Mapping the texture of plant protein blends for meat analogues

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amplitude sinusoidal strain input, the shape of the resulting stress waveform often deviates from a sinusoidal wave, with a significant contribution from higher-order harmonics. The LAOS information is typically extracted using Fourier-transform based methods (Hyun et al., 2011). Lissajous curves are used to facilitate the interpretation of a broad set of complex measurements. The so-called test space of the Lissajous curves is formed by two key parameters of LAOS deformation: frequency and strain amplitude. This test space is often shown in a Pippin plot (Ewoldt & McKinley, 2017; Pipkin, 1972; Szopinski & Luinstra, 2016; Zhou, Cook, & McKinley, 2010). To better quantify the transitions in non-linear behaviour, the energy dissipation ratio was calculated and presented by colour contours in the Pippin plot (Ewoldt, Hosoi, & McKinley, 2008; Tao et al., 2019). The energy dissipation ratio ($\phi$) as proposed by Ewoldt et al. (2008) and Ewoldt, Winter, Maxey, and McKinley (2010) is the ratio between the actual dissipated energy and the dissipation of a material showing perfect plastic behaviour. When $\phi = 0$, the rheological response is purely elastic, while $\phi = 1$ implies that the material displays perfect plastic (Ptaszek, 2014). A $\phi$ of $\pi$/4 corresponds to a material that behaves as a Newtonian liquid. Texture maps provide a compact overview of the rheological properties for any material of interest. They summarize non-linear rheological information into two-dimensional plots involving only characteristic key parameters. This allows us to map the non-linear rheological behaviour of a great number of samples in an intuitive way. Fig. 1 exemplifies this approach and includes stress and strain values from previous studies. Although different parameters can be chosen for these plots, most texture maps are based on the stress and strain at the end of the linear viscoelastic (LVE) regime to classify products into four quadrants (Fig. 1) (Hamann & MacDonald, 1992). Materials in quadrant 1 on the lower left, with low shear stress and shear strain, are classified as a soft, non-shaped commonly referred to as “mushy” (such as for grits and similar food materials). Materials in quadrant 2 on the lower right, with low shear stress and high shear strain, are often described as “rubbery” (such as gelatin). Quadrant 3 on the top right, with strong materials with high shear stress and shear strain that are not easily broken, indicates a “tough” texture (for example, fruit leather and dried fruits). Quadrant 4 on the top left, with delicate and easily broken materials with high shear stress and low shear strain, clusters products with a “brittle” texture (such as many baked or confectionery food products; Tunick & Van Hekken, 2010). Although the texture of food can be considered as a sensory property related to the human response, it is also often measured instrumentally in terms of mechanical or rheological proprieties (Altay & Gunasekaran, 2013). The latter study relate “texture” and used texture maps for instrumental responses such as the shear stress and strain at failure and classify those responses as rubbery, mushy, brittle and tough. Good examples of this approach are available for cheese (Truong & Daubert, 2001), soybean protein (tofu) and gelatin gum gels (Truong & Daubert, 2000), cross-linked waxy maize, tapioca, and Amioca starch dispersions (Genovese & Rao, 2003), mixed gelatine/FPI gels (Ersch, ter Laak, van der Linden, Venema, & Martin, 2015) and heat-induced PPI with microbial transglutaminase (Shand, Ya, Pietraski, & Wanasundara, 2008).

The objective of this study is to map the rheological properties of plant protein blends under conditions relevant to meat analogue processing in a compact way using texture maps and colour schemes. In this article, three rheological parameters are mapped: stress at the end of the LVE regime and the stress–strain crossover point are captured in texture maps, and the energy dissipation ratio is demonstrated with colour schemes. The dissipation ratio is represented by colour contours in strain–protein ratio diagrams.

2. Materials and methods

2.1. Materials

PPI (NUTRALYS F85G) and vital WG (VITENS CWS) were both purchased from Roquette Frères S.A. (St. Louis, MO, USA). SPI (SUPRO EX 37 IP) was purchased from Solae (Europe S.A.). PPI was composed of 78.6 wt% protein (N × 5.7), WG was composed of 72.4 wt% protein (N × 5.7), SPI was composed of 80.0 wt% protein (N × 5.7) on a dry weight basis, according to Dumas measurements. The manufacturer’s specifications indicated that the PPI contained 1 wt% dietary fibre, 9 wt% lipids, 4 wt% ash; SPI contained ≤1 wt% lipids, ≤5 wt% ash; and WG contained 10 wt% starch, 0.5 wt% cellulose fibre, 3 wt% lipids and 1 wt % ash. PPI, SPI and WG had an average dry matter content of 93.2 wt%, 92.8 wt%, and 92.3 wt%, respectively. Sodium chloride was obtained from Sigma-Aldrich (Zwijndrecht, the Netherlands).

2.2. Preparation of proteinaceous materials

Different ratios of protein were mixed (20/80, 50/50, 80/20) for the PPI–WG and SPI–WG blends. The sample preparation procedure has been described in detail previously by Grabowska et al. (2014). Protein blends (SPI, WG, PPI–WG and SPI–WG) were prepared with a final dry matter content of 40 wt% (Fig. 2). First, 1 wt% sodium chloride was dissolved in distilled water. Then the PPI, SPI and WG materials were prepared by dispersing PPI, SPI or WG powder in the saline solution (at room temperature), followed by mixing by hand using a spatula until a homogeneous paste was obtained. The protein material was then hydrated at room temperature for 30 min and the material was covered...

![Texture Map](image-url)
with Parafilm (Pechiney Plastic Packaging, Chicago, IL, USA) to prevent water evaporation. For the PPI–WG and SPI–WG blends, the WG was mixed into the hydrated PPI or SPI dispersion with a spatula directly before the rheological measurement.

2.3. Rheological properties

The rheological properties of the protein materials were measured with a closed-cavity rheometer (CCR) (RPA Elite, TA instruments, New Castle, DE, USA) (Emin, Quevedo, Wilhelm, & Karbstein, 2017). Approximately 6 g was placed in between two plastic films in the closed cavity, which was sealed with a closing pressure of 4.5 bar to prevent water evaporation at high temperature. The transformation of pea protein dispersion into a solid mass can be observed in Fig. 2 before and after measurement in the CCR, suggesting a kind of melting of the particles during the measurement. The geometry of the CCR has a radius of 22.5 mm, maximum height of the inner cavity of 4 mm and a biconical opening with an angle of 3.35\(^\circ\) for homogeneous transmission of the shear stress to the protein materials. The grooves on the surface of the cones prevent slippage. In this setup, the lower cone oscillates in strain-controlled mode while the upper cone remains stationary. First, the protein material was heated for 2 min at constant temperatures (i.e. 30 \(^\circ\)C, 100 \(^\circ\)C, 120 \(^\circ\)C and 140 \(^\circ\)C) without a shear treatment. Subsequently, strain sweep (0.01\%–1000\%) experiments were performed at these temperatures at a constant frequency (1 Hz). In a second type of test, the protein material was heated at constant temperatures (i.e. 30 \(^\circ\)C, 100 \(^\circ\)C, 120 \(^\circ\)C and 140 \(^\circ\)C) for 2 min and cooled to 30 \(^\circ\)C at a cooling rate of 5 \(^\circ\)C/min without shear treatment. After that, strain sweep experiments were performed at 30 \(^\circ\)C at a constant frequency (1 Hz).

A strain sweep experiment is used to determine the yield stress and the flow stress of a material. The yield stress is defined as the value of the shear stress at the end of the LVE regime. Here, we define this stress as the point where \(G'\) differs more than 5\% from its strain-independent value in the LVE regime (Fig. 3) (Nashif, Jones, & Henderson, 1985; Wereley et al., 2006). The flow stress is defined as the value of shear stress at the crossover point where the storage modulus is equal to the loss modulus (\(G' = G''\)).

2.4. Large amplitude oscillatory shear

The stress and strain data obtained from the LAOS measurements were analysed using the MITlaos software (version 2.1 beta, freeware distributed from MITlaos@mit.edu). The strain amplitude varied in the range of 0.01\%–1000\% at a constant frequency of 1 Hz at 30 \(^\circ\)C. Lissajous curves were used to relate the response of the protein materials to the imposed oscillatory strain. The area enclosed in a Lissajous curve is equal to the energy dissipated per unit volume during one complete cycle of the imposed oscillatory strain. The energy dissipated per unit volume in a single cycle is a function only of the first-order viscous Fourier coefficient (\(G_1''\)); calculated from the intensity and phase of the first-harmonic):

\[
E_d = \oint \sigma \, d\gamma = G_1'' \gamma_0^2
\]

The energy dissipated by a perfectly plastic material in a single cycle is equal to

\[
\langle E_d \rangle_{pp} = 4 \, \gamma_0 \sigma_{max}
\]

for a given strain amplitude (\(\gamma_0\)) and a maximum stress (\(\sigma_{max}\)). The ratio of the actual dissipated energy and the perfectly plastic
dissipation gives the energy dissipation ratio ($\phi$) as proposed by Ewoldt et al. (2010).

$$\phi = \frac{E_d}{(E_d)_{pp}} = \frac{\pi G''\gamma_0}{4\eta_{max}}$$  

(3)

3. Results and discussion

3.1. Texture maps at the end of the LVE regime

Fig. 4 presents the texture map of the PPI–WG blends at ratios of 0/100, 20/80, 50/50, 80/20 and 100/0 at 30 °C, at high temperature (100 °C), and heating at 100 °C and cooling to 30 °C. At 30 °C, PPI materials generally became brittle, whereas WG materials were rubbery. A blend of PPI and WG yielded products with intermediate values in hardness and deformability. More PPI in a blend led to increased stress and reduced strain making the product more brittle. Those values are compared with the stress and strain values obtained from products depicted in Fig. 1. PPI at 40 wt% is tougher than at 20 wt% and 23 wt% PPI (Moreno et al., 2020). The texture properties of PPI (20 wt%) with 5 wt% transglutaminase are tougher compared with only PPI (20 wt%), which have texture properties similar to pre-cooked chicken strips (Mattice & Marangoni, 2020). Upon heating, PPI products changed to more mushy behaviour, whereas WG products became tough (as indicated by the grey arrow in Fig. 4). More PPI in a blend led to lower stress and strain, making the product mushier. The addition of WG led to higher stress and strain, making the product stronger, but also more stretchable. To summarize, upon heating, a shift in the texture map is observed compared with that at 30 °C from brittle to mushy for PPI and from rubbery to tough for WG. A similar shift was observed for blends heated at 120 °C and 140 °C (appendix Fig. A1). After heating and cooling, more PPI in a blend led to reduced stress and strain, making the product more mushy. More WG, however, resulted in an increase in the stress and strain, making the product tougher. A similar trend from mushy to tough texture upon higher WG content in the blend was observed when blends were heated at 120 °C and 140 °C and cooled to 30 °C (appendix Fig. A1). The strengthening of WG and PPI–WG blends after heating and cooling compared with those at 30 °C suggests the formation of additional physical interactions; for example, hydrogen bonding. PPI-only dispersions gave a lower stress and strain after the complete measurement, implying that the network is weakened; for example, a lower ability to form additional physical interactions during cooling.

We compared the behaviour of PPI–WG blends with that of SPI–WG blends. Fig. 4 presents a texture map of the SPI–WG blends at ratios of 0/100, 20/80, 50/50, 80/20, and 100/0. At 30 °C, SPI products were commonly brittle. The combination of SPI and WG yielded products with intermediate values in hardness and deformability. The SPI–WG products showed slightly higher stress values compared with PPI–WG products. Heating SPI to 100 °C slightly transformed the material to rubbery behaviour (as indicated by the grey arrow in Fig. 4). The reduced stress observed in the texture maps of both PPI and SPI compared with 30 °C could be the effect of weakening of the physical interactions that stabilize the protein material, because the protein materials can now be considered as a melt. Heating WG resulted in tougher behaviour, whereas the SPI–WG blend gave slightly smaller strain values with higher SPI content, making the product less stretchable. An opposite trend was observed at higher temperatures (i.e. 120 °C and 140 °C) (appendix Fig. A1) and resulted in a higher strain for SPI and a lower strain for WG. The SPI–WG blend showed products with minimum values for stress and strain. For the SPI–WG blends, small differences were observed in the stress and strain values. This is in contrast to the outcomes with PPI–WG blends, where larger differences were observed in the stress and strain values between the components in the blend. After heating and cooling, both SPI and WG products have higher stress and strain compared with those at 30 °C and both show strengthening of the network, suggesting the formation of additional physical interactions. This is most pronounced for WG. After heating and cooling, the SPI–WG blend did not show products with intermediate values in hardness and deformability. This blend showed slightly higher stress compared with that at 30 °C and higher stress values compared with the PPI–WG blend.

The effect of temperature on both PPI–WG and SPI–WG blends at a 50/50 ratio is presented in a texture map in Fig. 5, at 30 °C, at high temperature (100 °C, 120 °C, 140 °C) and after heating at 100 °C, 120 °C, 140 °C and cooling to 30 °C. The plant protein blends heated to different temperatures covered a wide range of stresses and strains. Without heating, the stresses and strains of the SPI–WG and PPI–WG blends were similar. For the PPI–WG blends, heating at higher temperatures leads mainly to softer products, whereas, for the SPI–WG blends, heating leads to a tougher/rubbery character. After heating and cooling, both PPI–WG and SPI–WG products became tougher, meaning that heating resulted in a stronger material for the blends. This increase after 140 °C was also observed in a previous study in a tensile test at room temperature on PPI–WG product, sheared (39 s⁻¹) and heated (140 °C) in the shear cell (Schreuders et al., 2019). In general, the SPI–WG blends are tougher than the PPI–WG blends.

3.2. Texture maps at the crossover point

The texture properties at the crossover point of both the PPI–WG and SPI–WG blends are shown in Fig. 6. At 30 °C, PPI is characterized as brittle, whereas WG is characterized as rubbery. Combining PPI and WG in a blend yielded a lower intermediate crossover point in hardness and deformability. Heating made PPI products softer and WG products became less deformable. More PPI in a blend led to reduced crossover stress, whereas more WG in the blend led to increased crossover stress.
Heating to higher temperature resulted in a decreased stress for PPI (appendix Fig. A2). After heating and cooling, the PPI and WG materials became comparable with those at 30 °C, however, for WG a further increase in the temperature (i.e. 120 °C and 140 °C) resulted in larger crossover stress and smaller crossover strain (appendix Fig. A2).

SPI-based materials were commonly brittle, whereas WG materials were rubbery at 30 °C. With both SPI and WG, intermediate values in hardness and deformability were obtained in those products. Heating SPI shifted the crossover point to higher strain values and slightly lower stress values, whereas WG products became less deformable upon heating. Higher temperatures resulted in decreased stress for SPI. By combining SPI and WG in a blend, products with intermediate values in hardness and deformability were obtained. A further increase in the heating temperature (i.e. 140 °C) gave a smaller difference between the stress and strain values of SPI and WG (appendix Fig. A2). After heating and cooling, the SPI and WG products became comparable to those at 30 °C, however, increasing the temperature (i.e. 120 °C and 140 °C) resulted in increased stress of the crossover point for SPI and increased stress and decreased strain of the crossover point of WG (appendix Fig. A2).

A texture map for the crossover points is presented in Fig. 7 for both PPI–WG and SPI–WG blends at a 50/50 ratio at 30 °C, at high temperature (100 °C, 120 °C, 140 °C) and after heating at 100 °C, 120 °C, 140 °C and cooling down to 30 °C. At 30 °C, the crossover stress and strain values indicated that the SPI–WG blend became tough, whereas the PPI–WG blend became mushy. For both PPI–WG and SPI–WG blends, heating at higher temperatures led to reduced crossover stress, making the product softer. After heating and cooling, both PPI–WG and SPI–WG products had higher stress compared with those at 30 °C, meaning that heating resulted in a stronger material. After heating and cooling, both PPI–WG and SPI–WG blends at high temperatures resulted in higher stress, making both materials stronger. The results presented
Fig. 8. Colour scheme of the dissipation ratio ($\phi$) in a strain–protein ratio diagram for a PPI–WG and SPI–WG blend at different ratios at 30 °C, heated at 120 °C, and heated at 120 °C and cooled to 30 °C. The colour corresponds to the value of the dissipation ratio ($\phi$) in the colour bar, $\phi = 0$, elastic; $\phi = \pi/4$, viscous; $\phi = 1$, perfect plastic. The colour scheme of the dissipation ratio at increasing temperatures is shown in Video 1 (including heating at 100 °C and 120 °C and heated at 100 °C and 120 °C and cooled to 30 °C). Right: Lissajous curve of stress versus strain amplitude at three different strain amplitudes corresponding to the X symbol in the left panel (individual plots of normalized stress [solid lines] and elastic stress [dashed lines] vs. strain). (For interpretation of the references to colour in this figure legend, the reader is referred to the Web version of this article.)
Fig. 8. (continued).
here confirm that the SPI–WG blends are tougher than the PPI–WG blends.

3.3. Colour scheme to describe the dissipation ratio

A more detailed assessment of the non-linear viscoelastic behaviour of protein materials was obtained with Lissajous curves. The dissipation ratio was then calculated to summarize the essential non-linear behaviour (Euwoldt et al., 2008, 2010; Klost, Brzeski, & Drusch, 2020; Tao et al., 2019). The values are presented in a colour scheme to facilitate comparison. The left-hand panel of Fig. 8 shows these colour schemes for PPI–WG and SPI–WG. In the right-hand panel of Fig. 8, the corresponding elastic Lissajous curves are shown for the grid values of imposed strain amplitude and protein ratios marked by the crosses in the left-hand panel (colour scheme of the dissipation ratio). In the following, the dissipation ratios with increasing strain amplitudes of the SPI–WG and SPI–WG blends at ratios of 0/100, 20/80, 50/50, 80/20, and 100/0 (Fig. 8) are discussed. At 30 °C, PPI showed an increasing dissipation ratio for increasing strain amplitude. The elastic Lissajous curves had a line or narrow ellipse shape for small strain amplitudes, implying that the response of this material was mostly elastic at these strains. With a further increase in the strain amplitude, the area encompassed by the curve became wider. This is an indicator of increased viscous dissipation that allows the protein particles in the matrix to flow past each other, and eventually structure breakdown. The red dashed lines indicate the elastic contributions to the total stress. The dissipation ratio for increasing strain amplitudes remained constant for WG. The PPI–WG blend yielded products with intermediate dissipation ratios. At equal strain amplitude, more PPI in a blend gave a larger dissipation ratio. Heating WG lowered the dissipation ratios for almost all strain amplitudes and a more sudden transition to viscous behaviour. For WG, narrow ellipses were observed at low strain amplitude, indicating the predominant elastic behaviour. The dissipation ratio of PPI did not change upon heating, as indicated by only minor changes in the Lissajous curves of PPI. More PPI in the blend resulted in a gradual increase in the dissipation ratio for increasing strain amplitudes. Most PPI–WG blends yielded intermediate dissipation ratios. After heating and cooling, both PPI and WG became more elastic for a longer strain amplitude compared with the unheated materials. Again this abrupt transition in dissipation ratio for increasing strain amplitude was most pronounced for WG and also present in the blend containing a higher WG content. We now compare the dissipation behaviour of PPI–WG blends with that of SPI–WG blends at different temperatures. The dissipation ratios of unheated SPI–WG and PPI–WG blends at ratios of 20/80, 50/50 and 80/20 were comparable. SPI only showed a larger dissipation ratio for increasing strain amplitudes. Both SPI–WG and PPI–WG blends resulted in products with intermediate dissipation ratios. Heating led to lower dissipation ratios for SPI, WG and SPI–WG blend and resulted in similar elastic behaviour in the case of the SPI–WG blend for different protein ratios. In the Lissajous curves, narrow ellipses were observed at low strain amplitude, indicating the predominant elastic behaviour. Extensive deformation led to a sudden onset of viscous/plastic behaviour. After heating and cooling, both SPI and WG became more elastic across a wider range of strain amplitudes compared with untreated materials. The SPI–WG blend (50/50) showed lower dissipation ratios (~36% strain amplitude) compared with SPI and WG at similar strain amplitude, indicating increased elasticity. That could indicate synergetic effects between SPI and WG, indicative of specific interactions.

3.4. Combining texture maps and colour schemes to describe the dissipation ratio

Texture maps give an efficient and quantitative summary that give food product development teams and process engineers insight into the effects of ingredients and processing conditions on the material properties relevant to product texture. Table 1 gives an overview of all the results presented in the texture maps and colour schemes. Both maps revealed that SPI–WG is tougher than PPI–WG and that an increase in WG in the blend resulted in a more rubbery material. Similar differences between the protein materials were described in previous studies even though a much lower protein concentration (~10 wt%) was investigated than the concentration commonly used in high moisture extrusion cooking (~30 wt%). As observed in previous studies, PPI forms weaker and less elastic gels compared with SPI (Batista, Portugal, Sousa, Crespo, & Tatham, 1997), whereas pea protein and less elastic gels compared with SPI (Batista, Portugal, Sousa, Crespo, & Raymundo, 2005; Lam, Can Karaca, Tyler, & Nickerson, 2018; O’Kane, Happe, Vereijken, Gruppen, & Van Boekel, 2004). Batista et al. (2005) established a relationship between a stronger gel and more protein unfolding during and after thermal treatment. After protein unfolding, protein aggregates are formed through hydrophobic interactions and strengthened further due to the formation of disulphide bridges. The total number of cysteine residues differs between types of protein and the number of potential disulphide bonds that can be formed. The accessibility of free thiol groups and disulphide bonds are both important to network formation. Gluten contains relatively large amounts of cysteine (Shewry & Tatham, 1997), whereas pea protein contains relatively low amounts.

Table 1

| Difference between products* | Texture map | Colour scheme |
|-----------------------------|-------------|---------------|
| SPI–WG compared to PPI–WG   | End of the LVE regime | Crossover point |
| Effect of heating*          | Tougher     | Tougher       |
| WG                          | Tougher     | More elastic  |
| SPI                         | Slightly tougher | Slightly tougher |
| PPI                         | Muddy       | More elastic  |
| SPI–WG                      | Stronger/tougher | Slightly more elastic |
| PPI–WG                      | Stronger    | More elastic  |
| Increased ratio of WG in the blend | Rubber | Rubber* |
| SPI–WG                      | Rubbery/more deformable* | Rubber* |
| PPI–WG                      | Rubbery     | More elastic* |

Here confirm that the SPI–WG blends are tougher than the PPI–WG blends.

| Summary of the texture maps and colour schemes presented in this paper (marked with an asterisk) after heating and cooling. |
|---|---|---|
| Texture map | Colour scheme |
| End of the LVE regime | Crossover point |
| Tougher | More elastic |
| Slightly more brittle | More elastic |
| Muddy | More elastic |
| Stronger/tougher | Slightly more elastic |
| Stronger | More elastic |
| Rubber | Rubber* |
| Rubber/more deformable* | Rubber* |
| Rubber | More elastic* |
temperature and strain amplitude will influence the material. At larger strain, the protein aggregates in the matrix start to flow past each other. Heating and cooling transformed PPI into a slightly tougher product and WG into a more brittle product. This texture map in the non-linear regime is especially interesting for shear-induced structuring where the material is sheared beyond the linear regime. The linear and non-linear regimes also explain the different response of the protein materials after heating. Therefore, we conclude that analysing the combination of the two texture maps is important.

The texture of protein-based food products is influenced by both composition and process conditions. The main question is the mechanisms underlying the differences in stresses and strains of the blends. Two different situations can be observed in the texture maps:

1. A blend gives intermediate hardness and deformability, and intermediate values in stress and strain values. Heating PPI makes the blend weaker and less deformable, whereas WG increases the strain and stress making the gels tougher. For PPI-WG blends, the end of the LVE regime was observed in the blend with intermediate values in hardness and deformability of PPI and WG. Similarly for non-linear rheology, intermediate dissipation ratio values were observed.

2. Blends yield intermediate values in hardness and deformability but minimum stress and strain values. For SPI-WG, this behaviour was observed in the texture maps. We hypothesize that this could be due to phase inversion, the point in the texture map where blend components exchange their discontinuity. The blend with low WG content is SPI continuous. As the WG content increases in the blend, a continuous WG network is formed or a bi-continuous WG network that is entrapping the SPI network. In the dissipation ratio maps, a lower dissipation ratio was observed in the blend compared with the single components, which indicated increased elasticity in the blend. Furthermore, the stress and strain values of SPI and WG in the SPI-WG blend are closer together in the texture and dissipation maps, whereas the PPI and WG phases in the PPI-WG blend show a distinct difference.

4. Conclusion

The rheological properties of SPI, PPI and blends of these with WG were quantified using texture maps and dissipation ratios obtained from large-deformation Lissajous curves. Different composition and processing conditions were investigated. We showed that the three rheological parameters, (1) stress at the end of the LVE regime, (2) the stress-strain crossover point and (3) the dissipation ratio, provide a useful rheological fingerprint of these food products and materials.

As observed in the maps and schemes, heating induced more elasticity. In PPI-WG blends, PPI has lower strain, stress, and elasticity compared with WG. In SPI-WG blends, the texture properties are almost similar for the two components. SPI-WG blends are tougher and more elastic compared with PPI-WG blends. Mapping the rheological properties at the end of the LVE regime, the crossover point as well as the dissipation ratio as a function of small and large strain amplitudes, is useful for further understanding and use of dense protein blends.

CRediT author statement

Floor K. G. Schreuders: Investigation, Writing - Original Draft, Writing - Review & Editing; Leonard M.C. Sagis: Writing - Review & Editing; Igor Bodnar: Writing - Review & Editing; Philipp Erni: Writing - Review & Editing; Remko M. Boom: Supervision, Writing - Review & Editing; Atze Jan van der Goot (*corresponding author): – Supervision, Writing - Review & Editing

Declaration of competing interest

The authors report no conflicts of interest relevant to this article.

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Appendix A. Supplementary data

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