A Comprehensive Review on Grid Connected Photovoltaic Inverters, Their Modulation Techniques, and Control Strategies

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Abstract: The installation of photovoltaic (PV) system for electrical power generation has gained a substantial interest in the power system for clean and green energy. However, having the intermittent characteristics of photovoltaic, its integration with the power system may cause certain uncertainties (voltage fluctuations, harmonics in output waveforms, etc.) leading towards reliability and stability issues. In PV systems, the power electronics play a significant role in energy harvesting and integration of grid-friendly power systems. Therefore, the reliability, efficiency, and cost-effectiveness of power converters are of main concern in the system design and are mainly dependent on the applied control strategy. This review article presents a comprehensive review on the grid-connected PV systems. A wide spectrum of different classifications and configurations of grid-connected inverters is presented. Different multi-level inverter topologies along with the modulation techniques are classified into many types and are elaborated in detail. Moreover, different control reference frames used in inverters are presented. In addition, different control strategies applied to inverters are discussed and a concise summary of the related literature review is presented in tabulated form. Finally, the scope of the research is briefly discussed.

Keywords: grid-connected PV system; grid-connected PV inverters; multi-level inverters; modulation techniques; control strategies; current control

1. Introduction

Renewable energy (RE) plays a pivotal role in supporting the power system to meet the ever-increasing load demand. Among the renewable energy resources (RES), photovoltaic (PV) power units are gaining more interest due to (a) clean and emission free energy, (b) simple access, and (c) high return on investment [1]. Up to the year 2009, the majority of PV installations were made at a small level and were only connected to the distribution level. However, when the USA installed the first transmission level (230 kV) PV system in Florida [2], it drew the world’s attention. Therefore, the interest in large scale PV installation (transmission and sub-transmission levels) increased rapidly and as a result, globally the installed capacity of PV reached 505 GW by the end of 2018. The total installed capacity of PV from 2008–2018 is presented in Figure 1. The figure shows a dramatic increase in PV installation as in 2008 the installed capacity is 15 GW, and it increases to 505 GW at the end of 2018 [3].

Depending on the conversion system, two types of configuration systems are used for grid-connected PV power plants (GCPPPs), i.e., single and two stage conversion/configuration systems. A configuration is said to be a single stage, when there is a direct connection between the inverter input side and the PV array and is then connected to the grid through the transformer as
Among these topologies, a conventional 2-level inverter topology is very popular and widely used for small scale applications. However, this inverter is not appropriate for medium and large-scale applications as it suffers from high voltage stresses and high thermal losses that significantly decrease the efficiency of the system [5]. To overcome these problems, multilevel inverter (MLI) topologies were introduced for GCPPPs as they have the ability to provide good quality output waveforms with low harmonic distortion, lower stress on switches, a lesser requirement of passive filter, and require less maintenance [6–8]. The MLIs are classified into various types based on the power circuitry structure such as reduced switch [9,10], asymmetric [11], modular [12], and hybrid [13,14], etc. The quality of output waveforms of MLIs greatly depends on the modulation technique (MT) applied to the switches (metal oxide silicon field effect transistor, insulated gate bipolar transistor, etc.). The main tasks of MTs are to control and enhance the output waveforms and to minimize the total harmonic distortion (THD) as well as switching losses. Based on switching frequency the MTs are classified into high switching frequency (HSF) [15,16] and fundamental switching frequency (FSF) [17]. Both types of modulation techniques are further classified into various types that will be discussed later in this article in detail.

Figure 1. Total installed capacity of photovoltaic (PV) (2008–2018) [3].

Figure 2. PV configuration systems: (a) single stage and (b) two stage [4].

Due to the stochastic and unpredictable nature of PV, the functionality of the grid-connected inverters (GCIs) is not only limited to DC–AC conversion, but also has to provide various intelligent and ancillary services such as voltage regulation, frequency regulation, etc. [18]. As the operation of GCPPPs mainly depends on the control algorithm applied to the GCIs, the design of the controller is of main consideration and can therefore be categorized into two main segments. (1) Input (DC) side controller: the main responsibility of this controller is to extract or get the maximum available power details.
from the PV source by applying a maximum power point tracking (MPPT) algorithm [19]. (2) Grid (system) side controller: the system side controller must have the ability to perform many functions such as (a) grid synchronization, (b) control of reactive (Q) and active power (P), (c) control of DC-link voltage, and (d) injection of high-quality power [20,21]. In addition to these services, the grid operator may also demand intelligent services such as voltage regulation and harmonic compensation etc. [22].

In this article, the authors aim to provide a comprehensive review on PV systems. Different classifications of GCIs are discussed, and the comparative study of current and voltage source inverters are presented in a table form. Moreover, the features, advantages, and disadvantages of four different PV inverter configurations are discussed and presented. A basic circuitry and a detailed analysis of the most commonly used grid-connected multi-level inverter (GCMLI) topologies and their MTs are elaborated. Furthermore, different characteristics such as MT, switching frequency, and capacity, etc., of numerous related scientific articles on MLI topologies are presented in the table. A detailed analysis of two main types of modulation techniques and their subtypes is elaborated in detail. Later, different control structures and controller types that are applied to grid-connected inverters are thoroughly demonstrated. The important characteristics (reference frame, modulation technique, controller type, etc.) of different scientific articles are presented in table. The scope and trends of this research are broadly discussed later. The main contributions of the proposed review article are summarized and critically compared and associated with the other review papers already published in literature as shown in Table 1.

| Ref. | GS PV | PV CS | CI | IT | MT | CRF | CT | FS |
|------|-------|-------|----|----|----|-----|----|----|
| [23] | ✓     | ×     | ✓  | ✓  | ×  | ✓   | ×  | ✓  |
| [24] | ✓     | ×     | ×  | ✓  | ×  | ✓   | ×  | ×  |
| [25] | ×     | ×     | ×  | ✓  | ×  | ✓   | ×  | ×  |
| [26] | ✓     | ×     | ✓  | ✓  | ×  | ×   | ×  | ✓  |
| [27] | ✓     | ×     | ✓  | ✓  | ×  | ×   | ×  | ✓  |
| [19] | ×     | ×     | ×  | ✓  | ×  | ✓   | ×  | ×  |
| [28] | ×     | ✓     | ✓  | ×  | ×  | ✓   | ×  | ✓  |
| [29] | ×     | ×     | ×  | ✓  | ✓  | ×   | ×  | ×  |
| [30] | ×     | ×     | ×  | ✓  | ×  | ✓   | ×  | ×  |
| [31] | ×     | ✓     | ✓  | ×  | ✓  | ✓   | ×  | ×  |
| [32] | ×     | ✓     | ✓  | ✓  | ×  | ×   | ×  | ×  |
| [33] | ×     | ✓     | ✓  | ×  | ✓  | ×   | ×  | ×  |
| [34] | ✓     | ×     | ✓  | ✓  | ×  | ✓   | ×  | ×  |
| [OS] | ✓     | ✓     | ✓  | ✓  | ✓  | ✓   | ✓  | ✓  |

Abbreviations: GS PV: Global Status of PV, PV CS: PV Configuration System, CI: Classification of Inverter, IT: Inverter Topologies, CRF: Control Reference Frames, CT: Control Topologies, FS: Future Scope, and OS: Our Survey.

The remaining parts of the article are constructed as follows: Different classifications and configuration of GCIs are explained in Sections 2 and 3 respectively. Detailed analyses of grid-connected multi-level inverter (GCMLI) topologies under different descriptions are elaborated in Section 4. Various types of modulation techniques used to drive the switches are presented in Section 5. Various control reference frames used in 3-Φ GCPPPS are discussed in Section 6. In Section 7, the control strategies applied in different reference frames are presented. The scope of this research is carried out in Section 8. Lastly, a brief summary of this paper is concluded in Section 9.

2. Classification of Inverters

An inverter plays a very prominent role in grid-synchronization and is responsible for DC–AC inversion [35]. Inverters are generally categorized into line commutation inverters (LCI) and self commutation inverters (SCI) based on the commutation process (turned ON and turned OFF behavior).
A detailed taxonomy tree of the inverter classification is presented in Figure 3. A figure shows that SCIs are further divided into current source (CSI) and voltage source inverter (VSI). Moreover, VSIIs are further divided on the bases for their conduction mode (CM) into current CM (CCM) and voltage CM (VCM). The different classification of inverters is explained through a taxonomy tree in detail in this section [36].

![Figure 3. Classification of inverters [36].](image)

2.1. Line Commutated Inverter

Generally, in LCIs semi-controlled semiconductor devices such as thyristors are used as switches. In semi-controlled switches, the turn ON operation is controlled through the gate terminal whereas the turn OFF characteristics of the switches depends on the circuit parameters i.e., direction of current or voltage polarity. Therefore, in LCI a forced commutation is required to turn OFF the switches. For this purpose, different approaches are presented such as in case of half-bridge LCI an antiparallel diode is attached to enable the force commutation process (to turn OFF the switch) [37].

2.2. Self Commutated Inverter

A MOSFET or IGBT devices are usually used in SCI. MOSFETs are used for high frequency (20–800 kHz) applications having power ratings less than 20 kW. On the contrary, IGBTs are used for low frequency (20 kHz) applications having power ratings greater than 100 kW. The commutation operations of these switches are fully controlled through the gate terminal [38]. Therefore, it controls both the current and voltage output waveforms. High switching frequency devices are preferably used in grid-connected applications to reduce the inverter weight, filter size, and output waveform harmonics [39]. Moreover, SCI improves the grid power factor, suppresses the current harmonics, and shows high robustness to the grid disturbances. Due to the development of sophisticated switching devices and improvement in the control strategies, SCIs are preferably used as compared to LCI. The SCIs are further classified into current source inverter (CSI) and voltage source inverter (VSI).

2.2.1. Current Source Inverter

In CSI, a DC current source is connected as an input to the inverter; hence, the input current polarity remains the same. Therefore, the power flow direction is determined by the input DC voltage polarity. The current waveforms obtained at the output side of CSI are constant in amplitude but variable in width. The main disadvantage of using CSI is the utilization of a large inductor that is connected in series with the input side to handle the current stability issue [40]. The usage of an inductor makes the circuitry less efficient, bulky, and expensive [20].

2.2.2. Voltage Source Inverter

A DC voltage source is connected as an input to the VSI, hence the input voltage polarity remains the same. Therefore, the direction of input current determines the direction of power flow. The waveforms of an output AC voltage are constant in amplitude but variable in width. Moreover, a major drawback associated with VSI is the usage of a large capacitor that is connected in parallel with the input source [40]. The VSIIs are preferably used in grid-tied PV applications as compared to CSIs due to low power losses, high efficiency, low cost, and lightweight. Furthermore, based on their control mode VSIs are operated either in VCM or in CCM.
In VCM, an AC voltage is controlled and maintained at the point of common coupling (PCC). Whereas, in CCM a core control parameter of the controller is the line current and is regulated at PCC. The fault short circuit current in VCM is high as compared to CCM. Moreover, VCM is commonly used in those applications where maintaining the phase, frequency, and voltage at PCC are of major concerns such as off-grid or standalone PV systems. However, both CCM and VCM can be applied to the grid-tied PV VSIs, but the most preferable and commonly used method is CCM [36]. For grid-tied applications, about 81% of VSIs are operated in CCM while only 19% of VSIs are operated in VCM. The reason behind is that the VCM has no control over current while in CCM the current is the main control parameter. Therefore, in case of any grid disturbance, CCM can easily mitigate the current transients and harmonic distortion, and due to its current control structure, it can achieve a high power factor easily [41].

3. Configuration of PV Inverters

There are many types of PV array configuration in literature such as series, honeycomb, parallel, bridge linked, etc. [42]. Among them, the most commonly used configurations are the series or parallel and series connections. If the PV panels are attached in series with each other it is called a string, and if these are then connected parallel it forms an array. Basically, the PV modules are arranged in four types of configurations based on inverter type [43]. The design characteristics and main characteristics of these inverters are explained below.

3.1. Central Inverter

In this configuration system, to avoid the voltage amplification numerous panels are attached in series to make a string [44]. However, to increase the power level these strings are then attached in parallel to make an array. A complete diagram of the integration of series/parallel PV array with the grid through the central inverter is depicted in Figure 4a [45]. During shading (cloud cover) the PV output voltage are step-up by using a DC–DC boost converter and will be then fed to GCI. The most important drawback of this technology is the usage of a single MPPT for the whole system that causes panels mismatching; thus, the efficiency of the PV system decreases [43]. The other main drawback in this topology is that if the central inverter fails to operate, then the whole PV system will not be able to operate [46]. The central inverters have the lowest overall cost as compared to other configuration systems and are generally used for power ratings between 1–50 MW. Moreover, it shows a high robustness, require less maintenance, and have low AC power losses [2,20].

![Figure 4. Configuration of grid-connected PV inverters: (a) central; (b) string; (c) multi-string; and (d) AC modules [45].](image-url)
3.2. String Inverter

Currently, string inverter is the most frequently and commonly used technology and considered as a standard in GCPPPs [24]. In this configuration each string is connected independently to the inverter, thus it eliminates the usage of a string diode as presented in Figure 4b [45]. An individual MPPT is applied to every string therefore, partial shading and panels mismatching problems are greatly reduced in this configuration. Consequently, the overall system efficiency increases and is 1–3% higher as compared to the central inverter [47]. The application range of string configuration is up to 5 kW per string. Due to its modular structure, it can be expended to high ratings easily. In this topology, if the string inverter fails to operate it will only affect the operation of its related string rather than the whole PV system like in central configuration. String inverters have high flexibility, high reliability, low DC power and switching losses, and low cable cost. However, the overall cost of this configuration as high as compared to the central configuration due to high installation cost [2, 20].

3.3. Multi-String Inverter

It is a hybrid configuration, as it combines the beneficial and advantageous features of both string and central inverter configurations. Several strings are individually connected to the converter for voltage amplification (have a separate MPPT system) and are then connected to a centralized or single inverter as shown in Figure 4c [45]. This topology can integrate the PV strings of different orientation and different technologies to a grid. It has high structure modularity; therefore, it can be extended easily to high power ratings by connecting a new PV string to an already existing system [48]. The multi-string topologies are expensive as compared to central inverters but are cheap as compared to module integrated inverters. Multi-string configuration system covers a wide range of PV applications up to 50 kW [49]. However, due to its capability of integrating different ratings of PV strings causes a problem of high voltage variation at the inverter input side [2, 20].

3.4. Module Integrated or AC Module

An AC module presented in Figure 4d [45] has a low power rating, small in size, and is also known as micro-inverter [2]. AC modules are more suitable and preferably used in low power applications. In AC module, all the functions such as MPPT, voltage amplification, and inversion of DC–AC are performed in a single device called a module. These modules are separately connected at the back of every PV module through MPPT controller to eliminate the mismatch losses [50]. As modules have low power rating therefore high amplified voltage is required which causes a reduction in system’s efficiency. However, this shortcoming can be fully filled by using a highly efficient MPPT technique that makes it the most efficient topology as compared to other three topologies [51]. Due to its modular structure the enlargement can be made easily. As all the functions are carried out in a single module that makes this circuitry complex and requires high initial cost and maintenance.

A detailed comparative analysis of the performance evaluation of all four inverter configurations is made and tabulated in Table 2 [2, 20].
Table 2. Performance Evaluation of PV inverters [2,20].

| Performance  | Central | String | Multi-String | AC Module |
|--------------|---------|--------|--------------|-----------|
| Very High    | Variation of DC input voltage | ——     | ——           | Maintenance |
|              | Cables cost | Installation cost | ——           | Installation cost |
|              | Voltage balancing | ——     | ——           | MPPT efficiency |
|              | DC power loss | MPPT efficiency | ——           | Flexibility |
|              | Switching loss | Flexibility | ——           | Reliability |
|              | Panels mismatching | Reliability | ——           | |
|              | Robustness | ——     | ——           | |
| High         | ——     | ——     | Variation of DC input voltage | AC Cables cost |
|              | Installation cost | ——     | AC Power loss | |
|              | DC cables cost | ——     | ——           | Maintenance |
|              | DC voltage variation | ——     | ——           | MPPT efficiency |
|              | AC Power loss | ——     | ——           | Flexibility |
|              | Voltage balancing | ——     | ——           | Reliability |
|              | ——     | ——     | ——           | Robustness |
|              | ——     | ——     | DC and AC power loss | |
|              | ——     | ——     | Switching loss | Installation and cables cost |
|              | ——     | ——     | Panels mismatching | |
| Medium       | ——     | ——     | ——           | ——         |
|              | Installation cost | ——     | ——           | Maintenance |
|              | ——     | ——     | ——           | MPPT efficiency |
|              | ——     | ——     | ——           | Flexibility |
|              | ——     | ——     | ——           | Reliability |
|              | ——     | ——     | ——           | Robustness |
|              | ——     | ——     | DC Power loss | |
|              | ——     | ——     | Switching loss | |
|              | ——     | ——     | Panels mismatching | |
|              | ——     | ——     | ——           | |
| Low          | ——     | ——     | Voltage balancing | —— |
|              | ——     | ——     | ——           | Robustness |
|              | ——     | ——     | ——           | Cables cost |
|              | ——     | ——     | ——           | DC voltage variation |
|              | ——     | ——     | ——           | DC Power loss |
|              | ——     | ——     | ——           | Switching loss |
|              | ——     | ——     | ——           | Panels mismatching |
| Very low     | ——     | ——     | ——           | ——         |
|              | ——     | ——     | ——           | ——         |
|              | ——     | ——     | ——           | ——         |
| Power rating | 1–50 MW | 1–5 kW/string | 1–50 kW | 500–600 W |
| Cost         | Lowest cost | Costly than centralized inverter | Costly than centralized inverter | Highest cost |

The text in green shows the feasible characteristics, the text in red shows the disadvantage non-feasible characteristics, and text in blue shows the moderate characteristics.
4. Multi-Level Inverter Topologies

Due to rapid improvement and advancement in grid-connected inverter (GCI) topologies the overall cost of GCPPPs has decreased significantly. The MLI shows very efficient performance and offers many advantageous features for high and medium level grid-tied PV applications in comparison with 02 level inverter such as (a) as levels increase, the staircase in output waveforms also increase and a pure sinusoidal output is obtained; (b) generates low distorted input current; (c) has superior harmonic spectrum; (d) smaller common-mode voltage; (e) voltage change (dv/dt) is smaller in MLIs; (f) low switching losses; (g) has low filter requirement; and (h) can operate at low switching frequency [52].

A lot of research has been conducted on grid-connected MLI (GCMLI) and many topologies were introduced by researchers in the past. Therefore, based on power circuitry the GCMLIs are classified into VSI and CSI, these are then further classified into many subtypes as depicted in Figure 5. The VSIs are further classified into multilevel and 02-level inverter. The multilevel inverters are further divided into a single DC source (uses single DC source as input) and multiple DC sources GCMLIs (uses multiple identical or non-identical DC input sources). A single DC GCMLIs include flying capacitor (FC), neutral point clamped (NPC), active NPC, hybrid NPC, magnetic coupled, diode clamped with second capacitive divider, and full-bridge configuration with an ancillary circuit MLIs. While the multiple DC source MLIs include modular (M), assisted modular, dual voltage source, hybrid full-bridge, and cascaded H-Bridge (CHB) MLIs. Similarly, CSMLIs are divided into single DC source MLIs and multiple DC source MLIs. Among these MLIs the most commonly used topologies are NPC-GCMLI, FC-GCMLI, CHB-GCMLI, and M-GCMLI [29]. Therefore, in this section a basic configuration and related research work of these four GCMLIs will be discussed and will be presented schematically.

![Diagram](image_url)
4.1. Neutral Point Clamped GCMLI (NPC-GCMLI)

A three-level NPC for the first time was introduced by researchers in [53]. For generalized \( n \)-level, NPC topology uses \( 2(n-2) \), \( 2(n-1) \), and \( (n-1) \) number of clamping diodes, switches, and DC-link capacitors respectively as per phase [21]. In this topology, two conventional VSIs (2-level inverters) are stacked over one another. The positive point of lower inverter and negative point of upper inverter are accumulated mutually to make a new phase for the output. In this topology, every switch opposes the half of inverter’s voltage [54].

A basic circuit configuration of 03 level NPC is presented in Figure 6a, comprises of 02 clamping diodes (\( D_1 \) and \( D_2 \)), 04 switches (\( S_1, S_2, S_3, \) and \( S_4 \)), and 02 capacitors (\( C_1 \) and \( C_2 \)). This inverter can attain 03 voltage level (0, \(+V_{dc}/2\), and \(-V_{dc}/2\)) at the output. A 0 level is attained by turning ON \( S_2 \) and \( S_3 \), a value of \(+V_{dc}/2\) is accomplished in a case when \( S_2 \) and \( S_1 \) are in ON state, and a voltage level of \(-V_{dc}/2\) is attained by turning ON \( S_3 \) and \( S_4 \) [53]. Moreover, due to its modular structure, it can be expended easily for high power ratings. A detailed analysis of a 5-level NPC presented in [55] utilizes eight switches, 04 DC-link capacitors, and 06 free-wheeling diodes to achieve five voltage levels at the output. The capacitance requirement in this topology is low as it shares a common DC bus, makes it lightweight. However, the main disadvantage in NPC topology is that the complexity to balance the DC-link capacitor increases with the increment in the number of levels. Therefore, a proper DC-link voltage regulation is required to balance the DC-link. NPC is widely used in grid-connected applications due to fast dynamic response, small leakage current, simple structure, and high efficiency [56].

4.2. Flying Capacitor GCMLI (FC-GCMLI)

The FC-MLIs were first introduced by Foch and Maynerd in 1992 and are also known as clamping capacitor MLIs [57]. As compared to NPCMLI, the diodes are replaced with flying capacitors in FCMLI [25]. For a generalized \( n \)-levels, FC-MLI uses \((n-1)^*(n-2)/2\), \( 2(n-1) \), and \( (n-1) \) number of flying capacitors, switches, and DC-link capacitors respectively as per phase. A schematic circuitry of 3-level FC-GCMLI is presented in Figure 6b; 02 DC-link capacitors (\( C_1 \) and \( C_2 \)), utilizes 04 switches (\( S_1, S_2, S_3, \) and \( S_4 \)), and 01 auxiliary capacitor (\( C_0 \)) and can achieve 03 levels (0, \(+V_{dc}/2\), and \(-V_{dc}/2\)) at the output. A voltage level of \(+V_{dc}/2\) is attained when \( S_1 \) and \( S_2 \) are turned ON, and a \(-V_{dc}/2\) is accomplished by turned ON \( S_3 \) and \( S_4 \). While a 0 voltage level can be achieved when either \( S_2 \) and \( S_4 \) or \( S_1 \) and \( S_3 \) are turned ON [54]. As the researchers in [58], utilize 08 switches, 04 DC-link, and 06 auxiliary capacitors to attain the 05 voltage levels at output. However, this topology has high installation cost and has low efficiency due to high switching losses. Just like NPC-GCMLI, this topology also has a high modularity in structure and can be expended easily.

4.3. Cascaded H-Bridge GCMLI (CHB-GCMLI)

A CHB-GCMLI is formed by connecting 2 or more 1-\( \Phi \) H-bridge inverters having separate DC sources are connected in series to increase the voltage levels. For generalized \( n \)-levels, this topology utilizes \( 2(n-1) \) and \( (n-1)/2 \) switches and DC sources respectively as per phase [59]. The output voltage for \( n \)-level is \( n = 2s + 1 \), where \( s \) presents the input DC voltage sources count [60]. Each 1- \( \Phi \) H-bridge can generate 03 levels (0, \(+V_{dc}/2\), and \(-V_{dc}/2\)). \(+V_{dc}\) and \(-V_{dc}\) voltage levels are accomplished by turning ON \( S_1 \) and \( S_4 \), and \( S_2 \) and \( S_3 \), respectively. However, the voltage at the output port of the inverter is achieved by turning ON either \( S_3 \) and \( S_4 \) or \( S_1 \) and \( S_2 \) respectively. Furthermore, a 05 level CHB-GCMLI is formed by connecting two 1-\( \Phi \) H-bridge modules in a series manner as presented in Figure 6c. As 05 level CHB topology is the combination of series connected 02 H-bridges; therefore, the inverter output will be the summation of individual H-bridge output i.e., \( V_{out} = V_{s1}+V_{s2} \). Due to its scalable feature and high structure modularity, it can easily be expended to accomplish high voltage levels just by connecting a 1-\( \Phi \) H-bridge module in series. Moreover, CHB topology is compact as compared to NPC and FC due to the absence of clamping diodes and capacitors [59]. However, due to
usage of an individual DC source for every 1-Φ H-bridge this inverter faces the problem of voltage misbalancing among different phases.

Based on the nature of input sources, the CHB-GCMLIs are further categorized into symmetric and asymmetric topologies [61]. The topology is said to be symmetrical if the input voltage sources have the same magnitude. If the input DC voltage sources have different magnitudes then it is said to be an asymmetrical topology. The asymmetrical topologies are further classified into binary and trinary (voltage in a ratio of 2 and 3, respectively). The binary asymmetric CHB-GCMLIs are selected in the ratio of $2^0 V_{dc}, 2^1 V_{dc}, \ldots, 2^{n-1} V_{dc}$ [62], whereas the trinary asymmetric topologies are selected in the ratio of $3^0 V_{dc}, 3^1 V_{dc}, \ldots, 3^{n-1} V_{dc}$ [63]. The number of 1-Φ modules required for the generalized m-level binary CHB-GCMLI are $(m+8)/9$, while trinary CHB-GCMLI required $(m/9+3)/2$. The input sources are arranged in a trinary manner to achieve 09 level voltages in a topology proposed in [11]. It uses 02 H-bridges, and among them, one of the bridges is being fed into the FC inverter as presented in Figure 6d.

### 4.4. Modular GCMLI (M-GCMLI)

M-GCMLI is a scalable technology, where the number of sub-modules (SM) used in a topology is determined by the acquired output voltage level. It is formed by connecting several SMs (with a separate control system for every SM) in a cascaded manner. Due to the usage of a separate controller for every SM, very small harmonic contents are generated [64]. The features such as high quality output waveforms with low THD, high structure modularity, low component count, and compact size make this topology very feasible for high voltage applications. Moreover, with the increment in the levels, the switches count does not increase. A circuit configuration of a 3-Φ M-GCMLI presented in Figure 6e, have upper and lower arms connected in a series among the 2 DC terminals. Each arm contains many series connected SMs, and every individual SM is composed of 02 switches ($S_1$ and $S_2$), 01 DC capacitor (C), and 02 reverse diodes. Both the switches of SM cannot be operated at the same time i.e., when $S_1$ is turned ON $S_2$ must be turned OFF and vice versa. Hence, the operation of the SM can be defined for two operation modes. The first operating mode also known as the interleaved state is achieved by turning ON $S_1$ and turning OFF $S_2$. In the second operating mode, when $S_1$ is turned OFF and $S_2$ is turned ON, the SM is said to be in a bypassed state. Under usual operating situations, the voltage at the terminal of SM can either be 0 or equal to capacitor voltage [65]. Moreover, the fluctuation in the capacitor voltage and inter-phase current circulation will occur in SM if the DC voltage is unstable. Therefore, to make sure the DC voltage stability the arm of the lower bridge is required to be disconnect every time when SM gives an input at the upper arm and vice versa [66].

The pros and cons of these four MLIs are described in Table 3. From the above discussion, it is concluded that NPC-GCMLI, FC-GCMLI, and CHB-GCMLI are very suitable for small scale PV applications due to its simplicity and low THD. However, M-GCMLI is feasible for high voltage PV applications. The M-GCMLI is also modeled in combination with other inverter topologies such as NPC, FC, CHB, that further boost the performance of M-MC. Moreover, a detailed literature review of different scientific research articles related to different MLIs topologies used for grid integration is tabulated in Table 4. Different features of these various inverters such as the number of levels, number of phases, modulation technique, controller type, switching frequency, and their capacity are presented. The capacities of experimental prototypes of these existing GCMLIs are usually small and the auxiliary functionalities as discussed in the introduction part are still not perfect and require more exploration. Moreover, all the inverters presented have their own advantages and disadvantages. Therefore, it is very difficult to judge which inverter is better than the other. However, there are several key points that should be kept in mind while selecting an inverter for grid-connected PV applications. These are
• **Auxiliary Functionalities:** The inverter must have the ability to provide the auxiliary functionalities when demanded from the grid operator. Moreover, the voltage compensation mostly focused on voltage interruption, swell, and sag. While the current compensation mostly focused on active and reactive components. However, unbalance and harmonic compensation require further research.

• **Efficiency:** The selection of a grid-connected PV inverter is mainly based on its efficiency. The inverter must be capable to attain a high efficiency over a wide range of loads. Due to the technological advancement in the last few decades, the power losses of the inverter are greatly reduced, and high efficiency is achieved.

• **Anti-Islanding Detection:** A GCPVI must have the capability to detect the islanding situation and disconnect it from the grid for safety purposes, while supplying power to the local load. In these conditions, the function of the inverter is usually referred to as anti-islanding.

• **Cost:** The selection of an inverter mainly depends on the manufacturing and installation cost. There is a tradeoff between the manufacturing cost and the performance and power quality of the inverter. On the contrary, the installation cost mainly depends on land acquisition, labor, and local factors that vary from region to region.

• **Leakage Current:** In transformer-based inverters the leakage current is interrupted by the galvanic isolation. However, in transformer-less MLIs the leakage current is a major issue as it increases the losses, harmonics in the grid injected current, and electromagnetic interference. Therefore, for a grid-connected system those MLIs are needed to be selected that are capable of reducing the leakage current according to the international regulations.

• **Power Density and Capacity:** Generally, most of the experimental prototypes of GCMLIs are of low power density and capacity. Therefore, high power rated prototypes should be focused and enabled their integration with medium and high voltage grid connection.

• **DC-Link Capacitor:** The DC-link capacitor plays an important role in supplying the AC component of input current the inverter. The control and design of the DC-link capacitor is not an easy task and become more complex if their number rises.

• **Switching Frequency:** The switching frequency of small capacity GCMLIs is usually higher as compared to the large capacity inverters.

• **Semiconductor Devices:** The cost of GCPVIs mainly depends on the number and power ratings of the switches. Therefore, those topologies should be focused that have less number of switches with low voltage ratings.

• **Galvanic Isolation:** It is one of the most important requirements for safety purpose. In transformer-based inverter the galvanic isolation is provided by the transformer. However, in transformer-less inverter topologies, the isolation is achieved by using switches. Hence, the inverter should be selected according to the requirement of galvanic isolation.
### Table 3. Advantages and disadvantages of GCMLI.

| Type of GCMLI | Pros | Cons |
|---------------|------|------|
| NPC-GCMLI     | Simple design  
                 Fast dynamic response  
                 Low voltage rating switches are needed  
                 High efficiency  
                 During power outage it has the capability to provide an extra ride through facility  
                 Phase redundant | As level increases the clamping diode count increases  
                 As level increases the complexity to balance the DC-link increases  
                 DC-link voltage regulation is required |
| FC-GCMLI      | Low component count  
                 Low stress on components  
                 Low THD and have high modularity  
                 Provide modular solution to achieve high voltage level | As level increases the capacitor count increases  
                 As level increases the control system become more complicated  
                 High installation cost  
                 Less efficient due to low switching efficiency |
| CHB-GCMLI     | Good fault tolerance  
                 Highly reliable  
                 Suitable for all voltage levels  
                 High modularity  
                 Low component count | The inverter faces the problem of voltage misbalancing among the different phases  
                 Separate DC sources are used  
                 High thermal losses  
                 High conduction losses  
                 High voltage ripples through SMs capacitors  
                 Current flows within inverter  
                 Large quantity of DC voltage sources (isolated) are required |
| M-GCMLI       | As the level increase the power switches count not increases  
                 Simpler structure  
                 Low THD and have compact size | |

**Abbreviations:** THD: Total Harmonic Distortion; SM: Sub-modules; M-GCMLI: Modular Grid-Connected Multilevel Inverter.
Table 4. Analysis of different grid-connected multilevel inverters.

| Ref. | MLI Topology            | NOL | NOP | MT          | C     | SF (kHz) | CP (kW) |
|------|-------------------------|-----|-----|-------------|-------|----------|---------|
| [67] | CHB                     | 05  | 3-Φ | SV-PWM     | PI    | 10       | —       |
| [68] | M                       | 7   | 3-Φ | MC-PWM     | PI    | 10       | 0.4     |
| [69] | Reduced switch          | 7   | 1-Φ | MC-PWM     | —     | —        | —       |
| [70] | E-Type                  | 7   | 3-Φ | PWM        | —     | 20       | 4       |
| [71] | CHB                     | 13  | 1-Φ | PWM        | —     | 5        | —       |
| [72] | Three phase             | 5   | 3-Φ | MC-PWM     | —     | 20       | 1       |
| [73] | Diode Clamped           | 5   | 1-Φ | PWM        | —     | —        | —       |
| [74] | symmetrical             | 7   | 3-Φ | PWM        | —     | —        | —       |
| [75] | Hybrid                  | 5   | 3-Φ | PWM        | Finite Control Set-MPC | 6 | 7.5 |
| [76] | NPC Back to Back        | —   | 3-Φ | PWM        | MPC   | 10       | 0.28    |
| [77] | CHB                     | 5   | 1-Φ | LS-PWM     | FO-PID| 2        | —       |
| [78] | CHB                     | 7, 15 | 1-Φ | MC-PWM     | —     | —        | —       |
| [79] | CHB with T type         | m   | 3-Φ | PS-PWM     | PI    | 3        | 1       |
| [80] | Modular                 | m   | 3-Φ | LS-PWM     | PR    | 1        | —       |
| [81] | CHB                     | 7, 9 | 1-Φ | LS-PWM     | CPT   | 12       | 2       |
| [82] | Cascaded Full-bridge with FC | 9  | 1-Φ | PWM        | Hysteresis | 20  | —       |
| [83] | Asymmetrical Cascaded   | 17  | 1-Φ | SHE-PWM    | —     | —        | —       |
| [84] | Quasi Z-Source Based NPC | 5  | 1-Φ | LS-PWM     | PI    | 10       | 0.5     |
| [85] | Modified DC link        | 7   | 1-Φ | MC-PWM     | —     | 6        | —       |
| [86] | NPC                     | 3   | 3-Φ | SV-PWM     | —     | 2        | 1.1     |

Abbreviations: MLI Topology: Multilevel Topology; NOL: Number of Levels, NOP: Number of Phases, MT: Modulation Technique, C: Controller, SF: Switching Frequency, CP: Capacity, SV: Space Vector, LS: Level Shift, PS: Phase Shift, CPT: Continuous Power Theory, MC: Multi-carrier, and SHE: Selective Harmonic Elimination.
Figure 6. Power circuitry of grid-connected multi-level inverter (GCMLIs): (a) 3-level neutral point clamped (NPC) [53]; (b) 3-level flying capacitor (FC) [54]; (c) 3-level cascaded H-Bridge (CHB) [59]; (d) 9-level CHB with FC [11]; and (e) 3-Φ modular topology [65].

5. Modulation Techniques for Multi-Level Inverters

The operating sequence and the step duration of the switches used in MLIs must be controlled properly as it directly affects the system efficiency [87]. For this reason, various modulation techniques were introduced by researchers that will be discussed in detail in this section. The main task of MTs is to control the current and voltage while playing a prominent role in minimizing THD and switching losses. Based on switching frequency the MTs are mainly categorized as FSF and HSF that are further subdivided into many types as presented in the taxonomy tree in Figure 7.
5.1. High Switching Frequency (HSF)

The gating signals generated through this technique have multiple commutations in one cycle and these cycles either or not be identical with each other [88]. The high switching frequency MT is divided into pulse width modulation (PWM) and space vector modulation (SVM). These are described below.

5.1.1. PWM

The most popular and commonly used MT is PWM, where the gating signals are generated by comparing the sinusoidal reference waveform \(V_r\) with the carrier waveform \(V_c\). These signals are then fed to the gate of the switches to drive them. The behavior of PWM depends on two components, these are frequency and duty cycle [89]. Moreover, to generate gating signals 02 approaches, i.e., uni-polar and bi-polar approaches are used. To generate 03 voltage levels by using a uni-polar approach, two \(V_r\) signals having opposite phases are compared with \(V_c\). While in bipolar, one \(V_r\) is compared with \(V_c\) to generate 3-levels voltage in a 2-level inverter [90]. Recently, numerous research work is done on PWM schemes and are applied on different GCMLIs for different purposes, such as in 3-level NPC, a PWM scheme is applied to overcome the switching and conduction losses [91]. While a modified PWM scheme is proposed for reduced NPC to increase the level count, improve the output waveforms, and to reduce the inverter cost [92]. A PWM scheme is used to eliminate the harmonic contents for high and low modulation index areas in FC topology [93]. A PWM scheme applied in CHB topology for improving the supply line quality index [94]. Moreover, it is applied in M-MLI to enhance the power factor, reduces the harmonic content and voltage stress on switches, and ensures the fast dynamic response [95]. The PWM techniques are classified into two main types, named as carrier based and reference based PWM.

Carrier-Based PWM (MCB)

This technique is applied in GCIs to increase its performance. The MC-PWM schemes are classified into three types, these are phase shift carriers PWM (PSC-PWM), level shift PWM (LS-PWM), and hybrid...
PWM (H-PWM). In PSC-PWM, \( n - 1 \) carriers of same frequency and amplitude but shifted phase angles are placed in consecutive horizontal bands. However, in LS-PWM, \( n - 1 \) carriers are placed in adjoined vertical bands [96]. The LS-PWM method is further divided into constant and variable frequency methods. Variable amplitude [97], phase disposition [90], carrier overlapping [15], phase opposition and disposition (POD) [98], and alternative POD [88] are the five kinds of constant frequency MT. At last, the H-PWM combines the advantageous features of both LS-PWM and PSC-PWM techniques.

Reference-Based PWM

In the reference based (RB) PWM scheme, the reference signal waveform \( (V_r) \) is constantly compared with \( V_c \). The pulse will be generated only if \( V_r \) is above the \( V_c \); as a result the corresponding power switch will be turned ON. However, when \( V_r \) is below the \( V_c \); then no pulse will be generated, and the switch remained in turned OFF condition [79]. Depending on the structure of MLI, \( V_r \) can either be uni-polar or bipolar [97]. The RB-PWM methods are divided into seven different types, named as (a) trapezoidal PWM, (b) sinusoidal PWM (SPWM), (c) staircase modulation, (d) 60° PWM, (e) hybrid reference, (f) third harmonic injection (THI), and (g) discontinuous reference.

A trapezoidal reference is used to increase the RMS value of voltage and is formed by putting some constraint to limit the magnitude of the triangular waveform. The authors in [99], uses a methodology in which numerous trapezoidal waveforms are compared with a triangular carrier to create the switching pulses. However, if \( V_c \) is compared with \( V_r \) then this technique is said to be an SPWM [100]. In the staircase technique, the pulses are generated by choosing the step count according to the number of levels required in output waveforms. The selection of a suitable modulation frequency also plays an important role in this technique. However, this method is not recommended to use if the number of pulses in one cycle exceeds 15 [101]. In 60° PWM technique, the top of the pulses are made flat from 60° to 120° in positive and from 240° to 300° in negative half cycles, respectively [102]. This method eliminates the triple harmonics 3-\( \Phi \) output waveforms and reduces the switching losses. In a hybrid method, two reference signals are combined to make a hybrid reference signal and are used in such a manner that one reference signal is used in the primary half-cycle and the other is used in the second half-cycle. When the selected harmonics are injected to \( V_r \), then the THI reference is formed [103]. The discontinuous reference signals are utilized to adjust the voltage offset and to minimize the switching losses [104].

5.1.2. SVM

It is a digital modulating technique [105] and was first introduced in 1964, where the output waveforms are obtained by comparing the vector control signals with the reference waveform [106]. A plan in which SVM works is divided into 06 different sectors separated from each other on the bases of commutation behavior. The SVM uses a control algorithm to regulate and control the output voltages according to the requirements in any switching state [107]. An extensive amount of research work has been conducted on this technique such as; an improved SVM technique is applied to 5-level NPC-MLI to decrease the switching losses [108]. In \( n \)-level FC-MLI, the SVM technique is used to choose the appropriate switching states to balance and control the capacitor voltages [109]. In CHB-MLI, the SVM technique is applied to modulate the appropriate switching state selection in order to balance a DC-link [110]. A dual SVM method used for controlling the M-MLI with FC-MLI has been proposed in [111], the main task of this strategy is to balance the capacitor voltage.

5.2. Fundamental Switching Frequency (FSF)

FSF has one or more commutations per cycle [88] and is categorized in four main types; these are discussed below in detail.
5.2.1. Selective Harmonic Elimination (SHE)

A SHE method was first developed in 1964 and is also named as harmonic elimination method [112]. Its operating methodology is based on the development of a Fourier series for voltage waveform and the switching angles are used to remove the low order harmonic contents within the permissible limits. It can be applied either ONLINE or OFFLINE to the inverter, and is used to remove the specific low order harmonics, torque pulsation, and to minimize the switching losses [113]. A SHE method is widely used in high rated power electronics inverters and rectifiers to improve the output waveforms. However, it is not recommended to use it in inverters having high voltage levels, as an increment in voltage levels causes an increment in the number of equations. Recently, many intelligent algorithms such as bee algorithm (BA), genetic algorithm, and particle swarm optimization (PSO) etc., are combined with SHE techniques to enhance the output waveforms. A combination of BA and SHE is applied to 7-level CHB to enhance the harmonic profile [114]. Similarly, PSO is used in asymmetric CHB-MLI for the linearity of the switching angle and controlling the THD [115]. As compared to other MTs, SHE technique offers a high quality output waveforms and an efficient control over the harmonics.

5.2.2. Switching Angle Calculation (SAC)

SAC technique plays a prominent role in harmonics reduction and improving the quality of output waveforms. If the value of \( \alpha \) (\( \alpha \) is described as a moment in which a transition in voltage level occurs) is not selected properly, it can cause the quality issues in output waveforms of the inverter. Therefore, to obtain the desired smooth waveforms at the output, \( \alpha \) must be calculated perfectly with no error [116]. Usually, number of main switching angles required for \( n \)-level inverter is \( (n - 1)/2 \). The switching angles in the second quadrant (90°–180°) can be calculated as \( (\pi - \alpha_1) \). The switching angles in the third (180°–270°) and fourth (270°–360°) quadrants can be calculated as \( (\pi + \alpha (n - 1)/2) \) and \( (2\pi - \alpha_1) \), respectively [117]. The SAC is further classified into feed forward, half equal phase, equal phase, and half height method. The comparative analysis of these four methods for SAC is described in Table 5 [116]. Among these, the feed forward MT is highly recommended for RE applications especially for PV, as it can be applied to any voltage level due to the wide spectrum nature of \( \alpha \) and produce the output waveforms having very low THD.

| \( \alpha \) Calculation Methods | \( \alpha \), for \( i = 1, 2, \ldots \), \( (n - 1)/2 \) | THD in Output Voltage | Nature of \( \alpha \) | Remarks |
|---------------------------------|---------------------------------|----------------------|----------------|--------|
| Feed Forward                    | \( \sin^{-1}(i - 0.5)/n) \)     | Small                | High           | Feasible for any voltage level |
| Half Equal Phase                | \( 180°/(n + 1) \)              | High                 | Low            | Feasible for low voltage level |
| Equal Phase                     | \( 180°/n \)                    | High                 | Very Low       | Feasible for low voltage level |
| Half Height                     | \( \sin^{-1}(2i - 1)/(n - 1)) \) | Medium               | Moderate       | Feasible for medium and low voltage levels |

5.2.3. Space Vector Control (SVC)

The other name for SVC is the nearest vector control (NVC) and its main objective is to find the vector that is nearest or closest to the reference to reduce the distance or space error among them [118]. As SVC method is operated at low switching frequency therefore this technique has lack of capability of eliminating the low order harmonics just like in SHE method. SVC method is highly suitable and preferable to use for high voltage level MLIs. As the voltage level increases the vector density increases proportionally. Higher the vectors density the lesser will be the possibility of generating errors. Hence, causes a reduction in THD and ripples in the output waveforms. On the contrary, if the number of MLI voltage level decreases the errors increases causes an increment in THD and ripples [119]. A space vector control is applied to three levels NPC-multilevel inverter to regulate and balance the DC-bus
voltage [120]. The SVC method is utilized to enhance the quality of waveforms of cascaded MLI that is used to drive the induction motor [121].

5.2.4. Nearest Level Control (NLC)

NLC is a non-carrier method and is also called a round modulation technique. In NLC method, a sinusoidal reference is compared with the inverter output voltage to generate/select the nearest voltage level. A major dissimilarity between the NVC and NLC is the selection of the closest level rather than the vector and is simple to find the nearest level rather than the vector. NLC method is utilized to generate a better quality of voltage waveforms and reduces the ripples in the output/load current [122]. This technique directly computes and calculates the duty cycle and switching states for every inverter phase. Therefore, it is highly favorable for high power inverters, particularly for MLIs with a high count of levels. Moreover, by using NLC technique the count of switching events for high voltage levels is reduced as compared to PWM based techniques [123].

6. Controllers Reference Frames

In grid-tied PV systems, inverter plays a prominent role in energy harvesting and integration of grid-friendly power systems. The reliability, performance, efficiency, and cost-effectiveness of inverters are of main concern in the system design and mainly depend on the applied control strategy. The control strategy used for the grid-tied inverter is classified into a single loop, double loop, and triple loop systems.

A single loop control system is applied when only one variable (current or voltage) is required to be regulated and measured. The structure of a single loop is presented in Figure 8a, where $H_S$ presents the applied regulator. In case of current regulation, it provides good power flow regulation and harmonic rejection. However, a single sensor is used to protect the inverter from over-current [124]. In case of voltage regulation this control structure does not offer any protection from the short circuit or resonance damping; therefore, an additional prerequisite is needed to improve the system reliability and stability [125].

![Figure 8](image-url)

**Figure 8.** Controller structure: (a) single loop with $H_S$ regulator; (b) double loop with $H_D1$ and $H_D2$ are the outer and inner loop regulators respectively; and (c) cascaded pattern of triple-loop.
A double loop structure composed of two loops that are cascaded over one another and are used to regulate two variables. The structure of a double loop is presented in Figure 8b, where $H_{D1}$ and $H_{D2}$ present the outer and inner regulators respectively. An $H_{D2}$ is a fast internal loop that controls the grid injected current. The issues like protection of devices from the current and power quality enhancement are related to the current loop. The $H_{D1}$ is a slow external voltage loop that regulates the voltage at the DC-link. The power flow balancing and optimal regulation issues are generally associated with the DC-link external voltage controller [20]. The transfer functions of both loops (outer and inner) are independent from each other; therefore, both the loops can be designed in a decoupled manner. However, for stability purpose, the dynamic speed of an outer loop must be 5–20 times slower than the inner loop [126]. Instead of the cascade of current and voltage control loops, the cascade of power and voltage loops can also be used, and the grid injected current is controlled indirectly.

A triple loop control is the most modern structure presented in the literature [127,128] and is implemented in a cascaded manner as presented in Figure 8c, where $H_{T1}$, $H_{T2}$, and $H_{T3}$ are the applied regulators. The implementation and analysis of this structure is more complex than the single or double structures, as every loop bandwidth is limited by the response delay of the inner loop. Therefore, it is very difficult to attain width bandwidths for the most outer loop. Among the control loop structures, a triple loop structure provides more control flexibility and makes it more beneficial for the high performance of the grid-connected inverters.

The above discussed control loops are applied to the grid-tied inverter by using different reference frames. Therefore, for controlling the grid-tied inverter three reference frames ($dq$, $a\beta$, and $abc$) are used, that are discussed below.

### 6.1. dq Reference Frame

In this reference frame, the current and voltage in $abc$ frame are converted into synchronous current components ($I_d$ and $I_q$) and voltage components ($V_d$ and $V_q$) into $dq$ frame using a Park transformation. It converts the grid voltage and current into a reference system in which they revolve continuously with the grid voltage. By using this approach, the control variables are converted from the sinusoidal domain are transformed into DC domain which can easily be controlled and filtered [129]. In the last few years, numerous controllers are applied in a single loop structure such as proportional-integral (PI) [130], proportional (P) [131], dead-beat (DB) [127], proportional-resonant (PR) [132], in which the PR shows a prominent performance. PI is usually used in $dq$ reference frame in GCPPP's due to its simple configuration, uncomplicated control, and easy filtering. A generalized configuration of proportional integral (PI) applied in $dq$ reference frame to GCPV is presented in Figure 9a [133]. The current components in a $dq$ reference frame ($I_d$ and $I_q$) are then compared with the reference current components ($I_{dref}$ and $I_{qref}$). The error generated from the comparison is regulated by the PI regulator and the signal is feed to the PWM modulator to drive the switches of the inverter.

### 6.2. abc Reference Frame

An $abc$ reference frame is applied to 3-Φ systems without any transformation and for each grid current a separate controller is utilized, but the delta or star connections must be in consideration while designing a controller [22]. Numerous regulators are applied in double loop structures such as P-proportional resonant (PR) [134], P-PI [135], PI-PR [136], deadbeat (DB)-PI [137], and hysteresis current control (HCC)-PR [138]. Due to fast dynamic response, simple transfer function, lack of requirement for the modulator, and fast development the controller such as deadbeat and hysteresis are preferably used in $abc$ reference frame. On the contrary, if linear controllers such as PI and PR are used, then a modulator must be used so that the modulator creates the duty cycles for modulation purposes [24]. Moreover, the PI transfer function in $abc$ frame becomes more complex and causes an increment in the overall system complexity. The transfer function of PR is simple as compared to PI controller but more complex than the deadbeat and hysteresis controller. A generalized configuration of a current controller applied in a double loop structure is presented in Figure 9b [20]. In the outer
loop, PI regulator is used to regulate the DC-link voltage and generate a d component of reference current and is then transformed from dq reference frame to abc reference frame. In the inner loop a current controller such as deadbeat, sliding mode control (SMC), hysteresis, etc., are used to generate the switching pattern according to the requirement.

Figure 9. Generalized reference frame configuration of (a) dq, (b) abc, and (c) αβ.

6.3. αβ Reference Frame

In this reference frame, the current (I_a, I_b, and I_c) and voltage (V_a, V_b, and V_c) are converted into current (I_α and I_β) and voltage (V_α and V_β) in αβ frame by using a Clark transformation, respectively. It is used in both 3-Φ systems and sometimes in 1-Φ systems. In recent years numerous triple loop control strategies are developed that are applied in different reference frames such as DB-DB-PI [139], DB-proportional integral derivative(PID)-repetitive filter [140], and hysteresis
controllers (HC)-PI-P [141]. A generalized configuration of a triple loop proportional resonant (PR) control strategy applied in a cascaded manner in αβ reference frame is presented in Figure 9c [142]. Three PR controllers are applied in a cascaded manner to measure and regulate the grid injected current, capacitor voltage of an inductive capacitive inductive (LCL) filter, and current of the primary inductor of LCL filter. The control variables are converted into two sinusoidal quantities, which eliminate the steady-state errors and achieve a high gain around resonance frequency ($f_r$). Therefore, as compared to PI, PR controllers have gained more popularity due to the elimination of steady-state error and fast dynamic response, and they have been reported in different literature that they are related to the current control of power system [143]. However, the hardware implementation of PR in αβ frame is complex and the power factor is also not fully controlled.

7. Control Strategies for Grid-Connected PV Systems

A PV system is a power-electronics based system; therefore, their control plays a very prominent functionality in the smooth and stable operation of the power system. If a robust and suitable controller is not designed for the inverter then it causes grid instability and disturbances. Based on grid behavior and operating conditions, the controllers are divided into linear, predictive, robust, non-linear, adaptive, and intelligent controllers as shown in Figure 10 [144]. A detailed analysis of these controllers and their subtypes are discussed and presented schematically.

7.1. Linear Controllers

These controllers are designed on the foundation of the dynamics and features of the linear systems. A concept of classical feedback control is used while designing these types of controllers. They are further divided into three types and are described below.

7.1.1. Classic Controllers

The family of classic controllers includes P, PI, PID, and PD controllers. Moreover, these controllers are considered as the foundation of a linear system. Among all the controller types, these controllers

![Figure 10. Different types of control strategies](image-url)
are more frequently and commonly used in GCPPP and in many other commercial and industrial applications due to its easy implementation, realization, and simple structure.

7.1.2. Proportional Resonant (PR) Controllers

The popularity of PR controllers has increased over the last few years in grid-tied PV systems. PI and PR controllers have very much in common but there are two main differences between them. The first one is that the PI and PR controllers are operating in different reference frames. A PI controller efficiently tracks the DC signals in dq reference frame, while a PR controller allows the tracking of a sinusoidal signal in αβ reference frame. Whereas, the second difference is that the integration part in PR controller is different from PI controller. In PR controller, only those frequencies are integrated that are close to the resonant frequency. As a result, no phase shift and stationary magnitude errors are involved [145]. A generalized control structure of PR is presented in Figure 11a.

7.1.3. Linear Quadratic Gaussian (LQG) Controllers

LQG controller is formed by the combination of Kalman filter and LQ regulator. An LQG controller presented in Figure 11b shows that the controllers are designed and computed separately, according to the separation principle. An LQG controller performs its operation and functionality very smoothly in both time-variant and invariant systems [146].

7.2. Predictive Controllers (PC)

A system model used by PC predicts the behavior of the parameters in the future that are needed to be controlled and is well known for its ability to handle the non-linearities in the system. Due to fast dynamic response, PC has the capability of controlling the current at low noise and low harmonic distortion. As compared to classic controllers, PC is difficult in implementation, requires huge calculations, and should be matched with the accurate load [147]. A block presentation of PC is shown in Figure 11c, where for every switching state the system characteristics are predicted by grid current i(k) and switching states s(k).

7.2.1. Deadbeat Controllers

The first type in the family of PC is the deadbeat controller and is used in numerous modern applications. Moreover, a well-tuned deadbeat controller has a faster dynamic response as compared to other digital controllers. It has one sample delay, which consequently regulates the current in such a manner that, at the end of the next switching cycle, it achieves its reference. Therefore, for the compensation of the one sample delay, the researchers in [148] have applied an observer to the deadbeat controller structure as presented in Figure 11d [22]. A triple loop DB-DB-PI control structure applied to the inverter shows very good reference tracking ability with minimum delay [139]. Moreover, due to the usage of two DB controllers, it can easily handle the parameter mismatching problem.

7.2.2. Model Predictive Controller (MPC)

In MPC, the flexible measures are used and taken to define a cost function, which is intended to be reduced to choose the most favorable actions. By using this approach, a system model is developed to predict the performance of variables in a specified time. A generalized configuration of MPC is presented in Figure 11e [149]. A finite control set (FCS) MPC proposed in [150] is designed for the LCL filtered grid-connected inverter. High quality current waveforms are achieved, but it is very expensive and complex due to the requirement of a high number of sensors to measure the voltage (grid and capacitor) and current (inverter side and grid-injected). However, the FCS-MPC controllers that are proposed in [151,152] are applied to 02-level inverters have a simple implementation, having the capability to handle the constraints and non-linearities very easily, and have a fast dynamic response.
7.3. Robust Controllers

Robust controllers are designed on the basis of a control theory that is related to uncertainties of the system. The end goal of robust controllers is to achieve stability and robust performance even in the occurrence of incomplete modeling errors. This controller guarantees the stable performance of the close loop, in both single and multi-variable systems. A control configuration of the robust control scheme is sketched and presented in Figure 11f [153].

7.3.1. Mu-Synthesis Controllers

This approach is used to consider the consequences of uncertainties (unstructured and structured) on the system performance. In this approach, the concept of a controller design is dependent on a singular value that may be either a structured or an un-structured valve. The authors in [154] designed a \( \mu \)-synthesis controller for 3-\( \Phi \) grid-tied inverters and explain its importance in different power-related applications. However, this controller is not feasible for grid-connected applications due to unbalanced load conditions and has high voltage sags. This problem is tackled by the authors in [155] and proposed a \( \mu \)-synthesis controller. This controller is applied in a \( dq \) frame to the 3-\( \Phi \) inverter to control the active and reactive power. It is capable of handling the time-varying and unknown loads and show very flexible performance to the uncertainties. Moreover, this controller has a low computational burden as it is designed offline. A \( \mu \)-synthesis controller proposed in [156] is used to improve the performance of the secondary frequency in an islanding mode. This controller is highly flexible to uncertainties and controls the synthesis process. The numerical perturbations are collected into a single block as structured uncertainties.

7.3.2. H-Infinity Controllers

In this method, a solution to a control problem is only possible when a controller designer presents it in the form of an optimized problem. Moreover, the H-infinity method can solve the multi-variable system problems and have high computational complexity. The authors in [157] proposed a mixed approach of \( H^\infty \) and repetitive controllers to regulate the current of the grid-tied VSIs. Different responses such as steady-state response without local loads, non-linear local loads, and unbalanced resistive loads as well as the dynamic response without loads are also studied and investigated. This approach performs very well in terms of suppression of THD, but the main drawback of this approach is its slow dynamic response. An \( H^\infty \) controller designed for renewable integration has the potential to attain small tracking errors and have low THD in the grid injected current [158]. To improve the power quality and exchange of grid current the authors in [159] proposed an \( H^\infty \) repetitive control. It enables the inverter to inject the high-quality current into the grid, even in unbalanced or non-linear local loads. Moreover, this controller also has the capability to switch the inverter operation from grid-connected to stand-alone and vice versa.

7.4. Non-Linear Controllers

The non-linear controllers have high dynamic response and their performance and operation are astonishing as compared to linear controllers. However, the realization and design of these controllers are complicated. The non-linear controllers are subdivided into sliding mode, partial feedback linearization, and hysteresis gaussian controllers.

7.4.1. Sliding Mode Controllers (SMC)

SMC controllers are highly insensitive to load disturbances and variables variation. SMCs are applied to PWM inverters for voltage regulation. Therefore, in ideal conditions, with the help of SMC the steady-state response of in-varying systems can be achieved easily. Due to these reasons, the SMCs are widely and extensively used in PV systems. Despite all these advantages, some drawbacks are also associated with SMCs, such as (a) the performance of SMC depends on the sliding surface and the
choice of a suitable sliding surface is a very complicated task, (b) the selection of suitable sampling time is very important because inadequate sampling time causes high distortion and performance of SMC will be degraded, and (c) the major disadvantage of SMC is the chattering phenomena which is observed during the tracking of variable reference [160]. Therefore, to remove the shattering effects numerous other controllers are used with SMC, such as the authors in [161] who propose a direct power control SMC. It removes the disadvantages of the SMC and provides high-quality waveforms and control the active and reactive power without utilizing any additional current loop. However, an unwanted broad band-gap of harmonic is produced in this topology. The drawback is overcome by the work of authors in [162]. The chattering effect is greatly reduced by using a combination of adaptive, fuzzy logic controller (FLC), and SMC [163]. The FLC is adopted to approximate the uncertain disturbances that occur due to atmospheric variations, while the SMC is adopted to control the inverter performance. To enhance the performance of the inverter and compensate with the uncertainties of the system the authors in [164] propose a fast terminal sliding mode control (FTSMC) with fuzzy-neural network (FNN). An FTSMC is applied to the H-bridge to converge the tracking error to zero rapidly, whereas FNN is used to approximate the system uncertainties in real-time.

7.4.2. Partial or Full Feedback Linearization (PFL or FFL) Controllers

In the PFL method, the non-linearities that are associated with the system are canceled because of the transformation of the non-linear system into a partial or complete linear system. If the system having non-linearities are partially transformed into linear system, then it is known as PFL and if it is completely transformed then it is called as an FFL controller. Moreover, the system nonlinearities are canceled by establishing the non-linear terms within the system therefore they are not bound to a specific operating point. The DC-link voltage and grid injected current is controlled by using an FFL controller in [165]. The non-linear characteristics of the system are transformed into linear subsystems and then a control law is applied to these subsystems. However, it makes the PV model very complex and the switching characteristics are difficult to handle. To overcome these problems the authors in [166,167] modified the control architecture. Although the authors use an FFL approach, these controllers lack the capability to fully linearize the PV system. Therefore, to control the voltage across the DC-Link and grid injected current a PFL controller is designed in [168]. The non-linear system is not only partially transformed into a linear system but also makes it an independent system. Moreover, it also highlighted the stability issues in a 1-Φ grid-tied PV system.

7.4.3. Hysteresis Controllers (HC)

HC can produce the controlled switching pulses for VSI in a condition where there is an instantaneous comparison between the grid current and reference current. It can easily achieve objectives like (a) fast transient response, (b) simplicity, (c) robustness to variable parameters, and (d) independency from load parameters [169]. However, the main problem that occurs in HC controlled systems is to limit the measured current within its band limits that cause an undesirable variation in the switching frequency. Numerous HCC techniques are present in the literature to overcome this problem. An HC controller for grid-connected inverter proposed in [170] can attain a stable switching frequency while avoiding the control of the hysteresis band. On the contrary, the authors in [171] achieved a stable switching frequency by changing the hysteresis band. Moreover, a hybrid approach that combines the variable band HCC and SMC is proposed to maintain a rapid transient response, eliminate the steady-state error, and provide high robustness [172]. A stable switching frequency is achieved but due to usage of a single order SMC, this technique is unable to fully control the grid injected current and the system also faces the chattering effect. Therefore, the authors in [173] proposed a multi-resonant SMC with a variable band HC modulator. In this control strategy, the grid injected current is fully regulated by using third-order SMC while a hysteresis modulator is used to solve the chattering problem. A generalized structure of HC is sketched and presents it in Figure 11g.
7.5. Adaptive Controllers

The adaptive controllers have the ability to adjust the control actions automatically depending on the system operating conditions. An adaptive controller and a fourth order load current observer is designed for voltage regulation of 3-Φ inverter shows a very high performance even under the non-linear, unbalanced, and sudden load variation [174]. However, a main disadvantageous feature of this controller is high computational complexity. In [175], a combined approach of adaptive and deadbeat controller is used to exhibit the zero steady-state current error in grid-connected inverters. The adaptive controller is responsible for error correction and both these controllers work in a parallel manner thus conserving a fast dynamic response. A generalized diagram of the adaptive controller is presented in Figure 11h. The authors in [176] proposed an adaptive controller based on a resonant filter to handle the system uncertainties and to provide compensation for the harmonic distortion by measuring the load and capacitor currents by using a single sensor. However, the analysis of THD is not presented in this paper. To control the active and reactive power of grid-connected CSI inverter the authors in [177] proposed a non-linear adaptive controller. Under different atmospheric conditions, the controller performs very efficiently. However, the waveforms of the grid injected current and DC-link voltage as well as a detailed analysis of THD is not presented.

7.6. Intelligent Controllers

Automation is obtained by the intelligent controllers through the replication of biological intelligence. Moreover, these controllers do not require the system mathematical modeling and have the potential to approximate the non-linearities. The intelligent controllers are classified into three types. These are the following:

7.6.1. Neural Network (NN) Controllers (NNC)

The concept of designing an NN controller is based on the human nervous system. It is a connection of many artificial neurons that is simulated by the biological brain system. When an NN approach is used in a control system it can be trained either online or offline. NN can achieve high fault tolerance and has a potential to approximate the function mapping [22]. Moreover, NN controllers require very less system modeling; therefore, they are frequently adopted in many practical and industrial applications [178]. A combined approach of wavelet [179] and probabilistic fuzzy neural network (PFNN) [180], called a PWFNN is proposed in [181]. It is used to evaluate the grid injected reactive power to meet with the low voltage ride-through requirements. Moreover, the DC-link voltage is also regulated to balance the active power between the PV module and the inverter during faults. Similarly, another hybrid controller topology that combines PID, adaptive, neural, and fuzzy controllers is designed for the voltage regulation and management of energy storage system [182]. This controller can regulate the voltage at the point of common coupling by absorbing or injecting the reactive power through an inverter. Moreover, it also provides a robust and fast response in case of grid faults. A hybrid control scheme that combines the MPC and artificial neural network [ANN] is used to control the 02-level grid-connected inverter [183]. This controller improves the system performance for different kinds of loads and provides the output waveforms with low THD.

7.6.2. Repetitive Controllers (RC)

An RC controller is applied to a 3-Φ GCPVI improves the system output waveforms [1]. A concept of an internal model principle is utilized to design the RC. It can perform good rejection or tracking if any disturbance or reference is injected in a system (close loop). A generalized structure diagram of RC is described in [184] and is presented in Figure 11i. In this Figure, N presents the samples whereas \( Q(z^{-1}) \) and \( S(z^{-1}) \) present the transfer functions of the controller. The RC shows a very good performance for non-linear periodic load, but the transient response of the controller is not very attractive. To cope with this problem, it can be used (in a cascaded or parallel structure) with the highly
transient response controllers, such as hysteresis and deadbeat etc. Therefore, the authors in [185] proposed a PI+RC controller for grid-tied PV inverters. To enhance the adjustment capability and response time of the system a weighting factor is introduced in the PI branch.

Figure 11. Block diagram of controllers (a) proportional resonant (PR) [145]; (b) linear quadratic gaussian (LQG) [146]; (c) predictive controllers (PC) [147]; (d) deadbeat controllers [22]; (e) MPC [149]; (f) robust controllers [153]; (g) hysteresis controllers HC [173], (h) adaptive controllers [175], (i) repetitive controllers (RC) [184]; and (j) fuzzy logic controllers (FLC) [186].

While a weighting factor is introduced in the RC branch to eliminate the steady-state error. This approach not only simplifies the decoupling calculation and frame transformation but also reduces the THD of grid injected current. Similarly, to enhance the system reliability the authors in [142] proposed a control strategy that is applied to the 3-Φ GCPVI in triple loop structure (DB-PID-RC) in αβ frame system.

7.6.3. Fuzzy Logic Controllers (FLC)

The knowledge of a human being is used in FLC to define the control parameters, and is implemented to control the system dynamics. There are four components of the FLC method as presented in Figure 11j [186]. These are (a) Rule base: a collection of some rules that are defined according to application requirements that are to be controlled. (b) Fuzzification: in this process, the crisp or numerical input data is transformed into fuzzified data. (c) Interference mechanism: the fuzzified data is extracted and evaluated in this process, and a decision is made which rule should be applied according to the current status. (d) De-fuzzification: the fuzzified data is transformed
again into numerical input data and an appropriate control action is accomplished. To operate the PV system at a unity power factor the authors in [187] proposed an asymmetrical FLC controller GCPVIs. This controller efficiently maintains the load balancing and power quality, as well as the dynamic and steady-state responses of the linear and non-linear loads is also analyzed. An FLC proposed in [188] is applied to 3-Φ inverter in dq reference frame to the two-stage configuration system. The proposed controller has a fast dynamic response and tracks the reference current very precisely with no overshooting. The testing of 3-Φ GCPVI in real-time is presented in [189]. The results show that the FLC controller is capable to maintain a unity power factor and generate high-quality output power. The authors in [190] used FLC along with the back-stepping approach to maintain a DC-link voltage and deliver the power to the grid with a unity power factor. Moreover, the authors in [191] proposed an FLC to regulate the grid frequency in case of large PV integration.

Numerous scientific research articles were studied and among them, the literature review of 46 scientific articles is presented in tabular form in Table 6. Different parameters such as the type of current controllers and DC-link controllers used in different reference frames to control either power or current or voltage in 1-Φ or 3-Φ inverters are presented. Moreover, the number of control feedback loops, modulation technique, and type of filter utilized in different grid-connected applications are also presented. From the above discussion and the scientific article presented in Table 6, it is concluded that all these controllers have some disadvantages and limitations. For an instant, the PI and PID control strategies are unable to eliminate the steady-state error. On the other hand, due to fast dynamic response, flexibility, low harmonic distortion, and capability to handle the system non-linearities, the predictive controllers are one of the popular and well-established controllers for 3-Φ inverters. However, they require huge online calculations for solving an optimization problem. Due to the attractive characteristics of a robust controller concerning uncertainties in the system parameters, prior knowledge of input uncertainties is not required, and disturbance rejection in a set point it is widely implemented. However, it is not a feasible choice for the PV system due to rapid variations in the atmospheric conditions. Moreover, the intelligent controllers have the ability to approximate the system non-linearities and do not require system mathematical modeling, but they require a huge amount of data for training.

With time, more and more functionalities and requirements are identified for the grid-connected PV inverters. Therefore, to incorporate these functionalities a combined approach of the above discussed controllers can be used. A combination of RC controller with a controller having fast dynamic response such as classical or deadbeat can be a good option for grid-connected PV inverter. Similarly, a deadbeat controller has a rapid transient response but highly sensitive to system uncertainties. Therefore, it can be used in combination with the H∞ and µ synthesis controllers due to their high capability to handle the system uncertainties. The SMCs show a very reliable performance in GCPVIs because they are highly insensitive to variables variation and disturbances but cause a shattering effect. Therefore, it can be used with other controllers such as fuzzy, direct power control, NN to cope with the chattering effect. Moreover, the HC controller presents a very good performance in fulfilling the grid functionalities but to limit the measured current within its hysteresis band is a major drawback. Hence, a combined approach of HCC and high order SMC can be a feasible solution. The grid functionalities can be enhanced more by using a combination of three different controllers such as a combination of DB, classical controller, and RC can be used to control the grid-tied inverter. Similarly, a combination of adaptive, classical, and intelligent controllers can also be used. As the intelligent controls do not require exact system parameters for operation, the fast transient response of the classical controllers, and the adaptive capability of the adaptive controller make this combination a good choice for grid-connected PV inverters.
Table 6. Main characteristics of different controllers proposed in scientific articles.

| Ref. | NOP, CRF | CC | DLC | FL | CP | F | MT | A |
|------|----------|----|-----|----|----|---|----|---|
| [133] | 3-Φ, (adj) | MPC | — | M-L | C | L | SVM | PV |
| [139] | 3-Φ, (adj) | DB, PI | — | M-L | C, V | LCL | DPC | PV |
| [152] | 1-Φ | FSC-MPC | — | S-L | C | L | PWM | G |
| [154] | 3-Φ, (adj) | μ-synthesis | PI | M-L | C, V | LC | PWM | PV |
| [158] | 3-Φ, (adj) | H-infinity | PI | M-L | C | V | LC | PW | RE |
| [137] | 3-Φ, (adj) | SMC | — | S-L | C | L | PWM | PV |
| [162] | 3-Φ, (adj) | SMC-DPC | SMC-DPC | M-L | V, P | L | SVM | PV |
| [166] | 3-Φ, (adj) | FFL | LC | M-L | C, V | L | SVM | PV |
| [168] | 1-Φ | PFL | PFL | M-L | V, C | L | PWM | PV |
| [181] | 3-Φ, (adj) | Fuzzy Neural Network | Fuzzy Neural Network | M-L | V, P | L | PWM | PV |
| [182] | 3-Φ, (adj) | ANFISFID | ANFISFID | M-L | V, C | L | PWM | PV |
| [184] | 3-Φ, (adj) | Repetitive | — | S-L | C | L | SVM | PV |
| [192] | 3-Φ, (adj) | PI | — | M-L | V, C | LC | SVM | DG |
| [193] | 3-Φ, (adj) | Instantaneous Active | Reactive Control | PL, PR | M-L | V, P | L | PWM | G |
| [194] | 3-Φ, (adj) | PI | — | M-L | V, C | L | PWM | DG |
| [195] | 3-Φ, (adj) | I | — | S-L | C | L | PWM | DG |
| [196] | 3-Φ, (adj) | Reactive Power Control | PI | M-L | V, P | LC | PWM | PV |
| [198] | 1-Φ | PR | — | M-L | V, C | LCL | PWM | G |
| [199] | 1-Φ | PI, PR | — | S-L | C | LCL | PWM | G |
| [200] | 3-Φ, (adj) | PI, Hysteresis | PI | M-L | V, C | LC | PWM | G |
| [201] | 3-Φ, (adj) | PR | — | M-L | V, P | LCL | PWM | DG |
| [204] | 1-Φ | — | Adaptive droop | M-L | V | LCL | PWM | G |
| [202] | 3-Φ, (adj) | Adaptive | PI | M-L | V, C | LC | SPWM | DG |
| [203] | 3-Φ, (adj) | MPC | — | S-L | C | L | PWM | PV |
| [204] | 3-Φ, (adj) | Hysteresis MPC | — | S-L | C | LCL | PWM | G |
| [205] | 3-Φ, (adj) | Predictive DPC | PI | M-L | V, P | L | PWM | PV |
| [206] | 3-Φ, (adj) | MPC | — | S-L | C | LCL | PWM | G |
| [207] | 3-Φ, (adj) | Fuzzy | PI | M-L | V, C | L | SPWM | PV |
| [208] | 1-Φ | Fractional order PR | — | M-L | C, P | L | SPWM | PV |
| [209] | 3-Φ, (adj) | Fractional order PI | Fractional order PI | M-L | V, C | LCL | PWM | PV |
| [210] | 3-Φ, (adj) | PI | — | M-L | V, C | LCL | PWM | PV |
| [211] | 3-Φ, (adj) | PR | — | M-L | V, C | LCL | PWM | PV |
| [212] | 1-Φ | Fuzzy SMC | — | S-L | V | L | PWM | PV |
| [213] | 3-Φ, (adj) | Droop | — | M-L | V, C | LC | PWM | DG |
| [214] | 3-Φ, (adj) | PI | — | S-L | V | L | PWM | PV |
| [215] | 3-Φ, (adj) | PI | — | S-L | V | L | SPWM | PV |
| [216] | 3-Φ, (adj) | PI, MPC | PI, MPC | M-L | V, C | L | SVM | PV |
| [217] | 1-Φ | PI, Vector control | PI | M-L | V, C | L | SVM | PV |
| [218] | 3-Φ, (adj) | Fractional order SMC | — | S-L | C | L | PWM | PV |
| [219] | 3-Φ, (adj) | Voltage look-up table method | Voltage look-up table method | M-L | V, C | L | VMUT | DG |
| [221] | 3-Φ, (adj) | H-infinity | — | S-L | C | LCL | SVM | G |
| [222] | 3-Φ, (adj) | MPC | — | S-L | C | LCL | PWM | G |
| [223] | 1-Φ | Fractional order RC | — | S-L | C | LCL | PWM | G |

Abbreviations: CRF: Control Reference Frames, NOP: Number of Phases, CC: Current Controller, DLC: DC-Link Controller, FL: Feedback Loop, CP: Control Parameters, F: Filter, A: Application, M-L: Multiple loop, S-L: Single loop, V: Voltage, C: Current, P: Power, DG: Distributed Generation, and G: General.

8. Future Scope of Research

Due to rapid increase in population, industrialization, and commercialization the energy demand is increasing exponentially. Most of the energy demand is fulfilled by the conventional energy resources. However, due to CO2 emissions and other environmental concerns the world has adopted renewable energy resources for energy generation. Among the RES, solar energy is gaining more interest and among the RES its number comes after hydel and wind resource for energy generation. However, due to PV’s intermittent nature its penetration in such a large scale brings some side effects and challenges the security, reliability, and stability of the system. Therefore, for the accurate and robust integration of PV with utility grid the PE inverters to be examined and investigated so that they can meet the requirements specified by the operator and provide a high quality power with very low harmonic contents. In recent years, numerous developments have been made in the designing of highly reliable and efficient inverter topologies for grid-connected systems. A few of the active research topics in this domain are (a) the design of transformer-less inverter topologies that have a simple structure with high
structure modularity and attain the high voltage level by using fewer semiconductor switches, and (b) most of the MLI prototypes are of low capacity. Therefore, high power rated prototypes should be focused and enabled their integration with medium and high voltage grid connection (c) a combined approach of modulation techniques and intelligent algorithms (particle swarm optimization (PSO), genetic algorithm (GA), etc.) should be used to provide a high quality inputs to the grid with low harmonic contents, and (d) development of the GCMLIs control strategies that help in providing the intelligent and ancillary services and enhances the power quality and grid reliability.

9. Conclusions

This review article presents a comprehensive review on grid GCIIs, their modulation techniques, and control strategies. In this paper, initially the global status of PV along with the configuration systems used for the integration of PV with the grid is discussed. Then the inverters are classified into various types, and finally the VSIs and CSIs are compared with each other based on load dependency, power losses, etc. Based on the control modes VSIs are further classified into VCM and CCM, and it is concluded that about 81% of VSIs are operated in CCM while only 19% of VSIs are operated in VCM. In addition, four different configurations of GCPVIs are discussed and numerous features of these configurations are compared and presented in a tabular form. It is accomplished that the least expensive and the highest power rated technology is the central inverter and is most suitable for grid-tied applications. On the other hand, the most expensive, highly efficient, and low power rated technology is the module-integrated inverter and is very suitable for small residential applications. Moreover, string inverter configuration is the most commonly used technology for the grid-tied applications.

Furthermore, the circuit configuration, advantages, and disadvantages of the most commonly used GCMLIs are discussed and presented in a schematic manner. From the literature review, it is accomplished that the MLIs are most suitable for the grid-tied PV applications. As compared to 2-level conventional inverters, MLIs reduce the stress on switches, decrease the switching losses, and produce good quality output waveforms with low harmonic contents and high efficiency. Moreover, modulation techniques are divided into two main types based on their switching frequency. A detailed analysis of these two types of MTs and their sub-types are elaborated in detail and it is concluded that the most popular and commonly used MT is PWM.

Moreover, a comprehensive review on different control structures i.e., \(dq\), \(\alpha\beta\), and abc used in 3-Φ GCPPPs are presented. Furthermore, the control strategies applied in these three frames are divided into six different types; these are linear, non-linear, predictive, robust, adaptive, and intelligent controllers. These controllers and their sub-types are critically discussed and analyzed in the presence of different scientific articles and are tabulated in Table 6. Lastly, the future scope of this research article is presented. It is predicted that the performance of the GCPPPs will be improved and the cost will be reduced in the near future. This review paper will help the researchers and engineers to select the most appropriate inverter configuration system, MLI topology, MT, and control strategy according to the capacity, location, and power requirements of the PV system.

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