The Effect of Hyperbolic Two-temperatures Model on Waves Propagation in a Semi-conductor Medium Containing Spherical Cavities

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The effect of hyperbolic two-temperatures model on waves propagation in a semi-conductor medium containing spherical cavities
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Abstract
This article is interested in the study of the carrier density, the redial displacement, the conductive temperature, thermodynamic temperature and the stresses in a semi-conductor material containing a spherical hole. This investigation deals with the photo-thermo-elastic interactions in a semi-conductor medium in the context of the new hyperbolic two-temperatures model with one relaxation time. The Laplace transform technique are used to obtain the problem analytical solution by the eigenvalues methods and the inversions of the Laplace transform were performed numerically. Numerical results for semi-conductor materials are shown graphically and discussed.

Keywords: Laplace transforms; spherical cavity; thermal relaxation time; hyperbolic two-temperature; eigenvalues approach.

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Nomenclature
\begin{align*}
T &= T^* - T_o, T^* \quad \text{the variations of temperature} \\
T_o & \quad \text{the reference temperature} \\
t & \quad \text{the time} \\
u_i & \quad \text{the displacement components} \\
\rho & \quad \text{the density of material} \\
c_e & \quad \text{the specific heat at constant strain,} \\
\tau & \quad \text{the lifetime of photo-generated carrier,} \\
N &= n - n_o, n_o \quad \text{the carrier concentration at equilibrium,} \\
\gamma_n &= (3\lambda + 2\mu)d_n, d_n \quad \text{the electronic deformation coefficient,}
\end{align*}
\[ k = \frac{\partial n_o}{\partial T} \]  
the coupling parameter of thermal activation

\[ K \]  
the thermal conductivity

\[ \gamma_t = (3\lambda + 2\mu)\alpha_t, \alpha_t \]  
the linear thermal expansion coefficients

\[ \sigma_{ij} \]  
the components of stresses,

\[ D_e \]  
the carrier diffusion coefficient,

\[ \lambda, \mu \]  
the Lame's constants,

\[ T_1 \]  
the constant temperature

\[ \tau_o \]  
the thermal relaxation time

\[ q_o \]  
constant

\[ t_p \]  
the pulsing heat flux characteristic time

\[ s_b \]  
the speed of recombination on the surface

\[ R \]  
the internal radius of cavity

**Introduction**

The theory of thermoelasticity, which is the most common engineered structural material, plays an important role in steel stress analysis and applied mechanical science. It can describe the solid mechanical behavior of some common elastic materials like coal, concrete and wood. However, it cannot describe the mechanical behavior of many synthetic materials of polymer and elastomer type such as polyethylene. The temperature increment of body is not only caused by internal and external heat sources, but also by deformations of itself process during the micro-inertia of the microelement. In the first half of the last century, many authors used the theory of generalized thermoelasticity to describe elastic and thermal waves in elastic materials such as semiconductors (semi-insulating). In this case, semiconductor materials have been studied as an elastic support only. But at the end of the last century, various scientists studied semiconductor materials in particular their internal structures during microelectronic processes.

Biot [1] developed the coupled thermoelasticity theory (CD theory) when motivated the law of Fourier heat conduction that became appropriate for modern engineering applications spicily in high temperature case. But in low temperature case, the thermoelastic models are physically unacceptable and cannot obtain equilibrium state. Lord et al. [2] (LS) inserted one relaxation time in the heat conduction equation (Fourier’s law of heat conduction) to overcome this contradiction. The thermo-elasticity model with classical two-temperatures are presented by and Chen et al. [3],
Chen and Gurtin [4] and Williams and Gurtin [5], by using another depending on the classic two-temperature (the conductivity temperature $\phi^*$ and the thermodynamically temperature $T^*$).

Recently, Youssef et al. [6] investigated a new model in generalized thermoelasticity theory when they introduced the theory of hyperbolic two-temperature. Taye et al. [7] studied the hyperbolic two-temperature semiconductor thermoelastic wave by laser pulses. Saeed and Abbas [8] studied the hyperbolic two-temperatures photothermal interaction in a semi-conductor medium. Abbas et al. [9] discussed the hyperbolic two-temperature photothermal interactions in a semi-conductor material with a cylindrical cavity. Lotfy et al. [10] investigated the effect of variable thermal conductivity of a semiconducting medium with cavities under the fractional-order magneto-photothermal model. Lotfy et al. [11] investigated the response of Thomson and magnitic impact of semiconducor material due to laser pulses under photothermoelastic theory. Hobiny and Abbas [12] investigated the photothermal interaction in a two-dimension semi-conductor plane under the GN model. Ali et al. [13] studied the reflections of wave in a rotating semi-conductor nanostructure material through torsion-free boundary conditions. Yasein [14] discussed the influences of variable thermal conductivity of semi-conductor medium under photothermal model due to thermal ramp type. Lotfy et al. [15] discussed the Thomson and electromagnetic effects under the photo-thermal model of a rotator semiconductor materials with hydrostatic initial stress. Alzahrani and Abbas [16] studied the photo-thermoelastic interaction in a semi-conductor plane without energy dissipations. Abbas and Hobiny [17] used the finite differnce method to study the photothermal interaction in simecondactor medium. Youssef and El-Bary [18] studied the characterization of the photo-thermal interactions of a semiconductor solid sphere due to the fractional deformations, the thermal relaxation times, and various references temperature under L-S model. Lotfy et al [19] the photo-thermal excitations process during hyperbolic two-temperature model for magneto-thermo-elastic semiconductor material. Hobiny and Abbas [20] investigated the photo-thermal wave in an infinite semi-conductor medium containing cylindrical hole. Many authors [21-36] solved several problems by using numerical and analytical approaches for thermal and elastic waves.

This work is devoted to an investigate of the analyticcal solutions of photothermal interaction in semi-conductor mediums with a spherical hole under the new hyperbolic of two-temperatures thermo-elasticity. The effect of the two-temperature parameter on the thermodynamic and the
conductive temperatures, the stress, the radial displacement and the carrier density distributions have been depicted graphically.

**Basic equations**

In this article, theoretical dissuasions during the heat transport process when the internal structure of the semi-conductor is taken into consideration. The interactions between thermal and elastic waves of the plasma are generated in the context of the own temperature (both hyperbolic temperatures). The governing equations under photo-thermal model with the hyperbolic two-temperatures in semiconductor medium can be given by [6, 37, 38]:

The equations of motion:

\[ \mu u_{i,j} + (\lambda + \mu)u_{j,i} - \gamma_T N_i - \gamma_e T_i = \rho \frac{\partial^2 u_i}{\partial t^2}. \]  

(1)

The coupling between thermoelastic and plasma waves can be expressed as

\[ D_e N_{i,j} - \frac{N}{\tau} + \frac{k}{\tau} T = \frac{\partial N}{\partial t}. \]  

(2)

The equation of heat conduction

\[ K \phi_{i,j} = \left( 1 + \tau \frac{\partial}{\partial t} \right) \left( \rho c_e \frac{\partial T}{\partial t} + \gamma_T T \frac{\partial u_i}{\partial t} \right). \]  

(3)

The new hyperbolic of two-temperature relation

\[ \dot{\phi} - \ddot{T} = a \phi_{i,j}. \]  

(4)

The stress-strain relations are expressed as

\[ \sigma_{ij} = \mu \left( u_{i,j} + u_{j,i} \right) - \left( \gamma_T N + \gamma_e T - \lambda u_{k,k} \right) \delta_{ij}. \]  

(5)

Let us consider a homogeneous, isotropic unbounded semi-conductor medium containing a spherical hole, whose state can be expressed in terms of the space variable \( r \) and the time \( t \) which occupying the region \( R \leq r < \infty \). The radial displacement \( u_r = u(r,t) \) non-vanishing only due to symmetry, hence the equations (1)-(5) can be rewritten by:

\[ (\lambda + 2\mu) \left( \frac{\partial^2 u}{\partial r^2} + \frac{2}{r} \frac{\partial u}{\partial r} - \frac{u}{r^2} \right) - \gamma_T \frac{\partial T}{\partial r} - \gamma_e \frac{\partial N}{\partial r} = \rho \frac{\partial^2 u}{\partial t^2}, \]  

(6)

\[ D_e \left( \frac{\partial^2 N}{\partial r^2} + \frac{2}{r} \frac{\partial N}{\partial r} \right) = \frac{\partial N}{\partial t} - \frac{k}{\tau} T + \frac{N}{\tau}. \]  

(7)

\[ K \left( \frac{\partial^2 \phi}{\partial r^2} + \frac{2}{r} \frac{\partial \phi}{\partial r} \right) + \frac{E_e}{\tau} N = \left( 1 + \tau \frac{\partial}{\partial t} \right) \left( \rho c_e \frac{\partial T}{\partial t} + \gamma_T T \frac{\partial u_i}{\partial t} \right). \]  

(8)

\[ \frac{\partial^2 T}{\partial t^2} = \frac{\partial^2 \phi}{\partial t^2} - a \left( \frac{\partial^2 \phi}{\partial r^2} + \frac{2}{r} \frac{\partial \phi}{\partial r} \right), \]  

(9)

with

\[ \sigma_{rr} = (\lambda + 2\mu) \frac{\partial u}{\partial r} + \lambda \frac{2u}{r} - \gamma_T T - \gamma_e N. \]  

(10)
\[ \sigma_{\theta \theta} = \sigma_{\phi \phi} = \left( \lambda + 2\mu \right) \frac{u}{r} + \lambda \left( \frac{\partial u}{\partial r} + \frac{u}{r} \right) - \gamma_T T - \gamma_N N. \]

**Application**

The initial conditions are supposed to be homogeneous. The bounding internal surface of cavity have the boundary conditions by the following

\[ u(R, t) = 0, \]

\[ -K \frac{\partial \phi(r, t)}{\partial r} \bigg|_{r=R} = q_o \frac{t^2 e^{-\frac{t}{t_p}}}{16 t_p^2}, \]

\[ D_e \frac{\partial N(r, t)}{\partial r} \bigg|_{r=R} = S_o N(R, t). \]

To get main fields in dimensionless form, the following non-dimension variables can be used

\[ (r^*, u^*) = \eta c(r, u), \quad (\sigma_{rr}, \sigma_{\theta \theta}) = \left( \frac{\sigma_{rr}, \sigma_{\theta \theta}}{\lambda + 2\mu} \right), \quad q_o^* = \frac{q_o}{\eta c K}, \quad a^* = \frac{a}{c^2}, \]

\[ (t^*, \tau^*, \tau_o^*, t_p^*) = \eta c^2(t, t, \tau_o, t_p), \quad N^* = \frac{N}{n_o}, \quad \Phi^* = \frac{\phi}{\tau_o}, \quad T^* = \frac{T}{\tau_o}. \]

where \( \eta = \frac{\rho c_e}{K} \) and \( c^2 = \frac{\lambda + 2\mu}{\rho} \).

Using equation (15) for the main governing equations (dropping the superscript \(^*\)), yields:

\[ \frac{\partial^2 u}{\partial r^2} + 2u \frac{\partial u}{\partial r} \frac{2u}{r^2} - d_1 \frac{\partial T}{\partial t} - d_2 \frac{\partial N}{\partial r} = \frac{\partial^2 u}{\partial t^2}, \]

\[ \frac{\partial^2 N}{\partial r^2} + 2 \frac{\partial N}{\partial r} d_3 \frac{\partial N}{\partial t} + d_5 \frac{1}{r} N - d_4 T, \]

\[ \frac{\partial^2 \phi}{\partial r^2} + 2 \frac{\partial \phi}{\partial r} \frac{\partial \phi}{\partial r} = -d_5 \frac{1}{r} N + \left( 1 + \tau_o \frac{\partial}{\partial t} \right) \left( \frac{\partial T}{\partial t} + d_6 \frac{\partial u}{\partial r} + 2u \frac{\partial u}{\partial r} \right), \]

\[ \frac{\partial^2 \phi}{\partial t^2} = \frac{\partial^2 T}{\partial t^2} + a \left( \frac{\partial^2 \phi}{\partial r^2} + \frac{2}{r} \frac{\partial \phi}{\partial r} \right), \]

\[ \sigma_{rr} = \frac{\partial u}{\partial r} + d_7 \frac{2u}{r} - d_4 T - d_2 N, \]

\[ \sigma_{\theta \theta} = d_7 \frac{\partial u}{\partial r} + (1 + d_7) \frac{u}{r} - d_4 T - d_2 N, \]

\[ u(R, t) = 0, \quad \frac{\partial \phi(r, t)}{\partial r} \bigg|_{r=R} = -q_o \frac{t^2 e^{-\frac{t}{t_p}}}{16 t_p^2}, \quad \frac{\partial N(r, t)}{\partial r} \bigg|_{r=R} = d_8 N(R, t), \]

where \( d_1 = \frac{T_o \gamma_T}{\lambda + 2\mu}, \quad d_2 = \frac{n_o \gamma_n}{\lambda + 2\mu}, \quad d_3 = \frac{1}{\eta D_e}, \quad d_4 = \frac{k T_o}{n_o \eta p_e}, \quad d_5 = \frac{n_o E_o}{\rho c_e \tau_o}, \quad d_6 = \frac{\gamma_T}{\rho c_e}, \quad d_7 = \frac{\lambda}{\lambda + 2\mu}, \quad d_8 = \frac{S_o}{\eta c D_e}. \)
Laplace transform

For $G(r, t)$ function Laplace transform is defined by

$$\bar{G}(r, s) = L[G(r, t)] = \int_0^\infty G(r, t)e^{-st}dt. \quad (23)$$

Hence, the governing equations can be rewritten by

$$\frac{d^2\bar{u}}{dr^2} + \frac{2}{r} \frac{d\bar{u}}{dr} - \frac{2\bar{u}}{r^2} - d_1 \frac{d\bar{T}}{dr} - d_2 \frac{d\bar{N}}{dr} = s^2\bar{u}, \quad (24)$$

$$\frac{d^2\bar{N}}{dr^2} + \frac{2}{r} \frac{d\bar{N}}{dr} = d_3 \left(s + \frac{1}{r}\right)\bar{N} - d_4 \bar{T}, \quad (25)$$

$$\frac{d^2\bar{\phi}}{dr^2} + \frac{2}{r} \frac{d\bar{\phi}}{dr} = -\frac{d}{r} \bar{N} + (1 + s\tau_o) \left(s\bar{T} + s d_6 \left(\frac{d\bar{u}}{dr} + \frac{2\bar{u}}{r}\right)\right), \quad (26)$$

$$\bar{\phi} = \bar{T} + a \frac{d^2\bar{\phi}}{dr^2} + \frac{2}{r} \frac{d\bar{\phi}}{dr}, \quad (27)$$

$$\bar{\sigma}_{rr} = \frac{d\bar{u}}{dr} + d_7 \frac{2\bar{u}}{r} - d_1 \bar{T} - d_2 \bar{N}, \quad (28)$$

$$\bar{\sigma}_{\theta \theta} = d_7 \frac{d\bar{u}}{dr} + (1 + d_7) \frac{\bar{u}}{r} - d_1 \bar{T} - d_2 \bar{N}, \quad (29)$$

$$\bar{u}(R, t) = 0, \quad \frac{d\bar{u}(r, t)}{dr} \bigg|_{r=R} = \frac{-q_o t_p}{a(s t_p + 1)}, \quad \frac{d\bar{N}(r, t)}{dr} \bigg|_{r=R} = d_8 \bar{N}(R, t), \quad (30)$$

Differentiating equations (24), (25) and (26) with respect to $r$ and using equation (27), yields:

$$\frac{d^2\bar{u}}{dr^2} + \frac{2}{r} \frac{d\bar{u}}{dr} - \frac{2\bar{u}}{r^2} = x_{11} \bar{u} + x_{12} \frac{d\bar{N}}{dr} + x_{13} \frac{d\bar{\phi}}{dr}, \quad (31)$$

$$\frac{d^2}{dr^2} \left(\frac{d\bar{N}}{dr}\right) + \frac{2}{r} \frac{d}{dr} \left(\frac{d\bar{N}}{dr}\right) - \frac{2}{r^2} \frac{d\bar{N}}{dr} = x_{21} \bar{u} + x_{22} \frac{d\bar{N}}{dr} + x_{23} \frac{d\bar{\phi}}{dr}, \quad (32)$$

$$\frac{d^2}{dr^2} \left(\frac{d\bar{\phi}}{dr}\right) + \frac{2}{r} \frac{d}{dr} \left(\frac{d\bar{\phi}}{dr}\right) - \frac{2}{r^2} \frac{d\bar{\phi}}{dr} = x_{31} \bar{u} + x_{32} \frac{d\bar{N}}{dr} + x_{33} \frac{d\bar{\phi}}{dr}, \quad (33)$$

where

$$x_{11} = \left(s^2 - d_1 x_{31} \frac{a}{s^2}\right), \quad x_{12} = \left(d_2 - d_1 x_{32} \frac{a}{s^2}\right), \quad x_{13} = d_1 \left(1 - \frac{a}{s^2} x_{33}\right)$$

$$x_{21} = \frac{d_4}{r} \frac{a}{s^2} x_{31}, \quad x_{22} = \left(d_3 \left(s + \frac{1}{r}\right) + \frac{d_4}{r} \frac{a}{s^2} x_{32}\right), \quad x_{23} = \frac{d_4}{r} \left(\frac{a}{s^2} x_{33} - 1\right)$$

$$x_{31} = \frac{d_6 s^6 (1 + s t_o)}{(1 + s(1 + s t_o)(1 + d_6 d_1) \frac{a}{s^2})}, \quad x_{32} = \frac{d_2 s (1 + s t_o) d_6 - d_5}{(1 + s(1 + s t_o)(1 + d_6 d_1) \frac{a}{s^2})}, \quad x_{33} = \frac{s(1 + s t_o)(1 + d_6 d_1) \frac{a}{s^2}}{(1 + s(1 + s t_o)(1 + d_6 d_1) \frac{a}{s^2})}.$$

Now, it is possible to obtain the solutions of the equations (31), (32) and (33) by the eigenvalue approach proposed [39-44]. The vectors-matrix of equations (31-33) can be given by

$$DV = XV, \quad (34)$$

where $D = \frac{d^2}{dr^2} + \frac{2}{r} \frac{d}{dr} - \frac{2}{r^2}$, $V = \left[\bar{u}, \frac{d\bar{N}}{dr}, \frac{d\bar{\phi}}{dr}\right]^T$ and $X = \begin{bmatrix} x_{11} & x_{12} & x_{13} \\ x_{21} & x_{22} & x_{23} \\ x_{31} & x_{32} & x_{33} \end{bmatrix}$. 
The characteristic formulation of matrix $X$ are defined by

$$m^3 - m^2(x_{11} + x_{22} + x_{33}) + m(-x_{22}x_{33} + x_{11}x_{22} + x_{11}x_{33} - x_{21}x_{12} - x_{13}x_{31}) + x_{12}x_{23}x_{32} - x_{12}x_{22}x_{33} - x_{12}x_{23}x_{31} - x_{13}x_{21}x_{32} + x_{13}x_{22}x_{31} + x_{12}x_{21}x_{33} = 0,$$  \hspace{1cm} (35)

The eigenvalues of matrix $X$ are the three roots of equation (35) which define by the form $m_1, m_2, m_3$. Thus, the corresponding eigenvector $Y$ can be determined as:

$$Y = \begin{pmatrix} (x_{22} - m)x_{13} - x_{12}x_{23} \\ x_{23}(x_{11} - m) - x_{13}x_{21} \\ x_{22}(m - x_{11}) + x_{12}x_{21} + mx_{11} - m^2 \end{pmatrix}. \hspace{1cm} (36)$$

The solutions of equations (34) which are bounded as $r \to \infty$ can be given by

$$V(r, s) = \sum_{i=1}^{3} B_i X_i r^{-1/2} K_{3/2}(s_i r), \hspace{1cm} (37)$$

where $K_{3/2}$ is the modified of Bessel’s function of order $\frac{3}{2}$ and $n_i = \sqrt{m_i}$, $B_1, B_2$ and $B_3$ are constants can be computed by using the boundary conditions of problem. Thus, the variables solutions along $r$ and $s$ can be expressed by

$$\bar{u}(r, s) = \sum_{i=1}^{3} A_i U_i r^{-1/2} K_{3/2}(n_i r), \hspace{1cm} (38)$$

$$\bar{N}(r, s) = -\sum_{i=1}^{3} A_i N_i r^{-1/2} K_{1/2}(n_i r), \hspace{1cm} (39)$$

$$\bar{\phi}(r, s) = -\sum_{i=1}^{3} A_i T_i r^{-1/2} K_{1/2}(n_i r), \hspace{1cm} (40)$$

$$\bar{T}(r, s) = -\sum_{i=1}^{3} A_i \frac{T_i(1 - \frac{\alpha_i}{2\pi n_i^2})}{r^{1/2} n_i} K_{1/2}(n_i r), \hspace{1cm} (41)$$

Finally, Stehfest [45] numerical inversion method has been chosen as in [46] to get the numerical inversions of physical quantities.

**Numerical Results and Discussions**

To theoretically study the results obtained, the physical properties and physical constants of silicon (Si) as an elastic semiconductor material are used. The constants of silicon (Si) are used to do the numerical simulation and discussed the calculation results, the constants of Si can be given by [47]:

$\lambda = 3.64 \times 10^{10}(N)(m^{-2}), \tau = 5 \times 10^{-5}(s), n_o = 10^{20}(m^{-3}), s_o = 2 (m)(s^{-1}), T_o = 300(k), \mu = 5.46 \times 10^{10}(N)(m^{-2}), \alpha_t = 3 \times 10^{-6}(k^{-1}), d_n = -9 \times 10^{-31}(m^3), t_p = 0.5, \tau_o = 0.05,$
\[ \rho = 2330(kg)(m^{-3}), c_e = 695(J)(kg^{-1})(k^{-1}), E_g = 1.11 \text{ (eV)}, D_e = 2.510^{-3}(m^2)(s^{-1}). \]

Based on the above set of parameters, the calculations of physical variables (numerically) along the radial distance \( r \) for the generalized hyperbolic two-temperatures model and the classical two-temperatures theory are presented in figures 1–6. The numerical computational are carry out when using the above set of constants of field distributions of the basic quantities as (thermal waves (thermo-dynamical temperature distributions), the radial displacement distribution (strain wave), the radial and hoop stress which describe the mechanical waves distributions, the carrier density distribution (plasma waves). Figures 1 explain the variations of carrier density with respect to the radial distance \( r \). It is clear that it begin with its maximum values at the boundary \( r = R \) then it gradually decrease with the increasing of \( r \) until it reach to zeros. Figure 2 show the thermodynamic temperature variation with respect to the radial distance \( r \). It is observed that the thermodynamic temperature begins from the maximums values at the boundary \( r = R \) and reduces with the rising of the radial distance \( r \) until it comes to zero value. Figure 3 display the conductive temperature variations along the radial distance \( r \). It is observed that the it has maximum values at the boundary \( r = R \) after that it decreases gradually with the increasing of \( r \) to reach to zero. Figures 4 display the variation of radial displacement with respect to the radial distance \( r \). It observed that it starts from zero values which satisfy the boundary conditions then the radial displacement progressively increases up to peak values and then decreases again to reach to zeros. Figures 5 and 6 show the variations of radial and hoop stresses along the radial distance \( r \). It clear that the magnitudes of stresses started from the maximum values at the surface of cavity after that decreases rapidly as \( r \) increases to reach zero values. Finally, in compressions between the solutions, one can conclude that considering new hyperbolic two-temperatures photothermoelastic model have an important effect on the distributions of field quantities.

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**Availability of Data and Material**

There is no data or material that has been copied from elsewhere in the proposed manuscript.

**Author Contributions**
The authors have equal contribution in the paper.

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**Declarations**

The authors declare that the manuscript follows ethical standards as per the guidelines provided during manuscript submission.

**Conflict of Interest**

The authors declare that there is no conflict of interest in the proposed manuscript as far as the publication is concerned.

**Consent to Participate**

There is mutual understanding between the two authors and is a combined work.

**Consent for Publication**

The authors have full faith on the publisher hence the publisher has full right for publication as per their guidelines.

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Fig. 1 The carrier density variations versus the redial distance.

Fig. 2 The thermodynamic temperature variations versus the redial distance.
Fig. 3 The conductive temperature variations versus the radial distance.

Fig. 4 The displacement variations versus the radial distance.
Fig. 5 The radial stress variations versus the radial distance.

Fig. 6 The hoop stress variations versus the radial distance.