A Direct non-destructive method for determination of sulphur in ore samples using EDXRF spectrometry

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Abstract

A direct non-destructive Energy Dispersive X-Ray Fluorescence (EDXRF) method for the determination of sulphur, in solid uranium ores and intermediates obtained from the alkaline recovery process for uranium from its ores, has been developed. The method involves thorough grinding of a few mg of solid powder samples to fine particle size, mixing the fine powder thus obtained, with a few drops of 10% collodion in amyl acetate solution to make a paste. A very small amount of this paste was transferred with the help of the pestle tip, spread uniformly in the form of thin slurry on Mylar films, and dried to make very thin sample specimen on thin Mylar film supports. These specimens were presented for EDXRF measurements. A calibration plot was made by plotting the intensity ratios of S Kα and Rayleigh scattered peak of the excitation source (Ge Kα) against sulphur percent in the certified reference materials (CRMs). It was found that the precision obtained using this methodology was within 5% (±1σ) and the deviation of the EDXRF analytical results from the expected values of CRM was within 7%. The developed method was successfully applied for the determination of sulphur in the samples obtained from the different stages of the uranium ore processing using alkaline based leaching method.

Key words: EDXRF, Sulphur, Uranium ores, Rayleigh scattering

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Introduction:

The most important application of uranium is its use as nuclear fuel in the reactors for generation of electricity. Worldwide the U content in most of the ores varies from 0.02% to 0.2% as U₃O₈. Recovery of U, from the ores, is a very important step in nuclear fuel cycle, which involves dissolution of the ores and extraction of uranium from the ores efficiently. In view of presence of low grade uranium ores (400–2500 ppm U₃O₈) in India, the recovery process of uranium from its ore needs to be as efficient as possible [1]. Uranium is extracted from its ores, either by acidic leaching in sulphuric acid or by alkaline leaching in sodium carbonate [1, 2]. In India, carbonate based uranium ores are present in Tummalapalle in Andhra Pradesh and Gogi in Karnataka which requires alkaline leaching process. Under ambient temperature and atmospheric pressure, the gangue minerals present in the ores play a very insignificant role. However, under elevated temperature and pressure conditions, some of these minerals are susceptible to dissolution. Pyrite (FeS₂) is one of the most common sulphide ores, usually present upto 2% along with uranium ores. During alkaline leaching process, FeS₂ forms Fe(OH)₂, gets dissolved and starts leaching with the carbonate along with uranium. The dissolution of uranium ores associated with pyrites requires elevated temperature (< 100 °C) in oxidising conditions for complete dissolution. Presence of significant amount of sulphide in the ores, results in excessive consumption of the leachants and the reactive conditions required for its dissolution, in turn, dissolves some other gangue materials also in the alkaline leachants. This results in increased total dissolved solute (TDS) content in the leach liquor. These undesired materials in the leach liquor hinder the effective recovery of uranium from the ores [1]. In view of the above discussions regarding importance of sulphur in alkaline processing of uranium ores for uranium recovery, it is essential to determine the sulphur content in the ores as well as in the intermediate residues obtained at different stages of leaching process for optimising the leaching conditions. Such determinations shall be beneficial for adopting an efficient method of uranium recovery by alkaline dissolution process. This requires a simple and fast, preferably a non destructive method of sulphur determinations in uranium ores and processing materials on routine basis.

The conventional methods used for the determinations of sulphur are ion chromatography [3], and for analysis in solid samples directly, combustion of the samples in air atmosphere to form SO₂, followed by infrared detection of SO₂ for quantification is used [4]. However these techniques require either dissolution of the samples or heating the samples to high temperatures which make these methods time consuming as well as tedious. Sometimes samples are pyrohydrolysed and the sulphur content is collected in a condensate and then analysed. Pyrohydrolysis of solid samples for
separation of matrix followed by the determination of sulphur by inductively coupled plasma optical emission spectrometry (ICP OES) and ion chromatography (IC) are also used [5]. Recently, a triple quadrupole inductively coupled plasma mass spectrometry method was reported for determination of sulphur and phosphorus in UOC samples. Here also the samples are dissolved in HNO₃ using normal as well as microwave digestion method [6]. However, for sulphur determinations in uranium ores on routine basis, a simple and non destructive method will be more suitable.

X-Ray Fluorescence (XRF) is a fast, versatile and efficient multi-elemental determination method in solid samples with no requirement of sample dissolution [7]. Because of its numerous advantages, it is being widely used in several areas for research and routine sample analysis [8-10]. However, XRF suffers from severe matrix effect and requires matrix matched standards for quantification. There are many methods for minimising the matrix effect in XRF analysis [8]. Presentation of the sample in the form of thin specimens is one of the methods to minimize the matrix effect to some extent [11]. Further, in XRF, determination of low atomic number (Z) elements in presence of medium and high Z matrix elements is another challenge [12]. The fluorescence yields of the characteristic X-ray analytical lines of low Z elements are very less (e.g. 0.06 for sulphur). In addition, the low energy X rays emitted from low Z elements are absorbed appreciably by the medium and high Z elements, present in the sample, which have high mass absorption cross section. These factors lead to further decrease in the fluorescent intensity of the low Z elements when analyzed by XRF. Moreover, the X ray lines of medium and high Z elements interfere severely with the K lines of low Z elements. The Mo L line (2.29 keV) and Pb M line (2.34 keV) interferes with S Kα. Presence of these elements complicates the quantification process. So for XRF determination of sulphur having characteristic X-ray energy of 2.31 keV (S Kα), the above stated problems have to be taken care of.

In U ore samples, the quantity of sulphur is generally less than 2%, hence a proper sample preparation procedure, which will take care of the low sulphur concentration as well as the matrix effect, is needed. Dissolving the sample has many disadvantages such as addition of corrosive acids, incorporation of impurities, loss of volatile elements and it is time consuming tedious process. So, non destructive methods are preferred to avoid the above stated problems. Presentation of the sample as a thin paste and quantification using the primary scattered peaks of the target element is a very simple method for non destructive analysis of solid samples without addition of any internal standard [13]. This method of quantification is based on the fact that the intensities of the characteristic X-rays of the analyte element and that of the scattered peak vary in a similar way as
the composition of the matrix. In fact, it is reported that for elimination of matrix effect both Compton and Rayleigh scattered peaks can be used [13, 14]. Since, the ratio of the characteristic X-ray peak and the scattered peak, is less sensitive towards variation in composition and amount of the sample, it can be used for the correction of the matrix effects [13].

This paper describes the development of a direct non destructive Energy Dispersive (ED) XRF method for determination of sulphur in samples obtained during various stages of the alkaline leaching process of uranium ores. The method is very simple and is suitable for routine analysis of ore samples.

**Experimental:**

**Sample Preparation:**

The calibration plots for EDXRF analysis were made using CRMs for sulphur from “GEOSTATS PTY LTD”. The sulphur content in these ore standards were upto 2%. The details of these standards are given in Table 1. About 100 mg of the solid ore CRMs were first finely ground in a clean pestle mortar for about 10 minutes. A few drops of 10% collodion solution in amyl acetate solution were added to this fine powder in the mortar itself. Collodion is a very sticky solvent which sticks to any surface quite strongly after drying. The collodion mixed standard powders in the mortar were ground again for about five minutes. Uniform slurries of the standards were thus obtained. Each standard was processed in separate mortars to avoid cross contamination. The well mixed slurries were again ground with the tip of the pestle and the pestle tip was just touched at the centre of 4 μm thin Mylar films stretched uniformly over PET sample cups, used for EDXRF measurement of liquid samples. The Mylar films were uniformly stretched over these cups by enclosing them on the cups and pressed by same size PVC rings as shown in Fig. 1. The pestle was touched and slightly rubbed on the Mylar film, from inside of the cup so that a few mg of the sample was transferred on the Mylar film. The specimens formed were left to dry in ambient atmosphere. After drying a thin uniform film of the standards were formed on the Mylar. For each standard and sample, three such specimens were made and presented for XRF measurements. The sample obtained from the different stages of the uranium ore processing, using alkaline based leaching method, were also processed similarly and analyzed after measuring their EDXRF spectra in the similar manner.

**Instrumentation:**
For EDXRF measurements, a Jordan Valley EX-3600TEC EDXRF spectrometer having Rh X-ray tube target was used. The instrument is equipped with a twelve-position sample chambers and can measure the samples sequentially. There is a provision for using different X-ray filters, placed between the X-ray tube and sample holder. The filters can be used for reducing the background in particular energy range depending on the elements of interest. Three secondary targets Gd, Ge and Al are provided to excite elemental X-ray lines efficiently and reduce the spectral background as per the energy of absorption edges of the analytes. Maximum power capacity of the EDXRF spectrometer is 50 W with maximum voltage and current of 50 kV and 3000 μA, respectively. In order to excite S Kα efficiently and reduce the spectral background, Ge secondary target was used for excitation of the samples by Ge Kα (9.89 keV) generated from the secondary target. The current and voltage applied to the X-ray tube were 2000μA and 20 kV, respectively. The X-rays were detected by a peltier cooled Si-PIN diode detector, having a resolution of 140 eV (FWHM) at 5.9 keV. All measurements were carried out in air atmosphere. The measurement time was 1000 s for each specimen.

All the EDXRF spectra were processed using the EDXRF 32 program from ITAL structures, Italy. It is an X ray peak profile fitting program which is based on nonlinear least-squares fitting using Marquardt algorithm [15]. This program was used for processing and calculating the intensities of S Kα and Ge Kα lines. In this study we observed that the profile fitting of Ge Kα Rayleigh scattered peak was more precise compared to that of Compton scattered peak using this program. Hence, we have taken the Rayleigh scattered peak for normalizing the analyte peak intensity.

Results and Discussion:

Though EDXRF is a well established method for non destructive analysis of a variety of samples, determination of sulphur in uranium ore, having medium and high Z matrix elements is quite challenging due to several reasons discussed above. Presentation of solid samples in form of pellets requires more sample amount. As the pellets are of infinite thickness, during XRF analysis, high background and severe matrix effect are encountered. In order to overcome these problems, an EDXRF method with thin specimens was developed in our laboratory [11]. The thin film specimens were made by drying the solution samples on the scotch tape. However, dissolution of the ore samples is a difficult task. So, a thin film of the solid sample on the thin support was made
by placing the slurry of the sample on Mylar film. Since the specimens have been made using finely ground paste of the sample in collodion and presented it in form of thin film slurry, the matrix effects were minimised but not completely removed. Such matrix effect can be taken care by using the intensity ratio of the analyte peak and Compton or Rayleigh scattered peak of the target. Hence the calibration plot was made using the intensity ratios of analyte peak and the scattered Rayleigh peak of the exciting radiation (Ge Kα). Using such ratio for quantification, shall mitigate the matrix effect to a large extent as this ratio is insensitive to the variation in the matrix composition, but depends on the concentration of the trace analytes. In addition, taking such ratio shall also mitigate the error due to sample geometry and area of the sample exposed to the exciting X ray beam. Also, as stated above for efficient excitation of S Kα and reducing the background further, Ge secondary target excitation shall be beneficial. All above features were included in the present work for development of an accurate, fast and simple method for determination of sulphur in ore matrices. The EDXRF spectrum of a CRM containing 2% sulphur excited by Ge secondary target is shown in Fig.2. The X-ray peaks of Si, Ar, K, Ti, V, Cr, Fe, Cu and Zn along with the sulphur peak were observed in the EDXRF spectrum of the standard. The U M lines (3.17 keV) have interference with K Kα lines (3.31 keV) and have been shown in the figure. The EDXRF detection limit of sulphur was determined using the standard containing 0.51 ± 0.04 % sulphur and measurement time of 1000s and it was found to be to be 0.03%.

The sample obtained from the different stages of the uranium ore processing, contained traces of U and Pb. Using Ge secondary target the M lines of U and Pb can be excited. The Pb M lines (2.35 keV) interfere with S K line (2.31 keV). However, as Pb is present in a few ppm level and the M lines of Pb have very low fluorescence yield (0.03), the intensity of Pb M lines will be very less [16]. Moreover, the EDXRF 32 program was used for the elemental X-ray peak fitting and this program can take care of any X-ray interferences by profile fitting and gives individual intensities of interfering elemental X ray peaks [15]. So even if some traces of Pb was present in the sample, the EDXRF 32 program can calculate the area of S K peak and Pb M line contributions, seperately.

For making the calibration plot, the intensity ratios of S Kα and scattered peak of Ge Kα was plotted against the sulphur percentage in the CRMs. The calibration was found to be linear and is shown in the Fig. 3. The equation obtained was

\[ y = 136.26 x + 0.033 \quad (1) \]

and the \( R^2 = 0.9958 \). Despite variation in the amount of sample that was deposited on the mylar film support, a linear calibration was obtained indicating that the ratio of characteristic X –ray line of the
analyte and scatterer peak is not affected by any other parameter except the sulphur concentration. So the scattered peak acts as external standard which takes care of the matrix effect occurring in the sample. In order to validate the developed method, another set of the standards specimens were prepared and analysed using the above equation. The analytical results along with the accuracy and precision obtained are tabulate in Table 2. The precision obtained was within 5% (RSD, ±1σ) and the deviation of the EDXRF analytical results from the expected values was within 7%. Using the above calibration plot, the sulphur contents in some of the ores samples obtained during uranium ore processing, were determined. The samples were taken from different stages of ore processing process and analysed in similar manner as the standards. Different types of sample such as, finely ground ore samples without any processing, residues of samples before attaining the final temperature and pressure, and sample residues obtained after 6 hrs of leaching at the temperature of 130°C with 4kg/cm² O₂ pressure were analysed using the developed procedure. The analytical results obtained are given in Table 3.

Thus, a simple, non-destructive, direct EDXRF method for sulphur determination in uranium ore samples without the requirement of any laborious sample preparation procedure such as dissolution, separation or pressed pelletization was developed. The developed methodology will be useful for sulphur determination in not only uranium ores, but also in other similar matrices requiring sulphur determinations in fast and simple manner e.g. coal, soil, etc. The sample remains in same form as taken because the collodion evaporates after drying.

Conclusion:

A simple non-destructive direct EDXRF method for sulphur determination in solid ore samples was developed without addition of any internal standard. The method utilizes the calibration plot made by plotting intensity ratio of S Kα and Rayleigh scattered peak of the exciting radiation (Ge Kα) against the sulphur percentage present in the standards. The EDXRF specimens were presented in form of thin film made by mixing the ore powders in collodion solution. Use of thin film reduced the background considerably and took care of matrix effect whereas, use of secondary target as excitation source made the excitation efficient along with further decrease in the background. The developed method gave satisfactory results for the analysis of sulphur in ore standards containing sulphur within 2%. The precision obtained was within 5% (RSD, ±1σ) and the deviation of the analytical results from the expected values was within 7%. The developed method was successfully applied for the determination of sulphur in the different stages of the uranium ore processing using alkaline based leaching method.
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Fig.1. The EDXRF sample cup with thin mylar film streched by the PVC rings
Fig. 2. EDXRF spectrum of an ore CRM containing 2% Sulphur excited using Ge secondary target operated at 2000 μA and 20 kV
Fig. 3. Calibration plot for EDXRF determination of sulphur in ores samples.

|              | Value  | Standard Err |
|--------------|--------|--------------|
| Adj. R-Squa  | 0.99583|              |
| Intercept    | 0.03398| 0.04176      |
| Slope        | 136.260| 6.06076      |

Equation: $y = a + bx$
Table 1. The details of the ore standards used for calibration

| S.No | Standard   | Certified values of $S \pm 1\sigma\%$ |
|------|------------|--------------------------------------|
| 1.   | GS305-10   | 0.51 ± 0.04                          |
| 2.   | GS307-3    | 1.03 ± 0.09                          |
| 3.   | GS302-5    | 1.98 ± 0.10                          |

The values in ± are standard deviation values ($1\sigma$)
Table 2. Comparison of the analytical results obtained using EDXRF determined and certified values

| S.No | Certified values of S ± 1σ (in %) | EDXRF determined S ± 1σ (in %) | EDXRF (B) / Certified (A) |
|------|----------------------------------|--------------------------------|---------------------------|
| 1.   | 1.03 ± 0.09                      | 1.10 ± 0.05                    | 1.07                      |
| 2.   | 1.98 ± 0.10                      | 1.90 ± 0.1                     | 0.96                      |

The values in ± are standard deviation values (1 σ)
Table 3. EDXRF determined concentration of sulphur in some residues of uranium ore obtained at different processing stages

| Sample* | Leaching stage and sample description | EDXRF determined Sulphur % | Standard Deviation (1σ) | Relative Standard Deviation (%) |
|---------|----------------------------------------|-----------------------------|-------------------------|---------------------------------|
| Feed    | Ground ore                             | 0.64                        | 0.05                    | 7.8                             |
| 1T1     | Residue samples before reaching the required temperature and pressure | 0.70                        | 0.10                    | 14.3                            |
| 2T1     | Residue samples before reaching the required temperature and pressure | 0.70                        | 0.10                    | 14.3                            |
| 1T9     | After 6hrs of leaching, 4kg/cm² O₂ pressure, 130°C | 0.72                        | 0.05                    | 6.9                             |
| 2T9     | After 6hrs of leaching, 6kg/cm² O₂ pressure, 130°C | 0.47                        | 0.07                    | 14.9                            |
| 3T9     | After 6hrs of leaching, 10kg/cm² O₂ pressure, 130°C | 0.50                        | 0.10                    | 20                              |

*: Residue obtained after leaching of uranium from uranium ore samples at different stages of leaching
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