In this analysis, we introduced heat convective aspects of stagnation point movement of a magnetohydrodynamic (MHD) stream on a nonlinear oscillating plane with the impacts of velocity and heat slips with variable heat reservoir. By using some appropriate transformations, the governing differential equations are switched into an ordinary differential equation. The semi-analytical technique called Homotopy Analysis Method (HAM) has been applied to evaluate the ordinary differential equations. For convergence achievement, a numerical method BVPh2-midpoint method is also applied and an outstanding agreement is found. The impacts of the governing constraints on flow, motion, and temperature distributions are investigated in detail. We observed that the temperature distribution increases with nonlinear heat reservoir parameter. Our results, in some limiting situations, matched well with previously published results, which approve that our obtained results are correct.

1. Introduction

It is, to some extent, understood that the present generation depends on the achievements of physical sciences which are based on production industries. Magnetohydrodynamics (MHD) boundary-layer flow on an elongating surface is important because of its frequent uses in industrial engineering and various production processes such as the aerodynamic squeezing of polymers, rolling at high temperature, cooling control technology, and glass fiber production. The magnetohydrodynamics can display certain characteristics in heat conductivity as it has both fluid as well as magnetic features. Raju et al. [1] investigated an extensive study of the least squares finite element method over a varying boundary layer explored the stagnation flow. Gorla [2] studied a viscoelastic (a nonclassical) liquid of stagnation movement in pulsating magnetic field. Gorla concluded that the shear stress coefficients are directly proportional to the magnetic field. Takhar et al. [3] investigated magnetohydrodynamic nonlinear stagnation point interface movement. Besser et al. [4] presented a technique of annihilating the magnetic field in the limit of MHD equations for a noncompressible ionized fluid having constant viscosity and resistivity as exchange parameters. Massoudi and Ramezan...
examined the heat convective features of fluid (i.e., viscoelastic) at stagnation point flow. Ariel [6] studied multidirectional stagnation point movement of viscoelastic material. Mahapatra and Gupta [7] derived an exactly matched solution of Navier–Stokes equations which characterizes a uniform axisymmetric stagnation point flux towards an elongating surface. It is observed that the flow shows a boundary-layer arrangement when the velocity of the elongating sheet is smaller than the free stream velocity and a counter boundary layer is made when the starching sheet velocity is greater than the free stream velocity. Abel et al. [8] studied the influence of varying temperature source on magnetohydrodynamics heat convection in the fluid thin layer on a nonuniform elongating surface.

Yazdi et al. [9] evaluated the magnetohydrodynamics slip streaming on the nonuniform porous elongating sheet in the existence of a chemical process. The slip stream takes place if the distinctive size of flow regime is much smaller or the flow pressure is weak. Hsiao [10] has worked on an incompressible uniform MHD stagnation point movement of a second-order viscoelastic liquid and thermal conduction caused by a flow oscillating surface, and it is observed that viscoelastic liquid flow thermal effect is better than nonviscoelastic liquid flow thermal effect. Rasheed et al. [11] analyzed numerical and analytical investigation of thin-film nanofluid flow over an angular surface. Roşca et al. [12] analyzed numerical and analytical investigation of thin-film nanofluid in rotating channels with heat source. Khan et al. [20–25] discussed the impact of various non-Newtonian fluid materials for wire coating analysis in the existence of an unsteady heat reservoir as a result of the moving sheet. In this analysis, we studied the said constraints on flow and heat transfer.

2. Mathematical Formulation

Figure 1 demonstrates physical configuration of the considered problem. Here, we measured two-dimensional steady, flow, and transfer of heat analysis in case of an incompressible fluid in the occurrence of transverse magnetic field strength $B(x)$ affected normally on flow moment which give us a unique form given as follows:

$$B(x) = B_0 x^{(n-1)/2}, \quad B_0 \neq 0,$$  \hspace{1cm} (1)

where $n$ is a constant and $x$ is a coordinate along the plate measured from the leading edge. The plate is moving inside or outside the origin with the velocity $u(x) = ax^n$ in an exterior (in viscid) flow of the velocity $u_0 = ax^n$, where $u$ and $v$ are the corresponding velocity components in the $x$ and $y$ directions, respectively. Here, $T(x)$ is assumed as a temperature of the plate and ambient fluid is $T_\infty$, which is the constant temperature. The governing equations of continuity, momentum, and energy equations are as follows:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0,$$  \hspace{1cm} (2)

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \mu \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial y^2} - \frac{\sigma B^2(x)}{\rho} u,$$  \hspace{1cm} (3)

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial y^2} + \frac{q'''}{\rho c_p},$$  \hspace{1cm} (4)

where $\rho$ is the conductivity (electrical) of the fluid, $\alpha$ is the thermal diffusivity constant, and $u$ and $v$ are velocity components in the $xy$-plane, respectively.

The initial and boundary conditions are as follows:

$$u = v, \quad T = T_\infty, \quad \text{for any } x, y$$

$$v = 0, \quad u = ax^n + N_1 \frac{\partial u}{\partial y}, \quad T = T_0 + S_1 \frac{\partial T}{\partial y},$$

at $y = 0, \quad u = \mu_c(x) ax^n$

$$T \rightarrow T_\infty, \quad \text{as } y \rightarrow \infty$$
We guess the velocity slip factor $N_1$ and the temperature slip factor $S_1$ change with $x$ in the form $N_1 = N x^{(1-n)/2}$ and $S_1 = S x^{(1-n)/2}$, respectively, where $N$ and $S$ are positive slip constants. Furthermore, it is expected that surface temperature $T_W(x) = T_{co} + T_0 x^p$, where $T_0$ is the characteristics temperature parameter and $P$ is the wall temperature parameter. It is concluded from $N_1 = N x^{(1-n)/2}$ and $S_1 = S x^{(1-n)/2}$ against physical point of view, $n$ should vary in the range $0 \leq n \leq 1$. If $n > 1$, then $N_1$ and $S_1$ become singular at $x$ close to the leading edge of the plate. It is remembered that the boundary layer does not start at $x = 0$ but starts in the vicinity of the leading edge of the plate [33].

Therefore, the solution for $n > 1$ is realizable from the mathematical point of view. $C_p$ is the specific heat at constant pressure, $\sigma$ is the electrical conductivity, $B_0$ is the applied magnetic field, $\mu$ is the viscosity, $T$ is the temperature, $k$ is the thermal conductivity of the fluid, and $q'''''$ is the rate of nonuniform heat generation/absorption coefficient and defined as

$$q''''' = \left( \frac{k u_w(x)}{x v} \right) \left[ A^* (T_W - T_{co}) f' + B^* (T - T_{co}) \right],$$

where $A^*$ and $B^*$ are the conditions of space- and temperature-dependent heat generation/absorption, respectively. We notice that $A^* > 0$ and $B^* > 0$ for the internal thermal generation and $A^* < 0$ and $B^* < 0$ for the internal thermal absorption [28].

3. Transformation of PDEs into ODEs

Using self-similar solution by means of the similarity function $f$, define

$$u = a x^n f' (\eta),$$

$$v = -\frac{a v (n+1)}{2} x^{(n-1)/2} \left[ f (\eta) + \frac{n-1}{n+1} \eta f' (\eta) \right].$$

Evaluating equations (2)–(4) with the help of the boundary conditions given in (5) and using the similarity transformation techniques,

$$\psi = \sqrt{\frac{2av}{n+1}} x^{((n+1)/2) f (\eta)},$$

$$\theta (\eta) = \frac{T - T_{co}}{T_{co} - T_w},$$

$$\eta = \sqrt{\frac{a (n+1)}{2} x^{((n-1)/2) y}},$$

where $\psi$ denotes stream function, defined by $u = (\partial \psi / \partial y)$ and $v = -(\partial \psi / \partial x)$, and $\nu = \mu / \rho$ denotes kinematic viscosity. The governing partial differential equations (PDEs) given in equations (3) and (4) are transferred into ordinary differential equations. By using equations (6)–(8) in equations (2)–(4), we acquire a set of ordinary differential equations given below:

$$f'''' + f f'''' + \left( \frac{2n}{n+1} \right) \left[ 1 + (f')^2 \right] - M_n f' = 0,$$

$$\frac{1}{Pr} \theta'''' + f \theta' - \left( \frac{2n}{n+1} \right) f' \theta + \left( \frac{2n}{n+1} \right) \frac{1}{Pr} \left( A^* f' + B^* \theta \right) = 0,$$

where $Pr = (\nu / \alpha)$ denotes the Prandtl number, and the transferred boundary conditions given in equation (5) takes the form

$$f (0) = 0, \quad f' (0) = \lambda + \beta f'''' (0), \quad f''' (\infty) = 1,$$

$$\theta (0) = 1 + \sigma \theta' (0), \quad \theta (\infty) = 0,$$

where $\lambda = (c / a)$ is the moving parameter with $\lambda > 0$ corresponding to downstream movement of the plate from the origin, while $\lambda < 0$ corresponding to the moving of the plate into the origin $\beta = N \sqrt{(av (n+1)/2) / a}$ is the velocity slip parameter and $\sigma = S \sqrt{(a (n+1)/2)}$ denotes the temperature slip parameter. It is worth noticing when $n = 1$ (stagnation point flow), $p = 0$ (isothermal plate), and $\beta = \lambda = \sigma = 0$, equations (9) and (10) along with the boundary conditions (11) become identical for $m = 1$ (stagnation point flow and heat transfer) [34].

Physical quantities for local skin-friction coefficient $C_f$ and local Nusselt number $Nu_x$ in this problem are defined as

$$C_f = \frac{\tau_w}{\rho U_w^2 (x)},$$

$$Nu_x = \frac{q_w x}{k (T_w - T_{co})},$$

where skin friction (shear stress) along the plate is $\tau_w$, and wall heat $q_w$ is given by

$$\tau_w = \mu \left( \frac{\partial u}{\partial y} \right),$$

$$q_w = -k \left( \frac{\partial T}{\partial y} \right)_{y=0}.$$
\[ \sqrt{\text{Re}_x C_f} = \frac{n+1}{2} f''(0), \]
\[ \text{Re}_x^{(1/2)} \text{Nu}_x = \frac{n+1}{2} \left[ -\theta'(0) \right], \]
where \( \text{Re}_x = \frac{u_e(x)x}{\nu} \) denotes the Reynolds number.

### 4. Solution by HAM (Homotopy Analysis Method)

The governing nonlinear partial differential equations (3) and (4) are converted into nonlinear ordinary differential equations (9) and (10). To find the solutions of equations (9) and (10), five boundary conditions are required: three on equation of motion and two on equations of temperature, respectively. But here \( f''(\eta) \) and \( \theta'(\eta) \) are missing boundary conditions; hence, solving the boundary value problem of equations (9) and (10) is difficult. Therefore, in the boundary conditions given in equation (11) we replace infinity to the finite value. Equations (9) and (10) with boundary condition (11) are solved analytically by HAM and numerical by BVPh2-midpoint methods. The optimal HAM [35–37] gives better results compared with perturbation techniques and other conventional investigative techniques. Firstly, the optimal HAM gives us a remarkable flexibility to pick the equation type of linear subproblems. Secondly, the optimal HAM works regardless of the possibility that there does not exist any small/large physical parameter in determining equations and boundary/initial conditions. Particularly, unlike perturbation and other analytic techniques, the optimal HAM gives us an advantageous approach to guarantee the convergence of a series solution by presenting the supposed convergence control parameter into the series solution.

### 5. Convergence of the Optimal HAM Method

The auxiliary parameters \( f \) and \( \theta \) have a leading purpose of controlling the convergence of homotopic solutions. To get convergent solutions, we take the suggested values of these parameters. For this reason, residual errors are noticed for the momentum, and thermal energy equations by initiating the expressions are given as

\[ \Delta^f_m = \int_0^1 \left[ R_m^f(\xi, h_f) \right]^2 d\xi, \]
\[ \Delta^\theta_m = \int_0^1 \left[ R_m^\theta(\xi, h_\theta) \right]^2 d\xi. \]

The convergence of the parametric values computed through optimal HAM is listed in Table 1 using the values of the parameters \( \beta = 1.2, \lambda = 0.5, \text{Pr} = 2.0, \phi = 0.1 \), and \( \gamma = 0.1 \), while the error decay for 10th-order approximation is shown in Figure 2.

Here, \( \Delta^f_m + \Delta^\theta_m \) denotes the total discrete square residual error which is used to obtained optimal convergence control parameters.

### 6. Comparison of HAM/Numerical and Published Work

Table 2 shows the comparison of HAM, BVPh2-midpoint method, and published work reported by Bejan [34], and good agreement has been found.

### 7. Discussion on Results

In this paper, an analysis is introduced to investigate magnetohydrodynamic slip flow and thermal convection of the stagnate point of an elongating surface along with nonuniform oscillating plane along a free flow. The momentum and heat convection equations for the nearest neighbor layer of interface have been explained analytically and derived for various analytical equations for temperature profile. The outcomes of the semianalytical computations are displayed in different figures. The characteristic parameters which are investigated in this paper are power-law index \( n \), boundary-layer temperature \( P \), Prandtl number \( \text{Pr} \), magnetic field parameter \( M \), and spatial dependent heat reservoir parameters \( A^* \) and \( B^* \), respectively. We now continue to discuss the results. Figures 3 and 4 demonstrate the stream velocity profiles for the various values of \( \lambda \) (oscillating parameter) and \( \beta \) (velocity slip parameter), respectively. It has been observed that the rising of \( \lambda \) and \( \beta \) causes reduction in the width of the boundary-layer movement.

Figure 5 describes velocity and flow profiles of various input of power index variable \( n \) while the other parameters are kept fixed. It is observed that rising the power index variable, the stream movement and velocity rise, which cause an increment in the width of the momentum boundary wall layer. Figure 6 exhibits the velocity sketch for various input
of $M$. From here, it is detected that velocity along with the boundary-layer thickness reduces when $M$ is increased. This may be due to the application of electromagnetic force (Lorentz force).

Figures 7 and 8 depict the velocity profiles for the various inputs of $\lambda$ and $\beta$. In these figures, we can see that as the value of $\lambda$ advances, the thickness of velocity increases but we observed a reverse result when the velocity slip parameter $\beta$ increases. Figures 9 and 10 show the skin-friction profile for different values of $\lambda$ and $\beta$. In these profiles, it is clear that the
width of the skin-friction of boundary wall layer grows wider as the values of parameter \( \lambda \) increase and shrink with rising of the velocity slip flow parameter \( \beta \).

Figures 11 and 12 illustrate the temperature profile for various input values of power index \( n \) and some other physical variables which reveals that the thickness of the thermal-conducting boundary layer decreases with increasing the nonlinear stretching parameter \( n \). Because of electromagnetic (Lorentz) force, the thickness of the heat convective boundary layer increases as the magnetic field strength increases; henceforth, Figure 13 is sketched for the temperature dependence upon the magnetic field.

Figures 14 and 15 show the temperature profiles for different inputs of \( \Pr \). These figures illustrate that, on increasing the Prandtl number \( \Pr \), the thickness of the thermal-conducting boundary layer decreases; hence, the temperature decreases.

Temperature profile for numerous values of position-dependent heat reservoir parameter \( A^* \) and temperature-dependent heat reservoir parameter \( B^* \), respectively, is shown in Figures 16 and 17, respectively, while the wall temperature profile is given in Figure 18 which illustrates that the temperature on the boundary layer decreases as a result of rising the power index \( p \).

Figures 19 and 20 show temperature profile for the various input values of oscillating and velocity slip
parameters $\lambda$ and $\beta$, respectively. It is observed that, by increasing both $\lambda$ and $\beta$ parameters, the thickness of the thermal boundary layer increases.

Figures 21–23 represent the gradient of temperature sketch for different inputs of physical constrains like oscillating, temperature, and velocity slip parameters, respectively. The influence of this physical parameter is observed as the temperature profile increases with the
increasing value of the oscillating and velocity slip parameters, respectively, and the temperature gradient drops when the temperature slip parameter rises.

8. Conclusions

In this review, we have attempted to provide a glimpse of what we have studied from the stagnate point magnetohydrodynamic flow movement and thermal convection in the presence of velocity slip, thermal slip, and nonlinear heat reservoir. We deduced some significant observations from these results given as follows:

(i) By rising the power index, the velocity parameter rises, while in existence of magnetic field, a converse result is observed.

(ii) Whether magnetic field exists or not, the velocity rises by increasing the power-law index.

(iii) If the magnetic field value is zero, the temperature rises as the power index increases while falls when magnetic field is nonzero.

(iv) As the Prandtl number increases, the temperature falls irrespective of the magnetic field.

(v) In presence of uniform magnetic field, the temperature falls down as the parameters $A^*$, $B^*$, and $p$ increase. Also, the temperature rises when there is a variable magnetic field.
(vi) The oscillating parameter $\lambda$ decreases flow movement, velocity, variation of temperature in normal direction, skin friction, and heat transfer boundary layer.

(vii) The velocity slip parameter increases the thermal boundary layer and gradient of temperature but decreases the flow movement, velocity (momentum), and skin friction of the boundary interface layer.

(viii) The temperature slip parameter impacts merely on thermal interface layers which decreases the heat-convective boundary layer and so as reduces the gradient of temperature.

**Nomenclature**

- $C_p$: Specific heat
- $Pr$: Prandtl number
- $T_{\infty}$: Free stream temperature
- $v$: Velocity along $y$-axis
- $A^*$: Space-dependent internal heat generation
- $C_f$: Friction coefficient
- $q_w$: Wall heat flux
- $T_0$: Characteristic temperature
- $x$: Distance along the plate
- $B^*$: Temperature-dependent internal heat absorption
- $f$: Dimensionless stream function
- $Re_x$: Local Reynolds number
- $T_w$: Wall temperature
- $y$: Distance normal to plate
- $P$: Wall temperature parameter
- $K$: Thermal conductivity
- $n$: Nonlinear stretching parameter
- $u$: Velocity along $x$-axis
- $q''$: Nonuniform heat source/sink
- $Mn$: Magnetic parameter
- $Nu_x$: Local Nusselt number
- $T_f$: Local fluid temperature
- $u_w$: Velocity at wall
- $B_0$: Applied magnetic field

**Greek Symbols**

- $\psi$: Stream function
- $\beta$: Velocity slip parameter
- $\lambda$: Thermal jump parameter
- $\sigma$: Temperature slip parameter
- $\alpha$: Thermal diffusivity
- $\eta$: Similarity variable
- $\mu$: Dynamical viscosity
- $\theta$: Dimensional temperature
- $\nu$: Kinematic viscosity
- $\rho$: Density.

**Data Availability**

The data used to support the findings of this study are available from the corresponding author upon request.

**Conflicts of Interest**

The authors declare that they have no conflicts of interest.

**Acknowledgments**

The authors extend their appreciation to the Deanship of Scientific Research at Majmaah University for funding this work under Project Number RGP-2019-3. This research was supported by Basic Science Research Program through the National Research Foundation of Korea (NRF) Funded by the Ministry of Education (NRF-2017R1D1A3B03028309) and the Soonchunhyang University Research Fund.

**References**

[1] K. K. Raju, N. Muthiyalu, and G. V. Rao, “Least square finite element solution of stagnation point flow,” *Complex and Fluids*, vol. 4, no. 3-4, pp. 143–147, 1976.

[2] R. S. R. Gorla, “Non-Newtonian fluid at a stagnation point in the presence of a transverse magnetic field,” *Mechanics Research Communications*, vol. 3, no. 1, pp. 1–6, 1976.

[3] H. S. Takhar, C. D. S. Devi, and G. Nath, “MHD unsteady incompressible three-dimensional asymmetric stagnation point boundary layers,” *Mechanics Research Communications*, vol. 14, no. 1, pp. 29–35, 1987.

[4] B. P. Besser, R. P. Rijnbeek, and H. K. Biernat, “Planar MHD stagnation point flows with velocity shear, planet,” *Planetary and Space Science*, vol. 38, no. 3, pp. 411–418, 1990.

[5] M. Massoudi and M. Ramezan, “Heat transfer analysis of a viscoelastic fluid at a stagnation point,” *Mechanics Research Communications*, vol. 19, no. 2, pp. 129–134, 1992.

[6] P. D. Ariel, “Three-dimensional stagnation point flow of a viscoelastic fluid,” *Mechanics Research Communications*, vol. 21, no. 4, pp. 389–396, 1994.

[7] T. R. Mahapatra and A. S. Gupta, “Stagnation point flow towards a stretching surface,” *Canadian Journal of Chemical Engineering*, vol. 81, pp. 258–263, 2003.

[8] M. S. Able, J. Tawade, and M. M. Nandepapanavar, “Effect of non-uniform heat source on MHD heat transfer in a liquid film over an unsteady stretching sheet,” *International Journal of Non-Linear Mechanics*, vol. 44, no. 9, pp. 990–998, 2009.

[9] M. H. Yazdi, S. Abdullah, and I. H. Sopian, “Slip MHD flow over permeable stretching surface with chemical reaction,” in *Proceedings of the 17th Australian Fluid Mechanics Conference*, Auckland, New Zealand, December 2010.

[10] K. L. Hsiao, “MHD stagnation point viscoelastic fluid flow and heat transfer on a thermal forming stretching sheet with viscous dissipation,” *The Canadian Journal of Chemical Engineering*, vol. 89, no. 5, pp. 1228–1235, 2011.

[11] H. Rasheed, Z. Khan, I. Khan, D. Ching, and K. Nisar, “Numerical and analytical investigation of an unsteady thin film nanofluid flow over an angular surface,” *Processes*, vol. 7, no. 8, p. 486, 2019.

[12] N. C. Roşca, A. V. Roşca, and I. Pop, “Stagnation point flow and heat transfer over a non-linearly moving flat plate in a parallel free stream with slip,” *Communications in Nonlinear Science and Numerical Simulation*, vol. 19, no. 6, pp. 1822–1835, 2014.

[13] H. Dessie and N. Kishan, “MHD effects on heat transfer over stretching sheet embedded in porous medium with variable viscosity viscous dissipation and heat source/sink,” *Ain Shams Engineering Journal*, vol. 5, no. 3, pp. 967–977, 2014.
[14] H. U. Rasheed, Z. Khan, S. Islam, I. Khan, J. L. G. Guirao, and W. Khan, "Investigation of two-dimensional viscoelastic fluid with nonuniform heat generation over permeable stretching sheet with slip condition," *Complexity*, vol. 2019, Article ID 3121896, 8 pages, 2019.

[15] H. S. Hassan, "Symmetry analysis for MHD viscous flow and heat transfer over a stretching sheet," *Applied Mathematics*, vol. 6, no. 1, pp. 78–94, 2015.

[16] M. Shen, F. Wang, and H. Chen, "MHD mixed convection slip flow near a stagnation point on a non-linearly vertical stretching sheet," *Boundary Value Problems*, vol. 2015, p. 78, 2015.

[17] I. Khan, W. A. Khan, H. Ur Rasheed, I. Khan, and M. N. Siddalingappa, "Second order slip flow and heat transfer over a stretching sheet with non-linear Navier boundary condition," *International Journal of Thermal Sciences*, vol. 58, pp. 143–150, 2012.

[18] Z. Khan, H. U. Rasheed, I. Tlili, I. Khan, and T. Abbas, "Runge-Kutta 4th-order method analysis for viscoelastic Oldroyd 8-constant fluid used as coating material for wire with temperature dependent viscosity," *Scientific Reports*, vol. 8, no. 1, p. 14504, 2018.

[19] Z. Khan, H. U. Rasheed, I. Tlili, I. Khan, and T. Abbas, "Numerical simulation of double-layer optical fiber coating using Oldroyd 8-constant fluid as a coating material," *Optical Engineering*, vol. 57, no. 7. Article ID 076104, 2018.

[20] Z. Khan, H. U. Rasheed, I. Tlili, I. Khan, and T. Abbas, "Effect of magnetic field and heat source on upper-convected-maxwell fluid in a porous channel," *Journal of Coatings Technology and Research*, vol. 16, no. 19, p. 3074, 2019.

[21] Z. Khan, H. U. Rasheed, I. Tlili, I. Khan, and T. Abbas, "Shooting method analysis in wire coating withdrawing from a bath of Oldroyd 8-constant fluid with temperature dependent viscosity," *Open Physics*, vol. 16, no. 1, pp. 956–966, 2018.

[22] Z. Khan, H. U. Rasheed, I. Tlili, I. Khan, and T. Abbas, "Analytical and numerical solutions of Oldroyd 8-constant fluid in double-layer optical fiber coating," *Journal of Coatings Technology and Research*, vol. 16, no. 1, pp. 235–248, 2018.