Tunneling-percolation origin of nonuniversality: theory and experiments

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A vast class of disordered conducting-insulating compounds close to the percolation threshold is characterized by nonuniversal values of transport critical exponent $t$, in disagreement with the standard theory of percolation which predicts $t \approx 2.0$ for all three dimensional systems. Various models have been proposed in order to explain the origin of such universality breakdown. Among them, the tunneling-percolation model calls into play tunneling processes between conducting particles which, under some general circumstances, could lead to transport exponents dependent of the mean tunneling distance $a$. The validity of such theory could be tested by changing the parameter $a$ by means of an applied mechanical strain. We have applied this idea to universal and nonuniversal RuO$_2$-glass composites. We show that when $t > 2$ the measured piezoresistive response $\Gamma$, i.e., the relative change of resistivity under applied strain, diverges logarithmically at the percolation threshold, while for $t \approx 2$, $\Gamma$ does not show an appreciable dependence upon the RuO$_2$ volume fraction. These results are consistent with a mean tunneling dependence of the nonuniversal transport exponent as predicted by the tunneling-percolation model. The experimental results are compared with analytical and numerical calculations on a random-resistor network model of tunneling-percolation.

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I. INTRODUCTION

Despite that transport properties of disordered insulator-conductor composites have been studied for more than thirty years, some phenomena still remain incompletely understood. One such phenomenon is certainly the origin of nonuniversality of the DC transport near the conductor-insulator critical transition. According to the standard theory of transport in isotropic percolating materials, the bulk conductivity $\sigma$ of a composite with volume concentration $x$ of the conducting phase behaves as a power-law of the form

$$\sigma \sim \sigma_0 (x - x_c)^t,$$

where $\sigma_0$ is a proportionality constant, $x_c$ is the critical concentration below which the composite has zero conductivity (or more precisely the conductivity of the insulating phase) and $t$ is the DC transport critical exponent. The above expression holds true in the critical region $x - x_c \ll 1$ in which critical fluctuations extend over distances much larger than the characteristic size of the constituents. As a consequence, contrary to $\sigma_0$ and $x_c$ which depend on microscopic details such as the microstructure and the mean inter-grain junction conductance, the exponent $t$ is expected to be material independent. The universality of $t$ is indeed confirmed by various numerical calculations of random-resistor network models which have established that $t = t_0 \approx 2.0$ for three dimensional lattices to a rather high accuracy.\[3,4,5\]

Confirmations to the standard percolation theory of transport universality are found only in a limited number of experiments on real disordered composites. This is illustrated in Fig. 1 where we have collected 99 different values of the critical exponent $t$ and the critical threshold $x_c$ measured in various composites including carbon-black–polymer systems\[6-26\] and other metal-inorganic and -organic insulator granular metals are from Refs.\[26,39-48\]. The dashed line denotes the universal value $t_0 \approx 2.0$.
Examining all the data reported in Fig.1 one observes that the lack of universality is not limited to a particular class of materials, although the granular metals (empty diamonds in Fig.1) have somewhat less spread values of $t$ compared to the carbon-black and TFRs composites. Another important observation is that for the vast majority of the cases, the nonuniversal critical exponent is larger than $t_0$, and only few data display $t < t_0$. Finally, there is no clear correlation between $t$ and the critical concentration value $x_c$.

With the accumulation of experimental reports of nonuniversality, various theories have been proposed in order to find an origin to this phenomenon. In Ref.9 it was argued that, in carbon-black–polymer composites, long-range interactions could drive the system towards the mean-field regime for which $t = t_{\text{mf}} = 3.0$. This interpretation cannot however explain the observation of critical exponents much larger than $t_{\text{mf}}$, such as those of carbon-based composites or TFRs which display values of $t$ as high as $t \approx 5 - 10$. The authors of Ref.51 introduced the random-void (RV) model of continuum percolation where current flows through a conducting medium embedding insulating spheres placed at random. By using an earlier result they were able to show that for this model DC transport is described by an universality class different from that of standard percolation. The resulting critical exponent was found to be $t \approx 2.4$ for three dimensional systems. More recently, Balberg generalized the RV model in an attempt to explain higher $t$-values. The same author proposed also a model of transport nonuniversality based on an inverted RV model in which current flows through tunneling processes between conducting spheres immersed in an insulating medium. Within this picture, if the distribution function of the tunneling distances decays much slower than the tunneling decay, then the critical exponent becomes dependent of the mean tunneling distance $a$ and in principle has no upper bound.

In addition to the above models, there were also explanations pointing out that when Eq.(1) is used to fit experimental data not restricted to the critical region, “apparent critical exponents”, usually larger than $t_0$, could be misinterpreted as real critical exponents. Although this possibility cannot be excluded for some of the data reported in Fig.1 it is however quite unrealistic to identify the whole set of reported nonuniversal exponents as merely apparent.

The mean-field interpretation the RV model and its generalization, and the tunneling inverted RV model (also known as the tunneling-percolation model) have been devised to describe nonuniversality for various classes of materials. For example, the RV model applies in principle to composites where the linear size of the conducting particles is much smaller than that of the insulating grains so that the conducting phase can be approximated by a continuum. The tunneling-percolation model has been instead conceived to apply to those composites for which inter-grain tunneling is the main microscopic mechanism of transport, such as in carbon-black–polymer composites or in oxide-based TFRs. In principle, the two models could even coexist together if the continuum phase of a RV system is made of non-sintered conducting particles interacting through tunneling processes.

In this situation, the different proposed theories could account for the variety of nonuniversal exponents shown in Fig.1. However, it is also true that, in order to identify a given mechanism of nonuniversality for specific composites, little has been done beyond a mere fit to Eq.(1). For example, in Ref.52 the DC critical exponents have been examined together with the relative resistance noise exponent, and in Ref.53 a study on AC and magnetoresistive exponents for various composites has been presented. As a matter of fact, no conclusive answers have been reached and the different models of nonuniversality listed above have not proven to really apply to real composites.

In this paper we present our contribution to the understanding of the origin of transport nonuniversality by attacking the problem from a different point of view. In contrast with the mean-field hypothesis, the RV model and its extension, the tunneling-percolation model of Balberg predicts that the critical exponent $t$ acquires an explicit dependence upon a microscopic variable (the mean-tunneling distance $a$) which could be altered by a suitable external perturbation. So, if transport nonuniversality is driven by tunneling, it would be possible to change the value of the transport critical exponent $t$ by applying a pressure or a strain to the composite. Conversely, when a material belongs to some universality class (standard percolation theory, mean-field universality class, or the RV model) its exponent is expected to be independent of microscopic details and an applied strain would not change $t$.

We have applied this idea to RuO$_2$-based TFRs whose transport properties are known to be governed by inter-grain tunneling processes. In the following of this paper we show that the behavior of the piezoresistive response, i.e. the change of resistivity upon applied mechanical strain as a function of concentration $x$ of RuO$_2$, can be interpreted as due to a tunneling distance dependence of the DC critical exponent $t$, as originally proposed in Ref.51. The paper is organized as follows. In the next section we briefly review the tunneling-percolation theory and the RV model and its extension. In Sec.III we describe the theory of piezoresistivity for percolating composites and in Sec.IV we present our experimental results. The last section is devoted to a discussion and to the conclusions.

II. MODELS OF NONUNIVERSALITY

The RV models and the tunneling-percolation theory have one point in common. They all rely on the work of Kogut and Straley who first developed a theoret-
ical model of nonuniversality based on random-resistor networks. In this model, to each neighboring couple of sites on a regular lattice it is assigned with probability \( p \) a bond with conductance \( g \neq 0 \) and bond with \( g = 0 \) with probability \( 1 - p \). The resulting bond conductance distribution function is then:

\[
\rho(g) = ph(g) + (1 - p)\delta(g), \tag{2}
\]

where \( \delta(g) \) is the Dirac delta function and \( h(g) \) is the distribution function of the finite bond conductances. Close to the bond percolation threshold \( p_c \), the conductivity \( \Sigma \) of the network behaves as:

\[
\Sigma = \Sigma_0 (p - p_c)^t, \tag{3}
\]

where \( \Sigma_0 \) is a prefactor. In this and in the subsequent section we distinguish the conductivity \( \Sigma \) of a random-resistor network from that of real composites [Eq.(1)]. When \( h(g) = \delta(g - g_0) \) where \( g_0 \) is some nonzero value, Eq.(2) reduces to the standard bi-modal model for which, close to the percolation threshold, the network conductivity \( \Sigma \) follows Eq.(3) with \( t = t_0 \approx 2.0 \) for all three dimensional lattices. Instead, if \( h(g) \) has a power law divergence for small \( g \) of the form:

\[
\lim_{g \to 0} h(g) \propto g^{-\alpha}, \tag{4}
\]

where \( \alpha \leq 1 \), then universality is lost for sufficiently large values of the exponent \( \alpha \). For lattices of dimension \( D \), the resulting conductivity critical exponent is \( 25,59,60 \)

\[
t = \begin{cases} 
    t_0 & \text{if } (D - 2)\nu + \frac{1}{1-\alpha} < t_0 \\
    (D - 2)\nu + \frac{1}{1-\alpha} & \text{if } (D - 2)\nu + \frac{1}{1-\alpha} > t_0
\end{cases}, \tag{5}
\]

where \( t_0 \) is the universal value and \( \nu \) is the correlation-length exponent \( (\nu = 4/3 \text{ for } D = 2 \text{ and } \nu \simeq 0.88 \text{ for } D = 3) \). For \( D = 3 \) and by using \( t_0 \approx 2.0 \) and \( \nu \approx 0.88 \) the value of \( \alpha \) beyond which universality is lost is \( \alpha_c = 1 - 1/(t_0 - \nu) \approx 0.107 \). Only recently Eq.(4) has been demonstrated to be valid to all orders of \( \epsilon = 6 - D \) expansion in a renormalization group analysis.\(^{25,59,60}\)

In the original work of Refs.49, \( \alpha \) was considered as no more than a parameter of the theory without a justification on microscopic basis. This came later with the RV models and the tunneling-percolation theories.\(^{49,51,52}\) However, before discussing the microscopic aspect, we find it interesting to point out that Eq.(4) predicts that \( t \) cannot be lower than \( t_0 \) and it is in principle not bounded above. This is in qualitative agreement with the experimental values of \( t \) reported in Ref.44. Furthermore, Eq.(5) can give us some information on the distribution of \( t \) values expected by the theory. In fact, given some normalized distribution function \( f(\alpha) \) for the parameter \( \alpha \) and for \( D = 3 \), the distribution \( N(t) \) of the \( t \) values is:

\[
N(t) = \int_{-\infty}^{1} d\alpha f(\alpha) \delta(t - t(\alpha)) \int_{-\infty}^{\alpha_c} d\alpha f(\alpha) + \int_{\alpha_c}^{1} d\alpha f(\alpha) \delta \left(t - \nu - \frac{1}{1-\alpha}\right). \tag{6}
\]

If we assume that \( f(\alpha) \) can be approximated by a constant \( f \) for \( \alpha_c \leq \alpha \leq 1 \), then the above expression reduces to:

\[
N(t) = \left(1 - \frac{f}{t_0 - \nu}\right) \delta(t - t_0) + f \left(\frac{1}{t - \nu}\right)^2 \theta(t - t_0), \tag{7}
\]

which predicts a rapid decay \( N(t) \propto (t - \nu)^{-2} \) for \( t > t_0 \). Equation(7) is plotted in Fig.2 together with the distribution of \( t \) values reported in Fig.(1). The distribution \( N(t) \) has been renormalized to the number of data and the constant \( f \) has been fixed to reproduce the number of data with \( t \geq 3.0 \). There is an overall qualitative agreement between the distribution of the experimental \( t \) values and \( N(t) \). In particular, the asymmetry of the distribution and its tail for \( t > t_0 \approx 2.0 \) are well reproduced.

Fitting to a power law leads to a decay proportional to \( (t - \nu)^{-2.3 \pm 0.4} \) (see inset of Fig.2) which is in fair agreement with the predicted behavior \( (t - \nu)^{-2} \). Due to the limited number of \( t \) values available to us, the agreement with Eq.(7) could be fortuitous. However, the point here is that the gradual decrease of the number of times high values of \( t \) are reported is not necessarily due to “bad fits” to Eq.(7) but it can be, at least qualitatively, explained by the form of Eq.(6).

Let us now discuss the microscopic origin of the exponent \( \alpha \). According to the original RV model,\(^{25,59,60}\) the crucial parameter is the conducting channel width \( \delta \) left over from neighboring insulating spheres. For \( D = 3 \), the cross-section of the conducting channel has roughly the shape of a triangle and the resulting channel conductance \( g \) scales as \( g \propto \delta^{3/2} \). Hence, if \( p(\delta) \) is the distribution function of the channel width \( \delta \), the distribution \( h(g) \) of the conductances reduces to:

\[
h(g) = \int d\delta p(\delta) \delta(g - g_0 \delta^{3/2}), \tag{8}
\]

![FIG. 2: Distribution of the t-values reported in Fig.1. The solid line is Eq.4 renormalized in order to reproduce the total number of data. Inset: log-log plot of the distribution with a fit to the power law \( a(t - \nu)^{-b} \) with \( a = 192 \pm 62 \) and \( b = 2.5 \pm 0.4 \).](image-url)
where \( g_0 \) is a proportionality constant. For random distribution of equally sized spheres, \( p(\delta) \) is a constant for \( \delta \to 0 \) and Eq. (8) gives \( h(g) \propto g^{-1/3} \) for \( g \to 0 \). \( h(g) \) is therefore of the same form of Eq. (4) with \( \alpha = 1/3 > \alpha_c \) which, according to Eq. (3), predicts a critical exponent \( t = \nu + \frac{\delta}{3} \simeq 2.38 \). Despite that this value is only slightly larger than the universal exponent \( t_0 \simeq 2.0 \), the RV model has the merit of being a fully microscopic justification of Eq. (4). In order to allow for higher values of \( t \), in Ref. [32] it has been proposed to relax the condition that \( p(\delta) \) is a constant for \( \delta \to 0 \) by introducing the more general condition \( p \propto \delta^{-\omega} \) where \( \omega < 1 \). By using Eq. (8) one readily finds that \( h(g) \) is again given by Eq. (4) but with \( \alpha = \frac{1}{3} + \frac{2}{3} \omega \). Hence, the critical exponent is \( t = t_0 \) for \( \omega < \omega_c = \frac{4}{3} \alpha_c + \frac{1}{3} \simeq 0.4 \) or \( t = \nu + \frac{\delta}{3(1 - \omega)} \) for \( \omega > \omega_c \), i.e., \( t \) is no bounded above. The use of \( p \propto \delta^{-\omega} \) has been justified to be a simple ansatz to describe real composites in which correlations between the conducting and insulating phases may yield to deviations from the ideal RV system.

It is important to stress that the RV model of Ref. [32] does not give a breakdown of universality, but rather to a universality class different from that of the standard DC transport percolation on a lattice. In particular, the exponent \( t = \nu + \frac{\delta}{3} \) does not depend on the conductivity of the continuum and an applied isotropic strain or pressure, albeit affecting the channel width \( \delta \), does not change the relation \( g \propto \delta^{3/2} \). This should remain true also for the generalized RV theory of Ref. [32].

Contrary to the RV models, the tunneling-percolation theory of nonuniversality allows for a transport critical exponent dependent of the microscopic conductivities. In this model, current flows through tunneling processes between neighboring conducting spheres dispersed in an insulating medium and, for sufficiently low concentrations of the conducting spheres, the ensemble of tunneling bonds form a percolating network. The coexistence of tunneling and percolation has been recently settled by experiments probing the local electrical connectivity of various disordered systems, and a recent review on this issue can be found in Ref. [51]. In what follows, we consider the situation in which grain charging effects can be neglected with respect to the tunneling processes, as encountered in systems with sufficiently large conducting grains and/or high temperatures. Let us consider then the inter-particle tunneling conductance:

\[
 g = g_0 e^{-2(r-\Phi)/\xi}, \tag{9}
\]

where \( g_0 \) is a constant, \( \xi \) is the tunneling factor which is of the order of few nm, \( r \) is the distance between the centers of two neighboring spheres of diameter \( \Phi \) (\( r \geq \Phi \) for impenetrable particles). If we denote with \( P(r) \) the distribution function of adjacent inter-sphere distances \( r \), the bond conductances are then distributed according to:

\[
 h(g) = \int_\Phi^\infty dr P(r) \delta \left[ g - g_0 e^{-2(r-\Phi)/\xi} \right]. \tag{10}
\]

Balberg notices that if \( P(r) \) had a slower decay than Eq. (4) for \( r \to \infty \), then \( h(g) \) would develop a divergence for \( g \to 0 \). For example, by assuming that

\[
 P(r) = \frac{e^{-(r-\Phi)/(a-\Phi)}}{a-\Phi}, \tag{11}
\]

is a good approximation for the (normalized) distribution of inter-particle distances, then Eq. (10) would reduce to

\[
 h(g) = \frac{1 - \alpha}{g_0} \left( \frac{g}{g_0} \right)^{-\alpha}, \tag{12}
\]

with \( \alpha = 1 - \frac{\xi}{a-\Phi} \) where \( a \) is the mean distance between neighboring particles. For \( \frac{\xi}{a-\Phi} \leq 1 - \alpha_c \simeq 0.9 \), transport becomes nonuniversal with \( t = \nu + \frac{\delta}{2(1-\omega)} \). It is important to stress that here nonuniversality is not driven by geometrical factors as in the RV model, but rather by physical parameters such as \( \xi \) and \( a \). These can be different depending on the composite and can be modified by a suitable external perturbation. In fact, in the case of a applied pressure or strain, the mean tunneling distance \( a \) would change leading to a modification of the critical exponent \( t \). As already pointed out in the introduction, the detection of such an effect would be a direct signature of a tunneling-percolation-like mechanism of transport nonuniversality.

The tunneling-percolation theory in its original formulation relies on Eq. (11) which should be regarded as a phenomenological model of the distribution function of inter-particle distances. Recently, however, a microscopic derivation of Eq. (11) has been formulated for a bond-percolation regular network in which the bonds have probability \( p \) of being occupied by a string of \( n \) non-overlapping spheres. In this case, in fact, Eq. (11) is the exact distribution function for spheres placed in a one-dimensional channel and the resulting bond conductance distribution is proportional to \( g^{-\alpha_n} \) where \( \alpha_n = 1 - \frac{\xi}{a_n-\Phi} \) and \( a_n \) is the mean inter-particle distance for a bond occupied by \( n \) spheres. Despite of its over-simplification, this construction shows however that the tunneling-percolation mechanism of nonuniversality can be justified by a fully defined model, without need of phenomenological forms of \( P(r) \).

### III. THEORY OF PIEZORESISTIVITY

The sensitivity of the tunneling-percolation mechanism of nonuniversality to variations of the mean tunneling distance can be exploited by imposing a volume compression or expansion to the system. As we discuss below, under these circumstances the relative change of resistivity, i.e., the piezoresistive response, changes dramatically depending on whether the DC exponent is universal \( (t = t_0) \) or instead it is driven away from universality by the tunneling-percolation mechanism.
Let us consider the rather general situation in which a parallelepiped with dimensions $L_x, L_y$ and $L_z$ is subjected to a deformation along its main axes $x, y,$ and $z$. The initial volume $V = L_x L_y L_z$ changes to $V (1 + \phi)$ where $\phi = \varepsilon_x + \varepsilon_y + \varepsilon_z$ is the volume dilatation and $\varepsilon_i = \delta L_i/L_i$ are the principal strains along $\varepsilon_i$ with $i = x, y, z$. In the absence of strain, we assume that the conductivity $\Sigma$ of the parallelepiped is isotropic, so that the conductance $G_i$ measured along the $i$ axis is

$$G_i = \frac{\delta \Sigma_i}{\Sigma} - \varepsilon_i + \varepsilon_j + \varepsilon_k,$$

(13)

where

$$\frac{\delta \Sigma_i}{\Sigma} = - \Gamma_{\parallel} \varepsilon_i - \Gamma_{\perp} (\varepsilon_j + \varepsilon_k)$$

(14)

are the relative variation of the conductivity along the $i = x, y, z$ directions. The coefficients $\Gamma_{\parallel}$ and $\Gamma_{\perp}$ are the longitudinal and transverse piezoresistive factors defined as:

$$\Gamma_{\parallel} = - \frac{d \ln(\Sigma_i)}{d \varepsilon_i} = \frac{d \ln(\rho_i)}{d \varepsilon_i},$$

(15)

$$\Gamma_{\perp} = - \frac{d \ln(\Sigma_j)}{d \varepsilon_i} = \frac{d \ln(\rho_j)}{d \varepsilon_i} \quad (i \neq j),$$

(16)

where $\rho_i = \Sigma_i^{-1}$ is the resistivity along the $i$-axis and $\ln$ is the natural logarithm. The distinction between longitudinal, $\Gamma_{\parallel}$, and transverse, $\Gamma_{\perp}$, piezoresistive responses is important whenever the values of the strains $\varepsilon_i$ depend on the direction, as is encountered when the sample is subjected to uniaxial distortions as those induced in cantilever beam experiments (see next section).

In what follows, we are mainly interested in the isotropic (or hydrostatic) piezoresistive factor $\Gamma$ defined as the resistivity change induced by the isotropic strain field $\varepsilon_i = \varepsilon$ for all $i = x, y, z$:

$$\Gamma = - \frac{d \ln(\Sigma)}{d \varepsilon} = \frac{d \ln(\rho)}{d \varepsilon},$$

(17)

which can be obtained by applying an hydrostatic pressure to the parallelepiped. However, $\Gamma$ can also be obtained by setting $\varepsilon_i = \varepsilon$ in Eq. (14) yielding:

$$\Gamma = \Gamma_{\parallel} + 2 \Gamma_{\perp},$$

(18)

which is a useful relation when the experimental setup does not permit to apply an isotropic strain field.

Let us now study how the tunneling-percolation theory of non-universality affect the piezoresistive factor $\Gamma$. To this end, we assume that a cubic bond-percolation network is embedded in a homogeneous elastic medium and that the elastic coefficients of the network and the medium are equal. Under an isotropic strain field $\varepsilon_i = \varepsilon$ ($i = x, y, z$) the mean tunneling distance $a$ changes to $a(1 + \varepsilon)$ independently of the bond orientation. Hence, by assuming for simplicity that $\Phi \to \Phi(1 + \varepsilon)$, the tunneling parameter $\alpha = 1 - \frac{\delta^2}{\alpha}$ entering Eq. (3) becomes $\alpha \to \alpha + (1 - \alpha)\varepsilon$ for $\varepsilon \ll 1$. According to the discussion of Sec. III and to Eqs. (10) and (11), close to the percolation threshold $p_c$, the piezoresistive factor behaves therefore as:

$$\Gamma = \frac{\Gamma_0}{1 - \alpha},$$

(19)

$$\Gamma_0 = \frac{-d \ln(\Sigma_0)}{d \varepsilon} = -(1 - \alpha) \frac{d \ln(\Sigma_0)}{d \alpha},$$

(20)

$$\frac{d \varepsilon}{d \alpha} = \frac{1}{1 - \alpha},$$

(21)

where we have used $d \alpha/d \varepsilon = (1 - \alpha)$. The tunneling distance dependence of the DC transport exponent is therefore reflected in a logarithmic divergence of $\Gamma$ as $p \to p_c$. Instead, when $\alpha < \alpha_c$, the DC exponent remains equal to $\alpha_0$ also when $\varepsilon \neq 0$ and the resulting piezoresistive factor is simply equal to $\Gamma = \Gamma_0$, independently of the bond probability $p$.

It is worth to note that, as shown in Refs. 64, contrary to $\Gamma$, the breakdown of universality has no effect on the piezoresistive anisotropy defined as $\chi = (\Gamma_{\parallel} - \Gamma_{\perp})/\Gamma_{\parallel}$ which behaves as $\chi \propto (p - p_c)^{3}$ where the critical exponent $\lambda$ is independent of $\alpha$ also when $\alpha > \alpha_c$.

Equation (19) is an exact result as long as we are concerned with the $p - p_c$ dependence close to the percolation threshold. However, in addition to the prefactor of the logarithm, $\Gamma$ depends also on the tunneling parameter $\alpha$ through the term $\Gamma_0$. This dependence is far to be trivial. In fact, consider a tensile strain ($\varepsilon > 0$) which enhances the bond tunneling resistances leading to an overall enhancement of the sample resistivity. In this case, $\Gamma = d \ln(\rho)/d \varepsilon$ must be strictly positive. This means that $\Gamma_0 > 0$ when $\alpha \leq \alpha_c$ while, from Eq. (19), when $\alpha > \alpha_c$ $\Gamma_0$ does not need to be positive to ensure $\Gamma > 0$ because of the presence of the logarithmic divergence. In the next subsections we provide evidences that indeed $\Gamma_0$ changes sign in passing from $\alpha \leq \alpha_c$ to $\alpha > \alpha_c$ by showing that both the effective medium approximation and numerical calculations on cubic lattices give negative values of $\Gamma_0$ for nonuniversal DC transport. Together with the logarithmic divergence of $\Gamma$ for $p \to p_c$, a negative value of $\Gamma_0$ would be an additional signature of a tunneling-percolation mechanism of nonuniversality.

### A. Effective medium approximation

In the effective medium approximation (EMA) the conductivity $\Sigma = g/\ell$ of a bond percolation cubic lattice (with bond length $\ell$) is obtained by the solution of the following integral equation (see for example Ref. 2):

$$\int_0^\infty dg \rho(g) \frac{g - g}{g + 2g} = 0,$$

(22)
where \( \rho(g) \) is the distribution function of the bond conductances \( g \) given in Eq. (23). Close to the percolation threshold \( p_c \) \( (p_c = 1/3 \text{ in EMA}) \) and by using the tunneling-percolation distribution of Eq. (22) with \( g_0 = 1 \), the above expression reduces to:

\[
(1 - \alpha)\bar{g} \int_0^1 dg \frac{g^{-\alpha}}{g + 2\bar{g}} = \frac{3}{2} (p - p_c). \tag{23}
\]

It is clear that for \( \bar{g} \to 0 \) the integral in Eq. (23) remains finite as long as \( \alpha < 0 \), while for \( \alpha > 0 \) it diverges as \( \bar{g}^{-\alpha} \). Hence, for \( p \to p_c \) the conductivity \( \Sigma \) follows the power law behavior of Eq. (23) with \( t = 1 \) for \( \alpha < 0 \) and \( t = 1/(1 - \alpha) \) for \( \alpha > 0 \). The corresponding prefactor \( \Sigma_0 \) can be evaluated explicitly:

\[
\Sigma_0(\alpha < 0) = \frac{3}{2} \frac{\alpha}{1 - \alpha} \tag{24}
\]

\[
\Sigma_0(\alpha > 0) = \left[ \frac{3}{2^{1 - \alpha} \gamma(\alpha) \gamma(2 - \alpha)} \right]^{1/(1 - \alpha)} \tag{25}
\]

where \( \gamma \) is the Euler gamma function. Note that the above expressions gives \( \Sigma_0(\alpha \to 0) = 0 \), which is a result due to enforcing \( \Sigma \) to behave as Eq. (3). Actually, at \( \alpha = 0 \) and for \( \bar{g} \ll 1 \) Eq. (23) reduces to \( -\bar{g} \ln(2\bar{g}) = \frac{3}{2} (p - p_c) \) which leads to logarithmic corrections in the \( p - p_c \) dependence of \( \bar{g} \). For \( \alpha \neq 0 \), the logarithmic corrections are not important only in a region around \( p = p_c \) which shrinks to zero as \( \alpha \to 0 \).

\( \Sigma_0(\alpha) \) is plotted in Fig. 3 as a function of \( \alpha \). For \( \alpha < 0 \) \( (\alpha > 0) \), \( \Sigma_0(\alpha) \) is a decreasing (increasing) function of \( \alpha \). Hence, according to the second equality of Eq. (24), \( \Gamma_0 \) is expected to be positive for \( \alpha < 0 \) and negative for \( \alpha > 0 \). This is confirmed in the inset of Fig. 3 where \( \Gamma_0 \) is plotted as a function of \( \alpha \). Note that as \( \alpha \to 1 \), \( \Gamma_0 \) goes to \( -\infty \). In fact, from Eq. (25), in this regime \( \Sigma_0(\alpha) \approx \frac{1}{2} 2^{1/(1 - \alpha)} = \frac{1}{2} 2^t \) which implies that:

\[
\Gamma_0 \approx -\ln(3) \frac{dt}{de}. \tag{26}
\]

\section*{B. Monte Carlo calculations on cubic lattices}

To evaluate the \( \alpha \) dependence of the prefactor \( \Sigma_0 \) of Eq. (23) we have used the transfer-matrix method applied to a cubic lattice on \( N - 1 \) sites in the \( z \) direction, \( N \) sites along \( y \), and \( L \) along the \( x \) direction. Periodic boundary conditions are used in the \( y \) direction while a unitary voltage is applied to the top plane, and the bottom plane is grounded to zero. For sufficiently large \( L \) \( (L \gg N) \) this method permits to calculate the conductivity \( \Sigma_N \) per unit length of a cubic lattice of linear size \( N \). The transfer matrix algorithm is particularly efficient at the bond percolation threshold \( p_c \approx 0.2488126 \), and it is usually used in connection with finite size scaling analysis of \( \Sigma_N \) to extract highly accurate values of the DC exponent \( t \).

In performing the calculations we have considered the following geometries: \( N = 6 \) \( (L = 5 \times 10^7) \), \( N = 8 \) \( (L = 2 \times 10^7) \), \( N = 10 \) \( (L = 1 \times 10^7) \), \( N = 12 \) \( (L = 8 \times 10^6) \), \( N = 14 \) \( (L = 4 \times 10^6) \), and \( N = 16 \) \( (L = 2 \times 10^6) \). From Eq. (23), the resulting conductivity \( \Sigma_N \) for finite \( N \) at \( p = p_c \) can be written as:

\[
\Sigma_N = \Sigma_0(\alpha)[p_c - p_c(N)]^{t(\alpha)}, \tag{27}
\]

where we have explicitly written the \( \alpha \) dependence of the prefactor and of the exponent. In the above expression, \( p_c(N) \) is the percolation threshold of a finite systems of linear size \( N \). Only at \( N \to \infty \), \( p_c(N) \) coincides with the percolation threshold \( p_c \) of an infinite system, while for finite values of \( N \) the two quantities are related via a finite size scaling relation of the type:

\[
p_c - p_c(N) \approx A N^{-\nu}(1 + B N^{-\omega}), \tag{28}
\]

where \( \nu \approx 0.88 \) is the correlation length exponent, \( A \) and \( B \) are constant and \( \omega \) is the first scaling correction exponent. All the constants appearing in Eq. (28) depends solely on the connectivity of the network, and are therefore independent of the tunneling factor \( \alpha \). By inserting Eq. (28) in Eq. (27), the conductivity reduces to:

\[
\Sigma_N \approx \Sigma_0(\alpha) N^{-t(\alpha)/\nu}(1 + B N^{-\omega})^{t(\alpha)}, \tag{29}
\]

where

\[
\Sigma_0(\alpha) = \Sigma_0(\alpha) A^{t(\alpha)}. \tag{30}
\]

Our strategy to calculate \( \Sigma_0(\alpha) \) is the following. We first fit or numerical data of \( \Sigma_N \) with Eq. (29) by setting \( \omega \) fixed. In this way we obtain the exponent \( t(\alpha) \) and
the prefactor $\Sigma_0(\alpha)$. We repeat this procedure for various values of $\alpha$ ranging from $\alpha \simeq 1$ down to $\alpha = -\infty$ which corresponds to the Dirac delta distribution function $h(\infty) = \delta(g-1)$. In this limit, $\Sigma_0(\infty)$ is known with a rather good accuracy, permitting us to calculate from Eq. (29) the value of the constant $A$. In this way we finally obtain $\Sigma_0(\alpha) = \Sigma_0(\alpha)/A^{\alpha}$ by using the values of the exponent calculated before.

In Fig. 4 we plot the values of the exponent $t$ as a function of $\alpha$ obtained by setting $\omega = 1$ in Eq. (28). We have checked that this choice for $\omega$ produced the best overall agreement with the exact result Eq. (5) shown in Fig. 4 by the solid line. In accord with the $\alpha$-independence of $B$, we noticed little deviations from $B \simeq 0.7$ in the whole range of $\alpha$. The agreement between the calculated exponent and Eq. (5) is very good far away from $\alpha = \alpha_c \simeq 0.107$. In the vicinity of $\alpha_c$ the competition between two different fixed points leads to a less good agreement, as already noticed in previous works.

In Fig. 5 we report the calculated values of the prefactor $\Sigma_0(\alpha)$ of the finite size scaling relation Eq. (29) as a function of $\alpha$. Inset: behavior of $\Sigma_0(\alpha)$ as a function of $\log(-\alpha)/[1 + \log(-\alpha)]$ (where log is the logarithm to base 10) for $\alpha = -1, -10, -100, -1000$, and $\alpha = -\infty$. This latter case corresponds to a Dirac delta distribution function: $h(g) = \delta(g - 1)$ for which we obtain $\Sigma_0(\infty) = 0.960 \pm 0.007$.

Our final results for $\Sigma_0(\alpha) = \Sigma_0(\alpha)/1.55^{\alpha}$ are plotted in Fig. 6 where the $t(\alpha)$ values are those plotted in Fig. 4. As for the EMA case, $\Sigma_0(\alpha)$ decreases for $\alpha$ sufficiently smaller than $\alpha_c \simeq 0.107$ while it increases for $\alpha > \alpha_c$. Hence, also our Monte Carlo calculations confirm that the $p$-independent part $\Gamma_0$ of the piezoresistive response is positive or negative, depending whether $\alpha$ is less than or larger than $\alpha_c$, respectively. In the inset of Fig. 4 we report a semi-logarithmic plot of $\Sigma_0(\alpha)$ as a function of the DC exponent $t$. For high values of $t$, the data are reasonably well fitted by a relation of the form $\Sigma_0(\alpha) = ab^t$ with $a = 0.018 \pm 0.004$ and $b = 1.9 \pm 0.1$ (solid line in the inset of Fig. 6). Hence:

$$\Gamma_0 = -\ln(b) \frac{dt}{d\varepsilon} \simeq -0.6 \frac{dt}{d\varepsilon}, \quad (31)$$

confirming the asymptotic formula Eq. (20) obtained within EMA.
IV. EXPERIMENT

In this section we describe our experiments aimed to investigate the piezoresistive response of disordered conductor-insulator composites made of conducting RuO$_2$ particles embedded in a insulating glass. As shown in Fig.1 this kind of TFRs displays both universal ($t \simeq t_0$) and nonuniversal ($t > t_0$) behaviors of transport, although the factors responsible for such changes have not yet been identified. In addition, transport in such kind of materials is known to be governed by electron tunneling through the glassy film separating two neighboring conducting particles. Hence, RuO$_2$-based TFRs are ideal systems to test whether a tunneling-percolation mechanism of transport nonuniversality sets in.

Our samples were prepared starting with a glass frit with the following composition: PbO (75% wt), B$_2$O$_3$ (10% wt), SiO$_2$ (15% wt). In order to avoid crystallisation, 2% wt of Al$_2$O$_3$ was added to the glass powder. After milling, the glass powder presented an average grain size of about 3 $\mu$m, as measured from laser diffraction analysis. Thermogravimetric measurements showed negligible loss in weight, indicating glass stability and no PbO evaporation during firing up to 800 $^\circ$C, and differential scanning calorimetry measurements indicated a softening temperature of about 460 $^\circ$C. For the conductive phase we used two different RuO$_2$ powders with nominal grain sizes of 400 nm (series A) and 40 nm (series B). Transmission electron microscope analysis confirmed that the finer powder was made of nearly spherical particles with a diameter of about 40 nm, while the coarser powder had more dispersed grain sizes (100 nm mean) with less regular shape.

TFRs were then prepared by mixing several weight fractions of the two series of RuO$_2$ powder with the glass particles. An organic vehicle made of terpineol and ethyl cellulose was added in a quantity of about 30% of the total weight of the RuO$_2$-glass mixture. The so-obtained pastes were screen printed on 96% alumina substrates on pre-fired gold terminations. For the conductance measurements, eight resistors 1.5 mm wide and different lengths ranging from 0.3 mm up to 5 mm were printed on the same substrate. The resistors were then treated with a thermal cycle consisting of a drying phase (10 min at 150 $^\circ$C) followed by a plateau, reached at a rate of 20 $^\circ$C/min, of 15 min at various firing temperatures $T_f$ (see belowand Table I). After firing, the thickness of the films was about 10 $\mu$m.

In Fig.7 and Fig.8 we show scanning electron microscope (SEM) images of the surfaces of A and B series, respectively, with RuO$_2$ volume concentration $x = 0.08$. The firing temperature $T_f$ is $T_f = 525^\circ$C and $T_f = 600^\circ$C for the A series [Figs. 7(a) and (b), respectively], while

**FIG. 7:** SEM images of the surface of the A series with RuO$_2$ volume fraction $x = 0.08$ and nominal RuO$_2$ grain size of 400 nm (see text) for different firing temperatures $T_f$. (a): $T_f = 525^\circ$C; (b):$T_f = 600^\circ$C

**FIG. 8:** SEM images of the surface of the B series with RuO$_2$ volume fraction $x = 0.08$ and nominal RuO$_2$ grain size of 40 nm (see text) for different firing temperatures $T_f$. (a): $T_f = 550^\circ$C; (b):$T_f = 600^\circ$C
$T_f = 550^\circ C$ and $T_f = 600^\circ C$ for the B series [Figs. 8(a) and (b), respectively]. In the images, dark areas indicate highly conducting regions rich of RuO$_2$ clusters, while the white zones are instead made of insulating glass. The grey regions surrounding the RuO$_2$ clusters indicate that some conduction is present, although much lower than the dark areas, which we ascribe to finer RuO$_2$ particles dispersed in the glass. At the length scale shown in the figures the conducting and insulating phases are not dispersed homogeneously, with the RuO$_2$ clusters segregated between large glassy regions of few micrometers in size. This segregation effect in TFRs is well known and it is due to the large difference in size between the fine conducting particles and the much coarser glassy grains employed in the preparation of the resistors. Concerning the effect of the firing temperature, it is interesting to note that for the B series there is not much qualitative difference in the microstructure between $T_f = 550^\circ C$ [Fig. 8(a)] and $T_f = 600^\circ C$ [Fig. 8(b)], while for the A series it appears that the conducting phase is more clustered at low firing temperature [Fig. 7(a)] than at high $T_f$ [Fig. 7(b)], where the appearance of grey regions indicate larger RuO$_2$ dispersion in the glass.

In Fig. 8 we report the room temperature conductivity $\sigma$ measured for four different series of TFRs (see Table I) as functions of the RuO$_2$ volume concentration $x$. As shown in Fig. 8(a), $\sigma$ vanishes at rather small values of $x$, as expected when the mean grain size of the conducting phase ($40 \text{ nm}$ and $< 400 \text{ nm}$) is much smaller than that of the glass ($1-5 \mu m$). The same data are re-plotted in the ln-ln plot of Fig. 9(b) together with the corresponding fits to Eq. (11) (solid lines) and the best-fit parameters $\sigma_0$, $x_c$ and $t$ are reported in Table I. As it is clearly shown, our conductivity data follow the power law behavior of Eq. (11) with exponent $t$ close to the universal value $t_0 \approx 2.0$ for the A1 series ($t = 2.15 \pm 0.06$) or markedly nonuniversal as for the A2 case which displays $t = 3.84 \pm 0.06$. The B1 and B2 series have nearly equal values of $t$ ($t \approx 3.16$) falling in between those of the A1 and A2 series.

It is tempting to interpret the different transport behaviors of the A1 and A2 series by referring to the microstructures reported in Fig. 7. It appears that universal behavior is found for the more clustered samples [Fig. 7(a)] while the nonuniversal behavior is observed when the conducting phase is more dispersed in the glass [Fig. 7(b)]. This interpretation is coherent with the nonuniversality of both B1 and B2 series, which indeed display a large amount of RuO$_2$ dispersion evidenced by the grey regions in Figs. 8(a) and (b). As discussed in Sec. II the microstructure has a primary role for the onset of nonuniversality. This is certainly true for the tunneling-percolation model in which the microstructure governs the tunneling distribution function. In this respect, the SEM images reported in Figs. 7 and 8 may suggest that for the A1 series [Fig. 7(a)], since the RuO$_2$ grains are less dispersed, the tunneling distribution function is much narrower than those of the other series.

To measure the piezoresistive response, four resistors for each series and with equal RuO$_2$ content were screen printed in a Wheatstone bridge arrangement on the top of alumina cantilever bars $51 \text{ mm}$ long, $b = 5 \text{ mm}$ large, and $h = 0.63 \text{ mm}$ thick. The thermal treatment was the same as for the samples used to for the conductivity measurements. The cantilever was clamped at one end and different weights were applied at the opposite end. The resulting substrate strain $\varepsilon$ along the main cantilever axis can be deduced from the relation $\varepsilon = 6Mgd/(Eb^2)$, where $d$ is the distance between the resistor and the point of applied force, $E = 332.6 \text{ GPa}$ is the reduced Al$_2$O$_3$ Young modulus, $g$ is the gravitational acceleration and $M$ is the value of the applied weight. By fixing the main cantilever axis parallel to the $x$ direction, then in plain strain approximation the strain field transferred to the resistors is $\varepsilon_x = \varepsilon$, $\varepsilon_y = 0$, and $\varepsilon_z = -\nu/(1-\nu)\varepsilon$, where $\nu = 0.22$ is the Poisson ratio of $96\%$ Al$_2$O$_3$. Two different cantilevers were used for the measurements of the longitudinal and transverse piezoresistive signals obtained by recording the conductivity changes along the $x$ and $y$ directions, respectively. Then, according to Eq. (11):

$$\frac{\delta \sigma_x}{\sigma} = -\left(\Gamma_\parallel - \Gamma_\perp \frac{\nu}{1-\nu}\right) \varepsilon, \quad (32)$$

$$\frac{\delta \sigma_y}{\sigma} = -\Gamma_\perp \frac{1 - 2\nu}{1 - \nu} \varepsilon. \quad (33)$$

In Fig. 10(a) and Fig. 10(b) we plot the conductivity variations along the $x$ and $y$ direction respectively as a function of $\varepsilon$ for the A2 series. The RuO$_2$ volume fractions are $x = 0.23, 0.154, 0.11, 0.095,$ and $0.085$ from bottom to top. In the whole range of applied strains, the signal changes linearly with $\varepsilon$, permitting to extract from the slopes the linear fits of $\delta \sigma_i/\sigma$ vs $\varepsilon$ the values of the longitudinal and transverse piezoresistive factors.
Eq. (19) which predicts a logarithmic divergence at the
percolation threshold when the exponent $t$ is nonuniv-
versal. By using the equivalence between Eq. (17) and
Eq. (18) our data could then be used to verify this hy-
pothesis. This is done in Fig. 11(b) where $\Gamma$ is plotted as
a function of $\ln(x - x_c)$ with $x_c$ values extracted from the
conductivity data. In the entire range of concentrations,
and for all the series A1, ...,B2, $\Gamma$ is rather well fitted by
the expression:

$$
\Gamma = \begin{cases} 
\Gamma_0 & t = t_0 \\
\Gamma_0 - \frac{dt}{d\epsilon} \ln(x - x_c) & t > t_0 
\end{cases}
$$

which is Eq. (19) rewritten in terms of RuO$_2$ volume
concentration $x$. The A1 series, which has DC exponent
$t = 2.15 \pm 0.06$ close to the universal value, has no $x$
dependence of $\Gamma$, while the other series A2, B1, and B2,
characterized by nonuniversal exponents, display a loga-
	hropic divergence of $\Gamma$ as $x \rightarrow x_c$. This is in agreement
with the expectations of the tunneling-percolation the-
ory. Furthermore, as shown in Table I and in the inset
of Fig. 11(b), the factor $\Gamma_0$ is positive for the A1 series
and negative for A2, B1, and B2, in agreement with the
results of the last section. For the latter series, $\Gamma_0$
behaves as $\Gamma_0 = -(1.9 \pm 0.5)dt/d\epsilon$ (see inset of Fig. 11(b)) in
accord with the asymptotic relations obtained by EMA,
Eq. (26), and by our numerical calculations, Eq. (31).

The logarithmic divergence of $\Gamma$ for the series having

through Eqs. (22, 23). The so obtained $\Gamma_\parallel$ and $\Gamma_\perp$
values of the A2 series are plotted in Fig. 10(c) as a
function of RuO$_2$ volume concentration $x$. The main feature
displayed in Fig. 10(c) is that the longitudinal and the
transverse piezoresistive factors are not much different
and both seem to diverge as $x$ approaches the percolation
threshold $x_c \sim 0.067$. The fact that $\Gamma_\parallel \sim \Gamma_\perp$ is consis-
tent with the vanishing of the piezoresistive anisotropy
ratio $\chi = (\Gamma_\parallel - \Gamma_\perp)/\Gamma_\parallel$ at the percolation threshold, as
discussed in the previous section.

Note instead that the transport exponent for the A2
series is $t \approx 3.84$ (see Table I), that is much larger than
$t_0 = 2$. Hence the divergence of $\Gamma_\parallel$ and $\Gamma_\perp$ as $x \rightarrow x_c$
could well be the signature of a tunneling-percolation
mechanism of nonuniversality. In order to investigate
this possibility we plot in Fig. 11(a) the isotropic piezo-
resistive factor $\Gamma = \Gamma_\parallel + 2\Gamma_\perp$ for the A1, A2, B1, and
B2 series as a function of $x$. With the exception of the
A1 series which displays an almost constant piezoresis-
tive response, the other series clearly diverge at the same
critical concentration $x_c$ at which $\sigma$ goes to zero. Accord-
ing to the tunneling-percolation theory, $\Gamma$ should follow
Eq. (19) which predicts a logarithmic divergence at the

| Label | RuO$_2$ grain size | firing temperature $T_f$ | $x_c$ | $\ln(\sigma_0\Omega_m)$ | $t$ | $\Gamma_0$ | $dt/d\epsilon$ |
|-------|-------------------|--------------------------|------|-----------------------|----|-----------|-------------|
| A1    | 400nm             | 525°C                    | 0.0745 | 11.1 ± 0.3           | 2.15 ± 0.06 | 16.5 ± 4.5 | −0.6 ± 1.2 |
| A2    | 400nm             | 600°C                    | 0.0670 | 14.2 ± 0.2           | 3.84 ± 0.06 | −26.4 ± 4.8 | 16.2 ± 1.5 |
| B1    | 40nm              | 550°C                    | 0.0626 | 14.3 ± 0.5           | 3.17 ± 0.16 | −45.9 ± 9  | 26.1 ± 2.7 |
| B2    | 40nm              | 600°C                    | 0.0525 | 13.7 ± 0.7           | 3.15 ± 0.17 | −57.9 ± 7.2 | 33.0 ± 2.1 |

**FIG. 10:** (a) relative variation of conductivity along the $x$
axis as a function of applied strain $\varepsilon$ in cantilever bar
measurements of the A2 series for different contents $x$ of RuO$_2$.
From bottom to top: $x = 0.23, 0.154, 0.11, 0.095$, and 0.085.
Solid lines are linear fits to the data. (b) the same of (a) for the case in which the conductivity change is measured along the $y$-axis. (c) longitudinal $\Gamma_\parallel$, and transverse $\Gamma_\perp$, piezoresis-
tive factors obtained by applying Eqs. (22, 23) to the data of
(a) and (b), respectively.

**FIG. 11:** (a) Piezoresistive factor $\Gamma = \Gamma_\parallel + 2\Gamma_\perp$ plotted as
a function of RuO$_2$ volume concentration $x$. (b) $\Gamma$ as a function
of $\ln(x - x_c)$ and fits (solid lines) to Eq. (22). The fit param-
eters $dt/d\epsilon$ and $\Gamma_0$ are reported in Table I and in the inset,
together with $\Gamma = -1.9dt/d\epsilon$ (solid line).
nonuniversal values of $t$ and the corresponding negative values of $\Gamma_0$ are features which can be coherently explained by the tunneling-percolation model of nonuniversality. However, in previous studies, this possibility was neglected, and the divergence of $\Gamma$, already reported in Ref.37 for TFRS and in Ref.46 for carbon-black–polymer composites, was attributed to a different mechanism independent of the universality breakdown of $t$. This called into play the possibility of having nonzero derivative of the volume concentration $x$ with respect to the applied strain when the elastic properties of the conducting and insulating phases are different. For the particular case of RuO$_2$-based TFRS, one finds that $dx/d\varepsilon \simeq -Ax$ for small values of the RuO$_2$ concentration $x$. It is easy to show that in this limit $A \simeq 1-B_{\text{glass}}/B_{\text{RuO}_2}$, where $B_{\text{glass}}$ and $B_{\text{RuO}_2}$ are the bulk moduli of the glass and the conducting particles, respectively. Since $B_{\text{RuO}_2} \simeq 270$ GPa and $B_{\text{glass}} \simeq 40–80$ GPa, $A$ is expected to be different from zero and positive. If this reasoning held true, by differentiating Eq. (1) with respect to $\varepsilon$, and by keeping $t$ constant, $\Gamma = -d\ln(\sigma)/d\varepsilon$ would reduce to:

$$\Gamma = \Gamma_0 + At \frac{x}{x - x_c} = K_1 + K_2 \frac{x}{x - x_c}$$

(35)

where we have defined $K_1 = \Gamma_0 + At$ and $K_2 = Atx_c$. In Fig. 12 we have re-plotted the $\Gamma$ values of Fig. 1(a) as a function of $1/(x - x_c)$ with the same values of the critical concentrations $x_c$, extracted from the resistivity data. According to Eq. (35), $\Gamma$ should follow a straight line as a function of $1/(x - x_c)$ which, although being rather correct for the A2 series, is manifestly not true for the B1 and B2 series. In addition, the A1 series remains almost constant, implying that $A = 0$ for this case, contrary to the premises of Ref.37.

Besides from the bad fit with our data, the reasoning of Ref.37 is based on a misunderstanding of the actual physical meaning of $x$ appearing in Eq. (1). In fact, $x$ should be considered just as an operative estimate of the concentration $p$ of intergrain junctions with finite resistances present in the sample. Current can flow from one end to another of the composite as long as a macroscopic cluster of junctions spans the entire sample. Instead of $x$, an equally valid variable describing the intergrain junction probability $p$ would have been the concentration in weight of RuO$_2$, which is manifestly independent of applied strain (and of the elastic properties of the material).

The reasoning of Refs.16,37 is therefore non-consistent with the physics of percolation. However, one could tentatively argue that the applied strain actually changes the concentration $p$ of junctions by breaking some of the bonds. This situation could be parametrized by allowing a $p$ dependence of $x$ so that $dx/d\varepsilon \simeq (dx/dp)(dp/d\varepsilon)$. Also in this case however one would end with a $1/(x - x_c)$ divergence of $\Gamma$ which we have seen to lead to poor fits for our data (Fig. 12). In addition, the values of the applied strains in our measurements are so small ($\varepsilon \sim 10^{-4}$) that their effect is that of changing the value of the tunneling junction resistances without affecting their concentration $p$, so that one realistically expects that $dp/d\varepsilon = 0$. This is confirmed by the results of Fig. 12(a) which show no deviation from linearity for the entire range of $\varepsilon$ values.

In a previous publication7,35 we have re-analyzed the piezoresistive data reported in Ref.37 by assuming a logarithmic divergence of $\Gamma$ rather than the $1/(x - x_c)$ behavior of Eq. 36. The agreement with Eq. 34 was satisfactory and, furthermore, also in this case we obtained negative values of $\Gamma_0$. However, contrary to the present data, all the TFRS used in Ref.37 were nonuniversal, so it was not possible to establish the disappearance of the logarithmic divergence of $\Gamma$ when $t = t_0$.

V. CONCLUSIONS

In this paper we have presented conductivity and piezoresistivity measurements in disordered RuO$_2$-glass composites close to the percolation threshold. We have fabricated samples displaying both universal and nonuniversal behavior of transport with conductivity exponents ranging from $t \simeq 2$ for the universal samples up to $t \simeq 3.8$ for the nonuniversal ones. The corresponding piezoresistive responses changed dramatically depending on whether the composites were universal or not. For the composites with $t \simeq 2$, the piezoresistive factor $\Gamma$ showed little or no dependence upon the RuO$_2$ volume fraction $x$, whereas the nonuniversal composites displayed a logarithmic divergence of $\Gamma$ as $x - x_c \to 0$, where $x_c$ is the percolation threshold. We have interpreted the piezoresistivity results as being due to a strain dependence of the conductivity exponent when this was nonuniversal. As discussed in Sec. II a logarithmic divergence of $\Gamma$ is fully consistent with the tunneling-percolation model of nonuniversality proposed by Balberg a few years ago. According to this theory, when the tunneling distance between adjacent conducting grains has sufficiently strong...
fluctuations, the DC exponent acquires a dependence upon the mean tunneling distance $a$. An applied strain $\varepsilon$ changes $a$ to $a(1 + \varepsilon)$ which is reflected in a $\varepsilon$-modulation of the exponent $t$, and eventually to a logarithmic divergence of $\Gamma = -d\ln(\sigma)/d\varepsilon$ at $\varepsilon_c$. By studying an effective medium approximation of the tunneling-percolation model, and by extensive Monte Carlo calculations, we have shown that when $\Gamma$ diverges, the $\varepsilon$-independent contribution $\Gamma_0$ of $\Gamma$ becomes negative, in agreement with what we observed in the experiments.

In view of such agreement between theory and experiments, and given the fact that an alternative explanation based on a strain dependence of the integrain junctions, and given the fact that an alternative explanation based on the percolation picture (with its corresponding critical exponents) seems to survive well also in the low temperature tunneling regime, this was interpreted in terms of thermally activated voltage fluctuations across the tunneling barriers. A qualitatively similar enhancement of $\Gamma$ as the temperature drops is expected also in models based on variable-range hopping mechanism of transport. It should be however pointed out that in these works the problem of connectivity is not included so that the tunneling current flows on a network without percolation characteristics. Nevertheless, the percolation picture (with its corresponding critical exponents) seems to survive well also in the low temperature tunneling regime. Hence, a tunneling-percolation theory of piezoresistivity at low temperatures should be formulated by considering percolation networks where the simple tunneling process, Eq. (9), are combined with additional terms describing, e. g., grain charging effects and/or Coulomb interactions.

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