Protocol Article

Data on the removal of fluoride from aqueous solutions using synthesized P/γ-Fe₂O₃ nanoparticles: A novel adsorbent

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A B S T R A C T

High concentration of fluoride above the optimum level can lead to dental and skeletal fluorosis. The data presents a method for its removal from fluoride-containing water. P/γ-Fe₂O₃ nanoparticles was applied as an adsorbent for the removal of fluoride ions from its aqueous solution. The structural properties of the P/γ-Fe₂O₃ nanoparticles before and after fluoride adsorption using the Fourier transform infrared (FTIR) technique were presented. The effects of pH (2–11), contact time (15–120 min), initial fluoride concentration (10–50 mg/L) and P/γ-Fe₂O₃ nanoparticles dosage (0.01–0.1 g/L) on the removal of F⁻ on P/γ-Fe₂O₃ nanoparticles were presented with their optimum conditions. Adsorption kinetics and isotherm data were provided. The models followed by the kinetic and isotherm data were also revealed in terms of their correlation coefficients (R²).

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Keywords: Fluoride, P/γ-Fe₂O₃ nanoparticles, Aqueous solution, Isotherm, Kinetic

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Specifications Table

- Subject area
- More specific subject area
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2215-0161/© 2018 The Author(s). Published by Elsevier B.V. This is an open access article under the CC BY license (http://creativecommons.org/licenses/by/4.0/).
• Type of data
  • Image, table, and figure

• How data was acquired
  • All adsorption experiments were done in batch mode. After the adsorption process, the residual fluoride concentrations were estimated. The initial and residual fluoride concentrations in the solutions were analyzed using a UV-visible recording spectrophotometer (Shimadzu Model, CE-1021–UK) at 570 nm. Fourier-transform infrared spectroscopy (FT-IR) was done on a JASCO 640 plus machine (in the range of 400–4000 cm⁻¹) to determine the functional groups present in the adsorbent before and after fluoride adsorption. The pH of the solution was measured using a MIT65 pH meter.

• Data format
  • Raw and analyzed

• Experimental factors
  • The influence of pH, contact time, initial fluoride concentration and P/γ-Fe₂O₃ nanoparticles dosage on the adsorption process. Kinetic and isotherm parameters were also presented.

• Experimental features
  • Fluoride removal from aqueous solution using P/γ-Fe₂O₃ nanoparticles. P/γ-Fe₂O₃ nanoparticle characterization data obtained from FTIR. Kinetic and isotherm modeling of the removal process.

• Trial registration
  • Not applicable

• Ethics
  • Not applicable

Protocol data

• The presented data established that P/γ-Fe₂O₃ nanoparticles can be applied for the removal of fluoride with great efficiency.
• Data on the isotherm, kinetics, and effect of process variables were provided, which can be further explored for the design of a treatment plant for the treatment of fluoride-containing industrial effluents where a continuous removal is needed on a large scale.
• FTIR data for P/γ-Fe₂O₃ nanoparticles were also provided.
• The dataset will also serve as a reference material to any researcher in this field.

Description of protocol

Data

High concentration of fluoride is toxic and causes digestive disorders, fluorosis, endocrine, thyroid and liver damages, and also decreases the growth hormone [1,2]. In addition, it influences the metabolism of some elements such as calcium and potassium [3]. Fluoride must be properly reduced before its discharge to the water bodies. Adsorption can be considered as an effective method for the removal of fluoride [4,5]. The applicability of P/γ-Fe₂O₃ nanoparticles for fluoride removal was reported. Fourier transform infrared (FTIR) on the P/γ-Fe₂O₃ nanoparticles is given in Fig. 1. Fig. 2 shows the schematic illustration for the synthesis of P/γ-Fe₂O₃ nanoparticles. The functional groups present in the P/γ-Fe₂O₃ nanoparticles before and after fluoride adsorption are given in Table 1. The estimated adsorption isotherm and kinetic parameters are presented in Table 2.
Adsorption experiments

The adsorption experiment was conducted at batch mode using the one-factor-at-a-time (OFAT) method, that is, keeping a factor constant and varying the other factors to get the optimum condition of each variable. At first, for the purpose of this study, a stock solution of fluoride was prepared with distilled water from which other fluoride concentrations were prepared. The stock solution of fluoride (concentration of 1000 mg/L) was made by dissolving 2.21 g NaF in 1000 mL distilled water. A known mass of adsorbent (P/γ-Fe₂O₃ nanoparticles) was added to 1 L of the water samples containing different concentrations of fluoride. The pH of the water sample was adjusted by adding 0.1 N HCl or NaOH solutions. The removal efficiency was determined by varying the different adsorption process parameters such as pH (2–11), contact time (15–120 min), initial fluoride concentration (10–50 mg/L) and P/γ-Fe₂O₃ nanoparticles dosage (0.01–0.1 g/L). To create optimal conditions, the solutions were agitated using orbital shaker at a predetermined rate (150 rpm). After each experimental run, the solution was filtered and the filtrate was analyzed for the residual fluoride concentration. The initial and residual fluoride concentrations in the solutions were analyzed by a UV–vis recording spectrophotometer (Shimadzu Model: CE-1021-UK) at a wavelength of absorbance (λ_max): 570 nm [5].

Data analysis

The removal efficiency, \( R \) (%) and amount of fluoride adsorbed on P/γ-Fe₂O₃ nanoparticles, \( q_e \) (mg/g) of the studied parameters were estimated based on the following formulas [6–8]:

\[
\%R = \left(\frac{C_0 - C_f}{C_0}\right) \times 100
\]

(1)

Where \( C_0 \) and \( C_f \) are the initial and residual fluoride concentrations (mg/g), respectively.

\[
q_e = (C_0 - C_e) \times \frac{V}{M}
\]

(2)

Where \( C_0 \) and \( C_e \) are the initial and final equilibrium liquid phase concentration of fluoride (mg/g), respectively. \( M \) is the weight of the nano adsorbent (g) and \( V \) is the volume of the solution (L).
Influence of process variables

In this research, the influence of pH (2 - 11), contact time (15 - 120 min), initial fluoride concentration (15 - 50 mg/L) and P/γ-Fe₂O₃ nanoparticles dosage (0.01 - 0.1 g/L) on the removal efficiency was investigated.
Higher removal efficiency was obtained at pH of 7 (Fig. 3), an adsorbent dosage of 0.02 g/L (Fig. 4), the initial fluoride concentration of 25 mg/L (Fig. 5) and contact time of 60 min (Fig. 5). This optimum conditions of pH 7, adsorbent dosage: 0.02 g/L, contact time: 30 min and initial fluoride concentration: 25 mg/L gave an efficiency of 99% (Fig. 5).

### Isotherm and kinetic modeling

An important physiochemical subject in terms of the evaluation of adsorption processes is the adsorption isotherm, which provides a relationship between the amount of fluoride adsorbed on the
solid phase and the concentration of fluoride in the solution when both phases are in equilibrium [9].

To analyze the experimental data and describe the equilibrium status of the adsorption between solid and liquid phases, the Langmuir, Freundlich, and Temkin isotherm models were used to fit the adsorption isotherm data.

Several kinetic models have been applied to examine the controlling mechanisms of adsorption processes such as chemical reaction, diffusion control, and mass transfer [10]. Three kinetics models, namely pseudo-first-order, pseudo-second-order, and intraparticle diffusion models were used in this study to investigate the adsorption of fluoride on P/γ-Fe₂O₃ nanoparticles.

**Langmuir isotherm**

For the Langmuir model, it is assumed that adsorbates attach to certain and similar sites on the adsorbent’s surface and the adsorption process occurs on the monolayer surface. The Langmuir equation can be rearranged to linear form for the convenience of plotting and determining the

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**Fig. 4.** Effect of adsorbent dosage on the removal efficiency of fluoride. (Contact time: 30 min, optimum pH: 7, initial fluoride concentration: 10 mg/L).

**Fig. 5.** Effect of initial fluoride concentration on the removal efficiency of fluoride (optimum P/γ-Fe₂O₃ nanoparticles dosage: 0.02g/L, optimum pH: 7).
isorbent constants, $K_L$ and $q_m$ by drawing a curve of $1/q_e$ versus $1/C_e$ [11,12]:

$$\frac{C_e}{q_e} = \frac{C_e}{q_m} + \frac{1}{q_m K_L}$$

(3)

Where $q_e$ (mg/g) is the amount of fluoride adsorbed per specific amount of adsorbent, $C_e$ is the equilibrium concentration of the fluoride solution (mg/L), $K_L$ (L/mg) is Langmuir constant, and $q_m$ (mg/g) is the maximum amount of fluoride required to form a monolayer.

**Freundlich isotherm**

The Freundlich model is an empirical relationship between the parameters, $q_e$, and $C_e$. It is obtained by assuming a heterogeneous surface with nonuniform distribution of the adsorption sites on the adsorbent surface, and can be expressed by the following equation [13,14]:

$$q_e = K_f C_e^{1/n}$$

(4)

Where $K_f$ and $1/n$ are the Freundlich constants related to adsorption capacity and adsorption intensity, respectively. The Freundlich constants can be obtained by plotting a graph of Log $q_e$ versus Log $C_e$ based on the experimental data by applying the linear form of the Freundlich isotherm Eq. (4):

$$\log(q_e) = \log(K_f) + \frac{1}{n} \log(C_e)$$

(5)

**Temkin isotherm**

In Temkin model, the surface adsorption theory was corrected considering possible reactions between the adsorbent and adsorbate. This model can be expressed as the following equation [15]:

$$q_e = B_1 \ln(A_T) + B_1 \ln(C_e)$$

(6)

Where $A_T$ and $B_1$ are the Temkin constants. $B_1$ is related to the heat of adsorption and $A_T$ is the equilibrium binding constant.

**Lagergren kinetic model**

Adsorption kinetic models are used to examine the rate of adsorption process and the potential rate controlling step. The Lagergren (pseudo-first-order) rate equation is expressed as Eq. (7) [16,17]:

$$\log(q_e - q_t) = \log(q_e) - \frac{k_1}{2.303} t$$

(7)

**Ho kinetic model**

The Ho (pseudo-second-order) rate equation is given as [12,18]:

$$\frac{t}{q_t} = \frac{1}{K_2} + \frac{1}{q_e} t$$

(8)

Where $q_e$ (mg g$^{-1}$) and $q_t$ (mg g$^{-1}$) are the amounts of fluoride adsorbed at equilibrium and at time $t$, respectively, $k_1$ (min$^{-1}$) is the pseudo-first-order rate constant of adsorption, and $K_2$ (g mg$^{-1}$ min$^{-1}$) is the pseudo-second-order rate constant.

**Intraparticle diffusion**

For the intraparticle diffusion model (Eq. (9)), $c$ is the intercept (mg/g) and $K_{pi}$ is the slope. If intraparticle diffusion is involved in the adsorption process, then the plot of $t_{0.5}$ versus $q_t$ would result
in a linear relationship, and the intraparticle diffusion would be the controlling step if this line passed through the origin \((C = 0)\). When the plots do not pass through the origin \((C \neq 0)\), this is indicative of some degree of boundary layer control and this further shows that the intraparticle diffusion is not the only rate controlling step, but also other processes may control the rate of adsorption \([19,20]\).

\[
q_t = K_{pi}t^{0.5} + c
\]

(9)

Where \(q_t\) (mg/g) is the amount of fluoride adsorbed at time \(t\) (min) and \(K_{pi}\) (mg/g min) is the intraparticle diffusion model rate constant.

The estimated adsorption isotherm and kinetic parameter are presented in Table 2. Fig. 6 shows the adsorption kinetic (Ho) plot for fluoride removal on P/γ-Fe2O3 nanoparticles. The removal of fluoride on P/γ-Fe2O3 nanoparticles followed the Ho kinetic model with a correlation coefficient \((R^2)\) of 0.999 at 25 mg/L, suggesting that the rate-limiting step is a chemical adsorption process \([21]\). The isotherm data fitted into the Freundlich, Langmuir and Temkin isotherms but fitted more to the Langmuir isotherm, which indicates a monolayer adsorption on a homogeneous surface \([14]\).

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