Synthesis of Silicon Nitride Ceramic Material using Direct Nitridation Process

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Abstract — Silicon nitride has been widely employed as one of the most important engineering ceramics for many practical applications due to their excellent properties such as high temperature resistance, low density, high corrosion resistance and other mechanical properties. In this study, silicon nitride (Si₃N₄) ceramic materials was synthesized by a direct nitridation method of amorphous silicon powder under a flow mixture of argon and nitrogen or ammonia. The amorphous silicon powder was placed in a tube furnace at the temperature of from 1300°C to 1600°C for 30-800 min under a flow of gases mixture. The phase compositions and morphology of the obtained Si₃N₄ powder were characterized by using X-ray diffractometry (XRD) and SEM techniques, respectively. The α-Si₃N₄ formed at temperature of 1500°C under a mixed gases flow of 3 L/min for 400 composed of straight rod-like fibers with a length in the range of 5 to 100 μm and diameters of about 0.3-4 μm. The effects of gas flow rate, conversion temperature, reduction time and gas composition on the effectiveness of α-Si₃N₄ formation were investigated in detail. Effect of the auxiliary gases and synthesizing conditions for direct nitridation of Si₃N₄ on α phase content and phase transformation of α-Si₃N₄ to β-Si₃N₄ were also evaluated.

Keywords — Silicon nitride, direct nitridation, β-Si₃N₄, α-Si₃N₄

I. INTRODUCTION

Silicon nitride have been widely used in many fields of application such as automobile and aerospace industries, high speed air turbine bearing and biotechnology industry, catalyst supports. This ceramic materials could be employed as riser tubes, thermocouple sheaths, crucibles, filters for molten metals, high temperature gas filters, cutting tools, ball bearings and heat engine parts (turbine blades, gas turbines, turbocharger rotors, cam roller, rotor blades, nozzle), etc [1-4].

To date two well-known hexagonal crystal structures of silicon nitride, which are α-Si₃N₄ and β-Si₃N₄ phases, have been extensively studied. α-Si₃N₄ with stacking sequence in structure is commonly harder than β-Si₃N₄, however β-phase is considered to be more stable at high temperature than that of α-Si₃N₄[5].

Silicon nitride are commonly fabricated by five main methods such as carbothermal reduction and nitridation (CRN), silicon diimide process, vapor phase reaction process and plasma synthesis or direct nitridation of Si powder. In the carbothermal reaction approach, Si₃N₄ starts forming at 1400°C and phases are transformed from α-Si₃N₄ to β-Si₃N₄ at temperature of higher than 1600°C [6,7].

Figure 1 shows the crystal structure of silicon nitride, where silicon atoms (black) and nitrogen (green) form hexagonal crystal structures [8].

![Crystal Structure of Silicon Nitride](image)

In this study, silicon direct nitridation method was employed to fabricate Si₃N₄ ceramic material by placing Si powder under the gasses mixture of argon and nitrogen or ammonia [9-20]. The effect of the reaction conditions are assessed and optimized.

II. MATERIALS AND METHODS

2.1 Materials

For this study, the starting material is amorphous silicon powder which was received from Sigma-Aldrich, Inc (USA), with ammonia, nitrogen as a nitrogen gas precursor (China Abrasive Import & Export Corp., China, 99%)

2.2 Produce the silicon nitride powder

Si₃N₄ ceramic material was fabricated by using the silicon direct nitridation method. Typically, the amorphous silicon powder was placed into a graphite crucible coated with boron nitride BN with internal diameter of φ100 mm.
The nitridation reaction were carried out in a horizontal tube furnace (Gas pressure sintering GPS, FPW 100/150-2200-100-LA, Elatec Inc., USA) under the gases flow rate of 1 to 3 L/min of nitrogen gas (99.99%, China) and ammonia gas with the mixtures gas pressure is raised from 0.2 to 1 MPa at temperatures ranging from 1300°C to 1600°C for 30 to 800 min. The obtained powder were then sintered using a Self-propagating high temperature synthesis (SHS) system (model 1050, Sumitomo Coal Mining Co., Ltd). Before heating, the furnace was purged with nitrogen or ammonia-argon mixtures to remove the remaining air in the tube. The furnace was then heated at a ramp rate of 10°C/min to 1000°C, and then heating continued at 5°C/min to the final temperature. After reaching temperature, samples were held from 30 to 800 min before cooling. After the sintering process was completed, the furnace was cooled to room temperature with the cooling rate of 20°C/min.

After cooling to room temperature, the substrates were removed from the reactor to determine the amount of Si₃N₄ deposited, and for further characterizations.

2.3 Survey on properties of silicon nitride powder

The phase compositions of the silicon nitride powder were determined by X-ray diffraction (XRD; Siemens D500, Germany), using CuKα radiation (λ=1.5406 Å) with a step of 0.02° (2θ) and a scanning rate of 2° min⁻¹. The pattern was collected in the range from 10° to 90°.

The morphology of ceramic materials were investigated by scanning electron microscopy (SEM, FEI-Inspect F, JEOL, Japan). The operating parameters were 20kV for accelerating voltage, beam current 0.5 nA, 50 s life time and beam diameter of 1-2 μm.

The conversion of Si is determined by the formula:

\[
C = \frac{Si_o - Si_c}{Si_o} \times 100\%
\]

Where, C is the conversion percentage of Si, Si₀ is initial amount of Si, Siₐ is amount of Si after the reaction.

### III. RESULTS AND DISCUSSION

Illustrated in Figure 2 are SEM images of Si₃N₄ ceramic materials prepared with various flow rates. It can be seen from the figure that with the gases flow rate of 1 L/min, Si₃N₄ (mainly α-phase) is composed of dendritic fibers, while at 2 L/min is mostly composed of curvulate fibers with some anomalous particles. With the flow rate of 3 L/min the Si₃N₄ crystal is composed of straight rod-like fibers with a length in the range of 5 to 100 μm and diameters of about 0.3-4 μm. It is obvious that the completeness of Si₃N₄ crystals increases along with gas flow rates.

![Fig.2: SEM images of Si₃N₄ formed under different flow rates: (a) 1 L/min, (b) 2 L/min, (c) 3 L/min.](image)

The crystalline phase of Si₃N₄ at different reaction temperatures was investigated. The XRD patterns of the samples sintered at different temperatures are shown in Figure 3.

![Fig.3: XRD patterns of Si₃N₄ ceramic materials prepared at different temperatures in 75 vol% N₂-25 vol% Ar mixtures with gas flow rate of 3 L/min and 0.2 MPa](image)
It is obviously that $\alpha$-Si$\text{N}_4$ was evidently detected at 1300°C, however the intensity was relatively weak. The intensity of $\alpha$-Si$\text{N}_4$ peaks increased with increasing temperature. The XRD analysis showed that $\beta$-Si$\text{N}_4$ appeared at temperature of 1500°C. When the temperature increased to 1600°C, the amount of $\beta$-Si$\text{N}_4$ increased. Besides, $\beta$-Si$\text{N}_4$ appeared in the products and became the predominant crystalline phase when the synthesis temperature was above 1500°C. At 1600°C, the peak intensity of $\beta$-Si$\text{N}_4$ was higher than that obtained at 1500°C, which indicate the highly crystallinity of $\beta$-Si$\text{N}_4$ at high temperature.

**Effect of reaction temperature and time on phase composition and micromorphology of silicon nitride**

![Graph showing the effect of temperature on conversion of Si in 75 vol% N$_2$-25 vol% Ar mixtures at gas flow rate was 3 L/min and 0.2 MPa.](image)

Fig.4: Effect of temperature on conversion of Si in 75 vol% N$_2$-25 vol% Ar mixtures at gas flow rate was 3 L/min and 0.2 MPa

The effect of operating gas flow rates was investigated at flow rates from 1 L/min to 4 L/min for 400 min in the nitrogen-argon mixtures (75 vol% N$_2$) at 1300°C. Figure 5 shows the effect of N$_2$ flow on nitrogen content of prepared Si$_3$N$_4$ materials. The nitrogen content of Si$_3$N$_4$ powder increased along with the increase of N$_2$ flow and reach a maximal of 37.5% at the flow rate of 3 L/min. When the flow rate was further increase, the content of nitrogen was almost unchanged.

**Effect of ammonia and nitrogen on nitridation of silicon**

![Graph showing the effect of N$_2$ flow on nitrogen content of Si$_3$N$_4$ powders in 75 vol% N$_2$-25 vol% Ar mixtures at 1300°C and 400 min.](image)

Fig.5: Effect of N$_2$ flow on nitrogen content of Si$_3$N$_4$ powders in 75 vol% N$_2$-25 vol% Ar mixtures at 1300°C and 400 min.

The effect of ammonia and nitrogen on nitridation of silicon was investigated at different temperatures (1300°C, 1400°C, 1500°C and 1600°C) for 600 min in the nitrogen-argon mixtures (75 vol% N$_2$) with gas flow rate 3 L/min at 0.2 MPa. Figure 4 presents the effect of conversion efficiency of Si powder into Si$_3$N$_4$ on reaction temperature. It is obvious that the rate of Si nitridation increased when the temperature increase. The conversion of Si was 81 % in efficiency at the temperature of 1300°C. This increased to 85 % at 1400°C, 88 % at 1600°C, and reached the maximum 92 % at 1500°C after 400 min.

We found that the conversion of Si decreased when the temperature increased to 1600°C. This can be explained that at 1600°C, Si can be melted, so the Si surface is covered which decrease contact between Si and N$_2$ particles.

**Effect of operating gas flow rates on nitridation of silicon**

The effect of operating gas flow rates was investigated at flow rates from 1 L/min to 4 L/min for 400 min in the nitrogen-argon mixtures (75 vol% N$_2$) at 1300°C. Figure 5 shows the effect of N$_2$ flow on nitrogen content of prepared Si$_3$N$_4$ materials. The nitrogen content of Si$_3$N$_4$ powder increased along with the increase of N$_2$ flow and reach a maximal of 37.5% at the flow rate of 3 L/min. When the flow rate was further increase, the content of nitrogen was almost unchanged.
450 min, 500 min and 600 min for the mixture ratio of in 75 vol% N_2 – 25 vol% Ar, 55 vol% N_2 – 45 vol% Ar, 35 vol% N_2 – 65 vol% Ar, respectively. After the rate of Si nitridation was unchanged when time further increased. The rate of Si conversion under the flow of NH_3 – Ar mixture are shown in Figure 6b. After 350 min reaction, Si conversion was increased from 36% in 35 vol% NH_3 – 65 vol% Ar to 47% in 55 vol% NH_3 – 45 vol% Ar, 86% in 75 vol% NH_3 – 25 vol% Ar and reached the maximum of 92 % in 95 vol% NH_3 – 5 vol% Ar mixture.

**Fig.6: Effect of ammonia and nitrogen on nitridation of silicon at gas flow rate 3 L/min, 400 min and 1400°C: (a) N_2 - Ar; (b) NH_3 - Ar.**

It can be found that the effectiveness of Si nitridation in 75 vol% N_2 – 25 vol% Ar is similar to the rate of Si nitridation in 95 vol% N_2 – 5 vol% Ar. Therefore, the Si nitridation in 75 vol% N_2 – 25 vol% Ar mixture instead of the Si nitridation in 95 vol% N_2 – 5 vol% Ar mixture is selected as optimized N_2 – Ar mixture ratio. Furthermore, the rate of Si nitridation in 75 vol% NH_3 – 25 vol% Ar is same as the rate of Si nitridation in 95 vol% NH_3 – 5 vol% Ar. As a result, for NH_3 – Ar mixture the optimized ratio is 75 vol% NH_3 – 25 vol% Ar mixture.

**Fig.7: XRD patterns of samples after nitridation at (a) N_2-Ar; (b) NH_3-Ar.**
In the first stage, the conversion of Si in the NH₃-Ar mixture is lower than the conversion of Si in the N₂-Ar mixture. This can be explained that the molar of N₂ is double in comparison with NH₃. However, the reaction between Si and NH₃ may be easier than the reaction between Si and N₂.

Figure 7 illustrates the XRD pattern of the samples after nitridation by using N₂-Ar and NH₃-Ar mixtures. It is obvious that with N₂-Ar mixture, the obtained ceramic was mainly β-Si₃N₄ some traces of α-Si₃N₄. While with NH₃-Ar mixture α-Si₃N₄ is dominant phase in the ceramic materials.

IV. CONCLUSIONS

In short, silicon nitride (Si₃N₄) ceramic materials was successfully fabricated by a direct nitridation method. In the resultant ceramic materials, although β-Si₃N₄ was detected, but α-Si₃N₄ was the main phase of silicon nitride. Si₃N₄ ceramic materials can be obtained from amorphous silicon powder annealed at 1500°C under 75 vol% N₂ – 25 vol% Ar or 75 vol% NH₃ – 25 vol% Ar mixture at gas flow rate was 3 L/min for 400 min. The conversion of Si was 81 % in nitridation at 1300°C. It increased to 85 % at 1400°C, 88 % at 1600°C, and reached the maximum 92 % at 1500°C after 400 min. Percentages of α-Si₃N₄ content obtained with ammonia and argon is higher than those with nitrogen and argon. α-Si₃N₄ was detected at temperature of 1300°C, but the intensity was very weak. β-Si₃N₄ became apparent at the temperature of 1500°C. When the temperature increased to 1600°C, the amount of β-Si₃N₄ increased. Besides, β-Si₃N₄ appeared in the products and became the predominant crystalline phase when the synthesis temperature was above 1500°C. The nitrogen content of Si₃N₄ powder increased with the increase of N₂ flow and reached the maximum when the N₂ flow was 3L/ min.

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