Dynamical scattering models in optomechanics: Going beyond the 'coupled cavities' model

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Dynamical scattering models in optomechanics:
going beyond the ‘coupled cavities’ model

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Abstract. Recently we calculated the radiation field and the optical forces acting on a moving object inside a general one-dimensional configuration of immobile optical elements (Xuereb et al 2010 Phys. Rev. Lett. 105 013602). In this paper, we analyse the forces acting on a semi-transparent mirror in the ‘membrane-in-the-middle’ configuration and compare the results obtained from solving the scattering model to those from the coupled cavities model that is often used in cavity optomechanical systems. We highlight the departure of this model from the more exact scattering theory when the intensity reflectivity of the moving element drops below about 50%.

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1. Introduction

The nontrivial interplay between the external (motional) or internal degrees of freedom of a mobile scatterer coupled to a cavity field, and the cavity field itself has attracted considerable attention over the past two decades. Use has been made of a cavity field for, e.g., interaction with single atoms [1–4], cooling atomic motion [5–8], imposing spontaneous order through a Dicke phase transition in an ultracold atomic medium [9, 10], coupling to the motion of mechanical oscillators [11–18], and even cooling this motion down to the vibrational ground state [19–21].

The description of these systems, along with most of cavity quantum electrodynamics (CQED), follows the path of the ‘good cavity’ approximation [22]: the cavity mirrors, be they fixed [12, 18, 23–25] or moving [14, 24, 26], bind a region of space such that the electromagnetic field in that region is cut off from the outside world. In such a description, any highly reflective element inside the cavity divides the cavity itself into two coupled modes [12, 27] that communicate by tunnelling through this element. An alternative approach, based on a scattering picture, is possible. Such an approach can treat very general configurations in one dimension, owing to the power of the transfer matrix method (TMM) [25, 28–30]. In the right limits, the two approaches must of course give rise to the same physics, and indeed they do, even in the case of moving boundaries [30]. However, there is no guarantee that one TMM model is always equivalent to the same CQED model; it is the purpose of this paper to use the specific example of a scatterer inside a cavity, i.e., the ‘membrane-in-the-middle’ scheme [12, 15, 17, 18, 24, 31–34] to highlight the differences between these two approaches. Our work is not the first application of transfer matrices to this geometry; we mention, for example, that the TMM model for static scatterers was used in [25] to describe the coupling between the optical system and the motion of a micromechanical oscillator. Here, however, we make use of the TMM for moving scatterers [30, 35], which allows the calculation of such dynamical quantities as the friction force acting on the moving scatterer within the same framework. In this paper our investigation will be limited to single transverse-mode situations, but is extendible to multi-mode situations [17, 36] by allowing the scatterers to couple the different modes together, in the spirit of [37].

Indeed, suppose we have a scatterer, say an atom or a membrane, of amplitude reflectivity \( r (0 \leq |r| \leq 1) \) placed inside a cavity which, on its own, can be described very well using the ‘good cavity approximation’. One of two limiting descriptions is generally appropriate for this situation in the CQED picture. (i) If the scatterer were, e.g., an atom, with \( |r| \ll 1 \), the shape of the mode functions of the field inside the cavity will not change appreciably. In this case it is valid to treat the atom in a weak coupling approximation and assume that it essentially couples to the unperturbed cavity field. (ii) On the other hand, if the scatterer were a good mirror, with \( |r| \) approaching 1, this description is no longer valid. Not only does the mirror perturb the shape of the cavity field, but in the good cavity approximation it defines two new modes that communicate by a tunnelling of photons through the good mirror. This simple example shows the power of the TMM approach: the same TMM model is valid for both situations, and indeed for any situation in between, including absorbing scatterers, with the value of the polarizability \( \zeta \) of the scatterer determining which of the two situations is being described.

### Notes

3 This ‘weak coupling’ criterion is not related to the so-called strong coupling condition of CQED, which refers to the regime in which the internal coherent atom–light coupling leads to a dynamics on a time-scale shorter than the characteristic decay time of the dissipation processes. This kind of strong coupling can be achieved without distorting spatially the empty cavity mode functions.
There exists a more fundamental effect which calls for the TMM rather than using a simple coupled cavity mode approach. The TMM deals with moving boundary conditions in a way that goes beyond merely having a dynamically changing detuning: the spatial distribution of the electric field in the TMM also changes dynamically. For a more thorough discussion of this point we refer the reader to the recent work by Cheung and Law [38]. The TMM approach that we make use of assumes that the motion of the scatterer happens on a time-scale longer than that of the cavity field; the validity of our work is therefore limited to the regime \( \omega_m \ll \kappa_c \).

Describing the field solution obtained through the TMM in terms of one or more cavity modes is an approximation that we do not need to make in this model. Therefore, there is no restriction on the relative magnitude of the frequency splitting between adjacent cavity modes, and \( \kappa_c \) or \( \omega_m \).

The remainder of this paper shall be organized as follows. In the next section we will briefly summarize the general solution to the TMM with one moving scatterer [39, 40]. The following section will apply this general solution to the study of the ‘membrane-in-the-middle’ model and compare it to the commonly used CQED model [32], following which we will conclude.

### 2. General solution to the transfer matrix method with a moving scatterer

#### 2.1. The force acting on the moving scatterer

Consider the generic situation sketched in figure 1. Within the TMM, every scatterer in the situation is represented by a \( 2 \times 2 \) matrix \( M \). Free-space propagation at a wavenumber \( k \) is represented by

\[
M(k) = \begin{bmatrix} e^{ikx} & 0 \\ 0 & e^{-ikx} \end{bmatrix}.
\]

For a static scatterer, \( M \) is related simply to the amplitude reflectivity \( r \) and transmissivity \( t \) of the scatterer, via its polarizability \( \xi \), which may depend on \( k \):

\[
M(k) = \begin{bmatrix} 1 + i \xi & i \xi \\ -i \xi & 1 - i \xi \end{bmatrix} = \frac{1}{t} \begin{bmatrix} t^2 - r^2 & r \\ -r & 1 \end{bmatrix}.
\]
Static scatterers do not change the frequency of transmitted and reflected light. A moving scatterer, however, Doppler-shifts reflected light, and we represent this process by transforming $M$ into an operator $\hat{M}$ [30, 39]:

$$\hat{M}(k) = \hat{P} \times M(k) \times \hat{P}^{-1},$$

(3)

where the ‘Doppler-shift operator matrix’, $\hat{P}$, for a scatterer moving with velocity $v$, is

$$\hat{P} = \begin{bmatrix} 1 - \frac{v}{c}(1 - k_0 \partial_k) & 0 \\ 0 & 1 + \frac{v}{c}(1 - k_0 \partial_k) \end{bmatrix},$$

(4)

to first order in $v/c$ and under the assumption that the pump beam has a very narrow spread of wavenumbers about a central $k_0$. We use the shorthand notation $\partial_k \equiv \frac{\partial}{\partial k}$ throughout this paper and will drop the label $k$ wherever it is not necessary. To first order in the velocity $v$ of the scatterer, then, this transformation is remarkably simple and we may write down the general solution for the velocity-dependent force acting on the scatterer in the closed form [39, 40]. In terms of the notation in figure 1, we can define

$$\hat{M} = M_1 \times \hat{M}_S \times M_2 \equiv \begin{bmatrix} \hat{\alpha} & \hat{\gamma} \\ \hat{\delta} & \hat{\beta} \end{bmatrix} \text{ and } (M_1)^{-1} \equiv [\mu_{ij}].$$

(5)

Because of the invertibility of all transfer matrices, one is free to express the fields on the ‘left’ in terms of those on the ‘right’, or conversely by inverting the relevant matrix; the fields on the ‘right’ in terms of those on the ‘left’. The quantities $\mu_{ij}$ are therefore the elements of the transfer matrix relating the fields just to the left of the moving scatterer, cf figure 1, to the fields $A_1$ and $B_1$. The calculation consists of determining the matrix elements $\hat{\alpha}$, $\hat{\beta}$, $\hat{\gamma}$ and $\hat{\delta}$, which may be a lengthy, but in all cases straightforward, task requiring only sequential multiplication of $2 \times 2$ matrices. For later convenience the solution is cast in a form using velocity-independent quantities $\alpha_0$, $\alpha_1^{(0)}$, $\alpha_1^{(1)}$ etc, which are defined by the relations

$$\hat{\alpha} \equiv \alpha_0 + \frac{v}{c} \left( \alpha_1^{(0)} + \alpha_1^{(1)} \frac{\partial}{\partial k} \right), \quad \hat{\beta} \equiv \beta_0 + \frac{v}{c} \left( \beta_1^{(0)} + \beta_1^{(1)} \frac{\partial}{\partial k} \right),$$

(6)

$$\hat{\gamma} \equiv \gamma_0 + \frac{v}{c} \left( \gamma_1^{(0)} + \gamma_1^{(1)} \frac{\partial}{\partial k} \right) \text{ and } \hat{\delta} \equiv \delta_0 + \frac{v}{c} \left( \delta_1^{(0)} + \delta_1^{(1)} \frac{\partial}{\partial k} \right);$$

(7)

the explicit form of these quantities depends on the exact form of the system involved, in particular on the matrices $M_1$ and $M_2$, and no general expression can be given. Assuming that the pumping field is monochromatic about some wavenumber $k_0$, $B_1 = B_0 \delta(k - k_0)$ and $C_1 = C_0 \delta(k - k_0)$, we can write the field amplitudes $A = \int A(k) \, dk$ and $B = \int B(k) \, dk$ which are given, to first order in $v/c$, by:

$$A = \left( \mu_{11} \frac{\alpha_0}{\beta_0} + \mu_{12} + \frac{v}{c} \left[ \frac{\mu_{11}}{\beta_0^2} (\alpha_1^{(0)} \beta_0 - \alpha_0 \beta_1^{(0)}) - \frac{1}{\beta_0} \left( \frac{\partial}{\partial k} \frac{\mu_{11}}{\beta_0} (\alpha_1^{(1)} \beta_0 - \alpha_0 \beta_1^{(1)}) \right) \right] \right) B_0$$

$$+ \left( \frac{\mu_{11} \gamma_0 \beta_0 - \alpha_0 \delta_0}{\beta_0} \right) + \frac{v}{c} \left[ \frac{\mu_{11}}{\beta_0^2} (\beta_0^2 \gamma_1^{(0)} - \alpha_0 \beta_0 \delta_1^{(0)} - (\alpha_1^{(0)} \beta_0 - \alpha_0 \beta_1^{(0)}) \delta_1) \right]$$

$$- \left[ \frac{\partial}{\partial k} \frac{\mu_{11}}{\beta_0} (\beta_0 \gamma_1^{(1)} - \alpha_0 \delta_1^{(1)}) \right] + \frac{\delta_0}{\beta_0} \left[ \frac{\partial}{\partial k} \frac{\mu_{11}}{\beta_0} (\alpha_1^{(1)} \beta_0 - \alpha_0 \beta_1^{(1)}) \right] \right) C_0,$$

(8)
and
\[
B = \left( \mu_{21} \frac{\alpha_0}{\beta_0} + \mu_{22} + \frac{v}{c} \left\{ \frac{\mu_{21}}{\beta_0} (\alpha_1^{(0)} \beta_0 - \alpha_0 \beta_1^{(0)}) - \frac{1}{\beta_0} \left[ \frac{\partial}{\partial k} \frac{\mu_{21}}{\beta_0} (\alpha_1^{(1)} \beta_0 - \alpha_0 \beta_1^{(1)}) \right] \right\} \right) B_0
\]
\[
+ \left( \mu_{21} \frac{\gamma_0 \beta_0 - \alpha_0 \delta_0}{\beta_0} + \frac{v}{c} \left\{ \frac{\mu_{21}}{\beta_0} \left[ \beta_0^{2} \gamma_1^{(0)} - \alpha_0 \beta_0 \delta_1^{(0)} - (\alpha_1^{(0)} \beta_0 - \alpha_0 \beta_1^{(0)}) \delta_0 \right] \right\}
\]
\[
- \left[ \frac{\partial}{\partial k} \frac{\mu_{21}}{\beta_0} (\beta_0 \gamma_1^{(1)} - \alpha_0 \delta_1^{(1)}) \right] \right) \right) C_0,
\]

where the derivatives are all evaluated at \( k = k_0 \) and act on the frequency-dependent terms arising from free-space propagation or a \( k \)-dependent polarizability. The quantity \( |B_0|^2 \) \( (|C_0|^2) \) represents the rate of photons incident upon the system from the left (right), and therefore is dimensionally an inverse time.

To obtain these expressions one first solves for \( A_1(k) \) and \( D_1(k) \) in terms \( B_0 \) and \( C_0 \), and then substitutes the results into the matrix equations to obtain explicit expressions for \( A(k) \) and \( B(k) \). Upon noting that these expressions are valid to first order in \( v/c \) and that the pumping field is monochromatic, the integrals can easily be performed to yield equations (8) and (9). For single-sided pumping (e.g., \( C_0 = 0 \)), these expressions simplify significantly. We shall find it useful to express these results in the form \( A = A_0 + \frac{v}{c} A_1 \) and \( B = B_0 + \frac{v}{c} B_1 \), with \( A_{0,1} \) and \( B_{0,1} \) being independent of \( v \). For conciseness, let us now assume that \( \zeta \) does not depend on \( k \). For the case of an atom, this corresponds to pumping far off-resonance. Then, using the elements of \( \hat{M}_S \), we obtain
\[
\mathcal{C} = \int C(k) \, dk = \left[ (1 - i \zeta) A_0 - i \zeta B_0 \right] + \frac{v}{c} \left[ (1 - i \zeta) A_1 + 2i \zeta B_0 - i \zeta B_1 \right], \tag{10}
\]
and
\[
\mathcal{D} = \int D(k) \, dk = \left[ i \zeta A_0 + (1 + i \zeta) B_0 \right] + \frac{v}{c} \left[ 2i \zeta A_0 - i \zeta A_1 - (1 + i \zeta) B_1 \right]. \tag{11}
\]
We denote the velocity-independent parts of \( \mathcal{C} \) and \( \mathcal{D} \) by \( \mathcal{C}_0 \) and \( \mathcal{D}_0 \), respectively. The force acting on the scatterer can be finally written down as [30]
\[
F = \hbar k_0 (|A|^2 + |B|^2 - |\mathcal{C}|^2 - |\mathcal{D}|^2), \tag{12}
\]
which we can write as \( F = F_0 + \frac{v}{c} F_1 \), where
\[
F_0 = -2\hbar k_0 [(|\zeta|^2 + \text{Im}(\zeta)) |A_0|^2 + (|\zeta|^2 - \text{Im}(\zeta)) |B_0|^2 + 2 \text{Re} \{(|\zeta|^2 + i \text{Re}(\zeta)) A_0 B_0^* \}], \tag{13}
\]
and
\[
F_1 = -4\hbar k_0 [(|\zeta|^2 - |A_0|^2 - |B_0|^2) + (|\zeta|^2 + \text{Im}(\zeta)) \text{Re}(A_0 A_0^*) - 2 \text{Im}(\zeta) \text{Re}(A_0 B_0^*)
\]
\[
+ (|\zeta|^2 - \text{Im}(\zeta)) \text{Re}(B_0 B_0^*) + \text{Im}(\zeta) \text{Re}(A_0 B_0^*) + \text{Re} \{(|\zeta|^2 + i \zeta) A_1 B_0^* \}] \tag{14}
\]
the quantity \( dF/dv = F_1/c \) will henceforth be called the ‘friction coefficient’.

2.2. Momentum diffusion experienced by the moving scatterer

The field amplitudes calculated in the previous section are related to classical electromagnetic fields. We may now impose a canonical quantization on these fields [30], promoting each field
variable $A$, say, to an operator $\hat{A}$, such that $\langle \hat{A} \rangle = \sqrt{2\varepsilon_0 S/(\hbar k_0)} A$, $S$ being the mode cross-sectional area. The only two $a$ priori independent modes in our system are the two input modes $\hat{B}_1$ and $\hat{C}_r$, whose operators obey the usual time-domain bosonic commutation relations
\[
[\hat{B}_1(t), \hat{B}^\dagger_1(t')] = [\hat{C}_r(t), \hat{C}^\dagger_r(t')] = \delta(t - t'), \quad \text{and} \quad [\hat{B}_1(t), \hat{C}^\dagger_r(t')] = 0.
\] (15)

The commutation relations between each of the four fields $\hat{A}$, $\hat{B}$, $\hat{C}$ and $\hat{D}$ can then be built up; because $F$ is correct up to first order in $v/c$ we only need to evaluate expressions to the zeroth order in this section. The fluctuations in these fields will lead to a diffusion in momentum space, quantified by the diffusion coefficient $D$. Another contribution to $D$ is due to lossy scatterers: any absorptive scatterer effectively couples the system to a further ‘loss’ mode that is independent of the input fields and is necessary to preserve the canonical commutation relations [30]. Such loss modes can be included self-consistently into the TMM [40]. Losses in SiN intra-cavity elements tend to be of the order of $10^{-4}$ [12]. Such low losses do not change our results qualitatively or quantitatively [40], and will therefore be ignored here. Putting all of the above together we can write
\[
D \delta(t - t') = (\hbar k_0)^2 [A_0]^2 [\hat{A}(t), \hat{A}^\dagger(t')] + |B_0|^2 [\hat{B}(t), \hat{B}^\dagger(t')] + |C_0|^2 [\hat{C}(t), \hat{C}^\dagger(t')]
+ |D_0|^2 [\hat{D}(t), \hat{D}^\dagger(t')] + 2 \text{Re}[A_0^* B_0 [\hat{A}(t), \hat{B}^\dagger(t')] - A_0^* C_0 [\hat{A}(t), \hat{C}^\dagger(t')]]
- A_0^* D_0 [\hat{A}(t), \hat{D}^\dagger(t')] - B_0^* C_0 [\hat{B}(t), \hat{C}^\dagger(t')] - B_0^* D_0 [\hat{B}(t), \hat{D}^\dagger(t')]
+ C_0^* D_0 [\hat{C}(t), \hat{D}^\dagger(t')]).
\] (16)

It is instructive to explain how each of these commutators is calculated. Each of the four operators $\hat{A}$, $\hat{B}$, $\hat{C}$ and $\hat{D}$ can be written in terms of the input field operators $\hat{B}_1$ and $\hat{C}_r$. Thus, reading the coefficients $a_0 = \mu_{11} / \alpha_0 + \mu_{12}$ and $a_c = \mu_{11} (\gamma_0 \beta_0 - \alpha_0 \delta_0) / \beta_0$ from (8) for $v = 0$ gives
\[
\hat{A} = a_0 \hat{B}_1 + a_c \hat{C}_r,
\] (17)

whereby we can calculate
\[
[\hat{A}(t), \hat{A}^\dagger(t')] = (|a_0|^2 + |a_c|^2) \delta(t - t');
\] (18)

the other commutators follow similarly. Knowledge of $D$ and $F$ then allows us to obtain the temperature to which the scatterer will tend:
\[
\kappa B T = -c D / F_1,
\] (19)

where $\kappa_B$ is Boltzmann’s constant. These quantities, which can thus be fully determined from our scattering model, are some of the more important quantities of interest in optomechanical setups and atom-CQED, and allow us to describe the dynamical behaviour of such systems. Because of the complexity of the expressions resulting from this section, it is hard to make a direct analytical comparison between the above results and the CQED expressions for the force and diffusion coefficient. We note, however, that in one particularly simple case this comparison for the force was done explicitly and the resulting expressions found to be identical [30].

3. The ‘membrane-in-the-middle’ model

We begin by modelling the system in [12]: a two-mirror Fabry–Pérot cavity with a micromirror near its centre, operating at a wavelength $\lambda = 1064$ nm and having a length $L_c = 6.7$ cm,
The general optical systems in figure 1 have been replaced by identical mirrors that form a cavity around the moving scatterer. We will only consider situations where \(|x| \ll L_c\).

Figure 2. Our model for the ‘membrane-in-the-middle’ geometry: the general optical systems in figure 1 have been replaced by identical mirrors that form a cavity around the moving scatterer. We will only consider situations where \(|x| \ll L_c\).

The micromirror is modelled by its polarizability \(\zeta\) which, in light of the small losses observed in practice, is taken to be real and negative. Whereas the real experimental system corresponds to \(|\zeta| \lesssim 1\), we allow \(\zeta\) to vary freely in our model. The two quantities of interest in this section are the intensity of the field close to the micromirror, and the friction coefficient acting on the micromirror. The latter is useful in optomechanical cooling experiments; the interest here lies in the fact that cooling the motion of a micromirror is one way towards achieving higher sensitivity in metrology applications, most notably in gravitational wave detectors [26], force sensors [41] and magnetometers [42].

These quantities are summarized in figure 3, with the left panels showing the intensity at the mirror and the right panels the friction coefficient acting on the mirror. Each sub figure (a)–(f) explores a different value for \(\zeta\). For \(|\zeta| \ll 1\), the cavity field is close to the bare cavity field; in particular, the cavity resonances are only slightly perturbed by the presence and position of the micromirror. The opposite is true of the \(|\zeta| \gg 1\) case, where there is coupling between pairs of cavity modes, typified by the avoided crossing in the spectra. The resonance frequencies can be obtained analytically, in the limit of a good bare cavity, as frequency shifts from the bare resonances:

\[
\Delta \omega = \frac{c}{L_c} \tan^{-1} \left\{ \frac{\zeta^2 \cos(2k_0x) \pm \sqrt{1 + \zeta^2 \sin^2(2k_0x)}}{\zeta \left[ \cos(2k_0x) \mp \sqrt{1 + \zeta^2 \sin^2(2k_0x)} \right]} \right\},
\]

with \(L_c\) being the length of the cavity, \(x\) the position of the micromirror, and \(k_0 = 2\pi/\lambda\) the wavenumber of the light inside the cavity; (20) is identical to equation (4) in [32]. The two sets of solutions to (20) are, in the \(\zeta \to 0\) limit, separated by a free-spectral range. These cavity resonances, plotted as detuned cavity lengths \(\Delta L_c = (L_c/\omega)\Delta \omega\), are traced by means of the dashed black curves in the left panels of figure 3. We note that a unit on the vertical axis \((\Delta L_c = \lambda)\) is equal to twice the free-spectral range of the cavity.

In the standard optomechanical coupling Hamiltonian, the mirror–field coupling is represented by a term of the form

\[
\hat{H}_{\text{OM}}^{(1)} \sim \hbar \omega' \hat{x} \hat{a}^\dagger \hat{a},
\]

(21)
Figure 3. The field intensity (left panels) at, and the friction coefficient (right panels) acting on, the micromirror as the micromirror position ($x$) and cavity length ($L_c + \Delta L_c$) are scanned. The sub figures differ only in the polarizability of the mirror, as indicated. The cavity parameters are modelled from [12]. In the series of left panels, we note the progression from an almost bare cavity situation (a) to a very strong perturbation by the micromirror, leading to avoided crossings (f). The white dashed line traces a cavity node, whereas the black dashed lines (equation (20)) trace the cavity resonances. In the series of right panels, note that the friction coefficient is—as expected—a cooling force (blue) for red cavity detuning and a heating force (red) for blue detuning. The colour bars are on a logarithmic scale and are for 1 W of input power. (a) $\zeta = -0.100$, (b) $\zeta = -0.500$, (c) $\zeta = -1.000$, (d) $\zeta = -2.000$, (e) $\zeta = -5.000$ and (f) $\zeta = -10.000$. 
where $\hat{x}$ is the position operator of the mirror, and $\omega' \equiv \partial (\Delta \omega) / \partial x$. $\hat{a}$ is the annihilation operator of the field mode that has the dominant interaction with the micromirror; in the $|\xi| \to 0$ limit, these field modes are the bare cavity modes of the whole cavity. However, as $|\xi|$ increases, the micromirror effectively splits the main cavity into two coupled cavities, giving rise to symmetric and antisymmetric modes, seen as the higher (bright) and lower (dark) branches in figure 3(f) for $0 < x < \lambda / 4$; in such cases $\hat{a}$ is the annihilation operator belonging to one of these eigenmodes. We note that similar behaviour was observed in [32].

Certain effects, such as mechanical squeezing of the mirror position [43] and quantum non-demolition measurements on the mirror [44], require not linear coupling to $\hat{x}$ but quadratic coupling to $\hat{x}^2$:

\[
\hat{H}_{\text{OM}}^{(2)} \sim \hbar \omega'' \hat{x}^2 \hat{a}^\dagger \hat{a},
\]

with $\omega'' \equiv \partial^2 (\Delta \omega) / \partial x^2$. In our notation, we have

\[
\omega' = \pm \frac{2k_0c}{L_c} \frac{\zeta \sin(2k_0x)}{1 + \zeta^2 \sin^2(2k_0x)}^{1/2},
\]

and

\[
\omega'' = \pm \frac{4k_0^2c}{L_c} \frac{\zeta \cos(2k_0x)}{1 + \zeta^2 \sin^2(2k_0x)}^{3/2}.
\]

One thing we note immediately is that there is no value for $x$ such that $\omega' = \omega'' = 0$; in other words, the optomechanical coupling is restricted to be linear or quadratic, to the lowest order. Higher-order nonlinearities may be achieved by coupling different transverse modes of the cavity (see, e.g. the experimental results in [33, 36]) but are overwhelmed by the linear or quadratic couplings in a single-transverse-mode cavity. Moreover, the linear coupling $\omega'$ is bounded in the $\zeta \to \infty$ limit:

\[
|\omega'| \leq \frac{2k_0c}{L_c} \approx 2\pi \times 8.42 \text{ MHz nm}^{-1},
\]

with the numeric value corresponding to our parameters. In the same limit, $\omega''$ exhibits resonant behaviour (see figure 4), indicative of avoided crossings in the spectrum, peaking at a value of:

\[
|\omega''| \to \frac{4k_0^2c}{L_c} |\zeta| \approx 2\pi \times 0.10 |\zeta| \text{ MHz nm}^{-2}.
\]

We plot the lower ($\pm \to -$) branches of equations (23) and (24) in figure 4 for two values of $\xi$: $\xi = -1$, representative of realistic micromirrors, and $\xi = -10$, representative of a highly reflective micromirror. These correspond to cases (c) and (f) in figure 3, respectively. Coupling between the pairs of modes is not very strong for the $\xi = -1$ case; this is manifested by means of the smooth variation with $x$ of $\omega'$ and $\omega''$ in figure 4(a). The second case shows strong signs of the avoided crossing behaviour seen in figure 3(f), with $\omega'$ no longer behaving smoothly and $\omega''$ acquiring a resonance-like character. Note that, independently of the magnitude of $\xi$, the strongest quadratic coupling always occurs at the points where $\omega' = 0$.

In parameterizing our interaction in terms of a frequency shift $\Delta \omega$ we are effectively mapping the model originating from the TMM into a single-optical-mode model. It is important to note that this mode spans the entire cavity regardless of the nature of $\xi$; what depends on $\xi$ is the spatial profile of the mode. In the limit $\xi \to 0$, the field intensity is distributed uniformly...
Figure 4. Linear and quadratic optomechanical couplings as a function of mirror position for a very good cavity and for (a) \( \zeta = -1 \), and (b) \( \zeta = -10 \). In each figure we show the linear (solid curve) and quadratic (dashed curve) couplings, from equations (23) and (24). Note that the peak value of \( \omega'' \) is roughly proportional to \( \zeta \) whereas \( \omega' \) is bounded.

throughout the cavity, whereas for large \(|\zeta|\), it is concentrated on one side of the membrane. These two situations are, as we have already discussed, handled differently in the CQED model, the former in terms of a single optical mode, and the latter in terms of two coupled optical modes. To highlight the increasing discrepancy between the TMM and coupled-cavities model as \(|\zeta|\) decreases, we show in figure 5 the static force acting on the scatterer (i.e., the force when \( v = 0 \)) as predicted by the two models. For the coupled-mode model, we use the predictions of [32], which hold for \( |r| \rightarrow 1 \), and deliberately misapply them to cases where \( |r| \ll 1 \). From this model, given an input power \( P_{in} \), a tunnelling frequency \( g = c |t| / L_c \), and a detuning \( \Delta \) from resonance at \( x = 0 \), one obtains

\[
F_0 = -\frac{2\omega'\kappa_c}{k_0 c} \frac{\kappa_c^2 + (\Delta + \omega' x)^2 - g^2}{(2\kappa_c \Delta)^2 + (\kappa_c^2 + \omega'^2 x^2 + g^2 - \Delta^2)\Delta^2} P_{in},
\]

with \( \omega' = -2k_0 c / L_c \). For large \(|\zeta|\), the two descriptions are essentially identical; indeed, it is easy to understand that the description of two coupled cavities is a good one when the intensity reflectivity of the order of 50% (\(|\zeta| \sim 1\)), however, the coupled-cavity description does not work well and one must switch to a scattering model to describe the situation accurately. Physically, this discrepancy comes about because of the ansatz of two cavity modes that communicate through a (fixed) coupling rate \( g \). When the reflectivity of the central mirror is far from 100%, this coupling rate becomes more sensitive to the interference between the fields on either side of the central mirror, and in turn becomes a sensitive function of \( x \). However, the two models agree around the point where the two cavity modes approach most closely, for there the approximation of a constant \( g \) is still valid. For smaller \(|\zeta|\) still, as we have already mentioned, the predictions of the scattering model again agree with a CQED model of a scatterer (e.g., an atom) coupled to a single, essentially unperturbed, cavity field.
Figure 5. The static force (i.e., the force acting on the mirror when $v = 0$) computed from the scattering model presented here (left panels) and a model based on a modal decomposition [32] (right panels), showing only one pair of modes. Red and green regions represent forces pointing in opposite directions, as indicated on the colour bar. We note the agreement between the two models for $x \approx 0.25\lambda$ and for $\Delta L_c$ close to the resonances, especially for large $|\zeta|$. The discrepancies between the two sets of data, that are more pronounced for small polarizability, have significant consequences for any theory based on a coupled-cavity modal decomposition model. The black dashed lines (equation (20)) trace the cavity resonances in the scattering model. The absolute values on the colour bar relate to the left panels. (a) $\zeta = -0.100$, (b) $\zeta = -0.500$, (c) $\zeta = -1.000$, (d) $\zeta = -2.000$, (e) $\zeta = -5.000$ and (f) $\zeta = -10.000$. 

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4. Conclusion

We have developed a generically-applicable theory to describe the motion of scatterers in electromagnetic fields. By applying this theory to the specific case of a scatterer in a cavity, we have shown how the scattering description can be used to bridge the gap between atom-CQED models, which rely on the atom interacting with one single mode that spans the entire cavity, and membrane-CQED models, where the membrane splits the cavity field into two coupled modes. It is in the region of current experimental interest, with membrane intensity reflectivities of the order of 50%, that the discrepancy between the two descriptions starts emerging and where the usual ‘$|r| \to 1$’ limit of membrane-CQED cannot be taken.

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