Design and synthesis of bio-based UV curable PU acrylate resin from itaconic acid for coating applications

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ABSTRACT

UV curable PUA resin was successfully synthesized from polyol based on sustainable resource originated from itaconic acid (IA), isophorone diisocyanate (IPDI) and 2-hydroxyethyl methacrylate (HEMA). A polyol was synthesized by condensation reaction of IA with 16-hexanediol in the presence of p-Toluenesulfonic acid (pTSA). The synthesized PUA resin was characterized for its structural elucidation by using Fourier Transform Infrared Spectrophotometer (FTIR), \(^1\)H and \(^13\)C NMR spectroscopy. The synthesized UV curable PUA resin was incorporated in varying concentrations in conventional PUA coating system. The effects of varying concentration of synthesized UV curable PUA resin on rheology, crystallinity, thermal and coating properties were evaluated. The rheological behavior of the resins were evaluated at variable stress and result showed decrease in viscosity of resin as concentration of synthesized UV curable PUA resin increases in conventional PUA resin. The cured coatings have been evaluated for glass transition temperature (\(T_g\)) and thermal behavior by differential scanning calorimeter and thermogravimetric analysis respectively. The degree of crystallinity of the coatings was determined from X-ray diffraction patterns using the PFM program. It was found that increase in the mass proportion of IA based PUA in coatings, the coating becomes more rigid and crystalline. The synthesized UV curable PUA coatings showed interesting mechanical, chemical, solvent and thermal properties as compared to the conventional PUA. Further, cured coatings were also evaluated for gel content and water absorption.

1. Introduction

The coatings are widely used for various purposes such as decoration, protection, and some specific functions. The various types of polymeric resins such as epoxy, polyurethane, polyester and acrylate was used to formulate the coatings. To gain the application viscosity volatile organic chemicals (VOCs) are added in most coating formulations, which can be evaporated, and transport to atmosphere at ambient conditions. Such materials have been making many pollution risks such as: their ability to forming undesired photochemical ozone smog, and the potential to cause carcinogenic and mutagenic.[1,2] Environmental concerns and health related issue have stimulated researcher to develop environment friendly coatings with low or no VOC content.[3] To fulfill these requirements, researcher developed various type of coating such as high solid, water dispersible,[4] powder,[5] radiation (UV/EB) curing coatings.[6,7] Among them, UV-curing technology has been commonly used in various industrial sectors to achieve an ultrafast hardening of protective coatings, printing inks, adhesives, varnishes and composites. Compared with traditional thermal curing, UV-curing technology is becoming more and more acceptable for its various advantages, such as less organic solvent, shorter reaction time, lower energy consumption, and being environmental friendly and efficiency.[8,9]

Nowadays, UV-curable resins, such as epoxy acrylate, polyurethane acrylate (PUA), and acrylic resin, are available in the market. Among the various UV-curable resins, PUA has attracted great interest in the coatings and adhesives due to its unique properties, such as outstanding adhesion, excellent flexibility and chemical resistance. PUA resins are usually prepared by the reaction of a polyol with a diisocyanates to yield an isocyanate terminated oligomer and subsequently isocyanate terminated groups utilized to react with hydroxyl functional acrylic monomers incorporated the unsaturation at the end of the polymer backbone.[10]

Further, Fossil reserves are expected to deplete by the year 2050 if their present consumption rate continues.[11] For this reason, there is an increasing interest in the utilization of bio-based feedstock in both academic and
industry laboratories. The increasing worldwide interest for the use of sustainable resources is mainly due to the materials is derived from natural sources that are abundantly available. Their use would also contribute to global sustainability without depletion of limited resources. Also, sustainable resources are comparatively easy to handle with no or less toxicity and health related issues.[12,13] The increasing number of research studies devoted to the development of renewable resources based resins such as epoxy, polyester, polyurethane, Polyesteramide; reveals the great potential of renewable raw molecules and their ability to substitute for petrochemical-based materials. [14–20] In this context, many kinds of raw materials from renewable resources such as plant oils, rosins, terpenes, and sugars have been investigated as building blocks of polymeric materials.[21,22] Itaconic acid (IA) as a renewable material is attracting a lot of interest.[23] It is a white crystalline unsaturated dicarboxylic acid. IA produced by the fermentation of Aspergillus terreus from sugar is an efficient and promising diacid containing an active 11-disubstituted vinyl group.[23–25] The Aspergillus terreus is the most frequently used commercial producer of IA, several attempts also been made to find other microorganisms that are suited for efficient production of IA. Among the filamentous fungi, some ustilaginales species are known to produce IA. Because of its green synthetic procedure and great potential as a sustainable platform chemical and a building block for the production of polymers.[26] Former studies using IA as a starting material for polymeric materials mainly focused on two directions. One is the radical copolymerization of itaconate esters to prepare vinyl copolymers, and the other is the condensation polymerization of IA with diols to form polyesters.[27,28] The IA possessing two carboxyl groups and one carbon–carbon double bond, which has been proved to be suitable for the synthesis various resin for coating application. IA has also been reported as a potential raw material for synthesis various resin such as epoxy,[29] polyesteramine,[30] polyester,[27–31] polyamide.[32] A variety of biorenewable raw materials (such as vegetable oils, polysaccharides, natural rubbers, and their derivatives) is used for producing UV-curable coatings. Therefore, the combination of renewable resource and UV-curing method will provide us a ‘green+green’ strategy to prepare the thermosetting resins derived from biomass, which should have a bright future.

The aim of the present work was to utilize the IA to develop the UV curable PUA coating. The synthesis of IA based UV curable PUA resin was carried out in the two steps. The first step was the conversion of carboxylic group of itaconic acid in to the hydroxyl functional polyol via condensation reaction with 16 hexanediol in presence of pTSA catalyst. In second step, IA based polyol and excess IPDI react to prepare the NCO terminated PU prepolymer. Subsequently, NCO terminated PU prepolymer react with HEMA to incorporate the unsaturation at the end group. The developed resin was characterized for their physico-chemical and FTIR, $^1$H and $^{13}$C NMR spectroscopic analysis for structural elucidation. The synthesized UV curable IA based PUA resin incorporated in various concentrations into the conventional PUA. The effects of varying concentration of synthesized UV curable PUA resin on rheology, crystallinity, thermal and coating properties were evaluated. The synthesized UV curable PUA coatings showed interesting mechanical, chemical, solvent and thermal properties as compared to the conventional PUA.

2. Experimental

2.1. Materials

Itaconic acid [IA], 16-hexanediol, 4-methoxyphenol and para-Toluene sulphonic acid, 2-hydroxyethyl methacrylate and acetone were procured from SD Fine Chemicals Ltd. Mumbai, India. Isophorone diisocyanate was received from Bayer Materials Science Ltd., Mumbai, India. DIBUTYLTIN dilaurate (DBTDL, as the catalyst) was purchased from Amrut Industries Ltd Mumbai, India. PHOTOINITIATOR 2-Hydroxy-1-[4-4-[2-hydroxy-2-methyl-propionyl]-benzyl]-phenyl]-2-methyl-propan-1-one (IRGACURE® 127) was received from BASF, India. DIPROPYLENE glycol dialcyrate (Photomer® 4226) as reactive diluent was received from shepherd color company India.

2.2. Synthesis of itaconic acid based polyol (IAP)

IA (17.62 g, 135.4 mmol) and 16-hexanediol (32.01 g, 270.8 mmol) were charged into a round bottom four-necked flask equipped with a mechanical stirrer, a thermometer, a reflux condenser and a nitrogen inlet. The PTSA (0.5 mol% relative to itaconic acid) as the catalyst and MEHQ (0.5 wt% relative to the total weight of itaconic acid and 16 hexanediol) as the free radical polymerization inhibitor was added into the reaction flask. The reaction mixture was stirred and temperature was increased gradually up to 140 ºC in presence of N$_2$ atmosphere and progress of reaction was monitored by determining the acid value at regular interval of time. The reaction was stopped when acid value of reaction mixture reached below 10 mg of KOH per gram of resin. The synthesized IA based polyol was characterized for hydroxyl value, FTIR, $^1$H and $^{13}$C NMR analysis.

2.3. Synthesis of UV curable polyurethane acrylate resin

In the second step, 15.83 g (46.90 mmol) IA based polyol along with acetone (15 ml) were charged into the round
bottom flask under stirring in presence of \( \text{N}_2 \) gas inlet. After formation of homogenous mixture 0.1 wt% DBTDL and 21.93 g (98.67 mmol) IPDI mixed in acetone (10 ml) added dropwise under constant mechanical stirring. The reaction temperature was increased slowly up to 65 °C and maintained for next 3 h. The progress of reaction was monitored by FTIR analysis. The reaction was continued until the hydroxyl functional groups were completely consumed, it was confirmed by disappearance of the \( -\text{OH} \) peak from FTIR spectrum. Afterwards, 12.12 g HEMA (93.98 mmol) was added into the round bottom flask. The reaction temperature was maintained at 65 °C for next 4 h. The progress of reaction was monitor by FTIR analysis. The reaction was continued until peak corresponding to NCO functional group completely disappeared from FTIR spectrum. The reaction mixture was cool to room temperature and IA based UV curable PUA resin characterized for FTIR, \(^1\)H and \(^{13}\)C NMR analysis.

### 2.4. Formulation of UV curable PUA coating

The synthesized IA based PUA resin incorporated in various concentrations into the conventional PUA resin as shown in Table 1. The reactive diluent and photo initiator concentration kept constant in all formulations. The formulated coating was applied over the mild steel (MS) panels using bar applicator at 60-μm wet film thickness. The panels were cured by UV curing machine (UNIQUE UV Curing Machine, India) with the high-pressure mercury lamp (UV curing lamp Power 4 kW, wavelength: 30–400 nm) the exposure time was 20 s. The UV cured coatings were characterized for mechanical, chemical resistance, solvent resistance and thermal properties.

### 3. Characterization

#### 3.1. Physico-chemical analysis of resin

The acid value of IA based polyol was determined by the volumetric titration method according to ASTM D1980-87. The known quantity of resin sample dissolved in neutral butanol-toluene mixture and 3–4 drop of phenolphthalein indicator added, swirling gently and titrated against the 0.1 N alcoholic KOH solution. Equation (1) was used to determine the acid value of IA based polyol.

\[
\text{Acid value} = \frac{B \times N \times 56.1}{W}
\]

where \( B \) = Burette reading (ml), \( N \) = Normality of alcoholic KOH solution, \( W \) = weight of sample (g).

The hydroxyl value of IA based polyol was determined by acetic anhydride-pyridine method according to ASTM D4274-16. The calculation of hydroxyl value was done by using Equation (2).

\[
\text{Hydroxyl value} = \frac{(B - S) \times N \times 56.1}{W}
\]

where \( B \) = Burette reading for blank (ml), \( S \) = Burette reading for sample (ml), \( N \) = Normality of alcoholic KOH solution, \( W \) = weight of sample (g).

#### 3.2. Instrumentation

##### 3.2.1. FTIR analysis

The chemical structure of the IA based polyol, NCO-terminated PU prepolymer and PUA resin were identified by FTIR on a Bruker ATR spectrophotometer, USA. The spectra were observed in the 600 – 4000 cm\(^{-1}\) wavelength range.

##### 1\(^{\text{H}}\) and 13\(^{\text{C}}\) nuclear magnetic resonance spectroscopy

The supportive confirmation of chemical structure was given by \(^1\)H and \(^{13}\)C nuclear magnetic resonance (NMR) spectroscopy. \(^1\)H and \(^{13}\)C NMR spectra of the product were analyzed using Bruker DPX 800 MHz spectrophotometer with dimethyl sulphoxide (DMSO) as solvent.

##### Rheology

A rheometer (MCR 101, Anton Paar, Austria) with a parallel plat assembly was used to investigate the rheological behavior of the resins. Cone and plate rheometer (diameter: 25 mm, D-CP35-SN0) were separated by a distance of 0.5 mm during the rheological analysis. The rheological data analysis was performed using Rheoplus/32 V3.40 software supplied by the manufacturer. A temperature of 30 ± 0.5 °C was maintained constant during the rheological measurement.

##### DSC analysis

The glass transition temperature \( (T_g) \) of cured films was estimated using differential scanning calorimetry (DSC) TA Q100 analyzer (T. A. Instrument, USA). The film sample

| Code | PUA | IA based PUA | Reactive diluents | Photo initiator |
|------|-----|--------------|-------------------|-----------------|
| PUA  | 76  | 0            | 20                | 4               |
| PUA 1 | 56  | 20           | 20                | 4               |
| PUA 2 | 36  | 40           | 20                | 4               |
| PUA 3 | 16  | 60           | 20                | 4               |
| PUA 4 | 0   | 76           | 20                | 4               |
weighed accurately in aluminum pan and heated in 40 – 120 °C temperature range with heating rate 10 °C/min under nitrogen.

**Chemical resistance**

Chemical resistance property of the coatings performed according to the ASTM D-1308. The coated panel immersed in 5% w/w aqueous sodium hydroxide (NaOH) solution and 5% v/w hydrochloric acid (HCl) solution separately for 24 h at ambient temperature and its edges were sealed with adhesive tape. The coated panel was monitored for any visible defects like softening of film, blistering and separation of film from substrate.

**Solvent scrub resistance**

Solvent scrub resistance (ASTM D-4752) of coating was evaluated by using methyl ethyl ketone (MEK). Solvent scrub resistance of cured coatings was studied by rubbing the coating with a piece of white cotton saturated with solvent and maximum rubbing cycles were 200.

**Gel content**

Gel content of the cured coatings was determined by putting a known weight of coating sample (Wi) into xylene: DMF solvent (50: 50 by volume) for 24 h. Next day, a coating was removed from solvent and the residue dried in oven to achieve constant weight (Wr). Gel content calculated by using the Equation (3).

\[
\text{Gel content} = \frac{W_w}{W_d} \times 100
\]

where \( W_w \) = wet coating weight, \( W_d \) = dry coating weight

**Water absorption**

Water absorption of cured coatings was measured according to ASTM D-570. The cured coating was dried in oven until a constant weight achieved (\( W_f \)), then dipped into water at room temperature for 24 h. The coating film was removed from the water and dried with paper towel and weighed (\( W_i \)). Water absorption was calculated from the difference in the weights of the sample before and after soaking the water according to Equation (4).

\[
\text{Water absorption (\%)} = \left( \frac{W_i - W_f}{W_i} \right) \times 100
\]

where, \( W_f \) = weight of the sample after immersion in water. \( W_i \) = weight of the sample before immersion in water.

**Result and discussion**

**Physicochemical analysis**

UV curable PUA resin was synthesized from polyol based on sustainable resource originated from IA, IPDI and HEMA. UV curable PUA resin synthesis was carried out in the two steps. The progress of IA based polyol synthesis reaction was monitored by physicochemical analysis.
group. The FTIR spectrum in Figure 1(c) is for IA based UV curable PUA resin. The FTIR spectrum of PUA resin does not show the characteristic peak of –NCO at 2258 cm⁻¹. It indicates that all NCO groups react with the hydroxyl groups of HEMA and PUA resin is synthesized. The absorption peak at 810 cm⁻¹ illustrates that the acrylate C=C bond has been successfully incorporated at the end of PU acrylate resin chains. From above FTIR results, we conclude that IA based UV curable PUA resin is successfully synthesized.

**1H and 13C NMR analysis**

1H-NMR analysis of IA based polyol is shown in Figure 2. The signal obtained as multiplet at 1.33 and 1.58 ppm (G, H, I, J, 8H) could be attributed to the methylene protons of aliphatic chain. The sharp singlet at 2.18 ppm (k, 1H) corresponds to the proton of hydroxyl group; the absorption shift towards the downfield is due to the electronegative effect of oxygen atom. The multiplet signal at 3.96 ppm (C, 2H) and 3.34 ppm (D, 2H) correspond to the proton adjacent to carbonyl group of acid. The peak shift towards the downfield due to the deshielding caused due to electronegative effect of carbonyl group. The multiplet was assigned at 4.04 ppm (E, 2H) for the proton associating with a carbon atom near to the carbonyl group. The singlet corresponds to the vicinal bond of IA resonates at 6.16 ppm (A, 1H) and 5.77 ppm (B, 1H) that deshielded due to the movement of the electrons in the pi bond of the carbon–carbon double bond.[31] The 13C-NMR analysis of IA based polyol show in Figure 3. The two sharp peaks appear at 25 ppm (H, I) and 33 ppm (J) nearest to the TMS correspond to the carbon atom of aliphatic chain. There is absorption at 62 ppm (K) for the carbon of CH₂ that deshielded due to the adjacent hydroxyl group. There is absorption at 65 ppm (F) correspond to the carbon near to carbonyl group and shift towards down field in spectrum due to deshielded effect of carbonyl group. The peaks at 128 ppm (D) and 135 ppm (C) correspond to the double bonded carbon atom. The characteristic absorption peak that appears at extreme end of spectrum at 172 (A) and 166 ppm (B) corresponds to the carbonyl carbon of acid and ester respectively. Both of the carbon atoms appear at nearly same chemical shift value and they are highly deshielded. Thus from the 1H and 13C NMR spectrum data, we can confirm that IA based polyol resin is successfully synthesized. The 1H-NMR spectrum of IA based PUA resin is shown in Figure 4. The peak at 1.28 ppm is assigned to the cycloaliphatic protons. The triplet peaks at 3.95 ppm (E, 2H) and 4.10 (D, 2H) ppm are assigned for the CH₃ protons. The peak attributed at 6.04 ppm (A, 2H) and 5.60 ppm (B, 2H) are assigned to the protons of acrylate (CH=CH₂) which is the end group of PUA resin. The peak attribution of protons at the down field is due to the movement of the electrons.
Figure 2. $^1$H-NMR analysis of IA based polyol.

Figure 3. $^{13}$C-NMR analysis of IA based polyol.
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The lower viscosity of resin will undoubtedly play a positive role in improving its overall performance as final coatings. The chain structure and molecular structure of a polymer determine its rheological properties.[35] The rheological behavior of conventional PUA, PUA1, PUA2, PUA3 and PUA resins at variable shear rate is studied and results are in Figure 6. From Figure 6, increase shear rate does not show any change in the viscosity of conventional PUA, PUA1, PUA2 and PUA3 resin. In addition, viscosity of PUA4 resin is found to be lowest as compared to the conventional PUA, PUA1, PUA2 and PUA3 resin. From above study, we conclude that viscosity of conventional PUA resin drop dawn, as IA based PUA resin concentrations increase.

5. Coating characterization

DSC analysis

The $T_g$ of UV cured coatings was determined by DSC analysis and it is shown in Figure 7. The DSC analysis shows the $T_g$ (midpoint) of PUA, PUA1, PUA2, PUA3 and PUA4 values as 52.97, 59.32, 60.49, 61.77 and 62.03 °C respectively. The dense cross-linked structures have higher value of $T_g$ than less cross-linked cured coating. The crosslink density depends on the functional groups present in molecules.
UV curing as compared to the conventional PUA resin. Therefore, UV cured IA based PUA coatings have higher crosslink density compared with the conventional PUA and more the functional groups present in the resin backbone the higher the cross-linked structure.\cite{36,37} IA based PUA resin has one extra reactive site in the backbone for UV curing as compared to the conventional PUA resin. Therefore, UV cured IA based PUA coatings have higher crosslink density compared with the conventional PUA.

**Figure 5.** $^{13}$C-NMR analysis IA based PU acrylate.

**Figure 6.** Rheology study of PUA, PUA1, PUA 2, PUA 3 and PUA 4 resins.
weight% (char yield) at 700 °C are listed in Table 3. As shown in Figure 8, \( T_{d5} \) temperature of the cured coatings decreased from 331.67 °C for PUA to 280.33 °C for PUA4. Thermal stability of the UV cured PUA coatings are characterized by the statistic heat-resistant index temperature \( T_s \). The temperatures at 5% \( (T_{d5}) \) and 30% weight loss \( (T_{d30}) \) of the cured coating obtained in thermogravimetric analysis is used to calculate the \( T_s \) (Equation (5)). The calculated value of statistic heat-resistant index \( T_s \) of cured coating. In addition, the resulting urethane linkages also contribute to compact network through intermolecular hydrogen bonding which would also reduce the chain mobility of final structure and increase the \( T_g \) significantly. Hence, it is observed that \( T_g \) of the UV cured PUA coatings shifted to the higher value with the IA based PUA concentration increased into the coating. It may be due to the IA based PUA coatings formed dense cross linked structure than conventional PUA coating.

**TGA analysis**

Thermogravimetric analysis (TGA) method was used to study the changes in physical and chemical properties of materials as a function of increasing temperature. TGA analysis of cured coating is shown in Figure 8. Thermal degradation of PU is a very complex mechanism due to variety of products formed in the process that are indicative of the complexity of the degradation process. Thermal stability of UV cured PUA coatings mainly depends upon the number of hard and soft segments present in the final structure. The urethane linkages (–NH–COO) and structure of isocyanate used for curing are responsible for the hard segment while long alkyl chains of polyols presents soft segments in the final cured structure.[38] The values of 5 wt% \( (T_{d5}) \), 30 wt% \( (T_{d30}) \) loss degradation temperature and residual weight% (char yield) at 700 °C are listed in Table 3. As shown in Figure 8, \( T_{d5} \) temperature of the cured coatings decreased from 331.67 °C for PUA to 280.33 °C for PUA4.

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Gel content

The gel content of UV cured coatings was evaluated in methyl ethyl ketone (MEK) solvent for 24 h and result shown in Figure 10. The gel contents of PUA, PUA1, PUA2, PUA3 and PUA4 coatings are 98.63, 98.78, 98.95, 99.12 and 99.39 respectively. The results show that gel content of UV cured coating increase as the concentration of IA based PUA resin increase. The gel content is correlated to the crosslinked structure of cured coating film.[41] The cross-linked density of coating is related to the number of reactive sites present in the resin structure and more IA based PUA coatings have lower value than cured PUA coating.

\[ T_s = 0.49 \left[ Td5 + 0.6 \left( Td30 - Td5 \right) \right] \tag{5} \]

where \( T_s \) = statistic heat-resistant index temperature

The char yield value at 700 °C for PUA, PUA1, PUA2, PUA3 and PUA4 coatings are 3.51, 3.35, 3.99, 4.02 and 4.78 respectively. The coating degradation temperature not only has a relationship with the chemical structure of the network, it also has close ties with crosslink density of the network. The cross-linked density of coating increases with functional group and high cross-linked network has high thermal stability.[39] IA based PUA resin have more unsaturation in the backbone as compared to the conventional PUA resin and form more crosslinked structure when passed through the UV lamp. This higher cross linking density of IA based PU coating may be enhancing the thermal resistance properties. From TGA analysis study revealed that as the IA based PUA resin concentration increased in PUA coatings, thermal stability increase.

**XRD analysis**

The degree of crystallinity of the coatings was determined from XRD patterns using the PFM program. The 2θ scan range was 5–50°, because all the intense crystalline peaks are found in this range. The X-ray pattern of the UV curable PU coatings is shown in Figure 9. The XRD patterns of PUA coating exhibits broad peaks at about \( 2\theta = 15^\circ \) and \( 18^\circ \), indicating some degree of crystallinity. These peaks are assigned to the scattering from PUA chains with regular interplanar spacing. The peaks intensity at about \( 2\theta = 15^\circ \) and \( 18^\circ \) is increase as the mass proportion of IA based PUA resin increases. The determined percent crystallinity of PUA, PUA1, PUA2, PUA3 and PUA4 coatings from XRD analysis is 3.44, 3.62, 4.15, 5.24 and 6.79 respectively (Table 4). IA based PUA resin has one extra reactive site in the backbone for UV curing as compared to the conventional PUA resin and hence, higher crosslink structure formed compared to the conventional PUA coating.[40,41] Thus, as concentration of IA based PUA resin increase into the coatings, the coating becoming more rigid and crystalline.

### Table 3. Thermo gravimetric analysis of PUA, PUA1, PUA2, PUA3 and PUA4 coatings.

| Coatings | 5% (°C) | 30% (°C) | Ts (°C) | Residues at 700 °C |
|----------|---------|----------|--------|-------------------|
| PUA      | 331.67  | 418.00   | 204.82 | 3.51              |
| PUA1     | 318.00  | 410.00   | 200.90 | 3.35              |
| PUA2     | 294.00  | 407.00   | 199.43 | 3.99              |
| PUA3     | 287.00  | 400.00   | 196.00 | 4.02              |
| PUA4     | 280.33  | 389.00   | 190.61 | 4.78              |

### Table 4. Percent crystallinity of PUA, PUA1, PUA2, PUA3 and PUA4 coatings.

| Coatings | Crystallinity (%) |
|----------|-------------------|
| PUA      | 3.4475            |
| PUA1     | 3.6229            |
| PUA2     | 4.1554            |
| PUA3     | 5.2454            |
| PUA4     | 6.7993            |

**Table 3.** Thermo gravimetric analysis of PUA, PUA1, PUA2, PUA3 and PUA4 coatings.

**Table 4.** Percent crystallinity of PUA, PUA1, PUA2, PUA3 and PUA4 coatings.

**Figure 9.** XRD patterns of PUA, PUA1, PUA2, PUA3 and PUA4 coatings.

**Figure 10.** Gel content of PUA, PUA1, PUA2, PUA3 and PUA4 coatings.

**Gel content**

The gel content of UV cured coatings was evaluated in methyl ethyl ketone (MEK) solvent for 24 h and result shown in Figure 10. The gel contents of PUA, PUA1, PUA2, PUA3 and PUA4 coatings are 98.63, 98.78, 98.95, 99.12 and 99.39 respectively. The results show that gel content of UV cured coating increase as the concentration of IA based PUA resin increase. The gel content is correlated to the crosslinked structure of cured coating film.[41] The cross-linked density of coating is related to the number of reactive sites present in the resin structure and more
the reactive sites higher is the cross-linking density. IA based PUA resin have more reactive sites in the structure as compared to the conventional PUA resin. Therefore IA based PUA coatings formed have more crosslinked structure when cured through the UV irradiation lamp. The penetration of solvents in UV curable IA based PUA coating become difficult. All the coatings show gel content over 98% and confirm that coatings have excellent curing.

**Water absorption**

The behavior of coatings towards water is a most important property of coatings and which can determine their end application. The water absorption test was performed to evaluate the migration of water in cured coatings. The coatings were immersed in water for 24 h and the result is shown in Figure 11. The water absorption of UV curable PUA, PUA1, PUA2, PUA3 and PUA4 coatings is 0.95, 0.92, 0.87, 0.85 and 0.80 percents respectively. PUA4 coating show less water absorption than any other coating and it attributed to the highly cross-linked network. In addition, the water absorption of polymers is directly related to their free volume fraction and also to the presence of resin backbone. IA based PUA4 coating has aliphatic carbon chain backbone which not form any type of bond with water molecules and less free space for water absorption. Hence, IA based PUA4 coating has less affinity towards the water (Schemes 1 and 2).

**Chemical resistance**

The cured coatings were immersed in 5% HCl and 5% NaOH solution for 24 h to evaluate the chemical resistance properties. It was observed for loss of gloss or adhesion after the completion of test. The acid and alkali test show no damages to the coating while both test show slight reduction in gloss. All UV cured PUA coatings are form highly crosslinked structure by reacting the unsaturation in UV irradiation and hence, coatings has resistance towards the acid and alkali. In addition, PUA coatings have polar N–H groups present in the backbone that creates hydrogen bonding in it or with other molecules and that can be considered effective physical barrier to acid and alkali solution.

**Solvent resistance**

The solvent rub test conducted using methyl–ethyl ketone (MEK) and results revealed that the UV curable PUA coatings are sufficiently cross-linked. The high cross-linked networks have high resistance to the solvent rub and polar N–H groups of PUA coatings create a hydrogen bonding in it or with other molecules that enhance the solvent
rub resistance properties.[42] From above study, it is concluded that all UV curable PUA coatings form sufficiently strong cross-linked network to resist the solvent.

**Mechanical properties**

The UV curable PUA coatings are characterized for various mechanical properties and results are tabulated in Table 5. Scratch hardness tester checked the hardness of coatings and we observe excellent scratch hardness for UV curable conventional PUA and IA based PUA coatings. IA based PUA4 coating show better hardness properties as compared to the PUA, PUA1, PUA2 and PUA3 coatings. The observed results can be correlated to the cross-linked structure and strong crosslinking network which give good hardness properties.[41] IA based PUA resin have more reactive sites in the structure as compared to the conventional PUA resin and IA based PUA

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**Table 5. Mechanical properties of the UV-cured PUA coatings.**

| Properties            | PUA | PUA1 | PUA2 | PUA3 | PUA4 |
|-----------------------|-----|------|------|------|------|
| DFT (micron)          | 50–60 | 55–60 | 50–60 | 50–55 | 50–60 |
| Gloss (60°)           | 112.2 | 104.9 | 101.2 | 102.3 | 101.4 |
| Cross-cut adhesion    | Pass | Pass | Pass | Pass | Pass |
| Pencil hardness       | 4H   | 4H   | 5H   | 6H   | 5H   |
| Scratch hardness (g)  | 2100 | 2250 | 2200 | 2250 | 2350 |
| Impact resistance     | 112  | 112  | 112  | 112  | 112  |
| Flexibility (mm)      | 0    | 0    | 0    | 0    | 0    |

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**Scheme 2.** Synthesis route for UV curable PUA resin.
coatings form more crosslinked structure when undergoes UV curing. Hence, PUA4 coating showed high hardness value as compared to the PUA, PUA1, PUA2 and PUA3 coatings. All coatings show pencil hardness above 4H and this is due to the high crosslinking as discussed above. Coating adhesion with metal substrate was determined by crosscut test. The coatings show 100% adhesion to the metal substrates as measured by the cross-cut adhesion method. The UV curable PUA coatings have polar N–H groups present in the molecules that create hydrogen bond with metal substrate and improve the adhesion properties. Further, the flexibility of PUA, PUA1, PUA2, PUA3 and PUA4 coatings are observed to be excellent with no crack development during testing on conical mandrel apparatus. This can be attributed to the presence of long aliphatic chains and polar N–H groups along the chain length of PUA resin that creates hydrogen bonding in it or with other molecules.[42] In impact resistance test, all coatings have given good response to the high-speed load for intrusion impact test. This is due to the excellent balance maintained between the softer segments of long aliphatic chains of PUA and the hardness offered from high cross-linked structure of UV cured coatings. For extrusion impact test, all PUA coating show poor results as compared to the intrusion impact test. From the above study, UV curable IA based PUA coatings have shown better performance for all mechanical properties as compared to the conventional PUA coating.

6. Conclusion

The UV curable PUA resin is successfully synthesized from bio-based IA by simple condensation reaction in presence of pTSA catalyst. The IA based UV curable PUA resin synthesis is characterized by physicochemical analysis and further confirmed by FTIR, 1H and 13C-NMR spectroscopy. The synthesized IA based PUA resin incorporated in various concentrations into the conventional PUA and their effect on coating properties was studied. The DSC and TGA analysis show that thermal properties improve as concentration of IA based PUA resin increase in conventional PUA coatings. From XRD analysis, it is found that as concentration of IA based PUA in coatings increase; the coating becomes more rigid and crystalline. The UV curable IA based PUA coatings shows better mechanical, chemical resistance and solvent resistance properties as compared to the conventional PVA. From the above study, it is concluded that IA based UV curable PUA coating is good alternative to conventional PUA coating.

Disclosure statement

No potential conflict of interest was reported by the authors.

Funding

The work was supported by BRNS, DAE.

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