Analysis of the Effect of Loading on the Transformers Usage Time

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Abstract
The reliability and stability of the system in the operation of the electric power system is very important, in order to provide comfort in service to consumers. The transformer is a very important component in the electric power system, because it is used as a voltage adjuster for the load being served. This study discusses the effect of loading and temperature on the life shrinkage of 36/60 MVA power transformers in block 3 and block 4 carried out at PT. PJB UBJ O&M PLTMG Arun Lhokseumawe, Aceh. From the calculation results after 4 years the transformer operates, if the transformer is given a 100% load, the transformer will experience an age difference of 2.52 p.u./day so that it has a remaining life of 10 years. As for the transformer that is given a load of 90%, the transformer will experience an age difference of 1.44 p.u./day so that it has a remaining life to perform operations for another 18 years. Then for a transformer that is given a load of 80%, the transformer will experience an age difference of 0.67 p.u./day so that it will have a remaining life to carry out the operation again for another 38 years. From the above calculation, the origin of the temperature obtained for the ONAN type of cooler in block 3 is 0.71 p.u./day and in block 4 it is 0.70 p.u./day. While the ONAF type of cooler in block 3 is 0.004 p.u./day and in block 4 it is 0.005 p.u./day. This is in accordance with the regulation SPLN50/1982 regarding transformer life shrinkage.

Keywords: electric power system; transformer; loading effect;

Introduction
The rapid development of electricity demand at this time must be followed by optimization of electrical power system equipment so that electrical energy can continue to be distributed continuously and uninterruptedly to electricity consumers(Pandapotan & Warman, 2016).One of the most important pieces of equipment in the distribution of electric power is the power transformer. The function of this power transformer is to transform the voltage according to the needs of the load (Sulasno, 2001).

The transformer is a very important component in the electric power system, because it is used as a voltage adjuster for the load being served. Therefore, the quality of the transformer must be maintained so that it can last a long time (Solikhuddin, 2010). Many things affect the decline in age, such as the temperature of the transformer and the temperature around the transformer, the worst loading occurs at the peak of 100% with a relatively low average life expectancy. With the increase in the load factor and ambient temperature, the aging rate of the transformer increases and the life of the transformer decreases with the operation of the transformer(Andika et al., 2018).

PT. PJB UBJ O&M PLTMG Arun is a power plant with a capacity of 184 MW and supplies electrical power in the city of Lhokseumawe and its surroundings. Meanwhile, the increasing use of electrical power is increasing so that the effect of loading the power transformer is also a problem during the period of using the transformer (Sigit et al., 2011).

Literature Review
Transformer is an electrical equipment that is included in the classification of electric machines and serves to distribute electrical power from high voltage to low voltage or vice versa, with the same frequency(Petra, 2017). In operation, power transformers are generally grounded at the neutral point, according to the need for a safety or protection system(Situmorang, 2011). For example, a 150/70 kV transformer is earthed directly on the neutral side of 150 kV, and a 70/20 kV transformer is earthed with a resistance on the neutral side of 20 kV. The basic theory of the transformer is "If there is alternating electric current flowing through the iron core, the iron core will turn large and if the
magnet is surrounded by windings then at both ends of the winding there will be voltage around the magnet, so that an electromotive force (EMF) will arise (Bambang N & others, 2020).

Transformer oil is one of the liquid insulating materials used as insulation and coolant in transformers. As part of the insulating material, oil must have the ability to withstand breakdown voltages, while as a coolant, transformer oil must be considered capable of handling the heat generated, so with these two capabilities, the oil is expected to be able to protect the transformer from interference (Putra & Murdiya, 2017).

### Table 1. Transformer cooling type (Efendi, 2018)

| No | Cooling System Type | Media |
|----|----------------------|-------|
| 1  | AN                   | Natural Circulation |
| 2  | AF                   | Forced Circulation |
| 3  | ONAN                 | Natural Circulation |
| 4  | ONAF                 | Forced Circulation |
| 5  | OFAN                 | Natural Circulation |
| 6  | OAF                  | Forced Circulation |
| 7  | OFWF                 | Natural Circulation |
| 8  | ONAN/ ONAF           | Combination 3 and 4 |
| 9  | ONAN/ OFAN           | Combination 3 and 5 |
| 10 | ONAN/ OFAF           | Combination 3 and 6 |
| 11 | ONAN/ OFWF           | Combination 3 and 7 |

The IEC specifies a transformer life of 20 years or 7300 days, so the normal life loss is 0.0137% per day. Shrinkage due to hot temperatures can be seen in table 2.

### Table 2. Transformer cooling type (Sulasno, 2001)

| Media | 0°C | 80 | 86 | 92 | 98 | 104 | 110 | 116 | 122 | 128 | 134 | 140 |
|-------|-----|----|----|----|----|-----|-----|-----|-----|-----|-----|-----|
| Δ1 day| 0.125 | 0.25 | 0.5 | 1 | 2 | 4 | 8 | 16 | 32 | 64 | 128 |

### Materials & Methods

This study discusses the effect of loading and environmental temperature on shrinkage of 36/60 MVA power transformers block 3 and block 4 conducted at PT. PJB UB O&M PLTMG ArunLhokseumawe, Nangroe Aceh Darussalam. This research was conducted by direct observation to the field and the data obtained were in the form of observational data on transformers which became the object of research as well as observations of the temperature around the observation location. This study also uses quantitative data, namely data in the form of numbers such as transformer loading data for 24 hours.

For certain rated power conditions: Natural oil circulation increase in average coil temperature (measured by resistance) = 60°C. Top oil temperature rise (Δθwo) = 55°C. The increase in the average temperature of the oil (Δθo) = 40°C. The difference between the average temperature rises of the coil and the average temperature rise of the oil (Δθwo) = 21°C. (Source: PT PJB UB O&M PLTMG Arun, 2019).

Hot spot temperature rise ((Δθcw)) is arranged as follows (Syahputri Marantika, 2016)(Siahaan, 2018)(Perera et al., 2001):

\[
\Delta \theta_{cw} = \Delta \theta_b + 1.1 \Delta \theta_{wo} \quad (1)
\]

a. Top oil temperature rise

\[
\Delta \theta_b = \Delta \theta_{br} \left[ \frac{1+dK^2}{1+d} \right]^x \quad (2)
\]

Information:
- \( d \) = high ratio
- \( x \) = constant
- \( x = 0.9 \) (ONAN and ONAF)*
- \( x = 1.0 \) (OAF and OFWF)*
- \( \Delta \theta_{br} \) = suhu
- \( K \) = load factor (load supply/load rating)

b. Hot spot temperature rise

\[
\theta_c = \theta_a + \Delta \theta_{on} + \Delta \theta_{td} \quad (3)
\]

Information:
- \( \theta_a \) = ambient temperature
- \( \Delta \theta_{on} \) = increase in top oil temperature
- \( \Delta \theta_{td} \) = temperature difference between hot spots and top oil

\[
\Delta \theta_c = \Delta \theta_{br} \left[ \frac{1+dK^2}{1+d} \right] + (\Delta \theta_{cr} - \Delta \theta_{br}) K^2 y \quad (4)
\]
Information: \( \Delta \theta_{cr} \) = hot spot temperature rise  
\( y \) = constant  
\( y = 0,8 \) (ONAN and ONAF)  
\( y = 0,9 \) (OFAF and OFWF)  
\( \Delta \theta_{br} \) = increase in top oil temperature

c. Counting aging

\[
\int_{t_1}^{t_2} V \, dt = \frac{h}{3} (V_0 + V_n + 4(V_{odd}) + 2(V_{even})) = \frac{h}{3} (2V_n + 4(V_{odd}) + 2(V_{even})) \tag{5}
\]

Characteristic curve \( V, V_0 = V_n \)

Information :  
\( h \) =constant (1)  
\( T \) = time  
\( V_{odd}, V_{even} \) = relative thermal aging rate

Results and Discussion

Calculations For Constant Load

Calculations are carried out to obtain the effect of various kinds of loading on the power transformer. Then the magnitude of the load is made constant which can be seen in the following table.

| No | Transformer Load |
|----|------------------|
| 1  | 100              |
| 2  | 90               |
| 3  | 80               |

After calculating using the existing equations, it can be seen the value of the life loss on the power transformer and the remaining operating life based on each loading percentage can be seen in Table 4 below:

| No | Load | Loss of Age (p.u/day) | Age (Years) |
|----|------|-----------------------|-------------|
| 1  | 100  | 2.52                  | 10          |
| 2  | 90   | 1.44                  | 18          |
| 3  | 80   | 0.67                  | 38          |

Effect of Ambient Temperature

Table 5. Effect of Ambient Temperature on Constant Load

| No | Suhu (°C) | Life Loss (p.u/day) at Stable Load |
|----|-----------|-----------------------------------|
|    |           | 80% | 90% | 100% |
| 1  | 20        | 0.26 | 0.57 | 1.00 |
| 2  | 21        | 0.30 | 0.64 | 1.12 |
| 3  | 22        | 0.33 | 0.72 | 1.26 |
| 4  | 23        | 0.37 | 0.81 | 1.41 |
| 5  | 24        | 0.42 | 0.91 | 1.59 |
| 6  | 25        | 0.47 | 1.02 | 1.78 |
| 7  | 26        | 0.53 | 1.15 | 2.00 |
| 8  | 27        | 0.59 | 1.29 | 2.25 |
| 9  | 28        | 0.66 | 1.45 | 2.52 |
| 10 | 29        | 0.74 | 1.62 | 2.83 |
| 11 | 30        | 0.84 | 1.82 | 3.18 |
| 12 | 31        | 0.94 | 2.04 | 3.56 |
| 13 | 32        | 1.05 | 2.29 | 4.00 |

The calculation results can be seen in table 5 above, the temperature change from the lowest to the highest is namely 20°C to 32°C makes the age loss at each load change. For loading of 80% the life shrinkage on the transformer is at 0.26 p.u/day to 1.05 p.u/day. And for loading of 90% the life shrinkage on the transformer is at 0.57 p.u/day to 2.29 p.u/day. While for loading of 100% the life shrinkage on the transformer is at 1.00 p.u/day to 4.00 p.u/day. From the results of the analysis, it can be explained that the difference in age loss for each load is the same because the transformer has a constant load. So based on the SPLN 50/1982 regulation regarding the life loss of the transformer in accordance with the calculation results obtained.
Based on Figure 1 above, it is explained that the effect of ambient temperature greatly affects a constant load. It can be seen in Figure 4.1 that the greater the temperature given to the power transformer, the life loss obtained will be even greater by being given a high load, this can be proven at a high load, namely 100% of the resulting life loss is very large, which is 4 pu/days given the high temperature of the transformer, which is 32°C.

Calculations for Power Transformer Loading
The magnitude of the rated power of the power transformer at PT. PJB UBJ O&M PLTMG ArunLhokseumawe, Nangroe Aceh Darussalam used is 32/60 MVA (ONAN/ONAF). The power transformer load for block 3 on 20 November 2019 at 19:00 is 34.88 MW, 5.76 MVAR, while the power transformer load for block 4 on 20 November 2019 at 19:00 is 34.30 MV, 7.78 MVARs.

Figure 2 above is the calculation of thermal aging in block 3 every hour on the ONAN cooling system. From the picture it can be explained that at 19:00 hours has the highest life loss in every analysis and calculation carried out this is because the value of MW and MVAR in the power transformer in the ONAN cooling system is higher at 19.00 so that the resulting life loss is greater at 19:00 is 13.97 years.
Figure 3 above is the calculation of thermal aging in block 4 each hour in the ONAN cooling system. From the picture above, it can be explained that at 19:00 hours it has the highest life loss, because the MW and MVAR values in the power transformer in the ONAN cooling system are higher at 19:00 so the resulting life loss is greater at 19 hours 00 of 13.05 years.

![Figure 3](image1.png)

**Figure 3.** Calculation of thermal aging in block 4 each hour in the ONAN cooling system.

Figure 4 above is the calculation of thermal aging in block 3 at each hour in the ONAF cooling system. From the picture above, it can be explained that at 19:00, the age loss is the highest in every analysis and calculation carried out. This is because the value of MW and MVAR in the power transformer in the ONAF cooling system is higher at 19:00 so that the resulting life loss is greater at 19:00 by 0.033 years.

![Figure 4](image2.png)

**Figure 4.** Calculation of thermal aging block 3 at each hour (ONAF).

Figure 5 above is the calculation of thermal aging in block 3 at each hour in the ONAF cooling system. From the figure, it can be explained that at 19:00, the age loss is the highest in every analysis and calculation carried out. This is because the value of MW and MVAR in the power transformer in the ONAF cooling system is higher at 19:00 so that the resulting life loss is greater at 19:00 by 0.032 years.

![Figure 5](image3.png)

**Figure 5.** Calculation of thermal aging block 4 at each hour (ONAF).

From the analysis, the age loss caused by ambient temperature was obtained for the ONAN type of cooler in block 3 of 0.71 p.u/day and in block 4 of 0.70 p.u/day. While the ONAF type of cooler in block 3 is 0.004 p.u/day and in block 4 it is 0.005 p.u/day.

**Conclusions**

The conclusions that the author can draw from the research that has been done based on the results of calculations and analyzes carried out are as follows:

1. The effect of temperature on the calculation of the age loss is every increase in temperature starting from the lowest temperature of 20°C to the highest temperature of 32°C in Indonesia, at each load of 80%, 90% and 100%, a very rapid increase in age loss is obtained, namely for a load of 80% from the lowest 0.26 to the highest 1.05 pu/day and for the load 90% from the lowest 0.57 to the highest 2.29 pu/day and for the load 100% from the lowest 1.00 to the highest 4.00 pu/day.

2. From the calculation results at 80%, 90% and 100% constant loading, the age loss value is obtained, respectively, namely 0.67 p.u/day; 1.44 p.u/day and 2.52 p.u/day and for the remaining life of the power transformer, respectively, namely 38 years, 18 years and 10 years.

3. The transformer life loss value is based on loading data on November 20, 2019, namely the ONAN type cooling network in block 3 of 0.71 pu/day and in block 4 of 0.70 pu/day while on the ONAF type cooling network in block 3 of 0.004 pu/day and in block 4 of 0.005 pu/day. This is in accordance with the regulation SPLN50/1982 regarding transformer life shrinkage.
References
Andika, D. A. Y., Agus Supardi, S. T., & others. (2018). Effect of Loading on the Life of the Power Transformer at the 150 kV Palur Substation. Muhammadiyah University of Surakarta.
Bambang N. A., & others. (2020). Analysis of Transformer Costs Due to Total Power Loss Using the Annual Worth Method at the Wonogiri Hydroelectric Power Plant. Muhammadiyah University of Surakarta.
Efendi, S. R. I. M. (2018). Transformer Cooling System At PLTMG ARUN 184 MW. ETD Unsyiah.
Pandapotan, J., & Warman, E. (2016). Study of the Effect of Loading on Power Transformer Life Loss. Jurnal Singuda Ensikom, 3(1).
Perera, K., Lucas, J. R., Kumarasinghe, K., Dias, R., Athukorala, U., & Gunawardana, P. G. A. (2001). Estimation of optimum transformer capacity based on load curve. Trans. Inst. Elect. Eng. Sri Lanka, 3(1).
Petra, F. (2017). Overcurrent protection for 2000 KVA transformer, 3.3 KV/380-220 Volt voltage at PT Century Textile Indonesia.
Putra, R. K., & Murdiya, F. (2017). Characteristics of Alternating Current Translucent Voltage in Castor Oil (Jatropha curcas) as an Alternative to Liquid Insulation. Riau University.
Siahaan, C. (2018). Power Transformer Aging Model Assessment According to IEC/IEEE Standards and Economic Value Determination by Annual Rate Method.
Sigit, P., Sukamdi, T., & Karnoto, K. (2011). Analysis of the Effect of Loading on Power Transformer Life Loss. Department of Electrical Engineering, Faculty of Engineering Undip.
Situmorang, B. M. (2011). Analysis of Transformer Costs Due to Total Power Loss with the Annual Worth Method. University of Indonesia.
Solikhudin, M. (2010). Study of Interbus Interbus Transformer (IBT-1) 500/150 kV at GITET 500 kV Kembangan-West Jakarta. Faculty of Engineering, Postgraduate Program in Engineering, University of Indonesia. Jakarta.
Sulasno, I. (2001). TEngineering and Electric Power Distribution System. Volume I, Diponegoro University Publishing Agency, Semarang.
Syahputri Marantika, N. (2016). Calculation of Life Loss of 30 MVA Power Transformer Due to Loading on PT. Padang Cement. Padang State Polytechnic.