Theoretical prediction of Reynolds stresses and velocity profiles for barotropic turbulent jets

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Abstract – It is extremely uncommon to be able to predict the velocity profile of a turbulent flow. In two-dimensional flows, atmosphere dynamics, and plasma physics, large-scale coherent jets are created through inverse energy transfers from small scales to the largest scales of the flow. We prove that in the limits of vanishing energy injection, vanishing friction, and small-scale forcing, the velocity profile of a jet obeys an equation independently of the details of the forcing. We find another general relation for the maximal curvature of a jet and we give strong arguments to support the existence of a hydrodynamic instability at the point with minimal jet velocity. Those results are the first computations of Reynolds stresses and self-consistent velocity profiles from the turbulent dynamics, and the first consistent analytic theory of zonal jets in barotropic turbulence.

Theoretical prediction of velocity profiles of inhomogeneous turbulent flows is a long-standing challenge, since the nineteenth century. It involves closing hierarchy for the velocity moments, and for instance obtaining a relation between the Reynolds stress and the velocity profile. Since Boussinesq in the nineteenth century, most of the approaches so far have been either empirical or phenomenological. Even for the simple case of a three-dimensional turbulent boundary layer, plausible but so far unjustified similarity arguments may be used to derive von Kármán logarithmic law for the turbulent boundary layer (see for instance [1]), but the related von Kármán constant [2] has never been computed theoretically. Still this problem is a crucial one and has some implications in most of scientific fields, in physics, astrophysics, climate dynamics, and engineering. Equations (6), (7), (9), and (11) are probably the first prediction of the velocity profile for turbulent flows, and relevant for barotropic flows.

In this paper we find a way to close the hierarchy of the velocity moments, for the equation of barotropic flows with or without effect of the Coriolis force. This two-dimensional model is relevant for laboratory experiments of fluid turbulence [3], liquid metals [4], plasma [5], and is a key toy model for understanding planetary jet formation [6] and basics aspects of plasma dynamics on Tokamaks in relation with drift waves and zonal flow formation [7]. It is also a relevant model for Jupiter troposphere organization [8]. Moreover, our approach should have future implications for more complex turbulent boundary layers, which are crucial in climate dynamics in order to quantify momentum and energy transfers between the atmosphere and the ocean.

It has been realized since the sixties and seventies in the atmosphere dynamics and plasma communities that in some regimes two-dimensional turbulent flows are strongly dominated by large-scale coherent structures. Jets and large vortices are often observed in numerical simulations or in experiments, but the general mechanism leading to such an organization of the flow at large scales is subtle and far from being understood. For simplicity, we consider in this paper the case of parallel jets favored by the \( \beta \) effect, however without \( \beta \) effect both jets and vortices can be observed [4,9,10]. When a large-scale structure is created by the flow, a quasilinear approach may be relevant. Such a quasilinear approach requires solving a coupled equation for the mean flow and the Lyapunov equation that describes the fluctuations with a Gaussian approximation, just like the Lenard-Balescu equation in plasma kinetic theory. Numerical approaches and theoretical analysis have been systematically developed for fifteen years in order to solve and study such quasilinear or
related approximations [6,11]. In a recent theoretical paper, the range of validity of such an approach has been established by proving the self-consistency of the approximations of weak forcing and dissipation limit [12]. While this work gave theoretical ground to the approach, explicit formula for the Reynolds stress cannot be expected in general. However, in a recent work [13], an expression for the Reynolds stress has been derived from the momentum and energy balance equations by neglecting the perturbation cubic terms in the energy balance (this follows from the quasilinear approach justification [12]), but also neglecting pressure terms (not justified so far, see [14]). This approach surprisingly predicts a constant velocity profile for the outer region of a large-scale vortex in two dimensions that does not depend on the detailed characteristics of the stochastic forcing but only on the total energy injection rate $\epsilon$ expressed in m$^2$s$^{-3}$. Another analytic expression for the Reynolds stress has also been derived in the particular case of a linear velocity profile $U$ in [15]. For the case of dipoles for the 2D Navier-Stokes equations, the papers [16,17] following a computation analogous to the one given in [15], shows that if the vorticity is passively advected (the third term in equation (5) below is neglected), then the expression for the Reynolds stress discussed in [10] is recovered ([17] also discusses other interesting aspects related to parts of the flow for which this relation is not correct). What are the criteria for the validity of these results? Can we reconcile the different results giving a full theoretical justification and extend these for more general cases?

We start from the equations for a barotropic flow on a periodic beta plane with stochastic forcing

$$\partial_t V + V \cdot \nabla V = -\epsilon \nabla P + \beta dV + \sqrt{2\alpha} \eta, \quad (1)$$

where $V := (V_x, V_y)$ is the two-dimensional velocity field with $\nabla V = 0$. $r$ models a linear friction, and $f$ is a stochastic force white in time, with energy injection rate $\epsilon$, $\beta_d$ is the Coriolis parameter, $y$ the north-south coordinate. Following [12] we choose time and space units such that the mean kinetic energy is 1, and $L_x = 1$. The non-dimensional equations for the vorticity $\Omega = \nabla \times V$ are

$$\partial_t \Omega + V \cdot \nabla \Omega = -\alpha \Omega - \beta V_y + \sqrt{2\alpha} \eta, \quad (2)$$

where $\eta = \nabla \times f$, and $V$ denotes from now on the non-dimensional velocity. Now $\alpha = L \sqrt{\epsilon}$ is a non-dimensional parameter although we will often refer to it as the “friction”. $\beta = \sqrt{\epsilon} L^2 \beta_d$ is the non-dimensional Coriolis parameter. Equation (2) still has three non-dimensional parameters, $\alpha$, $\beta$ and $K$, the typical Fourier wave number where energy is injected.

Neglecting the pressure and cubic terms in the energy balance and enstrophy balance, it is straightforward to obtain the Reynolds stress expression

$$\langle uv \rangle = \frac{\epsilon}{U'}, \quad (3)$$

where $U' = dU/dy$. This generalizes the result obtained for a vortex [13] to the case of a jet with mean velocity $U$. Is it possible to justify those hypotheses on theoretical ground, uncover the validity range of (3), and to generalize it? We note that detailed numerical studies of the energy balanced have been discussed in several papers [10,18,19].

In order to derive eq. (3), the key idea is to use the already justified [12] quasilinear approximation in the limit of small forces and friction (inertial regime, $\alpha \ll 1$), and to further consider the limit of small-scale forcing ($K \gg 1$), with fixed $\beta$. In these limits, energy is injected at small scale and is dissipated at the largest scale of the flow. $\alpha \ll 1$ is the proper regime for most geophysical turbulent flows, for instance for giant gaseous planets like Jupiter [20,21], and many two-dimensional or rotating turbulence experiments. The small-scale forcing limit $K \gg 1$ is the most common framework for turbulence studies (see, for example, [14]) and relevant for Jupiter troposphere. Also, computing the pressure from the Navier-Stokes equations involves inverting a Laplacian. It is thus natural to expect the pressure term to have a power expansion in the parameter $\frac{\alpha}{K}$, and thus vanish in the limit of large $K$. The main idea is then to separate the flow $V$ in two parts, $V(r,t) = U(y,t)\mathbf{e}_x + \langle \mathbf{w}(r,t) \rangle$. The mean velocity $U(y)\mathbf{e}_x = \frac{1}{L_x} \int dx \mathbb{E}[V(x,y)]$ called the mean flow or zonal flow, is defined as both the zonal and stochastic average of the velocity field. In the following, the bracket $\langle \rangle$ will be used for this zonal and stochastic average. We are left with two coupled equations, one governing the dynamics of the mean flow, the other one describing the evolution of eddies. In the limit where $\alpha$ is small, it has been proven that fluctuations are of order $\sqrt{\alpha}$ and thus it is self-consistent to neglect nonlinear terms in the equation for fluctuations [12]. Then one can justify [12] that, at leading order in $\alpha$, the full velocity field statistics are described by a quasi-Gaussian field (the velocity field is not Gaussian, but the marginals when the zonal flow is fixed are Gaussian, justifying a posteriori a second-order closure corresponding to the quasilinear approximation). Using also the incompressibility condition, we obtain the quasilinear model

$$\partial_t U = -\alpha \langle \partial_y \langle \omega \rangle + U \rangle, \quad (4)$$

$$\partial_t \omega + U \partial_x \omega + (\beta - U') \omega = -\alpha \omega + \eta, \quad (5)$$

where we have introduced $\omega = \partial_x \mathbf{v} - \partial_y \mathbf{u} = \Delta \psi$, the vorticity of the fluctuations. Equation (4) shows that the typical time scale for the evolution of the mean flow $U$ is $\frac{1}{\alpha}$ which is, following our assumption $\alpha \ll 1$, much larger than the time scale for the evolution of eddies. Using this time scale separation, we will consider that $U$ is a constant
field in the second equation (5), and we will always solve $\omega(t)$ for a given $U$. We follow the strategy:

- First we solve the linear equation (5) and compute the stationary distribution ($\omega^2$) as a functional of $U$.

- The enstrophy balance for the fluctuations allows us to relate ($\omega^2$) to the divergence of the Reynolds stress tensor (see the Supplementary Material Supplementarymaterial.pdf (SM) for the computation of the Reynolds stress divergence in the inertial small-scale forcing limit).

- Last we can use this expression to close the first equation (4), and discuss possible stationary profiles $U$.

To reach the first objective, we take advantage of the asymptotic regimes $\alpha \to 0$ and $K \to \infty$. When we take those two limits, it is natural to ask whether they commute or not, and which non-dimensional parameter will govern the difference between $\alpha \to 0$ first or $K \to \infty$ first. Our asymptotic calculations show that the key parameter is the ratio between $\frac{U^\prime}{\alpha X}$ and $\alpha$. Taking the limit $\alpha \to 0$ first amounts to saying that $\frac{U^\prime}{\alpha X}$ is very large.

We first take the limit $K \to \infty$ while keeping $\alpha$ small but finite. The idea is to write eq. (5) in an integral form using the Green function of the Laplacian, and use the fact that the Green function decreases very fast when $\alpha K$ is very large. At this stage of the calculation, $\alpha$ is small but finite, and the expression for the Reynolds stress depends both on $\alpha$ and on the properties of the stochastic forcing. The complete calculation is reported in the SM. We emphasize that as long as $\alpha$ is kept finite, the Reynolds stress depends on the Fourier spectrum of the stochastic forcing $\eta$. The result shows that the Reynolds stress can be expressed analytically as

$$\langle uv \rangle = \frac{1}{2\alpha} \chi \left( \frac{U^\prime}{2\alpha} \right),$$

where the explicit expression of $\chi$ is a parametric integral, see SM. The stationary profile $U$ thus verifies $\frac{U^\prime}{\alpha X}^2 \chi(\frac{2U^\prime}{\alpha X}) = -U$, which can be integrated using a primitive $X$ of the function $x \to x\chi'(x)$ in

$$X \left( \frac{U^\prime}{2\alpha} \right) + \frac{1}{2} U^2 = C,$$

where $C$ is the integration constant. It is in itself remarkable that for some range of the parameters, the flow of the barotropic quasilinear model can be computed from a Newtonian equation like (7).

In eq. (7), $X$ plays the role of a potential as if the equation would describe a particle moving in a one-dimensional potential. The constant in the right-hand side is set by $U'(0)$ and depending on the value of this constant, there can be one, two or three solutions as shown in fig. 1.

If $C > X_{\text{max}}$, there is one solution for which $U$ never vanishes. As the total flow momentum is zero, such solutions with either $U > 0$ or $U < 0$ are not physical. If $X_0 < C < X_{\text{max}}$, there are three possible solutions, one is periodic, the other two diverge. The periodic solution corresponds to $\frac{U^\prime}{\alpha X}$ confined in the well of $X$. In that case the flow is periodic and the solution exchanges kinetic energy in the term $\frac{1}{2} U^2$ with potential energy $X(\frac{U^\prime}{\alpha})$. Outside the well, the solutions are diverging, one corresponds to an increasing $U$ and the other to a decreasing $U$. A linear stability analysis of the periodic solution of (7) shows that this solution is unstable whereas the diverging solution is stable. Thus, the periodic regular solution is not a suitable candidate for the stationary mean velocity profile $U(y)$. If we now take the limit of vanishing $\alpha$ in expression (6), a straightforward calculation using the explicit expression of $\chi$ (given in the SM) allows us to recover expression (3) for the Reynolds stress because $U(\alpha u) \to 1$ which is eq. (3) with dimensional units. The physical interpretation of the limiting case (3) is very enlightening. The term $U'(\alpha u)$ can be interpreted as the rate of energy transferred from small scale to large scale, therefore expression (3) is consistent: with the limit of large $K$, the evolution of eddies becomes local as if the perturbation only sees a region of width $\frac{K}{\alpha}$ around itself, and thus the different parts of the flow are decoupled. The other limit of small $\alpha$ forces the energy to go to the largest scale to be dissipated because the dissipation at small scales becomes negligible.

Let us study the other limit where $\alpha$ goes to zero first. The techniques used in this second case are very different than the previous one. We assume in this section that the linearized dynamics has no unstable modes. The calculation involves Laplace transform tools that were used in [22] to study the asymptotic stability of the linearized Euler equations. In the limit $\alpha \ll 1$, using [12], we derive in the SM the relation between the Reynolds stress
divergence and the long time behavior of a disturbance $\omega(y, 0)$ carried by a mean flow $U(y)$. This is an old problem in hydrodynamics, one has to solve the celebrated Rayleigh equation

$$
\left(\frac{d^2}{dy^2} - k^2\right) \varphi_\delta(y, c) + \beta - U''(y) \frac{\omega(y, 0)}{iK(U(y) - c - i\delta)} \varphi_\delta(y, c) = 0.
$$

(8)

where $\varphi_\delta(y, c) := \int_0^\infty dt \psi(y, t)e^{-ik(c+\delta)t}$ is the Laplace transform of the stream function, and $k$ is the $x$-component of the wave vector. The Laplace transform $\varphi_\delta$ is well defined for any non zero value of the real variable $\delta$ with a strictly negative product $\delta k$. $c$ has to be understood as the phase speed of the wave, and $k\beta$ is the (negative) exponential growth rate of the wave. Involved computations are then required to give the explicit expression of the Reynolds stress. Let us just mention that the difficulty comes from the fact that we have to take the limit $\delta \to 0$ first in eq. (8) before $K \to \infty$. Then we can relate $\omega(y, \infty)$ to the Laplace transform $\varphi_\delta$ taken at $\delta = 0$. The expression for the Reynolds stress in the inertial limit involves an integral with the profile $U$ in the denominator of the integrand. The integral is defined only in regions of the flow where $U'$ does not vanish, or to state it more precisely, where the parameter $\frac{KU'}{\pi}$ is large. Therefore, there exists a small region of size $\frac{\pi}{K}$ around the maximum where the asymptotic expansion breaks down. In the outer region away from the extrema, we recover the expression (3) in the inertial limit $\alpha \to 0$ first. For strictly monotonic velocity profiles $U$, we conclude that the inertial limit and the small-scale forcing limit commute and that expression (3) is expected to be valid.

Using expression (3) for the Reynolds stress, we can solve eq. (4) for the stationary profile. It writes

$$
\frac{d}{dy} \left( \frac{\epsilon}{U'} \right) + U = 0.
$$

(9)

Whatever the value of the free parameter $U'(0)$, all profiles $U$ are diverging in finite length. An example of such a profile $U$ is given in fig. 2(a). In red, we have plotted different solutions of eq. (9) together such that the mean velocity profile $U$ is composed of many diverging jets. In blue, we have drawn at hand what we expect qualitatively from a real velocity profile. An example of a real profile obtained by numerical simulations in [23] is displayed in fig. 2(b). The fact that eq. (9) predicts diverging profiles $U$ shows that the expression for the Reynolds stress (3) is not valid everywhere in the flow, but it holds only in the spatial subdomains where the flow is monotonic, not at the extrema. We observe that both divergences are regularized, by a cusp at the eastward jet maximum, and by a parabolic profile at the westward jet minimum. The second aim of this paper is to explain the asymmetric regularization of the eastward and westward jets.

Numerical simulations like the one performed in fig. 2(b) show that the mean velocity profile is regularized at a very small scale at its maximum. As we explained previously, there exists a region of typical size $\frac{\pi}{K}$ around the maximum where the asymptotic expansion for the Reynolds stress breaks down. It is thus natural to choose the ansatz $\tilde{U}(y) := U(\frac{\pi}{K})$. The scaling in $\frac{\pi}{K}$ implies that the ratio $U''$ is very large at the cusp because $U'' \propto K^2$. The cusp is then described by the inhomogeneous Rayleigh eq. (8).

If we put the ansatz $\tilde{U}$ in (8) and consider the limit of large $K$, we get

$$
\left( \frac{d^2}{dy^2} - \tan^2 \theta \right) \varphi_\delta(y, c) - \frac{\tilde{U}''(y)}{U'(y) - c - i\delta} \varphi_\delta(y, c) = 0.
$$

(10)

where $\cos \theta = \frac{\beta}{K}$. The solution of this equation with $\delta \to 0$ gives us the Laplace transform of the stream function with which we can express the Reynolds stress. The $\beta$-effect disappears completely from the equation of the cusp because in the region of the cusp, the curvature is so large that it overcomes completely the $\beta$-effect, as can be seen on the green curve of fig. 2(b). Equation (10) together with the equations linking the Reynolds stress with $\varphi$ have a numerical solution, which proves that our scaling $\tilde{U}(y) := U(\frac{\pi}{K})$ is self-consistent. This solution can not be expressed analytically and depends on the Fourier spectrum of the stochastic forcing. An example of a numerical integration of the Reynolds stress divergence $-\frac{\partial}{\partial y}(uv)$ for the cusp is displayed in fig. 3 for $\tilde{U}(y) = -\frac{\pi}{2}$ and a stochastic forcing with a semi annular Fourier spectrum where $\theta$ ranges between $-\frac{\pi}{2}$ and $\frac{\pi}{2}$. In fig. 3, the red curve is the asymptote $\tilde{U}''$ obtained from formula (3) with $\epsilon = 1$. When a jet is in a stationary state, the cusp profile joins smoothly the outer region of the jet where the result (3) is valid.
Another physical phenomenon at the maximum of the jet is called “depletion at the stationary streamlines” and has first been observed in [22]. It means that at critical latitudes where $U' = 0$, any vorticity perturbation of the flow $\omega$ has to asymptotically vanish with time. One main consequence of this phenomenon is the relation

$$U(y_{cr}) = -\frac{\epsilon K^2}{r U''(y_{cr})}, \quad (11)$$

where $y_{cr}$ is the latitude of the extremum. From (11) we learn that, even if the velocity profile of the cusp depends on the details of the forcing, the maximal curvature of the profile satisfies a more general relation, and it would therefore be very interesting to check it in full numerical simulations with different types of forcing spectra.

The previous discussion successfully explained the jet regularization of the eastward jet cusp. As clearly observed in fig. 2(b), and from Jupiter data, westward jets do not produce cusps. At first sight, it may seem that all the theoretical arguments used so far, the energy balance, the asymptotic expansions, and the results (3) and (11), do not break the symmetry between eastward and westward jets, as $\beta$ disappears from all these computations. However, as clearly stressed in [12], the whole theoretical approach relies on an assumption of hydrodynamic stability for $U$. The asymmetry is clearly visible in the Rayleigh-Kuo criterion, that states that when $\beta - U''$ changes sign, an instability may develop. We will now argue that the turbulent flow is constantly oscillating between a stable and unstable solution, in order to control the westward jet behavior. This means that the flow is not linearly stable, but only marginally stable. As shown in the following, the instability is localized at the extremum of the westward jet, and the unstable mode has a very small spatial extension. That’s why the flow can be considered as stable away from the westward extremum of the jet and the assumptions of expression (3) are satisfied.

To check this marginal stability hypothesis, we solved numerically the homogeneous PDE for a perturbation carried by a mean flow $U$.

$$\partial_t \omega + i k U \omega + i k (\beta - U'') \psi = 0. \quad (12)$$

We chose a parabolic mean velocity with a small perturbation at its minimum $U(y) = \gamma \frac{y^2}{2} - \eta e^{-\frac{y^2}{2}}$. The main curvature $\gamma$ is chosen to be slightly smaller than $\beta$, and we performed simulations using different values of $\eta$ and $\sigma$. The result of one of those simulations is displayed in fig. 4. The red curve shows the Rayleigh-Kuo criterion $\beta - U''$ which is locally violated around $y = 0$. The blue curve shows the amplitude of the perturbation $|\omega(y, t)| - 1$ from which we can then express the Reynolds stress divergence. We check that the growth rate of the perturbation is indeed exponential with time with a complex rate $c$.

In this paper we gave a global consistent picture of how a zonal jet is sustained in a steady state through continuous energy transfer from small scale to large scale. Equations (7) and (9) are probably the most striking results of this work, showing for the first time that it is possible to find closed equations for the velocity profile of turbulent flows. It illustrates that, although far from equilibrium, turbulent flow velocity profiles may be described by self-consistent equations, as density of other macroscopic profiles can be described in condensed matter physics. This is a fundamental property whose existence is far from obvious, and that no other approach was able to establish so far. In this paper, we have considered the case of a Rayleigh friction as the mechanism for removing energy that is transferred to the largest scale. Rayleigh
friction is a rather \textit{ad hoc} type of damping (although it can be justified in certain cases involving, \textit{e.g.}, Ekman pumping). If one would consider other kinds of friction, for instance scale-selective damping, provided that this damping actually acts on the largest scales of the flow, in a corresponding inertial limit we expect most of our results to easily generalize (the proper dissipation operator should then replace Rayleigh friction in eq. (4)). Indeed the processes that explain the computation of the Reynolds stress are inertial in nature and independent of the dissipation mechanisms. As an example, the case of viscous dissipation has been discussed in section 5.1.2 of \cite{12}, showing that while the regularization by viscosity is very different from the regularization by linear friction, the inertial results for the Reynolds stresses do coincide. This is true as far as the shear is non-zero and eq. (3) is concerned; by contrast the regularization of the cusp is dissipation dependent. In some specific cases, changing the dissipation mechanism may induce specific instability modes, like boundary layer modes due to viscous dissipation, however such effects are expected to be non-generic. Extension and generalizations of our approach can be foreseen for other geometries (on the sphere), for more comprehensive quasi-geostrophic models of atmosphere jets, and for classes of flows dominated by a strong mean jet, for instance in some instances of boundary layer theory.

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