Performance evaluation of zero-valent iron nanoparticles (NZVI) for high-concentration H$_2$S removal from biogas at different temperatures

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The removal performance of high-concentration H$_2$S (ca. 10 000 ppm) from simulated biogas by zero-valent iron nanoparticles (NZVI), with the majority of the particles in the size range of 60–150 nm, at different reaction temperatures (room temperature, 100 °C, 200 °C and 250 °C) were evaluated using a custom-designed quartz fixed-bed reactor. The results showed that the H$_2$S removal capacities of NZVI were quite limited at room temperature and 100 °C, being 12.56 and 14.77 mg H$_2$S gNZVI$^{-1}$; respectively. However, these values increased significantly to 391.02 (200 °C) and 488.95 (250 °C) mg H$_2$S gNZVI$^{-1}$. Scanning electron microscopy analysis showed that the products of the NZVI–H$_2$S reaction aggregated to form irregular polygonal-shaped structures. The main X-ray diffraction pattern peaks of the product matched well with troilite, and no pyrite was observed. The deconvolution of the X-ray photoelectron spectrometry peaks showed the presence of monosulphide (S$_2^{2-}$) and disulphide (S$_2^{2-}$) in the product, in which 36% of the sulphur existed as monosulphide and 64% as disulphide. It is proposed that the effective removal of hydrogen sulphide by NZVI at elevated temperatures can be attributed to the combination of nano-constituents, oxide shell and underlying Fe core to produce FeS similar to troilite and amorphous FeS$_2$.

1. Introduction

Biogas is produced from the anaerobic treatment of sewage sludge, the organic fraction of municipal solid wastes (OFMSW), animal manures or organic agro-industrial wastes.  The biogas produced by all these activities is rich in CH$_4$ (typically 35–75%), and its higher heating value is between 15 and 30 MJ Nm$^{-3}$. Biogas is a versatile renewable energy source and can be employed for combined heat and power (CHP), to produce compressed natural gas (CNG), as a drop-in replacement for gasoline, diesel, and jet fuel hydrocarbons or in advanced oxygenated fuels such as methanol and dimethyl ether (DME).

Sulphur compounds are common contaminants in biogas. Typical H$_2$S concentrations from manures and sewage sludge are 200–1500 ppm, with some reports of concentrations as high as 10 000 ppm. H$_2$S is generated both from the anaerobic degradation of sulphur-bearing organic molecules (mainly proteins) and through sulphate reduction by sulphate-reducing bacteria (SRB). With respect to landfills, construction and demolition debris, especially wallboard, which is largely composed of gypsum, degrade with relatively large releases of H$_2$S. The H$_2$S in biogas must be removed according to its downstream usage, as it can reduce the lifetime of metal pipe-work, combustion engines and compressors by corrosion and cause the release of harmful sulphur oxides (SO$_x$) as an air pollutant. The maximum acceptable H$_2$S content is ca. 100–500 mg Nm$^{-3}$ when biogas is used for combined heat and power, depending on the specific manufacturer, and the concentration should be further reduced to less than 5 mg Nm$^{-3}$ when used as fuel for vehicles. In China, when biogas is to be upgraded to pipeline-quality natural gas, the H$_2$S concentration should be less than 6 mg Nm$^{-3}$ to meet the requirement of standard natural gas (GB 17820-2012).

Nanoscale zero-valent iron (NZVI) has been used widely for treating hazardous and toxic wastes due to its diminutive size, large specific surface area and elevated reactivity for rapid contaminant transformation. It is well known that NZVI has an ability for the sequestration of sulphide compounds effectively in an aqueous environment. When situated in an aqueous environment, NZVI will undergo surface hydroxylation to form a thin oxide layer with a thickness of ca. 2–4 nm on the surface and between the individual particles. The amorphous oxide layer consists of a mixed phase of Fe(II)/Fe(III) in proximity to the
metallic core and a phase of predominantly Fe(0) oxide near the water interface,\textsuperscript{13,14} with a stoichiometry close to FeOOH.\textsuperscript{13,14} The amorphous oxide layer possesses the ability to sequester sulphide. Li et al. showed that H$_2$S can be immobilized on the NZVI surface effectively as disulphide and monosulphide species when the NZVI is present in an H$_2$S solution.\textsuperscript{15} The use of NZVI for sulphide removal from digested piggery wastewater was conducted by Chaung et al.\textsuperscript{16} The reported results showed that the complexity of the digested wastewater constituents limited the effectiveness of NZVI. We also reported in previous studies the long-term effectiveness of the \textit{in situ} removal of H$_2$S by NZVI in an anaerobic sewage sludge digester.\textsuperscript{4,17,18} Revealing that elimination of H$_2$S occurred \textit{via} the reaction with the oxide shell of NZVI to mainly form FeS and some FeS$_2$ and S$\delta$\textsuperscript{1}.

Few previous studies have focused on the elimination of H$_2$S by zero-valent iron nanoparticles (NZVI) in a dry process. The objectives of this study were (1) to evaluate the potential of NZVI for sulphide removal at different temperatures in a dry process; (2) to clarify the products and mechanism of the NZVI–sulphide reaction by different analysis technologies, such as X-ray diffraction, thermal gravimetric and differential thermal gravimetric, scanning electron microscopy-energy dispersive spectroscopy and X-ray photoelectron spectrometry.

2. Materials and methods

2.1. Test materials

Zero-valent iron nanoparticles (NZVI, on a 99.9% metal basis) were obtained from Shanghai Macklin Biochemical Co., Ltd. (Shanghai, China) without further treatment. Quartz wool (5–9 µm) was purchased from Aladdin Co. Ltd. in China. Quartz sand (100-mesh) was purchased from Qingdao Usolf Chemical Technology Co., Ltd.

2.2. H$_2$S removal experiments

The H$_2$S removal tests were carried out in a custom-designed quartz fixed-bed reactor, as shown in Fig. 1. A furnace (HF-500, Hunan Huashi equipment Co., Ltd) was used to provide uniform heating to the sample in the quartz column. Two K-type thermocouples were used to monitor the temperature of the furnace and reaction column, respectively. A mass flowmeter (S48 32/HMT, Horiba Meteron, China) was used to control the biogas flow into the quartz column.

The reactor exit was connected to a six-port Valco GC valve (VICI, Valco, Houston, TX, USA) and the H$_2$S concentration was monitored on-line (every 6.2 min) using a gas chromatograph (Sp-3420A, Beijing BFLR Analytical Instrument Co., Ltd., China) equipped with a flame ionization detector (FID) and a HayeSep R column (4’ × 1/8’). The breakthrough capacity was determined at an exit H$_2$S concentration equal to the 30% of inlet concentration. All reactions were carried out under a fume hood due to the high toxicity of H$_2$S.

Exactly 50 mg of NZVI and 0.95 g of 100-mesh quartz sand were mixed adequately to avoid possible channelling, and then were packed in a quartz column (8 mm i.d., at a fixed height of 270 mm). Quartz wool was packed at both the bottom and top of the NZVI/quartz sand mixture to facilitate the diffusion of gas.\textsuperscript{19} A synthetic mix of CH$_4$ (60%), CO$_2$ (39%) and H$_2$S (1%) was provided by Nanjing Tianze Gas Co. Ltd. Removal capacities of H$_2$S, expressed as x/M (mg H$_2$S g$^{-1}$ of material), were calculated according to Ros et al.\textsuperscript{20} by integrating the corresponding breakthrough curves and applying eqn (1).

$$ x = \frac{Q \times MW}{w \times V_M} \left( c_0 \times t_s - \int_0^{t_s} c(t)dt \right) \quad (1) $$

where $Q$ is the inlet flow rate (m$^3$ s$^{-1}$), $w$ is the weight of NZVI introduced into the column (g), $MW$ is the molecular weight of H$_2$S (34 g mol$^{-1}$), $V_M$ is the molar volume (22.4 L mol$^{-1}$), $c_0$ is the inlet gas H$_2$S concentration (ppmv), $c(t)$ is the gas outlet concentration (ppmv), and $t_s$ is the bed saturation/exhaustion time (s). To achieve statistical soundness, three experiments were carried out with each of the samples, and the average x/M values were calculated. Meanwhile, to analyse the X-ray diffraction, scanning electron microscopy and energy dispersive spectroscopy, X-ray photoelectron spectrometry of the NZVI–H$_2$S reaction product, 0.5 g pure NZVI, instead of 50 mg NZVI and 0.95 g quartz sand, was also packed in a quartz column for H$_2$S removal at 250 °C.

2.3. Analytical methods

For the X-ray diffraction analysis, a D8 Advance X-ray diffractometer (Bruker AXS Inc., Germany) was employed with an accelerating voltage of 40 kV and a current of 40 mA. The samples were examined at room temperature over the 2θ range of 10–90° using graphite-monochromated Cu Kα radiation. The step scan was 0.02°, and the measuring time increments were 0.1 s step$^{-1}$. The diffractograms were obtained with Diff-plus and analysed using MDI Jade 6.0 software.

For the scanning electron microscopy and energy dispersive spectroscopy analyses, both the NZVI and the NZVI–H$_2$S reaction product were prepared using double-sided carbon tape coated with platinum and were performed on a Hitachi S-4800 SEM equipped with a Bruker energy dispersive spectroscopy detector. Thermal gravimetric analysis and differential thermal gravimetric analysis were performed using a Mettler Toledo TGA2. The samples were heated from room temperature to 1000 °C at a heating rate of 10 °C min$^{-1}$ under air atmosphere.

Fig. 1. Schematic description of the experimental laboratory setup.
X-ray photoelectron spectrometry experiments were carried out on an RBD upgraded PHI-5000C ESCA system (Perkin Elmer) with Mg Kα radiation ($h\nu = 1253.6$ eV) or Al Kα radiation ($h\nu = 1486.6$ eV), according to Shen et al.21 In general, the X-ray anode was run at 250 W and the high voltage was kept at 14.0 kV with a detection angle at 54°. The pass energy was fixed at 23.5, 46.95 or 93.90 eV to ensure sufficient resolution and sensitivity. The base pressure of the analyser chamber was approximately 5 × 10$^{-8}$ Pa. The sample was directly pressed into a self-supported disk (10 × 10 mm), mounted on a sample holder and then transferred into the analyser chamber. The complete spectra (0–1100 (1200) eV) and the narrow spectra of all the elements with much higher resolution were both recorded by using a RBD 147 interface (RBD Enterprises, USA) through the AugerScan 3.21 software. Binding energies were calibrated by using the containment carbon (C 1s = 284.6 eV). The data analysis was carried out by using the XPSPeak 4.1, while the Lorentzian–Gaussian (%) was fixed to 20% for the sulphur component.

3. Results and discussion

3.1. Effect of temperature on H$_2$S removal

The performance of NZVI for H$_2$S removal as a function of time was tested at different temperatures, as shown in Fig. 2a. At room temperature (ca. 25 °C) and 100 °C, the breakthrough time measured for NZVI was quite short, indicating its low capacity for H$_2$S removal. The H$_2$S concentrations of the effluent of biogas were 2518 ± 225.1 and 126.9 ± 98.96 ppm after 6.2 minutes at 25 °C and 100 °C, respectively. When the reaction temperature was elevated to 200 °C and 250 °C, the breakthrough times were prolonged dramatically, no H$_2$S was detected within 256 min and 388 min, respectively. After that, the curves of H$_2$S concentration of the effluent were sigmoidal or S-shape at 200 °C and 250 °C. The removal capacities were derived from the curves, in which the breakthrough point was defined by 30% of the inlet concentration (3000 ppm). These are also shown in Fig. 2b. The H$_2$S removal capacities are 12.56 ± 0.43 and 14.77 ± 0.10 mg H$_2$S gNZVI$^{-1}$, respectively, at 25 °C and 100 °C. However, when NZVI was exposed to H$_2$S (ca. 10 000 ppm) at 200 and 250 °C, it presents breakthrough capacities as high as 391.03 ± 37.73 and 488.95 ± 27.72 mg H$_2$S gNZVI$^{-1}$, respectively. When biogas is used for combined heat and power, assumed that the maximum acceptable H$_2$S content is 500 mg Nm$^{-3}$, then the capacity of this setup for H$_2$S removal is 333.33 ± 9.44 and 423.10 ± 23.70 mg H$_2$S gNZVI$^{-1}$.

3.2. Scanning electron microscopy and energy dispersive spectroscopy analysis

Scanning electron microscopy analysis indicates that the pure NZVI particles were generally spherical in shape with the majority in the size range of 60–150 nm, and the iron nanoparticles are connected into chain-like structures possibly due to chemical aggregation, as shown in Fig. 3a. The energy dispersive spectroscopy for pure NZVI particles showed the presence of Fe and O (Fe: 95.17%, O: 4.83% (wt)) in this structure, the relatively high content of O can be explained by the presence of an oxide shell at the surface of the iron nanoparticles as they age,42 which was further confirmed by X-ray diffraction analysis.

To avoid the disturbance of quartz sand on the morphology analysis of the reaction product, the NZVI–H$_2$S reaction product at 250 °C without quartz sand was further characterized by scanning electron microscopy and energy dispersive spectroscopy, as shown in Fig. 3b. The structure of NZVI changed significantly after reaction. Compared with the unreacted NZVI, the space between the nanoparticles decreased remarkably, while the products of the NZVI–H$_2$S reaction were piled up to form irregular polygonal-shaped structures. The subsequent energy dispersive spectroscopy analysis showed that the presence of Fe and S (Fe: 62.86%, S: 37.14% (wt)). No elemental O was identified in the new structure, implying the depletion of O element to produce H$_2$O (g) in this process. Based on energy dispersive spectroscopy analysis, the atom and weigh ratios of Fe : S are approximately 0.97 and 1.7, respectively.

Additional experiment was conducted to analysis the difference of materials on bottom/top/inside after H$_2$S removal. After reaction at 250 °C, the materials at different layers were
separated carefully and further characterized by scanning electron microscopy-energy dispersive spectroscopy, as showed in Fig. 4. According to the scanning electron microscopy analysis, the products of the NZVI–H₂S reaction from different layers were all aggregated to form irregular polygonal-shaped structures, while the spacing between particles of the inside and bottom layer decreased obviously compared to the top layer. Energy dispersive spectroscopy showed that the contents of S were 33.96 ± 0.65%, 34.80 ± 0.53%, 32.32 ± 0.62%, respectively, from the materials on top, inside and bottom layer (Fig. 4). With respect to content of elemental S and Fe, no significant different was found at different layers.

3.3. X-ray diffraction analysis

Fig. 5 compared the X-ray diffraction patterns of untreated NZVI and NZVI–H₂S reaction products at different temperatures in the presence of quartz sand. With respect to untreated NZVI, the main peaks at the 2θ of 44.7°, 65.0° and 82.3° indicate the presence of metallic Fe (Fe⁰), while the weak peak at the 2θ of 35.8° showed the presence of iron oxide crystalline phases. After treated with H₂S at room temperature and 100 °C, the peaks represent zero-valent iron were also identified, although the intensity is lower due to the dilution of quartz sand (Fig. 5). No S-containing crystalline phase were characterized in the X-ray diffraction spectra at room temperature and 100 °C. At elevated temperature, weak peaks of iron sulphide at the 2θ of 29.9°, 33.7°, 43.2° and 53.1° appeared, and the peak intensities of zero-valent iron decreased significantly. The phenomenon indicated that H₂S is immobilized by NZVI at the temperature above 200 °C effectively and that most of the nanoscale iron particles were depleted to form iron sulphide during this process. An increase in the intensity of iron sulphide was also recorded when the reaction temperature increased from 200 to 250 °C.

The NZVI–H₂S reaction product at 250 °C without quartz sand was further characterized by X-ray diffraction, as shown in Fig. 6. The X-ray diffraction study shows that the reaction product is crystalline and composed primarily of Fe sulphides with a small amount of metallic Fe. The presence of metallic Fe can be partly explained by the unreacted metallic Fe due to channelling. The main peaks of iron sulphide are at the 2θ of 18.7°, 29.9°, 33.7°, 43.2°, 47.1°, 52.2°, 53.1° and 70.8°. The
The pattern of the sample displayed sharp peaks that matched well with the PDF card for troilite (89-3030), and no pyrite was observed.

3.4. Thermal gravimetric and differential thermal gravimetric analysis

Fig. 7 shows the thermal gravimetric and differential thermal gravimetric data of the NZVI–H₂S reaction product at 250 °C without quartz sand. The iron-to-sulphur ratio was determined by TGA. Assuming an initial stoichiometry of FeₓS of sample after sulphidation, values of \( x = 1.02 \) were determined. The data collected in air showed a gain in mass during room temperature to 400 °C, and this simply might be attributed to the oxidation of unreacted metallic Fe. After that, significant weight losses were detected at 400–450 °C and 540–670 °C can be due to the final oxidation to Fe₂O₃. The TG curve under air is similar with troilite prepared via the nonhydrolytic sol–gel reaction.

3.5. X-ray photoelectron spectrometry analysis

To investigate the composition and chemical state, the X-ray photoelectron spectrometry survey of the iron nanoparticles of untreated NZVI and NZVI–H₂S reaction (without quartz sand) at 250 °C were carried out. The full-range X-ray photoelectron spectrometry survey spectra showed that the major elements of NZVI–H₂S product were iron (Fe), sulphur (S), oxygen (O) and carbon (C), while the S 2p spectra indicated the presence of sulphur species (Fig. 8).

The S 2p narrow scans showed that no signal corresponding to the presence of sulphur was detected with respect to untreated NZVI (Fig. 9a). A reaction with H₂S, due to the S 2p peak having closely spaced spin–orbit components with \( \Delta = 1.16 \) eV and intensity ratio = 0.511,²⁴,²⁵ the spectrum can be deconvoluted into four overlapped peaks, with the S 2p 3/2 peak binding energies at 160.8 and 161.5 eV. According to the literature data, these two peaks should correspond to disulphide (S₂²⁻) and monosulphide (S₂⁻),¹⁵ respectively. The areas of the fitting curves were further calculated, and the results showed that approximately 36% of the sulphur on the surface existed as monosulphide and 64% as disulphide after the NZVI–H₂S reaction at 250 °C.

The X-ray photoelectron spectrometry survey of the Fe 2p of NZVI is shown in Fig. 9b. The binding energies of Fe 2p 3/2 and Fe 2p 1/2 for untreated NZVI were 711.0 eV and 724.5 eV, respectively. No distinct peak at approximately 706–707 eV was observed for untreated NZVI, in contrast to the results reported by Wen et al.,²⁶ confirming the presence of an oxide shell at the surface of the iron nanoparticles. A small peak at 707.0 eV was recorded with fresh NZVI by Wen et al.,²⁶ suggesting the presence of zero-valent iron (Fe⁰).²⁷ This difference can be explained by the ageing of the NZVI used in this study. After reacting with H₂S, the binding energies at 712.1 eV and 725 eV were assigned to Fe 2p 3/2 and Fe 2p 1/2. The separation of the Fe 2p 3/2 and Fe 2p 1/2 spin–orbit levels was 12.90 eV. The shift of the binding energies of Fe to the higher binding energy after reaction probably indicated the formation of iron sulphide.
It is well addressed that metal particles are oxidized when exposed to air or O, regardless of the synthesis method or particle morphology. Wang et al. further observed that iron nanoparticles will be instantly covered by an oxide shell that is typically ~3 nm thick when exposed to air at room temperature. This was consistent with our X-ray diffraction, energy dispersive spectroscopy and X-ray photoelectron spectrometry results. Research efforts have been conducted to clarify whether the oxide shell is FeO, x-Fe2O3, γ-Fe2O3, Fe3O4, an unknown phase, or a combination of several phases, using X-ray diffraction spectroscopy, electron diffraction, transmission electron microscopic imaging, and electron energy loss spectroscopy (EELS). Signorini et al. speculated that the structure of the oxide shell on the Fe nanoparticle varies as a function of the distance from the underlying Fe core; i.e., the outer surface of the oxide shell is expected to be γ-Fe2O3 and the inner region that is adjacent to the Fe core is expected to be Fe3O4. Wang et al. reported that the fine structural features are similar to those exhibited by Fe3O4, but with differences in the peak intensities and position, while no phase transition in the oxide shell was characterized. Moreover, Wang et al. showed that the oxide shell in the core-shell structured Fe nanoparticle is highly defective compared to the bulk form.

Though present at the surface of the iron nanoparticles exposed to air, the thick layer of Fe oxide cannot fully account for the high sulphide removal capacity. According to the scanning electron microscopy and energy dispersive spectroscopy analysis, the content of elemental O in the NZVI used is only 4.83%, indicating that the iron nanoparticles were far from being fully oxidized. Due to the absence of oxygen in simulated biogas, any increase in the formation of the oxide shell layer will be negligible during the reaction process even at elevated temperatures. Regardless of the formation of the oxide shell, electrons are still allowed to pass into the metal core, and the underlying Fe core also contributes significantly to sulphide removal. Additional experiments on zero-valent iron (100-mesh, 400-mesh and 800-mesh) were conducted, and the results are shown in Fig. 10. Generally, the sulphide removal capacities increase with increased reaction temperatures, but do not depend on the particle diameter of ZVI. Even though the sulphide removal increases with temperature, only 19.66, 23.12 and 15.15 mg H2S gZVI−1 were achieved, respectively, for 100-mesh, 400-mesh and 800-mesh ZVI at a reaction temperature of 250 °C. This phenomenon suggested that the decrease in the ZVI particle diameter, from microscale to nanoscale, significantly enhanced the reaction activity of Fe0-sulphide. The inevitable production of H2 from the Fe0-sulphide reaction, rather than the H2O formed during the iron oxides–sulphide reaction, would benefit the further utilization of biogas due to its high calorific value.

The iron-to-sulphur ratio of the NZVI–sulphide reaction products at 250 °C were 0.97 and 1.02, respectively, according to previous energy dispersive spectroscopy and TGA analysis. Due to the presence of unreacted metallic Fe which is confirmed by X-ray diffraction, the total iron-to-sulphur ratio of the NZVI–H2S reaction products should less than 1. The X-ray photoelectron spectrometry analysis showed the presence of monosulphide
(S\(^{-2}\)) and disulphide (S\(_2\)^{2-}) in the products, but no pyrite was observed by X-ray diffraction analysis. According to the above discussion, it is proposed that the effective removal of H\(_2\)S by NZVI at elevated temperatures can be attributed to the combination of two nano-constituents, the oxide shell and the underlying Fe core, to produce FeS similar to troilite and amorphous FeS\(_2\).

Additional experiment was conducted to assess the disturbance of impurities, such as hydrocarbons, on the removal of H\(_2\)S from biogas. Simulated biogas including impurities (CO, dimethyl sulphide, dichloroethene, tetrachloroethene, methylene chloride, toluene, ethylbenzene, \(\alpha\)-xylene, isobutane, isopentane, \(n\)-pentane, hexanes) was prepared according to Spiegel et al.\(^{30}\) and adopted for disturbance assessment, as showed in Table 1. The result showed that, the presence of hydrocarbons has little influence on H\(_2\)S removal; the H\(_2\)S removal capacity of NZVI was 494.0 ± 27.99 mg H\(_2\)S g\(^{-1}\)NZVI at 250 °C in the presence of impurities, as showed in Fig. 11.

**Table 1** Simulated biogas composition for disturbance assessment

| Compound         | Concentration (ppm) |
|------------------|---------------------|
| Methane          | 45%                 |
| Carbon dioxide   | 39%                 |
| Nitrogen         | 14.9%               |
| Hydrogen sulphide| 0.8%                |
| CO               | 0.3%                |
| Dimethyl sulphide| 8.0                 |
| Dichloroethene   | 33                  |
| Tetrachloroethene| 6.3                 |
| Methylene chloride| 12                |
| Toluene          | 35                  |
| Ethylbenzene     | 13                  |
| \(\alpha\)-Xylene| 22                  |
| Isobutane        | 100                 |
| Isopentane       | 970                 |
| \(n\)-Pentane    | 180                 |
| Hexanes          | 390                 |

Fig. 10 H\(_2\)S removal capacities of NZVI (100-mesh, 400-mesh and 800-mesh) at different temperatures (room temperature, 100 °C, 200 °C, and 250 °C).

Fig. 11 H\(_2\)S breakthrough curves of NZVI at 250 °C for simulated biogas including impurities.

Implications for use of NZVI to eliminate H\(_2\)S from real biogas were further discussed. Firstly, oxygen and vapor in biogas should be removed before the use of NZVI for H\(_2\)S removal, due to the forming of oxide shell and amorphous oxide layer, respectively, in the presence of oxygen and water. Secondly, the high cost of synthesized NZVI, using sodium borohydride as a traditional reducing agent, might hinder its application to H\(_2\)S removal for biogas. However, the new synthesis of iron nanoparticles utilizing tea leaf and sorghum bran extracts reported might provide an alternative and low-cost method of producing NZVI,\(^{31,32}\) further decreasing the cost of desulphurization with NZVI for biogas. The H\(_2\)S removal performance of iron nanoparticles produced by green synthesis should be further studied due to the difference in the diameter and shape of the particles, surface functional groups, etc. Thirdly, additional heating system is needed to provide elevated temperature (e.g. 250 °C) for NZVI–H\(_2\)S reaction with careful design to avoid the risk of explosion. Finally, the H\(_2\)S removal unit should be redesigned to meet the requirements of nano-sized desulfurizer, which is different from traditional commercial desulfurizer. Considerable efforts are still needed before the method can be accepted for commercial use.

4. Conclusions

The H\(_2\)S removal capacities of NZVI were quite limited at room temperature and 100 °C, being 12.56 and 14.77 mg H\(_2\)S g\(^{-1}\)NZVI, respectively. However, these values increased significantly to 391.02 (200 °C) and 488.95 (250 °C) mg H\(_2\)S g\(^{-1}\)NZVI at 250 °C.

The reaction products at 250 °C were further characterized to elucidate the reaction mechanism. Scanning electron microscopy analysis revealed that the products of NZVI–H\(_2\)S aggregated to form irregular polygonal-shaped structures. The main X-ray diffraction pattern peaks of the product (2θ of 43.2°, 29.9°, 33.7°, 53.1° and 70.8°) matched well with troilite, while no pyrite was observed. The X-ray photoelectron spectrometry peak
deconvolution of sulphur showed the presence of monosulphide ($S^{2-}$) and disulphide ($S_{2}^{2-}$) in the product, in which 36% of sulphur existed as monosulphide and 64% as disulphide. It is proposed that the effective removal of H$_2$S by NZVI at elevated temperatures can be attributed to the combination of the nano-constituents consisting of the oxide shell and the underlying Fe core to produce FeS similar to troilite and amorphous FeS$_2$.

**Conflicts of interest**

There are no conflicts to declare.

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