Development of the equipment of beam channels for applied and biomedical research at the NICA complex

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Abstract. The report deals with the construction of the ion beam transport line for applied and biomedical research at the NICA accelerator complex, JINR, Dubna. Calculations of the beam output channels from the Nuclotron and Booster are carried out. The used electronics is described. We also discuss the compilation and realization of the plan of treating a tumor located at a depth up to 30 cm.

1. Problem statement

The types of accelerated ions and the energies of beams at the Nuclotron and the future NICA accelerator complex are suited for applied research and certain practical applications [1] in the following fields: 1) nuclear power engineering; 2) studies of the radiation resistance of materials; 3) radiation biology and medicine.

The system for monitoring the extracted beams described in the present paper was developed within the framework of the project “Energy+Transmutation” [2].

This system should be a part of a more general set of detectors and systems that allow one to solve a number of applied problems from the list above with the use of purely electronic methods. The requirements set by radiation therapy were used as the basis for the development of the beam monitoring system. The flux of ions ranging from deuterons to carbon with an intensity ranging from 10⁵ to 10¹⁰ s⁻¹, a beam diameter of 3–4 mm, and an energy of up to hundreds of meVGy electronvolts per nucleon should irradiate an area of about 200 × 200 mm² with the help of scanning magnets. The system should be able to perform the following: 1) measure the position of a deflected beam at least once per millisecond in order to monitor the scanning magnet system; 2) measure the profile of a deflected beam in each position in order to monitor the quality of the beam itself; 3) measure the distribution of the target irradiation dose after each beam dump. In response to these tasks, test samples of detectors and electronics for them were constructed at department no. 5 of the Laboratory of High-Energy Physics (LHEP) JINR. Wire chambers were used in order to fulfill the first two requirements. The third requirement was satisfied with the use of a pixel chamber.

It is pertinent to note that the averaged ionization currents, which are produced by the beam particles in the detectors, and complete ionization charges are detected instead of the individual beam particles.

The constructed system that operates in real time finds practical use in nuclear engineering experiments conducted with the Nuclotron beams. It complemented the beam diagnostics system that was used until very recently and was based on the activation technique (the measurement of the integral beam dump over hours-long irradiation) and the photoplate exposure (the measurement of the beam profile in the target region and the beam position).

2. Monitoring chamber system

Functional test samples of detectors and electronics for them designed for monitoring the Nuclotron ion beam were constructed at LHEP department no. 5: 1) a wire chamber with front-end electronics
and detection electronics installed in a data acquisition crate located far from the beam channel and 2) a pixel ionization chamber built with the use of electronics designed at JINR.

This system is designed to perform the following functions: 1) conduct multiple measurements of the extracted beam profile and the beam position in the XY plane during the beam dump in a wide range of intensities from $10^5$ to $10^{10}$ s$^{-1}$; 2) determine the overall beam particle flux in the beam dump; 3) measure the distribution of the irradiation dose at the irradiated object in the XY plane.

2.1. Two-Coordinate Wire Beam Chambers

The chamber incorporates two signal planes for recording the projection of the beam intensity distribution onto the X and Y axes. The signal anode planes are placed between three high-voltage cathode planes. Each signal plane is basically an array of wires with a diameter of 25 μm made from gold-plated tungsten that are arranged with an interval of 2 mm. Each signal plane incorporates 96 wires. The corresponding active region size is $192 \times 192$ mm$^2$. Each wire may be connected to the detection electronics. High-voltage planes are made from stainless grid. The wire diameter is 50 μm. The grid cell size is $0.5 \times 0.5$ mm$^2$, and the interelectrode gap is 6.5 mm. The chambers are constantly purged with a gas mixture based on argon and carbon dioxide with the addition of propanol vapor. When the beam intensity is high, the chambers operate in the regime of collection of the ionization charges produced in the interelectrode gap. When the beam intensity is low, the chambers may operate in the gas multiplication regime at up to $10^4$ s$^{-1}$.

Wire Chamber Electronics. The wire chamber electronics incorporates the frontend electronics installed at a distance of up to 1.5 m from the beam, the ADC unit mounted in the remote data acquisition crate at a distance of no less than 30 m, and the so-called sequencer generating a train of control pulses for synchronizing the system operation. The sequencer is also located in the remote crate. A single the frontend electronics board incorporates 32 channels for recording the current values from the chamber wires at specific time points. The board is basically a multichannel analog memory element and an analog multiplexer for connecting the memory channels sequentially, one after another, to the remote ADC mounted in the data acquisition crate. Each board has a single analog output that is activated if the channel being triggered is located at this board. If this is not the case, the analog output is disabled. The outputs of all boards may be tied together for readout with a single ADC channel. Each board is addressed with the use of switches located on it. Thus, all the channels tied together for readout with a single ADC channel are lined up in a single queue with consecutive numbering. The boards are mounted in twos in NIM bins (i.e., a single bin incorporates 64 channels). In response to a signal from the sequencer, the instantaneous value of the input current is saved simultaneously in all channels of the system incorporating many boards. The channels from the general queue are then sequentially connected to the ADC with the help of a control pulse train.

In accordance with the technical requirements, the decay-time constant of the signal formed in the first stage was set to be equal to 330 μs. This means that we may perform data sampling with a period down to 1 ms in order to obtain correct data on the dynamics of changes that the beam is undergoing. The sequencer mounted in the data acquisition crate serves to generate (on command from the crate controller or upon the arrival of an external trigger signal) a pulse train that is needed in order to control the synchronous operation of the frontend electronics and the ADC. The output signals are displayed on the front panel. The sequencer was constructed using $2K \times 8$ memory. Prior to the start of operation in the acceleration run, the sequencer requires loading 2048 8-bit words, which set the needed configuration of the control pulse train at the output terminals, into the memory through the crate bus. When it is triggered by an external signal or on command through the crate bus, the internal generator produces 2048 pulses and stops. The pulse counter generates the address for the sequential readout of 8-bit words. Every bit of each successive word affects the generation of a signal through one of the eight output terminals at the front panel. Calibration dependences for
several detection channels incorporating the frontend electronics and the ADC in the data acquisition were obtained with the use of a test current supply. The voltage dependences of the chamber gas amplification for two gas mixtures based on argon and carbon dioxide with the addition of propanol vapor are used. The electronics for pixel chambers (to be discussed below) was used to measure these dependences. The charge passing between the chamber electrodes in unit time upon irradiation with a Sr-90 radioactive source was recorded.

The combination of the gas amplification capacity and the dynamic range of the detection electronics yields a dynamic range of the system of no less than five orders of magnitude.

Figure 1 shows examples of visualized data from the wire chambers displayed after each beam dump in the process of data acquisition:

1) beam profiles projected on the X and Y axes after the beam dump;
2) distributions of half-widths at half-maximum of the profiles for the X and Y projections in the process of data acquisition;
3) distributions of positions of the beam center in the wire chamber reference frame in the process of data acquisition.

2.2. Pixel Ionization Chamber
The basic design of this chamber is similar to the one of the wire chamber. The cathode is made from a grid of stainless wires with a diameter of 50 μm. The cell size is 0.5 × 0.5 mm². The anode plane is a removable element of the chamber. A plane made from glass-fiber laminate with a thickness of 1 mm was used in the considered case. The active region with an area of 160 × 160 mm² is divided into 256 separate sensitive pads (pixels). Each of them is connected to a terminal at the periphery of the printed board. The pixel size is 10 × 10 mm². The interelectrode gap may be varied in a wide range starting from 6.5 mm with the use of inserts.

The pixel chamber was purged in beam runs with the same gas mixture (based on argon and carbon dioxide with the addition of propanol vapor) that was used in the case of the wire chamber.

The pixel chamber electronics incorporates two unit types: the frontend electronics near the chamber and the data acquisition unit mounted in the data acquisition crate located far from the beam channel.

The frontend electronics of the pixel chamber is located up to 1.5 m from it and is based on the TERA06 microcircuit chip produced in Italy [3]. The main features of TERA06 are as follows. Each of the 64 channels converts the input current into pulse rate with continuous counting of the number of pulses by a 16-bit counter. The counter readings may be shifted into the 64-word output register at any specific time on command from the data acquisition unit. The register contents are read out word after word into the data acquisition unit mounted in the crate located far from the beam channel. The counter does not stop at this time. Thus, the system operates without dead time. The quantum of conversion of the input current into frequency is varied with the use of external potentials within the range from 100 to 800 fC. The maximum conversion frequency is 5 MHz. The average noise per channel is on the order of 1 1/s. The frontend unit and the data acquisition unit designed at JINR are used in the described system. With the chosen settings, the quantum of conversion of the input current into frequency is roughly equal to 600 fC. A total of 64 detection channels were used. This corresponded to an active area size of 80 × 80 mm² in the pixel chamber.

Figure 1 shows examples of visualized data on the two-dimensional distribution of the cumulative dose obtained in real time after each dump of the beam onto the target.

3. The channel for biomedical research.
One direction in the development of the JINR accelerator complex NICA is the design of a test bench for biomedical research based on the JINR Nuclotron. While designing the test bench, the general technique for manufacturing the hadronic therapy complex is tested. We present a calculation results for the optics of the charge particle transport channel of the hadronic therapy complex.

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This channel is intended for the transportation of the $^{12}$C$^{+6}$ carbon ions with an intensity of $\sim 2 \times 10^9$ and an energy of 100–550 MeV/nucleon. The channel (see fig. 2) starts near the F3 focus of the primary channel.

3.1. Setup Restrictions.
Additional restrictions of the transport problem arise in the use of specific optical elements and their mounting in the experimental hall. The following optical elements are used in the channel: dipole and deflecting magnets (SP-94) and a magnetic lens (ML-17).

The length of the transport channel is 12 m. The designed channel starts from a dipole magnet mounted in the primary transport channel at a distance of 5.25 m in front of the F3 focus of the primary channel. Optical elements (quadrupole lenses) are located over the channel. There is a beam trap at the end of the channel, the test bench in F$_k$ (focus C, see fig. 2) is right before the trap, and the beam scanning system is before the test bench. The scanning system consists of two similar deflecting magnets rotating at an angle of 90° around the axis relative each other.

One natural restriction of beam transportation is that the diameter of the vacuum pipeline is equal to 0.25 m, which passes through all the quadupole elements of the system. A magnet aperture of $0.3 \times 0.13$ m is a restriction at the final stage of the scanning system. The mutual position of the scan region and the system of scanning magnets is fixed.

The maximum current is limited for each quadrupole lens; this results in a limitation of the coefficient $K < 1.5 \, \text{m}^{-2}$ used for calculating the phase incursion on the lens at a preset energy range of 100–550 MeV/nucleon.

The beam cross section in the F3 focus of the primary transport channel is a circle 0.04 m in diameter [4-5], which makes it possible to define the initial conditions of beam propagation.

3.2. Results Obtained.
For a preset aperture and the magnet arrangement, we have [6]: 1) a minimum focus diameter of 2.8 mm for an emittance of $25\pi \, \text{mm mrad}$; 2) a minimum focus diameter of 5.6 mm for an emittance of $50\pi \, \text{mm mrad}$. The region of target scanning is restricted by an aperture of two successive magnets in a plane normal to the beam. The magnet aperture is $0.3 \times 0.13$ m for a specific channel; this agrees with the planned scan region of 0.1 \times 0.1 m. Solutions have been found for emittances of $25\pi \, \text{mm mrad}$ and $50\pi \, \text{mm mrad}$ based on the above specified restrictions. The beam cross section in the focus C (fig.2) is close to the minimum for the given scanning system geometry: 1) $3.0 \times 3.0$ mm for an emittance of $25\pi \, \text{mm mrad}$; 2) $5.6 \times 6.0$ mm for an emittance of $50\pi \, \text{mm mrad}$.

4. Initial Conditions.
To check the existence of a solution in other operating modes, other initial conditions of beam propagation in an additional channel were considered. The beam cross section in the F3 focus acts as a parameter determining these initial conditions.

In addition to a solution with a focus on the primary channel target of $0.04 \times 0.04$ m, we considered the solution for a focus of $0.1 \times 0.12$ m [6]. The beam cross section in the focus on a target for configurations with initial conditions corresponding to different beam sizes in the F3 focus of the primary channel (the emittance is $50\pi \, \text{mm mrad}$) is equal to 1) $5.6 \times 6.3$ mm for the focus $0.1 \times 0.12$ m and 2) $5.6 \times 6.0$ mm for the focus $0.04 \times 0.04$ m.

We suggest the following equipment for the additional channel: 1) magnetic lenses ML-17; 2) scanning and dipole magnets SP-94; 3) the pixel chamber and the wire chamber and readout electronics.

Conclusions
Test samples of the following systems were constructed: 1) two coordinate wire chambers with an active area size of $192 \times 192 \, \text{mm}^2$ and the electronics for them and 2) the pixel ionization...
chamber with an active area size of 160 × 160 mm² and 256 pads with a size of 10 × 10 mm² that is operated with the detection electronics based on the TERA06 microcircuit chip.

The systems ensure the monitoring of the extracted relativistic Nuclotron ion beams in real time and allow one to perform 1) multiple measurements of the beam profile, its center position, and its intensity during the beam dump; 2) measurements of the distribution of the cumulative target irradiation dose after each dump. The system was tested in a series of Nuclotron acceleration runs and performed efficiently at deuteron beam intensities of up to 10¹⁰ 1/s.

The construction of the carbon beam transport line for applied and biomedical research at the Nuclotron accelerator complex, JINR, Dubna is shown. We have studied the scheme and modes of magneto-optical elements of the channel. Used electronics described. We are discussed the compilation and realization of the plan of treating a tumor located at a depth up to 30 cm. Choice of beam scanning schemes and their optimization are shown.

Figure 1. The view of distribution of beam is for on-line monitoring of the carbon beam.

Figure 2. Position of the scanning system of magnets on a beam (CC). The scanning region in the beam focus (C).

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