Simulation of an Adaptive Method of Improving the Accuracy and Extending the Range of Frequency Signal Processing in a Frequency-to-Code Converter

Piotr Warda

Faculty of Electrical Engineering and Computer Science, Lublin University of Technology, Nadbystrzycka 30 A, 20-618 Lublin, Poland; p.warda@pollub.pl

Abstract: The article discusses the modification of one of the basic methods of converting successive periods of a variable frequency signal into numerical values representing them. The method performs the adaptive frequency selection of the clock signal in the system processing the consecutive periods of input signal. The signal processing error is analyzed on an ongoing basis, and the frequency change factor is selected. Algorithms describing the operation of the method are included. The program of the simulator of the measurement channel operation with a frequency carrier of information is described, which allows for the verification of the proposed method. Examples of the simulation results are included.

Keywords: frequency measurement; frequency-to-code converter; measurement channel with frequency carrier of information; LabVIEW

1. Introduction

Modern measuring systems are more and more often found to contain converters with a frequency output [1]. In this type of converter, information about changes in the processed quantity $x(t)$ is transferred via the frequency value of the converter output signal; hence, the devices are called physical-quantity-to-frequency (X/f) converters [2]. There are two common ways of converting the quantity $x(t)$ into a variable frequency signal [3]. In the first case, frequency-to-voltage conversion is used, and further processing involves an analogue-to-digital converter [4]. The second method is the conversion of the frequency signal directly into numerical values by a specialized frequency-to-code (f/N) converter [5].

The transmission of information by means of a frequency signal has many advantages [6]. Such a signal is resistant to interference and can be transmitted in a simple and effective way over long distances without the loss of information [7,8].

Company devices for continuous frequency measurement have been known for years [9]. However, one can still encounter research on new methods of frequency signal processing [10], reducing errors in frequency signal processing [11,12], or the estimation of processing accuracy [13,14].

Due to the wide possibilities of microprocessor systems, they have also been used in measurements of the variable frequency of the signal [15,16]. It is also very interesting to use the microprocessor system not only for frequency processing [2] but also for the adaptive correction of the system parameters during the measurement. This raises the possibility of increasing the accuracy of the results [2].

Research into new processing methods is very time-consuming. They can be implemented both by experiments and simulation. Experimental testing enables new processing methods to be unequivocally verified but requires a lot of time and is very expensive. There may also be significant problems with the selection of equipment for...
the experiment. The simulation test offers a limited possibility of verification. However, with the adoption of appropriate assumptions, it significantly supports the initial tests and accelerates the obtaining of information, allowing for decisions regarding the implementation of new methods in the physical model [17].

The simulation can be performed with the use of basic programming languages, such as C [18] or Python [19]. However, it is more convenient to use specialized software for this purpose, such as Matlab [20] or LabVIEW [21]. Matlab is a software dedicated to calculations [22]. However, compared to LabVIEW [23], it has a limited possibility of connecting external devices. Considering that, during the research, in order to verify the experimental work of the fragments of the virtual channel model, it may be very useful to process data generated in external devices, so it was decided to use the LabVIEW programming environment. It also has the advantage that, in the event of the need to use Matlab script, LabVIEW offers this possibility [24].

2. Converting Frequency into Numerical Values

The variable frequency signal can be measured using various methods [25]. One of them is the application of a microprocessor system that performs digital period measurement, supported by a counter with an additional register attached, which captures the current state of the counter [26]. The counter operating in this mode works continuously; i.e., after reaching its maximum value, it starts counting from the beginning. The reading of the counter status is performed by transferring the current contents of the counter totalizing register [27], without stopping the summation of pulses, to a special register that keeps the instantaneous value of the state [28].

In the present system, the reading of the counter status is controlled by a microprocessor. The system measures the frequency by determining the duration of a single period $T_{si}$ [14]. The block diagram of the system operating according to the proposed method is presented in Figure 1. Figure 2 shows the waveforms presenting the operation of the periods processing system of the signal of variable frequency.

The counter is controlled by a clock generator with the period $T_0$ (Figure 2c). The code output of the counter is connected through a register capturing the state of the counter to the microprocessor. A frequency signal with period $T_{si}$ is applied to the selected microprocessor input (Figure 2b). The microprocessor reads the counter state at the instants of receiving the start and end impulse $T_{si}$ (Figure 2d). In this way, in the memory of the microprocessor, information is collected in the form of numbers representing successive values of the periods $T_{si}$ of the variable frequency signal from the physical-quantity-to-frequency converter.

![Figure 1. Continuous frequency measurement using a single counter and state capturing register.](image-url)
The principle of continuous measurement of the periods of signal of a variable frequency with a single counter. The individual positions are shown: (a) exemplary waveform $x(t)$, (b) variable frequency waveform produced by the X/f converter, (c) clock signal waveform with frequency $f_0$, (d) counter reading of the f/N converter at the beginning and end of each period $T_{xi}$.

The frequency for a given $T_{xi}$ is determined by the formula:

$$f_{xi}(t) = \frac{1}{t_{i+1} - t_i} = \frac{1}{T_{xi}},$$

where: $t_i$, $t_{i+1}$—time instants when the characteristic slopes of the testing signal with variable frequency appear. The numerical value corresponding to the length of a given period $T_{xi}$ is described by the formula:

$$N_{xi} = N_{i+1} + N_{\text{max}} \ast O - N_i,$$

where: $N_i$ and $N_{i+1}$—the states of the totaling register of the counter at the times instants $t_i$ and $t_{i+1}$, respectively, $N_{\text{max}}$—capacity of the counter, and $O$—number of overflows of the counter during the measurement of each interval $T_{xi}$.

The $T_{xi}$ period estimate of the f/N converter input signal is calculated from the formula:

$$T_{xi} \approx \frac{N_{i+1} + N_{\text{max}} \ast O - N_i}{f_0}.$$

Hence, the estimated frequency of the tested signal can be described by the formula:

$$f_{xi} = \frac{1}{T_{xi}} = \frac{1}{T_0(N_{i+1} + N_{\text{max}} \ast O - N_i)},$$

where: $T_0$—the period of the clock generator output signal. In this way, the data for calculating the values of consecutive periods of the input signal of the f/N converter are obtained. Taking into account the sensitivity $S$ of the X/f converter, the data allow for a direct reconstruction of the waveform $x(t)$ (Figure 2a) by using the dependency:

$$x(t) = \frac{f_{xi}}{S}.$$
3. Errors of the Measurement Channel with a Frequency Carrier of Information

The accuracy of the direct conversion of the frequency signal periods into numerical values in the frequency-to-code converter is mainly limited by two components: the quantization error and the averaging error, which are described in [14].

The quantization error in measuring the period of a variable frequency signal depends on the value of the converted period of the signal [29]. The quantization error $\delta_k$ can be calculated from the dependence:

$$\delta_k = \frac{T_0}{T_{x_i}} \cdot 100\%.$$  \hspace{1cm} (6)

An example of the quantization error curve is shown in Figure 3.

Figure 3. An example of the quantization error curve for the frequency $f_0 = 10$MHz and the $T_{x_i}$ periods values of the quantized waveform varying from 10μs to 100μs.

The averaging error arises as a result of the integral action of the input quantity by the physical-quantity-to-frequency converter [14]. It was assumed that the test input signal $x(t)$ has a sinusoidal shape, the amplitude and the constant component of which are equal to each other, and the variability range is between $-X_m$ and $+X_m$. Taking the above into account, the relative error of averaging is calculated from the dependence [14]:

$$\delta_a = 0.5 \left( 1 - \frac{\sin \pi F T_{x_i}}{\pi F T_{x_i}} \right) \cdot 100\%.$$  \hspace{1cm} (7)

where $F$ is the frequency of the signal $x(t)$. This relationship shows that the averaging error depends on the value of the period $T_{x_i}$ and the frequency $F$. The error value increases with the increase of both of these parameters.

The analysis of the information processing error in the measurement channel with the frequency-to-code converter, after adopting the ideal X/f conversion (the work concerns the modification of the processing method in the f/N converter), allowed to determine the formula for the maximum total error [14] as:

$$\delta_e = \frac{T_f}{T_{x_i}} + 0.5 \left( 1 - \frac{\sin \pi F T_{x_i}}{\pi F T_{x_i}} \right).$$  \hspace{1cm} (8)
Formula (8) shows that the increase of the $T_{ni}$ period causes the increase of the averaging error, while its decrease causes the increase of the quantization error (Figure 4). An exemplary plot of the total error $\delta_0$ is shown in Figure 5.

There is a certain minimum between the values causing the increase of the above-mentioned errors at which the measuring system works with the highest accuracy [2]. The frequency of the clock frequency generator $f_0$ has an impact both on the quantization error $\delta_q$ and indirectly, by influencing the measurement of successive...
periods $T_{\alpha}$ of the frequency signal, also on the averaging error $\delta_{\alpha}$ [14]. The increase in the frequency of the clock generator reduces the quantization error and increases the resolution of the period measurement of the frequency signal [30]. Unfortunately, processing a larger number of pulses requires counters with greater capacity [31]. The opposite situation reduces the demand for the counter capacity but deteriorates the accuracy of the measurement [14]. The conclusion is that it is possible to choose such an output frequency value of the clock generator of the $f/N$ converter that will allow to achieve an acceptable compromise between the capacity of the counter and the value of the clock signal frequency. Of course, it should be remembered that the frequency of the clock signal will produce different error values depending on the frequency of the input signal of the $f/N$ converter [29]. The proposed method describes how to select the frequency of the clock signal to improve the information processing parameters in the measurement circuit with a frequency information carrier.

Figure 6 shows examples of the quantization and averaging errors for the signal $x(t)$ changing with the frequency of 1 Hz. It is evident that only one of the above-mentioned errors has the dominant value at the ends of the processing range.

For the upper range, where the period tends to the minimum values, the quantization error has a significant impact on the total error, and the averaging error is negligible in this case. The reverse is true for $T_{\alpha}$ reaching $T_{\text{max}}$. Taking the above into account, it is possible to use the transformed formulas for the errors mentioned to determine the value of the period $T_{\alpha}$ at which, and, thus, the value of $N_{\alpha}$ representing it, the given value of the resultant error is obtained. Since each measurement of the $T_{\alpha}$ period is performed as an independent measurement [14], the processing error is also determined as the maximum error of a single measurement.

![Figure 6](image.png)

**Figure 6.** Summary of sample quantization error and averaging waveforms for $F = 1$ Hz and $f_0 = 1$ MHz. The red line curve shows the course of the averaging error; the black line curve shows the plot of the quantization error.

Taking into account the considerations presented above, it can be assumed for the processing error $\delta_{\alpha}$ in the upper measuring range with a satisfactory approximation that
its value describes the Formula (6). Therefore, after transformation, it can be written that
the numerical value representing $T_\omega$ at which a given error occurs can be calculated from
the transformed dependence (6) taking into account Formula (3):

$$N_\omega = \frac{1}{\delta_\omega} - 100\%.$$  \hspace{1cm} (9)

In the lower part of the frequency conversion range, the value of the averaging error
[17] described by relationship (7) prevails. Due to the problem of the direct determination
of the dependence on the value of $N_\omega$ from the above-mentioned equation, the Taylor
series expansion [32] of the sinus function was used for the transformation; only the first
two unfolding elements were taken. As a result, after transformations and assuming the
processing range of the X/f converter to be $0 \times X_\omega$, the dependence on the averaging error
took the form:

$$\delta_\omega = \frac{(\pi FT_\omega)^2}{6} \times 100\%.$$ \hspace{1cm} (10)

The above dependence, after taking the Formula (3) into account, is used to obtain
the formula for the value of $N_\omega$ obtained for the given value of the processing error:

$$N_\omega = \frac{\sqrt{0.06\delta_\omega}}{\pi FT_\omega}. \hspace{1cm} (11)$$

The dependencies (9) and (11) allow to establish the $N_\omega$ threshold values at which
the change of the clock signal frequency $f_0$ in the f/N converter will improve the
information processing parameters.

Increasing $f_0$ reduces the quantization error. The use of a programmable frequency
multiplier [33] may enable an increase in the accuracy in the processing of
high-frequency signals of a variable frequency signal [29].

In the low frequency range, the value of the frequency $f_0$ influences the value of the
number $N_\omega$. The appropriate reduction of $f_0$ allows the information to be processed by the
f/N converter with a reduced number of signal pulses with the frequency $f_0$ registered by
the f/N converter counter with the maximum averaging error $\delta_\omega$ unchanged. Reducing the sum of pulses in the measurement of a given $T_\omega$ allows increasing the maximum
length of the $T_\omega$ period [34] that can be measured by the f/N converter.

4. Adaptive Method of Improving the Processing Parameters in the Frequency-to-Code
Converter

The presented method is not intended to compete with the systems realizing
high-speed analog-to-digital processing. Rather, it is recommended for using in a
measurement channel with a frequency information carrier in which the integrating
nature of the operation of the X/f converter allows the processing of signals with low
frequencies [14].

The discussed author’s method allows for the adaptive improvement of the
processing parameters in the frequency-to-code converter of successive periods of the
input signal with a variable frequency into its digital representation in a manner adapted
to the performance of the processor used in the frequency-to-code converter.

Frequency-to-code converters are often based on a counter system [3] that allows for
a continuous reading of the status without stopping the counter operation. Typically, the
counter circuit works with a processor with attached RAM memory. The reason is the
lack of the possibility of the clear, direct presentation of the current, rapidly changing
measurement results on a simple indicator (e.g., LED, LCD). Consequently, it is necessary
to process and store the obtained results, for example, in RAM or on a memory card, for
analyses performed with a certain delay, imposed by the adopted technical solutions in a
specific device. The presentation of the method is based on the previously shown structure of the microprocessor system of the f/N converter (Figure 1). The modification of the circuit is shown in Figure 7. The basic circuit in Figure 1 has been supplemented with a clock frequency divider/multiplier module \( f_0 \). The method allows reducing the error made during the measurement of successive periods of the variable frequency signal, thus increasing the measuring range of the device in which the measurement will be carried out with a similar processing error. The implementation of the method is possible with processor systems and programmable circuits widely used in practice that can perform such functions. The description of the operation of the program variants can be presented by an algorithm, a comparison table, and other methods. Due to the relatively low complexity of the algorithms, it was assumed that the operation of the adaptive method will be described using algorithms. The basic algorithm of the method is shown in Figure 8. The method of the adaptive improvement of the processing parameters in the frequency-to-code converter is carried out in several phases. In the first phase, the previously discussed basic measurement of the first period \( T_{xi} \) of the variable frequency signal is made.

![Diagram](image)

**Figure 7.** Structure of the f/N converter enabling the implementation of the adaptive method.

To simplify the considerations, it was assumed that a square wave signal with logical levels adapted to the voltage levels required by the processor is fed into the input of the f/N converter. Changes in the logic states at the processor input allow the processor software to determine the beginnings of subsequent \( T_{xi} \) periods. At the moment of detecting the beginning of the next \( T_{xi} \) the processor reads the current state of the counter, summing the pulses formed by the signal periods from the prescaler/frequency multiplier module and changing the frequency of the reference signal \( f_0 \) from the clock signal generator. The read state from the counter system is stored in RAM memory until the next state is read, corresponding to the detection by the processor software of the beginning of the next period \( T_{xi} \). Then, the processor calculates the difference of the successive states read from the counter, representing the period length \( T_{xi} \) of the variable frequency signal. At this point, the second phase of the frequency-to-code converter operation begins, carrying out the procedure correcting the frequency change factor \( f_0 \) of the signal from the reference frequency generator. The difference of states read from the counter system reflects the period value that takes into account the frequency change factor in the prescaler/multiplier module and the frequency of the signal from the clock signal generator. The computed difference \( N_{xi} \) is used to determine the value of the maximum processing error (8) made when measuring the period \( T_{xi} \) [14]. The value of \( N_{xi} \)
is stored in the RAM at the index \( i \). After detecting that the permissible value of the quantization error has been exceeded (option “\( Y \)” in Figures 8 and 9), the procedure determines the frequency change factor that allows reducing the processing error to the limit set in the program and sets the required frequency change factor in the prescaler/multiplier module.

**Figure 8.** Work algorithm of the \( f/N \) converter containing a microprocessor system with low efficiency.
Figure 9. Work algorithm of the f/N converter containing a microprocessor system of satisfactory efficiency.

In addition, the value of the frequency change factor is stored in the memory for use in computing the period value with index i+1. In the case that the error does not exceed the predetermined value (option “N” Figures 8 and 9), the procedure ends without changing the reference frequency correction coefficient, performing only the operation of assigning the period with index i+1 to the value of the coefficient of change as for the
period with index $i$. As a result, pairs of numbers are stored in the memory of the frequency-to-code converter: the calculated state differences corresponding to the successive periods $T_u$ and the values of the frequency change factor set in the prescaler/multiplier module when measuring the length of these periods. Thanks to this, the master device, which is most often a computer, can read the assigned, stored data pairs through the interface and calculate the values of the successive $T_u$ periods. The operation requires only taking into account the constant for a given converter frequency-to-code frequency of the clock signal, which can also be sent by the converter or entered directly into the master device software.

In the case of using a processor with sufficient computational speed compared to the rate of change of frequency of the processed variable frequency signal, it is possible to calculate the period value directly in the frequency-to-code converter. The algorithm for measuring the variable frequency with an f/N converter with a microprocessor system with a satisfactory performance is shown in Figure 9. In this case, the processor also calculates the difference of states read from the counter system, which represents the period value, taking into account the degree of frequency correction in the prescaler/multiplier module and the frequency $f_0$ of the generator model. The computed difference is used to determine the maximum value of the total error made in measuring the period $T_u$ [14], then the computed state difference is used to calculate the actual period value, which is then stored at a given index $i$ in the RAM. Upon detecting that the admissible quantization error value has been exceeded (option “Y”), the procedure calculates a frequency correction factor that allows the processing error (8) to be reduced to the limit set in the program and changes the frequency correction factor in the prescaler/multiplier module. In addition, the value of the frequency shift factor is stored in memory for use in computing the period value with the index $i+1$. If the error does not exceed the set value (option “N”), the procedure ends without changing the change factor of frequency, performing only the operation of assigning the $i+1$ period to the scaling factor value, such as for the period with the index $i$. In the case of the alternative algorithm, the master device has the ability to directly read the successive values of the period calculated in seconds.

5. Simulation of the f/N Converter Working in Adaptive Mode

   The simulator’s task developed by the author is to perform partial simulations for individual elements of the measurement channel with a frequency carrier of information and to present the final effect of the f/N conversion using the previously discussed processing method. During the simulator operation, the following steps are carried out:
   1. Simulator configuration, setting simulation parameters and test signal parameters;
   2. Simulation of the operation of the X/f converter, preparation of the $T_u$ period table representing the given test signal;
   3. F/N processing using the discussed method;
   4. The reconstruction of the $x(t)$ waveform from the collected numerical values $N_{uj}$
   5. Using the numerical representations of the test signal and the reconstructed signal to calculate the absolute error and relative information processing;
   6. Saving the simulation results under unique names in the form of a text file with data and a graphic file with the visualization of the simulator work results.

   Figure 10 shows the fragment of the application diagram with the presentation of the subroutines that perform the following sequence: creation of the $T_u$ period table, f/N processing, reconstruction of the $x(t)$ waveform, and creation of a unique name of data files containing information about the test signal parameters and simulator application configuration.
Figure 10. The fragment of the diagram showing the implementation of the simulation process, recreating the input waveform and creating a unique name for the data file.

Figure 11 shows the fragment of the diagram that realizes the setting of the \( N_{xi} \) threshold values that trigger the change of the clock signal frequency controlling the operation of the \( f/N \) converter counter. The upper Case structure [21] is activated if the current value of \( N_{xi} \) is greater than the value of \( N_{xi}^{\text{max}} \) set in the application panel (Figure 12). Then, the frequency change factor \( \text{Prec Lo} \) is set (Figures 11 and 12). The middle Case structure handles the case where the current numerical value of \( N_{xi} \) is between the set values of \( N_{xi}^{\text{min}} \) and \( N_{xi}^{\text{max}} \). Lastly, the lower Case structure handles the signal if the current \( N_{xi} \) is less than the given value of \( N_{xi}^{\text{min}} \). Then, the change factor \( \text{Presc Hi} \) is set.

Figure 11. The fragment of the diagram showing the process of comparing the set minimum and maximum states with the current state and depending on the obtained relation of selecting the next frequency division coefficient of the clock generator in the next iteration of the program.
In addition, on the application panel shown in Figure 12, one can directly read the maximum and minimum numerical values of \( N_i \) and check the parameters of the test signal, the setpoint value of the \( K \) conversion constant of the \( X/f \) converter, and the minimum and maximum value of the relative error of the test signal processing.

The colors of the curves on the charts denote: black—set waveform, blue—reconstructed waveform, orange—absolute error, purple—relative error.

The operation of an adaptive method for improving the conversion parameters of a “frequency-to-code” converter is discussed using an example of a selected design implementing continuous digital period measurement using a single counter. However, this is not the only possible structure to be used. The method can also be used in alternative structures, realizing measurement with two counters [8], the method of dependent counting [35], or any other method [3,25,34] realizing digital period measurement based on determining the product of the numerical value representing the length of the measured period and the length of the period \( T_0 \) of the clock signal from the reference generator. In these cases, decreasing the \( T_0 \) will increase the accuracy of determining the period \( T_{xi} \), while decreasing the \( T_0 \) will extend the measuring range of the “frequency-to-code” converter in the range of large values of \( T_{xi} \).

6. Results

In order to carry out the simulation, the calculations necessary for the configuration of the activation thresholds of setting the prescaler module/frequency multiplier were made. The calculations for the selected values of the resultant error \( \delta_i \) were made assuming that the \( f/N \) converter uses a clock signal with a frequency of 1MHz. The calculation results are given in Table 1.
Table 1. Calculation results of the threshold values of \( N_{\text{sh}} \).

| Error | Error/2 | \( N_{\text{sh}} \text{ min} \) | \( N_{\text{sh}} \text{ max} \) |
|-------|---------|-------------------------------|-------------------------------|
| %     | %       | -                            | -                            |
| 0.0001 | 0.00005 | 1,000,000.00                 | 779,70                        |
| 0.0002 | 0.00010 | 500,000.00                   | 1102,66                       |
| 0.0003 | 0.00015 | 333,333.33                   | 1350,47                       |
| 0.0004 | 0.00020 | 250,000.00                   | 1559,39                       |
| 0.0005 | 0.00025 | 200,000.00                   | 1743,46                       |
| 0.0006 | 0.00030 | 166,666.67                   | 1909,86                       |
| 0.0007 | 0.00035 | 142,857.14                   | 2062,88                       |
| 0.0008 | 0.00040 | 125,000.00                   | 2205,32                       |
| 0.0009 | 0.00045 | 111,111.11                   | 2339,09                       |
| 0.0010 | 0.00050 | 100,000.00                   | 2465,62                       |
| 0.0020 | 0.00100 | 50,000.00                    | 3486,91                       |
| 0.0030 | 0.00150 | 33,333.33                    | 4270,58                       |
| 0.0040 | 0.00200 | 25,000.00                    | 4931,24                       |
| 0.0050 | 0.00250 | 20,000.00                    | 5513,29                       |
| 0.0060 | 0.00300 | 16,666.67                    | 6039,51                       |
| 0.0070 | 0.00350 | 14,285.71                    | 6523,41                       |
| 0.0080 | 0.00400 | 12,500.00                    | 6973,82                       |
| 0.0090 | 0.00450 | 11,111.11                    | 7396,85                       |
| 0.0100 | 0.00500 | 10,000.00                    | 7796,97                       |
| 0.0200 | 0.01000 | 5000.00                      | 11,026,58                     |
| 0.0300 | 0.01500 | 3333.33                      | 13,504,74                     |
| 0.0400 | 0.02000 | 2500.00                      | 15,593,94                     |
| 0.0500 | 0.02500 | 2000.00                      | 17,434,55                     |
| 0.0600 | 0.03000 | 1666.67                      | 19,098,59                     |
| 0.0700 | 0.03500 | 1428.57                      | 20,628.84                     |
| 0.0800 | 0.04000 | 1250.00                      | 22,053.16                     |
| 0.0900 | 0.04500 | 1111.11                      | 23,390.90                     |
| 0.1000 | 0.05000 | 1000.00                      | 24,656.18                     |

The numerical values of \( N_{\text{sh min}} \) and \( N_{\text{sh max}} \) are given with two decimal places to accurately present the results. To configure the f/N converter, integer values that round the given values were used. The second column in the table needs an explanation. It represents half the error value in the first column. The reason is that the maximum error in the range of the high input frequencies of the f/N converter occurs during the error transitions from the negative maximum value to the positive error maximum for high frequencies. The problem is shown in Figure 13. As a result, the \( N_{\text{sh}} \) data representing two states read in the f/N converter counter causes an error with a value close to the double quantization error. Hence, the additional calculation in column 2 of the table appears.

In order to bring the simulation results closer to the real measurement, it was assumed that the test waveform would be a voltage waveform of a sinusoidal shape with a constant component of 3V, amplitude 2.85V, and frequency 1Hz. The simulation assumes that the X/f converter is perfect, and its conversion constant is 1m V/Hz.
Figure 13. Presentation of the formation of the maximum value of the quantization error.

Figure 14 shows the results of the simulation of the test signal processing by an f/N converter using the basic processing method. The effect was in line with the expectations. In the range of the high values of the instantaneous voltage, a very large influence of the quantization error $\Delta_k$ can be seen. In terms of the smallest instantaneous values of the test signal, a significant influence of the averaging error $\Delta_a$ is evident. The values of $N_{xi}$ represent the test signal ranged from 171 to 6656. The relative error of the information processing was within the range of $-0.29\%$ to $0.23\%$.

Figure 14. Results of the simulation of test signal processing by the f/N converter using the basic processing method.

Figure 15 shows the first simulation of the adaptive work of the f/N converter. The threshold values for $N_{xmin}=400$ and $N_{xmax}=1400$ were set. The waveforms obtained show that the clock generator frequency change in the range of large values is triggered at the wrong level of the $N_{xi}$ value. The quantization error was reduced only in a part of the range of higher instantaneous $u(t)$ values. In the range of the low voltage values, the adaptive work increased the changes in the processing error, but the maximum error in the discussed range remained unchanged. The instantaneous values of $N_{xi}$ varied in the
range from 200 to 3328. The information processing error \( \delta_\varepsilon \) varied from -0.245\% to 0.236\%.

Figure 15. Processing simulation results for the thresholds \( N_{\text{ximin}} = 400, N_{\text{ximax}} = 1400 \).

Figure 16 shows the simulation results of the f/N converter with the error threshold for the upper range voltages at 0.05\%, which corresponds to \( N_{\text{ximin}} = 1000 \). The lower range voltage threshold was set at 0.25\times 10^{-3}\%, which corresponds to setting the rounded value of \( N_{\text{ximin}} = 1744 \) (Table 1). The waveforms show that the threshold values have been chosen significantly better. The quantization error for the upper voltage range was reduced; also, the correction for low instantaneous voltages worked correctly. The values of \( N_{\text{xi}} \) were in the range of 342 to 4034, which shows that it is possible to increase the processing range by increasing the measurable maximum period of \( T_{\text{xi}} \). Compared to the previous simulation, the information processing error \( \delta_\varepsilon \) has been significantly reduced. Its value was within the range \(-0.146\% \div 0.143\%\).

Figure 16. The results of the simulation of processing for the thresholds \( N_{\text{ximin}} = 1000, N_{\text{ximax}} = 1744 \).

In summary, it can be stated that increasing \( f_0 \) for small values of \( T_{\text{xi}} \) periods reduces the quantization error \( \delta_\varepsilon \). Increasing \( T_{\text{s}} \) for large values of \( T_{\text{xi}} \) periods causes an increase in
the averaging error $\delta_a$, which forces an increase in the intermediate values of the processing error $\delta_\Sigma$ and a decrease in the numerical values of $N_{xi}$ representing the consecutive periods $T_{xi}$. However, the threshold value of $N_{imax}$ may be chosen such that the maximum processing error for the lower range will not change.

A question may be posed: is it permissible to set the $N_{xi}$ thresholds arbitrarily? The answer is given by the next two drawings presenting the results of subsequent simulations.

Figure 17 shows the results of the simulation of test signal processing with the threshold $N_{xi}$ set in the entire processing range of 171, which forced the f/N converter to work with the clock signal of $f_0/2$. As a result, $N_{xi}$ decreased: it changed in the range of $85 \div 3328$, but the information processing error $\delta_\Sigma$ increased noticeably. Its value was within the range $-0.586\% \div 0.58\%$.

Figure 18 shows the opposite. The clock frequency of the f/N converter was set to $2f_0$ to simulate the processing in the whole range. As a result, the regularity of the shape of the error curve $\delta_\Sigma$ increased in relation to the simulation shown in Figure 16; unfortunately, the error value remained at the same level. Doubling the frequency forced the counter to operate faster. The running value of $N_{xi}$ changed in the range of $342 \div 13313$.

![Figure 17. The results of the simulation of sinusoidal test wave processing by the f/N converter while forcing the period of the clock signal $2T_0$.](image-url)
Figure 18. Results of the simulation of test signal processing for the clock signal period of the f/N converter with a value of 0.5T0.

It can be concluded that the excessive and arbitrary increase in the frequency of the clock signal generator in the frequency-to-code converter in the incorrectly selected range of processed frequencies of the tested signal increases the demand for the counter capacity and does not give noticeable advantages in accuracy processing.

The presented simulation results for the test signal given in the article positively verify the assumptions of the method and confirm its effectiveness. It is known that the accuracy of processing and the results of information processing in the discussed system depend on the parameters of the signal x(t) and the counter capacity of the “frequency-code” converter. As the example of the resultant error plot shows (Figure5), depending on the frequency of the signal x(t) and the range of the period change Txi, different settings will be required to achieve an optimal compromise between the length of the period T0 and the capacity of the counter necessary to process the maximum required period Txi. For a waveform x(t) with different parameters, required conversion range, and required f/N converter counter volume, the threshold settings should be calculated each time, taking into account the maximum value of the conversion error occurring for the maximum frequency of the signal x(t) at the ends of the conversion range of the periods Txi.

It is reasonable to ask about the practical application of a “frequency-to-code” converter using a counter circuit to process successive periods of a variable frequency signal. The presented structure and method can be used, for example, in the case of the need to process the rotational speed and irregularity of engine rotation by means of a rotary-pulse converter [36]. Such a circuit directly produces a variable frequency signal. To convert it into a voltage signal for the conversion to digital form by an “analog-to-digital” converter would be to add another processing block generating additional errors. Other examples of transducers that directly produce a variable frequency signal include the string transducer [37] and the paddle flow transducer [38]. Moreover, in these cases, the presented direct conversion of frequency into numerical values can be advantageous. Of course, if necessary, the discussed solution can be used to process any variable frequency waveforms, e.g., from the output signals of popular “voltage-to-frequency” transducers.

7. Conclusions

The simulation studies show that the presented method of the adaptive operation of the f/N converter turns out to be effective in improving the operating parameters of the
It has been demonstrated that it is possible to select the $N_u$ threshold values to force a change in the frequency $f_0$ of the clock signal of the f/N converter, allowing to improve the accuracy of processing information about the test signal and to extend the processing range.

Possible problems that may occur with the wrong selection of the $N_u$ threshold values were indicated. It turned out that a considerable increase in the $f_0$ reduces the quantization error, unfortunately, at the same time, increasing the demand for the capacity of the counter.

It is possible to select the clock period of the f/N converter so that the maximum averaging error does not increase. The increase of period $T_o$ reduces the $N_u$ values obtained from the f/N converter counter, which allows longer $T_u$ periods to be processed. Generally, increasing $T_o$ allows to increase the lower range of measurable frequencies. The simulation results confirmed the correctness of the theoretical considerations.

The LabVIEW development environment turned out to be useful for the development of an effective and graphically readable simulator application.

**Funding:** This research received no external funding.

**Institutional Review Board Statement:** Not applicable.

**Informed Consent Statement:** Informed consent was obtained from all subjects involved in the study.

**Data Availability Statement:** The data presented in this study are available on request from the corresponding author. The data is stored in a custom format implemented in software. Some of the simulation data was stored only temporarily in computer memory while LabVIEW was processing it. If necessary, it is possible to repeat the simulations presented and generate a summary containing the necessary information.

**Conflicts of Interest:** The author declares no conflict of interest.

**References**

1. Pereira, J.M.; Postolache, O.A.; Girao, P.S. Analog to Digital Conversion Methods for Smart Sensing Systems. In *Advances in Measurement Systems*; Sharma, M.K., Ed.; InTech Open: Rijeka, Croatia, 2010.
2. Warda, P. Adaptive correction of the quantisation error in the frequency-to-code converter. In *Proceedings of the 22nd International Conference on Methods and Models in Automation and Robotics (MMAR)*, Miedzyzdroje, Poland, 28–31 August 2017; pp. 226–231.
3. Kirianaki, N.V.; Yurish, S.Y.; Shpak, N.O.; Deynega, V.P. *Data Acquisition and Signal Processing for Smart Sensors*; John Wiley & Sons, Ltd.: Chichester, UK, 2001.
4. Kurniawati, A.; Hamzah, T.; Indrato, T. A Low-Cost Transcutaneous Electrical Nerve Stimulation Measuring Device Using Frequency-to-Voltage and Current-to-Voltage. *J. Electron. Electron. Med. Inform.* (JEEEMI), 2020, 2, 65–70, doi:10.35882/jeeemi.v2i2.5.
5. Yurish, S.Y.; Kirianaki, N.V. Interface circuit design for frequency-time domain MEMS sensors. *J. Phys. Conf. Ser.* 2006, 34, 17.
6. Yurish, S.Y. Sensors and transducers: frequency output versus voltage output. *Sens. Transducers* 2004, 49, 302–305.
7. Duoshan, L.; Hefei Lianxin Power Supply Co Ltd.Inverter Direct Voltage Sampling Circuit for Concentration Storage Battery Emergency Power Supply. Chinese Patent CN107144728A, 28 May 2017.
8. Warda, P. Measurement Data Transmission in the Presence of Electromagnetic Field. In *Proceedings of the International Conference on Electromagnetic Devices and Processes in Environment Protection with Seminar Applications of Superconductors (ELMEOC & AoS)*, Naleczow, Poland, 3–6 December 2017.
9. *CTM-PER Continuous-Period Counter; User’s Guide*; Keithley MetraByte Co.: Taunton, MA, USA, 1990.
10. Helal, E.; Alvarez-Fontecilla, E.; Eissa, A.I.; Galton, I. A time amplifier assisted frequency-to-digital converter based digital fractional-N PLL. *IEEE J. Solid-State Circuits* 2021, 56, 2711–2723.
11. Swisulski, D.; Pawłowski, E.; Dorozhovets, M. Digital Processing of Frequency–Pulse Signal in Measurement System. In *Analysis and Simulation of Electrical and Computer Systems*; Springer: Cham, Switzerland, 2018; pp. 319–322.
12. Pawłowski, E. Świsulski, D. Problems with microprocessor voltage-to-frequency and frequency-to-voltage converters implementation. *Przegląd Elektrotechniczny* 2015, 91, 46–49.
13. Pawłowski, E. Spectrum analysis of measuring signals in sensors circuits with frequency output. In *Proceedings of the Optoelectronic and Electronic Sensors IV*, Gliwice, Poland, 13–16 June 2000; SPIE: Bellingham, WA USA, 2001; Volume 4516, pp. 181–186.
14. Warda, P. Error of conversion of “physical quantity-to-frequency” converter output signal. In Proceedings of the 14th International Conference on Optical and Electronic Sensors, Gdansk, Poland, 19–22 June 2016; Jasiriiski, P., Ed.; SPIE: Bellingham, WA USA, 2016; Volume 10161, doi:10.1117/12.2244496
15. Chu, L.; Wang, S.; Chen, P. Direct Current Bus Voltage Detecting Circuit of Power Unit. Chinese Patent CN202256484U, 30 May 2012.
16. Murillo, C.A.; Lóperez, B.C.; Celma, S. Voltage-to-Frequency Converters: CMOS Design and Implementation; Springer: New York, NY, USA, 2013.
17. Pawlowski, E. A simulation investigation into the signal reconstruction accuracy of the transducer with pulse frequency output. In Proceedings of the 2016 IEEE 21st International Conference on Methods and Models in Automation and Robotics (MMAR), Miedzyzdroje, Poland, 29 August–1 September 2016; pp. 762–766.
18. Palopoli, L.; Buttazzo, G.; Anciotti, P. A C language extension for programming real-time applications. In Proceedings of the Sixth International Conference on Real-Time Computing Systems and Applications RTCSA’99, Hong Kong, China, 13–15 December 1999; pp. 103–110.
19. Embarak, O. Data Analysis and Visualization Using Python; Apress: Berkeley, CA, USA, 2018; doi:10.1007/978-1-4842-4109-7.
20. Liu, J. Intelligent Control Design and MATLAB Simulation; Springer: Singapore, 2018, https://doi.org/10.1007/978-981-10-5263-7.
21. Kodosky, J. LabVIEW Proc. ACM Program. Lang. 2020, 4, 1–54. https://doi.org/10.1145/3386327.
22. Qingqing, Y.; Bin, S.; Na, Y. MATLAB Simulation for Electrically Excited Synchronous Motors with Low Switching Frequency. J. Syst. Simul. 2018, 30, 2168.
23. Nikitin, P.V.; Rao, K.S. LabVIEW-based UHF RFID tag test and measurement system. IEEE Trans. Ind. Electron. 2009, 56, 2374–2381.
24. Ying, L. The Simulation Design of PID Control Based on LabVIEW and MATLAB. In Proceedings of the 2018 International Symposium in Sensing and Instrumentation in IoT Era (ISSI), Shanghai, China, 6–7 September 2018; pp. 1–8, doi:10.1109/ISSI.2018.853212.
25. Goswami, J.C.; Hoefel, A.E. Algorithms for estimating instantaneous frequency. Signal Process. 2004, 84, 1423–1427.
26. Weltin-Wu, C.; Zhao, G.; Galton, I. A 3.5 GHz Digital Fractional-PLL Frequency Synthesizer Based on Ring Oscillator Frequency-to-Digital Conversion. IEEE J. Solid-State Circuits 2015, 50, 2988–3002, doi:10.1109/JSSC.2015.2468712.
27. Barrett, S.F.; Pack, D.J. Atmel avr microcontroller primer: Programming and interfacing. In Synthesis Lectures on Digital Circuits and Systems; Morgan & Claypool Publishers: Williston, VT, USA, 2012; Volume 7, pp. 1–244.
28. Yurish, S.Y. Intelligent opto sensors‘ interfacing based on universal frequency-to-digital converter. Sens. Transducers 2005, 56, 326–334.
29. Yurish, S.Y.; Reverter, F.; Pallas-Areny, R. Measurement error analysis and uncertainty reduction for period-and-time-interval-to-digital converters based on microcontrollers. Meas. Sci. Technol. 2005, 16, 1660.
30. Pawlowski, E. Software-based method of increasing the effective resolution of a measurement chain for a transducer with a pulse frequency output. In Proceedings of the 2017 22nd International Conference on Methods and Models in Automation and Robotics (MMAR), Miedzyzdroje, Poland, 28–31 August 2017; pp. 745–750.
31. Singh, H.K.; Bezboruah, T. Micro controller-based frequency to digital converter for interfacing frequency output sensors. In Proceedings of the 2015 International Conference on Electronic Design, Computer Networks & Automated Verification (ED-CAV), Shillong, India, 29–30 January 2015; pp. 34–37.
32. Groenwold, A.A.; Etman, L.F.P.; Snyman, J.A.; Rooda, J.E. Incomplete series expansion for function approximation. Struct. Multidiscip. Optim. 2007, 34, 21–40.
33. Inam, W.; Afridi, K.K.; Perreault, D.J. Variable frequency multiplier technique for high-efficiency conversion over a wide operating range. IEEE J. Emerg. Sel. Top. Power Electron. 2015, 4, 335–343.
34. Swisulski, D.; Hanus, R.; Zych, M.; Petryka, L. Methods of measurement signal acquisition from the rotational flow meter for frequency analysis. EPJ Web Conf. 2017, 143, 02124.
35. Kirianaki, N.V.; Yurish, S.Y.; Shpak, N.O. Methods of dependent count for frequency measurements. Measurement 2001, 29, 31–50.
36. Pawlowski, E. Simulation tests on errors of the measuring path with a frequency carrier of information. Pomiary Automatyka Kontroły 2014, 60, 607–609.
37. Tseytlin, Y.M. Vibrating Transducers. In Structural Synthesis in Precision Elasticity; Springer: Cham, Switzerland, 2006; pp. 221–264.
38. Signet 515 Rotor-X Paddlewheel Flow Sensors; Georg Fischer Signet LLC: Irwindale, CA, USA, 2020.