ORIGINAL ARTICLE

Effect of different curing times and distances on the microhardness of nanofilled resin-based composite restoration polymerized with high-intensity LED light curing units

Haifa Barakah *

Department of Restorative Dentistry, Lecturer at Collage of Dentistry, King Saud University, Riyadh, Saudi Arabia

Received 15 May 2021; revised 27 May 2021; accepted 30 May 2021
Available online 10 June 2021

KEYWORDS

LED; High intensity; Microhardness; Composite; Polymerization; Efficiency

Abstract  Purpose: This study examined the effect of different distances and curing times on the microhardness (VHN) of nanofilled resin-based composite (RBC) restorations polymerized with high-intensity LED LCUs.

Materials and methods: Seventy-five RBC specimens (2 mm thickness and 5 mm diameter) were fabricated from Tetric-N-Ceram (Ivoclar Vivadent). Each of the 25 specimens was polymerized by means of one of three types of high-intensity LED LCUs: (B) Blue-Phase-G2 (polywave LED, Ivoclar Vivadent), (E) Elipar S10 (single-peak, 3 M ESPE), and (P) Planmica Lumion (single-peak, Mectron) at three different distances (0 mm, 2 mm, and 4 mm) at 20 sec, 40 s, and 60 sec. A microhardness tester (NOVA, Innovatest, The Netherlands) was used to measure the VHN from the top and bottom surfaces. Data for VHN were analyzed using mixed ANOVA, followed by post hoc analyses with p-values < 0.05.

Results: A significant difference was found in VHN between all three LED LCUs, where (B) specimens had the highest means, followed by (E) and (P). Bottom surface VHN values were reduced significantly (p < 0.05) compared to top surface values in all LCU types. With increasing distances up to 2 mm and 4 mm, VHN values with (E) and (P) were significantly reduced on the top
1. Introduction

Global interest in performing aesthetic restorations has led to an increase in the use of light-curing units for polymerizing tooth-colored restorative materials (Frederick Allen Rueggeberg et al., 2017). The physical and mechanical properties of photocured composites are directly influenced by the level of conversion achieved during polymerization (Ribeiro et al., 2012). Thus, a high degree of conversion enhances the restoration wear resistance, hardness and flexural strength (J. L. Ferracane et al., 1997). Nanotechnology in manufacturing RBC restorative materials is being applied to dentistry (Mitra et al., 2003). Due to their small size, it is possible to incorporate more filler content (Nitta, 2005), which results in better mechanical properties (Leprince et al., 2013; Mitra et al., 2003).

The optimal conversion of the monomer in the resin composite material is directly related to irradiance (Calheiros et al., 2006; F. A. Rueggeberg et al., 1994) and exposure time (Vargas et al., 1998). Thus, photopolymerization using light-curing units with low irradiance presents poor physical properties such as increased wear and staining and a greater risk of pulp irradiation and recurrent caries (Barghi et al., 2007; Maghaireh et al., 2013; Piló et al., 1999; F. A. Rueggeberg et al., 1994). To obtain optimal physical properties and clinical performance of resin composite restorations, it is necessary to have sufficient irradiance energy for the monomer to be converted to a polymer during the polymerization reaction (Knežević et al., 2001; Yoon et al., 2002). This has led to the development of high-intensity light curing units, such as quartz–tungsten–halogen, plasma arc and light-emitting diode (LED) light (Barghi et al., 2007; Calheiros et al., 2006; Maghaireh et al., 2013). Nevertheless, LED sources have almost replaced other light curing systems (Jandt & Mills, 2013; Nomoto et al., 2009).

The manufacturers of the newly introduced high-intensity LED LCUs have claimed a sufficient depth of polymerization and superior physical properties of the RBC restoration along the whole depth of the 2 mm increment of composite restoration owing to their higher irradiance (Leprince et al., 2013).

Surface hardness testing has been shown in many studies to be a good indicator for the degree of conversion (DC) (Dionysopoulos et al., 2015); however, this is considered by others not a sufficient clinical indicator of the degree of conversion because a low-intensity light source also promotes superficial hardness, even when the deeper layers are not well polymerized. According to Morimoto et al., this was true at the top surface, which was not greatly affected by variations in irradiance (Morimoto et al., 2016). Several studies indicated a better DC and microhardness with high-intensity LED LCUs (Jandt & Mills, 2013). A logarithmic relationship was found between the hardness of dental composites and the received radiant exposure (energy density) (Davidson & de Gee, 2000; R. B. T. Price et al., 2004; Watanabe et al., 2015). Meanwhile, another study suggested that there is no benefit from increasing irradiance beyond approximately 1000 mW/cm² (Musanje & Darvell, 2003).

Microhardness values at the bottom surfaces of the restoration when there is a distance between the LC tip and the restoration, as in many clinical cases of deep class IIIs, may still represent a challenging validity even for present high-intensity LCUs (Elkorashy et al., 2013; Shimokawa et al., 2017; Yoon et al., 2002). Several studies concluded a reduced polymerization at the bottom surface of the restoration, and when it is performed from a distance, the effect of light will be even less (R. B. T. Price et al., 2004). Therefore, compensating by increasing the curing time has been proposed, and some have recommended up to 60 s of curing (Xu et al., 2006). Thus, this study examined the effect of different distances and curing times on the microhardness (VHN) of nanofilled RBC restorations polymerized with high-intensity LED LCUs.

2. Materials and methods

2.1. Restorative material

Details of the dental restorative material evaluated in the study and the LED LCUs are shown in Table 1. A total of 75 RBC disc-shaped specimens were fabricated from a single restorative material (Tetric-N-Ceram, Ivoclar Vivadent). The RBC restoration specimen was placed in a silicon mold (2 mm deep × 5 mm diameter) on a Mylar strip and a glass slide. Then, it was covered with another Mylar strip followed by a microscopic glass slide to prevent the formation of an air-inhibited layer on the top surface and pressed to extrude excess material to obtain a smooth, standardized exterior surface.

2.2. Polymerization

Twenty-five specimens were polymerized with one of the three LED LCUs assigned for the study according to their manufacturer’s instructions at an ambient temperature of 23° ± 1°C. The LCUs were calibrated to measure their irradiance value directly on a digital radiometer (with 0 mm distance) and from two different distances (2 mm and 4 mm) to evaluate the actual value that can reach the top of the specimen. The radiometer
Table 1

| Resin-based composite restorative material | Composite (shade) | Type | Recommended curing time | Composition | Manufacturer | Lot No. |
|-------------------------------------------|-------------------|------|-------------------------|-------------|--------------|--------|
|                                           | Tetric-N-Ceram    | Nanofilled, Shade A2 | 10–20 s with high irradiance LCUs (>1000 mW/cm²) | Dimethacrylates, additives, catalysts, stabilizer sand pigments, barium glass, ytterbium trifluoride, mixed oxide and prepolymerized filler (prepolymers) (56% vol.) | Ivoclar-Vivadent, AG, 9494 Schaan/Liechtenstein | Z017Y9 |

| Light curing units (LCUs) (LCU) | Type | Irradiance 0 mm | Irradiance 2 mm | Irradiance 4 mm | Manufacturer | Ser. No. |
|-------------------------------|------|---------------|---------------|---------------|--------------|---------|
| Blue phase G2 | blue/violet polywave LED | 1570 mW/cm² | 1390 mW/cm² | 1210 mW/cm² | Ivoclar Vivadent AG FL-9494 Schaan/Liechtenstein, Austria. | 222,788 |
| Elipar S10™ | Blue/Single-peak LCU | 1120 mW/cm² | 1010 mW/cm² | 890 mW/cm² | 3 M ESPE, D-82229 Seefeld, Germany. | 939,123,009,611 |
| Planmeca Lumion | Blue/Single-peak LCU | 1220 mW/cm² | 1070 mW/cm² | 700 mW/cm² | Mectron S.p.A., via Loreto 15’A, 16,042 Carasco-GE-Italy. | 309PG403 |

| Light curing radiometer Name | Description | Manufacturer | Ser. No. |
|-----------------------------|-------------|--------------|---------|
| Bluphase - meter            | 4,5 DC, 3x Battery LR6/AA/1,5 V DC | Ivoclar Vivadent AG FL-9494 Schaan/Liechtenstein, Austria. | 00,735 |

| Microhardness tester Name | Description | Manufacturer | Ser. No. |
|---------------------------|-------------|--------------|---------|
| NOVA                      | Weight: 37.5 kg Man. date: 2017 Power: 100 V-240 V/50–60 Hz/3A Model No.: 130 | INNOVATEST, Europe BV, Borgharenweg 140 6222 AA, Maastricht, The Netherlands | 13,002,178,648 |
was a Bluephase meter from Ivoclar Vivadent, which has a wavelength sensitivity of 400–510 nm and measures the irradiance from 100 to 1999 mW/cm². The irradiance values were obtained by means of three measurements of the LCUs.

During polymerization, three distances and three curing times were followed for each type of LCU: 0 mm distance for 20 sec, n = 5; 2 mm distance for 20 sec, n = 5; 2 mm distance for 40 sec, n = 5; 4 mm distance for 20 sec, n = 5; and 4 mm distance for 60 sec, n = 5 to simulate the clinical situations of deep proximal class II restorations. Table 1 shows the irradiance of each LCU that was applied for each distance. For the groups that received longer curing times, after each 20 sec treatment, a break of 4 sec was implemented to allow for heat dissipation. The specimens were then incubated in dark vials filled with distilled water for 24 h at 37°C to ensure complete polymerization.

2.3. Microhardness testing

A microhardness tester was used to measure the Vickers hardness number (VHN) from five indentations on the top and five on the bottom surfaces. The VHN was determined for each specimen using an INOVATEST microhardness tester device, as shown in Table 1. A diamond indenter was used to apply a load of 300 gm for 15 s. Five values were recorded from each surface tested. In total, 75 specimens were made (one RBC × three lights × three distances), and 750 microhardness readings were obtained (75 specimens × 5 VHN measurements × 2 surfaces × 1 time).

2.4. Statistical analysis

Data that were obtained from the microhardness tester were analyzed using the statistical software IBM SPSS version 27 (Armonk, NY: IBM Corp., 2020). Mixed ANOVA (combination of within-subject and between-subject factors) was used to address the main effect of LED LCU type, distance/polymerization time, the interaction term between LED LCU type and distance/polymerization time. Statistically significant interactions and main effects were followed up with post hoc analyses (Tukey’s HSD and simple effects). All inferential statistical analyses were conducted using a 0.05 level of statistical significance, with p-values < 0.05 interpreted as statistically significant.

3. Results

Descriptive statistical analysis shows that VHN values range from 32.1 to 63.7, with a mean of 49.65, a median of 51.60 and a standard deviation of 7.60. The histogram and box-whisker plot suggest a slightly skewed distribution but can be assumed to be approximately normal (Fig. 1).

The results showed statistically significant differences between the three LED LCU types (p-values < 0.001). BluePhase-G2 specimens had the highest VHN values (M = 55.18), Planmica Lumion had the lowest VHN values (M = 40.66), and Elipar S10 had the lowest VHN values (M = 52.05).

Distance and polymerization time have statistically significant impacts on VHN for each LCU. Table 2 and Fig. 2 summarize the statistically significant interactions that were found among the variables.

The top and bottom surfaces of Planmica reported the highest remarkable reduction in VHN values with increasing distances. At 2 mm/20 sec and 4 mm/20 sec, the VHNs were M = 42.46 and 39.70 for top surfaces and M = 45.56 and 37.17 for bottom surfaces, respectively. Even after increasing the curing time to 40 and 60 sec, the VHN of Planmica was still statistically significant, with the lowest values for both the top and bottom surfaces among all other groups (M = 45.56 and 46.71 for top surfaces, M = 36.46 and 39.90 for bottom surfaces).

On the other hand, the Blue-phase reported significantly the highest VHN compared to the other LCU types (p < 0.05),
and its performances were not affected by increasing distance (0 mm, 2 mm, 4 mm) on the top surfaces (M = 61.26, 59.45, 58.47, respectively) (p > 0.05). However, the bottom hardness was significantly reduced compared to the VHN values of the top at 0 mm, 2 mm, and 4 mm distances with a standard 20 sec curing time (M = 51.76, 54.39, 48.08, respectively). Interestingly, increasing the curing time with Blue-phase LCU did not significantly improve the VHN values, and it may actually have an inverse effect (p > 0.05).

The VHN values of Elipar S10 were intermediate compared to those of the other two LCUs. Its curing performance was significantly inferior to that of the Blue-phase and superior to that of Planmica. Its irradiance was affected by increasing the distance. A statistically significant reduction (p < 0.05) was shown in the results of VHN on the bottom (M = 52.62) surfaces compared to the top (M = 55.81). With distances of 2 mm and 4 mm, the bottom was (M = 45.13, 43.08) compared to the top (M = 52.37, 52.01). Upon increasing the curing time to compensate for the 2 mm/40 sec and 4 mm/60 sec distances, the VHN increased significantly (p < 0.05) on the top (M = 52.37, 61.11) and bottom (M = 52.81, 52.68) surfaces.

4. Discussion

Microhardness is an indirect measure of the degree of conversion of a material. It provides useful information on the depth of polymerization (curing) when measured on the top and bottom surfaces of a specimen (Aravamudhan et al., 2006; Jack L. Ferracane, 1985; Soh et al., 2003). Several studies have reported reduced DC and microhardness on the bottom side of the restoration. Additionally, increasing the distance could result in a significantly lower irradiance that can reach the surface of the resin in the tooth, which is often 2-8 mm away from the light tip (Cerciolani et al., 2008; R. B. Price et al., 2000; 2011; Xu et al., 2006). For that reason, compensation was recommended by increasing the curing time from 20 to 60 sec to ensure sufficient polymerization (XU et al., 2006). Accordingly, in the present study, an assumption was estimated for the curing time of the 2 mm distance groups (40 sec) and the 4 mm groups (60 sec) to compare between the tested high-intensity LCUs in their efficiency to polymerize the composite restoration from distance. The results showed that Blue-phase LCUs proved to have the highest performance among the other LCUs; even with distance, the readings of the bottom hardness were significantly higher than their counterpart LCUs. Its superior efficiency may be related to two factors: first due to its higher irradiance (up to 1750 mW/cm²) and second due to its spectral emission. The Blue-phase is a polywave LCU that can polymerize different photoinitiators other than camphorquinone. Blue light polymerizes camphorquinone at a wavelength of 570 nm (Leprince et al., 2013), while violet light is capable of polymerizing ivocerin-dibenzyol germanium derivative (Moszner et al., 2008) photoinitiators. Ivocerin has been incorporated in a Tetric-N-line composite material (Ivoclar Vivadent) for the purpose of enhancing their quantum efficiency and esthetic appearance by reducing the yellowish effect of the amine group that is incorporated as a coinitiator with camphorquinone. Moreover, when the manufacturer of a specific RBC restoration produces an LCU, it is usually considered more compatible with the restoration than other LC devices.

Manufacturers of Blue-phase LCUs have recommended a curing time of 10–20 sec, but in the present study, a 20 sec curing time was followed as a standard time for all the tested LCUs. When polymerizing from distance, increasing the curing time had no beneficial effect in increasing the bottom surface hardness with Blue-phase LCU. However, this was not the case with Elipar S10 and Planmica Lumion LCUs. Increasing the curing time (2 mm for 40 sec and 4 mm for 60 sec) contributed to significantly enhancing the top and bottom surface hardness. This could most likely be explained by the more time that was given to compensate for the distance, which allowed more of the irradiance to penetrate the whole thickness of the restoration and polymerize not only camphorquinone, which is com-
patible with their single peak spectrum (Shimokawa et al., 2017) but also has sufficient time to polymerize more of the other photoinitiators at the lower irradiance spectrum (370–460 nm wavelength) (Leprince et al., 2013).

A similar study was conducted by Shafadella et al. (Shafadilla et al., 2017), who concluded that curing distance and time both significantly affect the surface hardness of nanofilled composite resin. Their surface hardness results ranged from 72.40 kg/mm² to 80.33 kg/mm². They considered that the range of hardnnesses was acceptable since they were comparable to that of dentin and far less than that of enamel. In clinical applications, when a short curing distance is not possible, the curing time and the intensity of the light from the light-curing unit must be increased to achieve maximum surface hardness. However, the curing distance must still be no > 4-5 mm (Segal et al., 2015; Shafadilla et al., 2017). Another important factor that should not be overlooked during polymerization with high-intensity LCUs is heat production. It is evident (Hori et al., 2019; Mouhat et al., 2017; Weerakoon et al., 2002) that this can produce a harmful effect on the pulp. Thus, a lag break of 4 sec was performed in the present study between every 20 sec of polymerization to reduce the heat effect.

The status of the curing unit should be evaluated periodically to ensure that it is still in optimal condition. Several studies have revealed that light-curing units used in dental practices do not emit sufficient radiation to achieve maximum photopolymerization (Maghaireh et al., 2013; Strassler & Price, 2014). Accordingly, composite resin restorations may not experience sufficient polymerization, causing them to be resistant to low abrasion (Maghaireh et al., 2013). Therefore, to compensate, the light energy emitted by the light-curing unit must be increased (Krämer et al., 2008).

5. Conclusion

High-intensity LCUs have variable effects on the surface (top/bottom) hardness of Tetric-N-Ceram nanofilled RBC restorations. To obtain clinically acceptable hardness for RBC restoration, the choice of the LCU that matches the wavelength of the photoinitiators present in the restoration is the key factor for its success. The closer the tip of the LED light-curing unit is to the surface of the nanofilled composite resin restoration, the greater the surface hardness of the restoration. When that is not possible clinically, compensation with a longer curing time (2 mm/40 sec and 4 mm/60 sec) is highly recommended with Elipar S10 and Planmica Lumion LCUs to improve the material surface hardness. Further studies are indicated with other types of RBC restorative materials.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Acknowledgments

The author wishes to thank the following groups and individuals for their valuable contributions: the College of Dentistry Research Center at King Saud University for supporting this study (registration number: FR 0592); the Deanship of Scientific Research; clinical director at King Saud University; and Mr. Anton Svendrovski for his valuable contribution in the statistical part of this study.

References

Aravamudhan, K., Floyd, C.J.E., Rakowski, D., Flaim, G., Dickens, S.H., Eichmiller, F.C., Fan, P.L., 2006. Light-emitting diode curing light irradiance and polymerization of resin-based composite. J. Am. Dent. Assoc. 137 (2) https://doi.org/10.14219/jada.archive.2006.0147.

Barghi, N., Fischer, D.E., Pham, T., 2007. Revisiting the intensity output of curing lights in private dental offices. Compendium of Continuing Education in Dentistry (Jamesburg, N.J.: 1995), 28(7).

Calheiros, F.C., Kawano, Y., Stansbury, J.W., Braga, R.R., 2006. Influence of radiant exposure on contraction stress, degree of conversion and mechanical properties of resin composites. Dent. Mater. 22 (9). https://doi.org/10.1016/j.dental.2005.11.008.

Corciolani, G., Vichi, A., Davidson, C.L., Ferrari, M., 2008. The influence of tip geometry and distance on light-curing efficacy. Operative Dentistry 33 (3). https://doi.org/10.2341/07-94.

Davidson, C.L., de Gee, A.J., 2000. Light-curing units, polymerization, and clinical implications. J. Adhesive Dentistry 2 (3), 167-16773.

Dionysopeulos, D., Papadopoulos, C., Koliniotou-Koumpia, E., 2015. Effect of temperature, curing time, and filler composition on surface microhardness of composite resins. J. Conservative Dentistry 18 (2). https://doi.org/10.4103/0972-0707.153071.

Elkorashy, M.E., Shalaby, H.A., Khafagi, M.G., 2013. Effect of Curing Distance on the Degree of Conversion and Microhardness of Nano-Hybrid Resin Composites. January.

Ferracane, J.L., Mitchem, J.C., Condon, J.R., Todd, R., 1997. Wear and marginal breakdown of composites with various degrees of cure. J. Dent. Res. 76 (8), 1508–1516. https://doi.org/10.1177/00220345970760061401.

Ferracane, J.L., 1985. Correlation between hardness and degree of conversion during the setting reaction of unfilled dental restorative resins. Dent. Mater. 1 (1). https://doi.org/10.1016/S0109-5641(85)80058-0.

Hori, M., Fujimoto, K., Asakura, M., Nagase, Y., Mieki, A., Kawai, T., 2019. Measurement of exothermic heat released during polymerization of a light-curing composite resin: Comparison of light irradiation modes. Dent. Mater. J. 38 (4). https://doi.org/10.4012.dmj.2018-158.

Jandi, K.D., Mills, R.W., 2013. A brief history of LED photopolymerization. I. Dent. Mater. Vol. 29, Issue 6. https://doi.org/10.1016/j.dental.2013.02.003.

Knežević, A., Tarle, Z., Meniga, A., Štulato, J., Pichler, G., Ristić, M., 2001. Degree of conversion and temperature rise during polymerization of composite resin samples with blue diodes. J. Oral Rehabil. 28 (6). https://doi.org/10.1046/j.1365-2842.2001.00709.x.

Krämer, N., Lohbauer, U., Garcia-Godoy, F., Frankenberger, R., 2008. Light curing of resin-based composites in the LED era. I. Am. J. Dent. 21. Issue 3.

Leprince, J.G., Palin, W.M., Hadis, M.A., Devaux, J., Leclup, G., 2013. Progress in dimethacrylate-based dental composite technology and curing efficiency. Dent. Mater. 29 (2). https://doi.org/10.1016/j.dental.2012.11.005.

Maghaireh, G.A., Alzraikat, H., Taha, N.A., 2013. Assessing the irradiance delivered from light-curing units in private dental offices

Influence of radiant exposure on contraction stress, degree of conversion and mechanical properties of resin composites. Dent. Mater. 22 (9). https://doi.org/10.1016/j.dental.2005.11.008.
in Jordan. J. Am. Dent. Assoc. 144 (8) https://doi.org/10.14219/jada.archive.2013.0210.

Mitra, S.B., Wu, D., Holmes, B.N., 2003. An application of nanotechnology in advanced dental materials. J. Am. Dent. Assoc. 134 (10) https://doi.org/10.14219/jada.archive.2003.0054.

Morimoto, S., Zanini, R.A.M., Meira, J.B.C., Agra, C.M., Calheiroes, F.C., Nagase, D.Y., 2016. Influence of physical assessment of different light-curing units on irradiance and composite micro-hardness top/bottom ratio. Odontology 104 (3). https://doi.org/10.1007/s10266-015-0229-y.

Moszer, N., Fischer, U.K., Ganster, B., Liska, R., Rheinberger, V., 2008. Benzyl germanium derivatives as novel visible light photoinitiators for dental materials. Dent. Mater. 24 (7). https://doi.org/10.1016/j.dental.2007.11.004.

Mouhat, M., Mercer, J., Stangvaltuse, L., Örtengren, U., 2017. Light-curing units used in dentistry: factors associated with heat development—potential risk for patients. Clin. Oral Invest. 21 (5). https://doi.org/10.1007/s00784-016-1962-5.

Musanje, L., Darvell, B.W., 2003. Polymerization of resin composite restoration materials: Exposure reciprocity. Dent. Mater. 19 (6). https://doi.org/10.1016/S0109-5641(02)00101-X.

Nitta, K., 2005. Effect of light guide tip diameter of LED-light curing unit on polymerization of light-cured composites. Dent. Mater. 21 (3). https://doi.org/10.1016/j.dental.2004.03.008.

Nomoto, R., McCabe, J.F., Nitta, K., Hirano, S., 2009. Relative efficiency of radiation sources for photopolymerization. Odontology 97 (2). https://doi.org/10.1007/s00661-009-0105-8.

Pilo, R., Oelgiesser, D., Cardash, H.S., 1999. A survey of output intensity and potential for depth of cure among light-curing units in clinical use. J. Dent. 27 (3). https://doi.org/10.1016/S0300-5712(98)00052-9.

Price, R.B., DErand, T., Sedarous, M., Andreou, P., Loney, R.W., 2000. Effect of distance on the power density from two light guides. J. Esthetic Restorative Dentistry, 12(6). https://doi.org/10.1590/S1678-77572012000200015

Ribeiro, B.C.I., Boaventura, J.M.C., de Brito-Gonçalves, J., Rastelli, A.N. de S., Bagno, V.S., Saad, J.R.C., 2012. Degree of conversion of nanofilied and microybrid composite resins photo-activated by different generations of LEDs. J. Appl. Oral Sci., 20 (2), 212–217. https://doi.org/10.1590/S1678-77572012000200015

Rueggeberg, F.A., Caughman, W.F., Curtis, J.W., 1994. Effect of light intensity and exposure duration on cure of resin composite. Operative Dentistry 19 (1).

Rueggeberg, Frederick Allen, Giannini, M., Arrais, C.A.G., Price, R.B.T., 2017. Light curing in dentistry and clinical implications: A literature review. I. Brazilian Oral Res. 31. https://doi.org/10.1590/1807-3107BOR-2017.vol31.0061.

Segal, P., Lugassy, D., Mijiritsky, E., Dekel, M., Ben-Amar, A., Ormianer, Z., Matalon, S., 2015. The effect of the light intensity and light distances of LED and QTH curing devices on the hardness of two light-cured nano-resin composites. Mater. Sci. Appl. 06 (11). https://doi.org/10.4236/msa.2015.611106.

Shafadilla, V.A., Usman, M., Margono, A., 2017. Effects of distance from tip of LED light-curing unit and curing time on surface hardness of nano-filled composite resin. J. Phys. Conf. Ser. 884 (1). https://doi.org/10.1088/1742-6596/884/1/012095.

Shimokawa, C.A.K., Sullivan, B., Turbino, M.L., Soares, C.J., Price, R.B., 2017. Influence of emission spectrum and irradiance on light curing of resin-based composites. Operative Dentistry 42 (5). https://doi.org/10.2341/16-349-L.

Soh, M.S., Yap, A.U.J., Siow, K.S., 2003. The effectiveness of cure of LED and halogen curing lights at varying cavity depths. Operative Dentistry 28 (6).

Strassler, H.E., Price, R.B., 2014. Understanding light curing, Part I. Delivering predictable and successful restorations. I: Dentistry Today Vol. 33, Issue 5.

Vargas, M.A., Cobb, D.S., Schmit, J.L., 1998. Polymerization of composite resins: Argon laser vs conventional light. Operative Dentistry 23 (2).

Watanabe, H., Kazama, R., Asai, T., Kanaya, F., Ishizaki, H., Fukushima, M., Okiji, T., 2015. Efficiency of dual-cured resin cement polymerization induced by high-intensity LED curing units through ceramic material. Operative Dentistry 40 (2). https://doi.org/10.2341/13-357-L.

Weerakoon, A.T., Meyers, L.A., Symons, A.L., Walsh, L.J., 2002. Pulpal heat changes with newly developed resin photopolymerisation systems. Aust. Endodontic J. 28 (3). https://doi.org/10.1111/j.1747-4477.2002.tb00402.x.

Xu, X., Sandras, D.A., Burgess, J.O., 2006. Shear bond strength with increasing light-guide distance from dentin. J. Esthetic Restorative Dentistry 18 (1). https://doi.org/10.2310/6130.2006.00007.

Yoon, T.H., Lee, Y.K., Lim, B.S., Kim, C.W., 2002. Degree of conversion of dimethacrylate resin photo-activated with different light sources. J. Oral Rehabil. 29 (12). https://doi.org/10.1046/j.1365-2842.2002.00970.x.