Estimating Bathymetry from Multi-Mission Satellite Altimetry Data Using Gravity-Geologic Method over Malaysian Seas

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This manuscript is submitted to "Terrestrial, Atmospheric and Oceanic Sciences"

Running title: Estimating Bathymetry from Satellite Altimetry Data

Three Key Points:

1. Satellite altimetry data have been utilised to derive mean sea surface height.

2. Free-air gravity anomaly was computed using Fast Fourier Technique.

3. The Gravity-Geologic Method is employed in order to estimate bathymetry

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ABSTRACT

The conventional bathymetry survey uses a single beam echo sounder (SBES) and multi-beam echo sounder (MBES). However, this technique is challenging to map large ocean areas due to complexity, cost, and time-consuming. This study aims to estimate the multi-mission satellite altimetry bathymetry across the Malaysian Seas. Six satellite altimeter missions with 11 years of data have been utilised to derive mean sea surface height (MSSH). The Gravity-Geologic Method, a conventional terrain inversion method based on gravity data, is employed in this study to estimate bathymetry using a density contrast of 1.67 g/cm$^3$. The gravity-Geologic method utilises gravity effects to be converted into bathymetry by using an inversion process. The density contrast between the bedrock and the seawater influences the predicted bathymetry. Regional gravity was removed from the observed gravity in order to determine the short-wavelength gravity effects by using the control depths from the shipborne measurements. The findings were validated and compared with shipborne bathymetry data from the National Geophysical Data Centre (NGDC) and Global Bathymetry Models. The estimated bathymetry correlation analysis, $R$, showed the highest values recorded with 0.9942. These findings reveal that the estimated bathymetry using the Gravity-Geologic Method seems to improve the accuracy of the bathymetry by 69% when compared with the ETOPO1 global bathymetry model. Nonetheless, the estimated bathymetry records 38% improvement when compared to the DTU10 global bathymetry model. The final estimated bathymetry model in this study is known as the UTM18 Bathymetry Model.
Keywords: Bathymetry; Satellite Altimetry; Gravity-geologic Method; Gravity anomaly.
1. INTRODUCTION

Topography is essential in understanding the process of the Earth. It varies from small mountain valleys to large continental landmasses, which causes weather and climate variations. Due to tectonic activity, erosion, and sedimentation transfer, changes in the land have stimulated the need for detailed topography to investigate geological occasions. While, in the ocean, marine administrations can be organised, and marine geology, biology, and physical oceanography can be discovered with detailed bathymetry information given (Sandwell et al., 2001; Rosmorduc et al., 2006; Hell, 2011; Annan and Wan, 2020). Hence, it is vital to have knowledge of ocean bathymetries.

Traditionally, accurate mapping of the bathymetric ocean floor uses echo-sounding approaches. In recent days, modern multi-beam echo sounder (MBES) techniques have made the conventional single-beam echo sounder (SBES) obsolete whereby, the use of MBES has greatly improved the accuracy, efficiency, and spatial resolution of coastal and ocean mapping (Hell, 2011). Nevertheless, this technique is challenging to use in mapping large ocean floor areas, as it is time-consuming (Carron et al., 2001; Sandwell and Smith, 2001; Smith et al., 2005; Jena et al., 2012; Minzhang et al., 2014). According to Jena et al. (2012), collecting MBES bathymetry data for unexplored offshore areas is a challenging task. As airborne, space-borne optical, or hyperspectral sensors can reveal bottom topography in shallow areas, and these systems are applicable only at a depth of
water less than tens of metres (Smith et al., 2005; Kim et al., 2019). Optical images must be analysed using the attenuation of sunlight in water, the reflectance of the bottom of the ocean, and water properties in order to predict depths using optical images (Hsiao et al., 2016; Hugue et al., 2016; Tourian et al., 2017; Kasvi et al., 2019). All in all, optical images can obtain around 20 m of maximum bathymetry depth, according to the previous studies.

Ocean surface height anomalies for uniform reconnaissance of deep-sea floor topography and bathymetry modelling on a global scale can be retrieved from space-borne radar altimetry (Smith et al., 2005; Minzhang et al., 2014; Tugi et al., 2016; Breda et al., 2019; Annan and Wan, 2020). Currently, the sounding of ships and satellite altimetry gravity anomalies has constructed all high-resolution global bathymetry models, which depend on the 20–200 km waveband gravity anomalies. Therefore, researchers must be cautious when analysing the isostatic mechanisms of the seafloor (Minzhang et al., 2014). According to Xu et al. (2009), knowledge of the global ocean before the employment of satellite altimeter missions is spatially and temporally separated by scattered observations. Subsequently, this reflected insufficient information in the global components of ocean observation. However, the measurement of sea surface height from global ocean circulation can be obtained reliably and consistently with the implementation of satellite altimeter measurements. Satellite gravity missions have provided information on the gravity of the Earth,
allowing the derivation of marine gravity anomalies to explore the ocean basin (Yildiz, 2012; Sandwell et al., 2014; Yazid et al., 2016).

The measurement of the sea surface height is the concept of satellite altimeter, which can be determined from the time back and forth of the microwave pulse emitted by the satellite altimeter to the sea surface, and the power of the microwave pulse radiation is acknowledged (Chelton et al., 2001; Din et al., 2014; Zulkifle et al., 2019; Hamden et al., 2021). The primary measurement taken by the satellite altimeter is the measurement range, satellite height above the sea surface height as well as the altitude of the satellite with relation to the ellipsoid (orbital height). Current progress in satellite altimetry has led to improvements in high-resolution marine gravity fields (Andersen et al., 2010; Yazid et al., 2016) and global bathymetric models, which provide refined depth resolutions for the South China Sea (SCS) (Sandwell et al., 2014). This paper focuses on ocean floor bathymetry estimation for the Malaysian Seas using the space-borne technique, namely, satellite altimeters, to derive the marine gravity anomalies. Subsequently, the ocean floor bathymetry is estimated from the derived marine gravity anomalies. To the best of the authors' knowledge, no such study has been done in the Malaysian region, particularly in estimating bathymetry from a space-based approach using Gravity-Geological Method and comparing it to Global Bathymetry Models.

2. DATA AND METHODS
2.1 Study Area

The research area in this study encompasses the Malaysian Seas, i.e., the Malacca Straits, South China Sea, Sulu Sea, and Celebes Sea (refer to Figure 1). The limitations of the study area are ranged from the latitude and longitude of 0º 0' 0" N to 14º 0' 0" N and 95º 0' 0" E to 126º 0' 0" E, respectively.

2.2 Satellite Altimeter Data

Several satellite altimeter missions are found globally, but only six satellite altimeter missions, namely ERS-2, Jason-1, Envisat-1, Jason-2, CrySat-2, and SARAL, are used in this paper. For satellite altimetry data processing, the Radar Altimeter Database System (RADS) is utilised to cover altimetry data from 2005 to 2015. RADS also provides the measurements of satellite orbit altitude and altimeter range from the time taken by the return radar pulse from the satellite antenna returns to the satellite receiver to achieve the sea surface height (SSH) in RADS (Yahaya et al., 2016). The MSSH is then calculated from the SSH processing. A multi-mission satellite altimeter approach was applied in this study, where altimeter missions were used, and its information is listed in Table 1. Figure 2 meanwhile depicts the individual satellite track and the combination track of the multi-mission satellite altimeter used.
The altimeter has conducted the measurement by emitting a short radiation pulse to measure the required time to reflect the pulse from the sea surface. This measurement refers to the altimeter range, $R$, and this altimeter range provides the height of the instrument above the surface of the sea. From the round-trip travel time of the pulse, an estimated value of $R$ from satellite to mean sea surface (MSS) can be acquired. Figure 3 illustrates the principle of satellite altimeter in deriving sea level data.

The data extraction for SSH can be completed after the required correction has been made. Two corrections are found in the study, namely range and geophysical correction, to obtain the SSH (Din et al., 2014; Abazu et al., 2017). The range correction for obtaining the SSH was automatically applied in this system by using Equation 1. In geophysical correction, the effect of tidal height variations, $h_T$, and the ocean surface response to atmospheric loading, $h_a$, play a significant part in obtaining the SSH. There are four components to the tidal height variations effect: ocean tide, solid Earth tide, pole tide, and load tide. As stated by Andersen and Scharroo (2011), the ocean tide is regarded to be the most critical factor in generating fluctuations in the ocean surface compared to other effects, and it is caused by the attraction forces of the astronomical bodies (moon and sun) towards the Earth, as well as the Earth's gravitational pull and rotation. Like the ocean tides, the solid Earth tide compensates for temporal variation in land and ocean surface elevations caused by
tidal deformation of the underlying non-rigid Earth, including the ocean floor, due to the moon and sun attraction (Fok, 2012).

On the other hand, the pole tides a tidal effect of both the solid Earth and the oceans to the centrifugal potential caused by minor disturbances in the Earth's rotating axis, the polar motion which occurring durations mainly of 365 and 433 days (Desai, 2002 and Fok, 2012). Furthermore, the load tide is known as a correction for variations in height caused by changes in the tide-induced forces operating on the Earth's surface and can be computed using mathematical models such as the GOT4.10 model in RADS. The effects of tidal height variations, $h_T$ (solid earth tide, pole tide, ocean tide, and load tide effects), and the ocean surface response to atmospheric loading, $h_a$, must be considered in order to achieve the dynamic sea surface height, $SSH_d$ (see Equation 3). Equation 2 is the simplification of Equation 3.

\[
SSH_{Alt} = h - (R' + \Delta R_{Dry} + \Delta R_{Wet} + \Delta R_{Ion} + \Delta R_{SSB}) \tag{1}
\]

\[
SSH_d = SSH_{Alt} - h_T - h_a \tag{2}
\]

\[
SSH_d = h - (R' + \Delta R_{Dry} + \Delta R_{Wet} + \Delta R_{Ion} + \Delta R_{SSB}) - h_T - h_a \tag{3}
\]

where $R$ = Altimeter Range
\( R' \) = the nadir that ranges from the mass centre of the satellite to the sea surface, corrected for instrument effects

\( h \) = the height of the centre of mass of satellite to the reference ellipsoid

\( \Delta R_{Dry} \) = Delay of the atmospheric refraction range caused by the dry gases' component of the troposphere.

\( \Delta R_{Wet} \) = Delay of the atmospheric refraction range caused by water vapour and cloud liquid water content of the troposphere

\( \Delta R_{Ion} \) = Delay of the atmospheric refraction range caused by the free electron content of the ionosphere

\( \Delta R_{SSB} \) = range correction caused by the interaction of the large radar footprint and the sea surface.

The Sea State Bias (SSB) combines correction of the electromagnetic, skewness, and tracker biases.

\( h_T \) = tidal height variations (solid earth tide, pole tide, ocean tide, and load tide effects)

\( h_a \) = the ocean surface response to the atmospheric loading

Figure 4 illustrates the SSH processing flow in RADS. All data corrections are related to the user preferences and data types in the RADS system. The corrections applied in this study are summarised in Table 2. Crossover adjustment is carried out to limit errors in the satellite track and other long wavelength errors by minimising height differences between the ascending and
descending tracks at a crossover location (Hamid et al., 2018; Hamden et al., 2021). Subsequently, data filtering and data gridding are also implemented. The data provided by RADS is daily solution data is then processed to obtain climatology data in the form of average data. Afterward, the data obtained is filtered to ensure that the obtained data is free from errors of un-modelled tides, orbit error, or residual sea surface height variability (Andersen, 2008; Din et al., 2019) and then gridded. This paper employed a filter value of 2.0 and a block size or cell size of 0.25 degrees for the data grid.

2.3 Marine Gravity Anomaly from Satellite Altimeter

Three essential steps are employed to obtain the final output of the derived Free Air Gravity Anomaly (FAGA) from satellite altimetry data, which are the selection of the appropriate global FAGA from Global Gravity Models (GGMs), FAGA derivation using GRAVSOFT, and the validation of satellite-derived FAGA. In addition, the Least-Squares Modification of Stokes with Additive Corrections (LSMSA) method is used to obtain geoids based on the Stokes formula modifications. Computed geoid ($N_c$) is corrected with signal and noise corrections, the Residual Terrain Model (RTM), topographic correction, ellipsoidal correction, and atmospheric correction. After the geoid computation is completed, the gravity anomaly is derived using the Fast Fourier Transformation (FFT) technique.
According to Salam (2005), the gravity anomaly can be derived from the MSSH using Fast Fourier Transformation (FFT) technique and to implement this technique, GRAVSOFT software is used to derive the gravity anomaly of satellite altimeter under the GEOFOUR program. The FFT formula used in deriving the MSSH to the gravity anomaly is denoted in Equations 4 and 5 (Schwarz et al., 1990; Forsberg and Tscherning, 2003; Sandwell, 2004; Salam, 2005) as follows:

\[
F \left\{ (x, y, z) \right\} = F(u, v, w) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(x, y, z) e^{-2\pi i (ux + vy + wz)} \, dx \, dy \, dz
\]

\[
F^{-1} \left\{ (u, v, w) \right\} = F(x, y, z) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(u, v, w) e^{-2\pi i (ux + vy + wz)} \, du \, dv \, dw
\]

From Equations 4 and 5, the value of u, v, and w represent the frequency domain data of the spatial coordinate of x, y, and z, while i is the imaging unit (i=\sqrt{-1}). The symbol F represents the FFT function, while the F^{-1} is the inverse FFT function. The FFT technique is implemented in the GEOFOUR program to derive the gravity anomaly to the geoid or vice versa. The information of MSSH can be assumed as the geoid undulation, while N can be estimated using the Stokes Integral (Heiskanen and Moritz, 1967; Salam, 2005). The FFT implemented in the GEOFOUR program is the planar Stokes Integral, which can be clarified using Equation 6 as follows:

\[
N(x, y) = \frac{1}{2\pi g_\circ} \int \int \frac{\Delta g(x', y')}{\sqrt{(x-x')^2 + (y-y')^2}} \, dx' \, dy'
\]
where \( \Delta g \) = the gravity anomaly

\( g_o \) = the average of the gravity or the normal gravity

The cross-validation process is applied for the chosen satellite-derived free-air gravity anomaly (FAGA) for further computation. Hence, in this study, Surfer Software has been used to execute the cross-validation process in calculating the gridded error of the observation. The original data set is then given the known values for the geoid (N) observation location, and this information has been used to evaluate the grid error for the relative quality of the grid data (Golden Software, 2002). The gridded error is calculated by eliminating the first data set observation, and the remaining data are used to interpolate the value of the eliminated observation by using a specific interpolation algorithm at the same location of the deleted point. The new satellite-derived FAGA (filtered satellite-derived FAGA) dataset will be used to estimate the bathymetry after the interpolation process. Figure 5 shows the flowchart of the gravity anomaly derivation from the satellite altimeter.

\( N_{GGM} \) represents the geoid from the global geopotential model (GGM), while \( \Delta g, \Delta g_r, \Delta g_{GGM}, \) and \( MDT_{DTU15} \) represent the altimeter-derived gravity anomaly, the residual gravity, the gravity anomaly from the GGM model, and the mean dynamic topography model (MDT) 15 from DTU, respectively.
In this study, three filtering processes are used with seven different interpolation methods to acquire better results. Residual filtering is classified in Table 3, and from the results, only the best results are selected, and their RMSE and correlation values are then evaluated. The residual removal process has been executed parallel with the deletion of the satellite-derived FAGA at the same point as the residuals exceeded. The remaining derived-FAGA has been interpolated using the Surfer interpolation method, where the cell size of the interpolation is 0.25° and 0.1°. The size of the 0.25° cell is implemented to comply with the original size of the SSH primary satellite altimeter data. The size of 0.25° is approximately 27.75 km, while the size of 0.1° is approximately 11.1 km. This indicates that one observation is available for every 27.75 km and 11.1 km.

This interpolation is required in the grid creation of the long-wavelength gravity field, represented by the generation of regional gravity anomalies \( g_{REG}(i) \) using the Gravity-Geologic Method in the bathymetry estimation. Therefore, the interpolation method has to be selected, and in doing so, seven interpolation methods are tested to narrow down the selection of interpolation.

### 2.4 Computation of Bathymetry using Gravity-Geologic Method

A total of 12,362 points of shipborne bathymetry obtained from the National Geophysical Data Centre (NGDC) are employed to estimate the bathymetry with 6584 points used in the computation, while the remaining 5778 points are used in the validation process. A total of 6584 points of
shipborne bathymetry are used to compute the residual gravity by obtaining the regional gravity for the study area. Figure 6 shows the shipborne track of bathymetry, which was divided into two different colours. The green point data is utilised in the computation process, while the yellow points represent the data used in the validation process. The computation and validation data classifications were chosen randomly according to the coverage of the shipborne area. In this paper, the Gravity-Geologic Method is used to predict the bathymetry. The input data for the bathymetry prediction is the derived-FAGA from multi-mission satellite altimetry data.

According to Kim et al. (2010), the residual of the gravity effects is essential information for the acquisition of short-wavelength signals, and these signals are used to predict the depth of the bedrock. From this computation, the depth undulation can be predicted. Figure 7 shows the Gravity-Geologic Method geometry and the computed parameter related to the computation (Hsiao et al., 2010).

Two types of gravity field signals are produced, namely the shorter wavelength and the longer wavelength. The information from the shorter wavelength gravity field, residual gravity ($g_{RES}$), is generated based on local depth variations from the shipborne measurement (control points). The deepest depth of the shipborne measurement ($D$) represents the reference datum used in the Bouguer plate measurement. Meanwhile, a longer wavelength gravity field, regional gravity ($g_{REG}$)
is produced from the deeper mass variations. Then, the final depth was computed from the residual gravity (Hsiao et al., 2010; Wei et al., 2021).

Besides, by combining residual gravity \((g_{RES})\) with the regional gravity \((g_{REG})\), the observed Bouguer gravity anomaly \((g_{OBS})\) can be obtained. Equation 7 shows the \(g_{OBS}\) linear computation and the connection between \(g_{REG}\) and \(g_{RES}\). The subscript \(j\) indicates the control points with the measured depth; while subscript \(i\) represent the unmeasured depth of control points.

\[
g_{OBS}(i) = g_{RES}(i) + g_{REG}(i)
\]  \(\text{(7)}\)

According to Kim et al. (2010), the measured depth at the \(jn\) control point is assumed to be used in the estimation of the residual gravity field of the bedrock \((g_{RES})\), which produces the effect of the shorter wavelength from a simple Bouguer slab formula listed in Equation 8. Figure 7 shows the geometry of the Gravity-Geologic Method and the downward continuation method.

\[
g_{RES}(j) = 2\pi G (\Delta \rho) (E(j) - D)
\]  \(\text{(8)}\)

where;
\( G = \text{Gravitational constant, } 6.672 \times 10^{-8} \text{ cm}^3/\text{g sec}^2 \)

\( \Delta \rho = \text{Density contrast between seawater and bedrock (g/cm}^3\) \)

\( E (j) = \text{Depth at the } j^{th} \text{ control point (in meter)} \)

\( D = \text{The deepest depth of the control points as a reference datum (in meter)} \)

The importance of the control points is to determine the shorter wavelength effect in order to generate the regional gravity at the location of the control point. The residual of gravity represents the effect of the bedrock surface at the control point. This residual has been eliminated from the observed gravity Bouguer to obtain the estimated regional gravity (\( g_{\text{REG}} \)) that will represent the effect of the longer wavelength. Equation 9 shows the computation of the regional gravity field at the control point (\( g_{\text{REG}}(j) \)).

After \( g_{\text{REG}} (j) \) has been acquired, the regional gravity of the unmeasured depth \( i, g_{\text{REG}}(i) \) can be determined by interpolating the regional gravity \( g_{\text{REG}}(j) \) generated at the measured depth, \( j \) (control points), creating a gridded regional surface for the longer wavelength effect. Subsequently, the regional gravity that has been estimated at site \( i \) (\( g_{\text{REG}}(i) \)) is deducted from the observed gravity, \( g_{\text{OBS}}(i) \) in order to achieve the estimated residual of the gravity (\( g_{\text{RES}}(i) \))(see Equation 10).
\[ g_{\text{REG}}(j) = g_{\text{OBS}}(j) - g_{\text{RES}}(j) \] (9)

\[ g_{\text{RES}}(i) = g_{\text{OBS}}(i) - g_{\text{REG}}(i) \] (10)

A mass change below the ocean floor has caused the density contrast between seawater and the ocean floor to vary differently. It is known that the density \( (\rho) \) is 1.03 g/cm\(^3\) and 2.70 g/cm\(^3\) for the seawater and ocean floor bedrock. In the application of the Gravity-Geologic Method, the density contrast between the seawater and the ocean floor bedrock \( (\Delta \rho) \) with the assumed value of 1.67 g/cm\(^3\) is applied. According to Kim et al. (2010), the ocean floor bedrock density in the crust can be assumed to be between the mean range of 2.67 g/cm\(^3\) and 2.73 g/cm\(^3\). Essentially, the theoretical value of the density contrast (1.67 g/cm\(^3\)) may be higher than the specified value, as the derived-FAGA from satellite altimeter that has been compiled on the sea surface in Gravity-Geologic Method is affected by the ocean bottom sources (Roman, 1999; Kim et al., 2010).

An assessment of the global bathymetry model has been executed before the bathymetry computation using the Gravity-Geologic method is done where it is executed using the validation points obtained from NGDC (5778 points) of the shipborne bathymetry. In addition to that, this assessment has been conducted to determine the ocean depth differences between each model and apart from the validation points from the shipborne bathymetry. In this assessment, four bathymetry models, namely DTU10, ETOPO1, GEBCO, and Sandwell V18.1, are extracted from the global
bathymetry models. The validation points recorded in this study are around 5778 points, which subsequently followed the validation points of the shipborne bathymetry location.

3. RESULTS AND DISCUSSION

3.1 Statistical Analysis of the Global Bathymetry Models and the Shipborne Bathymetry

The data analysis of the global bathymetry models and the shipborne bathymetry from NGDC (refer to Figure 6) are listed in Table 4, including the minimum and maximum depth, the average of the data, and the standard deviation for both types of data used. Table 4 shows that the minimum depth value for the shipborne bathymetry data is -9.00 m, and the standard deviation of the data for the shipborne is 901.140 m. On the other hand, for the global bathymetry models, the model that logged the deepest depth is Sandwell V18, with -3452.180 m, while the DTU10 model recorded the minimum depth with the value of -1.421 m. The model with the nearest standard deviation value of the shipborne bathymetry data is the Sandwell V18.1 model with 904.147 m.

3.2 Statistical Analysis of the Type of Filter and the Interpolation Method

Earlier in Section 2.3, seven interpolation methods were used to grid the satellite altimeter Faga. Figure 8 shows the illustration of the gridded satellite altimeter Faga. As shown in Figure 8, the Local Polynomial method (Figure 8c) is not appropriate to be employed for deriving the satellite-
derived FAGA as it only gives values to grid nodes using a weighted least-squares fit on data contained inside the grid node's search area (Golden Software, 2002). The gridded factor used was the First Order polynomial with a power of 2. As for the computed bathymetry using Gravity-Geologic Method, the estimation is made according to the type of filter used, with a different interpolation method effect, with a cell size of 0.1° x 0.1° (~11 km). The interpolation size is chosen to be smaller than the original data size of SSH from the satellite altimeter, which is 0.25°, in order to get a better resolution of the estimated bathymetry. This assessment is executed to visualise the depths difference and the distinction between the bathymetry models and the ground truth data used (NGDC shipborne data).

All the statistical analyses explained in this section are done to examine the accuracy of the estimated bathymetry obtained using the Gravity-Geologic Method. Figure 9, which represents the RMSE value for all the estimated bathymetry, uses different colours of the bar to differentiate the type of filter applied to the satellite-derived FAGA. From the plotted results, the graph and RMSE values displayed are recorded to point at the minimum curvature interpolation since this interpolation method produces the lowest RMSE value. Filter 1 indicates the lower RMSE value with ±96.949 m compares to the other filter applied. However, the nearest neighbour and kriging interpolation method follow quite close to the RMSE values when Filter 1 is employed. Nevertheless, the minimum curvature is chosen since it gives a better RMSE value.
Surfer software executes the interpolation process. Several explanations concerning the minimum curvature interpolation are suggested in the literature, where according to Yang et al. (2004), the use of the minimum curvature is common in the earth sciences. From this interpolation, the resulting surface is analogous to a thin, linearly elastic plate that passes through each data value with a minimum amount of bending. Apart from that, previous studies conducted by Yang et al. (2004) and Vohat et al. (2013) suggest that interpolation produces the smoothest possible surface while respecting the data as closely as possible.

The grid from this interpolation is generated by repeatedly applying an equation over the grid in order to smooth the grid (Vohat et al., 2013). Hence, this method is believed to be the most suitable interpolation method here. However, the interpolation method yields the poorest RSME values in the radial basis function. All filters that are applied to radial basis function interpolation gave RMSE values of more than 200 meters. Conversely, the radial basis function fits with the source data, producing a smooth surface. Despite that, minimum curvature interpolation has been chosen as it practically yields the best-estimated bathymetry output in this study, and RMSE value is used as the indicator in choosing the best-estimated bathymetry. This minimum curvature method is also known as exact interpolators, as they seek to respect the data used in the study (Yang et al., 2004; Vohat et al., 2013).
From previous studies, minimum curvature interpolation has been mainly used to estimate the bathymetry using the Gravity-Geologic method (Sandwell and Smith, 2001; Roman, 1999; Kim et al., 2011). Therefore, towards selecting the final estimated bathymetry, the minimum curvature with Filter 1 is chosen as the best output. Concerning the final estimated bathymetry, the estimated bathymetry Filter 1 from minimum curvature interpolation, an alternative name has been made, namely the UTM18 Bathymetry Model. The UTM18 Bathymetry Model has been used to simplify the final estimated bathymetry in this study and to match with other global bathymetry models. Since the best-estimated bathymetry goes to the minimum curvature with the implementation of Filter 1, the gravity anomaly information used in the computation is charted.

### 3.3 Computation of Gravity Anomaly and Density Contrast Selection

Figure 10 illustrates the three components of gravity used in this study, namely the regional, residual and observed gravity anomaly. The comparison of all these components are plotted to visualise the pattern of gravity anomaly in order to calculate the bathymetry specifically at the latitude of 6.5°N and along the longitude 108°E to 112°E. Analysis along the longitude was made in accordance with the variability of the seabed from shallow water to deep water.

Figure 10 shows the \( g_{\text{obs}}(i) \) and the computed gravity anomaly, namely \( g_{\text{reg}}(i) \) and \( g_{\text{res}}(i) \), in which these three components of gravity anomaly are used in estimating the bathymetry. Based on the line graph plotted, the \( g_{\text{res}}(i) \) represents the short-wavelength information since it is computed...
based on the observation \((g_{\text{obs(i)}})\) and the regional gravity \((g_{\text{reg(i)}})\) data. Nevertheless, \(g_{\text{reg(i)}}\) is smoother than the residual gravity \((g_{\text{res(i)}})\) since the regional gravity represents the long-wavelength effects (Hsiao et al., 2010). With the readiness of these three gravity components, the production of the estimated bathymetry can be done smoothly.

The density contrast value used in the computation is approximately 1.67 g/cm\(^3\). With the implementation of the Gravity-Geologic method computation, a stronger and homogeneous density contrast between the seawater and the bedrock is applied. The depth to the marine density contrast also tends to be more profound. Therefore, the marine Bouguer slab calculations are not significantly affected by the effects of subsurface density errors (Kim et al., 2011).

### 3.4 Statistical Analysis of the Estimated Bathymetry Model with Shipborne Bathymetry and Global Bathymetry Models

Figure 11 (a) illustrates the best-estimated bathymetry using the Gravity-Geologic Method in which it is executed in a small area at the South China Sea, since this area has recorded several shipborne bathymetry data in various depth levels, from shallow to the deep ocean. Regarding Figure 11 (b), the bathymetry computed shows the maximum depth of approximately -3400 metres, while the minimum depth is less than -100 metres. The bathymetry is deeper as the longitude increases, from the west to the east part of the South China Sea, and is considered the deep ocean. Figure 11 (b)
reveals that the deep basin of this study area lies between 110°E to 114°E. The statistical analysis of the estimated bathymetry afterward is then evaluated.

The assessment of the selected estimated bathymetry is executed by comparing the UTM18 Bathymetry Model with the global bathymetry models to examine their depth differences with the ground truth data (validation data). Figure 12 shows the bathymetric profile along 6.5°N latitude and from 108°E to 112°E of longitude. In comparison, 4 global bathymetry models found in this study are used: ETOPO, GEBCO, Sandwell V18.1, and DTU10. From the results collected, the estimated bathymetry from Gravity-Geologic Method seemed to fit better with the NGDC shipborne bathymetry compared to other bathymetry models. This is because the data used for the computation is taken directly from the shipborne and considered the high-frequency bathymetry (short-wavelength) (Roman, 1999).

Moreover, the bathymetry predicted from Gravity-Geologic Method was influenced by the variation of the seabed terrain and the relative depth of the predicted area. Based on Figure 12, predicted bathymetry at longitude 111°E to 112°E shows the largest deviation compared to another longitude. Meanwhile, the bathymetry predicted using Gravity-Geologic Method (UTM18) is closer to NGDC data than the other global models. As the Gravity-Geologic method used the deepest depth from the computation data (NGDC depth) as a reference datum, this information was relatively used in predicting bathymetry. The increase of the depth may improve the predicted bathymetry. Another
factor for enhancing the predicted bathymetry is the estimation of the density contrast between the seawater and seabed topography.

Correspondingly, from the results shown in Figures 10 and 12, the pattern of the $g_{res(i)}$ and the estimated bathymetry from the Gravity-Geologic Method are reasonably similar since the gravity starts to decrease as the bathymetry goes deeper. The depth variation for the UTM18 Bathymetry Model and the global models is listed in Table 4, presenting the minimum, maximum, mean, and standard deviation of the bathymetries. This information is described to capture the variation of the Gravity-Geologic Method bathymetry with the NGDC shipborne and the global models used. Importantly, the statistical analysis of the differences between the estimated bathymetry and the global bathymetry models with the ground truth data (NGDC data) is presented in Table 5. The minimum, maximum, mean, and standard deviation of the UTM18 bathymetry information are -3499.200 m, -22.696 m, -1408.290 m, and 893.4105 m, respectively.

Based on the results shown in Table 5, it can be concluded that the estimated bathymetry from the UTM18 Bathymetry Model yields a better RMSE value compared to other bathymetry models. The UTM18 Bathymetry Model gives the lowest RMSE values with ±96.949 m accuracy, while ETOPO1 shows the poorest RMSE value with approximately ±314.359 m. The correlation analysis ($R$) of the UTM18 Bathymetry Model shows the highest values recorded with 0.9942. These
findings have revealed that the estimated bathymetry using the Gravity-Geologic Method appeared to improve the accuracy of the bathymetry by 69% when compared to ETOPO1 global bathymetry. Nonetheless, UTM18 Bathymetry Model recorded 38% improvement when compared to the DTU10 global bathymetry model.

According to Hsiao et al. (2010) and Kim et al. (2010), the accuracy of the Gravity-Geologic Method estimated bathymetry can be about 20 m to 40 m and ±74 m at the deep ocean. Regardless of other studies mentioned, the best RMSE result obtained through this study is ±96.949 m, which is quite large compared to previous studies. However, the types of data used, such as the shipborne bathymetry and the gravity anomaly data, as well as the density contrast parameter, might have contributed to this accuracy separation. The statistical analysis of the UTM18 Bathymetry Model with the other four global bathymetry models used is summarised, and all values are shown in Table 6. The analysis included the minimum, maximum, and mean differences, standard deviation, RMSE, and correlation. Additionally, these analyses were executed to attest to the consistency of the UTM18 Bathymetry Model with other global bathymetry models for bathymetry mapping.

Based on Table 6, the largest depth difference is recorded from the ETOPO1 bathymetry model, with a value of 1764.744 m. The estimated bathymetry from the UTM18 Bathymetry Model and DTU10 global bathymetry model shows a good correlation value of 0.99931 and reveals the lowest
RMSE value compared to other bathymetry models. Nevertheless, the UTM18 Bathymetry Model matches well with all the global bathymetry models, as all of the correlations are approximate to 1.

The histogram (in Figure 13) and scatter plot (in Figure 14) on the depth differences are also plotted, which subsequently illustrates the separation between the estimated bathymetry with the existing global bathymetry models, as well as the validation points (checkpoints). Figure 13 consists of five histograms, starting with the differences between the UTM18 Bathymetry Model, NGDC shipborne, and the global bathymetry model; a) NGDC shipborne, b) DTU10 bathymetry model, c) ETOPO1 bathymetry model, d) GEBCO bathymetry model, e) Sandwell V18.1 bathymetry model.

Generally, most of the depth differences lie between ±500 m. Nevertheless, according to the final result of the computation, the estimated bathymetry of UTM18 shows a good correlation with the NGDC shipborne bathymetry. It can be seen that the depth differences for the UTM18 Bathymetry Model lie between ±200 m, but most of the differences are in the range of ±50 m. There are more than 2500 points, which are recorded to have a depth difference between mentioned ranges. When compared to another global bathymetry, it appears that the depth differences from Sandwell global model lie between -200 m to 500 m. However, more than 2500 points have small depth differences compared to other global models. As for ETOPO1 bathymetry, some of the points have depth differences that exceeded ±500 m.
From the depth differences recorded, their distributions corresponding to the depth are plotted on the scatter plot in Figure 14. The distributions of the differences are also combined into the exact figure for the sake of understanding the distinction between each bathymetry model. As shown in Figure 14, most of the point differences lie between ±500 m. However, the difference recorded is significant between the depths of -500 m to -3000 m, especially for the Sandwell and ETOPO1 bathymetry models. Overall, the separation of the depths lies between ±500 m.

As mentioned earlier in this section, the estimated bathymetry in this study has a relatively large RMSE value, which is ±96.949 m. This may be due to the dynamic surface of the ocean may have influenced the accuracy of the estimated bathymetry due to the fluctuation of the ocean. Subsequently, the comparison between the global bathymetry models is conducted to evaluate the estimated bathymetry computed based on Gravity-Geologic Method (UTM18 Bathymetry Model), not to contend with the existing global bathymetry model.

Figure 14 discloses that the UTM18 Bathymetry Model has the most harmonious depth differences distribution where the majority of the differences lie at approximately ±250 m, with other points scattered outside that range. In contrast, some of the depth differences for the ETOPO1 model appeared to have deviated up to 2000 m. This result shows a resemblance outcomes obtained from
the study conducted by Kim et al. (2010), which recorded a depth difference of up to -2128.4 m from the comparison between shipborne bathymetry data and ETOPO1.

From the scatter plot, it can be summarised that the UTM18 Bathymetry Model has a good relationship with the NGDC shipborne data. Moreover, since 6584 points of shipborne measurement are included in the Gravity-Geologic Method computation, the accuracy of the estimated bathymetry can be enhanced and improvised. As the final output of the study, the map of the bathymetry for the Malaysian Seas has been plotted successfully. Figure 15 illustrates the UTM18 Bathymetry Model, covering the Malaysian Seas. Apart from that, the depth assimilation from Sandwell V18.1 Bathymetry Model is exploited for the area with no shipborne data and terrain area coverage due to sparse shipborne data. Figure 16 portrays the topography of the ocean over the Malaysian Seas, including the terrain area. From this figure, the undulation of the ocean topography can clearly be seen. The maximum depth for each sea is also gathered from the bathymetry computation. Table 7 summarises the maximum and the average depth of each sea along the latitude and longitude of 0ºN - 14ºN and 95ºE - 126ºE, respectively.

According to the results obtained from the bathymetry computation, the maximum depth for the Celebes Sea is -6100.990 m. Meanwhile, the Malacca Straits have been recorded with the shallowest bathymetry of -171.771 m. As for the South China Sea and the Sulu Sea, the deepest depth of these oceans turned out to be -5596.160 m and -5075.860 m, respectively. This information
has revealed that the Celebes Sea has the deepest ocean curvature compared to other seas. The bathymetry information gathered for each sea can be utilised for the exploration of the ocean, as well as to garner a better understanding of the ocean topography. Moreover, the uses of satellite altimeter with the combination of shipborne bathymetry data manage to estimate the mesoscale bathymetry information successfully. In brief, it can be postulated that the bathymetry computed by using the Gravity-Geologic Method can be easily upgraded with future satellite and shipborne measurements (Kim et al., 2010).

4. CONCLUSION

Over the years, the conventional technique in acquiring bathymetry has provided the most accurate bathymetry. However, this technique has its limitation, which can be overcome by using satellite altimeters. Satellite altimeter data can be used to obtain the gravity anomaly and can be used to predict the ocean bathymetry in extensive coverage without consuming the time it takes to obtain the data. This study proves that the gravity anomaly derived from satellite altimeter and satellite gravity mission is reliable in estimating the bathymetry of the ocean. With the combination of gravity anomaly from the satellite gravity missions, the acquired gravity anomaly data are dense, thus improving the result of this study, aiming to get a good estimation of bathymetry.
The use of Filter 1 (removal of the > ±100 m residual) also supports the computation of the bathymetry towards a better accuracy. Based on this computation, the RMSE value for the estimated bathymetry is ±96.949 m. Using the minimum interpolation method in the Gravity-Geologic method has improved the computed bathymetry compared to other interpolation methods applied. UTM18 Bathymetry Model has also revealed that its accuracy has improved by 69% compared to the ETOPO1 global bathymetry model. This condition demonstrates the reliability of the Gravity-Geologic method and bathymetry from the space-based technique.

In general, the computation of bathymetry using the Gravity-Geologic method required shipborne bathymetry as the ground reference or as a datum. Nevertheless, the estimated bathymetry produced by using the Gravity-Geologic method is not recommended for the navigational purpose since this computation includes the interpolation procedures, and also, the bathymetry is not referred to as the lowest astronomical tide (LAT). The consistency of the Gravity-Geologic method predictions with bathymetry estimated from other models attests to the effectiveness of the Gravity-Geologic method for bathymetry mapping. Undeniably, the predictions are not unique, and thus, the estimates must compute with care. All in all, the analytical simplicity of the Gravity-Geologic method makes it easy to update the bathymetry estimation once the new and improved data on the FAGA and bathymetric observations have emerged.
Acknowledgments

The authors are grateful to the National Geophysical Data Centre (NGDC) and the International Centre for Global Earth Model (ICGEM) for providing shipborne bathymetry and gravity anomaly data, respectively. Special thanks also to TU Delft, NOAA, Altimetrics LLC for providing altimetry data through the RADS server. This project is funded by the Ministry of Higher Education (MOHE) under the Fundamental Research Grant Scheme (FRGS) Fund, Reference Code: FRGS/1/2020/WAB07/UTM/02/3 (UTM Vote Number: R.J130000.7852.5F304).
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## Figure legends

| Figure Number | Figure Caption |
|---------------|----------------|
| 1             | Limitation for the study area. |
| 2             | Individual satellite track and the combination track from multi-mission Satellite Altimeter (ERS-2, Jason-1, Envisat-1, Jason-2, CryoSat-2 and SARAL). |
| 3             | Satellite Altimeter measurement in obtaining the sea surface height |
| 4             | Flowchart of the RADS Processing. |
| 5             | Flowchart of the derivation of gravity anomaly from MSS |
| 6             | Shipborne points used to estimate the bathymetry. |
| 7             | Geometry of the Gravity-Geologic Method (Hsiao et al., 2010). |
| 8             | The gridding method available in Surfer 8. a) IDTP, b) Kriging c) Local Polynomial, d) Minimum Curvature, e) Nearest Neighbour, f) Radial Basis Function g) Triangulation with Linear Interpolation (Units are in mGal). |
| 9             | The RMSE value for the estimated bathymetry based on the type of filter and the interpolation method used (green box shows the interpolation method used in obtaining the lowest RMSE value). |
| 10            | The regional (g_reg(i)), the observed (g_obs(i)), and the residual (g_reg(i)) gravity anomaly at the latitude of 6.5°N. |
| 11            | Estimated bathymetry with the minimum curvature interpolation from Filter 1; a) Map of the estimated bathymetry, b) The topography surface of the estimated bathymetry. |
| 12            | Comparison for bathymetry along the latitude of 6.5°N. |
| 13            | Bathymetry differences between UTM18 Bathymetry Model (using Gravity-Geologic Method) and a) NGDC shipborne, b) DTU10 bathymetry model, c) ETOPO1 bathymetry model, d) GEBCO bathymetry model, e) Sandwell V18.1 bathymetry model. |
| 14            | Scatter plot for the distribution of the depth differences. |
| 15            | UTM18 Bathymetry Model. |
| 16            | Topograsurface of UTM18 estimated bathymetry. |
Illustrations

Figure 1
The Combination of Multi-mission Satellite Altimetry

Figure 2

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Figure 3
Figure 4
MSS Derivation from Satellite Altimeter

Residual Sea Surface Height, $h_{\text{residual, derivation}}$

a) MSS – $N_{\text{GGM}}$
b) MSS – MDT_{DTU15} - $N_{\text{GGM}}$

Altimeter-derived Gravity Anomaly (Remove-restore)
$\Delta g = \Delta g_{e} + \Delta g_{\text{GGM}}$

Gravity Anomaly Blunder Detection (Gravity Anomaly Screening Method)
- Cross validation

Regridding of Gravity Anomaly

Figure 5
The Shipborne Track of Bathymetry

Figure 6
Figure 7
Figure 9
Figure 10

Gravity Anomaly Component

![Graph showing gravity anomaly component with lines for g_obs(i), g_reg(i), and g_res(i).]
Figure 11

Estimated Bathymetry with Minimum Curvature Interpolation (Filter 1)

b)

Depth (m)

Latitude

Longitude
Comparison between Bathymetry

![Comparison between Bathymetry](image)

Figure 12
Bathymetry Differences between UTM18 and NGDC Shipborne

Bathymetry Differences between UTM18 and DTU10 Model

Bathymetry Differences between UTM18 and ETOPO1 Model

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Figure 13
Figure 14

UTM18, DTU10, ETOPO1, GEBCO and Sandwell V18.1 Model vs NGDC Shipborne
Figure 15
### Tables

| Satellite Altimeter | Phase | Mission Period       | Cycle |
|---------------------|-------|----------------------|-------|
| ERS-2               | A     | 29 Apr 1995 – 04 Jul 2011 | 000 – 169 |
| Jason-1             | A     | 15 Jan 2002 – 26 Jan 2009 | 110 – 260 |
|                     | B     | 10 Feb 2009 – 03 Mar 2012 | 262 – 374 |
|                     | C     | 07 May 2012 – 21 Jun 2013 | 382 – 425 |
| Envisat-1           | B     | 14 May 2002 – 22 Oct 2010 | 033 – 113 |
|                     | C     | 26 Oct 2010 – 08 Apr 2012 |       |
| Jason-2             | A     | 04 Jul 2008 – 31 Dec 2015 | 000 – 276 |
| CryoSat-2           | A     | 14 Jul 2010 – 31 Dec 2015 | 004 – 074 |
| SARAL               | A     | 14 Mar 2013 – 31 Dec 2015 | 001 – 030 |

**Table 1:** Satellite Altimeter Missions used in this study (summarised from RADS, 2017).
| Correction/Model          | Limit (m) | Description                                           |
|--------------------------|-----------|-------------------------------------------------------|
| Orbit/Gravity field      | -         | All satellites: EIGEN GL04C                            |
|                          |           | ERS: DGM-E04/D-PAF                                    |
| Dry troposphere          | -2.4      | All satellites: Atmospheric pressure grids (ECMWF)    |
| Wet troposphere          | -0.6      | All satellites: Radiometer measurement                |
| Ionosphere               | -0.4      | All satellites: Smoothed dual-frequency, ERS: NIC09    |
| Dynamic atmosphere       | -1.0      | All satellites: MOG2D                                  |
| Ocean tide               | -5.0      | All satellites: GOT4.10                                |
| Load tide                | -0.5      | All satellites: GOT4.10                                |
| Solid earth tide         | -1.0      | Applied (Elastic response to tidal potential)          |
| Pole tide                | -0.1      | Applied (Tide produced by Polar Wobble)               |
| Sea state bias           | -1.0      | All satellites: CLS non-parametric ERS: BM3/BM4 parametric |
| Reference Engineering flag | -1.0      | DTU13 mean sea surface                                |
| Applied reference frame biases (cm) | -       | Jason-1                                               |

Table 2: Correction and models applied for RADS altimetry data processing.
| No. | Filtering of Cross-Validation                                                                 |
|-----|-------------------------------------------------------------------------------------------|
| Filter 1 | Removing the Δg residual that is more than 100 mGal (> 100 mGal)                          |
| Filter 2 | Removing the Δg residual that is more than 50 mGal (> 50 mGal)                           |
| Filter 3 | Removing the Δg residual that is more than 20 mGal (> 20 mGal)                           |

**Table 3:** The Δg cross-validation testing.
| Model          | Max     | Min     | Mean    | Std Dev |
|---------------|---------|---------|---------|---------|
| NGDC shipborne| -3444.000 | -9.000  | -1406.490 | 901.1403 |
| DTU10         | -3316.410 | -8.950  | -1380.880 | 882.0025 |
| ETOPO1        | -3468.500 | -5.000  | -1306.090 | 906.0392 |
| GEBCO         | -3431.680 | -1.421  | -1386.120 | 885.4462 |
| Sandwell V18.1| -3452.180 | -7.028  | -1345.020 | 904.1465 |

**Table 4:** Bathymetry data analysis for the shipborne and the bathymetry models (Units are in metres).
| Bathymetry Model | Max Diff. | Min Diff. | Mean diff. | RMSE | Correlation Analysis | Improvement Percentage (%) |
|------------------|-----------|-----------|------------|------|-----------------------|-----------------------------|
| UTM18            | 496.630   | -1089.700 | -1.808     | 96.949 | 0.9942                | -                           |
| ETOPO1           | 2019.201  | -856.712  | 100.396    | 314.359 | 0.9457               | 69                          |
| DTU10            | 878.325   | -890.982  | 25.6053    | 156.300 | 0.9853               | 38                          |
| GEBCO            | 853.886   | -1158.960 | 20.3680    | 174.654 | 0.9813               | 44                          |
| Sandwell V18.1   | 1777.784  | -654.783  | 61.4656    | 239.601 | 0.9671               | 60                          |

Table 5: Statistical analysis of the estimated bathymetry and the global bathymetry models with the ground truth data (NGDC data) (Units are in metres).
| Models       | Min Diff. | Max Diff. | Mean Diff. | Std Dev | RMSE   | Correlation |
|--------------|-----------|-----------|------------|---------|--------|-------------|
| UTM18 – ETOPO1 | -496.620  | 1764.744  | 102.204    | 291.591 | 308.9594| 0.99095     |
| UTM18 – DTU10 | -500.825  | 932.698   | 27.413     | 131.442 | 134.2589| 0.99931     |
| UTM18 - GEBCO | -654.700  | 844.718   | 22.176     | 145.521 | 147.1886| 0.99862     |
| UTM18 – Sandwell V18.1 | -416.308  | 1754.784  | 63.274     | 235.059 | 243.4064| 0.99608     |

**Table 6:** Statistics of the differences between the UTM18 Bathymetry model and the global bathymetry models (Units are in metres).
| Malaysian Seas       | Maximum depth (m) | Average Depth (m) |
|----------------------|-------------------|-------------------|
| Malacca Straits      | -171.771          | -50.734           |
| South China Sea      | -5596.160         | -1218.696         |
| Sulu Sea             | -5075.860         | -1934.880         |
| Celebes Sea          | -6100.990         | -4071.270         |

**Table 7:** Depth variation between Malacca Straits, South China Sea, Sulu Sea, and Celebes Sea

(Unit are in metres).