Relation between chemical composition, morphology, and microstructure of poly(ether ether ketone)/reduced graphene oxide nanocomposite coatings obtained by electrophoretic deposition

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ABSTRACT
The effect of the chemical composition on the morphology and microstructure of poly(ether ether ketone) (PEEK)/reduced graphene oxide (RGO) nanocomposite coatings is analyzed. RGO induced three main morphological features in the nanocomposites: (i) a large-scale co-continuous morphology related to nanosheets whose basal planes were mainly aligned with the coating surface, (ii) a dendritic morphology of PEEK domains, and (iii) irregular domains related to the deposition of PEEK particles wrapped by the nanosheets. The development of these morphological features was influenced by the RGO content, allowing the modification of the surface roughness. RGO also induced changes in the melting and non-isothermal crystallization of the polymeric matrix and promoted transcrysallisity in PEEK that, in turn, was a key factor in the development of the final microstructure. In addition, polymer chain mobility was observed to be hindered at high nanofiller concentrations, increasing the glass transition temperature, and diminishing the recrystallization of the polymeric matrix.

Introduction
Poly(ether ether ketone) (PEEK) is a semicrystalline thermoplastic and polyaromatic linear polymer that combines outstanding mechanical properties with high-temperature stability, and low smoke emission and flammability [1–5]. Due to these properties, PEEK is a high-performance polymer with applications in diverse areas, ranging from medicine to aerospace [5]. When used as coating, PEEK has good

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adhesion to metallic substrates. Moreover, the properties of PEEK-based coatings can be tailored to meet specific technological requirements by incorporating carbonaceous, ceramic, and metallic fillers whose dimensions are in the nano- or micro-scale [6]. In the field of advanced composites and nanocomposites coatings, the electrophoretic deposition (EPD) process has received increasing attention in recent years because it offers a good control of mass and thickness of the deposits whilst favoring the development of specific morphologies [7–9]. In our previous work, interesting morphological features were observed in PEEK/reduced graphene oxide (RGO) nanocomposite coatings obtained by electrophoretic co-deposition of PEEK and graphene oxide (GO) particles followed by a thermal treatment [10]. The electric field applied during EPD promoted the basal plane alignment of the GO nanosheets with the coating surface, meanwhile the thermal treatment and GO content induced a dendritic morphology of PEEK domains. Furthermore, the increase of GO nanosheet content was associated with the development of irregular domains related to the deposition of PEEK particles wrapped by GO nanosheets [10]. Incorporation of a small amount of reduced graphene oxide (RGO) into polymeric matrices can significantly improve mechanical and functional properties of the nanocomposites [11]. RGO is obtained by removing large amounts of oxygen-containing groups from GO by chemical, thermal, or other methods. Hence, RGO is a two-dimensional (2D) monolayer material made of crystalline domains that comprise sp² carbon atoms disposed of in a hexagonal or honeycomb lattice, and amorphous domains that result from the distortions provoked by residual sp³ C–O bonds [12–15]. The aforementioned intrinsic structure endows RGO with exceptional properties, for instance, flexibility, high Young’s modulus, and strength, high specific surface area, and excellent thermal, and electrical conductivity [13].

As is the case for other semicrystalline polymers, the properties of PEEK are heavily dependent on its crystallinity [16, 17]. In this respect, nano- and microfillers could affect the melting and crystallization processes of PEEK [18, 19], for instance, heterogenous nucleation promoted by existing surfaces could induce transcrystallinity in PEEK during its crystallization from the melt [20–24]. In this respect, carbon fibers have been shown to affect the nucleation and crystal growth rate in PEEK matrices, modifying not only the microstructure characteristics as a result of transcrystallinity (e.g., crystallinity degree and crystal orientation) but also the mechanical properties of the PEEK matrix [24]. Moreover, it has been reported that RGO can provoke variations in the nucleation, growth, and crystal orientation in semicrystalline polymers [25, 26], nonetheless, to the authors’ knowledge, the effect of RGO on the crystallization of PEEK has not been investigated to date. The effect of nano- and micro-fillers on crystallinity and other properties of polymer-based composites is strongly dependent on factors such as matrix-filler interaction, nanoparticle dispersion, nanoparticle size and shape, and alignment as in the case of nanosheets [27, 28]. Thus, the properties of PEEK/RGO nanocomposite coatings could be largely influenced by the preferential basal-plane alignment and the wrapping effect of the nanosheets, and a profound understanding of the microstructure-property correlation is required for optimising the desired properties of PEEK/RGO nanocomposite coatings.

In this work, the correlation between the morphology and crystalline structure of PEEK interacting with RGO nanosheets in electrophoretically obtained PEEK/RGO nanocomposites is meticulously analysed by varying the nanofiller content. Scanning electron microscopy, atomic force microscopy, confocal laser scanning microscopy, simultaneous thermal analysis, and grazing incidence X-ray diffraction were employed to characterise the prepared nanocomposites. To the authors’ knowledge this is the first study comprehensively characterising the interaction of RGO and PEEK in relation to PEEK crystallisation.

**Experimental**

**Materials**

PEEK powder VICTREX™ PEEK VICOTE™ 704 (Victrex PCL, UK) for coating of ferrous and nonferrous metals were used as the polymer matrix and its properties are summarised in Table 1 [29, 30]. Single-layer graphene oxide dispersed in deionized water (flake size 0.5–2.0 μm, thickness 0.6–1.2 nm, single-layer ratio > 80%, and concentration of 10 mg mL⁻¹) commercialised under the trademark of GNO1W001 (ACS Materials, USA) was used as the nanofiller. Ethanol denatured with about 1% methyl
ethyl ketone for analysis (EMSURE®/C210, Germany), and isopropanol 99.9% purity (Sigma-Aldrich, Germany) were utilised as the suspension medium for EPD process. Stainless steel 316 L foil with dimensions of 15 mm (width) × 0.2 mm (thickness) (Thyssenkrupp, Germany) was used for preparing the counter electrodes. The physical and chemical properties and chemical composition of stainless steel 316 L foil are listed in Table 2 [31]. VICTREX™ PEEK VICOTE™ 704, graphene oxide GNO1W001, and stainless steel 316 L foil are hereafter referred as PEEK, GO, and stainless steel, respectively.

### Preparation of the PEEK/RGO nanocomposite coatings

PEEK/RGO nanocomposite coatings were developed by electrophoretic co-deposition of PEEK particles and graphene oxide (GO) nanosheets, followed by thermal treatment. The preparation has been described in detail in our previous work [10] and is summarised in Fig. 1. Briefly, PEEK powder (3 wt%) was added into the non-aqueous media (40 mL of ethanol 95 vol% and 2-propanol 5 vol%), and ultrasonicated for an effective time of 6 min (active interval of 0.5 s, followed by an inactive one of 2.1 s) at constant amplitude value of 30%, Fig. 1a. Compositions of 0.5, 1.0 and 3.0 GO wt. % relative to the PEEK mass were prepared by adding 0.5, 1.0, and 3.0 mL of GO suspension (concentration of 10 mg mL⁻¹) to the previously ultrasonicated PEEK suspensions, Fig. 1b. Table 3 lists the nomenclature and characteristics of the suspensions prepared.

Stainless steel electrode plates (dimensions: 30 mm × 15 mm × 0.2 mm) were polished with a P600 CarbiMet™ grinding paper (Buhler Group, Switzerland) and subsequently cleaned for 30 min in ethanol using an ultrasonic bath. Prior to the EPD process, the suspensions were magnetically stirred for 24 h at 250 rpm and at room temperature. Two polished-and-cleaned stainless-steel electrodes were immersed into the suspension in a parallel plate arrangement. Based on our previous work, a constant voltage of 30 V, deposition time of 3 min, and 10 mm distance between electrodes were selected, as these EPD experimental conditions led to the uniform coatings, Fig. 1c. Once the EPD process was completed, the coated electrode plates were carefully extracted from the suspension to prevent damage to the deposited layer.

Prior to thermal treatment, the samples obtained by using EPD were dried in air at 150 °C for 3 h. The thermal treatment process, also in the ambient atmosphere, allowed densification of the coating and erased any thermal history effects of the polymeric matrix, as well as reducing the GO. The thermal treatment consisted of the following thermal cycles: (i) heating from ambient temperature to 380 °C at a rate of 10 °C min⁻¹, (ii) isothermal dwell at 380 °C for

### Tables

| Table 1 Properties of VICTREX™ PEEK VICOTE™ 704 [29, 30] |
| --- | --- | --- | --- |
| Property | Value |
| Density (kg m⁻³) | 1.32 |
| Melting temperature (°C) | 343 |
| Glass transition (°C) | 143 |
| Average particle size (µm) | 10 |

| Table 2 Properties and chemical composition of stainless steel 316 L. All the property values correspond to a temperature of 20 °C [31] |
| --- | --- |
| Property | Value |
| Density (kg m⁻³) | 8.0 |
| Melting temperature (°C) | 15 |
| Glass transition (°C) | 200 |
| Average particle size (µm) | 500 |
| Electrical resistivity (Ω mm² m⁻¹) | 0.75 |
| Linear thermal expansion coefficient (10⁻⁶ K⁻¹) | 16.0 |
| Yield strength (MPa) | 220 |
| Tensile strength (MPa) | 520–670 |
| Chemical composition (heat analysis in wt.%) | C 0.03/Si 1.00/Mn 2.00/P 0.05/S 0.015/Cr 16.50–18.50/Ni 10.0–13.00/N 0.10/Mo 2.00–2.50/Fe balance |
To the ultrasonic generator

(a) Tip sonication of PEEK suspension

Deagglomeration, and size reduction of PEEK particles

(b) GO incorporation and magnetic stirring

Densified PEEK/RGO coating on steel

(c) Electrophoretic deposition

(d) Dry and thermal treatment

Figure 1 Scheme of the methodology implemented in the preparation of the PEEK/RGO nanocomposite coatings involving EPD.

Table 3 Nomenclature and characteristics of the suspensions prepared

| Suspension   | Content                              | Nomenclature used for the thermally treated coatings |
|--------------|--------------------------------------|-----------------------------------------------------|
| PEEK         | GO suspension to ethanol/isopropanol (vol. %) |                                                             |
|              | GO to PEEK (wt. %)                    | Total solid content (%)                                |
|              |                                       |                                                     |
| PEEK         | 0                                    | 3.00                                                | PEEK-C |
| PEEK/0.5GO   | 1.25                                 | 0.5                                                 | NC-1   |
| PEEK/1.0GO   | 2.50                                 | 1.0                                                 | NC-2   |
| PEEK/3.0GO   | 7.50                                 | 3.0                                                 | NC-3   |

Regarding the PEEK-based coatings, the nomenclature corresponds to the materials after the thermal treatment. In all cases, the mass fraction of PEEK powder added into the ethanol/isopropanol media (ethanol 95 vol% and 2-propanol 5 vol%) was 3%.

Coating characterization

Scanning electron microscopy

The morphology of coatings was examined by scanning electron microscopy (SEM), using a field-emission scanning electron microscope ZEISS Gemini SEM 450 (ZEISS, Germany) equipped with an in-lens secondary electron detector. Graphene oxide is highly electron transparent because of its 2D structure and low atomic number, especially at high accelerating voltages when incident electrons can pass through the nanosheets more easily [32]. Hence, an accelerating voltage of 1 kV and probe current of 10 nA were selected to favor the observation of GO nanosheet details and to ensure a reliable comparison between different coatings. Prior to SEM characterization, the samples were dried at 60 °C for 24 h in a drying oven with natural convection (DL 115 DRY-line®, VWR International BVBA, Belgium) and subsequently coated with Au in a sputter coater (Q150T S Plus, Quorum, UK) to prevent the sample charging during measurement.

Atomic force microscopy

Topography was examined and phase images of the surface of PEEK and PEEK/RGO nanocomposite coatings were obtained using an atomic force microscope (AFM) Innova® (Bruker, Germany) in standard dynamic mode, which was provided with 20-bit DAC.
scan control and nanosensor tapping mode probes NCHV®. An effective resonance frequency of 160 kHz and a constant nominal force of 48 N m⁻¹ were considered. Areas of 1 × 1 µm² and 10 × 10 µm² were scanned with a resolution of 1024 × 1024 pixels at a scan speed of 10 µm/s. AFM micrographs were processed in the NanoScope® software (version 1.4).

Confocal laser scanning microscopy

Roughness was characterised in accordance with the ISO 251587-2:2012 by using confocal laser scanning microscopy (CLSM). A confocal microscope Sensofar Sneox (Sensofar, Germany) that incorporated an objective EPI 50 × and a high-resolution charge-coupled sensor (0.26 µm/pixel resolution, and 1360 × 1024 pixels area) allowed the generation of two-dimensional (2D) and three-dimensional (3D) images of the PEEK-based coatings. Non-contact optical profiles of observable areas (350.88 × 264.19 µm²) were recorded by considering a 30 s acquisition time and 8.5% light intensity. Roughness was evaluated over the total surface and in the characteristic areas of the samples: flat areas between the pores and inside the pores. To quantify the surface roughness, the arithmetical mean deviation (Sa) and the root mean square height (Sq) were used. SensoMAP Premium® software (version 7.4.8114) was used for analyzing the experimental data.

Simultaneous thermal analysis

Thermogravimetric analysis—differential thermal analysis (TGA-DTA), and differential scanning calorimetry–thermogravimetric analysis (DSC-TGA) were performed in a simultaneous thermal analyzer STA 449 FI Jupiter (NETZSCH-Gerätebau GmbH; Germany). Samples of PEEK/RGO coatings were prepared for the TGA-DTA and DSC-TGA analyses as follows: after EPD, coatings were dried in an air atmosphere at 150 °C for 3 h, and carefully detached from the metallic substrate using a spatula and placed on aluminum foil. Then, the samples were thermally treated under the same conditions used for the coatings. Finally, the aluminum foil was completely removed using precision pliers.

For TGA-DTA measurements, 10 mg of PEEK/RGO samples was placed into Al₂O₃ crucibles and measured under flowing nitrogen atmosphere (25 mL min⁻¹). The DSC-TGA measurements comprised four stages: (1) heating at a constant rate of 10 °C min⁻¹ from 100 to 380 °C, (2) isothermal stage at 380 °C during 5 min, (3) cooling at a constant rate of 2 °C min⁻¹ from 380 to 100 °C, and (4) a second heating at a constant rate of 10 °C min⁻¹ from 100 to 380 °C. The measurement of every sample was corrected by considering the blank curve that was previously recorded for the empty platinum crucible. Transition glass temperature, $T_g$, was determined from the step in the baseline of the corrected sample measurement and associated with the temperature at which the half point of the angle bisector determined by the tangents drawn on the heat flow curve above and below the transition temperature. Melting temperature, $T_m$, was considered as the temperature of the maximum deviation of the melting endotherm with respect to the baseline. The crystallization temperature, $T_c$, that associated with the minimum in the crystallization exotherm. The apparent enthalpy of the transition, $\Delta H_{ap}$, was determined from the corresponding transition area, taking the upper and lower limits of the integration at the corresponding deviations from the baseline of the thermogram. The degree of crystallinity, $\chi$, was calculated from the expression:

$$\chi = \frac{\Delta H_{ap}}{w \cdot \Delta H_0}$$

where $\Delta H_{ap}$ is the apparent enthalpy of the transition, $w$ is the weight fraction of RGO nanosheets, and $\Delta H_0$ is the melting enthalpy of 100% crystalline PEEK, for which a value of 130 J/g was adopted [33].
Grazing incidence angle X-ray diffraction

A parallel beam geometry was used for performing grazing incidence angle X-ray Diffraction (GIAXRD) on the PEEK-based nanocomposite coatings. Diffraction patterns were recorded using a Panalytical Empyrean DY1098 X-ray diffractometer (Malvern Panalytical Ltd, Netherlands) operated at 45 kV and 40 mA. The instrument was equipped with a conventional line focus Cu radiation tube, a parabolic Göbel mirror, and a 2D solid-state hybrid pixel X-ray PIXcel3D detector switched to proportional counter mode (1 channel open). In addition, 1/4° divergence fixed slit and 10 mm fixed mask were considered for limiting the penetration depth and beamwidth, respectively. The resulting intense quasi-parallel incident X-ray beam irradiated the stainless-steel substrates (dimensions of 15 mm × 15 mm) coated with the PEEK or PEEK/RGO nanocomposites. Background radiation was significantly reduced by using a 0.18° parallel plate collimator, and Kβ X-ray spectral line of Cu was suppressed by Nickel filter, maximizing the intensity of the Cu-Kα radiation (λ = 1.5406 Å). GAXRD patterns were recorded in the angular range (2θ) from 5 to 40° in step-scan mode which comprised increments of 0.026° and accumulated counts for each step of 10 s. With the aim of analyzing the crystalline phase changes at the proximity of the coating surface, the angle of incidence was set to 0.2° and 1° to vary the penetration depth. In addition, to determine the position and index of the characteristic diffraction peaks associated with the polymeric matrix and the nanofiller, the crystallinity degree of the PEEK matrix was estimated from the XRD diffractograms [33, 34].

Results and discussion

In the first part of this section, the main morphological features of PEEK/RGO nanocomposite coatings are discussed and their relationship with the chemical composition and microstructure is presented. Subsequently, the effect of the chemical composition on the melting and non-isothermal crystallization processes of PEEK is analyzed paying special attention to the relation between the microstructural characteristics and morphology.

Microstructure characterisation

The spherulitic morphology of PEEK formed during non-isothermal crystallization from the melt is heavily dependent on factors such as molecular weight, nucleation site, and seed density, and thermal treatment. Whilst fast cooling rates contribute to low crystallinity, slow rates promote the development of large spherulites. Spherulites that resulted from the slow cooling rate (2 °C min⁻¹) from melt are observed in the SEM micrographs of PEEK-C in Fig. 2a and b. PEEK-C spherulite size was in the range of tens to hundreds of microns, in agreement with that described in PEEK films [21].

In PEEK/RGO nanocomposite coatings, the nanofiller induced three distinctive morphological features: (i) a large-scale co-continuous morphology formed by the nanosheets, (ii) dendritic PEEK domains, and (iii) irregular domains related to the deposition of PEEK particles wrapped by the nanosheets. The large-scale co-continuous morphology suggests an assembly of the GO nanosheets that occurred during the EPD process, resulting in deposited nanosheets whose basal planes are aligned with the coating surface, as seen in Fig. 3a. The high electron transparency of the GO nanosheets, which is the consequence of their structure and low atomic number [32], allows deposited PEEK particles to be visualised underneath. After the thermal treatment that led to the PEEK/RGO nanocomposites by densifying the polymeric matrix and reducing the GO, the originally formed large-scale co-continuous morphology was retained, as observed in Fig. 3b. Other interesting morphological features of PEEK/RGO nanocomposite coatings are indicated in the SEM micrograph in Fig. 3b and further discussed below.

A representative dendritic domain such as that shown in Fig. 3b is illustrated in more detail in the SEM micrograph in Fig. 4. The formation of such domains was closely connected with the large-scale co-continuous ones, by being deposited on RGO nanosheets. Such dendritic PEEK morphology could emerge from two mechanisms that took place during the cooling from melt. The first mechanism, transcry stallinity or surface crystallisation, is a condition where crystals grow normal to an existing surface that serves as nuclei, in the present case, the RGO nanosheets. Transcrystallinity of PEEK provoked by heterogenous nucleation on diverse surfaces is a well-
known phenomenon [10, 21, 23, 24]. The second mechanism is related to crystal growth rate in thin films, in which transcrystalline growth could compete with the bulk spherulitic one for developing the crystalline phase depending, in a first instance, on the surface energy and interfacial free energy difference and, later on, the kinetics of crystallization [21, 28]. However, in the dendritic PEEK domains in PEEK/RGO nanocomposite coatings the suppression of bulk spherulitic growth was evident. Thus, the dendritic domains are obliged to grow perpendicularly to the surface, developing a thickness less than 1 μm, as observed in Fig. 4.

The irregular PEEK morphology is associated with the nanosheet wrapping effect during the EPD process [10]. RGO wrinkles that result from the thermal reduction effect and the van der Waal’s interactions [35], as well as irregular PEEK domains, are distinguished in Fig. 3b. To gain further insights into the effect of RGO on the irregular PEEK domains,
AFM topological and phase imaging were carried out. In Fig. 5a, an AFM topology image of a scanned area (5 × 5 μm²) shows an irregular PEEK domain with dimensions (approximately 4 μm length) comparable with that indicated in Fig. 3b. Surface stiffness/softness characteristics of the irregular PEEK domain and RGO wrinkles (b) are distinguishable in the scanned area of 5 × 5 μm². The AFM topology image collected over a smaller area (1 × 1 μm²), Fig. 5c, indicated an analogous morphology to that reported for the graphene oxide reduction of thin films [36]. Nevertheless, the corresponding AFM phase image, Fig. 5d, revealed granular structures in the order of one hundred of nanometres (indicated in orange). The flake size is several orders of magnitude larger (0.5–2.0 μm), so consequently, these inner granular structures could be related to PEEK. Large granular and small crystals of melt crystallised PEEK have recently been described [37], but this is the first time that this is reported for PEEK/RGO systems. As discussed further on the basis of the GIAXRD results, a transcrystalline growth into the irregular PEEK domains could develop on the RGO nanosheets, whilst spherulitic-like domains develop at the interior of the irregular PEEK domains distant from the nanosheets.
It is expected that the aforementioned morphologies depend largely on the nanosheet content. Dendritic and irregular PEEK morphologies are compared in Fig. 6 for the nanocomposites NC-1, NC-2, and NC-3. From the residual mass in the thermogravimetric curves (Fig. S1), the RGO wt% was estimated to be 2.7, 4.1, and 6.1 for the nanocomposite coatings NC-1, NC-2, and NC-3, respectively (RGO wt% values are indicated in the x-axis in Fig. 6). These nanosheet mass fractions were indeed larger than those utilized in preparing the EPD suspensions (GO to PEEK in Table 3), and they could be related to the difference in the charge and the electrophoretic mobility between the PEEK particles and GO nanosheets during the EPD process [38]. The highest nanosheet content (6.1 RGO wt%) inhibits the development of the dendritic PEEK morphology, as seen in Fig. 6c. By contrast, the irregular PEEK morphology evolves favorably by increasing the RGO wt%. The already mentioned morphological features were representative along the sample surface, Fig. 6d to f, contributing to the roughness.

Figure 6 SEM micrographs of PEEK/RGO nanocomposites NC-1, NC-2, and NC-3. The RGO wt% is indicated in the x-axis. Variations in the superficial dendritic and irregular PEEK morphology are observed as a function of RGO wt%. Wrinkles on RGO nanosheets are also indicated.

Figure 7a to d show the confocal images of the surface for the PEEK-C and PEEK/RGO nanocomposite coatings. PEEK spherulites are observed in the confocal image of PEEK-C in Fig. 7a. On the contrary, the CLSM did not confirm the formation of PEEK spherulites in the nanocomposite coatings, Fig. 7b to d. As a result, the roughness could be modified by adding RGO. The values of the roughness parameters $S_a$ and $S_q$ summarised in Fig. 7e increased with the RGO content due to irregular PEEK morphology. The changes in $S_a$ and $S_q$ showed a similar trend, but the increment was more pronounced for $S_q$ when comparing PEEK-C and NC-3.

**Melt and non-isothermal crystallization**

Figure 8a displays the first heating scan in a nitrogen atmosphere from 100 to 380 °C at the constant heating rate of 10 °C min$^{-1}$ for the PEEK-C. Above 145 °C, the baseline of the differential thermogram starts changing, and the glass transition is observed at $T_g = 163$ °C. The $T_g$ value depends on the thermal history and the physical method that is implemented for its measurement [39, 40]. However, the $T_g$ value measured in this work agrees with that obtained in the study of annealing of PEEK with different molecular weight using DSC [41]. Further increase of temperature provokes the melting of the PEEK crystalline phase, resulting in a large and broad
endotherm centered at $T_{m, II} = 347^\circ C$ (region II) with a shoulder at $T_{m, I} = 321^\circ C$ (region I). PEEK endothermic response is of complex nature and involves diverse factors such as molecular weight, crystallization history, time and temperature associated with annealing process, and scanning heating rate [41–46]. The PEEK-C endotherm shoulder in region I, Fig. 8a, corresponds to the melting of a small population of crystals that are developed during the DSC scan, while the endotherm peak in the region II represents the melting of the majority population of crystals that are formed during the non-isothermal crystallization of the PEEK-C from the melt [41].

On cooling from the molten state, nucleation and crystal growth takes place, and the crystalline microstructure is developed under non-isothermal
conditions. The exothermic peak is observed at 305 °C in the differential thermogram recorded at a constant cooling rate of 2 °C min⁻¹ from 380 to 100 °C in nitrogen atmosphere, Fig. 8a. This $T_c$ value agrees with those reported in the literature [44, 45]. A subsequent heating scan of PEEK-C under identical experimental conditions is also shown in Fig. 8a. The glass transition, and endothermic shoulder and peak temperatures ($T_{g,2}$, $T_{m,1-2}$, and $T_{m,II-2}$) are clearly distinguished in the differential thermogram. Although the values of the aforesaid parameters remained almost unchanged through the first and second heating scan, a slightly better defined exothermic shoulder in the second scan in Fig. 8a contributed to a minor increment of $\chi_m$-2 with respect to $\chi_m$ as shown in and Fig. 8 (b). Nevertheless, the values of degree of crystallinity $\chi_m$ and $\chi_m$-2 were in the interval of 30-40% described for PEEK [33, 34, 47]. On the contrary, the crystallinity degree related to the exotherm ($\chi_c$) and that associated with the second heating-scan endotherm ($\chi_m$-2) substantially differed from each other, as seen in Fig. 8b. This difference arises from the recrystallization process that takes place during the DSC scan [41].

Incorporation of nano- and micro fillers in PEEK could affect its melting and crystallization processes [18, 19]. The differential thermograms in Fig. 8a confirmed that RGO influenced the melting and crystallization behaviour of PEEK. These results were consistent with the observed changes in the morphology, that is, the development of dendritic PEEK morphology, the absence of spherulites in the PEEK/RGO nanocomposites, and the inner granular morphology, the absence of spherulites in the PEEK/RGO nanocomposites, and the inner granular structure in the irregular PEEK domains. In the first and second heating scans in Fig. 8a, the dotted arrows indicate the shift to lower temperature of the large and broad endotherm with the increase of the content of RGO wt.% to 6.1 wt% for NC-3. The shift of the endothermic shoulder to lower temperatures was even more significant, as documented by the comparison of $T_{m,1}$ and $T_{m,1-2}$ parameters with $T_{m,II}$ and $T_{m,II-2}$ in Fig. 8b. On the contrary, the glass transition temperatures of the first and second scan $T_g$ and $T_{g,2}$ respectively, increased for nanosheet content above 4.1 wt.% RGO. Nonetheless, the temperature variations of $T_g$ and $T_{g,2}$ were of similar order of magnitude as those of $T_{m,1}$ and $T_{m,II}$, as shown in Fig. 8b. This result implies that high RGO concentrations substantially inhibited the mobility of the PEEK polymeric chains, provoking changes in the PEEK glass transition, and in the reorganisation of the polymeric chains in crystals during the heating scan.

The hindering of polymer chain mobility induced by RGO is well known [48, 49]. Crystallization from the melt with low chain mobility generally results in an imperfect crystal structure [41]. The differential thermograms of the cooling scan in Fig. 8a indicated a shift of the exotherm to lower temperatures with the increasing RGO content. Figure 8b presents the effect of RGO on the estimated crystallinity of the exotherm ($\chi_c$). A slight increment of this parameter was observed at 2.7 wt.% of RGO, while at higher nanofiller content the crystallinity decreased. Crystallization and melting processes are intimately linked. Figure 8b shows that $\chi_c$ had a variation trend similar to $\chi_m$ and $\chi_m$-2. By using the difference between the $\chi_c$ and $\chi_m$-2 of PEEK-C as a reference (vertical bar in Fig. 8b), it was found that $\chi_c$ and $\chi_m$-2 values converge in the nanocomposite coatings, reaffirming the effect of RGO on the mobility of the PEEK polymeric chains and its reorganization.

As in other semicrystalline polymers, the properties of PEEK depend heavily on the crystalline microstructure. Thus, a control of the thermal treatment is critical for optimising and obtaining desirable properties of a polymer. Depending on the atmosphere, the molecular weight and crystallinity of PEEK could be diminished by using prolonged heating at temperatures higher than $T_m$ [43–45]. In the preparation of PEEK-C and PEEK/RGO nanocomposite coatings, no significant difference between the parameters of the first and second DSC scan was observed, Fig. 8a and b, even though the measurements were performed under a nitrogen atmosphere and the thermal treatment of the samples was carried out in air. Considering both the DSC and TG results (Fig. S1), an excellent control of the thermal treatment was achieved.

Although the crystalline phase in bulk semicrystalline polymers is mainly determined by spherulitic growth [50], transcristallinity could significantly influence the development of the crystalline phase in thin films [21, 28]. Crystalline microstructure characteristics, for instance, crystallinity degree and crystal orientation, vary from bulk to interface because transcristalline growth competes with the bulk spherulitic growth, concurrently occupying the volume of the material [28]. In this regard, the GIAXRD characterization of thin and ultrathin films by irradiating the sample at an extremely low
incident angle with the aim of discriminating between multiple underlying structures that could contribute to the diffraction pattern enables the determination of the characteristics of the crystalline microstructure at the proximity of the coating surface. So far, to the author’s knowledge, GIAXRD has not been implemented in the characterization of PEEK-based coatings prepared by EPD. Figure 9 shows representative GIAXRD diffractogram patterns of the NC-3 (6.1 wt% RGO) recorded at the incident angles of 0.2 and 1.0°. PEEK is characterized by an orthorhombic unit cell that is a result of its planar zig-zag conformation (–R–O–R–O–CO) alignment with the c-axis, giving rise to four characteristic peaks at the approximate 2θ values of 19°, 21°, 23°, and 29°, which are indexed as the (110), (111), (200), and (211) crystalline planes, respectively [45]. With respect to RGO, intercalation and exfoliation play a major part in the resulting XRD patterns of two-dimensional graphitic nanosheets because the distance between the layers could be altered [51, 52]. In Fig. 9, the crystalline plane (002) that is associated with the distance between RGO nanosheets was absent in the measured 2θ interval. Consequently, there is no contribution of the RGO structure to the GIAXRD diffractogram, allowing the estimation of the degree of crystallinity of the polymeric matrix in the PEEK/RGO nanocomposite coatings from XRD experimental data. On the other hand, the diffraction peak assigned to the (100) crystalline plane is found in the GIAXRD diffractogram recorded at the lower incident angle.

In contrast with the (110) plane, the GIAXRD diffractograms recorded at an incident angle of 1° (Fig. 10a) indicate that the diffraction intensity at the plane (200) markedly increased with the content of RGO. Two- and three-dimensional carbon-based structures could induce transcrysallinity or surface crystallisation in polymeric matrices, which in turn results in variations in XRD diffractogram intensities [10, 21, 23, 24]. These results agree with the dendritic PEEK domains and inner granular structures in the irregular PEEK domains. Figure 10b compares the crystallinity degree of the PEEK-based nanocomposite coatings estimated from GIAXRD measurements as a function of the RGO content. The crystallinity degree, χ_{XRD}, decreases with increasing RGO content, having a maximum at 2.7 wt.% RGO. The crystallinity degree derived from the DSC results (χ_{DSC}) is shown in Fig. 10b. Apart from the small deviation in the nanocomposite NC-3, a good match was found between GIAXRD results and DSC experimental data in estimating the PEEK crystallinity degree. The full width at the half maximum (FWHM) values of the peaks associated with the PEEK crystalline planes increased with increasing RGO content (Fig. 10b) except for the plane (200). FWHM is sensitive to microstructure alterations and varies inversely with the size of crystals, thus an increase of FWHM values implies a reduction of the crystallite size. A marked transcrysallinity at high RGO contents and the reduction of the PEEK crystallite size found by the GIAXRD measurements confirm the hindering effect of RGO on the mobility of the polymeric chains and its reorganization, in agreement with the results of the DSC analysis.

To analyze in greater detail the irregular PEEK domains that were predominant in the NC-3 (6.1 RGO wt%), GIAXRD diffractograms were recorded at the incident angles in the interval 1–5°. The diffractograms are presented in Fig. 11a. The intensity of the diffraction line corresponding to the (110) plane is lower than that of the (200) plane for values below 3°. At 4° the intensity of the diffraction lines of the (110) plane is higher and then decreases. Similarly, the crystallinity varies with the incident angle, however, its mean value is close to the estimated crystallinity from DSC measurements (36%). The χ_{DSC} is indicated in Fig. 11b by the dotted horizontal line. This
behavior in the GIAxRD diffractograms and their parameters, Fig. 11a and b, could be associated with the formation of a transcrystalline or granular PEEK structure inside the irregular PEEK domains at the proximity of the RGO nanosheets, whilst other crystalline structures could be formed away from the nanosheets. Further analysis is needed to clarify this point. It is expected that the changes in crystalline microstructure, e.g., degree of crystallinity and crystal orientation, will influence the tribological properties of PEEK/RGO nanocomposite coatings.

Moreover, the RGO content induced changes in the melting and non-isothermal crystallization of PEEK. Reduction of crystallinity degree and glass transition temperature in PEEK at high RGO contents was attributed to the low chain mobility impaired by the presence of the nanofiller. PEEK crystallinity degree estimated from GIAxRD experimental data, and the FWHM analysis agreed with DSC results, indicating a reduction of both the content of crystalline phase and the size of PEEK crystals with increasing RGO content. The dendritic PEEK morphology in PEEK/RGO nanocomposite coatings was attributed to the effect exerted by the RGO nanosheets, as the suppression of bulk spherulitic growth was evident. GIAxRD diffractograms recorded at different incident angles indicate the formation of different crystal structures in the interior of irregular PEEK domains, albeit further analysis is required.

**Conclusions**

The correlations between chemical composition, morphology, and microstructure of poly(ether ether ketone)/reduced graphene oxide nanocomposite coatings were analyzed. The RGO nanosheet content played an important role in the resulting morphology, allowing modification of the surface roughness.

**Figure 10** a GIAxRD diffractograms recorded at incident angle of 1° for the PEEK-C and nanocomposite coatings, and b their crystallinity parameters.

**Figure 11** GIAxRD diffractograms of NC-3 recorded at different angles of incidence (a), and their crystallinity parameters (b).
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Declarations

Conflict of interest There is no conflict of interest.

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