Effects of alternating current poling on the dielectric and piezoelectric properties of Pb(In0.5Nb0.5)O3–PbTiO3 crystals with a high Curie temperature

Junjie Xiong, a,b Zujian Wang, a Xiaoming Yang, a Rongbing Su, a Xifa Long b * abc and Chao He b * abc

The alternating current poling (ACP) method has been become more and more popular recently because of its advantages of being low cost, time saving and highly efficient. Few ACP studies have focused on relaxor-PT crystals with a high coercive field and high Curie temperature or the effects of ACP on intrinsic and extrinsic contributions. The effects of the electric field, frequency, and number of cycles of ACP on the piezoelectric and dielectric properties of (001)-oriented Pb(In0.5Nb0.5)O3–PbTiO3 ferroelectric crystals were studied. The dielectric permittivity $\varepsilon_{33}/\varepsilon_0$ and piezoelectric coefficient $d_{33}$ of an ACP sample are 3070 and 1400 pC N$^{-1}$, respectively, which are 14% and 18% larger than those of a DCP sample. Rayleigh analysis reveals that both intrinsic and extrinsic contributions are enhanced after ACP. The poling electric field, frequency and cycle number can influence the intrinsic and extrinsic contributions. The intrinsic contribution is significantly affected by the poling electric field, and cycle number, but it is not very sensitive to frequency, while the poling electric field, frequency and cycle number are very important for the extrinsic contribution. This work demonstrates that the uniform domain patterns are a critical factor for the enhancement of the piezoelectric properties.

1. Introduction

Relaxor-PbTiO3 (relaxor-PT) ferroelectric crystals, such as Pb(Mg1/3Nb2/3)O3–PbTiO3 (PMN–PT), have been widely used in sensors, actuators, and transducers, owing to their outstanding piezoelectric coefficient ($d_{33}$) and high electromechanical coupling factor ($k_{33}$) ($d_{33} > 2000$ pC N$^{-1}$, $k_{33} > 0.9$).1–3 Although rhombohedral PMN–PT crystals have ultrahigh piezoelectric performance, its low Curie temperature ($T_C \approx 150$ °C) and small coercive field ($E_c = 2–3$ kV cm$^{-1}$) restrict its applications at high temperature and high power. Pb(In0.5Nb0.5)O3–PbTiO3 (PIN–PT) crystals exhibit a high $T_C$ (>250 °C) and large $E_c$ (~8 kV cm$^{-1}$), which can fill the demands at a high temperature and high field.4,5 The piezoelectric properties of PIN–PT crystals ($d_{33} \sim 1500$ pC N$^{-1}$, $k_{33} \sim 85\%$) are not as excellent as those of the PMN–PT crystals. How to promote the piezoelectricity of PIN–PT crystals is a good issue for broader device applications.

In recent years, many methods have been introduced to further enhance the piezoelectric properties of relaxor-PT crystals. These strategies include adjusting the compositions, doping, using nano-electrodes, choosing better poling conditions and so on.6–19 For instance, recent studies found that Sm doped in a PMN–PT system can significantly improve the piezoelectricity.14,17 Davis et al. presented how to choose the optimal direction for poling to get a high piezoelectric performance.15 Design of the morphotropic phase boundary (MPB) can also get an excellent piezoelectric performance due to the flattened free-energy profile.18,19 A decrease of the domain size is on additional effective way to promote the piezoelectricity.18,19

Among the above methods, alternating current field poling (ACP) became more and more popular recently because of its advantages of low-cost, time-saving and high-efficiency. It has been reported that ACP is a highly efficient technique to get a high piezoelectric performance of PMN–PT crystals and can make a 40% enhancement of $d_{33}$,20 while the mechanisms of the ACP method are not clear enough. Many scientists put forward their ideas on the mechanisms of ACP. Chang et al. proposed that the reason for the excellent piezoelectric performance originates from the monoclinic phase (M$_A$).21 Luo et al. used domain growth theory to explain the transformation process of the domain structure.22 Qiu et al. presented a new idea that the improvement of the piezoelectric performance originates from polar nano regions (PNRs) or the local structure.23 He et al. subsequently investigated the Pb(Yb0.5Nd0.5)O3–PMN–PT
system, and concluded that a highly ordered domain structure results in a high piezoelectric performance after ACP. Qiu et al. proposed that the enhancement of piezoelectric performance is related to the decrement of the 71° domain wall. To summarize, ACP has become a promising poling method compared with the traditional direct current poling (DCP) method, but the mechanisms is still a big challenge. At present, most of the reported ACP studies have focused on relaxor-PT crystals with a low $E_c$, such as PMN–PT and PIN–PMN–PT, while little attentions is paid to relaxor-PT crystals with a high $T_c$ and large $E_c$. In addition, the enhancement of the piezoelectric properties after ACP are related to a change of domain configuration. It is generally said that the contributions of the domain wall motion are thought to be an extrinsic contribution, which is unclear.

In this work, the piezoelectric and dielectric properties of PIN–PT crystals with a large $E_c$ and high $T_c$ were studied using different poling electric fields, frequencies, and cycles of ACP. The Rayleigh analysis and domain structure were studied to track the relationship between the enhancement of piezoelectric properties and domain engineering.

2. Experimental procedure

The rhombohedral perovskite phase PIN–PT crystals with an $E_c$ of 8.6 kV cm$^{-1}$ and $T_c$ of 260 °C were grown in our lab using a top-seeded solution growth method. The details of the growth have been reported in our previous work. The actual composition was 0.66PIN–0.34PT examined by inductively coupled plasma atomic emission spectroscopy (ICP-AES, JY Ultima-2, Horiba Jobin Yvon, France). The natural {001} face can be obtained from as-grown crystals, and was examined using XRD. Then, crystals were cut into {001}-oriented samples: dimensions of $4 \times 4 \times 0.6$ mm$^3$ (plate mode) were used for the dielectric and piezoelectric measurements and of $5 \times 1 \times 1$ mm$^3$ (bar mode) for the electromechanical coupling factor measurements. The grown PIN–PT crystals exhibit a natural {001} face. The {001} crystal plates were cut parallel to the natural {001} face. And the cut crystal plates were examined using XRD. All the samples were annealed at 600 °C for 6 h, with the top and bottom electrodes shorted to eliminate the residual stress fully before each poling measurement.

In this work, a high-voltage supply amplifier/controller (Trek, model 610E) was used for DCP and ACP. The voltage presented in this work for DCP is a peak voltage ($V_{\text{peak}}$), while the voltage presented in this work for ACP is a root mean square voltage ($V_{\text{rms}}$) of the triangle voltage (Fig. 1b). The poling processes were carried out at ambient temperature in silicon oil to protect the samples. $d_{33}$ of PIN–PT single crystals was measured using a quasi-static $d_{33}$ meter (Chinese Academy of Sciences, Institute of Acoustics, ZJ-4AN, China). The free dielectric constant ($\varepsilon_{33}/\varepsilon_0$) were measured by an impedance analyzer (Keysight Technologies, E4990A, Santa Clara, CA, USA). $k_{33}$ was calculated from the resonance frequency ($f_3$) and anti-resonance frequency ($f_2$) according to IEEE standards. Piezo-response force microscopy (PFM, Asylum Research, Cypher ES, USA) was used to study the domain structure.

3. Results and discussion

3.1 Poling conditions

In the ACP process, the poling electric field, frequency and cycles can affect the piezoelectric performance and interact. The most important factor among the three is the electric field. Therefore, the influence of the electric field was firstly investigated in this work. In the process, the frequency and cycle were the fixed values [frequency: 10 Hz, cycle: 25], which refers to our experience and previous studies in PMN–PT and PIN–PMN–PT crystals. The influence of cycles was studied last because the cycles depend more on the electric field and frequency compared with other factors.

Fig. 1 shows the $d_{33}$, $\varepsilon_{33}/\varepsilon_0$ and $k_{33}$ of 0.66PIN–0.34PT crystals after DCP and ACP (10 Hz, 25 cycles) as a function of the electric field. The $d_{33}$ and $\varepsilon_{33}/\varepsilon_0$ of the DCP samples increased significantly from 790 pC N$^{-1}$ to 1180 pC N$^{-1}$ and 1950 to 2690, respectively, when the poling electric field increased from 8 to 12 kV cm$^{-1}$. The $d_{33}$ of the DCP samples decreased when the electric field increased above 16 kV cm$^{-1}$. The optimal DCP conditions were 12–16 kV cm$^{-1}$ (15 minutes). For the ACP samples, the maximum $d_{33}$, $\varepsilon_{33}/\varepsilon_0$ and $k_{33}$ were 1320 pC N$^{-1}$, 2950 and 85%, respectively, at an electric field of 11.6 kV cm$^{-1}$, which was 11.9%, 9.7% and 2% higher than that of the DCP samples. Therefore, the optimal ACP root mean square electric field was 11.6 kV cm$^{-1}$. Note that the variation of $d_{33}$, $\varepsilon_{33}/\varepsilon_0$ and $k_{33}$ had a decreasing trend when the electric fields were too large. The electrostrictive effect is generated in the poling process because of the rotation of domains. The crystals are prone to micro-cracking if the poling electric field is too large, which is considered as an over-poling effect.

Fig. 2 shows the $d_{33}$, $\varepsilon_{33}/\varepsilon_0$ and $k_{33}$ of 0.66PIN–0.34PT crystals after DCP and ACP (11.6 kV cm$^{-1}$, 25 cycles) as a function of frequency. The values of $d_{33}$ and $\varepsilon_{33}/\varepsilon_0$ increased dramatically from 1140 pC N$^{-1}$ to 1400 pC N$^{-1}$ and from 2620 to 3070, respectively when the poling frequency increased from 1 to 15 Hz. Further increasing the poling frequency, the $d_{33}$, $\varepsilon_{33}/\varepsilon_0$ gradually decreased. The values of $d_{33}$ and $\varepsilon_{33}/\varepsilon_0$ were 970 pC N$^{-1}$ and 2150 using 40 Hz poling. For the $k_{33}$-mode sample, the value of $k_{33}$ of the 0.66PIN–0.34PT crystals decreased with increasing frequencies (Fig. 2b). The highest $k_{33}$ was 86% at 1 Hz. The difference between the variation of $k_{33}$ and $d_{33}$ is related to the shape of the samples. The thickness of the $k_{33}$ mode (5 mm) was much larger than that of the $d_{33}$ sample (0.6 mm), which indicates that the frequency has a relatively large impact on the different thickness samples. Considering both the effect of the frequency on $d_{33}$ and $k_{33}$, the optimal poling frequency was 15 Hz. Compared with PMN–PT crystals, the piezoelectric and dielectric properties of 0.66PIN–0.34PT crystals after ACP are more dependent on frequency. The previous work revealed that the piezoelectric performances of PMN–PT and PIN–PMN–PT crystals can be significantly improved using low frequency ACP, while low frequency ACP does not show any good results for PIN–PT crystals. For PIN–PT crystals, it is hard to switch domains under and external field due its high coercive field. At a low frequency ACP, the domains can easily...
grow large, which further hinders domain switching. It is detrimental to rearrange domains and enhance the performance.

Fig. 3 shows the $d_{33}$, $e_{33}/e_0$ and $k_{33}$ of 0.66PIN–0.34PT crystals after DCP and ACP (15 Hz, 11.6 kV cm$^{-1}$) as a function of cycle. The values of $d_{33}$, $e_{33}/e_0$ and $k_{33}$ increased significantly from 690 pC N$^{-1}$, 1660 and 66% to 1400 pC N$^{-1}$, 3070 and 86%, respectively, when the ACP cycle increased from 5 to 25, and became invariant with a further increase of the ACP cycle. The optimal poling cycle was 25. The reported PMN–PT single crystals have the highest piezoelectric properties with poling cycles below 10.

The ACP process can reduce the energy required for domain rotation, which makes domain rotation easy. The poling cycle is the process of the reduction of the energy required for domain rotation. Compared with PMN–PT crystals, the PIN–PT crystal required more energy for domain rotation due to its higher coercive field. It is difficult to rearrange the domain structure of 0.66PIN–0.34PT crystals due to the large coercive field, resulting in the small enhancement after ACP.

### 3.2 Rayleigh analysis

The enhancement of piezoelectric and dielectric properties can be divided into the enhancement of intrinsic and extrinsic contributions. The intrinsic contribution originates from lattice distortion, while the extrinsic contribution originates from the domain wall and phase boundary motion. The degrees of intrinsic and extrinsic contributions can be well-distinguished by the Rayleigh law. The Rayleigh law can be expressed using the following formulas:

\[
P(E) = e_0(e_{\text{init}} + aE_0)E \pm a(E_0^2 - E^2)/2
\]

\[
e_r = e_{\text{init}} + aE_0
\]

where $P$ is the polarization, and $E_0$ is the amplitude of the measured AC field, $e_r$ is the total dielectric permittivity under the electric field. $e_{\text{init}}$ is $e_r$ when the limit $E_0$ tends to 0 and represents the reversible part, which consists of the intrinsic

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**Fig. 1** The (a) $d_{33}$, $e_{33}/e_0$, and (b) $k_{33}$ values of DCP and ACP (10 Hz, 25 cycles) 0.66PIN–0.34PT single crystals as a function of the electric field.

**Fig. 2** The $d_{33}$, $e_{33}/e_0$, and $k_{33}$ values of ACP (11.6 kV cm$^{-1}$, 25 cycles) 0.66PIN–0.34PT crystals as a function of frequency.

Compared with relaxor-PT crystals with a low $E_c$ (<6 kV cm$^{-1}$), the enhancement ratio of ACP 0.66PIN–0.34PT crystals is not as high as for these crystals. Polarization switching can reflect the domain wall motions and opposite domain nucleation and growth in the ACP process. The PMN–PT crystals have a fast domain nucleation and growth due to their low coercive field. It is difficult to rearrange the domain structure of 0.66PIN–0.34PT crystals due to the large coercive field, resulting in the small enhancement after ACP.

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Table 1 shows a comparison of the piezoelectric and dielectric properties of relaxor-PT crystals. Compared with relaxor-PT crystals with a low $E_c$ (<6 kV cm$^{-1}$), the enhancement ratio of ACP 0.66PIN–0.34PT crystals is not as high as for these crystals. Polarization switching can reflect the domain wall motions and opposite domain nucleation and growth in the ACP process. The PMN–PT crystals have a fast domain nucleation and growth due to their low coercive field. It is difficult to rearrange the domain structure of 0.66PIN–0.34PT crystals due to the large coercive field, resulting in the small enhancement after ACP.

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contribution and the reversible domain wall motion. For most relaxor-PT ferroelectrics, the intrinsic contributions play the dominant role in the reversible part, while the proportion of the reversible domain wall motion is small.\textsuperscript{40-42} Thus, \( \varepsilon_{\text{init}} \) is approximate to the intrinsic contribution of dielectric permittivity and \( aE_0 \) is the extrinsic contribution of dielectric permittivity. \( \alpha \) is the Rayleigh coefficient that represents the contribution of the domain wall motion and phase boundary. The ratio of the extrinsic contribution is expressed as:

\[
\text{Extrinsic ratio } = \frac{aE_0}{\varepsilon_{\text{init}} + aE_0}
\]

Eqn (1) describes the Rayleigh hysteresis, where the signs “+” and “−” correspond to decreasing and increasing electric field, respectively. To avoid the switching of domains, \( E_0 \) is selected far lower than half of the \( E_c \). In this work, the \( E_0 \) was 1–3 kV cm\(^{-1} \) and the extrinsic ratio was calculated at \( E_0 \) of 1 kV cm\(^{-1} \). From the slope of the \( P-E \) at a low electric field, the value of \( \varepsilon_{\text{init}} + aE_0 \) can be expressed as:

\[
\varepsilon_r = \varepsilon_{\text{init}} + aE_0 = \frac{(P_{\text{max}} - P_{\text{min}})}{2(E_0/\varepsilon_0)}
\]

where \( P_{\text{max}} \) and \( P_{\text{min}} \) are the largest and lowest value of polarization in the \( P-E \) hysteresis loops.

Fig. 4 shows the Rayleigh analysis of the 0.66PIN–0.34PT crystals under different electric fields. It can be easily obtained that the value of \( \varepsilon_r \) is linear with \( E_0 \), suggesting that the Rayleigh law is applicable for 0.66PIN–0.34PT crystals with \( E_0 \) from 1 to 3 kV cm\(^{-1} \). According to eqn (2), the intercept from the \( y \) axis represents \( \varepsilon_{\text{init}} \) and the slope of the lines represents \( \alpha \). Hence, the values of \( \varepsilon_{\text{init}} \) and \( aE_0 \) were found to be 2788 and 209, respectively, for the DCP samples. The value of \( \varepsilon_{\text{init}} \) was 2286 for the ACP samples under 6.96 kV cm\(^{-1} \), which was much smaller than that for the DCP samples. Further increasing the ACP electric field from 6.96 kV cm\(^{-1} \) to 11.6 kV cm\(^{-1} \), the values of \( \varepsilon_{\text{init}} \) and \( aE_0 \) all increased dramatically from 2286 and 214 to 2875 and 327, respectively, indicating that both the intrinsic and extrinsic contributions enhanced after ACP. The increment of the ratio of \( aE_0/(\varepsilon_{\text{init}} + aE_0) \) indicates the obvious enhancement of the extrinsic contribution. The highest value of \( aE_0/(\varepsilon_{\text{init}} + aE_0) \) was 0.102 at the poling electric field of 11.6 kV cm\(^{-1} \). It can be concluded that the extrinsic contribution is affected heavily by the ACP.

Fig. 5 shows the Rayleigh analysis of 0.66PIN–0.34PT ACP samples under different poling frequencies. With the increase of the frequency from 1 Hz to 15 Hz, the intrinsic contribution \( \varepsilon_{\text{init}} \) increased slightly from 2760 to 2919, while the extrinsic contribution \( aE_0 \) exhibited a great improvement from 226 to 351, and the proportion of \( aE_0/(\varepsilon_{\text{init}} + aE_0) \) increased significantly from 0.076 to 0.107. When the frequency exceeded 15 Hz, the values of \( \varepsilon_{\text{init}} \) and \( aE_0 \) began to decline. The values of \( \varepsilon_{\text{init}} \) and \( aE_0 \) were 2043 and 280, respectively, at 40 Hz, which were much smaller than those at 15 Hz. It can be concluded that a low ACP frequency has little effect on the intrinsic contribution. When the ACP frequency was high, both the intrinsic and extrinsic contributions declined significantly. Therefore, ACP of a moderate frequency is critical and necessary, such as 15 Hz in this work.

Fig. 6 shows the Rayleigh analysis of 0.66PIN–0.34PT ACP samples under different poling cycles. When the cycles increased from 5 to 25, the intrinsic contribution \( \varepsilon_{\text{init}} \) and the

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Table 1: Dielectric and piezoelectric properties of relaxor-PT crystals after DCP and ACP. \( T_c \): rhombohedral–tetragonal phase transition temperature

| Material            | \( E_c \) (kV cm\(^{-1} \)) | \( T_{\text{in}} \) (°C) | \( T_c \) (°C) | \( \varepsilon_{33} T_{\text{rt}}/\epsilon_0 \) DCP | \( \varepsilon_{33} T_{\text{rt}}/\epsilon_0 \) ACP | \( d_{33} \) (pC N\(^{-1} \)) DCP | \( d_{33} \) (pC N\(^{-1} \)) ACP | Difference \( d_{33} \) (%) | Ref. |
|---------------------|-----------------------------|---------------------------|----------------|-----------------------------------------------|-----------------------------------------------|-----------------------------|-----------------------------|--------------------------|-----|
| 0.52PMN–0.15PYbN–0.33PT | 5.4                         | 94                        | 180            | 5200                                         | 6800                                         | 1770                        | 2490                        | 41%                      | 8   |
| 0.75PMN–0.25PT       | 2.6                         | 93                        | 116            | —                                            | 6397                                         | 1220                        | 1730                        | 42%                      | 22  |
| 0.7PMN–0.3PT         | 2.3                         | 90                        | 130            | 6210                                         | 8140                                         | 1650                        | 1980                        | 20%                      | 21  |
| 0.72PMN–0.28PT       | —                           | 80                        | 123            | 7000                                         | 8900                                         | 1940                        | 2650                        | 37%                      | 31  |
| 0.25PIN–0.43PMN–0.32PT | —                           | 113                       | 180            | 4800                                         | 7120                                         | 1700                        | 2610                        | 54%                      | 32  |
| 0.66PIN–0.34PT       | 8.6                         | 160                       | 260            | 2690                                         | 3070                                         | 1180                        | 1400                        | 18%                      | This work |

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extrinsic contribution $aE_0$, and the proportion of $aE_0 / (E_{\text{init}} + aE_0)$, increased from 1787, 152, 0.078 to 2919, 351 and 0.107, respectively. Then, the values of $E_{\text{init}}$, $aE_0$, and $aE_0 / (E_{\text{init}} + aE_0)$ all became invariant when the cycles exceeded 25, indicating that the optimal poling cycle was 25 cycles.

The poling electric field, frequencies and cycles can influence the intrinsic and extrinsic parts of the ACP samples. The intrinsic contribution is significantly affected by the poling electric field and cycle, but it is not very sensitive to frequency, while the poling electric field, frequency and cycle is very important for the extrinsic contribution. The values of $E_{\text{init}}$, $aE_0$ and $aE_0 / (E_{\text{init}} + aE_0)$ were 2919, 351 and 0.107, respectively, with an electric field of 11.6 kV cm$^{-1}$, frequency of 15 Hz, and 25 cycles.

3.3 Domain structures

The enhancement of the piezoelectric and dielectric properties after ACP are related to the optimization of the domain morphologies. It should also be noted that 0.66PIN–0.34PT crystals have the rhombohedral perovskite phase. The ferroelectric crystals with the rhombohedral perovskite phase have eight spontaneous directions along (111). Poling along the (001) direction, the “4R” domain-engineered multi-domain structure is formed, exhibiting clear 109° and 71° domain walls.

Fig. 7 shows the PFM results of the unpoled, DCP and ACP samples. The scan area is 20 x 20 μm$^2$ for each image. The crystallographic orientation and poling direction are marked in the figure.

4. Conclusions

The effects of ACP on 0.66PIN–0.34PT crystals were studied, including changing the electric field, frequency, and cycle.
number. The optimal ACP conditions are an electric field of 11.6 kV cm\(^{-1}\), a poling frequency of 15 Hz, and a cycle number of 25. The \(\varepsilon_{33}/\varepsilon_0\) and \(d_{33}\) values were 3070 and 1400 pC N\(^{-1}\), respectively, after ACP, which were about 14% and 18%, respectively, better than those of conventional DCP samples, while the \(k_{33}\) values of both DCP and ACP 0.66PIN–0.34PT crystals had the same level. Rayleigh analysis revealed that both the intrinsic and extrinsic contributions were enhanced after ACP. The poling electric field, frequency, and cycle number can influence the intrinsic and extrinsic contributions. The highly regular, uniform domain structure of the 109° domains and low density of the 71° domains were the obvious differences between unpoled, ACP, and DCP samples. The uniform and stripe like 109° domain wall patterns are a critical factor for the enhancement of the piezoelectric properties via domain engineering.

**Conflicts of interest**

There are no conflicts to declare.

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