The effect of span length and girder type on bridge costs

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Abstract. Bridges have an important role in impacting the civilization, growth and economy of cities from ancient time until these days due to their function in reducing transportation cost and time. Therefore, development of bridges has been a knowledge domain in civil engineering studies in terms of their types and construction materials to confirm a reliable, safe, economic design and construction. Girder-bridge of concrete deck and I-beam girder has been used widely for short and medium span bridges because of ease and low-cost of fabrication. However, many theoretical and practical investigations are still undertaken regarding the type of beam girder; i.e steel composite or prestressed concrete. This paper evaluates the effect of bridge span and the type of girder on the capital cost and life cycle costs of bridges. Three types of girders were investigated in this research: steel composite, pre-tensioned pre-stressed concrete and post-tensioned pre-stressed concrete. The structural design was analyzed for 5 span lengths: 20, 25, 30, 35 and 40m. Then, the capital construction cost was accounted for 15 bridges according to each span and construction materials. Moreover, the maintenance required for 50 years of bridge life was evaluated and built up as whole life costs for each bridge. As a result of this study, the influence of both span length and type of girder on initial construction cost and maintenance whole life costs were assessed to support the decision makers and designers in the selection process for the optimum solution of girder bridges.

1 Introduction

Bridges have an important role in impacting the civilization life due to their function in reducing transportation cost and time. Therefore, the demand of bridges has been expanded dramatically these days in most countries. For example, it is registered that almost 1500 bridges per year were built in the USA between years 1996 to 2006 [1]. In Dubai, it is recorded that bridges reaches a number of 347 at the end of 2012[2]. Subsequent to this considerable increase in bridges number, low cost bridge construction is a big challenge facing the designer.

In this study, the cost of simply supported I-beam girder-bridge is investigated since it is the most popular because of ease and low-cost of fabrication together with its suitability for short and medium span. Furthermore, Boatman (2010)[3] explores that the service life for

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steel composite I-Beam or pre-stressed I-beam is about 45 years which is 17 years more than using box-girder beam. This is another reason behind choosing I-beam for this study. On the other hand, three kinds of construction materials are selected for the girders of bridge: steel composite girder, pre-tensioned pre-stressed concrete girder and post-tensioned pre-stressed concrete girder. Then, the effect of bridge span and the type of girder on the capital cost and life cycle costs of bridges is evaluated.

Many researchers have tried to answer the question of girder-bridge cost in respect of both span length and life cycle. For example, Jagtab and Shahezad (2016) [4] studied various spans of I-girder bridge to compare between the initial cost of using pre-stressed concrete girder or steel girder. In their work, it was found that steel beam is preferable for short span length up to 15m. Whereas, pre-stressed concrete girder is more economical in 37% for 24m span length. The saving may reach 46% for 36m span length. In 2016, Singh et al. [5] discussed two different span lengths for I-beam girder bridge: 20 m and 25m. Life service of 100 years was taken into consideration in the cost estimation. As a conclusion of their work, the pre-stressed I-girder bridge is the lowest cost compared to the composite steel I-girder. The concluded saving was 10% and 15% for 20m-span and 25m-span respectively. It is worth mentioning that Florida Department Of Transportation (FDOT) estimates the average cost of construction Pre-stress concrete I-girder simple span bridge as 12% less than using steel girder [6]. However, more studies still need to be undertaken to answer the bridge cost question according to span and materials in use where this paper analysed these costs for different spans.

2 Structural analysis of different simple-span bridges

2.1 Geometry, material properties and loading

Five simply supported Bridges of different span-lengths were studied in this paper: 20, 25, 30, 35 and 40m. The section of girder-bridge is shown in Figure 1. The distance among girders is 2.25m with slab thickness of 200mm and carriageway of 6.95m. The concrete barrier has a self-weight of 6.22kN/m. While, 5kN/m2 was assumed for both asphalt self-weight and service loading. Using BD 37/01 (2002) [7], live loads was applied to bridge as HA-UDL of 12.4 kN/m2 plus HA-KEL of 32.9kN/m and HB-45 unit as described in Figure 2. In this study, The total length of the HB vehicle was taken as 9.6 m which leads to most sever affect to the bridge.

The concrete material was considered to have a cylindrical characteristic compressive strength equals to 40MPa and modulus of elasticity of 35GPa. While, the steel reinforcement has 460MPa yield strength and 200GPa elastic modulus. For pre-stressed section design, super low relaxation 7-wire strands were used. Each strand has 12.9mm diameter and 186kN ultimate load.
2.2 FE modeling and results

Using SAP2000-Ver 15.0.1[8], elastic analysis was performed for all bridges using estimated sections (Appendix A). Table 1 presents the dimensions properties, the ultimate internal forces produced by the current analysis and the capacity (resistance) of each section. Both shear resistance and bending resistance for each section were obtained using BS 5950-3.1:1990 [9] for composite section and BS 8110-1:1997 [10] for pre-stressed
concrete section. From Table 1, it can be seen clearly that the section estimation was proper since the ultimate bending moment is almost same as bending capacity.

Figure 3 describes the relationship between the span length and depth of the girder for the three cases used in this research: composite section, pre-tensioned pre-stressed concrete and post-tensioned pre-stressed concrete. It can be explored that steel composite girder offers always lower depth up to 41% less for 40m bridge span.

Table 1. Dimensions properties, ultimate internal forces and capacity for each section.

| Sr No. | Girder Length (m) | Girder Type | Girder Depth (m) | Girder & Slab Depth (m) | Section Area with Slab (m²) | Section Area without Slab (m²) | Moment of Inertia (mm⁴) | No. of Tendons | Force in Tendons (KN) | ULS Moment (KN.m) | Shear Force (KN) |
|--------|-------------------|-------------|-----------------|-------------------------|-----------------------------|------------------------------|------------------------|----------------|---------------------|-----------------|-----------------|
| 1      | 40 m              | Pre-Tension | 2.2             | 2.2                     | 1.095                       | 0.645                        | 0.7163                 | 3 T           | 72                  | 9375            | 16770           |
| 2      | 40 m              | Post-Tension| 2.2             | 1.06                    | 0.6099                      | 0.5151                       | 0.5962                 | 74 B          | 74                  | 9635            | 16702           |
| 3      | 40 m              | Composite   | 1.1             | 1.3                     | 0.701                       | 0.151                        | 0.7163                 | 13607         | 12228               | 7514            | 1361            |
| 4      | 35 m              | Pre-Tension | 1.8             | 2                       | 1.055                       | 0.605                        | 0.5635                 | 62 B          | 8073                | 12956           | 12602           |
| 5      | 35 m              | Post-Tension| 1.8             | 1.035                   | 0.585                       | 0.3981                       | 0.5635                 | 74 B          | 9635                | 12977           | 12336           |
| 6      | 35 m              | Composite   | 0.92            | 1.12                    | 0.0494                      | 0.0145                       | 0.0494                 | 9552          | 9340                | 4080            | 1246            |
| 7      | 30 m              | Pre-Tension | 1.6             | 1.8                     | 1.015                       | 0.565                        | 0.4313                 | 52 B          | 6767                | 9885            | 9647            |
| 8      | 30 m              | Post-Tension| 1.6             | 0.975                   | 0.5249                      | 0.2953                       | 0.5249                 | 54 B          | 7031                | 9857            | 1289            |
| 9      | 30 m              | Composite   | 0.98            | 1.18                    | 0.0316                      | 0.0126                       | 0.0316                 | 6234          | 6010                | 3347            | 1158            |
| 10     | 25 m              | Pre-Tension | 1.4             | 1.6                     | 0.925                       | 0.475                        | 0.2967                 | 43 B          | 5999                | 7663            | 7055            |
| 11     | 25 m              | Post-Tension| 1.4             | 0.915                   | 0.4648                      | 0.2108                       | 0.4648                 | 46 B          | 7163                | 7465            | 6879            |
| 12     | 25 m              | Composite   | 0.91            | 1.11                    | 0.0286                      | 0.0108                       | 0.0286                 | 5390          | 5230                | 3083            | 1100            |
| 13     | 20 m              | Pre-Tension | 1.2             | 1.4                     | 0.91                        | 0.46                         | 0.2187                 | 30 B          | 4279                | 4795            | 4676            |
| 14     | 20 m              | Post-Tension| 1.2             | 0.855                   | 0.4047                      | 0.1435                       | 0.1435                 | 31 B          | 4036                | 4686            | 4567            |
| 15     | 20 m              | Composite   | 0.835           | 1.035                   | 0.0224                      | 0.0084                       | 0.0224                 | 4108          | 3584                | 2490            | 1036            |

3 Cost analysis of different simple-span bridges

This study carried out and compared two types of cost analysis for each bridge span: (a) comparison analysis for only the initial capital costs; and (b) cost analysis including the initial costs and 50-year life cycle costs encompassing the maintenance costs. The life cycle costs are derived using Eqs. (1)-(2) [11]:

\[ F_v = P_v (1 + i)^n \]  
\[ P_v = F_v [1/(1 + r)]^n \]

where,
\( F_v \) is Future Value of \( n \) number of years.
\( P_v \) is Present Value.
\( i \) is the inflation rate.
\( r \) is the interest rate.
Following the preparation of the structural design for the three types of bridges with five lengths for each type, the material quantities have been calculated for each girder and listed in bill of quantities. These materials include: concrete, steel, strands, grouting, etc. In addition, the rate for each item in the BoQ has been based on average rates of previous projects in United Arab Emirates. The results of the analysis have been illustrated by the following bar-chart figures.

Figure 4 shows the total capital costs in Emirati Dirhams (DHS) of 4-girder bridges of different span and different section type. It is evident that for spans between 20m and 30m, the composite girder has the least capital cost compared with the pre-tensioned and post-tensioned girders. However, for spans between 35m and 40m the composite girder is much expensive. The reason for that might be because of the structural loads and depths of girders required for short, medium and long spans.

Whereas, Figure 5 exhibits the 50-year life cycle costs for same bridges. It is worth mentioning that the daily cleaning, which is required for all types of bridges, was not included in the maintenance analysis, because it will not make any difference for the comparison analysis of this study. The daily cleaning will only add the same constant cost for all types of girders. From Figure 5, it is clear that, except for the 20m span, all other spans are more expensive with a composite girder compared to pre-tensioned and post-tensioned girders. For both cases in Figures 4 and 5, the growth percentage in cost is increased as the span length is increased.
Fig. 4. The total capital costs (present value) for 8 girders of different span and section type.

Fig. 5. The total 50-year total life cycle cost (future value) for 8 girders of different span and section type.

The conclusion can be seen in Figure 6 which demonstrates the relative differences in cost for both steel composite section and pre-stressed concrete section for all spans. Figure 6 clarifies the considerable impact of maintenance and life cycle costs. Without maintenance consideration, the cost of composite-girder bridge is lower than the pre-stressed one up to span 30m. While, the 50-year life cycle cost with maintenance is always lower for the pre-stressed bridge. It reaches 45% less than the steel composite
bridge for 40m span. On the other hand, the FDOT[6] cost can be applicable only for 35m bridge span for capital cost and 25m bridge span in case of maintenance costs. Otherwise, having pre-stressed bridge provides much lower cost.

![Graph showing cost differences](image)

**Fig. 6.** The relative differences in cost for both steel composite section and pre-stressed section.

### 4 Conclusions

In this paper, three types of girders were investigated: steel composite, pre-tensioned pre-stressed concrete and post-tensioned pre-stressed concrete. The structural design was analyzed for 5 span lengths: 20, 25, 30, 35 and 40m. Then, the capital construction cost and 50-year life cycle cost were accounted for 15 bridges according to each span and construction materials.

It was found that although steel composite section proposes lower section depth, but the life cycle cost of pre-stressed section is always lower and can reach 45% of the composite section cost in some cases. It was also evident that the longer the span of the girder the less expensive the pre-stressed section will be.

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APPENDIX A: Estimated sections for five different spans girder-bridge

Fig. A-1. Estimated sections for 20m-span bridge.

Fig. A-2. Estimated sections for 25m-span bridge.
**Fig. A-3.** Estimated sections for 30m-span bridge.

**Fig. A-4.** Estimated sections for 35m-span bridge.
Fig. A-5. Estimated sections for 40m-span bridge.