Optimization of pulsed vacuum osmotic dehydration of the cape gooseberry (*Physalis peruviana* L.) using the response surface methodology

Optimización de la deshidratación osmótica a vacío pulsante de uchuva (*Physalis peruviana* L.) por medio de la metodología de superficies de respuesta

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**ABSTRACT**

The objective of this study was to optimize mass transfer during pulsed vacuum osmotic dehydration (PVOD) of cape gooseberries (*Physalis peruviana* L.) by means of the surface response methodology. The effects of the factors temperature (25-45°C), solids (50-70°Brix), rotation speed (60-100 rpm), pressure (50-100 mbar) and number of vacuum pulses (1-3) on osmotic dehydration, weight reduction percentage (WR), water loss percentage (WL), and solid gain percentage (SG%) were assessed. Sucrose syrup at a 5/1 syrup/fruit ratio was used for 2 h. The results provided 45ºC, 70ºBrix, 99.99 rpm, 98.92 mbar and 2.87 pulse vacuum, for a WR of 47.52%, WL of 21.12%, and SG of 118.40% as the optimal conditions. Mathematic models were adjusted to the optimal conditions to describe the PVOD kinetics of cape gooseberries. Azuara’s penetration empiric model, a phenomenological model from the solution of Fick’s second law, and Peleg’s empiric model were used. The latter adjusted better to the experiment data.

**Key words:** kinetic parameters, mass transfer, osmotic pressure, pulsed vacuum, Fick’s law.

**RESUMEN**

El objetivo de este estudio fue optimizar la transferencia de masa durante la deshidratación osmótica a vacío pulsante (DOVP) de uchuvas (*Physalis peruviana* L.) mediante la metodología de superficies de respuesta. Se evaluó el efecto de temperatura (25-45°C), sólidos (50-70°Brix), velocidad de rotación (60-100 rpm), presión (50-100 mBar) y número de pulsos de vacío (1-3) sobre los parámetros de deshidratación osmótica pérdida porcentual de peso (%PP), pérdida porcentual de humedad (PH) y ganancia porcentual de sólidos (GS). Se utilizó jarabe de sacarosa en relación jarabe/fruta de 5/1 durante 2 horas. Los resultados entregaron como condiciones óptimas 45ºC, 70ºBrix, 99.99 rpm, 98.92 mbar y 2,87 pulsos de vacío, para una %PP de 47,52%, %PH de 21,12% y %GS de 118,40. A las condiciones óptimas se ajustaron modelos matemáticos para describir la cinética de DOVP de uchuvas. Se utilizó el modelo empírico de penetración de Azuara, un modelo fenomenológico a partir de la solución de la segunda ley de Fick y el modelo empírico de Peleg. Siendo este último el modelo que mejor ajustó los datos experimentales.

**Palabras clave:** parámetros cinéticos, transferencia de masa, presión osmótica, pulsos de vacío, ley de Fick.

**Introduction**

Colombia is the first world producer of the cape gooseberry (*Physalis peruviana* L.), a perennial plant, native to the South American Andes (Fischer et al., 2014), the second rank export fruit in this country (Márquez et al., 2009). It is a juicy pulpy berry with high levels of minerals, Fe and P, vitamins A and C, and fiber, among others (Marín et al., 2010). Its metabolites have shown hepatoprotective (Arun and Asha, 2007), anti-inflammatory (Wu et al., 2006), antioxidant (Stangeland et al., 2009; Wu et al., 2005), human hepatoma cell antiproliferative, anticarcinogenic (Wu et al., 2004a; Wu et al., 2004b) and anti-diabetic (Ryan et al., 2001) activities, among others (Restrepo et al., 2009). Losses from postharvest management represent between 20 and 25% of fruit production in developed countries and is even higher in developing ones, because of transport and storage problems (Zhu, 2006; Sharma et al., 2009). In the specific case of the Colombian cape gooseberry, 50% of the total production is not exportable because of the size (Castro et al., 2008) and may be used to make new products. Nevertheless, published studies on the cape gooseberry preservation methods are scarce (Castro et al., 2008).

Osmotic dehydration (OD) is a food preservation technique based on the reduction of water activity and moisture, in which the product is submerged in a solution with a high osmotic pressure, which creates a chemical potential gradient between the water/solute contained in the food and the water/solute outside the solution, generating a water flow from inside the product and to a lesser extent, entrance...
of solutes from the solution outside (Peiró et al., 2007), to reduce the difference in their chemical potentials in both sides of the vegetable cell membranes (Bekele and Ramsawamy, 2010). This technique presents advantages over other dehydration techniques since it preserves the sensorial and nutritional characteristics of the product (Peiró et al., 2007; Ozdemir et al., 2008; Chavan and Amarowicz, 2012). OD simultaneously includes processes of water reduction and solute gain (Saxena, et al., 2009; Bekele and Ramsawamy, 2010), in which mass transfer depends on pressure (Reyes et al., 2008; Corrêa et al., 2010), temperature (Zapata et al., 2011), solute concentration (Zapata and Montoya, 2012), syrup/fruit ratio (Akbarian et al., 2014) and agitation, among other variables (Reyes et al., 2008).

In recent decades, some researchers have worked on using OD vacuum to accelerate mass transfer in products such as sardine sheets (Reyes et al., 2008), melon (Fermin and Corzo, 2005), higos (Arreola and Rosas, 2007) and mango (Huayamave and Cornejo, 2005), among others (Mújica et al., 2003a).

Considering low investment cost, and easy implementation (Zapata et al., 2004), low energy consumption (Khan, 2012; Akbarian et al., 2014), as well as organoleptic and nutritional quality of the products obtained with OD (Peiró et al., 2007; Ozdemir et al., 2008; Chavan and Amarowicz, 2012), this technique represents an excellent alternative of preservation in rural areas, which would increase the income level of growers, as it would allow them to use lower quality fruits and give them added value. Response surfaces are very effective tools in optimization, which have been used in different food processes among which is OD (Valdez et al., 2007; Ozdemir et al., 2008; Chauhan et al., 2009). Their principal advantage is the reduction in the number of experiments necessary to obtain statistically valid results (Ozdemir et al., 2008), which are also faster and contain more information than the classical ones in which variables are assessed one at a time (Ozdemir et al., 2008).

The objective of the current study was to optimize the OD at pulsed vacuum (PVOD) of the cape gooseberry (Physalis peruviana L.) by means of response surface methodology. Furthermore, mathematic models were fitted to describe the behavior of the system in terms of the PVOD kinetic.

Materials and methods

Raw material preparation

Fresh cape gooseberry fruits (Physalis peruviana L.) were bought in a local market of Medellin, located at 6°13'55" N and 75°34'05" W. The origin of fruits were from farms at altitudes between 1,200 and 2,800 m a.s.l. Fruits with weights between 3 and 4 g and a soluble solid content between 14 and 15°Brix were selected, washed with alkaline detergent and disinfected with 4% quaternary ammonium; finally, they were peeled to facilitate mass transfer and physico-chemically characterized (AOAC, 1995) (Tab. 1).

### Table 1. Physiochemical composition of the cape gooseberry fruit 

| Analysis                          | Value (± standard deviation) |
|----------------------------------|------------------------------|
| Moisture (b.h.) (g/g)            | 79.23±2.74                  |
| Soluble solids (°Brix)           | 15.00±0.00                  |
| Acid titration (g citric acid/100 g sample) | 1.72±0.06               |
| Maturity index                   | 8.70±0.06                   |
| pH                               | 3.48±0.02                   |
| Aparent density (g cm⁻³)         | 1.01±0.03                   |
| Total phenols (mg tannic acid/g fruit DB) | 1.47±0.09                   |
| Weight (g)                       | 3.50±0.50                   |

Experiment design and statistical analysis of the cape gooseberry fruit PVOD

Osmotic solution and peeled cape gooseberry fruits were placed in a glass balloon with rotatory movement around an axis coupled to the vacuum input of a rotary evaporator (Büchi R-124, Switzerland), for 2 h. The ratio between the weight of the osmotic solution and the fruit was 5:1.

The response surface methodology (RSM) was applied to assess the effect of the factors: temperature (T: 25-45 °C), syrup solid concentration (B: 50-70 °Brix), rotation speed (S: 60-100 rpm), pressure (P: 60-100 mbar) and vacuum pulse (VP: 1-3) over the most important parameters of the cape gooseberry fruit PVOD process: weight reduction percentage (WR), water loss percentage (WL), and solid gain percentage (SG), according to the following Eqs. 1, 2 y 3:

\[
WR = \frac{w_i - w_f}{w_i} \times 100
\]

\[
WL = \frac{w_i x_{wi} - w_f x_{wf}}{w_i} \times 100
\]

\[
SG = \frac{w_i x_{wi} - w_f x_{wf}}{w_i} \times 100
\]

Where \(w_i\) is the initial weight and \(w_f\) the weight at t time, \(x_{wi}\) and \(x_{wf}\) are the initial moisture and solid fractions of the samples, respectively, \(x_{wi}\) and \(x_{ws}\) are the moisture and solid fractions at t time of the samples, respectively. Thirty-two runs were performed according to a composite central factorial design, \(2^{k-1}\) + star, with six central points and two axial ones as shown in Tab. 2. The experiment data were
analyzed using software Design-Expert 7.0 (Estat Ease, Minneapolis, MN). A second order polynomial equation was used to express response variables as a function of the factors as follows:

\[ Y = \alpha_0 + \alpha_1 X_1 + \alpha_2 X_2 + \alpha_3 X_3 + \alpha_1 X_1 X_2 + \alpha_1 X_1 X_3 + \alpha_2 X_2 X_3 
+ \ldots + \alpha_{12} X_1 X_2 X_3 + \alpha_1 X_1 X_2 X_3 + \alpha_2 X_2 X_3 + \alpha_3 X_3 \]

Where \( Y \) are the response variables (WR, WL or SG), \( \alpha_n \) are the model parameters and \( X_1, X_2, X_3, X_4 \) y \( X_5 \) are T, B, V, P and VP factors, respectively.

A VP corresponds to a vacuum for 5 min and relaxation of 10 min at atmospheric pressure. Each of the experiment unit was subjected to VP at first and then kept at an atmospheric pressure for 2 h, under the operational condition, as Tab. 2 indicates. Finally, the samples were dried and the solution on the surface was smoothly removes with paper towel. Samples were analyzed in water content, using an oven of forced air, model termolab 53® (Binder, Portugal), °Brix with a refractometer LR 45227® (Milton Roy Company, Ivyland, PA), and weight with an analytic scale CP2245® (Sartorius, Göttingen, Germany).

The analysis of variance (ANOVA) was made with a confidence level of 95%. Polynomial models were optimized to determine the levels of the factors that maximize WR, WL or SG.

**Cape gooseberry fruit PVOD kinetic modeling**

Assays were made to the optimal conditions found in the previous section to establish the kinetic behavior during the cape gooseberry PVOT for 4 h. Kinetic modeling was done using three different strategies: A penetration empirical model, proposed by Azuara et al., (1992); a phenomenological model from the solution of Fick’s second law (Crank, 1975) and Peleg’s empirical model.

**Penetration empirical model**

The model was based on mass balance to predict dehydration kinetics during the osmotic process, which determines the final equilibrium point, according to Eqs. 5 and 6.

\[ WL_t = \frac{\beta_1 (WL_{\infty})}{1 + \beta_1 t} \times 100 \quad (5) \]

\[ \frac{t}{WL_t} = \frac{1}{WL_{\infty}} (t) + \frac{1}{\beta_t WL_{\infty}} \quad (6) \]

where \( WL_t \) is the water/weight loss at time \( t \), \( WL_{\infty} \) is the corresponding quantity at infinite time (i.e., at equilibrium) and \( \beta_1 (\text{min}^{-1}) \) is the constant related to the rate of diffusion of water out. The equilibrium water loss \( (WL_{\infty}) \) and model constant \( \beta_1 \) were estimated from the slope and intercept of the plot \((t/WL_t) \) versus \( t \) (min) equation (6).

Similarly, Eq. 7 and 8 show the expression to solute gain:

\[ SG_t = \frac{\beta_2 t (SG_{\infty})}{1 + \beta_2 t} \quad (7) \]

\[ \frac{t}{SG_t} = \frac{1}{SG_{\infty}} (t) + \frac{1}{\beta_2 SG_{\infty}} \quad (8) \]

were \( SG_t \) is the solute gain at time \( t \), \( SG_{\infty} \) is the corresponding quantity at infinite time (i.e., at equilibrium) and \( \beta_2 \) (min\(^{-1}\)) is the constant related to the rate of solute transport to inside.

The equilibrium solute gain \( (SG_{\infty}) \) and model constant \( \beta_2 \) were estimated from the slope and intercept of the plot \((t /SG_t) \) versus \( t \) of equation (8).

**Phenomenological model**

To determine the effective diffusivity (\( D_{ef} \)) of the water and solute, a phenomenological model based on Fick’s second law for diffusion in an unsteady-state was used (Assis et al., 2016). To solve Fick’s equation, the following considerations were taken into account: spherical geometry, water or solid initial content (\( MC_0 \)), diffusivity and concentration in constant interphases, the resulting model is shown in Eq. 9 (Crank, 1975).

\[ W_{AorS} = \frac{6}{\pi^2} \sum_{i=1}^{6} \frac{1}{i^2} \exp \left[ -i^2 \pi^2 D_{ef} \frac{t}{r^2} \right] \quad (9) \]

where \( D_{ef} \) is the diffusive coefficient of water reduction or solute gain (m\(^2\)/s); \( i \) is the end of the series number; \( r \) is the average radius of samples (m); \( t \) is the time (s); \( W_{AorS} \) is water loss or solid gain dimensionless, which may be calculated with expression (10):

\[ W_{AorS} = \frac{MC(t) - MC_{eq}}{MC_0 - MC_{eq}} \quad (10) \]

where \( MC_0 \) is the water or solid content at the beginning (g); \( MC(t) \) is the water or solid content in the time instant \( t \) (g); \( MC_{eq} \) is the amount of water or solids in equilibrium (g), obtained from the model of Azuara et al. (1992) with Eqs. 6 and 8.

**Peleg’s empirical model**

Peleg (1988) proposed an equation to describe sorption curves that approach to equilibrium asymptotically. Park et al. (2002) rewrote the same equation as:

\[ MC_t = MC_0 \pm \frac{t}{k_1 + k_2 t} \quad (11) \]

here \( t \) is the time, \( h, k_1, \) and \( k_2 \) are Peleg’s constants.
The quality of the fit of the models was assessed with a linear correlation coefficient ($R^2$) and the mean relative percentage error (MRPE) (Eq. 12); both are statistic parameters widely used in food (Zapata et al., 2014).

$$MRPE = \frac{100}{n} \sum \left( \frac{|X_{ei} - X_{ci}|}{X_{ei}} \right)$$

where $X_{ei}$ is the experiment value; $X_{ci}$ is the estimated value from every model and $n$ is the number of observations.

## Results and discussion

### Cape gooseberry fruits PVOD process optimization using response surfaces

Table 2 shows the 32 random experimental runs of the composite central factor design used to assess T, B, V, P and VP effects on the WR, SG and WL.

While Tab. 3 shows the ANOVA, equations 13 to 15 show the fitted models for WR, SG and WL in function of the

| Assay | Factors | Response variables |
|-------|---------|--------------------|
|       | T (°C)  | B (**Brix**) | V (rpm) | P (mbar) | VP | WR (%) | WL (%) | SG (%) |
| 1     | 45     | 70          | 100    | 50       | 1  | 40.67  | 22.77  | 80.00  |
| 2     | 25     | 70          | 100    | 100      | 1  | 33.19  | 7.31   | 72.73  |
| 3     | 35     | 60          | 40     | 75       | 2  | 25.71  | 9.94   | 70.83  |
| 4     | 45     | 50          | 60     | 50       | 1  | 21.85  | 10.95  | 53.33  |
| 5     | 35     | 60          | 80     | 25       | 2  | 22.29  | 11.97  | 53.33  |
| 6     | 45     | 50          | 100    | 100      | 1  | 27.00  | 15.27  | 66.67  |
| 7     | 35     | 40          | 80     | 75       | 2  | 10.99  | 7.33   | 42.86  |
| 8     | 35     | 60          | 80     | 75       | 2  | 22.62  | 9.01   | 53.33  |
| 9     | 35     | 60          | 80     | 75       | 4  | 24.43  | 10.17  | 83.33  |
| 10    | 15     | 60          | 80     | 75       | 2  | 19.14  | 7.48   | 46.15  |
| 11    | 35     | 60          | 80     | 75       | 2  | 23.52  | 10.01  | 64.29  |
| 12    | 25     | 50          | 100    | 50       | 1  | 15.07  | 6.90   | 33.33  |
| 13    | 25     | 50          | 60     | 50       | 3  | 13.86  | 7.78   | 33.33  |
| 14    | 35     | 60          | 80     | 125      | 2  | 24.61  | 10.07  | 35.71  |
| 15    | 35     | 80          | 80     | 75       | 2  | 49.26  | 20.85  | 92.86  |
| 16    | 45     | 70          | 60     | 100      | 1  | 46.08  | 19.12  | 104.17 |
| 17    | 45     | 70          | 100    | 100      | 3  | 48.45  | 21.65  | 161.54 |
| 18    | 45     | 70          | 60     | 50       | 3  | 38.50  | 20.78  | 93.33  |
| 19    | 35     | 60          | 80     | 75       | 2  | 24.33  | 8.02   | 60.00  |
| 20    | 55     | 60          | 80     | 75       | 2  | 45.92  | 24.11  | 110.00 |
| 21    | 35     | 60          | 80     | 75       | 2  | 23.98  | 10.07  | 46.15  |
| 22    | 45     | 50          | 60     | 100      | 3  | 25.70  | 13.98  | 48.15  |
| 23    | 25     | 70          | 60     | 50       | 1  | 25.07  | 7.78   | 26.67  |
| 24    | 35     | 60          | 80     | 75       | 2  | 21.58  | 11.99  | 46.67  |
| 25    | 25     | 70          | 60     | 100      | 3  | 24.95  | 8.75   | 66.67  |
| 26    | 25     | 50          | 100    | 100      | 3  | 14.41  | 7.51   | 42.86  |
| 27    | 35     | 60          | 120    | 75       | 2  | 25.11  | 8.36   | 40.00  |
| 28    | 35     | 60          | 80     | 75       | 2  | 23.38  | 10.36  | 55.56  |
| 29    | 25     | 70          | 100    | 50       | 3  | 35.53  | 13.20  | 69.23  |
| 30    | 35     | 60          | 80     | 75       | 2  | 21.90  | 11.04  | 76.92  |
| 31    | 45     | 50          | 100    | 50       | 3  | 26.98  | 17.34  | 100.00 |
| 32    | 25     | 50          | 60     | 100      | 1  | 14.55  | 8.50   | 35.71  |

T, temperature; B, Brix; V, rotation speed; P, pressure; VP, number of vacuum pulses; WR, weight reduction; WL, water loss; SG, solid gain.
factors. The $R^2 (> 0.90)$ obtained for WR and WL suggests that these polynomial equations adequately represented the existing relationship between responses and factors with statistically significant effects ($P \leq 0.05$), while the $R^2$ for SG (0.6981) was the less representative value.

**TABLE 3.** ANOVA of the composite central factor design of cape gooseberry pulsed vacuum osmotic dehydration (PVOD) process.

| Factor | WL | WR | SG |
|--------|----|----|----|
| T      | $<$0.0001 | $<$0.0001 | $<$0.0001 |
| B      | $<$0.0001 | $<$0.0001 | 0.0002 |
| V      | 0.0107 |    |    |
| P      | 0.0553 |    |    |
| VP     |    | 0.0257 |    |
| T2     | $<$0.0001 | $<$0.0001 |    |
| TB     | 0.0076 |    |    |
| TP     |    | 0.0202 |    |
| $B^2$  | 0.0027 | 0.0002 |    |
| PB     |    | 0.025 |    |
| P VP   |    | 0.0343 |    |
| Lack of adjustment | 0.3038 | 0.0993 | 0.1661 |
| $R^2$  | 0.9028 | 0.9683 | 0.6981 |

See abbreviations in Tab. 1.

\[
WL = 63.31 - 1.37T - 1.48B + 0.015T^2 \\
+ 0.013TB + 0.01B^2 \\
\] (13)

\[
WR = 39.06 - 1.41T - 1.21B + 0.06V - 0.06P + 3.95VP + 0.023T^2 + 0.02B^2 + 5.42 \times 10^{-3}TP \\
- 0.05VP \\
\] (14)

\[
SG = 65.10 + 1.89T - 1.54B - 2.31P + 8.25VP \\
+ 0.04BP \\
\] (15)

**Factor effects on WL and WR in PVOD of cape gooseberry**

Taking into consideration that it is a dehydration process, water that exits the fruit becomes one of the most important parameters to assess, as well as the weight reduction percentage (WR), which indirectly measures the water reduction in the osmodehydrated product, important variables in transportation and storage of great volumes of product.

ANOVA’s composite central factorial design (Tab. 3) showed factors with a significant effect on the WR and WL variables, which are: T in its lineal ($P < 0.0001$) and quadratic ($P < 0.0001$) term, with negative and positive effects, respectively (13 and 14). Likewise, B significantly affected WR and WL in their lineal term ($P < 0.0001$), with a negative effect on both variables. B, in its quadratic term, had a higher significance on WR ($P = 0.0002$) than on WL ($P = 0.0027$), but, in both cases, the effect was positive. The B effect is explained by the osmotic pressure gradient between the fruit and the osmotic solution, which causes the exit of water from inside the fruit (Corrêa et al., 2010), the difference between lineal and quadratic terms indicate the existence of a maximum point in the T range used in the current work.

The V factor had an effect on WR on its lineal term ($P = 0.0107$) with a positive effect, this was due to the fact that OD can be enhanced by agitation or circulation of the syrup around the sample (Bekele and Ramaswamy, 2010). It can also be observed that there are significant interactions between T with B ($P = 0.0076$) and with P ($P = 0.0202$) on WL and WR, respectively, with positive effects in both variables. While a significant interaction, was only found between P with VP ($P = 0.0343$) in WR, with a negative effect.

Figures 1a and 1b show the response surface graphics for WL and WR in the PVOD process. The graphs show the B
and T factors interactions have over both variables, when P (75 mbar), V (80 rpm) and VP (2) factors stay constant.

It can be seen in both graphs that, as B and T increased, WL and WR did too, until reaching top values when B had 70°Bx and T was 40°C. The effects these two variables on WL and WR, is due to the fact that their increments favor the exit of water from the fruit (Lombard et al., 2008; Bekele and Ramaswamy, 2010), associated to its effect over mass transfer and Df during OD (Alakali et al., 2006) even in systems submitted to pulsed vacuum (Arreola and Rosas, 2007; Allali et al., 2010).

**Factor effects on SG in PVOD of cape gooseberry**

Solid gain (SG) is an important parameter in OD, because in some cases its increment is an undesirable phenomenon as it may be associated to organoleptic properties and product caloric content changes (Jalaee et al., 2011; Phisut, 2012); besides, it may favor the creation of a barrier in the surface of the product negatively affecting mass transfer in the system (Giraldo et al., 2003). On the other hand, if the idea is to cut down weight reduction in the product to avoid meaningfully affecting cost, an elevated SG may be desirable as it happens in glazed products (Giraldo et al., 2003). Table 3 shows factors with significant effects on the SG response variable include: in their lineal terms T (P<0.0001), B (P=0.0002) and VP (P=0.0257) and the interaction of P with B (P=0.025).

Equation 15 shows T has a positive effect on SG, which indicates this variable favors the entrance of solids in the fruit as an effect of its action on the diffusion coefficients (Alakali et al., 2006; Arreola and Rosas, 2007; Allali et al., 2010; Tortoe, 2010), while B had a negative effect, which is associated with the fact that high B values negatively affect the entrance of solids when favoring the creation of a barrier on the surface of the membranes of the product (Giraldo et al., 2003; Mujica – Paz et al., 2003; Ferrari y Hubinger, 2008). The VP factor had a significant positive effect over SG, which indicates the greater the number of applied vacuum pulses, the higher the gains in solids due to vacuum pulses provoke the opening of the fruit pores and the exit of entrained air. When the atmospheric pressure is restored, such pores are filled with the osmotic solution which affect the fruit solid gain (Huayamave and Cornejo, 2005; Arreola and Rosas, 2007). The P and B interaction had a positive effect on SG, possibly because the pressure reduction caused the expansion and exit of gas enclosed in the pores, and pores can be occupied by osmotic solution, thus increasing the mass transfer rate (Bekele and Ramaswamy, 2010), when increasing the vacuum this process increases too. On the other hand, the solution that entered the pores may exit along with the original liquid during the relaxation period at atmospheric pressure, but with concentrated solutions, the exit of the solute does not happen the same way, resulting in a higher SG (Mújica et al., 2003a). (Mújica et al., 2003b). To corroborate this behavior, note the graph for SG as a function of the more significant factors (T and B), V (80 rpm), VP (2) and pressure (75 mbar) values were noted (Fig. 2).

**Model optimization**

Equations 13, 14 and 15 were submitted to a maximization process to determine the combination of experimental factors which will simultaneously optimize the three response variables. This process aimed WR and WL were top, while SG were in moderated levels not to affect in an extreme way the flavor and caloric level of the product but do look for its top stability when reducing moisture. The levels of the factors predicted by models (Eqs. 13, 14 and 15) to maximize the response variables WR and WL are show in Tab. 4.

**Cape gooseberry fruit PVOD behavior in time function**

With the values defined in the optimization (Tab. 4), taking a vacuum pulse number 3, PVOD process was performed.
twice, registering data during 4 h (Figs. 3, 4 and 5). In these figures, at 6,600 s, WR, WL and SG, had values of 51.18%; 31.05% and 200.00%, respectively, all values higher to the predicted for the optimization process to 7,200 s (Tab. 4), corroborating the validity of the models obtained in the experimental design and the optimization process. The top values obtained at the end of the assay (10,200 s) were 58.16%, 38.45%, and 278.57%, for WR, WL and SG, respectively. In the case of WR and WL, their maximization is convenient for the preservation of the fruit, as they are associated with the reduction of the water available (water activity) for the development of microorganisms and enzymatic reactions (Zapata et al., 2004; Tiganitas et al., 2009), also reduce cost in transportation and storage. On the other hand, the high SG values, although associated with higher preservation, are not favorable because of their effect on flavor and caloric content.

The most significant changes in WR and WL appeared in the first 5,400 s (Figs. 3 and 4), while SG does not present such change in its graphic behavior (Fig. 5). WR and WL behavior approaches what has typically been observed in fruit OD (Alakali et al., 2006; Ngoran et al., 2009). Nevertheless, fast rising times are lower to the reported for other fruits in OD without vacuum application (Zapata et al., 2011; Zapata and Montoya, 2012), possibly due to the applied vacuum.

OD kinetic parameter behavior observed in Figs. 3 and 4 may be explained considering the first OD moments there are differences in the chemical potential of the species participating in the system (sucrose and water). The fruit interior had a greater water chemical potential and a lower solute one than the solution in the exterior. These differences driving force the movement of solutes inside and water outside the fruit (Ozdemir et al., 2008; Lombard et al., 2008). As the process time goes by, the substance entrance and exit causes a chemical potential differences reduction, taking the system closer to equilibrium, thus reducing entrance and exit of matter slowly until near zero,
just as the driving force propelling mass transfer reduces (Ozdemir et al., 2008).

The exit of water reduces weight and moisture while the solids of the product increase, that is, all kinetic parameters increase (WR, WL and SG). With the solute entrance, weight and solids increase, but moisture reduces, put in other way, WR reduces and the other parameters rise. At the beginning of the process (first 4,800 s) high water exit predominates over the solute entrance, which promotes increments in all kinetic parameters, while at the end of the process both, material entrance and exit, practically stop as the system reaches equilibrium, and therefore kinetic parameters keep stable (Figs. 3, 4 and 5).

**Dehydration kinetic modeling**

Experiment data presented in Figs. 3, 4 and 5 were used and adjusted with Eqs. 5-11.

**Empirical penetration model**

Table 5 shows the parameter values of Azuara’s model obtained from adjusting experimental data with Eqs. 5 and 7. Figures 3, 4 and 5 show the graphic behavior of the experiment and predicted data with Azuara’s penetration model. Both, $R^2$ and graphic behavior values, indicate an adequate setting of the experiment data with Azuara’s model.

**Phenomenological model**

Experiment data setting of $W_a$ and $W_s$ (Figs. 6 and 7) with equations 9 and 10, delivered the values of the effective diffusivity for water reduction and solute gain, $D_{ef, a} = 1.47 \times 10^{-9}$ and $D_{ef, s} = 1.25 \times 10^{-9}$, with MRPE of 11.46 and 20.20, respectively. The higher value of $D_{ef, s}$ with respect to $D_{ef, a}$ can be explained with base in opening of the fruit pores by effect of the vacuum pulses, which when atmospheric pressure is restored, are filled with the osmotic solution accelerating the solid gain (Huayamave and Cornejo, 2005; Arreola and Rosas, 2007). These values are in the same magnitude order of typical values reported in literature for different fruits and vegetables (Giraldo et al., 2004; Maldonado et al., 2008; Melquiades et al., 2009; Rastogi and Raghavarao, 2004).

Using the effective diffusivity values in equations 9 and 10, respectively, phenomenological model predicted values obtained deriving from Fick’s equation solution (Crank, 1975) (Figs. 6 and 7).

**Peleg’s empirical model**

Table 6 shows the parameters obtained with the setting of moisture and total solids experiment data in Peleg’s equation (Eq. 10), as well as the $R^2$ of each setting, and in the Figs. 8 and 9 the experiment values against the ones predicted by Peleg’s equation for moisture and total solids, respectively.

**TABLE 5.** Azuara’s model parameter values in cape gooseberries with pulsed vacuum osmotic dehydration.

|    | WR | WL | SG |
|----|----|----|----|
| WR<sub>∞</sub> | 60.606 | 46.434 | 333.333 |
| β | 0.071 | 0.019 | 0.016 |
| $M_{eq}$ | 39.516 | 44.462 | 60.667 |
| $R^2$ | 0.974 | 0.710 | 0.649 |
| MRPE | 2.90 | 19.610 | 13.510 |

See abbreviations in Tab. 2.
FIGURE 6. Experiment and predicted by Eq. 9 dimensionless water reduction ($W_A$) in pulsed vacuum osmotic dehydration for cape gooseberries.

FIGURE 7. Experiment and predicted by equation 10 dimensionless solute gain ($W_s$) in pulsed vacuum osmotic dehydration for cape gooseberries.

FIGURE 8. Experiment and predicted total solids in the time function in pulsed vacuum osmotic dehydration for cape gooseberries.

FIGURE 9. Experiment and predicted moisture in time function in pulsed vacuum osmotic dehydration for cape gooseberries.
TABLE 6. Peleg’s model parameter values in in pulsed vacuum osmotic dehydration for cape gooseberries.

| Variables                  | Parameters |
|----------------------------|------------|
|                            | $k_1$      | $k_2$      | $R^2$ | MRPE  |
| Moisture (%)               | 5.1x10^{-2} | 1.25x10^{-2} | 0.9855 | 0.55  |
| Total soluble solids       | 5.60 x10^{-2} | 5.20 x10^{-3} | 0.9934 | 0.90  |

The $R^2$ values (Tabs. 5 and 6), MRPE and analysis of graphic behavior (Figs. 3-9), showed the best adjust for the experiment data to the Peleg model, during cape gooseberry PVOD under current study conditions, followed by model derived from Fick’s equation and finally by the Azuara model. Nevertheless, the Peleg model, as an empiric model, does not provide a deeper understanding of the phenomenon, while the two others do, which is very usefully to scale up process and to extrapolate results. Additionally, it must be considered generality involved in the phenomenological model derived from Fick’s equation even without the best statistics. In any case, the excellent fit of Peleg model allow appreciate the application of this model in this process under condition set out in this study.

Conclusion

Operation conditions significantly affect the PVOD of cape gooseberries, principally temperature and °Brix affect WR and WL, while VP affects SG.

This process can be modeled through empirical and phenomenological models with satisfactory results and, in this way, sets out parameters to scale up the process.

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