Design and construction of a pressure stabilizing device of cement slurry used in Deep Soil Mixing Technology

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The article describes research carried out for design and construction of devices stabilizing the working pressure of cement slurry, with use of Deep Soil Mixing (DSM).

KEYWORDS: Deep Soil Mixing Technology (DSM), pressure stabilizing device, cement slurry, bentonite

Introduction

The design and construction of a device stabilizing the working pressure of cement slurry, which was used in Deep Soil Mixing (DSM) technology, was described. This technology is used worldwide to reinforce a weak building foundation and consists in constructing columns (screens) of cement ground (fig. 1) [1]. A steel stirrer is introduced into the soil, which is usually turned clockwise. At the same time, leaven is applied to the loosened soil, the main components of which are water and cement.

This technique is more and more widely used and is the subject of intensive experimental research and theoretical works [2, 3].

Fig. 1. Apertures made in DSM technology [1]

The AIE-400 electric injection aggregate from Bipromasz was used to supply the cement slurry. The aggregate (fig. 2) consists of two PPN-250 plunger mud pumps, working in pairs, in which the plungers work alternately to ensure continuity and uniformity of the pumped stream. The parameters of mud pumps are presented in tab. 1 [4].

One of the disadvantages of plunger pumps is the pulsation of the pumped medium, which, if the injection system is operated without a pressure stabilizing device (pulsation damper), leads to damage to the injection lines.
Fig. 2. AIE-400 injection aggregate [4]

| TABLE I. Operating parameters of the AIE-400 injection aggregate |
|---------------------------------------------------------------|
| **Mud pump** | PPN-250-2 pieces |
| **Inject** | cement and bentonite suspensions |
| **Capacity per cycle** | 4.6 × 2 dm³ |
| **Performance included in the assembly AIE-400** | to 400 dm³/min |
| **Maximum pressure** | 4 (6 for micropiles) MPa |
| **Drive** | actuator 50/36×250AH |

Manufacturers of injection aggregates recommend the use of an additional silencer (compensator) on the discharge line, the main task of which is to significantly reduce pressure pulsations in the widest possible frequency band with slight pressure losses, regardless of temperature or pressure fluctuations. Unfortunately, commercially available design solutions of pulsation dampers are not adapted to work with cement and bentonite slurries, because they have limited self-cleaning ability during continuous operation, as a result of which a lot of dirt remains in the damper chamber, which leads to damage to the device.

This paper presents a design solution for a piston pulsation damper with a system of continuous cleaning of the cylinder internal surfaces during operation.

**Design of a pressure stabilizing device**

The aim of the project was to develop a piston pulsation damper with a system of continuous cleaning of internal surfaces of the cylinder during operation, designed to reduce the pressure pulsation of cement and bentonite suspensions.

The developed structure of the pressure stabilizing device has a body with holes supplying and discharging the working medium. The body has also a cylinder sealed with a rubber ring.

Cylinder head with a pressure gauge and a four-pipe supplying working gas (nitrogen) to the cylinder is installed on the cylinder. A piston is mounted in the cylinder, which divides the cylinder chamber into an upper
part - above the piston - and a lower part - under the piston. A spring is attached to the piston and upper body, the side edges of which are resting on the inner surface of the cylinder.
In the lower part of the body, a truncated cone is installed, in which a tube with a liquid distribution nozzle attached inside the lower chamber is mounted.
In the developed solution, the nozzle has the shape of a truncated cone with holes arranged radially on the forming cone and an opening located axially on the face of the nozzle.
The piston is equipped with a socket, the shape of which corresponds to the shape of the nozzle.

**Principle of pressure stabilizing device work**

The fluid medium pumped by a piston or plunger pump, including non-Newtonian fluid or suspension, is fed to the pulsation damper via a conduit connected to the inlet of the fitting 14 embedded in the sleeve 13. Then the liquid flows through the pipe 15 and the nozzle 16, thereby filling the lower chamber 11 under the piston 9. The task of the nozzle 16 is to mix, form and direct the liquid stream so that it rinses the inner walls of the cylinder 4 and puts the elastic element 12 into additional vibrations that will intensify the process of mechanical cleaning of the inner surfaces of the cylinder 4.

**Fig. 3. Pressure stabilizing device [8]:**
1 - body, 2 - annular groove, 3 - rubber ring, 4 - cylinder, 5 - connecting screws, 6 - head, 7 - annular groove, 8 - O-ring, 9 - piston, 10 - upper chamber above the piston, 11 - lower chamber below the piston, 12 - spring element, 13 - conical sleeve, 14, 18 - inlet, 15 - pipe, 16 - nozzle, 17 - inspection hole, 19 - plug, 20 - intersection, 21 - pressure gauge, 22, 23 - nozzle holes, 24 - connector, 25 - socket
Continuous pressure change caused by the pump action affects the piston 9, which moves axially up and down along the cylinder 4. The change in piston position 9, caused by the change in the volume of the lower chamber 11 relative to the upper chamber 10, allows the pulsation of the pumped liquid to be suppressed by compressing and the expansion of the gas in the upper chamber 10 above the piston 9. The upward and downward moving piston 9 sets in motion a spring element 12, the edges of which rub against the inner surface of the cylinder 4, causing its mechanical cleaning. The spring element 12 is made of a spirally wound elastic material, the cross section of which may have the outline of a circle, square, rectangle, triangle, trapezoid and their derivatives with concave or convex sides.

**Calculations of the pressure stabilizing device**

The first stage of calculations of the pressure stabilizing device was to determine the volume of the working gas, on the basis of which the overall dimensions of the piston and cylinder height were determined. In order to determine the minimum required volume of working gas, the applications of producers of commercially available devices suppressing pulsations of the working medium [5, 6] and work [7], comprehensively describing the phenomena were used.

**TABLE II. Parameters for determining the volume of working gas in the chamber of the pressure stabilizing device**

| Parameter                          | Value       |
|------------------------------------|-------------|
| Temperature                        | 20°C        |
| Pump capacity                      | 400 L/min   |
| Pump type                          | Single Acting |
| Number of pump cycles              | 53/min      |
| Number of cylinders                | 2 pieces    |
| Pumping pressure                   | 40 bar      |
| Residual pulsation                 | 8.1%        |

**TABLE III. Input data and calculation procedure for the dimensions of the pressure stabilizing device**

| Input data                          | Value       |
|-------------------------------------|-------------|
| Working pressure                    | $P_p = 40$ bar|
| Piston diameter                     | $d_t = 120$ mm|
| Minimal gas density                 | $v_k = 15$ L  |

**Calculations**

**Piston surface area**

$A_k = \pi \cdot \left(\frac{d_t}{2}\right)^2$

$A_k = 11309.7$ mm$^2$

**Cylinder height**

$h_k = \frac{v_k}{\pi \cdot \left(\frac{d_t}{2}\right)^2}$

$h_k = 1326.3$ mm

**Force on the piston**

$F_k = P_p \cdot A_k$

$F_k = 45.2$ kN

**Corrosion allowance**

$C = 2$ mm

**Strength factor**

$k_r = 14$ MPa, $z = 1$ mm

**Cylinder wall thickness**

$g = \frac{P_p \cdot d_t}{(2.3 \cdot k_r - P_p) \cdot z} + C$

$g = 3.24$ mm

**Bottom thickness**

$h_d = 0.433 \cdot d_t \cdot \frac{P_p}{k_r}$

$h_d = 8$ mm

Data used to determine the volume of working gas in the chamber of the pressure stabilizing device is presented in tab. II.
The following calculation results were obtained: minimum working gas volume ~10÷15 l, initial loading pressure 24 bar. Knowing the volume of working gas, a piston diameter of °120 mm was chosen, on the basis of which the cylinder height of the pressure stabilizing device was determined. The input data and the calculation procedure of other overall dimensions of the pressure stabilizing device are presented in tab. III.

**Selection of materials from which the pressure stabilizing device will be made**

After calculating the minimum working gas volume and overall dimensions of the device for stabilizing the working pressure, the type of material and overall dimensions of the semi-finished products, from which the device will be built, were selected. They are listed in tab. IV.

**TABLE IV. Material type and overall dimensions of blanks**

| Part            | Material | Dimensions, mm |
|-----------------|----------|----------------|
| Head            | C45      | 160 × 160 × 35 |
| Body            | C45      | 200 × 160 × 100|
| Cylinder        | St52.3   | Ø120H8 × 1400  |
| Conical sleeve  | C45      | Ø150 × 80      |
| Piston          | C45      | Ø130 × 85      |
| Pipe            | C45      | Ø60 × 500      |
| Nozzle          | C45      | Ø150 × 80      |

**Machining the elements of the pressure stabilizing device**

Fig. 4 presents selected components of the pressure stabilizing device.

![Fig. 4. Parts of the pressure stabilizing device](image)

**Summary**

The design and assembly works carried out, aimed at developing and building a device for stabilizing the working pressure of cement slurry, which is used in DSM technology, indicate that the construction assumptions have been met.

Fig. 5 compares the 3D model with a built-in pressure stabilizing device. We have managed to develop a device that has the ability to self-clean during continuous operation. Preliminary tests have shown that the nozzle with the holes arranged radially on the forming cone directs the liquid stream as intended, causing the cylinder walls to be rinsed and cleaned. The solution became the subject of a patent application entitled "Pressure pulsation damper" [8].
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