Thermal noise and optomechanical features in the emission of a membrane-coupled compound cavity laser diode

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We demonstrate the use of a compound optical cavity as linear displacement detector, by measuring the thermal motion of a silicon nitride suspended membrane acting as the external mirror of a near-infrared Littrow laser diode. Fluctuations in the laser optical power induced by the membrane vibrations are collected by a photodiode integrated within the laser, and then measured with a spectrum analyzer. The dynamics of the membrane driven by a piezoelectric actuator is investigated as a function of air pressure and actuator displacement in a homodyne configuration. The high Q-factor (~3.4 \cdot 10^4 at 8.3 \cdot 10^{-3} \text{ mbar}) of the fundamental mechanical mode at ~73 kHz guarantees a detection sensitivity high enough for direct measurement of thermal motion at room temperature (~87 pm RMS). The compound cavity system here introduced can be employed as a table-top, cost-effective linear displacement detector for cavity optomechanics. Furthermore, thanks to the strong optical nonlinearities of the laser compound cavity, these systems open new perspectives in the study of non-Markovian quantum properties at the mesoscale.

The fast progress of cavity optomechanics has produced extraordinary advances in fabrication and characterization of nanomechanical objects\textsuperscript{1}, with impressive results towards the achievement of quantum effects in mesoscopic systems\textsuperscript{2–4}. Routinely dealing with sub-picometer displacements, the measure of an optomechanical system often requires complicated and expensive setups composed by optical interferometers and local oscillators to perform homodyne or heterodyne experiments. In this paper we show how a table-top, well known vibrometric technique such as the laser self-mixing\textsuperscript{7–9} can be pushed to measure the thermal motion of a typical optomechanical device, that is a metallic mirror mounted on a trampoline membrane\textsuperscript{10–12}. By shining a laser beam back into its resonant cavity after interacting with the external environment, an interferometric system is created which does not require any complicated arrangement or frequency demodulation. Showing the capability of detecting tens of pm displacements in its linear, stable regime, this technique would allow for detection of thermal noise up to cryogenic temperatures, making it an easy to implement, fast characterization benchmark for optomechanical resonators. At odds with standard optomechanical devices, such as whispering gallery mode resonators and optomechanical crystals, in which the displacement sensitivity is pushed towards the standard quantum limit, our technique offers a different advantage, integrating the high optical nonlinearities of the laser diode directly within the system. Moreover, by reaching the unstable dynamical regime, a rich and interesting physics can be accessed, which falls in the almost unexplored topic of active cavity optomechanics\textsuperscript{13,14}. Using the chaotic dynamics readily attainable in self-mixed lasers\textsuperscript{15,16} scenarios in which chaotic mechanical objects are created through radiation pressure effects can be easily imagined\textsuperscript{17}.

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The light-emitting, active medium is coupled to a mirror placed on top of a silicon nitride trampoline membrane. The membrane is mounted on a piezo ceramic actuator and placed inside a vacuum chamber, in order to drive its motion and control the environment pressure. When the membrane is displaced along the optical axis, the output signal is modulated according to equation (1). SEM image of the Si$_3$N$_4$ membrane. The yellow-colored square at the center of the membrane is the deposited gold layer. The white bar is 200 $\mu$m. The spectrum analyzer reports the power spectral density, and the total amount of displacement can be obtained through proper calibration. An example of measurement is reported for the membrane moved by the piezo actuator. The homodyne approach enables to collect the two motion quadratures of the membrane.

**Experimental setup**

**Optical bench and signal analysis.** The optomechanical laser setup is sketched in Fig. 1(a). The optical bench is a compound cavity working as a displacement sensor. The source includes a Littrow external cavity diode laser (ECDL), with lasing wavelength $\lambda_l \approx 945$ nm. The light-emitting, active medium is coupled to a Littrow angle reflection grating, placed at a distance $L = 1$ cm from the left facet of the diode. The zeroth diffraction order is reflected outside the ECDL and focused by an achromatic doublet (focal length 75 mm) onto a gold mirror placed on top of a silicon nitride trampoline membrane. The membrane is mounted on a piezo ceramic actuator and placed inside a vacuum chamber, in order to drive its motion and control the environment pressure when needed. The piezo actuator is a polymer covered multilayer, capable of elongating in one direction when biased, at a maximum frequency of some hundreds of kHz. The chip frame with the membrane is directly glued on its top surface and therefore is moving integrally with it. The membrane is then aligned to the optical path in such a way that light is reflected back into the ECDL to form a compound cavity. As the membrane moves, it changes the oscillation condition of the cavity. Normally this would simply cause a frequency shift in the lasing modes of the cavity: in our case, thanks to the feedback interferometric effect this translates into a modulation of the field amplitude in the laser cavity. The resulting laser radiation emitted from the right active region (AR) is collected by the integrated photodiode and the resulting voltage $V_{0} + \Delta V(t)$ is recorded by an oscilloscope and a spectrum analyzer. In the main experiment the external mirror is a gold layer deposited onto a silicon nitride membrane, which is mounted on a piezo actuator in order to drive its displacement by a voltage $V_p$. The resulted device is placed inside a vacuum chamber in order to control the environment pressure. The emitted radiation is focused by a lens onto a gold facet (labeled as 1 in Fig. 1(a)) is collected by an integrated photodiode (labeled as PD in Fig. 1(a)), which returns an electric potential proportional to the emitted power. For a fixed current bias, this potential, called readout voltage $V_{0}$, is measured with an oscilloscope and read out in the frequency domain. This is the essential quantity to be measured in order to demonstrate the working principle of the setup: by recording the modulation in the laser emitted power, informations about the motion of the membrane are recorded. A micrograph of the silicon nitride trampoline membrane employed in this work is shown in Fig. 1(b). A square-shaped, 5/45 nm Ti/Au layer is deposited on top of the 200 nm nitride, in order to improve its reflectivity. The first resonant mechanical mode oscillates orthogonally to the mirror surface, bending the tethers while keeping the central square parallel to the substrate. The mode frequency is $f_0 = 73279.0 \pm 0.3$ Hz with a quality factor $Q = 34000 \pm 3000$ (at 0.0083 mbar), limited by both squeeze film effect and thermoelastic damping of the four tethers. When the motion of the membrane is driven by a phase-coherent external displacement source, such as a piezo-ceramic actuator, the two quadratures of motion can be measured through the readout voltage. A typical measurement of amplitude and phase spectrum is shown in Fig. 1(c).
We numerically solved equations (1) with the parameters relative to our ECDL and found \( \Delta P \) orders of magnitude smaller than \( \Delta T \). In this case the e.m. radiation envelope can be assumed to evolve through states which verify equations (1) instantaneously\(^{25}\). This allows us to solve equations (1) for different static displacements of the membrane around its equilibrium position. For each position we can define the variation of the intracavity photon number \( \Delta P \) with respect to the photon number at the equilibrium position \( P_0 \). With the linear regime\(^{26}\) these two quantities are related to the readout voltage by \( \Delta P/P_0 = \Delta V/V_0 \). To estimate the sensitivity of our setup we roughly evaluated the numerical solution of equations (1) for displacements from 0 to 1 \( \mu \)m around the initial position. Given a readout voltage \( V_0 + \Delta V(t) \), the predicted linear displacement is

\[
\Delta x_{\text{theo}} = 1.212 \text{ [pm] } \text{ nV}^{-1} \Delta V.
\]

It is important to stress that the linear operation regime we found is valid only if there is no mode competition inside the cavity. If that is not the case, \( T_1 \) is not well defined anymore, and the Relative Intensity Noise (RIN) rises sensibly\(^{23,24}\).

### Table 1. Parameters employed to solve the theoretical laser equations.

| Parameter     | Value          | Description                           |
|---------------|----------------|---------------------------------------|
| \( I_0 \)     | 3.5 mA         | threshold current                     |
| \( I \)       | 63 mA          | current bias                          |
| \( V_r \)     | 2.15 \( \times \) 10^{-18} cm² | volume of the active region          |
| \( \tau_m \)  | 16 ps          | active region round-trip time         |
| \( q \)       | \(-1.6 \times 10^{-19}\) C | carrier elementary charge             |
| \( \tau_c \)  | 1.4 ns         | carrier lifetime                       |
| \( N_0 \)     | \( \tau_{th}/qV_r \) | threshold carrier density             |
| \( \tau_c \)  | 0.07           | diode left facet reflectivity         |
| \( r_0 \)     | 0.8            | grating maximum reflectivity          |
| \( \Delta \omega \) | \(\pi \times 50 \times 10^{12} \text{ rad s}^{-1}\) | grating spectral linewidth            |
| \( \omega_{cr} \) | 2\( \omega_{fc} \) | grating central frequency             |
| \( \tau_{G} \) | \(rg/(1 + i(\omega_{cr} - \omega_{fc})/\Delta \omega)\) | grating approximated reflectivity    |
| \( L \)       | 1.0 cm         | grating distance from diode left facet |
| \( \tau \)     | 2\( L/\omega \) | grating to left diode facet round-trip time |
| \( r_{ext} \) | 0.3            | SiN membrane reflectivity              |
| \( L_{ext} \) | 20 cm          | SiN membrane distance from diode left facet |
| \( \tau_{ext} \) | 2\( L_{ext}/c_0 \) | SiN membrane to diode left facet round-trip time |
| \( c_0 \)     | 3 \( \times 10^8 \) m/s | speed of light in vacuum               |

Connection between readout voltage and displacement: theoretical prediction. In this paragraph the relation between the readout voltage and the external mirror displacement is calculated within the semiclassical framework, in order to predict the sensitivity of the apparatus. The full derivation of the calculations is reported in section 1 of the Supplementary Information (SI). We consider a model system like the one sketched in Fig. 1(a). The Littrow ECDL is characterized essentially by the optical and electronic properties of the AR and the optical properties of the blazed angle grating\(^{22}\). In the traveling wave approximation the laser oscillation condition can be expressed with the following set of coupled equations\(^{23,24}\):

\[
\begin{align*}
I - I_0 &= \left( V - N_0 \right)/\tau_c + c_0 \left( n(n, N, P)g(n, N, P) + 1 \right), \\
\end{align*}
\]

The coefficients \( r_k \) and \( r_l \) are related to the amplitude of the right and left traveling wave at the AR facet interface, labeled as 2 in Fig. 1(a). The effective index \( n \) and the modal gain \( g \) are principle spectral functions of the laser carrier density \( N \) and the photon number \( P \); the other parameters employed are defined in Table 1. More details on the reflectivities, effective index and modal gain are reported in the SI. Equations (1) can be solved numerically to find \( N, P \) and the photon number \( \Delta P \), defined by the oscillation frequency of the membrane as \( \omega \). When the external mirror is moving, \( \tau_{ext} \) is modified, changing the solution of equations (1) as well. The cavity mode radiation envelope evolves with two different timescales: \( T_1 \), defined by the laser relaxation damping, and \( T_{M} \) defined by the oscillation frequency of the membrane as \( T_{M} = 1/\omega_{ext} \) (\( \sim 13 \mu s \)). We numerically solved equations (1) with the parameters relative to our ECDL and found \( T_1 \sim 10 \) ns for the lasing modes, roughly three orders of magnitude smaller than \( T_{M} \). In this case the e.m. radiation envelope can be assumed to evolve through states which verify equations (1) instantaneously\(^{25}\). This allows us to solve equations (1) for different static displacements of the membrane around its equilibrium position. For each position we can define the variation of the intracavity photon number \( \Delta P \) with respect to the photon number at the equilibrium position \( P_0 \). Within the linear regime\(^{26}\) these two quantities are related to the readout voltage by \( \Delta P/P_0 = \Delta V/V_0 \). To estimate the sensitivity of our setup we roughly evaluated the numerical solution of equations (1) for displacements from 0 to 1 \( \mu \)m around the initial position. Given a readout voltage \( V_0 + \Delta V(t) \), the predicted linear displacement is

\[
\Delta x_{\text{theo}} = 1.212 \text{ [pm] } \text{ nV}^{-1} \Delta V.
\]
Connection between readout voltage and displacement: experimental calibration. Using equation (3) we can link the measured voltage to the membrane displacement. To verify that our model well reproduces the experimental conditions, we carried out a calibration of the system by employing a commercial atomic force microscope (AFM). As the cantilever of the AFM has a mass comparable to the Si$_3$N$_4$ membrane and a resonance frequency of ~80 kHz, it is not possible to follow the motion of the membrane without strongly perturbing it. Therefore we chose to calibrate the motion using a mirror with the same reflectivity of the membrane, but deposited directly on the chip nitride film. The piezoelectric actuator was driven with a sinusoidal tone at frequency $f_0$ and amplitude ranging from 10 mVrms to 2 Vrms. The bulk displacement was then recorded with the AFM probe. We then measured the voltage readout obtained including the same mirror in the optomechanical setup, with the same driving conditions. The two sets of data are linearly proportional to the piezo drive, therefore we correlated the measured displacements with the voltage readout to get a calibrated setup sensitivity:

$$\Delta x_{cal} = \Delta x_V \cdot \frac{V_{t}}{V_{t0}}$$

Given the experimental $\Delta V(t)$, it is now possible to define the experimental RMS displacement $\Delta x \pm \delta x$, where $\delta x$ includes different contributions coming from the laser RIN, detector noise, calibration-induced error and the error on the theoretical linear fit. A detailed explanation of the different terms is reported in section 1.3 of SI.

Results and Discussion

Air pressure effect on the mechanical spectrum. We first characterized the effect of the air pressure on the motion of the suspended mirror. The membrane was placed inside a vacuum chamber, where the internal pressure was changed from 1 bar to $8.3 \cdot 10^{-3}$ mbar. The motion of the mirror was forced by a piezoelectric ceramic actuator, driven by a flat spectrum voltage defined as:

$$V_D(f) = 10 \text{ mV}_{\text{rms}}$$

through the whole frequency span.

At different pressures, we measured the spectrum of $\Delta V(t)$ in a homodyne scheme, by employing the piezo driving source as the local oscillator. The measurement resolution bandwidth (RBW) was 1.56 Hz, spanning over a 5 kHz spectral range centered on $f_0$. For the point at lowest pressure the RBW was 250 mHz and the frequency span was 200 Hz.

Using equation (4) the power spectral density is translated into the calibrated displacement spectral density ($DSD$), which measurements are reported in Fig. 2(a). The amplitude spectrum at 1 bar is clearly asymmetric, denoting a nonlinear dynamics of the oscillator; symmetry is gradually recovered as the pressure decreases. This behaviour is confirmed if we compare the total RMS displacements $\Delta x$ extracted from the spectra with the solutions of a classic forced linear harmonic oscillator (labeled $\Delta x_{HO}$), as shown in Fig. 2(b). The driving source has a fixed displacement spectrum, in order to resemble the effect of the piezo actuator, while $f_0$ and the damping rate are taken from the experimental data. More details on the model are reported in section 2 of the SI. As can be seen our experiment and theory show a fair agreement at high pressures; on the other hand, a wide discrepancy is found at low pressure. We attribute this effect to nonlinear effects induced by large deformations of the membrane, due to the reduced thin film damping and increased $Q$ factor of the resonator. While this is enough to get an amplitude saturation, the linewidth $\gamma_{tot}$, which is a parameter of the model, is basically unaffected and is still monotonically decreasing, as can be seen from the inset of Fig. 2(b). This fact produces the discrepancy, because $\Delta x_{HO} \propto 1/\sqrt{\gamma_{tot}}$. At the lowest pressure point, $Q$ factor assumes a value of $Q = 3.4 \pm 0.3 \cdot 10^4$, which we believe is still partially limited by thermoelastic damping.
Thermal and piezo-driven spectra. At the lowest achievable pressure \((8.3 \times 10^{-3} \text{ mbar})\), we focused on the displacement sensitivity of the apparatus, measuring the displacement spectra at different driving voltages of the piezo actuator. To increase the spectral resolution, the signals were acquired with a 250 mHz RBW, spanning over a 200 Hz spectral window centered on \(f_0\). The piezo driving voltage had the same functional shape described in equation (5), but its amplitude was varied in a range between 1 \(\mu\text{V}_{\text{rms}}\) and 100 \(\text{ mV}_{\text{rms}}\). Figure 3(a) shows the measured DSD for different driving voltages down to \(V_D = 0\). The \(\Delta x\) has been reported in panel (b). For large values of \(V_D\), it does not vary linearly with the piezo voltage; this can be due to a nonlinearity in the emitted power arising from mode competition inside the cavity, or to the breakdown of the linear elastic regime caused by the strong bending of the tethers which reduces the oscillation amplitude. As \(V_D\) is decreased, the linear behavior is recovered, and \(\Delta x_{\text{rms}}\) converges to the displacement induced by Langevin thermal fluctuations. By switching off \(V_D\) and directly acquiring the voltage signal, the thermal peak from the membrane is clearly visible, as reported in Fig. 3(c). Using again the results of our calibration (equation (4)), we estimate a thermal displacement of \(\Delta x = \pm 87,11\text{ pm}\). The experimentally found displacement has to be compared with the theoretical feedback evaluation, which gives a displacement of \(\Delta x_{\text{th}} = 40.7\text{ pm}\), where equation (3) has been used on the integrated voltage spectrum \((\Delta V = 33.6 \text{ nV}, V_0 = 5.5 \text{ mV})\). Both experimental and theoretical results are in good agreement.

By simply considering the phonon population at such temperature, we can have another rough theoretical estimate of the expected RMS thermal fluctuations by considering the equipartition theorem. The numerical simulations performed with a thermal transport finite-element-method solver (COMSOL Multiphysics) predict that the laser beam heats up the mirror to an average temperature of \(T = 354\text{ K}\). The resulting thermal fluctuation is

\[
\Delta x_{\text{th}} = \frac{2k_B T}{4\pi^2 m_{\text{eff}} f_0^2} \approx 38.3\text{ pm},
\]

where \(k_B\) is the Boltzmann’s constant and \(m_{\text{eff}} = 3.141 \times 10^{-11}\text{ Kg}\) the mechanical mode effective mass. Even in this case we have a reasonable agreement with the experimentally obtained displacement.

In conclusion, we employed a compound cavity laser diode for measuring small displacements of a silicon nitride trampoline membrane down to the thermal noise in the linear regime. The membrane movement directly shows in the laser emission thanks to the effect of optical feedback. By measuring average displacements as low as tens of picometers, our system can represent a fast, compact and cost effective optomechanical platform. Further upgrades of the setup, such as an improved environmental filtering and thermal and mechanical stabilization of the optical components, would push the resolution down to few pms, allowing for measurement of thermal motion at few K temperatures \((\Delta x \sim 10\text{ pm at } 30\text{ K})\). Moreover, the added functionality of getting a feedback directly on the laser source will enable the use of strong optical nonlinearities which can interact with mechanical elements through radiation pressure. In this active cavity optomechanical systems, schemes in which optical chaos is ingrained in a mechanical state can be readily imagined, opening the route to the investigation of a new class of mesoscale non-Markovian phenomena.
Methods
Sample fabrication and experimental setup. The trampoline membranes have been fabricated starting with a 300 nm LPCVD stoichiometric silicon nitride film grown on a 250 µm thick silicon FZ 2° wafer. The high temperature treatment (～800 °C) and the different thermal expansion between Si and Si₃N₄ gives the thin film a considerable tensile stress at room temperature (～900 MPa). At first the metallic mirrors were defined through e-beam lithography followed by a 5/50 nm Ti/Au thermal deposition and lift-off. A second aligned beam-write defined the membrane pattern which was transferred on the sample with plasma etching (CF₄/H₂). Finally the full membrane was released in a hot KOH solution. The membrane was mounted on a flat piezoceramic actuator from PI with a fundamental resonant frequency of 300 kHz. The full block was then placed in a vacuum chamber with optical access and carefully aligned with the laser optical path. Sample alignment was performed by using not-suspended mirrors placed on the same chip which were shaken by the piezo actuator. The drive voltage was a flat band voltage coming from the source port of a Hewlett Packard 89441A vector signal analyzer, which collected the drive voltage at port 1 and the readout voltage by the laser integrated photodiode at port 2. The scattering coefficient $S_{21}$ was then maximized to obtain a good optical alignment of the system. In order to exploit the linear operation regime for displacement detection, the laser was biased following the procedure described in section 1.3 of SI.

Theoretical modeling, simulations and calibration. Equation system (1) in the main text was numerically solved by using the commercial software Mathematica, with semi-empirical initial conditions and parameters independently extracted from the experiment. The membrane motion was simulated using a commercial FEM solver (Comsol Multiphysics) in order to predict the membrane frequency and motional mass. The simulation prediction was then independently confirmed by using a Polytech UHF-120 laser vibrometer. The calibration of the setup was performed with a Bruker Dimension Icon AFM. The deflection signal coming from the cantilever, in contact with the sample surface, was recorded in time using a high-speed detector (50 MHz bandwidth) following the Thermal Tune calibration protocol.

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Author Contributions
A.T. conceived and supervised the whole work. L.B. and A.P. conducted the main experiment and analysed the results, L.B. performed the theoretical calculations, A.P. fabricated the sample. L.B., A.P., L.M. and D.N.-U. devised the setup, L.B., A.A. and F.C. performed the calibration. L.B. and A.P. wrote the manuscript. All authors reviewed the manuscript.

Additional Information
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