Novel Biosensor Detection of Tuberculosis Based on Photonic Band Gap Materials

Arafa H Aly*, D. Mohamed+, Z. A. Zaky+, Z. S. Matar+, N. S. Abd El-Gawaad, A. S. Shalaby*,
Fatima Tayeboun, M. Mohaseb*

*Beni-Suef University, Faculty of Sciences, Physics Department, TH-PPM Group, Beni Suef, Egypt
+Umm-Al-Qura University, Faculty of Applied Science, Department of Physics, Mecca, Saudi Arabia
King Khalid University, Faculty of Science, Abha, Saudi Arabia
Bena-Suef University, Faculty of Sciences, Physics Department, Beni Suef, Egypt
Djillali Liabes University, Sidi-Bel-Abbes 22000, Algeria

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Tuberculosis is one of the most widespread infectious and deadliest diseases in the world. The death percentage is larger than that in the case of the current Coronavirus. Bio-photonic sensors represent a promising option for developing reliable, simple, and affordable tools for the effective detection of tuberculosis. In this paper, a novel design of an optical biosensor will be used as a tuberculosis detector based on a resonance cavity with high sensitivity in one-dimensional photonic crystals demonstrated theoretically. The results show that the increase of the defect layer thickness shifts the defect mode to a longer wavelength region. Besides, it is shifted to a shorter wavelength region via the increase of the incidence angle. The change in thickness of the defect layer and incident angle of light cause an optimization for our suggested structure and the sensitivity reaches 1390 nm/RIU. Our structure is very simple for industrial design.

Keywords: Tuberculosis, refractive index, photonic crystal, detector, sensitivity, biosensor.

1. Introduction

Photonic crystals (PCs) recently become one of the amazing favorite methods used in integrated optical circuits1-2, and many authors employing PCs in many valuable applications3-10. Photonic crystals consist of a multilayer of dielectric materials with low and high refractive indices that control the propagation of light. Photonic crystals have a very interesting region called the Photonic bandgap region (PBG) which is the frequency ranges that are not allowed to propagate in the structure11-12. By introducing the defects inside the photonic structure, scientists can control and adjust the PBG. Accordingly, many optical devices are produced such as optical filters13,14, optical switches15,16, photonic crystal fibers17-19.

Tuberculosis (TB) is one of the deadly serious and most widespread infectious diseases20. According to the World Health Organization (WHO), in 2017 there are around 1.6 million TB deaths, including 300,000 people living with HIV21. In 2019, data were informed by 202 countries and territories that account for more than 99% of the world’s population and roughly calculate the number of TB cases21. An accurate diagnosis very early on active pulmonary TB is crucial for the control of the disease and treatment of infected patients. It is very important to develop new techniques for detecting TB diagnosis because a large proportion of all TB cases (98%) in developing countries occur without access to biomedical analysis laboratories. Optical biosensors are considered as analytical detectors that transduce the blood reactions/interactions into an optical signal22. The biophotonic sensors have many advantages that distinguished them from conventional diagnostic techniques, such as single-step detection, ease of use, and most of the biosensor enabling better and rapid control over the measurement22. There are many types of biosensors such as electrical, piezoelectric, electrochemical, nanomechanical, magnetic, acoustic, and optical23-26. The optical transducer mechanism is the system that modulates the interaction with optical radiation in a detectable way22. As a particular photonic structure that can be used for sensing is a photonic crystal (PC), we develop a highly sensitive biosensor structure based on 1D-PC with a defect layer. The proposed design can be fabricated by many different ways as reported in literatures27-31.

We calculate the transmittance for s-polarized light by utilizing the transfer matrix method (TMM) and studying the effect of some parameters to achieve the highest performance of the sensor configuration.

2. Theoretical Model

In this part, we consider a 1D-PC structure consists of Air/(TiN/TiO2)N/D/(TiN/TiO2)N/Glass as shown in Figure 1. N is the number of periods. This structure consists of two dielectric media of thickness d1 and d2 with refractive indices n1 and n2. The structure is defected by a cavity between two identical periodic structures filled with various concentrations of TB blood samples. The thickness of this cavity is d3 with a refractive index n3. Our structure is kept between the air and a substrate layer (glass). These materials (TiN/TiO2) are matching with the experimental work by Wei et al.32. We can assume in this stage d3=209 nm. We have different concentrations of blood samples for TB patients with different refractive indices from

*e-mail: arafa.hussien@science.bsu.edu.eg
experimental work by Reddy et al.\textsuperscript{33}. We change the thickness of the defect layer and incident angle for s-polarized light to optimize the structure performance. By utilizing TMM, we can obtain the interaction between the incident light and the structure by the following equations\textsuperscript{5,34-36}:

\begin{equation}
M = \begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix} = D_o^{-1} \left( D_1 P_1 D_1^{-1} D_2 P_2 D_2^{-1} \right)^N D_s, \tag{1-a}
\end{equation}

\begin{equation}
M_l = \begin{pmatrix} \cos(k_l d_l) & j q_l \sin(k_l d_l) \\ j q_l \sin(k_l d_l) & \cos(k_l d_l) \end{pmatrix}, \tag{1-b}
\end{equation}

where, \( M_l \) is the matrix for individual layer \( l (l=A,B,C) \), then, the transmittance can be obtained based on the matrix elements to be:

\begin{equation}
T = \left| \frac{2 p + \left( (M_{11} + M_{12} p) p + M_{21} + M_{22} p \right)^N}{p} \right|^2, \tag{2-a}
\end{equation}

\begin{equation}
p = n \cos(\theta_s). \tag{2-b}
\end{equation}

Thus, the reflectance is given by:

\begin{equation}
R = 1 - T \tag{3}
\end{equation}

The transmittance (T) and the reflectance (R) are obtained according to the following relations\textsuperscript{12,37}.

\begin{equation}
R = \left| \frac{M_{21}^2}{M_{11}} \right|^2, \tag{4-a}
\end{equation}

\begin{equation}
T = \left| \frac{1}{M_{11}} \right|^2. \tag{4-b}
\end{equation}

The ratio of the change in the location of defect mode (\( \Delta \lambda \)) concerning the change in the refractive index of the defect layer (\( \Delta n \)) is called the sensitivity:

\begin{equation}
s = \frac{\Delta \lambda}{\Delta n}. \tag{5}
\end{equation}

The refractive index and peak resonant position of the normal blood sample are used as references to calculate \( \Delta \lambda \) and \( \Delta n \) for the different TB blood samples.

3. Results and Discussion

In Figure 2, we calculate the transmission spectrum of the structure. It illustrates the relation between transmittance spectra and wavelength range for defective 1D-PC at a thickness of the defect layer equals \( d_3 \). The thickness of TiN (\( d_1 \)) is 100 nm with refractive index \( n_1 = 1.2887 \) and the thickness of TiO\(_2\) (\( d_2 \)) is 109 nm with refractive index \( n_2 = 2.6143 \). Also, we utilize the normal blood sample as a defect layer at the number of periods \( N=7 \) and normal incidence \( \theta = 0^\circ \).

The PBG is noticed in Figure 2 shared between the visible and infrared region with left and right edges \( \lambda_L = 710 \text{ nm} \), and \( \lambda_R = 1038 \text{ nm} \), respectively. The bandwidth of the PBG is equal to 328 nm. The electromagnetic waves cannot propagate through structure at this PBG range except at only one wavelength which is called defect resonant mode. We can observe this defect peak in the PBG region with a high transmission rate reaches 99.99%.

Now, we add the infected TB samples (TB1, TB2, TB3, and TB4) as a defect layer within the present structure, and then we can obtain different results as shown in Figure 3. The significance of the defect layer in Figure 3 illustrates a
blue-shift in the position of the defect mode with changing the defect layer from TB1 to TB4 due to the decrease of the refractive indices of these samples, according to Table 1. The most infected sample (TB1) has the least refractive index. This behavior is matching the condition of standing wave:\(^6\)

\[ \Delta = m\lambda = n_{\text{eff}}G, \]

where \( \Delta \) is the optical path difference, \( m \) is an integer, \( \lambda \) is the wavelength of the incident light, \( n_{\text{eff}} \) is the effective refractive index of the defective 1D-PC, and \( G \) is the geometric path difference. The sensitivity is approximately \( 242.5 \) nm/RIU at incident angle \( \theta = 0^\circ \), the number of periods \( N=7 \) periods, and defected layer thickness is \( d_3=209 \) nm.

### 3.1. The selectivity of the sensor

Both Table 1 and Figure 3 clear the high selectivity of the proposed sensor for different diseases because each disease has a different value of the refractive index. As Polyacrylamide has the highest value of the refractive index, the defect peak that represents it appeared at the highest wavelength at 900.7 nm. Then the defect peaks of the cancer cells appeared from 888.7 nm (for MCF-7) to 886.1 nm (for Jurkat). Also, the defect peak continues to blue-shifts for hemoglobin to 833.7 nm as a result of the decreasing value of the refractive index of it. Finally, the peaks of TB infected samples appeared at the lowest wavelength because it has the lowest value of refractive indices. So, the proposed sensor has high selectivity.

### 3.2. The effect of the defect layer thickness

In this part, we will study the effect of increasing the TB sample layer thickness. If we changed the defect layer thickness within the structure from 209 nm to 1000 nm, we will notice that the number of defect peaks increases and shifted to a high wavelength region with the increase of the thickness of the defect layer as shown in Figure 4. This result agrees with previous works\(^{39,41}\). Therefore, we will use high thicknesses for the defect layer and compare them to get a sensor with high sensitivity. It is clear in Figure 4 that the resonant peak is shifted to a high wavelength region by increasing the defect layer thickness until it gets out from the PBG range and another peak enters the PBG.

It is clear from Figure 5 that sensitivity increases rapidly to be \( S=650 \) nm/RIU by increasing the defect layer thickness from \( d_3=209 \) nm to \( d_3=6000 \) nm. Also, a few increasing in the sensitivity to \( S=687.5 \) nm/RIU is noticed when the defect layer thickness increased from \( d_3=6000 \) nm to \( d_3=12000 \) nm. This behavior is matching the experimental and theoretical work in reference\(^{39,40,42}\). From the foregoing, increasing the geometric path difference of the defect layer leads to increasing sensitivity.

| Name of blood constituent | Refractive index |
|---------------------------|-----------------|
| Polyacrylamide            | 1.452           |
| MCF-7 cancer              | 1.401           |
| MDA-MB-231 cancer         | 1.399           |
| PC12 cancer               | 1.395           |
| HeLa cancer               | 1.392           |
| Jurkat cancer             | 1.390           |
| Hemoglobin                | 1.380           |
| TBN                       | 1.351           |
| TB1                       | 1.348           |
| TB2                       | 1.347           |
| TB3                       | 1.345           |
| TB4                       | 1.343           |

Figure 3. Transmittance spectra of defected PC with different blood components at \( N=7, \theta = 0^\circ \) and \( d_3=209 \) nm.

Figure 4. Transmittance spectra of defected 1D-PC by increasing the thickness of the defect layer for TBN at \( N=7 \) and incident angle \( \theta = 0^\circ \).
due to improving the interactions between light and blood TB samples\textsuperscript{42}. Hence, strong electric field confinement is associated with defective 1D-PC and thus enhances the performance of the defective 1D-PC as a biosensor. The maximum defect layer thickness which we considered in the proposed structure is $d_3=12000 \text{ nm}$ because another increase in the thickness causes the appearance of new peaks on the region of the electromagnetic wave spectra with a very small increase in the sensitivity.

4. Effects of Incident Angle

Here, the effect of changing the incident angle of the electromagnetic wave on the sensitivity of the proposed sensor will be studied. Figure 6 illustrates the behavior of the proposed sensor by changing the incident angle. At a certain defect layer thickness, $d_3=12000 \text{ nm}$, the increasing of the incident angle shifts the position of defect mode to a lower wavelength region. The behavior in these results can be explained based on Bragg-snell law\textsuperscript{40}.

$$m \lambda = 2d \sqrt{n_{\text{eff}}^2 - \sin^2 \theta} ,$$

where $m$ is the constructive diffraction order, $\lambda$ is the wavelength of the maximum reflected intensity, $d$ is the period, $n_{\text{eff}}$ is the effective refractive index of the defective 1D-PC, and $\theta$ is the angle of incidence. By increasing the incident angle in Figure 6, the sensitivity of the proposed sensor rapidly increases from $S=687.5 \text{ nm/RIU}$ at $\theta = 0^\circ$ to be $S=1375 \text{ nm/RIU}$ at $\theta = 80^\circ$. On the other hand, the transmittance of the defect peak decreases from 99% to 51%. For more increase in the incident angle, the transmittance decreases to 20% with a small increase in the sensitivity. So, the angle of $\theta = 80^\circ$ will be the optimum angle.

5. Effects of the Number of Periods

As clear in Figure 7, by increasing the number of periods from 4 to 6, the peaks begin to be sharp, and the
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The defect modes should have a high-quality factor for high-performance biosensor design. By calculating the quality factor, it leads to accurate sensor measurements. The quality factor can be calculated by this equation:

\[ Q = \frac{\lambda_d}{\text{FWHM}} \]  

where \( \lambda_d \) is the resonant wavelength and FWHM is the full width at half maximum of the transmission peak of defect mode. The resonant peaks become broader for the high TB concentration sample. From our proposed structure the simulation results reveal that the suggested biosensor has a Q-factor of about \( 2 \times 10^4 \) as shown in Table 2. It is known that a high Q-factor means a sharp resonant peak\(^3\). The ratio of sensitivity to the full width at half maximum of the resonant peaks is called the figure of merit (FoM):

\[ \text{FoM} = \frac{S}{\text{FWHM}} \]  

As clear in Table 2, the FoM value of the sensor is about \( 3.5 \times 10^4 \text{ RIU} \). Finally, the limit of detection for our suggested sensor is calculated from this equation\(^{41,42}\):

\[ \text{LoD} = \frac{\lambda}{20 \times S \times Q} \]  

As clear in Figure 8 and Table 2, LoD equals \( 1.5 \times 10^{-6} \text{ RIU} \). The value of LoD is very low that means the proposed sensor is good as it capable to resolve very small changes in the refractive index.

As clear in Table 3, the sensitivity of our proposed structure is higher than that previously reported for other structures. In 2020, Ramanujam et al. studied a theoretical sensitivity of a defected ring mirror 1D-PC for detecting mycobacterium tuberculosis bacteria. They achieved a sensitivity of 700 nm/RIU. The proposed structure achieved twice the value of sensitivity.

6. Conclusion

In the current work, we have simply constructed a theoretical strategy for a photonic detector via a 1D-PC consists of alternating layers to detect tuberculosis disease. The effect of different tuberculosis blood concentrations, changing the thickness of the defect layer, angle of the incident light, and the number of periods on the performance of the
proposed design was studied. By changing the concentrations of the tuberculosis blood sample from normal to infected samples, the defect peak is shifted to a lower wavelength region. Increasing the defect layer thickness and the angle of incidence enhance the sensitivity of the proposed sensor and the sensitivity reached 1390 nm/RIU and the LoD is about \(1.5 \times 10^{-6} \text{RIU}\).

7. References

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