A compact pulse-modulation cold air plasma jet for the inactivation of chronic wound bacteria: development and characterization

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A B S T R A C T

A compact low-temperature plasma jet device was developed to use ambient air as plasma gas. The device was driven by a 2.52-kV high-voltage direct-current pulse in a burst mode, with a repetition rate of 2 kHz. The maximum plasma discharge current was 3.5 A, with an approximately 10 ns full-width half-maximum. Nitric oxide, hydroxyl radical, atomic oxygen, ozone, and hydrogen peroxide—important reactive oxygen and nitrogen species (RONS)—were mainly produced. The amount of plasma-generated RONS can be controlled by varying the pulse-modulation factors. After optimization, the plasma plume length was approximately 5 mm and the treatment temperature was less than 40 °C. The preliminary bactericidal effects were tested on Staphylococcus aureus, Pseudomonas aeruginosa, and methicillin-resistant S. aureus (MRSA), and their biofilms. The results showed that the plasma can effectively inactivate S. aureus, P. aeruginosa, and MRSA in both time- and pulse-dependent manner. Thus, this produced plasma device proved to be an efficient tool for inactivating deteriorating bacteria. Further versatile utilization of this portable plasma generator is also promising.

1. Introduction

The number of patients with chronic wounds has been increasing constantly. Chronic wounds are normally defined as any acute wounds failing to heal within the expected time frame for that type of wound. Diabetic foot ulcers, pressure or decubitus ulcers, venous leg ulcers, and nonhealing surgical-site infections are the most common cases [1, 2]. These chronic wounds are a challenge to wound care professionals because they consume a great deal of health care resources and create a significant financial burden on the global health care system [3, 4, 5]. The important factors that contribute to delayed wound healing are the high level of bacteria and formation of biofilms. Biofilms are multicellular communities of bacteria held together by their self-made extracellular matrix. Staphylococcus aureus and Pseudomonas aeruginosa are commonly reported to form biofilms that are resistant to patients’ immune systems and a wide range of antibiotics, such as methicillin-resistant S. aureus (MRSA) [1, 2, 4].

Low treatment intensity and short treatment time required by cold atmospheric pressure plasmas (CAPPs) to stimulate wound healing have been proved to be the advantages of this alternative therapy [6, 7, 8, 9, 10]. One of the important effects of CAPPs on chronic wound healing is their bactericidal activity that is caused by generated reactive oxygen and nitrogen species (RONS). Because of their high reduction potential [11, 12, 13], these plasma-produced RONS—especially hydroxyl (OH) radical, atomic oxygen (O), ozone (O3), and hydrogen peroxide (H2O2)—can damage the phospholipid bilayer, proteins within the plasma membrane, and most intracellular components, such as nucleic acid, within the bacterial cell, leading to cell death [7, 14]. Meanwhile,
plasma-produced nitric oxide (NO) radical has shown stimulatory effects in wound healing and tissue regeneration [15, 16]. NO is an important cellular signaling molecule in human beings [17]. It can influence the immune system and stimulate cell proliferation, angiogenesis, and collagen synthesis, resulting in the reconstruction of damaged skin [1, 18]. Plasma jet is one type of CAPPs. It showed promising benefits in wound healing because of its capability to produce RONS independently of any conditions of the target surface, such as chemical component, electrical conductivity, roughness, treatment area, or wound depth. Most of the CAPP jet devices use noble gases such as helium (He), argon (Ar), or nitrogen (N₂) or their mixtures with a small amount of O₂, air, or water vapor as the plasma source [8, 19, 20]. However, using expensive inert gases—such as He and Ar, which are usually confined in a large container—as working gases limits the versatility of their applications. Thus, generating plasma jet devices that use ambient air as the source is of interest [21, 22, 23, 24, 25]. Moreover, air plasmas require shorter time to deactivate 90% of *Bacillus* spores compared to plasmas generated from pure He or He with a mixture of O₂ or air [26]. However, studies on the utilization of air plasmas are still scarce because of the variation of gas component and its necessity for the high ignition current that results in high plasma temperature and less plasma volume. On the contrary, most of the studies on pulse-modulation effects on reactive species generally focus on standard alternating-current (AC) signal, duty cycle modulation, and different frequency regime [27, 28]. Thus, because of the lack of research in this area, as well as the technical challenges, we developed a compact coaxial air plasma jet driven by kHz direct-current (DC) pulse modulation in a burst mode. The influence of modulation factors (number of pulses in a burst (NP), pulse delay time (PD), pulse width (PW), and
Fig. 3. V–I characteristics of the developed air plasma jet: (a) open-circuit voltage across the secondary coil of the transformer with 5 pulses in a burst, (b) the voltage and current waveform of the first discharge pulse, (c) overall 5 discharge pulses, and (d) photo of the developed air plasma jet. The air plasma jet was generated in a burst mode with pulse-modulation factors: PW = 1, PD = 12, NP = 5, BRR = 2, and applied air flow rate = 4 L/min. PW, pulse width; PD, pulse delay time; NP, number of pulses in a burst; BRR, burst repetition rate.

Fig. 4. (a) Instantaneous plasma dissipated power and energy deposition during 5 discharge pulses in a burst. (b) Dissipated plasma power as a function of NP and BRR. NP, number of pulses in a burst; BRR, burst repetition rate.
burst repetition rate (BRR)) on the produced reactive species had been investigated, together with its effects on the inactivation of wound bacteria.

2. Materials and methods

2.1. A compact pulse-modulation cold air plasma jet device

The developed plasma jet is a coaxial DC pulse-modulated kHz-driven atmospheric pressure air plasma jet. Typical ambient air at 25°C and 60% relative humidity (RH) was fed through the coaxial 0.5-mm-gap channel around the insulator rod by a DC air pump at 4 L/min. The plasma jet device comprised a 1.2-mm-diameter 304L stainless steel rod as a powered electrode and a 9-mm-inner-diameter aluminum rod as a grounded electrode with a 1-mm-diameter exit nozzle (Fig. 1a). The tip of the high-voltage (HV) electrode was located 1.0 mm above the grounded electrode. The powered electrode was driven by a series of HV pulses in a burst mode. The HV pulses were generated by a DC-DC converter and modulated by the control unit. The signals were then stepped up to a high voltage via a high-frequency transformer (1.5 kΩ of internal resistance). The pulse modulation consists of four key parameters: (1) PW (μs), defined as a pulse-on time; (2) PD (μs), defined by a period of fixed PW and varying pulse-off time; (3) NP; and (4) BRR (1/T kHz), defined as the number of pulse groups per second. The HV waveform that is generated in a burst mode with pulse factors PW = 1, PD = 12, NP = 5, and BRR = 2 is shown in Fig. 1(b).

2.2. Measuring electrical parameters of the plasma device

The voltage signal was measured using an HV probe (P6015A; Tektronix, Inc., United States), and the current was deduced from the voltage across the 57-Ω resistor measured by an HV probe (T3100; Qingdao Hantek Electronic Co., Ltd., China; see Fig. 1a). The V–I waveforms were recorded by a digital oscilloscope (TDS2014B; Tektronix, Inc., United States). In this study, the variations of the pulse-modulated condition had been studied for the correlation with the produced reactive species and bacterial inactivation effects. In addition, because the application focuses on wound healing, gas temperature would be limited to less than 40°C.

The instantaneous electrical powers P(t) and total energy (E) dissipated in a pulse of air plasma discharge [30] can be determined by

\[ P(t) = V(t)I(t), \]

\[ E = \int P(t)dt, \]

where \( V(t) \) and \( I(t) \) are the measured voltage and current, respectively.

2.3. Optical emission spectrum of the generated plasma

The optical emission of the plasma plume was measured by a broadband CCD spectrometer (Exemplar LS; BWTEK Inc., United States). The measured spectrum ranging from 200 to 850 nm was resolved by grating at 600 groove/mm and 25 μm slit width. The light emission from the OH band was detected by a high-resolution spectrometer with 0.05 nm resolution (AvaSpec-ULS3648, Avantes, the Netherlands), and the spectrum ranging from 220 to 340 nm was measured. The experimental configuration is shown in Fig. 1(a). The optical emission collected at about 1.0 cm away from the nozzle. Note that RH in the controlled experimental room was typically 60%.

2.4. Measuring O3 and NO radical concentrations

For the measurement of O3 and NO concentrations in the effluent of the air plasma jet, two gas detectors were employed: (1) model SKY2000–NO (Shenzhen YuanTe Technology Co., Ltd., China) for measuring NO concentration with a precision of 1 ppb, ranging from 0.05 to 250 ppm; and (2) model SKY2000–O3 (Shenzhen YuanTe Technology Co., Ltd., China) for measuring O3 concentration with a precision of 2 ppb, ranging from 0.05 to 250 ppm.

2.5. Measuring plasma temperature, ultraviolet radiation, patient leakage current, and O3 emission

To evaluate the human health risk of the developed air plasma jet, an assessment of a minimum set of potential risks—i.e., plasma temperature, ultraviolet (UV) emission, patient leakage current, and ozone emission—was performed [29, 31].

2.5.1. Measuring air plasma jet temperature

The plasma plume temperature is an important factor in plasma medicine applications. The temperature should not exceed a threshold of 40°C in general to avoid thermal damage or destruction of the living tissue. The air plasma jet temperatures were estimated from the temperature of the plasma-treated glass plate, because after the heat transfer from the plasma jet to the glass slide achieved a steady state, the maximum...
glass temperature at the center of the plasma jet contact zone was near the plasma gas temperature [32]. A thin glass slide of dimensions 22/C2 mm3 was perpendicularly placed at 5 mm from the plasma nozzle and was in contact with the plasma plume. The initial temperature of the glass plate was around 25°C. Infrared thermal images of the treated glass plate were captured by a thermal imaging camera (FLIR ONE; FLIR Systems Inc., United States; with 0.1°C resolution) from the backside of the glass plate as shown in Fig. 2(a).

2.5.2. Measuring UV emission
UV radiation is used in biomedical applications such as phototherapy, photochemotherapy, and antimicrobial [29, 31]. However, excess UV radiant exposure causes detrimental effects on the skin, such as erythema, hyperalgesia, inflammation, and deoxyribonucleic acid (DNA) damage [33]. According to the guidelines of the International Commission on Non-Ionizing Radiation Protection (ICNIRP), UV radiant exposure in the spectral region 200–400 nm incident upon the unprotected skin should not exceed 3 mJ/cm² [34]. To estimate UV radiation in terms of an optical power (W/cm²) [35] for continuous exposure of the skin generated by the air plasma jet, the spectral region in the 200–400 nm UV range of the air plasma jet was measured using the PM300 benchtop optical power meter (Thorlabs Inc., United States) with S120UV photodiode sensor (200–1100 nm). The UV sensor was located at 5 mm from the nozzle tip of the developed air plasma jet, as shown in Fig. 2(b).

2.5.3. Measuring patient leakage current
The patient leakage current can induce ventricular tachycardia or fibrillation and lead to cardiovascular collapse [36]. The safety standard for patient leakage current should be ≤10 μA for AC and ≤50 μA for DC. The evaluations of the patient leakage current of the developed air plasma jet were carried out using the equivalent circuit of human body impedance [31], as presented in Fig. 2(c). The circuit consists of resistor R1 (10 kΩ ± 5%), R2 (1 kΩ ± 5%), and C1 (0.015 μF ± 5%).

\[
I = \left[ \sum_{t=1}^{n} \frac{|V(t)|}{R_2} \right] f, \tag{3}
\]

where \(I\) is the patient leakage current, \(V(t)\) is the measured voltage, \(t_{int}\) is the integration time for a single pulse, \(\Delta t\) is the inverse count rate, and \(f\) is the pulse repetition rate.

2.5.4. Measuring O3 concentration
O3 is one of the most prominent ROS, which plays a crucial role in wound disinfection. However, a high O3 concentration is toxic, with harmful effects on the human respiratory system. According to the European Union directives (2002/3/EG) for long-term expositions, usually as daily 8-h time averages, the O3 concentration in ambient air should not exceed 0.055 ppm [29]. To estimate the O3 concentration in ambient air generated by the developed air plasma jet, the O3 concentration at different positions around the plasma jet was measured by an O3 gas detector (SKY2000–O3; Shenzhen YuanTe Technology Co., Ltd., China).

The actual O3 concentrations were detected at a different working distance \((D)\) under three different measuring angles 45°, 90°, and 180° to the plasma propagation axis [31], as shown in Fig. 2(d).

2.6. Measuring H2O2 density and acidity of the treated liquid
To evaluate the quantity of air plasma–produced H2O2 on a wet and dry treated surface, semiquantitative H2O2 test strips (QUANTOFIX Peroxide 1000; Macherey-Nagel GMbH & CO. KG, Germany) with 15 ×
18 mm² area were used [37, 38, 39]. The dry strips were used in the concentration distribution of H₂O₂ generated in the gas phase, whereas the wet strips were used to detect the distribution of H₂O₂ produced by the interaction of the air plasma jet with water molecules on the surface of the test strips. These strips can be used to monitor H₂O₂ concentration in the range of 50–1000 ppm, where color reaction changes from white to brown. The wet test strips can be achieved by splashing 1 cm³ of deionized (DI) water on the test strips. The plasma head was located 0.5 cm above the surface of the test strips. The air plasma jet can weakly acidify a liquid solution, when interacting, as a result of the production of nitrous acid (HNO₂) and nitric acid (HNO₃) [18]. The acidity of 1 cm³ of DI water after air plasma jet exposure was evaluated by LAQUAtwin compact pH meter pH-11 (HORIBA, Ltd., Japan).

2.7. Bactericidal effects on S. aureus, P. aeruginosa, and MRSA

To assess the bactericidal effects of the developed atmospheric air plasma jet on common bacteria complicating chronic wound healing, S. aureus (TISTR 2329) and P. aeruginosa (TISTR 2370) from Thailand Institute of Scientific and Technology Research (TISTR, Thailand) and MRSA (ATCC 33591) from American Type Culture Collection (USA) grown on agar culture media were treated [40, 41]. For biological studies, the jet was sustained by a DC pulse in a burst mode with PW = 1, PD = 12, BRR = 2, and gas flow rate = 4 L/min. In addition, the nozzle was fixed at the center of the agar plate and 0.5 cm above the surface, while the number of pulses and treatment time were varied. The experiments were performed at room temperature (25°C) and approximately 60% RH.

3. Results and discussion

3.1. Pulse-modulation cold air plasma and its radicals

Fig. 3 shows the V–I characteristics of the air plasma jet generated in a burst mode with the following pulse-modulation factors: PW = 1, PD = 12, NP = 5, and BRR = 2. Fig. 3(a) shows the profile of open-circuit voltage from an HV transformer with 5 pulses in a burst, which was used to generate the air plasma jet. When the applied electrical potential on the couple of plasma generator electrodes reached 2.52 kV of air breakdown voltage (Vb), the transient spark discharge [42] occurred. The discharge generated a high DC pulse that reached 3.5 A with approximately 10 ns full width at half-maximum, as shown in Fig. 3(b). When the filamentary transient spark discharge is formed, the electric potential across the discharge gap drops to almost zero. This drastic change is due to the series of 1.5 kΩ internal resistance of the HV transformer [43], which limits the current through a discharge channel. The transition to thermal spark or arc discharge is prevented by this self-pulsing feature.
During the pulse-off time, negative voltage was observed because of the back electromotive force, but the reversed current was limited. Because of gas preheating and memory effect created by the previous discharge [44], the breakdown voltage of the next potential pulses is relatively lower, ranging from 1.25 to 1.5 kV. Similarly, the discharge current pulses are broader and smaller, ranging from 0.25 to 0.75 A (as presented in Fig. 3c). In addition, some broad delay ripples are also observed. This could be due to the internal snubber circuit. A photo of the air plasma jet generated in a burst mode with PW = 1, PD = 12, NP = 10, and BRR = 2. The air plasma dissipated power as a function of NP and BRR is presented in Fig. 4(b). Thanks to the self-pulsing discharge mode and low dissipated power, thermalization of the developed air plasma could be avoided.

The electricity power dissipated in the air plasma for 5 pulses in a burst is shown in Fig. 4(a). In the first discharge pulse, a peak power of 4.8 kW was reached, and the corresponding energy dissipation was 56 μJ. During the pulse-off time, no power pulses were observed. Because of the gas preheating and accumulated excited metastable species—e.g., O, O₂ (a¹Δg), and N₂ (A³Σ), which were produced mainly by the first pulse—the next four transient spark discharge pulses could be generated using lower electrical power [44, 45]. However, the width of the latter four discharge pulses was observed to be broader than that of the first pulse. The power deposited in the second to fifth discharge pulses ranged from 0.24 to 0.49 W corresponding to energy deposition from 21 to 30 μJ, respectively. The total dissipated power in a burst of 5 pulses was approximately 169 μJ and the average power for BRR = 2 was 0.32 W. The air plasma dissipated power as a function of NP and BRR is presented in Fig. 3(d). Thanks to the self-pulsing discharge mode and low dissipated power, thermalization of the developed air plasma could be avoided.

**Fig. 11.** (a) The measured voltage pulse from human body impedance model provided in Fig. 2(c) with NP = 10. (b) The calculated patient leakage current with different NP. The experimental parameters were PW = 1, PD = 12, and BRR = 2 and measured at 1 and 5 mm from the nozzle tip. NP, number of pulses in a burst; PW, pulse width; PD, pulse delay time; BRR, burst repetition time.

**Fig. 12.** Ozone concentration at different positions around the air plasma source. The air plasma jet was generated with a condition: PW = 1, PD = 12, NP = 10, and BRR = 2. PW, pulse width; PD, pulse delay time; NP, number of pulses in a burst; BRR, burst repetition rate.

**Fig. 13.** The H₂O₂ concentrations on peroxide test strips increased following exposure time and NP. The wet test strips were exposed to the plasma plume with the nozzle fixed at 0.5 cm above the strips. The air plasma jets were generated with fixed parameters: PW = 1, PD = 12, and BRR = 2. The different conditions were (a) NP = 5, exposure time (t) = 30 s; (b) NP = 5, t = 60 s; (c) NP = 10, t = 30 s; and (d) NP = 10, t = 60 s H₂O₂, hydrogen peroxide; NP, number of pulses in a burst; PW, pulse width; PD, pulse delay time; BRR, burst repetition rate.
and then decreased to 18 μs of PD at 1 μs PW. Clearly, the optimized PD for reactive species production of this cold air plasma jet device is about 12 μs. The strong increase of atomic H and O as a function of higher NP is shown in Fig. 7(b). In addition, 1.5 μs PW shows a strong influence on the increase of atomic H and O of about 1.5–2.0 times for the case of 1.0 or 1.25 μs of PW, which was not significant difference on the production of H and O. Further investigation was observed with the strong increase of atomic O3 and NO as a function of higher NP (Fig. 8).

3.2. Device risk assessment

Fig. 9 presents the time-dependent maximum glass slide temperatures at different NP. The maximum plasma-treated glass temperature with NP = 10 was roughly 35°C. This means the maximum plasma temperature at NP = 10 of the developed air plasma jet was less than a threshold 40°C plasma temperature for biomedical applications. Beside the plasma temperature, the tissue heating is also a function of contact time [29]. In a practical application, the tissue damage due to overheating can be prevented by moving around the plasma jet over the treated surface.

The UV emission spectrum (200–400 nm) of the air plasma jet generated with PW = 1, PD = 12, NP = 10, and BRR = 2 is presented in Fig. 10. The most UV radiation generated by the air plasma jet was in the spectral range of UVB (280–315 nm) and UVA (315–400 nm), which emitted from the excited N2 and OH molecules [49]. The maximum effective UV power (~Euv) integrated with the ICNIRP relative weighting function S(λ) was 34 μW/cm² at a distance of 5 mm from the nozzle tip. The limiting UV treatment duration for the air plasma jet with the maximum effective UV power was around 90 s.

Fig. 11(a) presents an example of the measured voltage pulse from the equivalent circuit of human body impedance as shown in Fig. 2(c). The calculated patient leakage current of the developed air plasma jet as a function of D and NP is shown in Fig. 11(b). The leakage currents were mostly below the threshold of 10 μA and seemed independent of NP. Fig. 12 shows the O3 concentration measured at different distances and angles with respect to the air plasma jet axis. The high O3 concentration occurred near the plasma nozzle tip, and the maximum O3 concentration of the developed cold air plasma jet was 7.2 ppm at 0.5 cm of 180°. O3 concentration strongly decreased with increasing distance from the plasma jet nozzle tip and dropped to almost zero at 30 cm of all direction.

To summarize, four different investigations—plasma temperature, UV emission, patient leakage current, and O3 emission—were performed to assess the potential human risk of the developed air plasma jet. The results indicate that the temperatures of the air plasma jet were mostly less than the threshold of 40°C. The low plasma gas temperature was

| Bacteria | Exposure Time (s) |
|----------|------------------|
|          | Control | 10   | 20   | 30   | 40   | 50   | 60   |
| SA       |         |      |      |      |      |      |      |
| PA       |         |      |      |      |      |      |      |

Fig. 15. Effect of the developed cold air plasma jet on inactivation of *Staphylococcus aureus* and *Pseudomonas aeruginosa*. The bacteria were grown in nutrient broth prior to spreading on to agar plate. They were then exposed to the air plasma jet with the nozzle fixed at the center, 0.5 cm above the agar. The exposure was conducted for the indicated time period, and the bacteria were incubated at 37°C for 18–24 h before pictures were taken. The air plasma jet was generated under pulse-modulation condition: PW = 1, PD = 12, NP = 5, and BRR = 2. The plate diameter was 9 cm. PW, pulse width; PD, pulse delay time; NP, number of pulses in a burst; BRR, burst repetition time; SA, *Staphylococcus aureus*; PA, *Pseudomonas aeruginosa*.
caused by the self-pulsing discharge mode and low plasma dissipated power. The maximum effective UV power of the air plasma jet generated with the condition PW = 1, PD = 12, NP = 10, and BRR = 2 was 34 μW/cm², and the corresponding limiting exposure duration was around 1.5 min. In a practical application, the tissue damage due to overheating and excess UV radiant exposure of 3 mJ/cm² can be prevented by moving around the plasma jet over the wound area. Thus, there are very short plasma contact times at one and the same point, and a local spot treatment over several seconds would not exceed the thresholds. The calculated patient leakage currents were mostly below the threshold of 10 μA. The high O₃ concentrations were found near the plasma nozzle tip, and they decreased strongly with increasing distance from the plasma source exit nozzle. The gap of 30 cm was the minimum safe distance for the user to stay away from the plasma jet nozzle tip. For the air plasma jet generated with fixed parameters PW = 1, PD = 12, and BRR = 2, the plasma temperature, UV radiation power, and O₃ concentration could be reduced by decreasing NP.

### 3.3. Liquid chemistry and cell biology

Plasma-produced OH and H₂O₂ density on the treated surface is strongly dependent on the surface humidity [50]. An interaction of the air plasma jet with water molecule can produce reactive oxygen and hydrogen species such as OH and H₂O₂ [51]. Thus, to investigate the production of H₂O₂ in gas phase, dry peroxide test strips were exposed to the air plasma plume, but no color change was detected from the strips. This result implied that H₂O₂ concentration in gas phase was less than 50 ppm (the minimum testing range of this test strip). Next, to investigate the production of H₂O₂ in liquid phase, the wet surface of the test strips was exposed to the air plasma jet, and the color changes of the peroxide test strips were recorded, as shown in Fig. 13. H₂O₂ concentrations in liquid phase increased as a function of NP and exposure time. The color-changing zones show that the active area of the test strips was larger than the diameter of the air plasma plume, which was around 1 mm, and that high H₂O₂ concentrations were at the centers of the affected areas and decreased along the radial distance. OH is a highly reactive radical with the oxidizing potential of 2.8 V, but its reactivity limits its lifetime. H₂O₂ is a more stable form of OH with a much longer lifetime [38]. Because of its lower oxidizing potential of 1.7 V, H₂O₂ can diffuse through a thin layer of water and also decompose to form a higher reactive OH radical [20]. Taken together, these implied that H₂O₂ was produced by an interaction of the long-lifetime plasma species especially O₃ with water molecule on the surface of the test strips [52] and the radial distribution of H₂O₂ concentrations was the effect of diffusion of O₃ from the center of the plasma plume.

The interaction of nitric oxide (NO) and nitrogen dioxide (NO₂) with water molecule leads to the formation of nitrite (NO₂⁻), nitrate (NO₃⁻), nitrous acid (HNO₂), and nitric acid (HNO₃) [53]. In Fig. 14, the pH of DI water decreased with the increasing exposure time. This indicated that NO₂ and NO₃ increased as a function of exposure time. These nitrite and nitrate can deconstruct to NO, which can play a crucial role in stimulating wound healing [18]. NO₂ in the acidified solution can also further react with plasma-produced H₂O₂ to form a strong oxidant peroxynitrite (ONOO⁻), which can damage both cell membrane and DNA of bacteria [54]. Furthermore, the air plasma-induced acidification of the treated surface with a parallel accumulation of nitrite and nitrate would help wound healing by controlling wound infections and increasing antimicrobial activities [18, 55].

The inactivation of Staphylococcus aureus and P. aeruginosa on agar plates is time dependent (Fig. 15). When these bacterial cells were exposed to the air plasma jet, their cell wall, plasma membrane, and intracellular component (e.g., DNA) could be damaged by the produced RONS [56]. The capability of the pulse-modulation cold air plasma jet on MRSA inactivation is shown in Fig. 16. This figure also affirms that the bacterial inactivation effects are dependent on NP and plasma exposure time. Fig. 17 indicates the time-dependent bactericidal area of MRSA on agar
surface. When the air plasma jet was treated to the bacteria, the cells were covered by a thin layer of liquid or were on agar media; both contained a sufficient amount of water molecules to interact with the released active species [20]. For this developed plasma jet, the interaction of relatively long-lifetime species such as O, O₃, and O₂ (ΔΩ) in the plasma plume with water molecules in liquid or agar media leads to the formation of OH radical [20, 57, 58], which has nonselective strong oxidizing properties. When considering the effects of exposure time on the area of bacterial inactivation, it might be explained by the spatial distribution on the agar surface of the plasma-produced long-lifetime species such as O, O₃, and O₂ because of diffusion–convection transport [50, 59, 60]. However, the study of the spatial distribution of each species is beyond the scope of this article.

4. Conclusions

The developed compact air plasma jet had pulse parameters—NP, PW, PD, and BRR—that can be modulated to control the dissipated power, plasma temperature, UV concentration, and patient leakage current of the air plasma jet to be within a level suitable for medical applications. The developed air plasma jet can produce a controllable amount of NO, OH, and O₂. By fixing factors on pulse modulation, the plasma source can be optimized for RONS generation. The interaction between the produced active species with the surrounding H₂O molecule led to the production of H₂O₂, NO₂, NO₃, HNO₂, and HNO₃ in liquid phase of the media, such as DI water. Furthermore, the bactericidal effects of the developed air plasma jet on S. aureus, P. aeruginosa, and MRSA were efficient and controllably time dependent.

Declarations

Author contribution statement

Phuthidhorn Thana: Conceived and designed the experiments; Performed the experiments; Analyzed and interpreted the data; Wrote the paper.

Apiwat Wijaikhum, Chakkraong Kuensaen: Analyzed and interpreted the data; Wrote the paper.

Pipath Poramapijitwat: Performed the experiments.

Jomkhwan Meerak, Athipong Ngamjarurojana: Contributed reagents, materials, analysis tools or data.

Suruepon Sarapirom: Conceived and designed the experiments; Analyzed and interpreted the data; Contributed reagents, materials, analysis tools or data.

Theerawan Boonyawan: Conceived and designed the experiments; Contributed reagents, materials, analysis tools or data; Wrote the paper.

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Competing interest statement

The authors declare no conflict of interest.

Additional information

No additional information is available for this paper.

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