Bone ongrowth and mechanical fixation of implants in cortical and cancellous bone

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William Robert Walsh
UNSW Sydney
✉️ w.walsh@unsw.edu.au Corresponding Author
ORCID: 0000-0002-5023-6148

Matthew Henry Pelletier
UNSW Sydney

Nicky Bertollo
UNSW Sydney

Vedran Lovric
UNSW Sydney

Tian Wang
UNSW Sydney

Per Morberg
Umea Universitet Medicinska fakulteten

William Chase Harington Parr
UNSW Sydney

Dario Bergadano
Medacta International

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Abstract

Background What is the right surface for an implant to achieve biological fixation? Surface technologies can play important roles in encouraging interactions between the implant surface and the host bone to achieve osseointegration. Pre-clinical animal models provide important insight into in-vivo performance related to bone ongrowth and implant fixation.

Methods A large animal model was used to compared the in vivo response of HA and plasma sprayed titanium coatings in a well reported adult ovine model to evaluate bone ongrowth in terms of mechanical properties in cortical sites, histology and histomorphometry in cortical and cancellous sites at 4 and 12 weeks.

Results Titanium plasma sprayed surfaces outperformed the HA coated samples in push-out testing in cortical sites while both surfaces supported new bone ongrowth and remodeling in cortical and cancellous sites.

Conclusions While both HA and Ti plasma provided an osteoconductive surface for bone ongrowth, the Ti plasma provided a more robust bone-implant interface that ideally would be required for load transfer and implant stability in the longer term.

Introduction

Implant stability remains the foundation to which clinical success can be built upon for any implant in bone be it a dental implant \([1, 2]\) or joint replacement system \([3-5]\).

Surgical exposure and bone preparation combined with advances in manufacturing, surface technology and geometry participate in primary stability and osseointegration during the healing process. Osseointegration, where a direct living bone – implant interface \([1, 2]\) is achieved through bone ongrowth to a surface or ingrowth into porous domains dictates load transfer \([6]\), bone remodeling and long-term fixation. Importantly, new bone formation on a surface can be encouraged by material, surface topology \([7-9]\),
porosity [3, 4, 10, 11] and chemistry [12, 13]. Improving both the rate, quantity and quality of osseointegration has been the topic of research for decades.

What is the right surface for an implant? How rough or porous or coated does a material have to be facilitate fixation for a successful clinical outcome? The vast number of material science and manufacturing techniques available today is astounding. Choosing the “best” surface needs to consider design, manufacturing, cleaning, sterilization, mechanical properties, biocompatibility, implantation and in vivo response. Clearly this is a big task for all stakeholders involved in arthroplasty with the aim of achieving the best clinical outcome. The anatomic site also plays an important role in choosing an implant and a surface where osseointegration is part of the clinical paradigm [14].

Surface technologies can play important roles in encouraging interaction between the implant surface and the host bone. Hydroxyapatite (HA) coating on metal substrates have an extensive material science and preclinical foundation [7, 8, 15] as well as clinical and retrieval data [16] supporting this technology. An HA coating presents a surface that can broadly be compared to the mineral component of bone [17] that can participate in protein adsorption, cellular attachment and ideally promote osseointegration. Coating metal surfaces with titanium can also be achieved using plasma spraying techniques to provide a rough surface for bony fixation [13, 18–20]. This technology also has preclinical data [21, 22] and clinical data [18, 19, 21, 23, 24] to support its use.

This study used radiographic, mechanical testing and histology in a well reported adult ovine model to evaluate osseointegration of two commonly used arthroplasty implant surface technologies in cortical and cancellous bone [7, 8, 12, 13, 25–30]. The null hypothesis was that there were no differences in bone fixation and mechanical properties as well as histological reaction between a hydroxyapatite coated titanium alloy and a titanium plasma coated titanium alloy dowel.
Materials And Methods

Titanium alloy implants in the form of cylindrical dowels (6 × 25 mm) were used in this study. The implants were vacuum plasma sprayed Ti or grit blasted and coated with 80 microns of hydroxyapatite. One implant from each group was used for surface characterisation. Stereozoom images were taken at 1-10x magnifications using an M125C Encoded Stereo Microscope (Leica microsystems, Wetzlar, Germany) and electron microscopy following sputter coating Emitech K575X Sputter Coater (Quorum Technologies, Lewes, United Kingdom) with FEI Nova NanoSEM 230 field-emission scanning electron microscope (FE-SEM) (Thermo Fisher Scientific, Waltham, USA). Implant surface roughness was performed with Olympus DSX510 Digital Microscope (Olympus Corp, Tokyo Japan). A portion of the HA coating was removed with a scalpel blade and absorbance spectra generated between 400 and 4000 cm\(^{-1}\) based on 64 background subtracted scans using a Spectrum Two FT-IR Spectrometer (PerkinElmer, Waltham, USA). A hydroxyapatite standard was obtained from a local supplier (Sigma-Alderich, CAS: 1306-06-5) and analysed under the same conditions for comparison.

All surgical procedures were performed following institutional ethical clearance on 8 adult cross-bred wethers (2 years old). Animals were received from our open paddock farm and acclimatized for a minimum of 7 days prior to surgery in pairs on deep litter in climate-controlled facilities. Pre-emptive analgesic was provided using transdermal fentanyl patches 24 hours before surgery and to provide smoother sedation and anaesthetic induction [13]. Animals were sedated with an intramuscular (IM) injection of Xylazine (0.2 mg/kg) followed by Ketamine IM (6 mg/kg) 15 minutes later. All animals received 1 g of Cephalothin (18 – 22 mg/kg) intravenously and 5 mL oxytetracycline (200 mg/mL) at 18 to 22 mg/kg intramuscularly. Benacillin (Procaine penicillin 150 mg/mL) 1 mL/10 kg was
given IM. The transdermal fentanyl patches were replaced with new ones (to provide a minimum of 72 hours of postoperative analgesia [31]) and Carprofen (Rimadyl 50 mg/mL) at 3 to 4 mg/kg IM given before surgery. Animals were transferred to the operating room table and anaesthesia maintained using isoflurane (1.5%–3%) and oxygen (2 L/min) throughout the procedures. Animals were allowed weight bearing immediately following recovery from anaesthetic. Animals were monitored and recorded daily for the first 7 days. After 7 days they were monitored daily but only recorded weekly.

This bilateral model allows two cancellous and three bicortical implants per side. Ten dowels (five each side) were implanted using an established osseointegration model in two year old adult cross bred wethers [7, 8, 12, 13, 25–30]. The sample size for this study was 8 implants per group in cortical sites and 5 implants per group in cancellous sites. This sample size has been shown to provide adequate power (Beta error 10%) at Alpha set to 0.05 to detect approximately a 20% difference between groups with a standard deviation of 15%. All implants were randomized in the cortical and cancellous sites. Sites were prepared with saline irrigation during drilling to minimise any thermal damage. Bicortical sites in the anteromedial aspect of the tibia were prepared with a 4.5 mm three-fluted drill (Surgibit, Orthopedic Innovations, Sydney) to create a pilot hole followed by a 6 mm diameter drill-bit for line to line implantation of the dowels. Dowels in the cancellous sites were implanted using a gap model [26] in the cancellous bone of medial distal femoral condyles and proximal tibias. A 4.5 mm three-fluted drill pilot hole was created, over-drilled with 5.5 mm drill to create a press fit for the dowels with the site. A step drill (6, 8 and 10 mm) was used to create a 6 mm hole for the line to line, 8 mm hole for the 1 mm gap and 10 mm hole for a 2 mm gap. The implants were inserted using an impactor into the press fit drilling scenario and centralized in the hole. The periosteum, soft tissues, and dermis were closed in layers using 3 – 0 and 2 – 0 resorbable suture, respectively.
Animals were euthanized following sedation at 4 weeks and 12 weeks. The surgical sites were examined for signs of adverse reaction or infection. The harvested bones were X-rayed in the anteroposterior and lateral views using a Faxitron (Faxitron, Wheeling, IL) and digital plates (AGFA CR MD4.0 Cassette). Radiographs in the anteroposterior and lateral views to determine implant placement, adverse bony reactions as well as evidence of radiographic changes at the implant bone interface. Cancellous sites were isolated using a saw, fixed in cold phosphate buffered formalin and processing using routine polymethylmethacrylate (PMMA) embedding. The cortical sites were isolated using a saw in the axial plane. These samples were sectioned in the sagittal plane to isolate the medial and lateral specimens for push out testing followed by PMMA hard-tissue histology. Prior to mechanical testing the specimens were polished using a Buehler polisher perpendicular to the long axis of the implant to remove any periosteal bone overgrowth. Implants were tested for implant-bone interface shear strength using a standard push-out test. Specimens were tested at 0.5 mm/min on a calibrated servo-hydraulic testing machine (MTS Mini Bionix®, MTS Systems Inc., Minneapolis, Minnesota, USA). The cortical thickness was obtained from histology images and was used in shear stress calculations following formalin fixation and PMMA embedding. Peak Load, stiffness and energy to failure was determined by plotting of the load-deformation curve and calculated using MatLab script (MATLAB R2016a, MathWorks, Natick, Massachusetts, USA).

The shear stress was calculated according to the following relation:

$$\sigma = \frac{Load}{\left(\frac{c_1 + c_2}{2}\right) \pi \cdot d_i}$$

Equation 1: Shear stress calculation where \(\sigma\) is shear stress, \(c_1\) and \(c_2\) are cortical
Formalin-fixed samples were sequentially dehydrated in increasing concentrations of ethanol before infiltration in methylmethacrylate and polymerization using established techniques. Embedded cortical and cancellous dowels were sectioned along the long axis of the implants using a Leica SP 1600 Microtome (Leica Biosystems, Nussloch, Germany). A minimum of two thin (~15 – 20 micron) sections were cut from each dowel. The sections were briefly etched in acidic ethanol (98 mL ethanol 96% and 2 mL HCl 37%) and stained with methylene blue followed by basic fuchsin. The stained slides were reviewed under low magnification to provide an overview of the section and histomorphometry. The implant-bone interface and local reactions were carefully examined at higher magnification for the presence of inflammatory cells or local particulate in the cancellous and cortical sites. The cancellous sites were also examined based on the implant conditions at press-fit, line to line, 1- and 2-mm gaps for local reactions.

PMMA images at the bone implant interfaces were used to determine bone ongrowth and percentage of bone-contact with the implant [12, 13, 26, 27]. The proximal and distal bone – implant interfaces of the cortical bone were evaluated for each slide and a mean value based on 2 slides per site was used for statistical analysis. Similarly, the proximal and distal bone – implant interface in the cancellous sites was used to provide a mean bone ongrowth value for each implantation condition.

Mechanical and histomorphometric data was analysed using a two-way Analysis of Variance (implant, and time) for cortical as well as cancellous sites and post-hoc testing when appropriate using SPSS (version 25, IBM, Armonk, New York, USA).

Results

The surface topology of the implants from stereo-zoom and electron microscopy images is presented in Figs. 1 and 2. Differences in the surface topologies can be seen for both
groups at various magnifications up to 100,000x with the globular appearance of calcium phosphate as well as the lack of distinct surface features for the Ti plasma coating beyond 5000x magnification. A uniform HA coating was present on the Ti-HA samples with a surface roughness Ra of 5.557 microns. The Ra surface roughness of the Ti-Plasma revealed a surface was 22.906 microns. The FTIR spectra (Fig. 3) of HA standard and the HA coating collected from the implant revealed the typical spectra of calcium phosphate with major corresponding mineral peaks of Phosphate (PO$_4^{3-}$) and Carbonate (CO$_3^{2-}$) identified.

Surgery was completed without incident and no adverse events were encountered during this study. All wounds were well healed and there was no evidence of adverse reactions to either implant group in cortical or cancellous sites at both time points. Radiographs at 4 and 12 weeks revealed no evidence of adverse reactions in cortical and cancellous sites. A progression in healing in the cortical sites was noted with time for both groups as well endosteal bone formation within the marrow cavity.

Mechanical testing data is summarized in Table 1. The mechanical properties increased with time for both groups between 4 and 12 weeks (P < 0.05). No Statistical differences at the P < 0.05 level was found at 4 weeks between groups. Statistical differences were detected at 12 weeks for force, energy and shear stress with Ti Plasma group outperforming the Ti HA group.

| Group       | Weeks | Force (N) Mean | Force (N) SD | Energy (Nmm) Mean | Energy (Nmm) SD | Stiffness (N/mm) Mean | Stiffness (N/mm) SD | Shear Stress MPa Mean | Shear Stress MPa SD |
|-------------|-------|----------------|--------------|-------------------|----------------|-----------------------|---------------------|-----------------------|---------------------|
| Ti HA       | 4     | 876.3          | 327.6        | 247.7             | 206.6          | 3879.2                | 1612.1              | 10.6                  | 3.3                 |
|             | 12    | 1894.9         | 519.5        | 483.4             | 290.7          | 8724.0                | 3727.4              | 18.9                  | 4.0                 |
| Ti Plasma   | 4     | 1121.2         | 541.2        | 358.1             | 260.8          | 4281.1                | 1663.0              | 11.8                  | 4.9                 |
|             | 12    | 3110.9         | 890.6        | 735.3             | 215.0          | 10795.0               | 3438.5              | 26.5                  | 3.4                 |

Examples of the histology in the cortical and cancellous sites at 4 and 12 weeks are presented in Figs. 4–6. The cortical sites were implanted in a line to line manner and
revealed new bone formation directly on the HA coating as well as on the Ti Plasma coating without any intervening fibrous tissue interfaces at 4 and 12 weeks. Bone remodeling occurred with time for both groups in the cortical sites without any evidence of HA coating resorption between 4 and 12 weeks. Histology in the cancellous sites in the 4 implantation conditions (2 mm gap, 1 mm gap, line to line and press fit) demonstrated the positive attributes of the HA coating in the 2 and 1 mm gap at 4 weeks with new woven bone ongrowth while the line to line and press fit conditions were similar. Cancellous histology at 12 weeks improved with time without the presence of any fibrous tissue and was similar for both groups.

Histomorphometry for bone ongrowth in the cortical sites improved with time for both groups (P < 0.05) while no differences were detected between groups at 4 and 12 weeks (Fig. 7). Histomorphometry in the cancellous sites at 4 weeks (Fig. 8) revealed differences between the Ti HA and Ti Plasma in the 2 mm and 1 mm gap and press fit conditions, with Ti HA exhibiting significantly (P < 0.05) more bone ongrowth than the plasma sprayed Ti group, while no differences were detected in the line to line or press fit conditions. Histomorphometry in the cancellous sites at 12 weeks (Fig. 8) revealed a difference between groups in the press fit conditions, with Ti HA exhibiting significantly (P < 0.05) more bone ongrowth than the plasma sprayed Ti group. No other differences were detected at 12 weeks.

Discussion

In vitro and pre-clinical studies are often used as part of the development of any medical devices as a precursor to human clinical use. An understanding of how materials and their coatings respond in vivo prior to human clinical use is an important component in the development as well as evolution of medical devices. The current study compared the in vivo response of a Ti alloy implant coated with HA compared to a plasma sprayed Ti in an
established ovine model where implants were placed in cortical as well as cancellous sites at 4 and 12 weeks. This study was limited in the lack of long-term data where bone remodeling as well as resorption of the HA coating could play a role. While both HA and Ti plasma provided an osteoconductive surface for bone ongrowth, the Ti plasma provided a more robust cortical bone-implant interface that ideally would be required for load transfer and implant stability in the longer term.

Differences in chemistry and macro-, micro- and nano- topography were present between the Ti-HA and Ti Plasma implants as shown in the stereozoom, electron microscopy, surface roughness and FTIR (Figs. 1 and 2). The bone-implant interface available for osseointegration with these features plays an important role in the in vivo response. The SEM and FTIR of the Ti-HA coating was similar to osteoconductive bone graft [32, 33] and differs from osteoinductive calcium phosphate [34, 35].

Mechanical testing revealed the Ti Plasma implants outperformed the Ti HA implants in the cortical sites at 4 weeks and achieved statistical significance at 12 weeks (Table 1). The fixation provided by the Ti Plasma surface can be attributed to the plasma titanium coating features that presents a large surface area for bony contact and some ingrowth as well as ongrowth due to the coating topography as shown in the surface roughness and imaging data. New bone formation into the peaks and valleys of the Ti Plasma surfaces allows for fixation at the micro level allowing the bone-implant interfaces a greater capacity to resist shear forces. Mean bone ongrowth to the implant surfaces were similar between groups at 4 and 12 weeks and improved with time. Four-week histology at the implant-bone interface in cortical sites demonstrated direct bone ongrowth to the surface in both groups without the presence of any intervening fibrous tissues or inflammatory cellular response. Cortical histology at 12 weeks presented an increase in bone maturity in both groups along with presence of Haversian bone demonstrating remodeling. Bone was
in direct contact with the HA coating which did not appear to have resorbed to any extent within the time frame of this experiment. The cancellous gap model was able to demonstrate the potential benefits of the HA coating where direct bone contact is limited. New bone was observed in the cancellous gap sites in the Ti HA group that could be attributed to the presence of the calcium phosphate coating and local biological benefits [8, 36]. This effect was particularly apparent at the early (4 week) time point.

Preclinical studies are models and regardless of complexity cannot replicate the human scenario where loading, articulations, wear particles and patient related factors including co-morbidities play a role in the overall clinical outcomes. Preclinical studies have limitations but allow for tighter control of variables such as animal age, implant geometry, implantation conditions that can help identify the advantages as well as disadvantages of different technologies. A variety of large animal preclinical models have been used to examine the bone-implant interface with cylindrical dowels to evaluate bone ingrowth and ongrowth to different materials and surface coatings in cortical sites in sheep [7, 8, 12-14, 25-28, 37, 38] and dogs [11, 15, 39-41] as well as cancellous sites as performed in this study [12, 13, 26, 28] and intercondylar sites [37, 38, 42]. Care should always be taken when making the jump to the human clinical scenario. A strength of all these models is however in the detailed reporting of implant characterization, mechanical properties and histology at the bone-implant interface that allows for important comparisons and contrasts, which is generally difficult to achieve with clinical implantations. The bicortical implant sites enables a direct measure of implant fixation and calculation of shear stress and corresponding histology at the implant-bone interface.

List Of Abbreviations

σ is shear stress, c1 and c2 are cortical thickness on each side of the implant in the histology section and d is implant diameter
Declarations

Ethics approval and consent to participate
UNSW Ethics approval 15/29B
Consent for publication
Not applicable
Availability of data and materials
The datasets used and/or analysed during the current study are available from the corresponding author on reasonable request.
Competing interests
None
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DB is an employee of Medacta International
Authors' contributions
WRW and DB designed the study and wrote the manuscript, WRW, MHP, NB, TW performed the experiments and analysed the data, PM and WCP contributed to planning and manuscript review.
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References

1. Albrektsson T, Brånemark P-I, Hansson H-A, and Lindström J, Osseointegrated titanium implants: requirements for ensuring a long-lasting, direct bone-to-implant anchorage in man. Acta Orthopaedica Scandinavica, 1981. 52(2): p. 155-170.
2. Branemark P-I, Osseointegration and its experimental background. J prosthet Dent, 1983. 50: p. 399-410.
3. Camron H, Pilliar R, and Macnab I, The rate of bone ingrowth into porous metal. Journal of biomedical materials research, 1976. 10(2): p. 295-302.
4. Spector M, Historical review of porous-coated implants. The Journal of Arthroplasty, 1987. 2(2): p. 163-177.
5. Bloebaum RD, Mihalopoulus NL, Jensen JW, and Dorr L, Postmortem analysis of bone growth into porous-coated acetabular components. JBJS, 1997. 79(7): p. 1013-22.
6. Ducheyne P, Aernoudt E, De Meester P, Martens M, Mulier JC, and Van Leeuwen D,
Factors governing the mechanical behavior of the implant-porous coating-trabecular bone interface. Journal of biomechanics, 1978. 11(6): p. 297-307.

7. Svehla M, Morberg P, Zicat B, Bruce W, Sonnabend D, and Walsh WR, Morphometric and mechanical evaluation of titanium implant integration: comparison of five surface structures. J Biomed Mater Res, 2000. 51(1): p. 15-22.

8. Svehla M, Morberg P, Bruce W, Zicat B, and Walsh WR, The effect of substrate roughness and hydroxyapatite coating thickness on implant shear strength. J Arthroplasty, 2002. 17(3): p. 304-11.

9. Novaes Jr AB, Souza SLSd, Barros RRMd, Pereira KKY, Iezzi G, and Piattelli A, Influence of implant surfaces on osseointegration. Brazilian dental journal, 2010. 21(6): p. 471-481.

10. Bobyn J, Pilliar R, Cameron H, and Weatherly G, The optimum pore size for the fixation of porous-surfaced metal implants by the ingrowth of bone. Clinical orthopaedics and related research, 1980(150): p. 263-270.

11. Bobyn J, Stackpool G, Hacking S, Tanzer M, and Krygier J, Characteristics of bone ingrowth and interface mechanics of a new porous tantalum biomaterial. The Journal of bone and joint surgery. British volume, 1999. 81(5): p. 907-914.

12. Bertollo N, Sandrini E, Pria PD, and Walsh WR, Osseointegration of Multiphase Anodic Spark Deposition Treated Porous Titanium Implants in an Ovine Model. The Journal of Arthroplasty, 2015. 30: p. 484-488.

13. Walsh WR, Bertollo N, Christou C, Schaffner D, and Mobbs RJ, Plasma-sprayed titanium coating to polyetheretherketone improves the bone-implant interface. The Spine Journal, 2015. 15(5): p. 1041-1049.

14. Walsh WR, Pelletier MH, Wang T, Lovric V, Morberg P, and Mobbs RJJTSJ, Does implantation site influence bone ingrowth into 3D-printed porous implants? The Spine
Journal, 2019. 11( ): p. 1885-1898.

15. Cook SD, Thomas KA, Kay JF, and Jarcho M, Hydroxyapatite-coated titanium for orthopedic implant applications. Clinical orthopaedics and related research, 1988. 232(225): p. 43.

16. Bauer TW, Stulberg BN, Ming J, and Geesink RG, Uncemented acetabular components: histologic analysis of retrieved hydroxyapatite-coated and porous implants. The Journal of arthroplasty, 1993. 8(2): p. 167-177.

17. Surmenev RA, Surmeneva MA, and Ivanova AAJAb, Significance of calcium phosphate coatings for the enhancement of new bone osteogenesis-a review. Acta biomaterialia, 2014. 10(2): p. 557-579.

18. Hozack WJ, Rothman RH, Eng K, and Mesa J, Primary cementless hip arthroplasty with a titanium plasma sprayed prosthesis. Clinical orthopaedics and related research, 1996(333): p. 217-225.

19. Lombardi AV, Berend KR, Mallory TH, Skeels MD, and Adams JB, Survivorship of 2000 tapered titanium porous plasma-sprayed femoral components. Clinical orthopaedics related research, 2009. 467(1): p. 146-154.

20. Meding JB, Keating EM, Ritter MA, Faris PM, and Berend ME, Minimum ten-year follow-up of a straight-stemmed, plasma-sprayed, titanium-alloy, uncemented femoral component in primary total hip arthroplasty. JBJS, 2004. 86(1): p. 92-97.

21. Mallory TH, Lombardi Jr AV, Leith JR, Fujita H, Hartman JF, Capps SG, Kefauver CA, Adams JB, and Vorys GC, Minimal 10-year results of a tapered cementless femoral component in total hip arthroplasty. The Journal of arthroplasty, 2001. 16(8): p. 49-54.

22. Matassi F, Botti A, Sirlelo L, Carulli C, and Innocenti M, Porous metal for orthopedics implants. Clinical Cases in Mineral and Bone Metabolism, 2013. 10(2): p. 111.
23. Bourne RB, Rorabeck CH, Patterson JJ, and Guerin J, Tapered titanium cementless total hip replacements: a 10-to 13-year followup study. Clinical Orthopaedics Related Research, 2001. 393: p. 112-120.

24. Marshall AD, Mokris JG, Reitman RD, Dandar A, and Mauerhan DR, Cementless titanium tapered-wedge femoral stem: 10-to 15-year follow-up. The Journal of arthroplasty, 2004. 19(5): p. 546-552.

25. Svehla M, Morberg P, Bruce W, and Walsh WR, No effect of a type I collagen gel coating in uncemented implant fixation. Journal of Biomedical Materials Research - Part B Applied Biomaterials, 2005. 74(1): p. 423-428.

26. Bertollo N, Matsubara M, Shinoda T, Chen D, Kumar M, and Walsh WR, Effect of surgical fit on integration of cancellous bone and implant cortical bone shear strength for a porous titanium. J Arthroplasty, 2011. 26(7): p. 1000-7.

27. Chen D, Bertollo N, Lau A, Taki N, Nishino T, Mishima H, Kawamura H, and Walsh WR, Osseointegration of porous titanium implants with and without electrochemically deposited DCPD coating in an ovine model. J Orthop Surg Res, 2011. 6: p. 56.

28. Bertollo N, Da Assuncao R, Hancock NJ, Lau A, and Walsh WR, Influence of Electron Beam Melting Manufactured Implants on Ingrowth and Shear Strength in an Ovine Model. J Arthroplasty, 2012. 27(8): p. 1429-1436.

29. Walsh WR, Pelletier MH, Bertollo N, Christou C, and Tan C, Does PEEK/HA enhance bone formation compared with PEEK in a sheep cervical fusion model? Clinical Orthopaedics and Related Research®, 2016. 474(11): p. 2364-2372.

30. Mobbs RJ, Parr WC, Choy WJ, McEvoy A, Walsh WR, and Phan K, Anterior Lumbar Interbody Fusion Using a Personalized Approach: Is Custom the Future of Implants for Anterior Lumbar Interbody Fusion Surgery? World neurosurgery, 2019. 124: p. 452-458.
31. Christou C, Oliver RA, Rawlinson J, and Walsh WR, Transdermal fentanyl and its use in ovine surgery. Research in veterinary science, 2015.

32. Walsh WR, Oliver RA, Christou C, Lovric V, Walsh ER, Prado GR, and Haider T, Critical size bone defect healing using collagen-calcium phosphate bone graft materials. PloS one, 2017. 12(1): p. e0168883.

33. Walsh WR, Vizesi F, Michael D, Auld J, Langdown A, Oliver R, Yu Y, Irie H, and Bruce W, Beta-TCP bone graft substitutes in a bilateral rabbit tibial defect model. Biomaterials, 2008. 29(3): p. 266-71.

34. van Dijk LA, Barbieri D, Barrère-de Groot F, Yuan H, Oliver R, Christou C, Walsh WR, and de Bruijn JD, Efficacy of a synthetic calcium phosphate with submicron surface topography as autograft extender in lapine posterolateral spinal fusion. Journal of biomedical materials research Part B, 2019. 107: p. 2080-2090.

35. van Dijk LA, Duan R, Luo X, Barbieri D, Pelletier M, Christou C, Rosenberg AJ, Yuan H, Barrère-de Groot F, and Walsh WR, Biphasic Calcium Phosphate with Submicron Surface Topography in an Ovine Model of Instrumented Posterolateral Spinal Fusion. JOR Spine, 2018: p. e1039.

36. De Groot K, Wolke J, and Jansen J, Calcium phosphate coatings for medical implants. Proceedings of the Institution of Mechanical Engineers, Part H: Journal of Engineering in Medicine, 1998. 212(2): p. 137-147.

37. Bloebaum R, Willie B, Mitchell B, and Hofmann A, Relationship between bone ingrowth, mineral apposition rate, and osteoblast activity. Journal of Biomedical Materials Research Part A, 2007. 81(2): p. 505-514.

38. Bloebaum RD, Abdo NT, Hofmann AA, Epperson RT, Olsen RE, and Chalayon O, Transcortical or intracondylar? Which model is accurate for predicting biomaterial attachment in total joint replacement? Journal of Biomedical Materials Research Part
39. Cook SD, Thomas KA, Kay JF, and Jarcho M, Hydroxyapatite-coated porous titanium for use as an orthopedic biologic attachment system. Clinical orthopaedics related research, 1988(230): p. 303-312.

40. Cook SD, Walsh KA, and Haddad JR, Interface mechanics and bone growth into porous Co-Cr-Mo alloy implants. Clinical orthopaedics related research, 1985(193): p. 271-280.

41. Hayashi K, Inadome T, Tsumura H, Nakashima Y, and Sugioka Y, Effect of surface roughness of hydroxyapatite—coated titanium on the bone-implant interface shear strength. Biomaterials, 1994. 15(14): p. 1187-1191.

42. Willie BM, Bloebaum RD, Bireley WR, Bachus KN, and Hofmann AA, Determining relevance of a weight-bearing ovine model for bone ingrowth assessment. Journal of Biomedical Materials Research Part A, 2004. 69(3): p. 567-576.

Figures
Figure 1

Stereo-zoom images of the implants examined in the study. A) Titanium alloy dowel coated with hydroxyapatite. B) Titanium alloy coated with plasma sprayed titanium.
Figure 2

Electron microscopy images at 1000x, 5000x, 10000x, 20,000x, 50,000x and 100,000x for A) Titanium alloy dowel coated with hydroxyapatite. B) Titanium alloy coated with plasma sprayed titanium. These images illustrate the
differences in surface topography between the two implants examined in this study.
Figure 3
FTIR spectra for the hydroxyapatite coating which was on the Ti alloy dowel compared to a standard hydroxyapatite.
Figure 4

Representative histology images in the cortical sites at 4 weeks for the A) Titanium alloy dowel coated with hydroxyapatite. B) Titanium alloy coated with plasma sprayed titanium. New bone ongrowth without any fibrous tissue was present for both groups.
Representative histology images in the cortical sites at 12 weeks for the A) Titanium alloy dowel coated with hydroxyapatite. B) Titanium alloy coated with plasma sprayed titanium. Bone remodeling without any adverse reactions was noted for both groups. The HA coating remained intact. The failure during push out testing can be seen in the low magnification image for the Ti Plasma (B).
Representative histology images in the cancellous sites (2 mm, 1 mm gaps, line to line and press fit) at 4 and 12 weeks for the A) Titanium alloy dowel coated with hydroxyapatite. B) Titanium alloy coated with plasma sprayed titanium. Histology and in the cancellous sites in the 4 implantation conditions (2 mm gap, 1 mm gap, line to line and press fit) demonstrated the positive attributes of the HA coating in the 2 and 1 mm gap at 4 weeks with new woven bone ongrowth while the line to line to line and press fit conditions were similar. Cancellous histology at 12 weeks improved with time without the presence of any fibrous tissue and was similar for both groups.
Figure 7

Histomorphometry for bone ongrowth in the cortical sites improved with time for both groups (P<0.05) while no differences were detected between groups at 4 and 12 weeks.
Figure 8
Histomorphometry in the cancellous sites at 4 weeks revealed differences between the Ti HA and Ti Plasma in the 2 mm and 1 mm gap and press fit conditions (P<0.05) while no differences were detected in the line to line implantation or press fit conditions. Histomorphometry in the cancellous sites at 12 weeks revealed a difference between groups in the press fit conditions (P<0.05). No other differences were detected at 12 weeks.