Adenosine triphosphate (ATP) is known to be released from the erythrocyte in an oxygen (O2) dependent manner. Since ATP is a potent vasodilator, it is proposed to be a key regulator in the pathway that mediates micro-vascular response to varying tissue O2 demand. We propose that ATP signaling mainly originates in the capillaries due to the relatively long erythrocyte transit times in the capillary and the short ATP diffusion distance to the electrically coupled endothelium. We have developed a computational model to investigate the effect of delivering or removing O2 to limited areas at the surface of a tissue with an idealized parallel capillary array on total ATP concentration. Simulations were conducted when exposing full surface to perturbations in tissue O2 tension (PO2) or locally using a circular micro-outlet (~100 μm in diameter), a square micro-slit (200 × 200 μm), or a rectangular micro-slit (1000 μm wide × 200 μm long). Results indicated the rectangular micro-slit has the optimal dimensions for altering hemoglobin saturations (SO2) in sufficient number capillaries to generate effective changes in total [ATP]. This suggests a threshold for the minimum number of capillaries that need to be stimulated in vivo by imposed tissue hypoxia to induce a conducted micro-vascular response. SO2 and corresponding [ATP] changes were also modeled in a terminal arteriole (9 μm in diameter) that replaces 4 surface capillaries in the idealized network geometry. Based on the results, the contribution of terminal arterioles to the net change in [ATP] in the micro-vascular network is minimal although they would participate as O2 sources thus influencing the O2 distribution. The modeling data presented here provide important insights into designing a novel micro-delivery device for studying micro-vascular O2 regulation in the capillaries in vivo.

Keywords: adenosine triphosphate (ATP), microcirculation, capillaries, computational model, simulation, local PO2 perturbation, O2 regulation, micro-delivery device
means only those cells closest to the wall experience the largest change in O2 saturation (SO2) and hence contribute to the signal. Cells flowing in the centerline will be experiencing a lesser drop in SO2 and any released ATP will be carried downstream (Ellis et al., 2012).

Venous may also be involved in the regulation of O2 supply since they act as the collectors of large populations of deoxygenated ATP-releasing erythrocytes. However, the diversity in the erythrocyte SO2 levels as they drain from various upstream capillaries indicates that venules may only contribute to the overall vaso-dilatory signal (Ellis et al., 2012). Fine-tune regulation of O2 distribution to specific capillaries or microvascular units in the microcirculation demands the signal be highly localized. This may only be achieved at the capillary level. Erythrocytes traverse capillaries with long transit times and are in almost direct contact with the capillary endothelium. Hence, released ATP, mediated by erythrocyte deoxygenation, will be effectively transferred to purinergic receptors on the endothelium. Many studies have shown that the capillary endothelium is conductive when locally stimulated by vasodilators (Dietrich, 1989; Dietrich and Tynml, 1992a,b; Song and Tynml, 1993; Collins et al., 1998; Bagher and Segal, 2011). Therefore, we hypothesize that the capillary bed is the major site for O2 regulation in the microcirculation (Ellis et al., 2012).

To test this hypothesis, we have been examining the microvascular response to local perturbations in tissue O2 tension (PO2) using a novel O2 micro-delivery tool (Ghonaim et al., 2011). We have created an O2 micro-delivery (and removal) system that allows for altering local tissue PO2 and hence erythrocyte SO2 in a few selected capillaries at the surface of the Extensor Digitorum Longus (EDL) muscle of the rat (Figure 1). This system replaces the gas exchange chamber originally used in our group to alter surface tissue PO2 of the entire bottom surface of the muscle (Ghonaim et al., 2011; Ellis et al., 2012). The chamber is positioned in the platform of an inverted microscope and is connected to computer controlled gas flow meters which allows for capturing video images of the microvascular response to PO2 perturbations while simultaneously controlling chamber PO2 levels. Erythrocyte SO2 values are calculated based on a dual-wavelength image capture system and video sequences are post-processed to extract functional images and hemodynamic information as previously described (Ellis et al., 1990, 1992; Japee et al., 2004, 2005a,b).

In our novel O2 micro-delivery setup, ultrathin plastic/glass sheet patterned with an O2 delivery micro-outlet replaces the gas permeable membrane in the original chamber (Ghonaim et al., 2011; Ellis et al., 2012). Data presented earlier (Ghonaim et al., 2011) show that circular micro-delivery outlets (100 μm in diameter) can alter SO2 in single capillaries flowing directly over the outlet. However, in order to elicit microvascular responses, the optimal outlet dimensions should allow for a sufficient number of capillaries within a network to be stimulated to produce a large enough ATP signal. This should be accomplished while ensuring the high localization of the stimulus to affect only the desired capillaries. This requires testing with various O2 outlet sizes and dimensions. Combining the possible technical challenges involved in creating multiple designs of the O2 micro-delivery device with the inherent complexities of the O2 regulation system led us to develop a computational model for the system under investigation.

Recently, Goldman et al. (2012) presented a theoretical mathematical model based on previous work by Goldman and Popel (1999) and Arciero et al. (2008) to describe O2 and ATP transport in the rat EDL microcirculation when using the original O2 exchange chamber. In this study we employ the same approach to calculate SO2 and ATP changes in selected capillaries flowing over an O2 delivery outlet of specific dimensions. Three designs of the O2 delivery micro-outlet were tested: circular outlet (100 μm in diameter), square outlet (200 × 200 μm), and rectangular slit (200 μm long × 1000 μm wide). Average capillary SO2 and ATP level at steady-state were calculated at various chamber PO2 levels (15, 40, and 150 mmHg) relative to a zero flux boundary condition. In order to simplify the system under investigation, an idealized three dimensional (3D) parallel array capillary geometry has been used. Simulations were also run on a 3D idealized array geometry in which a terminal arteriole (9 μm in diameter) replaced 4 capillaries and was positioned 30 μm from the bottom tissue surface. These simulations allowed for investigating the potential role of the terminal arteriole in O2 regulation. Confirming previous findings (Ghonaim et al., 2011), the results indicated that radial O2 diffusion from an O2 delivery micro-outlet regardless of its dimensions is limited to

![Figure 1](image-url)
~50 μm, while axial diffusion affects ~100 μm of tissue. The rectangular slit has the important property of ensuring that capillaries surrounding the network of interest are all experiencing the same PO2 drop, which minimizes re-oxygenation and emphasizes the ATP signal. This design also produces sufficient ATP release in multiple capillaries that it should be able to consistently elicit micro-vascular responses, although this remains to be confirmed experimentally. The results presented here also predict minimal contribution of terminal arterioles to the net magnitude of ATP emerging from capillary network although they would participate as O2 sources and hence influence the O2 distribution. In the future, 3D capillary networks reconstructed from experimental data can be modeled which will provide more realistic data and help more closely predict changes in various parameters.

MATERIALS AND METHODS

OXYGEN TRANSPORT MODEL

In this work, O2 transport and ATP transport were modeled in an idealized 3D capillary network consisting of an array of parallel capillaries (oriented in the y direction). The computational model of O2 transport was based on a finite-difference model described by Goldman and Popel (1999, 2000, 2001). In the model, the reaction-diffusion equation below was used to describe time-dependent tissue PO2, \( P(\bar{x}, y, z, t) \):

\[
\frac{\partial P}{\partial t} = \left[ 1 + c_{\text{Mb}} \frac{dS_{\text{Mb}}}{\alpha dP} \right]^{-1} \left\{ D \nabla^2 P - \frac{1}{\alpha} M(P) + \frac{1}{\alpha} D_{\text{Mb}} c_{\text{Mb}} \nabla \right\}
\]

(1)

where \( D \) is the tissue O2 diffusion coefficient, \( \alpha \) is the tissue O2 solubility, and \( M(P) \) is consumption rate of O2 in tissue (Table 1). O2 transport in tissue was facilitated by the presence of myoglobin where \( c_{\text{Mb}} \) is myoglobin concentration, \( D_{\text{Mb}} \) is the myoglobin diffusion coefficient, and \( S_{\text{Mb}}(P) = P/(P + P_{50,\text{Mb}}) \) is the myoglobin O2 solubility. Convective transport of O2 in the micro-vessels at each axial location \( y \) was described using the following time-dependent mass balance equation for capillary SO2, \( S(y,t) \):

\[
\frac{\partial S}{\partial t} = \left[ C + \alpha_v \frac{dP_b}{dS} \right]^{-1} \left\{ -u \left[ \tilde{C} + \tilde{a}_v \frac{dP_b}{dS} \right] \frac{\partial S}{\partial y} - \frac{1}{\pi R} \int j \cdot d\bar{d} \right\}
\]

(2)

where \( u \) is the mean blood velocity, \( R \) is the capillary radius, \( j \) is the O2 flux at \((y,\theta)\) out of the capillary, \( C \) and \( \tilde{C} \) are blood O2-binding capacities, respectively, directly related to hemocrit:

\[
C = H_T C_{\text{Hb}} \quad \tilde{C} = H_D C_{\text{Hb}}
\]

where \( H_T \) is tube (volume-weighted) hemocrit, \( H_D \) is discharge (flow-averaged) hemocrit, and \( C_{\text{Hb}} \) is the binding capacity of hemoglobin (Table 1) (Goldman and Popel, 2001). \( P_b \) is the blood PO2, and \( \tilde{a}_v \) and \( \tilde{a}_p \) are volume- and flow-weighted blood O2 solubilities, respectively (Goldman and Popel, 2001), where,

\[
\tilde{a}_v = H_T a_{\text{cell}} + (1 - H_T) a_{\text{pl}}
\]

\[
\tilde{a} = H_D a_{\text{cell}} + (1 - H_D) a_{\text{pl}}
\]

where \( a_{\text{cell}} \) and \( a_{\text{pl}} \) are the O2 solubilities inside the erythrocyte and in the plasma (Goldman and Popel, 2001). The O2 flux at the capillary-tissue interface was given by:

\[
j = \kappa (P_b - P_w)
\]

(3)

where \( \kappa \) is the mass transfer coefficient and \( P_w \) is the tissue PO2 at the capillary surface. \( \kappa \) is a function of hematocrit as it describes the effect of RBC spacing on O2 diffusion and exchange between capillary and tissue (Eggleton et al., 2000). At the capillary surface, the boundary condition was specified as:

\[
- D \tilde{a}_v \frac{\partial P_w}{\partial n} = j
\]

(4)

where \( n \) is the unit vector normal to the capillary surface and \( j \) is given by equation (3). In the model presented here, zero O2 flux conditions (no O2 exchange across tissue boundary) were specified at the tissue boundaries, except where PO2 was fixed on part or all of the bottom surface to represent the effect of the O2 exchange chamber (see below). As in the model described by Goldman and Popel (1999), Michaelis–Menten consumption kinetics, \( M = M_0 P/(P + P_{50}) \), and the Hill equation for the oxy-hemoglobin saturation curve, \( S(P) = P^n/(P^n + P_{50}^n) \), were used along with the above O2 transport equations to calculate tissue O2 transport.

Hemodynamic parameters (erythrocyte mean velocity, \( \nu_{bc} \), and hemocrit, \( H_T \)) were determined from in vivo experimental measurements in the EDL muscle of the rat. The capillary

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Table 1 | Parameter values used in oxygen and ATP transport simulations.

| Parameter | Value |
|-----------|-------|
| \( \alpha \) | 3.89 × 10^{-5} ml O2 ml^{-1} mmHg^{-1} |
| \( D \) | 2.41 × 10^{-5} cm^2 s^{-1} |
| \( P_{CT} \) | 0.5 mmHg |
| \( a_{\text{Mb}} \) | 1.02 × 10^{-2} ml O2 ml^{-1} |
| \( D_{\text{Mb}} \) | 3 × 10^{-7} cm^2 s^{-1} |
| \( P_{50} \) | 37 mmHg |
| \( \kappa \) | 2.7 |
| \( P_{50, Mb} \) | 5.3 mmHg |
| \( C_{\text{Hb}} \) | 0.52 ml O2 ml^{-1} |
| \( \nu_{bc} \) | 1.45 × 10^{-2} cm s^{-1} |
| \( H_T \) | 0.19 |
| \( H_D \) | 0.2 |
| \( C_0 \) | 1.4 × 10^{-9} mol s^{-1} cm^{-3} |
| \( C_1 \) | 0.891 |
| \( k_d \) | 2.0 × 10^{-4} cm s^{-1} |
network consisted of 72 parallel capillaries, each of which was discretized into 50 cylindrical segments, and the tissue domain surrounding the capillaries had dimensions of $216 \times 532 \times 500 \, \mu m$ and was discretized into 7,304,853 computational nodes using a grid spacing of approximately $2 \, \mu m$ (Figure 2A). Capillary entrance $SO_2$ (65%) and the tissue $O_2$ consumption rate ($1.5 \times 10^{-4} \, ml \, O_2/ml/s$) were set based on previous experimental data (Fraser et al., 2012).

For simulations that included a terminal arteriole in the 3D network geometry, the arteriole (9 $\mu m$ in diameter) was positioned $\sim 30 \, \mu m$ from the bottom tissue surface and replaced 4 capillaries in the original parallel array capillary geometry (Figure 2B). Simulations including the arteriole were run at both 65 and 80% arteriolar entrance $SO_2$.

**ATP TRANSPORT MODEL**

ATP transport in the idealized 3D capillary network was modeled as described by Goldman et al. (2012), based on the $O_2$ transport mathematical model described above (Goldman and Popel, 2000). Using a capillary entrance ATP concentration of zero, plasma [ATP] was calculated by using a finite-difference method to solve the following continuum partial differential equation (Goldman et al., 2012):

$$
(1 - HT) \frac{\partial [ATP]}{\partial y} = -u (1 - HD) \frac{\partial^2 [ATP]}{\partial y^2} + HT Ca (1 - C1S) - \frac{1}{R} kd [ATP] \tag{5}
$$

where $u$ is the mean blood velocity at axial location $y$, $HD$, and $HT$ are the discharge and tube hematocrit, respectively, and $R$ is capillary radius. $Ca$ and $C1$ (Table 1) are constants used to linearly approximate the ATP release rate as a function of $SO_2$, while $kd$ provides an approximation of ATP degradation by the endothelium as previously described (Arciero et al., 2008).

To calculate the steady-state distributions of tissue $O_2$ and capillary $SO_2$ and [ATP], time-dependent $O_2$ transport and ATP transport simulations were run, using zero initial conditions for all variables, until there were minimal changes in tissue $O_2$ consumption and $PO_2$, and capillary $O_2$ flux, $SO_2$ and [ATP] between consecutive time steps.

**TISSUE $PO_2$ BOUNDARY CONDITIONS USED TO MODEL OXYGEN EXCHANGE CHAMBER**

For the idealized capillary geometry, 3D tissue $PO_2$ distribution and capillary [ATP] at steady state were calculated for $O_2$ delivery using full gas exchange chamber, circular micro-outlet ($100 \, \mu m$ in diameter), square micro-outlet ($200 \times 200 \, \mu m$), or a rectangular micro-slit ($1000 \, \mu m$ wide $\times$ $200 \, \mu m$ long). For each chamber type, simulations were run at 3 $PO_2$ boundary conditions either over full surface (with full gas exchange chamber) or only at the micro-slit opening: 15, 40, and 150 mmHg. For the cases in which the $PO_2$ boundary condition is altered only at the microslit opening, the rest of the tissue surrounding the micro-slit is set to zero $O_2$ flux boundary condition. The results from all simulations were compared to a fourth control case in which full surface is set to zero $O_2$ flux boundary condition.

For the idealized capillary geometry that includes the terminal arteriole, $O_2$ diffusion was modeled for full chamber or a rectangular micro-slit ($1000 \, \mu m$ wide $\times$ $200 \, \mu m$ long) at the 4 $PO_2$ boundary conditions discussed above. Each set of simulations was run with arteriolar entrance $SO_2$ of 65% or to 80%. Table 2 lists

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**Table 2 | List of boundary conditions used in oxygen and ATP transport simulations.**

| Network specifications | Chamber type tested | Corresponding figure in manuscript | $PO_2$ condition at chamber outlet (in each chamber type tested) |
|------------------------|---------------------|-----------------------------------|---------------------------------------------------------------|
| Capillary array        | Full chamber        | 3                                 | - Zero $O_2$ flux (Control)                                  |
|                        | Circle              | 4                                 | - 40 mmHg                                                   |
|                        | Square              | 5                                 | - 15 mmHg                                                   |
|                        | Rectangle           | 6                                 | - 150 mmHg                                                  |
| Capillary array with arteriole (entrance $SO_2 = 65\%$) | Full chamber | 8                                 | - Zero $O_2$ flux (Control)                                  |
|                        | Rectangle           | 10                                | - 40 mmHg                                                   |
|                        |                     |                                   | - 15 mmHg                                                   |
|                        |                     |                                   | - 150 mmHg                                                  |
| Capillary array with arteriole (entrance $SO_2 = 80\%$) | Full chamber | 9                                 | - Zero $O_2$ flux (Control)                                  |
|                        | Rectangle           | 11                                | - 40 mmHg                                                   |
|                        |                     |                                   | - 15 mmHg                                                   |
|                        |                     |                                   | - 150 mmHg                                                  |

**Summary of transport simulations, chamber types, and boundary conditions.**
the summary of simulations and boundary conditions used in this study.

RESULTS

MATHEMATICAL MODELING OF SO2-DEPENDENT ATP RELEASE IN CAPILLARY NETWORKS IN RESPONSE TO LOCALIZED TISSUE PO2 PERTURBATIONS

In this study, the release of ATP in capillaries mediated by tissue hypoxia and the de-saturation of hemoglobin was modeled in a 3D idealized parallel capillary network. The dependence of the magnitude of total ATP release on the number of deoxygenated capillaries was also examined. Based on our previously described experimental work (Ghonaim et al., 2011), we mathematically simulated O2 delivery to and removal from selected capillaries on the surface of skeletal muscle tissue (rat EDL) using three designs of O2 exchange micro-outlets used in our in vivo experiments (Figure 1). In order to compare local O2 perturbations using the micro-outlets to global perturbations using the full gas exchange chamber (Ghonaim et al., 2011; Ellis et al., 2012), O2 delivery to and removal from the entire bottom tissue surface was also modeled. For each set of simulations, 3D tissue PO2 distribution profiles and corresponding 3D capillary [ATP] maps were generated. Plots of calculated SO2 and [ATP] along the length of selected capillaries (21, 18, 17, 54) at steady state were also created. All simulations were run using software written in Fortran, and the results were analyzed and the plots were produced using MATLAB.

Full surface gas exchange chamber

In this set of simulations, the 3D PO2 distribution in the tissue and corresponding SO2 and [ATP] distribution along capillary length were modeled for the control scenario in which the full bottom tissue surface is exposed to PO2 perturbations. This would experimentally simulate using the full gas exchange chamber. As shown in Figure 3, at 40 mmHg, steady-state tissue PO2 and capillary [ATP] distributions are comparable to the no-flux control condition. At the venular end of the capillaries, SO2 values ranged from ~50% for surface capillaries (21, 18, and 17) to ~40% for capillaries deeper than 100 μm into the tissue (capillary 54), and the corresponding capillary [ATP] values were within 15% of those at zero O2 flux boundary condition. However, under imposed tissue hypoxia (15 mmHg), the surface capillaries dropped their SO2 by ~70% which corresponded to ~40% higher steady state capillary [ATP] relative to zero flux condition (Figure 3C). This was clearly depicted in the corresponding vessel map (Figure 3B). The deeper capillary (54) was less affected with ~30% lower hemoglobin SO2 and ~12% increase in ATP release relative to zero flux. Exposing the full tissue surface to relatively high capillary PO2 (150 mmHg) had the most significant impact on [ATP] in the capillary network. At 150 mmHg, hemoglobin SO2 in both surface and deep tissue capillaries converged to ~100% with ~70% decrease in steady state [ATP] relative to no-flux (Figure 3C). The depth of the PO2 perturbation into the tissue when using the full gas exchange chamber was ~100 μm as shown in the 3D PO2 profiles (Figure 3A).

Circular O2 delivery micro-outlet

To investigate the effect of limiting the number of capillaries stimulated by local tissue PO2 perturbations, we started by modeling capillary SO2 and [ATP] changes when using a circular O2 micro-outlet (100 μm in diameter, see Figure 1). Similar to previously discussed data (Ghonaim et al., 2011), substantive changes in local tissue PO2 due to diffusion outwards from the circular outlet is limited to less than ~50 μm, as shown in the 3D tissue PO2 profiles (Figure 4A). Also, the hypoxic and hyperoxic stimuli were highly localized to only those capillaries directly over the micro-outlet (17, 18, 21) as shown in the vessel maps (Figure 4B). At 40 mmHg chamber PO2 level, calculated capillary SO2 and [ATP] were in close agreement with the no-flux control for both surface and deep tissue capillaries with values being within ~1 and ~3%, respectively (Figure 4C). Under imposed hypoxia, the capillary SO2 dropped as capillaries crossed the micro-outlet region reaching a minimum value ~40 μm downstream of the outlet after which SO2 levels increased slightly due to re-oxygenation by surrounding capillaries. At the venular end, steady state SO2 levels in surface capillaries were 15% lower relative to zero flux while capillary 54 experienced only a 6% drop in SO2. This corresponded to only 10% increase in [ATP] in surface capillaries while [ATP] in capillary 54 remained unchanged relative to zero flux. At 150 mmHg, the increase in capillary SO2 level is observed directly over the micro-outlet region reaching a maximum at the outlet exit. The capillary SO2 levels dropped sharply downstream of the outlet due to O2 diffusion into adjacent capillaries and tissue. Surface capillary SO2 decreased to ~63 and deep tissue capillaries to 51% ~200 μm downstream of the outlet. This corresponded to ~40% decrease in [ATP] in surface capillaries and ~20% decrease in [ATP] of deeper tissue capillaries relative to zero flux condition.

Square O2 delivery micro-outlet

Next, we simulated the effect of increasing the area of O2 exchange, and hence perturbing a greater number of capillaries, by simulating an O2 delivery micro-outlet 200 × 200 μm square. Similar to the circular micro-outlet design and as previously described (Ghonaim et al., 2011), the change of local tissue PO2 surrounding the square outlet is limited to less than ~50 μm, as shown in the 3D tissue PO2 profiles (Figure 5A). In the case of the square micro-outlet, a larger number of surface capillaries experience the PO2 perturbations, 7 of which were directly over the micro-outlet (Figure 5B). Also, capillaries at both sides of those directly over the outlet seemed to be slightly affected by the PO2 perturbations. At 40 mmHg, calculated SO2 and capillary [ATP] distributions were similar to the no-flux control with surface capillaries having 15% higher SO2 and 10% lower [ATP] values relative to zero flux condition (Figure 5C). As observed with the circular micro-outlet, re-oxygenation of stimulated capillaries following imposed hypoxia (15 mmHg) was at ~40 μm downstream of the square micro-outlet (Figure 5C). At the capillary venular end, SO2 level of surface capillaries dropped by ~51% while capillary 54 experienced only a 15% drop in SO2 relative to zero flux. This corresponded to ~32% increase in [ATP] in surface capillaries.
while only 7% increase in [ATP] in capillary 54 relative to zero flux. At 150 mmHg, capillary SO₂ levels increased across the micro-delivery outlet reaching maximum values at the venular end of the outlet region. Similar to the results observed with the circular micro-outlet, SO₂ values sharply dropped downstream of the square micro-outlet bringing surface capillary SO₂ to ~83% and deeper capillaries to ~70% ~200 μm downstream of the outlet. This corresponded to ~66% decrease in [ATP] in surface capillaries and ~42% decrease in [ATP] of deeper tissue capillaries.

**Rectangular O₂ delivery micro-slit**

The largest dimensions for an O₂ delivery micro-outlet currently being tested in our *in vivo* studies are for a rectangular micro-slit (1000 μm wide × 200 μm long). Since the 3D tissue dimensions in our computational model are less than the
width of the experimental micro-slit, the effect of the slit extends to both edges of the tissue allowing us to visualize the depth of the PO2 distribution into the tissue. As shown in the 3D PO2 plots (Figure 6A), the PO2 perturbations extended ~100 μm into the tissue with local tissue PO2 changes similar to what was observed with other outlet designs. All surface capillaries shown on the vessel map are affected by the PO2 perturbation as the outlet covers the entire surface width (Figure 6B).

At 40 mmHg, calculated SO2 and capillary [ATP] distributions were similar to the no-flux control with surface capillaries having 17% higher SO2 and 10.3% lower [ATP] values relative to zero flux O2 boundary condition (Figure 6C). Under imposed hypoxia (15 mmHg), re-oxygenation of de-saturated surface capillaries was not observed within 200 μm downstream of the micro-slit. However, capillary SO2 seemed to plateau approximately 100 μm downstream of the micro-slit. At the capillary

FIGURE 4 | Simulations of 3D PO2 and capillary [ATP] distribution in a tissue with idealized parallel capillary arrangement (72 hexagonally packed capillaries). In these simulations, we are modeling O2 delivery through a circular oxygen micro-delivery outlet (100 μm in diameter) to bottom tissue surface using novel micro-delivery approach (see Figure 1). Tissue surface directly on top of the micro-delivery outlet is exposed to 15, 40, or 150 mmHg chamber PO2 level relative to a zero flux control boundary condition (A) Spatial 3D tissue PO2 distribution (mmHg) at capillary entrance perspective (B) a capillary exit perspective showing combined X-Z plane slice at Y = 150 μm and Y-Z plane slice at X = 277 μm (C) bottom perspective of a vessel map depicting distribution of [ATP] (mol/L = M) along the capillaries. Bolded arrow marks capillary entrance (D) Plots of SO2 (%) and [ATP] changes along capillary length in selected capillaries (21, 18, 17, 54) marked by arrows on the vessel map. Capillaries 21 and 17 are 16 μm from tissue surface, capillary 18 is 33 μm from tissue surface, and capillary 54 is deeper in the tissue, at 133 μm, and hence it is not shown in the current perspective of the vessel map.
Ghonaim et al. Modeling SO₂-dependent capillary [ATP] changes

FIGURE 5 | Simulations of 3D PO₂ and capillary [ATP] distribution in a tissue with idealized parallel capillary arrangement (72 hexagonally packed capillaries). In these simulations, we are modeling O₂ delivery through a square oxygen micro-delivery outlet (200 × 200μm) to bottom tissue surface using our previously described novel micro-delivery approach (see Figure 1). Tissue surface directly on top of the micro-delivery outlet is exposed to 15, 40, or 150 mmHg chamber PO₂ level relative to a zero flux control boundary condition (A). Spatial 3D tissue PO₂ distribution (mmHg) at capillary entrance perspective (B) a capillary exit perspective showing combined X–Z plane slice at Y = 150 μm and Y–Z plane slice at X = 277 μm (C) bottom perspective of a vessel map depicting distribution of [ATP] (mol/L = M) along the capillaries. Bolded arrow marks capillary entrance (D) Plots of SO₂ (%) and [ATP] changes along capillary length in selected capillaries (21, 18, 17, 54) marked by arrows on the vessel map. Capillaries 21 and 17 are 16 μm from tissue surface, capillary 18 is 33 μm from tissue surface, and capillary 54 is deeper in the tissue, at 133 μm, and hence it is not shown in the current perspective of the vessel map.

venular end, SO₂ level of surface capillaries dropped by ~56% while capillary 54 experienced a ~20% drop in SO₂ relative to zero flux condition. This corresponded to ~35% increase in [ATP] in surface capillaries and only 8% increase in [ATP] in capillary 54 relative to zero flux. At 150 mmHg, capillary SO₂ levels increased across the micro-delivery outlet reaching maximum values at the venular end of the outlet region. Similar to the results observed with the previously discussed micro-outlet designs, SO₂ values instantly dropped downstream of the rectangular micro-slit bringing surface capillary SO₂ to ~90% and deep capillaries to ~80% ~200 μm downstream of the outlet. This corresponded to ~69% decrease in [ATP] in surface capillaries and ~55% decrease in [ATP] of deeper tissue capillaries.
FIGURE 6 | Simulations of 3D PO2 and capillary [ATP] distribution in a tissue with idealized parallel capillary arrangement (72 hexagonally packed capillaries). In these simulations, we are modeling O2 delivery through a rectangular oxygen micro-delivery outlet (1000 μm wide × 200 μm long) to bottom tissue surface using our previously described novel micro-delivery approach (see Figure 1). Tissue surface directly on top of the micro-delivery outlet is exposed to 15, 40, or 150 mmHg chamber PO2 level relative to a zero flux control boundary condition (A) Spatial 3D tissue PO2 distribution (mmHg) at capillary entrance perspective (B) a capillary exit perspective showing combined X–Z plane slice at Y = 150 μm and Y–Z plane slice at X = 277 μm (C) bottom perspective of a vessel map depicting distribution of [ATP] (mol/L = M) along the capillaries. Bolded arrow marks capillary entrance (D) Plots of SO2 (%) and [ATP] changes along capillary length in selected capillaries (21, 18, 17, 54) marked by arrows on the vessel map. Capillaries 21 and 17 are 16 μm from tissue surface, capillary 18 is 33 μm from tissue surface, and capillary 54 is deeper in the tissue, at 133 μm, and hence it is not shown in the current perspective of the vessel map.

Comparing change in relative ATP magnitude in response to varying the area of imposed tissue hypoxia

The change in the total magnitude of ATP (ATPtot) in the modeled network relative when imposing a hypoxic challenge (15 mmHg boundary condition) was calculated as percent increase above ATPtot at zero flux (Figure 7). Percent increase in ATP magnitude in the network was compared when exposing all of the bottom tissue surface to hypoxia (full chamber) or locally using the three micro-outlet designs discussed above. As shown in Figure 7, the total ATP magnitude increased with increase in micro-outlet dimensions and essentially the number of capillaries experiencing the PO2 drop. The percent increase in ATPtot was more than doubled when locally perturbing tissue PO2 using the rectangular micro-slit compared to the other micro-outlet
In order to investigate the role terminal arterioles play in regulating \( SO_2 \)-mediated ATP signaling in capillary networks, particularly in the EDL muscle where larger arterioles are located much deeper in the tissue, the 3D idealized capillary geometry was modified to include a terminal arteriole, 9 \( \mu \text{m} \) in diameter, positioned 30 \( \mu \text{m} \) away from bottom tissue surface. The 3D tissue PO\(_2\) distribution as well as \( SO_2 \) and [ATP] in the arteriole (ves-\( \text{sel} \) 69) and in the surrounding surface (capillaries 14 and 17) and deep tissue capillaries (represented by capillary 50) were modeled.

Simulations were run for the case in which the full tissue surface is exposed to PO\(_2\) perturbations (original gas exchange chamber) and for the case of spatially limited O\(_2\) delivery using the rectangu-\( \text{lar} \) O\(_2\) delivery micro-slit. Also, the effect of varying arteriolar entrance \( SO_2 \) on the overall magnitude of ATP in response to altered tissue PO\(_2\) was examined.

**Full surface gas exchange chamber at 65 and 80% arteriolar entrance \( SO_2 \)**

In the 3D tissue PO\(_2\) profiles and [ATP] vessel maps generated for these simulations, the PO\(_2\) perturbations were shown to affect the terminal arteriole to a much lesser extent than the surface capillaries (Figures 8A,B, 9A,B). Also, these simulations showed the influence of the arteriole as an O\(_2\) source on the \( SO_2 \) levels of nearby surface capillaries. For instance, the steady state \( SO_2 \) level in capillary 14, positioned right next to the arteriole, was \(~25\%\) higher than the zero flux control condition when exposed to 40 mmHg chamber PO\(_2\) and identical to the \( SO_2 \) level of the terminal arteriole (Figures 8, 9). However, the \( SO_2 \) level of the deeper tissue capillary (50), which was located at the same depth as capillary 54, was unchanged relative to zero flux. In general, the different arteriolar entrance \( SO_2 \) has no effect on the surface or deep tissue capillaries and had minimal influence on the arterio-\( \text{lar} \) \( SO_2 \) at steady state. At 15 mmHg, the \( SO_2 \) level of the terminal arteriole entering at 65\% dropped by 60\% relative to zero flux condition corresponding to 44\% increases in [ATP]. A smaller drop in SO\(_2\) was calculated (52\% decrease) for the arteriole entering at 80\% corresponding to 40\% increase in [ATP]. The \( SO_2 \) level in the surrounding surface capillaries as well as deeper tissue capillaries dropped by \(~70\%\) and 35\%, respectively, corresponding to \(~45\%\) and 16\% higher steady state capillary [ATP] relative to zero flux (Figures 8C, 9C). At 150 mmHg, hemoglobin SO\(_2\) levels in surface and deep tissue capillaries as well as in the arteriole converged to \(~100\%\) with \(~77\%\) decrease in steady state [ATP] in the capillaries and 75\% decrease in [ATP] in the arteriole relative to zero flux control (Figures 8C).
FIGURE 8 | Simulations of 3D PO2 and capillary [ATP] distribution in a tissue with idealized parallel capillary arrangement (68 hexagonally packed capillaries), which includes a traversing terminal arteriole (vessel 69) at an entrance SO2 of 65%. In these simulations, we are modeling O2 delivery to bottom tissue surface using the full gas exchange chamber (Ghonaim et al., 2011; Ellis et al., 2012). Full bottom tissue surface is exposed to 15, 40, or 150 mmHg chamber PO2 level relative to a zero flux control boundary condition (A) Spatial 3D tissue PO2 distribution (mmHg) at capillary entrance perspective (B) a capillary exit perspective showing combined X–Z plane slice at Y = 150 μm and Y–Z plane slice at X = 266 μm (C) bottom perspective of a vessel map depicting distribution of [ATP] (mol/L = M) along the arteriole and surrounding capillaries. Bolded arrow marks arteriolar and capillary entrance (D) Plots of SO2 (%) and [ATP] changes along vessel length in selected vessels (14, 17, 69-arteriole, 50) marked by arrows on the vessel map. Capillary 17 is 16 μm from tissue surface, the arteriole and capillary 14 are 33 μm from tissue surface, and capillary 50 is deeper in the tissue, at 133 μm, yet is shown adjacent to the arteriole in the current perspective of the vessel map.

steady state magnitude of ATP in the arteriole (ATPart) at various tissue PO2 conditions was calculated and normalized against total ATP magnitude in the network (ATPtot) under zero flux condition (Figure 12). The relative arteriolar ATP magnitudes were calculated when full tissue surface is exposed to the PO2 perturbations (full gas exchange chamber) or to local perturbations using the rectangular O2 delivery micro-slit. As shown in Figure 12, the arteriolar ATP magnitude decreased with increase in chamber PO2 level. However, the model suggested that under hypoxic conditions (15 mmHg), the terminal arteriole would contribute less than 3% of the total ATP signal originating from a capillary network. Also, although the percent decrease in ATP magnitude in the arteriole is similar to that calculated
FIGURE 9 | Simulations of 3D PO2 and capillary [ATP] distribution in a tissue with idealized parallel capillary arrangement (68 hexagonally packed capillaries), which includes a traversing terminal arteriole (vessel 69) at an entrance SO2 of 80%. In these simulations, we are modeling O2 delivery to bottom tissue surface using the full gas exchange chamber (Ghonaim et al., 2011; Ellis et al., 2012). Full bottom tissue surface is exposed to 15, 40, or 150 mmHg chamber PO2 level relative to a zero flux control boundary condition (A) Spatial 3D tissue PO2 distribution (mmHg) at capillary entrance perspective (B) a capillary exit perspective showing combined X-Z plane at \( Y = 150 \mu \text{m} \) and Y-Z plane slice at \( X = 266 \mu \text{m} \) (C) bottom perspective of a vessel map depicting distribution of [ATP] (mol/L = M) along the arteriole and surrounding capillaries. Bolded arrow marks arteriolar and capillary entrance (D) Plots of SO2 (%) and [ATP] changes along vessel length in selected vessels (14, 17 – arteriole, 50) marked by arrows on the vessel map. Capillary 17 is 16 \( \mu \text{m} \) from tissue surface, the arteriole and capillary 14 are 33 \( \mu \text{m} \) from tissue surface, and capillary 50 is deeper in the tissue, at 133 \( \mu \text{m} \), yet is shown adjacent to the arteriole in the current perspective of the vessel map.

for the total network when increasing chamber PO2 from 15 to 150 mmHg, the absolute change in ATP magnitude (moles) in the arteriole is \( \sim 95\% \) less. Finally, it should be noted that [ATP] in the arteriole is \( \sim 20\% \) lower when limiting area of PO2 perturbations using the rectangular micro-slit.

**DISCUSSION**

In the microcirculation, ATP is released from the erythrocytes in an SO2 dependent manner. Released ATP would bind to purinergic receptors on the vascular endothelium which activates a signaling pathway leading to the opening of Ca\(^{2+}\)-gated K\(^+\) channels and the hyperpolarization of the endothelial cell
FIGURE 10 | Simulations of 3D PO2 and capillary [ATP] distribution in a tissue with idealized parallel capillary arrangement (68 hexagonally packed capillaries), which includes a traversing terminal arteriole (vessel 69) at an entrance SO2 of 65%. In these simulations, we are modeling O2 delivery through a rectangular oxygen micro-delivery outlet (1000 μm wide × 200 μm long) to bottom tissue surface using our previously described novel micro-delivery approach (see Figure 1). Tissue surface directly on top of the micro-delivery outlet is exposed to 15, 40, or 150 mmHg chamber PO2 level relative to a zero flux control boundary condition (A) Spatial 3D tissue PO2 distribution (mmHg) at capillary entrance perspective (B) a capillary exit perspective showing combined X–Z plane slice at Y = 150 μm and Y–Z plane slice at X = 266 μm (C) bottom perspective of a vessel map depicting distribution of [ATP] (μmol/L = M) along the arteriole and surrounding capillaries. Bolded arrow marks arteriolar and capillary entrance (D) Plots of SO2 (%) and [ATP] changes along vessel length in selected vessels (14, 17, 69-arteriole, 50) marked by arrows on the vessel map. Capillary 17 is 16 μm from tissue surface, the arteriole and capillary 14 are 33 μm from tissue surface, and capillary 50 is deeper in the tissue, at 133 μm, yet is shown adjacent to the arteriole in the current perspective of the vessel map.

(Ellsworth et al., 2008; Tran et al., 2012). The hyperpolarization signal is then conducted upstream through gap junctions. At the arteriolar wall, the incoming hyperpolarization signal is conducted to the SMC layer through myo-endothelial gap junctions resulting in vaso-relaxation and increase in erythrocyte supply rate (Ellsworth et al., 2008; Tran et al., 2012). The magnitude of the hyperpolarization signal would depend on the number of endothelial cells activated along the capillary and on the total number of capillaries stimulated within a network under hypoxic conditions. This understanding of how erythrocyte-released ATP controls micro-vascular O2 delivery is consistent with the modeling results presented in this paper. The net increase in total ATP magnitude in the network with increase in the area exposed to hypoxia is the summative contribution of additional stimulated...
FIGURE 11 | Simulations of 3D PO2 and capillary [ATP] distribution in a tissue with idealized parallel capillary arrangement (68 hexagonally packed capillaries), which includes a traversing terminal arteriole (vessel 69) at an entrance SO2 of 80%. In these simulations, we are modeling O2 delivery through a rectangular oxygen micro-delivery outlet (1000μm wide × 200μm long) to bottom tissue surface using our previously described novel micro-delivery approach (see Figure 1). Tissue surface directly on top of the micro-delivery outlet is exposed to 15, 40, or 150 mmHg chamber PO2 level relative to a zero flux control boundary condition (A) Spatial 3D tissue PO2 distribution (mmHg) at capillary entrance perspective (B) a capillary exit perspective showing combined X–Z plane slice at Y = 150μm and Y–Z plane slice at X = 266μm (C) bottom perspective of a vessel map depicting distribution of [ATP] (mol/L = M) along the arteriole and surrounding capillaries. Bolded arrow marks arteriolar and capillary entrance (D) Plots of SO2 (%) and [ATP] changes along vessel length in selected vessels (14, 17, 69-arteriole, 50) marked by arrows on the vessel map. Capillary 17 is 16μm from tissue surface, the arteriole and capillary 14 are 33μm from tissue surface, and capillary 50 is deeper in the tissue, at 133μm, yet is shown adjacent to the arteriole in the current perspective of the vessel map.

capillaries (Figures 3–7). Also, these results help explain our observations of no vascular response when experimentally testing the effect of O2 delivery through a circular micro-outlet (100μm in diameter) in vivo (Ghonaim et al., 2011). Although this design maybe optimal for locally altering SO2 in single capillaries, the stimulus would probably not be sufficient to elicit a micro-vascular response. Increasing the dimensions of the micro-outlet would be necessary to stimulate a large enough number of capillaries, thus amplifying total magnitude of ATP release and signal.

Also, as our modeling data suggest, increasing the micro-outlet dimensions minimizes the effect of stimulated capillary
needed to elicit a micro-vascular response. This indicates the rectangular micro-slit would be optimal for stimulating enough capillaries by imposed hypoxia to generate high enough ATP signal.

The limited amount of change in tissue PO₂ due to diffusion (∼50 μm), as measured from the 3D tissue PO₂ profiles, beyond the edge of the micro-outlets (Figures 4A–6A and 4B–6B) was consistent with our previous observations (Ghonaim et al., 2011). The simulations indicated that the PO₂ perturbations are highly localized to only those capillaries directly over the micro-outlet region. Experimentally, the results suggest that the micro-outlet should be positioned at least 50 μm downstream of the terminal feeding arteriole to ensure that micro-vascular responses are only elicited from the capillaries positioned directly over the outlet. The extent of axial O₂ diffusion in the tissue when using the rectangular micro-slit was 50% deeper than that previously modeled for the circular micro-outlet (Figures 6B, 10B, 11B) (Ghonaim et al., 2011) and similar to that of the full surface model (Ghonaim et al., 2011; Ellis et al., 2012). Due to the shape of the PO₂ profile, the maximal axial diffusion distance is estimated from the center of the outlet. The increase in the axial diffusion distance might be a compromise when using larger O₂ micro-outlets. With our current microscopic techniques we are unable to resolve vessels deeper than 60 μm.

Since in our experiments, we examine micro-vascular signaling from selected capillaries, it was critical that we assess the possible contribution of arterioles beyond our ability to focus. Since arterioles have relatively higher erythrocyte velocities than in the capillaries, they are anticipated to experience a much lesser change in SO₂ in response to PO₂ perturbations. This was supported by our simulation data (Figures 8–11). The main effect of a nearby terminal arteriole on a capillary within 50 μm is that it would act as an O₂ source. As shown in our modeling data (Figures 8D–11D), higher measured SO₂ in a capillary relative to other capillaries with comparable flow rates in the same preparation might imply the presence of a nearby arteriole. Since arterioles in the EDL muscle preparation are deeper in the tissue, their contribution to the total magnitude of ATP in a locally stimulated capillary network is probably negligible. The contribution of a terminal arteriole positioned directly over the micro-slit ∼30 μm from bottom surface was calculated to be less than 3% of the total magnitude of the ATP (Figure 12). Hence, when locally stimulating capillaries, even in the presence of an underlying arteriole, the observed micro-vascular responses mediated by intra-luminal ATP would be primarily due to ATP released in the stimulated capillaries.

In conclusion, we have modeled SO₂-dependant changes in [ATP] at steady state in 3D idealized parallel capillary networks in response to local PO₂ perturbations. As the number of affected capillaries increases, the total magnitude ATP in the network increases. The results indicated that O₂ delivery or removal to overlaying tissue through a rectangular micro-slit (1000 μm wide × 200 μm long) would be optimal relative to other micro-outlet designs of smaller dimensions or a full surface classical exchange type chamber. Using the rectangular micro-slit it is anticipated...
that a sufficient number of capillaries will be stimulated to produce a large enough magnitude of ATP to elicit microvascular responses. This would be accomplished while maintaining the stimulus localized to the selected capillaries. The results also indicated that terminal arterioles have minimal influence on the total magnitude of ATP in the network under hypoxic condition. Hence, when locally stimulating the capillary bed, the majority of the signal elicited by ATP release would originate in the capillaries. The computational model presented provides valuable insights into how to study the ATP release mechanism and signaling in capillary networks in vivo. The modeling data help guide us in the design of an optimal tool for studying SO2-dependent ATP release in capillaries. In the future, we aim to model time-dependent ATP release to local PO2 perturbations in a realistic capillary network geometry reconstructed from experimental data. Combining our in vivo experimental observations with computational modeling of the dynamics of SO2-dependent ATP release will help provide a more comprehensive understanding of O2 mediated blood flow regulation in microvascular networks.

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