High Isolation and Ideal Correlation Using Spatial Diversity in a Compact MIMO Antenna for Fifth-Generation Applications

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Received 28 April 2020; Revised 20 June 2020; Accepted 3 July 2020; Published 24 July 2020

1. Introduction

In recent years, fifth generation (5G) has attracted a lot of attention from researchers. This generation is different from the previous ones: it is not only interested in the world of mobile telephony but also addresses other sectors that have an impact on our daily life, such as energy, health, media, transport, and industry. 5G is announced as the true enabler of the Industry 4.0, which is considered to be the fourth industrial revolution technology [1]. In addition, 5G will also have an intense impact on the Internet of Things (IoT) and will be its key element by supporting the connection of a huge number of objects to the Internet.

In other words, 5G has the objective of changing the world by connecting everything to everything. To meet these aims, it is necessary to attain high speed, which is one of the important characteristics of 5G that have been established by the International Telecommunication Union (ITU). In this context, 3GPP (3rd Generation Partnership Project) Release 15 introduces 5G technology to meet the declared ITU-2020 objectives including higher spectral efficiency, greater numbers of users, reduced end-to-end latency, higher device connection densities, prolonged device battery life, thousand-fold system capacity, hundredfold energy efficiency, ultrahigh data rate, and ultrawide radio coverage [2, 3].

Hence, the 5G is intended to deliver superfast communication speeds of up to 10 Gb/s. However, to meet this growing demand for multigigabit per second, millimeter-wave is considered to be the most important technology and is a potential candidate for 5G mobile communication [4]. Furthermore, higher data rates and capacities require more bandwidth [5].

Furthermore, 5G technology can operate in two categories of frequencies: sub-6 GHz and high frequencies known as millimeter waves. There are many works in the literature concerning this topic for low frequencies, such as [6–9]. However, we can find plenty of papers for high frequencies [10–22]. In this work, we chose the millimeter waves band, precisely 28 GHz, for several reasons. It has huge bandwidth compared to microwave frequencies.
Opposing to signals in bands below 6 GHz, the mm-Wave signal has a shorter wavelength, which offers several benefits, such as the small size of the device (making it possible to group a big number of antennas in a compact ensemble), narrow beam width, and better resolution [23]. Among the challenge in the application of millimeter waves are rain attenuation and atmospheric absorption caused by weather, resulting in propagation losses, but many studies [24, 25] have been carried out and demonstrated that propagation losses at 28 GHz are not significant compared to other frequencies. The Federal Communications Commission (FCC) has announced the spectrum of 27.5–28.35 GHz for 5G, and this band is proposed for mobile use [26].

The interference that can be created by obstacles such as buildings, trees, as well as bad weather, is one of the challenges of 5G. To overcome this, it is essential to use antenna technologies like Multiple Input Multiple Output (MIMO) [27]. Additionally, the MIMO antenna is used to increase the SNR value, improve channel capacity, enhance data rate, and improve Quality of Service (QOS). To evaluate the performance of a MIMO system, the isolation between antenna elements is regarded as one of the important parameters. There are many techniques for enhancing isolation by using Electromagnetic Band Gap (EBG) structures [28], Metamaterial Polarization Rotator (MPP) Wall [29], neutralizing line [8, 30], Defected Ground Structure (DGS) [8, 16], splitting resonators (SRRs) [31], metal strips [18], and self-decoupled structure [7].

The goal of this paper is to propose a compact MIMO antenna operating at millimeter-wave frequency for fifth-generation applications. By using the spatial diversity technique, high isolation was obtained. The MIMO antenna operates at 28 GHz, and the measured bandwidth covers well the band specified by the FCC for 5G (27.5 GHz–28.35 GHz). The performance of MIMO antenna such as the isolation between two ports, ECC, diversity gain, and TARC are studied. Moreover, the simulated results are validated by the experimental ones and showed an excellent agreement. The suggested MIMO antenna has the advantages of compact size, high isolation, low envelope correlation coefficient, simple structure, and easy to fabricate. Hence, the proposed antenna is a good candidate for MIMO applications and also suitable for use in 5G cellular mobile communication.

2. Antenna Geometry

To design a MIMO antenna, we will first design a single antenna; then, two elements of this single antenna are placed next to each other to construct the desired MIMO antenna, using the technique of spatial diversity. The proposed MIMO antenna design steps are presented in the following section.

2.1. Single Antenna Configuration. The first step is to design a single element antenna for 28 GHz frequency band using the 3D simulator electromagnetic CST Microwave Studio. The radiating element of the proposed antenna is in the shape of “5,” as shown in Figure 1. It is printed on a 13 × 12.8 mm2 FR4 substrate with permittivity of $\varepsilon_r = 4.4$ and thickness of $h = 1.6$ mm. In the bottom side of the substrate, a full ground plane is placed. The patch is fed using 50 Ω microstrip line. Table 1 presents the details of the optimized dimensions parameters.

![Figure 1: Design of the proposed single antenna.](image)

Figure 2 illustrates the evolution stages of the proposed single antenna; and the simulated return loss of three antenna configurations is shown in Figure 3.

The conception starts with a conventional microstrip patch antenna, which provides resonance at 23.3 GHz frequency. In a second step, an L-shaped slot is introduced into the radiating element to improve the return loss and shift the resonant frequency to 24.6 GHz. In the third step, another L-shaped slot is used to increase the resonance frequency and also to enhance the impedance matching. As can be seen from Figure 3, the corresponding result of the proposed antenna (step 3) shows that the return loss is more than 30 dB at 28 GHz, which is the desired frequency.

2.2. Two-Elements MIMO Configuration. In a second step, two elements of the single antenna are placed adjacent to each other to form a MIMO antenna that operates at 28 GHz, the band licensed for fifth-generation. The two radiating elements are closely spaced with a distance separation of $D = 1$ mm $= 0.41 \lambda$, with $\lambda$ being free space wavelength at the center frequency. Figure 4 illustrates the configuration of the proposed 5G MIMO antenna.

3. Decoupling Analysis

3.1. Mutual Coupling. Spatial diversity is the first kind of isolation improvement technique of MIMO antennas. Then, we will use this technique to ensure the isolation between closely packed antenna elements. In designing MIMO antenna, basically, two types of configurations were being suggested. Figures 5(a) and 5(b) show the asymmetric and
symmetric designs of the proposed MIMO antenna, respectively. The simulated S parameters for both configurations are illustrated in Figures 6 and 7.

From Figure 6, it can be seen that the reflection and transmission coefficients are \( S_{11} \approx -54.45 \, \text{dB}, \ S_{12} \approx -33.37 \, \text{dB}, \ S_{21} \approx -34.19 \, \text{dB} \) at 28.115 GHz frequency, while \( S_{22} \approx -31.53 \, \text{dB}, \ S_{12} \approx -33.09 \, \text{dB}, \ S_{21} \approx -33.85 \, \text{dB} \) at 28.085 GHz frequency.

On the other hand, from Figure 7, we can conclude that \( S_{11} = S_{22} \) and \( S_{12} = S_{21} \) due to the symmetry. The obtained reflection coefficient is \( S_{11} = S_{22} = -38.86 \, \text{dB} \), and the isolation between port 1 and port 2 is \( S_{12} = S_{21} = -36.51 \, \text{dB} \) at the desired frequency 28 GHz. Consequently, there is a lower mutual coupling between the two ports. It is clear that the isolation is better for the second configuration (Figure 5(b)). So, this MIMO antenna configuration has been considered in this work. The spacing constraint must be present to guarantee the compactness of the overall size. The value of the isolation is greater than 35 dB in this approach for \( D = 1 \, \text{mm} \).

Finally, we can conclude that the isolation was achieved without using any additional decoupling structure while maintaining a minimum spacing of 1 mm (0.41 λ) between the antenna elements.

### 3.2. Surface Current Distributions

In this section, the distribution of surface currents at the desired 28 GHz mm-wave frequency for the two antenna ports will be studied in order to confirm the decoupling between antenna elements.

Figure 8 represents the simulated surface current distributions when port 1 is excited, and the other port is terminated at 50Ω and vice versa for port 2. From Figure 8(a), it is clear that the current is mainly concentrated around the first element of the MIMO antenna (port 1), while it is focused around the second element of the proposed MIMO antenna (port2), as can be seen in Figure 8(b). Furthermore, the coupling current concentration between the MIMO antennas is negligible. Therefore, it can be concluded that very good isolation between the two antenna elements is ensured.
4. Fabrication, Measurement Results, and Discussion

4.1. Fabricated Antennas. The process of analyzing an antenna involves three main stages: firstly, the design of the antenna through simulation software; secondly, the manufacturing, and finally, the measurements.

Based on the obtained designs, which are optimized using Computer Simulation Technology (CST) Microwave Studio Software in Section 2, the fabrication of these two antennas (single element antenna and two elements MIMO antenna) is performed using a printed circuit board (PCB) milling machine: the LPKF Proto Mat E33, which is available in our laboratory. Then, the measurement of the S parameters is carried out using the PNA-L Network Analyzer N5234A (10 MHz–43.5 GHz). The photograph of the fabricated prototype of a single antenna and MIMO antenna is illustrated in Figure 9.

4.2. S Parameters. The measured and simulated reflection coefficient curves of the single 5G antenna are shown in Figure 10. An excellent agreement can be observed between simulation and measurement results.

As illustrated in Figure 10, the measured and simulated −10 dB impedance bandwidths are (27.36–29.39 GHz) and (26.56–29.3 GHz), respectively. Moreover, at the resonant frequency, the simulated reflection coefficient $S_{11}$ is −30.73 dB, while the measured one is −20.58 dB, which signifies a good adaptation. To make this comparison more clear, Table 2 summarizes the results of the proposed single antenna for the fifth generation.

Because of the symmetric structures of the proposed antenna (i.e., $|S_{11}| = |S_{22}|$ and $|S_{12}| = |S_{21}|$), only the measurement of $S_{11}$ and $S_{12}$ was carried out.

Figure 11 shows the measured and simulated reflection coefficient of the proposed MIMO antenna, corresponding to −37.17 dB and −38.93 dB, respectively, at the 28 GHz millimeter-wave frequency band.

The measured and simulated transmission coefficients curves are shown in Figure 12. An acceptable agreement appears for both measured and simulated isolation between the two antenna elements. The isolation is very high; its value
Figure 8: Surface currents distributions of (a) port 1 and (b) port 2 at 28 GHz.

Figure 9: Photograph of the prototypes: (a) single antenna and (b) MIMO antenna.
is 41.36 dB for the experimental results and 36.51 dB for simulation, meaning that the two antennas are independent of each other. From all these features, we can conclude that the proposed MIMO antenna has a good performance, as indicated in Table 3.

### 5. MIMO Antenna Performance Parameters

For the evaluation of a Multiple Input Multiple Output antenna, it is important to analyze some parameters: the envelope correlation coefficient “ECC” which represents the main parameter, the diversity gain “DG” and total active reflection coefficient “TARC” as well as the efficiency and gain. Therefore, the purpose of this section is to calculate each of these parameters.

#### 5.1. Efficiency and Gain

The simulated realized gain and efficiency of the proposed 5G MIMO antenna are illustrated...
in Figure 13. At the resonance frequency of 28 GHz, it is clear that the MIMO antenna offers a gain of 6.68 dBi and the total efficiency is about 80%.

5.2. Envelope Correlation Coefficient and Diversity Gain. The Envelope Correlation Coefficient indicates the degree of independence of the radiation patterns of two antennas. Using the correlation coefficient, we can understand the level of coupling that exists between the antenna ports in the MIMO system. Minimizing the mutual coupling would involve reducing the correlation coefficient between the port pairs.

There are two approaches to calculate the correlation coefficient: the far-field radiation pattern [7] and the S parameters [31]. Its value should be less than 0.5 [32]. The envelope correlation coefficient ECC for two-element antennas is calculated using the following equation:

\[
ECC = \rho_e = \frac{|S_{11}^* S_{12} + S_{21}^* S_{22}|^2}{(1 - |S_{11}|^2) (1 - |S_{22}|^2) (1 - |S_{12}|^2)}
\]  

The diversity gain is related to the ECC, and they are linked by the following equation:

\[
DG = 10 \sqrt{1 - |\rho|^2},
\]

where \(|\rho|^2 = \rho_e\).

The measured and simulated ECC and DG for the proposed MIMO antenna are shown in Figure 14. As can be seen from this figure, the value of simulated ECC is an ideal value of 1.15 \times 10^{-7} at 28 GHz frequency, while the corresponding diversity gain value is around 10, which means that the proposed MIMO antenna has a good performance.

5.3. Total Active Reflection Coefficient. The total active reflection coefficient is the square root of the sum of all reflected powers at the ports, divided by the sum of all incident powers at the ports of an N-port antenna. TARC can be obtained directly from the scattering matrix by the following equation [33]:

\[
\Gamma = \frac{\sqrt{\sum_{i=1}^{N} |b_i|^2}}{\sqrt{\sum_{i=1}^{N} |a_i|^2}}
\]
where \( b_i \) and \( a_i \) are the reflected and incident signals, respectively.

After simplification, equation (3) became as follows [34]:

\[
TARC = \sqrt{\frac{(S_{11} + S_{12}e^{j\theta})^2 + (S_{22} + S_{21}e^{j\theta})^2}{2}}.
\]  

(4)

Figure 15 represents the measured and simulated TARC of the proposed MIMO antenna. As can be seen from this figure, it is better than \(-10\) dB at the operating band.

5.4. Radiation Pattern. The 3D radiation pattern of the proposed 5G MIMO antenna is reported in Figure 16 for the two antenna ports: port 1 and port 2 at the desired frequency 28 GHz. As can be remarked from this figure, the suggested antenna is directional and has a maximum directivity of 7.74 dBi.

Furthermore, Figure 17 shows the simulated far-field radiation patterns of the proposed MIMO antenna in E-plane and H-plane copolarization, cross-polarization at 28 GHz when port 1 is excited, and other port are terminated with a 50 \( \Omega \) load.
6. Performance Comparison

Table 4 displays the performance comparison between the proposed MIMO 5G antenna and recently published articles. This comparison has been made in terms of overall size, the bandwidth, isolation, ECC, and diversity gain.

According to Table 4, our antenna has a compact size compared to other published designs, very high isolation, and an ideal ECC compared to all listed references. Furthermore, the proposed antenna has a simple structure and sufficient bandwidth.

Finally, based on these results and performances, we can say that the suggested antenna is suitable for MIMO system applications and is a good candidate for 5G applications.

7. Conclusion

In this paper, a two-port, multiple-input, multiple-output antenna with high isolation and low correlation for 5G applications was presented. This antenna is a symmetrical arrangement of two single antennas having a compact size of 12.8x13x1.6 mm³. Prototype antennas are manufactured and measured. A good agreement is obtained between measurements and simulations. The measured bandwidths of the proposed antennas cover the 28 GHz band (27.5–28.35 GHz) allocated by the Federal Communications Commission for 5G applications.

The isolation between the two elements of the MIMO antenna is 41.36 dB at the resonant frequency. Using the spatial diversity technique, high isolation was achieved without adding any other technique. The envelope correlation coefficient has a value of 1.15 x10⁻¹⁰, whereas the diversity gain is around 10 dB, while the TARC is less than −10 dB in the operating band. Moreover, the gain and efficiency of the proposed MIMO antenna are also analyzed and are shown to be satisfactory. These results show that the proposed antenna has the main advantages, such as compact size, high isolation, and low ECC when compared to other works. As a consequence, the proposed antenna may be useful for 5G MIMO applications.

Data Availability

All data generated during this study are included in this article.

Conflicts of Interest

The authors declare that they have no conflicts of interest.

Acknowledgments

This work was carried out with the support of the CNRST within the framework of the Research Excellence Scholarship Program. The authors would like to thank Professor Mohamed TAOUZARI of ENSA, Hassan 1st University, Berrechid, Morocco, for his support with regards to the measure of the proposed antennas.

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