Magnetoelastic and magnetostrictive properties of Co$_2$XAl Heusler compounds

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We present a comprehensive first-principles electronic structure study of the magnetoelastic and magnetostrictive properties in Co-based Co$_2$XAl ($X = V$, Ti, Cr, Mn, Fe) full Heusler compounds. In addition to the commonly used total energy approach, we employ the torque method to calculate the magnetoelastic tensor elements. We show that the torque-based methods are, in general, computationally more efficient and allow us to unveil the atomic and orbital contributions to the magnetoelastic constants in an exact manner, as opposed to the conventional approaches based on second-order perturbation with respect to the spin-orbit coupling. The magnetostriction constants are in good agreement with available experimental data. The results reveal that the main contribution to the magnetostriction constants, $\lambda_{100}$ and $\lambda_{111}$, arises primarily from the strain-induced modulation of the $\langle d_{z^2} | L_z | d_{xy} \rangle$ and $\langle d_z^2 | L_x | d_z \rangle$ spin-orbit coupling matrix elements, respectively, of the Co atoms.

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I. INTRODUCTION

The development of efficient and scalable means to manipulate the magnetic state has been one of the main foci of scientific research in the field of condensed-matter physics and material science in the past century. The use of magnetoelastic materials employed in multiferroic heterostructures offers a promising avenue for efficient, scalable, and nonvolatile magnetic-based memory devices [1]. Magnetoelasticity is a phenomenon in which a deformation of the crystal shape results in a change in magnetic orientation and vice versa. In addition to applications in multiferroic-based magnetic memory devices, compounds with a large magnetoelastic constant are also of great interest in the development of efficient magnetomechanical actuators [2], magnetic field sensors, strain-mediated miniaturized multiferroic-based antennas, and other energy converter devices [3–5]. Therefore, development of a concise and efficient framework to calculate the magnetoelastic constants and understand their microscopic origin is of paramount importance in the search for magnetoelastic materials [6–8].

Even though rare-earth 3$d$ metal compounds, such as Terfenol-D, exhibit the highest magnetostrictive values (1500–2000 ppm) at room temperature, their use in industrial applications is hindered by the need for high-saturation magnetic field (due to their large magnetocrystalline anisotropy), brittleness, and high material costs [9]. Subsequently, highly magnetostrictive rare-earth-free Fe-based alloys were developed, such as Fe$_{62.5}$Ga$_{15}$ (galfenol) [10,11] and Fe$_{62}$Al$_{15}$ (alfenol) [12], which display large strain at moderate field and excellent ductility. In addition, spinel ferrites (Co$_{1-x}$Fe$_2$O$_4$, NiFe$_2$O$_4$) with large magnetostriction [7] and high magnetic ordering temperatures were recently used in magnetostrictive-piezoelectric composites to enhance the interfacial magnetoelastic coupling [13].

Another remarkable class of materials is the Heusler ternary intermetallic compounds that crystallize in the $L_2$ structure and have stoichiometric composition of $X_2YZ$ (space group $Fm\bar{3}m$), where $X$ and $Y$ are transition metal elements and $Z$ is an element from the $p$ block [14,15]. They show a wide range of remarkable properties such as half-metallicity [14], high Curie temperatures [16], giant tunnel magnetoresistance [17,18], magnetic shape memory [19], superconductivity [20], topological Weyl fermions [14,21,22], and the anomalous Nernst effect [23]. More specifically, the cobalt-based Heusler compounds such as Co$_2$XAl ($X = Ti, V, Cr, Mn, Fe$) offer an interesting playground for spintronics applications since they have high Curie temperatures and some of them are predicted to be half-metallic ferromagnets [14,15]. Nevertheless, their magnetoelastic and magnetostrictive properties remain unexplored both experimentally and theoretically.

Here, we provide a general framework in which we employ different approaches to calculate the magnetoelastic and magnetostriction tensor elements of Co$_2$XAl ($X = V, Ti, Cr, Mn, Fe$) full Heusler compounds from first-principles electronic structure calculations. The first one is the well-known approach based on total energy calculations, and the other two are based on the torque and spin-orbital torque methods. We show that the torque-based methods are computationally more efficient and allow for the atomic and orbital decomposition of the magnetoelastic constants, which can, in turn, elucidate the underlying atomic mechanisms.

II. THEORETICAL FORMALISM

A. Magnetocrystalline anisotropy

The origin of the magnetocrystalline anisotropy (MCA) energy is the spin-orbit interaction and can be determined,
within density-functional theory, from the second-variation method employing the scalar-relativistic eigenfunctions of the valence states [24,25]. In first-principles electronic structure calculations two approaches are often used to calculate the MCA, namely, the total energy and torque methods.

**Total energy approach.** The total energy \( E_{\text{tot}}(\vec{m}) \) is determined for several magnetic orientations described by the unit vector \( \vec{m} \), which in turn is fitted to lowest order in the magnetic degrees of freedom, given by

\[
E_{\text{tot}}(\vec{m}) = E_{\text{el}} + \sum_{ij} K_{ij}^m m_i m_j .
\]

Here, \( K_{ij}^m \) are the MCA tensor matrix elements, and \( m_i \) are the components of the magnetization orientation unit vector \( \vec{m} \).

As an alternative approach, instead of the total energy, one can employ the so-called force theorem [26], in which the dependence of the electronic energy on the magnetization value of the angular derivative of the spin-orbit coupling (SOC) Hamiltonian at an angle \( \theta = 45^\circ \),

\[
T(\theta) = \sum_{nk} \langle \Psi_{nk}^{\text{SOC}} | \frac{\partial H_{\text{SOC}}}{\partial \theta} | \Psi_{nk}^{\text{SOC}} \rangle_{\theta = 45^\circ}.
\]

Here, \( \Psi_{nk}^{\text{SOC}} \) is the nth relativistic eigenvector at the \( k \) point, and \( \theta \) is the angle between the magnetization direction and the surface normal.

The one-electron Kohn-Sham Hamiltonian can be expressed as [28,29]

\[
\hat{H} = \hat{H}_k(\vec{k}) + \hat{\Delta}(\vec{k}) \cdot \vec{m} + \hat{H}_{\text{soc}}(\vec{k}),
\]

where the first, second, and third terms represent the kinetic, exchange, and SOC contributions, respectively. In a nonorthonormal atomic-orbital basis set, the eigenenergies and eigenstates are calculated from the generalized eigenvalue problem, \( \hat{H}|n\vec{k}\rangle = \epsilon_{nk} |n\vec{k}\rangle = \epsilon_{nk} \hat{O}_{nk}|n\vec{k}\rangle \), where \( \hat{O}(\vec{k}) \) is the overlap matrix. In this case, the torque is given by [28]

\[
\tau_{\text{MCA}} = -\vec{m} \times \langle \hat{\Delta} \vec{\sigma} \rangle,
\]

where the equilibrium expectation value is calculated from

\[
\langle \cdots \rangle = \frac{1}{N_k} \sum_{nk} \langle \vec{n}\vec{k} | \cdots | \vec{n}\vec{k} \rangle \frac{\epsilon_{nk} - \mu_0}{O_{nk}} .
\]

Unlike the total energy method, the torque approach involves a vector for the fitting to the magnetization orientation, and also it does not require the calculation of a reference energy, making it computationally more efficient. Furthermore, the torque method can be used to calculate the local (site-resolved) contribution to the MCA energy since the exchange splitting \( \Delta \) is often a well-defined local quantity.

In this paper, instead of the aforementioned torque method we employ a different approach we recently developed [30] based on the canonical forces, \( F_\theta = \vec{n} \times \vec{\tau} = -\langle \hat{\Delta} \vec{\sigma} \rangle \) and \( F_\phi = \vec{e}_z \cdot \vec{e}_\phi = -\langle \hat{\Delta} \vec{\sigma} \rangle \), where \( \theta \) (\( \phi \)) is the polar (azimuthal) angle, \( \vec{n} = \sin \vec{e}_\phi - \cos \phi \vec{e}_z \), and \( \vec{e}_\phi \) is the unit vector along \( \phi \). Applying the unitary operator \( \hat{U} = e^{i\frac{\epsilon_{nk} \phi}{2}} \) on the Hamiltonian to reorient the exchange splitting term along the \( z \) axis, we find

\[
F_q = 2\text{Re} \left\{ \hat{U} \frac{\partial \hat{U}^+}{\partial \hat{q}} \hat{H}_{\text{soc}} \right\} . \quad q = \theta, \phi.
\]

Using Eq. (7) for \( q = \theta \), one can obtain an explicit expression for the MCA-induced torque,

\[
\tau_{\text{MCA}} = \langle \vec{\xi} \vec{L} \times \vec{\sigma} \rangle,
\]

which we refer to as the “spin-orbital” torque approach [29,30] as opposed to the original torque method given by Eq. (5). It should be pointed out that Eq. (8) is exact and no approximation was involved in its derivation.

Equation (8) can be interpreted as the torque induced by the anisotropic orbital moment accumulation \( \vec{L} \) on the spin \( \vec{\sigma} \) of the valence electrons. Since the SOC strength \( \vec{\xi} \) is diagonal in the atomic-orbital basis set and a well-defined local quantity, we can use Eq. (8) to decompose the torque on each atom. This decomposition allows us, in turn, to elucidate the atomic origin of the MCA as opposed to the local MCA-induced field on each atomic spin given by Eq. (5). Therefore, the advantage of using Eqs. (7) and (8) is that they allow us to unveil the underlying origin of the MCA. Employing Eq. (8), the atom and orbital contributions to the total torque can be written as

\[
\langle \alpha | \vec{\xi} \vec{L} \times \vec{\sigma} | \beta \rangle = \sum_{ss'} \rho_{\alpha ss'}^{1,ab} | I_{\alpha s} \vec{L} \times \vec{\sigma} | I_{\beta s'} \rangle ,
\]

where \( I \) is the atomic index, \( \alpha, \beta (s,s') \) are the orbital (spin) indices, and

\[
\rho_{\alpha ss'}^{1,ab} = \frac{1}{N_k} \sum_{nk} (I_{\beta s'} | n\vec{k} \rangle f(\epsilon_{nk} - \mu_0) O_{nk} (n\vec{k} | I_{\alpha s} \rangle)
\]

is the density matrix.

**B. Magnetoelastic effect**

Magnetoelastic coupling is the interaction between the magnetization and the strain in a magnetic material. In the presence of strain \( \epsilon_{ij} \), the modified primitive lattice vectors \( \vec{a}'_j \) are given by \( (\vec{a}'_j - \vec{a}_j) \cdot \vec{e}_j = \sum_i \vec{a}_i \cdot \vec{e}_i \epsilon_{ij} \), where \( \vec{e}_j \) represent unit vectors in Cartesian coordinates. To lowest order in the lattice deformation (i.e., small strain) and magnetization orientation, the total energy per equilibrium volume is given by

\[
E(\vec{m}) = E_0 + \frac{1}{2} \sum_{i \in s, j \in I} C_{ij}^{ss'} \epsilon_{ij} \epsilon_{kl} + \sum_{ij} K_{ij}^m (\epsilon_{kl}) m_i m_j .
\]
where $C_{kl}^{ij}$ are the elastic stiffness constants, often represented by a $6 \times 6$ matrix. To linear order in strain, the MCA tensor matrix elements have the form $K_{ij}^{kl}(\epsilon_{kl}) = C_{kl}^{ij} + \sum_{k<l} B_{kl}^{ij} \epsilon_{kl}$, where $B_{kl}^{ij}$ denote the magnetoelastic tensor elements.

The magnetostriction effect, first identified in 1842 by Joule [31], is a property of ferromagnetic materials that causes them to change their shape when subjected to a magnetic field. In the absence of an external stress, the strain induced on the crystal structure due to the reorientation of the magnetization can be calculated by setting $\partial E(\delta)/\partial \epsilon_{kl} = 0$,

$$\epsilon_{kl} = - \sum_{ij} h_{kl}^{ij} u_i u_j,$$

where $h_{kl}^{ij} = \sum_{k<l} S_{kl}^{ij} B_{kl}^{ij}$ are the magnetostriction tensor elements and $S_{kl}^{ij}$ are the elastic compliance constants. Under the applied strain $\epsilon_{ij}$, the relative change in the length of the material $\delta l/l$ along a direction given by the unit vector $\vec{u}$ can be calculated \[32,33\] by $\delta l/l = \sum_{ij} \epsilon_{ij} u_i u_j$. Using Eq. (12) for the strain, the relative change in the length due to the reorientation of the magnetization can be calculated by

$$\frac{\delta l}{l} = - \sum_{ijkl} h_{kl}^{ij} u_i u_j m_k m_l.$$  \hspace{1cm} (13)

Given that the components of the unit vectors $\vec{u}$ and $\vec{m}$ describe the directions of the relative change in the length and magnetization, respectively, are independent, the basis set in Eq. (13) consisting of $u_i u_j$ and $m_k m_l$ is overcomplete. One approach to resolve this issue is to switch to the spherical Harmonics basis set [34], which is more advantageous, especially when dealing with ensemble averaging. In the following we use this approach to obtain a general expression for the polycrystalline magnetostriction constant. Using the second-order spherical Harmonics, we can rewrite Eq. (13) in the form

$$\frac{\delta l}{l} = \frac{4\pi}{5} \sum_p \lambda_{p}^{(0)} Y_{2,p}(\vec{m}) + \frac{4\pi}{5} \sum_{pq} \lambda_{pq}^{(2)} Y_{2,p}(\vec{m}) Y_{2,q}(\vec{u}),$$

where the isotropic (volumetric) magnetostriction constant $\lambda_{p}^{(0)}$ ($p = 1, \ldots, 5$) and anisotropic magnetostriction constants $\lambda_{pq}^{(2)}$ can be expressed (see the Appendix) in terms of $h_{kl}^{ij}$ and $Y_{2,p}$ are the real spherical harmonics, given by

$$Y_{2,p}(\vec{\rho}) = \sqrt{\frac{15}{4\pi}} \left( x^2 - y^2, 3z^2 - 1, 2xy, xz, yz \right).$$

For a polycrystalline structure the field-induced relative change in the length has the form $\delta l/l = \lambda_s P_z(\vec{m} \cdot \vec{u})$, where $P_z(x)$ denotes the Legendre polynomials of order 2. Therefore, the average magnetostriction constant $\lambda_s$ can be calculated by

$$\lambda_s = \frac{5}{(4\pi)^3} \int d\Omega_m d\Omega_u \frac{\delta l}{l} P_z(\vec{m} \cdot \vec{u}) = \frac{1}{5} \sum_p \lambda_{pq}^{(2)}.$$  \hspace{1cm} (16)

For a cubic crystal structure the magnetostriction constant matrix $\lambda_{pq}^{(2)}$ is diagonal, and the magnetic-field-induced shape deformation is given by

$$\frac{\delta l}{l} = \frac{4\pi}{5} \left[ \lambda_{[100]} \sum_{p=1,2} Y_{2,p}(\vec{m}) + \lambda_{[111]} \sum_{p=3,4,5} Y_{2,p}(\vec{m}) \right].$$  \hspace{1cm} (17)

In this case, for the polycrystalline magnetostriction constant we obtain $\lambda_s = (2\lambda_{[100]} + 3\lambda_{[111]})/5$ \[32\].

III. COMPUTATIONAL APPROACHES

We have employed two ab initio electronic structure codes to determine the magnetoelastic tensor elements. The first is the plane wave Vienna ab initio Simulation Package (VASP) \[35,36\], where we have employed the total energy approach. The second is the linear combination of atomic orbitals (LCAO) OPENMX package \[37–39\], where one can employ any of the four approaches, namely, the total energy, the band energy [Eq. (2)], the torque [Eq. (5)], or the spin-orbital torque [Eq. (8)] approach. Throughout the remainder of the paper all OPENMX results employ the more computationally efficient spin-orbital torque approach.

(1) Structural relaxations were carried out using VASP \[35,36\] within the generalized gradient approximation as parameterized by Perdew, Burke, and Ernzerhof \[40\] (PBE) when the largest atomic force is smaller than 0.01 eV Å$^{-1}$. The pseudopotential and wave functions are treated within the projector augmented-wave method \[41,42\]. The plane wave cutoff energy was set to 500 eV, and an $18^3$ k-point mesh was used in the Brillouin zone (BZ) sampling. Total energy calculations were carried out for nine different magnetization orientations, $\vec{m} = [1,0,0], [0,1,0], [0,0,1], [1,1,0], [1,1,0], [1,0,1], [1,0,1], [0,1,1],$ and [0,1,1]. The MCA tensor elements in Eq. (11) were then calculated by

$$K_{zz} = 0,$$

$$K_{xx} = E^{[1,0,0]} - E^{[0,0,1]},$$

$$K_{yy} = E^{[0,1,0]} - E^{[0,0,1]},$$

$$K_{xy} = \frac{E^{[1,1,0]} - E^{[1,1,0]}}{2},$$

$$K_{yz} = \frac{E^{[0,1,1]} - E^{[0,1,-1]}}{2},$$

$$K_{xz} = \frac{E^{[1,0,1]} - E^{[1,0,-1]}}{2}. $$ \hspace{1cm} (18a)

For a cubic crystal structure the field-induced relative change in the length has the form $\delta l/l = \lambda_s P_z(\vec{m} \cdot \vec{u})$, where $P_z(x)$ denotes the Legendre polynomials of order 2. Therefore, the average magnetostriction constant $\lambda_s$ can be calculated by

$$\lambda_s = \frac{5}{(4\pi)^3} \int d\Omega_m d\Omega_u \frac{\delta l}{l} P_z(\vec{m} \cdot \vec{u}) = \frac{1}{5} \sum_p \lambda_{pq}^{(2)}.$$  \hspace{1cm} (16)

(2) Using the lattice parameters determined from VASP calculations, the tight-binding Hamiltonian $H_k$ and overlap $O_k$ matrices were calculated in the LCAO OPENMX package \[37–39\]. We adopted the Troullier-Martins-type norm-conserving pseudopotentials \[43\] with partial core correction. We used $24^3$ k points in the first BZ and an energy cutoff of 350 Ry for numerical integrations in the real-space grid. For the exchange correlation functional the Local Spin Density Approximation (LSDA) \[44\] parameterized by Perdew and Zunger \[45\] was used. The MCA tensor elements $K_{ij}$ are determined via the spin-orbital torque [Eq. (8)] method

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for three magnetization directions, \( \vec{m} = [1,0,0], [1,0,1], \) and [0,1,1], from the expressions

\[
\begin{align}
\varpi_{MCA}^{[1]} & = [0,2K_{xx},-2K_{yy}], \\
\varpi_{MCA}^{[0]} & = [K_{xx}+K_{yy},K_{zz}-K_{xx},-K_{yy}-K_{zz}], \\
\varpi_{MCA}^{[1]} & = [K_{yy}-K_{zz},-K_{xx}-K_{yy},K_{zz}].
\end{align}
\]

The magnetoelastic constant tensor elements \( B_{ij}^{kl} \) are determined from MCA calculations under 12 strain \( \varepsilon_{kl} \) values of \( \varepsilon_{xx} = \pm \delta_{x}, \varepsilon_{yy} = \pm \delta_{y}, \varepsilon_{xy} = \pm \delta_{x}, \varepsilon_{xy} = \pm \delta_{y}, \varepsilon_{xz} = \pm \delta_{x}, \) \( \varepsilon_{yz} = \pm \delta_{y}, \) where \( \delta_{x} = \delta_{y} = 0.01. \) The magnetoelastic constant tensor elements are then simply given by

\[
B_{ij}^{kl} = \frac{K_{ij}(\varepsilon_{kl} = \delta_{x}) - K_{ij}(\varepsilon_{kl} = -\delta_{x})}{2\delta_{x}}. \tag{20}
\]

It should be noted that the symmetry of the crystal structure can significantly reduce the number of independent configurations (induced strain and magnetization directions) required to obtain the magnetoelastic tensor elements. In particular, in cubic systems, only two nonzero independent magnetoelastic constants exist that are referred to as \( B_{1} = B_{111} = B_{122} = B_{133} = -B_{222} = B_{233} \) and \( B_{2} = B_{113} = B_{123} = B_{132} = B_{231} = B_{312} = B_{321}. \) These constants corresponding to the normal and shear-induced MCAs, respectively.

**IV. RESULTS AND DISCUSSION**

The Heusler compounds \( \text{Co}_2\text{XAl} \) crystallize in the cubic \( L2_1 \) structure (space group \( Fm\overline{3}m \)) which is shown in the inset of Fig. 1(a). The Co atoms occupy Wyckoff position \( 8c \) (1/4, 1/4, 1/4); the \( X \) and Al atoms are located at \( 4a \) (0, 0, 0) and \( 4b \) (1/2, 1/2, 1/2), respectively. As depicted in Fig. 1(a), this structure consists of four interpenetrating fcc sublattices, two of which are equally occupied by \( X \) \([14,15]\).

The calculated lattice constants shown in Fig. 1(b) demonstrate a monotonic decrease with increasing atomic number of the \( X \) element, consistent with their corresponding atomic radius. We have also carried out PBE+U calculations where we used the values of \( U \) for the \( d \) orbitals of Co and the \( X \) elements from Ref. \([46]\). The effect of \( U \) on the lattice constants [blue dashed curve in Fig. 1(b)] shows a slight increase of the lattice constant when compared to the case without \( U \). The results are in good agreement with the experimentally reported data \([47–62]\), denoted by black stars in Fig. 1(b). Heusler compounds are known for their well-behaved magnetic properties in terms of their total number of valence electrons. The total magnetic moment per formula unit is shown in Fig. 1(c) versus the \( X \) element (sorted with respect to its atomic number). In agreement with the Slater-Pauling curve \([63]\), the magnetic moment per formula unit is an integer number that depends linearly on the number of valence electrons per formula unit \( N_v \), given by \( M_s = N_v - 24 \left( M_s = 34 - N_v \right) \) for \( X \leq Fe \). Surprisingly, the results are relatively insensitive to the exchange correlation functional (PBE, PBE+U, or LSDA), and except for \( \text{Co}_2\text{CrAl} \), the \( ab \ initio \) results are in relatively good agreement with the experimentally reported findings in Refs. \([47–62]\). The slight increase of the magnetic moment in \( \text{Co}_2\text{MnAl} \) due to the inclusion of \( U \) is in agreement with previous density functional theory (DFT) calculations \([46]\). The origin of the discrepancy in the case of \( \text{Co}_2\text{CrAl} \) is attributed to \( B2 \)-like disorder and antiferromagnetic coupling of Cr with its neighbors, leading to ferrimagnetic behavior \([64]\).

For cubic crystal structures the elastic energy is given by

\[
E_{el} = \frac{1}{2} C_{11}(\varepsilon_{xx}^2 + \varepsilon_{yy}^2 + \varepsilon_{zz}^2) + \frac{1}{2} C_{44}(\varepsilon_{xy}^2 + \varepsilon_{yz}^2 + \varepsilon_{xz}^2)
\]

\[
+ C_{12}(\varepsilon_{xx}\varepsilon_{yy} + \varepsilon_{yy}\varepsilon_{zz} + \varepsilon_{xx}\varepsilon_{zz}), \tag{21}
\]

where the subscripts in \( C_{ij} \) correspond to the Voigt notation \( [(1, 2, 3, 4, 5, 6)] = [xx, yy, zz, xy, xz, yz] \). In Fig. 1(d) we present the calculated (using VASP) elastic constants \( C_{11}, C_{12}, \) and \( C_{44} \) versus \( X \) elements. The results are in good agreement with previous first-principles electronic structure calculations \([65]\). The solid (dashed) lines in Fig. 1(d) correspond to the DFT calculations without (with) the Hubbard \( U \) term. The inclusion of \( U \) results in an overall decrease of the \( C_{11} \) and \( C_{12} \) elastic constants and a small change in \( C_{44} \). Elastic stability of a compound requires that all eigenvalues of the \( 6 \times 6 \) elastic matrix be positive. For a cubic crystal structure the eigenvalues are \( C_{44}, C_{11} + 2C_{12}, \) and \( C_{11} - C_{12}, \) corresponding to shear, bulk, and tetragonal shear moduli, respectively. The results for the elastic constants presented in Fig. 1(b) demonstrate that all compounds are stable under any elastic deformation.

The magnetoelastic energy for a cubic crystal structure is given by \([32]\)

\[
E_{me} = B_1(\varepsilon_{xx} m_x^3 + \varepsilon_{yy} m_y^3 + \varepsilon_{zz} m_z^3)
\]

\[
+ B_2(\varepsilon_{xy} m_x m_y + \varepsilon_{yz} m_y m_z + \varepsilon_{xz} m_z m_x). \tag{22}
\]
The results of VASP calculations using PBE without (with) the ferrites. In Fig. 3(b) we show the magnetostriction constants of magnitude than the corresponding values for the spinel family.

The polycrystalline magnetostriction constant using PBE and NiFe$_2$O$_4$ [7]. The magnetoelastic coupling constants range from about $-15$ to $+10$ MPa, which are higher by an order of magnitude than the corresponding values for the spinel ferrites. In Fig. 3(b) we show the magnetostriction constants $\lambda_{[100]}$ and $\lambda_{[111]}$ and the average magnetostriction constant $\lambda$, suitable for polycrystalline systems, versus the $X$ element. The polycrystalline magnetostriction constant using PBE+$U$ (dashed green curve) is approximately 50% lower than the corresponding values without $U$ (solid green curve). Since the difference between the magnetoelastic constants obtained from VASP and OPENMX is small, we show in Fig. 3(b) only the magnetostriction constants calculated from VASP. For comparison we also display the available experimental values of $\lambda$ for Co$_2$MnAl [66] and Co$_2$FeAl [67] at room temperature. To understand the underlying origin of the magnetoelastic properties across the series we have used Eq. (9) employed in the OPENMX DFT package to resolve the total torque into the spin-and-orbital contributions to the magnetoelastic constant $K^{xx}$ and $K^{xy}$ of magnitude than the corresponding values for the spinel ferrites CoFe$_2$O$_4$ [7]. The magnetoelastic coupling constants range from about $-15$ to $+10$ MPa, which are higher by an order of magnitude than the corresponding values for the spinel ferrites. In Fig. 3(b) we show the magnetostriction constants $\lambda_{[100]}$ and $\lambda_{[111]}$ and the average magnetostriction constant $\lambda$, suitable for polycrystalline systems, versus the $X$ element. The polycrystalline magnetostriction constant using PBE+$U$ (dashed green curve) is approximately 50% lower than the corresponding values without $U$ (solid green curve). Since the difference between the magnetoelastic constants obtained from VASP and OPENMX is small, we show in Fig. 3(b) only the magnetostriction constants calculated from VASP. For comparison we also display the available experimental values of $\lambda$ for Co$_2$MnAl [66] and Co$_2$FeAl [67]. Overall, the DFT+$U$ results are in better agreement with the experimentally reported room-temperature values. It should be noted that since thermal spin and phonon fluctuations are not taken into account in the DFT calculations, one should not expect very good agreement between the results of the two different $ab$ initio packages. The effect of $U$ is to reduce both magnetoelastic constants by a factor of 2.

Figure 3(a) shows that the magnetoelastic constant $B_1$ is negative for all members of the Co$_2$XAl family, except for Co$_2$TiAl, which is positive. The solid (dashed) lines in Fig. 3(a) are the results of the calculation using OPENMX with the LSDA exchange correlation functional (stars). For comparison we also show the experimental values (black stars) for Co$_2$MnAl [66] and Co$_2$FeAl [67] at room temperature.

To understand the underlying origin of the magnetoelastic properties across the series we have used Eq. (9) employed in the OPENMX DFT package to resolve the total torque into its atomic and orbital contributions. In Figs. 4(a) and 4(b) [Figs. 4(c) and 4(d)] we show the orbital and atomic contributions to the magnetoelastic constant $K^{xx}$ ($K^{xy}$) versus $X$ elements. The MCA constants originate primarily from the $X$ elements, shown in the left and right panels, respectively. On the left-hand ordinate in Fig. 4 we display $K^{xx}$ (meV/f.u.) and $K^{xy}$ (meV/f.u.). In Fig. 4(b) we show the magnetoelastic constants $K^{xx}$ and $K^{xy}$ calculated from the “spin-orbital” torque approach under $\varepsilon_{xx}$ and $\varepsilon_{xy}$ strains, respectively, for the Co$_2$XAl ($X$ = Ti, V, Cr, Mn, Fe) family.
the nonzero matrix elements of the three components of the orbital angular momentum operators, $\hat{L}_x$, $\hat{L}_y$, and $\hat{L}_z$.

For a cubic crystal structure subject to strain along $z$, the nonzero MCA constant, $K_{xx} = K_{yy}$, is given by

$$K^{xx} = -\frac{1}{2MCA}\cdot \hat{e}_z = -\frac{1}{2}\langle \hat{L}_z \hat{\sigma}_z - \hat{L}_z \hat{\sigma}_x \rangle,$$

(23)

where the first and second terms correspond to the in-plane ($xy$-plane) and out-of-plane ($z$-axis) contributions of the strain-induced orbital moment accumulation, respectively. This is consistent with Figs. 4(a) and 4(b), where the magnetoelastic constant $B_1$ is dominated by the contribution of the strain-induced $\hat{L}_z$ orbital moment accumulation of the Co atoms. The $\langle d_{x^2-y^2}\vert \hat{L}_z \vert d_{x^2-y^2} \rangle$ contribution to $B_1$ can be further decomposed into the spin-diagonal and spin-off-diagonal components, where, according to the second-order perturbation approach, the former (latter) yields positive (negative) contributions to the uniaxial MCA. Under a tensile strain along $z$ we find a significant reduction of $\langle d_{x^2-y^2}\vert \hat{L}_z \vert d_{x^2-y^2} \rangle$, resulting in a negative sign for $B_1$.

Similarly, using the spin-orbital torque expression and the strain-induced MCA under biaxial $\varepsilon_{xy}$ strain, the magnetoelastic constant $K^{xy}$ is given by the expression

$$K^{xy} = -\frac{1}{2MCA}\cdot \hat{e}_z = -\frac{1}{2}\langle \hat{L}_x \hat{\sigma}_y - \hat{L}_y \hat{\sigma}_x \rangle,$$

(24)

In the rotated frame of reference where the magnetization is along $z$, Eq. (24) shows that the spin-diagonal (spin-off-diagonal) matrix elements contribute to the orbital moment accumulation along $y$ (x). Similar to the $K^{xx}$ magnetoelastic constant, the main contribution to $K^{xy}$ arises from the Co atoms, where the negative sign of $B_2$ is mainly due to the $\langle d_{x^2-y^2}\vert \hat{L}_z \vert d_{x^2-y^2} \rangle$ orbital momentum matrix element. The sign reversal of $K^{xy}$ for $X = \text{Mn}$ is due to the relatively large positive contribution to the strain-induced orbital moment accumulation along the $y$ axis.

V. CONCLUSION

In summary, we have presented a detailed first-principles study of the magnetoelastic and magnetostrictive properties of Co$_2$XAl full Heusler compounds that crystallize in the $L_2_1$ structure. We described three computational approaches to calculate the magnetoelastic and magnetostriiction tensor matrix elements. The first one is the well-known approach based on total energy calculations. The other two novel approaches are based on the torque [28] and spin-orbital torque [30] approaches, respectively. The latter two are computationally more efficient and allow the atomic and orbital decompositions of the magnetoelastic constants which can, in turn, elucidate the underlying atomic mechanisms. In addition, a general approach was presented to determine the average magnetostriiction constants that is suitable for polycrystalline systems in terms of the magnetostriiction tensor matrix elements. The results of the different computational approaches, using both the VASP and OPENMX packages, agree well, and they are also in good agreement with available experimental data.

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APPENDIX

The isotropic (volumetric) magnetostriiction constants $\lambda^{(0)}_p$ and anisotropic magnetostriiction constants $\lambda^{(2)}_{pq}$ can be expressed in terms of the magnetostriiction tensor elements $h^d_{ij}$,

$$\lambda^{(0)}_1 = \frac{1}{9} \sum_i (2h_{zz}^{zz} - h_{xx}^{xx} - h_{yy}^{yy}),$$

(A1a)

$$\lambda^{(0)}_2 = \frac{1}{3\sqrt{3}} \sum_i (h_{zz}^{zz} - h_{yy}^{yy}),$$

(A1b)

$$\lambda^{(2)}_{11} = \frac{1}{9} \left( 4h_{zz}^{zz} + h_{xx}^{xx} + h_{yy}^{yy} + h_{zz}^{zz} - 2h_{xx}^{xx} - 2h_{yy}^{yy} + h_{zz}^{zz} - 2h_{xx}^{xx} - 2h_{yy}^{yy} \right),$$

(A2a)

$$\lambda^{(2)}_{12} = \frac{1}{3} \left( h_{xx}^{xx} + h_{yy}^{yy} - h_{zz}^{zz} - h_{zz}^{zz} \right),$$

(A2b)

$$\lambda^{(2)}_{21} = \frac{1}{3\sqrt{3}} \left( 2h_{zz}^{xx} - h_{xx}^{xx} - h_{yy}^{yy} - 2h_{zz}^{xx} + h_{zz}^{xx} + h_{yy}^{yy} \right),$$

(A2c)

$$\lambda^{(2)}_{1p} = \frac{1}{3\sqrt{3}} \left( 2h_{zz}^{xx} - h_{xx}^{xx} - h_{yy}^{yy} - 2h_{zz}^{xx} + h_{zz}^{xx} + h_{yy}^{yy} \right),$$

(A2d)

$$\lambda^{(2)}_{2p} = \frac{2}{3\sqrt{3}} \left( 2h_{xx}^{xx} - h_{xx}^{xx} - h_{yy}^{yy} \right), \quad p = yz, xz, xy,$$

(A2e)

$$\lambda^{(2)}_{2q} = \frac{2}{3} \left( h_{xx}^{xx} - h_{yy}^{yy} \right), \quad p = yz, xz, xy,$$

(A2f)

$$\lambda^{(2)}_{p q} = \frac{4}{3} h_{pp}^{pq} \quad p, q = yz, xz, xy,$$

(A2g)
where we used the following expressions:

\[ \int d\Omega d\epsilon_{x}(x^2) = -\frac{4\pi}{45}, \]  
(A3a)

\[ \int d\Omega d\epsilon_{y}(y^2) = -\frac{4\pi}{45}, \]  
(A3b)

\[ \int d\Omega d\epsilon_{z}(z^2) = \frac{16\pi}{45}, \]  
(A3c)

\[ \int d\Omega d\epsilon_{x-y}(x^2) = \frac{4\pi}{15}, \]  
(A3d)

\[ \int d\Omega d\epsilon_{x-y}(y^2) = -\frac{4\pi}{15}, \]  
(A3e)

\[ \int d\Omega d\epsilon_{x-y}(z^2) = 0. \]  
(A3f)

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