Multiple-patterning colloidal lithography-implemented scalable manufacturing of heat-tolerant titanium nitride broadband absorbers in the visible to near-infrared

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Abstract
Broadband perfect absorbers have been intensively researched for decades because of their near-perfect absorption optical property that can be applied to diverse applications. Unfortunately, achieving large-scale and heat-tolerant absorbers has been remained challenging work because of costly and time-consuming lithography methods and thermolability of materials, respectively. Here, we demonstrate a thermally robust titanium nitride broadband absorber with >95% absorption efficiency in the visible and near-infrared region (400–900 nm). A relatively large-scale (2.5 cm × 2.5 cm) absorber device is fabricated by using a fabrication technique of multiple-patterning colloidal lithography. The optical properties of the absorber are still maintained even after heating at the temperatures >600 °C. Such a large-scale, heat-tolerant, and broadband near-perfect absorber will provide further useful applications in solar thermophotovoltaics, stealth, and absorption controlling in high-temperature conditions.

Introduction
Broadband perfect absorbers1–8 have many possible uses, such as thermophotovoltaics9–11 and thermal emitters12–14, but practical applications have been limited by the lack of scalable fabrication method and by their poor thermal durability. Broadband perfect absorbers are typically realized by plasmonic nanostructures bonded to metallic reflective layer separated by a dielectric spacer in which noble metals are commonly used1,15, but these materials are costly. Therefore, refractory materials have been introduced as candidates for broadband absorbers due to their high-temperature tolerance, chemical stability, mechanical durability, and low cost16–20.

Titanium nitride (TiN) has comparable plasmonic properties to gold (Au) in the visible and near-infrared (NIR) region, and has therefore been used in solar heat generators and photodetectors21–24. However, most previous studies have used electron beam lithography to pattern the nanostructures, and this method limits a scale to a few hundred micrometers. To be implemented in practical applications, a method to fabricate TiN nanostructure in a large scale is in high demand.

Colloidal lithography is widely used to create periodic 2D nano-sized patterns on a variety of substrates. It can fabricate templates or masks for use in creation of various nanostructures, such as nanohole, nanodisk, nanopillar, and nanocone, which have been applied to various photonic devices25–28. A consecutive use of the colloidal lithography, which is referred to as multiple-patterning colloidal lithography (MPCL), enables fabrication of hierarchical...
nanostructures, such as hollow nanocone, nanotower, and nanoring\textsuperscript{29–34}. However, these methods have only been used to etch silicon or polymers, while not being extended to etch other materials.

Here, we use MPCL to fabricate a large-scale (2.5 cm × 2.5 cm) near-perfect absorber that is composed of ring-shaped TiN structures. To best of our knowledge, it is the first demonstration of applying MPCL to etch a refractory metal, which is focused on the fabrication approach to overcome the limitations of practical use as a large-scale absorber. The device has polarization-independent absorption of 95.4\% under normal incidence and high absorption at incident angles up to θ = 40° at visible and NIR wavelength (400 < λ < 900 nm). The near-perfect absorption of our device remains even after heating at temperature up to 600 °C. We expect that our cost-effective and scalable absorber is a promising candidate for large-scale applications, such as photothermal devices and thermal emitters that require polarization-independent, angle-insensitive, heat-tolerant, and broadband absorption.

Results and discussion

Device optimization and fabrication

The proposed broadband ring-shaped TiN absorber has a metal–insulator–metal (MIM) structure that uses a perfectly-reflective TiN layer, silicon dioxide (SiO\textsubscript{2}) dielectric layer, and a top composed of ring-shaped TiN nanostructures in a hexagonal array. The ring-shaped nanostructure has advantages in absorption due to its better impedance matching with air compared to disk-shaped structures\textsuperscript{16,19}, and can be fabricated in large scale using MPCL.

Particle swarm optimization (PSO)\textsuperscript{35} is used to optimize the structural parameters of the TiN absorber to have the highest absorption in the visible and NIR region. For this purpose, we develop a lab-built PSO by linking commercial software (COMSOL Multiphysics 5.5, Livelink for MATLAB, MATLAB 2019; Fig. 1a). First, finite-element method simulation is performed to calculate the absorption from randomly selected initial parameters. The objective function indicates the function to be optimized, and is defined by subtracting the square of the average absorption in 400–900 nm region from unity. Then the optimization proceeds to minimize the fitness value of this objective function. At each iteration, minimum fitness value is set as the local best. If the new local best is smaller than the minimum fitness value in history (global best), the local best is set as the new global best. The cycle is repeated until fitness converges or until the maximum number of iterations is applied.

Fig. 1 Optimization and schematic of a ring-shaped TiN absorber. a Flow chart of the particle swarm optimization (PSO) algorithm to optimize the broadband titanium nitride (TiN) ring-shaped perfect absorber. b Fitness curve of PSO algorithm. The fitness value converges to 0.026 after 100 iterations. c Schematic and parameters of a ring-shaped TiN absorber. The optimized dimensions are P = 300 nm, D = 181.09 nm, W = 79.27 nm, and H\textsubscript{ring} = 60 nm, H\textsubscript{layer} = 150 nm, and H\textsubscript{dielectric} = 58.09 nm.
The outer diameter \((D)\) and width \((W)\) of the ring structure of the top ring-shaped nanostructure, and the thickness \(H_{\text{dielectric}}\) of the SiO\(_2\) dielectric layer are considered as parameters for optimization, and other parameters such as period \(P\) and thickness of ring structure \(H_{\text{ring}}\) are fixed due to the feasible fabrication for a TiN absorber. The initial ranges of parameters are set to \(0 < D < 300\) nm and \(10 < W < 150\) nm to prevent them from exceeding the outer diameter. One hundred iterations are repeated until the optimal value is found. Each iteration considers 30 particles, so a total of 3000 particles are evaluated to identify the final parameters for optimal ring-shaped absorber. After 100 iterations, the fitness converges to \(<0.026\) (Fig. 1b).

The optimal dimensions of the proposed ring-shaped TiN absorber (Fig. 1c) are \(P = 300\) nm in a hexagonal array, \(D = 181.09\) nm, \(W = 79.27\) nm, and \(H_{\text{ring}} = 60\) nm on the layers deposited by TiN \((H_{\text{layer}} = 150\) nm) and SiO\(_2\) \((H_{\text{dielectric}} = 58.09\) nm) in sequence. As such, optimization techniques can help in designing optical structures and can be further advanced using machine learning or deep learning\(^{36-40}\).

Schematic illustration to fabricate the TiN ring-shaped absorber is described (Fig. 2a). TiN–SiO\(_2\)–TiN MIM structure is prepared on silicon substrate, then MPCL is used to prepare highly ordered TiN ring-shaped structures; the period and diameters are determined by controlling the size of the polystyrene (PS) nanosphere and the oxygen plasma etching time. A PS monolayer is firstly prepared on the top layer of the prepared MIM structure (Fig. 2b). PS nanospheres with a diameter of 300 nm are chosen to match the period between nanoring structures. The hexagonally arranged PS monolayer is etched using oxygen plasma to reduce the PS diameter to the optimized \(D\). A top TiN layer is etched using reactive ion etching (RIE) with Cl\(_2\) and BCl\(_3\) gas by using the PS beads as a mask. The RIE yields a nanodisk structure, then a second PS etching is performed to achieve the optimized \(W\) (Fig. 2c). A 8-nm thick nickel (Ni) layer is deposited as a hard mask under Cl\(_2\) gas using electron beam (e-beam) evaporator; then all remaining PS nanospheres are removed by sonication in toluene for an hour. The second TiN etching is performed (Fig. 2d). The Ni mask is removed by 1 mol/L HCl solution to complete the final TiN nanoring structure. These processes yields ring-shaped nanostructure array that is consistent with the optimized parameters (Fig. 2e). In order to fabricate elaborate nanostructure, there are several issues to be considered. First, the etching conditions must be precisely controlled\(^{41}\) because the intrinsic property of dry etching process can make the ring-shaped structure slightly tapered. Second, the uniformity of the structure can be
improved by using nanospheres with lower size distribution. Third, random tilting of the etched PS nanospheres during the RIE etching can be prevented by enhancing the adhesion between PS nanospheres and TiN layer by heating.

**Optical properties**

For numerical demonstration, we calculate absorption of the ring-shaped TiN absorber; refractive indices of TiN and SiO₂ are taken from the literature. The result shows 95.9% average absorption at 400–900 nm and the highest absorption at 650 nm (Fig. 3a). High absorption of the proposed design is experimentally demonstrated using spectroscopy. Unpolarized light is illuminated at normal incidence onto the sample. The measured spectra of ring-spectroscopy. Unpolarized light is illuminated at normal incidence without ring-shaped structure, it absorbs >31% light in the visible-NIR region. The slight difference between measurement and simulation is attributed to fabrication imperfections of placement and size distributions of the nanostructure. Photographs (Fig. 3a, inset) of ring-shaped absorber and MIM structure show obvious darkness obtained by the absorption characteristic.

To understand the mechanism of the high absorption, we examine the total power dissipation density

\[
Q_{\text{abs}} = \langle J \cdot E \rangle = \rho |E|^2 = \frac{1}{2} \varepsilon_0 \varepsilon'' \omega |E|^2
\]

where \( \rho \) is the electrical conductivity, \( \varepsilon_0 \) is the permittivity of a vacuum, \( \varepsilon'' \) is the imaginary part of the relative permittivity of the material, \( \omega \) is angular frequency, and \( |E| \) is the amplitude of the total electric field inside the material. \( Q_{\text{abs}} \) is extracted from each TiN layer. \( Q_{\text{abs}} \) can be a criterion to evaluate the contribution of the absorbed electromagnetic power from each TiN layer.

Absorption can be explained as a field localization by localized surface plasmons (LSPs) and by intrinsic loss of the material. The absorption contributions of each TiN layer verify the specific mechanisms (Fig. 3b). The LSPs occur at the surface near the nanostructures, so the absorption by the LSP should be caused by the ring-shaped nanostructure. In the region of \( \lambda > 600 \) nm, TiN exhibits metallic properties, which lead to plasmonic resonance. Thus, the absorption is dominated by the ring structure. However, compared to noble metals, such as Au, TiN has weak metallic properties, so it has localized fields inside the ring structure. In addition, unlocalized waves can pass through the top layer and arrive at the underlying TiN bulk layer due to its large skin depth. The broad high absorption is attributed to two absorptions in the ring structure and bulk TiN layers simultaneously. In the range of \( \lambda < 600 \) nm, the bottom TiN layer contributes more absorption than the ring structure does. This difference means that the intrinsic loss at the bulk TiN layer is dominant. TiN can be a lossy dielectric material in this region, so the bottom TiN layer absorbs a large portion of incident light at high frequencies.

For further investigation, the impedance-matching condition of the proposed absorber is analyzed. Under the assumptions that the absorber structures are homogeneous, the effective impedance (Fig. 4a) of the proposed structure is retrieved using the S-parameter retrieval method as

\[
z = \pm \sqrt{\frac{(1 + S_{11})^2 - S_{21}^2}{(1 - S_{11})^2 - S_{21}^2}}
\]

The effective impedance is calculated under the condition of plane wave from air. The effective impedance shows the real part of the calculated effective impedance is close to 1, and the imaginary part is close to 0, so the
impedance matches that of free space in the visible and NIR regions. Thus, reflection is weak and absorption is dominant over the desired wavelength region.

Normalized plots of electric and magnetic field distribution on the xy- and xz-planes are plotted in Fig. 4b, c. We analyzes the fields at $\lambda = 900$ nm and $\lambda = 450$ nm, which are the resonance peaks in TiN ring and layer, respectively (Fig. 3b). At $\lambda = 900$ nm, the electric field distribution shows an electric dipole resonance at the top ring antenna, whereas the magnetic field distribution is relatively weak. This result demonstrates that the absorption is mainly caused by the ring-shaped nanostucture. In contrast, at $\lambda = 450$ nm, the magnetic field distribution shows a magnetic dipole resonance as a result of coupling between the TiN layers. The antiparallel current density $J_d$ leads a loop bringing an artificial magnetic dipole moment. Thus, the ring-shaped TiN absorber excites electric and magnetic resonances, which increase the localized electromagnetic field at the corresponding wavelength.

The ring-shaped absorber is radially symmetrical, so its absorption is not greatly affected by polarization or incident angle of light at $\theta < 40^\circ$ (Fig. 5a, b). However, at $\theta > 40^\circ$, absorption decreases because the confinement of the EM field weakens. This degradation occurs because the resonances are sensitive to polarization and incident angle. Nevertheless, our observation confirms that absorption $>90\%$ is maintained at an angle of $40^\circ$ in both p- and s-polarizations. This characteristic means that the proposed absorber can be widely used in practical fields, such as photothermal applications.

**Heat tolerance**

The proposed absorber is expected to have a great heat tolerance as a result of TiN’s high melting point of $2930^\circ$C. To confirm the heat tolerance of the ring-shaped TiN absorber, it is heated in a vacuum chamber at $600^\circ$C for 6 h and cooled down to room temperature. We confirm that the TiN absorber maintains its shape and optical properties even after heating at high temperature (Fig. 6a).
Even at a high temperature near 600 °C, TiN and SiO₂ show only slight changes in their permittivities, but each retains its original optical properties quite well⁴⁶,⁴⁷. If the TiN absorber is protected by an atomic layer deposited coating or sealing, it may tolerate even much higher temperatures¹⁶.

For practical applications such as solar and photovoltaic fields, we test the photothermal stability of the TiN absorber under natural-like condition in an open environment. White light from a high-power xenon lamp is collimated and illuminated at fabricated samples that are fixed on slide glass. The sample is far enough from the source to avoid a direct thermal effect by the high temperature of the lamp. MIM structure is measured and compared to the TiN absorber for the photothermal activity. After being illuminated for same duration (5 min), the temperature of each sample is captured using an infrared camera (Testo 885, Testo; Fig. 6b). The temperature of the TiN absorber increases to >80 °C, which is 25.5 °C higher than that of MIM structure. The high absorption in our devices, combined with the ring-shaped nanostructure opens a gateway for efficient energy extraction in photothermal applications, due to advantages of low-cost and compatibility with large-scale fabrication.

**Conclusion**

We have reported a large-scale heat-tolerant TiN broadband absorber that shows >95% of unpolarized light absorption in the visible–NIR range of 400 < λ < 900 nm. We propose the implementation of cost-effective MPCL with refractory metal for fabrication of a centimeter scale ring-shaped absorber. Because of the heat-tolerant characteristic, the TiN absorber retains high absorption after heating up to 600 °C. This absorber will find wide applications in solar thermophotovoltaics, stealth, and further absorption controlling in high-temperature conditions.

**Materials and methods**

**Materials**

Suspensions of PS nanospheres with 0.3-μm diameter were used (Thermo Fisher Scientific). Absolute ethanol and toluene were used (Sigma Aldrich). Deionized water was obtained from a water purification system (Ultima Duo 300, Azzota Scientific). Hydrochloric acid (1 mol/L) was used (Samchun Chemical).

**Fabrication**

TiN and SiO₂ layers of MIM were deposited using DC Sputtering and e-beam evaporator. The PS colloidal monolayer were self-assembled into hexagonally closed-packed arrays on the TiN layer by using an air interface method. The diameters of the PS nanospheres were reduced by oxygen RIE (VITA, Femto Science) at 80 W with 30 sccm O₂. The top TiN layer was first etched at 100 W with 25 sccm Cl₂ and 100 sccm BCl₃. Then a second PS etching was performed in the same conditions. Then an 8-nm thick Ni layer was deposited by e-beam evaporator at a deposition rate of 0.3 Å/s. Then, the PS nanospheres were removed by sonication in toluene. A second TiN etching was performed in the same condition as the first etching. Finally, the Ni mask was easily removed by immersion in 1 mol/L hydrochloric acid for 10 min, followed by rinsing with DI water.

**Characterization**

A UV–VIS–NIR spectrometer (Cary 5000, Varian Co.) with diffuse reflectance accessory (Internal DRA-2055, Varian Co.) was used to characterize the absorption of the large-area sample in the wavelength range 400–900 nm, using white reflectance standards (Ocean optics) as a
reference. The wavelength-sampling step was 1 nm. We defined absorption as 1-reflectance. Fabricated TiN absorber structures were observed using a scanning electron microscope (Hitachi S4800) at 3 kV.

The thermal images were taken by an infrared camera (Testo 885, Testo), and the temperature was determined using Testo IRsoft software. The emissivity of 0.34 and room temperature of 21 °C were used for calibration. For calibration, we used an approach to directly measure the emissivity value of the infrared camera using a contact thermometer.

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J.R., J.K.K, D.L. and M.G. initiated and developed the idea. D.L. and M.K. performed numerical simulations. D.L. and M.G. performed experiments. D.L., M.G., MK, JJ, CC, JKK and J.R prepared the manuscript. J.R and J.K.K supervised the research. All authors participated in the discussion and approved the final manuscript.

Conflict of interest
The authors declare that they have no conflict of interest.

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