Time resolved particle dynamics
in granular convection

J.M. Pastor\textsuperscript{a}, D. Maza\textsuperscript{a}, I. Zuriguel\textsuperscript{a}, A. Garcimartín \textsuperscript{a,}\textsuperscript{*}
J.-F. Boudet\textsuperscript{b}

\textsuperscript{a}Depto. de Física y Mat. Apl., Facultad de Ciencias, Universidad de Navarra, 31080 Pamplona, Spain
\textsuperscript{b}CPMOH, Université de Bordeaux I, 33405 Talence Cedex, France

Abstract

We present an experimental study of the movement of individual particles in a layer of vertically shaken granular material. High-speed imaging allows us to investigate the motion of beads within one vibration period. This motion consists mainly of vertical jumps, and a global ordered drift. The analysis of the system movement as a whole reveals that the observed bifurcation in the flight time is not adequately described by the Inelastic Bouncing Ball Model. Near the bifurcation point, friction plays an important role, and the branches of the bifurcation do not diverge as the control parameter is increased. We quantify the friction of the beads against the walls, showing that this interaction is the underlying mechanism responsible for the dynamics of the flow observed near the lateral wall.

\textit{Key words:} Granular flow, Convection
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1 Introduction

Granular convection is a patent example of how collective movement of grains can give rise to an ordered yet complex behavior. As soon as 1831, M. Faraday \cite{Faraday1831} reported a long range flow developed in a vertically shaken granular layer. This flow is called \textit{granular convection} because of the likeness between it and the movement of a liquid layer heated from below. Although many works have dwelt on this topic, the origin of this convective movement, and in particular

\textit{Email address:} angel@fisica.unav.es (A. Garcimartín).
the role of the lateral walls or the boundaries, is not fully understood. In 1989, P. Evesque and J. Rajchenbach [2] published an article where they showed experimentally that the threshold for collective motions to appear corresponds to the acceleration of gravity $g$. This is why the acceleration of the external driving is often given in the form of an adimensional number $\Gamma = \frac{A\omega^2}{g}$, where $A$ is the amplitude and $\omega$ is the frequency of the forcing. They also described that a heap grows changing the shape of the free surface of the medium, as a consequence of the grains circulating in a “convective” fashion.

Almost at the same time, C. Laroche et al. [3] reported both the importance of interstitial air for the deformation of the granular layer and the development of a compactation front that splits the layer into two zones, a solid one and a liquid one. The origin of convection, according to these authors, would be directly related to the air circulating among the grains. This effect determines the rising of material at the center of the layer and a flow of grains going down near the walls, which influence the material by increasing its porosity with respect to the central zone. Nevertheless, subsequent studies [4][5] have revealed that the walls can by themselves provide the driving force for convection, at least for a two-dimensional geometry. This point was finally demonstrated by the works of the Chicago group [6], who used NMR techniques to show that wall friction does affect the velocity profile of the particles. It should be noted that the shaking was conveyed in this case in the form of short pulses, or “taps”, separated by rest periods much longer than the pulse itself. At the same time, enlightening ideas were put forward, and tested numerically, setting the framework in which to understand the collective behavior of granular matter. Following an analogy with hydrodynamics, models were developed that qualitatively predicted the long range ordering of a shaken granular media, even though simplifications sometimes made them unrealistic [7] [8] [9][10].

Above the convective threshold, a granular layer can also undergo a rich array of instabilities. In 1989 S. Douady et al. [11] showed that beyond a certain value of $\Gamma$ the flight of the grains experiences a period doubling bifurcation, in a way essentially equivalent to a solid body that is placed on a vibrating plate [12]. As a layer of granular material is strongly dissipative, it can be considered perfectly inelastic, and its behavior as a whole can be modeled by an inelastic ball on a vibrating plate. This simple model, known as the Inelastic Bouncing Ball Model (IBBM) has been discussed by several authors [13][14][15] and successfully used to describe the temporal dynamics of a shallow granular layer (without convection) [16] as well as the dilation of a thick granular layer [17]. Moreover, as the system is spatially extended, it can also undergo spatial instabilities associated to the breaking of translational symmetries between different zones of the layer, that can oscillate with different phases [16].

More recently, it has been shown how the convective velocity field depends on
Fig. 1. Experimental set-up. A granular layer is vibrated by means of a shaker (S), which is in turn controlled by a function generator (FG). The acceleration is measured with an accelerometer (A). An oscilloscope (O) is used to monitor the instantaneous acceleration. The movement of the particles adjacent to the wall is recorded with a high-speed camera (C). The devices are controlled from a PC.

In this article we present an experimental study of the motion that a dense granular system develops when it is submitted to a vibration in the same direction than gravity. By detecting the time at which the layer collides with the shaking plate, flight times of the granular layer as a whole are measured, and the temporal bifurcations are described. At the same time, the movement of the particles near the container walls has been tracked with a high-speed recording system. By tracking the grains within an oscillation period, the friction effects caused by walls can be quantified and its influence on the global circulation is assessed.

2 Experimental set-up

Convection can be observed with almost any granular material, irrespective of shape, size or surface features. We have used glass beads with a diameter of 0.5 ± 0.1 mm, but we checked that sand gives the same qualitative results. The relative effect of cohesive forces (such as humidity or static charges) is important if the beads are much smaller than this. On the other hand, it is desirable to have as many grains as possible, and this particular size offers a good compromise. We put a big number of beads (typically of the order of $10^4$) inside a cylindrical box made of glass. The fact that both the beads and the box are of the same material reduces the amount of electrical charges created by friction. We also sprinkled the box with antistatic spray. The diameter of the box is 52 mm and it is high enough to avoid grains falling over when vibrated. This box is attached to a TiraVib 52100 magnetic shaker capable of delivering a sinusoidal acceleration of up to $15 \, g$ with a distortion smaller than 0.05 $g$. The shaker is commanded by a Stanford Research DS345 function generator. The vibration is characterized with an accelerometer attached to the box that has a
sensitivity of 100 $mV/g$, whose signal is picked by a Hewlett-Packard HP54510 digitizing oscilloscope. Both the oscilloscope and the function generator are connected to a PC. A sketch is provided in Fig. 1.

The frequency of the external vibration $f$ was kept constant at $f = 110$ Hz. We had previously found that the features of convection do not change qualitatively with frequency [18] provided that it is higher than 60 Hz. The acceleration was therefore changed by regulating the vibration amplitude $A$. The size of the granular layer is given in terms of the dimensionless height $N = h/\phi$, where $h$ is the thickness of the layer and $\phi$ the particle diameter.

We used a high-speed camera (Motionscope Redlake, model 1105-0003) with a macro lens and a VCR to record the movement of the grains at 1000, 2000 or 4000 frames per second. Under proper illumination, each glass sphere will reflect a bright spot that has been tracked with the following procedure. Once transferred to the computer, the movie was split into individual frames. A morphological image processing was performed on each frame to obtain the centroid of one bright spot in the first recorded frame. As the spheres budge less than one diameter from one frame to the next, the position of the bright spot is easily identifiable in the subsequent frame. Repeating the procedure for all the recorded frames and by tracking several beads, a set of grain positions versus time was obtained from each movie. Note that only spheres adjacent to the walls are accessible with this method, and we can only measure the velocity in the plane of the wall. An alternative method that has also been used, yielding the same results, is to calculate the correlation function between consecutive frames. In this case, the averaged velocity of all the beads in the frame is obtained.

3 Motion of the center of mass

Let us begin by describing the motion of the layer as a whole without considering the movement of the individual grains. Under this assumption, and considering the layer as a perfectly inelastic solid, its center of mass will begin to fly when its acceleration overcomes the gravity. From then on, the material will perform a free flight, and will lose all its energy when it collides with the plate. If the acceleration of the container is at that moment smaller than $g$, as in Fig. 2.a, the layer gets stuck to the container base until it departs from the base again when the acceleration exceeds the gravity. The layer spends therefore a time $\tau$ in the flight and a time $T - \tau$ (where $T$ is the period of the container oscillation) stuck to the container base in each cycle.

The flight time $\tau$ grows with $\Gamma$ until it reaches the value of oscillation period of the forcing $T$. If the granular layer is considered as a point mass, this
Fig. 2. Parabolic flight predicted by the Inelastic Bouncing Ball Model (top) and the acceleration measured by the oscilloscope for $\Gamma = 2.37$ and $N = 33$ (bottom). The collisions of the granular layer against the base of the container are evident in the signal from the accelerometer. The value of the acceleration equal to $-g$ is marked with a horizontal dotted line; the granular layer gets loose at this coordinate. Remarkably, the flight time measured in the experiment, $\tau$ suffers a phase delay with regard to the predicted by the IBBM. Take off and collision are marked with vertical dotted lines.

happens for $\Gamma = \sqrt{1 + \pi^2}$. At that point, the flight time undergoes a saddle-node bifurcation with the stable branch corresponding to a flight time $\tau = T$ [12]. This lasts until $\Gamma = \sqrt{4 + \pi^2}$, where a period doubling bifurcation takes place. Beyond that point, the particle can either perform a long flight (longer than $T$) or a short flight (shorter than $T$), depending on the container acceleration at the time of the collision. As $\Gamma$ increases, the long flight grows longer and the short flight shorter. Above $\Gamma = \sqrt{1 + 4\pi^2}$ only the long flight survives, and when it reaches the value $2T$ it bifurcates again.

The validity of this model to reproduce the interaction of the granular layer as a whole with the vibrating plate can be assessed by comparing its predictions to the experimental measurement of $\tau$ (see Fig. 2.b). In order to do this, we have taken the value predicted by the IBBM for the phase at the beginning of the flight: $\phi_i = \arcsin(1/\Gamma)$. There is no way to obtain this value from the acceleration signal, as the take off does not leave any trace on it. In principle this value is not prone to be affected by the friction between the grains and
Fig. 3. (a) Dimensionless flight time $\tau$ of the granular layer measured in the acceleration signal (*symbols*). When $\tau$ reaches $T$ the flight time undergoes a period doubling: a long and a short flight are performed every two cycles. The line indicates the values predicted by the IBBM. (b) The same data but now the solid line is a numerical simulation including the air effects (as in the Kroll analysis). This analysis improves the fit somewhat. The dotted line is the same than the solid one in (a).

the container or the presence of interstitial gas, because at take off the relative velocity between the granular layer and the vibrating plate is zero. The collision time can be obtained experimentally from the measured acceleration, as in Fig. 2.b. The flight times obtained in this way, subtracting the take-off times from the collision times, are displayed in Fig. 3.a along with the bifurcation diagram predicted by the IBBM. Clearly the model reproduces quite well the flight times of the center of mass for $\Gamma \lesssim 2.7$, as has already been demonstrated [17]. Above this value, the model is not valid anymore. The measured flight times are shorter than those predicted, and the bifurcation point is at $\Gamma = 4.8 \pm 0.1$. Beyond that point, the branches grow but eventually they seem to saturate. Another remark is that the system bifurcates directly from a monotonically growing solution to a period two solution, without showing the saddle-node bifurcation predicted by the model.

It is conceivable that one cause for this behaviour could be associated to the effects of the interstitial gas on the granular layer. The layer should then be considered as a porous medium whose porosity changes as it detaches from the base. A pioneering study of those dynamics has been done by Kroll [23] and refined by Gutman [24], who introduced air compressibility and a coupling with the porosity of the medium.

Let us introduce the hypothesis of Kroll (which is easier than Gutman’s to perform) in the numerical simulation of our problem. Considering the inelastic ball as a porous piston interacting with the air in the cell (a similar analysis has been recently reported for the case of granular segregation [25]), the numerical analysis of the flight time suggests that air effects on the systems should be measurable but ought not to change the dynamics (see Fig. 3.b), *i. e.* the
saddle-node bifurcation is still present (its range of stability is even increased) and the branches diverge as the flight time approaches $2T$.

In order to test the air influence on the flight time, we evacuated the container to $10^{-2}\text{Torr}$ and we collected data for the same range of $\Gamma$. Results are shown on Fig. 4.a. The agreement of measured data in vacuum with the IBBM is excellent up to $\Gamma \sim 2.3$, better than in the presence of air. Up to that value, flight times are a bit shorter if there is interstitial air. Nevertheless, above $\Gamma \sim 2.3$ the measured flight times do not fit to the IBBM even in vacuum. The bifurcation point is noticeably changed, even though it is still beyond the place predicted by the IBBM; the saddle-node bifurcation is neither observed. Beyond the bifurcation, the branches behave similarly in both cases (in vacuum and in air); a remarkable feature in vacuum is a region where flight times are bivaluated ($4.7 < \Gamma < 5$). It is interesting to note the similarity of the branches between them and the likeness to the branch before the bifurcation point; this will be analyzed elsewhere.

From the comparison of both curves (see Fig. 4.a), the one in air and the one in an evacuated container, it is evident that although air does affect granular convection, this is manifested basically in the location of the bifurcation point, that gets closer to the predicted by the IBBM. It is reasonable to think that a higher vacuum would lead to an even better agreement. But it still does not explain why the branches do not diverge and why the saddle-node bifurcation goes unobserved.
Another feature that is lacking in the model is the finite duration of the collision between the inelastic ball and the plate. The extent of this time is a considerable portion of the oscillation period \( T \), as can be appreciated in Fig. 4.b. This implies that the velocity of the center of mass at take off is not necessarily well defined. If the collision lasts for some time, it is reasonable to think that there is a delay that leads to a decrease in the initial velocity of the center of mass, and therefore to shorter flight times. This phenomenon is associated to the propagation of a shock wave front [26] that will be described elsewhere, and it has significant consequences for \( \Gamma > 3 \), when the duration of the collision becomes similar to the time that the granular layer spends stuck to the vibrating plate. For flight times shorter than 80% of the period, however, a finite collision time should not affect the flight time and we should search for another cause.

The key could be the interaction of the particles with the lateral wall of the container. Thus, the wall would exert an effective force on the inelastic ball larger than gravity that would affect not only the initial phase of the flight [5] (its effects on the initial velocity being negligible) but the acceleration during the entire flight as well, resulting in an effective force applied to the grains during the flight bigger than gravity. Assuming that this force is independent of the relative movement between the particles and the container wall, we can estimate its value by comparing the measured flight times with those predicted by the IBBM. We therefore introduce an effective control parameter such as \( \Gamma_{eff} = \frac{4\omega^2}{g_{eff}} \) which depends on an effective acceleration \( g_{eff} \) whose value is 10.6 \( m/s^2 \). This is the value that must be introduced in the IBBM in order to recover the measured flight time. This will be described in detail in the next section, where the movement of individual grains is dealt with.

4 The motion of individual grains

Till here we have described the motion of the granular layer as a whole. But there is motion in the frame of reference of the layer: the convective flow. Let us now study the movement of individual particles. The convective motion –it has been described previously [18],[6] – is much slower than the vibration, so it could somehow be expected that the motion of individual beads is a combination of flights similar to those of the IBBM coupled with a slow drift.

In our experiment we have tracked the position of individual beads near the lateral wall. The measurement have been performed near the surface, where the downward velocity peaks. The paths of the beads in the plane of the wall do not divert much from the vertical: azimuthal velocities are typically less than 10% of the vertical velocities. Note, however, that there can be motion in the radial direction; this component is not accessible in our experiment. Therefore
Fig. 5. The vertical position of a bead, tracked during about 10 cycles at 2000 samples per second. The container was being vibrated at $\Gamma = 2.59$ (a) and at $\Gamma = 5.81$ (b). The height of the layer was $N = 100$ in both cases. The origin of distances is arbitrary. Note the increasing in the drift velocity when $\Gamma$ grows.

we will restrict in the following to the vertical direction except when explicitly indicated.

The vertical position of a single bead at $\Gamma$ below and above the period doubling point is plot on Fig. 5. The beads roughly follow the same sort of movement described by the IBBM, with a conspicuous difference: there is a distinct drift downwards. We can consider the motion as consisting of two components: a fast one (the jumps at frequency $f$) and a slow one, which is the drift. The velocity of the latter (the convective motion) is about an order of magnitude smaller than the peak value of the former. Below $\Gamma \simeq 6$, we have observed that this configuration always forms a toroidal convective roll: the beads go down near the wall and they rise near the center of the container (see Fig. 6).

5 Friction against the walls

We are now able to discuss the origin of the downward movements near the lateral wall. The motion of a single particle has been shown to consist of a “fast” component (the jumps at the driving frequency $f$ or $f/2$) and a “slow” component (the drift giving rise to convection). Clearly, there must be some mechanism imposing a net shear on the grains in order to induce the flow depicted in Fig. 6. With the aim of investigating this subject, we took a closer look at the trajectories of the particles during each cycle.

A large number of trajectories of single grain flights recorded during one cycle, such as those displayed in Fig. 5, is shown in Fig. 7.a The common origin has been chosen as the moment when the particles collide with the base. Obvi-
Fig. 6. The convective velocity field at the top of the layer, near the lateral wall and at the bottom of the layer (from top to bottom; only part of the layer is represented.) Note the different scales. This figure corresponds to $N = 33$ and $\Gamma = 1.90$. The velocity field has been obtained by particle tracking at a small sampling rate (25 frames per second) effectively filtering out the rapid movement at the excitation frequency. The small crosses in the top and bottom plots mark the center of the container.

Ovaly, the measured positions of individual beads are too noisy to obtain clean paths. This is mainly due to the rearrangements of grains during the flight and to the fact that beads rotate. In order to regroup all the trajectories, the origin for all the paths has been arbitrarily chosen at the maximum of the flight. Near this point, almost all of the trajectories should have the same dynamics. We implemented an algorithm to find the maximum that chooses
Fig. 7. (a) The trajectories of many grain flights are plotted together. The origins of the positions are the places where velocity changes sign. The data corresponds to $\Gamma = 2.5$, a value of the forcing where flight times for an evacuated container and a container with air are the same. It is difficult to fit these data because of their dispersion.

(b) The same data, but now the maximum height has been chosen as the common reference. In order to relate them to the movement of the vibrating plate, the phase at the moment of collision has been adjusted to the experimental data (this point is marked with a star in the plot). From this phase, the experimental points have been displaced so their trajectories are tangent to the base at the beginning of the flight. The dotted line corresponds to the flight as predicted by the IBBM. Particles do reach a lower height, and they finally go down further than expected from a “free” flight. The difference $\Delta h$ divided by the oscillation period gives the velocity of the convective flow. The dashed line is a quadratic fit. Although the fit could be deemed good, the initial phase for the flight as obtained from the fit (arrow) does not coincide with $\Gamma = g$.

seven points around this zone an fits the trajectory to a parabolic flight, and then regroups all the trajectories using the calculated maximum as the reference. Using this method, the temporal coordinate where the particle touches the base has a lower dispersion. We use the mean value of these coordinates and the corresponding time determined from the oscilloscope to adjust the phase between the vibrating plate and the flights of the grains.

In figure 7.b we show the regrouped trajectories compared with the trajectory predicted by the IBBM. (We have displaced vertically the measured trajectories so that they are tangent to the plate oscillation). It seems clear that although the particles begin the flight for a phase almost equal to the one predicted by the IBBM, they finish the flight well below the position were they would land after a free flight. This difference, averaged for an oscillation period, is just the velocity of the slow drift giving rise to the convective flow [18].

From the comparison between the experimental data and the trajectory predicted by the IBBM it is clear that an acceleration larger than gravity is acting
on the particles (as can be seen in Fig. 7. b, this can be easily deduced because the heights reached in the flights, with the same initial condition, are rather different in the measured data and the IBBM). If this acceleration is constant during the flight time, the path of the particles in a space-time diagram should fit to a parabolic trajectory. We have fit a parabola, leaving all the parameters free except the maximum, which we have taken as a common origin for all the grains. This fit is shown in Fig. 7. b. The fit seems acceptable, and the effective acceleration during the flight would be \( g_f = 10.63 \pm 0.04 \text{ m/s}^2 \). This value matches the \( g_{eff} \) estimated from the flight times. Although the data are fitted reasonably well, the match is not completely satisfying. As stated above, the position of the maximum is fixed and then the acceleration and the initial velocity are free parameters of the fit. The value obtained for the initial velocity does not agree with the one predicted by the IBBM, and differs from the one that can be extracted from the data.

In order to improve the quality of the fitting, we have tried another approach by introducing a viscous dissipation which depends on the velocity of the grains. Then the ballistic trajectory of the grain will be modeled by the expression \( \ddot{z} + \gamma \dot{z} = -g_{\nu} \), where \( z \) is the position of the particle and \( \gamma \) represents the dissipative coefficient. The fit is shown in Fig 8.a. The value obtained for the initial velocity is in close agreement with the experimental data, and the value for the effective acceleration \( g_{\nu} = 12.77 \pm 0.07 \text{ m/s}^2 \) is larger than the obtained from the flight times. The dissipation can also be taken into account by introducing a term which depends on the relative velocity between the grains and the wall, so that \( \ddot{z} + b\dot{z} - g_{\nu} (\Gamma \sin(\omega t + \phi) - 1) = 0 \), with \( \dot{z} \) being now the relative velocity between the grains and the lateral wall. The fit is shown in Fig 8.b. The value obtained for the effective acceleration is now \( g_{\nu} = 11.9 \pm 0.1 \text{ m/s}^2 \). In both cases, the initial velocity is correctly reproduced.

It is not easy to choose which one of the fits is better. In any case, the introduction of a dissipation which depends on the velocity clearly improves the quality of the analysis, and the effective acceleration \( g_{\nu} \) that is found for the particles near the wall, where the trajectories of the grains have been tracked, is larger than the one found from the flight times for all the granular layer as a whole, \( g_{eff} \). Therefore, the difference between \( g_{eff} \) and \( g_{\nu} \) must be due to the wall-particle interaction. This difference between both values would amount to the net stress that the walls cause on the granular layer, thus imposing the downward flow near the wall.

A similar fit could be performed for the region after the period doubling (Fig. 5.b), but a better temporal resolution is needed.
Fig. 8. (a) The same data than in Fig. 7 but with a viscous dissipation that depends on the velocity of the grains included in the simulation. Now the fit (dot-dashed line) is better, and the initial phase for the flight is correctly predicted. The value obtained for the effective acceleration is now $g_ν = 12.77 \pm 0.07$ m/s$^2$. The dotted line corresponds to the IBBM.

(b) Same data than in (a) with a viscous dissipation proportional to the relative velocity between the grains and the lateral wall. The effective acceleration obtained from the fit is $g_ν = 11.9 \pm 0.1$ m/s$^2$.

6 Conclusions and discussion

From the analysis carried out we can conclude the following.

For $Γ \lesssim 2.7$ the Inelastic Bouncing Ball Model reproduces quite well the jumps of the granular medium as a whole, just as had been previously reported for the dilation of the upper layer [17]. Nevertheless, flight times are a little bit shorter than predicted by the model. We have verified that the cause for this is the interstitial air. When the container is evacuated, the agreement between the modified model and the measured data is excellent. We have therefore introduced in the model the interaction between air and the grains so that the agreement when there is air in the container is improved.

Above $Γ \sim 2.7$ the model is unable to faithfully reproduce the dynamics observed in the experiment. According to the model, the flight time should increase monotonically until a saddle-node bifurcation appears; then it should remain constant for a finite range of the control parameter. Afterwards it should suffer a period-doubling bifurcation. The saddle-node bifurcation has not been observed in our experiments. Besides, flight times are much lower than predicted both in the presence of air and in vacuum. The finite duration of the collision between the granular layer and the vibrating plate can be the cause for this discrepancy. A deeper study of this subject will be presented elsewhere.

The critical value for the control parameter where the period doubling bifur-
cation takes place is noticeably influenced by the presence of interstitial gas. For a moderate vacuum, such as the one reached in our experiment, the critical value of $\Gamma$ approaches the predicted one for an inelastic model but is still larger than it. Remarkably, flight times in vacuum below the bifurcation are almost indistinguishable from those measured in air. This suggests that the presence of air affects mainly the stability of the solutions for the flight times after the bifurcation.

Just above the period doubling bifurcation, the model fits quite well the branches if the container is evacuated. In air, the flight times are smaller than those predicted by the IBBM. In neither case, however, the divergence predicted by the model as $\Gamma$ grows larger is observed: flight times change slowly. This behaviour is probably caused by the finite duration of the collision as well.

Therefore, even though near the points where the solutions change (i.e. $\Gamma = 1$ and the period doubling bifurcation) the system can be modeled as a perfectly inelastic body, when the control parameter is increased there is a certain point where the model loses validity. Finite duration of the collision is suspected to be involved.

In this work we have focused in the region below the bifurcation point, where flight times in air and in vacuum are almost the same. From the study of the trajectories described by the particles near the lateral wall we have checked that they are subjected during their flight to a net force larger than gravity. A quadratic fit of the flight allows us to estimate the value of effective gravity, that agrees quite well with the one inferred from the measurement of the flight time. The quadratic fit implies a constant external force.

The quadratic fit, however, does not yield a correct value for the initial velocities (i.e. the velocities with which the grains take off when they begin the flight). In order to improve this, we have introduced a viscous dissipation. The trajectory is correctly reproduced, including the initial velocity. Remarkably, the value obtained for the effective acceleration is bigger than that obtained from the flight time measurements. The difference between both effective accelerations suggests that there is an extra force acting on the grains near the walls larger than the average over all the granular layer. This would be the cause of the downward movement near the walls that sets the sense of the convective flow.
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