Effect of pile and heat exchanger properties on total heat extraction of an energy pile - A numerical study

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Abstract. Geothermal energy is one of the potential energy resources to meet future energy demand keeping environmental pollution under control. This paper presents the use of geothermal energy for space heating from energy pile. An energy pile with a single U tube heat exchanger of polyethylene (PE) pipe was modeled in this study. The effect of pile and heat exchanger properties on the total heat extraction was studied by the finite element analysis using COMSOL Multiphysics. The 3D model was developed and validated based on the literature reported results of an experimental thermal performance of a borehole equipped with a single and double U tube heat exchanger. Tetrahedral elements were considered for simulation of a 3D model. The model of a single energy pile of certain dimensions with different soil layers was considered, each soil layer was associated with different temperature. The effect of various parameters such as the length of concrete pile, the diameter of concrete pile, the thickness of U pipe, the inner diameter of U pipe and velocity of fluid inside the U pipe on amount of heat extraction was studied for an energy pile equipped with a single U tube heat exchanger. It was observed that the most influential parameters in increasing the outlet temperature of the heat exchanger loop are the diameter of the concrete pile, the inner diameter of U pipe and the velocity of fluid inside the U pipe.

1 Introduction

Due to the rapid increase of population and improved living standards energy consumption has been increased continuously for the last couple of decades. Out of the total world energy demands, 80% energy produced from fossil fuels and the rest 20% produced from renewable energy sources [1-2]. For the large scale use of fossil fuels there is an enormous increase in greenhouse gas emission, which is responsible for global warming. For that, many countries are focusing to reduce the use of fossil fuel by increasing the utilization of renewable energy. The use of renewable energy provides up to 50% CO2 emission reduction for new buildings [3-4]. The present study provides one of the efficient technology that can be used to heat building using an energy pile. An energy pile is a pile equipped with individual or several pipe circuits in order to enable the exchange of heat with the surrounding soil. The energy pile also known as heat exchanger pile as it helps to transfer the heat in between the ground and earth surface. Brine, usually water with antifreeze agent is circulated with a certain velocity inside the PE pipe to extract or inject heat energy from the ground or into the ground. This technology is being used for space heating or cooling. During the winter session, when the ground soil temperature is higher than the surface temperature, the brine inside PE pipe extracts the heat from the soil and injects it into the surface to increase surface temperature and vice versa during the summer session.

Sivasakthivel et al. [5] performed an experimental investigation on the thermal performance of single and double U tube heat exchangers by focusing on its effectiveness. The effect on ground temperatures, heat extraction and injection rate and its effects on surrounding and ground formations were studied. Cecinato and Loveridge [6] prepared some specific models of a thermal pile to find out the influence of pile, pipe and fluid properties on the outlet temperature. It was concluded that the surface area of pipe available for heat transfer is the most influential factor to increase energy efficiency. The velocity of fluid does not have a significant impact on the overall energy exchanged. Aydin and Sisman [7] analyzed the heat transfer rate for multi U tube boreholes also measured the average fluid inlet and outlet temperature. Bozis et al. [8] described effects of various design parameters on the heat transfer efficiency of energy piles. Although some studies carried out in the past on the use of energy pile, further investigation is required for its better understanding and wider application.

This paper presents the use of geothermal energy for surface heating from an energy pile. In the present study, an energy pile with a single U tube heat exchanger of polyethylene (PE) pipe was modeled as shown in Fig. 1. In the Figure, Tg, Tf are the ground and fluid temperatures, respectively; c is the distance measured from the exposed concrete surface to the nearest surface of the U tube. The effect of pile and heat exchanger properties on the total heat extraction by an energy pile
was studied by the finite element analysis using COMSOL Multiphysics. The 3D model was developed and validated based on the results reported in the literature by Sivasakthivel et al. [5], on the experimental investigation on the thermal performance of a borehole equipped with single and double U tube heat exchangers. A parametric study was carried out after model validation.

Heat transfer in porous medium model was selected for simulation of soil, concrete and PE pipe. Laminar flow physics was considered for brine (fluid), transfer inside the PE pipe. The initial temperature of different soil layers was assigned from 290K to 308K, respectively are shown in Fig. 2 and the initial temperature of the fluid was considered the same as surface temperature. The dynamic viscosity of water was assumed as 1.002×10^{-3} Pa.s. Due to the pressure difference between the inlet and outlet openings, fluid flows with a certain velocity. The velocity of the fluid depends on the pressure difference between the inlet and outlet openings. With increasing the pressure difference between the inlet and outlet openings of the U pipe, the velocity of the fluid is increased. During mesh generation, tetrahedral elements were created and simulation was carried out for 365 days.

Table 1: Material properties used for parametric study.

| Material Properties | Soil  | Concrete | PE tube | Salt Water |
|---------------------|-------|----------|---------|------------|
| Thermal Conductivity, k (W/(m.K)) | 1.25 | 1.8 | 0.5 | 0.614 |
| Specific Heat Capacity, C_p (J/(kg.K)) | 1710 | 880 | 1900 | 4200 |
| Density, ρ (kg/m^3) | 1800 | 2500 | 950 | 1000 |

2 Model preparation

The numerical modelling was carried out using COMSOL Multi-physics software. COMSOL is a 3-Dimensional finite element based software. For the parametric study a soil domain of 10m×10m×30m was considered to ensure that there is no boundary effect on the simulation. Ten different soil layers of thickness of 3.0m was considered (shown in Fig. 2). Inside the soil domain a concrete pile of diameter (D) 0.4m and length (L) 25m was considered. A single U pipe of Polyethylene (PE) was built inside the concrete pile considering clear cover (c) of 25mm. Both the openings of the U pipe at the pile top were named as inlet and outlet openings. The properties of each soil layers were considered the same, however the temperature of each soil layers were increased with increasing the depth from the ground surface as shown in Fig. 2. As the temperature of the earth is increasing towards its center from the earth surface [9]. The material properties of soil and concrete were considered from Ferrantelli et al. [10]. Properties of other materials were considered from various literatures [11-16]. The properties of the materials are shown in Table 1.

Validation of a 3-D model with the experimental study

The 3D model was validated by comparing the numerical results with the experimental thermal performance of ground heat exchangers reported by Sivasakthivel et al. [5]. Sivasakthivel et al. [5] performed an on field investigation of a borehole heat exchanger (BHX) in the BRGM campus, Orleans, France. The test set up was 50.0m long single and double U-tube heat exchanger installed in a 180 mm diameter borehole, and
was filled with grout. The thickness and external diameter of the U tubes were 3mm and 32mm, respectively. In order to circulate water into the heat exchanger a 750L water tank was installed. Normal tap water was used for experiments and to avoid the freezing of water anti-freezer solution was mixed. During heating mode fluid was circulated inside the heat exchanger at the rate of 0.6 m³/hr or 0.312 m/s. In order to measure the ground temperature in different modes of operation ‘pt100’ temperature sensors were installed at different depths near the borehole heat exchangers. During the experiments, both inlet and outlet temperature of the U pipe and fluid flowrates were monitored for a period of 8 hours. A constant ground temperature of 15°C and the thermal properties of the soil were assumed uniform throughout the depth of the ground.

Table 2: Material properties used for each domains in the validation problem (data from Sivasakthivel et al. [5]).

| Property                          | Soil | Grout | PE tube | Salt Water |
|----------------------------------|------|-------|---------|------------|
| Thermal Conductivity, k (W/m.K) | 2    | 2     | 0.5     | 0.614      |
| Specific Heat Capacity, C_p (J/(kg.K)) | 1150 | 1150  | 1900    | 4200       |
| Density, ρ (kg/m³)              | 1800 | 2200  | 950     | 1000       |

Fig. 3: Model validation with experimental study (Sivasakthivel et al. [5]).

In the present study, the experimental investigation performed by Sivasakthivel et al. [5] was validated using a 3D finite element model in COMSOL Multiphysics software. For numerical analysis a soil domain of 2m×2m×55m was selected. Soil boundary was considered far away from the borehole to ensure that there is no effect of boundary on the simulation results. A 50m long borehole with a diameter 180mm was built at the center of the soil domain and filled with grout properties. A heat exchanger U pipe with external diameter and thickness of 32mm and 3mm, respectively were inserted inside the borehole by maintaining a clear cover of 25mm. After preparation of the whole geometry respective domain was assigned by the respective material properties. The material properties, which were used in all the domains were taken from Sivasakthivel et al. [5] are presented in Table 2. Some of the properties were considered from other literature (Ferrantelli et al. [10]). The constant ground temperature of 15°C was considered during the model simulation. The laminar flow of the fluid with a velocity of 0.312 m/s was considered during the simulation of the 3D model. After the simulation, the inlet and outlet temperature of the U pipe were compared with the experimental data given in the literature by Sivasakthivel et al. [5]. Fig. 3 shows that the numerical results flow similar trends with the experimental data. The small difference in the results may be attributed due to the assumption of some parameters, which were not provided in the literature by Sivasakthivel et al. [5].

4 Results and Discussions

After validation of the 3D model with the experimental results, a series of parametric studies were carried out on a concrete pile of diameter 0.4m and length 25m. A heat exchanger U pipe of outside diameter 25mm and thickness 3mm were inserted inside the concrete pile by maintaining a clear cover of 25mm. To find out the most effective parameter to increase the surface temperature as well as the outlet temperature of a heat exchanger U pipe, a series of simulations were carried out by varying parameters. The model simulation was carried out for 365 days. The inlet temperature of the U pipe was considered 288K or 15°C and the outlet temperature was noted after the simulation. When fluid flows with a certain temperature along the pipe, it exchanges the heat with the ground as there is a temperature difference between fluid and surrounding soil. If the fluid temperature is less than the ground temperature, then the heat transferred from the ground to the fluid and therefore the fluid temperature is increased. Whereas if the fluid temperature is more than the ground temperature then heat transferred from the fluid to the ground and therefore the fluid temperature is decreased. The temperature of the fluid was noted to change with increasing the length of the pipe. For the cumulative effect of both the phenomena, outlet temperature was found to differ from the inlet temperature of the U pipe. As a results surface temperature or outlet temperature of the U pipe was noted to increase or decrease.

4.1 Effect of inner diameter of U pipe

To find out the effect of inner diameter (d) of the U pipe in increasing the outlet temperature, several model simulations were conducted for different diameters (d). Fig. 4 shows that with increasing the value of (d) from 12mm to 25mm, the outlet temperature is increased by 4.5K, when the diameter was more than 25mm the outlet temperature was noted to decrease for a constant pressure difference 100Pa between the inlet and outlet.
openings. One parameter of an energy pile was varied keeping all other parameters constant. According to Poiseuille’s law i.e., eq. [1], the fluid flow rate was increased with increasing the diameter of the U pipe for a constant pressure difference as per eq. [1]. Therefore, for the higher value of (d), fluid velocity was maximum.

\[ Q = \frac{\pi R^4 \Delta P}{8nL} \]  

(1)

where, \( Q \) is the volumetric flow rate, \( R \) is the pipe radius, \( \Delta P \) is the pressure difference between the two ends, \( n \) is the dynamic viscosity of the fluid and \( L \) is the length of the pipe.

Due to the high velocity of the fluid there was less time to inject the heat into the ground, when the fluid temperature was greater than the ground temperature. As a result, the outlet temperature of the U pipe is increased. For diameter greater than 25mm due to the higher value of (d), fluid velocity was found to be maximum. For that there was very less time to extract the heat from the ground when the fluid temperature is less than the ground temperature. As a result, the outlet temperature of the U pipe is decreased.

To find out the effect of fluid velocity in increasing the outlet temperature.

4.2 Effect of diameter of the concrete pile

To find out the effect of the diameter of the concrete pile in increasing the outlet temperature several model simulations were carried out for different pile diameters (D). In this case similar trends of results were observed with the effect of the inside diameter of U pipe. Fig. 5 shows that with increasing the value of (D) from 0.2m to 1.0m, the outlet temperature of the U pipe is increased by 4.25K. When the D was more than 1.0m the outlet temperature was observed to decrease for a constant pressure difference of 100Pa between the inlet and outlet. As the cross sectional area and the pressure difference between the inlet and outlet opening of U pipe is constant, therefore the velocity of the fluid was constant. For increasing the diameter of the concrete pile up to 1.0m, the length of the lower portion of the U pipe (i.e. horizontal part of U pipe) is increased. Therefore, the time taken by the fluid to cover this length was increased by increasing the value of (D). As the ground temperature at the lower portion of the U pipe is more than the upper portion of the pipe, hence it extracts more heat from the ground. Therefore, the outlet temperature of the U pipe is increased. For the diameter (D) greater than 1.0m, the temperature of the fluid was observed to be higher than the ground temperature, so that heat transferred took place from fluid to ground. Therefore, the outlet temperature of the U pipe is decreased.

![Fig. 5: Effect of the diameter of the concrete pile in increasing the outlet temperature.](image)

4.3 Effect of fluid velocity

To find out the effect of fluid velocity in increasing the outlet temperature several model simulations were carried out for different values of the pressure difference between the inlet and outlet openings of U pipe. Fig. 6 and Fig. 7 show that with increasing the pressure difference between the inlet and outlet openings from 50Pa to 300Pa outlet temperature of the U pipe is increased by 4.5K. The velocity of the fluid is increased by increasing the pressure difference between the inlet and outlet. Due to the higher velocity of the fluid, there is less time to decrease the fluid temperature when fluid temperature is more than the ground temperature. As a result, the outlet temperature of the U pipe is increased. Fig. 7 also shows that with increasing the pressure difference from 50Pa to 300Pa velocity of the fluid, is increased from 0.010m/s to 0.025m/s.

4.4 Effect of length of the energy pile

Fig. 8 shows that with increasing the length of the pile (L) from 15m to 25m, the outlet temperature of the U pipe does not change significantly. In both cases, the results were noted to be similar for pressure difference (\( \Delta P \)) at 100Pa.
4.5 Effect of thickness of the U pipe

To find out the effect of thickness of the U pipe in increasing the outlet temperature of the U pipe several model simulations were conducted for different values of thickness (t) of the U pipe with a pressure difference of 100Pa between the inlet and outlet openings of the U pipe. Fig. 9 shows that with increasing the thickness of the U pipe from 3mm to 10mm, outlet temperature does not change significantly. For all the cases, it shows similar results. With an increasing the time of simulation, the outlet temperature of the U pipe is increasing because the ground temperature is higher than the fluid temperature therefore continuous heat transfer from the ground to the fluid takes place.

Fig. 9: Effect of thickness of U pipe in increasing the outlet temperature.

4 Conclusions

From the numerical analysis of an energy pile equipped with a single heat exchanger U pipe following conclusions are obtained.

This study provides the use of geothermal energy in increasing the surface temperature in terms of outlet temperature of the U pipe. From the parametric study, it was observed that the most influential parameter in increasing the outlet temperature is the inner diameter of the U pipe and the diameter of the energy pile. It is also noted that with increase the velocity of the fluid outlet temperature is also increased.

The length of the pile and the thickness of the U pipe do not have a significant effect on the outlet temperature of the heat exchanger.

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