Effect of Centrifugal Casting on Microstructures and Properties of Hypereutectic Al-18wt.%Si Alloy

Zhao CHEN1,a, Yong SU2,b, and Sheng-Wei GONG3,c

School of Material Science and Engineering, Hefei University of Technology, Hefei 230009, China

aemail address: chenzhao0807@163.com
bemail address: suyong1963@126.com
cemail address: gongshengwei1994@163.com

Key words: Centrifugal casting; Al-18wt.%Si Alloy; Primary Si; In-situ composites.

Abstract. Apply the centrifugal casting process to the preparation of hypereutectic Al-18% Si alloy cylinder liners. In-situ gradient composites of Al-18wt.%Si Alloy, which possess the microstructures of accumulated primary Si from outer layer to inner layer, have been acquired by changing the rotation rate of centrifugal casting. The distribution of primary Si, the microstructure and hardness of the material were investigated. It was found that with the increase of centrifugal rotation rate, the primary Si of the outer layer is gradually shifted to the inner layer. And the rate is greater, the primary Si refinement effect is better. Meanwhile, the hardness of the material increased with the increase of the number of the primary Si.

Introduction

Hypereutectic Al-Si alloy is an excellent wear-resistant materials, excellent casting properties, low coefficient of thermal expansion. Preparation of hypereutectic Al-Si alloy cylinder, compared with cast iron cylinder liners, a significant decline in weight, high thermal conductivity, improve engine efficiency, in addition to aluminum engine block due to the popularity of applications, high power operation, coefficient of thermal expansion of aluminum cylinder body and traditional cast iron cylinder liner vary widely, can cause distortion of the cylinder liner deformation, however, the use of high silicon aluminum alloy cylinder liner helps to improve engine life[1]. Centrifugal casting method of preparing Al-Si alloy cylinder liner has merit of the simple production process and high efficiency. Under centrifugal casting technology, small density primary phase segregates the interior part of the cast, so that it can greatly improve the wear resistance of the inside of the cylinder liner. Due to similar density of Al and Si (Al: \( \rho =2.7\text{g/cm}^3 \), Si: \( \rho =2.33\text{g/cm}^3 \)), the centrifugal rotation rate control is particularly important, the appropriate centrifugal rotation can improve segregation of primary silicon in the interior part of the cast, but also can avoid crack, segregation and other defects on the casting [2]. By changing the rotational rate of the centrifugal casting, study the segregation case of primary silicon of Al-18%Si alloy at different acceleration field, material microstructure and hardness.

Experimental method

Experimental materials

Using ZL109 alloy and industrial pure silicon as raw materials, the refining agent is C2Cl6, the modifier adopts Cu-P14 and Al-RE10 intermediate alloy, melting into Al-18wt.%Si alloy in the Crucible resistance furnace.
Experimental process

Horizontal centrifuge is used in this experiment. For the three tests, of which the centrifugal rotation rates respectively adopt 1300rpm, 1100rpm and 1600rpm, in addition to the different rotation rates, the same processes are as follows, before casting, metal mold will be preheated to 250°C. When the alloy begins to melt, the surface is covered with a layer of covering agent, and then the temperature is increased to a refining temperature. Furnace temperature to be stabilized, add C2Cl6 refining and let stand for 10 minutes, Slag with a skimming spoon, then quickly warmed to metastrophic temperature (800 ~ 820°C), until the temperature stabilizes, adding P-RE compound modifier. After stirring fully, the solution surface a layer of coating agent to prevent oxidation of the alloy, heat for 30 minutes, began to cool. After the temperature dropped to refining, refining once again. Standing, and then the temperature was raised to 800°C, poured into a metal mold centrifugal casting mold, using three different centrifugal rotation rate to complete centrifugal casting. Obtained castings by centrifugal casting as a cylindrical part, has a diameter of 90mm, a wall thickness of 10mm, a height of 400mm.

In the middle of casting, intercept a sample height of 20mm ring, then intercept on this sample width of 20mm square samples. Grinding and polishing the circular cross section of the sample in the radial direction, then etching it with aqueous solution of HF of a volume fraction of 0.5% for 20s. On the sample after etching, from the outer wall to the inner wall, in turn select three different fields of view, observe its microstructure under metallurgical microscope.

Experimental results and analysis

Metallographic structure analysis

Figure 1 shows the microstructure of castings in the radial cross-section, in which Fig. a, d, g is the outer layer of the cast microstructure, Fig. b, e, h is the middle layer of the cast microstructure, and Fig. c, f, i is the inner layer of the cast microstructure. When the rotational rate is 1100rpm, casting organizations do not exist obvious stratification, which is composed of the white dendritic α (Al), flocculent eutectic (α + Si) and bulk primary crystal silicon; When the rotational rate is 1300rpm, the outer layer is of the presence of α (Al) matrix and a large number of eutectic silicon and a small amount of primary silicon, the primary silicon has begun to significantly shifted the inner layer, the middle layer aggregates a portion of primary silicon, the inner layer of primary silicon is more, and the majority of the angular block; When the rotational rate is 1600rpm, the stratification is very clear. The outer layer is almost invisible to the primary silicon, which is composed of a large number of flocculent eutectic silicon and α (Al) matrix. The middle layer has a small part of the primary silicon gathered together. In the inner layer, a large number of bulk primary silicon is enriched, but the sizes and the edges of the primary silicon are smaller and less than that of the primary silicon when the rotational rate is 1300rpm.

In view of this, with increasing speed, primary silicon gradually shifted to the inner layer. And the faster rate, the more intense exercise, the collision with each other leads to that the massive primary silicon was fractured. It helps refine the primary silicon.

| Si     | Fe  | Cu  | Mn  | Mg  | Cr  | Ni  | Ti  | Al   |
|--------|-----|-----|-----|-----|-----|-----|-----|------|
| 18.076 | 0.249 | 4.619 | 0.04 | 0.185 | 0.152 | 4.172 | 0.019 | the remaining |
Fig.1 Microstructure of Al-18wt.%Si alloy (×100)
(a),(b),(c): 1100r/min; (d),(e),(f): 1300r/min; (g),(h),(i): 1600 r/min; (a),(d),(g): Outer layer;
(b),(e),(h): Middle layer; (c),(f),(i): Inner layer.

Hardness testing of casting samples in different locations

Using HV-1000 type micro Vickers hardness tester, were measured on the micro-hardness of the
alpha (AL) matrix and primary crystal Si, loading alpha phase is 10g, loading the primary silicon is
50g, and their loading times are 15s, the measured micro-hardness of alpha phase is 83.0HV, and
the micro-hardness of primary Si is 887.5HV. It can be known that the primary silicon as a hard
phase, the higher the content, the greater the hardness of materials.

Using HB-3000B type Brinell hardness tester, with a diameter of 5.0 mm steel ball head and the
load is 250KG, the loading time is 30s. On the sample of radial direction from outside to inside in
turn select the distance from the outermost 2.0, 5.0 and 8.0mm three different locations, each region
along the circumferential direction were tested three points, and then take the average. Meanwhile,
T6 heat-treatment for casting, and the heat-treatment process is: solid solution temperature of
515±5°C, solution time of 7h, artificial aging temperature of 185±5°C, aging time of 11h\(^4\). Repeat
the above work, and test the hardness of castings after heat-treatment.
Tab.2 Hardness of casting samples in different locations

| Grade Position | G 1100rpm# Cast | G 1100rpm# Heat-treatment | G 1300rpm# Cast | G 1300rpm# Heat-treatment | G 1600rpm# Cast | G 1600rpm# Heat-treatment |
|----------------|------------------|---------------------------|-----------------|---------------------------|-----------------|---------------------------|
| Outer layer    | 106.7            | 113.7                     | 98.0            | 102.7                     | 96.1            | 101.1                     |
| Middle layer   | 105.4            | 110.7                     | 103.9           | 108.2                     | 101.2           | 105.3                     |
| Inner layer    | 104.0            | 110.0                     | 114.3           | 118.0                     | 118.3           | 121.3                     |

When the rotating speed is 1100rpm, it has no hierarchical difference in castings hardness; when the rotating speed is 1300rpm and 1600rpm, middle layer and inner layer hardness is significantly higher than the outer layer and the inner layer hardness maximum; Consistent with the results of metallographic analysis, the primary silicon as a hard phase, the level of its content determines hardness of the material, when the rotational speed is 1100rpm, the primary silicon without segregation phenomenon, the primary silicon present segregation at speed of 1300rpm and 1600rpm, gathered from the outer to the middle layer and inner layer, the inner primary silicon content is higher, thus, its hardness is larger; When the rotating speed is 1600rpm, the inner layer hardness of casting reach to maximum, as 118.3 HBS.

In addition, the micro-hardness of α phase in the heat-treatment state was 95.9HV, which was significantly increased compared with the as cast state. This shows that the solid solution strengthening of the matrix was obtained after heat-treatment. According to the composition of the material, mainly due to the solubility of Cu under heating conditions significantly increased, namely to the second phase CuAl2 dissolve into the matrix. After quenching can obtain single supersaturated α phase solid solution, resulting in solid solution strengthening; Meanwhile, CuAl2 precipitated from the matrix in the aging process. Due to the small size, high dispersion, the ability to not easy to distort, also causing lattice distortion in the matrix to form the stress field, which has a clear blocking effect on the movement of the dislocation, thus increasing the plastic deformation resistance of the alloy to improve the strength and hardness\[^{[5]}-^{[6]}\]. This is consistent with the increase in hardness after heat treatment of castings. When the centrifugal rate reaches 1600rpm, the hardness of the cylinder liner’s inner layer can reach 121.3HBS after heat-treatment by T6.

Conclusion

(1) With the increase of centrifugal rotation rate, the primary Si of the outer layer is gradually shifted to the inner layer. When the rate reaches 1600rpm, the inner layer of the casting is formed as a primary silicon enrichment layer. And the faster rate, the more intense exercise,
the collision with each other leads to that the massive primary silicon was fractured. It helps refine the primary silicon;

(2) The hardness of Al-18%Si alloy composites is determined by the content of primary silicon. When the primary silicon content is in a gradient distribution, the hardness of the material also shows a gradient distribution;

(3) After heat-treatment by T6, the casting hardness will increase slightly. Mainly due to the solid solution strengthening of the matrix is obtained after heat-treatment. When the final centrifugal rotation rate reaches 1600rpm, the hardness of the cylinder liner’s inner layer can reach 121.3HBS after heat-treatment by T6.

Acknowledgements

This research is completed under the guidance of Professor Su. Here, thanks very much for his help.

References

[1] LAI Hua-qing, FAN Hong-xun, XU Xiang. Study and Application of Hypereutectic Al-Si Alloys[J]. Automobile Technology & Material, 2001 (10): 21-24.
[2] Wang Qudong, Ding Wen-jiang, Jin Jun-ze. In-situ Surface Composites Fabricated by Centrifugally Casting Hypereutectic Al-Si Alloy[J]. ACTA MATERIAE COMPOSITAE SINICA, 1998, 15(3):7-13.
[3] Criado A J, Martinez J A, Calabres R. Growth of eutectic silicon from primary silicon crystals in aluminum-silicon alloys[J]. Scripta Materialia, 1997, 36(l): 47-54.
[4] Sun Yu, Chen Jin, Sun Guo-xiong. Evolution of Si Phase in Al-Si Alloy and Its Effect on Mechanical Properties[J]. Special Casting & Nonferrous Alloys, 2006(6): 01-03.
[5] LI Run-xia, LI Rong-de, ZHAO Yu-hua. Effect of Heat-treatment on Eutectic Silicon Morphology and Mechanical Property of Al-Si-Cu-Mg Cast Alloys[J]. Trans. Nonferrous Met. Soc. China, 2004, 14(3): 496- 500.
[6] Wolverton C, Ozolins V. Entropically Favored Ordering: the Metallurgy of Al$_2$Cu Revisited[J]. PHYS REV LETT, 2001, 24(86): 5518-5521.