The importance of geometry in the corneal micropocket assay

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Abstract

The corneal micropocket assay is an experimental protocol for studying vessel network formation, or neovascularization, \textit{in vivo}. The assay is attractive due to the ease with which the developing vessel network can be observed in the same animal over time. However, it is difficult to relate observations of neovascularization in the hemispherical geometry of the cornea to predictions from mathematical (\textit{in silico}) models and observations from \textit{in vitro} models, which mostly adopt planar geometries. Here, we develop a three-dimensional, off-lattice mathematical model of neovascularization in the cornea, with a new repulsion model for the interaction of vessels with tissue boundaries. The model allows us to: i) investigate how the hemispherical geometry of the cornea influences vessel network formation and ii) identify the metrics of neovascularization that are most robust to geometrical differences between typical \textit{in silico}, \textit{in vitro} and \textit{in vivo} tissue domains. We predict that two-dimensional geometries lead to increased vessel ‘merging’, or anastomosis, relative to three-dimensional versions, with differences being most pronounced when circular geometries are adopted. Cuboidal geometries lead to patterns of neovascularization that most closely mimic the \textit{in vivo} case. The ‘distance of the vascular front to the limbus’ is found to be a robust metric of neovascularization across the studied tissue domains, while densities of tip cells and vessels and ‘vascularized fraction’ are more sensitive to domain choice. Given the widespread adoption and attractive simplicity of planar tissue domains, the differences identified in the present study should prove useful in relating the results of previous and future \textit{in silico} and \textit{in vitro} studies of neovascularization to \textit{in vivo} observations in the cornea.

Author summary

Neovascularization, or the formation of new blood vessels, is an important process in development, wound healing and cancer. The corneal micropocket assay is used to better understand the process and, in the case of cancer, how it can be controlled with drug therapies for improved patient outcomes. In the assay, the hemispherical shape of the cornea can influence the way the vessel network forms. This makes it difficult to directly compare results from experiments with the predictions of mathematical models or cell culture experiments, which are
typically performed on flat substrates or planar matrices. In this study, we use mathematical modeling to investigate how the hemispherical shape of the cornea affects vessel formation and to identify how sensitive different measurements of neovascularization are to geometry.

Introduction

Neovascularization, or new blood vessel formation, is an important process in development, wound healing, cancer and other diseases. The corneal micropocket assay, shown in Fig 1, is widely used for studying neovascularization in vivo [1–3]. The assay involves the implantation of a pellet containing pro-angiogenic compounds into the cornea of a small rodent and observation of the resulting vessel formation over time. An attractive feature of the assay is the relative ease with which neovascularization can be observed in the same animal at multiple time-points. In rodents, the cornea is hemispherical, with a thickness on the order of 10 to 20 vessel diameters [4]. The pellet is not usually located on the pole of the cornea; it is shifted slightly toward the base or limbus. It is evident from experimental images that the geometrical configuration of the cornea-pellet system influences neovascularization patterns [1]. As shown schematically in Fig 1C, new vessel formation is often focused in the region where the distance between the pellet and limbus is smallest, with vessels tending to grow toward the pellet.

Fig 1. Schematics of the corneal micropocket assay and typical in silico and in vitro geometries. A) An image of the micropocket assay from Connor et al. [5]. B) The placement of a pellet of radius $r_p$ into the cornea at height $h$ from the limbus, where $h$ is the distance along the shown y or z axis. C) The resulting neovascularization, quantified by distance $d$ of the front to the limbus. D) A typical planar model of the cornea-pellet system, with the pellet width $w$ set equal to cornea width $W$ for one-dimensional mathematical models. E) A typical circular model.

The attractive features of the micropocket assay make it a good candidate for comparing vessel network formation with mathematical (in silico) and in vitro models. However, it is important to understand how the geometry of the cornea-pellet system affects vessel network formation relative to the planar tissue domains used in typical two- and three-dimensional (2D,
3D) cultures and mathematical models, a selection of which are shown in Figs 1D and E.

As reviewed in Jackson and Zheng [6], many mathematical models of neovascularization have been motivated by the micropocket assay, providing valuable insights into the process [5,7,14]. To date, these models have adopted either one-dimensional (1D) or 2D representations of the cornea-pellet system, with the former allowing efficient, continuum modeling of the developing vessel network by the solution of systems of partial differential equations (PDEs) [5,10,11]. However, the in vivo configuration of a cylindrical pellet placed ‘off-center’ in a hemispherical volume is most naturally described using a 3D representation. While there are many 3D mathematical models of sprouting angiogenesis [15–19], none have focused on the particular geometry of the cornea-pellet system. Doing so brings the additional challenges of needing to use a relatively large simulation domain and accounting for the interaction of vessels with curved tissue boundaries at the epithelial and endothelial surfaces of the cornea.

In the present study, we develop a discrete, 3D, off-lattice mathematical model of neovascularization in the cornea-pellet system, focusing on emulating the in vivo configuration. We use a simplified treatment of the underlying biology, focusing instead on how the adoption of different in vitro and in silico geometries, including planar 2D and 3D cultures in rectangular or circular configurations, affects vessel network formation relative to the in vivo case. The primary strengths of the study are: i) the simulation of neovascularization in large, 3D tissue domains and ii) the ability to compare predictions across several different geometries and with different biophysical processes activated and de-activated. These attributes are facilitated by the use of the open source Microvessel Chaste simulation library [20], recently developed by the authors.

As part of this comparison we also identify metrics of neovascularization with high and low sensitivity to the choice of tissue domain. As a result, we can predict which in vitro and in silico tissue domains most closely resemble the conditions of the in vivo experiment and which metrics of neovascularization are most suitable for performing comparisons. Given the widespread adoption and attractive simplicity of planar tissue domains, the differences identified here should prove useful in relating and translating the results of previous and future in silico and in vitro studies of neovascularization to in vivo observations in the cornea.

Materials and methods

Neovascularization is simulated in seven different tissue domains, representing those typical of in silico and in vitro modeling studies and the in vivo assay. A phenomenological model of sprouting angiogenesis is adopted, motivated by several previous studies [6,7,14,21], but extended to 3D. A ‘soft-contact’ model is also introduced to account for interactions of migrating vessels with the cornea boundaries. It is assumed that the pellet contains a single pro-angiogenic compound, Vascular Endothelial Growth Factor 165 (denoted VEGF in the present study). Two situations are considered, one where the concentration of VEGF in the tissue domain is described by a time-independent, spatially varying field where VEGF levels decrease linearly from the pellet, and the other where VEGF dynamics are explicitly modeled, following approaches in Tong and Yuan [7] and Connor et al. [5].

The simulated tissue domains, angiogenesis model and VEGF dynamics model are described in this section, along with details of the numerical schemes used for their solution.
**Tissue domains**

Fig 2 shows 3D renderings of each of the studied domains, along with the naming convention used when presenting results. The pellet radius $r_p = 200 \, \mu m$ is based on data from Connor et al. [5], but reduced from their value of 300 $\mu m$ to facilitate placement in the cornea. In 3D simulations, pellets are assumed to have a thickness of $T_p = 40 \, \mu m$ and are situated mid-way between the epithelial and endothelial sides of the cornea. In 2D simulations, the cornea thickness is neglected, while in 3D a value of $T = 100 \, \mu m$ is used [4]. The cornea radius is fixed at $R = 1300 \, \mu m$, which is a suitable value for mouse [4]. The ‘Hemisphere’ geometry is formed by a 360° revolution of a circular arc of radius $R$ and angle 90° about the polar axis, followed by an extrusion through a distance $T$ along the inward normal to the revolved surface, giving a 3D volume. The cylindrical pellet is placed inside this volume and is completely enclosed by it. For the Hemisphere, the pellet height $h$ above the limbus is the distance as projected into 2D, as would be typically measured in experimental images, rather than the distance along the geodesic from the limbus to the pellet.

![Diagram of tissue domains](image)

**Fig 2.** 3D renderings of the studied tissue domains, including dimensions. 3D renderings of the studied simulation domains, including adopted abbreviations. Domain dimensions are included in $\mu m$, following the notation in Fig 1, and $T$ is the cornea thickness.

All simulations begin with a single blood vessel positioned a small height $\varepsilon = 100 \, \mu m$ above the base of the cornea and mid-way between the epithelial and endothelial sides of the cornea.
The vessel occupies the entire width (or circumference) of the domain at that position. Vessels are discretized into straight line segments joined by ‘nodes’, shown schematically in Fig 3. Each segment represents an arbitrary number of endothelial cells. Initially, nodes are placed \( \frac{1}{E_L} = 20.0 \) \( \mu m \) apart, where \( E_L \) represents the number of endothelial cells per vessel length [22].

**Angiogenesis model**

A simple, phenomenological model of sprouting angiogenesis is used. The average rate of sprout formation at a node located at \( x \) is [21]:

\[
P(x, t) = P_{max} \bar{L}_s E_L \frac{c(x, t)}{c(x, t) + c_{50}}
\]

where \( P_{max} \) is the rate of sprouting per cell, \( c(x, t) \) is the VEGF concentration at location \( x \) and time \( t \), \( c_{50} \) is the VEGF concentration at which the rate of sprouting is half-maximal and \( \bar{L}_s \) is the averaged length of the two line segments joined to the node. In addition, a simple description of lateral inhibition is used, with \( P = 0 \) within a distance \( \frac{1}{E_L} \) of a node that has already been selected for sprouting. Simulations are discretized in time using a fixed step of \( \Delta t = 1.0 \) h. In each time step a random number \( z \in [0, 1] \) is chosen from a uniform distribution at each node and a sprout forms if \( z < P \Delta t \). A different random number is generated at each node.

After sprouting, migrating tips, illustrated in Fig 3, are assumed to move at constant speed \( s = 10 \) \( \mu m \) h\(^{-1}\). This speed is chosen so that the average time for the vascular front to reach the pellet is on the order of 4 days, which is consistent with experimental observations [1]. A persistent, off-lattice random walk is used to describe the migration of tips through the extracellular matrix of the stroma [6,7,14]. The migration direction \( m \) is given by:

\[
m = \frac{m_p + \chi \nabla c}{1 + \chi} \nabla c
\]

where \( \chi \) is a dimensionless weighting parameter controlling chemotactic sensitivity, \( m_p \) is a unit vector in the persistence direction and \( \nabla c \) is the gradient of the VEGF concentration. The random persistence direction \( m_p \) is obtained by rotating the unit tangent vector along the vessel \( \tau \) an angle \( \theta_{\text{tip}} \) away from its original direction in an arbitrary plane, as shown in Fig 3. The angle \( \theta_{\text{tip}} \) is chosen from a normal distribution with zero mean and standard deviation \( \sigma \).

An important distinction from previous studies is that the finite extents of the cornea are accounted for: migrating tips are not permitted to leave the simulation domain. A ‘soft contact’ model is adopted so that tips approaching the boundary of the domain are gradually deflected along the tangent to the bounding surface. Biologically this represents tip cells failing to penetrate the stiffer tissue present on the epithelial and endothelial cornea surfaces, while ‘soft’ contact is chosen for more robust numerics. The strength of the repulsion from the boundary increases as the boundary is approached according to:

\[
\phi(x) = \phi_{max} \frac{d_{\text{crit}} - d(x)}{d_{\text{crit}} + d(x)}
\]

where \( d(x) \) is the minimum distance to the domain boundaries, \( d_{\text{crit}} \) is the distance to the boundary at which repulsion is activated and \( \phi_{max} \) is the dimensionless maximum repulsion.
Fig 3. The discretized vessel network representation and an application of the boundary repulsion model. A) The discretized vessel network showing ‘nodes’, ‘vessels’ and ‘tips’. Directions used in the migration rule are also shown. B) An application of the boundary repulsion model, with vessels deflected along a circular boundary. A distance map $d(x)$ to the boundary (in $\mu$m) and distance map gradient directions $\nabla d$ are also shown with arrows.

The repulsion biases the motion along the tangent to the bounding surface according to:

$$ r = \phi \nabla d $$

(4)

where the $\hat{\cdot}$ operator produces a random unit tangent. The position of migrating nodes is updated from $x(t)$ to $x(t + \Delta t)$ at each time step:

$$ x(t + \Delta t) = x(t) + s \frac{m + r}{|m + r|} \Delta t. $$

(5)

where $s$ is the tip velocity and $\Delta t$ is the time step size in hours. Fixed values of the repulsion strength $\phi_{\text{max}} = 5$ and critical repulsion distance $d_{\text{crit}} = 25 \mu$m are used for all simulations. These values are chosen to ensure a gradual deflection away from the surface, without overly influencing the migration of tips that are far away from the boundaries. An example application of the boundary repulsion model, taken from a simulation, is shown in Fig 3B.

Endothelial tip cells are known to find and merge with other endothelial tips and immature blood vessels during migration, in a process known as anastomosis [23]. There is still
uncertainty about the mechanisms by which they meet, but mechanical and chemical guidance are known to contribute [23]. When moving from 2D to 3D models of sprouting angiogenesis it is necessary to define a region within which tips will merge with vessels and each other to allow for the identification of intersections. In this study, a relatively small radius of $r_{ana} = 5 \, \mu m$ is used, which is on the order of the vessel radius.

**VEGF dynamics**

VEGF dynamics are treated in two different ways in this study. In the first case, the pellet dynamics are ignored and a time independent, spatially varying VEGF concentration field is imposed in the tissue domain. In the second case, the dynamics of VEGF release from a nylon pellet are explicitly modeled.

For the first case, a constant VEGF gradient between the limbus and the pellet is applied, given by:

$$\frac{dc}{dx} = \frac{c_p}{h + \varepsilon},$$

where $x$ is a positional coordinate along the geodesic between the limbus and pellet, $\varepsilon$ is a small offset from the base, corresponding to the position of the initial vessel, and $c_p$ is the VEGF concentration in the pellet, which is assumed to be constant in time in this case. By specifying:

$$c(\varepsilon) = c_p \frac{\varepsilon}{h + \varepsilon},$$

the same concentration and concentration gradient magnitudes are maintained at the limbus in all representations. Aside from the Hemisphere, the concentration at the base is 0 nM and at height $h + \varepsilon$ (the pellet location) it is $c_p$.

For the second case, the transport and decay of the VEGF in the pellet are considered, meaning that $c_p$ can now change over time. The dynamics of VEGF in the pellet are not known in detail, but as per Tong and Yuan [7] a high rate of reversible binding to the nylon pellet constituents is assumed. Under this assumption it is possible to derive the following relationship between the total $c_p$ and free $c_f$ amounts of VEGF in the pellet [5]:

$$c_f = \frac{c_p}{\theta},$$

where $\theta \geq 1$ is a dimensionless binding parameter. Free VEGF can decay in the pellet at a rate $\lambda_p$ or leak through the cornea-pellet interface, which has an effective permeability $\kappa_p$. It is assumed that the VEGF concentration is spatially uniform within the pellet, which has volume $\Omega_p$. Balancing mass leads to the following differential equation describing the time rate of change of VEGF in the pellet:

$$\frac{dc_p}{dt} = -\lambda_p c_f - \frac{\kappa_p}{\Omega_p} \int_{\partial \Omega} (c_f - c) \, d\Omega,$$

where the integral is over the pellet surface $\partial \Omega$ and $c$ is the concentration of VEGF in the cornea, at the interface. The initial concentration $c_p(t = 0)$ can be determined from the implanted VEGF mass $m = 300 \, \text{ng}$ [5] by:

$$c_p(t = 0) = \frac{m}{1000 \, \text{MW}_{\text{VEGF}} \Omega_p}.$$
where the VEGF molecular weight $\text{MW}_{\text{VEGF}}$ is 45 kDa or 45 000 g mol$^{-1}$ and the factor of $\frac{1}{1000}$ converts from mol m$^{-3}$ to M.

It is assumed that VEGF diffuses isotropically in the cornea, with a diffusion coefficient $D = 2.52 \times 10^{-7}$ m$^2$ h$^{-1}$ [24,25] and decays naturally at a rate $\lambda = 0.8$ h$^{-1}$ [26]. It is also assumed to enter perfused vessels (and be washed away) and bind to endothelial cells. Combining these processes, we deduce that the dynamics of VEGF in the cornea can be described by the following reaction-diffusion equation:

$$\frac{\partial c}{\partial t} = D \nabla^2 c - \lambda c - \frac{2\pi R_v \rho \kappa_v (c - c_b)}{c + c_{50}} + n k_{ec} \frac{c}{c + c_{50}}.$$ (11)

Here $\kappa_v = 3 \times 10^{-4}$ m h$^{-1}$ [27,28] is the permeability of vessels to VEGF, $R_v = 5\, \mu\text{m}$ [29,30] is the assumed vessel radius, $c_b = 0$ M is the amount of VEGF in the blood, assuming it is quickly removed, and $\rho$ and $n$ are respective vessel line and tip densities. The parameter $k_{ec}$ is the rate of VEGF binding per endothelial cell and $c_{50}$ is the VEGF concentration at which the rate of binding is half maximal.

The extent to which VEGF will pass through the outer cornea layers is not clear, nor whether it will pass through the epithelial layer and into the aqueous humor or the collagen-rich limbus. It is assumed that the rate of such leakage is low, and no flux boundary conditions are imposed on all outer surfaces of the cornea $\partial \Omega_{\text{cornea}}$, that is:

$$D \mathbf{n} \cdot \nabla c |_{\partial \Omega_{\text{cornea}}} = 0$$ (12)

where $\mathbf{n}$ is the inward surface normal. On the cornea-pellet interface the following mass balance is assumed:

$$- D \mathbf{n} \cdot \nabla c |_{\partial \Omega} = -\kappa_p (c_f - c),$$ (13)

where $c_f = \frac{c_p}{\theta}$ is the amount of free VEGF in the pellet.

Eqns (9)-(13) are solved numerically (detailed below), subject to the initial condition of no VEGF in the cornea. In the 2D geometries, the cornea-pellet interface $\partial \Omega$ is a line of length $w$ for the planar case or $2\pi r_p$ for the circle. In the Planar3D geometries it is a rectangle of height $T$ or $T_p$, depending on whether a finite sized pellet is assumed, and width $w$. In the remaining geometries, the interface is the entire outer surface of the spatially resolved pellet.

### Parameter values

Table 1 summarizes the parameter values adopted in this study. Parameter values with sources denoted as ‘This Study’ are discussed in this section unless previously introduced.

A pellet thickness of $T_p = 40\, \mu\text{m}$ is used in this study, which is less than the $T_p = 60\, \mu\text{m}$ value reported in Connor et al. [5]. This is to facilitate placement of the pellet in the simulated Hemisphere geometry. The chemotactic sensitivity range $\chi \in [0,0.5]$ is chosen to cover extreme cases where the resulting vessel network is not directed towards the pellet and highly directed towards it. The range of the deviation in persistence angle $\sigma \in [0,20]$ degrees covers cases where straight vessels form, through to cases with vessels with tortuosity similar to that observed in experimental images of the assay. The global time step $\Delta t = 1$ h is chosen to give average segment lengths of 10 $\mu\text{m}$, which leads to a physically realistic vessel tortuosity. The initial offset from the limbus of $\varepsilon = 100\, \mu\text{m}$ is in agreement with experimental images [5].
The amount of growth factor in implanted pellets is usually known by mass, with a value of 300 ng for VEGF reported in Connor et al. [5]. For our pellet volume of 0.0075 mm$^3$ and VEGF molecular weight of 45 kDa, this corresponds to a pellet concentration of approximately $c_p = 1330 \, \mu$M, which is adopted for the dynamic VEGF model. For the time-independent VEGF model lower pellet concentrations of $c_p = 1$ to 100 nM are used, which give similar concentrations at the limbus to the dynamic model in the early stages of the simulation. The bound fraction of VEGF in the dynamic model $\theta = 30$ is chosen to give a time of VEGF depletion in the pellet of approximately 4 days.

Simulation details

Simulations are performed using the open-source Microvessel Chaste library developed by the authors [20], which is a plug-in for the Chaste library for soft tissue modeling [31]. This allows efficient modeling of neovascularization in a range of different geometrical configurations and, thanks to its modular construction, allows different biophysical features of the sprouting angiogenesis model to be activated and de-activated.

The VEGF PDE is solved using the finite element method with linear basis functions. A simple forward-Euler time-stepping scheme is adopted, with suitable time steps identified by convergence studies. The maximum PDE solution time step is 0.05 h and a typical grid side length is 30 \, \mu m.

Simulation results are presented in terms of the ‘vessel line density’ $\rho(x, t)$, which is defined as the vessel length per unit volume, and ‘tip density’ $n(x, t)$, which is the number of migrating tips per unit volume. Densities are calculated on structured grids, with values averaged over grid cells that are equidistant from the limbus. To reduce noise caused by the sampling of discrete vessels and tips onto the grids, two Gaussian smoothing passes are applied to $\rho$ and $n$ before further processing [33].

CPU times for 90 simulated hours on a single processor range from 15 seconds for the Planar2D case, with a fixed VEGF field, to 30 minutes for the Hemisphere and dynamic VEGF model. The most computationally expensive elements of the simulation are the PDE solution times and spatial searches for anastomosis events.

Results

Fig 4A shows simulated vessel networks after 85 hours (3.5 days) for the case with a fixed VEGF concentration field. Anastomosis is found to be more prevalent in the 2D domains, leading to a reduced number of tips and greater confinement of tips toward the advancing front. In 3D, the presence of multiple vessels through the cornea thickness is evident. In the Circle2D case, there is a tendency for tips to move together as the center is approached, this focusing effect being due to the domain geometry.

Fig 4B quantifies the maximum tip and vessel line densities in each domain after 85 hours, with and without anastomosis. Without anastomosis, the circular domains have tip densities higher than the planar domains and Hemisphere by a factor of 1.7 due to geometrical effects. Despite the extra vessel length and volume available for sprouting in 3D, line and tip densities are similar to the 2D cases. When anastomosis is active, the tip and line densities in the 2D cases decrease by greater amounts than in 3D. In the planar domain, the tip density decreases by a factor of 5.3 for the Planar2D case but only 1.8 for the Planar3D case. Similarly, it
Fig 4. 2D and circular domains lead to increased anastomosis. A) Simulation results for a fixed VEGF gradient 85 hours after pellet implantation. B) A comparison of maximum tip and line density across the studied domains after 85 hours, with and without anastomosis and with $c_p = 20$ nM. Error bars show one standard deviation from the mean, with five random realisations per observation. C) The change in maximum tip density with time in one random realisation per geometry, with anastomosis.
decreases by a factor of 6.4 for the Circle2D case, but only 2.1 for the Circle3D. These results show that the 2D domains lead to greater anastomosis, with the highest tendency for anastomosis in the circular domains. This effect becomes increasingly apparent as the initial pellet concentration $c_p$ is varied from 1 through to 100 nM (shown in S1 Fig). As shown in Fig 4C and the full tip and line density profiles in S2 Fig, the differences between 2D and 3D domains become more pronounced with time, as the capacity for sprouting in 2D is reduced due to anastomosis and lateral inhibition. The increasing density in the circular domains with time is again due to geometric effects.

Fig 5A shows predicted VEGF concentrations in each domain after 1 hour for the dynamic VEGF model. VEGF distributions are quite different across each domain, showing the importance of choosing a suitable representation of the pellet. The Planar2D and Planar3D domains have a relatively high VEGF concentration at the cornea-pellet interface along the entire domain width $W$. When pellets of finite width are used the region of higher concentration is localized to a line of length $w$ on the interface. The Planar3D case, with finite pellet width, has a noticeably lower VEGF concentration than the 2D case, due to the pellet thickness $T_p$ being smaller than that of the cornea $T$. In the circular domains, the situation is reversed, with higher VEGF concentrations in the 3D domain due to a greater surface density at the cornea-pellet interface. A higher concentration is observed in the Hemisphere for the same reason.

Over time the VEGF in the pellet depletes, with the decay term in Eqn (9) being dominant. This leads to a similar rate of decay across all domains, as shown in Fig 5B. The VEGF has largely decayed after 4 days, with a 95 % reduction from the maximum value in the tissue at this time.

The variation in VEGF concentrations shown in Fig 5A, combined with the greater tendency for anastomosis in 2D and circular domains shown in Fig 4, leads to a variety of predicted maximum tip and line densities across the studied domains for the dynamic VEGF model, as shown in Fig 5C. In this case, higher densities are predicted in the planar geometries with extended pellets, while geometries with the finite pellet width have a lower density, more comparable with the Hemisphere, due to focusing of the vascularized region. When the pellet is moved closer to the limbus the general trend is for an increase in the maximum tip density. In relative terms, the tip density increases most in the Hemisphere and Planar3D geometry with finite pellet, both by a factor of 1.7, although in absolute terms the density in the Planar3DFinite geometry is approximately half that of the Hemisphere. In contrast, in the circles, the tip density is reduced by a factor of 1.25 as the pellet is moved towards the limbus. This is a geometric effect, due to the breaking of symmetry as the pellet is moved away from the center of the circle. The dynamics of the maximum densities are similar to those shown in Fig 4C, with the rate of density increase being greatest in the circular domains.

Fig 6 summarizes the locations of the vascular front across all of the studied domains at 85 hours, with activation and de-activation of various biophysical features of the angiogenesis model. The ‘distance of the vascular front to the limbus’, $d$ in Fig 1, is found to be a reasonably robust metric of neovascularization, with similar values predicted across all domains. For the dynamic VEGF model shown in Fig 6B, the variation from the Hemisphere value across all domains for the predicted vascular front location is at most 3.7 percent, while there is a 34 percent change in the location itself when the pellet is moved.

The location of the maximum tip density and half-maximum tip density are useful additional metrics in cases where they can be measured. As shown in Fig 6C, these metrics are more
Fig 5. Line and tip density predictions are sensitive to pellet representation. A) A comparison of VEGF concentrations for the dynamic model in each domain at 1 hour and $h = 1.0$ mm. B) The change in maximum VEGF concentration with time for one set of random realisations of the case with $h = 1.0$ mm. C) A comparison of maximum tip and line densities across the studied domains for $h = 1.0$ mm and $h = 0.7$ mm. Error bars show one standard deviation from the mean, with five random realisations per observation.

sensitive to changes in the biophysical mechanisms of network formation than the front location. For example, the tendency for tip cells to be positioned closer to the moving front in 2D domains (shown in Fig 4A) is captured in the bottom glyph in Fig 6C. The effect of strong
Fig 6. ‘Distance to limbus’ is a robust metric of neovascularization. A) A schematic showing measured locations of the tip density profile for comparison in B and C. Locations correspond to the positions of maximum density, half-maximum density and 1% of the maximum density. The ‘distance to limbus’ metric is taken to be equivalent to the location with 1% of the maximum density. B) A comparison of tip density profiles for the dynamic VEGF model and different values of $h$. C) A comparison of tip density profiles for the fixed VEGF field and activation and de-activation of different biophysical features (indicated by ‘-‘). Error bars show one standard deviation from the mean, with five random realisations per observation.

chemotaxis is similar, as shown in the top glyph. When chemotaxis is relatively weak, or the degree of persistence in the random walk is low, the location of the maximum tip density is moved closer to the limbus. These tendencies are captured across all domains using the maximum tip density and half-maximum tip density location metrics, although they are more sensitive to domain choice than the front location. In all cases the front velocity is approximately constant in time and is similar across all domains.

Fig 7A shows the different predicted vessel network patterns in a selection of domains as the pellet is moved closer to the limbus for the dynamic VEGF model. Differences in vessel network...
formation are not well captured by the ‘distance to limbus’ metric in this case. Although the maximum tip and line density metrics used in Fig 5 are useful in the context of modeling, they can be difficult to measure experimentally. This is because endothelial tip cells are not obvious at typical imaging resolution, while line density measurements are subject to potential errors as multiple vessels may overlap through the cornea thickness [7]. In contrast, it is easier to estimate the ‘vascularized fraction’ or volume of the domain with vessels divided by total domain volume directly from images. In the present study this metric is calculated by accumulating the volume of the cells in the structured grid used in the calculation of densities that are occupied by vessels and dividing by the volume of all cells in the grid.

As shown in Fig 7B the ‘vascularized fraction’ metric captures the differences in vascularization between domains shown in Fig 5B, and also captures the trend for increased vascularization when the pellet is moved closer to the limbus in all domains, except for the circles. As such, the metric is predicted to be useful for differentiating neovascularization patterns and translating observations across geometries.

Fig 7. ‘Vascularized fraction’ is a useful proxy for tip and line densities. A) Simulation results at 85 hours showing different degrees of vascularization in different simulation domains for $h = 1.0$ mm and $h = 0.7$ mm. B) The corresponding ‘Vascularized Fraction’ for each pellet height. Error bars show one standard deviation from the mean, with five random realisations per observation.
Discussion

Summarizing the results in Figs 4, 5, 6 and 7, it is predicted that the small, but finite, thickness of the cornea can have an important effect on vessel network formation relative to 2D assays and models, reducing the likelihood of vessels anastomosing. The positioning of the pellet affects the resulting neovascularization in the Hemisphere, with increased focusing observed as the pellet is moved towards the limbus. Circular domains lead to increased anastomosis relative to planar domains and the hemispherical cornea. Circular domains also have a markedly different sensitivity to pellet positioning.

The curvature of the cornea is predicted not to affect neovascularization, with good agreement between the Planar3D domain with a finite pellet and Hemisphere simulations. One-dimensional mathematical models do not capture the vascularized fraction of the Hemisphere but, as shown in Fig 6, predictions of front locations from the models are in agreement with the Hemisphere model. It is also envisaged that the results presented in this study will be useful in the future formulation of PDE models of neovascularization in the cornea. In particular, they give insights into front locations and line and tip density profiles in cases where direct formulation of PDE analogues is challenging, such as accounting for off-lattice random walks with anastomosis and symmetry breaking in the positioning of the spatially resolved pellet.

The ‘location of the vascular front’ is predicted to be robust to the choice of domain, suggesting that it could be used to relate in silico predictions or in vitro observations to in vivo. The ‘vascularized fraction’ is predicted to be sensitive to domain choice, in particular the manner in which VEGF is introduced to the system. This may help to relate observations in planar domains to those in the in vivo assay.

In the present work, a simplified model of neovascularization is adopted, with the primary focus being on comparing predicted neovascularization across different geometries, which has not been performed for the cornea before. By varying phenomenological parameters, such as the chemotactic strength $\chi$ and deviation in the persistence angle $\sigma$ (as shown in Fig 6), and physical parameters, such as the VEGF concentration in the pellet $c_p$ (as shown in S1 Fig), through a range of values, it is possible to account for a variety of vascular patterning behaviors. Suggested extensions to the adopted modeling are: i) the inclusion of blood flow and vessel regression, which may reduce overall vessel densities and average vessel lengths and ultimately halt the progression of the moving front [40], ii) a more detailed model of endothelial cell proliferation and migration [6], which would remove the need for a phenomenological migration speed $s$ and may lead to a front velocity that is not constant in time, iii) models of tip attraction [40] and mechanical interaction with extracellular matrix [6], which may encourage extra anastomosis by guiding tips to locate each other and iv) modeling detailed feedback between a metabolically active tissue and the vasculature [40].

Further, there is scope for more detailed parameter studies, such as an investigation of the relationship between pellet location and ‘vascularized fraction’ and the sensitivity of predictions to the anastomosis radius $r_{ana}$. More quantitative comparison with experimental measurements of the kind in Tong and Yuan [3] and Connor et al. [5] is now possible, due to the focus on modeling the actual geometry of the cornea-pellet system in the present study. Such comparisons would be useful for model validation. In particular, a comparison of experimentally measurable metrics, such as front locations and vascularized fractions, with model predictions while varying pellet loading and positioning would be a useful validation step. Figs 5C and
Figs 7B make clear and experimentally testable predictions regarding how the representation of the VEGF pellet affects vessel network formation in different geometries. Exploring these further, via dedicated experiments in a collection of corresponding geometries, would be also be useful.

**Conclusion**

In this study we use a newly developed 3D, off-lattice mathematical model of neovascularization in the cornea to study how: i) the geometry of the cornea-pellet system in the micropocket assay affects vessel network formation and ii) which metrics of neovascularization are most sensitive to geometrical differences between typical *in silico*, *in vitro* and *in vivo* tissue domains. We predict that:

- 2D and circular domains lead to increased anastomosis, even relative to the thin cornea geometry,
- predictions of neovascularization are highly sensitive to the geometrical treatment of the VEGF-containing pellet,
- measuring the distance of the growing vascularized front to the limbus leads to predictions that are robust to differences in domain choice,
- vascularized fractions can serve as a useful proxy for densities of migrating tips or vessel line densities, which are more difficult to measure. These metrics can better distinguish underlying vascular patterning than the distance to the limbus,
- predictions from planar domains with a finite pellet representation are in closest agreement with those of the hemisphere domain. 3D domains give closer tip and line density predictions to the hemisphere than 2D.

All raw data and software used in this study are available on the Zenodo public archive at [https://doi.org/10.5281/zenodo.995721](https://doi.org/10.5281/zenodo.995721). Instructions for reproducing the study figures are included in the archive.

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**Supporting information**

S1 Fig. Max tip and line densities as the pellet concentration $c_p$ is increased from 1 to 100 nM. Max tip and line densities after 85 simulated hours for the case with a constant VEGF concentration field. Differences between geometries become more pronounced as the pellet concentration increases.
S2 Fig. Full tip and line density profiles sampled every 5 hours for selected domains. Full tip and line density profiles for a single random realisation in a selection of domains for the case with a constant VEGF concentration field.

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Table 1. Adopted parameter values for the neovascularization simulations.

| Parameter                              | Symbol | Value       | Unit       | Source   |
|----------------------------------------|--------|-------------|------------|----------|
| Pellet Radius                          | $r_p$  | 200         | µm         | This Study |
| Pellet Thickness                       | $T_p$  | 40          | µm         | This Study |
| Cornea Thickness                       | $T$    | 100         | µm         | [4]      |
| Cornea Radius                          | $R$    | 1300        | µm         | [4]      |
| Endothelial Cells Per Vessel Length    | $E_L$  | 0.05        | µm$^{-1}$  | [22]     |
| Max Sprouting Rate Per Cell            | $P_{max}$ | 0.015     | h$^{-1}$   | [21]     |
| Half-Max Sprouting Concentration       | $c_{50}$ | 0.65       | nM         | [32]     |
| Sprout Speed                           | $s$    | 10          | µm$ h^{-1}$| This Study |
| Chemotactic Sensitivity                | $\chi$ | [0, 0.5]    | -          | This Study |
| Deviation in Persistence Angle         | $\sigma$ | [0, 20]    | degrees    | This Study |
| Critical Distance for Repulsion        | $d_{crit}$ | 25        | µm         | This Study |
| Max Repulsion Strength                 | $\phi_{max}$ | 5        | -          | This Study |
| Global Time Step                       | $\Delta t$ | 1        | h          | This Study |
| Pellet Height                          | $h$    | [0.7, 1.0]  | mm         | [5, 7]   |
| Offset From Limbus                     | $\varepsilon$ | 0.1    | mm         | This Study |
| Pellet Concentration                   | $c_p$  | 1 - 100, $1.33 \times 10^6$ | nM         | This Study |
| Bound VEGF Fraction                    | $\theta$ | 30        | -          | This Study |
| Rate of VEGF Decay in Pellet           | $\lambda_p$ | 0.8     | h$^{-1}$   | [26]     |
| VEGF Permeability                      | $\kappa_p$ | 1.12e-7 | µm h$^{-1}$ | [5]      |
| VEGF Diffusivity in Cornea             | $D$    | $2.52 \times 10^{-7}$ | m$^2$ h$^{-1}$ | [24, 25, 34] |
| Rate of VEGF Decay in Cornea           | $\lambda$ | 0.8     | h$^{-1}$   | [25, 36] |
| Vessel Permeability to VEGF            | $\kappa_v$ | 3.e-4   | m h$^{-1}$ | [27, 28] |
| Vessel Radius                          | $R_v$  | 5          | µm         | [29, 30] |
| Rate of VEGF Binding to ECs            | $k_{ec}$ | 4e-19    | mol h$^{-1}$ per cell | [37, 39] |