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Research Article

Keywords: Process parameters optimization, Process reliability, Monte Carlo, Hooke-Jeeves algorithm, particle swarm optimization

Posted Date: June 24th, 2021

DOI: https://doi.org/10.21203/rs.3.rs-641033/v1

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Machining-Reliability-based Optimization of Process Parameters for Marine Diesel Engine Block Hole System Using HJ-PSO

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ABSTRACT The processing quality of the block hole system affects the working performance of the marine diesel engine block directly. Choosing an appropriate combination of process parameters is a prerequisite to improve the accuracy of the block hole system. Uncertain fluctuations of process parameters during the machining process would affect the process reliability of the block hole system, resulting in an ultra-poor accuracy. For this reason, the RBF method is used to establish the relationship between the verticality of the cylinder hole and process parameters, including cutting speed, depth of cut, and feed rate. Taking the minimum cylinder hole verticality as the goal and setting the process reliability constraints of the cylinder hole based on Monte Carlo, a reliability optimization model of processing parameters for cylinder hole is established in this paper. Meanwhile, an improved particle swarm algorithm was designed to solve the model, and eventually, the global optimal combination of process parameters for the cylinder hole processing of the diesel engine block in the reliability stable region was obtained.

KEY WORDS Process parameters optimization, Process reliability, Monte Carlo, Hooke-Jeeves algorithm, particle swarm optimization.

I. INTRODUCTION

The block, which is a large thin-walled structure component, is one of the most important parts of the marine diesel engine. The processing of the block holes is a key process in block processing and their quality would affect the performance, accuracy, and life of the block directly. The processing parameters, such as the cutting speed, the feed rate, and so on, play a vital role to ensure the accuracy of holes machining. Therefore, optimizing the process parameters according to the processing requirements of the block hole system is of great significance to improve the processing quality of the diesel engine block.

It is a common method to optimize the process parameters by exploring the relationship between the process parameters and the optimization objective through the experimental design. Awale et al. [1] researched the influence of high-speed turning parameters on the surface roughness of harden AISI S7 tool steel by signal-to-noise ratio analysis method, and the results showed that higher cutting speed and lower feed rate can significantly improve the surface quality of hardening AISI S7 tool steel. Campatelli et al. [2] conducted milling experiments on AISI 1050 carbon steel workpiece by NMV1500DC five-axis milling machine, and the process parameters with the lowest environmental footprint were obtained based on the response surface method, which are higher cutting speed, feed rate, and chip section. Pervaiz et al. [3] used Taguchi analysis to design inclined drilling tests of Inconel 718 under different process parameters, and the test results showed that feed rate has the greatest impact on cutting force, while spindle speed has the greatest impact on cutting power and cutting temperature parameter.

The intelligent optimization algorithm has also been effectively applied to the optimization of process parameters. Genetic algorithm [4, 5] and simulated annealing algorithm [6, 7] take the output of the prediction model as the fitness function. Based on the rule algorithm, the optimal combination of process parameters can be solved through repeated iterations to meet the required fitness requirements. Particle swarm optimization algorithm [8, 9] has become a widely used algorithm in process parameter optimization by its relative real value particle structure and faster iteration speed. However, with the progress of intelligent control optimization theory, the defects of standard intelligent optimization algorithms are gradually exposed. For example, the convergence speed is slow and the precision is low under multiple constraints for genetic algorithm [10], and the
optimization result of particle swarm optimization algorithm is easy to fall into the local optimal solution because of its randomness [11]. Therefore, the improvement of intelligent optimization algorithms has become a way to obtain more accurate optimal solutions of process parameter combination. Taking material removal rate and surface roughness as optimization objectives, Chu et al. [12] obtained the optimal combination of process parameters of the lathe through Hybrid Taguchi Genetic Algorithm. Tan Y et al. [13] proposed a new chaotic search strategy and introduced it into particle swarm optimization (PSO) for solving nonlinear integer and mixed-integer constrained programming problems. Xiang Xu et al. [14] proposed an improved artificial bee colony algorithm to solve constrained optimization problems. This algorithm selects individuals by using fixed-proportion direct comparison rules and introduces the optimal solution information in the scout bee stage so that the scout bees have more chances to search near the optimal point.

There are many types of research on the optimization of process parameters, but few people pay attention to the influence of the uncertainty fluctuation of process parameters on the processing quality. Tian [15] provides a method to establish and evaluate the process reliability model of the diesel engine block, but this method can’t control the process reliability of the block from the process design itself. Therefore, based on his research, this paper integrates the reliability theory in the process of optimization, and the reliability stability region of the block is selected based on the Monte Carlo method. Taking the minimum verticality of the diesel engine block cylinder hole as the optimization objective, the Hooke-Jeeves algorithm is combined with the particle swarm optimization algorithm to solve the established reliability optimization model.

II. ESTABLISHMENT OF APPROXIMATE MODEL

A. DESIGN VARIABLES AND OPTIMIZATION OBJECTIVES

During the operation of a marine diesel engine, the piston and the crankshaft movement center are in a vertical relationship. The verticality of the cylinder hole to the crankshaft hole axis directly affects the reliability of the diesel engine. Therefore, the minimum verticality of the cylinder hole to the crankshaft hole is the optimization goal. Select cutting speed $v_c$, cutting depth $a_p$, and feed rate $f$ as design variables. According to production experience, select the parameter value range of design variables as shown in Table 1. $X_i^{(L)}$ and $X_i^{(U)}$ means the upper and lower limits of design variables. The three-dimensional simplified model of the diesel engine block is shown in Figure 1.

| Design Variable | $v_c$(m/min) | $a_p$(mm) | $f$(mm/r) |
|-----------------|--------------|-----------|-----------|
| $X_i^{(L)}$     | 99.852       | 0.3       | 0.4       |
| $X_i^{(U)}$     | 166.42       | 0.5       | 0.6       |

Figure 1. Three-dimensional simplified model of the diesel engine block

B. EXPERIMENTAL DESIGN

The construction of the approximate model depends on the selection of sample points. Commonly used experimental design methods include Design of experimental, Orthogonal experimental design, Central composite design, and Latin hypercube sampling. Among them, the Latin hypercube sampling has good uniformity and projection characteristics, which can make all test points as evenly distributed in the design space as possible, thereby improving the fitting accuracy of factors and responses [16]. Therefore, the Latin hypercube sampling is used to select the three design variables, and their distribution is shown in Figure 2.
Figure 2. Three-dimensional distribution diagram of sample points of design variables

According to the three-dimensional scatter plot, it can be seen that the distribution of sample points in the design space is relatively uniform, and each area is occupied by sample points, and the space utilization rate is high. Based on the sample points of the Latin hypercube sampling, the cylinder hole machining test was carried out, and the test results are shown in Table 2.

Table 2. Sampling test results of Latin hypercube test

| Test number | \( v_c \)(m/min) | \( a_p \)(mm) | \( f \)(mm/r) | \( \perp \)(mm) |
|-------------|------------------|---------------|--------------|----------------|
| 1           | 156.546          | 0.4           | 0.46         | 0.0503         |
| 2           | 139.838          | 0.45          | 0.51         | 0.0507         |
| 3           | 143.288          | 0.35          | 0.41         | 0.0495         |
| 4           | 122.052          | 0.42          | 0.45         | 0.0469         |
| 5           | 141.231          | 0.41          | 0.51         | 0.0457         |
| 6           | 118.453          | 0.46          | 0.57         | 0.0531         |
| 7           | 109.77           | 0.37          | 0.52         | 0.0439         |
| 8           | 114.028          | 0.44          | 0.48         | 0.0501         |
| 9           | 150.647          | 0.45          | 0.54         | 0.0521         |
| 10          | 130.538          | 0.35          | 0.44         | 0.048          |
| 11          | 116.903          | 0.38          | 0.48         | 0.047          |
| 12          | 146.499          | 0.39          | 0.53         | 0.0508         |
| 13          | 123.032          | 0.47          | 0.4          | 0.0519         |
| 14          | 134.297          | 0.41          | 0.49         | 0.0445         |
| 15          | 166.325          | 0.34          | 0.59         | 0.0535         |
| 16          | 135.912          | 0.36          | 0.46         | 0.0509         |
| 17          | 127.579          | 0.32          | 0.53         | 0.0477         |
| 18          | 137.862          | 0.42          | 0.46         | 0.0478         |
| 19          | 125.124          | 0.43          | 0.56         | 0.0492         |
| 20          | 131.848          | 0.5           | 0.49         | 0.0533         |
| 21          | 154.121          | 0.38          | 0.55         | 0.0478         |
| 22          | 144.647          | 0.3           | 0.52         | 0.0504         |
| 23          | 100.885          | 0.4           | 0.48         | 0.0492         |
| 24          | 133.862          | 0.37          | 0.5          | 0.0492         |
| 25          | 127.921          | 0.42          | 0.55         | 0.0485         |

C. VERTICALITY OF CYLINDER HOLE TO THE CRANKSHAFT HOLE MODELING BASED ON RBF METHOD
The relationship between the verticality of the cylinder hole to the crankshaft hole and design variables needs to be determined through machining tests. The process of optimizing process parameters involves multiple tests, which results in serious time consumption and cost. Therefore, approximate model technology is used to build a model that meets the accuracy requirements and has low computational cost to establish the mapping relationship between variables and responses. Subsequent optimization work based on this model will greatly reduce the optimization cost and speed up the optimization process.

Commonly used approximate models include response surface model, multiple adaptive regression spline model, kriging model, support vector regression model(SVR), and radial basis function model(RBF). Process parameter optimization of diesel engine block hole system is a small sample problem. In the case of limited sample size, SVR and RBF can obtain better fitting results. Compared with SVR, RBF has a more prominent fitting effect on nonlinear problems [17], so the RBF method is chosen to establish an approximate model of cylinder hole verticality.

The basis of the RBF is the function approximation theory, which is a feedforward neural network with strong global optimization capabilities [18]. The RBF is usually composed of an input layer, a hidden radial basis layer, and an output linear layer, the network structure of the RBF is shown in Figure 3. The radial basis function is radially symmetric, and the Gaussian function is commonly used:

$$G_i(x) = \exp\left(-\frac{\|x - c_i\|^2}{2\sigma_i^2}\right), i = 1, 2, L, p$$

Among them, $x$ is the m-dimensional input vector; $c_i$ is the center of the $i$-th basis function; $\sigma_i$ is the variance of the $i$-th basis function; $p$ is the number of perceptual units.

The input layer of the RBF network realizes the nonlinear mapping from $x \rightarrow G_i(x)$, and the output layer realizes the linear mapping from $G_i(x) \rightarrow y_R$, namely:

$$y_R = \sum_{i=1}^{p} w_{ki} G_i(x), k = 1, 2, L, q$$

Among them, $q$ is the number of output nodes, $w_{ki}$ is the adjustment weight between the $k$-th output layer and the $i$-th hidden layer nerve.

**D. RBF MODEL PREDICTION RESULTS AND ANALYSIS**

The verticality of the cylinder hole to the crankshaft hole is predicted based on the established RBF model, test data of No.16 to 25 are input into the RBF model, and the output results are obtained. Comparing the actual value and the predicted value, as shown in Table 3. The line graph of the value comparison is shown in Figure 4.

| Test number | Actual value | Predictive value |
|-------------|--------------|------------------|
| 16          | 0.0509       | 0.04937          |
| 17          | 0.0477       | 0.047751         |
| 18          | 0.0478       | 0.0473           |
Take test data of No.16 to 25 as the test sample points, and use R-squared to judge the fit of the model, the mathematical model is expressed as follows:

$$R^2 = 1 - \frac{\sum_{i=1}^{m} (y_i - \hat{y}_i)^2}{\sum_{i=1}^{m} (y_i - \bar{y})^2}$$  

(3)

Among them, $m$ is the number of validation sample points, $y_i$ is the actual value of the sample points, $\hat{y}_i$ is the predicted value calculated by the approximate model, and $\bar{y}$ is the average value of the test sample point set. When the $R^2$ value is closer to 1, the accuracy of the approximate model higher.

The root mean square error is used to measure the deviation between the predicted value and the actual value. The expression is as follows:

$$RMSE = \sqrt{\frac{\sum_{i=1}^{m} (y_i - \hat{y}_i)^2}{m}}$$  

(4)

Among them, $m$ is the number of test sample points, $y_i$ is the actual value of the test sample points, and $\hat{y}_i$ is the predicted value of the approximate model. The closer the RMSE value is to 0, the smaller the deviation between the predicted value and the actual value.

After calculation, the R-square value corresponding to the test sample is 0.904513, and the RMSE value is 0.00005. The established RBF model is relatively accurate and meets the accuracy requirements of the approximate model.

### III. ESTABLISHMENT OF CONSTRAINTS

The residual stress will affect the fatigue strength and life of the diesel engine block, and its release process will deform the cylinder hole of the block, thereby affecting the accuracy and stability of the block. In order to ensure the accuracy of the diesel
engine block hole system, the surface residual stress of the diesel engine block after machining is required to be less than a certain value, and the probability that the residual stress after machining is less than a given value is used as the reliability index.

The Third Wave AdvantEdge FEM software is used to simulate the boring process of the cylinder hole. Figure 5 shows the curve of residual stress along depth direction simulated by the AdvantEdge software when the cutting speed is 166.46r/min, the cutting depth is 0.4mm, and the feed is 0.4mm/r. According to the figure, it can be seen that the residual stress on the surface of the workpiece is mainly tensile stress, and the residual stress in the inner layer of the workpiece is mainly compressive stress; the surface residual stress is the largest, and the residual tensile stress decreases rapidly along with the depth of the layer. The residual stress transitions to compressive stress at a depth of about 0.3mm. The compressive residual stress reaches its maximum at a depth of 0.5mm, and then the residual stress slowly tends to 0.

![Figure 5. Curve of residual stress with depth obtained by AdvantEdge FEM](image)

Taking cutting speed, cutting depth, and feed rate as independent variables, the residual stress on the cylinder hole surface is the response value. According to the central composite response surface method test plan, 17 sets of residual stress simulation tests by AdvantEdge software are carried out. The test results are shown in Table 4.

| Test number | Coding variable | Actual variable | Response σR (Mpa) |
|-------------|----------------|-----------------|-----------------|
| 1           | -1 1 0         | 99.852 0.5 0.5  | 270             |
| 2           | 1 -1 0         | 166.46 0.3 0.5  | 466             |
| 3           | 0 1 -1         | 133.156 0.5 0.4 | 600             |
| 4           | 0 1 1          | 133.156 0.5 0.6 | 642             |
| 5           | -1 -1 0        | 99.852 0.3 0.5  | 390             |
| 6           | 0 -1 1         | 133.156 0.3 0.6 | 575             |
| 7           | -1 0 -1        | 99.852 0.4 0.4  | 270             |
| 8           | 0 0 0          | 133.156 0.4 0.5 | 510             |
| 9           | 1 0 -1         | 166.46 0.4 0.4  | 565             |
| 10          | 0 -1 -1        | 133.156 0.3 0.4 | 523             |
| 11          | 0 0 0          | 133.156 0.4 0.5 | 510             |
| 12          | -1 0 1         | 99.852 0.4 0.6  | 315             |
| 13          | 1 0 1          | 166.46 0.4 0.6  | 530             |
| 14          | 0 0 0          | 133.156 0.4 0.5 | 510             |
| 15          | 0 0 0          | 133.156 0.4 0.5 | 510             |
| 16          | 1 1 0          | 166.46 0.5 0.5  | 517             |
| 17          | 0 0 0          | 133.156 0.4 0.5 | 510             |

Based on the test data, the response surface fitting model is established as shown in (5).

\[ \sigma_R = -308 + 32.72 \times v_r - 4100 \times a_p - 3200 \times f - 0.12 \times v_r^2 + 3300 \times a_p^2 + 4200 \times f^2 + 12.84 \times v_r \times a_p - 6.01 \times v_r \times f - 250 \times a_p \times f \]

(5)
According to the response surface model, the contour plot between the process parameters is drawn, as shown in Figure 6.

![Contour Plot](image)

(a) 2D contour plots \((a_p, v_c, \text{ and } \sigma_R)\)

![Contour Plot](image)

(b) 2D contour plots \((a_p, f, \text{ and } \sigma_R)\)

![Contour Plot](image)

(c) 2D contour plots \((v_c, f, \text{ and } \sigma_R)\)

**Figure 6.** 2D contour plots of the process parameters

It can be seen from the contour diagram that the cutting speed has the greatest influence on the residual stress on the surface of the cylinder hole, followed by the cutting depth and the feed rate, and the larger residual stress is concentrated at the cutting speed of 130r/min-155r/min.

Assuming that the process parameters meet the normal distribution, set the mean and standard deviation as shown in Table 5, \(N(\mu, \sigma)\) represents a normal distribution with the mean value of \(\mu\) and standard deviation of \(\sigma\).

**Table 5.** The distribution parameters of machining parameters
The Monte Carlo method (MCM) is a numerical calculation method that generates random numbers based on the probability distribution of the input and realizes distribution propagation by re-sampling them.

Based on the established response surface model, MCM is used to perform 10,000 calculations to count the number of unsatisfactory residual stresses on the surface, so that the process reliability of the cylinder hole can be obtained. The allowable value of surface residual stress is set to 550Mpa. The standard deviations of the three variables remain unchanged and change the variable mean to calculate the corresponding reliability. The fluctuation curves of the reliability concerning the three variables are shown in Figure 7.

| Distribution | $v_c$ | $a_p$ | $f$ |
|--------------|-------|-------|-----|
| $N(\mu, \sigma)$ | $N(99.852,10)$ | $N(0.4,0.01)$ | $N(0.5,0.02)$ |

![Fluctuation curve of reliability concerning cutting speed](a)

![The fluctuation curve of reliability concerning cutting depth](b)
Fluctuation curve of reliability concerning feed

According to the fluctuation curve, it can be seen that the influence of cutting speed on block reliability is not significant, but cutting depth and feed rate have great influence on block reliability, and their fluctuation curves are similar. It is speculated that both of cutting depth and feed rate are related to material cutting amount. When the cutting depth and feed rate are small, the chip takes away a lot of heat, which reduces the residual stress of cylinder hole. With the increase of cutting speed and feed rate, the heat carried by the chip is limited, and the cutting thermal effect is enhanced, which leads to the continuous increase of residual stress on the surface of the cylinder hole the variable interval with relatively stable reliability fluctuation is selected as the reliability stability region constraint of the diesel engine block cylinder hole machining, as shown in Table 6, where $X_R^{(L)}$ and $X_R^{(U)}$ respectively represent the reliability stability region interval the lower limit and upper limit.

### Table 6. Reliability stability region

| Design Variable | $v_c$ (m/min) | $a_p$ (mm) | $f$ (mm/r) |
|----------------|---------------|------------|------------|
| $X_R^{(L)}$    | 99.852        | 0.342      | 0.472      |
| $X_R^{(U)}$    | 124.932       | 0.402      | 0.514      |

IV. RELIABILITY OPTIMIZATION OF PROCESS PARAMETERS

A. PROCESS PARAMETERS OPTIMIZATION MODEL

To optimize the process parameters of the cylinder hole, the main research is to minimize the verticality of the cylinder hole to the crankshaft hole. Based on this and based on the obtained constraints, an optimization model of the cylinder hole process parameters of the diesel engines block can be constructed:

Find $v_c$, $a_p$, $f$

$$\text{Min } V(v_c, a_p, f)$$

- $99.852 \text{ m/min} \leq v_c \leq 124.932 \text{ m/min}$
- $0.342 \text{ mm} \leq a_p \leq 0.402 \text{ mm}$
- $0.472 \text{ mm/r} \leq f \leq 0.514 \text{ mm/r}$

Among them, $v_c$, $a_p$, $f$ are the cutting speed, depth of cut, and feed rate, respectively, and $V$ is the verticality of the cylinder hole to the crankshaft hole.

B. PARTICLE SWARM SINGLE-OBJECTIVE OPTIMIZATION ALGORITHM BASED ON HOOKE-JEEVES ALGORITHM

1) HOOKE-JEEVES ALGORITHM DESCRIPTION

Hooke-Jeeves is a direct search method. Its core idea is to find out the optimal descent direction of the function by calculating and comparing the value of the function to solve the target optimization problem [19]. The search steps are as follows:

Step1: Given the initial point $x^{(1)} \in \mathbb{R}^n$, initial step size $\delta$, acceleration factor $a \geq 1$, reduction rate $\beta \in (0, 1)$, accuracy $\varepsilon > 0$. Let $y^{(1)} = x^{(1)}$, $k = 1$, $j = 1$;
Step 2: If \( f(y^{(j)} + \delta e_j) < f(y^{(j)}) \), then let \( y^{(j+1)} = y^{(j)} + \delta e_j \), go to Step 4; otherwise, go to step 3;

Step 3: If \( f(y^{(j)} - \delta e_j) < f(y^{(j)}) \), then set \( y^{(j+1)} = y^{(j)} - \delta e_j \), go to Step 4; otherwise, \( y^{(j+1)} = y^{(j)} \), go to step 4;

Step 4: If \( j < n \), then set \( j = j+1 \), go to step 2; otherwise, go to Step 5;

Step 5: If \( f(x^{(k+1)}) < f(x^{(k)}) \), then go to Step 6; otherwise, go to Step 7;

Step 6: set \( x^{(k+1)} = y^{(j+1)} \), let 
\[
y^{(j)} = x^{(j)} + \alpha (x^{(j+1)} - x^{(j)})
\]

set \( k = k+1, j = 1 \), go to Step 2;

Step 7: If \( \delta \leq \varepsilon \), stop the iteration and get the point \( x^{(k)} \). Otherwise, let \( \delta = \beta \delta \), \( y^{(1)} = x^{(k)} \), \( x^{(k+1)} = x^{(k)} \), and set \( k = k+1, j = 1 \), go to Step 2.

According to the search step of the Hooke-Jeeves method, it can be seen that the search efficiency is greatly affected by the position of the initial point. For different initial points, the optimization accuracy and optimization speed will fluctuate greatly. Therefore, in order to ensure that it can efficiently search for the best, we should ensure that it has a better initial position.

2) IMPROVED PARTICLE SWARM OPTIMIZATION ALGORITHM BASED ON HOOKE-JEEVES ALGORITHM

The particle swarm optimization algorithm (PSO) is derived from the study of bird predation behavior. It uses a particle to simulate individual birds. Each particle is regarded as a searching individual in the search space. The current position of the particle is a candidate solution for the optimization problem. The flight process is the process of searching for individuals. Particles have two attributes: speed and position. Speed represents the speed of movement, and position represents the direction of movement. The optimal solution searched for by each particle is called the individual extremum. The optimal individual extremum in the particle swarm is the global optimal solution to the optimization problem that is sought. The speed and position are constantly updated to iterate, and finally, the optimal solution that reaches the termination condition is obtained. The calculation formula for the update speed \( V_{id} \) and position \( X_{id} \) is as follows:

\[
V_{id} = \omega V_{id} + C_1 \text{rand} () (P_{id} - X_{id}) + C_2 \text{rand} () (P_{gd} - X_{id}) \tag{6}
\]

\[
X_{id} = X_{id} + V_{id} \tag{7}
\]

Where \( \omega \) is the inertia factor, \( C_1 \) and \( C_2 \) are the individual learning factor and the environmental learning factor respectively, and their value range is [0,4] generally. \( \text{rand} () \) is the random number on [0,1]. \( P_{id} \) represents the \( d \)-th dimension of the individual extremum of the \( i \)-th variable and \( P_{gd} \) represents the \( d \)-th dimension of the global optimal solution.

The flying speed of the particles in the particle swarm optimization algorithm affects the global convergence of the algorithm. A larger speed can ensure that the particles quickly fly to the vicinity of the optimal solution, but they will fall into the dilemma of local optimality [20]. Therefore, this paper combines the Hooke-Jeeves algorithm with the particle swarm optimization algorithm. First, the particle swarm optimization algorithm is used to locate the area where the target extremum is located in the design space, and then the Hooke-Jeeves algorithm is used to accurately search the area, and finally, the best design result is obtained. The steps are shown in Figure 8.
C. ALGORITHM PARAMETER SETTING

In order to prove the superiority of the improved particle swarm optimization algorithm based on the Hooke-Jeeves algorithm (HJ-PSO) in solving parameter optimization problems, the algorithm is compared with the particle swarm algorithm. The particle swarm optimization algorithm parameters are set as: inertia factor $\omega = 0.9$, individual learning factor, and environmental learning factor $C_1 = C_2 = 0.9$, the number of max iterations is 20, the number of particles is 10, and the maximum flight speed is 100. The parameters of HJ-PSO are set as follows: initial step size $\delta = 0.5$, reduction rate $\beta = 0.5$, acceleration factor $\alpha = 1$, accuracy $\varepsilon = 10^{-6}$, other parameters are the same as the particle swarm algorithm, and its parameter settings are shown in Table 7.

| Table 7. HJ-PSO algorithm parameters
|-------------------------------------------------|
| Maximum iterations of PSO | 10 |
| Maximum iterations of Hooke-Jeeves | 10 |
| Inertia factor $\omega$ | 0.9 |
| Individual learning factor $C_1$ | 0.9 |
| Environmental learning factor $C_2$ | 0.9 |
| Number of particles $M$ | 10 |
| Maximum flight speed $V_{\text{max}}$ | 100 |
| Initial step $\delta$ | 0.5 |
| Reduction rate $\beta$ | 0.5 |
| Acceleration factor $\alpha$ | 1 |
| Accuracy $\varepsilon$ | $10^{-6}$ |

D. ANALYSIS OF OPTIMIZATION RESULTS

Using PSO and HJ-PSO to solve the optimization model respectively. All the algorithms run independently for 20 times, and the average value and variance of the objective function optimization results of each algorithm are shown in the Table 8.
Table 8. Comparison of optimization results

|              | PSO     | HJ-PSO  |
|--------------|---------|---------|
| mean value   | 0.04336 | 0.04302 |
| standard deviation | 5.262E-4 | 4.956E-5 |

According to the mean comparison of the optimization results, it can be seen that under the same number of iterations, HJ-PSO gets better optimization results than PSO algorithm when searching the global optimal value. In addition, the comparison of standard deviation shows that the stability of HJ-PSO is significantly better than that of PSO.

Set the number of iterations to 100, and use HJ-PSO to solve the optimal combination of process parameters for the verticality machining of cylinder hole. The solving process is shown in the Figure 9.

![Figure 9. Comparison of algorithm optimization efficiency](image)

As can be seen from the figure that the HJ-PSO algorithm converges when the number of iterations reaches about 35, and the corresponding objective function value is 0.04294.

E. VERIFICATION TEST

The optimal combination of process parameters can be obtained by improving the particle swarm algorithm as follows: cutting speed is 99.852m/min, cutting depth is 0.352mm, and feed is 0.508mm/r. Use the obtained combination of process parameters to perform a verification test. The verticality of the cylinder hole measured by the verticality measuring instrument is 0.0436, which is less than the minimum verticality in the historical data. The cylinder hole of workpiece is shown in Figure 10. However, the error between the optimization result value and true value is 1.53%, and it is considered as the influence of process system error.

![Figure 10. Cylinder hole of workpiece](image)

V. CONCLUSIONS
In this paper, based on the reliability theory, the improved particle swarm optimization algorithm is used to optimize the processing parameters of the cylinder hole of the diesel engine block. The important conclusions are as follows.

1. The cutting speed has the greatest influence on the surface residual stress of the cylinder hole, followed by the cutting depth and feed rate.

2. The reliability of the cylinder hole machining process fluctuates greatly with the change of cutting speed and less with the change of cutting depth.

3. Compared with the general particle swarm optimization algorithm, the efficiency and results of the improved particle swarm optimization algorithm are improved.

4. Through the improved particle swarm optimization algorithm based on the Hooke-Jeeves algorithm, the optimal combination of processing parameters of cylinder hole is obtained as follows: the cutting speed is 99.852m/min, the cutting depth is 0.352mm, the feed rate is 0.508mm/r. Based on the optimal combination of processing parameters of the cylinder hole, the actual processing of the block can be guided.

The process of the diesel engine block is complex, so the study in this paper only focuses on the process parameters of the process. In the future, the quality transfer relationship between the multiple processes of the block can be studied, and more accurate optimization results can be obtained.

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ACKNOWLEDGEMENTS

This work was supported in part by Subproject of the China National Key Research and Development Program “Network Collaborative Manufacturing and Intelligent Factory” Special Project: Research on Monitoring Diagnosis and Predictive Maintenance Technology of Key Shipbuilding Equipment for Efficacy Improvement under Grant 2020YFB1712602, in part by the Research Fund for young teachers of Jiangsu University of science and technology under Grant 1022932001, and in part by Research and Practice Innovation Plan for Postgraduates in Jiangsu Province under Grant SJCX21_1759.
COMPETING INTERESTS STATEMENT
The authors declare no competing interests.