Computational fluid dynamic analysis following recurrence of cerebral aneurysm after coil embolization

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ABSTRACT

Hemodynamic factors are thought to play important role in the initiation, growth, and rupture of cerebral aneurysms. However, hemodynamic features in the residual neck of incompletely occluded aneurysms and their influences on recanalization are rarely reported. This study characterized the hemodynamics of incompletely occluded aneurysms that had been confirmed to undergo recanalization during long-term follow-up using computational fluid dynamic analysis. A ruptured left basilar-SCA aneurysm was incompletely occluded and showed recanalization during 11 years follow-up period. We retrospectively characterized on three-dimensional MR angiography. After subtotal occlusion, the flow pattern, wall shear stress (WSS), and velocity at the remnant neck changed during long-term follow-up period. Specifically, high WSS region and high blood flow velocity were found near the neck. Interestingly, these area of the remnant neck coincided with the location of aneurysm recanalization. High WSS and blood flow velocity were consistently observed near the remnant neck of incompletely occluded aneurysm, prone to future recanalization. It will suggest that hemodynamic factors may play important roles in aneurismal recurrence after endovascular treatment.

Key words: Cerebral aneurysm, endovascular treatment, hemodynamics recanalization, wall shear stress

Introduction

Cerebral aneurysms are treated by means of either endovascular coiling or surgical clipping. Despite their widespread use, these therapeutic modalities are not always successful in eliminating the risk of subsequent aneurysm rupture and subarachnoid hemorrhage (SAH). Regarding the coiling technique, one of the primary failure mechanisms leading to aneurysm regrowth, recanalization, and rebleeding is coil compaction.[1,2] The aneurysms with remnant necks after endovascular occlusion are prone to recanalization, whereas the underlying mechanisms of this phenomenon are not totally clear.[3,4] We have a primary interest in the hemodynamic influences in recanalization of partially occluded aneurysms.

Yet, even in the best cases, the coiling material accounts for less than 50% of the total treated aneurysm volume.[5,6] Consequently, coil compaction can occur and is especially problematic for giant aneurysms, large aneurysms containing thrombi, and aneurysms that project along the direction of blood flow in the parent artery. In addition, loose packing of coils can lead to coil unraveling and migration into the parent artery and subsequent aneurysm regrowth. Numerous evidences suggest that the intra-aneurysmal hemodynamic patterns may have a profound impact on the development of cerebral aneurysms. Using computational fluid dynamics (CFD) analysis, researchers have identified that high-velocity and high-shear stress of the flow impingement may have positive effects on the growth of cerebral aneurysms.[7-9] The aim of the present study was to characterize the hemodynamic changes of the partially embolized aneurysms that were predisposed to recanalization in a long term.

Materials and Methods

Clinical and imaging data

A 58-year-old female patient presented with headache and
SAH in July 2000. Angiography revealed left basilar-SCA small aneurysm [Figure 1a]. This aneurysm was treated via endovascular embolization with coils. Immediately after coil embolization, the aneurysm was completely occluded and the left superior cerebellar artery (SCA) was preserved [Figure 1b]. The patient could not come for follow-up due to her schedule, and we could not follow up at the outpatient clinic. Six years after the initial coil embolization, we noticed a small neck remnant at 3D-MRA. The neck remnant gradually enlarged and cerebral angiography showed recurrence of the aneurysm [Figure 2]. Then, coil embolization was carried out again in March 2007. Immediately after the coil embolization showed disappearance of the aneurysm and preservation of SCA, a remnant was observed at the SCA origin [Figure 2b]. The follow-up using 3D-MRA revealed re-enlargement of the remnant neck to recanalize the aneurysm to drastically grow further [Figure 3], and it ruptured in May 2011.

**Hemodynamic modeling**

A patient-specific CFD model of the aneurysm was constructed from the 3D-MRA image using previously developed methods. The image was filtered, and segmentation was performed with a seeded region growing algorithm to reconstruct the topography of the vascular network followed by an isosurface deformable model to adjust the geometry to the vessel boundaries. The vascular model was then smoothed with a nonshrinking algorithm, and the vessels were truncated perpendicularly to their axes. A volumetric grid composed of tetrahedral elements was generated by an advanced front method with a resolution of 0.15 mm, including three layers prism-layered mesh with a resolution of 0.01 mm, resulting in approximately a 3.2 million-element mesh.

After meshing, we used ICEM CFD software 13.0 (ANSYS Inc., Berkeley, CA, USA) to generate the configuration files that specified the settings of blood properties, boundary conditions, and the time step for fluid field computation. Concerning the calculation scheme, three-dimensional segregated solver and second-order implicit formulation

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**Figure 1:** (a) Cerebral angiography revealed left basilar-SCA small aneurysm; (b) Immediately after coil embolization, the aneurysm was completely occluded.

**Figure 2:** (a) Seven years after the initial coil embolization, cerebral angiography showed recurrence of the aneurysm; (b) Immediately after the second coil embolization showed disappearance of the aneurysm, but a neck remnant was observed.
in time were selected. Blood flow was considered as an incompressible non-Newtonian fluid and modeled by the unsteady Navier-Stokes equations in 3D. The vessel walls were assumed rigid, and no-slip boundary conditions were applied at the walls. The average Reynolds number was within the range of normal blood flow in the human cerebral arteries, indicating a laminar flow condition. The density and dynamic viscosity of blood were specified as 1050 kg/m$^3$ and 0.0035 mPas, respectively. The pressure-velocity coupling method was SIMPLE, and the pressure term was solved by the PRESTO method. Momentum term of Navier-Stokes equation was discretized with the second-order upwind difference scheme and solved by algebraic multigrid (AMG).

**Results**

**Aneurysm geometries**
The 3D aneurysm geometry was prepared based on the 4-year follow-up 3D-MRA DICOM data of the patient. A neck remnant was observed in April 2008; i.e. 1 year after second coil embolization [Figure 4a]. The subsequent follow-up revealed that the neck remnant kept growing with skewed morphology, and the third coil embolization was carried out as it ruptured in May 2011 [Figure 4b-d].

**Stream line**
After the second coil embolization, blood flow entered the remnant neck and formed a small vortex [Figure 5a]. Subsequent follow-up revealed regrowth of the neck remnant. The blood infiltration (spiral vortex blood flow) was observed only at the neck remnant region while the blood inflow was not observed at the enlarged aneurysm dome [Figure 5b-d]. Vector analysis of the flow velocity revealed that the flow rate at the aneurysm neck was consistently faster than the other aneurysm regions during the follow-up period, and showed the presence of impingement [Figure 6a-d].

**Wall shear stress and pressure**
The high-flow regions of the remnant neck matched with the high-WSS regions (impingement regions), and the WSS

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**Figure 3:** Four years after the second coil embolization, cerebral angiography revealed re-enlargement of the remnant neck to recanalize the aneurysm to drastically grow further.

**Figure 4:** The 3D aneurysm geometry was prepared based on the 3D-MRA DICOM data of the patient (a) One year after second coil embolization; April 2007; (b-d) The neck remnant kept growing with skewed morphology, aneurysm ruptured in May 2011.
Figure 5: (a) After the second coil embolization, blood flow entered the remnant neck and formed a small vortex; (b, c, d) Spiral vortex blood flow was observed only at the neck remnant region while the blood inflow was not observed at the enlarged aneurysm dome.

Figure 6: (a-d) Vector analysis of the flow velocity revealed that the flow rate at the aneurysm neck was consistently faster than the other aneurysm regions during the follow-up period, and showed the presence of impingement. The aneurysm wall pressure tended to be higher at the enlarged aneurysm than at the neck [Figure 8a-d].

Discussion
The long-term follow-up after treatment of cerebral aneurysms
with detachable coils was reported previously. Raymond et al.\cite{raymond2012} reported the results of 31 aneurysms at the basilar bifurcation. Of the 29 surviving patients, 27 underwent 6-month follow-up angiography, and 12 underwent another follow-up angiographic examination 1 year later. Recurrence or re-growth of the remnant was seen in 7 patients (24%). Cognard et al.\cite{cognard2012} reported a recurrence rate of 14% in 148 initially totally occluded aneurysms. Remnant regrowth occurred in 6 of 18 subtotally
occluded aneurysms. It is possible that incomplete obliteration modifies the intra-aneurysmal hemodynamic forces and thus may promote the growth and even rupture of some aneurysms.

Angiographically demonstrated complete obliteration of an aneurysm sac after endovascular coil embolization does not mean that the aneurysm sac is completely filled with coils. Computer-assisted analysis of the aneurysm volume and the introduced coil mass revealed that the coil mass did not exceed 30% of the aneurysm sac volume despite complete packing on angiography.[16] Recanalization of the intracranial aneurysms treated with detachable coils depends on various factors including the aneurysm size, neck width, aneurysm location, history of rupture, and immediate post-embolization angiographic results.[1,12,13] Previous studies have shown that recanalization was more common in large and wide-neck aneurysms.[14]

The bifurcation or termination aneurysms reportedly show higher recanalization rate than those of other locations, suggesting that the aneurysm location and hemodynamic stress might be closely related to the risk of recanalization. It is generally considered that the arterial flow stress induces more frequent recanalization.[15]

Cerebral aneurysms are preferentially located at the outer curvatures, bifurcations, or branching points of the brain vessels. As shown by CFD modeling, these vascular segments are affected by complex hemodynamic forces, including impinging flow and alteration of WSS.[15] which may induce pathological remodeling of the vascular structure, transmitted by the endothelial cells.[16,17]

Several studies demonstrated that the residual neck of subtotally embolized aneurysms that underwent subsequent recanalization may be associated with high-flow velocity and WSS.[18,19] An impressive finding is that the high-velocity and WSS region coincided with the location of future aneurysm recanalization. Boet et al.[18] stated that the paraclinoid/ophtalmic segment artery aneurysms were more susceptible to recanalization after primary treatment, and they hypothesized that the high-shear stress imposed on the aneurysm in this particular position might contribute to recurrence. Luo et al.[19] reported the high-WSS and blood flow velocity were consistently observed near the remnant neck of partially embolized aneurysms prone to future recanalization, suggesting that the hemodynamic factors may have an important role in aneurysmal recurrence after endovascular treatment. Ortega et al.[20] performed CFD simulation within a patient-derived basilar aneurysm model. They identified a blood flow impingement adjacent to the remnant neck and found an increase in WSS.

Our results and those of Ortega et al.[20] and Luo et al.[19] indicated that a localized postembolization high WSS at the remnant neck area might contribute to the development of recanalization. Elevation of WSS can cause endothelial injury and thus initiates wall remodeling and potential degeneration. Vascular endothelial malfunction and/or abnormal shear stress field can cause overexpression of the endothelium-dependent NO production, leading to a lower, nonphysiological local arterial tone via processes connected to the scarcity and apoptosis of wall-embedded smooth muscle cells and remodeling. This results in disturbance of the equilibrium between the blood-pressure forces and the internal wall stress forces, in favor of the former, and subsequently dilates the arterial wall locally. The resulting abnormal blood shear stress field is the driving factor for further growth of the aneurysmal geometry. This geometrical growth stretches the collagen and elastin fibers of the medial and adventitial layers, leading to internal stress that contributes to the arterial stiffness. Eventually, the biomechanical system equilibrates at a state where the internal wall stresses and the transmural pressure are equal while the local hemodynamics cannot alter the arterial properties any more. At this point, the elastin and the collagen fibers are constantly under a nonphysiologically large mechanical load and eventually undergo remodeling.[21,22] High WSS and fast blood flow may hamper the local blood coagulation process and prevent formation of blood clots inside the aneurysm.[23,24] Furthermore, the pressure caused by high-speed blood flow may lead to coil compaction, especially in aneurysms with a wide neck, which is thought to be a determining factor in recanalization.[3,25]

Our present data revealed that WSS of the enlarged aneurysm dome after recanalization gradually decreased and the aneurysm ruptured. The low WSS within aneurysms was the cause of localized blood-flow stagnation against the wall in the dome. Blood stagnation causes dysfunction of flow-induced NO, which is usually released by mechanical stimulation due to increased shear stress. This dysfunction results in aggregation of the red blood cells, as well as accumulation and adhesion of both platelets and leukocytes along the intimal surface. This process may cause intimal damages, leading to infiltration by white blood cells and fibrin inside the aneurysm wall, all of which have been detected in pathological examinations of aneurysm walls. The inflammation leads to localized degeneration of the aneurysm wall, resulting in a lower pressure threshold at which the physiological tensile forces could be supported. The aneurysm wall progressively thins and finally may cause the tissue to tear. It is considered that some forces applied to the thinned aneurysm wall ultimately cause aneurysm rupture.

**Limitation of this study**

The case study sample warrants some caution. It is conceivable that this study is not representative of the patient population at large. Moreover, our current study has several limitations common to most CFD analysis, which should be considered when evaluating the results. There are several sources of error that can affect the accuracy of the numeric simulations.
The vascular geometry was approximated from 3D-MRA image data and may have distortions from the process of construction and image optimization. The flow conditions were not patient specific but were derived from measurements on healthy subjects. Several assumptions were made for the CFD calculations, including outflow boundary conditions, rigid walls, and Newtonian properties. The wall biomechanics and perianeurysmal environment were not considered.

**Conclusions**

High WSS and blood flow velocity were consistently observed near the remnant neck of incompletely occluded aneurysms prone to future recanalization, suggesting that the hemodynamic factors may have an important role in aneurysmal recurrence after endovascular treatment.

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