TITLE:
Anionic polymerization using flow microreactors

AUTHOR(S):
Takahashi, Yusuke; Nagaki, Aiichiro

CITATION:
Takahashi, Yusuke ...[et al]. Anionic polymerization using flow microreactors. Molecules 2019, 24(8): 1532.

ISSUE DATE:
2019-04-18

URL:
http://hdl.handle.net/2433/241256

RIGHT:
© 2019 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (http://creativecommons.org/licenses/by/4.0/).
Anionic Polymerization Using Flow Microreactors

Yusuke Takahashi and Aiichiro Nagaki *

Department of Synthetic Chemistry and Biological Chemistry, Graduate School of Engineering, Kyoto University, Nishikyo-ku, Kyoto 615-8510, Japan; takahashiy@sbchem.kyoto-u.ac.jp
* Correspondence: anagaki@sbchem.kyoto-u.ac.jp; Tel.: +81-75-383-2729; Fax: +81-75-383-2727

Academic Editors: Maurizio Benaglia and Miquel A. Pericàs
Received: 28 March 2019; Accepted: 16 April 2019; Published: 18 April 2019

Abstract: Flow microreactors are expected to make a revolutionary change in chemical synthesis involving various fields of polymer synthesis. In fact, extensive flow microreactor studies have opened up new possibilities in polymer chemistry including cationic polymerization, anionic polymerization, radical polymerization, coordination polymerization, polycondensation and ring-opening polymerization. This review provides an overview of flow microreactors in anionic polymerization and their various applications.

Keywords: flow synthesis; anionic polymerization; styrene; alkyl methacrylate; block copolymer; end functionalized polymer

1. Introduction

A microreactor is a flow-type chemical reaction device, which typically consists of micromixers and microtube reactors at a micrometer scale. A number of significant chemical conversions have been conducted in flow microreactors and have received significant research interests from both academia and industry [1–25]. Recent studies identified unique characteristics of flow microreactors, which allowed many challenging, or even impossible, organic syntheses in macro-type batch reactors to be successfully performed. In a flow microreactor system, the selectivity of a chemical reaction can be dramatically improved by fast mixing and efficient heat transfer, which are derived from short diffusion paths and high surface-to-volume ratios, respectively [26–29]. Likewise, short residence time in a microchannel enabled extremely unstable intermediates to be used in numerous useful chemical reactions [30–46]. Moreover, the use of flow microreactor system is quite effective from the viewpoint of the improvement of some safety due to smaller reaction volume and higher surface to volume ratio compared to batch reactors. Collectively, these features of flow microreactor systems have opened up new possibilities for various chemical reactions for organic synthesis [47–57].

Applications of flow microreactors appear to be particularly promising in polymerization in which a series of repeated chemical reactions turns small monomers into chain-like polymers. The reviews on various polymerization methods performed in microreactors were published by Hessel et al., Wilms et al., Mcquade et al., Serra et al., Frey et al. and Junkers [58–65]. The main purpose of this review is to provide a brief up-to-date overview on applications of flow microreactors for anionic polymerization with the insight into industrial use; therefore, the paper focuses on synthetic research rather than theoretical research.

2. Characteristic Features of Flow Microreactors

Flow microreactors can influence the very essence of chemical reactions because of the characteristic features derived from having small flow-type structures.

(1) Fast mixing [66,67]: With highly active reagents, a reaction is initiated immediately after mixing solutions; therefore, it is crucial to reach solution equilibrium quickly to ensure proper control
over such reaction. Mixing occurs due to molecular diffusion. Theoretically, the time required for molecular diffusion is proportional to the squared length of the diffusion path. Having a much shorter diffusion path, a microreactor can achieve a mixing rate which is not achievable in a macroreactor. The working principle of a typical micromixer (a multilamination-type micromixer [68]) is shown in Figure 1. The solution 1 and the solution 2 are divided into flow segments with small width by a microstructure. Efficient and fast mixing, owing to short diffusion paths, takes place at the interfaces of the flow segments.

![Figure 1. Working principles of a multilamination-type micromixer.](image)

(2) Temperature control: Heat is transferred between the interior and exterior of a reactor through the reactor surface; therefore, the surface area per unit volume of the reactor is a major factor that ensures excellent heat transfer. Volume is equal to the cubed length of a reactor and surface area is equal to the squared length: the shorter the length, the higher the surface-to-volume ratio. When compared micro spaces to macro spaces, the former generally have much larger surface-to-volume ratios (Figure 2). Hence, heat transfer occurs more rapidly in a flow microreactor, enabling fast cooling/heating and precise temperature control.

![Figure 2. Numerical aspects of decreasing size. Effect of downsizing reactor on surface-to-volume ratio.](image)

(3) Residence time control: The time duration during which a solution remains inside a reactor is called the residence time. In flow reactors, the residence time increases with the length of the channel and decreases with the flow speed. By shortening microchannel lengths, the residence time in flow microreactors can be greatly reduced. Extremely short residence time allows reactions involving unstable short-lived reactive intermediates to be precisely controlled. Unstable reactive species can be transferred to another location for the next reaction before they decompose (Figure 3). By taking
advantage of this feature, chemical transformations that are very difficult or impossible in macroreactors can be achieved in microreactors [69–72].

Figure 3. Principle of generation and reaction of unstable short-lived reactive intermediates based on residence time control in a flow microreactor.

3. Living Anionic Polymerization

3.1. Controlled/living Anionic Polymerization of Vinyl Monomers

Living anionic polymerization has been one of the most important reactions for polymer synthesis since it was first reported by Michael Szwarc in the 1950s [73–81]. The nature of anionic polymer ends, being chemically active with no capping agent, makes this polymerization method especially powerful by utilizing these ends for various complex polymer syntheses such as end-functionalized polymers, block copolymers, star polymers and graft copolymers [82–85]. In addition, living anionic polymerization is considered to be more ideal than radical polymerization because the former, requiring no termination and chain transfer reaction, usually results in lower polydispersity index (PDI = Mw/Mn). However, the anionic polymerization has been performed under strictly dehydrated conditions since an anionic living polymer end is very sensitive to moisture. This requirement of reaction condition greatly hinders industrial application. In addition, cryogenic condition, such as $-78 \, ^\circ \text{C}$, is required when anionic polymerization is performed in polar solvents with batch macro reactors [86]. In terms of industrial application, the usefulness of the polymerization is deteriorated by such requirement. On the other hand, with nonpolar solvents, the polymerization can be carried out at higher temperatures but much longer reaction time is needed for completion. Despite the aforementioned restriction, a number of remarkable advancements have been made on polymer synthesis by living anionic polymerization performed in flow systems. In fact, the kinetic studies on anionic polymerization in a continuous flow have been reported by Szwarc and Schulz et al. [87,88] and Lochmann and Muller et al. [89,90]. This polymerization strategy continues to expand the possibility of living anionic polymerization using flow microreactor systems and to innovate a way of developing functional materials in the field of polymer chemistry.

3.2. Controlled/living Anionic Polymerization of Styrenes in Polar Solvent Using Flow Microreactor Systems

Anionic polymerization of styrenes is a very useful technique for polystyrene synthesis because the polymerization can be modulated to produce polymers with accurately targeted molecular weights (Mn) and molecular weight distributions (Mw/Mn). The polymerization is applied for the synthesis of structurally well-defined polymers such as end functionalized polymers and block copolymers [91]. With a polar solvent, batch microreactors should only be performed under cryogenic conditions such as $-78 \, ^\circ \text{C}$ to control the reactivity. On the other hand, flow microreactors can be used under much milder conditions such as $0 \, ^\circ \text{C}$ as reported by Nagaki and Yoshida [92]. Solutions of styrene in tetrahydrofuran (THF) and s-BuLi (in hexane) were mixed in a T-shaped micromixer M and the polymerization occurred in a microtube reactor R. The reaction was quenched by MeOH at the reactor outlet, resulting in
polystyrene with a narrow molecular weight distribution (Mn = 1200–20,000, Mw/Mn = 1.09–1.13) (Figure 4). Polymer synthesis of narrower molecular weight distribution would be achieved by further purification of reagents and/or their effective mixing, although no such results are reported.

Highly controlled polymer dispersity was due to two factors: precise control of the initiation reaction by the fast mixing of initiator and monomer and the speedy removal of reaction heat by precise temperature control. Moreover, the molecular weight was also easily controlled just by changing the flow rates of monomer and initiator solutions. Furthermore, this method can be applied for various styrene derivatives having silyl, methoxy, alkynyl and alkylthio groups on the benzene ring. Löwe and Frey also reported anionic polymerization of styrene at 20 °C using a flow microreactor [93]. Their method successfully produced polystyrenes having a broad range of molecular weight within several seconds while the molecular weight distributions were narrow (Mn = 1700–70,000, Mw/Mn = 1.09–1.41). In addition, the flow microreactor allowed the polymerization to be performed under more easily attainable conditions, reducing/eliminating the need for strict dryness of apparatus and high vacuum techniques in batch macro reactors. In a flow system, residual impurities and moisture can be removed just by running monomer and/or initiator solution through a reactor before a desired polymer product is collected at the reactor outlet. Löwe and Frey reported another flow microreactor application, anionic polymerization of 2-vinylpyridine (2VP) (Figure 5). When performed in batch macro reactors, the polymerization needs inorganic salts such as lithium chloride to control the reaction. However, the reaction can be quenched in a timely manner by precise residence time control so that it prevents carbanionic living polymer ends from reacting with electron-poor pyridine ring [94,95].
Syntheses of complex polymers can be performed by integrating several flow microreactors. In other words, a multistep reaction of structurally well-defined polymers such as end-functionalized polymers and block copolymers can be conducted in one go just by putting several micromixers and microtube reactors together while effectively utilizing the livingness of polymer ends. For example, polystyrenes with silyl group at their terminals were generated by functionalizing living polymer ends with chlorosilanes such as chlorotrimethylsilane and chlorodimethylvinylsilane [92]. The block copolymers composed of two different styrenes were also synthesized in quantitative yields at 0 and 24 °C in the integrated flow microreactor system (Figure 6).

Another effective strategy for complex polymer synthesis is the functionalization of anionic living polymer ends with epoxides, which have high reactivity toward nucleophiles because of ring strain. Use of functionalized epoxides enables a further transformation. For example, the use of flow microreactors allowed various functionalized polymers to be readily generated by the following procedures: polymerization of styrene and end-functionalization with the various glycidyl ethers having acetal structures such as ethoxy ethyl glycidyl ether (EEGE), 1,2-isopropylidene glyceryl glycidyl ether (IGG) and 2-phenyl-1,3-dioxane glycidyl ether (PDGE) (Figure 7) [96]. The acetal and ketal protecting groups in the glycidyl ethers are stable toward the highly reactive carbanionic living polymer ends but they can be easily cleaved under acidic conditions to afford multi-hydroxyl end-functionalized polymers (Figure 8).

**Figure 6.** The integrated flow microreactor system for poly(styrene)-block-poly(styrene derivatives) synthesis in THF. M1, M2: micromixer; R1, R2: microtube reactor.

**Figure 7.** A flow microreactor system for anionic polymerization of styrene in THF initiated by s-BuLi and subsequent functionalization reaction with epoxides. M1, M2: micromixer; R1, R2: microtube reactor.
Living anionic polymerization has been also utilized for syntheses of complex branched polymers, including star polymers and dendrimer-like star-branched polymers. Having unique and interesting properties in solution and also in liquid and solid state, these branched polymers have attracted much attention from theoretical, synthetic and practical points of view. Among them, block copolymers having different polymer chains on a core are especially interesting. To synthesize such a structure, at the first step, only one polymer chain has to be selectively introduced to a core molecule, which has multiple reaction sites. In a batch macro reactor, an excess amount of multifunctional core is necessary to prevent the formation of multi adducts, requiring one extra step of separating unreacted core before proceeding to the next step [97–99]. A flow microreactor can effectively solve this problem by suppressing the disguised chemical selectivity [100–111]. As shown in Figure 9, the end-functionalization with one equivalent of dichlorodimethylsilane leads to the selective formation of a product that has a single polymer chain on silicon (Mn = 1400, Mw/Mn = 1.13) while the use of a batch macro reactor results in lower controllability (Mn = 1300, Mw/Mn = 1.21). Extremely fast 1:1 micromixing of the living polymer chain and dichlorodimethylsilane enables the selective introduction of a single polymer chain into silicon. Therefore, the subsequent reaction with another living polymer chain using an integrated flow microreactor system gives block copolymers having two different polymer chains on a silicon core. Based on the present method, more complex macromolecular structures such as miktoarm stars, star block copolymers and block graft copolymers would also be effectively synthesized.

Figure 8. Synthesis of multi-hydroxyl end-functionalized polystyrenes.

Figure 9. An integrated flow microreactor system for the synthesis of block copolymers having two different polymer chains on a silicon core (M1, M2, M3, M4: T-shaped micromixers; R1, R2, R3, R4: microtube reactors).
3.3. Controlled/living Anionic Polymerization of Styrenes in Nonpolar Solvent Using Flow Microreactor Systems

Anionic polymerization of styrenes could be conducted in nonpolar solvents at room temperature in a macro batch reactor only when the reaction time was significantly prolonged. Another drawback of this reaction is that the polymerization needs to be performed with <20% by volume styrene because higher volumes of styrene leads to a rapid increase in reaction temperature. With flow microreactors, both disadvantages can be readily resolved. In fact, controlled anionic polymerization of styrene initiated by s-BuLi in cyclohexane as a nonpolar solvent can be conducted at 80 °C by using a flow microreactor system to obtain polystyrenes in quantitative yields within 1 ~ 5 min (Figure 10). In the case of the polymerization of styrene with higher monomer concentrations (25~42%, by volume styrene), the polystyrene can be generated at 60 °C in cyclohexane using an aluminum-polyimide microfluidic device (Figure 11) [112]. Moreover, the molecular weight distributions of the polymers are influenced by channel patterns: straight, periodically pinched, obtuse zigzag and acute zigzag channels.

![Figure 10](image1.png)

**Figure 10.** A flow microreactor system for anionic polymerization of styrene in cyclohexane at 80 °C initiated by s-BuLi. M: T-shaped micromixer; R: microtube reactor.

![Figure 11](image2.png)

**Figure 11.** An aluminum-polyimide microfluidic device for anionic polymerization of styrene initiated by s-BuLi in cyclohexane at high concentrations at 60 °C.

3.4. Controlled/living Anionic Polymerization of Alkyl Methacrylates Using Flow Microreactor Systems

Poly(alkyl methacrylate)s with well-defined structures are of significant research interest as they are versatile materials—such as plastics, adhesives and elastomers—that contain a number of different reactive functions. Living anionic polymerization is considered a superior method for poly(alkyl methacrylate)s synthesis because it is much faster than living radical polymerization, requiring no capping agent. However, to obtain the polymers of narrow molecular weight distribution, cryogenic condition such as -78 °C is compulsory when using a batch macro reactor [113,114]. In industrial production, maintaining such low temperatures can be a huge environmental and economic burden, limiting its useful polymerization. Living anionic polymerization of alkyl methacrylates initiated by 1,1-diphenylhexyllithium using a flow microreactor produces the corresponding poly(alkyl...
methacrylate(s) with controlled molecular weight distribution under more accessible temperatures (methyl methacrylate (MMA): Mw/Mn = 1.16, −28 °C), (butyl methacrylate (BuMA): Mw/Mn = 1.24, 0 °C), (tert-butyl methacrylate (t-BuMA): Mw/Mn = 1.12, 24 °C). Precise control of the reaction temperature and fast mixing of a monomer and an initiator seem to be responsible for successful polymerization (Figure 12) [115]. Moreover, polymethacrylates synthesized by flow microreactor polymerization might give a different structure compared with that of the conventional batch method because optimized reaction temperatures would be different.

For synthesis of end-functionalized polymers and block copolymers, it is crucial to control and maintain livingness of the reactive carbanionic polymer ends. The livingness of the polymer ends can be evaluated in a flow microreactor system as shown in Figure 13. A solution of an alkyl methacrylate and that of 1,1-diphenylhexyllithium are mixed in micromixer M1 and the polymerization is carried out in microtube reactor R1. Then, a solution of the same monomer is introduced at micromixer M2, which is connected to microtube reactor R2 where the sequential polymerization takes place. By changing the length of R1 with the fixed flow rate, how the residence time in R1 can influence the product can be analyzed. With any residence time, the addition of the second monomer solution resulted in molecular weight increase. However, the longer the residence time in R1, the molecular weight distribution also increases, presumably because of decomposition of the polymer end (Figure 14). By choosing an appropriate residence time in R1 (MMA: 2.95 s, BuMA: 0.825 s), the sequential polymerization can be successfully carried out without significant decomposition of the living polymer end [116]. Moreover, the subsequent reaction of the living polymer end with a different alkyl methacrylate leads to the formation of a block copolymer that has narrow molecular-weight distribution (Table 1).

![Figure 12. A flow microreactor system for anionic polymerization of alkyl methacrylates initiated by 1,1-diphenylhexyllithium. M1, M2: T-shaped micromixer; R1, R2: microtube reactor.](image1)

![Figure 13. An integrated flow microreactor system for the sequential anionic polymerization of alkyl methacrylates initiated by 1,1-diphenylhexyllithium. M1, M2: T-shaped micromixer; R1, R2: microtube reactor.](image2)
weight distribution control at easily accessible temperatures such as from 24 to \(28^\circ\text{C}\). Another advantage of flow-microreactor-controlled polymerization is the ease with which a reaction system can be expanded just by connecting multiple micromixers and microreactors, which can exclude extra steps of isolation and purification and requires minimal modulation to reaction conditions. In fact, by using integrated flow microreactor systems, the polystyrene living polymer end, which is produced by butyllithium initiated anionic polymerization of styrenes as well as alkyl methacrylates. Characteristic features of flow microreactor systems, including fast mixing, fast heat transfer and precise residence time control, allows molecular weight distribution to be controlled in a precise manner even under more accessible conditions such as temperatures from 24 to \(28^\circ\text{C}\). Another advantage of flow-microreactor-controlled polymerization is the ease with which a reaction system can be expanded just by connecting multiple micromixers and microreactors, which can exclude extra steps of isolation and purification and requires minimal modulation to reaction conditions. In fact, by using integrated flow microreactor systems, the polystyrene living polymer end, which is produced by butyllithium initiated anionic polymerization of styrene, can be effectively trapped with 1,1-diphenylethylene and the resulting organolithium species can be used as a macro initiator for anionic polymerization of alkyl methacrylates. Therefore, styrene–alkyl methacrylate diblock copolymers can be synthesized with a high level of molecular weight distribution control at easily accessible temperatures such as from 24 to \(28^\circ\text{C}\) (Figure 15) [117]. Moreover, triblock copolymers can be also synthesized by sequential introduction of styrene and two different alkyl methacrylates in a similar manner (styrene–\text{\textdaggerleftert\textdaggerright}-butyl methacrylate–methyl methacrylate triblock copolymer: \(\text{Mn} = 8800, \text{Mw/Mn} = 1.23\), styrene–\text{\textdaggerleftert\textdaggerright}-butyl methacrylate–butyl methacrylate triblock copolymer: \(\text{Mn} = 9000, \text{Mw/Mn} = 1.35\)) (Figure 16).

**Table 1.** Block copolymerization of alkyl methacrylates initiated by 1,1-diphenylethyllithium using the integrated flow microreactor system.

| Monomer-1 | Monomer-2 | Mn   | Mw/Mn |
|-----------|-----------|------|-------|
| MMA       | -         | 3200 | 1.17  |
| MMA       | MMA       | 8600 | 1.29  |
| BuMA      | -         | 4700 | 1.22  |
| BuMA      | BuMA      | 9900 | 1.39  |
| BuMA      | \(^1\text{BuMA}\) | 9000 | 1.31  |
| \(^1\text{BuMA}\) | -         | 5300 | 1.13  |
| \(^1\text{BuMA}\) | \(^1\text{BuMA}\) | 10000 | 1.13  |
| \(^1\text{BuMA}\) | BuMA     | 9500 | 1.16  |
| \(^1\text{BuMA}\) | MMA      | 8400 | 1.15  |

**3.5. Controlled Living Anionic Block Copolymerization of Styrenes and Alkyl Methacrylates Using Integrated Flow Microreactor Systems**

As mentioned above, flow microreactors are effective for accomplishing the controlled anionic polymerization of styrenes as well as alkyl methacrylates. Characteristic features of flow microreactors, including fast mixing, fast heat transfer and precise residence time control, allows molecular weight distribution to be controlled in a precise manner even under more accessible conditions such as temperatures from 24 to \(28^\circ\text{C}\). Another advantage of flow-microreactor-controlled polymerization is the ease with which a reaction system can be expanded just by connecting multiple micromixers and microreactors, which can exclude extra steps of isolation and purification and requires minimal modulation to reaction conditions. In fact, by using integrated flow microreactor systems, the polystyrene living polymer end, which is produced by butyllithium initiated anionic polymerization of styrene, can be effectively trapped with 1,1-diphenylethylene and the resulting organolithium species can be used as a macro initiator for anionic polymerization of alkyl methacrylates. Therefore, styrene–alkyl methacrylate diblock copolymers can be synthesized with a high level of molecular weight distribution control at easily accessible temperatures such as from 24 to \(28^\circ\text{C}\) (Figure 15) [117]. Moreover, triblock copolymers can be also synthesized by sequential introduction of styrene and two different alkyl methacrylates in a similar manner (styrene–\text{\textdaggerleftert\textdaggerright}-butyl methacrylate–methyl methacrylate triblock copolymer: \(\text{Mn} = 8800, \text{Mw/Mn} = 1.23\), styrene–\text{\textdaggerleftert\textdaggerright}-butyl methacrylate–butyl methacrylate triblock copolymer: \(\text{Mn} = 9000, \text{Mw/Mn} = 1.35\)) (Figure 16).
The anionic polymerization of block copolymers comprising fluorine-containing monomers has been extensively studied due to the polymer’s unique and highly valuable physical properties; however, maintaining the livingness of their extremely unstable growth ends has always been too challenging, requiring an additive such as lithium chloride to control the reaction. Integrated flow microreactor systems proved to be effective to solve this problem, taking advantages of precise controls on temperature and residence time [118]. An example of one of the fluorine-containing monomers, 2-(nonafluorobutyl)ethyl methacrylate (NFBEMA), will be discussed. First, an optimal reaction condition is identified by analyzing the conversion rate of the first monomer and the molecular distribution of the block copolymer as shown in Figures 17 and 18 (temperature: −40 °C, residence time: 7.9 s). Under the optimal condition, the NFBEMA polymer is generated and then is used for block copolymerization with alkyl methacrylates and alkyl acrylate, all of which can be performed in one flow (NFBEMA–tert-butyl methacrylate–alkyl methacrylate: Mn = 29000, Mw/Mn = 1.15) (Figure 19). Moreover, the fluorine-containing triblock copolymer can also be synthesized by integrated flow microreactor system (NFBEMA–tert-butyl methacrylate–NFBEMA triblock copolymer: Mn = 16,000, Mw/Mn = 1.10).
Figure 17. Flow microreactor system for the sequential polymerization of 2-(nonafluorobutyl)ethyl methacrylate (NFBEMA) initiated by 1,1-diphenylhexyllithium. M1, M2: T-shaped micromixer; R1, R2: microtube reactor.

Figure 18. Three-dimensional temperature-residence time map of sequential polymerization of 2-(nonafluorobutyl)ethyl methacrylate (NFBEMA).

Figure 19. Size exclusion chromatography traces of block copolymers synthesized by the integrated flow microreactor system. Dashed line: 2-(nonafluorobutyl)ethyl methacrylate (NFBEMA) homopolymer. (a) 2-(nonafluorobutyl)ethyl methacrylate (NFBEMA) (polymerization temperature; T = −40 °C)/tert-butyl methacrylate (tBuMA) (T = 20 °C), (b) 2-(nonafluorobutyl)ethyl methacrylate (NFBEMA) (T = −40 °C)/methyl methacrylate (MMA) (T = −30 °C), (c) 2-(nonafluorobutyl)ethyl methacrylate (NFBEMA) (T = −40 °C)/tert-butyl acrylate (tBuA) (T = −20 °C).
4. Anionic Ring Opening Polymerization Using Flow Microreactor Systems

The ability of flow microreactors to effectively control highly reactive monomers can be utilized for reactions involving substantially dangerous compounds such as ethylene oxide [119]. Controlling reactions with ethylene oxide can often be quite difficult and the handling of the compounds requires a great deal of caution in batch macro reactors. In comparison, the distinctively small size of a flow microreactor can prevent reaction heat from accumulating and keep the amount of ethylene oxide used at any given time minimal, resulting in a much safer process [120]. The anionic ring opening polymerization [121] of ethylene oxide initiated by alkoxy anion is performed within 30 min residence time at 120 °C under pressurized condition, acquiring monoalkyl-ether terminated PEGs in high yield and narrow molecular weight distribution (Mn = 2100, Mw/Mn = 1.06) (Figure 20) [122].

The characteristics of flow microreactors, such as efficient mixing and fast heat/mass transfer, increase reaction rate. For organocatalyzed ring opening polymerization [123,124] of ε-caprolactone (CL) and ε-valerolactone (VL), the apparent polymerization rate constant (k_{app}) in a flow microreactor is larger than that in a batch macroreactor (in flow microreactor: k_{app} = 0.00602 min^{-1} (CL) and 0.159 min^{-1} (VL), in batch reactor: 0.00286 min^{-1} (CL) and 0.079 min^{-1} (VL)) [125]. Furthermore, an integrated flow microreactor system enables block copolymerization even in ring opening polymerization (Figure 21). A series of monomer introduction produces well-defined poly(ε-valerolactone)-block-poly(ε-caprolactone) and poly(ε-caprolactone)-block-poly(ε-valerolactone).

5. Continuous Production Using Flow Microreactor Systems

One of the most important advantages of a flow microreactor is that a laboratory-scale reaction can be readily adapted to an industrial-scale production simply by continuously running a reaction for a long period of time. In a case of flow anionic polymerization of styrene initiated by n-BuLi, about 1 kg of polystyrene was produced over 3-h reaction time with high molecular weight and narrow molecular weight distribution (Mn = 8000, Mw/Mn = 1.1) [126]. The polymers of various molecular weights
(Mn = 5000 to Mn = 14,000) with narrow molecular weight distribution (Mw/Mn = 1.08–1.16) were successfully synthesized simply by changing the relative flow rate and the concentration of solutions of styrene and initiator. In order to produce polymers with higher molecular weights, the suppression of pressure increase and/or the use of high pressure pump would be necessary.

In terms of the industrial production process, it is important to be able to stop and restart an operation easily. The Smoothflow pump has a structure which allows a solution to be contained in its pump head during a resting time. This feature offers significant superiority for a reaction operation with a reactant solution which is unstable to air and/or water. (Figure 22). A great deal of information has been acquired in laboratories and pilot plants, which should profit the further development of this field to realize commercial plants for making polymers in the near future [127].

Figure 22. Schematic diagram of the flow microreactor system.

6. Conclusions

The examples shown in this review demonstrate the great usefulness of flow microreactor systems for the structural control and production of polymers by anionic polymerization. Spatial integration improves the efficiency and speed of structurally-defined polymer synthesis by conducting a series of reactions in one flow. In addition, a reaction is controlled in a way that does not require extremely cryogenic conditions, removing one of the major obstacles for industrial use. Further development of the anionic polymerization method based on continuous flow synthesis is expected and this technology can greatly contribute to polymer production in the near future.

Author Contributions: A.N. and Y.T. wrote and revised the manuscript.

Funding: This work was partially supported by the Grant-in-Aid for Scientific Research on Innovative Areas 2707 Middle molecular strategy from MEXT (no. 15H05849), Scientific Research (B) (no. 26288049), Scientific Research (S) (no. 26220804), Scientific Research (S) (no. 25220913), Scientific Research (C) (no. 17865428), AMED (no. 18067420), the Japan Science and Technology Agency’s (JST) A-step program (no. 18061567), CREST and the Ogasawara Foundation for the Promotion of Science & Engineering.

Conflicts of Interest: The authors declare no conflict of interest.

References

1. Hessel, V.; Hardt, S.; Löwe, H. Chemical Micro Process Engineering; Wiley-VCH Verlag: Weinheim, Germany, 2004.
2. Wirth, T. Microreactors in Organic Synthesis and Catalysis; Wiley-VCH Verlag: Weinheim, Germany, 2008.
3. Hessel, V.; Schouten, J.C.; Renken, A.; Yoshida, J.I. Micro Process Engineering; Wiley-VCH Verlag: Weinheim, Germany, 2009.
4. Watts, P.; Wiles, C. Micro Reaction Technology in Organic Synthesis; CRC Press: New York, NY, USA, 2011.
5. Fletcher, P.D.; Haswell, S.J.; Pombo-Villar, E.; Warrington, B.H.; Watts, P.; Wong, S.Y.; Zhang, X. Micro reactors: Principles and applications in organic synthesis. Tetrahedron 2002, 58, 4735–4757. [CrossRef]
6. Jähnisch, K.; Hessel, V.; Löwe, H.; Baerns, M. Chemistry in microstructured reactors. Angew. Chem. Int. Ed. 2004, 43, 406–446. [CrossRef] [PubMed]

7. Kiwi-Minsker, L.; Renken, A. Microstructured reactors for catalytic reactions. Catal. Today 2005, 110, 2–14. [CrossRef]

8. Doku, G.N.; Verboom, W.; Reinholdt, D.N.; van den Berg, A. On-microchip multiphase chemistry—A review of microreactor design principles and reagent contacting modes. Tetrahedron 2005, 61, 2733–2742. [CrossRef]

9. Watts, P.; Haswell, S.J. The application of micro reactors for organic synthesis. Chem. Soc. Rev. 2005, 34, 235–246. [CrossRef]

10. Geyer, K.; Codee, J.D.C.; Seeberger, P.H. Microreactors as tools for synthetic Chemists—the chemists’ round-bottomed flask of the 21st century? Chem. Eur. J. 2006, 12, 8434–8442. [CrossRef] [PubMed]

11. Whitesides, G. The origins and the future of microfluidics. Nature 2006, 442, 368–373. [CrossRef] [PubMed]

12. deMello, A.J. Control and detection of chemical reactions in microfluidic systems. Nature 2006, 442, 394–402. [CrossRef]

13. Song, H.; Chen, D.L.; Ismagilov, R.F. Reactions in droplets in microfluidic channels. Angew. Chem. Int. Ed. 2006, 45, 7336–7356. [CrossRef] [PubMed]

14. Kobayashi, J.; Mori, Y.; Kobayashi, S. Multiphase organic synthesis in microchannel reactors. Chem. Asian J. 2006, 1, 22–35. [CrossRef] [PubMed]

15. Brivio, M.; Verboom, W.; Reinholdt, D.N. Miniaturized continuous flow reaction vessels: Influence on chemical reactions. Lab Chip 2006, 6, 329–344. [CrossRef]

16. Mason, B.P.; Price, K.E.; Steinbacher, J.L.; Bogdan, A.R.; McQuade, D.T. Greener approaches to organic synthesis using microreactor technology. Chem. Rev. 2007, 107, 2300–2318. [CrossRef][PubMed]

17. Ahmed-Omer, B.; Brandtand, J.C.; Wirth, T. Advanced organic synthesis using microreactor technology. Org. Biomol. Chem. 2007, 5, 733–740. [CrossRef] [PubMed]

18. Watts, P.; Wiles, C. Recent advances in synthetic micro reaction technology. Chem. Commun. 2007, 443–467. [CrossRef]

19. Fukuyama, T.; Rahman, M.T.; Sato, M.; Ryu, I. Adventures in inner space: Microflow systems for practical organic synthesis. Synlett 2008, 2008, 151–163.

20. Lin, W.; Wang, Y.; Wang, S.; Tseng, H.-R. Integrated microfluidic reactors. Nano Today 2009, 4, 470–481. [CrossRef] [PubMed]

21. McMullen, J.P.; Jensen, K.F. Integrated microreactors for reaction automation: New approaches to reaction development. Annu. Rev. Anal. Chem. 2010, 3, 19–42. [CrossRef] [PubMed]

22. Ley, S.V. The changing face of organic synthesis. Tetrahedron 2010, 66, 6270–6292. [CrossRef]

23. Webb, D.; Jamison, T.F. Continuous flow multi-step organic synthesis. Chem. Sci. 2010, 1, 675–680. [CrossRef]

24. Yoshida, J.; Kim, H.; Nagaki, A. Green and sustainable chemical synthesis using flow microreactors. ChemSusChem 2011, 4, 331–340. [CrossRef] [PubMed]

25. Noël, T.; Su, Y.; Hessel, V. Organometallic Flow Chemistry; Springer International Publishing: Cham, Switzerland, 2016.

26. Chambers, R.D.; Holling, D.; Spink, R.C.H.; Sandford, G. Elemental fluorine Part 13. Gas-liquid thin film microreactors for selective direct fluorination. Lab Chip 2001, 1, 132–137. [CrossRef] [PubMed]

27. Jähnisch, K.; Baerns, M.; Hessel, V.; Ehrfeld, W.; Haverkamp, V.; Löwe, H.; Wille, C.; Guber, A. Direct fluorination of toluene using elemental fluorine in gas/liquid microreactors. J. Fluor. Chem. 2000, 105, 117–123. [CrossRef]

28. Ducry, L.; Roberge, D.M. Controlled autocatalytic nitration of phenol in a microreactor. Angew. Chem. Int. Ed. 2005, 44, 7972–7975. [CrossRef] [PubMed]

29. Wakami, H.; Yoshida, J. Grignard exchange reaction using a microflow system: From bench to pilot plan. Org. Process Res. Dev. 2005, 9, 787–791. [CrossRef]

30. Usutani, H.; Tomida, Y.; Nagaki, A.; Okamoto, H.; Nakami, T.; Yoshida, J. Generation and reactions of o-bromophenyllithium without benzyne formation using a microreactor. J. Am. Chem. Soc. 2007, 129, 3046–3047. [CrossRef]

31. Nagaki, A.; Tomida, Y.; Usutani, H.; Kim, H.; Takabayashi, N.; Nakami, T.; Okamoto, H.; Yoshida, J. Integrated micro flow synthesis based on sequential Br-Li exchange reactions of p-, m- and o-dibromobenzenes. Chem. Asian J. 2007, 2, 1513–1523. [CrossRef]
32. Nagaki, A.; Kim, H.; Yoshida, J. Aryllithium compounds bearing alkoxy carbonyl groups. Generation and reactions using a microflow system. Angew. Chem. Int. Ed. 2008, 47, 7833–7836. [CrossRef] [PubMed]

33. Nagaki, A.; Takizawa, E.; Yoshida, J. Oxiran anion methodology using microflow systems. J. Am. Chem. Soc. 2009, 131, 1654–1655. [CrossRef]

34. Nagaki, A.; Kim, H.; Yoshida, J. Nitro-substituted aryl lithium compounds in microreactor synthesis: Switch between kinetic and thermodynamic control. Angew. Chem. Int. Ed. 2009, 48, 8063–8065. [CrossRef]

35. Tomida, Y.; Nagaki, A.; Yoshida, J. Carboli thiation of conjugated enynes with aryllithiums in microflow system and applications to synthesis of allenylsiline s. Org. Lett. 2009, 11, 3614–3617. [CrossRef]

36. Nagaki, A.; Takizawa, E.; Yoshida, J. Generation and reactions of α-silylo xiran yllithium in a microreactor. Chem. Lett. 2009, 38, 486–487. [CrossRef]

37. Nagaki, A.; Takizawa, E.; Yoshida, J. Generations and reactions of N-t-butylsulfon yl-aziridinyllithiums using microreactors. Chem. Lett. 2009, 38, 1060–1061. [CrossRef]

38. Nagaki, A.; Kim, H.; Usutani, H.; Matsu o, C.; Yoshida, J. Generation and reaction of cyano-substituted aryllithium compounds using microreactors. Org. Biomol. Chem. 2010, 8, 1212–1217. [CrossRef]

39. Nagaki, A.; Kim, H.; Moriwaki, Y.; Matsu o, C.; Yoshida, J. A flow microreactor system enables organolithium reactions without protecting alkoxy carbonyl groups. Chem. Eur. J. 2010, 16, 11167–11177. [CrossRef]

40. Nagaki, A.; Takizawa, E.; Yoshida, J. Generation and reactions of oxiranyllithiums by use of a flow microreactor system. Chem. Eur. J. 2010, 16, 14149–14158. [CrossRef] [PubMed]

41. Tomida, Y.; Nagaki, A.; Yoshida, J. Asymmetric carboli thiation of conjugated enynes: A flow microreactor enables the use of configurationally unstable intermediates before they epimerize. J. Am. Chem. Soc. 2011, 133, 3744–3747. [CrossRef] [PubMed]

42. Kim, H.; Nagaki, A.; Yoshida, J. A flow-microreactor approach to protecting-group-free synthesis using organolithium compounds. Nat. Commun. 2011, 2, 264. [CrossRef] [PubMed]

43. Nagaki, A.; Yamada, S.; Doi, M.; Tomida, Y.; Takabayashi, N.; Yoshida, J. Flow microreactor synthesis of disubstituted pyridines from dibromopyridines via Br/Li exchange without using cryogenic conditions. Green Chem. 2011, 13, 1110–1113. [CrossRef]

44. Nagaki, A.; Tokuoka, S.; Yamada, S.; Tomida, Y.; Oshiro, K.; Amii, H.; Yoshida, J. Perfluoroalkylation in flow microreactors: Generation of perfluoroalkyllithiums in the presence and absence of electrophiles. Org. Biomol. Chem. 2011, 9, 7559–7563. [CrossRef] [PubMed]

45. Asai, T.; Takata, A.; Nagaki, A.; Yoshida, J. Practical synthesis of photochromic diarylethenes in integrated flow microreactor. ChemSusChem 2012, 5, 339–350. [CrossRef]

46. Nagaki, A.; Matsu o, C.; Kim, S.; Saito, K.; Miyazaki, A.; Yoshida, J. Lithiation of 1,2-dichloroethene in flow microreactors: Versatile synthesis of alkenes and alkynes by precise residence-time control. Angew. Chem. Int. Ed. 2012, 51, 3245–3248. [CrossRef] [PubMed]

47. He, P.; Watts, P.; Marken, F.; Hasw ell, S.J. Self-supported and clean one-step cathodic coupling of... Derivatives in a micro flow reactor. Angew. Chem. Int. Ed. 2006, 45, 4146–4149. [CrossRef] [PubMed]

48. Tanaka, K.; Motomatsu, S.; Koyama, K.; Tanaka, S.; Fukase, K. Large-scale synthesis of immunoactivating natural product, pristane, by continuous microfluidic dehydration as the key step. Org. Lett. 2007, 9, 299–302. [CrossRef] [PubMed]

49. Sahoo, H.R.; Kralj, J.G.; Jensen, K.F. Multi-step continuous flow microchemical synthesis involving multiple reactions and separations. Angew. Chem. Int. Ed. 2007, 46, 5704–5708. [CrossRef] [PubMed]

50. Horning, C.H.; Mackley, M.R.; Baxendale, I.R.; Ley, S.V. A microcapillary flow disc reactor for organic synthesis. Org. Process Res. Dev. 2007, 11, 399–405. [CrossRef]

51. Fuku yama, T.; Kobayashi, M.; Rahman, M.T.; Kamata, N.; Ryu, I. Spurring radical reactions of organic halides with tin hydride and TTMS using microreactors. Org. Lett. 2008, 10, 533–536. [CrossRef] [PubMed]

52. Tricotet, T.; O’Shea, D.F. Automated generation and reactions of 3-hydroxymethylindoles in continuous-flow microreactors. Chem. Eur. J. 2010, 16, 6678–6686. [CrossRef]

53. Browne, D.L.; Baumann, M.; Harji, B.H.; Baxendale, I.R.; Ley, S.V. A new enabling technology for convenient laboratory scale continuous flow processing at low temperatures. Org. Lett. 2011, 13, 3312–3315. [CrossRef]

54. Carter, C.F.; Lange, H.; Sakai, D.; Baxendale, I.R.; Ley, S.V. Diastereoselective chain elongation reactions using microreactors for application in complex molecule assembly. Chem. Eur. J. 2011, 17, 3398–3405. [CrossRef]
55. Zaborenko, N.; Bedore, M.W.; Jamison, T.F.; Jensen, K.F. Kinetic and scale-up investigations of epoxide aminolysis in microreactors at high temperatures and pressures. Org. Process Res. Dev. 2011, 15, 131–139. [CrossRef]
56. Noël, T.; Kuhn, S.; Musachio, A.J.; Jensen, K.F.; Buchwald, S.L. Suzuki-Miyaura cross-coupling reactions in flow: Multistep synthesis enabled by a microfluidic extraction. Angew. Chem. Int. Ed. 2011, 50, 5943–5946. [CrossRef] [PubMed]
57. Gutierrez, A.C.; Jamison, T.F. Continuous photochemical generation of catalytically active [CpRu]+ complexes from CpRu(n4-C4H4)PF6. Org. Lett. 2011, 13, 6414–6417. [CrossRef]
58. Hessel, V.; Löwe, H.; Serra, C.; Hadziioannou, G. Polymerisationen in mikrostrukturierten reaktoren: Ein überblick. Chem. Ing. Tech. 2005, 77, 1693–1714. [CrossRef]
59. Steinbacher, J.L.; McQuade, D.T. Polymer chemistry in flow: New polymers, beads, capsules and fibers. J. Polym. Sci. Part A Polym. Chem. 2006, 44, 6505–6533. [CrossRef]
60. Wilms, D.; Klos, J.; Frey, H. Microstructured reactors for polymer synthesis: A renaissance of continuous flow processes for tailor-made macromolecules? Macromol. Chem. Phys. 2008, 209, 343–356. [CrossRef]
61. Hessel, V.; Serra, C.A.; Hesse, V.; Hadziioannou, G. Microreactors—A review on passive and active mixing principles. Macromolecules 2012, 45, 9551–9570. [CrossRef]
62. Junkers, T. Precise macromolecular engineering via continuous-flow synthesis techniques. J. Flow Chem. 2017, 7, 106–110. [CrossRef]
63. Kakuta, M.; Bessoth, F.G.; Manz, A. Microfabricated devices for fluid mixing and their application for chemical synthesis. Chem. Rec. 2001, 1, 395–405. [CrossRef] [PubMed]
64. Hessel, V.; Löwe, H.; Schönfeld, F. Micromixers—A review on passive and active mixing principles. Chem. Eng. Sci. 2005, 60, 2479–2501. [CrossRef]
65. Junkers, T. Precise macromolecular engineering via continuous-flow synthesis techniques. Chem. Eng. Sci. 2001, 56, 4509–4516. [CrossRef] [PubMed]
66. Wilms, D.; Klos, J.; Frey, H. Microstructured reactors for polymer synthesis: A renaissance of continuous flow processes for tailor-made macromolecules? Macromol. Chem. Phys. 2008, 209, 343–356. [CrossRef]
67. Hessel, V.; Löwe, H.; Serra, C.; Hadziioannou, G. Micromixer-assisted polymerization processes. Chem. Eng. Sci. 2011, 66, 1449–1462. [CrossRef]
68. Serra, C.A.; Chang, Z. Microfluidic-assisted synthesis of polymer particles. Chem. Eng. Technol. 2008, 31, 1099–1115. [CrossRef]
69. Tonhauser, C.; Natalello, A.; Löwe, H.; Frey, H. Microflow technology in polymer synthesis. Macromolecules 2012, 45, 9551–9570. [CrossRef]
70. Serra, C.A.; Chang, Z. Microfluidic-assisted synthesis of polymer particles. Chem. Eng. Technol. 2008, 31, 1099–1115. [CrossRef]
71. Tonhauser, C.; Natalello, A.; Löwe, H.; Frey, H. Microflow technology in polymer synthesis. Macromolecules 2012, 45, 9551–9570. [CrossRef]
80. Goseki, R.; Ito, S.; Matsuo, Y.; Higashihara, T.; Hirao, A. Precise synthesis of macromolecular architectures by novel iterative methodology combining living anionic polymerization with specially designed linking chemistry. *Polymer 2017*, *9*, 470. [CrossRef][PubMed]

81. Goseki, R.; Tanaka, S.; Ishizone, T.; Hirao, A. Living anionic polymerization of 1,4-divinylbenzene and its derivatives. *React. Funct. Polym. 2018*, *127*, 94–112. [CrossRef]

82. Frechet, J.M.J. Functional polymers and dendrimers: Reactivity, molecular architecture and interfacial energy. *Science 1994*, *263*, 1710–1715. [CrossRef]

83. Percec, V. Frontiers in polymer chemistry. *Chem. Rev. 2001*, *101*, 3579–3580. [CrossRef]

84. Ito, S.; Goseki, R.; Ishizone, T.; Hirao, A. Successive synthesis of well-defined multiarmed miktoarm star polymers by iterative methodology using living anionic polymerization. *Eur. Polym. J. 2013*, *49*, 2545–2566. [CrossRef]

85. Ito, S.; Goseki, R.; Ishizone, T.; Hirao, A. Synthesis of well-controlled graft polymers by living anionic polymerization towards exact graft polymers. *Polym. Chem. 2014*, *5*, 5523–5534. [CrossRef]

86. Jagur-Grodzinski, J. *Living and Controlled Polymerization: Synthesis, Characterization and Properties of the Respective Polymers and Copolymers*; NOVA: New York, NY, USA, 2006.

87. Bhattacharyya, D.N.; Lee, C.L.; Smid, J.; Szwarz, M. Reactivities and conductivities of ions and ion pairs in polymerization processes. *J. Phys. Chem. 1965*, *69*, 612–623. [CrossRef]

88. Figini, R.V.; Hostalka, H.; Hurm, K.; Löhrr, G.; Schulz, G.V. Zur Kinetik anionischer Polymerisationsvorgänge. *Z. Phys. Chem. 1965*, *45*, 269–285. [CrossRef]

89. Baskaran, D.; Müller, A.H.E. Kinetic investigation on metal free anionic polymerization of methyl methacrylate using tetraphenylphosphonium as the counterion in tetrahydrofuran. *Macromolecules 1997*, *30*, 1869–1874. [CrossRef]

90. Hofe, T.; Maurer, A.; Müller, A.H.E. Ein neuer Stroemungsrohreaktor fuer die Kinetik schneller chemischer Reaktionen. *GIT Labor Fachz. 1998*, *42*, 1127.

91. Tonhauser, C.; Frey, H. A road less traveled to functional polymers: Epoxide termination in living carbanionic polymerization. *Macromolecules* 1988, *21*, 3081–3089. [CrossRef]

92. Nagaki, A.; Tomida, Y.; Yoshida, J. Microflow system controlled anionic polymerization of styrenes. *Macromolecules 2008*, *41*, 6322–6330. [CrossRef]

93. Wurm, F.; Wilms, D.; Klos, J.; Löwe, H.; Frey, H. Carbanions on tap—Living anionic polymerization in a microstructured reactor. *Macromol. Chem. Phys. 2008*, *209*, 1106–1114. [CrossRef]

94. Natalello, A.; Morsbach, J.; Friedel, A.; Alkan, A.; Tonhauser, C.; Müller, A.H.E.; Frey, H. Living anionic polymerization in continuous flow: Facilitated synthesis of high-molecular weight poly(2-vinylpyridine) and polystyrene. *Org. Process Res. Dev. 2014*, *18*, 1408–1412. [CrossRef]

95. Morsbach, J.; Müller, A.H.E.; Berger-Nicoletti, E.; Frey, H. Living polymer chains with predictable molecular weight and dispersity via carbanionic polymerization in continuous flow: Mixing rate as a key parameter. *Macromolecules 2016*, *49*, 5043–5050. [CrossRef]

96. Morsbach, J.; Wilms, D.; Wurm, F.; Nicoletti, E.B.; Maskos, M.; Löwe, H.; Frey, H. Multihydroxyl-functional polystyrenes in continuous flow. *Macromolecules 2010*, *43*, 5582–5588. [CrossRef]

97. Pennisi, R.W.; Fetters, L.J. Preparation of asymmetric three-arm polybutadiene and polystyrene stars. *Macromolecules 1988*, *21*, 1094–1099. [CrossRef]

98. Iatrou, H.; Hadjichristidis, N. Synthesis of a model 3-miktoarm star terpolymer. *Macromolecules 1992*, *25*, 4649–4651. [CrossRef]

99. Rózga-Wijas, K.; Chojnowski, J.; Fortuniak, W.; Ścibiorek, M.; Michalska, Z.; Rogalski, L. Branched functionalised polysiloxane–silica hybrids for immobilisation of catalysts. *J. Mater. Chem. 2003*, *13*, 2301–2310. [CrossRef][PubMed]

100. Yoshida, J.; Nagaki, A.; Iwasaki, T.; Suga, S. Enhancement of chemical selectivity by microreactors. *Chem. Eng. Tech. 2005*, *3*, 259–266. [CrossRef]

101. Nagaki, A.; Tagai, M.; Suga, S.; Aoki, N.; Mae, K.; Yoshida, J. Control of extremely fast competitive consecutive reactions using micromixing. *J. Am. Chem. Soc. 2005*, *127*, 11666–11675. [CrossRef][PubMed]

102. Suga, S.; Nagaki, A.; Yoshida, J. Highly selective Friedel–Crafts monoalkylation using micromixing. *Chem. Commun. 2003*, *354–355*. [CrossRef]

103. Suga, S.; Nagaki, A.; Tsutsui, Y.; Yoshida, J. “N-Acyliminium ion pool” as hetero diene in [4+2] cycloaddition reaction. *Org. Lett. 2003*, *5*, 945–949. [CrossRef][PubMed]
104. Suga, S.; Tsutsui, Y.; Nagaki, A.; Yoshida, J. Cycloaddition of “N-acryliminium ion pool” with carbon-carbon multiple bond. *Bull. Chem. Soc. Jpn.* 2005, 78, 1206–1217. [CrossRef]

105. Nagaki, A.; Takabayashi, N.; Tomida, Y.; Yoshida, J. Synthesis of unsymmetrical biaryls by means of mono-selective reaction of polyhalaarenes using integrated microflow system. *Org. Lett.* 2008, 18, 3937–3940. [CrossRef] [PubMed]

106. Nagaki, A.; Takabayashi, N.; Tomida, Y.; Yoshida, J. Synthesis of unsymmetrically substituted biaryls via sequential lithiation of dibromobioaryls using integrated microflow systems. *Beilstein J. Org. Chem.* 2009, 5, No16. [CrossRef] [PubMed]

107. Ishigaki, Y.; Suzuki, T.; Nishida, J.; Nagaki, A.; Takabayashi, N.; Kawai, H.; Fujiwara, K.; Yoshida, J. Hysteric tricolor electrochromic systems based on the dynamic redox properties of unsymmetrically substituted dihydrophenanthenes and biphenyl-2,2′-dyl dications: Efficient precursor synthesis by a flow microreactor method. *Materials* 2011, 4, 1906–1926. [CrossRef]

108. Suzuki, T.; Uchimura, Y.; Ishigaki, Y.; Takeda, T.; Katono, R.; Kawai, H.; Fujiwara, K.; Nagaki, A.; Yoshida, J. Non-additive substituent effects on expanding prestrained C-C bond in crystal: X-ray analyses on unsymmetrically substituted tetraarylpyracenes prepared by a flow microreactor method. *Chem. Lett.* 2012, 41, 541–543. [CrossRef]

109. Midorikawa, K.; Suga, S.; Yoshida, J. Selective monoiodination of aromatic compounds with electrochemically generated I+ using micromixing. *Chem. Commun.* 2006, 36, 3794–3796. [CrossRef] [PubMed]

110. Kataoka, K.; Hagiwara, Y.; Midorikawa, K.; Suga, S.; Yoshida, J. Practical electrochemical iodination of aromatic compounds. *Org. Process Res. Dev.* 2008, 12, 1130–1136. [CrossRef]

111. Hessel, V.; Hofmann, C.; Löwe, H.; Meudt, A.; Scherer, S.; Schönfeld, F.; Werner, B. Selectivity gains and energy savings for the industrial phenyl boronic acid process using micromixer/tubular reactors. *Org. Process Res. Dev.* 2004, 8, 511–523. [CrossRef]

112. Iida, K.; Chastek, T.Q.; Beers, K.L.; Cavicchi, K.A.; Chun, J.; Fasolka, M.J. Living anionic polymerization using a microfluidic reactor. *Lab Chip* 2009, 9, 339–345. [CrossRef] [PubMed]

113. Zune, C.; Jérôme, R. Anionic polymerization of methacrylic monomers: Characterization of the propagating species. *Prog. Polym. Sci.* 1999, 24, 631–664. [CrossRef]

114. Baskaran, D. Strategic developments in living anionic polymerization of alkyl (meth)acrylates. *Prog. Polym. Sci.* 2003, 28, 521–581. [CrossRef]

115. Nagaki, A.; Miyazaki, A.; Yoshida, J. Microflow system controlled anionic polymerization of MMA. *Macromolecules* 2009, 42, 4384–4387. [CrossRef]

116. Nagaki, A.; Miyazaki, A.; Tomida, Y.; Yoshida, J. Anionic polymerization of alkyl methacrylates using flow microreactor systems. *Chem. Eng. J.* 2011, 167, 548–555. [CrossRef]

117. Nagaki, A.; Tomida, Y.; Yoshida, J. Synthesis of polystyrenes-poly(alkyl methacrylates) block copolymers via anionic polymerization using an integrated flow microreactor system. *Macromolecules* 2010, 43, 8424–8429. [CrossRef]

118. Nagaki, A.; Akahori, K.; Takahashi, Y.; Yoshida, J. Flow microreactor synthesis of fluorine-containing block copolymers. *J. Flow Chem.* 2014, 4, 168–172. [CrossRef]

119. Núñyken, O.; Pask, S.D. Ring-opening polymerization-an introductory review. *Polymers* 2013, 5, 361–403. [CrossRef]

120. Brocas, A.-L.; Mantzaridis, C.; Tunc, D.; Carlotti, S. Polyether synthesis: From activated or metal-free anionic ring-opening polymerization of epoxides to functionalization. *Prog. Polym. Sci.* 2013, 38, 845–873. [CrossRef]

121. Hu, X.; Zhu, N.; Fang, Z.; Guo, K. Continuous flow ring-opening polymerizations. *React. Chem. Eng.* 2017, 2, 20–26. [CrossRef]

122. Furuta, A.; Okada, K.; Fukuyama, T. Efficient anionic ring opening polymerization of ethylene oxide under microfluidic conditions. *Bull. Chem. Soc. Jpn.* 2017, 90, 838–842. [CrossRef]

123. Baeten, E.; Vanslambrouck, S.; Jérôme, C.; Lecomte, P.; Junkers, T. Anionic flow polymerizations toward functional polyphosphoesters in microreactors: Polymerization and UV-modification. *Eur. Polym. J.* 2016, 80, 208–218. [CrossRef]

124. Vandenberg, S.A.; Zuilhof, H.; Wennekes, T. Clickable polylactic acids by fast organocatalytic ring-opening polymerization in continuous flow. *Macromolecules* 2016, 49, 2054–2062. [CrossRef]

125. Zhu, N.; Feng, W.; Hu, X.; Zhang, Z.; Fang, Z.; Zhang, K.; Li, Z.; Guo, K. Organocatalyzed continuous flow ring-opening polymerization to homo- and block-polylactones. *Polymers* 2016, 84, 391–397. [CrossRef]
126. Nagaki, A.; Nakahara, Y.; Furusawa, M.; Sawaki, T.; Yamamoto, T.; Toukairin, H.; Tadokoro, S.; Shimazaki, T.; Ito, T.; Otake, M.; et al. Feasibility study on continuous flow controlled/living anionic polymerization process. *Org. Process Res. Dev.* **2016**, *20*, 1377–1382. [CrossRef]

127. Mastan, E.; He, J. Continuous production of multiblock copolymers in a loop reactor: When living polymerization meets flow chemistry. *Macromolecules* **2017**, *50*, 9173–9187. [CrossRef]

© 2019 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (http://creativecommons.org/licenses/by/4.0/).