Formulation of Multiple Diffraction by Trees and Buildings for Radio Propagation Predictions for Local Multipoint Distribution Service

1. Introduction

Since microwave and millimeter wave communications systems are considered for use in a local multipoint distribution service (LMDS) [1-3], it is necessary and important to develop propagation prediction tools to facilitate good system design leading to excellent service. It is appropriate to implement a high transmitter antenna and building rooftop receiver antennas for small cells, which provide line-of-sight (LOS) propagation paths between transmitter and receivers. As reported in a study of the LMDS radio channel [1], radio propagation impairments for LMDS systems should be studied. The effects of vegetation, buildings, and rain and other precipitation on radio propagation must be considered and included in the design of the system. Several models for attenuation in vegetation media are available [4]. The effects of rain and other precipitation on radio propagation have been studied for many years for satellite and terrestrial telecommunications and for radar remote sensing. However, the suitability of the existing models and results for LMDS systems needs to be investigated. In particular, tree canopies that extend above the building rooftop heights block LOS propagation paths and cause signal attenuation, depolarization, and multipath. For a wavelength \( \lambda \) much larger than the size of tree leaves and branches, e.g., 900 MHz, a theoretical model has been proposed to compute the diffraction effects of tree canopies and buildings [5]. Unfortunately, \( \lambda \) at centimeter and millimeter frequencies (1 cm at 30 GHz) may be on the order of sizes of tree leaves and branches and even much smaller. Therefore, the...
model proposed for use in mobile radio systems is not valid for LMDS propagation predictions [5]. There is a lack of engineering solutions for LMDS systems, and a need for better understanding of the propagation mechanism, especially for propagation environments including vegetation and buildings.

This paper studies the diffraction of tree canopies that extend above the building rooftop heights and of buildings and explains the effects of diffraction on radio propagation. A closed-form expression for multiple diffraction by trees and buildings is presented in Sec. 2, derived from the uniform geometrical theory of diffraction (UTD) [6] and from physical optics (PO), as well as from existing models for vegetation [4,7]. It is known that UTD itself may become incorrect when the rooftop of each multiple diffraction building (modeled as an edge) lies in the transition zone of rooftops of the preceding diffraction buildings as indicated in Fig. 1. Because of this, PO-based results are applied for multiple edge diffraction near and in the transition zone [8,9]. The physical optics approximation is accurate in and near the transition zone but generally involves multiple dimension integration due to the multiple diffraction. The behavior of the closed-form diffraction formulation in and near the transition zone is examined and presented in Sec. 3. Numerical results of the formulation are presented and discussed in Sec. 4, along with their relevance to the LMDS radio channel. The entire work is summarized in Sec. 5.

2. Multiple Diffraction Formulation

This section presents the multiple forward diffraction expression for trees and buildings as represented in Fig. 1. The diffraction modeling of Fig. 1 (a) is indicated in Fig. 1 (b). A multiplication of a knife-edge diffraction and a tree attenuation and phase factor is used to account for the diffraction of a row of buildings and a tree canopy above the building rooftop height. The rows of buildings or trees are numbered 1 to $n$. There is no direct ray from transmitter to receiver, because the tree canopies extend above the average building rooftop height and block the LOS propagation path. The strongest ray suffers attenuation by the tree canopy.

Consider an incident plane wave $E_0$ and the corresponding total field $E_{n+1}$ at the reference point $n+1$ (receiver) as defined for the formulation of multiple diffraction in previous investigations [10,5]. Let $k_0$ be the wave-number in free space, $\alpha$ be the elevation angle, $d$ be the average separation distance between rows of trees or buildings, and $g = \sin \alpha \sqrt{d/\lambda}$ be a group parameter.

In the range of $g > 0$, the closed-form expression for the field ratio $E_{n+1}/E_0$ or $|E_{n+1}/E_0|$ is

\[ E_{n+1}/E_0 = \frac{1}{d} \sum_{m=1}^{n} \frac{1}{d_m} \sin \theta_m - \sin \theta_{n+1} \]

Where $\theta_m$ is the angle of the $m$th building or tree.

**Fig. 1.** Radio propagation in the presence of rows of trees and buildings. (a) Diffraction by buildings and tree canopies extending above the building rooftop heights. (b) Diffraction modeling of Fig. 1 (a): a multiplication of a knife-edge diffraction and a tree attenuation and phase factor accounting for a row of buildings and a tree canopy above the building rooftop height.
\[ \frac{E_{\text{on}}}{E_0} = A \left( 1 + \frac{D_{s,h}}{\sqrt{d}} \right) - e^{-j\pi/4} \left[ -\sqrt{\pi \Delta k d \cdot e^{j\pi/4} \pm (-1)} \right], \quad (5) \]

where the subscripts “s” and “h” of \( D_{s,h} \) and \( D_{c,h} \) denote soft and hard boundaries, respectively, and they take signs “−” and “+” on the right-hand side of Eqs. (2) and (5). The hard boundary corresponds to vertical polarization transmission and reception in the vertical plane. The transition function \( F(X) \) can be approximated by \( F(X) \approx \sqrt{\pi}X^{n/4} \) for \( X < 10^{-3} \) and \( F(X) \approx 1 \) for \( X > 10 \). Many LMDS propagation environments would have have \( X > 10 \). For example, at 30 GHz, \( d = 40 \) m, and \( \alpha \geq 1.62^\circ \). Eq. (4) results in \( X > 10 \). Equation (1) may fail when \( g \) is small, especially as \( g \to 0 \), corresponding to the grazing aspects of incidence and observations. The failure of UTD multiple diffraction may occur for \( g < 0.1 \) as stated in Ref. [12].

For \( 0 \leq g = \alpha \sqrt{d}/\lambda < 0.1 \) and a grazing incidence of \( \alpha \to 0 \), the expression for \( E_{\text{on}}/E_0 \) is

\[ \frac{E_{\text{on}}}{E_0} = A \left( 1 + \frac{D_{s,h}}{\sqrt{d}} \right) e^{-j\pi/4} \left[ \frac{1}{\sin(\alpha/2)} \pm \frac{1}{-\cos(\alpha/2)} \right]. \quad (6) \]

\[ D_{s,h}(\alpha = 0) = -e^{-j\pi/4} \left[ \sqrt{2\pi \Delta k d} \cdot e^{j\pi/4} \pm (-1) \right], \quad (7) \]

where \( \gamma_n \) is a function of the number of rows of buildings \( n \). The expression \( 1/\sqrt{3n+1} \) by Wallfish and Bertoni [8] was used here; it approximates \( \Gamma(n+1/2)/(\sqrt{n}!) \) derived in Ref. [9] which is valid for both hard and soft boundaries. The factor \( 1/\sqrt{3n+1} \) accounts for the multiple forward diffraction by \( n \) rows of buildings at grazing incidence, i.e., \( E_{\text{on}}/E_0 \) at \( \alpha \to 0 \). Equation (6) is derived by writing

\[ \frac{E_{\text{on}}}{E_0} = A \left( 1 + \frac{D_{s,h}}{\sqrt{d}} \right) e^{-j\pi/4} \left( \mathcal{H} \right) \quad (8) \]

and determining \( \mathcal{H} \) when \( 0 \leq g < 0.1 \). The hybrid function \( \mathcal{H} \) (including tree attenuation effects) comes from UTD and physical optics that is accurate in the transition zone. It takes the advantages of both methods. One may approximate Eq. (8) as

\[ \frac{E_{\text{on}}}{E_0} = \frac{A^{1+\gamma_n}}{\sqrt{3n+1}} \quad (9) \]

for \( g \to 0 \), i.e., \( \alpha \to 0 \) and \( k_0 d (1 - \cos \alpha) \to 0 \). Equation (9) is a multiplication of the multiple-building diffraction factor \( 1/\sqrt{3n+1} \) and the tree attenuation factor \( A^{1+\gamma_n} \). The building factor \( 1/\sqrt{3n+1} \) is valid when the
building separation distance is much larger than the wavelength \((d \gg \lambda)\); the tree attenuation factor \(A\) is valid at 10 GHz to 40 GHz [4]. Therefore, Eq. (9), which is an approximation, can hold for the range 20 GHz to 40 GHz. This means that \(\mathcal{H}\) can be approximated as

\[
\mathcal{H} \approx \frac{1-\alpha n/\sqrt{3n+1}}{-D_\lambda \beta n/\sqrt{d}} \, .
\] (10)

The function \(\gamma_n\) ranges from 0 to \(n-1\), resulting in variations of tree attenuation. In the numerical calculations for this work, \(\gamma_n \approx 0\) was taken. This should be adequate to indicate the tree effects for LMDS systems. LOS propagation paths in the absence of trees are nearly constant when the number of rows of trees or buildings is larger than about 10, 4 dB to 5 dB for wider trees. This corresponds to a constant value of \(\gamma_n\) for \(n \approx \pm 10\).

Since \(k_0 d \gg 1\) and \(\alpha\) is small leading to \(\cos(\alpha/2) = 1\), the second term on the right-hand sides of Eqs. (2), (5), and (7) is negligibly small compared with the first term. Therefore, both Eqs. (6) and (1) are dependent on but insensitive to the polarization (type of boundaries). Since \(d\) is in the range of about 30 m to 100 m or even larger, the condition \(k_0 d \gg 1\) is valid at the microwave and millimeter wave frequencies being used for LMDS systems.

3. Asymptotic Expressions

To examine Eqs. (6) and (1) for small \(\alpha \approx 2 \sin (\alpha/2)\) and small \(g \approx \alpha \sqrt{d/\lambda}\), one may approximate Eq. (3) by

\[
F(X) \approx \left[ \sqrt{\pi X - 2X e^{\pi/4}} \right] e^{\pi/4 + i X} \, .
\] (11)

where \(X = \pi g^2\) is small [6]. For the purposes of practical engineering applications, the approximation of Eq. (11) can be taken for \(0 \leq X < 0.3\) corresponding to \(0 \leq g < 0.3\). One thus derives from Eq. (2)

\[
D_\lambda / \sqrt{d} = -1/2 + g e^{\pi/4} \, .
\] (12)

As a result, Eq. (1) can be approximated by

\[
E_{out}/E_0 = A \left( \sqrt{2} - A e^{-j\Delta\lambda /d} \right) + \frac{2\sqrt{2}}{2 - \sqrt{2} - 2A e^{-j\Delta\lambda /d}} g e^{j\pi/4} \, .
\] (13)

for \(0.3 > g > 0.1\) and \(n\) sufficiently large (\(n \approx 6\) for \(A = 1\) from numerical calculation). Further, Eq. (13) becomes

\[
E_{out}/E_0 \approx \frac{2\sqrt{2}}{2 - \sqrt{2} - 2A e^{-j\Delta\lambda /d}} A g \, .
\] (14)

for \(0.3 > g > |1/2 - 2A e^{-j\Delta\lambda /d}/\sqrt{2}| \geq 0.1\). Similarly, Eq. (6) can be approximated by

\[
E_{out}/E_0 \approx A \left( A \gamma_n/\sqrt{3n+1} \right) + 2g (1-A \gamma_n/\sqrt{3n+1}) e^{i\pi/4} \, .
\] (15)

and becomes

\[
E_{out}/E_0 \approx 2A g \, .
\] (16)

for \(n \gg 1\). The settled field \(Q\) from Eq. (14) of Walisch and Bertoni is

\[
Q = 0.1 \left[ \frac{\alpha \sqrt{d/\lambda}}{0.03} \right]^{0.9} \approx 2.35 g^{0.9} \, .
\] (17)

for \(\alpha \sqrt{d/\lambda}\) ranging about 0.02 to 0.4 [8]. If we consider the case \(A e^{-j\Delta\lambda /d} = 1\), i.e., the absence of trees, Eq. (14) (valid for \(0.3 > g > 0.147\)) and Eq. (16) become

\[
E_{out}/E_0 \approx 1.55 g \, .
\] (18a)

\[
E_{out}/E_0 \approx 2g \, .
\] (18b)

It is interesting to see that these two asymptotic expressions are comparable with Eq. (17). For small \(g\), the deviation of Eq. (18a) from Eq. (17) becomes large.
For \( n = 6 \) and \( A = 1 \), Eq. (15) becomes

\[
\frac{E_{n+1}}{E_0} \approx 0.229 + 1.54 g e^{\pi/4}.
\] (19)

One can also write Eq. (13) as

\[
\frac{E_{n+1}}{E_0} \approx 0.227 + 1.55 g e^{\pi/4}.
\] (20)

Incidentally, Eq. (1) smoothly approaches Eq. (6) when \( g \to 0.1 \) and \( A e^{-jDkD} = 1 \) for \( n \leq 6 \). Both Eq. (6) and Eq. (1) also apply to a soft boundary that corresponds to horizontal polarization transmission and reception in the vertical plane.

4. Numerical Results

Figures 2 and 3 present numerical results of Eqs. (1) and (6). The relative attenuation \( A_{md} \) in dB is derived from

\[
A_{md} = 20 \log_{10} \left| \frac{E_{n+1}}{E_0} \right|.
\] (21)

Due to the presence of trees, the relative attenuation for trees and buildings is severe at \( \alpha = 0.5^\circ \), where \( g \) takes the values 0.617 and 0.501 for \( d = 50 \text{ m} \) and \( d = 33 \text{ m} \), respectively. In the absence of trees, the attenuation of buildings varies around the value of free space and the building effect is negligible, since an LOS propagation path between transmitter and receiver antennas exists and plays an important role for \( g > 0.4 \), corresponding to sufficiently high transmitter antennas [8,10]. The parameter \( g \) depends on frequency, elevation angle, and separation distance between buildings. The existence of an LOS path (a direct wave component) depends only on the elevation, i.e., for \( \alpha > 0 \). The LOS propagation path becomes dominant when the elevation angle \( \alpha \) is sufficiently large resulting in \( g > 0.4 \). In the presence of trees, the tree canopies that extend above the building rooftop heights block the LOS propagation path and cause additional signal attenuation. Based on the analysis of experimental data, a recent study of the LMDS radio channel concludes that a serious propagation impairment is signal attenuation caused by tree canopies [1].

![Fig. 2. Attenuation relative to free space attenuation for a receiver at the rooftop of building number \( n+1 \) for a 50 m distance separation between trees and buildings.](image-url)
It is seen that the differences between the relative attenuation for trees and buildings and the attenuation for the buildings only are insensitive to the number of edges modeling the trees and buildings. At \( g = 0 \), i.e., \( \alpha = 0 \), Eq. (6) becomes \( A_{1+g} \sqrt{n+1} \), which is a multiplication of the diffraction factors for tree canopy and buildings. At an angle of \( \alpha > 0 \), the absolute value of relative attenuation \( A_{1d} \) increases as the separation distance \( d \) between trees or buildings decreases. Equation (6) generates the results for \( \alpha = 0.05 \), where \( g \) takes the values 0.0617 and 0.0501 for \( d = 50 \) m and \( d = 33 \) m, respectively. For a fixed elevation angle \( \alpha \), \( g \) decreases with \( d \). It is known that the multiple building forward diffraction loss increases as the group parameter \( g \) decreases [8,10].

Since the depth \( \Delta d \) is an input parameter, more numerical calculations for other values of \( \Delta d \) are available. Also, there are several models of attenuation due to vegetation media at centimeter and millimeter wavelengths and these models can be taken as inputs of the present formulation of Eqs. (1) and (6) [4].

5. Conclusion

A closed-form expression for multiple forward diffraction by tree canopies and buildings has been derived and presented in order to make propagation predictions at centimeter and millimeter wavelengths for local multipoint distribution service. When the transmitter antennas are sufficiently high, the attenuation of the buildings varies around the value of free space and the building effect is negligible, because a line-of-sight propagation path between transmitter and over building rooftop receiver antennas exists and plays a major role. When trees extend above the building rooftop heights, they block the LOS propagation path and cause additional signal attenuation. The attenuation effect of the buildings is significant if the transmitter antennas are not high enough as \( \alpha \to 0 \). The attenuation due to rows of tree canopies and buildings increases as the separation distance between trees or buildings decreases. When enough measurement data become available, a comparison of the formulation with measurements and
experimental studies of $\gamma_0$ would lead to refinement or significant improvement of the prototype formulation given here.

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6. References

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