D-Flat: A Differentiable Flat-Optics Framework for End-to-End Metasurface Visual Sensor Design

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Optical metasurfaces are planar substrates with custom-designed, nanoscale features that selectively modulate incident light with respect to direction, wavelength, and polarization. When coupled with photodetectors and appropriate post-capture processing, they provide a means to create computational imagers and sensors that are exceptionally small and have distinctive capabilities. We introduce D-Flat (Db), a framework in TensorFlow that renders physically-accurate images induced by metasurface optical systems. This framework is fully differentiable with respect to metasurface shape and post-capture computational parameters and allows simultaneous optimization with respect to almost any measure of sensor performance. Db enables simulation of millimeter to centimeter diameter metasurfaces on commodity computers, and it is modular in the sense of accommodating a variety of wave optics models for scattering at the metasurface and for propagation to photosensors. We validate Db against symbolic calculations and previous experimental measurements, and we provide simulations that demonstrate its ability to discover novel computational sensor designs for two applications: single-shot depth sensing and single-shot spatial frequency filtering.

In order to accelerate the pace of research in metasurface visual sensing, we present D-Flat (Db), an open-source TensorFlow framework for the simultaneous optimization of metasurface shape and post-capture processing algorithms. Db is computationally efficient. It enables gradient-based, end-to-end optimization of one or more millimeter to centimeter diameter metasurfaces together with the post-capture processing parameters of a convolutional neural network (CNN) or any other differentiable computation. Db is designed...
to enable fast experimentation. Different computational-sensing models and architectures can be assembled quickly and easily using minimal code. We demonstrate in this paper the inverse-design of two distinct metasurface imaging systems optimized with different objectives. Lastly, D♭ is designed to be modular, providing developers with the ability to include future implementations of metasurface design and post-capture processing algorithms.

To enable the inverse design of large-area metasurfaces, D♭ leverages a standard, cell-based approach [Yu et al. 2011]: It partitions the metasurface into sub-wavelength cells of equal size, evaluates the optical response of the nanoscale shape in each cell independently, and then jointly propagates the field of per-cell responses to the photosensor or other imaging planes. This approach is an approximation that circumvents the computational intractability of solving directly for the electromagnetic field (with nanometer resolution) across the entire millimeter-scale metasurface. Previous reports have shown that it is sufficiently accurate when neighboring cells contain similar types of structures (e.g., nanocylinders or nanofins as depicted in Figure 1b-c) [Khorsasaniejad et al. 2016; Pestourie et al. 2018]. In this way, the task of designing a metasurface becomes that of designing the nanostructures of each cell, treating each cell as a modular component, and spatially arranging the cells to achieve the desired modulation of the entire incident field.

D♭ currently supports two types of differentiable models to evaluate the optical response of each cell. These two approaches are complementary and are well suited for different design tasks or target metasurface sizes. First, it incorporates the auto-differentiable implementation of rigorous coupled-wave analysis (RCWA) published by Colburn and Majumdar [Colburn and Majumdar 2021]. RCWA directly solves for the optical response of each cell under the locally periodic assumption by computing numerical solutions to Maxwell’s equations. While its computational cost is high compared to wavelength and polarization. The image of the scene as captured on the photosensor can then be computed by evaluating and appropriately summing the optical system’s response to each of the scene’s sources. For 3D scenes comprised of textured, slanted planes at different depths, we incorporate an accelerated renderer that replaces the summation over point sources by approximate, piece-wise 2D convolutions of textured layers with the system’s point-spread functions, as introduced by Guo et al. [Guo et al. 2019] (Section 2.3).

Along with this paper, we present the framework as a validated, maintained open-source software accessible at https://tinyurl.com/

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1Recent domain decomposition methods achieved full-area field simulations but only for micron-diameter devices [Lin and Johnson 2019].

2The theory of RCWA was originally introduced for nanophotonics by Lalanne and Silberstein [Lalanne and Silberstein 2000].
Here, \( \mathcal{L} \) is a loss function to be minimized and measures the difference between the obtained output and the desired output. Examples of computational parameters \( \Psi \) and optimization demonstrations with \( D \) are provided in Section 4.

2.1 Metasurface Cell Models

At the heart of the proposed framework and one particular distinction which sets it apart from other diffractive simulators is a differentiable treatment of the metasurface optical response. We define a metasurface \( \Pi \) as a collection of cells on a regular grid of points \( \chi \) at the metasurface plane. The nanostructures in each cell are then defined using a set of shape parameters \( \pi \):

\[
\Pi = \{ \pi(x', y') | (x', y') \in \chi \},
\]

\[
\pi(x', y') = (\pi_1, \pi_2, ..., \pi_i, ..., \pi_D) \in \mathbb{R}^D, \tag{2}
\]

where \( D \) is the dimensionality of the given nanostructure type. As an example, single nanocylinders placed at the center of each cell (Figure 1b) are parameterized by the cylinder radius \( r \) with \( D = 1 \), nanofins (Figure 1c) by the fin widths \( w_x \) and \( w_y \) with \( D = 2 \), and the set of four ellipses (Figure 10b) by the set of four major and minor axes lengths with \( D = 8 \). In the limit of free-form nanostructures, \( D \) becomes particularly large as the parameters \( \pi_i \) may correspond to the binary inclusion of a dielectric at each point within the cell.

An optical model \( M : \mathbb{R}^D \rightarrow \mathbb{C} \) prescribes the mapping between the cell parameters \( \pi \) and its optical response in terms of a local transmittance \( A \) and phase-delay \( \theta \) imparted to an incident wave-front:

\[
M(\pi(x', y'), \Theta) = A(x', y') \exp(-j\theta(x', y')) , \tag{3}
\]

where \( \Theta \) represents the state of the incident light defined by direction, wavelength \( \lambda \), and polarization. The functionality of the assembled metasurface can then be defined by applying this complex modulation to the field incident at each cell

\[
u(x', y', \Theta) = M(\pi(x', y'), \Theta)u(x', y', 0^+, \Theta), \tag{4}
\]

where \( 0^+ \) and \( 0^- \) represents the plane immediately before and after the optics, respectively.

Equation 4 is a statement of linear optics, while Equation 3 is specific to metasurfaces. Unlike with conventional diffractive optical elements (DOEs), the cell size considered is sufficiently small relative to the operating wavelengths so that there is no energy in higher-order diffraction channels other than the zeroth order; as a result, only a single pair of transimission and phase values per state \( \Theta \) needs to be modeled in the output [Yu et al. 2011]. Moreover, as many structures have an optical response that varies weakly with incident angle, we may presume normal incidence. The optical model can be readily generalized to account for scenarios where either assumption is not valid, such as in non-local metasurfaces with a tilt-dependent response [Kwon et al. 2018].

In order to optimize the metasurface under the constraint of modulation functions that are achievable by realistic nanostructures, the modulation function in Equation 3 must be differentiable with respect to the shape parameters \( \pi \). Notably, there is no simple analytic relation for the optical mapping \( M \) that may be derived from first principles which is valid for general nanostructures.

2.1.1 Physical Optical Model

Physical models determine the gradients of the mapping in Equation 3 by solving Maxwell’s equations directly, for a given cell. While there exists many methods (and many open source packages) for solving the field equations, including finite-difference (FDFD, FDTD) and finite-element (FEM) methods [Jarem and Banerjee 2016], rigorous coupled-wave analysis (RCWA) [Liu and Fan 2012] is largely the standard choice in metadynamics design owing to its computational efficiency, particularly for small cell sizes and high aspect ratio nanostructures. This approach avoids iterative solvers and Krylov methods by formulating the scattering problem as an eigen-equation.

Given the ability to solve the forward equation, gradients in the reverse direction are typically obtained by the adjoint method [Johnson 2007; Miller 2013]. The adjoint method yields directly an analytical solution to the gradients of the field with respect to dielectric inclusions at each point in the cell. Notably, we instead desire the gradients with respect to the shape parameters \( \pi \). While this can be done using the adjoint method, it requires the user to manually implement additional, shape-dependent derivations each time a new nanostructure type is introduced. Alternatively, this burden on users of the framework can be side-stepped entirely by employing an auto-differentiable (AD) field solver. Automatic differentiation stores the mathematical operations performed in a calculation so that the analytical chain rule for differentiation can be efficiently performed to yield the exact numerical gradients.

In recent years, there have been numerous AD field packages published. We modify and port the Tensorflow RCWA implementation [Colburn and Majumdar 2021] into \( D \). Technical details are deferred to the original work. In physical models, each cell must be individually discretized into a Cartesian grid to be numerically evaluated. Consequently, the required memory scales non-linearly with the resolution of the grid, and the computational cost for evaluating the mapping is generally found to be orders of magnitude greater than that of the neural optical model. For this reason, coupling a physical model for the optical layer with complex algorithms, like deep neural networks, is challenging. Alternatively, the computational cost is largely invariant to the value of \( D \) and requires no pre-evaluated training data.

2.1.2 Neural Optical Model

The neural optical model is more efficient in inference than physical models and is similarly accurate. It uses trained MLPs to approximate Equation 3:

\[
M(\pi, \Theta) \approx \text{MLP}(\pi, \Theta), \tag{5}
\]

The MLP takes the cell parameters and the light state as an input and outputs the predicted transmittance and phase delay imparted by the cell. Given supervised training data \( \{(\pi, M(\pi, \Theta))\}_{k=1,\ldots,N} \) pre-generated by physical field solvers, we minimize the squared loss function to train the neural optical model via stochastic gradient descent:

\[
\arg\min_{\Theta} \sum_{k} \sum_{\Theta} (M(\pi, \Theta) - \text{MLP}(\pi, \Theta; w))^2, \tag{6}
\]

where \( w \) are the parameters of the MLP.

While \( D \) includes a compatible physical model (a Fourier-based method) to generate the training data, it is beneficial in some cases to utilize an efficient finite-difference time-domain (FDTD) solver.
instead [Gedney 2011]. Time-domain methods allow one to evaluate the optical response for many incident wavelength states with a single simulation by Fourier transformation of the time-domain field behavior. In contrast, frequency space methods require an additional simulation for each wavelength probed, although they are more efficient. For this work, we utilize the commercial FDTD software by Ansys Lumerical Inc., to generate several finely-sampled broadband datasets for training.

The neural optical model serves as a differentiable proxy to the physical model, with substantially lower computational and memory cost per query. As a consequence, this representation enables the optimization of large, 2D metasurfaces in conjunction with complex algorithms—the limitation being the need to pre-generate training data. It is important to recognize, however, that the training data need not densely or uniformly sample all instantiations of $\pi$ due to the generalization power of MLPs. For large $D$, e.g., multiple fins placed in a single cell with each having several degrees of freedom, it is possible to consider an adaptive learning method where the neural optical model queries the physical model for the labelled data that will best improve the models accuracy.

2.1.3 Shape Constraints. For both the physical model and the neural optical model, one must impose constraints when optimizing the shape parameters $\pi$. While obtaining gradients with respect to the shape parameters rather than dielectric inclusions inherently ensures that only generally fabricable shapes are designed, we still require bounds on these degrees of freedom to ensure meaningful dimensions (e.g. structure widths that are positive and smaller than the cell size or separation distances consistent to fabrication tolerances). For the parameterizations discussed in this work, these bounds take the form of simple inequality constraints on the minimum and maximum dimensions, $a_i \leq \pi_i \leq b_i$. To enforce these, we utilize a parameter-transformation method alongside standard unconstrained optimization. Specifically, for each cell, we back-propagate gradients to a latent parameter $z_i \in \mathbb{R}$ which is differentially related to the shape parameters by the analytic transformation, $\pi_i = a_i + (b_i - a_i) \frac{\tanh(z_i) + 1}{2}$, $\pi_i \in \pi$.

(7)

For more complicated and general constraints, this technique may still be used but with an alternate construction of the transformation function, potentially a pre-trained generator network or a set of nested functions.

2.2 Propagation Models

Given the complex field after the optics, e.g. after applying Equation 4, the propagation of the field in free space is prescribed fully by the theory of Fourier optics. In this section, the theory is reviewed with focus on the particular implementations included in D0. In summary, D0 incorporates four different propagation models for scalar fields which provide trade-offs between generality and efficiency. In addition to the full scalar diffraction model, it includes efficient propagators for metasurfaces with radial symmetry (e.g., metalenses) and for cases where the distance between the metasurface and photosensor is relatively large (i.e., paraxial propagation).

As in Figure 1a, the wavefront after the metasurface propagates towards the photosensor placed a distance $z$ after the lens. The field at the new plane, $u(x, y, z)$, can be computed by evaluating the first Rayleigh-Sommerfield solution of diffraction [Goodman 2017]:

$$u(x, y, z) = \int_{x', y'} u(x', y', 0^+) d x' d y'. \quad (8)$$

The full transfer function $h(x, y, z)$ is the impulse response function for free space propagation:

$$h(x, y, z) = \exp \left(\frac{jk}{\lambda z}(x^2 + y^2)\right). \quad (9)$$

If $r \gg \lambda$, as is often the case in computational imaging, a binomial approximation (the Fresnel approximation) can be introduced and the impulse response function can be simplified:

$$h(x, y, z) = \exp \left(\frac{jk}{2z}(x^2 + y^2)\right). \quad (10)$$

This approximation enables a more computationally efficient form for Equation 8 when substituted:

$$u(x, y, z) = \frac{\exp \left(\frac{jk}{\lambda z}(x' y')\right)}{\sqrt{2\pi}} \int_{x', y'} \exp \left(\frac{jk}{2z}(x'^2 + y'^2)\right) dx' dy'. \quad (11)$$

This is referred to as the Fresnel diffraction integral. In this approach only, the output grid differs from the input grid unless zero-padding of the initial field is used. This padding is handled internally in D0 to return fields on a user-specified grid. Evaluation of the diffraction equation can then be done utilizing a single Fourier transform operation.

Notably, another computationally efficient form of Equation 8 can be given which provides an exact treatment for the impulse response function. In some cases, it is also more memory efficient than Equation 11, as the input and output grids are the same without need for padding. In the frequency domain, Equation 8 can be reformulated as:

$$U(k_x, k_y, z) = U(k_x, k_y, 0^+) H(k_x, k_y, z), \quad (12)$$

where $U$ denotes the Fourier transform of $u$ and $H$ is the Fourier transform of the full $h$ [Sherman 1967]:

$$H(k_x, k_y, z) = \exp \left(\frac{jk^2 z}{2} - \frac{k_x^2}{k^2} - \frac{k_y^2}{k^2}\right). \quad (13)$$

The propagated field can then be numerically evaluated via:

$$u(x, y, z) = \mathcal{F}^{-1} \left(\mathcal{F}(u(x, y, 0^+) H(k_x, k_y, z))\right), \quad (14)$$

where $\mathcal{F}^{-1} (\cdot)$ indicates the inverse Fourier transformation. Equation 14 is referred to as the angular spectrum method (ASM).

To achieve acceptable accuracy with either propagation method, careful attention must be paid to the spatial sampling that is used in the discrete Fourier transforms. In particular, the initial field after the metasurface $u(x, y, 0^+)$ should be sufficiently upsampled if needed to satisfy the Whittaker-Shannon sampling theorem. The required sampling rate can be deduced directly from the Fourier bandwidth of $u$; however, a challenge exists in that there is no simple, analytic theory to determine this bandwidth for arbitrary
fields. In general, one would iteratively increase the sampling rate and evaluate the intensity of the field relative to the aliasing criteria (in practice, researchers often use an arbitrary upsample factor based on inspection). This is not suitable for inverse design where the field changes substantially and the computational graph for rendering should ideally remain fixed.

To address this, we introduce an alternative method. In all cases, we instead consider the Fourier-bandwidth of a quadratic phase exponential bounded by the same field aperture as \( u \). This bandwidth condition emerges naturally when the metasurface imparts an appropriate modulation to focus an incident field. An analytic relation for this Fourier bandwidth can then be derived and is dependent on \( \lambda \) and \( z \). Consequently, when dealing with multiple wavelengths or sensor distances, the computational graph is automatically branched with an appropriate, distinct upsample factor applied in each case. After the branched calculations are done, \( D \) (in practice, researchers often use an arbitrary upsample factor based on inspection). Without loss of generality, we may assume that the light is of incoherent to each other (e.g., scattering under incoherent illumination). Furthermore, we assume that the PSFs vary slowly and smoothly with \( \rho \) and \( z \), such that, 

\[
\rho, z \rightarrow 0
\]

For this work, we have introduced an auto-differentiable, approximate quasi-discrete Hankel transform based on the derivation in [Guizar-Sicairos and Guitierrez-Vega 2004].

\( \mathbb{D} \) implements the four different computations (Equation 11, 14, 15, 16) as auto-differentiable layers. Similar to the optical models, the most suitable or efficient choice for the propagator layer depends on the computational imaging task.

### 2.3 Accelerated Rendering Model

In this section, we briefly review the image formation model and the approximate rendering approach utilized in this paper. We treat the scene to be imaged as a collection of point light sources that are incoherent to each other (e.g., scattering under incoherent illumination). Without loss of generality, we may assume that the light is of a single wavelength and polarization, as a similar numerical process can be repeated to render images of the scene under different states.

Consider a scene \( S \) where every point is completely visible to the optics. Given that the transport of intensity is linear, the image \( I \) may be defined as the weighted summation of the intensity point spread functions \( f \) (PSFs) produced by each point source on the surface of the scene, i.e. \( \{ p_i = (x_i, y_i, z_i) \in S \} \), such that,

\[
I(x, y) = \sum_i T_i f(x, y; p_i),
\]

where \( T_i \) indicates the total energy of light emitted from the point source \( p_i \) that passes through the metasurface. Specifically, the

\[
\mathbf{PSF}\; f(x, y; p_1) \text{ is the intensity distribution at the measurement plane, produced by a spherical wave which originated at the point } (x_i, y_i, z_i) \text{ and interacted with the optics. It can be numerically computed using the methods in Section 2.1 and 2.2 via:}
\]

\[
f(x, y; p_1) = |u(x, y, z; x_i, y_i, z_i)|^2, \tag{18}
\]

where \( z_s \) is the distance from the metasurface to the photosensor.

For scenes that consists only of textured 3D planes (e.g., Figure 3a), we use an approximation to accelerate the rendering. We first assume that the memory effect holds such that the metasurface displays translational invariance for PSFs of the same depth. In other words, a point \( p_i = (x_i, y_i, z_i) \) produces a PSF equal to that from a source on-axis at the same depth but spatially shifted:

\[
f(x, y; p_1) = f(x - \tilde{x}_i, y - \tilde{y}_i; (0, 0, z_i)), \tag{19}
\]

where \( \tilde{x}_i \) and \( \tilde{y}_i \) are inhomogeneous coordinates of the point \( p_i \):

\[
\tilde{x}_i = x_i z_s / z_i \text{ and } \tilde{y}_i = y_i z_s / z_i. \tag{20}
\]

Furthermore, we assume that the PSFs vary slowly and smoothly with depth, such that we may calculate PSFs directly at only a few points \( p_j = (0, 0, z_j) \) and approximate the others via linear interpolation:

\[
f(x, y; p_i) = \sum_j \omega_{ij} f(x - \tilde{x}_i, y - \tilde{y}_i; p_j), \tag{21}
\]

where \( \omega_{ij} \) is the interpolation coefficient, dependent on the point \( p_i \).
The image of a non-occluded scene $S$ can then be approximately rendered by combining Equations 17 and 21:

$$I(x, y) = \sum_i \sum_j T_i \omega_i^j f(x - \tilde{x}_i, y - \tilde{y}_i; p_j), \quad (22)$$

$$= \sum_j T(x, y) \omega_j^3 (x, y) \ast f(x, y; p_j), \quad (23)$$

where $\ast$ denotes a spatial convolution. The interpolation coefficient has been redefined via $\omega_i^j (\tilde{x}_i, \tilde{y}_i) = \omega_i^j$, and $T(\tilde{x}_i, \tilde{y}_i)$ corresponds to the pinhole image of the scene (an all in-focus, geometrically magnified image at the photosensor plane). While the linearly interpolated PSFs are an approximation to the true PSFs, the accelerated rendering closely resembles the synthesized result from ray tracing (see Figure 3).

Lastly, we consider rendering scenes with occlusions, where certain points in the background are only partially visible to the optics. We render the depth boundaries using the layered-mask approximation in Guo et al. [Guo et al. 2019]. A scene $S$ is divided into layers $\{S_l, l = 1, 2, 3, \ldots\}$, where points in each layer $S_l$ are not self-occluded. The framework then renders an image $I_l(x, y)$ of each layer individually using Equation 22 and the corresponding mask $M_l(x, y)$, an image of the segment with uniform texture, $T(x, y) = 1$. The final image of the scene is synthesized by summing over the layer images and masks via:

$$I(x, y) = \sum_l I_l(x, y) \prod_s (1 - M_s(x, y)). \quad (24)$$

### 3 VALIDATION

#### 3.1 Optical Model Validation

For the demonstration of the neural optical model, we focus discussion here on the set of cells containing nanocylinders and nanofins (depicted in Figure 1b,c). These two shapes have been two of the most commonly used nanostructures for designing metasurface-based imaging systems [Chen et al. 2021; Lin et al. 2021a; Tseng et al. 2021]. Nanocylinders are polarization insensitive, while nanofins are polarization dependent due to their asymmetric shape.

Importantly, for this validation, we desire a cell parameterization $\pi$ for which it is feasible to densely sample the parameter space and evaluate the broadband, ground-truth optical response. Notably, although the nanofins have just two parameters ($D = 2$), assuming a fixed cell size and fin height, generating the dataset for a 350 nm wide cell utilizing FDTD as discussed in section 2.1.2 involved evaluating 2304 instantiations which took approximately 200 hours of parallel compute time on a 64-core server CPU. For cell parameterizations with larger values of $D$, one would ideally query training data in a non-uniform, data-driven manner or utilize RCWA and sparsely sample incident wavelengths.

This FDTD-generated dataset for nanofins and the corresponding output of a trained neural optical model is displayed for several discrete wavelengths in Figure 4. The model takes in fin widths $w_x$, $w_y$, and wavelength $\lambda$ and outputs the predicted transmittance $A$ as well as the sin$(\cdot)$ and cos$(\cdot)$ of the phase delay $\theta$ for both $x$ and $y$ polarized light:

$$\{w_x, w_y, \lambda\} \rightarrow \{A_x, \sin \theta_x, \cos \theta_x, A_y, \sin \theta_y, \cos \theta_y\} \quad (25)$$

### Table 1. Performance Per Cell Evaluation for Optical Models.

| Optical Model      | # Parameters | FLOPs | MAE Test Set$^3$ |
|--------------------|--------------|-------|------------------|
| NO-D128-fins      | 18 k         | 37 k  | 0.035            |
| NO-D256-fins      | 68 k         | 139 k | 0.025            |
| NO-D512-fins      | 276 k        | 540 k | 0.021            |
| NO-D1024-fins     | 1.05 m       | 2.13 m| 0.019            |
| NO-D64-cylinder   | 5 k          | 10 k  | 0.043            |
| NO-D128-cylinder  | 17 k         | 36 k  | 0.024            |
| NO-D256-cylinder  | 68 k         | 138 k | 0.018            |
| RCWA-(512, 49)    | NA           | 365.27 m | 0.062            |
| RCWA-(512, 81)    | NA           | 1.620 b | 0.055            |
| RCWA-(512, 121)   | NA           | 5.38 b | 0.051            |

Dealing with the projection of the phase rather than the value directly is important to correctly handle the discontinuity in phase-wrapping. The displayed model used for this mapping has two hidden, dense layers with 1024 neurons in each (hence the name NO-D1024-fins in Table 1).

For this work, we tested different dense architectures to probe how the number of neurons in each layer affects the accuracy. While not displayed, we also explored changing the number of hidden layers; however, we found that two hidden layers provided sufficient accuracy while minimizing the number of trainable parameters. In Figures 14-15, we show a similar display comparing the FDTD data against the nanofin MLP predictions as the number of neurons in each of the two hidden layers are reduced. The neural models for the nanocylinders are treated in the same way as the nanofins but with an input of $(r, \lambda)$ and an output for just x-polarized light. A display of the nanocylinder MLP predictions are shown in Figure 16. All models utilize a leaky ReLU activation function and are trained on a desktop GPU with a MSE loss (Equation 6) and a standard Adam optimizer.

Empirically, we find that all neural optical models considered in this work are expressive enough to learn the general features of the optical response, for both nanocylinders ($D = 1$) and nanofins ($D = 2$). Moreover, some models are able to identify the cells that experience complex light-matter resonances. The resonances can be observed as the sharp dips in transmission in Figure 4a. In practice, it is only important to identify the presence of these resonant cells (rather than to accurately characterize their optical response), since one will try to avoid their selection when designing metasurfaces to improve robustness to fabrication non-idealities.

The accuracy of the neural optical model depends on the number of trainable weights in the MLP and the dimensionality $D$ of the cells. While the method to query training data also has substantial influence, we consider only the case of uniform sampling of the cell’s parameter space. To quantify the accuracy, we utilize as a metric the mean absolute error (MAE) of the complex modulation, $\text{MAE}$. For RCWA, the MAE relative to FDTD is computed over cell transmission values only. The phase may have a global, constant offset without loss of accuracy. Due to computational limitations, the MAE is taken over a reduced sized set from the test cells.
Fig. 4. (Neural model: NO-D1024-fins) MLP-predicted transmission (a) and phase (b) imparted by a nanofin on a 350 nm cell for incident light linearly polarized along x and y. Inputs to the MLP are wavelength $\lambda$ and the nanofin widths $w_x$ and $w_y$ (as depicted in Figure 1c). The results are compared to the FDTD simulated dataset, which was generated by sweeping widths between 60 and 300 nm with a 5 nm step size and for wavelengths between 310 and 750 nm with a 1 nm step size. The MLP results are displayed for a grid of nanofin widths upsampled at 4x the resolution of the FDTD dataset.

taken over the testing set (cells which were not shown during training). The MAE for different models are listed in Table 1, and we note that changes in this metric are found to be well correlated to the visual changes in accuracy that one can observe in Figures 14-16. As a benchmark, we also profile the auto-differentiable RCWA implementation included in D♭. For the RCWA calculations, cells are discretized into a $512 \times 512$ Cartesian grid, the structure is assembled, and the electromagnetic fields are directly solved for. The accuracy of this calculation is set by the number of Fourier harmonics, and we consider 49, 81, and 121 modes (Table 1). In practice, 121 modes are often used to obtain converged results. Evaluating the optical response of each cell by this method takes approximately $5 \times 10^9$ floating point operations (FLOPs).

In contrast, we note that the smallest nanofin model displayed (two hidden dense layers of 128 neurons) correctly predicts the general features of the optical response with disagreement localized around only some of the resonant cells. In this case, the model requires a factor of approximately $10^5$ times fewer FLOPs to evaluate the optical response of the cell as compared to the RCWA physical model. We find that the NO-D512-fins model (two hidden layers of 512 neurons) presents a nice balance between accuracy and computational cost. In summary, there is a trade-off between accuracy and computational advantage for the neural models and further optimizing this interplay for higher dimensional shapes is a topic of future investigation.

3.1.1 Alternative Implicit Representations. As potential alternatives to the proposed neural optical model, we also consider and test the usage of other implicit representations to differentiably approximate the optical response of cells. Specifically, we evaluate the performance of a multivariate polynomial model, as introduced recently for metasurface end-to-end design by Tseng et al. ([Tseng et al. 2021]), and the performance of standard elliptic radial basis function networks (ERBFNs). To the best of our knowledge, the latter has not previously been applied in the context of this problem.

The multivariate polynomial approach formulates the optical model in a linear, matrix form; the shape parameters and the incident wavelength are used as feature inputs and a coefficient matrix for each output is fitted to the FDTD data by the method of least squares. We consider different values for the maximum polynomial degree. The ERBFN is similar to the MLP approach in that both are a class of feed-forward neural networks with dense connections; however, the ERBFN instead utilizes a single hidden layer of neurons with an elliptic Gaussian activation function$^4$ [Dash et al. 2016; Formally, they also differ in that the ERBFN computes a Euclidean distance between inputs and weights while the standard MLP architecture utilizes dot products]
we observe that the MLP can achieve better accuracy in identifying with increasing polynomial order before converging to an accuracy (see ERBF-2048 in Figure 14a as an example). To predict resonant cells where the ERBFN fails (Figure 14b), different FLOPs for cell evaluations are obtained by changing the maximum order for the multivariate polynomial model and the number of neurons in the hidden layer(s) for the ERBFN and the MLP model.

Kononenko and Kukar 2007]. The center coordinate and the standard deviations for the radial Gaussian activation function of each neuron is a learnable parameter that can be optimized via gradient descent, alongside the weights and bias of the dense connections to the output layer. The number of neurons (and consequently the number of radial basis functions used to represent the high-dimensional data) is a free-parameter. The predicted optical response generated by a representative polynomial model and ERBFN after fitting/training is displayed in Figure 14b for the nanocylinder test set and in Figure 16b for the nanofin test set. Different FLOPs for cell evaluations are displayed for different sizes of the ERBFN and the MLP model.

For both types of cells considered in this paper, the polynomial model presents relatively low error in predicting the transmittance and phase. In the case of nanocylinders, the model begins to overfit with increasing polynomial order before converging to an accuracy comparable with RCWA. For nanofins, the large size of the training data and the higher dimensional input/output limited the maximum polynomial order that can be fitted by standard (non-iterative) regression methods to 15. In this case, the model is unable to localize any resonant cells and can only describe the general, low spatial frequency structures in the data.

In contrast, we find that the ERBFNs achieve comparable accuracy to the MLPs and present another reasonable approach for low dimensional cells shapes (i.e., $D = 1, 2$). For both nanocylinders and nanofins, the range of model errors when evaluating the test set are similar, although the ERBFN has reduced computational cost for the nanocylinder cells relative to the MLP. On the other hand, we observe that the MLP can achieve better accuracy in identifying high spatial frequency features in the data which enables the MLP to predict resonant cells where the ERBFN fails (see ERBF-2048 in Figure 14b as compared to Dense-512 in Figure 14a as an example).

While there are numerous variations to this study that could be done, e.g., tweaks to the ERBFN architecture, hyper-parameter tuning, or batched training for the polynomial regression, we highlight that the goal of the implicit representation here is not to absolutely minimize computation but to instead achieve a balance of computational cost, accuracy, and generality relative to auto-differentiable field solvers. While ERBFNs unsurprisingly perform well for these two shape families, the accuracy of this neural architecture requires having a number of hidden nodes roughly similar to the permutations of the input space, e.g., the curse of dimensionality [Alpaydin 2014]. The neural optical models, however, perform well for both cases examined and are known to generalize better as the dimensionality increases for more complicated cell structures. Moreover, recent work on Fourier feature mapping by Tancik et al. [Tancik et al. 2020] further suggests a route for improvements when using the more general, deep MLP architecture.

3.2 Propagation Model Validation
To validate the differentiable propagators included in Dδ, we first demonstrate its ability to reproduce in simulation the experimental fields measured by Lim et al. [Lim et al. 2021]. There, a metasurface was designed that produces a structured, 2D phase singularity at the sensor plane in the shape of a heart. A phase singularity is a point (or set of points) in a complex scalar field where the phase has a discontinuity making it undefined and these points are characterized by zero intensity. They are more commonly found in the unstructured form of optical speckle [Goodman 2020]. Phase singularities make an ideal test-case for 2D propagation studies due to their sensitivity to field perturbations.

A scanning electron microscope (SEM) image of the fabricated metasurface is shown in Figure 6a. In the leftmost panel (b) of the same figure, the experimentally measured intensity along with the reconstructed phase is displayed for the scenario where the metasurface is illuminated by a uniform plane wave and the photosensor is placed a distance after the metasurface. Given knowledge of the metasurface shapes placed in each cell, we may define the field immediately after the metasurface according to Equation 4. We then propagate this field and simulate a similar measurement at the sensor plane utilizing the implemented methods discussed in section 2.2. Here, we use both the 2D ASM method (Equation 14) and the 2D Fresnel diffraction integral (Equation 11) and display the computed results in Figure 6b. Additional comparison of the simulated and experimental measurements for different sensor distances are displayed in Figure 17. In all cases, we find good agreement between the experiment and the forward simulations.

Alternatively, we also verify all four propagators released in this work by examining the computed intensity at the sensor plane for several metasurfaces designed to focus light. The required phase modulation needed to focus an incident plane wave to a diffraction-limited focal spot a distance $f$ after the metasurface is given by a hyperbolic phase function [Khorasaninejad et al. 2016]:

$$\theta(p') = \frac{2\pi}{\lambda} \left( f - \sqrt{p'^2 + f^2} \right).$$ (26)
The resulting intensity distribution at the sensor should then match that prescribed by the Airy disk:

\[ I(\rho) = \left( \frac{2J_1(\chi)}{\chi} \right)^2; \chi = kR \sin \left( \frac{\rho}{\sqrt{f^2 + \rho^2}} \right) \]  

(27)

where \( J_1 \) is the Bessel function of the first kind of order one and \( R \) is the radius of the circular aperture on the metasurface. The results of this analysis are shown in Figure 18 with additional details in Appendix B. We find good agreement between the theoretical Airy profile and the computed intensity at the sensor for metalenses with different ratios of \( R/f \) and using all four implemented propagators. When the ratio is larger than 0.3 (NA=0.29), the Fresnel approximation breaks down and as expected, only the ASM method is accurate.

While the required phase profile for focusing with a metasurface is known a priori, we can instead combine the auto-differentiable optical layer and the propagator layer and probe by inverse design the metasurface \( \Pi \) that the framework discovers for focusing light of a single wavelength. Due to memory limitations in utilizing the physical model as the optical layer for 2D calculations, we inverse design a radially-symmetric metasurface with the objective function:

\[ \arg \max_{\Pi, \Theta} \sum_{x', y'} P(y) \left( u(x', y', 0^-)M(\Pi, \Theta) \right) \delta(x = 0, y = 0). \]  

(28)

\( P(\cdot) \) denotes application of the propagator layer, here chosen to be the radial Fresnel method, \( x \) and \( y \) denotes coordinates on the sensor plane, and \( \Theta \) corresponds to the incident, linear polarization states. In other words, we seek to maximize the intensity of the field measured at the center pixel of a photosensor. The results of this optimization are displayed in Figure 7. For the metasurface, we consider the placement of nanofin cells and utilize both the RCWA physical model and the neural optical model. Although not done here, \( \Theta \) can be readily expanded to include incident wavelength for the inverse design of an achromatic focusing metasurface (all the models introduced in this work are broadband and the propagator layer calculations are efficiently batched over wavelength).

While nanofins generally produce polarization sensitive metasurfaces, the optimization in both cases learns to create a mostly polarization insensitive device by selecting only square nanostructures (\( w_x = w_y \)). The optimized phase profiles imparted by the designed metasurfaces are found to closely match the theoretical focusing profile in Equation 26 (Figure 7a). Moreover, although only the intensity at the central pixel was maximized, the intensity distribution across the rest of the photosensor is found to converge to the shape of the analytic Airy disk (Figure 7b), demonstrating that the learning framework is physically consistent. Almost all energy that is incident on the metasurface is focused at the photosensor, although the peak intensity is slightly less than that predicted by the Airy disk since the transmittance of the placed cells are less than unity.
The inverse-designed metasurface has a slightly better energy efficiency than that obtained by a metasurface forward-designed to implement the hyperbolic phase profile by dictionary look-up due to interpolation.

4 DEMONSTRATION

In this section, we demonstrate via simulation the usage of D♭ to co-optimize a metasurface Π in conjunction with a post-capture processing algorithm for two important visual sensing applications, incoherent opto-electronic image processing and snapshot depth sensing. Both applications exploit an optical setup similar to that depicted in Figure 7a.

A multifunctional metasurface produces two, unique PSFs carried on two orthogonal, linear polarization states (0° and 90°). A linear polarization-mosaicked photosensor, e.g., the SONY IMX264MZR photosensor, is then modeled to simultaneously capture the two images, I₀ and I₉₀, formed by the optics. For simplicity, we consider incident light of a single wavelength, λ = 532 nm; the simulations can be readily repeated for the broadband case. The width w of each metasurface cell is chosen to be 350 nm, consistent to the trained neural optical models discussed in this work. We assume that the energy of 0° and 90° polarized light are the same in the incident field, which can be enforced in practice by adding a 45° linear polarizer in front of the metasurface. The two rendered images, I₀ and I₉₀, are fed into different post-capture processing algorithms depending on the application. We use D♭ to differentiably model the optics and algorithm, and to jointly optimize the metasurface shape and the algorithmic parameters according to the objective function defined for each task.

4.1 Single-Shot Incoherent Image Processing

In the optics community, there has been a long and rich history of designing optical systems for image processing [Lee 1981]. Numerous systems have been proposed and demonstrated for applying spatial frequency filters on a field, such that the captured image corresponds directly to a processed or spatially-differentiated rendering of the scene without any digital operations required

[5Kwon et al. 2018; Zhou et al. 2019, 2020]. Notably, these purely optical filtering methods all require that the scene is illuminated by coherent rather than incoherent light. This fundamental restriction can be understood by considering that an imaging system whose output is the derivative of the in-focus, incoherent image would require an intensity PSF with both positive and negative values—a condition which can not occur. Physically, the restriction is equivalent to the fact that the removal of signal cannot be achieved optically by destructive interference with incoherent addition of fields.

To circumvent this limitation, we propose a new method based on extending the opto-electronic theory of two-pupil synthesis [Chavel and Lowenthal 1976; Lohmann and Rhodes 1977] to metasurfaces. The theory proposes that the removal of signal required for general spatial frequency filtering operations may be done digitally via the pixel-by-pixel subtraction of two images, captured on two co-designed optical systems. The benefit is a potentially substantial reduction in computational cost for image processing while the downside in practice stems from difficulties with photon noise. By leveraging the polarization-dependent optical response of the metasurface cells, the two required optical systems can be realized with a single optical component and more over, the two distinct images can be captured from the same perspective.

The net image which results from the digital subtraction of the two captured images, I₀ and I₉₀, may be given via:

\[ I₀ - αI₉₀ = T * (f₀ - αf₉₀) = T * f', \quad (29) \]

where T is an all-in-focus, magnified image of the scene, commonly referred to as a pinhole image. f₀ and f₉₀ are the two PSFs which form I₀ and I₉₀. All I, T, and f are functions of the detector spatial coordinate (x, y), over which the convolution ∗ is applied. The coefficient α is introduced as a scalar constant that can be digitally applied and accounts for differences in total transmitted energy between the two PSFs. While each intensity PSF produced by the polarization multiplexed metasurface is individually positive, the digitally subtracted image corresponds to an effective PSF f(x, y) which may be positive and negative. In this sense, the digital output of the opto-electronic system can provide a spatially filtered or differentiated rendering of the scene for just two FLOPs per pixel. Moreover, given the checkerboard-mosaicced structure of the linear polarization filters at the photosensor, the scalar multiplication and the digital subtraction of the neighboring pixels signal can theoretically be done by analog circuitry enabling incoherent image differentiation without any digital, post-processing operations for the first time.

While f' may be correlated directly to convolutional kernels that one may apply digitally, identifying the optics which realizes a given f' is an inverse-problem that has no simple, analytic solution [Jahns and Lohmann 1982; Mait 1987; Mait and Rhodes 1989]. Instead, we use D♭ to learn an optimal metasurface Π and scalar α for different filters and to design the functionality to be depth-invariant over a reasonable working range. To optimize the system, we require as an input the labeled data pair (S_k, Z_k), where S_k is a series of fronto-planar scenes at different depths and Z_k is the corresponding, filtered image. The optimization is then done for a single wavelength by minimizing the L2 loss, starting from the initial condition of a uniform metasurface:

\[ \arg\min_{Π,α} \sum_k \| (I₁(S_k) - αI₂(S_k)) - Z_k \|^2 \]

\[ I₁(S_k) = \text{render}(S_k, M(Π, Θ), P), \quad Θ \in \{0°, 90°\}. \quad (30) \]

We utilize this approach to design a metasurface-based opto-electronic system which produces in the net image a first-derivative rendering of the scene. For this example, we utilize a nanofin neural optical model and the 2D Fresnel integral propagator, and design the 1.5 mm diameter metasurface shown in Figure 8a. The labeled training data consists of a scene corresponding to the displayed pinhole image and its first derivative along x, obtained by convolution with the 3x3 Sobel kernel (Figure 8b,c). To enable depth invariant operation, we use the same labeled pair for three scene distances between 0.5 and 1.0 m in front of the metasurface. This optimization is carried out on a single, desktop Quadro RTX 4000 GPU using an
Adam optimizer with a fixed learning rate of $1e^{-3}$ and took approximately 40 minutes to train. We find that the net image produced by the co-designed metasurface matches well with the true first derivative (Figure 8c).

The PSFs $f_0^\circ$ and $f_{90^\circ}$ for this optimized metasurface along with the net PSF $f' \circ$ for the opto-electronic system is displayed for a scene depth of 0.75 m in Figure 9a. Notably, the net PSF learned by the optimization is antisymmetric with negative values in the left half and positive values on the right, matching the structure of the Sobel kernel that was used to generate the labeled data but was otherwise hidden to the optimizer. This suggests that the learned system can perform image differentiation to arbitrary scenes even when trained on a single example. Moreover, we find that the net PSF is largely depth invariant over the trained range (9b,c), facilitating usage in real-world applications.

The learned functionality can also be better understood by examining the optical transfer function (OTF) of the system, the frequency-space analogue of the PSF. A review of the OTF is given in Appendix C with the OTF for the system displayed in Figure 19. Here, we find that the transfer function of the optimized, opto-electronic system matches the definition of the first derivative (up to a proportionality constant) for a range of spatial frequencies about $f_x = 0$. Disagreement occurs for high spatial frequency components and is unavoidable given the finite frequency bandwidth of the optics. This limitation introduces the error seen for the squares in Figure 8c; however, the accuracy of the operation can be improved by designing a metasurface with a larger diameter.

Extending from the previous discussion, we also show that the RCWA physical model may be used as the optical layer to solve a similar image processing problem but with a higher dimensional cell parameterization of $D = 8$. Using the same objective function of Equation 30 but re-targeted to a labeled training data pair corresponding to a second derivative, we optimize the radially symmetric metasurface shown in Figure 10a,b. The ground-truth, differentiated image is obtained by convolving the pinhole image with the 3x3, discrete Laplacian kernel. Rather than simple nanofins, we consider the placement of four ellipses in each cell, with each ellipse having a trainable major and minor axis length. The physical model then solves Maxwell’s equations at each cell and for each training step and the auto-differentiable framework yields the gradients of the loss with respect to the shape parameters. A standard Adam optimizer with a fixed learning rate of $1e^{-2}$ is used and the training takes approximately 40 minutes on the same desktop GPU.

In panel (c), the pinhole image used to train the metasurface (an image of a binary Siemens star) is displayed alongside the two photosensor images and the net image produced by the optimized opto-electronic system. To highlight the generality, panel (d) displays the simulated results for a test image. In both cases, we again find good agreement and observe that the metasurface-based imaging system learns to work in conjunction with the simple algorithm...
Fig. 10. The RCWA physical model is coupled with the radial propagator and renderer to optimize a metasurface which enables capture of the second-derivative of a scene. (a) The corresponding phase modulation imparted by the optimized $\Pi$. A different phase delay is experienced for $0^\circ$ and $90^\circ$ linearly polarized light. (b) A top-down view of the optimized cells at select radial locations along the lens. (c) The pinhole image used for training is shown alongside simulations of the images produced by the metasurface and captured on the photosensor. The subtraction of the two images is done digitally post-measurement. (d) Same as c, but for an unseen test image.

Fig. 11. (a) Schematic depiction of the computational imaging architecture for single shot depth sensing. A metasurface produces two distinct, optical responses on two, linear orthogonal polarization states. The two images of the scene are formed and measured on the polarization mosaicked photosensor pixels. The distance between the metalens and the photosensor is set to 40 mm. The two images are then passed to a U-net which produces a depth map of the scene. (b) The U-net architecture used in this work. Rectangles denote 2D dense convolutional layers with 3x3 kernels, a ReLu activation function, and channel depth denoted by the overlaid number. Down arrows between blocks utilize a 2x2 maxpooling while the up arrows denote 2x2 upsampling.

4.2 Single-Shot Depth Sensing

In this section, we leverage the efficiency of the proposed neural optical model to enable the co-optimization of a millimeter scale metasurface with the parameters of a deep neural network for single-shot depth sensing. To the best of our knowledge, an optimization of this type has not been done previously with metasurface-based optics. For both optimization scenarios discussed here, we find that the framework is able to learn the underlying image filter by only looking at a single example.

We note that the co-design of a DOE with similar neural network architectures for depth sensing has been explored previously in [Ikoma et al. 2021; Wu et al. 2019].

schematically depicted in Figure 11a. The working principle of this camera is based on depth-from-defocus (DfD). The metasurface forms two images, $I_0$ and $I_90$, at the photosensor, each with a distinct depth-dependent blur. The pair of images are then fed into a U-net which outputs a depth map of the scene.

While it is possible for a sufficiently expressive U-net to generate depth predictions based on learned object statistics rather than cues from optical defocus, we encourage the latter by limiting the receptive field of the network. The receptive field size defines the number of pixels in the input image which are used to generate a depth prediction for each pixel at the output. The U-net architecture considered in this work is shown in Figure 11b and utilizes 3x3 kernels throughout. The receptive field size is shown in the inset of Figure 12b. As the receptive field is small relative to the features in the image, we hypothesize that the U-net will be constrained to generate predictions based primarily on defocus. Notably, we emphasize that depth from defocus can be realized utilizing a single, 2D image as the input. Previous work on monocular depth estimation (MDE), however, have utilized neural network architectures with substantially more parameters (here, the network contains only 1.94 M parameters) and with a larger receptive field [Alhashim and Wonka 2018; Eigen et al. 2014; Liu et al. 2016]. In consideration of a smaller computational architecture, we are motivated to utilize the capabilities of metasurfaces to encode two distinct PSFs simultaneously given recent demonstrations of a low computation,
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Fig. 12. Single shot depth sensor utilizing the co-design of a metasurface and a U-Net. The simulated system simultaneously captures two differently blurred images (a,b) of a scene using the setup in Figure 11. It then processes the two images using a U-Net, which outputs the predicted depth map (c) of the scene. The receptive field of the U-Net (orange box in (b)) is relatively small compared to the scale of image features, thus the network has to infer depth from local features such as image defocus, instead of from global, semantic features. During training, the metasurface cells are jointly optimized with the U-Net parameters. The PSFs of the system before and after the optimization at a sample depth is shown in (e). A 2D histogram of the predicted depth vs true depth on the 50 image testing set is displayed in (f).

Fig. 13. The simulated, initial (top) and trained (bottom) PSFs for the metasurface used in the depth sensor, for five depth values within the optimized range.

Deterministic depth-from-differential-defocus algorithm based on two images [Alexander et al. 2016; Guo et al. 2019]. For constrained neural architectures, co-optimization based on two images should outperform single image estimates.

Using the nanofin neural optical model and the Hankel-based radial Fresnel propagator, we inverse-design a 3 mm diameter, radially-symmetric metasurface in conjunction with the U-Net parameters. The metasurface is initialized to focus light from depths of 0.3 m and 0.5 m at the photosensor for 0° and 90° linearly polarized light, respectively. For the optimization, we generate randomly synthesized scenes with the foreground and segmentation masks assembled from the Freiburg-Berkeley motion segmentation dataset [Ochs et al. 2014] and the background from the COCO dataset [Lin et al. 2014]. Ground-truth depth maps consist of slanted planes. With both the scene and true depth as model inputs \( \{(S_k, Z_{true,k})\}_{k=1,2,...} \), we utilize a training set of approximately 5000 scene-depth pairs and minimize the L1 loss via,

\[
\arg \min_{\Pi,\Psi} \sum_k \|\text{U-Net}(I_0(S_k), I_{90}(S_k)) - Z_{true,k}\|,
\]

where \( I_i \) is a polarization-dependent, rendered image similar to Equation 30 but utilizing the accelerated, slanted-plane depth rendering algorithm discussed in Section 2.3. Photon noise is added to the captured images [Hasinoff 2014].

In Figure 12, we display the simulated performance of the optimized snapshot depth sensor for a test scene. The two predicted images produced by the metasurface (displayed in images a,b in the same figure) are in focus for different depths. The U-net successfully learns to recover a depth map of the scene based on the two image input, and in Figure 12f, we show a 2D histogram of the depth estimation performance across the test set containing 50 scenes. Across the optimized depth range, we find good performance.

The initial and trained PSFs for the two polarization states are shown in Figure 13 (the PSF for one depth is extracted and magnified in Figure 12e). Remarkably, we observe that while the PSFs do change during training, the differences are relatively subtle. This suggests that the U-net architecture considered here, although relatively small compared to traditional MDE architectures, is still powerful enough to work in conjunction with the optics without having to depend heavily on finely-tuning the PSFs. Moreover, we believe that yet smaller and simpler neural architectures may be utilized in conjunction with two images and may be needed to realize the full potential of co-optimization rather than co-design for DfD with metasurfaces.
5 CONCLUSION AND FUTURE OUTLOOK

In this work, we present a complete and auto-differentiable design framework for the co-optimization of metasurfaces and computational algorithms. We provide multiple, efficient and validated implementations for all stages of the design pipeline: field propagation, metasurface optical transformations, and rendering. While part of this work’s contribution is the coherent synthesis and integration of prior research (some disjoint to the topic of metasurfaces), we also introduce the principle of the neural optical model—the usage of a multilayer perceptron to differentiably map nanoscale shapes to their local optical response. We discuss in detail the benefits of the neural optical model as an implicit representation, relative to auto-differentiable field solvers, and benchmark the performance against alternative approaches. We find that the neural optical model yields state of the art accuracy while being highly generalizable; consequently, it enables a new path forward for end-to-end metasurface design.

In addition to the neural model, we also propose two new, theoretical metasurface-based computational imaging systems and demonstrate the usage of the framework to train them. We leverage the polarization multiplexing ability of a metasurface to capture two images in a single shot and from the same perspective, a feat which cannot be easily done with a single optic by other means. We then utilize this functionality to demonstrate a path for compact, incoherent opto-electronic image processing based on two-pupil synthesis and for efficient depth sensing based on a small receptive field U-net and depth from differential defocus.

The source code for the framework is released as an open source package to the community, in addition to pre-trained, ready-to-use neural models. We believe that there is substantial room for further explorations and demonstrations including extending the MLP approach to higher dimensional cell shapes. New and specialized, adaptive sampling algorithms will likely be needed in order to efficiently generate the required training data for the MLP, as pre-computing the optical response for all parameter combinations will be infeasible for complicated cells. Moreover, the simple cell libraries utilized in this work enabled a straightforward method to impose constraints on the metasurface parameters. The development or implementation of alternative techniques is needed when the allowed values for the MLP inputs are conditional on one another. Previous research on dispersion engineering suggests that these higher dimensional cells are required in order to more freely engineer the optical response with respect to incident wavelength [Chen et al. 2018; Li et al. 2021].

While co-optimization of optical hardware and computational parameters is not a new idea, it is our opinion that the development of co-designed metasurface based systems remains in a nascent stage. The potential in applying end-to-end design of multiple images alongside modern and emerging techniques in image processing may likely continue to lead to the discovery of vision systems with substantially reduced computational costs.

Table 2. Performance Per Cell Evaluation for All Surrogate Models

| Optical Model       | # Parameters | FLOPs | MAE Test Set |
|---------------------|--------------|-------|--------------|
| Poly-14-cylinder    | 360          | 717 k | 0.18         |
| Poly-17-cylinder    | 513          | 1.02 k| 0.14         |
| Poly-23-cylinder    | 900          | 2.3 k | 0.095        |
| Poly-30-cylinder    | 1.40 k       | 5.38 b| 0.082        |
| ERBF-32-cylinder    | 0.2 k        | 4.36 k| 0.074        |
| ERBF-64-cylinder    | 0.4 k        | 513 k | 0.047        |
| ERBF-128-cylinder   | 0.9 k        | 1.8 k | 0.029        |
| ERBF-256-cylinder   | 1.8 k        | 5.38 k| 0.026        |
| ERBF-512-cylinder   | 3.6 k        | 0.97  | 0.029        |
| NO-D32-cylinder     | 1 k          | 2.8 k | 0.074        |
| NO-D64-cylinder     | 5 k          | 10 k  | 0.019        |
| NO-D128-cylinder    | 17 k         | 36 k  | 0.024        |
| NO-D256-cylinder    | 68 k         | 138 k | 0.018        |
| Poly-5-fins         | 336          | 666   | 0.20         |
| Poly-8-fins         | 990          | 1.97 k| 0.13         |
| Poly-11-fins        | 2.18 k       | 4.36 k| 0.09         |
| Poly-15-fins        | 4.90 k       | 9.8 k | 0.069        |
| ERBF-128-fins       | 1.5 k        | 3 k   | 0.062        |
| ERBF-256-fins       | 3 k          | 7 k   | 0.040        |
| ERBF-512-fins       | 6 k          | 14.0k | 0.036        |
| ERBF-1024-fins      | 12 k         | 28 k  | 0.032        |
| ERBF-2048-fins      | 25 k         | 55 k  | 0.026        |
| NO-D32-fins         | 1 k          | 3 k   | 0.068        |
| NO-D64-fins         | 5 k          | 10 k  | 0.047        |
| NO-D128-fins        | 18 k         | 37 k  | 0.035        |
| NO-D256-fins        | 68 k         | 139 k | 0.025        |
| NO-D512-fins        | 267 k        | 540 k | 0.021        |
| NO-D1024-fins       | 1.05 m       | 2.18 m| 0.019        |
| RCWA-(512², 49)     | NA           | 363 m | 0.062        |
| RCWA-(512², 81)     | NA           | 1.62 b| 0.055        |
| RCWA-(512², 121)    | NA           | 5.38 b| 0.051        |

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A NEURAL OPTICAL MODEL ADDITIONAL INFORMATION

In this section, we provide additional figures for the evaluation and analysis of the neural optical model. Discussion is provided in the main text. In Figure 14 and 15, the transmission and phase predictions for x- and y-polarized light incident on a 350 nm cell with a centered nanofin structure is displayed for several trained neural optical models along with the alternative ERBF and multivariate polynomial models. In Figure 16, predictions on the nanocylinder cells are shown against the FDTD computed optical response. The mean absolute error, FLOPs, and number of parameters of all models tested in this work (some not visually shown in the figures) are listed in Table 2.

B PROPAGATED FIELD VALIDATION

As introduced in Section 3.2 of the main document, we present one validation for the field propagators included in D by analyzing
the intensity produced at the focal plane of various metasurfaces (metasurfaces which are designed to focus light as diffraction-limited lenses). We consider a field just after the metalens, assuming plane wave incidence, according to the hyperbolic phase profile introduced in Equation 26 of the main text:

\[ u(\rho', 0^+) = \exp \left( -\frac{j2\pi}{\lambda} \left( f - \sqrt{\rho'^2 + f^2} \right) \right) \]  

(32)

where \( f \) is the focal length and \( \rho' \) denotes radial coordinates on the metasurface plane, \( \rho' = \sqrt{x'^2 + y'^2} \). In this analysis, we assume
that the metalens implements the required phase-delay at each cell exactly and without modulating the field intensity; In other words, we consider only the propagation of this ideal field to the sensor plane. In the main text of Section 3.2, this assumption is eased when the metasurface is inverse designed to discover the placement of nanofin cells that focus light.

Here, we consider the field on a grid after a 100 μm diameter metalens with square cells of 350 nm. The grid at the sensor plane is finely sampled at 50 nm. We consider instantiations of metalenses that are designed to focus light at sensor distances of 100, 150, and 200 μm and for incident wavelengths λ of 380, 532, and 700 nm, respectively. The intensity at the sensor plane for each case is then computed and a central slice through the intensity profiles are shown in Figure 18. These sensor distances are chosen as they correspond to different values of the imaging numerical aperture, NA = r/f, where r is the radius of a circular aperture on the metalens. The NA is a useful metric as it relates to the range of angles over which the system operates. Moreover, it is understood that the Fresnel approximation (one assumption of paraxial optics) breaks down for large NA values. In this regime, we expect only the angular spectrum method (ASM) to produce the correct, propagated fields.

The calculations in Figure 18 are plotted alongside the theoretic Airy disk profile. We find good agreement between the theoretic Airy intensity and the propagated fields. For NA larger than 0.30, the Fresnel approximation becomes less accurate while the radial and 2D ASM calculations are still in strong agreement.

C INCOHERENT IMAGE DIFFERENTIATION ADDITIONAL DETAILS

To better understand the spatial frequency filter imposed by the metasurface based system, it is useful to consider the optical transfer function (OTF). By taking the Fourier transform of both sides of Equation 29 in the main text, we obtain the frequency-space relation:

\[ \mathcal{F}(\bar{I}_0) = T \cdot \mathcal{F}(I - \alpha f_0) = \mathcal{T} \cdot \mathcal{F}(f') , \]  

(33)

where \( \mathcal{T} \) and \( \mathcal{F} \) denotes the Fourier transform of \( I \) and \( T \) respectively. The significance of this representation is that it reveals that the frequency content in the captured images \( I \) corresponds to the frequency content in the pinhole image \( T \) modulated by a spatial frequency filter. This spatial frequency filter is the Fourier transform of the PSF and is referred to as the optical transfer function (OTF) by convention. Just as we assign an effective, net PSF \( f' \) to the
Fig. 16. MLP-predictions for the transmittance (top row) and phase (bottom row) imparted by a 180 nm cell with 600 nm tall nanocylinders of different radii placed at the center (as depicted in Fig. 1b of the main document). The FDTD optical response is shown along with different, pre-trained neural optical models labeled as Dense-N; the models consists of two hidden, dense layers with N neurons in each. As with the nanofins, we find a continuous trade-off between model accuracy and number of parameters (see Table 1 in the main document for quantitative measures).

Fig. 17. Complementary to Figure 6 in the main document. The predicted intensity and phase of the field at the sensor plane is computed with D-♭ using (a) the angular spectrum method and (b) the Fresnel diffraction method. In (c), the experimental measurements taken by Lim et al. and published in [Lim et al. 2021] are shown. Four different metasurface to sensor distances are considered.

![Image](image-url)

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opto-electronic system, we may define an effective, net OTF via:

$$\text{Net OTF} = F(f')$$.

The operation of image differentiation is well defined in frequency space as it corresponds to a particular, complex-valued spatial frequency filter. We may then compare the net OTF of the optimized system to this ideal filter.
The net PSF and the net OTF for the optimized imaging system that applies a first derivative to the pinhole image (section 4.1) is displayed in Figure 19. As noted in the caption, the OTF is consistent to the definition of a first derivative for low spatial frequencies. Disagreement will always occur at high frequencies and this can be understood by recognizing that any physical, optical system must have a high spatial frequency cut-off. This cutoff may be set by the pixel size or by the diffraction-limit and sufficiently high frequency components in a scene cannot be imaged. In other words, the OTF must go to zero for high frequencies. The net PSF and the net OTF for the second-derivative imaging system is similarly displayed in Figure 20.

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Fig. 18. See the text in Appendix B for more details. Each graph in the figure corresponds to a different metalens instantiation, which imparts the hyperbolic phase profile required to focus an incident plane wave of a particular wavelength λ to a particular sensor distance. A radial slice of the intensity profile at the sensor plane is shown, as computed by the four propagators included in Db. The analytic intensity profile prescribed by the Airy disk is also plotted in red. The simulated calculations should match closely to the Airy profile with disagreement only for the Fresnel method at large NA.
Fig. 19. The net PSF $f'$ for the optimized imaging system introduced in section 4.1 (Figure 8) of the main text is reproduced. This effective PSF results in the first-derivative image of a scene and corresponds to an object to metasurface distance of 0.75 m. To the right, we show the real and imaginary parts of the OTF obtained by taking the Fourier transform of $f'$. Notably, there is zero modulation transfer for the zero-spatial frequency component. For a small range around $f_x = 0$, the real part is approximately linear while the imaginary part is anti-symmetric, consistent to the definition of the first derivative.

Fig. 20. (a) Enlarged images of the pinhole image and the net image from Figure 10 in the main document. The metasurface visual system enables a second-derivative rendering of the scene for two FLOPs per pixel. (b) The two PSFs for the optimized metasurface are shown alongside the effective, net PSF $f'$. The discovered effective PSF has a similar shape to the conventional Laplacian of Gaussian kernel used for edge-detection. (c) The real part of the net OTF is shown. The imaginary part of the OTF is approximately zero for all spatial frequencies. The real part of the net OTF has an approximately quadratic shape near $f_x = 0$. These features are consistent to the frequency definition of a second derivative.

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