Theoretical Studies on InGaAs/InAlAs SAGCM Avalanche Photodiodes

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Abstract

In this paper, we provide a detailed insight on InGaAs/InAlAs separate absorption, grading, charge, and multiplication avalanche photodiodes (SAGCM APDs) and a theoretical model of APDs is built. Through theoretical analysis and two-dimensional (2D) simulation, the influence of charge layer and tunneling effect on the APDs is fully understood. The design of charge layer (including doping level and thickness) can be calculated by our predictive model for different multiplication thickness. We find that as the thickness of charge layer increases, the suitable doping level range in charge layer decreases. Compared to thinner charge layer, performance of APD varies significantly via several percent deviations of doping concentrations in thicker charge layer. Moreover, the generation rate \( G_{bta} \) and band-to-band tunnel is calculated, and the influence of tunneling effect on avalanche field was analyzed. We confirm that avalanche field and multiplication factor \( (M_n) \) in multiplication will decrease by the tunneling effect. The theoretical model and analysis are based on InGaAs/InAlAs APD; however, they are applicable to other APD material systems as well.

Keywords: Avalanche photodiodes, Theoretical analysis, Simulation, Charge layer, Tunneling effect

Background

In\(_{0.53}\)Ga\(_{0.47}\)As (referred to hereafter as InGaAs) avalanche photodiodes (APDs) are the most important photodetectors for short-wave infrared detection. They are significant in traditional fields, such as optical fiber communication, reconnaissance applications, and remote sensing. InP and In\(_{0.52}\)Al\(_{0.48}\)As (referred to hereafter as InAlAs) have the same lattice spacing with InGaAs and great avalanche breakdown characteristics; therefore, they are the suitable multiplication layer materials of InGaAs APDs in the traditional applications. In recent years, due to the quick development of single-photon detection in quantum key distribution [1], time-resolved spectroscopy [2], optical VLSI circuit inspection [3], and 3D laser ranging [4], APDs as the key component in these applications have attracted increasing attention [5, 6]. Pellegrini et al. described the design, fabrication, and performance of planar-geometry InGaAs/InP devices which were developed for single-photon detection with the single-photon detection efficiency (SPDE) 10% at 1550 nm (200 K) [7]. Tosi et al. presented the design criteria of a novel InGaAs/InP single-photon avalanche photodiode (SPAD) with high SPDE (30%, 225 K), low noise, and low timing jitter [8]. In simulation, a device model based on experimental data was built to predict dark count rate (DCR) and SPDE of InGaAsP/InP SPADs in [9], and an integrated simulation platform that can evaluate the decoy-state quantum key distribution performance of InGaAs/InP SPADs was built in [10]. Acerbi et al. presented design criteria for InGaAs/InP single-photon APDs with a custom SPAD simulator [11]. For InGaAs/InAlAs APDs, a mesa structure SPAD InGaAs/InAlAs was demonstrated to achieve the SPDE of 21% (260 K); however, high DCR was observed and was attributed to excessive tunneling current [12]. Then, [13] used a thick InAlAs avalanche layer in InGaAs/InAlAs APDs to improve the SPDE (26%, 210 K) and decrease the DCR \( (1 \times 10^8 \text{ Hz}) \). In simulation of InAlAs-based APDs, a device model that based on the Monte Carlo method was established to

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study the basic characterization of InGaAs/InAlAs APDs in [14], and the influence of charge layer and multiplication layer on punchthrough voltage and the breakdown voltage were studied with steady-state 2D numerical simulations in [15]. Compared to InAlAs-based APDs, researches of InP-based APDs are more comprehensive and in depth in theory and simulation. However, InAlAs-based APD is increasingly used in place of InP as it has a larger band gap that can improve the breakdown characteristics both in the APDs and SPADs [16]. The ionization coefficient ratio of electron (α) to hole (β) in InAlAs is larger compared to InP, and, hence, it has low excess noise factor and high gain-bandwidth product. Moreover, InAlAs exhibits a large increase in breakdown probability with overbias ratio, making InAlAs SPADs have lower DCR [17]. Some important properties and conclusions regarding InAlAs-based APDs were obtained from previous studies, such as the low excess noise can be achieved in InAlAs structures with both thick and thin avalanche regions [18]. The tunneling threshold electric field in the absorption (InGaAs) is 1.8 × 10^5 V/cm, and the tunneling current becomes the dominant component of the dark current in the high field [14]. A vertical-illumination structure has larger optical tolerance, but it has a more serious tradeoff between the carrier transit time and responsivity [19]. Moreover, theoretical model, structure (thickness and doping), electric field, and other InAlAs-based APD parameters have been studied in [20–22]. However, these studies only focused on influences of common APD structure parameters, such as the absorption layer thickness, multiplication thickness, and charge layer doping level. The relationship between the structure parameters and performance of the InAlAs-based APD has not yet been fully understood and optimized.

In this paper, a theoretical study and numerical simulation analysis based on the vertical structure of InGaAs/InAlAs for 1.55-μm wavelength detection were investigated. We built a theoretical model to study the influence of structure parameters on device and detailed relationship of each layer in APDs. The design of the charge layer with different multiplication thickness, influence of the thickness on the doping level in charge layer, and the tunneling effect on the avalanche field in the multiplication were analyzed and simulated.

**Methods**

In this section, a mathematical relationship between the device parameters and electric field distribution in the device was built, which was applied to analyze the charge layer and the tunneling effect. Concurrently, a simulation model that included simulation structure, material parameters, and basic physical models was built. The theoretical analysis model and simulation model was based on the vertical structure of SAGCM InGaAs/InAlAs APD.

**Theoretical Model and Analysis of Charge Layer**

Device parameters, such as doping level, thickness, materials, and structure, were used to build the mathematical model for calculating the electric field distribution in APD. The basic physical theories that include Poisson equation, depletion-layer model, and PN junction model of semiconductor device can be found in chapters 1, 2, and 4 in [23] and [24]. The junction multiplication factor equation can be found in [25], and material parameters of semiconductor are from [26]. The presented model adopts Poisson equation, tunneling current density equation, depletion-layer model, junction theory model, and the local model of avalanche gain. The simplified mathematical coordinate system of the APD that includes basic structure parameters (materials, thickness, doping, and dielectric constant) is presented in Fig. 1. It is a simplified SACM APD structure that ignores grading layer. The materials of the contact layer, charge layer, and multiplication layer are InAlAs, and the absorption layer is InGaAs. The junctions of layers are separated by X_m, X_m, X_a, and X_p by the x coordinate. Doping levels are expressed by N_ο, N_₁, N_₂, N_₃, and N_₄, the layer thicknesses are expressed by w_0, w₁, w₂, w₃, and w₄, and dielectric constants are expressed by ε_ο, ε₁, ε₂, ε₃, and ε₄ of contact A, multiplication, charge, absorption, and contact B, respectively.

Equation 1 is the Poisson equation, which can solve the electric potential distribution using the charge density ρ. In this equation, ρ is equal to dopant ion N in the depletion-layer model, w is equal to the thickness of depletion layer, and ε is the dielectric constant of the material. In the common PN junction electric field distribution model, ρ is a variable that depends on the depletion-layer thickness w and dopant ion N. In this model, it changes after considering the tunneling effect. However, before considering the tunneling effect, we first built the electric field distribution using a common method.

\[
\frac{d\xi}{dx} = \frac{\rho}{\varepsilon} = \frac{q \times N}{\varepsilon}
\]

By solving the Poisson equation with the device parameters, the mathematical expression of the max electric field
is obtained. This expression is determined by the penetration thickness variation in the depletion layer shown in Formulas 2 and 3. In this expression, the parameters that include doping levels \( N \), thicknesses of depletion layer \( w \), and dielectric constants \( \varepsilon \) of different layers can be found in Fig. 1.

\[
\xi_{\text{max}}(w) = \sum_{k=1}^{4} \left( \frac{q \times N_k \times w_k}{\varepsilon_{sk}} \right) \quad (2)
\]

\[
\xi_{\text{max}}(w) = \frac{q \times N_0 \times w_0}{\varepsilon_{s0}} \quad (3)
\]

Then, the electric field distribution can be derived in all points using Formulas 4 and 5. The boundary condition ignores the built-in potential \( V_{br} \) in Formula 6; therefore, the mathematical relationship between depletion layer thickness and bias voltage can be calculated.

\[
\xi_{x,w} = \xi_{\text{max}}(w) + \sum_{k=1}^{4} \left( \frac{q \times N_k \times |x|}{\varepsilon_{sk}} \right) (X_p < x < 0) \quad (4)
\]

\[
\xi_{x,w} = \xi_{\text{max}}(w) \cdot \frac{q \times N_0 \times x}{\varepsilon_{s0}} (0 < x < X_n) \quad (5)
\]

\[
V_{bias} + V_{bi} = - \int_{-w_0}^{w_1 + w_2 + w_3 + w_4} \xi(x, w) dx \quad (6)
\]

Finally, the mathematical relationship between electric field distribution and bias voltage in the device is obtained using Formulas 7–11:

\[
\xi(x, V_{bias}) = \xi_{\text{max}}(V_{bias}) + \frac{q \times N_1 \times |x|}{\varepsilon_{s1}} (0 \leq x \leq X_m) \quad (7)
\]

\[
\xi(x, V_{bias}) = \xi_{\text{max}}(V_{bias}) + \frac{q \times N_1 \times w_1}{\varepsilon_{s1}} + \frac{q \times N_2 \times |x-X_m|}{\varepsilon_{s2}} (X_m \leq x \leq X_c) \quad (8)
\]

\[
\xi(x, V_{bias}) = \xi_{\text{max}}(V_{bias}) + \frac{q \times N_1 \times w_1}{\varepsilon_{s1}} + \frac{q \times N_2 \times w_2}{\varepsilon_{s2}} + \frac{q \times N_3 \times |x-X_c|}{\varepsilon_{s3}} (X_c \leq x \leq X_a) \quad (9)
\]

\[
\xi(x, V_{bias}) = \xi_{\text{max}}(V_{bias}) + \frac{q \times N_1 \times w_1}{\varepsilon_{s1}} + \frac{q \times N_2 \times w_2}{\varepsilon_{s2}} + \frac{q \times N_3 \times w_3}{\varepsilon_{s3}} + \frac{q \times N_4 \times |x-X_a|}{\varepsilon_{s4}} (X_a \leq x \leq X_p) \quad (10)
\]

\[
\xi(x, V_{bias}) = \xi_{\text{max}}(V_{bias}) - \frac{q \times N_0 \times x}{\varepsilon_{s0}} (0 \leq x \leq X_n) \quad (11)
\]
From the model, once the boundary of the depleti-
on layer reaches the contact region, Formulas 7–11
can be used to analyze the electric field in each
layer. In the practical APD, the absorption and
mul tiplication layers are unintentionally doped in
trinsic layers. \( N_3 \) and \( N_1 \) are less than \( N_2 \). Thus, For-
mula 9 is approximately equal to Formula 12. It is
the reason that charge layer can control the electric
field distribution in the device.

\[
\xi(x, V_{bias}) = \xi_{\text{max}}(V_{bias}) + \frac{q \times N_1 \times w_1}{\varepsilon_{s_1}} + \frac{q \times N_2 \times w_2}{\varepsilon_{s_2}} + \frac{q \times N_3 \times |x-X_c|}{\varepsilon_{s_3}} + \frac{q \times N_3 \times X_c}{\varepsilon_{s_3}} - X_c \geq x \geq X_a
\]  
(12)

In Formula 8, the electric field difference between
mul tiplication and absorption is determined using
the product of \( N_2 \) and \( w_2 \). \( N_2 \) is the doping level in
the charge layer and \( w_2 \) is the charge layer thickness.
For a suitable electric field distribution in InGaAs/
InAlAs APD, the electric field in the absorption
layer (InGaAs) should be within the interval values
of 50–180 kV/cm that ensure enough velocity for
the photo-induced carriers and avoid the tunneling
effect in the absorption layer [10]. That is, the
avalanche field in multiplication should decrease to
50–180 kV/cm in absorption by the charge layer.
Thus, we can use Formula 8 to find optimal calcu-
lated doping level and thicknesses of charge layer.
When the multiplication layer is 200 nm (the ava-
lanche field \( E \) in the multiplication is \( 6.7 \times 10^5 \) V/cm
while the multiplication layer is 200 nm [27]); the
calculated values of doping level and thickness in
the charge layer are compared with results from
[28–33] in Fig. 2. The region of theoretical values is
in good agreement with the experimental data. This
result proves that Formula 8 can be used to predict
the doping level with different thicknesses in the
charge layer when the multiplication thickness is
certain.

We calculate the optimal doping level for different
thicknesses of the charge layer with the multipli-
cation layer of 300, 500, and 700 nm, and the results
are presented in Fig. 3. This result illustrates that
the tolerance in the doping level in charge layer is
related to its thickness and the range of doping level
decreases with the thickness increase in charge layer.

![Fig. 2 Comparison of theoretical results and experiment data from various reports (\( w_m = 200 \) nm). Closed symbols: the doping level and thickness of charge layer with multiplication thickness of 200 nm (black square, black circle, black triangle, black right-pointing triangle) and
231 nm (black diamond, black down-pointing triangle) in the references. Presents the calculated values of charge layer (doping level and thick-
ess) by Formula 8 (the absorption field is 50–180 kV/cm). When the absorption field is 50 kV/cm, the upper limit of the doping level in the
charge layer can be obtained. When the absorption field is 180 kV/cm, the lower limit of the doping level in the charge layer can be obtained.
We compare the theoretical results and experiment data from various reports. The region of theoretical values is in good agreement with the ex-
erimental data. Dashed lines the calculated values of doping level and thickness by the formula.](image-url)
That is, if we apply a thick charge region, only a small range of doping level in the charge layer would exist to satisfy the optimal electrical filed. As a result, the performance of APD varies significantly via several percent deviations of doping concentrations in the thicker charge layer. In the “Results and Discussion” section, the practical structures of APDs were simulated to study and verify the theoretical analysis, which includes influence of charge layer thickness on doping level range in the charge layer and the variety of performance for different charge layer thickness in APDs.

**Theoretical Model with Consideration of Tunneling**

The above analysis model is about electric field distribution in the device and based on the premise that \( \rho \) is the dopant ion in the depletion layer. If a sufficiently high electric field exists within the absorption layer, the local band bending may be sufficient to allow electrons to tunnel [34]. Therefore, electron tunneling can occur. From the tunneling schematic diagram in Fig. 4, when the absorption layer has a breakdown tunneling, the tunneling effect changes the charge density \( \rho \), the positive charge in absorption increases, and the negative charge in the multiplication and charge layers increases. Thus, \( \rho \) is not equal to the dopant ion charge density in the...
depletion layer while the tunneling effect appears. The formulas that were discussed earlier will change after considering the tunneling effect.

The generation rate $G_{bbt}$ of band-to-band tunnel is described in Formula 13 [35, 36].

$$G_{bbt} = \left( \frac{2m^*}{E_g} \right)^{1/2} \frac{q^2 E_p^2}{(2\pi)^{3/2}} \exp\left( -\frac{\pi}{4q\hbar E_p} \left( 2m^* \times E_g^3 \right)^{1/2} \right)$$

$$= A \times E_p^2 \times \exp\left( -\frac{B}{E_p} \right)$$

(13)

In Formula 13, $E_g$ is the energy band gap of InGaAs, $m^*$ (equal to 0.04 $m_o$) is the effective reduced mass, $E_p$ is the breakdown electric field in the absorption layer, and $\gamma$ is a user-definable parameter that is usually restricted to 1~2. The $A$ and $B$ are the characterization parameters. We calculate the $G_{bbt}$ with different $\gamma$, and the results are shown in Fig. 5. It can be found that $G_{bbt}$ adapts the same order of magnitude for the charge layer doping level while $\gamma$ is restricted to 1~1.5.

As a result, charge density $\rho$ is a variable and determined by the tunneling effect and the dopant ion in the absorption tunnel. On this occasion, Formula 1 will be changed to Formula 14 and the electric field in the multiplication layer will be described by Formula 15. $w_{tunnel}$ is the effective depletion layer of the tunneling process [35]. Thus, the changing of avalanche field can be described by Formula 16, and the avalanche field will decrease in the multiplication with the tunneling effect.

$$\frac{d\xi}{dx} = \frac{\rho}{\varepsilon} = \frac{q \times (N + G_{bbt})}{\varepsilon} \cdot E_p > 1.8 \times 10^5 V/cm$$

$$\xi(x, V_{bias}) = \xi_{max(V_{bias})} \div \frac{q \times (N1 \times |x| + G_{bbt} \times w_{tunnel})}{E_{s1}} \div (0 \geq x \geq X_m)$$

(15)

$$\delta\xi(x, V_{bias}) = \delta E = \frac{q \times G_{bbt} \times w_{tunnel}}{E_{s3}}$$

(16)

The electron and hole ionization coefficients are described by Formulas 17 and 18 in [18]. $E$ is the avalanche field in multiplication.

$$\alpha = a_e e^{-b_n} / E$$

(17)

$$\beta = a_p e^{-b_p} / E$$

(18)

The effect of carrier avalanche is accounted by the impact ionization model. Considering the extremely low carrier density of the multiplication layer compared to charge layer, it is reasonable to assume that the electric field is uniform throughout the
multiplication layer. Therefore, the multiplication factor \((M_n)\) can be expressed as the following Eq. 19. Here, \(w_m\) is the multiplication layer thickness and \(k\) is the impact ionization coefficient ratio defined by \(\alpha/\beta\). Since \(k\) varies very slowly with the electric field, \(k\) is approximately constant for a slight variation of \(w_m\) [37].

\[
M_n = \frac{k-1}{k \times e^{-\left(\frac{1}{k}\right)w_m}}
\]

(19)

Assuming constant \(w_m\) and bias voltage, differentiation of \(M_n\) with respect to electron ionization coefficients is in Formulas 20 and 21.

\[
\delta M_n|_{w=\text{const},V=\text{const}} = M_n^2 e^{-\left(\frac{1}{k}\right)w_m} \times w_m \delta \alpha
\]

(20)

\[
\delta \alpha = \frac{\delta \alpha}{\delta E} = \alpha_n b_n e^{\frac{\delta \alpha}{\alpha_n b_n}} \frac{1}{E^2}
\]

(21)

In Formulas 20 and 21, \(\delta \alpha/\delta E\) is positive. It is assumed that 20% of a total depletion absorption layer is \(w_{\text{tunnel}}\) and the absorption layer is 400 nm thick. By solving Formula 16, the relationship between the \(\delta E\) and the absorption field with different \(\gamma\) is presented in Fig. 6. It can be found that \(\delta E\) adapts the same order of magnitude for the avalanche field in the multiplication. Thus, the tunneling effect has an influence on the avalanche field and the \(M_n\) will decrease with the tunneling effect. In the analysis, we assumed that the negative charge is non-multiplied in the multiplication and the model will be more rigorous after taking it into consideration. To verify and analyze the influence of tunneling effect on practical structure of APDs, we simulated the relationship between the tunneling effect and multiplication avalanche field in details in the “Results and Discussion” section.

Structure and Simulation Model

A semiconductor device simulation of TCAD was used for simulation and analysis. This simulation engine defines physical models in simulation, and the results have a physical meaning [20]. The basic physical models were presented as follows. The drift-diffusion models, including the Poisson and carrier continuity equations, were used to simulate the electric field distribution and diffusion current \(I_{\text{DIFF}}\). Band-to-band tunneling model was used for the band-to-band tunneling current \(I_{\text{B2B}}\), and the trap-assisted tunneling model was used for trap-assisted tunneling current \(I_{\text{TAT}}\). The generation-recombination current \(I_{\text{GR}}\) was described by the Shockley–Read–Hall recombination model, and the Auger recombination current \(I_{\text{AUGER}}\) was described by the Auger recombination model. The dark current was described clearly by those mechanisms [38]. Avalanche multiplication was described by the Selberherr impact ionization...
model. Other basic models, including the Fermi-Dirac carrier statistics, carrier concentration-dependent, low field mobility, velocity saturation, and ray-tracing methods, were used for the simulation model, and a rigorous simulation model was built. 

Device structures in the simulation were similar to the experimental structures in [13]. The schematic cross-section of the top-illuminated SAGCM InGaAs/InAlAs APD is shown in Fig. 7. The structures from top to bottom are sequentially named as InGaAs contact layer, InAlAs cladding layer, InAlGaAs grading layer, InGaAs absorption layer, InAlGaAs grading layer, InAlAs charge layer, InAlAs multiplication layer, InAlAs cladding layer, InP contact layer, and InP substrate. The thickness and doping of each layer are also presented in Fig. 7. To avoid the influence of thickness on simulation results, we choose two simulation structures. One simulation structure is named as APD-1 (multiplication and absorption layers are 800 and 1800 nm, respectively), and the other simulation structure is named as APD-2 (multiplication and absorption layers are 200 and 600 nm, respectively).

To test the simulation model, the experiment data in [13] were compared with the simulation results. In this simulation, we used the same structure in the reference, and the current-voltage characteristics of the device were given. Figure 8 shows our simulation results and the experiment results in the reference. They have the similar punch-through voltage $V_{pt}$ and breakdown voltage $V_{br}$. Moreover, the simulation and experiment results correspond well. Therefore, the model in our simulation is accurate. The parameters mentioned above are listed in Table 1.

Results and Discussion

In this section, the theoretical analysis and conclusions were studied by simulation in details. First, the influence of charge layer thickness on doping level tolerance in charge layer was studied in the “Influence of Charge Layer Thickness” section. Then, relationship between the tunneling effect and multiplication avalanche field was analyzed and verified in the “Tunneling Effect on the Electric Field Distribution” section.

Influence of Charge Layer Thickness

From [14], a suitable field distribution in InGaAs/InAlAs APD should comply with those rules. The guarantee $V_{pt} < V_{br}$ and $V_{br} - V_{pt}$ should have a safety margin for processing variations in temperature fluctuations and operation range. In the absorption layer, the electric field should be larger than 50–100 kV/cm to ensure enough velocity for the photo-induced carriers. Concurrently, the electric field must be less than 180 kV/cm to avoid the tunneling effect in the absorption layer. Electric field distribution greatly influences the device performance. The choice of electric field in the absorption layer has a balancing of the tradeoff between small transit time, dark current, and high responsivity for the practical requirement.

In the simulation, we used the structure of APD-1 (multiplication is 800 nm thick) and adjusted the charge layer thickness from 50 to 210 nm to study the influence of charge layer thickness on doping level range and verify the theoretical conclusions in analytical model. In the simulation, we selected different doping level ranges in the charge layer so that the electric field distribution complies with the rules. The simulation results on the relationship between thickness and doping level range in the charge layer are presented in Fig. 9a. As the charge layer thickness increases, the suitable doping level range in charge layer decreases. A relatively large doping level range exists in the thin charge layer, and under this doping level range, the device will have a suitable electric field distribution. Apparently,
the doping level range is determined by charge layer thickness. The simulation result of APD-2 (with a thickness of multiplication of 200 nm) is presented in Fig. 9b, which has a similar result. Moreover, it can be found that the calculated results of Fig. 2 and simulation results of Fig. 9b match well as shown in Fig. 9c. The small difference between the calculated results and simulation results is caused by the different values of avalanche field in the simulation and calculation. The avalanche field in simulation engine is used $6.4 \times 10^5$ V/cm, while in the calculation, we use the value of $6.7 \times 10^5$ V/cm from [27].

The charge layer thicknesses of 210 and 50 nm (APD-1) were selected to show the simulation details and the influence of doping level on the electric field distribution. Figure 10a, c shows the current simulation results of different doping levels in thicknesses of 210 and 50 nm, respectively. Figure 10b, d shows the electric field distribution simulation results using the same structure. The simulation results show that thicknesses of 210 and 50 nm have doping level ranges of $1.0 \times 10^{17} - 1.3 \times 10^{17}$ cm$^{-3}$ and $3.9 \times 10^{17} - 5.7 \times 10^{17}$ cm$^{-3}$, respectively.

Clearly, the device with a charge layer thickness of 210 nm only has a relatively narrow and suitable doping level. A minimal change in the doping level has greatly influence the current-voltage characteristic and electric field distribution. As a result, the performance of APD varies significantly via several percent deviations of doping concentrations in the thicker charge layer. This conclusion is the same as the theoretical analysis. Concurrently, when designing APD structures, choosing a thin charge layer will give a high level of doping tolerance, as well as confer APD with good controllability.

Finally, the relationship between charge layer and multiplication thickness was simulated. Figure 11a presents the avalanche field with multiplication region thicknesses of 100, 200, and 300 nm in the APD-2 structure (with a charge layer thickness of 70 nm). Figure 11b presents the charge layer doping range with different multiplication thicknesses at the suitable electric field distribution condition. The

| Table 1 | Material parameters used for InGaAs/InAlAs APD simulation [18, 26] |
|---------|----------------------|
| Parameters/InAlAs | Units | Electron | Hole |
| Impact coefficient a | cm$^{-1}$ | $2.1 \times 10^6$ | $2.4 \times 10^6$ |
| Impact coefficient b | V/cm | $1.62 \times 10^6$ | $1.86 \times 10^6$ |
| Effective threshold energy | ev | 3.2 | 3.5 |
| SRH lifetime | s | $1 \times 10^{-6}$ | $1 \times 10^{-6}$ |
| Energy band gap | ev | 1.46 |
| Parameters/InGaAs | Units | Electron | Hole |
| BBT coefficient A | 1/V cm | $7.2 \times 10^9$ |
| BBT coefficient B | V/cm | $5.2 \times 10^6$ |
| Energy band gap | ev | 0.75 |
charge layer thicknesses are 50, 70, and 90 nm. Clearly, a high avalanche field exists in the thin multiplication layer. As the multiplication region thickness decreases, the electric field difference between multiplication and absorption layers increases. As a result, a thin multiplication layer needs a high product of the charge layer doping level and thickness to reduce the high avalanche field.

**Tunneling Effect on the Electric Field Distribution**

The simulation in this part will study the tunneling effect on the electric field in the device. From the theoretical analysis, the tunneling effect has an influence on the avalanche field in multiplication. Thus, the simulation will design to study the influence of electric field in the absorption layer that exceeds the tunneling threshold value. First, group A, with the structure of APD-1, charge layer thickness of 90 nm, and different charge layer doping levels of $1.4 \times 10^{17} - 2.4 \times 10^{17}$ cm$^{-3}$, was simulated for electric field distribution when the device avalanche breaks down. The result is shown in Fig. 12a. When the charge layer doping level exceeds $2.0 \times 10^{17}$ cm$^{-3}$, the field in the absorption layer becomes lower than the tunneling threshold field and the avalanche field in the multiplication layer reaches the same value. However, when the doping level is less than $2.0 \times 10^{17}$ cm$^{-3}$, the field in the absorption layer decreases with the decrease of the doping level in charge layer. Similar results were observed in the APD-2 structure (with a charge layer thickness of 90 nm and doping level of $2.2 \times 10^{17} - 3.6 \times 10^{17}$ cm$^{-3}$) (Fig. 12b). That is, if the electric field in the absorption layer
tunneling threshold value at or over the breakdown voltage, then the breakdown electric field in the multiplication will decrease.

Groups B (APD-1 thickness of 90 nm, doping level of $2.4 \times 10^{17} \text{ cm}^{-3}$) and APD-2 thickness of 90 nm, doping level of $3.6 \times 10^{17} \text{ cm}^{-3}$) were designed to demonstrate the relationship between the threshold electric field in the absorption layer and avalanche field in the multiplication layer. The multiplication and absorption electric fields vary with the bias voltage on the device. As shown in Fig. 12c, d, when the electric field in the absorption layer reaches the tunneling threshold value, the avalanche breakdown electric field in the multiplication gradually decreases. Moreover, when the absorption field exceeds the tunneling threshold, the avalanche breakdown electric field in the multiplication layer plummets. Furthermore, the absorption field slope increases when the electric field in the absorption layer exceeds the tunneling threshold.

The phenomenon in Fig. 12 can be explained by the theoretical analysis that tunneling has an influence...
on the charge density in the “Methods” section. When the electric field reaches the tunneling threshold value in the absorption layer, the charge density $\rho$ becomes unequal to the dopant ion. The multiplication field will decrease as the negative ion increases, and the absorption field will increase as the positive ion increases. Concurrently, the absorption field slope will increase due to the tunneling effect. As a result, the electric field in the absorption should be less than the tunneling threshold value to maintain the high field in the multiplication layer and the low dark current when the device avalanche breaks down.

**Conclusions**

In summary, we have presented a theoretical study and numerical simulation analysis involving the InGaAs/
InAlAs APD. The mathematical relationship between the device parameters and electric field distribution in the device was built. And the tunneling effect was taken into consideration in the theoretical analysis. Through analysis and simulation, the influence of structure parameters on the device and the detailed relationship of each layer were fully understood in the device. Three important conclusions can be obtained from this paper. First, the doping level and thickness of the charge layer for different multiplication thicknesses can be calculated by the theoretical model in the "Methods" section. Calculated charge layer values (doping and thickness) are in agreement with the experiment results. Second, as the charge layer thickness increases, the suitable doping level range in charge layer decreases. Compared to the thinner charge layer, the performance of APD varies significantly via several percent deviations of doping concentrations in the thicker charge layer. When designing APD structures, choosing a thin charge layer...
will give a high level of doping tolerance, as well as confer APD with good controllability. Finally, the $G_{int}$ of tunneling effect was calculated, and the influence of tunneling effect on the avalanche field was analyzed. We confirm that the avalanche field and multiplication factor ($M_n$) in the multiplication will decrease by the tunneling effect.

**Abbreviations**

2D: Two-dimensional; APD: Avalanche photodiode; DCR: Dark count rate; SACM APDs: Separate absorption, charge, and multiplication avalanche photodiodes; SAGCMAPDs: Separate absorption, grading, charge, and multiplication avalanche photodiodes; SPAD: Single-photon avalanche photodiode; SPDE: Single-photon detection efficiency; SRH: Shockley–Read–Hall

**Acknowledgements**

The authors acknowledge Xinjing Hou, Xiuli Li, Junying Zhang, and Yongwang Zhang for valuable discussions.

**Funding**

This work was supported in part by the National Key R&D Program of China (2017YFF0104803), the National Natural Science Foundation of China (Grant no. 61675195, 11504155), the National Thousand Talents Program of China, the Major State Basic Research Development Program of China (Grant no. 2013CB632103), and the Scientific Research Foundation for the Returned Overseas Chinese Scholars, State Education Ministry.

**Availability of Data and Materials**

The datasets supporting the conclusions of this article are included within the article.

**Authors’ Contributions**

SYC initiated the research, built the theoretical model, carried out the simulation, and supervised all the work. SYC, YZ, SR, CBL, and SF drafted the article. All authors read and approved the final manuscript.

**Competing Interests**

The authors declare that they have no competing interests.

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**Received:** 20 December 2017 Accepted: 29 April 2018

**Published online: 21 May 2018**

**References**

1. Zbiden H, Bechmann-Pasquinucci H, Gisin N, Ribordy G (1998) Quantum cryptography. Applied Physics B 67(6):743–748

2. Bargigia I, Tosi A, Shehata AB, Frera AD, Farina A, Bassi A et al (2012) Time-resolved diffuse optical spectroscopy up to 1700 nm by means of a time-gated InGaAs/InP single-photon avalanche diode. Appl Spectrosc 66(8):944

3. Stefan F, Tosi A, Zappa F, Cova S (2004) CMOS circuit testing via time-resolved luminescence measurements and simulations. Instrum Meas IEEE Trans 53(1):163–169

4. Schreiber U, Werner C, Kamerman GW, Singh UN (2002) Laser radar ranging and atmospheric lidar techniques. Proc SPIE Int Soc Opt Eng 3865:1–160

5. Hadfield RH (2009) Single-photon detectors for optical quantum information applications. Nat Photonics 3(12):696–705

6. Zhang J, Itzler MA, Zbiden H, Pan JW (2015) Advances in InGaAs/InP single-photon detector systems for quantum communication. Light Sci Appl 4(5):1–13

7. Pellegrini S, Warburton RE, Tan LJ, Ng JS, Krysa AB, Groom K et al (2006) Design and performance of an InGaAs/InP single-photon avalanche diode detector. IEEE J Quantum Electron 42(4):397–403

8. Tosi A, Calandri N, Sanzaro M, Acrieti F (2014) Low-noise, low-jitter, high detection efficiency InGaAs/InP single-photon avalanche diode. IEEE J Selected Top Quantum Electron 20(6):192–197

9. Donnelly JP, Duer EC, McIntosh KA, Dauler EA, Oakley DC, Groves SH et al (2006) Design considerations for 1.06-μm-SuSIn InGaAs/InP Geiger-mode avalanche photodiodes. IEEE J Quantum Electron 42(8):797–809

10. Ma J, Bai B, Wang LJ, Tong CQ, Jin G, Zhang J et al (2016) Design considerations of high-performance InGaAs/InP single-photon avalanche diodes for quantum key distribution. Appl Opt 55(27):7497

11. Acerbi F, Anti M, Tosi A, Zappa F (2013) Design criteria for InGaAs/InP single-photon avalanche diode. IEEE Photonics J 5(2):6802009–6802009

12. Meng X, Tan CH, Dimler S, David JP, Ng JS (2014) 1550 nm InGaAs/InAlAs single photon avalanche diode at room temperature. Opt Express 22(19):22608–22615

13. Meng X, Xie S, Zhou X, Calandri N, Sanzaro M, Tosi A et al (2016) InGaAs/InAlAs single-photon avalanche diode for 1550 nm photons. R Soc Open Sci 3(3):150584

14. Meier HTJ (2011) Design, characterization, and simulation of avalanche photodiodes

15. Chen J, Zhang Z, Zhu M, Xu J, Li X (2017) Optimization of InGaAs/InAlAs avalanche photodiodes. Nanoscale Res Lett 12(1):33

16. Goh YL, Marshall ARJ, Massey DJ, Ishikawa H, Anan T, Makita K et al (2007) Avalanche multiplication in InAlAs, IEEE Trans Electron Devices 54(1):11–16

17. Mun SCLT, Tan CH, Dimler SJ, Tan LJJ, Ng JS, Yu LG et al (2009) A theoretical comparison of the breakdown behavior of In0.52Al0.48As and InP near-infrared single-photon avalanche photodiodes. IEEE J Quantum Electron 45(5):566–571

18. Goh YL, Marshall ARJ, Massey DJ, Ng JS (2007) Excess avalanche noise in In0.52 Al0.48 As, IEEE J Quantum Electron 43(6):503–507

19. Nada M, Muramoto Y, Yokoyama H, Ishibashi T (2014) Vertical illumination InAlAs avalanche photodiode for 50-Gbit/s applications. Int Conf Indium Phosphide Relat Mater–1–2

20. Czuba K, Jurczcyk J, Kaniowski J (2015) A study of InGaAs/InAlAs/InP avalanche photodiode. Solid State Electron 104:109–115

21. Zhao K (2008) III–V single photon avalanche detector with built-in negative feedback for NIR photon detection. Dissertations & Theses – Gradworks, San Diego

22. Kleinow P, Rutz F, Aidam R, Bronner W, Heussen H, Walther M (2016) Charge-layer design considerations in SAGCM InGaAs/InAlAs avalanche photodiodes. Phys Status Solidi A 213(4):925–929

23. Hu C (2010) Modern semiconductor devices for integrated circuits, Prentice Hall, Tokyo

24. Sze SM (1970) Physics of semiconductor devices, Phys Today 23(6):75–75

25. Hsieh HC, Sargeant W (1989) Avalanche buildup time of an InP/InGaAsP/InAlAs/GaInAs SAGM avalanche photodiode. IEEE J Quantum Electron 25(2):705–710

26. Levinstein MEM (1996) Handbook series on semiconductor parameters. World Scientific, Singapore

27. Rouvie A, Carpenter D, Lagay N, Decobert J, Carpentier D, Achouche M (2009) High gain * bandwidth product over 140-GHz planar junction AlInAs avalanche photodiodes. IEEE Photon Technol Lett 21(1):53–55

28. Li B, Lv QQ, Cui R, Yin WH, Yang XH, Han Q (2015) A low dark current mesa-type InGaAs/InAlAs avalanche photodiode. IEEE Photon Technol Lett 27(1):34–37

29. Duan N, Wang S, Zheng XG, Li X, Li N, Campbell JC et al (2005) Detrimental effect of impact ionization in the absorption region on the frequency response and excess noise performance of InGaAs/InAlAs SACM avalanche photodiodes. IEEE J Quantum Electron 41(4):568–572

30. Watanabe I, Sugou S, Ishikawa H, Anan T, Makita K, Tsuji M et al (1993) High-speed and low-dark-current flip-chip InAlAs/InGaAs quaternary well superlattice APDs with 120 GHz gain-bandwidth product. IEEE Photon Technol Lett 5:677–679

31. Lahrichi M, Derouin E, Carpentier D, Lagay N (2009) Avalanche multiplication in InAlAs. IEEE Trans Electron Devices 56(1):163–169

32. Rahman M, Nishino S, Ishikawa H, Anan T, Makita K, Tsuji M et al (2005) High-speed InGaAs/InAlAs superlattice avalanche photodiodes with 120 GHz gain-bandwidth product. IEEE Photon Technol Lett 17(1):53–55

33. Watanabe I, Tsuji M, Makita K, Taguchi K (1996) Gain-bandwidth product analysis of InAlGaAs/InAlAs superlattice avalanche photodiodes. IEEE Photon Technol Lett 8(2):269–271
33. Kagawa T, Kawamura Y, Iwamura H (1992) InGaAsP/InAlAs superlattice avalanche photodiode. IEEE J Quantum Electron 28(6):1419–1423
34. Hurkx GAM, Klaassen DBM, Knuvers MPG (2002) A new recombination model for device simulation including tunneling. IEEE Trans Electron Devices 39(2):331–338
35. Ando H, Kanbe H, Ito M, Kaneda T (1980) Tunneling current in InGaAs and optimum design for InGaAs/InP avalanche photodiode. Jpn J Appl Phys 19(6):L277–L280
36. Hurkx GAM, De Graaff HC, Kloosterman WJ, Knuvers MPG (1990) A novel compact model description of reverse-biased diode characteristics including tunneling. Solid state device research conference, 1990. Essdec 90. European, pp 49–52
37. Park C-Y, Hyun K-S, Kang SG, Kim HM (1995) Effect of multiplication layer width on breakdown voltage in InP/InGaAs avalanche photodiode. Appl Phys Lett 67(25):3789–3791
38. Wen J, Wang WJ, Hu WD, Li N, Li ZF, Lu W (2016) Origin and optimization of large dark current increase in InGaAs/InP APD. International conference on numerical simulation of optoelectronic devices.