Exothermic synthesis of ceramic materials based on barium and strontium aluminosilicates

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EXOTHERMIC SYNTHESIS OF CERAMIC MATERIALS BASED ON BARIUM AND STRONTIUM ALUMINOSILICATES

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Ceramic materials were synthesized in the RO(R=Ba, Sr)–Al₂O₃–SiO₂ system using exothermic synthesis from solutions containing barium and strontium nitrates, silica and organic reducing agents (glycine and carbamide). It was shown that only the use of a mixture of glycine and carbamide as well as the addition of ammonium nitrate allows carrying out a complete exothermic synthesis with the formation of an X-ray amorphous product with a small fraction of the crystalline phase. It was established that monophase materials based on barium and strontium aluminosilicates (BaAl₂Si₂O₈ and SrAl₂Si₂O₈) are formed when the obtained X-ray amorphous product is heat-treated at the temperatures above 1000°C. Ceramics from synthesized materials sintered at 1550°C has a high refractoriness, open porosity of 0–1.0%, compressive strength of 115–120 MPa; dielectric constant of 3.25–6.0 (at the frequency of 1 MHz) and the loss tangent of (1.5–5.2)·10⁻³. The results shows that the exothermic synthesis ensures the preparation of nano- and submicrocrystalline powders in the system RO(R=Ba, Sr)–Al₂O₃–SiO₂. Materials based on the obtained aluminosilicates can be used in the manufacture of protective structures for devices operating in the radio frequency band, in radar installations of aviation and rocket technology, etc.

Keywords: radiotransparent ceramics, slavsonite, celsian, microstructure, dielectric constant, dielectric loss tangent.

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Introduction

To protect the elements of the radio transmitting and receiving paths in aerospace, aviation and rocket technology, various organic (plastics, textolites, etc.) and inorganic (ceramics, glasses, glassceramics, etc.) radiotransparent materials are used. Inorganic materials are more promising for creating radiotransparent protective elements of electronic equipment structures as they are characterized by high uniformity of properties, heat resistance and radio transparency in a wide frequency range of radio frequencies. In particular, ceramic materials exhibit thermal stability and high heat resistance, which allows them to be used at high temperatures (up to 2000°C) [1–5].

Radiotransparent materials are dielectrics that do not change the amplitude of the electromagnetic wave passing through them and do not cause a chaotic change in its phase. The transparency of these materials for radio waves means that they have very small dielectric losses in the range of operating temperatures and practically do not reflect radio waves [5].

The main materials for antenna fairings of aircraft and radiotransparent elements of various designs are radio-transparent materials based on quartz [1–5], silicon nitride [1,3–4] and RO–Al₂O₃–SiO₂ systems (where R=Li₂, Na₂, Mg, Ca, Sr, Ba, Zn) [1–6]. In addition, these types of ceramics are widely used in the manufacture of technical ceramic products (capacitors, inductors, electrical insulators, etc.) operating at elevated frequencies.

Comparative characteristics of compounds for producing ceramic radiotransparent materials and products are presented in Table 1 [5,7–10]. Analysis of physical-mechanical, thermophysical and electrophysical properties allows us to conclude that it is advisable to fabricate radiotransparent ceramic materials based on aluminosilicates in the RO–Al₂O₃–SiO₂ (R=Ba, Mg, Sr) systems by directed
which have a set of necessary characteristics.

The effect of the structure on the physical and mechanical properties of a monophase ceramic is mainly associated with the dispersion of the crystalline phase: the strength of the material decreases with an increase in the grain size. At the same time, the dielectric properties are mainly associated with the purity and homogeneity of the monophase material and, in the case of polyphase ceramics and composite materials, with the uniformity of the dispersed crystalline phase distribution, which ensures the constancy of properties over the volume of the material. Thus, one of the most significant factors in the manufacture of ceramic is the homogeneity of the material, which requires thorough mixing of the components of the raw material composition.

To carry out the synthesis of ceramic based on RO–Al₂O₃–SiO₂ systems (where R=Ca, Sr, and Al), the method of solid-phase synthesis from oxides, carbonates and natural compounds is currently used [11–14]. The use of natural compounds introduces impurities that deteriorate the electrophysical characteristics of materials. In addition, it is necessary to carry out burning at high temperatures to obtain the target phase when using the solid-phase synthesis method.

One of the promising and developing methods for preparing ceramic materials in the nanocrystalline state is an exothermic synthesis from solutions, which uses the internal energy of the system. The advantages of the exothermic synthesis from solutions are as follows: the possibility of producing pure ceramics with minimal impurities, a decrease in the size of the crystalline formations due to the intensive gas evolution during the synthesis and a short exposure time to high temperatures, and the creation of unique temperature-time conditions for the synthesis, which promote the formation of new crystalline and amorphous phases.

The aim of this work is to synthesize and study ceramic barium and strontium aluminosilicate materials by using the exothermic synthesis from solutions of organic-salt compositions.

**Experimental**

As initial components, we used chemically pure barium, strontium, aluminum and ammonium nitrates (Ba(NO₃)₂, Sr(NO₃)₂, Al(NO₃)₃·9H₂O, NH₄NO₃), as well as silicon oxide (SiO₂, aerosil A-300). Carbamide (CH₄N₂O) and glycine (C₂H₄NO₂) were used as organic components.

In general, the reaction of preparation of barium, strontium and aluminum oxides (Me = Ba, Sr, and Al) with the participation of these components can be written as follows:

\[
\text{Me}^9\text{(NO₃)}_g + \left(\frac{5}{6} \varphi \right) \text{CH}_4\text{N}_2\text{O} + \frac{\varphi}{4} (\varphi - 1)\text{O}_2 = \text{Me}^9\text{O}_g + \left(\frac{5}{6} \varphi \right) \text{CO}_2 + \frac{\varphi}{6} \left(\frac{5\varphi + 3}{6}\right) \text{N}_2 + \left(\frac{10}{6} \varphi \right) \text{H}_2\text{O};
\]

\[
\text{Me}^9\text{(NO₃)}_g + \left(\frac{5}{9} \varphi \right) \text{C}_2\text{H}_5\text{NO}_2 + \frac{\varphi}{4} (\varphi - 1)\text{O}_2 = \text{Me}^9\text{O}_g + \left(\frac{10}{9} \varphi \right) \text{CO}_2 + \frac{\varphi}{18} \left(\frac{5\varphi + 9}{18}\right) \text{N}_2 + \left(\frac{25}{18} \varphi \right) \text{H}_2\text{O},
\]

Table 1

| Compound   | Formula   | Coefficient of linear thermal expansion, \(\times10^6\), deg⁻¹ | Apparent density, g cm⁻³ | Melting point, °C | Mohs hardness | Dielectric constant, \(\varepsilon\) | Dielectric loss tangent, \(tg\eta \times10^3\) |
|------------|-----------|---------------------------------------------------------------|---------------------------|-------------------|---------------|-----------------------------------|-----------------------------------------------|
| Quartz ceramics | SiO₂ | 0.6 | 1.94–2.05 | >1300 (softening) | 7.0 | 3.3–3.5 | 0.1–0.3 |
| Mullite | Al₅Si₃O₁₈ | 6.2 | 3.00–3.10 | 1810 | 6.0 | 7.0 | 0.5–1.0 |
| Willemite | Zn₃SiO₄ | 3.2 | 3.90–4.10 | 1512 | 5.0–6.0 | 5.5 | 0.2–2.0 |
| Spodumene | LiAl₅Si₃O₁₈ | 0.9 | 3.10–3.20 | 1425 | 6.5–7.0 | 8.5–9.0 | 7.0–20.0 |
| Cordierite | Mg₃Al₅Si₃O₁₈ | 2.6 | 2.55–2.75 | 1460 | 6.0–6.5 | 4.0–7.0 | 0.5–3.0 |
| Anorthite | CaAl₅Si₃O₁₈ | 6.1 | 2.72–2.75 | 1550 | 6.0–6.5 | 6.0–7.0 | 0.2–3.0 |
| Slavsonite | SrAl₅Si₃O₁₈ | 6.5 | 3.27 | 1765 | 6.0–6.5 | 6.0–7.0 | 1.1–5.0 |
| Celsian | BaAl₅Si₃O₁₈ | 2.7 | 3.10–3.40 | 1740 | 6.0–6.5 | 6.5–7.0 | 0.1–3.0 |
| Corundum | Al₂O₃ | 7.5 | 3.7–3.9 | 2050 | 9.0 | 9.0–10.0 | 0.1–2.0 |

K.B. Podbolotov, A.T. Volochko, G.V. Lisachuk, R.V. Krivobok, V.V. Voloshchuk
where $\varphi$ is the ratio of the reducing agent to the oxidizing agent, and $\delta$ is the metal valence.

The ratio of the reducing agent to the oxidizing agent is defined as the ratio of the actual reducing agent/oxidizing agent ratio to the stoichiometric reducing agent/oxidizing agent ratio. So, $\varphi=1$ corresponds to stoichiometry and the supply of atmospheric oxygen is not required to complete the oxidation in this case. The inequality $\varphi>1$ (or $<1$) corresponds to the case of excess (or deficiency) of the reducing agent. In the case of $\varphi>1$, a reducing atmosphere is formed from the products of incomplete oxidation of the reducing agent, which contributes, in the case of metal synthesis, to the production of pure metal under normal conditions (without specially created reducing or inert atmosphere).

In the course of the exothermic reaction, the resulting oxides $\text{BaO}$, $\text{SrO}$, $\text{Al}_2\text{O}_3$ and silicon oxide interact with the formation of aluminosilicates:

$$\text{MeO} + \text{Al}_2\text{O}_3 + \text{nSiO}_2 = \text{MeO} \cdot \text{Al}_2\text{O}_3 \cdot \text{nSiO}_2. \quad (3)$$

The compositions for the synthesis were calculated based on the above synthesis reactions, taking into account the composition of the target compositions (Table 2) and the ratio of the reducing agent to the oxidizing agent $\varphi=1.25$.

### Table 2

| Number | Phase composition, wt.% | Content of oxides, mol.% |
|--------|-------------------------|--------------------------|
|        |                         | $\text{BaO}$ | $\text{SrO}$ | $\text{Al}_2\text{O}_3$ | $\text{SiO}_2$ |
| C-1    | $\text{BaAl}_2\text{Si}_3\text{O}_8 \sim 100$ | 25.0 | 0.0 | 25.0 | 50.0 |
| S-1    | $\text{SrAl}_2\text{Si}_3\text{O}_8 \sim 100$ | 0.0 | 25.0 | 25.0 | 50.0 |
| CS-11  | $\text{BaAl}_2\text{Si}_3\text{O}_8 \sim 50$ | 12.1 | 12.9 | 25.0 | 50.0 |

To prepare the solution, the components were weighed and transferred with simultaneous stirring into a heat-resistant glass with water, which was heated to the temperature of 60–80°C to improve dissolution. Silica was preliminary wetted with alcohol and then added to the resulting solution of the components under continuous stirring. Then, the solution was homogenized by stirring it for 25–30 min.

The initiation of the synthesis process was carried out by thermal treatment of a solution of the components (dry gel) pre-dried at 80°C in an oven at the temperature of 500°C.

In general, the synthesis process can be described in the following way. After placing the solution in the furnace, the solution is heated and water is removed with the formation of a gel-like structure from organic components with silica particles and nitrates distributed in it, which then foams. With a further increase in temperature, the foam ignites and its combustion is accompanied by a bright glow. After the end of the combustion reaction, the resulting material has a foam-like, spongy and highly porous structure.

The powders obtained as a result of the synthesis were subjected to the heat treatment in a laboratory furnace at the temperatures of 1000–1200°C to determine changes in the phase composition with holding at the maximum temperature for 1 h.

To prepare sintered ceramic samples, the powders obtained after heat treatment at 1000°C were milled in a wet ball mill in an aqueous medium for 8 h. From the obtained powders using a binder (polyvinyl acetate solution), a compacted powder was prepared and the samples were pressed in the form of a cylinder. The samples were sintered at the temperatures of 1250–1550°C.

X-ray phase analysis of the synthesis products was carried out on an Al-27 mini diffractometer using a copper Cu-K$_\alpha$ cathode. The international card index PDF-2 (2004) and the HighScorePlus software were used to identify crystalline phases.

The study of the microstructure was carried out using a TescanMira 3 scanning electron microscope equipped with an OxfordIns electron probe local chemical analysis system.

The determination of the density and porosity of the material was carried out according to the state standard GOST 2409 by the method of hydrostatic weighing. The mechanical strength in compression was determined on a ZD-10 testing machine in accordance with the state standard GOST 473.6. The determination of the electrophysical characteristics of the samples was carried out using an E7-20 immittance meter in the frequency range of 500 Hz to 1 MHz at the temperature of 20°C.

### Results and discussion

Visual observation of the course of the synthesis process showed that the initiation of the combustion process does not occur when carbamide is used. When glycine is used, the synthesis reaction proceeds in a low-intensity smoldering mode.

According to the data of X-ray phase analysis, the formation of phases of barium and strontium aluminosilicates (Fig. 1,a) does not occur in the case of using carbamide as a reducing agent. The phase composition is represented by barium and strontium nitrates as well as oxides and carbonates, which indicates an insufficient temperature of the process and is associated with a low intensity of the reaction.
of exothermic synthesis. When glycine is used, the reaction with barium nitrate also does not provide the formation of the necessary phases of aluminosilicates. However, when using strontium, the intensity of the process increases and the formation of the phases of carbonates and strontium oxides is observed in small amounts. In addition, an X-ray amorphous phase is formed, which, apparently, consists of aluminosilicates. When glycine is used, the powder of the material has a black-brown color, which is apparently due to the presence of carbon and products of incomplete decomposition of organic substances.

It follows from the experimental results that the synthesis process in barium- and strontium-containing systems is low-exothermic and an increase in heat release during the reaction interaction is required. To this end, it is possible to use additives that can exothermically interact with the components of the mixture. However, it is necessary to ensure the absence of impurities in the resulting material. These conditions are met for ammonium nitrate, which is capable of exothermic interaction with organic compounds and is completely decomposed at high temperatures. In addition, a reducing agent has a strong effect on the synthesis process; quite often, the combination of reducing agents increases the exothermic effect and accelerates the process. An increase in the content of the additive and the combination of reducing agents were carried out by using a barium-containing system (compositions C-1), since in this system the synthesis process is the least exothermic due to the high thermal stability of barium nitrate. Ammonium nitrate was introduced in a ratio of 1 mol NH₄NO₃ to 1 mol of the total oxides (ΣₓEₖOₓ) to obtain the barium aluminosilicate phase at φ=1.25. The method for preparing the solution is similar to that for compositions without ammonium nitrate.

Evaluation of the combustion intensity of the compositions showed that the highest combustion intensity, which is expressed in the maximum brightness of the glow in the combustion wave and the appearance of an open flame above the surface of the mixture, was detected in the cases of the compositions containing glycine and carbamide at a ratio of 1:1 (50:50). Figure 1,b shows the XRD patterns of a mixture containing glycine and carbamide in equal molar fractions. In this case, the formation of the crystalline phase of barium aluminosilicate BaAl₂Si₂O₈ is observed. According to X-ray structural analysis, the crystallite size is 13–15 nm. At the same time, the presence of silicon and aluminum oxides is also noted as well as a high degree of amorphization of the resulting material.

The materials synthesized in strontium- and barium-strontium-containing systems with the addition of ammonium nitrate and a mixture of reducing agents (carbamide and glycine), as shown by X-ray phase analysis data, are completely X-ray amorphous. This indicates that a product with either a glassy structure or a crystallite size of less than 2 nm is formed.

In order to complete the process of phase
Exothermic synthesis of ceramic materials based on barium and strontium aluminosilicates

formation, crystallization and removal of possible impurities of organic compounds, the resulting powders were calcined in air at temperatures of 1000–1200°C. The phase composition of materials is shown in Fig. 2.

As can be seen from the presented data, the process of phase formation and crystallization is completed during heat treatment. At the same time, a high purity of the obtained materials is achieved with a main phase content of more than 95%.

The microstructure of the powder obtained after heat treatment of the barium aluminosilicate composition (C-1) at 1000°C is shown in Fig. 3.

The structure is represented by a highly porous foam-like substance with various sizes of crystalline aggregates of irregular shape. The crystallite size is about 20–50 nm.

Samples in the form of cylinders were prepared from the synthesized powders calcined at 1000°C by
the method of semi-dry pressing. These samples were used in the study of physicochemical characteristics. The main properties of the samples depending on the burning temperature are shown in Fig. 4.

The dependence of the characteristics of synthesized materials on the firing temperature shows that the formation of a material with minimum porosity in the RO(R=Ba, Sr)–Al₂O₃–SiO₂ system is observed at a high temperature (1550°C). At this temperature, the highest degree of sintering is characteristic of the material obtained on the basis of the composition CS-11; the open porosity is 0–1.0% and the compressive strength is 115 MPa. Compositions C-1 and S-1 sintered at this temperature have an open porosity of the order of 11–12%. Such a high sintering temperature is possibly associated with the minimum amount of impurities and the monophasic nature of the material. XRD patterns of a thin section of the surface of sintered samples showed the presence of pure phases, similar to powders after calcination at 1200°C. Sintering at temperatures ≤1400°C apparently proceeds by a diffusion mechanism, and only in the region of high temperatures (≥1500°C) the amount of the formed liquid phase becomes sufficient to change the sintering mechanism to a liquid phase with a significant acceleration of the material compaction.

The results of the studies of electrophysical characteristics of the samples are shown in Fig. 5 and Table 3.

### Table 3
**Electrophysical characteristics of the samples at 1 MHz**

| Characteristic            | Value   |
|--------------------------|---------|
| Dielectric constant, ε   | 3.25    | 4.55    | 5.72    |
| Dielectric loss tangent, tgd·10⁻⁷ | 5.20     | 1.47     | 2.17     |

Thus the exothermic synthesis of nano- and submicrocrystalline powders in the RO(R=Ba, Sr)–Al₂O₃–SiO₂ system and the resulting ceramic materials on their basis can be used in the manufacture of protective structures for devices operating in epy radio frequency band and technical ceramic products (capacitors, inductors, electrical insulators, etc.) operating at elevated frequencies.

### Conclusions
Ceramic materials were synthesized in the RO(R=Ba, Sr)–Al₂O₃–SiO₂ system using the technology of exothermic synthesis from solutions containing barium and strontium nitrates, silica and organic reducing agents (glycine and carbamide). It is shown that only the use of a mixture of glycine and carbamide as well as addition of ammonium nitrate allows carrying out an exothermic process with complete conversion of the initial components.
In this case, an X-ray amorphous product with a small fraction of the crystalline phase is formed. During heat treatment of the product obtained during exothermic synthesis, crystalline phases of barium and strontium aluminosilicates (BaAl₂SiO₅ and SrAl₂SiO₅) are formed. The structure of the material is highly porous with different sizes of crystalline aggregates of irregular shape, with the crystallite size being about 20–50 nm.

The highest degree of sintering at the temperature of 1550°C is inherent in the material obtained on the basis of the composition CS-11, its open porosity is 0–1.0% and compressive strength is 115 MPa. Compositions C-1 and S-1 sintered at this temperature exhibit an open porosity of the order of 11–12%. It is shown that the dielectric constant of the obtained samples is 3.25–6.0 at the frequency of 1 MHz, the minimum values correspond to ceramics based on barium aluminosilicate. The dielectric loss tangent (tgδ) at the frequency of 1 MHz is (1.5–5.2)×10⁻³.

Thus, there is the possibility to use the exothermic synthesis technology to fabricate nano- and submicrocrystalline powders in the RO(R=Ba, Sr)=Al₂O₃–SiO₂ system. Materials based on the obtained aluminosilicates can be used in the production of technical ceramic.

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ЕКЗОТЕРМІЧНИЙ СИНТЕЗ КЕРАМІЧНИХ МАТЕРОІАЛІВ НА ОСНОВІ АЛЮМОСИЛКАТІВ БАРЮ І СТРІЮЦІЇ

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Проведено синтез керамічних матеріалів в системі РO(R=Ba, Sr)=Al₂O₃–SiO₂ при застосуванні технології екзотермічної синтезу з розчинів, що включають нітрати барію і стріюції, кремнезем і органічний відновник (гліцин і карбамід). Показано, що тільки при використанні суміші гліцину і карбаміду, а також добавки нітрату амонію можливе здійснення нової екзотермічної синтезу з формуванням рентгеноаморфного продукту з малою частиною кристалічної фази. Встановлено формування монокристаліків на основі алюмосілікатів барію (BaAl₂SiO₅) і стріюції (SrAl₂SiO₅) термообробкою отриманим рентгеноаморфним гідроксидом при температурі понад 1000°С. Кераміка з синтезованих матеріалів, спечена при температурі 1550°С, характеризується високою вогнетривкістю, відкритою порис-
EXOTHERMIC SYNTHESIS OF CERAMIC MATERIALS BASED ON BARIUM AND STRONTIUM ALUMINOSILICATES

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Ceramic materials were synthesized in the RO(R=Ba, Sr)–Al₂O₃–SiO₂ system using exothermic synthesis from solutions containing barium and strontium nitrates, silica and organic reducing agents (glycine and carbamide). It was shown that only the use of a mixture of glycine and carbamide as well as the addition of ammonium nitrate allows carrying out a complete exothermic synthesis with the formation of an X-ray amorphous product with a small fraction of the crystalline phase. It was established that monophase materials based on barium and strontium aluminosilicates (BaAl₂Si₂O₇ and SrAl₂Si₂O₇) are formed when the obtained X-ray amorphous product is heat-treated at the temperatures above 1000°C. Ceramics from synthesized materials sintered at 1550°C has a high refractoriness, open porosity of 0–1.0%, compressive strength of 115–120 MPa; dielectric constant of 3.25–6.0 (at the frequency of 1 MHz) and the loss of 0–1.0%, compressive strength of 115–120 MPa; dielectric constant of 3.25–6.0 (at the frequency of 1 MHz) and the loss tangent of (1.5–5.2) × 10⁻³. The results shows that the exothermic synthesis ensures the preparation of nano- and sub-microcrystalline materials sintered at 1550°C has a high refractoriness, open porosity of 0–1.0%, compressive strength of 115–120 MPa; dielectric constant of 3.25–6.0 (at the frequency of 1 MHz) and the loss tangent of (1.5–5.2) × 10⁻³.