Orbital angular momentum comb generation from azimuthal binary phases

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Abstract. Since Allen et al. demonstrated 30 years ago that beams with helical wavefronts carry orbital angular momentum (OAM), the OAM of beams has attracted extensive attention and stimulated lots of applications in both classical and quantum physics. Akin to an optical frequency comb, a beam can carry multiple various OAM components simultaneously. A series of discrete, equally spaced, and equally weighted OAM modes comprise an OAM comb. Inspired by the spatially extended laser lattice, we demonstrate both theoretically and experimentally an approach to producing OAM combs through azimuthal binary phases. Our study shows that transition points in the azimuth determine the OAM distributions of diffracted beams. Multiple azimuthal transition points lead to a wide OAM spectrum. Moreover, an OAM comb with any mode spacing is achievable through reasonably setting the position and number of azimuthal transition points. The experimental results fit well with theory. This work presents a simple approach that opens new prospects for OAM spectrum manipulation and paves the way for many applications including OAM-based high-security encryption and optical data transmission, and other advanced applications.

Keywords: orbital angular momentum; orbital angular momentum comb; azimuthal binary phase.

Received Apr. 9, 2022; revised manuscript received May 7, 2022; accepted for publication May 27, 2022; published online Jun. 29, 2022.

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[DOI: 10.1117/1.APN.1.1.016003]

1 Introduction

Similar to macroscopic objects, particles such as photons,1 electrons,2 and neutrons3 can also carry angular momentum. The angular momentum of a photon is of two types, with the spin angular momentum (SAM) corresponding to circular polarization4 and the orbital angular momentum (OAM) determining the helical wavefronts of a beam.5 Actually, OAM is an inherent feature of a beam whose complex amplitude comprises a helical term \( \exp(il\phi) \), where \( l \) is the OAM eigenvalue and known as the topological charge associated with an OAM value \( lh \) (\( h \) is the reduced Planck’s constant) per photon, and \( \phi \) denotes the azimuthal angle.6,7 One or more phase singularities determined by multiple OAM components are present for an OAM beam, thus leading to a doughnut-shaped transverse intensity.6,8,9 OAM offers an additional degree of freedom and leads to new possibilities for photonics research. Over the past 30 years, beams carrying OAM have found a wide variety of applications, including large-capacity communications9–13 rotation detection,14–16 optical tweezers and manipulation,17,18 imaging,19 gravitational wave detection,20,21 and quantum information processing.22,23

Previous research has provided a variety of schemes to generate OAM beams, such as direct output from a laser24–28 or endowing a Gaussian beam with spiral phases outside the laser resonator.29–35 Nevertheless, most of the aforementioned methods concentrate only on the generation of single or simple multiplexed OAM modes. Beams carrying a wide series of discrete, equally spaced, and manipulated OAM components with identical intensities, namely the OAM comb, are conducive to current OAM-based scenarios. For instance, multiplexed OAM multicasting enables one-to-multichannel data transmission, further enlarging the dimensions of OAM-based optical communications.35,36 The OAM comb can also act as a flexible key for holographic encryption and decryption.36,37 Currently,
schemes such as mode iteration, pattern-search algorithm, adaptive modification, and pinhole plates have been reported to tailor the OAM spectrum or produce an OAM comb. However, these schemes may face problems such as long response or calculation time, complex systems, and lower diffraction efficiency, which motivated us to develop a simple, flexible, and functional approach to selectively manipulate OAM combs.

In this study, we overcome the aforementioned limitations by demonstrating a specially designed azimuthal 0-π binary phase-only grating for the selective manipulation of OAM combs. Several transition points were embedded in a spiral phase along the azimuth to tailor the OAM spectrum of the diffractive beams. The number and position of the azimuthal transition points were optimized to produce arbitrary OAM combs, where the optimized results were fixed and could be employed for various scenarios at any time. A proof-of-principle experiment was performed to demonstrate the performance of the proposed azimuthal binary-phase gratings. These favorable results were in good agreement with our simulations. This study offers a real-time, flexible, simple, and accurate method for generating beams with complicated OAM spectra, which paves the way for classical/quantum optical communications, holographic encryption and decryption, and other advanced applications in the future.

2 Results and Discussion

2.1 Azimuthal Phase Modulation: From Continuation to Binarization

Previous studies have illustrated that a continuous azimuthal phase, namely a spiral phase plate (SPP), can bring a pure single OAM mode for the incident beams. In other words, such spiral phase, namely a spiral phase plate (SPP), can bring a pure single OAM component with respect to the fundamental mode \( l = 0 \). In other words, such spiral phase, namely a spiral phase plate (SPP), can bring a pure single OAM component with respect to the fundamental mode \( l = 0 \).

In this case, we overcome the aforementioned limitations by demonstrating a specially designed azimuthal 0-π binary phase-only grating for the selective manipulation of OAM combs. Several transition points were embedded in a spiral phase along the azimuth to tailor the OAM spectrum of the diffractive beams. The number and position of the azimuthal transition points were optimized to produce arbitrary OAM combs, where the optimized results were fixed and could be employed for various scenarios at any time. A proof-of-principle experiment was performed to demonstrate the performance of the proposed azimuthal binary-phase gratings. These favorable results were in good agreement with our simulations. This study offers a real-time, flexible, simple, and accurate method for generating beams with complicated OAM spectra, which paves the way for classical/quantum optical communications, holographic encryption and decryption, and other advanced applications in the future.

2.2 Azimuthal Binary Phase with Multiple Transition Points

In this case, we overcome the aforementioned limitations by demonstrating a specially designed azimuthal 0-π binary phase-only grating for the selective manipulation of OAM combs. Several transition points were embedded in a spiral phase along the azimuth to tailor the OAM spectrum of the diffractive beams. The number and position of the azimuthal transition points were optimized to produce arbitrary OAM combs, where the optimized results were fixed and could be employed for various scenarios at any time. A proof-of-principle experiment was performed to demonstrate the performance of the proposed azimuthal binary-phase gratings. These favorable results were in good agreement with our simulations. This study offers a real-time, flexible, simple, and accurate method for generating beams with complicated OAM spectra, which paves the way for classical/quantum optical communications, holographic encryption and decryption, and other advanced applications in the future.

2.3 OAM Comb Manipulation

To produce the desired OAM combs, a feasible way is to find a proper set of transition points. From the scalar diffraction theory, the far-field diffraction field \( E \) of an incident plane wave can be calculated approximatively through Fourier transform of the transmittance function of azimuthal binary phases. Thus, \( E \) from Eq. (2) reads \( E = F[\exp(iP_B)] \), where \( F \) denotes Fourier transformation. On the basis of the helical harmonic \( \exp(il\phi) \), the diffraction field \( E \) can be decomposed into the summation of infinite helical term with various complex weights \( a_i \) :

\[
E(r, \phi) = \frac{1}{\sqrt{2\pi}} \sum_{i=-\infty}^{\infty} a_i \exp(il\phi).
\]

The complex weights in Eq. (3) read

\[
a_i = \frac{1}{\sqrt{2\pi}} \int_{0}^{2\pi} E(r, \phi) \exp(-i\phi) d\phi.
\]

Actually, \( |a_i|^2 \) corresponds to the intensity of OAM channel \( i \). By now, a mind map of OAM comb manipulation emerges...
clearly, as the azimuthal transition points lead to azimuthal nodal lines determine the diffraction fields, and such fields further determine the intensity of each OAM channel $|a_l|^2$. In other words, the final OAM spectrum is a function of azimuthal transition points $\phi_\kappa$ as $|a_l|^2 = f(\phi_\kappa)$ indeed (Supplementary Note 2). To find a proper set $\{\phi_\kappa\}$ for the desired OAM comb, several evaluation parameters are necessary. Here two parameters are introduced, one of which is the efficiency defined as $\eta = (\Sigma_{l \in L}|a_l|^2)/\Sigma_{l \in Z}|a_l|^2$, where $L$ and $Z$ denote the set of topological charges of desired OAM comb and the integer set separately. The other is the uniformity as $U = 2 \min|a_l|^2/(\max|a_l|^2 + \min|a_l|^2)$, where $l \in L$, $\min\{}$ and $\max\{}$ denote taking the minimum and maximum, respectively. Note that $\eta$ must be $< 1$ because a single phase-only grating cannot produce coaxial multiplexed OAM modes with desired OAM distributions, and there must be irrelevant and undesired OAM modes.\(^{38}\) $\{\phi_\kappa\}$ calculation is available through iteration embedded numerical simulation. In each iteration, one must evaluate the value of $\eta$ and $U$ to decide how to adjust the transition points set $\{\phi_\kappa\}$ until an ideal scenario where the finally calculated transition points contribute to highest efficiency $\eta$ and uniformity $U$. Usually such process is complex and time-consuming, which incommodes the practical application of OAM comb. Zhou and Liu\(^ {43}\) have already demonstrated numerical

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Fig. 1  Binarizing continuous azimuthal phases into $0-\pi$ azimuthal binary phases. (a) The binarization of continuous azimuthal phases with one and two nodal lines (the first- and second-order SPPs) under the threshold $P_{th} = \pi$. The binarized phase can produce symmetric OAM components with respect to $l = 0$ mode, compared with the corresponding continuous azimuthal phases. (b) The $0-\pi$ phase binarized under various binarization threshold $P_{th}$ as $\pi/4$, $\pi/2$, $3\pi/4$, $\pi$, $5\pi/4$, $3\pi/2$, and $7\pi/4$, respectively. First to fourth lines in panel (b): the phase distribution, the phase versus the azimuthal angle $\phi$, the simulated far-field diffraction pattern, and the corresponding calculated OAM spectrum.
solutions for $0-\pi$ binary Dammann gratings, which can expand the incident beam along the $x$ direction to achieve a one-dimensional (1D) equal-intensity laser array with both high efficiency and high uniformity. In Ref. 43, multiple lateral ($x$) transition points are introduced within one grating period $T$, resulting in multiple presented diffraction orders ($x$-expanded modes) featured as $\Sigma \exp \left(i 2\pi mx/T \right)$, where $m$ corresponds to the $m$th diffraction order. Here, we move from “$x$-space” to “$\phi$-space,” where the azimuthal ($\phi$) transition points in one azimuthal period ($\Pi = 2\pi$) lead to OAM superposed modes ($\phi$-expanded modes) featured as $\Sigma \exp \left(i \phi p / \Pi \right)$. The resulting fields in the above two “spaces” have identical forms. Their only difference is that one expands the incident beam along the $x$ coordinate while the other along the $\phi$ coordinate. Such phenomena imply that the numerical solutions given in Ref. 43 are also effective to be employed in the azimuth to produce various OAM superposed modes with equal intensities.

We map the numerical solutions presented in Ref. 43 from “$x$-space” to “$\phi$-space” (Supplementary Note 3) to generate azimuthal $0-\pi$ binary phases, calculate the far-field diffractions through the scalar diffraction theory for incident Gaussian beams, and then analyze the OAM spectra (Supplementary Note 4). As displayed in Fig. 3(a), an azimuthal binary phase can produce nine equal-intensity OAM modes with topological charges ranging from $-4$ to $+4$. It has six azimuthal transition points as $0$, $0.4190$, $0.8087$, $1.7963$, $2.8693$, and $3.7127$. The efficiency and the uniformity of the obtained OAM comb are calculated as 78.32% and 99.61%, which are high enough for OAM comb manipulation. In addition, we also attempt to generate OAM combs with other OAM mode intervals $\Delta l$. Such manipulation is based on the scaling property of the Fourier transform, where if $F \{f(x)\} = F(u)$, then $F \{f(x/a)\} = |a| F(au)$ with $a$ the scale factor. So, here scaling the azimuthal phase $\phi$ contributes to $F \{T \phi / \Delta l \phi' \} \propto \Sigma \exp(i \Delta l \phi')$, where $\phi'$ is the azimuthal angle in the far field. As an example, we scale the azimuthal angle in Fig. 3(a) with scale factors $\Delta l = 2$ and $\Delta l = 3$, and the final obtained OAM combs are given in Figs. 3(b) and 3(c). Note that the OAM comb is present through normalized intensity, where the calculated or experimentally measured intensity of each OAM channel is normalized with respect to the maximum intensity among all the present OAM channels. In both of the two scenarios, there are also nine OAM
modes with equal intensities. However, their topological charge distributions are totally different; one is $-8$ to $+8$ with $\Delta l = 2$, the other is $-12$ to $+12$ with $\Delta l = 3$. Such phenomena illustrate that it is practicable to produce OAM combs with various OAM mode intervals through azimuthal scaling and provide a more flexible scheme of OAM comb manipulation. Additionally, OAM range is limited to $-15$ to $+15$ here. When extending such a present range, in Figs. 3(b) and 3(c) one can see undesired side OAM modes distributions similar to Fig. 3(a), but the only difference is the space between adjacent OAM channels.

Proof-of-principle experiments are also carried out to show the practical operability (Supplementary Notes 5–7). In the experiment, we encode the azimuthal $0-\pi$ binary phase onto a liquid-crystal spatial light modulator (SLM) to accomplish the phase-only modulation. The OAM spectra are analyzed with the back-converted method as a series of spiral phases ($l_1$, $l_2$, $\ldots$, $l_N$), also known as anti-SPPs in some literature, are encoded simultaneously on the SLM and then the intensity of center bright spot is calculated to represent the relative intensity of the OAM channel $-l$ to $l$. We first generate an OAM comb consisting of 64 OAM states ranging from $-63$ to $+63$ with the OAM mode interval $\Delta l = 2$. The experimentally captured intensity patterns and OAM spectrum and its corresponding simulation results are given in Fig. 4(a). The uniformity of the experimental result is evaluated as 92.04%, which is lower than that of the simulation at 98.16%. In addition, the similarity, which implies the consistency between the experimental and theoretical results suggested by the work\(^{44,45}\) is evaluated as 96.49%. We also generate an OAM comb consisting of 32 OAM states ranging from $-62$ to $+62$ with the OAM mode interval $\Delta l = 4$, the results of which are shown in Fig. 4(b). In this case, the uniformities of the experimental and simulated results are 90.95% and 98.86%, respectively, and the similarity is analyzed as 93.36%. The numbers of azimuthal transition points $\{\varphi_k\}$ for the above two cases are 70 and 68 separately (Supplementary Note 6). The measured OAM spectra in the experiment show little difference compared with simulation, where the intensities emerge in some irrelevant OAM channels and some power is likely to leak from desired to undesired OAM components. In fact, such “leakage” is meaningless and makes no physical sense because inevitable inter-channel crosstalk is introduced during the data-processing of the back-conversion-based OAM spectrum measurement.

3 Conclusions

We showed that binarizing a spiral phase into $0-\pi$ binarization results in multiple OAM components that are symmetric with respect to the fundamental mode ($l = 0$) of equal intensity. In this case, there are two azimuthal transition points constituting the two nodal lines that divide phases 0 and $\pi$. When more transition points are introduced, the resulting OAM spectrum becomes more complex. Nevertheless, the OAM distribution can be tailored by adjusting the number and value of azimuthal transition points to accomplish arbitrary OAM comb manipulations. Finding a proper set of azimuthal transition points is crucial for OAM comb manipulation; however, it is complicated because of repetitive iterations. Therefore, based on previous reports on the numerical solutions of lateral transition points to construct a 1D beam lattice that expands the incident beam along the $x$ axis, we build a mapping between the $x$ axis in
Fig. 4 Experimentally generated OAM combs. (a) Experimental results of an OAM comb consisting of 64 OAM states ranging from −63 to +63 with the OAM mode interval Δl = 2. (b) Experimental results of an OAM comb consisting of 64 OAM states ranging from −62 to +62 with the OAM mode interval Δl = 4. In both of the cases the OAM spectra are measured through anti-SPP based OAM back-conversion.
Cartesian coordinates and the $\phi$ axis in polar coordinates, thus transforming the optimal solution of transition points along the $x$ axis into that of the azimuth along the $\phi$ axis to accomplish a fast binary phase calculation. In the simulation, we successfully produce various OAM combs following the above hypothesis. We also show how to adjust the mode interval between adjacent OAM modes inside the OAM comb by scaling the azimuthal coordinates. In the proof-of-principle experiment, OAM combs consisting of up to 64 OAM components with the largest absolute value of OAM state 63 are generated, whose uniformity reaches 92.04% and fits well with the theory. We also attempt to adjust the OAM mode interval in practice and produce an OAM comb comprising 32 OAM components whose OAM states range from $-62$ to $+62$ with a mode interval of 4. The uniformity is evaluated to be 90.95%. The favorable experimental results illustrate that our proposed method exhibits good performance for tailoring OAM combs in practice.

In addition, the OAM states can be shifted by illuminating the $0-\pi$ binary phase-only grating with a higher-order optical vortex. Alternatively, this may be done by integrating the OAM combs whose components are asymmetric with respect to the fundamental mode ($l=0$) can also be achieved. The ability to generate a beam with a specifically tailored OAM spectrum is crucial for OAM applications; e.g., the unique key of holographic encryption and decryption. In addition, the proposed approach provides a convenient method for the practical generation of high-dimensional OAM combs, namely, an available high-dimensional Hilbert space; thus, it can find potential in high-dimensional photon entanglement and will inspire applications in quantum key distribution and quantum teleportation. Iteration methods are typically employed to optimize phase-only gratings to produce a multiplexed OAM beam. However, these complicated processes are time-consuming and may be inconvenient for practical applications. Herein, we demonstrate a simple approach in which azimuthal binary phases are introduced to manipulate arbitrary OAM combs with equal mode intensities. Furthermore, the azimuthal transition points can be easily calculated by mapping the numerical solutions of the binary lateral phases. In summary, our proposal opens new avenues for OAM comb manipulation and lays the foundation for applications in many OAM-based systems.

Acknowledgments

This work is supported by National Natural Science Foundation of China (NSFC) (11834001, 61905012), National Defense Basic Scientific Research Program of China (JCKY2020602C007), and National Postdoctoral Program for Innovative Talents (BX20190036). The authors declare no competing financial interests.

Availability of Data and Materials

The simulated and experimental data that support the works of this study are available from the corresponding authors on request.

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