Dual Frequency Orbiter-Radar System for the Observation of Seas and Tides on Titan: Extraterrestrial Oceanography from Satellite

Marco Mastrogiuseppe
Division of Geological and Planetary Sciences, California Institute of Technology, Pasadena, CA 91125, USA; mmastrog@caltech.edu; Tel.: +1-626-628-6899

Received: 16 July 2019; Accepted: 6 August 2019; Published: 14 August 2019

Abstract: Saturn’s largest moon, Titan, is believed to have a ~100 km thick ice shell above a global ocean of liquid water. Organic materials, including liquid hydrocarbon lakes and seas in its polar terrain, cover Titan’s surface, which makes it a world of two oceans. The RADAR instrument on board Cassini, was able to probe lakes and seas during few dedicated altimetric observations, revealing its capability to work as a sounder. Herein, we describe the design of, and scientific motivation for, a dual frequency X/Ka-band radar system that is able to investigate Titan’s subsurface liquid water ocean, as well as the depth and composition of its surface liquid hydrocarbon basins. The proposed system, which could take advantage of the telecommunications dish, can operate as a sounder, as Synthetic Aperture Radar (SAR) able to map the surface at tens meters of scale resolution, and when data are acquired from close-adjacent orbits, as a repeat-pass SAR interferometer (InSAR). The instrument, which is based on the architecture of the Cassini RADAR, can also characterize Titan’s interior by using geophysical measurements of the tidal amplitude to derive high accuracy estimates of the Love number h2 from a 1500 km circular orbit.

Keywords: bathymetry; radar system; extraterrestrial oceanography; geophysical measurements

1. Introduction

Titan, the second largest moon in our solar system, has been repeatedly observed by the Cassini spacecraft during its 13 years exploration of the Saturnian system (2004–2017). The Cassini RADAR instrument was capable of operating in multimode as a Synthetic Aperture Radar (SAR) for surface imaging, as a radar altimeter for topography measurements, as a scatterometer for surface composition and, in passive mode, as a radiometer for brightness temperature [1]. The instrument has provided imaging at 300 m/pixel for about 20% of the surface of the moon and ~50% has been mapped at 1500 m/pixels, as well as 40 topographic profiles have been acquired in altimetry mode. This dataset enabled the identification and characterization of several geomorphologic features.

Hundred meters high dunes fields [2], which are spread across the equator (±30° in latitude), covering about 15% of the whole surface [3,4] have been observed by the instruments in different modes (i.e., SAR, altimetry, radiometry). Their shape is believed to be the result of a general eastward transport of cohesive organic solids [5], their morphology being similar to the terrestrial dunes seen in Namib, Sahara, and Arabian deserts [6], and their material is likely to be composed by solid hydrocarbons, mixed with water ice at interdune [7–10]. Instruments on board Cassini also revealed the presence of mountains [11–13], craters [14] with possible cryovolcanic origin [15], in addition to a complex hydrological system that is made of liquid hydrocarbons with possible subsurface connection [16]. Other features, interpreted as empty lakes, have been mapped by Cassini and have been object of several works [17–19]. Their formation is still the object of studies, although some hypothesis regarding their endogenic origin has been recently proposed [20].
The presence of standing hydrocarbons liquid bodies on Titan was revealed by Cassini on 22 July 2006, during the fly-by T16, when the radar mapped a collection of 10–100 km diameter lakes present in the northern hemisphere [21]. Later observations revealed the existence of an active hydrological cycle of methane [22], and the presence of large northern basins identified as seas, or maria: Kraken Mare, Ligeia Mare and Punga Mare [23]. A detailed description and mapping of the Titan’s polar terrains is reported in [24]. Specific observations that were planned and executed over the major seas and lakes in altimetry mode, made the direct measurements of depth—bathymetry and composition of few hydrocarbon basins present on Titan possible [25–27], revealing the ability of Cassini to work as a radar sounder despite the relative high operative frequency (13.7 GHz). The same observations were also used to constrain the roughness of seas and lakes on Titan from surface amplitude analysis returns [27–30] and to detect the presence of fluvial networks of channels and canyons filled with liquid hydrocarbons [31].

Here, we propose a radar system that is able to provide three-dimensional high resolution bathymetric maps of Titan seas and lakes at multiple frequencies, allowing for the investigation of any possible spatial [32,33] or seasonal [34] variation in composition of the liquid and/or sea floor properties. The system will additionally enable the investigation of any suspended particulates—material, density heterogeneities of the liquid column within a resolution of few meters. The use of an X band frequency could permit the detection of the seafloor of the largest Titan’s sea, Kraken Mare, which is either too deep or too absorptive for being detected by the Cassini RADAR. Moreover, the radar system used in off-nadir configuration can provide high resolution mapping and, when optimal orbit configurations are met, repeated passes could be used for interferometric synthetic aperture radar (InSAR) processing in order to obtain high resolution topography. After two years of operation, Titan global topography could be available at km horizontal scale and meters scale vertical resolution, allowing much better accuracy than the one available today from Cassini [35].

In addition, synthetic aperture algorithms that were applied to the altimetry data could provide remarkable enhancement in spatial resolution when compared to the Cassini capabilities [36]. Further applications could include the investigation of any ephemeral event on specific areas of Titan, as rarely observed by Cassini [37,38], the estimation of the liquid level of seas and lakes, characterization of rivers, sea and lake roughness, rain detection, atmosphere/clouds absorption, and dielectric properties estimation of solid and liquid. Finally, the system can be used to estimates the tides for the investigation of Titan’s internal ocean by using repeated passes observations in altimetry mode acquired over the same location at different epochs. The selected radar frequencies and a suitable system design allow for this radar multimode instrument to operate alternatively as an altimeter, SAR, sounder, and/or radiometer by means of a programmable and adaptive on-orbit reconfiguration.

2. Materials and Methods

2.1. Bathymetric Measurements of Titan’s Seas

The possible presence of a hydrocarbon global ocean on Titan, its depth, and composition, have been investigated prior to the Cassini arrival through atmospheric-surface modelling [39–42] and ground based radar observation [43]. However, Cassini revealed that a global ocean of liquid hydrocarbons is not present, but large liquid filled basins are found to be mostly distributed at the northern hemisphere in form of seas and lakes. Differently, the southern hemisphere only shows few small liquid filled basins, in addition to the largest southern lake Ontario and a large number of basins that have been interpreted as paleoseas [44]. The dichotomy of the northern and southern hemisphere lakes distribution has been attributed to a long scale climate variation that is induced by the orbital configuration of Titan respect to Saturn [45].

Since the Cassini arrival, the depth and composition of Titan’s seas and lakes have been an object of interest for several studies [46–49], while the first opportunity to perform a direct measurements of Titan’s seas was only possible during fly-by T91 on May 2013, across the second largest sea,
Ligeia Mare [25]. This represented the first direct measurement of an extraterrestrial bathymetric profile. The experiment that was conducted from 1500 km of altitude allowed for the radar on board Cassini, to directly probe the sea down to a maximum depth of 170 m. Data that were acquired from this observation were used to create a topographic profile of the seafloor of Ligeia Mare and to constrain the liquid composition from signal attenuation [25,50]. Assuming a ternary mixture of methane-ethane-nitrogen composition, while using the laboratory measurements of [51] and applying the Lorentz-Lorenz formulation with nitrogen mixing ratios, as determined by [52], the measured loss tangent ($4 \pm 1 \times 10^{-5}$) was converted into a mixture of approximately 71% CH$_4$, 12% C$_2$H$_6$, 17% N$_2$, which indicated that Ligeia was methane dominated at the time of observation. Moreover, by combining the information relative to the areal extension that was obtained from SAR images and assuming an average value of depth of 70 m, the authors were able to extrapolate the total liquid volume of the basin, which resulted in $\sim 10^4$ km$^3$ [25].

By means of the waveform fitting approach that was able to reproduce the saturation effects at the receiver [50], Mastrogiuseppe and colleagues re-analyzed saturated altimetric data that were acquired during fly-by T49 on 21 December 2008, to extract information regarding the depth and composition of southern Ontario Lacus [53]. An optimized signal processing, which adopted super resolution techniques [54,55], revealed the presence of lakebed signal reflections at $\sim 50$ m of maximum depth, which was consistent with the indirect measurements of bathymetry as extrapolated from the shorelines slope measured from altimetry [46]. Assuming a similar ternary composition, the best fit loss tangent at Ontario Lacus ($6 \pm 3 \times 10^{-5}$) was found to be consistent with $\sim 47\%$ CH$_4$, $\sim 40\%$ C$_2$H$_6$, and $\sim 13\%$ N$_2$. Similarly to Ligeia, Ontario appeared methane dominated, but the measured best fit loss tangent could indicate an increased abundance of higher order hydrocarbons, as observed from spectral VIMS analysis [56]. A detailed description of Ontario lacus and its geomorphology is described in [57,58].

Following the T91 observation of Ligeia Mare, other experiments, which aimed at investigating Titan’s seas and lakes in sounding mode, have been planned and executed. Specifically, during the fly-bys T104 on August 2014, T108 on January 2015 and T126 on April 2017, the Cassini RADAR observed the largest sea Kraken Mare, Punga Mare and the northern Lake District, respectively. While the seafloor was not detected at Kraken, which suggested that the sea was either too deep or too absorptive, a clear detection of the subsurface of Punga Mare was observed with a maximum depth of 120 m. Similarly, during fly-by T126 the RADAR was able to probe Winnipeg Lacus down to 100 m of depth from an altitude of 1200 km [27]. The loss tangent analysis of these two observations indicates that the northern lakes and Punga Mare were similar in composition to Ligeia Mare during the time of observation. Table 1 reports the composition and bathymetry of the observed seas and lakes.

| Sea/Lake       | Estimated Depths | Tan Delta | Latitude | Composition $^1$ CH$_4$/C$_2$H$_6$/N$_2$ | Epoch of Observation | Fly-By |
|----------------|------------------|-----------|----------|----------------------------------------|----------------------|--------|
| Ligeia Mare    | 20–170 m         | 4 $\pm 1 \times 10^{-5}$ | 77°–82°N | 71/12/17%                             | May 2013             | T91    |
| Punga Mare     | 20–120 m         | 3 $\pm 1 \times 10^{-5}$ | 83°–84°N | 80/20/0%                              | January 2015         | T108   |
| Baffin Sinus   | 20–60 m          | 3 $\pm 1 \times 10^{-5}$ | 80°–81°N | 80/20/0%                              | January 2015         | T108   |
| Winnipeg       | 20–100 m         | 4 $\pm 1 \times 10^{-5}$ | 78°N     | 69/15/16%                            | April 2017           | T126   |
| Ontario        | 20–60 m          | 6 $\pm 3 \times 10^{-5}$ | 72°S     | 47/40/13%                            | December 2008        | T49    |
| Kraken Mare    | Not Detected     | -         | 60°–80°N | -                                     | August 2014          | T104   |

$^1$ Composition values are referred to best fit loss tangent and does not include errors.

In Figure 1, we report a SAR mosaic of the northern polar region and the T91, T104, T108 altimetric tracks over the seas. The bottom part of the figure shows the relative radargram and bathymetric products that were obtained after processing. Figure 2 shows the SAR images of Ontario and Winnipeg Lacus and a waveform that was selected over the deepest portion of the track.
2.2. Proposed System: Dual-Frequency Ka/X Bands Multimode Radar Orbiter

Cassini provided important information regarding Titan’s seas with only limited number of tracks. Radar investigation from an orbiter and in-situ measurements are envisaged in order to determine a detailed variability of sea composition, as well as the depth and composition of Titan’s largest sea (Kraken Mare) [59,60]. Herein, we propose a dual-frequency radar system operating at X (7.5 GHz) and Ka (32 GHz) bands from a 1500 km circular orbit. A 50 MHz bandwidth system capable to provide 3 m of vertical resolution on free space has been selected in order to achieve sufficient accuracy for bathymetric measurements, Titan’s imaging, and tides investigation. Data volume reduction will be accomplished through dedicate on board processing that will be applied to the specific radar mode.

Figure 1. (a) Synthetic Aperture Radar (SAR) image mosaic of Titan’s northern polar terrain and altimetric tracks acquired during fly-bys T91, T104, and T108 over Ligeia Mare, Kraken Mare, and Punga Mare, respectively. (b) Radargram obtained from T91 and relative bathymetry of Ligeia. (c) Radargram of Kraken Mare (T104) where no seafloor was detected. (d) Radargram of Punga Mare (T108) and relative bathymetry.
The onboard processing should be designed according to the various operative mode of the radar system. The Ka band has been designed for shallow bathymetry investigation and topographic measurements taking advantage of the higher signal to noise ratio (SNR) and the reduced footprint. While the deepest part of the hydrocarbons seas could be difficult to probe at this frequency due to the high absorption, this band could provide high resolution bathymetry close to the shorelines or the composition and depth of shallow lakes.

We report the SNR calculated according to the radar equation and while taking a pulse limited geometry into account:

$$SNR = \frac{P_t \cdot G_{ant}^2 \cdot \lambda^2 \cdot \sigma \cdot B \cdot T}{(4\pi)^3 \cdot H^4 \cdot K \cdot T_{eq} \cdot B \cdot \sqrt{N}}$$

where all of the variables are reported in Table 2.

The radar cross section $\sigma$ can be evaluated according to the scenario which is expected to be observed. When considering an illuminated surface of area $A_{surf}$, reflectivity $\Gamma$ and a roughness with an rms slope equal to $m$, according to the Geometric Optics (GO) formulation, the radar cross section can be expressed as:

$$\sigma = \sigma^0 \cdot A_{surf} = \frac{\Gamma}{2m^2} \cdot A_{surf}$$

When considering the pulse-limited geometry, the illuminated area can be calculated as:

$$A_{surf} = 2\pi \cdot H \cdot \delta_r$$

where $\delta_r$ is the range resolution, which is related to the radar bandwidth by the following:

$$\delta_r = 0.88 \cdot \frac{c}{2B}$$
Table 2. Radar Parameters for the proposed system.

| Symbol  | Quantity               | Unit   | Value   |
|---------|------------------------|--------|---------|
| P<sub>t</sub> | Tx Power               | [W]    | 40      |
| L       | Antenna size           | [m]    | 4       |
| G<sub>ant</sub> | Antenna Gain         | [dB]   | 54 (K<sub>a</sub>) |
|         |                        |        | 42 (X)  |
| T       | Tx Chirp Length        | [µs]   | 150     |
| H       | Altitude               | [km]   | 1500    |
| λ       | Wavelength             | [m]    | 0.009 (K<sub>a</sub> band) |
|         |                        |        | 0.04 (X band) |
| N       | Pulses #               |        | 45      |
| B       | Bandwidth              | [MHz]  | 50      |
| T<sub>eq</sub> | Eq. Temp. Rx          | [K]    | 1000    |
| K       | Boltzmann constant     | [J/K]  | 1.38 × 10<sup>-23</sup> |
| δ<sub>r</sub> | Vertical res.         | [m]    | 3       |
| R<sub>az</sub> | Horizontal res.      | [m]    | 6000    |
| V<sub>t</sub> | Tangential Velocity   | [km/s] | 1.5     |

In Figure 3, a plot of the SNR at Ka and X band is shown, which is calculated for different values of the rms slope and $\Gamma = -11$ dB. In Table 2, we report the radar parameters and spatial resolution for the proposed system.

2.3. High-Resolution SAR and Interferometry Mode

Here, we discuss the design of the main parameters for the proposed radar system when operating in off-nadir configuration as a SAR for high resolution mapping of Titan, and as an interferometer while using repeated passes [61,62] in order to obtain three-dimensional (3D) topography of the moon.

In Table 3, we report the main requirements for the proposed system.

Table 3. SAR system main requirements.

| Requirements                  | Unit  | Value |
|-------------------------------|-------|-------|
| Ground Resolution             | [m]   | ≤20   |
| Height Measurements Accuracy  | [m]   | <5    |
| Height Resolution             | [m]   | <50   |
| Radiometric Resolution        | [dB]  | <1.2  |
| Noise Equivalent              | [dB]  | ≤-15  |

The system can operate in strip map mode, allowing for collecting images over specific areas of the moon with a pixel resolution better than 20 m and a radiometric resolution better than 1.2 dB,
depending on the geometry of the observation. The horizontal resolution can be easily achieved via a matched filter applied to each received waveform and a multi-look can be performed in the azimuth direction, as well as in range when the off-nadir angle allows for sufficient ground resolution. The azimuthal resolution will be obtained while using a SAR processing applied to the received echoes. The pulse repetition frequency (PRF) of the system must be properly selected in order to correctly sample the Doppler bandwidth and avoid overlapping of the received echoes with transmitted waveforms. The off-nadir angle will vary according to the target of interest, however we will consider a values between 10–30 degree for the present analysis.

According to (5), the maximum resolution achievable in cross track direction ranges from 6 to 17 m for off-nadir angles of 30° and 10°, respectively:

\[ R_{\text{range}} = \frac{c}{2B \sin(\alpha)} \] (5)

The limit for the azimuth resolution is driven by the antenna system according to the physical dimension of the antenna in along track (L):

\[ R_{\text{az}} = \frac{L}{2} \] (6)

which for the proposed system reach a value of \( R_{\text{az}} = 2 \text{ m} \).

Based on the ground resolution requirements, a multi-look average by a factor of 10 can be always performed, therefore according to (7), the radiometric resolution requirements in Table 3 can be always achieved:

\[ R_r = 10 \log_{10} \left[ 1 + \left( 1 + \frac{1}{\text{SNR}} \right) \frac{1}{\sqrt{NL}} \right] \] (7)

The main parameter that remains to be set is the SAR PRF. A lower bound can be set to 0.8 KHz, as obtained from the antenna physical dimension and tangential velocity \( V_t \) from:

\[ \text{PRF}_{\text{min}} > \frac{2V_t}{L} \] (8)

It is worth noting that this limit does not depend on the operative frequency.

The upper bound can be calculated from (9) in order to avoid the overlapping of transmitted and received waveforms.

\[ \text{PRF}_{\text{max}} < \frac{c L \cos(\alpha)}{2 \lambda H \tan(\alpha)} \] (9)

We found values of 66 KHz and 15 KHz for the Ka and X bands, respectively.

The calculated PRF only indicates the lower and upper limits and it should be adjusted for accounting of the ambiguity of the returned echoes. For our proposal, we found as good choice a PRF of 5 KHz, which is able to satisfy the PRF requirements at both frequencies.

2.4. Interferometric System

The proposed system can also operate as an interferometer by means of repeated passes when the favorable orbital conditions are met. The height resolution can be defined as the value of the height, which generates a phase rotation of the signal equal to \( 2\pi \) and it is defined by:

\[ \Delta q \approx \frac{\lambda H \tan(\alpha)}{2B_s \cos(\alpha)} \] (10)

where \( B_s \) is the spatial baseline (i.e., distance of repeated tracks).

Therefore, the baseline must be greater than 50 m in Ka and 220 m in X band in order to obtain an height resolution better than the requirements in Table 3; these requirements are followed by an
upper limit value of the baseline, which is dictated by the decorrelation of the signal when a scenario is observed from different angles of view. Such an upper limit can be calculated using:

\[
\sigma_{\Delta \phi} = \frac{1}{\sqrt{2N_L}} \sqrt{(1 + \text{SNR}^{-1})^2 - \rho^2}
\]  

(11)

where \(\rho\) is the modulus of the complex correlation coefficient, which only depends on the geometric parameters:

\[
\rho = 1 - \frac{2r_y B_s \cos^3(\alpha)}{\lambda H}
\]  

(12)

and \(r_y\) is the along track ground resolution.

Assuming no co-registration errors, normalized errors can be calculated while using the following:

\[
e_n = \sqrt{N_L} \frac{\sigma_q}{r_y}
\]  

(13)

where \(\sigma_q\) is the error on the estimated heights and it can be obtained combining the height resolution in (10) and the phase error as reported in (11).

Optimum horizontal baseline can be calculated by imposing a limit on the error. In Figure 4, we plot the error as function of the horizontal baseline for a system having 10 dB of SNR and \(N_L = 10\). We found an optimal \(B_s\) ranging from 220 to 1200 m and 50 to 260 m for the X and Ka band, respectively (see Figure 4), for example, while considering errors \(e_n < 0.2\).

Figure 4. Optimal baseline evaluation as function of the normalized error for X band (a) and Ka band (b).

2.5. Tides Measurements and Global Topography

Saturn’s largest moon, Titan, hosts a subsurface liquid water ocean that is likely composed of water and ammonia [63–66]. Titan also hosts extensive organic deposits across its surface and a hydrological cycle of hydrocarbons exchanged between the surface and atmosphere, making the environment of this moon particularly attractive in terms of extraterrestrial habitability [67,68]. Titan’s ice shell is expected to be ~100 km in thickness [69,70], therefore an investigation of the ocean performed while using
typical radar sounding systems, such as MARSIS and SHARAD [71,72], becomes challenging due to the limited penetration capability of such instruments. Alternatively, a radar altimeter can indirectly characterize subsurface properties, such as density of the internal ocean and ice shell thickness, through geophysical measurements of the tidal potential Love number $k_2$ and $h_2$. Such estimation can be performed via tides and topography measurements, along with the support of gravitational data through radio science instruments [73].

Tides models on Titan have been investigated for the solid surface [74] as well as for the polar hydrocarbons liquids [75–79]. A detailed description of the effects of tides on Titan’s polar liquid hydrocarbons is reported in [80]. The maximum vertical solid surface displacement is estimated to range between 10 m and 30 m at the poles and equator, respectively, for a model that accounts for the presence of an ocean [81]. The tidal Love numbers ($h_2$ and $k_2$) should be estimated with an accuracy on the order of 1% and 0.1% in order to investigate the characteristics of the ocean and the thickness of the ice shell, respectively, which requires centimeter-scale knowledge of the tidal amplitudes.

Altimetry satellites, such as POSEIDON [82], have provided centimeter scale accuracy of terrestrial surface height measurements, which allows for a global ocean characterization and topography at very high accuracy [83], obtained while using a radar system with hundreds MHz bandwidth, and knowledge of the spacecraft ephemerids in order of ten centimeters. Radar altimetry has greatly improved our knowledge of ocean tides on Earth [84]. Instruments, such as Jason1 and ERS, have observed the Earth more than 15 years, providing information regarding the global changes in both ocean circulation and sea level. A radar altimeter can measure tides using a network of single-point crossovers or though repeat adjacent ground tracks (see Figure 5) separated by less than the cross-track radar footprint [85]. Both of the methods provide differential measurements of the surface height (i.e., using the two-way travel time echo) acquired at the same location, but different true anomalies.

![Figure 5](image-url)

**Figure 5.** (a) Tides estimation via repeated ground track. (b) The crossover technique allows for having one differential range measurement for each pair of observation. (c) Repeated adjacent track configuration is less frequent, but it allows for multiple measurements for each pair.

The estimation of tidal amplitudes can be performed while using an inverse model and the Love number $h_2$ can be estimated with an accuracy that will mainly depend on the number of crossovers, the altimeter range accuracy, and the spacecraft positioning errors. When a large percentage of footprint superimposition is available, differential range measurements can be performed with an accuracy that is better than the radar resolution. While the crossover technique only allows few measurements for each pair of orbits, repeat ground tracks allows for multiple measurements while using a single pair of observations (see Figure 5). However, repeated ground tracks require the orbits to be close enough to have substantial overlap between footprints, and such a configuration is rarely met when compared to the crossovers that naturally occur in typical orbital geometries. The adjacent ground track technique (see Figure 5c) is particularly attractive, as long repeated ground tracks permit a large number of overlapped footprints to be collected and the potential Love number $h_2$ can be estimated with high
accuracy after acquiring only a few pairs of repeat passes. Observations should be planned in order to observe tides at different phases, for example, when the true anomaly of Titan is at 0 and 180 degree.

3. Discussion and Results

3.1. Sounding Mode Operative Frequency Optimization

The X band frequency has been designed to provide bathymetry and composition of the deepest portion of the seas, taking advantage of the improved penetration capabilities at a lower frequency. The trade-off for operative frequency selection has been investigated, as shown in Figure 6. The detection capabilities of a radar system operating from 1500 km circular orbit and using a 4 m dish antenna are shown as function of operative frequency for different values of liquid loss tangent (3 × 10^{-5} and 1 × 10^{-4}) and depths (50, 100, 200, and 400 m).

Figure 6. Detection capabilities of the proposed system for different values of liquid loss tangent (3 × 10^{-5} and 1 × 10^{-4}) and depths (50, 100, 200, and 400 m) as function of operative frequency. Note that for shallow depths and low values of loss tangent (a) panel), Ka performs better than the other bands thanks to the higher SNR achieved from the increased antenna gain. For greater depths and larger values of loss tangent, the SNR at higher frequencies decreases due to the column liquid attenuation and lower frequencies are preferred.

The curves in Figure 6 are obtained by combining SNR, as calculated in Figure 3, and subsurface power return $P_{ss}$ according to the following formulation:

$$\frac{P_s}{P_{ss}}_{dB} = \Gamma_{s|dB} - (1 - \Gamma_{ss})^2_{dB} - \Gamma_{ss|dB} + K_{dB} + \frac{f_s}{fs}_{dB}$$

(14)

With

$$K_{dB} = 27 \cdot \tan \delta \cdot f \cdot \Delta \tau$$

(15)

where $\tan \delta$ is the loss tangent of the media, $f$ is the central frequency expressed in MHz, and $\Delta \tau$ is the two-way travel time expressed in microseconds and related to the depth by the follow:

$$\Delta \tau = 2d \cdot n / c$$

(16)

where $n$ is the index refraction of the media and $c$ is the speed of light.

Terms $\Gamma_{s|dB}$ and $\Gamma_{ss|dB}$ are the surface and subsurface reflectivity (in decibel) that are related to dielectric property $\varepsilon_r1$ and $\varepsilon_r2$ by the following:

$$\Gamma_s = \left| \frac{1 - \sqrt{\varepsilon_r1}}{1 + \sqrt{\varepsilon_r1}} \right| \quad \Gamma_{ss} = \left| \frac{\sqrt{\varepsilon_r1} - \sqrt{\varepsilon_r2}}{\sqrt{\varepsilon_r1} + \sqrt{\varepsilon_r2}} \right|$$

(17)
We can note that, for shallow depths and low loss tangent, the Ka system provides better performance thanks to the higher signal to noise ratio that was achieved as the frequency is increased (see Figure 3 panel (a)).

The two operative frequencies could be interlaced or selected according to the scientific target. Specifically, the quasi-simultaneous use of the two frequencies can be used to improve the estimation of liquid loss tangent from radar attenuation. Similar techniques that aim to estimate radar attenuation at different frequencies and for increasing depths have been also applied to Martian sounders data [86–88] as well as Cassini data [2,26,27]. The X band frequency could provide the detection of the sea floor of Kraken Mare, allowing for mapping the overall seabed topography of Titan’s seas. If Kraken has a similar loss tangent to Ligeia, the X band frequency would penetrate to depths of up to 800–900 m. Moreover, a three dimensional bathymetric map could be generated while using repeated passes observations, and the liquid attenuation could be estimated with a high accuracy at both frequencies and at different locations (both different lakes/seas as well as different locations within each lake/sea), allowing for the investigation of spatial and temporal variation of the liquid composition and depth. When combined with any radiometric measurements, the system could provide additional information regarding the dielectric properties of Titan’s liquid, as well as sea floor and the exposed solid surface [89,90]. A multilayer simulator [91] has been used to generate simulations for the proposed system in order to present how radar products would appear when observing Titan’s seas. Specifically, in Figure 7, a comparison between the radagrams of Ligeia Mare is shown that would be obtained by adopting the system parameters of the Cassini radar and those of the proposed architecture. Please note that loss tangent values that were adopted to generate Figures 6 and 7 are only indicative and reliable relationship of loss tangent as a function of frequency for any specific materials deserves further investigation by direct laboratory experiment.

![Figure 7](image.png)

**Figure 7.** (a) Simulation Ligeia Mare T91 observation. Loss tangent of the liquid has been set at $4 \times 10^{-5}$, $\varepsilon_1$ and $\varepsilon_2$ to 1.7 and 3.1, respectively. Subsurface roughness term $f_\text{ss}$ has been set to match observed radar amplitude. (b,c) Ka and X bands, respectively, simulations of T91 observation while using the proposed radar system.

Note that these simulations are not intended to capture the full characteristics of the radar echoes waveform (i.e., roughness and pulse-limited effects), but only to qualitatively show the effects of attenuation as frequency increases and the radar parameters are kept constant.
3.2. Tides Estimation Using Repeated Ground Tracks: Simulation and Results

Herein, we investigate tides amplitude estimation accuracy from radar data simulation. We simulate the radar response of the proposed system using a fractal surface and a facets based simulator [2]. Surface characteristics are chosen by taking into account the available information regarding Titan’s topography and the backscattering at each facets is represented via Hagfors scattering. Each overlap of ground tracks is simulated over a $4000 \times 100$ km surface, which represent the observed topography that was acquired from the pole to equator at true anomalies of 180 and 0 degrees. Tidal effects are included while using the model that was reported by [81], in which it allowed the vertical surface displacement to vary as a function of the latitude for a fixed longitude of 0 degrees. Figure 8a reports the result of the surface displacement due to tides. A PRF of 5 KHz, a 32 GHz Ka frequency, and a bandwidth of 50 MHz have been used to simulate 1330 bursts that were acquired along 4000 km surface. The same realization of the fractal surface is used twice, including tidal surface variation while assuming an $h^2$ equal to 1.45 and different values of horizontal baselines for the two adjacent ground tracks. In Figure 8b, we show the result of the application of an OCOG tracking algorithm [92] applied to the two products, in which blue and red indicate the first and second acquisition at opposite true anomalies and horizontal baseline of 2 km. It is possible to note that the effects of tides are already notable in the retrieved altimetry.

![Figure 8](image-url)

**Figure 8.** (a) Tidal surface displacement at opposite true anomalies 0 and 180 degree, and for latitudes varying from the Pole to the Equator at 0 degree of longitude. (b) Over plot of the result of OCOG algorithm applied to the first (blue) and second (red) repeated ground tracks. (c) Detected signal from repeated passes, 2 km adjacent ground tracks. In blue is the results of the OCOG algorithm, and in black is the cross correlation method. The red curve indicates the actual difference of the model.

We use two different methods for the estimating the Tidal Love number $h^2$ from synthetic data. While the first method uses the difference of the altimetry from the two passes while using the OCOG
algorithm, the second method exploits the knowledge of the offset between the two altimetry profiles, which were obtained by using the cross-correlation technique applied to the individual pairs of echoes (i.e., echoes of the two ground tracks at minimum distance). Figure 8c shows the detected tidal signal that was obtained while using the proposed methods. From our results, the cross correlation technique results are more accurate than the OCOG method, especially when the horizontal baseline (i.e., distance between the repeated ground tracks) is moderate, for example, less than 1 km for the proposed system.

The tidal Love number $h_2$ can be estimated while using a least square solution to solve the linear system that relates the observable tidal surface displacement to the Love number [82].

The results in Table 4 shows that estimation of $h_2$ can be performed with an accuracy of 0.1–0.2% from a single pair of repeated ground tracks when the cross-track separation is close enough to keep the received signal correlated. Table 4 shows the same scenario that we evaluated, except for varying the cross-track spacing between the two ground tracks and the RMS height of the simulated fractal surface.

Table 4. Accuracy of the estimate Love number $h_2$.

| $B_h$ [km] | $\sigma_H$ [m] | Mean OCOG | Err OCOG | Mean OCOG (%) | Err xcor | XCOR (%) |
|-----------|---------------|-----------|----------|---------------|---------|----------|
| 3         | 20            | 1.50      | 0.027    | 1.79          | 1.50    | 0.026    | 1.72     |
| 3         | 30            | 1.41      | 0.040    | 2.86          | 1.42    | 0.04     | 2.83     |
| 2         | 20            | 1.42      | 0.025    | 1.77          | 1.44    | 0.017    | 1.21     |
| 1         | 20            | 1.45      | 0.012    | 0.84          | 1.45    | 0.005    | 0.32     |
| 0.6       | 30            | 1.47      | 0.012    | 0.83          | 1.45    | 0.004    | 0.25     |
| 0.3       | 30            | 1.44      | 0.008    | 0.57          | 1.45    | 0.002    | 0.13     |

$^1$ xcor calculates shifts using cross-correlation of waveforms.

We can note that, for baselines smaller than 0.5 km, the Love number can be estimated within 0.2% of accuracy while only using a single pair of repeated orbits. Using only a few observations that were dedicated to the repeated adjacent track mode, this modeling shows that $h_2$ can be estimated to within the required accuracy that is necessary to characterize the density of the internal ocean ($\sim$0.1%). Similarly, when considering cross-overs, a distance that is smaller than 0.5 km and a number of them close to one-thousand is sufficient to allow for a very accurate estimate of Titan’s Love number.

4. Conclusions

The Cassini mission, and in particular its RADAR instrument, have revealed the presence of several geological features and landscapes which have greatly improved our understanding of Titan’s complex environment [93]. Here, we have described the design and the scientific motivation of a dual frequency radar system for the exploration of Titan seas and tides from a 1500 km circular orbit. The proposed system could provide new insights and help to answer the scientific questions that were raised during and after the Cassini mission [94]. The orbiter could provide information regarding the global composition and topography of the moon by combing data that were acquired from future in situ mission such as DragonFly, the robotic rotorcraft lander designed to explore Titan on 2034. The studies presented here have general validity and they could be used in the framework of terrestrial applications, as well as future missions. Specifically, tides are an object of interest for the exploration of the interior of the Galilean moons and the techniques presented here could be proposed for next coming missions, such as Europa Clipper and RIME [95]. Moreover, the bathymetry and composition studies reported here could benefit the interpretation of ground penetrating radars, which are becoming an attractive tool for the exploration of shallow terrestrial lakes and rivers [96].

Funding: This research was funded by NASA, grant number [80NM0018D004].

Acknowledgments: The author was originally supported by the Italian Space Agency. The author is grateful to Charles Elachi and Steve Wall for the fruitful discussions about the Cassini mission and the interpretation of RADAR data. The author would also thanks Marica Raguso, Valerio Poggiali and Alex Hayes, whose comments helped to improve the quality of this work.
Conflicts of Interest: The authors declare no conflict of interest. The funders had no role in the design of the study; in the collection, analyses, or interpretation of data; in the writing of the manuscript, or in the decision to publish the results.

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