Mechanical behavior of actin and spectrin subjected to high strain rate: A molecular dynamics simulation study

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ABSTRACT

Recent nanoscopy and super-resolution microscopy studies have substantiated the structural contribution of periodic actin-spectrin lattice to the axonal cytoskeleton of neuron. However, sufficient mechanical insight is not present for spectrin and actin-spectrin network, especially in high strain rate scenario. To quantify the mechanical behavior of actin-spectrin cytoskeleton in such conditions, this study determines individual stretching characteristics of actin and spectrin at high strain rate by molecular dynamics (MD) simulation. The actin-spectrin separation criteria are also determined. It is found that both actin and spectrin have high stiffness when susceptible to high strain rate and show strong dependence on applied strain rate. The stretching stiffness of actin and forced unfolding mechanism of spectrin are in harmony with the current literature. Actin-spectrin model provides novel insight into their interaction and separation stretch. It is shown that the region vulnerable to failure is the actin-spectrin interface at lower strain rate, while it is the inter-repeat region of spectrin at higher strain rate.

1. Introduction

Axonal cytoskeleton in neuron is comprised of microtubules (MT) [1] tau proteins [2,3], neurofilaments (NF) [4], and microfilaments (MF) [5]. Most mechanical contribution to the stability of the cytoskeleton comes from MTs, but recent studies emphasize on a combination of contribution of the other major components. The structural contribution of actin to axonal cytoskeleton has been substantiated very recently. Globular G-actins lead to formation of filamentous F-actins, which eventually form periodic rings along the circumference of axon [6]. The periodic actin rings are connected by spectrin tetramers [7]. Therefore, the actin-spectrin network determines the axonal mechanical behavior. However, the current literature does not consist sufficient number of studies on mechanical behavior of actin, spectrin, and actin-spectrin network – especially in high strain and strain rate scenario, although deformation of axonal cytoskeletal components is an important concern in different injury scenarios [8–12]. This study attempts to explore the three aspects mentioned above by performing molecular dynamics (MD) simulation, as this methodology provides convenience in the specific length scale (~10 s of nanometers) of sub-axonal components.

1.1. Actin: Mechanical insights in literature

There are several studies focusing on mechanical behavior of actin existent in current literature. The convenience of studying actin comes from its conserved structure. Since 1990’s, most mechanical properties of actin have been investigated, such as response to tensile loading and stiffness [13–19], persistence length [20–23], torsional aspects [20,21,24–28], severing mechanism [29], viscoelasticity [30,31], etc. have been determined. Computational studies such as molecular dynamics studies have particularly contributed to substantiate mechanical properties of actin [14,32]. Specifically, recent comprehensive review work has concluded that the Young’s modulus of actin may vary from megapascal to gigapascal range [18]. Furthermore, computational modeling of actin has been diverse – from fully atomistic to coarse-grained [33].

1.2. Spectrin: Mechanical insights in literature

Studies on spectrin has been performed mostly from biological perspective [34], and therefore, functionality has been the prime focus of such research. Furthermore, most of the studies have been limited to erythroid spectrins, leading to limited mechanical insight into axonal spectrin [35]. The limited mechanical insight that can be gathered from the current literature are on shear [36]...
or deformation [37,38] response of erythroid spectrin. However, a number of studies focusing on forced unfolding have provided insight regarding multiple intermediate regions in spectrin structure [39–43], destabilization criteria [44] and required force to disentangle spectrin filament [45,46].

1.3. Periodic actin-spectrin skeleton: Role in axon and high strain rate scenario

The periodicity of actin-spectrin is not only limited to the main axon, but also found in dendrites and axon initial segment [6,47–53], which is an early age phenomenon for most species [54]. While the substantiation of the periodic actin-spectrin structure and the contribution to axonal stability are significant findings [55–58], the mechanical behavior at high strain rate scenario, such as actin-spectrin separation stretch is still absent in the literature. To address such limitations, biochemical and biological approaches will dictate the actin-spectrin network studies over the next few years [59,60]. Nevertheless, the very recent mechanical studies are promising, such as the one performed on chicken dorsal root ganglion [61] depicting that axonal cytoskeletal components can provide shock-absorbing support to the axon. Such studies are paving the pathway to determine the specific contribution of actin and spectrin to the stability of the periodic network.

From the literature review, it is evident that more mechanical studies are required focusing on spectrin and actin-spectrin network, which can be achieved by computational approaches as depicted by molecular level studies on other axonal cytoskeletal components [11,62]. Keeping these aspects in consideration, this study attempts to provide novel insights regarding the specific mechanical behavior of such cytoskeletal components at extreme strain rate – which will play an instrumental role in developing a bottom-up axon model focusing on high strain rate scenario and contribute to the existent computational axon models.

2. Method

The required PDB file and FASTA sequence for actin and spectrin structures are obtained from RCSB and Uniprot protein data banks, and then simulation-compliant models are built based on the predicted structures obtained from the i-TASSER predictor software [63]. The reason of proceeding with i-TASSER predicted structure is its reliability quantified by CASP and recent successful implementation of predicted structure in MD simulations [11,64,65].

The PDB files are converted into LAMMPS [66] readable data files that implements OPLS force field [67,68] for simulation. The simulation box is filled with explicit water molecules, for which MARTINI force field [69] is used for van der Waals interaction parameters. Required Na⁺ and Cl⁻ ions were added to obtain charge neutralization for explicit solvent simulations.

The general scheme of the simulation comprises of:

a. Minimizing potential energy at 310 K (the flat potential energy vs time graph ensures well equilibration),

b. Using inner and outer cutoff of LJ potentials as 10 and 12, respectively,

c. Using solver pppm (particle–particle particle-mesh), which facilitates the computation of long-range coulombic interaction,

d. NVT equilibration of the system with 100 fs temperature damping parameter (first 100 ps),

e. NPT equilibration of the system with target pressure of 1 bar (for another 100 ps),

f. Performing tensile tests by pulling the residues along the length axis, towards the opposite direction, at the strain rates of 10⁶ s⁻¹ and 10⁹ s⁻¹ [62]. It is assumed that –0% of strain is sufficient to obtain the stiffness data.

Table 1 summarizes the box size of the systems and the specific tensile test schemes.

2.1. Tensile test on 6-actin and 12-actin models

To determine mechanical property of actin, 6-actin and 12-actin models are utilized. Both models are built from existent literature. The 6-actin model is obtained from “actin filament pointed end” structure found by electron microscopy deposited with PDB ID 2Y83 [70], while the 12-actin model is obtained from the cryo-EM structure of actin deposited with PDB ID 3G37 [71]. The objective of tensile test is to observe strain rate dependence and difference between the stretching mechanism between short and long F-actin filaments.

2.2. Tensile test on α-spectrin and β-spectrin

For α-spectrin and β-spectrin, the models are built from Uniprot structures – for non-erythrocytic α-spectrin (gene: SPTAN1) [72] and β-spectrin (SPTBN2) [73] structures. These sources facilitate specification of domains and repeat regions, which is utilized in the modeling and tensile tests. The tensile test scheme is similar to that of actin. The simulation-compliant versions are created by using the last seven (7) repeats and the EF hand regions for α-spectrin, while the first seven (7) repeats and the actin binding domain are used for β-spectrin. According to the comprehensive
review study on spectrin [7], 19–20 repeats in α-spectrin and 1–2 repeats in β-spectrin are sufficient for actin-spectrin modeling, and therefore, it is ensured that these repeats are included in the standalone spectrin models. The specification of the residue numbers of both spectrin isoforms are provided in Table 1. Aside from obtaining the mechanical property, another objective of the tensile test on standalone spectrin is to observe the unfolding mechanism.

2.3. Determination of actin-spectrin interaction

For actin-spectrin interaction model, two β-spectrin filaments (a smaller version with the actin-binding domain and the first two repeats) [7] are attached to the 12-actin surface, and then pulled at the opposite directions. The objective of applying two different strain rates is to observe the strain rate dependence and possible separation mechanism. This ensures that possible high strain rate scenarios are covered where either of the axonal cytoskeletal components might be susceptible to stretching.

2.4. Stress-strain calculation and tensile test schemes

Calculation of the stress and strain are similar to recently published MD work on axonal cytoskeletal component of neuron [11]. In a simple manner, the stress–strain calculation scheme can be pointed out as:

a. Obtaining stress values from per-atomic stress tensor in LAMMPS, which is associated with the volume of the respective group of atoms,
b. Calculating approximate volume of the group of atoms by implementing Voronoi feature of LAMMPS, which is included in the voro++ package,
c. Dividing the (stress × volume) data by the approximate volume from Voronoi calculation to obtain the stress data,
d. Obtaining strain values from displacement data of atoms [74],
e. Maintaining NVT ensemble throughout the tensile test, with a 100 fs temperature damping parameter.

As a relevant note, visualization snapshots are obtained by OVITO [75]. All the simulations were carried out by the STAMPEDE2 and Lonestar supercomputers of Texas Advanced Computing Center (TACC).

3. Results

3.1. Mechanical behavior of actin

For 6-actin and 12-actin systems, uniaxial tensile tests are performed at two strain rates, $10^8$ s$^{-1}$ and $10^9$ s$^{-1}$. Figs. 1–3 show the stress–strain response and tensile test snapshots for the 6-actin system, while Figs. 4–6 show the same for the 12-actin system. It is observed that both 6-actin and 12-actin behave as stiffer material at higher strain rate. However, the stretching stiffness is in the range found in the literature, even at such high strain rate.

3.2. Mechanical behavior of spectrin

For α-spectrin and β-spectrin systems, uniaxial tensile tests are performed at two strain rates, $10^8$ s$^{-1}$ and $10^9$ s$^{-1}$. Figs. 7–9 show the stress–strain response and tensile test snapshots for the α-spectrin system, while Figs. 10–12 show the same for the β-actin system. It is observed that spectrin also behaves as stiffer material when susceptible to higher strain rate. However, the extent of dependence on the strain rate is relatively lower, as spectrin goes through unfolding stage of the interrepeat domains unlike actins (which manifest stretching of the F-actin filaments even at low strain due to strong bond between G-actins in the filament) as depicted by the snapshots.

Table 2 summarizes the stiffness result based on the linear fit of 10% strain vs stress data of actin and spectrin models.

3.3. Actin-spectrin interaction

For actin-spectrin systems, tensile tests are performed at two strain rates, $10^8$ s$^{-1}$ and $10^9$ s$^{-1}$ by attaching two β-spectrin to the surface of a 12-actin system, and then pulled away towards the opposite directions. Figs. 13 and 14 show the tensile test snapshots for the system for $10^8$ s$^{-1}$ and $10^9$ s$^{-1}$, respectively. It is depicted that not only the separation differs according to the applied strain rate, but also the failure mechanism. At lower strain rate, the prone-to-failure region is the actin-spectrin interface, while at higher strain rate, it is the inter-repeat regions of spectrin.

4. Discussion

The tensile tests performed in this study provides novel insights into mechanical behavior of actin, spectrin, and actin-spectrin cytoskeleton in axon. However, as a computational study, some common issues must be addressed – such as selection of force field, application of strain rate, and using predicted structure for protein.
First, selection of appropriate force field is vital for realistic representation of a biophysical scenario. In this study, OPLS force field is used for simulations, as it is specifically fine-tuned for protein simulation [76,77]. Recently it is found that non-reactive force field such as CHARMM can successfully capture high deformation phenomena for cytoskeletal components of neuron [11,62]. As a benchmark test, the tensile test on α-spectrin is performed for both CHARMM and OPLS force fields, which shows comparable results as depicted in the Appendix 1.

Second, the strain rates used in this study for the tensile tests fall into “extreme” range for axonal cytoskeletal components. However, recent computational study on such components has found such range of strain rates as relevant to cavitation bubble implosion (blast-induced traumatic brain injury (TBI) scenario) [62]. And third, proceeding with predicted structure obtained from the FASTA sequence available in the protein data bank (PDB) is justified due to increased application and successful implementation in the recent years [11,64,65,78].

In the following sub-sections, the specific aspects of the obtained results, their impact, and future directions are discussed.

4.1. Mechanical behavior of actin in high strain rate scenario

Studies that explored the failure mechanism of actin have emphasized the effect of actin-severing proteins, such as cofilin [27,79]. While it is admitted that both biochemical and mechanical aspects should be considered for determining mechanical behavior of actin at high strain rate, it can be argued that effect of mechanical loading (applied tension on the protein in this study) will be most significant at extreme strain rate scenario, which is shown in recent studies on other axonal cytoskeletal components of neuron [11,62]. Furthermore, from the results of both 6-actin and 12-actin systems it is substantiated that actin behaves as a stiffer material at higher strain rate. Increase of extensional and torsional stiffness is established in the literature [14], which is in harmony with the finding of the current study. Therefore, from the perspective of extensional stiffness, it can be asserted that mechanical behavior of actin is maintained throughout a large range of tensile loading. The only difference between the 6-actin and 12-actin system is the failure mechanism. For 6-actin or shorter system, actin tends to fail along the junction of G-actin to G-actin. Similar type of failure is also observed for MTs at extreme strain rate, which fails along the line of the tubulin junction when susceptible to tensile loading [62]. As there is mainly electrostatic and van der Waals bond i.e. non-bonded interactions between G-actins, it is expected that these bonds will be broken before the covalent bonds within the G-actin atoms. However, for longer system (12-actin), the pulled region is substantially smaller than the overall filament length, and therefore, the tensile load can be carried along the length of the whole filament – leading to high stretchability. The range of stiffness is, however, coherent with recent review work [10], which suggests that at high strain rate, actin stiffness will be at the high end of the range proposed (400 MPa-2.5GPa) [14–19,32].
4.2 Mechanical behavior of spectrin in high strain rate scenario

Similar to that of actin, the mechanical behavior of spectrin can also be explained from the biochemical perspective [34]. Earlier atomic force microscopy (AFM) studies on spectrin tandem repeats and single spectrin have established that susceptibility to tensile loading leads to unfolding and stretching, which is impressively close to the observation in the current study [39,40,42]. Furthermore, the high stretchability can be attributed to the initial “folded” state of the repeat regions and the inter-repeat regions, which get unfolded due to applied high strain rate. Although the force required to unfold spectrin has been found to be small [45], it can be asserted that due to having multiple un-foldable regions throughout the structure, axonal spectrin can have high stretchability. However, the multiple fold is attributed to the mechanical strength of the spectrin filament, and unfolding leads to vulnerability to failure. It is discussed in recent studies that axonal cytoskeletal components provide mechanical stretchability due to their

Fig. 4. Stress–strain response of 12 actin system for two strain rates.

Fig. 5. Snapshots of tensile test on 12-actin system at strain rate $1 \times 10^8$ s$^{-1}$. Strain: a) 0%, b) 5%, c) 10%. The atoms being pulled are shown in red color. For the rest, the default coloring of OVITO software is retained. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

Fig. 6. Snapshots of tensile test on 12-actin system at strain rate $1 \times 10^9$ s$^{-1}$. Strain: a) 0%, b) 10%, c) 20%, d) 30%, e) 40%, f) 50%. This longer filament does not show failure by fragmentation, rather it shows increased stretchability. The atoms being pulled are shown in red color. For the rest, the default coloring of OVITO software is retained. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)
inherent capacity to stretch even more than 100% of their initial length [61], and therefore, it can be assumed that this capacity is originated from the ability of membrane-associated proteins in axon which contain folded regions i.e. spectrins. Therefore, the results on spectrin not only substantiates the structural and mechanical insights present in the current literature, but also provides indirect causation of the ability of axon to stretch significantly.

4.3. Actin-Spectrin interaction in high strain rate scenario

There is little insight present in the current literature regarding actin-spectrin network [61]. From the actin-spectrin models in the current study, it is substantiated that even at high strain rate, actin-spectrin lattice can provide substantial mechanical support. Also, two different manners of failure can be observed according to the applied strain rates. At lower strain rate, there is significant stretch in spectrin, but the primary failure-prone region is the actin-spectrin interface. However, the scenario is different at higher strain rate, as the tensile loading gets less amount of time to be propagated through the spectrin filament and manifested at the interface region. Therefore, it is observed that the more damage-prone area is the inter-repeat regions of spectrin – same observation obtained in standalone spectrin tensile tests performed in this study. In other words, at a high strain rate scenario, there could be occurrence of different failure along the periodic actin-spectrin lattice: such as separation of spectrin from actin surface, substantial spectrin unfolding, or both. In any case, the result is disorientation of the axonal cytoskeleton of neuron, regarding
which this study provides a novel, strictly mechanical insight from high strain rate perspective. However, for more comprehensive insight, length-dependent tests could also be performed as the F-actin models in this study. For this purpose, different number of repeats might be implemented in the actin-spectrin models. Optimistically, the future works will be considering coarse-grained models to accommodate longer filament lengths and multiscale approach to obtain lattice-level mechanical response.

5. Conclusion

In this study, mechanical behavior of actin, spectrin, and actin-spectrin interaction at high strain rate are determined. The major findings can be summarized as below:

![Fig. 10. Stress–strain response of β-spectrin system for two strain rates.](image)

![Fig. 11. Snapshots of tensile test on β-spectrin system at strain rate $1 \times 10^8$ s$^{-1}$. Strain: a) 0%, b) 5%, c) 10%. The atoms being pulled are shown in red color. For the rest, the default coloring of OVITO software is retained. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)](image)

![Fig. 12. Snapshots of tensile test on β-spectrin system at strain rate $1 \times 10^9$ s$^{-1}$. Strain: a) 0%, b) 20%, c) 40%, d) 60%. The unfolding of the inter-repeat domains is manifested strongly at high strain rate. The atoms being pulled are shown in red color. For the rest, the default coloring of OVITO software is retained. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)](image)

### Table 2

| Model      | Stiffness (MPa) | $1 \times 10^8$ s$^{-1}$ | $1 \times 10^9$ s$^{-1}$ |
|------------|----------------|--------------------------|--------------------------|
| 12-actin   | 919            | 2054                     |                           |
| 6-actin    | 852            | 1816                     |                           |
| Spectrin-α | 973            | 2107                     |                           |
| Spectrin-β | 1120           | 1067                     |                           |
Fig. 13. Actin-spectrin interaction at strain rate $1 \times 10^9 \text{s}^{-1}$. a) 0%: initial, b) 6%: stretching of $\beta$-spectrin, c) 12.5%: onset of separation, d) 18.75%: complete separation. Legend: Yellow: 12-actin, Green: $\beta$-spectrin, Red: atoms being pulled. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

Fig. 14. Actin-spectrin interaction at strain rate $1 \times 10^9 \text{s}^{-1}$. a) 0%: initial, b) 23.5%: stretching and unfolding of $\beta$-spectrin, c) 42.3%: onset of separation, d) 58.75%: complete separation. Legend: Yellow: 12-actin, Green: $\beta$-spectrin, Red: atoms being pulled. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)
a. Actin: Both short and long F-actin filaments show stiffer characteristics at higher strain rate. Short filament tends to fail at the G-actin to G-actin junction, while long filament shows increased stretchability.
b. Spectrin: Both α-spectrin and β-spectrin show high stretchability. Unfolding of inter-repeat regions is strongly manifested at higher strain rate.
c. Actin-spectrin: Failure occurs at actin-spectrin interface at lower strain rate, while significant unfolding of spectrin occurs at higher strain rate.

This study not only substantiates recent findings on periodic axonal structure of cytoskeleton, but also provides novel insights regarding the mechanical behavior and interaction. Therefore, this study will provide pathway for bottom-up axon modeling, contribute to refinement of existent computational axon models, and invoke further research focusing on high strain rate scenario.

Author contributions

M.I.K. performed prediction of the structures, ran the simulations, interpreted the results, and wrote the manuscript. S.F. made and optimized all the models of actin and spectrin. A.A. designed the study and revised the manuscript. All the authors reviewed the manuscript.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Appendix A

Appendix 1. Comparison between CHARMM and OPLS force field results: Tensile test on α-spectrin

To compare CHARMM with respect to OPLS, two identical models are created for α-spectrin, and the tensile test is performed at strain rate $1 \times 10^8$ s$^{-1}$ as per the “Method” section in this manuscript. Fig. A1 shows the stress–strain response for both force fields, which depicts that both force fields similar results. Furthermore, Fig. A2 shows that both CHARMM and OPLS shows similar manner of unfolding in α-spectrin. Considering these findings, it can be concluded that both force fields are equally eligible candidates for such simulations.

Fig. A1. Comparison between CHARMM and OPLS tensile test results for α-spectrin. For CHARMM, the stiffness is 1164 MPa, while for OPLS, it is 1120 MPa.
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Fig. A2. Tensile test snapshots at 0%, 5%, and 10% strain for α-spectrin created by a-c) OPLS, d-f) CHARMM. Atoms being pulled are shown in red color. For the rest, the default coloring by OVITO is retained.
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