Supporting quantum technologies with an ultralow-loss silicon photonics platform

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Abstract. Photonic integrated circuits (PICs) are expected to play a significant role in the ongoing second quantum revolution, thanks to their stability and scalability. Still, major upgrades are needed for available PIC platforms to meet the demanding requirements of quantum devices. We present a review of our recent progress in upgrading an unconventional silicon photonics platform toward this goal, including ultralow propagation losses, low-fiber coupling losses, integration of superconducting elements, Faraday rotators, fast and efficient detectors, and phase modulators with low-loss and/or low-energy consumption. We show the relevance of our developments and our vision in the main applications of quantum key distribution, to achieve significantly higher key rates and large-scale deployment; and cryogenic quantum computers, to replace electrical connections to the cryostat with optical fibers.

Keywords: silicon photonics; quantum key distribution; quantum computers; cryogenic photonics; superconducting nanowire single-photon detectors; quantum technologies; superconducting qubits; silicon qubits.

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1 Introduction

We are presently living in the so-called second quantum revolution, where the focus has shifted from pure science to technologies and applications.1 Photonic technologies are expected to play a major role, not only in quantum applications but also in classical configurations to support solid-state quantum systems. In particular, photonic integrated circuits (PICs) offer unique opportunities for different quantum technologies to scale up system complexity and integration density while providing unmatched performance and stability.2–6 In this regard, the micron-scale silicon photonics platform7 brings with it a unique set of properties and building blocks. This includes low propagation losses (down to 3 dB/m demonstrated to date8,9), broadband and low-loss coupling to fibers (≈0.5 dB), fast (>40 GHz) and responsive (≈1 A/W) integrated germanium photodetectors,10 upreflecting mirrors (URM) for broadband and low-loss coupling to arrays of detectors, tight bends11 enabling high-integration density, efficient phase shifters, low-loss Mach–Zehnder interferometers, multimillion Q ring resonators,9,12 polarization insensitive operation, and polarization splitters13 and rotators, including all-silicon Faraday rotators (FRs).14

A relevant example application is large-scale deployment of quantum key distribution (QKD), for which we are developing efficient multiplexed receivers. A second interesting case is the use of our photonic integration technology to scale up superconducting quantum computers by controlling and reading out the qubits in the cryostat through classical optical links. In this case, the major challenge is the development of suitable electrical-to-optical and optical-to-electrical converters (OECs) operating at cryogenic temperatures.

We will cover these ongoing developments as follows, showing our recent results as well as our plans to further exploit the platform. In Sec. 2, we will first give an overview of the thick-silicon photonics platform, with a special focus on the most relevant features for quantum technologies. In Secs. 3 and 4, we will cover the ongoing developments for QKD and quantum computers and then conclude in Sec. 5 and briefly mention other promising future developments and applications.

2 Overview of VTT Thick Silicon-on-Insulator Platform

We can divide the building blocks of the platform into two main categories: passives and actives. In this context, “active” means
anything requiring an electrical control, such as thermo-optic phase shifters and electro-optic modulators, or electrical read-out, such as a photodiode. An overview of the main building blocks available on the platform is sketched in Fig. 1 with the notable exception of phase modulators based on PIN diodes, which are explained in detail in Sec. 2.2. We fabricate our PICs on 150-mm diameter silicon-on-insulator (SOI) wafers (to be upgraded soon to 200 mm) with 3-μm thick device layer (±100 nm uniformity) using a UV stepper (365 nm wavelength) and a modified Bosch process\textsuperscript{15,16} to etch the waveguides.

2.1 Passive Building Blocks

2.1.1 Types of waveguides

The five main waveguide types available on the platform are: rib waveguides, strip waveguides, down-tapered strip waveguides, strip waveguides with a thin pedestal, and down-tapered strip waveguides with a thin pedestal (the latter is the only type missing in Fig. 1). For rib waveguides, trenches are partially etched (typically 1.2-μm deep etch) on both sides of the waveguide. Single-mode operation can be achieved for both transverse-electric (TE) and transverse-magnetic (TM) polarization with a suitable choice of the rib width\textsuperscript{11} (typically \( \leq 3 \) μm). On the contrary, all four possible strip waveguide cross sections are inherently multimode. Nevertheless, we carefully design the optical circuits so that excitation of the higher-order modes (HOMs) is always negligible in the connecting waveguides, ensuring effective single-mode operation of the whole circuit.

2.1.2 I/O coupling

We fabricate the vertical waveguide facets of our PICs at wafer scale by first etching the silicon facet and then depositing a suitable antireflection coating, which can be made of either a single dielectric layer or multiple layers.

The coupling loss to optical fibers can be as low as 0.5 dB, provided that the mode field diameter is about 2.5 μm, which is achieved with lensed (or tapered) fibers or small core fibers with high numerical aperture. Fiber arrays must be used instead in configurations where the PIC has several inputs and outputs. Given the limited assembly precision of fiber arrays and considering that the tolerance to misalignments scales inversely with the mode size, low-loss coupling can be ensured only by arrays of standard single-mode fibers (SMFs) with mode diameter around 10 μm. This requires suitable mode size converters, like the one shown in Fig. 2, fabricated by etching arrays of 12-μm-wide rib and strip waveguides on an SOI wafer with a 12-μm-thick device layer, and then tapering the thickness of the output strip waveguides down to 3 μm by polishing each optical interposer chip. We are presently working toward further reduction of coupling losses below 0.5 dB by implementing 3D printed lenses,\textsuperscript{18} directly printed on the waveguide facets at wafer scale. This way, we aim to couple the PIC directly to SMFs and fiber arrays with ultralow-loss and relaxed alignment tolerance\textsuperscript{19} (Fig. 3).

Light can also be coupled to the PIC vertically from URMs (see Figs. 1 and 4), which are wet etched with a negative angle. Their working principle is total internal reflection, and coupling losses are practically the same as for the vertical facets. The antireflection coating for URMs is the same as for vertical facets. The wet etching process occurs along crystalline planes, meaning that the mirrors can be fabricated only along the four orthogonal crystal planes with Miller indices of 110, 110, 110, and 110. One of the advantages of URMs is the possibility of using them to test the fabricated PICs at wafer scale.

Compared to grating couplers typically used in submicron waveguides, URMs support both TE and TM polarizations with negligible polarization-dependent loss, and they operate over the whole transparency range of silicon, from 1.2 to 7 μm wavelength. We additionally stress here that thick-SOI PICs can operate over the whole transparency range of silicon. In particular, one can design a rib waveguide to be single mode at all the wavelengths in that broad spectral range, spanning several octaves.\textsuperscript{17} We must emphasize that, above 3 μm wavelength, absorption in the silica cladding [including the buried oxide (BOX) and the top cladding, see Fig. 1] contributes to propagation losses. However, due to the strong confinement in the

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**Fig. 1** Sketch of the main building blocks available on the thick-SOI platform. Typical thickness of the device layer is 3 μm, whereas the BOX thickness can vary from 400 nm to 3 μm. We define “active” building blocks as those requiring electrical pads for either control or readout.
thick silicon core, propagation losses remain below 1 dB/cm up to about 4 μm wavelength, and low propagation losses can be achieved up to 7 μm wavelength by selectively removing the silica cladding all around the waveguide. This is in strong contrast to thin SOI-based Si photonics platforms where propagation losses are typically above 1 dB/cm even at telecom wavelengths because of stronger interaction with the sidewall roughness. Furthermore, the power fraction in the cladding of submicron waveguide modes is orders of magnitude larger compared to thick-SOI waveguides, meaning that the absorption in the silica cladding already becomes unbearable beyond 2.5 μm wavelength. Operation in the mid-IR is critical for many gas sensing applications—including quantum sensing—and also to exploit the strong third-order nonlinearity of silicon; further, the larger optical mode size in thick SOI enables avoiding saturation caused by strong two-photon absorption (and associated free-carrier absorption) at wavelengths shorter than 2.2 μm. Although the large cross section of the waveguides is not ideal for efficient excitation of nonlinear effects including parasitic two-photon absorption, the unique combination with ultralow propagation losses is advantageous in many applications.

2.1.3 Tight bends enabling high-integration density

It is generally assumed that waveguides with micron-scale cross sections require bending radii on the order of several millimeters. This is because the index contrast ensuring single-mode operation in a micron-scale waveguide would inherently lead to

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Fig. 2 (a) Sketch of different mode size conversions starting from an SMF coupled to the 3-μm thick waveguides of a thick-SOI PIC using an optical interposer fabricated on 12-μm thick SOI. The sketch also shows how the mode size can be reduced further even to couple light to submicron waveguides on a flip-chip bonded PIC that can be evanescently coupled through suitable inverse tapers. (b) Micrograph of a 12-μm thick rib waveguide of a fabricated optical interposer; (c) micrograph of a strip waveguide polished down to about 3-μm thickness on the opposite facet; (d) near-field image (infrared camera) of the TE and TM modes at the output facet of the interposer [shown in (c)]; and (e) packaged 3-μm thick-SOI PIC coupled to a fiber array through an optical interposer.

Fig. 3 (a) SEM image of polymer lenses 3D printed in front of the end facets of four rib waveguides; (b) near-field picture of the output mode of a rib waveguide taken with an infrared camera; (c) near-field picture of the output of a lensed rib waveguide [same scale as (b)].
high radiation losses for tighter bends. In the platform, we have developed two solutions to this limitation: turning mirrors based on TIR [Figs. 5(a) and 5(b)] and tight adiabatic bends referred to as the Euler bends [Fig. 5(a)]. The first approach applies to both rib waveguides and strip waveguides, whereas the second requires high-index contrast strip waveguides.

TIR mirrors allow for compact layouts, such as the imbalanced Mach–Zehnder interferometer (MZI) shown in Fig. 5(b), which also shows the very low-loss (≈0.02 dB) waveguide crossings easily achievable on the platform. Turning mirrors can be designed with almost any turning angle, and their losses can be made as low as 0.1 dB per turn using parabolic shapes and/or making the waveguide sufficiently wide. In fact, the main loss mechanism is light diffraction due to the partial lack of lateral guidance in the mirror region. Remarkably, turning mirrors work over the entire (from 1.2 to 7 μm) wavelength transparency region of silicon and can be designed to simultaneously work equally well for both TE and TM polarizations, despite the polarization-dependent offset induced by the Goos–Hänchen shift. Nevertheless, the nonnegligible loss makes them unsuitable for circuits requiring a large number of bends, e.g., long spiral waveguides.

For this reason, we have also developed more conventional waveguide bends to achieve much lower losses. They are based on strip waveguides, ensuring negligible radiation loss due to strong light confinement. The only limitation is that they support several HOMs that get easily excited in a tight bend. We have, therefore, introduced and patented a geometry with gradual a change of curvature, using the Euler spiral geometry as shown in Figs. 5(c), 6(a), and 6(b). This way, tight bends with loss lower than 0.02 dB can be achieved with effective bending radii of a few tens of microns, enabling, e.g., compact race track resonators with quality factor Q of up to 14 million.

Even though, in general, the wavelength range of operation of the bends is not as wide as that of turning mirrors, bends can be designed to cover bandwidths of several hundreds of nanometers up to a few microns. An interesting property of Euler bends is that they very efficiently transmit most of supported HOMs (i.e., those with effective index sufficiently higher than the cladding refractive index), as highlighted in Fig. 6(c). In other words, the bends preserve the mode power distribution, which is useful when designing PICs for mode multiplexing and when using spatial modes as a quantum degree of freedom (see also Sec. 5). It is worth mentioning that turning mirrors also preserve the HOM power distribution under reflection.25

2.1.4 Polarization management
Micron-scale silicon waveguides support both TE and TM polarizations with very similar spatial mode distributions, the same propagation losses, and very similar effective indices. Indeed, strip waveguides with a square cross section can support TE and TM fundamental modes with identical propagation constants. Any possible residual birefringence induced by material
strain can be easily compensated by fine-tuning the waveguide width.

Most of the building blocks, including multimode interference (MMI) splitters, can be designed to support both polarizations at the same time. On the other hand, in many applications (including telecom and sensing), polarization can be used as a degree of freedom, in which case a polarization splitter/combiner is needed and preferably also different types of polarization rotators. We are presently developing a wide portfolio of building blocks for polarization management, including MZI polarization beam splitters (PBSs)\textsuperscript{13,38} [see Fig. 7(a)] and rotators.\textsuperscript{39} Remarkably, we have demonstrated the use of silicon itself as a magneto-optic material and achieved Faraday rotation in zero-birefringence waveguides.\textsuperscript{14} Our ultimate goal is to build a fully integrated all-silicon circulator based on splitters/combiners and reciprocal and nonreciprocal rotators [Fig. 7(b)].

We conclude this section by mentioning that Faraday mirrors are commonly used in quantum photonics, including QKD systems (see Sec. 3), to ensure stable operation,\textsuperscript{40,41} as the polarization of the reflected light is always orthogonal to the input polarization (i.e., antipodal on the Poincaré sphere).\textsuperscript{42} Faraday mirrors can be achieved in the platform by combining an FR with a back-reflector, such as an MMI reflector or a Sagnac loop.\textsuperscript{43}

**2.1.5 Low-loss wavelength filters**

We have demonstrated several different types of wavelength filters, including ring resonators with $Q$ up to 14 million,\textsuperscript{9,12} 

![Fig. 6](image1) (a) The linear change of the curvature $1/R$ as a function of the length $s$ in an Euler bend, starting from zero, reaching up to $1/R_{\text{min}}$, and then going back to zero symmetrically. (b) Example layout of a 90-deg Euler bend (or L-bend) with unity minimum bending radius, showing the resulting effective radius $R_{\text{eff}}$. (c) Simulation of the transmission of the TE\textsubscript{00} mode and of five horizontal higher-order TE modes of a 1.5-μm-wide strip waveguide at the output of a 90-deg Euler bend as a function of the minimum bending radius. The five HOM TE\textsubscript{n0} modes ($n = 1, \ldots, 5$) have $n$ nodes in the horizontal direction and zero nodes in the vertical direction. The wavelength is 1.55 μm.

![Fig. 7](image2) (a) Sketch of an MZI exploiting the form birefringence of waveguides of different widths to serve as a PBS. (b) Scheme of a possible implementation of an integrated light circulator by combining PBSs, FRs, and reciprocal polarization rotators on chip.
compact MMI resonators, flat-top lattice filters, and flat-top ring-loaded MZIs. Some of these filters can be designed to have <0.5 dB excess loss. We have also demonstrated low-loss echelle gratings and arrayed waveguide gratings (AWGs). In Fig. 8(a), we show the layout of an AWG with a small footprint due to the use of Euler bends. The device is polarization-independent because of the incorporation of strip waveguides with a square cross section. Excess loss is in the 2- to 3-dB range, and the extinction ratio (ER) is larger than 25 dB. We have also demonstrated AWGs with loss in the 1- to 2-dB range, and an ER exceeding 30 dB on all channels. We are presently working on further reduction of excess loss by improving design and fabrication of the star coupler. For echelle gratings like the one shown in Fig. 8(a), we have already demonstrated excess loss lower than 1 dB for both polarizations with an ER exceeding 20 dB for all channels.

2.1.6 Interfacing micro- and nanoscale devices

The low propagation loss of micron-scale waveguide technology comes with the price of weak interaction with any element integrated directly on top of the waveguides. This problem has been successfully addressed with different fabrication techniques that do not jeopardize the performance of the platform. For example, recently we have been developing a light escalator made of hydrogenated amorphous silicon (a-Si:H) to interface micron-scale waveguides with submicron waveguides, thin layers including 2D materials, and superconducting nanowires. We grow a submicron layer of a-Si:H (refractive index around 3.65) on top of the crystalline device layer (refractive index around 3.48 at a 1550 nm wavelength), and pattern it to achieve adiabatic light coupling. The simulation in Fig. 9(a) shows how the light propagates from the thick silicon waveguide to the thinner a-Si:H layer. The a-Si:H layer thickness can be optimized to maximize the overlap of the propagating light with, e.g., a graphene layer (for applications such as light detection or modulation) or a superconducting nanowire single-photon detector (SNSPD, also see Sec. 2.2) sandwiched between crystalline silicon (c-Si) and a-Si:H, similar to what is sketched in Fig. 9(b). Furthermore, crystalline silicon can also be selectively removed and replaced with a deposited silica layer before depositing the a-Si:H layer, as sketched in Fig. 9(c). The resulting high-index contrast a-Si:H waveguide allows us to interface the micron-scale waveguide with submicron waveguides including plasmonic slot waveguides or even just PICs based on submicron silicon waveguides that can be simply bonded on top of the a-Si:H waveguide and evanescently coupled via inverse tapers. Both types of escalators can be fabricated using the same fabrication process. Another unique opportunity to couple micron-scale waveguides to nanophotonic devices comes from the URM. In fact, there are cases requiring the light to propagate across a functional surface (unlike the escalator case, where it propagates along it). In these cases, functional surfaces can be fabricated or just transferred on top of the flat output surface of the mirror (which is made of crystalline smooth silicon, not etched). This is a straightforward way to integrate metasurfaces, including waveplates, metalenses, or electro-optic modulators. However, the limited size of the mirror (3 μm in the waveguide propagation direction, i.e., a few wavelengths) may present a challenge for the design of the metasurface.

2.2 Active Building Blocks

We can divide the active elements in two main categories: electrical-to-optical converters (EOCs), which, in the thick-SOI platform, are basically all phase shifters (either thermo-optic or electro-optic) and OECs, i.e., photodetectors.

2.2.1 Phase shifters

We implement thermo-optic phase shifters by implanting a thin silicon pedestal at the bottom of strip waveguides [Fig. 10(a)]. We usually cut away the remaining part of the pedestal to achieve lower power consumption, reaching about 25 mW per π-shift, with both rise time and decay time of about 15 μs (i.e., a speed of about 66 kHz). Very recently, we have also demonstrated ~2 mW per π-shift (not yet published) by fabricating the heaters on special cavity-SOI wafers, which limits the heat flow through the substrate.

Placing the heaters in direct contact with the silicon layer ensures a significant reduction of thermal cross talk compared to heaters based on metal wires placed on top of the waveguide upper cladding. This is a major advantage for complex circuits requiring several thermo-optic phase shifters. By design, thermo-optic phase shifters come with no excess loss.

When higher speed is needed, we can reach about 2–3 MHz using simple PIN junctions, with only one implantation level, as sketched in Fig. 10(b). In this case, the refractive index changes due to carrier injection inducing plasma dispersion. The power consumption for a π-shift is lower than 5 mW. Nevertheless, plasma dispersion inherently adds amplitude modulation on top of the phase modulation, due to the Kramers–Kronig relations. The loss associated with a π-shift is on the order from 1 to 2 dB.

Fig. 8 (a) Compact AWG with 100-GHz channel spacing and 5-nm free spectral range exploiting Euler bends and nearly zero birefringence waveguides, ensuring polarization-independent operation. (b) Cyclic echelle grating with 100-GHz channel spacing.
Indeed, when made sufficiently long, the same type of PIN junction is also used for variable optical attenuators.

To overcome these limitations, we are also developing phase modulators relying on the so-called electric-field-induced Pockels effect (EFIPE, see Fig. 10(c)), in close collaboration with the University of Tokyo. For these modulators, we expect significantly lower excess loss due to the high-reverse bias (electric field of about 40 V/μm, as close as possible to the breakdown). In particular, we do not expect any major amplitude modulation associated with phase modulation. Furthermore, we aim to reach modulation speeds exceeding 1 GHz and possibly approaching 10 GHz. We also expect the power consumption to be in the microwatt range per \(\pi\)-shift, which is important for cryogenic applications. In fact, EFIPE works well also at cryogenic temperatures because it is not affected by carrier freeze-out, unlike plasma dispersion.

With the goal of achieving extremely low-power consumption in combination with modulation speeds exceeding 100 GHz, we are also developing plasmonic modulators in collaboration with ETH Zürich and the company Polariton Technologies. In addition to the conventional approach based on nonlinear polymers, we are also exploring the possible use of a-Si:H as nonlinear material based on EFIPE. We point out that plasmonic modulators are also particularly suitable for cryogenic applications, since they do not rely on charge carriers and operate with ultralow power dissipation. The main limitation of plasmonic phase shifters is the high excess loss, typically exceeding 5 dB. However, as explained in Sec. 3, this can be acceptable in some applications.

To conclude this section, we point out that a key missing building block for quantum PICs (QPICs) in all platforms is a suitable phase shifter to simultaneously enable a small footprint, ultralow power consumption, high-speed, ultralow optical loss, and cryogenic operation, or at least a subset of these properties, depending on the application. Recent results demonstrate that using microelectromechanical systems is a promising path for both submicron silicon and silicon nitride platforms. This approach can result in losses below 0.5 dB, speeds from a few MHz to beyond 100 MHz, and footprints ranging from about 100 μm × 100 μm to 1 mm × 1 mm. One additional avenue, which we are presently exploring for faster and more compact phase shifters, is to place electro-optic metasurfaces on top of URM s. Here the goal is to access the full nonlinear coefficient of electro-optic polymers, which is typically reduced by one order of magnitude in plasmonic slot waveguides.

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**Fig. 9** (a) 3D simulation using the eigenmode expansion method of the adiabatic power transfer from a 3-μm thick c-Si waveguide to a 400-nm thick and 200-μm long a-Si:H tapered waveguide fabricated on top. (b) 3D sketch of two escalators to couple light to the a-Si:H waveguide and then back to the 3-μm thick waveguide, showing where a functional layer can be sandwiched between the two silicon types in the region where the light is guided in a-Si:H. (c) A different type of escalator to couple light to submicron waveguides.

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**Fig. 10** Top views and cross sections of the three main types of phase shifters available on the platform: (a) thermo-optic (also see Fig. 1); (b) electro-optic, based on plasma dispersion through carrier injection in a PIN junction; (c) electro-optic, based on EFIPE with a high-inverse bias voltage through a PIN junction.
2.2.2 Detectors

The platform includes monolithically integrated germanium (Ge) photodiodes (PD), with responsivity on the order of 1 A/W at a 1550 nm wavelength, meaning 80% quantum efficiency. We have developed both high-speed PDs and monitor PDs. The high-speed PDs exceed 40-GHz speed when operated with 1-V reverse bias,10 with a dark current of about 4 μA, whereas monitor PDs are operated with lower bias voltage and have about 10-nA dark current with about 1-GHz speed. We are presently starting cryogenic characterization of the PDs to determine the temperature dependence of dark current,69 responsivity, signal-to-noise ratio,69 speed, carrier freeze-out, and wavelength range of detection. We are also developing avalanche photodetectors71 exploiting the avalanche effect in silicon72 and also plan to operate them in Geiger mode to achieve single-photon avalanche detectors.73

Additionally, in collaboration with ETH Zürich, we are also developing high-speed plasmonic Ge detectors to exceed 500 GHz analog bandwidth.74,75 Here the main driver is not the detection efficiency but high-speed operation at a few deg. Kelvin, with the goal of developing suitable OECS to transfer a large amount of data to the cryostat. As explained in more detail in Sec. 4, the idea is to drive superconducting electronics (e.g., single-flux quantum, SFQ) using optical fibers.

With cryogenic and quantum applications in mind, we are also developing guided-wave SNSPDs, with the final goal of coupling them through a light escalator [Fig. 9(b)]. In order to speed up the detector development, we have started fabricating the devices sketched in Fig. 11(c). We first oxidized a silicon wafer, deposited superconducting NbN on the thermal oxide, and patterned the nanowires using e-beam lithography, as shown in Fig. 11(a). Next, we deposited a-Si:H and patterned the waveguides [Fig. 11(b)] including inverse tapers to improve fiber coupling from the chip edge. The optical fiber is aligned using a nanopositioner in the cryostat. In parallel, we are also developing amorphous alternatives76,77 to crystalline NbN, targeting improved fabrication yield of the detectors.

The SNSPD is the closest thing to an ideal single-photon detector demonstrated to date, with detection efficiencies exceeding 97% extending into the telecom wavelength range,78 speeds in the GHZ range,78 jitter even lower than 3 ps,80 and dark counts under 0.1 Hz.81 However, for some quantum realizations,82 high precision flip-chip bonding at the wafer scale, which is needed to generate light on chip.

Integration of TESs on optical waveguides has already been demonstrated on other platforms.88,89 Our integration approach is in line with what we explained above for SNSPDs and leverages the TES pixel90 and SQUID-based readout technology93 developed at VTT. From a broader perspective, the in-house integrated superconducting device technology based on Nb cross junctions95 can provide interesting opportunities for the quantum upgrade of the micron-scale platform (also see Sec. 4).

For example, we presently use the technology for the TES read-out circuits,99 SQUID magnetometers,93 and different Josephson parametric devices.94,95 Furthermore, in collaboration with the Royal Institute of Technology KTH and with the company Single Quantum, we are also exploring the possible use of single SNSPDs as efficient PNR detectors.96,97

2.3 Hybrid Integration

Several different PIC technologies are available, including most mature submicron and micron-scale silicon and silicon nitride platforms, and micron-scale indium phosphide platforms, as well as the more recent lithium niobate on-insulator platforms and compound-on-insulator platforms.106 Each material system comes with its strengths and weaknesses, and suitable combinations of complementary systems are thus often needed to achieve fully integrated solutions. A quintessential case is the lack of monolithically integrated light sources in all platforms not based on compound semiconductors, where either heterogeneous integration106 or hybrid integration1,107 is needed to generate light on chip.

Our main focus at VTT is on hybrid integration based on high-precision flip-chip bonding at the wafer scale, which is suitable for mid-volume production in a complementary metal oxide semiconductor (CMOS) fabrication facility like ours. Unlike with heterogeneous and monolithic integration, in the

![Fig. 11](image-url) (a) SEM picture of a fabricated NbN SNSPD before a-Si:H deposition; (b) micrograph of a detail of a fabricated chip after etching the a-Si:H waveguides; (c) sketched cross section of an a-Si:H waveguide with the NbN nanowire embedded (in green).
hybrid approach, the silicon process and the III-V process (or the process of any other complementary material system) can happen in parallel in two different fabrication facilities, which comes with several advantages. These include shorter overall lead time, reduced process flow complexity, reduced constraints and trade-offs for the two material systems, and decoupled yield of the two processes, resulting in higher overall yield, i.e., higher cost efficiency. Another advantage of hybrid integration is that it is not bound to the constraints that may arise in monolithic integration regarding, e.g., CMOS compatibility and thermal budgets. Furthermore, hybrid integration can be made with commercially available dies (e.g., light sources or photodetectors) which can lead to even higher cost efficiency.

Using either vertical facets or URMs, we can easily integrate devices where light propagates, respectively, in-plane, such as distributed Bragg reflector lasers, semiconductor optical amplifiers, or electro-absorption modulators, or out-of-plane, such as vertical cavity emitting lasers or free-space photodetectors. In particular, the URM can be a key component for QPICs, as it is extremely low-loss, broadband, and polarization-independent. For example, it can be used to efficiently couple light from deterministic single-photon sources based on quantum dots in vertical cavities or to couple single photons or Gaussian states to arrays of short SNSPDs [see Fig. 12(b)]. We stress here that, even though we have a clear path to monolithic integration of SNSPDs (see Sec. 2.2), based on the above considerations, hybrid integration will be the most efficient integration approach for large SNSPD arrays until we develop a SNSPD fabrication process with sufficiently high yield.

3 QKD Receivers

A first example application that can be enabled by the thick-SOI platform is QKD networks with higher key rates and/or longer working distance. In fact, PIC solutions are in the product roadmap of major QKD players because of their unmatched scalability and scalability. Indeed, several examples of PIC-based implementations have been reported to date, covering different types of QKD schemes. We have identified a clear path for how the platform could support the development and large-scale deployment of high-performance QKD systems for both discrete variable (DV) QKD and continuous variable (CV) QKD, as briefly presented in the following.

3.1 DV-QKD

DV-QKD systems are most suitable to cover long distances. The longest QKD link reported to date reached 830 km using a special configuration with a central node, whereas the longest point-to-point link exceeded 400 km (corresponding to about 70 dB loss in ultralow loss fibers). The best commercial systems are typically limited to the 100- to 150-km range, mainly to ensure secure communication with key rates high enough to be useful. In fact, in the DV-QKD implementations most suitable for long distances, the key rate scales linearly with the link transmission probability $\eta$, which is the probability of a transmitted photon being detected at the receiver, accounting for all possible transmission and coupling losses as well as the limited detector efficiency. In stark contrast to classical optical communication links, such key rate scaling implies a large mismatch between the transmission speed and the detection speed. In other words, the detector can be orders of magnitude slower than the modulator, which is a unique opportunity to combine the fastest ever achieved optical modulators with the most efficient single-photon detectors demonstrated to date, namely plasmonic modulators and SNSPDs, respectively. Transmitter speeds of present QKD systems are on the order of a few GHz, meaning that plasmonic phase and amplitude modulators could be used to boost the key rate by at least two orders of magnitude, while being still well-matched by SNSPDs on the receiver side. In fact, present commercial SNSPDs can easily exceed 10-MHz count rates with more than 80% detection efficiency and will possibly exceed GHz count rates and 95% detection efficiency in the future. We stress that the high losses of plasmonic modulators, which are a strong limitation for classical optical communication, are not at all a problem for practical DV-QKD transmitters, which are based on strongly attenuated light sources. On the other hand, high losses are not tolerable for the receiver, so plasmonic modulators are not an option for protocols (such as the standard BB84) where modulators are also needed to choose the measurement basis on the receiver side. Nevertheless, this is not a strong limitation, given that the most robust protocols for

![Fig. 12](image-url)
practical DV-QKD rely on passive receivers, requiring no modulators.\textsuperscript{122,124,125}

The combination of plasmonic modulators and SNSPDs becomes even more attractive when considering that some of the most promising DV-QKD protocols, including measurement-device-independent (MDI) QKD\textsuperscript{126,127} and twin-field QKD\textsuperscript{20,123,129} connect the users through a central unit (completely untrusted) where all the photon detections occur [Fig. 12(a)]. Large-scale deployment of these systems can be achieved by providing all users with low-cost transmitters (achievable with plasmonic chips) while deploying a central detection unit, owned by the operator, to host a table-top closed-cycle cryostat where thousands of SNSPDs can be economically cooled down and operated in parallel. In this vision, the cryostat would be connected to tens of hundreds of fibers, and each fiber should carry tens to hundreds of wavelength division multiplexed (WDM) signals.

To this end, at VTT we are presently fabricating low-loss AWGs to demultiplex the WDM signals coming from a single fiber and couple them to flip-chip-bonded arrays of SNSPDs designed and fabricated by Single Quantum to match our layout [see Fig. 12(b)]. Monolithic integration of AWGs and SNSPDs has been already demonstrated\textsuperscript{128} but with high losses both for fiber coupling and demultiplexing. Furthermore, monolithic integration of large SNSPD arrays is still challenging, due to the relatively poor SNSPD fabrication yield. Hybrid integration of SNSPD chips (with only two detectors) has been demonstrated with submicron silicon waveguides\textsuperscript{129} for time multiplexed MDI-QKD. The coupling losses demonstrated therein were very high, as grating couplers were used to couple both the optical fiber and the SNSPDs. We instead aim at a solution simultaneously ensuring high yield, broadband low-loss fiber coupling, and low demultiplexing loss, which can be even made polarization-insensitive with a suitable design of the SNSPD geometry.\textsuperscript{130,133} The final goal is full monolithic integration of a DV-QKD receiver on the thick-SOI platform, providing much better and more stable control of relative phase and time jitter, therefore leading to higher fringe visibility.

3.2 CV-QKD

An alternative approach is CV-QKD, which relies on Gaussian states instead of single photons. The main advantage is that its implementation\textsuperscript{134} requires only standard telecom components used for classical coherent optical communication, and, in particular, there is no need for single-photon detectors. The main drawback is that secure implementations scale quadratically with the transmission probability $P$, which limits the operation range to about 50 km (or to be more rigorous, 10-dB loss, assuming standard 0.2 dB/km fiber loss). Furthermore, unlike DV-QKD, the receiver speed must match the transmitter speed. On the transmitter side, plasmonic modulators are again the perfect choice, given that their losses can be easily tolerated, and they can easily achieve both phase and amplitude ultrafast modulation simultaneously.\textsuperscript{135} Ultrafast phase modulation is needed also on the receiver side, but only on the local oscillator and not on the quantum states,\textsuperscript{136} meaning that some modulator losses are acceptable. Detection is typically done using shot-noise-limited balanced pulsed homodyne detectors\textsuperscript{137} whose operation speed and stability can greatly benefit from PIC integration and dedicated electronics.\textsuperscript{138}

We, therefore, plan to exploit fast Ge PDs in combination with our in-house expertise in ultrafast electronics\textsuperscript{139,140} to develop balanced photodetectors with a speed above 50 GHz. We stress that even though the speed of our present Ge PDs is limited to about 40 GHz, suitably designed Ge PDs with smaller volumes have been recently demonstrated to reach up to 265 GHz.\textsuperscript{135} In our vision, the CV-QKD receiver will be monolithically integrated on our thick-SOI platform, to include the ultrafast plasmonic phase modulator and the balanced photodiode. Also in this case, the PIC will ensure much better and more stable control of relative phase and time jitter compared to realizations based on optical fibers, therefore, leading to improved overall performance of the whole QKD system.

On the transmitter side, integration of the plasmonic devices on our platform would not be strictly necessary, but it could improve operation stability, e.g., through integrated Faraday mirrors (see Sec. 2.1) not available in any other PIC platform. Similar considerations apply to DV-QKD transmitters. Indeed, many practical implementations of both DV- and CV-QKD rely on Faraday mirrors.\textsuperscript{41,122,125}

The platform can also support quantum communication applications beyond QKD. A promising path is the development of acousto-optical devices to efficiently transduce superconducting qubits or spin qubits into optical qubits and vice versa. Such transducers would allow us to connect quantum processors via optical quantum states in optical fibers and create more powerful quantum computers based on multiquantum-processor architectures, even using quantum computers located several kilometers away. With this application in mind, together with the University of Bristol, we are exploring the possible realization of efficient piezoelectric microwave-to-optical transducers.\textsuperscript{136}

4 Scaling-Up Cryogenic Quantum Computers

A second example application is the use of optical fibers to transfer data to and from superconducting quantum computers, aiming to scale up the number of qubits and achieve useful universal quantum computing. We are currently in the “noisy intermediate-scale quantum” era,\textsuperscript{137} which means that significant applications are expected already in the short- and medium-term with a limited number of noisy qubits. However, it is generally agreed that universally useful quantum computers will require about one million qubits.\textsuperscript{138}

To date, the most advanced universal quantum computers are based on superconducting qubits and operated at temperatures below 50 mK, which is required to minimize thermal noise. A highly scalable approach based on silicon qubits is also quickly evolving\textsuperscript{139-143} and requires low temperatures as well. In all cryogenic quantum processors, electrical transmission lines are used to carry the electrical signals driving and reading the qubits inside the cryostat. Even though this approach is feasible when dealing with a few hundreds of qubits, it becomes challenging for thousands of qubits and not viable anymore when approaching one million qubits. In fact, electrical cables come with a detrimental trade-off between bandwidth and thermal conductivity. For these reasons, at VTT, we are intensely developing the next generation of communication interfaces for cryogenic qubits, using optical fibers and suitable OECs and EOCs.

There are at least two significantly different research directions for the optical control of superconducting quantum technology: (i) a number of OECs generate the drive signals of
a quantum computer at the cryogenic temperature. Here the OEC must receive an optical signal from room temperature that is directly suitable for driving the qubits and their gates. (ii) A number of cryogenic OECs receive digital optical input signals and convert them into digital electrical signals driven into a superconducting SFQ device. The SFQ is a superconducting processor for classical data that can also generate drive signals for the quantum computer, as shown in Fig. 13. The packaging density (crucial for scaling up) of both approaches can be supported by integrated optical techniques, such as WDM for multiplexing multiple signals into the same optical fiber.

The control of qubits has already been demonstrated for the first approach. This approach benefits from the possibility of using existing electrical qubit drive electronics whose signals are simply converted into an optical form with an EOC at room temperature. However, at the small signal levels required by quantum computers, OECs suffer from shot noise, which can be detrimental for driving their analogue signals into sensitive quantum computers. The second approach is significantly more tolerant to shot noise, since the OECs only need to generate digital signals for SFQ, which can generate quantized analogue signals based on digital input data.

Our vision follows this second approach, illustrated in Fig. 13, where a large amount of data from a supercomputer is serialized by a suitable EOC and sent through an optical fiber to a cryogenic OEC to drive SFQ logic. After inputting the data into the quantum processor, the SFQ co-processors use the calculation output to drive a suitable cryogenic EOC that, through another optical fiber, sends the results to a deserializing OEC that communicates back to the supercomputer.

The serializer and deserializer are in general needed because the speed of SFQ logic is typically much higher than the speed of standard CMOS electronics. SFQ is a promising choice due to its ultralow energy dissipation, which is mandatory when working at the ultralow temperatures required by superconducting quantum computers.

CMOS electronics can also be used in cryogenic environments, where low temperatures allow lower operating voltages and thus lower power consumption. Cryo-CMOS uses traditional CMOS components that are tailored toward low-temperature operation. However, with CMOS circuits, it is very hard to have sufficiently small dissipation. For example, the total power dissipation of only two-spin qubit processor read-out and control circuitry operated at 3 K was 330 mW, which is already on the high end of the tolerance level of the modern cryostats. Furthermore, reaching high enough clock rates (>1 GHz) at low temperature is a significant challenge that, if not solved, implies higher qubit overhead. The strong points of the cryo-CMOS technology are the existing fabrication infrastructure and the advanced design tools and expertise.

More dramatic gains in energy efficiency are possible using SFQ technology. This technology and its variants, such as energy efficient SFQ, represent bits as short (∼1 ps) pulses produced by switching processes in superconducting tunnel junctions called Josephson junctions. The typical energy of these pulses is only 0.2 aJ, and the pulses can be processed at speeds exceeding 100 GHz. In the past, their use has been limited by the requirement of cryogenic temperature operation and medium packing density of components. For qubit interfacing purposes, neither of these issues is relevant. Superconducting electronics based on SFQ logic dissipates <1% of the energy dissipated by CMOS electronics and enhanced variants (eSFQ or eRSFQ logic) can even dissipate <0.1% compared to the CMOS systems. SFQ controllers additionally enable vastly superior clock frequencies, in extreme cases even above 700 GHz. With advanced thermal management, the SFQ controllers could be even directly integrated with the qubit processor altogether removing the need for very complex cabling solutions.

As part of this vision, we are presently developing, together with our partners, several PIC solutions for different building blocks. For example, in Fig. 14, we show a long-term vision of how to replace a prototype serializer, presently based on optical fibers and discrete components, with a fully integrated PIC solution. A III-V reflective semiconductor optical amplifier, including a saturable absorber, is flip-chip bonded on the silicon chip where it is coupled to an integrated, compact, and low-loss external cavity to create an integrated mode-locked laser (IMLL). The generated wavelengths are then separated by a low-loss integrated demultiplexer. The signal in each waveguide is finally modulated independently through an array of amplitude modulators, each driven by relatively slow electrical signals (from 1 to 2.5 GHz). The resulting signals are first delayed by multiples of a suitable delay unit and finally recombined through a wavelength multiplexer. We are presently developing passive PICs combining the delay lines and the final multiplexer. We will test them as part of the free-space serializer prototype we have already built.
A second example is the cryogenic OEC that we are building using SNSPDs. In this particular application, we are more interested in their detection speed rather than extremely high detection efficiency, given that we can afford to use multiple photons per pulse. Together with our collaborators, we are trying to achieve the ultimate SNSPD speed. A simple approach is to make the nanowire as short as possible, but experimental results clearly show that latching becomes an issue in doing so. Active electrical quenching has also been proposed but without dramatic improvements. In order for the OEC speed to approach the SFQ speed, we are also exploring different multiplexing approaches, addressing arrays of SNSPDs instead of single detectors. In this approach, we avoid using the optical serializer at room temperature and replace it with an electrical serializer inside the cryostat, resulting in major underexploitation of the fiber bandwidth. The simplest brute force approach is space division multiplexing, i.e., coupling each SNSPD with a dedicated fiber. We are indeed developing 2D fiber arrays suitable for cryogenic illumination of detector arrays. A finer approach is to use WDM the same way as in Fig. 12(b), where a single fiber carries several wavelengths. Time division multiplexing could also be an option, but it would require active control of a network of relatively fast switches.

The most demanding part of the vision in Fig. 13 is by far the cryogenic EOC. In fact, the energy and the voltages available from the SFQ electronics are very low (attojoules per bit and microvolt, respectively), and thus driving a fast optical modulator inside the cryostat is very challenging. Even though plasmonic modulators have been demonstrated to work with <1 V and attojoule the energy level, driving them with SFQ is still nontrivial and requires some major development, which we are presently tackling.

Together with our partners, we are presently developing the SFQ processors in parallel as well as PIC-enabled EOCs and OECs, and we plan to start testing combinations of these different building blocks in the next few years as proofs of concept of our vision. In the long run, this will support the development of the Finnish quantum computer, which has recently achieved the first milestone of five qubits and is now targeting 50 qubit superconducting quantum computer by 2024. At the same time, the same optical interfacing technology will help scale up also the customized silicon qubit platform that we are codeveloping.

5 Other Interesting Applications and Conclusions

To conclude, we briefly mention that the thick-SOI technology can support many other quantum technology developments. For example, we have just started a project with KTH to integrate their thin lithium niobate waveguides on our platform. We have also ongoing discussions with Tampere University on how to exploit the multimode behavior and mode preservation capabilities of our PICs (see Sec. 2.1) to support spatial shaping of their qubits. We have also identified turbulence mitigation for satellite QKD as a promising application of our low-loss PICs with efficient phase shifters and integrated responsive detectors. We additionally have an ongoing collaboration with the Max Planck Institute for Quantum Optics to implant erbium in our silicon waveguides to achieve quantum emitters with narrow linewidth.

We have introduced the thick-SOI platform with a special focus on the unique features that make it attractive for different quantum technologies, and we have also provided an overview of the ongoing developments to make it even more attractive in the near future. We presented two concrete cases elaborating in detail our vision of how PIC-based solutions will be able to support the large-scale deployment of high-performance QKD networks based on both DV–QKD and CV–QKD as well as the scaling-up of useful cryogenic quantum computers.

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Quantum key distribution systems, employing continuous-variable quantum key distribution, have demonstrated significant progress. A photonic integrated quantum secure communication system, as described by M. Avesani et al. (2021), has shown promise in high-fill-factor superconducting microwire detectors with reduced polarization sensitivity. Another advancement is the single-photon detector implemented in a 2D photonic crystal cavity, as reported by B. Patra et al. (2021). These developments highlight the importance of theoretical and experimental progress in improving the efficiency and security of quantum key distribution networks.
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