Characterizing and Engineering Biomimetic Materials for Viscoelastic Mechanotransduction Studies

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The mechanical behavior of soft tissue extracellular matrix is time dependent. Moreover, it evolves over time due to physiological processes as well as aging and disease. Measuring and quantifying the time-dependent mechanical behavior of soft tissues and materials pose a challenge, not only because of their labile and hydrated nature but also because of the lack of a common definition of terms and understanding of models for characterizing viscoelasticity. Here, we review the most important measurement techniques and models used to determine the viscoelastic properties of soft hydrated materials—or hydrogels—underlining the difference between viscoelastic behavior and the properties

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and descriptors used to quantify viscoelasticity. We then discuss the principal factors, which determine tissue viscoelasticity in vivo and summarize what we currently know about cell response to time-dependent materials, outlining fundamental factors that have to be considered when interpreting results. Particular attention is given to the relationship between the different time scales involved (mechanical, cellular and observation time scales), as well as scaling principles, all of which must be considered when designing viscoelastic materials and performing experiments for biomechanics or mechanobiology applications. From this overview, key considerations and directions for furthering insights and applications in the emergent field of cell viscoelastic mechanotransduction are provided.

**Keywords:** viscoelasticity, hydrogels, viscoelastic mechanotransduction, mechanical testing, cell mechanical memory, time scaling

**Impact Statement**

Our tissues are viscoelastic: they respond to mechanical stresses and strains in a time-dependent manner. Their mechanical behavior also evolves over time due to growth, aging, remodeling, repair, and fibrosis. These changes are transmitted to cells, resulting in a two-way flow of interactions between cells and their microenvironment known as dynamic reciprocity.1-3

The main structural component of soft tissues is the extracellular matrix (ECM), which is essentially a hydrogel: a biphasic viscoelastic material composed of a solid polymeric network interpenetrating an aqueous solution.4 Among the network’s components are collagen, responsible for tissue stiffness and strength, and elastin, which endows extensibility and resilience. The behavior of the solid phase can be related to the tissue’s elastic properties, usually described by an elastic modulus (E). The interfibrillar liquid is mainly composed of water and solutes such as glycosaminoglycans (GAGs), proteoglycans, and glycoproteins. Its resistance to flow is quantified through viscosity (µ). GAGs and proteoglycans also contribute to tissue compressive stiffness, thanks to their high level of hydration.5,3,5

Studying the role of mechanical factors involved in the cell–microenvironment relationship enables the investigation and control of cell behavior through material design. In particular, reproducing the wide range of mechanical behavior manifested by the ECM is fundamental for generating physiologically relevant in vitro models and to improve the performance of tissue substitutes for regenerative medicine applications.5

Mechanotransduction, the ability of cells to sense, respond and adapt to mechanical signals, has long been investigated as a function of substrate rigidity and is generally associated with cell response to elasticity. But—as tissues are viscoelastic—it is only part of the story. For elastic materials, mechanotransduction can be associated with elastotransduction, i.e., cell response to time invariant stress and strain (Fig. 1 A). In the case of viscous materials (Fig. 1B), we can speak of viscotransduction (cell response to the resistance to flow of a material). Finally, in viscoelastic materials, as the viscous and elastic components cannot be decoupled, cell response to time dependent stress and strain should be referred to as viscoelastic mechanotransduction (Fig. 1C).

The purpose of this review is to provide a reference for scientists wishing to explore the fascinating and emerging field of viscoelastic mechanotransduction by bringing together fundamental aspects of viscoelasticity relevant to the study of soft hydrated biomaterials and tissues, the state of the art in hydrogel design and our current understanding of cell response to time-dependent material behavior.

**Modeling and Measuring Viscoelasticity**

Although the theory of viscoelasticity and viscoelastic models are noted in textbooks—and in some excellent reviews8-15—there is some confusion on the terms used to define different models, on the relationships between their viscoelastic constants and the physical interpretation of time and material constants. We begin therefore by introducing some fundamental concepts for understanding and quantifying the mechanical behavior of hydrogels.

For the sake of clarity and consistency, we refer to material mechanical behavior as its intrinsic comportment, which is often described by the terms such as stiff, soft, floppy, and elastic, while the mechanical properties are quantities used to define and describe the behavior through mathematical models. The properties will depend on the nature of the material as well as the models and methods used to extract parameters and quantitative descriptors (time constants, equilibrium and instantaneous elastic moduli or storage and loss moduli).16 Additionally, we use the term time dependent when referring to classical viscoelastic behavior in which resistance or compliance to deformation is a function of time, distinguishing it from time-evolving viscoelasticity, which arises from variations in viscoelastic descriptors over time.

**Viscoelastic models**

For small deformations, the viscoelastic behavior of hydrogels is related to both solid network deformation and viscous phenomena such as molecular entanglements, chain
sliding, and short-range water flow. At higher deformations, water flow occurs over a larger range resulting in “poro-viscoelastic” behavior. For a given specimen with characteristic length, $L$, and a water self-diffusion constant, $D$, under an experimental observation time, $T_{\text{obs}}$, viscoelastic phenomena are observed for characteristic relaxation time $t_{\text{relax}} \approx T_{\text{obs}}$, whereas poroelastic phenomena can be observed when $L^2/D \approx T_{\text{obs}}$.\footnote{17,18} Given that soft tissues and hydrogels are generally tested under bulk compression or tension, with typical dimensions of the order of 1 cm, poroelastic phenomena will only manifest in the laboratory when experiments last several hours or for high deformations.

Thanks to their general applicability, linear viscoelastic models (also known as lumped parameter models or viscoelastic solid models) are often the preferred choice in biomaterial studies and as such will be the focus of this review. Other mechanical models are summarized in the Supplementary Information SI1. Linear models describe the relationship between deformation ($\varepsilon$) and applied stress ($\sigma$) through linear combinations of parameters, typically springs and dashpots.\footnote{15,19} The parameters do not have any real physical significance, but it is useful to associate the dashpots (viscous coefficient $[\eta_i]$) with friction, viscosity, sliding, entanglements, and solvent flow and the springs (elastic modulus $[E_i]$) with the deformation of the solid network (Fig. 2A). The two elements can be combined to generate different linear viscoelastic models, which can be grouped into two main families: the generalized Maxwell (GM) and generalized Voigt (GV) (Fig. 2B, C). Although they are mechanically equivalent,\footnote{15} the mathematical derivation of the GM model response is simpler for strain inputs, while the GV model response is more suitable for stress inputs. We encourage the use of a common terminology; however, the reader will find that these names are not unique; alternative terms are summarized in the Supplementary Information SI2.

**Viscoelastic testing**

Material elastic properties are generally derived by analyzing the stress–strain curve resulting from tensile or compressive tests. The elastic modulus is estimated from the slope of the first linear part of the curve. In the case of viscoelastic materials, this region depends on the strain rate and is referred to as the linear viscoelastic region (LVR). Its slope is defined as the apparent elastic modulus ($E_{\text{app}}$).\footnote{20,21} We add here a note about stiffness: strictly speaking, stiffness is an extrinsic property, even though it is often used interchangeably with rigidity or elastic modulus. Although the term should be avoided when referring to viscoelastic materials, it is so deeply entrenched in the field of mechanobiology as to be unavoidable. We can relate the stiffness to $E_{\text{app}}$ at high strain rates, which in turn closely approximates the instantaneous elastic modulus ($E_{\text{inst}}$, see the “Derivation of material descriptors” section).

A variety of testing methods have been developed to derive quantitative descriptors of the time-dependent behavior of viscoelastic materials.\footnote{21–23} They can be classified on the basis of the type of input: a strain or stress step, ramp, or sinusoid (see the Supplementary Information SI3 for details, where we also discuss the difference between bulk and local tests).

**Derivation of material descriptors**

For any of the models in Figure 2B, C, equations for the stress or strain as a function of time or frequency can be derived by substituting the Laplace transform of the inputs in the model transfer function (Supplementary Information SI4). The equations can be fitted to the experimental stress–time or strain–time curves or frequency spectra to derive the model lumped parameters (Supplementary Information SI4).

The lumped parameters can be used to derive the material descriptors: $E_{\text{inst}}$, the instantaneous modulus, is the initial (i.e., $t \to 0$) elastic response when the viscous components

![FIG. 1.](image-url)
are “shorted” out and do not deform while sustaining the load. \( E_{eq} \) is the equilibrium modulus, which represents the response after viscoelastic dynamics have occurred \((t \to \infty)\). In these conditions, the piston is completely dissipated, and it cannot support a load; it can be considered analogous to an “open circuit.” The time constants \( \tau_i \) are also descriptors of the material’s behavior and are given by the ratio of the coefficients \((\eta_i/E_i)\) for \( t \to \tau_i \) for each dashpot and spring pair in the GM or GV models.

Figure 3A summarizes the workflow for deriving model parameters and the related viscoelastic descriptors for a strain step input. Examples of typical mechanical responses and descriptors for different hydrogels are shown in Figure 2B. Further theoretical details are illustrated in the Supplementary Information (Supplementary Fig. 2S).

In general—and for the sake of simplicity (see the Supplementary Information SI5) —a single characteristic time, as obtained with the first-order models, is sufficient to describe material viscoelastic behavior. For a strain input, we define a relaxation time \( (\tau_{relax}) \), which is the time in which the stress decays to \( 1/e \) \( (\approx 37\%) \) of the initial stress. For a stress input, the retardation time \( (\tau_{retard}) \) is defined as the time necessary to reach \( \approx 63\% \) \((1-1/e)\) of the equilibrium strain. The relationship between characteristic relaxation time and retardation time is given in the Supplementary Information SI6.

The descriptors for sinusoidal stimuli are expressed using a complex elastic modulus, \( E^*(\omega) \), composed of a real or storage modulus \( E'(\omega) \)—related to the ability of the material to return energy—and an imaginary or loss modulus \( E''(\omega) \)—associated with the energy lost in “internal friction” (e.g., molecular motions, relaxation processes). The ratio between descriptors \( E''/E' \) defines \( \delta \), known as the loss or damping factor, which allows the derivation of the relaxation time as the reciprocal of the peak frequency. \( \delta \) represents the phase difference between the input and output sinusoid: \( \delta = 0 \) for ideally elastic materials (all the energy is stored in the material) and \( \delta = 90^\circ \) for an ideally viscous liquid (all the energy is dissipated).\(^{26}\)

Figure 4 shows the relationships between material behavior and viscoelastic descriptors in the time and frequency domain. When \( E_{inst} = E_{eq} \) and \( \tau_{relax} \to \infty \) (i.e., the stress never relaxes during observation), the material has an ideal elastic or solid-like behavior (Fig. 4A, B). For \( E_{eq} \approx 0 \) and \( \tau_{relax} \to 0 \) (i.e., the stress instantaneously relaxes), the material is defined as a pure viscous or liquid-like (Fig. 4B). However, if \( \tau_{retard} \to 0 \) (i.e., there is no retardation in reaching the equilibrium strain), the material behavior is elastic, \textit{vice versa}, if the retardation time is much longer than the observation time, or \( \to \infty \), it is purely viscous. Between these extremes, the material can be considered a viscoelastic solid. Similarly, materials behave as elastic solids for high \( E' \) values and low \( E'' \) values and, \textit{vice versa}, they behave as viscous fluids for low \( E' \) and high \( E'' \) (Fig. 4C). In all cases, \( T_{obs} \) plays a crucial role in determining whether a material can be considered elastic, viscoelastic, or viscous (see section “Time and material behavior”).

Note that the viscoelastic descriptors obtained in the frequency domain can be derived from those in the strain–rate domain and \textit{vice versa}.\(^{21,27,28}\) As an example, the equation reporting the relationship between the frequency and time domain descriptors for the first-order GM model can be found in the Supplementary Information SI4.

**Time and material behavior**

That the perception of viscoelasticity depends on the observation time was noted by Reiner, who defined the Deborah number as the ratio between the relaxation time and observation time: \( De = \tau_{relax}/T_{obs} \). In the case of \( De \gg 1 \), the material is expected to manifest elastic solid behavior; while, if \( De << 1 \), the material will behave as a viscous liquid. When the relaxation...
FIG. 3. (A) Workflow for identifying material viscoelastic properties. (B) Mechanical response for different hydrogels: PDMS, PAAM, and soft collagen. For typical observation times, PDMS has solid-like behavior: $E_{eq}$ and $E_{inst}$ are similar and $\tau_{relax}$ is higher than $T_{obs}$. Collagen is very soft and liquid-like: $E_{eq}$ and $E_{inst}$ are significantly different and $\tau_{relax}$ is low. PAAM generally shows an intermediate viscoelastic behavior. PAAM, polyacrylamide; PDMS, polydimethylsiloxane. Color images are available online.

FIG. 4. Viscoelastic “phase diagrams” illustrating the elastic to viscous spectrum material behavior as a function of (A) equilibrium and instantaneous modulus ($E_{eq}$ and $E_{inst}$) for a fixed observation time ($T_{obs}$). (B) Equilibrium modulus, characteristic relaxation time ($\tau_{relax}$), and retardation time ($\tau_{retard}$) for a fixed $T_{obs}$. (C) Storage and loss modulus ($E'$ and $E''$) for a fixed frequency ($\omega$). Color images are available online.
Table 1. Properties and Phenomena Associated with Material Elastic and Viscous Behavior

| Elastic behavior | Viscous behavior |
|------------------|------------------|
| Also defined as: |                  |
| “Solid-like”     | “Liquid-like”    |
| Conservative     | Dissipative      |
| Time independent | Time dependent   |
| Materials with   | Materials with   |
| memory           | no memory        |

| Associated with                  |
|----------------------------------|
| Polymer concentration/           |
| cross-linking                    |
| Polymeric–liquid interaction     |
| Polymer chain entanglements      |

| Viscosity, elastic, or shear moduli and characteristic times |
|-------------------------------------------------------------|
| Liquid phase resistance to “flow,” μ                       |
| Liquid phase 1/μ (fluidity)                                |
| ε’ or G’                                                   |
| ε” or G”                                                   |
| δ                                                           |
| τ_relayion or De                                           |
| τ_retardation                                             |
| Strain rate dependence                                    |

|                        |
|------------------------|
| ∴ G’ is the storage shear modulus and G” is the loss shear modulus. |
| ↑, increase; ↓, decrease. |

How do tissue mechanics change over the different stages of life and in health and disease? During growth, there is a high turnover of ECM components, which contributes to tissue remodeling and reinforcement in response to mechanical stimuli. In adulthood, feedback mechanisms based on ECM reorganization and cross-linking and a precise balance between degradation and deposition guarantee homeostasis and adaptation.

During maturation and remodeling (e.g., wound healing), collagen and elastin undergo precisely modulated cross-linking through the action of enzymes. The resulting increase in stiffness helps tissues to achieve structural resistance. Enzymatic mediated cross-linking reaches a plateau during maturation, but tissue rigidity continues to increase with age. ECM aging is characterized by cross-linking arising from uncontrolled nonenzymatic oxidative reactions with glucose (glycation). Although these reactions are slower than enzymatic ones, the relatively long half-lives of ECM components (∼10 years for collagen, ∼60 years for elastin) make glycation-mediated cross-linking significant. Moreover, the deceleration of collagen turnover coupled with the extremely low elastin renewal rate implies irreversible changes in tissue form and function, which result from mechanical fatigue, damage or proteolytic degradation. Since ECM viscosity is directly proportional to the concentration of its constituents, the loss of collagen results in an increase in fluid mobility in tissues, which is manifested by a decrease in viscosity.

However, excessive or uncontrolled collagen deposition and cross-linking are responsible for organ dysfunction in fibrotic and degenerative diseases (e.g., pulmonary fibrosis, liver cirrhosis, cardiovascular disease and systemic sclerosis). These conditions are associated with fibroblast hyperproliferation, in which the cells tend to differentiate into collagen-secreting myofibroblasts, and with the upregulation of cross-linking enzymes such as lysyl oxidase. Table 2 recaps the main factors involved in different pathophysiological process and consequent effects on tissue mechanical behavior. Elasticity and viscosity trends have been considered separately to highlight their contributions. However, tissue elastic and viscous behaviors are intrinsically related and, typically, cannot be decoupled.

Understanding cell response to viscoelasticity

Since Pelham and Wang first observed the effect of substrate elasticity on fibroblasts in 1997, mechanobiology studies have increased exponentially. Historically, cells have been cultured on rigid plasticware, and controlling and measuring material elastic constants are relatively easy. As a consequence, cell response to viscoelasticity is still poorly understood and results are often contradictory. Some studies report on an increase of cell spreading area and differentiation on viscoelastic substrates with respect to elastic ones whereas others describe the opposite. These conflicting results have been related to the different cell types and culture conditions (e.g., two-dimensional [2D] vs. three-dimensional [3D]). Cell spreading depends on cytoskeletal tension, which in turn depends on substrate mechanics. Thus, one might expect that substrate forces relax.
over time on soft time-dependent materials, resulting in lower cytoskeletal tension and spreading. However, in some cases, the higher deformability of these substrates may give rise to localized ligand clustering resulting in local stiffening in response to cell movements such that spreading is improved with respect to an elastic substrate with the same ligand density.\textsuperscript{42,53} Moreover, in 3D, cell migration is likely easier in soft gels than in more elastic ones; since the cells are not “caged” in a stiff matrix, they can move and produce their own extracellular environment.\textsuperscript{50,51,53} Cell volumetric expansion, which in 3D is determined by the “dimensionality” of cell-ECM interaction, is indeed an important factor able to drive cell spreading and commitment. For instance, Caliari \textit{et al.} reported that mesenchymal stem cells (MSCs) showed increased spreading and YAP/TAZ nuclear translocation in 2D while the opposite was observed in 3D, suggesting that cell behavior is not only regulated by stiffness but also by the complex interplay of environmental factors.\textsuperscript{54} Major \textit{et al.} found similar results with adipose-derived MSCs. They also showed that fast relaxing gels allowed greater cell volume expansion with respect to slow relaxing ones.\textsuperscript{55} The main studies on cell response to viscoelasticity are summarized in Table 3, highlighting cell types and their behavior as a function of substrate viscoelasticity.

**Engineering Hydrogel Viscoelasticity**

To recap, cells and tissues are exquisitely mechanoresponsive at all stages of life, in sickness and in health. Reproducing the stiffness and time-dependent as well as time-evolving range of mechanical behavior manifested by the ECM is fundamental for better understanding cell–material interaction and designing materials for biomedical applications.\textsuperscript{6,51}

### Table 2. Tissue Mechanical Variations During Pathophysiological Processes

| Growth/maturation | Adulthood | Aging | Fibrosis |
|-------------------|-----------|-------|----------|
| $E$ (elastic modulus/behavior) | ↑ | ~ | ↑ | ↑ |
| $\mu$ (viscosity) | ↑ | ~ | ↓ | ↑ |
| $\eta$ (viscous coefficient/behavior) | ↓ | ~ | Depends on the relative variation of $E$ and $\mu$ | ↓ |

**Main factors involved**

| Hydrogel type | Cell type | Reference |
|---------------|-----------|-----------|
| Enzymatic controlled cross-linking | Huh7 cell line, hepatocellular carcinoma cells | 52 |
| Collagen physiological remodeling with loads | 3T3 fibroblasts | 47 |
| ECM deposition | 3T3 fibroblasts | 57 |
| Balance between ECM deposition and turnover | Elastin damage accumulation | 62 |
| Glycation | Collagen hyperproduction | 62 |
| Collagen deposition | LOX upregulation | 62 |

**Time scales**

| Growth/maturation | Adulthood | Aging | Fibrosis |
|-------------------|-----------|-------|----------|
| From days to years | 2,3 | 2,37–39,56,91–94 | 2,94,95 |

| References | |
|------------|---|
| 2,33–36,89,90 | 2,37–39,56,91–94 |

As tissues mature, age, or remodel over time, the mechanical properties also evolve.

\textsuperscript{~}, almost constant; ECM, extracellular matrix; LOX, lysyl oxidase.

### Table 3. Summary of the Main Studies on Cell Response to Viscoelasticity

| Cell response with increasing gel viscous behavior | Hydrogel type | Cell type | Reference |
|--------------------------------------------------|---------------|-----------|-----------|
| ↑ Spreading, proliferation, differentiation | PAAm | MSCs | 43 |
| PAAm | Huh7 cell line, hepatocellular carcinoma cells | 52 |
| PEG thioester norbornene | 3T3 fibroblasts | 47 |
| RGD alginate | 3T3 fibroblasts | 57 |
| 3D | Hyaluronic acid | MSCs | 54 |
| PEG | C2C12 myoblasts | 96 |
| RGD PEG alginate | MSCs, 3T3 fibroblasts | 42,58 |
| Hyaluronic acid and collagen | MSCs | 58 |
| ↓ Spreading, proliferation, differentiation | PAAm | 3T3 fibroblasts | 47 |
| PAAm | Hepatocytes | 52 |
| PAAm loaded with carbonyl iron particles | MSCs | 46 |
| Collagen loaded with carbonyl iron particles | Coronary artery smooth muscle cells | 62 |
| Hyaluronic acid | MSCs | 54,61 |

2D, two-dimensional; 3D, three-dimensional; MSCs, mesenchymal stem cells; PAAm, polyacrylamide; PEG, polyethylene glycol; RGD, arginine, glycine, aspartate.
Modulation of viscoelastic (time-dependent) properties

Hydrogel viscoelasticity can be modulated using different techniques, and the gel will have (approximately) constant mechanical properties throughout the culture period. An increase in the polymer or cross-linker concentration (and consequently in the degree of cross-linking of the polymer network) results in a shift toward a more elastic behavior. For instance, by varying the proportion of acrylamide and bis-acrylamide, Cameron et al. demonstrated that MSC spreading and differentiation increased with decreasing loss moduli (corresponding to decreasing gel relaxation times). Similarly, using polymers with different molecular weight or modulating the formation of reversible cross-links results in gels with different viscoelastic behavior. Alternatively, the mobility of the polymeric chains can be improved by the addition of spacers, thus increasing gel dissipative properties. The use of alginate with different molecular weights and of alginate with polyethylene glycol (PEG) spacers allows greater spreading in both MSCs and fibroblasts. As these methods mainly act on the gel polymeric network, they concomitantly alter the elastic and the viscous component since the two phenomena cannot be decoupled. Cacopardo et al. reported an alternative and unique approach whereby the gel’s viscous properties—and hence the mechanical testing scales range from nanometers to centimeters and should be selected according to the material under testing. Moreover, the ability of the cells to sense and respond to the time-dependent substrate properties should be considered in the light of the range of time scales of the different players involved. The first player is the substrate, which has one or more characteristic relaxation times. The second player is the cell, whose response is related to its ability to bind to adhesion molecules and transduce the substrate tension into a biochemical signal.

Modulation of time-evolving properties

A few recent efforts to mimic tissue dynamics and study how cells adapt and respond to a mechanically evolving context have been reported. Generally, the viscoelastic properties of gels can be modulated over time through agents, which modulate the formation or degradation of cross-links, although not all methods can be used in the presence of cells. For example, enzymatic cross-links exploit enzyme reaction kinetics to enable the tuning of gel viscoelastic properties over time. Chemical reactions with slow kinetics can also be used to generate gels with time-evolving viscoelasticity. Finally, the use of responsive materials represents an intriguing strategy to modulate gel viscoelasticity on-demand. As an example, MSC spreading on magneto-responsive gels was reduced when the gels were switched from elastic to liquid-like behavior.

Perspectives for Viscoelastic Mechanotransduction Studies

As we explore the new field of cell viscoelastic mechanotransduction through viscoelastic material engineering, it is important to bear in mind a number of factors, which are crucial for posing specific research questions and interpreting data. They will also impact on the way in which experiments are designed.

Mechanosensing time and spatial scales

Cells are able to sense substrate mechanics, thanks to the formation of focal adhesions (FAs), which are molecular complexes that act like bridges between the ECM and the cytoskeleton. Typically, the size of FAs is between 0.25 and 10 µm and their lifetime is in the range of tens of minutes, depending on cell type and substrate. The cell integrates these local signals eliciting a measurable response.

The ambiguity of the results on cell response to viscoelasticity is not only due to different experimental conditions (such as cell types, substrate materials, mechanical testing methods) but also due to an intrinsic difficulty in their interpretation due to the diverse spatial and time scales involved. As discussed in the Supplementary Information SI3, the mechanical testing scales range from nanometers to centimeters and should be selected according to the material under testing. Moreover, the ability of the cells to sense and respond to the time-dependent substrate properties should be considered in the light of the range of time scales of the different players involved. The first player is the substrate, which has one or more characteristic relaxation times. The second player is the cell, whose response is related to its ability to bind to adhesion molecules and transduce the substrate tension into a biochemical signal.

According to the molecular clutch theory, cell adhesion is related to both the time needed to form cell–ECM bonds and their lifetime; this interval of time can be referred as the cell sensing time (Tcell). Typically, higher than Tbnd, allowing the formation of stable bonds able to trigger mechanotransduction pathways. As shown in Figure 6A, the substrate characteristic relaxation times (τrelax) should be comprised within the cells’ sensing time window to allow them to “perceive” the substrate dynamics and activate pathways, which may result in a quantifiable difference in their behavior in response to substrate viscoelasticity. If Tcell is too short with respect to τrelax, the cells can sense only the instantaneous material response. However, if the time required to (and maintain) the bonds exceeds τrelax, cells are likely to “perceive” only the equilibrium material response. As an example, using 3T3 fibroblasts seeded on hyaluronic acid gels, Gong et al. showed that substrate viscoelasticity can regulate cell spreading depending on the relationship between substrate relaxation time and cell binding time and duration. Therefore, the investigation of cell response to viscoelasticity cannot prescind from accurate design of substrate viscoelastic dynamics according to the cell sensing time window, which may differ according to cell type or disease states.

The third factor is the observation time (Tobs), which may differ according to the material and the mechanical testing method (Supplementary Information SI3), experimental parameters should be carefully chosen to obtain meaningful results.

Time and mechanical scaling

The general allometric equation is $Y = aM^b$, where $Y$ is the physiological parameter of interest (metabolic rate, cell number, etc.), $M$ is the body mass, $b$ is the allometric scaling
| Method | Material | Effect | Compatibility with 3D cell encapsulation | Direct modulation of the viscous phase | Reference |
|--------|----------|--------|----------------------------------------|----------------------------------------|-----------|
| Viscoelastic substrates (time-dependent behavior, constant viscoelastic descriptors) | Polymer concentration, cross-linker ratio | PEG-alginate | $\uparrow$ [PEG spacer]: $G'$, $\downarrow G''$ | Yes | No | 57 |
| | | PAAm | $\uparrow$ [bis-acrylamide]: $G'$, $\downarrow G''$ | No | No | 43 |
| | | HMWLP-PAAm | $\uparrow$ [HMWLP]: $\sim G'$, $\uparrow G''$ | No | No | 47 |
| | | Boronate ester-PEG | $\uparrow$ [boronate]: $\sim G'$, $\uparrow G''$ | Not specified | No | 49 |
| Liquid phase viscosity | | Dextran – Agarose/ PAAm | $\uparrow$ [dextran]: $\sim E_{eq}$, $\downarrow E_{inst}$, $\downarrow \tau_{relax}$ | Yes | Yes | 19 |
| Chemical cross-linking | | GTA-Gelatin | $\uparrow$ [GTA]: $\uparrow E_{eq}$, $\uparrow E_{inst}$, $\uparrow \tau_{relax}$ | No | No | 23,56 |
| Time-evolving viscoelastic substrates (time-evolving behavior, viscoelastic descriptors are a function of time) | Enzymatic or chemical reactions with slow kinetics | mTG-GTA-Gelatin | $\uparrow$ incubation time: $E_{eq}$, $E_{inst}$, $\tau_{relax}$ (after 1 day) | No | No | 56 |
| | | mTG-Gelatin | $\uparrow$ incubation time: $E_{eq}$, $E_{inst}$, $\tau_{relax}$ | Yes | No | 40 |
| | | MA-HA | $\uparrow$ incubation time: $G'$, $\uparrow G''$ | Yes | No | 59 |
| Photo-cross-linking (e.g., UV) | | MA-HA | $\uparrow$ exposure time: $G'$, $\uparrow G''$ | Yes | No | 60 |
| | | NA-HA | $\uparrow$ exposure time: $\sim G'$, $\downarrow G''$ | Yes | No | 61 |
| | | Thioester-PEG | $\uparrow$ exposure time: relaxation curve slope | Yes | No | 45 |
| Magnetic | | Fe(CO)$_5$ – PAAm/ Collagen | $\uparrow$ exposure time: $G'$, $\uparrow G''$ | Not specified | No | 46,62 |

GTA, glutaraldehyde; HA, hyaluronic acid; HMWLP, high-molecular-weight linear polymers; MA, methacrylate; mTG, microbial transglutaminase; NA, nitrobenzyl acrylate; UV, ultraviolet.
exponent, and \( a \) is a constant. “Physiological time,” defined as the species-dependent chronological time period required to complete a physiological event, is known to vary between different sized organisms following allometric scaling laws. The scaling exponent for physiological times (gestation time, lifespan, etc.) is ubiquitously \( b \approx 1/4 \). Thus, characteristic times and time-evolving processes in downscaled \textit{in vitro} cultures are expected to be shorter than \textit{in vivo}. In fact, time scaling in cell cultures is a well-known phenomenon, although its extrapolation and translation to whole organisms have never been formalized as has the scaling of metabolic rate.

Mechanical tailoring \textit{in vitro} is typically focused on mimicking the amplitude of the mechanical—be they elastic or viscoelastic—properties associated with biological processes, often neglecting to consider their typical timescales. In this perspective, it would be of interest to investigate the relationships between the timescales observed in \textit{in vitro} mechanotransduction experiments and their \textit{in vivo} parallels to tease out scaling laws for cellular processes associated with mechanical cues.

\textbf{Mechanical memory}

Recent studies demonstrate that cells remember the past mechanical characteristics of their environment and their ability to respond to new mechanical stimuli depends on their mechanical history. For example, stem cell priming on stiff substrates reduces their epigenetic plasticity (i.e., the ability to modify their phenotype), blocking the transcription of new genes required for the adaptation to a new environment. This type of memory has also been observed for other cells such as lung fibroblasts, which showed persistent myofibroblast activity after 3 weeks on polydimethylsiloxane substrates with a pathological stiffness, even after switching to a softer substrate.

The longer cells are cultured on stiff substrates, the less they respond to substrates with different mechanical properties (Fig. 6C). In particular conditions, depending on the combination of substrate stiffness and culture duration, cell mechanical memory can be restored. The promoter of this reversible memory effect is thought to be the YAP/TAZ complex, which acts as a mechanical rheostat mediating the mechanical dosing. Yang et al. were the first to demonstrate that YAP/TAZ translocation in MSCs was reversible after 7 days of culture of stiff PEG gels.

Nonetheless, the routine use of plasticware typical of standard cell extraction and culture protocols is likely to affect the cell behavior observed during experiments. Researchers should be aware of these issues when investigating mechanobiological responses, and we suggest that efforts be made to establish new standardized cell culture protocols for preserving or resetting native cell mechanosensitivity.

\textbf{Decoupling mechanics from other factors}

When designing microenvironments for mechanobiology studies, in addition to mechanical factors, it is important to provide the cells with adequate topographic and biochemical cues, and, especially in 3D, to guarantee sufficient space for cell expansion. However, little attention is paid to the consideration of these interacting factors, which may lead to misinterpretation of results. In fact, typical experiments consist of comparing cell behavior on 2D plastic substrates with that of cells on 2D or 3D gels. Not only are the mechanical properties different, but features such as surface roughness, surface chemistry, and haptotactic cues may also differ (Fig. 5).

There is a considerable body of work focusing on the decoupling of stiffness from ligand density and some articles dealing with stiffness and topography or mineral content. The issue of decoupling interacting effects in mechanotransduction studies is exacerbated in 3D gels, wherein the increase of polymer concentration and crosslinking not only alters the mechanical behavior of gels but also affects oxygen, nutrient diffusion, and cell volume. As a consequence, changes in cell response may be influenced, or even overshadowed by factors other than the mechanical properties of the cell environment. A current challenge for \textit{in vitro} research is the isolation or decoupling of mechanical properties from other variables to

\textbf{FIG. 5.} Difference between 2D and 3D gels in mechanobiology studies: when altering gel mechanical behavior in 3D (typically increasing polymer concentration or cross-linking), properties such as biochemical cues (adhesion sites), transport (oxygen and nutrient diffusion), and dimensionality (volume available for cell expansion) also differ. The interacting effects may cloud the understanding of mechanical response in 3D. 2D, two-dimensional; 3D, three-dimensional. Color images are available online.
fully understand and thus direct cell behavior by specifically tuning environmental cues, which engineers can design and control (Fig. 6B).

Conclusions

This review aims at encouraging a more rigorous and harmonized approach toward investigations in mechanotransduction, embracing the entire spectrum of elasto- and visco-transduction to include viscoelastic mechanotransduction. It highlights the importance of designing biomimetic viscoelastic materials with characteristic time responses, which are compatible with experimental times and also relevant to physiological/pathological times under investigation. Some of the future challenges in the field of viscoelastic mechanotransduction (summarized in Fig. 6) are discussed. Among these, there are novel strategies to control factors, which influence cell response, decoupling mechanical properties from substrate biochemistry, topographical features, and mass transport.

An intriguing question, as yet unexplored, is that of time scaling of cellular responses from in vitro to in vivo and vice versa. A final challenge is the definition of cell culture protocols, which can reset cell mechanical memory to a common baseline, crucial for facilitating meaningful comparisons across different studies.

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All authors significantly contributed to the conceptualization and writing of this review.

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Supplementary Material

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