Modelling the kinked jet of the Crab nebula

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ABSTRACT
We investigate the dynamical propagation of the South-East jet from the Crab pulsar interacting with supernova ejecta by means of three-dimensional relativistic magnetohydrodynamic (MHD) numerical simulations with the PLUTO code. The initial jet structure is set up from the inner regions of the Crab nebula. We study the evolution of hot, relativistic hollow outflows initially carrying a purely azimuthal magnetic field. Our jet models are characterized by different choices of the outflow magnetization (σ parameter) and the bulk Lorentz factor (γj). We show that the jet is heavily affected by the growth of current-driven kink instabilities causing considerable deflection throughout its propagation length. This behaviour is partially stabilized by the combined action of larger flow velocities and/or reduced magnetic field strengths. We find that our best jet models are characterized by relatively large values of σ (>1) and small values of γj ≲ 2. Our results are in good agreement with the recent X-ray (Chandra) data of the Crab nebula South-East jet indicating that the jet changes direction of propagation on a time-scale of the order of few years. The 3D models presented here may have important implications in the investigation of particle acceleration in relativistic outflows.

Key words: instabilities – MHD – shock waves – pulsars: individual: Crab nebula – ISM: jets and outflows.

1 INTRODUCTION
Pulsars lose their rotational energy through a relativistic wind of waves and particles. The interaction of these outflows with the surrounding ambient produces Pulsar Wind Nebulae (PWNe), observable from radio to γ-rays. PWNe often show a torus–jet structure [see e.g. Kargaltsev & Pavlov (2008) for a review, and the Chandra images of the Crab, Vela and B1509-58 Nebulae]. Several theoretical (Lyubarsky & Kirk 2001; Lyubarsky 2002; Pétri & Lyubarsky 2007) and numerical (Komissarov & Lyubarsky 2003; Del Zanna et al. 2006; Del Zanna, Amato & Bucciantini 2004, hereafter dZAB04) studies attempted to explain and reproduce this structure.

The Crab nebula is surely the most popular and studied PWN. It is powered by a pulsar with a very large spin-down luminosity, Lsd = 5 × 1038 erg s−1, that is carried away by a relativistic and highly magnetized wind. According to estimates of the number of pairs emitted by the Crab Pulsar, the energy flux carried by the wind is dominated by the Poynting flux while close to the star, and dominated by the particles when close to the termination shock (Kennel & Coroniti 1984). First theoretical (Kennel & Coroniti 1984) and numerical (Komissarov & Lyubarsky 2003; dZAB04) studies suggested that the magnetization parameter, defined as the ratio between the Poynting flux and the kinetic energy of the particles, should lie in the range 10−3 ≤ σ ≤ 10−2 at the termination shock.

Low values are required to avoid the excessive axial compression of high σ one-dimensional (1D) and two-dimensional (2D) models, that push the pulsar wind termination shock too close to the pulsar (Lyubarsky 2012; Komissarov 2013). Nevertheless, as recently pointed out by Porth, Komissarov & Keppens (2013), three-dimensional (3D) high-σ models of PWN have the same morphology of 2D axisymmetric low-σ models owing to the presence of kink instabilities (Begelman 1998) that reduce the axial compression and lead to uniform pressure within the Nebula. In addition, a lateral dependence of the wind magnetization, that increases towards the axis yielding σ ≥ 1 close to the poles, was proposed by recent investigations (Lyubarsky 2012; Komissarov 2013). In these models, the Nebula and the jet would be therefore injected with a highly magnetized plasma, and they would be regions of strong magnetic dissipation (Komissarov 2013; Porth et al. 2013).

Unexpectedly, the Crab nebula produces strong and day-long γ-ray flares (Abdo et al. 2011; Tavani et al. 2011; Striani et al.

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1 The Crab nebula average magnetic field is $B \simeq 0.2$ mG.

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solvers. For the present purpose we employ the HLLD Riemann solver of Mignone, Ugliano & Bodo (2009) and revert to the HLL solver in the presence of strong shocks following the hybrid approach described in the appendix of Mignone et al. (2012). The divergence-free condition of the magnetic field is accurately treated using the constrained transport method.

2.2 Initial and boundary conditions

Our initial conditions draw upon the same configuration used by dZAB04 where a freely expanding supernova remnant (SNR) initially fills the region \( 0.2 < r/r_\text{ej} < 1 \) where \( r \) is the spherical radius and \( r_\text{ej} = 1 \) ly (see Fig. 2). The supernova ejecta is unmagnetized with total mass given by

\[
M_\text{ej} = \int_0^1 \rho_\text{ej} 4\pi r^2 \, dr ,
\]

and a radially increasing velocity profile \( v_z = v_\text{ej} r/r_\text{ej} \) where \( v_\text{ej} \) is fixed by the condition

\[
E_\text{ej} = \int_0^1 \frac{1}{2} \rho_\text{ej} v_z^2 4\pi r^2 \, dr .
\]

Here we take \( M_\text{ej} = 3M_\odot \) and \( E_\text{ej} = 10^{51} \, \text{erg} \) in accordance with equations (5) and (6) of dZAB04. Further out, for \( r/r_\text{ej} > 1 \), the fluid is uniform and static with density and pressure values representative of the interstellar medium (ISM), i.e. \( \rho_\text{ism} = 1 \times 10^4 \, \text{cm}^{-3} \) and \( p = 10^{-10} \rho_\text{ism} c^2 \), where \( m_p \) is the proton mass.

Differently from dZAB04, however, we do not include the PWN for \( r/r_\text{ej} < 0.2 \) but consider, instead, a static hot plasma region where jet acceleration is assumed to take place. Density and pressure in this region are denoted with \( \rho_s \) and \( p_s \) while the magnetic field is absent (see also Fig. 2).

As the acceleration mechanism cannot be consistently described within our model, we assume that the jet has already formed as the result of the magnetic hoop stress and collimation processes taking place around the polar axis. For this reason, the jet is modelled as a continuous injection of mass, momentum, magnetic field and energy from the lower z-boundary inside the circular nozzle \( R < R_j \) where \( R = \sqrt{x^2 + y^2} \) is the cylindrical radius and \( R_j = 3 \times 10^{16} \, \text{cm} \) is the jet radius. Here inflow values are prescribed in terms of constant density \( \rho_j = \rho_s \) and axial velocity

\[
v_z(R) = \sqrt{1 - \frac{1}{\gamma_j^2}} ,
\]

where \( \gamma_j \) is the bulk Lorentz factor.

Since present axisymmetric models of PWN adopt a purely toroidal field we initialize the magnetic field to be azimuthal with the following radial profile (Komissarov 1999; Mignone et al. 2009):

\[
B_\phi(R) = \begin{cases} 
B_m \frac{R}{a} & \text{for } R \leq a , \\
B_m \frac{a}{R} & \text{for } R > a ,
\end{cases}
\]

where \( a \) encloses a cylinder carrying a constant current and \( B_m \) sets the magnetic field strength. We take \( a = R_j/2 \) and fix the value of \( B_m \) from the jet magnetization parameter \( \sigma \):

\[
\sigma = \frac{\bar{B}^2}{4\pi \rho_j \gamma_j^2} ,
\]

where \( \bar{B}^2 = B_m^2 a^2 (1 - 4 \log a)/2 \) is the average magnetic energy inside the beam.

The gas pressure is recovered from the radial momentum balance across the jet which, in absence of rotations, takes the form

\[
\frac{dp}{dR} + \frac{1}{R^2} \frac{d}{dR} \left( \frac{R^2 B_\phi^2}{8\pi \gamma^2} \right) = 0 ,
\]

where, for simplicity, a constant value of \( \gamma = \gamma_j \) is used. The previous equation has solution

\[
p(R) = \begin{cases} 
\rho_s + \frac{B_m^2}{4\pi \gamma_j^2} \left( 1 - \frac{R^2}{a^2} \right) & \text{for } R \leq a , \\
\rho_s & \text{for } R > a ,
\end{cases}
\]

where \( \rho_s \) is the ambient pressure determined by flow Mach number \( M_s = v_z/c_{s, \text{amb}} \). Note that in this configuration the pressure is maximum on the axis and monotonically decreases until \( R = a \) where it matches the ambient pressure. The maximum value is obtained from equation (11) with \( R = 0 \) and it takes the value

\[p_s = p(0) = \rho_s + B_m^2/(4\pi \gamma_j^2) .\]

Consequently, highly magnetized jets also possess larger internal energies (see Table 1).

Figure 2. 2D schematic representation of the initial condition. The jet enters from the nozzle at the bottom boundary into a hot cavity region confined by the SNR expanding into the outer ISM. Tick labels are given in units of the jet radius \( R_j \).
Table 1. Simulation cases describing our initial jet configuration. While $\gamma_j$ and $\sigma$ are the primary parameters used in our model we also give the derived values of magnetic field strength ($B_0$, fourth column), ambient pressure ($\rho_i$, fifth column), on-axis pressure ($p_j$, sixth column) and the ratio between average thermal and magnetic pressures (plasma $\beta$, last column).

| Case | $\gamma_j$ | $\sigma$ | $B_0 / \sqrt{4\pi \rho_j c^2}$ | $p_n / \rho_j c^2$ | $p_j / \rho_j c^2$ | $\beta$ |
|------|------------|----------|-------------------------------|--------------------|-------------------|--------|
| A1   | 2          | 0.1      | 0.92                          | 0.88               | 1.09              | 4.53   |
| A2   | 2          | 1        | 2.91                          | 0.88               | 3.00              | 0.57   |
| A3   | 2          | 10       | 9.21                          | 0.88               | 22.1              | 0.18   |
| B1   | 4          | 0.1      | 1.84                          | 9.07               | 9.28              | 11.37  |
| B2   | 4          | 1        | 5.83                          | 9.07               | 11.2              | 1.17   |
| B3   | 4          | 10       | 18.4                          | 9.07               | 30.3              | 0.15   |

As axisymmetric models of PWN predict hot and hollow jets, we prescribe the jet mass density to be $\rho_j = n_j m_p$, with $n_j = 10^{-3}$ cm$^{-3}$ and set the sonic Mach number $M_s = 1.7$. In such a way the initial density contrast between the SNR and the jet is $\approx 10^6$. Conversely, we leave $\gamma_j$ and $\sigma$ as free parameters and perform computations with two different values of $\gamma_j = 2, 4$ and three different magnetizations $\sigma = 0.1, 1, 10$ for a total of six cases, as shown in Table 1. This choice of parameters is consistently based on the results obtained from the 2D axisymmetric simulations of dZAB04 (also repeated by our group with good agreement) from which comparable values of density, pressure and magnetic fields could be inferred.

In the injection nozzle, we perturb the transverse velocities by introducing pinching, helical and fluting modes with corresponding wave numbers $m = 0, 1, 2, 3$ and low-frequency ($l = 5, \ldots, 8$) modes are given by $\omega_l = c_l/(1/2, 1, 2, 3)$ and $\omega_l = c_l/(0.03, 0.06, 0.12, 0.25)$. The amplitude of the perturbation is chosen in such a way that the fractional change in the Lorentz factor is $\epsilon = 0.05$:

$$v_x = \frac{A}{24} \sum_{m=0}^{2} \sum_{l=1}^{8} \cos (m \phi + \omega_l t + b_l)$$  \hspace{1cm} (12)

where $b_l$ are randomly chosen phase shifts while high- ($l = 1, \ldots, 4$) and low-frequency ($l = 5, \ldots, 8$) modes are given by $\omega_l = c_l/(1/2, 1, 2, 3)$ and $\omega_l = c_l/(0.03, 0.06, 0.12, 0.25)$. The amplitude of the perturbation is chosen in such a way that the fractional change in the Lorentz factor is $\epsilon = 0.05$:

$$A = \sqrt{(1+\epsilon)^2 - 1} / \gamma(1+\epsilon).$$  \hspace{1cm} (13)

The computational domain is defined by the Cartesian box $x, y \in [-L/2, L/2]$ and $z \in [0, L_z]$ with $L = 50R_j$ and $L_z = 80R_j$ covered by $320 \times 320 \times 768$ computational cells. The grid resolution is uniform in the $z$ direction and inside the region $|x|, |y| < 10$ where $192 \times 192$ zones are used. The grid spacing increases geometrically outside this region up to the lateral sides of the domain.

We employ outflow (i.e. zero-gradient) boundary conditions on the $x$ and $y$ sides of the computational box as well as on the top $z$ boundary. In the ghost zones at the bottom $z$ boundary and outside the injection nozzle, we set $v_x, B_x$ and $B_y$ to be anti-symmetric with respect to the $z = 0$ plane while the remaining quantities are symmetric. Fluid variables inside and outside the nozzle are then smoothly joined using a profile function:

$$q = q_j + \frac{q_j - q_i}{\cosh (R/R_j)} \tau,$$  \hspace{1cm} (14)

where $q_i$ is a fluid variable value inside the nozzle, and $q_j$ is the symmetric (or anti-symmetric) value with respect to the $z = 0$ plane. Finally, we use $n = 8$ for density, velocity, pressure and vertical component of the field while $n = 6$ is used for $B_x$ and $B_y$.

3 RESULTS

The six simulation cases introduced in Table 1 show remarkable differences in several aspects such as the propagation velocity, large-scale morphology, interaction and mixing with the environment. These will be discussed in the following.

As the computations produced a significant amount of data (≈8TB) an efficient post-processing analysis is crucial in order to reduce and extract relevant quantitative results. Our experience has shown that several morphological and dynamical aspects can be readily interpreted by means of horizontally averaged quantities defined as

$$\bar{Q}(t, z) = \langle Q(x, t) \rangle \equiv \frac{\int Q(x, t) \chi \, dx \, dy}{\int \chi \, dx \, dy},$$  \hspace{1cm} (15)

where integration is performed over horizontal planes at constant $z$, $Q(x, t)$ can be any flow quantity, $\chi = (x, y, z)$ is the position vector and $\chi$ is a weight (or filter) function used to include or exclude certain regions of the flow according to specific criteria.

We select, for instance, computational zones containing more than 50 per cent of the jet material and moving at least at 25 per cent of the speed of light using

$$\chi_j = \begin{cases} T & \text{for } T > 0.5 \text{ and } |v| > 0.25, \\ 0 & \text{otherwise}, \end{cases}$$  \hspace{1cm} (16)

where $T$ is the passive scalar obeying equation (4).

3.1 Overall features

During the very early phases of evolution, the jet propagates almost undisturbed until it impacts the backward dense layers of the SNR. From this time on (typically $\approx 1$ year), we observe a drastic deceleration as the jet pushes against the much heavier material of the remnant.

After a few tens of years, the typical structure consists of a large over-pressurized turbulent cocoon enclosing a collimated magnetized central spine moving at mildly relativistic velocities. This is illustrated in Fig. 3 where a volume rendering of thermal pressure and magnetization parameter $\sigma$ is shown for each of the six cases at the end of the simulation.\footnote{A collection of movies for the simulation cases presented here can be found at http://plutocode.ph.unito.it/\CrabJet/}.

The cocoon appears to be weakly magnetized and the field remains mainly concentrated in the beam (a similar structure is also observed in the 2D simulations of dZBL04) preserving the initial toroidal structure. Along the jet spine the flow experiences a series of acceleration and deceleration phases owing to the presence of conical recollimation shock waves (or working surfaces) corresponding to regions of jet pinching.

The large-scale morphology is characterized by elongated curved structures which, depending on the case, may considerably depart from axial symmetry. The amount of bending and twisting varies according to the combination the flow Lorentz factor and magnetization ($\sigma$) and it is described in more detail in Section 3.3.

3.1.1 Jet position

Fig. 4 shows the jet head position as a function of time, measured as the maximum height $z(t)$ at which jet material has propagated.
Figure 3. 3D contour surfaces of the gas pressure (blue) and $\sigma$ parameter (orange) for the six jet configurations. Tick labels are given in units of the jet radius, $R_j = 3 \times 10^{16}$ cm. Low-speed jets with $\gamma_j = 2$ (Cases A1, A2 and A3) are shown, from left to right, in the top panel, while high-speed jets with $\gamma_j = 4$ (Cases B1, B2 and B3) are shown in the bottom panel. Snapshots are taken at different times when the jet has approximately reached the end of the computational domain.

Figure 4. Jet head position as a function of time for the six simulation Cases A1, A2, A3 (black, green and red solid lines) and B1, B2, B3 (corresponding dashed lines). The thin dotted line on the left represents the position of the outer supernova shock. Low-speed jets advance slowly ($0.016 \lesssim v_{\text{head}}/c \lesssim 0.023$) owing to the large density contrast and evolve entirely within the remnant confined by the outer SN shock (see Fig. 2). For increasing magnetization the propagation is driven by the additional magnetic pressure support while the mechanism of instability tends to saturate. Conversely, jets with larger $\gamma_j$ (Cases B1, B2 and B3) advance more rapidly ($0.05 \lesssim v_{\text{head}}/c \lesssim 0.078$) and cross the outer SN shock (dotted line) at earlier times ($t < 50$ yr) where they suddenly accelerate because of the reduced density contrast. In particular, owing to its low magnetization and relatively large kinetic energy, the B1 jet is very little affected by the growth of CD modes and its trajectory remains essentially parallel to the axis. With increasing magnetization, the jets in Cases B2 and B3 are slowed down by appreciable bendings of the flow direction and show comparable propagation speeds.

3.2 Jet internal structure

The jet structure does not remain homogeneous during its propagation but, rather, shows substantial variations of several fluid quantities all along its length. Broadly speaking, we are able to identify two regions with different properties. In the back-end region, close to
3.2.1 Pinching.

A common feature that can be identified all along the jet is the presence of pinching regions corresponding to the formation of magnetized shock waves. These can be distinguished, for instance, by looking at the horizontally averaged electromagnetic and matter kinetic energies

\[
E_{\text{em}}(t, z) = \left\langle \frac{B^2 + E^2}{8\pi}, \chi_j \right\rangle 
\]

(17)

\[
E_{\text{kin}}(t, z) = \left\langle \rho \gamma (\gamma - 1), \chi_j \right\rangle ,
\]

(18)

where the weight function \( \chi_j \) selects only material that is mainly composed by jet particles (see equation 16).

In Fig. 6 we plot \( E_{\text{em}}, E_{\text{kin}} \) and the maximum Lorentz factor \( \gamma_{\text{max}} \) (taken on xy planes) as functions of \( z \) just before the jet has exited the computational domain or encountered the outer supernova shock. Average magnetic and kinetic energies exhibit quasi-periodic oscillations along the beam due to jet pinching with the corresponding formation of internal shocks with large compression factors. These cycles are more evident in the slowly moving jets that reveal shocks with larger strengths. Here the frequency of oscillations increases with \( \sigma \) and magnetic fields tend to dissipate more rapidly.

Indeed, as discussed in Mignone et al. (2010), the presence of a dominant azimuthal magnetic field component prevents the inner jet core from interacting with the surrounding, thus substantially reducing the loss and transfer of momentum. The net effect of this shielding mechanism is to sustain the kinetic energy at the expenses of magnetic energy, thus leading to a significant decrease of \( \sigma \) along the beam. This is best illustrated in Fig. 7, where we show a 2D colour distribution map of the horizontally averaged \( \sigma \) parameter normalized to its initial value.

3.2.2 Fragmentation

As the jet advances into the remnant, the propagation is accompanied by the formation of highly intermittent unstable structures during which jet fragmentation is frequently observed. These events take place on a short time-scale (typically less than a year) and in correspondence of large kinked deflection where the jet beam temporarily breaks down forming strong intermediate shock waves resembling the main termination shock. A typical example is

Figure 5. Volume rendering of the magnitude of the current density \( J = \nabla \times B/(4\pi) \) for the A3 jet, at \( t = 89.48 \text{ yr} \) showing the formation of helical structures in the front-end regions.

Figure 6. Average profiles of the electromagnetic (top) and kinetic (middle) energies normalized to their initial value at \( z = 0 \) as functions of the vertical distance \( z \) at different times (reported in the legend) for the six simulation cases. The bottom panel shows the maximum Lorentz factor. Regions of strong compression are evident by the quasi-periodic oscillations. The Lorentz factor grows immediately upstream of the shocked flow where magnetic and kinetic energies are smaller and drops discontinuously in the post-shock regions.
of, e.g., the \( \sigma \) parameter might have a relation with the synchrotron signature, although some hints of such structures are present in the X-ray maps of the jet terminal part (see left panel in Fig. 14). On the other hand, the locations of our jets that correspond to higher values of the jet terminal part (see right panel in Fig. 14). On the other hand, the locations of our jets that correspond to higher values of \( \sigma \) do not have an equivalent observed optical or X-ray rendering of the \( \sigma \) illustrated in Fig. 8 where we show, from left to right, a volume rendering of the \( \sigma \) parameter normalized to the initial injection value as a function of time (abscissa, in years) and vertical height (ordinate, in light-years) for the six cases. Note the substantial decrease of \( \sigma \) in the more magnetized cases (A3 and B3).

We point out that the features produced in our jet fragmentation (hot-spots) do not have an equivalent observed optical or X-ray signature, although some hints of such structures are present in the X-ray maps of the jet terminal part (see left panel in Fig. 14). On the other hand, the locations of our jets that correspond to higher values of \( \sigma \), the \( \sigma \) parameter might have a relation with the synchrotron processes responsible for the optical and X-ray emission. This issue will be further investigated in forthcoming studies.

### 3.2.3 Magnetic field topology.

In order to gain some insight on the topology of magnetic field, we first compute the average flow direction by integrating, for each \( z \), the velocity vector on horizontal planes:

\[
\hat{n}(z) = \frac{\langle \mathbf{v}, \chi_j \rangle}{|\langle \mathbf{v}, \chi_j \rangle|},
\]

with \( \chi_j \) defined by equation (16). We then decompose the magnetic field into components that are parallel and perpendicular to the direction given by \( \hat{n} \):

\[
\mathbf{B} = B_t \hat{n}(z) + B_{\perp},
\]

where \( B_t = \mathbf{B} \cdot \hat{n}(z) \) is the magnetic field component parallel to the horizontally averaged velocity vector and \( B_{\perp} \) is the component of the field perpendicular to it. The average cosine between magnetic field and mean flow direction is then simply obtained from:

\[
\bar{\theta}_{n,B} = \arccos \left( \frac{B_t}{|\mathbf{B}|} \chi_j \right).
\]

Fig. 9 shows that the magnetic field in the jet remains essentially perpendicular to the (average) flow trajectory for most of the jet length while it acquires a poloidal component immediately after the terminal reverse shock. This is confirmed by the direct 3D visualization of the magnetic field lines in proximity of the beam (shown in Fig. 10 for the A2 jet) which reveals that the field retains the initial toroidal shape that progressively evolves into a bent helical structure with a small pitch. Indeed, as mentioned in Section 3.2, the magnetic field acts as an effective screening sheath that hampers the development of small-scale perturbations at the interface between the jet and the surrounding.

### 3.3 Jet deflections

A remarkable feature observed in several runs is a curved trajectory featuring large time-dependent deflection of the jet beam away from the main longitudinal \( z \)-axis (see Fig. 3). As discussed by Mignone et al. (2010), this behaviour may be ascribed to the onset of CD instabilities triggered by the presence of a toroidal magnetic field component (see also Moll et al. 2008; Porth 2013). This result is confirmed by numerical investigations of infinitely long periodic jets adopting the same initial structure (Mignone et al., in preparation) revealing the presence of CD instabilities with a rapid growth of the \( m = 1 \) (or kink) mode.

We introduce a measure of the deflection radius \( \bar{R}(t, z) = \sqrt{\bar{x}(t, z)^2 + \bar{y}(t, z)^2} \) and the deflection angle \( \phi(t, z) = \tan^{-1}(\bar{y}(t, z)/\bar{x}(t, z)) \) by computing at each time and vertical height the centroids \( \bar{x}(t, z) \) and \( \bar{y}(t, z) \):

\[
\bar{x}(t, z) = \langle x, \chi_j \rangle, \quad \bar{y}(t, z) = \langle y, \chi_j \rangle,
\]

and choosing the weight function \( \chi_j \) as in equation (16).

Fig. 11 plots the maximum of \( \bar{R}(t, z) \) over the spatial coordinate \( z \) as a function of time. Cases A2 and A3 show the largest bendings reaching values in excess of \( \approx 20 \) jet radii. Although to a less degree, Cases B2 and B3 are also prone to appreciable wiggling (\( \bar{R}_{\text{max}} \approx 10 \)) whereas Case B1 propagates almost parallel to the main longitudinal axis with very weak bending of the beam.

A more detailed investigation is given in Figs 12 and 13 showing 2D coloured distribution maps of the deflection radius \( \bar{R} \) and angle \( \phi \) as functions of time and vertical coordinate. Jets become increasingly more flexed as they propagate from the injection region up to the head where they attain the largest deformations (Porth 2013). The shape of these deformed structures roughly resembles the morphological features that can be inferred from observational data. This is shown in Fig. 14 where we present a qualitative comparison between the X-ray Chandra observation of the terminal part of the jet in 2010 (top panel) and our simulated jet (Case A2, bottom panel).

For moderate and strong magnetizations in low-velocity jets (A2 and A3), the deflection keeps growing indefinitely during the course...
The kinked jet of the Crab nebula

Figure 8. Jet fragmentation for the A2 case illustrated through a sequence of close-by frames at $t \approx 93$ (left column), $t \approx 93.3$ (central column) and $t \approx 93.6$ (right column) years. From top to bottom the figure shows, respectively, the volume rendering of the $\sigma$ parameter, thermal pressure, current density magnitude $|J| = |\nabla \times B/(4\pi)|$ and bulk flow Lorentz factor.

of the simulation. In these cases we observe, for $t \lesssim 50$ yr, a change in the propagation direction on a time-scale of $\sim 10$ yr while, afterwards, jet material keeps flowing along a particular curved direction established by the large-scale backflow circulation pattern and changes direction very slightly. Here the inertia of the flexed jet becomes so effectively large that any restoring mechanism is unable to push the beam back along the main longitudinal axis. In the corresponding higher velocity cases (B2 and B3) the amount of bending...
Figure 9. Average angle between the magnetic field vector and the mean flow direction as a function of $z$ for Cases A1, A2 and A3 (solid lines). The dotted lines show the (approximate) position of the terminal reverse shock for the three cases. The evolution times correspond to those indicated in Fig. 3.

Figure 10. Magnetic field lines and pressure volume map for the A2 jet at $t \sim 130$ yr.

is reduced owing to the increased inertia which acts as a stabilizing factor. In these cases the jet changes its propagation angle by a large amount ($\approx 180^\circ$ or more) around the main longitudinal axis over a time period $\lesssim 40$ yr (see the right panels in Fig. 13).

We point out, however, that previous simulations (not shown here) have demonstrated that the evolution of the trajectory and the corresponding amount of deflection may be noticeably affected by the shape of the initial perturbation (given by equation 12).

Figure 11. Maximum radial deflection as a function of time for the different cases discussed in the text. Solid lines refer to Cases A1 (black), A2 (green) and A3 (red) while dashed lines refer to Case B1, B2 and B3, respectively.

We thus conclude that the magnetization parameter $\sigma$ plays a crucial role in destabilizing the jet: weakly magnetized configurations (A1 and B1) are less affected by the growth of instability than the corresponding moderately (A2 and B2) and highly (A3 and B3) magnetized models which show comparable growth rates. The effect of the Lorentz factor, on the other hand, is that of reducing the growth of instability, in accordance with the results obtained from the linear stability analysis of Bodo et al. (2013).

3.3.1 Flow direction

The change in the jet trajectory is associated with a corresponding variation of the average propagation velocity. We compute the average angle $\bar{\theta}$ between the velocity vector and the axial direction by integrating, on constant $z$-planes, the projected velocity:

$$\bar{\theta}_\pm = \cos\left(\frac{v_z, \pm}{|v|}, x_j\right),$$

(23)

where $v_z, + = \max(v \cdot \hat{e}_z, 0)$ and $v_z, - = \min(v \cdot \hat{e}_z, 0)$ are used to discriminate between jet material moving in the positive or negative vertical direction, respectively. In other words, $\bar{\theta}_+ \in [0, 90^\circ]$ gives a measure of the forward flow while $\bar{\theta}_- \in [90^\circ, 180^\circ]$ is associated with the backflow motion. The filter function is defined as usual (equation 16).

Fig. 15 shows a coloured distribution map of $\bar{\theta}_+$ as a function of time and vertical distance. In all cases, sudden changes in the trajectory occur at the jet head where magnetic field are amplified and the flow is abruptly decelerated through the termination shock. However, low-speed jets tend to assume a large-scale curved structure since the average propagation angle gradually changes from $\approx 0^\circ$ (straight propagation) close to the launching region up to $\approx 90^\circ$ at the jet head. Conversely, high-speed jets are stabilized by the larger Lorentz factor and propagate more parallel to the longitudinal axis building large kicks mainly in proximity of the jet head. Here the velocity is drastically reduced and the magnetic field is increased, thus de-stabilizing the motion.
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3.3.2 Backflow motion

The departure from axial symmetry produced by kinked deformations has the side effect of promoting a predominantly one-sided backflow motions along the negative $z$ direction. This is shown in Fig. 16 where we plot a 2D colour map of $\bar{\theta}$ (computed from equation 23) as a function of time and vertical height. Backflows are strongest in Case A1 and progressively lessen at larger magnetizations or for larger Lorentz factor cases (e.g. they are almost absent in the B1 jet). A 3D view is given in Fig. 17 for the small Lorentz factor jets. In the most prominent cases, the backflow is able to survive over a distance of $\approx 1$ ly and for several years before its kinetic energy is dissipated in the form of turbulent motion during the interaction with the ambient medium.

3.4 Dissipation

A crucial aspect in the modelling of magnetically driven outflows is the dissipation of magnetic fields at both large and small scales. This is discussed in the following sections.

Figure 12. 2D coloured distribution maps of the average deflection radius $\bar{R}$ (in units of the jet radius) as a function of time (abscissa, in years) and vertical height (ordinate, in light-years) for the six simulated cases. The amount of deflection at a given time $t$ and height $z$ is quantified by a different colour given by the varied shades of blue ($\bar{R} \in [0, 5]$), green ($\bar{R} \in [5, 10]$), orange ($\bar{R} \in [10, 15]$) and red ($\bar{R} \in [15, 20]$).

Figure 13. 2D coloured distribution maps (similar to Fig. 12) of the average deflection angle $\bar{\phi}$ as a function of time (abscissa, in years) and vertical height (ordinate, in light-years) for the six simulated cases.

3.4.1 Large-scale dissipation

Energy dissipation at large scale may be quantified by comparing the electromagnetic to thermal energy ratios inside the jet with that of the turbulent cocoon. We distinguish the two regions by taking advantage of the passive scalar $T$ and choosing different weight functions. Inside the jet we compute

$$\bar{E}_{\text{em},j} = \left\langle \frac{B^2 + E^2}{8\pi}, \chi_j \right\rangle, \quad \bar{E}_{\text{th},j} = \left\langle \frac{p}{\Gamma - 1}, \chi_j \right\rangle,$$

(24)

with $\chi_j$ defined by equation (16). This choice ensures that only high-velocity regions containing more than 50 per cent of the jet material are included. On the other hand, in the environment we define

$$\bar{E}_{\text{em},e} = \left\langle \frac{B^2 + E^2}{8\pi}, \chi_e \right\rangle, \quad \bar{E}_{\text{th},e} = \left\langle \frac{p}{\Gamma - 1}, \chi_e \right\rangle,$$

(25)

using $\chi_e = 1$ when $T < 1/2, |v| > 0.01$ which includes moving material that has already mixed. The ratio $\bar{E}_{\text{em}}/\bar{E}_{\text{th}}$ is plotted for the jet (solid lines) and the environment (dash–dotted lines) in Fig. 18 at the end of each simulation case, just before reaching the end of the computational domain. Inside the jet, the ratio between magnetic and thermal energies presents gradually decreasing quasi-periodic
oscillations (see Section 3.2) that drop sharply at the jet termination shock. Conversely, the energy distribution proportions inside the cocoon are more homogeneous and settle down to approximately the same values ($\lesssim 10$ per cent) independently of the value of jet $\sigma$. This demonstrates that both Poynting and kinetic energy fluxes are efficiently diverted at the termination shock and thereafter scattered and dispersed via the backflow to feed the cocoon. During this process the field becomes significantly randomized and the energy distributions reach a state far from equipartition, independently of the initial magnetization. From this perspective, jets appear to be a very efficient way to dissipate magnetic energy through the interaction of the head of the jet with the surrounding remnant.

### 3.4.2 Small-scale dissipation

Although our simulations do not include dissipation mechanisms other than numerical that acts at the cell size, it is instructive to localize strong current sheets that may host regions where particle acceleration is likely to take place. In Fig. 19 we plot the maximum value of the current density, $J_{\text{max}}(z) = \text{max}_{xy} |\nabla \times \mathbf{B}|/(4\pi)$ as a function of the vertical height at three successive simulation times for the A2 and A3 jets. Current peaks take place in regions of strong pinching where the flow is shocked. According to the broad distinction of back-end and front-end regions given in Section 3.2, these structures may have considerably different lifetimes. While the inner regions of the jet have reached a quasi-steady periodic structure with little time-variability, the outer regions reveal the formation of short-lived current peaks that diffuse on a time-scale which is of the same order or less than our temporal resolution, approximately $\sim 3.8$ months. The 3D spatial distribution of the current density, corresponding to the dashed line in the bottom panel of Fig. 19, is shown at $t = 64.73$ yr in Fig. 20 for the A3 jet. Note that the formation of the strong current peak at $z \approx 1$ ly occurs concurrently with the development of a jet kink and the abrupt change of flow direction. The sudden rise of these localized current peaks favours the formation of reconnection layers where induced electric fields may lead to efficient particle acceleration. This possibility will be addressed in future works.
Figure 16. Same as Fig. 15 but for the negative \( z \) direction. In this case, \( \dot{\theta} \) ranges from 90\(^\circ\) (white) to 180\(^\circ\) (dark red).

4 SUMMARY

In this work, we have presented numerical simulations of 3D relativistic magnetized jets propagating into a heavier SNR. The proposed jet models aim at investigating the dynamics and morphology of the bipolar outflows observed in the Crab nebula. Our initial configuration stems from the results of previous 2D axisymmetric numerical models of PWNe (dZAB04) that predict the formation of hot under-dense jets as the result of the magnetic hoop stress collimation process. Using these models to constrain our input parameters, we have performed numerical simulations of jets initially carrying a purely azimuthal field by varying the bulk flow Lorentz factor \( \gamma \) and the ratio between Poynting and kinetic energy fluxes (\( \sigma \)) at the injection region.

Our results show that jets with moderate/high magnetic fields (\( 1 \lesssim \sigma \lesssim 10 \)) are prone to large-scale non-axisymmetric CD instabilities leading to prominent deflections of the jet beam away from the axis. This effect is enhanced by the high-density contrast (\( \sim 10^6 \)) between the jet and the SNR which leads to the formation of a strongly perturbed beam and largely over-pressurized cocoons. The typical time-scale for the formation of these curved patterns is, for the representative parameters adopted in our model, of the order of a few years and thus compatible with observations. While the \( |m| = 1 \) kink mode is mainly responsible for the formation of non-axisymmetric morphologies, the presence of axial pinch modes engenders a knotty structure with a chain of strong intermediate shocks with large compression factors. High variability is observed in the outer regions where the dynamics is strongly influenced by the interaction of the jet material with the ambient medium. Here rapid variations of the flow properties are characterized by the formation of intermediate magnetized shocks in proximity of sudden kinked deflection of the flow trajectory. These are short-lived episodes leading to the formation of intermittent unstable structures such as sporadic jet fragmentation or strong reconnection layers on a time-scale of a few months.

Our computations demonstrate that the development of these unstable patterns is more pronounced in relatively low-\( \gamma \) jets (\( \gamma_j \approx 2 \)) which show the largest deflections and evolve entirely inside the remnant. Conversely, jets with larger Lorentz factor (\( \gamma_j \gtrsim 4 \)) propagate with larger inertia, are less affected by the growth of pinch or kink modes and drill out of the remnant in less than 50 years. Furthermore, jets with low magnetic fields (\( \sigma \approx 0.1 \)) are weakly affected by the onset of CD modes and tend to propagate more parallel to the longitudinal axis.

Based on our relativistic 3D MHD simulations, for the first time we can conclude that moderate to high-\( \sigma \) jets with relatively small Lorentz factors (Case A2 and A3) are the most likely candidates to
Figure 18. Ratio between average electromagnetic and thermal energies inside the jet (solid lines) and outside in the cocoon (dot–dashed). Plots in the top and bottom panels refer to the slower and faster jet cases, respectively.

Figure 19. Maximum current density taken over \( xy \) planes as a function of \( z \) for the A2 jet (top) and A3 jet (bottom). The solid, dashed and dotted lines mark, respectively, three different close-by simulation times reported in the corresponding legends. The largest peaks are shown by the dashed lines.

Figure 20. 3D contour plot of the current density after \( t = 64.73 \text{ yr} \) for the A3 jet. Six surfaces of constant current density are displayed using different colours; see the attached legend. The current peak at \( z \approx 1 \text{ ly} \) corresponds to the one shown by the dashed line in the bottom panel of Fig. 19.

account for the dynamical behaviour observed in the Crab nebula jet. In particular, the change in orientation of the jet recently noticed (Weisskopf et al., in preparation) can be reproduced by our simulations. Our findings are complementary to 3D numerical calculations (Mizuno et al. 2011; Porth et al. 2013) studying the effects of large values of \( \sigma \) in pulsar winds.

Future extensions of this work will take into account the full 3D structure of the PWN, allowing us to model the jet launching region and the collimation process. Furthermore, our results can be used as a starting point for a detailed analysis of the impulsive particle acceleration mechanism in the Crab nebula as due to induced electric fields at the localized reconnection layers in the termination zone of the jet.

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