A novel UWB reconfigurable filtering antenna design with triple band-notched characteristics by using u-shaped coppers

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ABSTRACT
This paper proposed an UWB antenna with triple reconfigurable notch filters. By presenting there U-shaped coppers in the design, the potential triple interference in UWB applications can be rejected. Six PIN diodes are putted on the coppers to represent the OFF and ON tunable status in order to add reconfigurable characteristics to the UWB antenna. By using this ON and OFF tunable method, the current distribution of the proposed design changes and enables the antenna to have eight operation modes. The results prove that the proposed design can operate over the entire UWB frequency range (3.1 GHz to 10.6 GHz) and can filter out the target signals from the WLAN upper band (5.725 to 5.825 GHz), WLAN lower band (5.15 to 5.35 GHz) and X band frequency system (7.9 to 8.4 GHz) in one of the tunable configurations.

Keywords: Monopole antenna, Reconfigurable filtering antenna, Triple-band notched, U-shaped coppers

1. INTRODUCTION
Ultra-wideband (UWB) technology is a radio technology that has low power consumption, wide impedance bandwidth and high data rate for short-range. UWB has been integrated with many applications in other fields, for example in radar detection sensor [1], medical engineering [2], and wireless communications. Due to robustness against fading, multiple accurate positioning and low cost transceivers [3], the interest in UWB application has gained the tremendous attention from the researcher.

There are challenges in UWB technology. One of these challenges is UWB technology as reported in [4] is facing interference problem with other narrowband systems such as WiMAX (3.3 to 3.7 GHz), HiperLAN2 (5.47 to 5.725 GHz), WLAN (5.15 to 5.35 GHz, 5.725 to 5.825 GHz) and X band satellite frequency system (7.9 to 8.4 GHz).

In [5], integrating a band stop filter with the UWB antenna in separate element successfully reduces the possible interference and remove the interfering signals. In contrast, it increases complexity, loss, weight and cost of the design. Consequently, it is desirable to integrate the UWB antenna and filter into a single element to increase the performance of filtering antenna design.

Most researchers nowadays tend to integrate band rejected structure in the UWB antenna design to provide band notch characteristics and reject unwanted frequency [6], [7]. Different techniques have been introduced to obtain the band notch elements such as introducing parasitic strips near the ground plane or the radiation patch [8][9] and by cutting different shaped slots in the ground plane or the radiation patch. For example, by cutting C-shaped [10], U-shaped [11], H-shaped [12], p-shaped [13], and L-shaped slots [14]. However, the band rejection structures on the radiation patch and ground plane effect the
performance of radiation. Moreover, many techniques are studying and only fixed notched band is produced [15]-[18].

Recently, the research interest in reconfigurable filtering-antenna have increased dramatically [19], [20]. With the development of modern technology, the numbers of narrow interference communication and license bands are expanding in the UWB range band frequency. Thus, to cope with the this situation, reconfigurable become another notable aim of UWB antenna design which can be used as a normal UWB antenna and as single, dual and triple band notched [21].

This paper proposed an UWB triple reconfigurable filtering antenna. First, the proposed antenna is modified to formed the antenna with better return loss performance and able to cover all the UWB bandwidth. Then, three U-shaped coppers are inserted on the antenna to generate the band notched elements. Lastly, six PIN diode are located on the coppers which act as a reconfigurable system in this design. Eight modes of operation are produced by controlling the ON/OFF condition of the PIN diode states.

If the proposed antenna be compare with [22], it should note that the numbers of mode of design has been increase from four to eight modes. In other references [23], although they can achieve triple notched filter there are disadvantages, including only fixed notched is introduced and the size of antenna in [23] is larger than in proposed design.

Furthermore, in [24], [25], they generated single and dual reconfigurable, respectively against triple reconfigurable notched in presented design. In addition, in [26], although they successfully produced triple reconfigurable notched filter there are negative issue including produce excessive band rejection in WLAN frequency which leads to reject wanted signal. Another advantage is the proposed design is simple since only U-shaped copper are utilized compared than in [27].

### 2. ANTENNA DESIGN

Figure 1 shows the configuration of the proposed UWB antenna which is designed using a circular modified monopole antenna. The proposed antenna is mounted on Roger Duroid 5880 which has a thickness is 0.787 mm and relative permittivity is 2.2. The antenna design is fed by 50 ohm of impedance transmission line and partially ground plane printed on the lower side of the antenna. From [28]-[30], by modifying the patch and feedline of the ordinary monopole antenna, the performance gain is improved while improving the return loss characteristic. Figure 1 illustrates the structure of the proposed UWB antenna with feedline and patch modification with the optimum value in millimeter.

Figure 2 shows the simulated result of the reflection coefficient for the proposed UWB antenna design. From the result, it can be concluded that the antenna cover from 3.1 GHz to 11.21 GHz, which cover all the UWB antenna bandwidth. The propose design also provide better skirt selectivity frequency than reported in [31] which is average above -20dB.

![Figure 1. Simulated structure of antenna with feedline and patch modification of UWB antenna](image-url)
3. TRIPLE NOTCHED BAND DESIGN

In this section, we introduce three U shaped notch filter to act as a triple band rejection to reject potential interference from WLAN (5.15 to 5.35GHz, 5.725 to 5.825 GHz) and uplink of X band satellite communication system (7.9 to 8.4 GHz) in UWB frequency. In [32][33], U-shaped coppers notch filter are designed by using the (1) and (2):

\[ L = \frac{\lambda_g}{2} \]  

\[ \lambda_g = \frac{c}{f_{\text{notch}} \sqrt{\varepsilon_{\text{eff}}}} \]  

where: \( \lambda_g \) = Guided wavelength of the notch frequency  
\( L \) = Approximated length of the U-shaped copper  
\( \varepsilon_{\text{eff}} \) = Antenna effectiveness

The band rejection elements on the ground plane and radiation patch influence the UWB radiation characteristics. Therefore, in this research U-shaped coppers are avoiding that area. The design then are optimized by using a parametric study to increase the performance of filtering antenna.

The dimension and design of the U-shaped coppers are shown in Table 1 and Figure 3, respectively. From the study, each band notched filter can be tuned independently and can perform the operation separately. Figure 4 shows the fabricated design of the proposed design in Figure 3.

| Parameter | Values (mm) | Parameter | Values (mm) |
|-----------|-------------|-----------|-------------|
| La        | 5.95        | Wa        | 12          |
| Lb        | 4.7         | Wb        | 11.5        |
| Lc        | 8.0         | Wc        | 10.38       |
Figure 3. The simulated design of U-shaped coppers in the proposed design. (a) Top view (b) Bottom view

Figure 4. The fabricated design of U-shaped coppers in the proposed design. (a) Top view (b) Bottom view

Figure 5 shows the reflection coefficient for antenna design in Figure 3 and Figure 4 for simulation and measurement process. Simulated result shows that the S11 of the proposed design is less than 2 from 3GHz to 11.2 GHz, except for the unwanted band notched frequency from 5.15 GHz to 5.35 GHz, 5.725 GHz to 5.825 GHz and 7.9 to 8.4 GHz. However, the frequency shift between the simulated and measured results can be Noticed. From [24][26][34] and after going through further study, it may happen due to fabrication tolerance and inaccuracy during cutting the edge of substrate in the fabrication process. Table 2 explains the comparison between simulated and measured results of the proposed triple band notched UWB antenna in Figure 3 and Figure 4.

![Figure 5: S11 results for antenna design in Figure 3 simulation and measurement design.](image)

**Table 2. Comparison of Triple Notched Band Frequency in Simulation and Measurement Design**

| Bandwidth (GHz) | Simulation | Measurement |
|-----------------|------------|-------------|
| 3.02-11.17      | 3.02-11.17 | 4.16- more than 14 |
| Notched-Band (GHz) | 5.15-5.35 | 5.725-5.825 | 7.9-8.4 |
|                 | 5.2-5.48   | 5.82-6.1    | 7.76-8.3 |

The surface current distribution is studied to understand the principle of the proposed UWB monopole antenna with triple band-notched and investigate the influence radiating coppers toward the UWB antenna. From Figure 6, the current distribution at the notch 5.2 GHz, 5.8 GHz and 8 GHz is focused mainly on the left side of feedline, right side of the antenna and above the ground, respectively. It is indicated that all three coppers are capable of rejecting the band notched.
4. RECONFIGURABLE NOTCHED BANDS DESIGN

The PIN diode are putted on the coppers to behave as variable resistor with ON and OFF operating states [35], [36]. Frequency reconfigurable can achieve by control and changing the equivalent RLC circuit of the PIN diode. Table 3 explains the lumped RLC network condition, according to the RLC equivalent circuit in both state (ON/OFF) [37].

The position of the diode is investigated. As reported in [38], the used of the PIN diodes result a small frequency shift to lower frequency. However, this frequency shift can be overcome by adjusting the placement of diode or adding the number of diodes on the antenna. Here, after going further on the parametric study, the position of the diode is optimized and the number of diodes is added to six diodes. Figure 7 shows the optimum position of diodes in this design.

| RLC circuit | Details | State |
|-------------|---------|-------|
|             | 1. Forward biased. | On |
|             | 2. Has a low resistance which allow the current to pass. |
|             | 3. Acts as short circuit. |
|             | 4. Existence of notch. |
|             | 1. Reversed biased. | Off |
|             | 2. Has a large resistance which block the current to flow. |
|             | 3. Acts as open circuit. |
|             | 4. Absent of notch. |

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Table 4 explains the operating modes of the purposed reconfigurable triple band notch conditions. The mode of the targeted notched band of WLAN upper band (5.725–5.825 GHz), WLAN lower band (5.15-5.35 GHz) and X satellite band (7.9-8.4 GHz) are controlled by the On and OFF states of PIN diodes. These operational modes enable the antenna to have eight modes of operation by control the changes in current distribution of the patch.

Table 4. Operating Modes of the Purposed Reconfigurable Triples Band Notched Conditions

| Mode | PD1 | PD2 | PD3 | PD4 | PD6 | Notched Band          |
|------|-----|-----|-----|-----|-----|-----------------------|
| 1    | OFF | OFF | OFF |     |     | UWB antenna           |
| 2    | OFF | OFF | ON  |     |     | 7.9 GHz               |
| 3    | OFF | ON  | OFF |     |     | 5.725 GHz             |
| 4    | OFF | ON  | ON  |     |     | 5.725 GHz and 7.9 GHz |
| 5    | ON  | OFF | OFF |     |     | 5.15 GHz              |
| 6    | ON  | OFF | ON  |     |     | 5.15 GHz and 7.9 GHz  |
| 7    | ON  | ON  | OFF |     |     | 5.15 GHz and 5.725 GHz|
| 8    | ON  | ON  | ON  |     |     | Triple band-notched   |

Figure 8 shows the simulated reflection coefficient of eight combination modes in Table 4. In OFF states, which is in mode 1, the proposed design operated in 3.12 to 11.2 GHz frequency bands which covers the full UWB applications and act as the design in Figure 1.

On the other hand, it other all modes (from mode 2 to mode 8), the reflection coefficient of the proposed design during the ON state is less than -10dB in the corresponding rejected frequency. The activation of diode produced the bandstop filtering element. No operation resonance is generated and all the signal is reflected back. As a result, it generates the impedance mismatching to achieve the targeted rejection band.

Figure 8. Simulated reflection coefficient of eight operating modes in Table 4. (a) Mode 1, Mode 2 and Mode 3 (b) Mode 4, Mode 5 and Mode 6 (c) Mode 7 and Mode 8
5. CONCLUSION

This paper presented circular modified monopole antenna with triple bands reconfigurable for UWB application from WLAN (5.15 GHz and 5.75 GHz) and X-band satellite (7.25 GHz). Three U-shaped coppers is inserted in the UWB antenna design to generate three bandstop filters. Tunable technique is introduced to control the operational mode in this design and can be used to reject reject single, dual or triple notch band in UWB range of frequency. Further investigation of reconfigurable notch filter will be carried out in future works in order to investigate the overall performance of this design through the experimental works. Furthermore, biasing circuit need to be considered in this design to increase the performance reconfigurable UWB antenna.

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