Abstract—The effect of blade number on small Horizontal Axis Wind Turbine (HAWT) has been studied experimentally and numerically in this research. The turbine blade is made of a flat metal sheet and the tip was formed to shape a winglet. The 5-blades turbine was tested inside a wind tunnel for performance investigation at different wind speeds. The experiment was conducted under various wind speed, i.e. 3.5 m/s, 3.9 m/s, 4.3 m/s, 4.6 m/s dan 5 m/s. Furthermore, three wind turbines geometry with different blade number (3, 4, and 5 blades) were built for numerical study purpose by using Ansys Fluent and the results were compared to the experimental one. The results show that the blade number does increase the wind turbine torque and there is also more power generated from the turbine with more blade numbers since torque is related to pressure. Moreover, the winglet helps the blade to retain the flow and increases the pressure on the blade surface. However, the experimental measurements obtained were smaller than the numerical predictions about 50% on the average since more unidentified losses existed and not accounted for the calculation.

Index Terms—Computational fluid dynamics, blades number, horizontal axis wind turbine, wind energy, performance.

I. INTRODUCTION

The demand for electrical energy continuously grows every year [1], it was projected that world energy demand would increase by approximately 50% between 2018 and 2050 [2]. Currently, 85% of the world’s energy consumption depends on fossil fuels, the principal CO$_2$ emission source [3], [4]. Moreover, the fossil fuel industry, as the primary producer and consumer of energy, is the leading contributor to climate change. On the other hand, petroleum-based fuels are nonrenewable, and the reserves continuously depleted. In order to fulfill the demand, humans must find other sources of energy that more eco-friendly to depend on. Electrical generation from renewable energy will be a prospective solution to fulfill the demand since the sources were abundant [5].

Wind energy is one of the fastest-growing energy sources in the world with zero-emission and pollution. The wind turbine produces electricity by converting the wind’s kinetic energy into mechanical energy. Wind energy is more reliable than other renewable energy sources since it can generate power 24 hours a day and not depend on sunlight. Compared to solar energy, as an example, which is dependent on sunlight and weather conditions.

The wind power manufacturer generally uses a horizontal or vertical wind turbine to generate power from wind flow. Commonly, it consists of blades pointed into the wind and connected to the rotor and then to a generator. This system requires larger blades, taller towers, and more areas of land to gain higher energy output. To capture more wind energy, manufacturers mounted the rotor at the top of the tall tower since wind speed near the ground surface was very low. However, complaints of a threat to wildlife, noise and visual pollution, and high production and maintenance cost continues to obstruct the development [6]. As the solution, SheerWind developed Invelox that offers a novel concept of wind power generation, especially for low wind speed applications [7]. The design, as shown in Fig. 1, captures wind with a funnel and directs it through a shrouded venturi to increase the speed. The turbine generator is placed safely at ground level to convert the energy into electrical energy (reduced installation and maintenance cost). The invention of Invelox influenced other researchers to study the system that can enhance the wind power from the flow at the atmospheric boundary layer.

![Fig. 1. SheerWind Invelox wind power system.](Source: SheerWind, 2012).

The information gathered from the experimental test tend to be limited since many parameters are not accessible because of the limitation of equipment capabilities or adequate tools. The use of CFD can help to provide detailed data on flow characteristics that very useful for understanding the flow behavior [8]. The investigation of Invelox numerically has been conducted to study the advantages in terms of power generation compared to the
conventional wind generation system. The simulation shows that the wind speed at the venturi section gives 6-8 times more power [9]. Furthermore, the application of wind turbines for a small scale has been investigated to know the effect of the blade number on the performance [10]. The study shows that the number of blades affects the performance, with a more significant number of blades, give better results [11]. However, the number of blades should be determined carefully to obtain the cost-benefit and weight reduction [12].

Small scale wind turbine experimental and numerical investigation has been reported in this article. This work aims to investigate the influence of the blade number on the wind turbine performance for the future application inside an Invelox venturi section and determine the most effective blade number for the design. Three turbine models with a different number of winglet blades were compared in various wind speeds. A mathematical model introduced for predicting the pressure distribution on the surface of the blade to obtain the power coefficient.

II. WIND TURBINE POWER CALCULATION

The power generated by the wind turbine is a very important parameter that has to be predicted before it is actually produced. The turbine behavior under different wind speed is another point that has to be studied in order to understand the estimated energy values. Reference [13] describes the mathematical model of wind turbine power and energy output. It begins with the equation of work (W) that is equal to the amount of energy transferred or converted by force, i.e.:

$$W = E = F \cdot s$$

where $F$ is the applied force and $s$ is objects’ displacement. Newtons’ second law of motion describes that force is equal to mass ($m$) times acceleration ($a$). Hence, work can be rewritten as;

$$E = m \cdot a \cdot s$$ \hspace{1cm} (1)

From the equation of motion, the acceleration ($a$) can be written as;

$$a = \frac{v^2 - u^2}{2s}$$

where $v$ is the wind speed, and $u$ is the object velocity. Since the object was initially at stationary condition, i.e., $u=0$, the motion equation can be simplified as;

$$a = \frac{v^2}{2s}$$ \hspace{1cm} (2)

Hence, the kinetic energy of an object in motions can be described by substituting (2) in to (1).

$$E = \frac{1}{2} mv^2$$

Thus, the energy flow rate or the power generated by wind is defined as;

$$P = \frac{dE}{dt} = \frac{1}{2} \frac{v^2}{t^2} \frac{dm}{dt}$$ \hspace{1cm} (3)

As mass flow rate can be written as;

$$\frac{dm}{dt} = \rho Av$$ \hspace{1cm} (4)

Furthermore, by substituting the mass flow rate equation in to (3), the power equation can be written as;

$$P = \frac{1}{2} \rho Av^3$$ \hspace{1cm} (5)

And by applying Betz law [14] into the power equation, the extractable power by the wind turbine can be estimated as follows;

$$P_{WT} = 0.59 \frac{1}{2} \rho Av^3$$ \hspace{1cm} (6)

where $A$ is the turbine swept area, as shown in Fig. 2.

III. METHODOLOGY

A. Experimental Setup

The wind turbine tests, as shown in Fig. 3, were conducted at the Mechanical Engineering Laboratory, Universitas Mercu Buana. The low-speed wind tunnel consists of a square test section with 0.8 meter width and 3 meter length. A large bell mouth screen and a honeycomb flow straightener were mounted at the wind tunnel inlet.
A wind turbine model, shown in Fig. 4, was fabricated for the current investigation consisting of 5 blades made of a flat metal sheet. The turbine blade has an overall 300 mm diameter. The blade tip was formed to shape a winglet with an angle of pitch 10 degrees. The turbine then tested inside the wind tunnel for performance investigation at different wind speeds, i.e., 3.5 m/s, 3.9 m/s, 4.3 m/s, 4.6 m/s, and 5 m/s. The digital anemometer was used to measure the wind speed inside the tunnel. The turbine shaft was connected to a 12VDC small brushed permanent magnet (PMDC) generator with armature resistant \( I_a \) of 0.43 Ω. The generated output power was measured by using a digital power meter, and the shaft speed was monitored by using a non-contact tachometer.

### B. Numerical Model Application

Furthermore, a CAD geometry was constructed to model the 5-blades turbine based on the actual wind turbine dimension. An unstructured mesh was built to model the wind tunnel domain and then subtracted by the 3D wind turbine geometry using Boolean operation [15]. The turbines were simulated in various wind velocity using ANSYS Fluent, and the results were compared to the experimental one. The boundary conditions of the domain were set to match the experimental conditions. Shear Stress Transport (SST) turbulence model was used to model the transient viscous flow [16], [17]. The second and the third model, as shown in Fig. 5, was constructed with different blade numbers (3 and 4 blades) and simulated numerically under the identical boundary condition and numerical setup.

IV. RESULTS AND DISCUSSION

The wind turbine performance and effect of various blade numbers are discussed here. The turbine was investigated experimentally inside a wind turbine at various wind velocity of 3.5 m/s, 3.9 m/s, 4.3 m/s, 4.6 m/s, and 5 m/s. Furthermore, the numerical simulation has been performed with blade number variation of 3, 4, and 5 blades. Both results compared and discussed below.

#### A. Effect of Blade Number

Fig. 6 shows the comparison of pressure contour for different turbine designs. The results were obtained from the numerical simulation at a wind velocity of 5 m/s. The results show that the pressure concentration does exist at the blade tip. The figures demonstrate that the winglet helps the blade to retain the flow and increases the pressure on the blade surface. More blades number shows more pressure that occurred on the turbine surface. As a result, more power generated from the turbine with more blade numbers since torque is related to pressure.

![Fig. 6](image)

For the investigation of blade number effect on torque and power output, the numerical results were presented in Fig. 7. The power extracted from the wind turbine was transmitted to the generator by the rotating shaft in the form of torque. The estimated power was calculated by multiplying the torque, angular velocity, and power coefficient (Betz’s number). The results show that the pressure, power, and torque increased as the higher blade number since torque is the summation of pressure and viscous stress integration [18]. It is shown that the power was increased by 32% as the
number of blades increased from 3 to 4 and 4 to 5. Similar results have been reported to show that the higher number of blade turbine has a better performance [10], [12], [19]. However, the maximum blade number is limited to specific value, since increasing the blade number will give additional weight [12].

B. Effect of Wind Speed

Fig. 8 shows the comparison of power output from the numerical, experimental, and theoretical results of the various turbine design. The experimental results obtained by reading the power output from the generator connected to the rotor and the theoretical results acquired from the multiplication of air density, rotor swept area, power by three of wind velocity, and Betz number [14] as defined in (6). Betz law states that the theoretical power output is the maximum power that can be produced by a wind turbine system. The result shows that increasing the wind speed by 1 m/s would double the power generated by the turbine. It would be interesting to expand the study for a wind turbine with more blade number to know the critical point that effect on the performance changes for future work.

C. Effect of Generator Losses

Many factors contributed to energy losses, such as aerodynamic and generator resistances, was occurred during the wind energy conversion [20]. In this calculation, the losses attributed by the generator were considered since turbine losses were already included in Betz limit. Fig. 9 demonstrates the mechanical power conversion in to electrical in the generator. The figure shows that not all mechanical power converted to electrical power, and the output reduced by the energy losses. The major losses that occurred on the generator can be categorized into the following groups; shunt field excitation, brush drop and stray load, armature winding, brush friction and part of the armature iron, mechanical windage, and part of the electromagnetic. As a result, the generator output power measurements are likely to be lower than the mechanical power transferred by the wind turbine rotor. The following major losses were described and accounted for the output energy reduction. These losses are; 1) copper losses that caused by the electric current flows in a conductor with limited resistance; 2) iron/core losses, including the hysteresis and eddy current losses from the magnetic field; 3) mechanical losses which caused mostly by friction in bearings and brushes and rotational air-friction. Some previous studies [21]-[23] were benefited by estimating the power losses from the known equations as follow;

\[
P_{\text{armature}} = I_a^2 R_a
\]
\[
P_{\text{fm}} = V I_{\text{fm}}
\]
\[
P_{\text{mech}} = 1.5 F v 10^{-5}
\]

where;
\(I_a\) = armature current (A)
\(R_a\) = armature resistant (Ω)
\(V\) = Voltage (V)
\(I_{\text{fm}}\) = magnetic field current (A)
\(F\) = radial force in the bearing (N)
\(v\) = perimeter speed of bearing (m/s)
\(d\) = roller diameter (m)

However, the losses computation, as described in the above formula, requires complete design information. For more computational simplification, Safiuddin [24] proposes a model of expression for determining the rated losses from DC machine based on statistical multiple regression techniques as shown in (7). The expression was a function of rotational speed (ω) in RPM, armature volume \(d^2 l\) (DSQL) in cubic, and the percentage of armature droop (delta).

\[
\% \text{ losses} = 3.832+ \frac{2545.22}{\text{RPM}} + \frac{5751.54}{\text{DSQL}} + 0.389 \Delta - 1.424 \frac{\text{RPM}}{\text{DSQL}} - 0.2795 \frac{\text{DSQL}}{\text{RPM}}
\]  

(7)

Fig. 7. Comparison of mechanical power results from numerical simulation with different blades design.

Fig. 8. Mechanical power generated from different wind velocity.

Fig. 9. Energy losses in the wind turbine.
where \( \Delta R = 100 \, I, \frac{R}{V} \).  

The mechanical power predictions obtained from numerical simulation were subtracted by the losses calculated from the above equation, and results were compared to the experimental measurements and presented in Fig. 10. The figure shows that the experimental results were lower than numerical prediction results about 50% on the average. As an accumulative result, the actual generator efficiency was lower than the prediction since there were more unidentified losses that occurred and not accounted for the calculation. From the studies previously conducted, Kang and Meneveau [25] suggest that measuring the output power from the generator can lead to misleading information about the performance of the wind turbine and questioned the validity of the result. For future works, it was essential to measure the rated power losses of the generator for a better understanding of the wind turbine performance. The better solution to solve the problem was by measure the shaft torque directly using a high-precision rotary torque sensor as performed by Bastankhah and Porté-Argel [26].

V. CONCLUSION

The effect of blade number on small Horizontal Axis Wind Turbine (HAWT) performance has been studied experimentally inside a wind tunnel and numerically using a commercial software. The results show that the blade number does increase the wind turbine torque and output power. The winglet affects the performance by increasing the pressure on the blade surface and concentrating the wind flow at the blade tip. The power generated from experimental measurements was lower than the numerical prediction. The energy losses from the wind turbine and generator contributed to performance reduction.

CONFLICT OF INTEREST

The authors declare that there is no conflict of interest regarding the publication of this article.

AUTHOR CONTRIBUTIONS

AFS wrote the manuscript and conducted the CFD analysis; MK fabricated and assembled the turbine; SS and his team performed the experiment using a wind tunnel and analyzed the experimental data; and IA provided the measurement tools and other experimental equipment. All authors had approved the final version.

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