Power exhaust of the baffled snowflake divertor in TCV

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Abstract.
A nitrogen-seeded, baffled Snowflake Minus Low-Field Side (SF-LFS) is geometrically-optimised in TCV, increasing divertor neutral pressure, to evaluate the roles of divertor closure (comparing with an unbaffled SF-LFS) and magnetic geometry (comparing with a baffled Single Null, SN) in power exhaust and core-divertor compatibility. Baffles in the SF-LFS configuration are found to reduce the peak outer target heat flux by up to 23%, without significantly affecting the location of the inter-null radiation region or the core-divertor compatibility. When compared to the baffled SN, the baffled SF-LFS exhibits a reduction in outer target heat flux by up to 66% and the ability to balance the strike-point distribution of heat flux. These benefits are less significant with N₂ seeding, with similar peak target quantities (such as heat flux, electron temperature and ion flux) and divertor radiated power. Despite a radiating region located farther from the confined plasma for the SF-LFS than the baffled SN, no change in core confinement is observed. Core effective charge even indicates an increase in core impurity penetration for the SF-LFS.

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1. Introduction

In future fusion devices, material limits will constrain reactor operation, highlighting divertor detachment as an essential operational regime \cite{1, 2}. Divertor vs main chamber neutral compression has been identified as a key parameter in accessing divertor detachment, that can be increased by increasing divertor closure \cite{2, 3, 4}. Alternative Divertor Configurations (ADCs) are being considered for future reactors to help mitigate heat fluxes arriving at the wall \cite{1, 6, 7}. To this end, TCV’s capacity to operate a wide range of ADCs has been enhanced by modifiable gas baffles \cite{8}.

One such ADC is the Snowflake Minus Low-Field Side (SF-LFS) configuration \cite{9, 10, 11, 12}, that features a secondary X-point in the LFS common flux region. The additional strike-points and extended region of low poloidal field in this geometry are modelled to increase divertor radiative losses and to lower target temperatures \cite{11, 12, 13, 14}. A reduced peak outer target heat flux with respect to the standard Single Null (SN) configuration was already observed on TCV in the unbaffled SF-LFS, together with the ability to balance the ratio of power reaching each of the two active outer strike-points \cite{15, 16}.

Highly-radiative scenarios, achieved with impurity seeding, can greatly enhance divertor power dissipation. In the SN configuration, under detached conditions, an X-point radiator was observed with impurity seeding, where the dominant radiation is located in the vicinity of the X-point, reaching inside the confined region \cite{17, 18, 19}. Conversely, nitrogen seeded experiments in the unbaffled SF-LFS featured a strongly radiating region between the two X-points \cite{20}, that was further from the core plasma than for the SN, showing potential for improved core-divertor compatibility. Reactor relevance will require the core impurities to remain below some critical concentration in order to maintain fusion performance and plasma stability \cite{21}. Therefore, assessing the impact of the radiation region displacement in the SF on core performance and core impurity levels is of high importance.

This study explores the performance of the baffled SF-LFS geometry, in terms of power exhaust and divertor-core compatibility, to appraise the combined effect of increased divertor closure and the complex magnetic geometry. In section \ref{section2}, the development of the baffled SF-LFS configuration is described. The divertor conditions of this geometry are then determined, beginning in section \ref{section3} with a comparison of the target heat fluxes with baffled SN and unbaffled SF-LFS geometries. Section \ref{section4} explores the effect of N$_2$ seeding on these divertor conditions, assessing both the effect on divertor radiated power and mitigation of target heat fluxes. Section \ref{section5} investigates the core-divertor compatibility of all configurations presented in this study, to compare the impact of magnetic geometries and divertor closures upon core impurity penetration and confinement. Finally, section \ref{section6} presents the key conclusions and outlook of this study.

2. Development of baffled SF-LFS configuration

The first generation of TCV baffles were designed to maximise the core-to-divertor neutral compression in the standard SN geometry whilst remaining compatible with a variety of other divertor geometries \cite{8} (see for example the study of long-legged ADCs with baffles \cite{22}). The SF-LFS features an even higher flux expansion in the null-point region than the SN, and so requires the development of a baffle-optimised geometry to maximise neutral compression whilst minimising plasma-baffle interaction. Two baffled SF-LFS geometries were developed with different X-point separations, together with a reference SN configuration, see figure \ref{fig1} (a)-(c). The SF-LFS configuration increases the LFS connection length with respect to the SN, with no compromise on the HFS connection length, figure \ref{fig1} (d)-(e).

An experimental database of discharges was constructed for each of these three geometries, with and without baffles, to explore the effect of increased divertor closure. In this section, the experimental set-up of these discharges is first outlined, followed by a description of the divertor diagnostics used within the study. We then assess the effectiveness of this geometric baffle-optimisation, by comparing the baffled geometries with their unbaffled counterparts and initial, non-optimised baffled SF-LFS discharges, in terms of divertor neutral pressure and plasma-baffle interaction.

2.1. Experimental set-up

The SF-LFS and SN configurations are ohmically-heated L-mode discharges in deuterium, with a plasma current $I_p = 245$ kA, operated in ‘reversed’ toroidal magnetic field ($\nabla B$ ion drift directed upwards, away from the X-point) of $B_t = 1.44$ T, figure \ref{fig2}. The line-averaged core density is maintained at approximately $\langle n_c \rangle_l = 4.7 \times 10^{19}$ m$^{-3}$, corresponding to a Greenwald fraction of $\sim 0.25$, figure \ref{fig2} (d). N$_2$ is injected during the stationary phase of these discharges, to increase radiative cooling and approach detached conditions, figure \ref{fig2} (f). Several discharges were performed in each configuration, baffled and unbaffled, to increase diagnostic coverage.
Figure 1: (a)-(c) Poloidal view of the magnetic equilibrium reconstructions of baffled geometries. For each geometry, the parallel connection length $L_{||}$ is given from the outboard midplane to the (d) LFS and (e) HFS targets, as a function of the upstream distance from the primary separatrix, $d_{ru}$, with colours corresponding to the magnetic equilibria in (a)-(c).

In the SF-LFS geometry, the secondary X-point causes the outer scrape-off layer (SOL) to split into two outer strike-points (OSPs) magnetically-connected to the SOL, referred to as SP2 and SP4 [11]. The X-point separation determines the power balance between SP2 and SP4 in attached conditions [15, 16], and is quantified by $d_{RX2}$, the distance between the two separatrices at the outboard midplane. Accordingly, two SF-LFS geometries with different $d_{RX2}$ were developed to investigate the effect of divertor closure on the SF-LFS power sharing capability. The X-point separations in the baffled SF-LFS discharges are $d_{RX2} = 6.9 \pm 0.2$ mm and $d_{RX2} = 3.7 \pm 0.3$ mm (with errors corresponding to fluctuations within the discharge), figure 2 (c). The heat flux decay width, $\lambda_q$, of the reference SN geometry is $\sim 3.9$ mm [23]; comparatively, these SF-LFS geometries represent ‘large’ and ‘small’ X-point separations respectively. Unbaffled discharges were also performed for the same X-point separations, with $d_{RX2} = 6.6 \pm 0.7$ mm and $d_{RX2} = 3.0 \pm 0.5$ mm.

2.2. Divertor diagnostics

Figure 3 shows the poloidal position of the divertor diagnostics relevant to this study. The divertor neutral pressure is measured by a baratron pressure gauge at the divertor floor, shown in green in figure 3 (a). The D$_2$ and N$_2$ injection valves, that include flow measurements, are located either side of this pressure gauge.

Langmuir probes cover all strike-points and the plasma-facing sides of the baffles, and are operated in swept bias mode to measure ion saturation current density, $j_{sat}$, target electron temperature, $T_e$, floating potential, $V_{fl}$, and the electric current when grounded, $j_0$, as detailed in [24, 25]. The target heat flux parallel to the magnetic field, $q_{||}$, can be calculated as the sum of contributions from electrons (e), ions (i) and the recombination process (rec), as performed in [26],

$$q_{||} = 2T_e(j_{sat} - j_0) + (2.5T_e + eV_{sh})j_{sat} + E_{pot}j_{sat}, \quad (1)$$

where $E_{pot} = 15.8$ eV is the potential energy per incident ion, including the recombination energy and half the molecular bonding energy, and $V_{sh}$ is the potential drop across the sheath,

$$V_{sh} = -\frac{1}{2} \ln \left( \frac{4\pi m_e}{m_i} \right) T_e + V_{fl}. \quad (2)$$

Here, we assume thermalisation between ions and electrons $(T_i = T_e)$ and account for non-ambipolar conditions (non-zero SOL currents).

The target heat flux is also measured by the vertical (VIR) and horizontal (HIR) infrared systems, using the temperature variation of the machine wall tiles [23]. The fields of view of each system are portrayed in figure 3 (a). The HIR measures heat...
Figure 2: Typical time traces of (a) $I_p$, (b) $P_{ohm}$, (c) $d\gamma_X$, (d) $\langle n_e \rangle_1$, and the Greenwald fraction, and the injected gas flow of (e) $D_2$ and (f) $N_2$ for each of the three baffled magnetic geometries: large $d\gamma_X$ SF-LFS (orange), small $d\gamma_X$ SF-LFS (purple), SN (green). The SF shape is established at $\sim\,0.6\,s$, with the desired X-point separation obtained at $\sim\,0.80\,s$ and $\sim\,0.96\,s$ for the large and small $d\gamma_X$ values, respectively.

fluxes at SP1 and SP2 for the SF-LFS and the SN’s inner strike-point (ISP), whereas the VIR views the SN’s OSP. Note that SP3 of the SF-LFS is inactive: it receives negligible heat and particle fluxes. IR measurements are used to complement the LP results, but remain incomplete as no IR data at SP4 is yet available. The heat flux profiles from both LPs and IR are plotted in this work as a function of the normalised poloidal magnetic flux, $\rho_\psi = \sqrt{(\psi - \psi_0) / (\psi_{LCFS} - \psi_0)}$, where $\psi$ is the poloidal magnetic flux and $\psi_0$ and $\psi_{LCFS}$ are inferred at the magnetic axis and at the last closed flux surface (primary separatrix) respectively.

The plasma radiated power is measured by a recently-upgraded bolometry system, RADCAM [27], with coverage of both the core and divertor regions of TCV (see figure 3 (b)). This system is used for the baffled discharges outlined above, but was not yet available for the older, unba ffled discharges.

2.3. Geometric baffle-optimisation

An optimal distance between the SOL and LFS baffle exists where the divertor neutral pressure is maximised, due to competition between divertor closure and plasma-baffle interaction. Increasing further the SOL proximity to the LFS baffle increases the plasma recycling flux on the baffle and reduces divertor neutral pressure, weakening the benefit of gas baffles [28]. The SOL-baffle proximity is strongly affected by the plasma vertical position within the vessel, core plasma shape and $d\gamma_X$. Thus, baffle-optimised SF-LFS geometries were designed to maximise the SOL-baffle distance, while maintaining a sufficiently large $d\gamma_X$ to approach
Figure 4: Divertor neutral pressure measurements from the divertor floor pressure gauge for the un baffled (blue), baffled but not optimised (magenta) and baffle-optimised (orange) SF-LFS configurations. The vertical dashed line at 1s represents the beginning of a N₂ seeding ramp. Results are shown from repeat discharges in each geometry.

Figure 5: Profiles of the ion saturation current density parallel to the magnetic field \( (j_{\text{sat}}) \) measured by LPs at the LFS baffle and active outer strike-points (SP2, SP4) of the baffle-optimised SF-LFS configuration with \( dx_{X2} \sim 6.9 \) mm. The separatrices are indicated by solid lines and the position of the LFS baffle tip is indicated by a dashed line, at \( \rho_\psi = 1.069 \pm 0.005 \).

3. Target conditions of the baffled SF-LFS

In the SF-LFS geometry, the power distribution between the active outer strike-points depends upon the X-point separation: the higher \( dx_{X2} \), the higher the ratio of the heat fluxes reaching SP2 to SP4. Of the two SF-LFS geometries considered in this study (see figure 6), the case with \( dx_{X2} \sim 3.7 \) mm presents a more balanced peak heat flux \( q_{\text{peak}} \) distribution between the outer targets, while the case with \( dx_{X2} \sim 6.9 \) mm presents a higher \( q_{\text{peak}} \) at SP2 than SP4.

Compared with the baffled SN, a reduction in \( q_{\text{peak}} \) is observed at the outer divertor in the baffle-optimised SF-LFS (see figure 6 (a)-(b)), as seen in previous studies without baffles [15]. Note that while the LPs and IR show fair agreement for measured \( q_{\text{peak}} \) profiles, discrepancies remain in the magnitude of \( q_{\text{peak}} \), with the VIR reporting generally higher and the HIR generally lower values than the LP-measured \( q_{\text{peak}} \). The SF-LFS case with \( dx_{X3} \sim 3.7 \) mm presents a significant parallel heat flux reduction in the outer divertor with respect to the SN configuration, with IR measuring a reduction of 66% and LPs of 57%. For the SF-LFS case with larger X-point separation \( dx_{X2} \sim 6.9 \) mm, IR sees a reduction of 59%, and LPs of 57%. This heat flux reduction coincides with a reduction in the \( T_{\text{peak}} \) and \( V_{\text{sh}} \), rather than a strong reduction in \( T_{\text{peak}} \). Furthermore, this reduction with respect to the SN is stronger for the SF-LFS with small \( dx_{X2} \) since the heat fluxes at SP2 and SP4 are more balanced. For the remainder of this paper, the focus

\( J_{\text{sat}} \) balanced peak heat flux distribution at the OSPs.

For the baffle-optimised SF-LFS geometries, the divertor neutral pressure approximately doubles compared to the equivalent un baffled geometry (shown in figure 4), similarly to the baffled standard SN configuration at these upstream conditions [3]. This difference is maintained throughout the discharges, even when seeding N₂ into the divertor. The first attempts of baffled SF-LFS discharges, that were not baffle-optimised, have comparable divertor neutral pressure to the un baffled cases, demonstrating the need for attentive geometric optimisation.

As expected, the baffle-optimisation also strongly reduces the particle flux impinging the plasma-facing side of the LFS baffle. In the baffle-optimised SF-LFS geometry, the magnetic flux surface \( \rho_\psi \sim 1.07 \) (corresponding to an upstream distance from the separatrix of \( dr_u \sim 22 \) mm) is intercepted by the LFS baffle tip (see figure 5). By contrast, for the geometry which is not baffle-optimised, the baffle tip intercepts \( \rho_\psi \sim 1.04 \) (correspondingly \( dr_u \sim 12 \) mm), being much closer to the core plasma (not shown). The ion flux recycled at the plasma-facing LFS baffle surface is considerably reduced by the geometric optimisation, becoming comparable to that of the reference SN (in which the LFS baffle tip intercepts \( \rho_\psi \sim 1.09, dr_u \sim 27 \) mm).

Note that the HFS baffle interaction remains negligible for all baffle-optimised geometries. The baffle-optimised SF-LFS configuration thus allows for a fairer comparison of target behaviour between configurations.
will be placed upon the case with \( dr_{X2} \sim 6.9 \) mm, while the small \( dr_{X2} \) case will be used to investigate the generality of results to the SF-LFS.

When compared with the un baffled configuration, the baffle-optimised SF-LFS presents a \( q_{||}^{\text{peak}} \) reduction of \( \sim 18\% \) at SP2 and \( \sim 23\% \) at SP4, as shown in figure 6(c). LP data suggest that this reduction coincides strongly with a reduction in \( T_{e}^{\text{peak}} \), with no strong change in \( T_{e}^{\text{peak}} \). This is also seen for the SF-LFS case with small \( dr_{X2} \) (not shown here), and is therefore assumed to be a general feature of the SF-LFS configuration. Over the range \( dr_{X2} = [2.0, 7.1] \) mm, the baffles reduce \( q_{||}^{\text{peak}} \) almost symmetrically at each active outer strike-point, so the dependence of outer target \( q_{||}^{\text{peak}} \) distribution on \( dr_{X2} \) is largely unaffected by baffles.

At the inner target, we note that all configurations exhibit comparable \( q_{||} \) profiles, demonstrating that the outer target \( q_{||} \) is not simply reduced from the change in in-out power sharing with changing geometry. We conclude that the baffled SF-LFS exhibits a clear peak outer target heat flux reduction, with respect to both the un baffled SF-LFS and the baffled SN in the absence of \( N_2 \) injection.

4. Evolution of divertor conditions with \( N_2 \) seeding

The mitigation of target heat flux requires significant radiative losses in the divertor, which can be increased by impurity seeding. In this section, the effect of \( N_2 \) injection on the target heat fluxes and divertor radiated power is reported. The time-integrated \( N_2 \) flux is used as a proxy for divertor \( N_2 \) content, since the absolute divertor \( N_2 \) concentration cannot yet be measured on TCV. This quantity represents an upper limit for the divertor \( N_2 \) content, as it accounts for neither wall-retention, exhaust to the TCV pumps nor core penetration of the impurity, which cause the actual divertor \( N_2 \) content to be lower. Nevertheless, it is considered a useful parameter in comparing the detachment properties of the different configurations. In these scenarios, only partial detachment \cite{29} can be achieved, as \( N_2 \) causes plasma disruption before pronounced detachment. The lowest \( T_{e}^{\text{peak}} \) measured is 6.2 eV, similar to the minimum target temperatures measured in other \( N_2 \) seeding experiments on TCV \cite{19}.

4.1. Target heat flux mitigation

In all configurations, a general decrease in peak target ion flux \( (T_{||}^{\text{peak}}) \), electron temperature \( (T_{e}^{\text{peak}}) \) and heat flux \( (q_{||}^{\text{peak}}) \) is observed in the outer divertor with \( N_2 \) injection as the outer divertors begin to detach (see figure 7). In the baffled SF-LFS, LP-measured \( q_{||}^{\text{peak}} \) decreases strongly with the start of \( N_2 \) seeding, but quickly plateaus to an approximately constant value of \( 2.3 \pm 0.3 \) MWm\(^{-2}\). This represents the overall peak of the outer targets, which for the SF-LFS is the maximum of SP2 and SP4, and for the SN is simply the OSP peak. Peak target temperature and ion...
fluctuations in the floating potential may also be due to a limitation in the LP measurement, where a modification of the plasma resistance or fluctuations in the floating potential may lead to an over-estimation of the electron temperature. Compressed magnetic fields at the inner strike-point, the peak target heat flux to the inner target.

Compared with the baffled SN, we see a clear reduction of $q_\parallel^{\text{peak}}$ in the baffled SF-LFS until a time-integrated $N_2$ flow of $\sim 4 \times 10^{19}$ molecules. This heat flux reduction comes with only a slight reduction in $T_e^{\text{peak}}$ — the presence of baffles appears to have a stronger effect on $T_e^{\text{peak}}$ than this change in magnetic geometry. Injecting additional $N_2$ tends to make $q_\parallel^{\text{peak}}$ equal for the two configurations. Note that the stagnation of $q_\parallel^{\text{peak}}$ with $N_2$ seeding in the baffled SN occurs at a higher quantity of injected $N_2$ than for the baffled SF-LFS.

At the inner strike-point, the peak target heat flux is comparable across all geometries, including those with $N_2$ injection. We conclude that the heat flux reduction observed in the baffled SF-LFS with respect to all other cases is not simply due to a redirection of power to the inner target.

Figure 7: Peak outer target (a) parallel heat flux, (b) electron temperature, (c) parallel ion flux, plotted as a function of the time-integrated $N_2$ flux. Data measured by LPs (markers) present the overall outer target peak value (considering both SP2 and SP4 for the SF-LFS), whereas heat flux data measured by IR (lines) consider only SP2, as SP4 data is not available. Dashed lines indicate where the outer target heat flux is expected to peak at SP4. Results are shown from repeat discharges in each geometry.

For a time-integrated $N_2$ flow of approximately $3 \times 10^{19}$ molecules, $q_\parallel^{\text{peak}}$ at SP2 becomes lower than at SP4, while at SP4 $q_\parallel^{\text{peak}}$ decreases very little with further $N_2$ injection. Divertor cooling with $N_2$ injection increases the neutral mean free path, potentially allowing neutrals to travel further into the confined plasma rather than remaining, and dissipating power, in the divertor. This may explain the observed $q_\parallel^{\text{peak}}$ stagnation. Figure 7 (a) also displays IR-measured $q_\parallel^{\text{peak}}$, but only for SP2 as data is not available for SP4. From a time-integrated $N_2$ flow of $\sim 3 \times 10^{19}$ molecules, the IR data is marked by a dashed line for the SF-LFS configurations, as the SP2 peak is no longer expected to represent the overall peak of the outer targets. The IR data before this line is in fair agreement with the LPs, within the experimental scatter.

When compared with the unbaffled SF-LFS, the baffled SF-LFS exhibits a clear decrease in $q_\parallel^{\text{peak}}$ for zero to moderate levels of $N_2$ seeding, coincidentally with a reduction in $T_e^{\text{peak}}$. For high injection levels of $N_2$, the difference in both $q_\parallel^{\text{peak}}$ and $T_e^{\text{peak}}$ between the configurations is reduced, where the unbaffled SF-LFS displays continuous reductions, but the values remain constant in the baffled SF-LFS. The colder baffled divertor may reduce the radiative efficiency of $N_2$, hence stagnating the reduction of peak target heat flux. This will be discussed further in the following sub-section. However, the stagnation of electron temperature may also be due to a limitation in the LP measurement, where a modification of the plasma resistance or fluctuations in the floating potential may lead to an over-estimation of the electron temperature in detached conditions [30].

Compressed magnetic fields at the inner strike-point, the peak target heat flux to the inner target.
Figure 8: Poloidal plots of plasma emissivity from bolometry for (a)-(c): the baffled SF-LFS, and (d)-(f): the baffled SN configurations. From left to right, the quantity of time-integrated N$_2$ flux is increased: (a),(d): $\sim 0$ molecules; (b),(e): $\sim 3.0 \times 10^{19}$ molecules; (c), (f): $\sim 6.0 \times 10^{19}$ molecules.

4.2. Divertor radiated power

The plasma emissivity calculated from tomographic inversions of the bolometry data gives an indication of regions of strong radiated power, as shown in figure 8. The baffled SF-LFS exhibits a radiation region between the two X-points, whereas an X-point radiator is seen for the baffled SN configuration. The inter-null radiation region is observed in the SF-LFS for both X-point separations, with and without baffles, and before and during the N$_2$-seeded phase of the discharge (the small $dr_{X2}$ and unbaffled cases are not shown here). This is therefore a key feature of the SF-LFS geometry. These regions increase in size and intensity with N$_2$ seeding, moving closer to the confined plasma region, as apparent in figure 8.

The radiated exhaust power, $P_{\text{rad}}$, is calculated by integrating the plasma emissivity over the divertor volume and X-point region (see yellow region inset in figure 8). To account for small variations in the Ohmic heating power and core conditions in each configuration, we compare the radiated power fraction, by evaluating the ratio of $P_{\text{rad}}$ to the power entering the SOL, $P_{\text{SOL}}$. $P_{\text{SOL}}$ is the input (Ohmic) heating power minus the core radiated power. For simplicity, the core is defined as the region above the HFS baffle tip, as shown by the purple region inset in figure 9 excluding the X-point region while fairly comparing two magnetic geometries with different core shapes. The divertor radiated power fraction thus obtained (figure 9) is at most 10% higher in the baffled SF-LFS than in the baffled SN configuration, up to a time-integrated N$_2$ flux of approximately $4 \times 10^{19}$ molecules. Similar values are obtained for the small $dr_{X2}$ case (not shown) within the experimental scatter. This increase between SF and SN is similar to the radiated power fraction increase from simulations ($\sim 7\%$) [12]. With further N$_2$ seeding, the difference between the configurations is diminished as the divertor radiated power in the baffled SN increases faster with N$_2$ than for the SF-LFS. At temperatures below $\sim 10$ eV, the radiative efficiency of N$_2$ decreases [32], which could explain the slower increase in radiated power fraction with further N$_2$ seeding. This coincides with a smaller difference in peak target heat flux between the geometries. The following section will explore the core-divertor compatibility, to determine whether this difference in performance should be ascribed to a difference in divertor volume N$_2$ retention between the two configurations.

5. Core-divertor compatibility

As part of the assessment of the SF-LFS configuration as a potential divertor solution for future reactors, we must consider divertor-core compatibility alongside power exhaust enhancements, to limit core impurity pollution and the degradation of energy confinement. Two complementary metrics will be used in this assessment: the core effective charge and the main plasma energy confinement time.
5.1. Core effective charge

The core effective charge is defined in the usual manner as,

\[ Z_{\text{eff}} = \frac{\Sigma n_i Z_i^2}{n_e}, \quad (3) \]

where \( n_i \) is the density of each ion species \( i \) and \( Z_i \) is the charge number of that species. \( Z_{\text{eff}} \) is estimated from measurements of \( V_{\text{loop}} \) and the profile-averaged core temperature from Thomson scattering, assuming steady state conditions and neo-classical conductivity \[33, 34\].

The core effective charge is shown in figure 10 (a), as a function of the time-integrated \( N_2 \) flux. Initially, \( Z_{\text{eff}} \) is only slightly above 1, the value of an undiluted deuterium plasma, but then increases once \( N_2 \) seeding begins. Measurements of core carbon density suggest that this increase in \( Z_{\text{eff}} \) is in fact due to an increase in core nitrogen content, rather than a variation in electron or carbon density.

In the SF-LFS configuration, baffles only slightly reduce \( Z_{\text{eff}} \). We expect that while the colder divertor would be more transparent to impurities, the increased divertor closure would simply decrease the probability of impurities entering the core plasma. Comparing with the baffled SN, the baffled SF-LFS configuration exhibits an up to 25% higher \( Z_{\text{eff}} \), suggesting stronger core impurity penetration. The SF-LFS case with small \( dx_2 \) displays a slightly milder trend, but still with an up to 20% increase in \( Z_{\text{eff}} \). This may signify a SOL in the SF-LFS that is more transparent to impurities than for the baffled SN. Furthermore, this suggests that a radiation region located further away from the core plasma, figure 8 did not necessarily improve core compatibility. This will need to be explored in future experiments under higher power conditions, where low-Z impurity screening can increase \[35\].

5.2. Energy confinement time

We now focus on the energy confinement time, \( \tau_{\text{exp}} \), defined as,

\[ \tau_{\text{exp}} = \frac{W_{\text{MHD}}}{P_{\text{in}}}, \quad (4) \]

where \( W_{\text{MHD}} \) is the plasma stored energy and \( P_{\text{in}} \) the input heating power, which in this case is only Ohmic. Although diamagnetic loop measurements are often used to measure the stored plasma energy, it is difficult to compensate the flux measurement sensitivity to poloidal magnetic fields \[36\], which, across the studied configurations, can differ greatly. Here, \( W_{\text{MHD}} \) is estimated by integrating the core electron temperature and density profiles, from Thomson scattering, over the plasma volume,

\[ W_{\text{MHD}} = 2\pi \int (3n_e T_e) R dR dZ, \quad (5) \]

where \( R \) and \( Z \) are the poloidal coordinates. We assume \( T_i = T_e \) that impurity densities are in the trace limit. The latter assumption can lead to an overestimation of \( W_{\text{MHD}} \) by up to 15%. CXRS (Charge eXchange Recombination Spectroscopy) measurements of \( T_i \) were only available for a small subset of the data presented, and so are not used, but confirm the trends observed by the assumption \( T_i = T_e \).

Figure 10 (b) shows the energy confinement time for the discharges presented in the study. Initially, the baffled SF-LFS shows a slightly lower energy confinement time than the baffled SN (11% at most). As \( N_2 \) is injected, this difference reverses, with the SF-LFS now showing a ~16% increase in \( \tau_{\text{exp}} \) compared to the SN. Overall, we conclude that no strong,
systematic difference between the three configurations is discerned.

6. Conclusion

Baffled SF-LFS geometries have been successfully developed on TCV to explore the effect of divertor closure on the power exhaust and divertor-core compatibility of the SF-LFS, compared with standard baffled SN configurations. In the Ohmic L-mode discharges investigated herein, the SF-LFS shows a peak outer target heat flux reduction of around 20% with baffling, and maintains the inter-null radiation region observed without baffles, with no significant effect on core-divertor compatibility. The baffled SF-LFS presents promising power exhaust features over the baffled SN in terms of outer target heat flux reductions and balance of strike-point heat flux with baffling, and maintains the inter-null radiation peak outer target heat flux reduction of around 20%.

Moving forward, further experiments will explore the effect of increasing SOL opacity to neutrals, by increasing the separatrix density and input power, to investigate whether any SF-LFS benefits are maintained while seeding impurities. In parallel, we will develop EMC3-EIRENE simulations of the experimental scenarios presented herein, while further exploring the roles of divertor radiative losses and/or core impurity penetration in target heat flux mitigation.

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Moving forward, further experiments will explore the effect of increasing SOL opacity to neutrals, by increasing the separatrix density and input power, to investigate whether any SF-LFS benefits are maintained while seeding impurities. In parallel, we will develop EMC3-EIRENE simulations of the experimental scenarios presented herein, while further exploring the roles of divertor radiative losses and/or core impurity penetration in target heat flux mitigation.

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