed flow rate = 2.5 mL/h  
                     (Fixed bed reactor) | 99    | 98.9  | 98    | [79]       |
| 34     | La-promoted Ni/Al₂O₃ | T = 923–850 °C  
                     P = 1 atm  
                     WHSV = 3.6 × 10⁴ mL⁻¹ h⁻¹  
                     (Fixed bed reactor) | 96    | 98.9  | 95    | [80]       |
| 35     | LaₓCaₓNiO₃ perovskite-oxides (Impregnation method) | T = 550 °C  
                     P = 1 atm  
                     Cat. Wt. = 200 mg  
                     WHSV = 2.5 hr⁻¹  
                     (Fixed bed reactor) | 100   | 80    | 80    | [81]       |
| 36     | Ni and Ni—Co/alumina (Impregnation method) | T = 300–700 °C  
                     P = 1 atm  
                     WHSV = 10 hr⁻¹  
                     (Fixed bed reactor) | -     | -     | 83    | [82]       |
| 37     | Ni/α—Al₂O₃ and α—Al₂O₃ modified by ZrO₂ and CeO₂ (Impregnation method) | T = 600 °C  
                     P = 1 atm  
                     Feed flow rate = 0.022 cm³ min⁻¹  
                     (Fixed bed reactor) | 90    | 95.6  | 86    | [83]       |
| 38     | LaNiO₃ and LaCoO₃ | T = 700 °C  
                     P = 1 atm  
                     (Fixed bed reactor) | 100   | 98    | 98    | [84]       |
| 39     | 0.25 CoAl, 0.625 CoAl Co₅O₄ | T = 260 °C  
                     P = 5 MPa  
                     WHSV = 24.5 h⁻¹  
                     (Fixed bed reactor) | 98    | 29    | 10    | [85]       |
| 40     | Co-Ce/Hap (Impregnation method) | T = 750 °C  
                     P = 1 atm  
                     (Fixed bed reactor) | 99    | 79    | 7.2   | [86]       |
| 41     | Co/SBA-15 with Zr, Ce and La (Impregnation method) | T = 500–600 °C  
                     P = 1 atm  
                     WHSV = 7.7 h⁻¹  
                     (Fixed bed reactor) | 100   | 72    | 72    | [87]       |
| 42     | Laₓ-Ceₓ-CoO₃ (Co—precipitation method) | T = 700 °C  
                     P = 1 atm  
                     (Fixed bed reactor) | 100   | 68    | 68    | [88]       |
| 43     | Co/Al₂O₃ (Impregnation method) | T = 723–923 K  
                     P = 1 atm  
                     GHSV = 5 × 104 mL_gly h⁻¹ mL_cat⁻¹  
                     (Fixed bed reactor) | 65    | 80    | 52    | [89]       |
Table 2. Cont.

| S. No. | Catalyst | Reaction Condition/Reactor | X (%) | S (%) | Y (%) | References |
|--------|----------|-----------------------------|-------|-------|-------|------------|
| 44     | Ceria/Ir, Co and Ni (deposition—precipitation method) | T = 250–600 °C, P = 1 atm, GHSV = 11,000 mL g\text{cat}^{-1} h^{-1} (Fixed bed reactor) | 100   | 85    | 85    | [90]       |

X = Conversion, S = Selectivity, Y = Yield.

3. Glycerol Dehydration

Acrolein was obtained by anhydrous glycerol decomposition in the existence of solid catalysts such as alkali–metal acid sulfates and phosphorus pentoxide in the 19th century [91,92]. Hence, the suggested route is illustrated in Figure 4. Acrolein is transformed directly into targeted high-value-added derivative products because of its toxic effects. Acrolein is an intermediate in producing acrylic acid and acrylic polymers in the industry. The consumption of acrolein is also for the production of DL-methionine, and 3-methylthio-propionaldehyde is produced as an intermediate here [93]. Early studies concentrated on homogeneous catalysts in the aqueous phase under near- or supercritical conditions. However, the vapor phase over heterogeneous catalysts are chosen due to the predicted high cost of the reaction vessel and separation concerns [10]. However, until the end of the twentieth century, when cheaper glycerol from the biodiesel synthesis process became accessible, these early works in both the gaseous and liquid phases remained unexplored [93].

Figure 4. Reaction route for glycerol dehydration to produce acrolein and acetol.

The high selectivity was achieved due to the control of 1st dehydration reaction. Tsukuda et al. proposed this mechanism, where 3-hydroxypropionaldehyde formation was favorable over the acetol formation, which is considered a byproduct of the primary reaction step; further, this mechanism (Figure 5) suggested two hydrogenation steps: first from acrolein and second from acetol to achieve allylic alcohol and 1,2-PDO, simultaneously [94,95]. So many solid acid catalysts have been used for dehydration of glycerol for acrolein production through zirconia, heteropoly acid, niobia, and alumina catalysts [96–98].
The high selectivity was achieved due to the control of the first dehydration reaction. Lin et al. investigated \( \beta \) zeolites (HNa–\( \beta – \kappa \)) for the production of acrolein through glycerol dehydration. In total, 65% glycerol transformed to produce 23.3% acrolein yield at HNa–\( \beta – 0 \) catalysts at 200 °C. It was speculated that smaller pores increased selectivity but reduced activity for acrolein production. An increase in temperature favored the selectivity of acrolein. After being employed in the reaction test (see infra) and recalcination at 450 °C in the air for 4 h, the XRD patterns of these zeolitic catalysts were substantially identical. These results showed that the ion-exchange technique, subsequent calcination, and reaction tests did not result in any visible changes in the zeolitic crystal structure. As the Na/Al ratio increased, the apparent surface area of the HNa-\( \beta – \kappa \) zeolites decreased. At the same time, the pore width reduced as the Na\(^+\)/Al ratio increased, which could explain why Na\(^+\) is larger than H\(^+\) when residing in the zeolitic channel. According to the pore diameter data, these pore widths correspond to the 12-membered ring in the b-zeolites and the 10-membered ring in the H-MFI zeolite. Na\(^+\)/H\(^+\) ratio increment also enhanced acrolein selectivity and decreased glycerol conversion. The highest acrolein yield was achieved due to the replacement of acidic sites with non-active Na\(^+\) sites [99].

Ren et al. investigated MnHPO\(_4\) and meso-zeolite (H-ZSM-5) catalyst prepared by the ion-exchange technique and concluded that the less strong acid amount was more beneficial for the production of acrolein and also coke suppressed in glycerol dehydration. A 100% transformation of glycerol was achieved for all reactions and 84.7% highest acrolein yield over meso-zeolite (HZSM-5) supported on MnHPO\(_4\) catalysts [100]. Meso and microporous zeolite by one-step synthesis technology for acrolein formation from glycerol dehydration. HZSM-25 catalyst achieved 99% glycerol transformation and 80% acrolein selectivity at 450 °C, 1 atm, and 38.47 h\(^{-1}\) WHSV. The high acidity and fast diffusion of species in synthesized ZSM-5 supported acrolein production from dehydration of glycerol. Diffraction peaks of five types of transition metal hydrogen phosphates supported on meso-HZSM-5 were also shown to exhibit this behavior [101]. Qureshi et al. investigated nano H-ZSM-5 highly crystalline catalyst for glycerol dehydration through hydrothermal technique. A 98% glycerol transformation occurred to produce 87% acrolein selectivity at HZSM-5 (Si/Al = 75) at 320 °C, 1 atm, and 4 h\(^{-1}\) WHSV. According to these findings, the catalysts with a Si/Al ratio of 75–100 had a higher crystallinity than the other samples. The SEM pictures revealed the catalyst’s surface morphology, particle size, and crystal aggregation. The exterior surface of all H-ZSM-5 catalysts produced was uniform and had a highly oriented shape. The catalysts exhibit consecutive crystal lattices and a smooth surface, according to TEM pictures of H-ZSM-5 with a Si/Al ratio of 75 [102].

Yun et al. investigated marigold-like silicon dioxide (silica) functionalized through groups of sulfonic acid (MF–FS) and zeolite (HZSM-5) catalysts for the production of acrolein from glycerol dehydration. The maximum acrolein yield was 73%, with 100%
glycerol transformation achieved over MF-CS catalyst at 250 °C. Bronsted acid sites in MF-FS catalyst promoted stability as well as selectivity for acrolein production [103]. Chai et al. studied acrolein production through dehydration on various solid acid-base catalysts synthesized by the impregnation method. A 100% glycerol transformation was achieved with 65% acrolein selectivity over 15 wt.% WO₃/ZrO₂ catalyst at 315 °C, 1 atm, and 80 h⁻¹ GHSV. For acrolein production, Bronsted acidic sites were superior to Lewis acidic sites [94]. Xie et al. investigated microwave absorbing catalysts for acrolein production from glycerol dehydration. Most notably, the catalyst stability by microwave heating technique was much better than the heating process by electric. WO₃/ZrO₂ at SiC coated microwave absorbing catalyst was synthesized. The complete glycerol transformation (100%) was achieved with 70% acrolein selectivity by 250 °C microwave heating [104].

Shan et al. investigated fabricated nanosheet MFI zeolite catalyst for glycerol dehydration for acrolein production [105]. A 99.7% transformation of glycerol was achieved with 81.8% acrolein at 320 °C and 1 atm. Compared to conventional ZSM-5 zeolite (CMZ-X), MFI zeolites nanosheets were more active as well as stable for glycerol dehydration reaction in the gas phase. The nanosheet MFI zeolites (NMZ-X) decreased the rate of coke deposition which resulted higher stability as well as activity. The zeolites in CMZ-X produced with tetrapropylammonium hydroxide as the structural guiding agent were shown as uniform 400 nm particles with cylindrical intergrowth. The NMZ-X Si/Al molar ratio has a significant impact on the morphologies of nanosheet MFI zeolites. NMZ-100 appears to be a three-dimensional multi-lamellar stacking of MFI nanosheets with intergrowth. The NMZ-100 particles had a diameter of roughly 1.5 µm and were made up of 30–40 nm thick lamellar stacking. Meanwhile, NMZ-50 demonstrated similar MFI nanosheet lamellar stacking, but the particle size (500 nm) and lamellar stacking thickness (approximately 10 nm) were substantially less. NMZ-30, on the other hand, looks like cotton balls and could not tell the MFI nanosheets from the SEM image. NMZ-30 was well-crystallized and exhibited nanosheet MFI zeolite properties, as indicated by the XRD patterns. It was discovered that Al content had a crucial impact on the development of NMZ-X by comparing TEM pictures of nanosheet MFI zeolites with varied Si/Al molar ratios. Due to the abundance of unstable Si–O–Al units, it was difficult to generate large area MFI nanosheets with a low Si/Al molar ratio [105].

3.2. Titania Catalysts for Glycerol Dehydration

Titanium oxide (Titania) has three crystalline phases: brookite, anatase, and rutile. Amid all, the anatase phase has vital applications [106–109]. Babaei et al. investigated TiO₂ catalysts for acrolein production for glycerol dehydration. It was mentioned that the central hydroxyl group adsorption on the surface had the best geometry and energy (30.91 kcal/mol) for dehydration reaction to acrolein. The glycerol dehydration to acrolein is followed by removing water molecules. The TiO₂ surface exhibited more activity in proton transfer reaction with 89.1 kcal/mol E (activation energy) comparing the above two routes for acrolein formation [109]. Ulgen et al. synthesized WO₃/TiO₂ catalyst through the impregnation method for acrolein formation from glycerol dehydration. Maximum acrolein selectivity of 80% and the complete conversion of glycerol was achieved over WO₃/TiO₂ catalyst at 280 °C. In most cases, a larger BET surface area was associated with better glycerol conversion. Titania-supported tungsten oxide systems were ideal catalysts for the dehydration reaction of glycerol due to their longer service time, decreased deactivation speed, and much lower pricing [110].

3.3. Silica Catalysts for Glycerol Dehydration

Wang et al. focused on low-temperature (210–230 °C) glycerol dehydration to acrolein through temperature-programmed surface reaction (TPSR). A series of acid catalysts (lewis acid catalysts, supported heteropolyacids and superacids, molecular sieves, and metal oxides) synthesized by the impregnation method has been screened for glycerol dehydration at low temperature (210 °C) through TPSR. SiW/SiO₂, as well as SO₄²⁻/TiO₂
achieved high acrolein selectivity (85% and 86%) simultaneously. The maximum glycerol transformation was achieved at 94.4% at 230 °C [111]. Rosas et al. investigated some most active catalysts, namely, NH₄ and La modified β zeolites, Pd and La modified Y zeolites, hierarchical zeolite (ZSM-5), WO₃ modified ZrO₂, WO₃ modified TiO₂, ZrOₓ modified NbOₓ, WO₃-SiO₂ modified ZrO₂, NbOₓ-WOₓ modified Al₂O₃, H₃PO₄ modified MCM-41, SAPO-40, and NbPSi for glycerol dehydration reaction in the gas phase. A 100% conversion was obtained at 300–325 °C. In this, the gas-phase catalytic process was more suitable than the liquid-phase due to high acrolein yields (>70%) [112]. Silica and phosphate supported copper catalyst for glycerol dehydration to produce acetol. Silica and phosphate supported copper catalyst produced through sodium silicate neutralization with the orthophosphoric acid and added copper nitrate. After this, 58.3% acetol selectivity and 100% glycerol transformation were achieved on CuSP catalyst at 220 °C, and atmospheric pressure. Lewis acidic sites were responsible for the increase in selectivity of acetol [113]. Basu et al. investigated silica-supported copper chromite catalyst synthesized through a sol-gel technique for dehydration of glycerol for acetol production. The transformation of glycerol reached 100% with 70% maximum selectivity of acetol for 40 wt.% Copper chromite loading on silica at 220 °C and atmospheric pressure. The spent and oxidized catalyst presented lower selectivity and conversion compared with reduced form catalyst due to cupric ion in reduced form catalyst, which worked as Lewis acid sites in dehydration [114].

3.4. Alumina Catalysts for Glycerol Dehydration

Mesoporous alumina was prepared with different precipitants through a continuous precipitation method for gas-phase glycerol dehydration for acrolein production by Lima et al. A 99% glycerol transformation occurred at alumina catalyst prepared at 7 pH with NaOH precipitant at 500 °C. Results revealed high carbon formation and higher olefins production, which showed the production of carbon is related to these by-production formations. The sample synthesized with KOH had the largest specific surface area (432 m² g⁻¹) among the influences of the precipitating agent, whereas the sample created with Na₂CO₃ had the lowest specific surface area (432 m² g⁻¹) (48 m² g⁻¹). The specific surface area of the produced material was similarly affected by the pH of the precipitation. Due to the type of precipitate generated, samples prepared at pH 5 (389 m² g⁻¹ of Na₂CO₃ precipitant and 359 m² g⁻¹ of NaOH) have a greater specific surface area than those prepared at pH 7. When precipitation was carried out at pH 7, the resulting residue was weakly crystalline, creating pseudo-boehmite. At pH 5, an amorphous precipitate was formed, yielding a microcrystalline boehmite with a higher specific area [115].

Kim et al. investigated silica and alumina catalyst for glycerol dehydration reaction in gas-phase for production of acrolein. The conversion of glycerol was 50% along with 16% acrolein selectivity achieved over Si₉₆₃₇Al₆₄Oₓ catalyst at 315 °C and 62 h⁻¹ WHSV. It was concluded that the yield of acrolein depended on the brensted acid sites. As Si mole fraction was increased up to 0.8, the intensity of the Al₂O₃ XRD peak increased and subsequently declined as Si mole fraction was increased. Due to the tetrahedral interaction between Al and SiO, the degree of crystallinity is determined by the Al concentration contained in SiO₂. The specific surface areas of the silica–alumina increased dramatically when Al (or Si) species were added, compared to SiO₂ and -Al₂O₃. The catalyst pore volume followed a volcano-like pattern in relation to the mole fraction of Al, while the average pore diameter shrank as the mole fraction of Al increased. The catalysts’ pore size distributions revealed a noticeable variation in pore diameter with regard to the Al content. For silica–aluminas with Al mole% of less than 0.2, a relatively broad pore size distribution was discovered [116].

A summary of some more reported literature on glycerol dehydration over various catalysts to produce acrolein is represented in Table 3 [92,99–136].
Table 3. Acrolein production from glycerol dehydration using various catalytic systems under optimal reaction conditions.

| S. No. | Catalyst | Reaction Conditions/Reactor | X (%) | S (%) | Y (%) | References |
|--------|----------|-----------------------------|-------|-------|-------|------------|
| 1      | HPA, H-SiW, H-PW and H-PMo/γ-Al₂O₃ (Impregnation method) | T = 275 °C  
        P = 1 atm  
        Feed flowrate = 1.68 mL/h (Fixed bed reactor) | 99 | 42.1 | 41.7 | [92] |
| 2      | β zeolites (HNa–β–κ) | T = 200 °C  
        Cat. Wt. = 1 g  
        Feed flowrate = 12 mL/h (Fixed bed reactor) | 65 | 35.8 | 23.3 | [99] |
| 3      | MnHPO₄ and meso-Zeolite (Ion exchange method) | T = 300 °C  
        Cat. Wt. = 0.5 g  
        Feed flowrate = 0.023 mL/h (Fixed bed reactor) | 100 | 84.7 | 84.7 | [100] |
| 4      | Zeolite (one-step synthesis) | T = 723 K  
        P = 1 atm  
        Cat. Wt. = 80 mg  
        Feed flowrate = 0.05 mL/h | 99 | 80.8 | 80 | [101] |
| 5      | HZSM-5 (Hydrothermal Technique) | T = 320 °C  
        P = 1 atm  
        WHSV = 4 h⁻¹ (Fixed bed reactor) | 98 | 88.8 | 87 | [102] |
| 6      | WO₃/TiO₂ (Impregnation method) | T = 280 °C  
        P = 1 atm | 100 | 80 | 80 | [110] |
| 7      | Pd/LaY Zeolite | T = 573 K  
        P = 1 atm  
        GHSV = 5993 h⁻¹ (Fixed bed reactor) | 93 | 94.2 | 87.6 | [112] |
| 8      | Silica supported copper chromite (Sol gel method) | T = 220 °C | 100 | 70 | 70 | [114] |
| 9      | Zeolite (Fluidised bed reactor) | T = 290–650 °C  
        WHSV = 282–388 hr⁻¹ | 100 | 62.1 | 62.1 | [117] |
| 10     | Sulfated zeolite (Precipitation method) | T = 290–390 °C  
        P = 1 atm  
        GHSV = 18,000–360 hr⁻¹ (Continuous flow reactor) | 49 | 42 | 20.58 | [118] |
| 11     | Na-ZSM-5 and H-ZSM-5 | T = 315 °C  
        P = 1 atm  
        Feed flow rate = 23.4 mol/h (Fixed bed reactor) | 75.8 | 63.8 | 48.36 | [119] |
| 12     | ZSM-23, HY, Mor, H and SBA-15, CVD, Hβ (Impregnation method) | T = 250 °C  
        P = 70 bar (Autoclave with stirrer) | 95 | 18.5 | 17.58 | [120] |
| 13     | WO₃/TiO₂ (Sol–gel and solvothermal method) | T = 200–400 °C  
        P = 1 atm  
        WHSV = 22.9 Eθkit. g/cat/h (Fixed bed reactor) | 88 | 87.5 | 77 | [121] |
Table 3. Cont.

| S. No. | Catalyst                          | Reaction Conditions/Reactor                  | X (%) | S (%) | Y (%) | References |
|--------|----------------------------------|---------------------------------------------|-------|-------|-------|------------|
| 14     | WO₃/TiO₂                         | T = 280 °C                                  | 95    | 73    | 69.4  | [122]      |
|        |                                  | P = 1 atm                                   |       |       |       |            |
|        |                                  | (Fixed bed reactor)                         |       |       |       |            |
| 15     | WOₓ/TiO₂                          | T = 400 °C                                  | 100   | 80    | 80    | [123]      |
|        | Sand NbOₓ/TiO₂                    | P = 25 and 33 MPa                           |       |       |       |            |
|        |                                  | (Fixed bed reactor)                         |       |       |       |            |
| 16     | HPW/TiO₂ (Impregnation method)   | T = 280 °C                                  | 100   | 74    | 74    | [124]      |
|        |                                  | P = 1 atm                                   |       |       |       |            |
|        |                                  | GHHSV = 4400 h⁻¹                            |       |       |       |            |
|        |                                  | (Fixed bed reactor)                         |       |       |       |            |
| 17     | Al₂O₃-, SiO₂-, and TiO₂-/Nb- and W-oxide (Impregnation method) | T = 305 °C                                  | 100   | 66.2  | 66.2  | [125]      |
|        |                                  | P = 1 atm                                   |       |       |       |            |
|        |                                  | (Fixed bed reactor)                         |       |       |       |            |
| 18     | H₃P₂W₁₈O₆₂/MCM-41-SUP (Supercritical Impregnation method) | T = 320 °C                                  | 94    | 72    | 67.7  | [126]      |
|        |                                  | P = 1 atm                                   |       |       |       |            |
|        |                                  | Cat. Wt. = 0.5 g                            |       |       |       |            |
|        |                                  | WHSV = 0.6 h⁻¹                              |       |       |       |            |
|        |                                  | (Fixed bed reactor)                         |       |       |       |            |
| 19     | Al doped SBA-15 (post synthesis method) | T = 325 °C                                  | 100   | 31    | 31    | [127]      |
|        |                                  | P = 1 atm                                   |       |       |       |            |
|        |                                  | Feed flowrate = 0.1 mL/hr                   |       |       |       |            |
|        |                                  | (Fixed bed reactor)                         |       |       |       |            |
| 20     | WO₃/Zr Doped Mesoporous SBA-15   | T = 325 °C                                  | 97    | 42.3  | 41    | [128]      |
|        |                                  | P = 1 atm                                   |       |       |       |            |
|        |                                  | (Fixed bed reactor)                         |       |       |       |            |
| 21     | Silica-Supported Phosphotungstic Acid (sol–gel method) | T = 280 °C                                  | 99    | 30    | 27    | [129]      |
|        |                                  | P = 1 atm                                   |       |       |       |            |
|        |                                  | (Fixed bed reactor)                         |       |       |       |            |
| 22     | Tungsten oxides dispersed on Al₂O₃, ZrO₂, and SiO₂ | T = 315 °C                                  | 98    | 70    | 68.6  | [130]      |
|        |                                  | P = 10 kPa                                  |       |       |       |            |
|        |                                  | GHHSV = 400 h⁻¹                             |       |       |       |            |
|        |                                  | (Fixed bed reactor)                         |       |       |       |            |
| 23     | Bulk, nanorod and MOF-derived γ-Al₂O₃ | T = 240–340 °C                              | 80    | 74    | 59.2  | [131]      |
|        |                                  | WHSV = 2.4 h⁻¹                              |       |       |       |            |
|        |                                  | (Fixed bed reactor)                         |       |       |       |            |
| 24     | Pt/γ-Al₂O₃ (Impregnation method) | T = 375 °C                                  | 90    | 65    | 58.5  | [132]      |
|        |                                  | P = 1 atm                                   |       |       |       |            |
|        |                                  | feed flowrate = 12 mL/h                     |       |       |       |            |
|        |                                  | (Continuous flow reactor)                   |       |       |       |            |
| 25     | ZrO₂ & Ceria/Alumina             | T = 300 °C                                  | 100   | 85    | 85    | [133]      |
|        |                                  | GHHSV = 12,000 h⁻¹                          |       |       |       |            |

4. Glycerol Hydrogenolysis

The catalytic hydrogenolysis reaction is completed in two steps: hydrogenation and dehydration. Such a type of reaction system depends mainly on one catalyst particle size along with its structure [134,135]. Fan et al. concluded that the glycerol conversion would be more promising when using an enzymatic approach for glycerol to 1,3-PDO [136]. Sun et al. studied glycerol hydrogenolysis to produce C₃ products such as 1,2-PDO and
1,3-PDO [137]. The reaction route for glycerol hydrogenation producing ethylene glycol, methanol, ethanol, and methane [61]:

\[
C_3H_8O_2 + H_2O \leftrightarrow C_2H_6O_2 + CH_3OH \tag{5}
\]

\[
C_2H_6O_2 + H_2 \leftrightarrow CH_3CH_2OH + H_2O \tag{6}
\]

\[
CH_3OH + H_2 \leftrightarrow CH_4 + H_2O \tag{7}
\]

The reaction route for glycerol hydrogenation into propylene glycols (1,2-propanediol (1,2-PDO), and 1,3-propanediol (1,3-PDO)) were shown as (Figure 6) [138]. So many heterogeneous catalysts were utilized for hydrogenolysis reaction in which noble metals (Au, Rh, Pd, Pt, and Ru) based catalysts were utilized or non–noble metals (Ni, Co, and Cu) based catalysts were used [139–153].

Figure 6. Production of 1,2-PDO and 1,3-PDO through dehydration and hydrogenation of glycerol.

4.1. Nickel Catalysts for Glycerol Hydrogenolysis

Bulk Ni phosphide catalyst prepared through hydrothermal method for glycerol hydrogenolysis for production of 1,2-PDO. 95% 1,2-PDO selectivity along with 5.4% glycerol conversion was achieved over Ni₃P catalyst at 190 °C and 5.5 MPa. It was concluded that low conversion was achieved over the catalysts which were treated at low temperature (190 °C). Hexagonal morphology was shown by bulk nickel phosphide catalyst. After annealing, the sample synthesized at a pH of 9 predominantly showed metallic nickel diffraction peaks, but the sample produced at a higher pH value (pH 12) was found to be pure amorphous metallic nickel as determined by XRD. When the pH was reduced to 7, the comparatively strong diffraction peaks of Ni₃P were seen. All diffraction peaks of the annealed sample may be assigned to the Ni₃P phase when the pH value is 5. The influence of annealing temperature is also demonstrated. More substantial diffraction peaks and larger particle sizes resulted in a higher annealing temperature (600 °C), resulting in a lower dispersion degree, which is usually undesirable for catalysts. It is discovered that Ni₃P has a hexagonal prism shape, and its length-to-diameter ratio is 2 to 1 [141].

Zhang et al. studied macro-mesoporous carbon (MMCs) encapsulated in Ni nanoparticles catalysts synthesized by dual-templating technique for glycerol hydrogenolysis to 1,2-PDO. On hierarchical catalysts, the glycerol conversion of 95.5% was achieved along with 77.1% selectivity of 1,2-PDO over Ni/MMC-6 catalyst at 210 °C and 4 MPa. Ni supported on multiporous carbon was highly active, stable, and selective catalysts for hydrogenolysis of glycerol to PDO. These catalysts’ performance was attributed to their

feed flowrate = 12mL/h (Continuous flow reactor)
large surface area and pore volume proposed to reduce mass transfer limitation in the system. The total surface area and pore volume of the Ni/MMC-X materials were found to be much greater than those of the Ni/C micro and Ni/CNT (Ni modified carbon nanotubes) materials \[154\].

Chimentão et al. investigated zinc–supported Cu and Ni catalysts for glycerol hydrogenolysis. 100% transformation of glycerol was achieved over Ni/ZnAl catalyst. 55% and 49% selectivity of hydroxyacetone and 29% and 26% yield of hydroxy acetone were achieved over Cu/ZnAl and Cu/ZnO catalyst simultaneously at 300 °C. Ni promoted catalysts that formed methane, and Cu promoted catalysts that acetol formation. The thermodynamically stable phase of zinc oxide at ambient conditions is zincite, which crystallizes in the hexagonal wurtzite structural type. It was mentioned that the acidity of ZnAl and ZnO promoted activity. Adsorption and acidity played a vital role in the transformation of glycerol \[155\]. The catalyst has both acidic as well as basic sites. The basic sites' influence must also be considered. The mechanism of glycerol dehydration for acetol formation over basic sites was proposed \[95\]. The reaction mechanism proposed over basic sites began with the dehydrogenation step rather than the dehydration step \[156\] (Figure 7).

![Figure 7. Reaction process over basic sites of HZSM-5 catalyst for glycerol conversion.](image)

In this, 2,3-dihydroxypropanal, through dehydration and hydrogenation produced acetol and/or through the retro-aldol reaction of formaldehyde and 2-hydroxyethanal (hydroxyacetaldehyde) to produce ethylene glycol through hydrogenation \[93,95,156\]. The glycerol hydrogenolysis mechanism is suggested in two steps for propylene glycol (1,2-PDO, 1,3-PDO) production: dehydration and hydrogenation. The mechanism of glycerol hydrogenolysis involves dehydration first and then hydrogenation. The different dehydration intermediates of glycerol correspond to propylene glycol through hydrogenation. The tautomeric equilibrium is indicated as a double-arrow between the dehydration intermediates (Figure 8) \[157,158\].
4.2. Copper Catalysts for Glycerol Hydrogenolysis

Bimetallic Ru–Cu nanoparticles supported over the series of TiO$_2$ catalysts prepared from the impregnation method for hydrogenolysis of glycerol for 1,2-PDO production was studied [142]. 53.9% glycerol conversion and 93.2% 1,2-PDO selectivity were achieved of 2.5Ru-2.5Cu/TiO$_2$ catalyst at 200 °C and 2.5 MPa. The best performance was shown by 2.5Ru-2.5Cu/TiO$_2$ catalyst and concluded that the addition of Ru-Cu-based catalyst enhanced 1,2-PDO selectivity. Copper-supported activated carbon through the impregnation method for glycerol production of 1,2-PDO [159]. The maximum glycerol transformation of 23%, along with 20% 1,2-PDO selectivity, was achieved over copper (Cu) supported on activated carbon treated at 750 °C (Cu/CGran(750)) at 220 °C and 5 MPa. The interaction of Cu species with carbon support was minimized at high temperatures, leading to large Cu particles. Novel bi-functional Cu–Mg/SiO$_2$ catalyst through chemisorptions–hydrolysis technique for production of 1,2-PDO from hydrogenolysis of glycerol and 89.5% transformation of glycerol, as well as 92.1% selectivity of 1,2-PDO achieved over Cu$_{0.1}$-Mg$_{0.2}$, supported SiO$_2$ catalyst at 210 °C and 4 bar [160]. The result revealed that Cu species were enough active sites for maximum activity, the addition of copper reduced the Lewis acid sites and enhanced the Bronsted acid sites. Shan et al. investigated Cu/SBA-15 catalyst through a simply grinding technique and impregnation method for 1,2-PDO production from hydrogenolysis of glycerol. A 90.3% transformation of glycerol along with 97.3% 1,2-PDO selectivity was achieved at 10% Cu/SBA-15 prepared through grinding method at 230 °C and 4 MPa. Cu/SBA-15 catalysts with large surface areas showed excellent stability as well as activity in the hydrogenolysis reaction of glycerol [161].

4.3. Platinum Catalysts for Glycerol Hydrogenolysis

Feng et al. studied tungsten (W) and aluminum (Al) doped into SBA-15 through one-step technology in the acidic medium for glycerol hydrogenolysis for 1,3-PDO production. Diffraction peaks were detected clearly after the metal ions were incorporated into the SBA-15 framework, suggesting that the SBA-15 mesoporous structure was well conserved after the direct synthesis [162]. The glycerol transformation was 66%, and 50% 1,3-PDO selectivity was achieved over Pt supported (W+Al) modified SBA-15 catalyst at 160 °C and 6 MPa. Niu et al. investigated WO$_x$-supported Pt catalysts prepared through hydrothermally and impregnation method for hydrogenolysis of glycerol to 1,3-PDO [163]. Pt doped over HWO$_3$ catalyst produced 63.4% glycerol transformation and 43.1% 1,3-
PDO selectivity at 5 MPa and 160 °C. The enhancement in performance showed the Pt nanoparticle dispersion, the high acidic nature, and the interaction of HWO₃. The tungsten modification effect on phosphate-supported zirconia Pt catalyst for hydrogenolysis to produce 1-propanol [164].

Wang et al. achieved glycerol conversion 100% and 81% 1–Propanol yield was achieved at Pt/7WOₓ–ZrP catalyst at 270 °C and 2 MPa. It was concluded that the modification of ZrPWOₓ increased the catalyst’s total acidity, which was beneficial for glycerol conversion and also enhanced Pt nanoparticles dispersion. The addition of WOₓ mainly improved Lewis acid sites, while Bronsted acid sites remained the same. Various supported, as well as unsupported, Pt–W-based catalysts to produce 1,3-PDO from the hydrogenolysis of glycerol. Among all, Pt-WOₓ doped Al₂O₃ provided the best activity and selectivity and showed strong dispersion of Pt over WOₓ which promoted strong Bronsted acidic sites [165].

4.4. Iron Catalysts for Glycerol Hydrogenolysis

Heterogeneous iron-containing nanocrystals for the hydrogenolysis of glycerol and mentioned that the incorporation of Fe metal positively affected selectivity and activity of catalysts for glycerol hydrogenolysis towards 1,2-PDO [153]. The recent achievements in Fe–based heterogeneous catalysts in the hydrogenolysis and hydrogenation process are outlined in this review. Lopez et al. studied hydrotalcite-supported transition metals (Fe, Zn, Ni, and Cu) prepared by the coprecipitation technique for hydrogenolysis of glycerol for 1,3-PDO production and 89.7% glycerol transformation along with 82.6% yield and 92% selectivity of 1,2-PDO was achieved over 15 wt.% Cu supported on hydrotalcite (HDTs-Cu) catalyst at 3.4 MPa and 200 °C. The highest activity and 1,2-PDO selectivity were achieved over copper-modified catalysts even with 62% purity of crude glycerol employed.

By comparing these peaks, it was discovered that when the metals iron, nickel, copper, and zinc were replaced in the environment with laminar octahedral brucite coordination, the intensity of the characteristic peak (003) increased, indicating an increase in structural integrity by assuming trilaminar rhombohedral layer stacking. When the surface properties of several HDT-type catalytic materials were characterized, an area drop was seen when the cation ionic radius (ionic radius, Fe, Ni, Cu, and Zn) increased. However, HDT-Ni was an exception because its area value was lower than those achieved with materials containing Cu and Zn. Ni has a shorter ionic radius than Cu and Zn; therefore, it was hypothesized that the catalyst incorporating Ni would have a larger surface area. This can likely be linked to the material’s synthesis or maturation [166].

4.5. Cerium Catalysts for Glycerol Hydrogenolysis

Cerium (Ce) promoted Cu/Mg catalyst through coprecipitation method for production 1,2-PDO through hydrogenolysis of glycerol. The activity of catalysts for glycerol hydrogenolysis was achieved in order: Cu/Mg < Cu/Ce1/Mg < Cu/Ce5/Mg < Cu/Ce3/Mg. The markable point was that CeO₂ and Cu/Mg with atomic ratio = 3/5 catalyst might be used several times for hydrogenolysis reaction of glycerol without reducing activity. It is worth noting that the Cu/Ce1/Mg and Cu/Ce3/Mg samples revealed varied XRD peaks corresponding to CuO phases, but the metallic Cu phase showed no XRD peaks. When compared to pure CeO₂, the CeO₂ diffraction peaks of Ce-promoted Cu/Mg materials were moved to the higher angle side. This odd observation could be due to the interaction between CeO₂ and Cu/Mg samples [139].

4.6. Silver Catalysts for Glycerol Hydrogenolysis

A series of silver-modified catalysts for hydrogenolysis of glycerol produced 1,2-PDO; 78.8% conversion and 54.2% selectivity of 1,2-PDO over Raney-Ni₃₄Ag catalyst at 210 °C and 4 MPa. Ag modified catalyst presented better activity and enhanced C₃ product selectivity contrasted with unmodified Raney nickel (R-Ni) catalyst. At low and high magnification, SEM pictures of the R-Ni-based catalysts revealed a prominent porosity
zone, indicating that fresh R-Ni is a high-surface-area catalyst made up of reduced Ni particles. R-Ni had a BET surface area of 21.1 m²gcat⁻¹ after drying and passivation, which increased to 42.4 m²gcat⁻¹ when a modest amount of Ag was added to R-Ni and reduced significantly when more Ag was added [140].

Summary of some more reported literature related to glycerol reforming over heterogeneous catalysts to produce propylene glycol (1,2-PDO, 1,3-PDO), and ethylene glycol is represented in Tables 4 and 5.

**Table 4.** Glycerol hydrogenolysis over various catalytic systems for 1,2-PDO production.

| S. No. | Catalysts | Reaction Conditions/Reactor | X (%) | S (%) | Y (%) | References |
|--------|-----------|-----------------------------|-------|-------|-------|------------|
| 1      | Nickel phosphide | T = 463 K P = 5.5 MPa (Autoclave reactor) | 5.4   | 95.3  | 5.15  | [141]      |
| 2      | 2.5Ru-2.5Cu/TiO₂ (Impregnation method) | T = 473 K P = 2.5 MPa Cat. Wt. = 0.6 g | 53.9  | 93.2  | 50.2  | [142]      |
| 3      | Cu₀.₁-Mg₀.₂ supported SiO₂ (Chemisorption–hydrolysis method) | T = 210 °C P = 45 bar | 89.5  | 92.1  | 81.2  | [160]      |
|        |           | (Autoclave reactor)         |       |       |       |            |
| 4      | 10% Cu/SBA-15 (Grinding and Impregnation method) | T = 503 K P = 4 MPa | 90.3  | 97.3  | 87.9  | [161]      |
| 5      | hydrotalcite supported Fe, Zn, Ni, and Cu (Coprecipitation method) | T = 200 °C P = 3.4 MPa | 92    | 89.8  | 82.6  | [166]      |
| 6      | Ni–Cu/Al₂O₃ (Sol–gel method) | T = 723 K P = 1 bar (Autoclave reactor) | 33.5  | 85.9  | 28.8  | [167]      |
| 7      | Raney Ni | T = 230 °C P = 40 bar (Autoclave reactor) | 80    | 54    | 43.2  | [168]      |
| 8      | Cu over Al₂O₃, ZnO and Cr₂O₃ | T = 190 °C P = 1 atm (Fixed bed reactor) | 100   | 96.2  | 96.2  | [169]      |
| 9      | Cu over boehmite (Chemical reduction method) | T = 473 K P = 4 MPa Cat. Wt. = 0.8 g (Autoclave reactor) | 77.5  | 92.5  | 71.2  | [170]      |
| 10     | B₂O₃ on Cu/SiO₂ (Precipitation–gel method) | T = 200 °C P = 5 MPa WHSV = 0.075 h⁻¹ (Fixed bed reactor) | 98.5  | 96.7  | 95.2  | [171]      |
| 11     | Pt, Pd and Ni/Fe₃O₄ (Impregnation method) | T = 493 K P = 25–50 bar Cat. Wt. = 0.5 g (Fixed bed reactor) | 81    | 79    | 70    | [172]      |
| 12     | Alumina supported bimetallic Pt–Fe (Impregnation method) | T = 513 K P = 20 bar Cat. Wt. = 0.5 g (Batch reactor) | 86.2  | 58.2  | 50.2  | [173]      |
Table 4. Cont.

| S. No. | Catalysts | Reaction Conditions/Reactor | X (%) | S (%) | Y (%) | References |
|--------|-----------|----------------------------|-------|-------|-------|------------|
| 13     | Fe₂O₃ at CuMgAl | T = 190 °C  
P = 2 MPa | 77.8  | 99    | 77    | [174]     |
| 14     | Ce promoted Ni/SBA-15 (Incipient method) | T = 473 K  
P = 2.4 MPa  
Cat. Wt. = 0.6 g (Autoclave Parr reactor) | 50    | 28    | 14    | [175]     |
| 15     | Ni/Ce–Mg (Precipitation and impregnation method) | T = 215–245 °C  
P = 4.1–6.9 MPa  
Cat. Wt. = 5.0 g (Batch reactor) | 80.47 | 74.4  | 59.9  | [176]     |
| 16     | Ni–Co bimetallic supported on γ-Al₂O₃ (Impregnation method) | T = 220 °C  
P = 6 MPa  
Cat. Wt. = 2.0 g (Autoclave reactor) | 63.5  | 60.4  | 38.4  | [177]     |
| 17     | Ni–Ag/γ-Al₂O₃ (co-impregnation method) | T = 180–260 °C  
P = 1 atm  
WHSV = 2.01 h⁻¹ (Fixed bed reactor) | 80    | 58    | 46.4  | [178]     |
| 18     | Ag/Al₂O₃ (Impregnation method) | T = 400–500 °C  
P = 2.1 MPa (Batch reactor) | 46    | 96    | 44.2  | [179]     |
| 19     | Ag-OMS-2 (Precipitation method) | T = 200 °C  
P = 50 atm  
Cat. Wt. = 28.0 g (Fixed bed reactor) | 70    | 90    | 63    | [180]     |

X = Conversion, S = Selectivity, Y = Yield.

Table 5. Glycerol hydrogenolysis over various catalytic systems for producing 1,3-PDO, propylene glycol, and ethylene glycol.

| S. No. | Product | Catalysts | Reaction Conditions/Reactor | X (%) | S (%) | Y (%) | References |
|--------|---------|-----------|----------------------------|-------|-------|-------|------------|
| 1      | 1,3-PDO | Pt–sulphated zirconia | T = 170 °C  
P = 7.3 MPa | 66.5  | 83.6  | 55.6  | [181]     |
| 2      | 1,3-PDO | Pt–WO₃ on Al-based supports and Ir–ReOₓ/SiO₂ (Impregnation method) | T = 403 K  
P = 4 MPa  
T = 110–140 °C  
P = 2–5 MPa (Fixed bed reactor) | 84.5  | 26    | 30    | [83]      |
| 3      | 1,3-PDO | Pd–Ni bimetallic (Co-precipitation method) | T = 493 K  
P = 6 MPa (Autoclave reactor) | 70.2  | 45.6  | 32    | [182]     |
| 4      | Ethylene glycol | Cu–Ni (Impregnation method) | T = 250 °C  
P = 40 bar  
WHSV = 2.5 h⁻¹ (Fixed bed reactor) | 90    | 77.8  | 70    | [184]     |
| 5      | Propylene glycol | Cu/HMS, (Ru–Cu)/SiO₂, (Impregnation method) | T = 240 °C  
P = 8 MPa (Fixed bed reactor) | 100   | 91    | 91    | [185]     |
Table 5. Cont.

| S. No. | Product        | Catalysts                        | Reaction Conditions/Reactor                  | X (%) | S (%) | Y (%) | References |
|--------|----------------|----------------------------------|---------------------------------------------|-------|-------|-------|------------|
| 7      | Propylene glycol | Al, Ba and Zn promoter in copper chromite | $T = 493 \text{ K}$  
$P = 5 \text{ MPa}$  
Cat. Wt. = 1 g  
(Fixed bed reactor) | 34    | 90    | 30.6  | [186]     |

X = Conversion, S = Selectivity, Y = Yield.

5. Conclusions

The knowledge of various catalysts, such as nickel, platinum, ruthenium, copper, cadmium, zeolite, titanium, alumina, iron, cerium, silver, and rhodium, steam reforming process, dehydration process, and hydrogenolysis process of glycerol was reviewed and cataloged. Numerous researchers have described various ways of converting glycerol into value-added products, such as hydrogen, acetal, acrolein, ethylene glycol, propylene glycol (1,2-propanediol, 1,3-propanediol), etc., via several reactions under different reaction conditions. These chemical compounds have a clear monetary value and can help the biodiesel industry.

Many research efforts are ongoing to overcome challenges and explore new frontiers to search for new products. Those challenges involve the selection of catalyst for some products and reaction conditions, severe difficulty in separating the catalyst from desired products, and low yields of the products with long catalytic reaction runs. Today, researchers and engineers are exploring new technologies, highly novel and tolerant catalysts, improving reactor systems and activation methods, and coordinating the chemical and biological catalysts to improve the weaknesses involved with each catalyst. The modern improvement in technology and economical use of crude glycerol for value-added product formulation clearly demonstrate that crude glycerol may play a critical part in the bio-refining industry’s fulfillment.

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