The Biomechanical Effect on the Adjacent L4/L5 Segment Under S1 Superior Facet Arthroplasty: A Finite Element Analysis

Zewen Shi
Ningbo University

Lin Shi
Ningbo No 2 Hospital: Ningbo Huamei Hospital University of Chinese Academy of Sciences

Xianjun Chen
Ningbo No 2 Hospital: Ningbo Huamei Hospital University of Chinese Academy of Sciences

Jiangtao Liu
Ningbo No 2 Hospital: Ningbo Huamei Hospital University of Chinese Academy of Sciences

Haihao Wu
Ningbo No 2 Hospital: Ningbo Huamei Hospital University of Chinese Academy of Sciences

Chenghao Wang
Ningbo No 2 Hospital: Ningbo Huamei Hospital University of Chinese Academy of Sciences

Zeming Chen
Ningbo University

Fang Yang
Ningbo University

Sheng Yu
Ningbo University

Qingjiang Pang (mailto:pangqingjiang@ucas.ac.cn)
Ningbo No 2 Hospital: Ningbo Huamei Hospital University of Chinese Academy of Sciences

Research article

Keywords: Superior facet, Finite element, Range of motion, Stress

DOI: https://doi.org/10.21203/rs.3.rs-142777/v1

License: © This work is licensed under a Creative Commons Attribution 4.0 International License. Read Full License
Abstract

Background. The superior facet arthroplasty is important for intervertebral foramen microscopy. To our knowledge, no study about the postoperative biomechanics of adjacent L4/L5 segments after different methods of S1 superior facet arthroplasty. To evaluate the effect of S1 superior facet arthroplasty on lumbar range of motion and disc stress of adjacent segment (L4/L5) under the intervertebral foraminal plasty.

Methods. Eight finite element models (FEMs) of lumbosacral vertebrae (L4/S) had been established and validated. The S1 superior facet arthroplasty was simulated with different methods. Then, the models were imported into Nastran software after optimization. 500N preload was imposed on the L4 superior endplate and 10 Nm was given to simulate flexion, extension, lateral flexion and rotation. The range of motion (ROM) and intervertebral disc stress of L4-L5 spine were recorded.

Results. The ROM and disc stress of L4/L5 increased with the increasing of the proportions of S1 superior facet arthroplasty. Compared with the normal model, the ROM of L4/L5 significantly increase in most directions of motion when S1 superior facet formed greater than 3/5 from ventral to dorsal or 2/5 from apex to base. The disc stress of L4/L5 significantly increase in most directions of motion when S1 superior facet formed greater than 3/5 from ventral to dorsal or 1/5 from apex to base.

Conclusion. In this study, the ROM and disc stress of L4/L5 were effected by the unilateral S1 superior facet arthroplasty. It is suggested that the forming range from ventral to dorsal should be less than 3/5 of S1 upper facet joint. It is not recommended to form from apex to base.

1. Introduction

In recent years, percutaneous transforaminal endoscopic discectomy (PTED) has been accepted as an alternative treatment for disc herniation due to its advantages over traditional open surgery[1–3]. However, the working channel is often difficult to establish in L5/S1 segment as high iliac crest, hyperplastic articular process and narrow foramen intervertebrale. In these cases, the articular process arthroplasty is needed[4]. In the long term, the degeneration of responsible segment and adjacent segments are clinically common after facet arthroplasty. Though the effect of S1 superior articular process arthroplasty on responsible segment had been reported[5], the effect on adjacent segment (L4/L5) has not been unreported.

In this study, finite element model was used to simulate S1 superior articular process arthroplasty. The S1 superior articular process was formed parallel to the S1 upper endplate from the apex to the base and perpendicular to the S1 upper endplate from the ventral to the dorsal. The effect of adjacent segment (L4/L5) biomechanical change was explored.

2. Materials And Methods

2.1. Research object and data collection

Eight healthy volunteers were selected, whose age range from 22 to 29 years old. X-ray of the lumbosacral vertebra was taken to exclude pathological conditions. Computed tomography scan of the lumbar spine was
obtained with 1.0 mm thickness. The work has been approved by the Hospital Ethical Committee (Hwa Mei Hospital, University of Chinese Academy of Science) and that subjects gave informed consent to the work.

2.2. Normal finite element model

The computed tomography images were post-processed for boundary detection with the Mimics 17.0 (Materialise, Belgium), then geometric models were established. Geomagic Studio 10.0 (Geomagic, USA) was used to import the spine modes for repair, noise reduction. Hypermesh 13.0 (Altair, USA) was used to generate the FE mesh for analysis. Nastran 2012 (MSC, USA) was used to construct finite element models (FEMs). The material properties of the model were listed in Table 1 using the results of previously published studies[1, 6, 7].

Table 1
Material properties of FE models

| Component                   | Element type                  | Elastic modulus (MPa) | Poisson ratio |
|-----------------------------|-------------------------------|-----------------------|---------------|
| Cortical bone               | Isotropc, elastic tetra element | 12000.0               | 0.30          |
| Cancellous bone             | Isotropc, elastic tetra element | 100.0                 | 0.20          |
| End plate                   | Nonlinear spring element      | 2000.0                | 0.20          |
| Fibres of annulus fibrosis  | Rebar                         | 92.0                  | 0.45          |
| Matrix of annulus fibrosis  | Neo-Hookean, hex element      | 4.2                   | 0.45          |
| Nucleus pulposus            | Incompressible fluid element  | 1.0                   | 0.50          |
| Anterior longitudinal ligament | Tension only, truss element  | 7.8                   | 0.30          |
| Posterior longitudinal ligament | Tension only, truss elements | 10.0                  | 0.30          |
| Supraspinous ligament       | Tension only, truss elements  | 8.0                   | 0.30          |
| Interspinous ligament       | Tension only, truss elements  | 8.0                   | 0.30          |
| ligamentum flavum           | Tension only, truss elements  | 10.0                  | 0.30          |
| Intertransverse ligament    | Tension only, truss elements  | 10.0                  | 0.30          |
| Capsular ligament           | Tension only, truss elements  | 15.0                  | 0.30          |
| Articular cartilage         | Nonlinear spring element      | 25.0                  | 0.40          |
| Articuli intervertebrales   | Sliding surface to surface contact | 10.0      | 0.30          |

2.3. The establishment of the facet arthroplasty finite element model

The surgical models were constructed based on the validated intact model (M1). Geomagic was used to simulate unilateral S1 superior superior articular process arthroplasty. The S1 superior superior articular
process was graded formed (1/5, 2/5, 3/5, 4/5, 5/5) parallelly to the S1 upper endplate from the apex to the base (transverse plasty) and perpendicularly to the S1 upper endplate from the ventral to the dorsal (longitudinal plasty), respectively. The models established were defined as M2-M10 (M2-M5 represents transverse plasty 1/5 – 4/5, M6-M9 represents longitudinal plasty 1/5 – 4/5, and M10 represents plasty 5/5) (Fig. 1).

2.4. Boundary and loading conditions

The inferior surface of the S1 vertebra was constrained completely (Fig. 2). A vertical load of 500 N and a torque of 10 N·M were applied to the L4 to simulate the weight of the body and various loading conditions of the lumbar spine. The torque along the axis generate flexion, extension, forming contralateral flexion, forming side flexion, forming contralateral rotation, forming side rotation. The ROM and intervertebral disc von Mises stress of adjacent segment (L4/L5) were quantified.

2.5. Statistical analysis

SPSS 19.0 software was adopted for statistical analysis in this study. Data was represented by x ± s. ANOVA was used between groups, and Dunnett analysis was used for pairwise comparison. Herein, P < 0.05 was considered to be statistically significant.

3. Results

3.1. Validation of the FEM

The displacement nephogram of normal model were acquired (Fig. 3). Intact FEMs were validated by comparing the ROM of the L4/L5 and L5/S1 with the results of the test performed by Yamamoto and Zhitaou Xiao[6, 7]. The ROM of the intact FEMs was in the range of reported data[6, 7], and the result had been published in previous study by our research group[5] (Table 2).

|                  | This study | Yamamoto’s study | Zhitaou Xiao’s study |
|------------------|-----------|------------------|----------------------|
|                  | Flexion extension | Lateral flexion | Lateral rotation | Flexion extension | Lateral flexion | Lateral rotation | Flexion extension | Lateral flexion | Lateral rotation |
| L4-L5            | 12.19 ± 2.61   | 11.46 ± 1.53    | 5.09 ± 1.22        | 14.8 ± 2.10        | 12.2 ± 2.25     | 3.7 ± 1.50       | 14.20             | 13.23             | 4.23             |
| L5-S1            | 14.67 ± 3.37   | 11.32 ± 1.85    | 3.06 ± 1.70        | 16.9 ± 2.05        | 11.3 ± 2.35     | 2.5 ± 0.75       | 17.29             | 12.56             | 2.70             |

3.2. ROM of L4/L5 segment

In transverse forming, ROM of L4/L5 increased significantly in lateral flexion and lateral rotation. The growth rates of forming contralateral flexion, forming side flexion, forming contralateral rotation and forming side rotation were 8%-18%, 4%-35%, 22%-27%, 0%-18%, respectively (Fig. 4a). In longitudinal forming, ROM of L4/L5
increased significantly in flexion, lateral flexion and axial rotation. The growth rates of flexion, forming contralateral flexion, forming side flexion, forming contralateral rotation and forming side rotation were 3%-17%, 2%-18%, 6%-35%, 5%-27% and 0%-18%, respectively (Fig. 4b).

3.3. Intervertebral disc stress of L4/L5 segment

In longitudinal and transverse forming, intervertebral disc stress of L4/L5 increased significantly in flexion, lateral flexion and forming contralateral rotation. In transverse forming, the growth rates of flexion, forming contralateral flexion, forming side flexion, forming contralateral rotation were 20%-27%, 22%-25%, 13%-17% and 30%-36%, respectively (Fig. 5a). In longitudinal forming, the growth rates of flexion, forming contralateral flexion, forming side flexion, forming contralateral rotation were 4%-27%, 9%-25%, 5%-17%, 4%-36%, respectively (Fig. 5b).

4. Discussion

Due to the anatomical characteristics of L5/S1 segment, posterior approach is generally the preferred method of spinal endoscopy. However, the posterior approach is difficult for patients with stenosis of vertebral canal, small inter-laminar space and extreme lateral lumbar disc herniation. In addition, research has shown that the lumbar instability would occur after the medial of inferior articular process is removed more than 1/2 through the posterior approach[8]. At this time, the posterolateral approach is needed. However, in L5/S1 segment, the superior articular process arthroplasty is usually needed to enlarge the foramen intervertebrale under posterolateral approach so as to reduce the interference in nerves and expand the surgical indications[9]. Unilateral S1 superior articular process reconstruction has a great impact on the biomechanics of the responsible segment, and the results has been published in previous studies by our research group[5]. Adjacent disc degeneration often occurs after PTED, and the annual risk rate of clinically related adjacent segmental diseases is reported to be 0.6–3.9%[10, 11]. However, there has been no consensus about the effects of S1 superior articular process forming on the biomechanics of adjacent L4/L5 segment. Hence, it is of great significance to explore the effect of S1 superior facet arthroplasty on the biomechanics of L4/L5 through finite element analysis, and indirectly reflect the effect of S1 superior articular process arthroplasty on the risk of adjacent segment degeneration.

The biomechanical study of facet joint and spinal degeneration has been deepened gradually, with the popularity of the technology of PTED. Matsuo et al[12] showed that the degenerative lumbar spondylolisthesis is significantly related to the sagittal and axial angles of the facet joints. It can be seen that the facet joint plays an important role in spinal degeneration. As we know, facet arthroplasty can reduce the stability and increase the risk of degeneration of the responsible segment[5, 13, 14]. However, the effect of S1 superior articular process arthroplasty on the ROM of adjacent L4/L5 segment has not been reported. The results of this study showed that the ROM of L4/L5 segment increased significantly in flexion, lateral flexion and lateral rotation, when the longitudinal forming was more than or equal to 3/5. Compared with the normal model, the difference was statistically significant. In lateral bending and lateral rotation, the ROM of L4/L5 segment increased significantly, when the transverse forming was more than or equal to 2/5. Compared with the normal model, the difference was statistically significant. These results suggest that the ROM of adjacent L4/L5 segment would be affected after the longitudinal shape of S1 superior articular process is more than or equal to 3/5 or the transverse shape is more than or equal to 2/5.
As we know, 25% of the axial compressive stress and 40%–65% of the rotational and shear stress of the lumbar spine are borne by the facet joint[15]. The increased stress of the intervertebral disc caused by the asymmetry of the articular process contributes to the increased risk of lumbar degeneration[16]. Qian et al[14] reported that 1/4 of L5 unilateral superior articular process forming could increase the stress of the same segment of intervertebral disc. However, few study about the effect of S1 superior facet arthroplasty on the adjacent disc stress has been reported. The results of this study showed that the disc stress of L4/L5 segment increased significantly in flexion, contralateral flexion and contralateral rotation after the longitudinal forming was more than or equal to 3/5. Compared with the normal model, the difference was statistically significant. In flexion, extension, lateral flexion and contralateral rotation, the disc stress of L4/L5 segment increased significantly after the transverse forming was more than or equal to 1/5. Compared with the normal model, the difference was statistically significant. It was worth noting that the stress of the L4/L5 disc increased most obviously when it rotated to the contralateral side of the forming. This is consistent with the statement that the facet joint plays a major role in the torsional stiffness of the intervertebral disc[17]. In other words, the disc stress of adjacent L4/L5 segment would be affected after the longitudinal form of S1 upper joint is more than or equal to 3/5 or the transverse form is more than or equal to 1/5, resulting in an increased risk of degeneration of adjacent segment.

In terms of experimental methods, three-dimensional finite element method has been widely used in orthopedic field, especially as a high simulation method in spine[18]. However, in another way, the accuracy of the research is decreased by the finite element method owing to it is a method of simplifying the complexity. In addition, this study infers the relationship between facet arthroplasty and adjacent segment degeneration from the immediate influence, failing to monitor the whole degeneration process dynamically. In the experimental design, the apex and basal part are common locations for S1 superior articular process arthroplasty. In addition, the original shape of foramen intervertebrale should be maintained and the destruction of anatomical structure should be reduced as far as possible. Two experimental methods were designed, parallel to S1 upper endplate from the top to the base and perpendicular to S1 upper endplate from ventral to dorsal under the premise of taking the upper edge of S1 pedicle as the lowest level.

5. Conclusions

In conclusion, the S1 superior articular process of the lumbar spine is not only of great significance to the biomechanics of the same segment, but also to the adjacent segment. It is possible that the stability of adjacent L4/L5 segment would be decreased and the stress of intervertebral disc would be increased after unilateral S1 superior facet arthroplasty. It is suggested to form ventral to dorsal of unilateral S1 Superior articular process arthroplasty should be controlled less than or equal to 3/5 and it is not recommended to form from apex to base, combining with the previous study of the effect of S1 superior articular process arthroplasty on the same segment[5]. Otherwise, the long term risk of adjacent segment degeneration would be increased.

List Of Abbreviations

Finite element models (FEMs)
Range of motion (ROM)
Percutaneous transforaminal endoscopic discectomy (PTED)

**Declarations**

**Ethics approval and consent to participate**

This study was approved by the Hospital Ethics Committee (Hwa Mei Hospital, the Affiliated Hospital of University of Chinese Academy of Science).

**Funding**

The Public Welfare Technology Research Program of Zhejiang Province (grant No.LGF19H060003), Natural Science Foundation of Zhejiang Province (grant No.LY16H060001), Natural Science Foundation of Ningbo (grant No. 2014A610244), Medical and Health Technology Plan Program of Zhejiang Province (grant No.2014KYB234), Medical and Health Technology Plan Program of Zhejiang Province (grant No.2019KY178).

**Conflicts of interest/Competing interests**

The authors declared that they have no conflicts of interest/competing interests to this work.

**Consent to participate**

Written informed consent for participate was obtained from all participants.

**Consent for publication**

Written informed consent for publication was obtained from all participants.

**Availability of data and material**

All data and material are fully available.

**Authors’ contributions**

Qingjiang Pang contributed to the conception of the study; Zewen Shi, Fang Yang, Zeming Chen, Sheng Yu performed the experiment; Lin Shi, contributed significantly to analysis and manuscript preparation; Zewen Shi, Jiangtao Liu, Haihao Wu performed the data analyses and wrote the manuscript; Xianjun Chen, Chenghao Wang helped perform the analysis with constructive discussions.

**Acknowledgements**

This work was supported by the Public Welfare Technology Research Program of Zhejiang Province (grant No.LGF19H060003), Natural Science Foundation of Zhejiang Province (grant No.LY16H060001), Natural Science Foundation of Ningbo (grant No. 2014A610244), Medical and Health Technology Plan Program of Zhejiang Province (grant No.2014KYB234), Medical and Health Technology Plan Program of Zhejiang Province (grant No.2019KY178).
References

1. Pan Z, Ha Y, Yi S, et al. Efficacy of transforaminal endoscopic spine System(TESSYS) technique in treating lumbar disc herniation. Med Sci Monit. 2016; 22(2): p. 530-9. doi:10.12659/msm.894870.

2. Kim JE, Choi DJ. Unilateral biportal endoscopic spinal surgery using a 30° arthroscope for L5-S1 foraminal decompression. Clin Orthop Surg. 2018; 10(4): p. 508-12. doi:10.4055/cios.2018.10.4.508.

3. Kapetanakis S, Gkasdaris G, Angoules AG, et al. Transforaminal Percutaneous Endoscopic Discectomy using Transforaminal Endoscopic Spine System technique: Pitfalls that a beginner should avoid. World J Orthop. 2017; 8(12): p. 874-880. doi:10.5312/wjo.v8.i12.874.

4. Sinkemani A, Hong X, Gao ZX, et al. Outcome of microen-doscopic discectomy and percutaneous transforaminal endoscopic discectomy for the treatment of lumbar disc herniation: a comparative retrospective study. Asian Spine J. 2015; 9(6): p. 833-40. doi:10.12659/MSM.913326.

5. Shi ZW, Liu JT, Yu X, et al. The biomechanical effects of graded upper articular process arthroplasty on lumbar spine: A finite element study. J Orthop Sci. 2020; 25(5): p. 793-799. doi: 10.1016/j.jos.2019.10.012.

6. Yamamoto I., Panjabi MM., Crisco T, et al. Three-dimensional movements of the whole lumbar spine and lumbosacral joint. Spine. 1989; 14(11): p. 1256-60. doi: 10.1097/00007632-198911000-00020.

7. Xiao Z, Wang L, Gong H, et al. Biomechanical evaluation of three surgical scenarios of posterior lumbar interbody fusion by finite element analysis. Biomed Eng Online. 2012; 11(1): p. 1-11. doi: 10.1186/1475-925X-11-31.

8. Adams MA, Hutton WC, Staff SRR. The resistance to flexion of the lumbar intervertebral joint. Spine. 1980; 5(3): p. 245-53. doi: 10.1097/00007632-198005000-00007.

9. Ning C, Wang Y, Xu F, et al. Percutaneous endoscopic lumbar discectomy by transfacet joint approach: a case report. Medicine. 2018; 97(48): p. e13373. doi: 10.1097/MD.0000000000013373.

10. Radcliff KE, Kepler CK, Jakoi A, et al. Adjacent segment disease in the lumbar spine following different treatment interventions. Spine J. 2013; 13(10): p. 1339-1349. doi: 10.1016/j.spinee.2013.03.020.

11. Lawrence BD, Hilibrand AS, Brodt ED, et al. Predicting the risk of adjacent segment pathology in the cervical spine: a systematic review. Spine. 2012; 37(22): p. 52-64. doi: 10.1097/BRS.0b013e31826d60fb.

12. Matsuo Y, Kaito T, Iwasaki M, et al. 3D morphometric analysis of laminae and facet joints in patients with degenerative spondylolisthesis. Mod Rheumatol. 2015; 25(5): p. 756-60. doi: 10.3109/14397595.2015.1008673.

13. Erbulut DU. Biomechanical effect of graded facetectomy on asymmetrical finite element model of the lumbar spin. Turk Neurosurg. 2014; 24(6): p. 923-8. doi: 10.5137/1019-5149.JTN.11984-14.2.

14. Qian J, Yu SS, Liu JJ, et al. Biomechanics changes of lumbar spine caused by foraminotomy via percutaneous transforaminal endoscopic lumbar discectomy. Zhonghua Yi Xue Za Zhi. 2018; 98(13): p. 1013-1018. Chinese. doi: 10.3760/cma.j.issn.0376-2491.2018.13.012.

15. Zeng ZL, Zhu R, Wu YC. et al. Effect of graded facetectomy on lumbar biomechanics. J Healthc Eng.2017; 20(17): p. 7981513. doi: 10.1155/2017/7981513.

16. Rong X, Wang B, Ding C, et al. The biomechanical impact of facet tropism on the intervertebral disc and facet joints in the cervical spine. Spine J. 2017; 17(12): p. 1926-1931. doi: 10.1016/j.spinee.2017.07.009.
17. Bezci SE, Eleswarapu A, Klineberg EO, et al. Contribution of facet joints, axial compression, and composition to human lumbar disc torsion mechanics. J Orthop Res; 2018. doi: 10.1002/jor.23870.

18. Imai K, Ohnishi I, Bessho M, et al. Nonlinear finite element model predicts vertebral bone strength and fracture site. Spine. 2006; 31(16): p. 1789-94. doi: 10.1097/01.brs.0000225993.57349.df.

Figures

Figure 2

Normal lumbosacral vertebral finite element model

Figure 3
Normal model displacement nephogram

Figure 4
Lumbar motion of L4/L5 segment after S1 superior facet arthroplasty

Figure 5
Lumbar disc stress of L4/L5 segment after S1 superior facet arthroplasty