Desorption isotherms and isosteric heat of protein hydrolysate from tilapia slaughtering by-product

Isotermas de dessorção e calor isostérico do hidrolisado proteico do subproduto de abate de tilápia

Júlio Cesar Adams Haab1, Gracielle Johann2*, Edson Antonio da Silva1, Melissa Gurgel Adeodato Vieira3

1Universidade Estadual do Oeste do Paraná (UNIOESTE), Curso de Engenharia Química, Toledo/PR - Brasil
2Universidade Tecnológica Federal do Paraná (UTFPR), Curso de Engenharia de Bioprocessos e Biotecnologia, Dois Vizinhos/PR - Brasil
3Universidade Estadual de Campinas (UNICAMP), Escola de Engenharia Química, Campinas/SP - Brasil

*Corresponding Author: Gracielle Johann, Universidade Tecnológica Federal do Paraná (UTFPR), Curso de Engenharia de Bioprocessos e Biotecnologia, Estrada para Boa Esperança, Km 04, CEP 89660-000, Dois Vizinhos/PR - Brasil, e-mail: grajohann@gmail.com

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Abstract

Due to the by-products generated during the processing of meat, biomolecules derived from these by-products, in the form of protein hydrolysates, have been studied for being used as raw materials to produce food. In the present study, the tilapia slaughtering by-products were hydrolyzed, under 60 °C for 2 hours, and spray-dried under 130 °C. After the drying process, equilibrium isotherms of the by-products were obtained through the dynamic method, under temperatures of 20 °C, 35 °C, and 50 °C. All the equilibrium curves presented type III behavior and in the adjustment of the empirical models, the White and Eyring model represented more properly the experimental data of equilibrium. This model presented the highest value of the determination coefficient and lower values of the Sum of the Squares of Residuals (SSR), Relative Mean Error (RME), and Akaike Information Criteria (AIC). The isosteric desorption heat, calculated by the Othmer method, varied from 2395 to 5682 kJ/kg, for equilibrium moisture contents between 0.09 and 0.30 kg/kg. The equation obtained for the calculation of the isosteric desorption heat of the tilapia by-product hydrolysate can be employed in calculations related to the modeling, simulation, optimization, and control of industrial-scale drying processes.

Keywords: Drying; Desorption heat; Fish; Storage.

Resumo

Durante o processamento de carne, subprodutos são gerados. Biomoléculas derivadas desses subprodutos, na forma de hidrolisados proteicos, estão sendo estudadas para serem usadas como matéria-prima na produção de alimentos. No presente estudo, os subprodutos do abate da tilápia foram hidrolisados a 60 °C por 2 h e secos por atomização a 130 °C. Após o processo de secagem, foram obtidas isotermas de equilíbrio para os subprodutos pelo método dinâmico, nas temperaturas de 20 °C, 35 °C e 50 °C. Todas as curvas de equilíbrio apresentaram comportamento do tipo III e, no ajuste dos
models empíricos, o modelo de White e Eyring representou mais adequadamente os dados experimentais de equilíbrio. Este modelo apresentou o maior valor do coeficiente de determinação e os menores valores da soma dos quadrados dos resíduos, erro médio relativo e Critérios de Seleção de Akaike. O calor isostérico de dessorção, calculado pelo método de Othmer, variou entre 2.395 e 5.682 kJ/kg, para teores de umidade de equilíbrio entre 0,09 e 0,30 kg/kg. A equação obtida para o cálculo do calor isostérico de dessorção do hidrolisado do subproduto da tilápia pode ser empregada em cálculos relacionados a modelagem, simulação, otimização e controle de processos de secagem em escala industrial.

Palavras-chave: Secagem; Calor de dessorção; Peixe; Armazenamento.

Highlights

- The White and Eyring model is suitable for predicting the desorption data of NT by-product
- The energy required during the NT by-product drying was achieved by Othmer method
- The results are useful for drying design, predicting energy demand and storage conditions

1 Introduction

Due to growing aquaculture production, only in the year 2018, around 179 million tons of fish were produced worldwide (Food and Agriculture Organization of the United Nations, 2020). The demand for fish protein, essential amino acid, and fatty acid grows along with the population throughout the world as well as its preference for fish and the health advantages associated with its consumption (Desai et al., 2018; Kobayashi & Park, 2018). In this group is the tilapia, a common designation of cichlids fish species, found in America, Asia and Africa, where it can be considered the most important freshwater fish (Al-Deghayem et al., 2017). Although 22 species are commercially grown, Nile tilapia (Oreochromis niloticus), NT, represents 90% of the commercial production (Miranda et al., 2010). This production generates a large amount of by-product, mainly composed of viscera, head, skin, bone, and muscle tissue (Shu & Tsai, 2016), which represents a significant volume of raw material that is rich in proteins and fatty acids from the omega-3 series (Feltes et al., 2010; Zapata & De La Pava, 2018).

In this sense, the increasing amount of food by-products originated by modern society represent not only a resource problem but also an environmental and economic problem besides being a moral challenge. The generation of huge volumes of by-products from animal slaughtering leads to the development of new processes for the treatment and exploitation of these by-products. It can produce alternative sources, preserve the environment, and evolve in the attendance of more demanding environmental laws. Regarding animal slaughtering by-products management, like the NT, one practice that has been highlighted is the extraction, isolation, and use of biomolecules originating from these by-products. The obtainment of a protein hydrolysate, for use as a raw material to produce pet and human food, represents a possibility of value aggregation.

However, due to the high contents of water and protein, the hydrolysate is very susceptible to decomposition. One option is to subject it to the most common meat preservation technique, i.e., drying technique (Chabbouh et al., 2013). Although, for further use of protein hydrolysate in drying industrial scale, techniques of modeling and simulation are indispensable. Without them, the project, control, and optimization of unit operations are unfeasible. Still, only with the previous knowledge of the desorption isotherms and the isosteric heat is possible to design a drying system. These thermodynamic properties are essential in processes that involve simultaneous heat and mass transfer, as drying operations. Desorption isotherms are unique for each product (Galdeano et al., 2018) and very important, since, once the breakeven point is known, it can estimate the time needed to reach it, avoiding unnecessary energy expenditure during the drying operations, and provide information about the safe moisture contents (Botelho et al., 2019). In turn, isosteric heat is considered an essential parameter in energy demanded on drying processes because it is related to the amount of energy to remove the free water (Oliveira et al., 2017).
In the literature, there are some works that evaluated the equilibrium isotherms for hydrolysates produced from aquatic meat products, such as Antarctic krill meat (Zhang et al., 2002), horse mackerel, chub mackerel, white croaker, sardine, and flying fish (Khan et al., 2003), as well as NT meat (Candido & Sgarbieri, 2003), and mussel meat (Silva et al., 2012). However, there is only one paper that evaluated the isosteric heat of tilapia viscera (Camaño Echavarria et al., 2021) and there are no studies that evaluated the equilibrium isotherms and isosteric heat of the NT slaughtering by-products. So, the present work aimed at obtaining of the desorption isotherms and the calculation of the isosteric heat of the protein hydrolysate produced from NT slaughtering by-products. This evaluation allowed the application of the obtained data in studies of modeling, simulation, and optimization of the dried NT slaughtering by-product protein hydrolysate production and storage for commercial use.

2 Material and methods

The tilapia slaughtering by-product, composed of head, spine, and tail, was collected after the fish processing in the Tilapia Brazilian slaughterhouse of the municipality of Toledo (24° 43’ 12” S; 53° 44’ 36” W, and altitude of 550 m). The experimental procedure for the hydrolysis followed in this work was identical to that described by Dieterich et al. (2014). The by-product was cooled at approximately 5 °C at the facility, packed in thermal boxes, and immediately taken to the laboratory, where the hydrolysis took place. Approximately 2 h elapsed from slaughter to hydrolysis. The by-product, still fresh, was ground in an electric grinder and hydrolyzed in a 5 kg bench reactor. The hydrolysis was carried out with a proteolytic enzyme from *Bacillus licheniformis* (Alcalase® 2.5L, Novozymes) in a 5 L Pyrex beaker, under an aqueous medium, with 15% of water and 0.2% of enzyme (related to the total mass of by-product from NT). For heating, a common kitchen burner powered by LPG was used under 60 °C and continuously stirred (350 rpm) by a mechanical stirrer (Marconi MA-03) for 2 h. After this process, the reaction was interrupted by keeping the temperature of the reactive medium at 90 °C for 20 min. The product was then filtered, bottled, and cooled to 8 °C.

Seeing that it was produced from a greasy raw material, the NT by-product protein hydrolysate presents a high oil content, of approximately 15% (Schössler et al., 2012). That oil, when heated inside the spray dryer, tends to adhere to the walls of the drying chamber, thus reducing yield and affecting the quality of the dehydrated product. Then, the raw hydrolysate was centrifuged in bench equipment ROTINA 420 from HETTICH, for 15 min at 8000 rpm. The supernatant oil was removed from the bottles manually. The remaining contents (protein and aqueous phases) were stirred until re-composition and then fed into the dryer.

The protein content determination of the hydrolysate was carried out in duplicate, according to the methodology of AOAC (Association of Official Analytical Chemists, 1995). The analysis was conducted at the Food Quality Laboratory (LQA) at *Universidade Estadual do Oeste do Paraná* (UNIOESTE) campus Toledo.

The hydrolysates were dried on an MSD 1.0 bench spray dryer from LABMAQ of Brazil, at the facilities of the Food Centre Laboratory from the Federal Technological University of Paraná – Medianeira. This equipment is composed of a drying chamber and cyclone built-in stainless steel. The operating procedure consisted of turning on the air blower at the minimum flow rate of 20 L/min. The electric resistance was turned on to keep the initial temperature at 70 °C. The drying air temperature was increased by 10 °C steps until reaching 100 °C, when was started the feeding of water at a flow rate of 0.21 L/h. Then, the temperature was raised to 130 °C, when the product feed was initiated. The feeding is provided by a peristaltic pump, with a flow rate capacity from 0.2 to 1.0 L/h. The maximum inlet drying air temperature used was 200 °C.

The air circulation system is composed of a 500 W air blower and a 3500 W electric resistance. The drying chamber has 50 cm in height and a diameter of 20 cm. The atomization of the liquid feed is obtained through
a pressurized double fluid nozzle. The liquid feed is mixed with compressed air before the injection on the nozzle. This mixture is then forced through the orifice on the nozzle, creating a fog (spray) inside the drying chamber. For the experiments described a nozzle with an orifice of 1.2 mm in diameter was used. The dried product passes through the cyclone, where the hot and moist air is expelled from the top and the powder is collected in a glass bottle at the bottom. After the spray-drying, 0.1 g samples were dried in a vacuum kiln brand Quimis, model Q819V2, at 70 °C for 24 h, and kept in a desiccator until room temperature was reached.

For the desorption isotherm experiment, firstly the samples were humidified until 95% in a Dynamic Vapor Sorption (DVS) equipment made by Surface Measurement Systems (SMS) model DVS 002. The equipment belongs to the Analytical Resources and Calibration Laboratory of the Chemical Engineering Faculty of the State University of Campinas – São Paulo, Brazil. The equipment has a microbalance, that measures the moisture loss of the sample, by dragging an inert gas, with relative humidity and controlled temperature. Moisture was generated from mass flow drivers, mixing the flows of dry gas and saturated steam in certain proportions, to obtain the desired relative humidity. After the samples reached 95% of relative humidity, the experimental desorption run atomically started inside the DVS. The desorption isotherms were obtained in the range of 95 to 0% (in 10.6% step) of relative humidity, at temperatures of 20 °C, 35 °C, and 50 °C (Wani & Kumar, 2016). The moisture content of hydrolysates samples was measured according to the AOAC method (Association of Official Analytical Chemists, 1995).

The equilibrium moisteres were calculated in dry base (d.b.) and then the isotherms were drawn according to the water activity, for each one of the three experimental temperatures. The models presented in this work are in Table 1, where $X_E$ is the equilibrium moisture content, d.b., $a_W$ is the water activity, $A$, $B$, $C$, and $k$ are model parameters, and $X_m$ is the monomolecular moisture content, d.b.

| Model                        | Equation                                      |
|------------------------------|-----------------------------------------------|
| Langmuir (Langmuir, 1916)    | $X_E = \frac{A B a_W}{1 + B a_W}$            |
| White and Eyring (White & Eyring, 1947) | $X_E = \frac{1}{A + B a_W}$                     |
|                          | $X_E = \exp(A + B a_W)$                        |
| Caurie (Caurie, 1970)       | $X_E = A + B \left(\frac{a_W}{1-a_W}\right)$ |
| Chirife and Iglesias (Chirife & Iglesias, 1978) | $X_E = A + B \left(\frac{a_W}{1-a_W}\right)^{1/n}$ |
| Oswin (Oswin, 1946)        | $X_E = A - B \ln(1-a_W)$                      |
| Smith (Smith, 1947)        | $X_E = A - B \ln(1-a_W)$                      |
| Brunauer–Emmett–Teller (BET) (Brunauer et al., 1938) | $X_E = \frac{X_m C a_W}{(1 - a_W)(1 + (C - 1)a_W)}$ |
| Guggenheim–Anderson–De Boer (GAB) (Van der Berg & Bruin, 1981) | $X_E = \frac{X_m C a_W}{(1 - K a_W)(1 + (C - 1)K a_W)}$ |

Using the Maple 13® software, the parameters of the models were estimated, applying the NonlinearFit command, Modified Newton method with a converging criterion of $10^{-11}$.

For the representativeness analysis of the desorption models, statistical tests of determination coefficient ($R^2$), Sum of Squares of Residues (SSR), Relative Mean Error (RME), and Akaike Information Criteria (AIC) were used.

The isosteric heat of desorption can be defined as the total heat of desorption minus the latent heat of vaporization of pure water at the system temperature, Equation 1:

$$q_{st} = Q_{st} - \bar{e}_V$$

where:
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$q_{st}$ – isosteric heat of desorption, kJ/kg;
$Q_{st}$ – total heat of desorption, kJ/kg; and,
$\tilde{e}_V$ – latent heat of vaporization of pure water at the system temperature, kJ/kg.

According to Brooker et al. (Brooker et al., 1992), the latent heat of vaporization of pure water is defined by Equation 2, valid for 273.15$<T_{ABS}<338.72$:

$$\tilde{e}_V = 2.503 \times 10^3 - 2.386(T_{ABS} - 273.15)$$

(2)

where:
$T_{ABS}$ - absolute temperature, K.

There are several methods to obtain the isosteric heat of desorption, being the Clausius-Clapeyron equation the most extensively used, relating the changes in water activity with temperature. An alternative method was developed by Othmer (Othmer & Brown, 1940), which assumes that the isosteric heats of desorption and condensation have the same functional dependency with temperature.

The Othmer Equation establishes that, once the equilibrium moisture, $X_E$, is known in different temperatures and vapor pressures, $P_V$, and in known values of partial pressures, $P_P$, the relation between the heat of vaporization of pure water, $\tilde{e}_V$, and the total heat of desorption, $Q_{st}$, can be determined. Thus, from an equilibrium liquid-vapor system, the relationship is defined by Equation 3:

$$\left(\frac{\partial \ln P_V}{\partial \ln P_P}\right)_{X_E} = \frac{Q_{st}}{\tilde{e}_V}$$

(3)

where:
$P_V$ – vapor pressure, Pa; and
$P_P$ – partial pressure.

To achieve the heat of desorption of NT slaughtering by-product protein hydrolysate, $Q_{st}$, the water activity, $a_W$, was computed using an equilibrium moisture content value, $X_E$, from a suitable isotherm. This procedure was repeated for each experimental temperature (20 °C, 35 °C, and 50 °C), when also the vapor pressure, $P_V$, was evaluated. Finally, the partial pressure, $P_P$, was obtained from the values of $a_W$ and $P_V$. This procedure was repeated using different equilibrium moisture content (Djendoubi et al., 2009; Toujani et al., 2011), since according to the Othmer Method the ratio total heat of desorption and heat of vaporization of pure water, $Q_{st}/\tilde{e}_V$, is temperature-independent, varying only with the equilibrium moisture content. The value $Q_{st}/\tilde{e}_V$ was determined from the slope after plotting $\ln P_V$ versus $\ln P_P$ at constant $X_E$. The relationship between $Q_{st}$ and $X_E$ was found by regression technique.

3 Results and discussion

After the hydrolysis process, the protein hydrolysate obtained presented an average protein content of 79.18% and moisture content of 0.126 d.b. The adjusted model parameters to the desorption isotherms from the protein hydrolysate are presented in Table 2. In Table 3, the statistical analysis is presented based on the experimental data and those obtained by simplified desorption models. Although the experimental range was from 0.95 to 0.0 $a_W$, the model’s fit was done in the range 0.739 to 0.0 $a_W$. The other values were not considered while evaluating the results, when using all the experimental points with the fits which had less accuracy. This fact could be attributed to the difficulties in conducting measurements at high $a_W$, which implies low water diffusion and high time to reach the equilibrium (Leuk et al., 2016).
Table 2. Adjusted model parameters to the desorption isotherms.

| Models                  | A       | B       | Xm      | C       | K       |
|-------------------------|---------|---------|---------|---------|---------|
|                         | 20 ºC   | 35 ºC   | 50 ºC   | 20 ºC   | 35 ºC   | 50 ºC   | 20 ºC   | 35 ºC   | 50 ºC   |
| Langmuir               | 1.744   | 1.833   | 2.453   | 0.290   | 0.219   | 0.135   | -       | -       | -       |
| White and Eyring       | 11.473  | 16.375  | 18.403  | -12.064 | -18.252 | -20.210 | -       | -       | -       |
| Caurie                 | -2.695  | -3.297  | -3.436  | 2.238   | 2.906   | 2.881   | -       | -       | -       |
| Iglesias and Chirife   | 0.091   | 0.054   | 0.044   | 0.100   | 0.097   | 0.084   | -       | -       | -       |
| Oswin                  | 0.088   | 0.057   | 0.050   | 1.097   | 0.057   | 1.307   | -       | -       | -       |
| Smith                  | 0.074   | 0.037   | 0.028   | -0.197  | -0.169  | -0.169  | -       | -       | -       |
| BET                    | -       | -       | -       | 0.096   | 0.085   | 0.074   | 6.26E+06| 10.685  | 8.960   |
| GAB                    | -       | -       | -       | 0.084   | -0.060  | 0.057   | 5.53E+08| 1.000   | 55.243  |

Table 3. Statistical evaluation of the adjusted models to the experimental data of the equilibrium isotherms.

| Models                  | R²       | SSR     | RME (%) | AIC     |
|-------------------------|----------|---------|---------|---------|
| Langmuir               | 0.674    | 1.165   | 34.23   | -9.422  |
| White and Eyring       | 0.987    | 0.055   | 6.37    | -35.988 |
| Caurie                 | 0.918    | 0.370   | 17.74   | -18.850 |
| Iglesias and Chirife   | 0.975    | 0.091   | 9.00    | -30.895 |
| Oswin                  | 0.984    | 0.160   | 6.96    | -25.426 |
| Smith                  | 0.889    | 0.407   | 19.10   | -17.953 |
| BET                    | 0.860    | 1.131   | 22.16   | -9.657  |
| GAB                    | 0.887    | 1.037   | 17.29   | -10.351 |

According to the results in Table 3, it was possible to verify that the models which better adjusted to the experimental data were the White and Eyring and Oswin. These models presented the highest value of the determination coefficient (R²) 0.987 and 0.984, and lower values of RME between 6.37 and 6.96, respectively for White and Eyring and Oswin model.

In the Figures 1A and 1B are presented the residue distribution for White and Eyring and Oswin models, which showed the deviation between the observed and the model estimated values.
Regarding Figures 1A and 1B, we can see that both models presented a random distribution of residues and were adequate to represent the tilapia slaughtering by-product protein hydrolysate desorption isotherm. With similar goodness of fit test, the AIC can be used as an additional parameter to select the best model. As the lower AIC values indicated a better fit of the model, the values of -35.988 and -25.426 (Table 3), respectively for White and Eyring and Oswin model, allowed us to take the White and Eyring model as the best in predicting the desorption isotherms from NT slaughtering by-product protein hydrolysate.

The White and Eyring model had a similar form to the Oswin model. This Oswin model was developed for sigmoidal curves and is the best empirical model for predicting protein isotherms (Ibarz & Barbosa-Canovas, 2014) in addition to being suitable for a wide range of isotherms. However, when tested, the Oswin model showed a slightly lesser fit compared to the White and Eyring model. This model is suitable for high values of water activity (Ibarz & Barbosa-Canovas, 2014) and materials of long-chain chemicals (Jian & Jayas, 2021).

In Figure 2 is illustrated the experimental desorption data of the protein hydrolysate of NT slaughtering by-product, as well as the adjustment of the White and Eyring and Oswin models to the experimental data.

According to Figure 2, it could be verified that all the desorption curves were concave and presented a type III isotherm, that behavior is non-sigmoidal (J shape) according to the BET classification (Brunauer et al., 1940). This type of isotherm is common for foods with water-soluble solids (Marques et al., 2022), in which the solid matrix adsorbs small amounts of water at low water activity, $a_W$, and large quantities of water at high water activity (Blahovec & Yanniotis, 2009). When $a_W$ is low, the equilibrium moisture content, $X_E$, increases linearly with $a_W$, and when $a_W$ is high, the equilibrium moisture content, $X_E$, of the solid increases exponentially, due to the formation of capillary condensation region (Bastıoğlu et al., 2017). This step is clear in Figure 2 for $a_W > 0.4$. When $a_W \approx 0.6$, in which the food is considered dried (Moreira et al., 2005), if the temperature rises from 20 °C to 50 °C, the $X_E$ value must be reduced from 0.25 to 0.19 d.b. for avoiding the growth of microorganisms (Rahman, 2007).
Our findings were similar to those found in previous work for tilapia viscera (Camaño Echavarria et al., 2021) and other protein hydrolysates, for instance from okara (Justus et al., 2021), mussel meat (Silva et al., 2012), and chicken meat (Kurozawa et al., 2009). Nevertheless, different results were reported when testing hen egg white powder (Rao & Labuza, 2012), whey powder (Zhou et al., 2014), and rice (Gomes & Kurozawa, 2021) protein hydrolysates. These studies obtained sigmoid-shaped (type II) isotherms, in which $X_E$ increases with the increase of $a_W$, characteristic of starchy food (Carmo & Pena, 2019). The flattening observed when comparing type II with type III isotherm is associated with the number of hydroxyl groups. Whether there are more accessible hydroxyl groups to bind water, the weaker the interactions and the higher the molecular relaxation mechanisms will be (Verruck et al., 2018). The different results may be related to the desorption curves which are influenced by huge features (e.g., composition, structure, and treatments of the material) (Chen et al., 2017).

Concerning Figure 2, it could be observed that, as the temperature was reduced, $X_E$ of the protein hydrolysate of NT slaughtering by-product increased. It happens, once lower temperatures imply less kinetic energy and, therefore, the molecules bond to the solid with higher strength (Kuenzel & Ranjbar, 2019). In the experiments, there was an increase of 15 °C between each experimental temperature. However, the gap observed between the curve obtained for a lower temperature, 20 °C, and the other curves, 35 °C, and 50 °C was more accentuated. This indicated that, at a lower temperature, $X_E$ of the protein hydrolysate of NT slaughtering by-product was more influenced by temperature. As the temperature increased, however, its influence was reduced.

Based on our results, we can affirm that the White and Eyring model can be applied as a powerful tool for predicting the stability and moisture behavior during the drying and storage process of NT slaughtering by-product. This knowledge about the suitable sorption isotherm of materials susceptible to deterioration, like NT slaughtering by-product, is crucial for avoiding chemical and biochemical undesirable losses (e.g., color, texture, odor, and taste). For the White and Eyring model, the parameters A and B were adjusted as a logarithm equation and presented a well-defined behavior as a function of temperature. In Figure 3 is showed the relationship of the parameters to the temperature.

![Figure 3](image)

Figure 3. A and B White and Eyring model parameters.

It can be seen from Figure 3 that parameter A was positively influenced by the increase in temperature, in contrast to parameter B, which decreased with the increase in experimental temperature. The adjustments obtained for the parameters of the White and Eyring model as a function of temperature, with $R^2$ greater than 0.970, are represented by Equations 4 and 5:

\[
A = 7.669 \ln(T) - 11.331 
\]  
(4)

\[
B = -9.08 \ln(T) + 14.835 
\]  
(5)

Thus, the White and Eyring model with the Equations 4 and 5, can be applied to predict the $X_E$ of the NT slaughtering by-product protein hydrolysate in the temperature range of 20 °C to 50 °C. This type of approximation is useful when predicting the sample behavior under nontested temperature. For example, in simulation, design, optimization, and control of drying process in which the temperature varies with the time, that are common in the industry. In these applications, the sorption isotherms added with a kinetic mathematical model may represent the best operational conditions based on an objective function.
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The total heat of desorption, $Q_{st}$, and the net isosteric heat of desorption, $q_{st}$, both calculated with Othmer’s relation and White and Eyring model, as well as the latent heat of vaporization of pure water, $\lambda_V$, are displayed in Figure 4.

Figure 4. Net isosteric heat of desorption, $q_{st}$ (kJ/kg), total heat of desorption, $Q_{st}$ (kJ/kg), and latent heat of vaporization of pure water, $\lambda_V$ (kJ/kg).

Regarding Figure 4, it is observed that with the increase in the $X_E$ the total heat of desorption, $Q_{st}$, approaches the vaporization heat for pure water, $\lambda_V$. This behavior is due to the weakening of the bonding energy between the water molecules in the liquid state. When the by-product presented lower $X_E$, the interaction energy between the water molecules and the first layer of desorption was bigger than the energy that keeps the molecules together on the successive layers (Wan et al., 2016).

An exponential relation was used to adjust $Q_{st}$ as a function of $X_E$. With an $R^2$ of 0.994, the equation obtained was represented by Equation 6:

$$Q_{st} = 2454.22 + 3.82\exp(0.605/X_E)$$  

The calculated $Q_{st}$ ranged from 2395 to 5682 kJ/kg, respectively, for $X_E$ of 0.09 and 0.3 (d.b.). Similar value order of $Q_{st}$ was achieved in literature, such as for sardine muscles, ~2692 to ~3742 kJ/kg (Djendoubi et al., 2009), frozen raw pork meat, ~2200 to ~3600 kJ/kg (Clemente et al., 2009), fresh beef, ~2200 to ~4700 kJ/kg (Ahmat et al., 2014), and tilapia viscera, 2422 to 3083 kJ/kg (Camaño Echavarria et al., 2021).

The amount of required energy to remove 1 kg of water was inversely proportional to $X_E$. At $X_E < 0.14$ d.b., it could be seen a slight change of $X_E$ that significantly raised the desorption heat. In this sense, there is significant biochemical stability of the protein hydrolysate under low $a_W$. This result is associated with the reduction in the heat of desorption which is synonymous with less biochemical stability of protein hydrolysate, due to the greater $a_W$, which implies the activation of enzymes and the development of microorganisms that degrade food (Lavelli et al., 2017).

The lower the $a_W$ as well as the lower $X_E$, as confirmed by the desorption isotherms in Figure 2, the greater will be the energy required to remove the moisture present in the solid matrix. These results are in agreement with the ones verified for protein hydrolysate of anchovy fillet (Moraes & Pinto, 2012). It was observed that small additions on the $X_E$ entailed great decreases in the desorption heat. This fact can be explained by the existence of a greater quantity of not bonded water when the amounts of water are greater. As the moisture decreases, the amount of free water also decreases, therefore the energy required for evaporation increases. The amount of energy required becomes not only that one required for simple evaporation, but also the one required to break the bonding between water and solid matrix (Bahar et al., 2017).

4 Conclusion

In this paper, desorption isotherm and isosteric heat of desorption of NT slaughtering by-product were evaluated. The desorption isotherms were determined by the dynamical model, under temperature conditions of 20 °C, 35 °C,
and 50 °C. Eight models were tested to describe the relationship between the equilibrium moisture content and the water activity. All the desorption isotherm was type III and the empirical model of White and Eyring was the best in predicting the experimental data, $R^2$ of 0.987. The isosteric heat of desorption, obtained using Othmer’s equation, ranged from 2395 to 5682 kJ/kg, for equilibrium moisture content between 0.09 and 0.3 kg/kg. At equilibrium moisture content below 0.14 d.b., slight changes in the moisture implied significant raises in the heat of desorption. An exponential equation was adjusted to relate the isosteric heat of desorption with the equilibrium moisture content. The obtained results can be employed in drying projects, filling the gap in predicting the energy demand and the suitable storage condition of NT slaughtering by-product. Thus, our results represent a useful contribution to realizing the kinetic drying of NT slaughtering by-product as well as the process design.

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