Optimization of Input Cutting Parameters on Cutting Force During Vortex Tube Jet Assisted Machining of Ti-6Al-4V.

Balaji. Nelge, Vinayak. Kale

Abstract: Titanium alloy materials machining is difficult, expensive and leads to wear and tear of the tool. The improvement in the tool life and use of optimal process parameters during machining is necessary to obtain better work piece surface finish. Here main aims to evaluate the effect of input process parameters on cutting force in Vortex Tube Jet Assisted CNC Machining of Titanium Alloy material. Taguchi L27 orthogonal array design matrix were used for experimentations by employing a Vortex Tube Jet Assisted cooling system. The significantly affecting process parameters are identified through ANOVA, and optimal parameters were identified using Taguchi and RSM. A mathematical model is proposed to estimate cutting forces based on selected input process parameters. The result reveals that the most influencing parameter is depth of cut (d). Whereas cutting speed and feed are influences very less. The cutting force (Fc) estimated from the proposed model is in close agreement with experimental results.

Keywords: ANOVA, Cutting force, Taguchi, VTJA.

I. INTRODUCTION

The conventional turning operations are performed using a variety of single-point cutting tools. These tools are not operated at appropriate process parameters, the tool life, and machining quality decreases whereas the cost of the product increases. To maintain the desired surface quality and tool life it is necessary to select appropriate process parameters and their range. The appropriate process parameters selection helps in reduction of cutting force (Fc) on the single-point cutting tool, many researchers highlighted the importance of cutting forces to enhance the tool life and improve surface finish.

The cutting process parameters, tool geometry, and material properties significantly influence on cutting force, quality of surface, tool wear, chip formation and cutting temperature. The Titanium alloy materials are used where elevated temperatures, high strength to weight ratio, corrosion-resistant, toughness, and biocompatibility are required, hence it is popularly used in automotive, medical appliances, aerospace, marine, and chemical industries. Titanium alloy has been an area of research for the past few decades. The thrust research areas in the field of titanium alloy are an improvement in surface finish, machinability, tool wear resistance, reduced force in the cutting tool, thermal analysis.

Suárez, A et al. [1] studied that HPC and flood cooling face-turning of nickel-alloy 718. By using HPC more than 10% tool wear and Fc were reduced. Jafarian, G et al [2] investigated the effect of machining time on the surface roughness at the different cutting parameters by using neural network model and also implemented Non-Dominated Sorting Genetic Algorithm to optimize tool life and surface roughness. Lin et al. [3] suggest that regression analysis used for analysis the surface roughness and Fc. Zang et al [4] used MQL and MQCL cooling methods. In MQCL tool life increased by 1.57 times than MQL. Berrimingham et al [5] reported that high-pressure cryogenic coolant is effective coolants for extending the tool life. Feng and Wang [6] investigated the influence of work piece hardness, f, d, Vc rake angle, and time on surface roughness by developing an empirical model. Philip S D et al [7] applied dry turning on cast DSS ASTM 955 grade5A work material. TiC and TiCN coated carbide cutting tool inserts are used. S/N ratio and Analysis of Variance were applied to optimize the machining parameters. Pervaiz, S et al [8] Machinability of hard material was studied to investigate the surface integrity defects, residual stresses, cracking and, microstructure characteristics using different cutting tool materials, wear mechanisms and, modes of failure. Aouic et al. [9] and Ozel et al. [10] implemented RSM to optimize the effect of cutting parameters on work piece hardness, Fc and surface roughness. Suresh et al. [11] TiC-coated tungsten carbide tool were used for machining of mild steel. RSM used for the analysis of Fc established during turning. Tao Chen et.al [12] studied the optimization of Fc on the turning of GCr15 steel by setting the optimal value of process parameters. Fratila D et.al. [13] Used Taguchi method in combination with Grey Relational Analysis with consideration of best-suited parameters like f, d, Vc, and tool nose radius. A. Pal et al [14] studied the influence of affecting parameter on Fc, chip tool interface temperature and surface roughness during the hard and soft turning. The effect of axial, radial and tangential forces were estimated in three different directions and revealed that the radial force is 15-20% higher than tangential force whereas axial force is higher than 102-112%.

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Zawada-Tomkiewicz et al [15] characterized the EN41Cr4 low chromium alloy steel was machined workpiece surface through turning operation. Guo Y.B et al [16] employed the methodology to study the residual stresses produced during machining of steel whereas FEM was adopted to study the interrelationships among residual stresses, microstructures, and tool-wear.

The above literature review visualizes that researchers have carried out a study on surface finish, Fc and other performance parameters in turning operations by adopting different traditional cooling systems and coolants. However, limited literature is reported in research articles using the Vortex Tube Jet Assisted (VTJA) cooling system in combination with Ti-6Al-4V material with different cooling strategies. Therefore, the present study focuses on the effect of process parameters in concurrence with VTJA cooling systems to estimate optimal process parameters for obtaining the desired machining force and effect of surface finish.

II. MATERIALS AND MACHINE

The annealed Ti-6Al-4V material was selected for the study since it has good mechanical properties such as it operates at elevated temperatures, better wear-resistant, toughness, and lightweight as compared to the other materials alloys. The samples of 20 mm diameter × 100 mm length are considered for the study. The ceramic-based cutting tool inserts have excellent capability of machining of hardened and short chipping materials under stable conditions. The details of the triangular geometry insert (TNGA160404) specifications and geometric dimensions selected for machining are given in Fig. 1.

Fig 1 Cutting Tool Insert dimensions.

A VTJA cooling method is implemented during the turning of titanium alloys. The vortex tube is a part of the VTJA cooling system which was designed and developed to provide low-temperature air stream to carry heat generated during machining. This vortex tube operates over the pressures range of 2 to 5 N/mm². The pneumatic air pressure of 5 N/mm² was given input to the vortex tube and it provides 5°C pressurized cooled air over a cutting tool and work piece interaction region. The specifications and dimensions of the vortex tube are shown in Fig. 2.

The vortex tube is located on TC35 Industrial type of CNC machine during experimentation is shown in Fig. 3. It operates over a spindle speed range of 50 to 3500 rpm and a maximum power of 10 KW. The Ti-6Al-4V specimens were turned under influence of cold air stream emerging out from VTJA at a combination of different process parameters obtained from Taguchi’s L27 orthogonal array design matrix. Fig. 3(a) and Fig. 3(b) show the experimental setup and work pieces machined at different combinations of process parameters during the conduction of experiments. The effect of cooling on machining response parameters such as surface finish and machining force was assessed.

III. CUTTING FORCE (FC) MEASUREMENT

The cutting forces were measured using a three-dimensional tool dynamometer. It comprises of three independent digital display units and calibrated to display force directly. The Fc measuring unit includes self-regulating strain gauge bridges for measuring strains in three independent directions. The input process parameters and the response of the average of three tangential Fc measured using dynamometer are given in Table 2.

Table II: Cutting force measured using dynamometer

| Run | speed | feed  | DOC  | Fc   |
|-----|-------|-------|------|------|
| 1   | 1000  | 0.10  | 0.5  | 26.333 |
| 2   | 1000  | 0.10  | 1.0  | 41.6667 |
| 3   | 1000  | 0.10  | 1.2  | 38.333 |
| 4   | 1000  | 0.15  | 0.5  | 28.0000 |
| 5   | 1000  | 0.15  | 1.0  | 39.6667 |
| 6   | 1000  | 0.15  | 1.2  | 51.333 |
| 7   | 1000  | 0.20  | 0.5  | 29.0000 |
| 8   | 1000  | 0.20  | 1.0  | 50.333 |
| 9   | 1000  | 0.20  | 1.2  | 53.0000 |
| 10  | 1200  | 0.10  | 0.5  | 15.0000 |
| 11  | 1200  | 0.10  | 1.0  | 32.0000 |
| 12  | 1200  | 0.10  | 1.2  | 33.333 |
| 13  | 1200  | 0.15  | 0.5  | 23.333 |
| 14  | 1200  | 0.15  | 1.0  | 37.333 |

Fig.2: Schematic diagram of Vortex Tube
determine the optimum Fc under Vortex tube jet-assisted air cooling conditions.

IV. STATISTICAL ANALYSIS OF EXPERIMENTAL DATA

The affecting input machining parameters like Vc, f, and d are varied as per orthogonal array L27 and the Fc was measured and analysed using MINITAB 17 software. The value of S/N Ratio and Means obtained by considering smaller the better option [7]. The significantly affecting process parameters were ranked through ANOVA. These are given in Table 3. It also enables to perform the simultaneous test and the P-value obtained from the analysis is depicted in Table 4. The regression coefficients for Fc, Root mean-square and adjusted Root mean-square values obtained from regression analysis are 96.81 % and 95.12 % respectively.

Table III: Ranking of process parameters

| Level | Speed | Feed | Depth of Cut |
|-------|-------|------|--------------|
| 1     | -31.71| -28.90| -27.39       |
| 2     | -30.12| -30.98| -31.94       |
| 3     | -30.39| -32.33| -32.89       |
| Delta | 1.59  | 3.43  | 5.50         |

Table IV: ANOVA of Cutting Force

| Sources         | DF | Adj SS | Adj MS | F-Value | P-Value |
|-----------------|----|--------|--------|---------|---------|
| Model           | 9  | 3220.41| 357.82| 57.25   | 0.000   |
| Linear          | 3  | 2780.57| 926.86| 148.29  | 0.000   |
| Speed           | 1  | 89.10  | 89.10  | 14.26   | 0.002   |
| Feed            | 1  | 759.79 | 759.79| 121.56  | 0.000   |
| Depth of cut    | 1  | 1942.19| 1942.19| 310.74  | 0.000   |
| Square          | 3  | 121.63 | 40.54  | 6.49    | 0.004   |
| Speed*speed     | 1  | 110.05 | 110.05| 17.61   | 0.001   |
| Feed*feed       | 1  | 2.24   | 2.24   | 0.36    | 0.557   |
| Doc*Doc         | 1  | 9.35   | 9.35   | 1.50    | 0.238   |
| 3-Way Interaction| 3  | 117.40 | 39.13  | 6.26    | 0.005   |
| Speed*speed     | 1  | 69.91  | 69.91  | 11.18   | 0.004   |
| Speed*Doc       | 1  | 13.33  | 13.33  | 2.13    | 0.162   |
| Feed*Doc        | 1  | 34.16  | 34.16  | 5.47    | 0.032   |
| Error           | 17 | 106.25 | 6.25   |         |         |
| Total           | 26 | 3326.67|        |         |         |

The analysis of mean effect plot for means and S/N ratio obtained from Taguchi’s analysis the optimum combination of control factor for predicting minimum Fc along with the prominent control factors are shown in Fig. 4. A Smaller is the better characteristics feature was chosen for analysis to

VI. RESULT AND DISCUSSIONS

Hardness is measured by micro hardness testing machine Figure show the effect of depth of cut (0.5, 1.0, 1.2 mm) on hardness for all values of the spindle speeds (Vc) (1000, 1200, 1500 rpm). As the depth of cut raised from 0.5 to 1.2mm, the hardness of Ti-6Al-V varied from 360HV to 415HV at different feed (f) 0.1, 0.15, and 0.20 mm/rev. This is as a result of lower depth of cut 0.5mm, at 0.1 mm/rev with increase in Vc from 1000 to 1500 rpm hardness also slightly increases. Only for 0.15mm/rev feed, increase in Vc then hardness is decreases. When depth of cut rises from 0.5 mm to 1.2 mm then overall increasing speed and feed then hardness is decreases. Fc depends upon hardness of material [8]. For constant depth of cut, various feed and speed, hardness are measured on micro hardness tester. Which is shown in below.

Fig: 4 Main Effect Plot for Means

Fig: 5 Hardness variation with cutting speed for a depth of cut 0.5mm at various feed
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The effect of process parameters such as $V_c$, $f$, $d$ on $F_c$ and surface finish has been discussed in the following section. The influential point shown in Fig. 8 affects the slope of the regression line. The residual plot shows a random distribution of data around the horizontal line in positive and negative sides, this pattern of distribution indicates that the model provides a decent fit to the data and suitable for the non-linear model. Therefore second-order polynomial equation (1) is considered for the study.

The contour plot is shown in Fig. 9(a) illustrates that the $F_c$ of 20-25 Kgf is obtained by setting speed range between 1100 rpm to 1550 rpm and feed rate at 0.1 revs/mm. However Fig. 9(b) depicts that less than 20 Kgf is obtained at less than 0.5 mm d and 1100-1500rpm $V_c$. Whereas Fig. 9(c) provides a $F_c$ lesser than 20 Kgf for the $d$ and $f$ less than 0.65 mm and 0.15 mm / rev respectively.

The ANOVA results are shown in Table 4 also confirm that interaction between $f$ and $d$ was significant for getting the desired $F_c$ in Ti-6Al-4V Machining under VTJA cooling environment. The regression model with the $P$ values less than 0.002 indicate that the three cutting parameters. The most significant among all these are the $f$ and $d$ which is very much in bonded with the analysis of variance. In this experimentation cutting condition vortex tube cooling allows reducing the main $F_c$ due to improved and near chip tool interaction. VTJA has mainly reduced the amount of heat and friction at the contact point of tool and work piece. In this experimentation optimum force obtain by using the regression equation is 17.173 Kgf.

The Lower power consumption by machine tools is observed when the machining tool is subjected to a minimum $F_c$. The contour plot is shown in Fig. 9 helps to predict the required $F_c$ by referring to these contour plots. The contour plot is shown in Fig. 9(a)-Fig. 9(c) reveals the minimum $F_c$ obtain at the speed <0.15mm/rev., depth of cut <0.65mm and speed in the range of 1100 to 1500 rpm. The range of process parameters selected for the study disclosed that the depth of cut plays an important role in obtaining lower $F_c$ whereas the combination of $V_c$ and $f$ does not contribute more to minimizing the $F_c$. The surface plot shown in Fig.10 helps for 3D visualization of responses. This plot represents the nature of the response parameter by holding input parameters at a constant speed of 1250 rpm, ‘$d$’ of 0.85 mm and ‘$f$’ 0.15 mm/rev. Fig. 10(a) and Fig. 10(b) reveals that the $F_c$ rises non-linearly with an increase in $f$ - $V_c$ and $V_c$-$d$ combinations respectively. However, Fig 10(c) depicts the linear variation of $F_c$ with the increase in $f$ and $d$ value.
whereas by actual reading optimal \( F_c \) noted was 15 Kg\( f \) at 0.10 mm/rev of feed, 0.5 mm of the \( d \), and 1200rpm \( V_c \).

VII. CONCLUSIONS

The presented research work focused on the study of the process parameters in the presence of VTJA cooling systems to estimate the optimal \( F_c \) by implementing Taguchi and RSM. The following conclusions are drawn based on experiment and statistical methods.

1. The depth of cut is the most influencing parameter on turning single point cutting tool whereas least affected by speed under VTJA. Cooling condition.
2. The proposed analytical model predicts the optimal solution within the accuracy of 12.65 % as compared to the experimental results.
3. Hardness is affects to \( F_c \), in VTJA Machining depth of cut rise from 0.5 mm to 1.2 mm then overall feed and hardness are decreases.

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