High rate oxygen reduction reaction during corrosion of ultra-high-purity magnesium

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Comprehending the corrosion mechanism of magnesium is of major interest in diverse fields. Typically, hydrogen evolution reaction is considered as the only cathodic reaction during Mg corrosion. However, recent works demonstrate importance of considering oxygen reduction reaction (ORR) as a second cathodic process at specific conditions. With oxygen micro-optode, we show that ORR rate was higher on slower corroding ultra-high-purity Mg (UHP-Mg), while lower on faster corroding commercially pure Mg (CP-Mg), where massive hydroxide layer impeded oxygen permeation. These findings shed light on yet another facet of complex mechanism of Mg corrosion.

npj Materials Degradation (2020)4:42; https://doi.org/10.1038/s41529-020-00146-1

Magnesium, owing to its low density and high strength-to-weight ratio, has become a fascinating technological material attracting enormous academic and industrial interest. However, limited corrosion resistance of Mg confines its structural application including aerospace, automotive, and biomedical fields. Hence, promoting the understanding of the fundamental principles of corrosion behavior paves the path to further enhancement of corrosion protection for Mg and extends its industrial application.

It has been extensively acknowledged that hydrogen evolution reaction (HER) is the main cathodic reaction during Mg corrosion at neutral or even alkaline conditions unlike other metals (zinc, iron etc.), where oxygen reduction reaction (ORR) is the main cathodic process. A convincing explanation for the predominance of HER is the highly negative corrosion potential exhibited by Mg.

Even though compelling evidence supports HER as the primary cathodic reaction, ORR, as a secondary cathodic reaction, has progressively earned its value in the corrosion behavior of Mg and its alloys. It has been reported that ORR might participate in the formation of corrosion products of AZ91D during NaCl induced atmospheric corrosion. Wang et al. found that AZ31 exhibited different potentiodynamic behaviors in NaCl under deaerated and aerated conditions, where ORR caused higher current density. Recently, dissolved oxygen (DO) was found to be consumed on the surface of Mg coupled to Al and Cu, which certainly was not expected. Afterwards, direct DO consumption was measured by Silva et al. in active, and even relatively passive, corrosion regions of CP-Mg in NaCl solution. Simultaneous measurements of local DO concentration and current density (by SVET) was performed. Moreover, Strebl et al. provided the evidence for the contribution of ORR to cathodic processes on Mg alloy during atmospheric corrosion. In spite of these compelling evidences collected by different scientific groups, varying conditions and methods, the essential role of ORR during corrosion of Mg remains largely unexplored and poses a number of questions.

In Mg corrosion research, impurities, especially Fe particles embedded in Mg matrix have been considered as suitable cathodically active sites. Thus, cathodic reaction and growth kinetic of corrosion products have been significantly influenced by size, content, and distribution of impurities, which probably have potential relevance to ORR. The relation between impurities and oxide growth kinetic on Mg surface under ambient exposure condition was reported by McIntyre and Chen two decades ago. They found that Mg containing impurities of iron or manganese oxidized more rapidly than pure Mg and intensifying oxidation was found around impurities. DO consumption was detected by Xavier et al. during corrosion process occurring on Fe/Mg couple immersed in 0.1 M NaCl aqueous solution by setting different tip potential of scanning electrochemical microscopy. Höche et al. discovered that Fe and other noble metal impurities could re-deposit on Mg surface and enlarge the cathodic area. Further experimental evidence for Fe re-deposition was supplied by Mercier et al. A similar mechanism for Cu re-deposition during AZ91 corrosion was proposed and conclude that Cu could not be protected by Mg and tended to be oxidized due to the involvement of ORR. However, it has not been clarified until now whether the contribution of ORR to cathodic process is constant or it differs for Mg of varying purity grades and degradation rates.

In this work, oxygen consumption on Mg of two different purity grades was systematically investigated by in situ monitoring DO concentration in a mildly aggressive medium with localized techniques. This comparative study aimed at understanding the correlation between the intensity of ORR and impurity level. The evolution of Mg corrosion was elaborated regarding the variation of oxygen consumption particularly at the initial stage prior to visible filiform corrosion.

COUNTERINTUITIVELY HIGH RATE ORR ON SLOWLY CORRODING UHP-MG

Figure 1a shows the distribution of local concentration of DO over the surfaces of CP-Mg and UHP-Mg immersed in 0.05 M NaCl electrolyte recorded by a micro-optode DO sensor. Clear consumption of DO was observed on both specimens, and DO
consumption was higher in the middle of the sample typical for a diffusion-controlled ORR. This primarily indicates that ORR occurred all over Mg surface rather than exclusively on cathodic impurities. The lowest detected DO concentration was 2.5 ppm on UHP-Mg while 5.1 ppm on CP-Mg. This was unexpected because the corrosion rate of UHP-Mg was much lower than that of CP-Mg as also shown by the results of hydrogen evolution and accompanying weight loss measurements (Table 1). At first sight, one could expect higher rate of oxygen reduction during cathodic process on CP-Mg.

Considering the variation of DO concentration is also time-dependent, DO concentration was continuously measured in the midpoint of the sample in order to capture the time-varying process and avoid the edge effect (Fig. 1b). Once the specimens encountered the electrolyte, DO concentrations close to the magnesium/electrolyte interface sharply decreased due to the

![Image](image_url)

**Fig. 1** CP-Mg and UHP-Mg in air saturated 0.05 M NaCl electrolyte. a the visual appearance and distribution of oxygen concentration above the surface. b the evolution of local DO concentration in the midpoint of each sample.

| Sample | Evolved hydrogen (mL cm\(^{-2}\)) | Weight loss calculated from evolved hydrogen (mg cm\(^{-2}\)) | Weight loss (mg cm\(^{-2}\)) | Contribution of ORR (%) |
|--------|-----------------------------------|-------------------------------------------------|----------------------------|------------------------|
| CP-Mg  | 59.3 ± 2.3                        | 61.1 ± 2.5                                      | 61.9 ± 2.7                 | 1.3 ± 0.4              |
| UHP-Mg | 1.11 ± 0.06                       | 1.45 ± 0.01                                     | 1.74 ± 0.02                | 16.5 ± 0.3             |
suddenly fierce ORR. The minimum DO concentration on UHP-Mg remained longer than that on CP-Mg, indicating that ORR rate maintained persistently higher on UHP-Mg. Subsequently, DO consumption was impeded, and DO concentration above CP-Mg started to increase and reached ~6.8 ppm in 1 h. By contrast, a moderate increase of DO concentration was displayed on UHP-Mg resulting in 4.6 ppm after 1 h, manifesting incessant DO consumption on the surface of UHP-Mg. The linear increment of DO concentration demonstrated that ORR rate decreased constantly and reach the plateau in 1 h due to the oxygen diffusion control. The difference of ORR rate observed for two grades of Mg was explained by different permeability of formed Mg(OH)2 to O2 dissolved in NaCl electrolyte.

**CONSIDERABLE CATHODIC ORR CONTRIBUTION ON SLOWLY CORRODING MG**

The results of this work promote better understanding of underlying mechanism of magnesium corrosion. Commonly, hydrogen evolution test is a typical measurement to quantify the corrosion rate of Mg. However, for magnesium possessing low degradation rate, ORR plays a significant role in total cathodic process. Strebl et al. estimated that during atmospheric corrosion of AZ91 alloy, ORR contribution to total cathodic reaction may reach 60% at certain relative humidity. Concomitantly, benefitting from the sealed construction of the eudiometer, ORR contribution to the total cathodic process was calculated based on the evolved hydrogen and weight loss after 24 h (Table 1). For slowly corroding UHP-Mg, the contribution of oxygen reduction reaction to the total cathodic process was reaching up to ~16.5%, while for faster corroding CP-Mg this contribution was at least ten times smaller, accounting only to 1.3%. Even though these values were calculated using H2 collection and weigh loss measurements which are certainly subjected to experimental errors probably of the order of those attributed to the ORR, in particular for the systems with low corrosion rates, measuring only HER (by H2 evolution test) leads to underestimated values of corrosion rates for slowly corroding Mg and its alloys. The most reliable test method in this case remains the weight loss measurement. The difference between the corrosion rate derived from hydrogen evolution and weight loss measurements has been reported before. Typically, this difference was attributed to rather high solubility of hydrogen gas in test electrolyte. This, obviously, remains a valid argument, but significant contribution of ORR should be also taken into account. Understanding the function of dissolved oxygen would not only provide insights into the fundamental research but also enlighten innovations in corrosion control strategies.

In summary, this work demonstrated that a significant amount of oxygen was consumed for ORR during corrosion of Mg in 0.05 M NaCl electrolyte. Most interesting, the higher level of oxygen consumption was revealed for slower corroding ultra-high-purity Mg.
Mg, compared to lower rate of oxygen consumption by commercially pure Mg. Although the corrosion rate of two materials correlated with the level of impurities, ORR rate was two times higher for UHP-Mg at the initial corrosion stage (remaining DO concentration 2.5 ppm for UHP-Mg vs 5.1 ppm for CP-Mg in Fig. 1a). This counterintuitive behavior was explained by different morphology of main corrosion product, Mg(OH)\(_2\) formed on Mg surface immediately upon immersion. Thinner Mg(OH)\(_2\) generally formed on slowly dissolving UHP-Mg (ca. 70 nm) allowing diffusion of dissolved oxygen to the Mg/Mgo\(_2\) interface. Stacked Mg(OH)\(_2\) formed on rapidly corroding CP-Mg (ca. 280 nm thick) restricted diffusion of oxygen molecules to CP-Mg interface. Moreover, CP-Mg interface could also be covered by \(\mathrm{H}_2\) bubbles, hampering surface interaction with \(\mathrm{O}_2\) molecules. These results provided additional experimental evidence for the strong role of ORR in corrosion of magnesium. The corrosion rates estimated based on \(\mathrm{H}_2\) evolution measurements underestimate the actual corrosion damage, more precisely shown by weight loss analysis, and the difference is especially high for slowly corroding magnesium.

**METHODS**

**Samples**

Commercially pure Mg (CP-Mg) and ultra-high-purity Mg (UHP-Mg; the elemental composition shown in Table 2) were machined in the rod shape (\(\Phi = 2 \text{ mm}\)) and embedded in epoxy resin with a round face exposed as a working surface (Fig. 1). The specimens were abraded successively with SiC papers from 1000 grit to 4000 grit and then cleaned in absolute ethanol. The test electrolyte was 0.05 M NaCl aqueous solution (pH = 5.8) prepared using deionized water and analytical grade reagent.

**Instrumentation**

A FireStingO2 fiber-optic oxygen micro-sensor coupled with an oxygen concentration meter, both from PyroScience\textsuperscript{TM} were employed to monitor the DO concentration. A needle-type retractable micro-otode with the diameter of 50 \(\mu\)m detected the DO concentration locally, 50 \(\mu\)m above the surface (Fig. 1). The specimens were sputtered with a protective layer of platinum. FIB milling was subsequently adapted to produce a thin foil (~100 nm thick) via the standard in situ lift-out sample preparation routine in order to produce electron transparent lamellae.\textsuperscript{30} The cross-section micrographs were taken in STEM mode with the accelerating voltage of 30 kV.

**REFERENCES**

The authors declare that all data supporting the findings of this study are available within the paper.

Received: 1 July 2020; Accepted: 18 November 2020;
Published online: 23 December 2020

| Table 2. The elemental composition of CP-Mg and UHP-Mg. |
|---|---|---|---|---|---|---|---|---|
| Element content/wt.% | Fe | Si | Mn | Al | Cu | Ni | Zr | Mg |
| CP-Mg | 0.0342 | 0.0001 | 0.00237 | 0.00402 | 0.00037 | <0.0002 | <0.0005 | Bal. |
| UHP-Mg | 0.0012 | <0.0001 | 0.00037 | 0.00291 | <0.0002 | <0.0005 | Bal. |

**DATA AVAILABILITY**

Projects generated during this study and bioinformatics data will be available to the community on request.

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npj Materials Degradation (2020) 42
Published in partnership with CSCP and USBT
ACKNOWLEDGEMENTS

Mr. Cheng Wang, Mr. Di Mei, Ms. Linqian Wang, and Mr. Min Deng thank China Scholarship Council for the award of fellowship and funding (No. 201806310128, 201607040051, 201706370183, and 201606370031). The technical support of Mr. Daniel Streath, Mr. Volker Heitmann, and Mr. Ulrich Burmester during this work is gratefully acknowledged.

AUTHOR CONTRIBUTIONS

C.W. conducted the experiments, data analysis, plotted figures, and wrote the first draft of the manuscript. D.M. and G.W. conducted experiments. D.M., L.W., and M.D. contributed to data analysis and plotting figures. S.V.L. contributed to establishing experimental approaches, plotting figures and writing text. S.V.L. and M.L.Z. contributed to developing the overall research strategy, data analysis, manuscript review, and supervised the work. All coauthor read and edited the manuscript.

FUNDING

Open Access funding enabled and organized by Projekt DEAL.

COMPETING INTERESTS

The authors declare no competing interests.

ADDITIONAL INFORMATION

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