Slot-die coating large-area formamidinium-cesium perovskite film for efficient and stable parallel solar module

Zhichun Yang1†, Wenzun Zhang1,†, Shaohang Wu1,3,†, Hongmei Zhu1†, Zonghao Liu1†, Zhiyang Liu1, Zhaoyi Jiang1, Rui Chen1, Jing Zhou1, Qian Lu1, Zewen Xiao1, Lei Shi1, Han Chen4, Luis K. Ono5, Shasha Zhang6, Yiqiang Zhang6, Yabing Qi5, Liyuan Han4*, Wei Chen1

Perovskite solar cells have emerged as one of the most promising thin-film photovoltaic (PV) technologies and have made a strong debut in the PV field. However, they still face difficulties with up-scaling to module-level devices and long-term stability issue. Here, we report the use of a room-temperature nonvolatile Lewis base additive, diphenyl sulfoxide (DPSO), in formamidinium-cesium (FACs) perovskite precursor solution to enhance the nucleation barrier and stabilize the wet precursor film for the scalable fabrication of uniform, large-area FACs perovskite films. With a parallel-interconnected module design, the resultant solar module realized a certified quasi-stabilized efficiency of 16.63% with an active area of 20.77 cm². The encapsulated modules maintained 97 and 95% of their initial efficiencies after 10,000 and 1187 hours under day/night cycling and 1-sun equivalent white-light light-emitting diode array illumination with maximum power point tracking at 50°C, respectively.

INTRODUCTION

Perovskite solar cells (PSCs) have attracted considerable interest in both research and industrial fields on account of their skyrocketing efficiency, ease of fabrication, and cost-effectiveness. Currently, the biggest challenges hampering the commercialization of this emerging photovoltaic (PV) technology are the scale-up of PSCs to module level without notable efficiency loss and affording their long-term stability (1, 2).

To fabricate high-efficiency perovskite solar modules (PSMs), it is essential to deposit uniform and high-quality perovskite films with full coverage over large scale (3). Up to now, the scalable deposition methods, such as spray coating (4), electrochemical deposition (5), soft-cover deposition (6), inkjet printing (7), doctor blading (8, 9), slot-die coating (10, 11), hybrid chemical vapor deposition (12), and vacuum evaporation (13), have been used to fabricate large-area perovskite films for PSMs. Among these methods, the solution ink-based coating methods are superior thanks to their compatibility with continuous industrial production line processing, low equipment requirements, and low manufacturing cost. Many efforts have been made to use solution-based scalable methods to coat large-area CH3NH3PbI3 (MAPbI3) films for modules and achieved impressive device performance (8, 9, 12, 14). However, the volatile properties and thermal decomposition of methylammonium (MA) cations limit the device’s long-term stability (13).

Formamidinium-cesium (FACs) mixed-cations perovskites have been demonstrated to be promising to achieve dominant operational stability in small-size (<1 cm²) PSCs (15, 16). It is thus desirable to construct highly efficient and stable PSCs with FACs perovskites (17). However, the successful solution systems for scalable coating of MAPbI3 films are not completely compatible with FACs perovskites resulting from the different solvation characteristics of MAPbI3 and FACs perovskites (18) and their different crystallization kinetics (19). For example, a fraction of I− ions are usually substituted with Br− ions in FACs perovskites to stabilize the photoactive phase. This makes the nucleation and growth of FACs perovskites to be accelerated with the increasing Br content, which is likely due to the higher the diffusivity of Br− than I− in the solvent as a result of smaller ionic radius (20). These characteristics largely increase the difficulty and complexity for scalable solution coating of high-quality FACs perovskite films over large area (21). Galagan et al. (21) reported the use of roll-to-roll slot-die-coated FA0.85Cs0.15PbI2.85Br0.15 perovskite on a flexible polyethylene terephthalate/indium tin oxide substrate by the use of the nontoxic solvent of dimethyl sulfoxide/2-butoxyethanol, which is compatible with industrial manufacturing, and a moderate cell efficiency of 13.5% with an active area of 0.09 cm² was achieved. Guo et al. (22) developed a vacuum-assisted precrystallization strategy to produce dense and uniform FA0.95Cs0.05PbI3 films with high crystallinity with the help of adding 30% MACI, and they achieved a decent cell efficiency of 16.63% with an active area of 0.09 cm². Lim et al. (23) used D-bar coating to deposit a large-area (FAPbI3)0.875(CsPbBr3)0.125 film by adding MACI as well as hexamethylphosphoramide Lewis base additive in perovskite/N,N′-dimethylformamide (DMF) solution, and the as-fabricated n-i-p mini-module achieved an efficiency of 17.01% with an active area of 18.66 cm². Nevertheless, so far, the reported strategies for the successful fabrication of FACs perovskite films over large area are very limited, and a credible third-party certification of the associated large-area devices’ efficiencies is also lacking.

Similar to other PV technologies, the module design of PSMs plays an important role in charge collection, device performance, as
well as device stability (24). To date, most of the reported PSMs are based on the series-connection design, which consists of subcells interconnected through P1-P2-P3 etched lines (I). In such a design, the metal electrodes are in direct contact with the perovskite at the P2 channels, which causes potential concerns for the long-term stability of PSMs due to the possible reaction of the perovskite with the metals (I, 25). An ingenious solution is to adopt a parallel-interconnected module design that does not have these P1-P2-P3 interconnections and avoids direct contact of the metal electrode/grid with the perovskite to favor the long-term stability. In addition, the parallel PSMs with a low-voltage/high-current feature are well matched with silicon solar cells, which is beneficial for their potential application in perovskite/silicon tandem solar modules. Given that perovskite/silicon tandem solar modules have become an important direction of industrial development (26), it is of specific importance to evaluate the operational stability of the parallel PSMs at the present stage.

In this work, we introduce a room-temperature nonvolatile Lewis base additive with strong coordination capability, i.e., diphenyl sulfoxide (DPSO), into FA_{0.83}Cs_{0.17}Pb_{1.83}Br_{0.17} precursor solution for coating large-area perovskite films and assemble them into parallel-interconnected solar modules. DPSO is demonstrated to impressively enlarge the nucleation energy barrier, effectively retard the natural nucleation of perovskite during the slot-die coating process, and stabilize the wet precursor film. Coupled with less toxic antisolvent n-hexane extraction, high-quality FA_{0.83}Cs_{0.17}Pb_{1.83}Br_{0.17} perovskite films with a size over 200 cm² are produced with high reproducibility. As a result, our p-i-n-structured PSMs with the parallel design have realized a certified quasi-stabilized efficiency of 16.63% with an active area of 20.77 cm², which is the highest for parallel-designed PSMs to date. With a nonpermeable electrode barrier design, the encapsulated parallel PSMs show remarkable operational stabilities, retaining 97% of the initial efficiency after 10,000 hours under day/night cycling and 95% of the initial efficiency under continuous light illumination with maximum power point (MPP) tracking at 50°C for 1187 hours.

**RESULTS**

**Slot-die coating large-area FACs perovskite films**

Here, a MA-free perovskite with the composition of FA_{0.83}Cs_{0.17}Pb_{1.83}Br_{0.17} is used as the light absorber (16, 27). To fabricate large-area perovskite films, the perovskite precursor ink is first coated on a substrate to form a wet film via slot-die coating (fig. S1, A and B). Then, the obtained wet film is treated by antisolvent n-hexane bath extraction to form a solid-state intermediate film. After further thermal annealing, a fully crystallized perovskite film is formed.

We first used pure DMF and a mixture of DMF and N-methyl-2-pyrrolidinone (NMP) (denoted as DMF-NMP) as solvents to prepare FACs perovskite precursor solutions. A first visual inspection of the perovskite film in the pure DMF case (fig. S1C) shows a rough film with white precipitates and poor coverage. When DMF-NMP was used, the corresponding perovskite film showed improved morphology, but some rough areas with white precipitates are still observed (fig. S1C). From this comparison, it is found that the solvent volatilization time of the wet precursor film plays a critical role in determining the perovskite film morphology. To further improve the perovskite film quality, we introduce a room-temperature nonvolatile Lewis base DPSO (boiling temperature, 206°C to 208°C, 13 mmHg) into the DMF-NMP system that functions as an additive to modulate the perovskite nucleation/growth. The corresponding perovskite film showed notably improved film quality with a more uniform and mirror-like morphology than the other two cases (fig. S1C).

**Wet film stabilization**

In general, there are three stages during perovskite crystallization: (i) solution stage, (ii) nucleation and fast-growth stage, and (iii) slow-growth stage. The mechanism of nucleation and crystal growth in the film formation process can be explained by the LaMer theory (2, 28, 29). To reveal the role of DPSO in the perovskite nucleation and growth process, we studied its influence on the coated wet films stability. We first monitored the apparent evolution of the wet films fabricated from the above three solvent systems (DMF, precursor 1; DMF-NMP, precursor 2; and DMF-NMP-DPSO, precursor 3) by optical microscopy (Fig. 1A and movies S1 to S3). It is observed that the wet film stability of three precursors is gradually improved when DMF is replaced by DMF-NMP and DMF-NMP-DPSO, respectively. This observation indicates that the rapid natural supersaturation, uncontrollable nucleation, and grain growth processes in precursor 1 are retarded by the introduction of NMP or NMP-DPSO. The quantitative wet film stable times of three precursors were further evaluated by the absorbance intensity evolution of three precursor films as a function of time at the wavelength of 550 nm (Fig. 1B). With the introduction of DPSO, precursor 3 shows a wet film stable time of approximately 8 min, which is much longer than that of DMF (30 s) and DMF-NMP (100 s) cases. The largely extended wet film stable processing time enables a delicate control of the following antisolvent extraction and achievement of uniform and mirror-like perovskite films (14). Above results also imply that DPSO should show strong interaction with the chemical components within the precursor solution and affect the wet film stability as well as the perovskite nucleation and growth.

To further study the escape of solvent molecules from the wet films, thermogravimetric analysis (TGA) measurements of three precursor solutions based on DMF, DMF-NMP, and DMF-NMP-DPSO were performed (Fig. 1C). It is observed that the temperature ranges of the first weight loss stages for the three cases gradually shift to higher temperatures, i.e., DMF (31°C to 71°C), DMF-NMP (31°C to 98°C), and DMF-NMP-DPSO (31°C to 106°C). This observation clearly suggests that the removal of solvent from the wet films is suppressed when NMP and DPSO are used. In addition, the DMF-NMP-DPSO ink exhibits the slowest solvent evaporation speed among the solutions. This is likely due to the enhanced interaction of DPSO with the other species in the precursor solution. The perovskite precursor solution evaporation speed is retarded with the addition of DPSO, while we consider that the coordination effect of DPSO with perovskites may be much more important to inhibit the precursor crystallization rate than the reduction of solvent volatilization.

To further investigate the evolution of the chemical components in the wet films during their natural drying process, x-ray diffraction (XRD) measurements were also conducted. As shown in Fig. 1 (D to F), obvious XRD peaks at around 7.5° can be observed for all three cases, and they are likely assigned to CsBr-FAI-PbI₂-DMF [Pb_{3}I_{12}Br_{6} polymorphs], CsBr-FAI-PbI₂-DMF-NMP [Pb_{3}I_{12}Br_{6} polymorphs], and CsBr-FAI-PbI₂-DMF-NMP-DPSO [Pb_{3}I_{12}Br_{6} polymorphs], respectively (30, 31). The evolutions of XRD peak...
intensity for the three cases are also consistent with the above wet film stable time study. With the evaporation of the solvent molecules, lead polyhalide colloids serve as nucleation centers, and the nucleation and subsequent crystal growth starts when the precursor concentration reaches the minimum supersaturated concentration limit, leading to the formation of CsBr-FAI-PbI₂-S complexes (S represents generic solvent or additive molecules). Together, the above results confirm that the natural nucleation process has been successfully suppressed when DMF-NMP-DPSO is used to form a much more stable wet film, which facilitates the subsequent controllable nucleation for high-quality perovskite films when followed by the subsequent antisolvent extraction step.

It has been widely revealed that the perovskite solution is a cluster-containing solution rather than a real solution (32). The colloidal distribution within the perovskite precursor solution considerably affects the subsequent perovskite nucleation and growth progress (33). To study the colloidal properties within the precursor solutions, we measured dynamic light scattering (DLS) spectra of the three precursor solutions. As shown in Fig. 1G, the colloid size is gradually reduced with the sequential introduction of NMP and DPSO compared with the pure DMF case, which is probably a result of the interaction of NMP and DPSO with the colloids (34, 35). In terms of the dependence of the Gibbs free energy change on cluster size (33, 36), we propose that the smaller cluster size implies a higher Gibbs free energy barrier for the formation of the crystal nucleus (fig. S2). Thus, the DMF-NMP-DPSO–based solution shows a higher nucleation barrier than the DMF and DMF-NMP cases. This is also the reason for the much slower nucleation and the longer wet film stable time, as observed in Fig. 1 (A and B) and movies S1 to S3.

To further reveal the underlying mechanism for the improved wet film stability and slower perovskite nucleation when DPSO is used, the interaction of DPSO with the chemical components within the precursor solution is studied. As DPSO is a Lewis base, which has been used as a ligand to interact with Sn⁴⁺ or other metal ions (37), we first consider its interaction with Pb²⁺ due to the Lewis acid base interaction. In the solution, DPSO molecules could act as ligands coordinating to the Pb²⁺ ions, competing with other ligands such as I⁻, DMF, and NMP in the precursor solutions. This interaction is

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Fig. 1. Precursor ink engineering to stabilize the wet film. (A) Semi–in situ observation of perovskite precursor film morphology evolutions over time with an optical microscope (scale bar, 100 μm). The perovskite precursors dissolved in DMF, DMF-NMP, and DMF-NMP-DPSO are denoted as precursors 1, 2, and 3, respectively. (B) Optical absorbance evolution of perovskite precursor films as a function of time at the wavelength of 550 nm. a.u., arbitrary units. (C) TGA of perovskite inks without the addition of CsBr. (D to F) Semi–in situ XRD measurements of precursor films based on DMF (D), DMF-NMP (E), and DMF-NMP-DPSO (F). (G) DLS spectra of FACs perovskite precursor solutions. The concentrations of all samples are 0.5 mM. Unless otherwise specified, DMF, DMF-NMP, and DMF-NMP-DPSO represent the perovskite precursors dissolved in different solvents with or without additive, and the precursor films were dried in ambient air at room temperature during the measurements.
verified by the largely increased solubility of lead(II) iodide (PbI₂) with the further addition of DPSO when compared with the DMF and DMF-NMP cases (fig. S3). Furthermore, to confirm the interaction of solvents and DPSO molecules with the perovskite precursor species, ultraviolet-visible (UV-vis) absorption measurements of the diluted precursor solutions (0.5 mM) were carried out (fig. S4). The characteristic absorption peak assigned to the PbI₂S₄ species (S represents generic solvent or additive molecules) located at the wavelength of 324 nm for the pure DMF case is slightly shifted to 326 nm for the DMF-NMP case, indicating that some of the DMF molecules are replaced by NMP in PbI₂S₄ species (38). Moreover, the characteristic absorption peak of PbI₂S₅⁺ species located at the wavelength of 264 nm for the DMF and DMF-NMP cases is further shifted to 266 nm with the introduction of DPSO, indicating that some DMF and/or NMP molecules are further substituted by DPSO (39). The room-temperature nonvolatile feature of DPSO causes its interaction with the perovskite precursor species to be stable and not considerably affected by the removal of DMF or NMP during the coating and the natural drying process of the wet films.

To further investigate the interaction between DPSO and other components within the perovskite precursor solution, we studied the bonding nature of the adducts using Fourier transform infrared (FTIR) spectroscopy measurements. Figure 2A shows FTIR spectra for fingerprint regions of bare DMF, PbI₂-DMF, and formamidinium iodide (FAI)-PbI₂-DMF adducts (full spectra can be found in fig. S5A). The characteristic stretching vibration peak of C=O at around 1670 cm⁻¹ for a bare DMF molecule shifts to 1653 cm⁻¹, indicating the formation of a PbI₂-DMF adduct for the DMF case. The shifted stretching vibration frequency of C=O is owing to the formation of dative bond by sharing lone pair electrons in oxygen with Pb²⁺ (40). The stretching vibration peak of C=N for bare FAI appears at 1715 cm⁻¹, while the vibration frequency is negligibly changed in the FAI-PbI₂-DMF adduct, which may be ascribed to the weak interaction of DMF molecule with FAI. In contrast, the characteristic stretching vibration peak of C=O at around 1670 cm⁻¹ for a bare NMP molecule shifting to 1653 cm⁻¹ and a C=O splitting peak appears at 1627 cm⁻¹ after the introduction of PbI₂, indicating successful coordination of the NMP molecule with Pb²⁺ (Fig. 2B and fig. S5B) (18).

Fig. 2. Interaction between the solvent or additive molecules and perovskite precursor species. (A to C) FTIR spectra of fingerprint regions for C=O and S=O stretching vibrations. (A) C=O stretching detected from DMF (solution, black), PbI₂-DMF (powder, red), FAI (powder, blue), and FAI-PbI₂-DMF (powder, orange). (B) C=O stretching detected from NMP (solution, black), PbI₂-NMP (powder, red), and FAI-PbI₂-NMP (powder, orange). (C) S=O stretching measured for DPSO (powder, black), PbI₂-DPSO (powder, red), and FAI-PbI₂-DPSO (powder, orange). The blue line represents the spectra of FAI (powder). (D to I) Molecular structures resulting from DFT calculations. Molecular structures of (D) PbI₂-DMF, (E) PbI₂-NMP, (F) PbI₂-DPSO, (G) FA⁺-DMF, (H) FA⁺-NMP, and (I) FA⁺-DPSO. (J) Interaction energy of solvent or additive molecules with the perovskite precursor species FA⁺ and PbI₂.
In addition, the stretching vibration peak of C=O for bare FAI appears at 1715 cm$^{-1}$, while the vibration frequency is shifted to 1720 cm$^{-1}$ in the FAI-PbI$_2$-NMP sample, further indicating the formation of FAI-PbI$_2$-NMP adduct (18). As shown in Fig. 2C and fig. S5C, it is found that the S=O characteristic stretching vibration peak of a bare DPSO molecule at 1037 cm$^{-1}$ shifts to 968 cm$^{-1}$ for PbI$_2$-DPSO sample, indicating the formation of PbI$_2$-DPSO adduct. Moreover, the stretching vibration peak of C=N for bare FAI at 1715 cm$^{-1}$ shifts to 1710 cm$^{-1}$ for FAI-PbI$_2$-DPSO sample, which indicates the formation of FAI-PbI$_2$-DPSO adduct. In contrast to the molecules. The interaction energies of the corresponding bonds are able to shift in the FTIR spectra of FAI-PbI$_2$-DPSO and FAI-PbI$_2$-NMP and 3133 cm$^{-1}$ for FA cations in FAI-PbI$_2$-DMF, the peaks consider- with DMF. 

The results clearly verify the interaction of the solvents as well as DPSO with the perovskite species. To further study the different strengths of interactions between DPSO as well as NMP and DMF with PbI$_2$ and FAI, we conducted density functional theory (DFT) calculations to quantify their different interaction energies. Figure 2 (D to I) shows the stabilized molecular structures, and the calculated interaction energy results are summarized in Fig. 2J and table S1. As expected, PbI$_2$ bonds with the oxygen in DMF, NMP, and DPSO molecules. The interaction energies of the corresponding bonds are calculated to be $-0.980$ eV for PbI$_2$-DPSO, $-0.765$ eV for PbI$_2$-NMP, and $-0.627$ eV for PbI$_2$-DMF. The results indicate that the interaction energy of PbI$_2$ with DPSO is stronger than that with NMP and DMF. Moreover, DPSO also shows a stronger interaction energy with FA cations ($-1.496$ eV) versus NMP ($-1.429$ eV) and DMF ($-1.331$ eV) by hydrogen bonding. These results are in agreement with the TGA analysis and DLS measurements, which further confirm that a much higher energy barrier must be overcome to enable perovskite nucleation/growth for the DMF-NMP-DPSO case compared with the other two cases. It also indicates that the wet film stable time is synergistically determined by the vapor pressure of the solvent or additive molecules (the solvent and additive properties are summarized in table S2) and their interactions with perovskite precursors.

**Perovskite film morphology**  
To obtain perovskite films, the wet films were further treated via a less toxic n-hexane antisolvent bath treatment (AST) and thermal annealing. Antisolvent extraction can facilitate the removal of the redundant solvents from the wet film and achieve a controllable precursors.

With respect to the crystallographic properties of the intermediate films, for the DMF case with AST at different time stages, it is clearly observed that the as-deposited perovskite intermediate films mainly consist of δ phase ($11.8^\circ$ and $26.2^\circ$) perovskite rather than the preferred photoactive α phase (Fig. 3A) ($15, 42$). This is attributed to the rapid evaporation of DMF from the wet films along with the overwhelming uncontrollable natural nucleation. For the DMF-NMP case, obvious peaks at 13.9° assigned to the (101) crystal planes of photoactive α phase perovskite are observed (Fig. 3B), while the peaks at 11.8° and 26.2° ascribed to the unfavorable δ phase can still be detected. In contrast, the phase transformation from a much stable precursor wet film of DMF-NMP-DPSO case is complete, and the preferred α phase without any impure phase is obtained for the films treated by antisolvent at different time stages (Fig. 3C). We propose that the preferred α phase is favored by a stable CsBr-FAI-PbI$_2$-DMF-NMP-DPSO intermediate phase, which is due to the strong interaction between the nonvolatile DPSO additive and precursor molecules evidenced by the DFT calculations and FTIR results.

With respect to the final perovskite morphology evolutions, the DMF-NMP-DPSO ink can deliver compact and uniform perovskite films from stable wet films within 8 min compared with the other two cases with random structures (Fig. 3D). The poor film coverage and inhomogeneous morphology are probably ascribed to the heterogeneous and uncontrollable natural nucleation process that can cause serious current loss in PSMs and lead to inferior device performance (fig. S7 and table S3).

Because DPSO has a high sublimation temperature and strong chelating capability with perovskite species, it inspires us to investigate whether DPSO still exists in the obtained perovskite film after AST and thermal annealing treatment. We used x-ray photoelectron spectroscopy (XPS) to measure the S 2p signal in the corresponding perovskite films (fig. S8). Compared with the sample without either AST or annealing treatment, the sample without AST but with thermal annealing at 150°C for 30 min shows negligible change of the S 2p signal, implying that 150°C annealing cannot remove DPSO in the final perovskite film. In contrast, in the DMF-NMP-DPSO–based perovskite film with both AST and annealing treatment, negligible S 2p signal in the XPS spectrum could be detected. This observation suggests that DPSO in the obtained film is below the detection limit of XPS after being effectively extracted from the wet film with the help of AST. As a result, high-quality perovskite films with the preferred pure photoactive α phase are obtained (fig. S9), which is beneficial for high-performance device fabrication.

**Optical and electronic properties of large-area perovskite films**

A uniform and high-quality perovskite film over large area is essential for high-performance PSMs. With the optimized perovskite precursor solution of DMF-NMP solvents containing DPSO additive, we slot-die–coated the FACs perovskite films on fluorine-doped tin oxide (FTO)/NiMgLiO substrate with the size of 20 cm by 14 cm (movie S4). Film thickness could be simply controlled by adjusting the concentration of the perovskite precursor ink (fig. S10). As shown in Fig. 4A, the coated perovskite film is mirror like.

To further examine the uniformity of the slot-die–coated perovskite film, we performed photoluminescence (PL) mapping of a 5 cm by 5 cm sample cut from a 20 cm by 14 cm perovskite film sample on glass substrate (Fig. 4B). The film shows homogeneous PL intensity, which suggests good uniformity of the large-area perovskite films. Besides, their optical uniformity is further verified by UV-vis. We cut one 20 cm by 14 cm sample from FTO/NiMgLiO substrate into 12-piece 4 cm by 4 cm (Fig. 4C) samples and measured their UV-vis absorbance spectra. It is found that all 12 samples show nearly identical optical absorption response in Fig. 4D, suggesting a good uniformity of the optical properties over large scale.

To further analyze the electronic uniformity of the deposited perovskite film over large area, one sample on glass substrate (20 cm by 14 cm) was cut into 12 pieces with a size of 4 cm by 4 cm.
for time-resolved PL (TRPL) characterization. The TRPL decay curves were fitted with a biexponential function

$$Y = A_1 \exp\left(-t/\tau_1\right) + A_2 \exp\left(-t/\tau_2\right) + y_0$$  

(1)

where $A_1$ and $A_2$ are the relative amplitudes and $\tau_1$ and $\tau_2$ are the lifetimes for the fast and slow recombination, respectively. As shown in Fig. 4E, 12 pieces of samples give an average PL lifetime of 137.0 ns with a standard deviation (SD) of ±13.8 ns (the steady-state PL peak for the obtained perovskite film is detected before TRPL measurement as shown in fig. S11A, and the TRPL fitting results are exhibited in fig. S11B and table S4). The narrow distribution of TRPL lifetime indicates a good uniformity of the
defect nature over large scale within the large-area perovskite films.

Furthermore, a 20 cm by 14 cm perovskite film sample on FTO/NiMgLiO substrate was cut into 12 pieces with the size of 4 cm by 4 cm to fabricate PSCs with an active area of 1 cm², with the device configuration of “FTO/NiMgLiO/FA₀.₈₃Cs₀.₁₇PbI₂.₈₃Br₀.₁₇/LiF/C₆₀/bathocuproine (BCP)/Bi/Ag” (43). Figure 4F shows the photocurrent density–voltage (J-V) curves of the 12 devices. All devices show nearly identical device performance and give an average efficiency of 18.2 ± 0.2% (table S5). The centrally distributed device performance of the 12 devices further verifies the uniformity of the perovskite film over large scale.

**PSM structure and performance**

To apply the above large-area perovskite films to a module device, PSMs with a configuration of FTO/NiMgLiO/FA₀.₈₃Cs₀.₁₇PbI₂.₈₃Br₀.₁₇/LiF/C₆₀/BCP/Bi/Ag are manufactured (43). Figure 5A illustrates the cross-sectional electron microscopy (SEM) image of the PSMs. In our PSMs, all of the functional layers including the charge transport layers, perovskite layer, and electrodes are constructed with scalable fabrication methods (Fig. 5, B and C). This makes our PSM fabrication strategy promising for mass production with high technical reproducibility.

In addition, our PSMs are based on a parallel-interconnected design, as shown in Fig. 5B and fig. S12A, which is different from the commonly reported PSMs with the series-interconnection design (table S6). The silver grids in our modules are designed to act as current collectors. They are beneficial to minimize the efficiency loss induced by the series resistance of the FTO substrate (fig. S12, B to E), which is a recognized reason for the efficiency mismatch between small-area devices and PSMs (1, 17). Compared with the series-connected design, the parallel-connected module can realize less energy loss induced by the performance mismatch of adjacent subcells, which has been reported in dyesensitized solar modules (24). Such a module design avoids the direct contact between the perovskite and metal electrode/grid, as the direct contact of metal with perovskite at the P1-P2-P3 interconnection regions in series-connected PSMs was reported to be detrimental for module stability because of the reaction of the perovskite with metal (25). The parallel module design is thus believed to be beneficial for PSMs’ long-term stability.

**Fig. 5. PSM structure and performance.** (A) High-resolution cross-sectional SEM image of a complete PSM. (B) Three-dimensional structure schematic diagram of the designed module connected in parallel. (C) Cross-sectional schematic illustration of the fabricated module coupled with the deposition methods of the functional layers. (D) J-V curves of PSMs including a stabilized efficiency output and the device performance before and after stabilized test. FF, fill factor. (E) Reproducibility of PSMs (30 samples were tested); the inset is the optical image of some fabricated modules. Photo credit: Zhichun Yang, Huazhong University of Science and Technology.
operation. In addition, it has been confirmed that an ultrathin lithium fluoride (LiF) interlayer (0.8 nm) is effective for large-area perovskite films’ surface passivation, which can improve the open-circuit voltage ($V_{OC}$) of the PSMs (fig. S13 and table S7) (44). Moreover, a chemically inert bismuth interlayer (20 nm) is introduced between the BCP layer and the Ag electrode to serve as a robust permeation barrier layer to hamper Ag interdiffusion as well as the reaction of Ag with perovskite (45).

To check the PSM performance, we sent our module to the Newport Corporation Technology and Application Center PV Lab, which is a globally recognized PV testing center for certification. The module gives a quasi-stabilized power conversion efficiency (PCE) of 16.63% with an active area of 20.77 cm² (Fig. 5D and fig. S14). The detailed performance output includes the stabilized efficiency, and the efficiencies before and after stabilized test at forward and reverse scans are also provided. The well-overlapped results reflect that our PSMs exhibit negligible hysteresis and very stable output both before and after the stabilized current-voltage (I-V) sweep configuration test (fig. S15). The corresponding external quantum efficiency result is exhibited in fig. S16. To the best of our knowledge, this is the first certified efficiency report of parallel-design PSMs (table S6). To verify the manufacturing reproducibility of our scheme toward efficient PSMs, we measured the device performances of 30 modules (Fig. 5E, fig. S17, and table S8). The narrow efficiency distribution confirms that our efficient solar modules are highly reproducible. It should be noted that the geometric factor (GFF) of our parallel module is around 92.7% (fig. S18). Thus, the aperture efficiency is estimated to 15.42%. This value can be further improved by optimizing the laser scribing process to achieve higher GFF (46), reducing defects by interface engineering to suppress charge recombination (3) and developing more effective coating methodologies for electron or hole transport layers (47).

**PSM stability**

We further evaluate the operational stability of our parallel PSMs. For stability tests, a highly compact and hydrophobic Al₂O₃ layer (fig. S19) was further deposited by atomic layer deposition (ALD) on top of the Ag electrode without sacrificing efficiency. Then, the module was carefully encapsulated by a cover glass with a hollow space via a hot melt adhesive membrane, and the four edges were further wrapped with butyl rubber/Al tape. First, an accelerated aging test of the encapsulated PSM was conducted under continuous 1-sun equivalent white-light light-emitting diode (LED) in ambient air with MPP tracking at the temperature around 50°C. The corresponding results are shown in Fig. 6A and fig. S20. The cover glass encapsulated module without the ALD Al₂O₃ layer retained 80% of its initial value ($T_{90}$) after 736 hours. In contrast, the module encapsulated simultaneously with ALD Al₂O₃ and a cover glass (ALD Al₂O₃/cover glass) retained 95% of its initial efficiency ($T_{95}$) after aging for 1187 hours. Beyond that, the real day/night cycling stability of ALD Al₂O₃/cover glass encapsulated PSMs was also studied (Fig. 6B, fig. S21, and table S9). Aging PSCs under light/dark cycles is another important protocol to mimic the device real working stability in practical application (table S10). The reversible degradation/recovery of PSCs has been studied in such light/dark cycling test (48, 49). Such reversible performance is found to be caused by a reversible ion redistribution that induced by regular polling and electric field intensity changes during day/night cycles (49). It is also reported that new recombination centers could form in the perovskite bulk or at the interfaces under test of day/night cycling combined with elevated temperature (50). Outdoor test conditions are highly demanding, as the devices are characterized by real day (sunlight)/night (dark), seasonal, and weather cycles that correspond to drastic variations in irradiation, temperature, and moisture (51, 52). Here, to mimic the potential practical application scenarios such as building integrated PVs of perovskite PV technology, the fabricated module connected to a mini electric fan (~0.3 W) was placed near the indoor windows under real sunlight without humidity control for over 1 year and periodically taken to measure I-V curves under a standard solar simulator. The device temperature did not exceed 55°C even in the summer because the indoor temperature was controlled by an air conditioner. Our indoor day/night cycling test has mimicked the real working conditions of a solar power window, which is normally integrated with human-living buildings. The PSM retains 97% of its initial efficiency after aging for 10,000 hours. This test also demonstrated that for the working conditions of an indoor environment (with air conditioner in summer) for PSMs, the $T_{90}$ lifetime of PSMs could possibly exceed 5 to 6 years if the linear decrease of 3 to 4% PCE per year is valid in the following years. It is suggested that this indoor day/night cycling test makes sense and has a certain guiding effect on the differentiated application scenarios of perovskite PV technology.

The good stability of our PSMs is suggested to be ascribed to the following critical points: (i) The high-quality and thermally stable FACs perovskite film over large area made by our room-temperature nonvolatile wet film stabilizer strategy, in combination with other function layers’ up-scaling fabrication, can largely prevent the formation of pin holes and the resultant shunt paths across the device, which could induce intermediates’ decomposition reactions and performance degradation; (ii) the robust permeation barrier design of Bi/Ag electrode as well as the further ALD-Al₂O₃ thin-film encapsulation and the mechanical protection with a cover glass that can prevent the corrosion of Ag electrode, blocking the ingress of H₂O/O₂ from the ambient atmosphere and slowing down the fast volatilization of the degraded perovskite species during long-term aging (53). In combination of Bi and Al₂O₃ barriers, the as-fabricated PSMs could withstand water immersing for several minutes without notable color change compared with the module without ALD Al₂O₃ thin-film encapsulation (movie S5), which visually proves the barriers’ nonpermeability. It is being revealed that the integration of a nonpermeable barrier in PSCs is important for the long-term stability, which can affect the equilibrium of perovskite decomposition reaction from the perspective of thermodynamics (3, 54, 55). (iii) The parallel module design avoids the direct contact of metal electrode/grid with perovskite and allows an adequate space between the grids or electrodes and the perovskite layer. The ALD-Al₂O₃ thin-film encapsulation further isolates the perovskite or its degradation by-products with metal electrode/grid. This can prevent the unexpected contact or corrosive reaction between the metal electrode/grid and perovskite from the cross-sectional direction in the interconnection region as demonstrated in the series-designed PSMs (2, 25). All above convicently guarantee the good stability of our solar modules.

**DISCUSSION**

In conclusion, perovskite ink engineering by using room-temperature nonvolatile DPSO as the wet film stabilizer was conducted to achieve...
improved wet film stability for slot-die coating of large-area FACs perovskite films. Coupled with less toxic antisolvent extraction, high-quality FACs perovskite films are obtained over large area. As a result, a certified quasi-stabilized efficiency of 16.63% with an active area of 20.77 cm² was achieved for our parallel-interconnection solar module design based on the above strategy. Moreover, our encapsulated solar module remains 97% of its initial efficiency after operating for 10,000 hours under real day/night cycling. Our solar module also achieves a T₉⁵ lifetime of 1187 hours under continuous 1-sun equivalent white-light LED illumination with MPP tracking at the temperature around 50°C.

Our demonstration paves a way for scalable fabrication of large-area and stable PSMs toward the commercialization of this promising thin-film PV technique.

**MATERIALS AND METHODS**

**Materials**

Nickel(II) acetylacetonate (95%), DMF (anhydrous, 99.8%), acetonitrile (anhydrous, 99.8%), and lithium fluoride (≥99.99%) were purchased from Sigma-Aldrich. Magnesium acetate tetrahydrate (99%) and lithium acetate (99%) were all purchased from Wako Co., Japan. Ethanol (analytically pure) and isopropanol were purchased from Sinopharm Chemical Reagent Company, China. FAI (99.9%) was provided by Hangzhou Zhongneng Photoelectricity Technology Co. Ltd. C₆₀ was purchased from Luminescence Technology Corp. Cesium bromide (CsBr, 99.99%), PbI₂ (≥98%), DPSO (> 99.0%), BCP (>99.0%), n-hexane (anhydrous, > 96%), and NMP (>99.0%) were purchased from Tokyo Chemical Industry Co. Ltd. All chemicals were used as received without any purification unless otherwise specified.

**Methods**

**Precursor ink engineering**

Perovskite precursor ink (1.3 M) (FA₀.₈₃ Cs₀.₁₇ PbI₂.₈₃ Br₀.₁₇, denoted as FACs) was prepared for the optimization of precursor inks. For the DMF-based precursor solution, 0.0941-gCsBr, 0.3712-gFAI, and 1.1986-gPbI₂ were dissolved in 2 ml of DMF. For the DMF-NMP-based precursor solution, 0.0941-gCsBr, 0.3712-gFAI, and 1.1986-gPbI₂ were dissolved in 2-ml mixed solvent of DMF and NMP (volume ratio = 1:1, denoted as DMF-NMP). For the DMF-NMP-DPSO-based precursor solution, 0.0941-gCsBr, 0.2630-gDPSO, 0.3712-gFAI, and 1.1986-gPbI₂ were dissolved in 2-ml mixed solvent of DMF and NMP (volume ratio = 1:1, denoted as DMF-NMP-DPSO). After that, the solutions were stirred for 12 hours at room temperature and filtrated before use. Typically, the DMF-NMP-DPSO precursor ink was used for slot-die coating large-area perovskite films for the corresponding characterization and fabricating PSMs. In particular, the optimal amount of DPSO additive is determined by the device performance and provided in fig. S7 and table S3.

**PSM fabrication**

A line (denoted as P1; the optical microscope image is exhibited in fig. S12B) was laser-scribed (27 W, 1064 nm, 40 kHz) on an FTO-coated glass substrate (TEC 8, Nippon Sheet Glass Co. Ltd.). Then, the scribed substrate was cleaned in an ultrasonic bath with detergent, deionized water, alcohol, and isopropanol for 15 min, respectively. After that, a NiMgLiO layer (hole transport layer) was deposited on the above cleaned FTO substrate. NiMgLiO solution was prepared with a mixed solvent of acetonitrile and ethanol (volume ratio = 95.5:100 ml) of nickel acetylacetonate with the addition of magnesium acetate tetrahydrate and lithium acetate. The prepared
solution (the mole atomic ratio is Ni:Mg:Li = 80:15:5, and the total metal ion concentration is 0.02 M) was sprayed by an air nozzle on the heated FTO substrate (570°C). After spraying coating, the samples were further treated at 570°C for another 40 min and cooled naturally. Afterward, the perovskite layer was deposited in a dry air glovebox (humidity <3%) by slot-die coating technology. In detail, the prepared perovskite ink (1.3 M, DMF-NMP-DPSO) was squeezed out with a feed pump speed of 166.67 μl/min, the gap between the slip and the coated substrate was 150 μm, and the substrate moving speed was 5000 μm/s. After that, the coated precursor wet film was transferred to an antisolvent bath of n-hexane (300 ml) for 2 min and taken out for annealing on a hotplate at 150°C for 30 min. Then, the LiF, C60, and BCP layers were deposited by thermal evaporation at the vacuum of <5.0 × 10⁻⁴ Pa, and the evaporation rate was controlled at 0.1 Å/s, respectively. The deposited layers were laser-scribed (14 W, 1064 nm, 500 μm/s) with a designed speed of 5000 μm/min, and the coated substrate was 150 μm, and the substrate moving speed was 5000 μm/s. After that, the coated precursor wet film was transferred to an antisolvent bath of n-hexane (300 ml) for 2 min and taken out for annealing on a hotplate at 150°C for 30 min.

Then, the LiF, C60, and BCP layers were deposited by thermal evaporation at the vacuum of <5.0 × 10⁻⁴ Pa, and the evaporation rate was controlled at 0.1 Å/s for the thickness of 0.8, 30, and 1 nm, respectively. The deposited layers were layer-scribed (14 W, 1064 nm, 500 μm/s) with a designed speed of 5000 μm/min, and the coated substrate was 150 μm, and the substrate moving speed was 5000 μm/s. After that, the coated precursor wet film was transferred to an antisolvent bath of n-hexane (300 ml) for 2 min and taken out for annealing on a hotplate at 150°C for 30 min. Then, the LiF, C60, and BCP layers were deposited by thermal evaporation at the vacuum of <5.0 × 10⁻⁴ Pa, and the evaporation rate was controlled at 0.1 Å/s for the thickness of 0.8, 30, and 1 nm, respectively. The deposited layers were laser-scribed (14 W, 1064 nm, 500 μm/s) with a designed speed of 5000 μm/min, and the coated substrate was 150 μm, and the substrate moving speed was 5000 μm/s. After that, the coated precursor wet film was transferred to an antisolvent bath of n-hexane (300 ml) for 2 min and taken out for annealing on a hotplate at 150°C for 30 min.

**Module encapsulation**

First, the modules for stability tests were all encapsulated by an ALD Al₂O₃ film unless otherwise specified. Briefly, trimethyl aluminum (TMA, Sigma-Aldrich) and deionized water were injected sequentially into the ALD chamber. The chamber pressure was <0.1 Pa, and the temperature was kept at 100°C. A single ALD cycle consisted of TMA pulse for 6 s, N₂ purging for 12 s, H₂O pulse for 6 s, and N₂ purging for 12 s. After that, 45 cycles were repeated for 27 min. Second, a cover glass was further attached on the top of each PSM to provide mechanical protection. To achieve this, a cover glass sheet was carefully sealed on top of ALD-Al₂O₃ along its edges with butyl rubber/aluminum tape. After the corresponding encapsulation process, the fabricated solar modules were performed for stability test. The cover glass-encapsulated PSMs were the modules with cover glass encapsulation but without ALD Al₂O₃ film encapsulation.

**Module stability test**

The operational aging test was performed at the MPP tracking under continuous white-light LED array illumination, and the light intensity was calibrated to achieve the same Isc from the PSMs measured under a standard solar simulator (AM 1.5G, 100 mW cm⁻²). The tests were carried out in ambient air, and the module temperature was at around 50°C.

The real day/night cycling test was carried out by placing the fabricated PSM indoor close to the window, without any humidity control. The encapsulated module maintained 97% of its initial efficiency after 10,000 hours under real day/night cycling with a load of mini electric fan (~0.3 W). After aging for several days, it was tested under a standard solar simulator. It should be mentioned that the day/night cycling test in our work was carried out in a human living environment, which helped to reduce the effect of heat radiation and rain effect. The device temperature did not exceed 55°C even in the summer because the indoor temperature was controlled by an air conditioner.

**Characterization**

Semi-in situ microscopy observations for the evolution of precursor wet films based on various perovskite precursors were carried out by an optical microscope equipped with a camera and a computer (HOMA-2000, Xipaike Co., China). UV-vis spectra of perovskite films were obtained from a Lambda 950 UV-vis spectrophotometer (PerkinElmer Co., USA). The absorption spectra of perovskite precursor solution were measured by a UV-vis near-IR spectrophotometer (SolidSpec-3700, Shimadzu). The volatility of perovskite precursor solutions was characterized by TGA (TGA8000, PerkinElmer Co., USA). The measurement was carried from room temperature to 150°C at a heat rate of 10°C/min under ambient air. DLS spectra of perovskite precursor solutions were done by a ZetaSizer Nano-ZS 90 (Malvern Instruments Ltd., Worcestershire, UK). To ensure the accuracy of the test results, the tube was washed three times by DMF solvent before injecting the perovskite precursor solution. Steady-state PL spectrum was measured using a LabRAM HR800 (Horiba Jobin Yvon) equipped with a laser, and the excitation source wavelength is 532 nm. TRPL measurements were conducted by a fluorescence spectrometer with an excitation wavelength of 478 nm (DeltaFlex, Horiba). PL mapping was carried out with a PL microscopic spectrometer (Flex One, Zolix, China) with mapping ability. The excitation source of PL is a continuous-wave laser with the wavelength of 532 nm, and the mapping was performed with a step size of 0.005 mm. Specially, for steady-state PL, TRPL, and PL mapping characterization, the large-area perovskite thin films were slot-die-coated on a glass substrate under the same deposition condition with their deposition on the charge-transport layer, except that the glass needed be treated with O₂ plasma for 15 min. XRD characterization was performed on an Empyrean x-ray diffractometer with Cu Ka radiation (PANalytical B.V., Netherlands). FTIR spectroscopy spectra were recorded by a VERTEX 70 FTIR microscope (Bruker Co., Germany). The surface morphology and cross-sectional images of samples were observed by a field-emission SEM (FEI NOVA NanoSEM 450). XPS measurements were performed on an AXIS-ULTRA DLD-600 W Ultra spectrometer (Kratos Co., Japan). A black mask with an illuminated aperture area (or active area, determined as the sum of areas of individual subcell aperture mask areas) of 20.77 cm² was used for PV performance measurements under standard AM 1.5G simulated sunlight (Oriel Class AAA, XES-160S1, SAN-EL ELECTRIC CO., LTD., Japan) with a source meter (Keithley 2601 B), and the simulated light intensity (100 mW cm⁻²) was calibrated with a reference silicon solar cell. We sent one of the best modules to an independent solar cell–accredited laboratory (Newport, USA) for certification.

**The preparation of adduct powders**

Pb₁₂·DMF adduct. Pb₁₂ (461 mg) was dissolved in 600 μg of DMF, which was magnetically stirred for 12 hours. Then, 400 μl of solution was dropped on a glass substrate (5 cm by 5 cm) and spun at 1000 rpm for 120 s. The film was peeled off by a knife and dried at 50°C in vacuum oven for 2 hours, which was collected for FTIR spectroscopy measurement.

FAI-Pb₁₂·DMF adduct. FAI (172 mg) and 461 mg of Pb₁₂ were dissolved in 600 μg of DMF, which was magnetically stirred for 12 hours. Then, 400 μl of solution was dropped on a glass substrate (5 cm by 5 cm) and spun at 1000 rpm for 120 s. The film was peeled off by a knife and dried at 50°C in vacuum oven for 2 hours, which was collected for FTIR measurement.

Pb₁₂·NMP adduct. Pb₁₂ (461 mg) was dissolved in 654 μg of NMP, which was magnetically stirred for 12 hours. Then, 400 μl of...
solution was dropped on a glass substrate (5 cm by 5 cm) and spun at 1500 rpm for 300 s. The film was peeled off by a knife and dried at 60°C in vacuum oven for 6 hours, which was collected for FTIR measurement.

**FAI·Pbl₂-NMP adduct.** FAI (172 mg) and 461 mg of Pbl₂ were dissolved in 654 mg of NMP, which was magnetically stirred for 12 hours. Then, 400 μl of solution was dropped on a glass substrate (5 cm by 5 cm) and spun at 1500 rpm for 300 s. The film was peeled off by a knife and dried at 60°C in vacuum oven for 6 hours, which was collected for FTIR measurement.

**Pbl₂-DPSO adduct.** Pbl₂ (461 mg) and 101.1 mg of DPSO were dissolved in 600 mg of DMF, which was magnetically stirred for 12 hours. Then, 400 μl of solution was dropped on a glass substrate (5 cm by 5 cm) and spun at 1200 rpm for 120 s. The film was peeled off by a knife and dried at 80°C in vacuum oven for 6 hours, which was collected for FTIR measurement.

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**Supplementary Materials**

Supplementary material for this article is available at http://advances.sciencemag.org/cgi/content/full/7/18/eabg3749/DC1

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