Fabrication and Characterization of Woven and Non-woven Textiles Derived from Natural Resources

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Abstract: The present work investigated the properties of long fibers derived from oil palm empty fruit bunches (OPEFB) for the potential woven and non-woven textiles production. Several characterizations such as XRD, FTIR, SEM-EDX, DSC, and mechanical testing were carried out to understand the properties comprehensively. This study found that the OPEFB has the potential for the production of woven and non-woven textiles. The properties of OPEFB fibers were comparable with synthetics fibers that are commonly used in the textile industry. XRD analysis confirmed the structural properties, while the FTIR showed the biomolecules’ bonding characteristics. In general, the physical and mechanical properties of the OPEFB fibers depend on surface modification and chemical treatments.

Keywords: Oil palm empty bunches; natural fibers; mechanical properties.

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1. Introduction

The effort to increase the number and variety of textile products, especially the organic raw material for woven fabrics, which is sourced from waste utilization, is an innovation in increasing the diversity of organic non-cotton textile raw materials and solving the national palm oil solid waste problem into high economic products [1-4]. Oil palm empty fruit bunches (OPEFB) are solid waste from palm oil production, produced into long fibers by chemical-physical extraction methods [5-7]. Surface modification of the resulting long fibers can produce organic fibers with mechanical properties similar to synthetic fibers for the textile industry [8,9].

The extent of oil palm plantations in Indonesia can meet the national need for vegetable oil and its derivatives as well as export fulfillment. The problems in palm oil production are the production of solid waste and the release of liquid waste Palm Oil Mill Effluent (POME) that should be given special attention [10-12]. Utilization of OPEFB with technology and producing organic fiber products that can be woven (woven and non-woven) in order to increase economic value has a strategic role in the development and supply of national textiles [13,14]. This strategy can be realized through real contributions in producing applicable material engineering for palm oil products and diversifying competitive textiles.
This study analyzes the behaviors of long fibers derived from OPEFB for the potential woven and non-woven textiles production. Several characterizations such as XRD, FTIR, SEM-EDX, DSC, and mechanical testing were carried out. Findings from this study exhibited that the OPEFB can potentially produce woven and non-woven textiles. The properties of OPEFB fibers were comparable with synthetics fibers that are commonly used in the textile industry.

2. Materials and Methods

2.1. Materials.

The main material used in this study is OPEFB obtained from from PTPN VIII Cikasungka, Bogor Regency. Long fiber was synthesized in the Manunggal Alam UKM, Wirajaya Jasinga, Bogor, West Java. Non-woven fabrics were manufactured at Center for textiles, Bandung. Woven fabrics were made at UKM Bintang Terang Putra Majalaya, Bandung.

2.2. Alkaline peroxide treatment.

The alkaline peroxide treatment was carried out in accordance with the previous works. Briefly, OPEFB fibers are mixed with 0.4% sodium hydroxide solution. The mixture was heated at 60 °C in a water bath and stirred at 200 rpm for 1 hour. Then, the mixture was filtered and washed with distilled water. Further, the solid residue is mixed with 4% hydrogen peroxide solution. 50% sodium hydroxide is added to the suspension until the pH of the suspension reaches 11.5. The suspension was then heated at 80 °C at different reaction times, which are 30, 90, 180, and 360 min. Then, the suspension was filtered and the residue was washed to a neutral pH. The size of the long fiber is measured based on the IAWA (International Association of Wood Anatomy) standardization with the average dimensions of the fibers measured using an optical microscope.

2.3. OPEFB fiber surface modification.

OPEFB fiber surface modification was carried out by immersion variations with a sunsoft solution at a concentration ranging from 2 - 10% w/w and time variation ranging from 6-14 h at room temperature. Then, the modified OPEFB fibers were dried under the sun until the moisture content reached 20%. After drying, the fiber samples were put in a drying oven at 100 °C for 8 h until the moisture content was less than 7%. The resulting soft OPEFB fibers are then subjected to a mechanical process with a spinning machine to unite or twist the OPEFB fibers into a surface-smooth strand followed by a homogeneous diameter. Woven fibers are made using ATBM woven webbing and non-wovens are made using sewing equipment.

2.4. Characterization.

Testing the quality of OPEFB fiber is carried out with a chemical composition based on the standards of the Pulp and Paper Industry Technical Association (TAPPI). The density was carried out using the Archimedes method. Thermal testing was carried out in accordance with SNI 08-1512-89 vertical test textile standards. Several characterizations were carried out to determine the properties of samples, such as by using XRD, FTIR, SEM-EDX, DSC, and ASTM. In the preparation, the OPEFB woven fibers were cut to 40 x 40 cm and immersed in...
ATH solution with various concentrations of 15 phf, 30 phf, and 60 phf. Furthermore, the OPEFB woven fibers were immersed in ATH and oven for 2 h at 100 °C. Furthermore, the sample was subjected to a burn test using SNI Textile standardization with 5 repetitions for each concentration. In addition, mechanical tests were also carried out to determine the effect of increasing the concentration of ATH on the mechanical properties of the fibers to be used as a filler in composites.

3. Results and Discussion

3.1. XRD analysis.

The optimum value for used fiber as a material for making woven and non-woven fabrics is based on variations in concentration and dyeing during the extraction process at room temperature (Figure 1). The best results were based on testing the chemical composition of OPEFB with TAPPI standards, namely the resulting cellulose content of 55.08%, 25.06% for hemicellulose, 19.14% for lignin, 5.24% for extractive substances, 5.97% for water content, 3% for fat content and 80.14% for holocellulose [15].

OPEFB fiber microstructure was examined using an XRD instrument to analyze crystallinity, Miller's index, and phase structure [16,17]. Figure 1 and Figure 2 show that the OPEFB used fibers have a monoclinic phase structure with $a \neq b \neq c$ and $\alpha = \gamma = 90^\circ 0 \neq \beta$ with a crystal peak angle at $2\theta = 22^\circ$ at hkl 002 [18]. Some peaks look amorphous at $2\theta = 35$–80 degrees. Indexing of the diffraction profile was performed using powder-X that result in lattice...
parameters $a = 7.87$, $b = 10.31$, $c = 10.13$ and $a = g = 90$, $b = 120$. In the crystalline region of cellulose, each atom occupies a regular position in the lattice periodically and it is repeated until a solid structure is formed based on its crystallography. The higher the crystallinity of cellulose, the stronger the properties of the bio composite-forming material against deformation [19]. Meanwhile, in the amorphous region, there is no visible peak, where the atoms making up the OPEFB fibers are not at the lattice point, therefore, they are not brave. It reflects that the method has not made OPEFB fibers with high cellulose purity with a high degree of crystallinity. The energy generated during the production process has not been able to penetrate the cell walls optimally. 3.2. FTIR analysis.

Molecular groups in OPEFB fibers were tested using FTIR. It was assessed to obtain information on the role of OPEFB fibers in binding with other materials together in the molecular building of composite structures. Figure 3 shows the FTIR image of the OPEFB fiber sample. The transmittance peak of the FTIR spectra reflects chemical functional groups. The peak seen at wave number $3700–3200$ cm$^{-1}$ shows the O − H stretching of the cellulose hydroxyl groups. The absorbance peak at $3300–3450$ cm$^{-1}$ indicates the presence of O − H stretching of the cellulose hydroxyl groups [20,21]. The transmittance of the wavenumbers $3333$ cm$^{-1}$ to $3348$ and $3379$ cm$^{-1}$ are intra-and intermolecular hydrogen bonds. 3000 and 2800 cm$^{-1}$ are aliphatic saturation C − H stretching vibrations [22]. Kubovský, Kačíková [23] explained that the occurrence of a bond between $3300–3600$ cm$^{-1}$ is the stretching of lignin (intramolecular hydrogen bond in phenolic groups, OH stretching of alcohols, phenols, acids and weakly bounded absorbed water). Lignin also had bands about 2900 cm$^{-1}$ (C−H stretching in methyl and methylene groups).

As shown in Figure 3, it can be seen that the wavenumber 1605 to 1589 cm$^{-1}$ is C = C stretching vibration and stretching symmetric of lignin. The peaks of 1450 and 1435 cm$^{-1}$ indicate O − H and symmetric CH$_2$ at C$_6$ of cellulose [24]. The transmittance peak at $1250$ cm$^{-1}$ is C − O stretching aryl alkyl ether lignin. Carboxylic acid groups and tertiary amides can be found in the wavenumbers 1260 to 1240 cm$^{-1}$. A peak at 1049 cm$^{-1}$ indicates the presence of silica groups Si − O − Si and SiO − H. The OPEFB fiber sample shows a peak at wave number 663 cm$^{-1}$ is COH.

![Figure 3. FTIR spectra of OPEFB fibers.](https://biointerfaceresearch.com/)

3.3. Surface morphology and thermal properties.

Micro morphology was assessed using an optical microscope (MO) and scanning electron microscope (SEM) instruments to analyze changes in the surface of OPEFB fibers.
Figure 4 shows that the extracted OPEFB fibers have a waxy layer, have pores, trachea and a rough surface.

Thermal testing with DSC aims to determine the response of OPEFB fibers to heat which includes endothermic, exothermic, glass transition and melting points, which will be correlated with a flame test. The OPEFB fiber material in the endothermic phase ($\Delta H = 128 \text{ J g}^{-1}$) is the first phase when the material absorbs heat for water evaporation until the initial temperature of 48 ºC to 79 ºC [20]. Then, the glass transition phase occurs when the material is in rubber formation 121 ºC and melts at 270 ºC. When the material receives a heat response, the next step is the exothermic phase ($\Delta H = 32.8 \text{ J g}^{-1}$) at 307 ºC. The next stage is carbonization. The areas under the endothermic and exothermic curves show the change in enthalpy ($\Delta H$), which is the energy required to change the thermal phase of the material (Figure 5).

![Image](https://doi.org/10.33263/BRIAC122.18141823)

**Figure 4.** OPEFB fiber morphology by means of (a) MO; (b) SEM 100x; (c) SEM 800x.

### 3.4. Mechanical properties.

To determine the external deformation ability of the material, tensile strength (TS) testing on single OPEFB and woven fibers was carried out using ASTM D638 with 5 repetitions. Based on Table 1, it can be explained that the TS bundle fiber has an average value of 30.99 MPa. Meanwhile, the TS of EFB fiber in the form of yarn as raw material for woven is 80 MPa. The OPEFB fiber bundle obtained from the treatment process has a high tensile strength when two opposing vertical forces are applied during the test. Compared with woven OPEFB fibers arranged from bundles of bundles with spun physical bonds between the fibers to form yarn, the arrangement of OPEFB fibers into webbing has a higher mechanical strength. This is because the tensile strength test, the breaking strength when given the opposite vertical tensile force at the base and tip of the sample per unit area, is calculated based on the breaking of the fibers and the bonds between the fibers on the woven very strong. Testing mechanical properties in automotive component applications emphasized a single fiber. TKSS fibers have a role in spreading the accepted deformation along the fibers in the polymer matrix without breaking. Therefore, information regarding tensile strength is needed. Meanwhile, bullet-proof materials require information on the ability of OPEFB fibers in the form of woven threads (a collection of several fiber bundles) to inhibit or absorb kinetic energy after the collision. Furthermore, the bullet can become lodged in the material, or the bullet has an unresponsive impact after the impact.

Mechanical analysis of tensile test on woven OPEFB fibers was carried out to determine the tensile strength of the fibers [25]. The analysis is needed to determine the feasibility of fibers as a filler material in composites. This test was carried out on woven fiber samples with
variations in the concentration of ATH, namely 15 phf (TK-1), 30 phf (TK-2), 60 phf (TK-3) with 3 repetitions of each. The tensile test that follows ASTM D638 is a test by carrying out the pull/stretching of a test rod that continuously increases due to the load acting on the test rod until the test rod breaks. The measurement process is carried out using a Computer Control Electronic Universal Testing Machine with a displacement speed of 50 mm min⁻¹. The gauge length of the sample is 50 mm. Several parameters are used to analyze mechanical properties, such as tensile strength, elongation at break, and Young's modulus.

Tensile strength is defined as the maximum tensile (stress) that can be achieved by the specimen when the specimen breaks/tears. Based on the tensile test results on each sample, it is known that the tensile strength increases with increasing concentration. At the highest ATH concentration (60 phf), the highest tensile strength was obtained at 476.61 MPa. Furthermore, for the ATH concentration of 15 phf and 30 phf the tensile strength values were 374.33 MPa and 424.8 MPa, respectively. A number of studies have stated that adding a flame retardant, for example, ATH, to a specimen will generally reduce mechanical properties. However, other researchers stated that the addition of ATH concentration at a certain concentration actually increases the tensile strength value. It is caused by ATH inhibits the mobility of the matrix used. The flame retardant (FR) in a specimen acts as a nucleating agent that can reduce tensile strength and reduce elongation at break, except in specimens with lower FR concentrations. However, it indicated that the ATH concentration used in this study was still relatively low. The high ATH concentration did not decrease the tensile strength of the sample.

Elongation at break is the increase in the length of a test piece when it is stretched until it breaks, expressed as a percent (%) of the length of the test piece before being stretched [26]. The test is carried out in order to determine the stress and strain properties of the specimen. Based on the results of the tensile test, it is known that the percentage of elongation at break increases with an increase in concentration. At 15 phf and 30 phf ATH concentrations, it is known that the elongation at break value is 0.18%. Then at the ATH concentration of 60 phf, the elongation at break value increased by 0.02%, which was 0.20%.

Young modulus measures the strength or elasticity of a material when stress is applied [27]. This value is obtained from the ratio of stress and strain based on the stress curve (y-axis) - strain (x-axis). The greater the young modulus value, the stiffer the material can be, and vice versa [28]. Based on the test results on the three samples, it is known that the highest modulus young value is found in the woven fiber sample with the highest ATH concentration (60 phf) of 2.83 GPa. Meanwhile, for woven fibers with a concentration of 15 phf and 30 phf, they were 2.73 GPa and 1.49 GPa, respectively. In this case, it means that the addition of ATH concentration causes the fiber to be inelastic/stiff. ATH has the form of pollen with water-insoluble properties. This dense and rigid nature causes the limitation of the motion of the polymer molecules. Based on the results of the mechanical test above, ballistic testing was carried out on samples with a concentration of ATH 60 phf.

In this study, the burn test was carried out to determine the ability of the fiber to withstand a given flame. The combustion test carried out refers to the ASTM D6413 standard, wherein this test, the time of flame, burn, and length of fiber burned (coal) is analyzed by repeating each of 5 times. Fibers measuring 30 x 5 cm are glued to the frame of the test equipment with a clamp. Then a flame 3 cm long is applied to the fibers and held for up to 12 seconds. Furthermore, 3 test parameters, such as flame, burn, and coal, are analyzed. The best results on the sample are used as core composite sandwiches.
Based on Table 2, the sample with the best fire resistance ability at the highest concentration is the TK-3 sample (60 phf concentration), with flame, burn, and coal length times were 3,706 s, 17,648 s, and 6.3 cm, respectively. The high concentration of ATH results in high thermal properties and fire resistance. The role of ATH in fibers with high concentrations is quite effective in inhibiting the propagation of larger (long) flames. The relatively low flame time records evidence it. The length of the intact fibers burned at this concentration ± 3 cm and left a little black mark along the ± 3.3 cm. High burn resistance can be caused by a large amount of ATH filling the void in the fiber bundle. In the ATH coating process, the woven fibers are firstly immersed for ± 15 min. This causes a widening of the fiber surface and an ATH filling. The retention of flame on the fiber (thermal decomposition) occurs through an endothermic process which is the basic principle of the mechanism of action of ATH. The thermal decomposition of ATH takes place at 220 °C. The decomposition process produces several water vapor (3H₂O), reducing the interaction between the fiber surface and oxygen (O₂). The aluminum (Al₂O₃) formed acts as a surface protector for the fibers. Therefore, further spread of the fire did not occur. In general, the present work has contributed significantly to the development of material derived from natural resources.

![Figure 5. Thermal properties of OPEFB.](image)

| Repetition | Tensile Strength (MPa) non-woven | Tensile Strength (MPa) woven | Tensile Strength (MPa) bundle fiber |
|------------|----------------------------------|-----------------------------|-----------------------------------|
| 1          | 5.45                             | 80.44                       | 34.11                             |
| 2          | 3.27                             | 79.61                       | 34.11                             |
| 3          | 6.55                             | 81.27                       | 25.59                             |
| 4          | 7.39                             | 82.10                       | 27.06                             |
| 5          | 4.73                             | 78.78                       | 34.11                             |
| Average    | 5.48                             | 80.44                       | 30.99                             |

**Table 2.** Burn test of several prepared samples.

| Sample | Flame (s) | Burn (s) | Coal (cm) |
|--------|-----------|----------|-----------|
| TK-3   | 3.706 ± 2.31 | 17.648 ± 7.96  | 6.3 ± 1.44 |
| TK-2   | 45.626 ± 42.81 | 82.21 ± 88.14  | 9.4 ± 4.02  |
| TK-1   | 131.53± 91.76 | 350.294 ± 222.85 | 23.9 ± 5.96 |
| TK-0   | 175.146 ± 33.20 | 613.748 ± 179.2  | 30 ± 0     |

Although several synthetic materials have been established, the current trend focuses on how they can be derived from natural resources because of their hugely available in the

[https://biointerfaceresearch.com/](https://biointerfaceresearch.com/)
environment and their performance is comparable with the synthetic materials [29-33]. Therefore, the development of materials derived from natural resources has been more popular and has been applied for various applications [34-39].

4. Conclusions

This study aimed to analyze the behaviors of long fibers derived from OPEFB for the potential woven and non-woven textiles production. Findings from this study exhibited that the OPEFB can potentially produce woven and non-woven textiles. The properties of OPEFB fibers were comparable with synthetics fibers that are commonly used in the textile industry.

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Conflicts of Interest

The authors declare no conflict of interest

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