Membrane Heating in Living Tissues Exposed to Nonthermal Pulsed EM Fields

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A bio tissue model consisting of multilayer spherical cells including four nested radial domains (nucleus, nuclear membrane, cytoplasm and plasma membrane) is worked out to derive the cell heating dynamics in presence of membrane capacitance dispersion under pulsed electromagnetic exposure. Two possible cases of frequency-dependent membrana models are discussed: plasma and nuclear membranes are dispersive, only the nuclear memebane is dispersive. In both models an high localized heating of the membranes occurs, without significant temperature rise in the cytoplasm and nucleoplasm.

Keywords: Bioelectromagnetic interaction, Effective Medium Theory, Non-thermal effects, Pulsed (EM) Fields.

I. INTRODUCTION

Substantial efforts on behalf of the Scientific Community have been recently addressed to the experimental assessment and theoretical investigation [1] of the response of living cells to ultrashort (sub-nanosecond) intense (MV/m) electromagnetic field pulses (see also [2] for a tutorial). Cell exposure to pulsed EM fields in the nsec-µsec range is known to produce transient or permanent permeabilization (electroporation [3]) of the cytoplasmic membrane, depending on pulse amplitude, through a peculiar breakdown phenomenon occurring when the transmembrane potential difference exceeds some critical level (∼1V). Cell response to ultrashort pulses is markedly different. Basically, the integrity of the cytoplasmic membrane is not directly affected, although the transmembrane potential difference may largely exceed the poration breakdown threshold. Substantial permeabilization of the organelles, including the nucleus is observed instead, usually triggering an apoptotic response (signaled, e.g., by externalization of phosphatidylserine [4]), which eventually (typically several minutes after exposure) leads to membrane dissolution and cell remnants removal by macrophages. Such a mechanism may hold a potential for cancer treatment [5]. In fact, effective selective destruction of several types of tumors, including skin melanomas and colorectal carcinomas (two of the ‘big killers’), up to complete remission, have been reported after suitably tuned ultrashort EM pulse exposure [6]. This mechanism of action differs completely from that of microwave hyperthermia [8], where tumor necrosis is induced by selective heating of the neoplastic tissue. Exposure to ultrashort pulses, on the contrary, does not produce any sensible macroscopic thermal response, nor (killing the cells through apoptosis) an inflammatory response. In order to understand the underlying physical mechanisms, it is necessary to develop a model providing a good tradeoff between simplicity and realism. Most studies are based on the cell model proposed by Schwan et al. [9]-[11] consisting of a single spherical cell (extracellular medium, plasma membrane and cytoplasm) whose electromagnetic constitutive parameters are treated as frequency independent. On the other hand, it is well known that the membrane specific capacitance is strongly frequency-dependent [12]. In [13] we investigated the thermal response of a simple cell model (spherical homogeneous, with frequency dependent membrane capacitance) to a pulsed-electromagnetic field by solving the coupled electromagnetic and heat-diffusion problems. Our findings suggest that whenever the pulse duration is small compared to the thermal relaxation constant of the cell membrane, and the membrane capacitance drops to its low asymptotic high-frequency value in the pulse spectral bands, one may observe a steep increase in the membrane temperature, up to physiologically significant levels, the average (cytoplasm) temperature remaining essentially unaffected. Similar conclusions were obtained in [14] following a more sophisticated approach which combines Smoluchowski equation to describe membrane response, the heat equation and molecular dynamics simulations, to gauge the impact of localized membrane heating on membrane poration.

In this paper we extend the analysis of [13] to the more realistic case where the cell is part of a bio-tissue. We also adopt a more general cell model consisting of four radially nested domains (nucleus, nuclear membrane, cytoplasm and plasma membrane supposed concentric), including frequency dependence of both the plasma and nuclear membranes. In the paper the membrane capacitive models used do not depend on voltage, this implies that the analysis holds only when the external electric fields are not strong or long enough to create membrane pores.

In order to solve the pertinent electromagnetic boundary value problem, in the quasi-static limit, we use Effective Medium Theory (henceforth EMT) throughout [15]. Numerical simulations based on this more realistic model confirm the occurrence of a steep temperature raise in the plasma membrane, without any significant temperature variation in the cytoplasm and nucleus.

The paper is accordingly organized as follows. In Section II we use EMT to derive the effective permittivity of a tissue; in Section III we derive the response of
a cell inside a tissue, connecting the local field to the external (impressed) field. In Section IV we solve the coupled electromagnetic and heat-diffusion problems for a (multilayer) spherical cell with linearized, dispersive nuclear and plasma membranes, embedded in a tissue and exposed to a (pulsed) monochromatic electromagnetic field, using a toy model for membrane capacitance dispersion. Representative numerical results are briefly illustrated and discussed in Section V. Conclusions follow in Section VI.

II. CELLS IN A TISSUE

Living tissues are regular assemblies of densely packed cells. Cubic lattices, e.g., including the simple-cubic (sc), body-centered cubic (bc) and face-centered cubic (fc) arrangements sketched in Fig. 1, have been suggested as simple tissue morphology models [16]. The ratio between the cell radius \( R_c \) and the lattice unit-cell side length \( d_{\text{latt}} \) in Fig. 1 determines the cell volume fraction \( f_c \),

\[
f_c = \frac{4}{3} \frac{\pi}{N_c} \left( \frac{R_c}{d_{\text{latt}}} \right)^3,
\]

\( N_c \) being the number of bio-cells contained in the lattice unit-cell (1, 2 and 4 for the sc, bc and fc cubic lattices, respectively). The maximum volume fractions correspond to touching cells, and are 0.52, 0.64 and 0.74 for sc, bc and fc cubic lattices, respectively. In this paper we consider separate living cell (no touching cells) in the tissue.

The cells density reported above is the maximum volume fraction that can be obtained for a suitable value of ratio \( R_c/d_{\text{latt}} \), as can be seen by equation (1).

In order to model dense tissue we approximate the cells arrangement like a face centered cubic lattice; this geometry allow us to keep \( f_c \) higher than the maximum volume fraction of sc and bc cubic lattice and in the same time \( f_c \) is below the maximum value 0.74 which correspond to touching spherical cells. Furthermore \( f_c \) cubic lattice seems to be the most realistic model for a living tissue [17].

A. Effective Permittivity of a Single Cell

A simple model of a living cell is sketched in Figure 2: a stratified sphere, where \( R_p \) is the radius of the cytoplasm, \( \delta_p \) is the thickness of the plasma membrane, so that \( R_c = R_p + \delta_p \), \( R_n \) is the radius of a spherical organelle (assumed concentric for simplicity), and \( \delta_n \) is the thickness of the inner membrane. In the spirit of EMT [15], the multilayered cell depicted in Figure 2 can be modeled as a homogeneous sphere with an equivalent permittivity \( \epsilon_c \). A simple EMT formula is available [15] for the effective permittivity of a homogeneous sphere coated by a single layer,

\[
\epsilon_c = \frac{1 - 2G}{1 + G} \epsilon_{\text{shell}}
\]

where

\[
G = \frac{\epsilon_{\text{shell}} - \epsilon_{\text{core}}}{2\epsilon_{\text{shell}} + \epsilon_{\text{core}}} \left( \frac{R_{\text{core}}}{R_{\text{core}} + \delta_{\text{shell}}} \right)^3
\]

where \( \epsilon_{\text{core}}, \) and \( \epsilon_{\text{shell}}, \) are the core and shell complex permittivities, \( R_{\text{core}} \) is the core radius and \( \delta_{\text{shell}} \) the shell thickness. This formula can be used recursively, by assuming the core to be in turn a layered sphere, and \( \epsilon_{\text{core}} \) its effective permittivity, to obtain an explicit formula for the equivalent permittivity of the stratified cell in Figure 2 which is not reported for brevity.

![FIG. 1: The simple-cubic (sc), body-centered cubic (bc), and face-centered cubic (fc) lattice models. The lattice unit-cell side length \( d_{\text{latt}} \) is displayed.](image1)

![FIG. 2: Nucleated spherical cell (four concentric layers) exposed to a local field \( E_{\text{loc}} \). The origin of reference system is the cell center.](image2)
B. Effective Permittivity of Tissue

Letting $\epsilon_h$ the permittivity of the host medium in which the cells are dispersed, we may use Bruggemann formula [15] to derive the effective permittivity $\epsilon_{eff}$ of the bio-tissue as follows

$$f_c \frac{\epsilon_c - \epsilon_{eff}}{\epsilon_c + 2\epsilon_{eff}} + (1 - f_c) \frac{\epsilon_h - \epsilon_{eff}}{\epsilon_h + 2\epsilon_{eff}} = 0$$

(4)

where $\epsilon_c$ and $f_c$ are the equivalent cell permittivity and the cell volume fraction in the tissue, respectively. We note in passing that Bruggemann formula, which treats the host and the inclusions in a symmetric way, is more appropriate for modeling a densely packed tissue, compared to the Maxwell-Garnett formula used in [18], which is accurate only when $f_c \ll 1$ [15].

C. Average vs Local Field

Let $E_{eff}$ the effective (average) field in the effective medium with permittivity $\epsilon_{eff}$ representing the tissue; $E_{loc}$ the local field to which a single cell is actually exposed (see Fig. 2), and $E^{(c)}$ and $E^{(i)}$ the local external and intracellular fields including the cell response to $E_{loc}$. Under the quasi-static approximation, consistent with the use of EMT, and assuming the effective and local fields as linearly polarized parallel to the lattice edge, we may write following [19] (see Fig. 3) for the relevant notation

$$E_{eff}d_{latt} = \int_{-d_{latt}/2}^{R_c} E_z^{(c)}(z) \, dz$$

$$+ \int_{-R_c}^{R_c} E_z^{(i)}(z) \, dz + \int_{R_c}^{d_{latt}/2} E_z^{(c)}(z) \, dz$$

(5)

and [20]

$$\left\{ \begin{align*}
E_z^{(i)}(z) &= \frac{3\epsilon_h}{\epsilon_c + 2\epsilon_h} E_{loc}, \\
E_z^{(c)}(z) &= \frac{2(\epsilon_c - \epsilon_h)}{\epsilon_c + 2\epsilon_h} \left( \frac{R_c}{z} \right)^3 + 1 \right\} E_{loc},
\right. \tag{6}
$$

Equations (5), (6) can be combined to relate the effective and local fields as follows:

$$E_{loc} = \frac{E_{eff}}{1 + 2 \frac{R_c}{d_{latt}} \frac{\epsilon_h - \epsilon_c}{\epsilon_c + 2\epsilon_h}}.$$

(7)

It should be noted that the analysis carried out in this work holds only when the external electric fields are not strong or long enough to induce the formation of membrane pores.

D. Average vs Impressed Field

Finally we consider a tissue specimen in vacuum. The effective field in the tissue $E_{eff}$ is related to the vacuum applied field $E_0$ in a way which depends on the tissue specimen geometry and orientation with respect to the applied field. We shall consider the case where the tissue forms a circular disc (like a cultured cell layer in a Petri glass). Also, for the sake of simplicity, we shall assume that the disc diameter is also electrically small. Thus, again in the quasi-static limit,

$$E_{eff} = \Xi(\epsilon_{eff}, \epsilon_0, \epsilon_{sub})E_0$$

(8)

where $\epsilon_{sub}$ is the dielectric constant of the tissue substrate (e.g., glass). The explicit form of the factor $\Xi(\epsilon_{eff}, \epsilon_0, \epsilon_{sub})$ can be obtained in the quasi-static approximation using EMT, under suitable assumptions about the tissue and substrate dimensions. For the simplest case where $\epsilon_{sub} \approx \epsilon_0$, $\Xi(\epsilon_{eff}, \epsilon_0, \epsilon_{sub}) = \epsilon_0/\epsilon_{eff}$ if the field is orthogonal to the tissue and $\Xi(\epsilon_{eff}, \epsilon_0, \epsilon_{sub}) = 1$ if the field is parallel to the tissue.

Equations (7) and (8) provide the needed relationship between the field $E_0$ applied to a tissue specimen, and the local field $E_{loc}$ seen by each cell in the tissue. All equations in this section can be rewritten in terms of the complex material conductivities, modulo the usual substitution $\epsilon \rightarrow \sigma/\omega$.

III. FIELDS AND POWERS IN A TISSUE CELL

It is now possible to derive the electromagnetic field and dissipated power distribution for each cell embedded in a tissue, by solving the single (spherical, multilayer) cell boundary value problem whose geometry is sketched in Fig. 2. In the quasi-static approximation, the total
field can be derived from the (spectral) scalar potential

\[ \Phi(\vec{r}, \omega) = \Phi_0(\vec{r}) - E_{\text{loc}}(\omega) \rho \cos \vartheta + \Phi_s(\vec{r}, \omega), \]  

where \( E_{\text{loc}} \) is the local field acting on the cell, \( \Phi_0(\vec{r}) \) is the resting potential

\[ \Phi_0(\vec{r}) = [1 - U(\rho - R_n)]V_n + [1 - U(\rho - R_p)]V_p, \]  

\( U(\cdot) \) being Heaviside’s step-function, \( V_n, V_p \) the cytoplasmatic and nuclear transmembrane potentials, and

\[ \frac{\Phi_s(\vec{r}, \omega)}{E_{\text{loc}}} = \left\{ \begin{array}{ll}
\Xi(\omega) \rho \cos \vartheta & \rho < R_n \\
\Psi(\omega) \rho^{-2} \cos \vartheta & \rho > R_c \\
\Theta(\omega) \rho^{-2} + \Sigma(\omega) \rho \cos \vartheta & R_n < \rho < R_c
\end{array} \right. \]  

the (dipolar) cell-response potential. The functions \( \Xi(\omega), \Psi(\omega), \Theta(\omega), \Sigma(\omega) \) are determined by enforcing continuity of the (radial, inward) current density across the cell and nuclear membranes, viz.

\[ \sigma_{\text{eff}}(\omega) \frac{\partial \Phi}{\partial \rho}|_{\rho=R_c+\delta_\rho} = \sigma_2(\omega) \frac{\partial \Phi}{\partial \rho}|_{\rho=R_p} = \Upsilon_1(\omega)\delta \Phi_1, \]  

\[ \sigma_2(\omega) \frac{\partial \Phi}{\partial \rho}|_{\rho=R_n+\delta_\rho} = \sigma_3(\omega) \frac{\partial \Phi}{\partial \rho}|_{\rho=R_n} = \Upsilon_3(\omega)\delta \Phi_3, \]

where

\[ \delta \Phi_1(\vartheta, \omega) = \Phi(R_p + \delta_\rho, \vartheta, \omega) - \Phi(R_p, \vartheta, \omega) - V_p = \Phi_s(R_p + \delta_\rho, \vartheta, \omega) - \Phi_s(R_p, \vartheta, \omega), \]  

and

\[ \delta \Phi_3(\vartheta, \omega) = \Phi(R_n + \delta_\rho, \vartheta, \omega) - \Phi(R_n, \vartheta, \omega) - V_n = \Phi_s(R_n + \delta_\rho, \vartheta, \omega) - \Phi_s(R_n, \vartheta, \omega), \]

are the transmembrane excess potentials of the plasma and nuclear membrane. In equations \( 12, 15 \), \( \sigma = \sigma - j \omega \tau \) is the complex frequency-dependent conductivity, and the suffixes \( \text{eff}, 2, 3 \) refer to the external (effective) medium, cytoplasm and nucleus, respectively. \( \Upsilon_1(\omega), \Upsilon_3(\omega) \) are the cytoplasmatic and nuclear membrane specific admittances \( (ohm^{-1}m^{-2}) \). These latter can be written

\[ \Upsilon_1(\omega) = G_1(\omega) + j \omega C_1(\omega) = \delta^{-1}_p \delta_1(\omega) \]  

\[ \Upsilon_3(\omega) = G_3(\omega) + j \omega C_3(\omega) = \delta^{-1}_p \delta_3(\omega) \]

where \( G \) and \( C \) denote the pertinent membrane specific conductance and capacitance, \( \sigma \) the complex membrane conductivity, and \( \delta \) the membrane thickness. Hereinafter the (carrier) frequency dependency of the spectral quantities is implicit and omitted for lighter notation. After some simple algebra, neglecting the membrane thickness, one gets

\[ \Xi = 1 - 9 \Upsilon_1 \Upsilon_3 R_p^4 R_n \sigma_{\text{eff}} \Gamma^{-1} \]
A. Power Deposition in the presence of Membrane Dispersion

In the following we specialize eqs. (25) to (28) to include membrane(s) specific capacitance dispersion adopting the model [13] in two cases: a) both membranes are dispersive; b) only the nuclear membrane is dispersive. The two models take into account the morphological differences existing between the organelle membrane and the cell membrane [21]. The model [13] introduces the functional form of $C_i(\omega)$ and/or $C_3(\omega)$, for the positive frequency axis we have

$$C_i(\omega) = C_\infty - \frac{1}{2}(C_\infty - C_0)\text{Erfc} \left( \frac{\omega - \omega_0}{\Delta \omega} \right) \quad i = 1 \text{ or } 3$$

where Erfc(·) is the complementary error function. Capacitance for negative frequencies are obtained by $C_i(-\omega) = C_i(\omega)$. With reference to the case a), eqs. (25) to (28) reduce to:

$$\frac{P_1}{|E_{loc}|^2} = \frac{3}{2} \pi R_p^4 |\Re[\Upsilon_1]|,$$

$$\frac{P_2}{|E_{loc}|^2} = \frac{1}{2} \pi \sigma_2 R_p^5 \left| \frac{\Upsilon_1}{\sigma_2} \right|^2,$$

$$\frac{P_3}{|E_{loc}|^2} = \frac{27}{8} \pi R_n^2 \Re[\Upsilon_3] \left| \frac{R_n \Upsilon_1}{\sigma_2} \right|^2,$$

$$\frac{P_4}{|E_{loc}|^2} = \frac{27}{8} \pi R_n^3 \sigma_4 \left| \frac{R_n \Upsilon_3 \Upsilon_1}{\sigma_2^2} \right|^2.$$

If only the inner membrane is dispersive as supposed in case b), eqs. (25) to (28) yield

$$\frac{P_1}{|E_{loc}|^2} = \frac{2}{3} \pi R_p^4 |\Re[\Upsilon_1]| \left| \frac{3 \sigma_{eff} \sigma_2}{\Upsilon_1 (2 \sigma_{eff} + \sigma_2)} \right|^2,$$

$$\frac{P_2}{|E_{loc}|^2} = 2 \pi \sigma_2 R_p^3 \left| \frac{\sigma_{eff}}{2 \sigma_{eff} + \sigma_2} \right|^2,$$

$$\frac{P_3}{|E_{loc}|^2} = \frac{27}{2} \pi R_n^4 \Re[\Upsilon_3] \left| \frac{\sigma_{eff}}{2 \sigma_{eff} + \sigma_2} \right|^2,$$

$$\frac{P_4}{|E_{loc}|^2} = \frac{3}{2} \pi R_n^5 \sigma_4 \left| \frac{9 \Upsilon_3 \sigma_{eff}}{2 \sigma_{eff} + \sigma_2} \right|^2.$$

IV. TEMPERATURE EVOLUTION

We first study the thermal evolution of tissue under the adiabatic approximation i.e. the temperature field changes are slow with respect to the EM field dynamics. We find that with suitable EM carrier a relevant rapid increase in membrane temperature occurs while the average cell temperature does not rise. In the following section the full thermal response analysis confirms the order of magnitude calculation displaying quantitative features of proposed models.

A. Adiabatic Approximation

The power dissipated in each elementary cube of tissue in Figure 1 is

$$P_{eff} = \frac{\omega \text{Im}[c_{eff}]}{2} |E_{eff}|^2 d_{att}.$$  (38)

Each elementary cube contains four cells, where the total dissipated power is

$$P_{cells} = 4(P_1 + P_2 + P_3 + P_4).$$  (39)

Accordingly, the fraction of power absorbed by the tissue which is actually dissipated in the cells is $\eta = P_{cells}/P_{eff}$. The volume density $Q_i$ of the power dissipated in each regions of the cell can be directly related to the macroscopic tissue Specific Absorption Rate (SAR) as follows:

$$\tilde{Q}_i = \xi \text{SAR} \frac{\eta_1 + \sum_{j \neq i} \eta_j V_j}{V_i}, \quad i = 1 \ldots 4,$$  (40)

where $\eta_i$ and $V_i$ are the pertinent mass densities [kg/m$^3$] and volumes, respectively.

On time-scales much shorter than the typical heat-diffusion time constant $\tau_D$ across the cell subregions [27] the temperatures $\Theta_i$ will evolve adiabatically, so that

$$\frac{\partial \Theta_i}{\partial t} \approx \frac{\tilde{Q}_i}{\eta_i c_{i}^{(p)}},$$  (41)

where $c_{i}^{(p)}$ are the pertinent (constant-pressure) heat capacities.

Hence, for case a) in section III A we have

$$\frac{\partial \Theta_1}{\partial t} \approx \frac{\tilde{Q}_1}{\eta_1 c_1^{(p)}} \approx \frac{SAR R_p}{\eta_1 c_1^{(p)}} \frac{\eta_2}{(3 \sigma_2 \Re[\Upsilon_1] + R_p |\Upsilon_1|^2)},$$

$$\frac{\partial \Theta_3}{\partial t} \approx \frac{\tilde{Q}_3}{\eta_3 c_3^{(p)}} \approx \frac{3}{4} \frac{SAR R_p R_n^2 c_3^{(p)}}{\eta_3 c_3^{(p)}} \frac{\eta_2}{\Re[\Upsilon_1] |\Upsilon_1|^2}.$$  (42)
\[
\frac{\partial \Theta_2}{\partial t} \approx \frac{\dot{Q}_2}{\eta_2 c_i^{(p)}} \approx SAR \frac{R_p}{3 c_i^{(p)}} Re[\bar{\bar{\Theta}}_1] \sigma_2^2, \quad (44)
\]

\[
\frac{\partial \Theta_4}{\partial t} \approx \frac{\dot{Q}_4}{\eta_4 c_i^{(p)}} \approx \frac{9}{4} SAR \frac{\eta_2}{\eta_4 c_i^{(p)}} \frac{R_p^2 R_p}{\sigma_4^2} \frac{\bar{\bar{\Theta}}_4}{[\bar{\bar{\Theta}}_1]^2}, \quad (45)
\]

Similarly, for case b) in section IIIA, we have

\[
\frac{\partial \Theta_1}{\partial t} \approx \frac{\dot{Q}_1}{\eta_1 c_i^{(p)}} \approx SAR \frac{\eta_2}{\eta_1 c_i^{(p)}} \frac{\sigma_2}{[\bar{\bar{\Theta}}_1]^2}, \quad (46)
\]

\[
\frac{\partial \Theta_2}{\partial t} \approx \frac{\dot{Q}_2}{\eta_2 c_i^{(p)}} \approx SAR \frac{4\sigma_2 R_p^3}{c_i^{(p)} (4\sigma_2 R_p^3 + 27R_p^4 Re[\bar{\bar{\Theta}}_3])}, \quad (47)
\]

\[
\frac{\partial \Theta_3}{\partial t} \approx \frac{\dot{Q}_3}{\eta_3 c_i^{(p)}} \approx \frac{9}{4} SAR \frac{R_n^2}{\delta_n} \frac{\eta_2}{\eta_3 c_i^{(p)}} \frac{Re[\bar{\bar{\Theta}}_3]}{\sigma_2^2}, \quad (48)
\]

\[
\frac{\partial \Theta_4}{\partial t} \approx \frac{\dot{Q}_4}{\eta_4 c_i^{(p)}} \approx SAR \frac{R_n^2}{c_i^{(p)}} \frac{\eta_2 \sigma_4}{\eta_4 \sigma_2^2} [\bar{\bar{\Theta}}_3]^2. \quad (49)
\]

Some order of magnitude estimate can be obtained using (42-43) and (46-49), together with the physical parameters in Table I and II. Furthermore, we assume \(R_p = 10^{-3} m, R_n = 3 \cdot 10^{-4} m, \delta_p = \delta_n = 10^{-8} m\).

Results are very similar to formulas presented in [13] and suggest the possibility that the inner and/or the outer membrane temperature may rise up to levels at which biological damages occurs.

### B. Thermal Response

In this subsection the tissue thermal response is obtained using the separate cells approximation valid for short (nanoseconds) EM pulsed field. The time evolution of the temperature \(\Theta\) in the cell is obtained by solving the (coupled) heat diffusion equations

\[
\eta_i c_i^{(p)} \frac{\partial \Theta_i}{\partial t} - \nabla \cdot (\chi_i \nabla \Theta_i) = \dot{Q}_i, \quad i = 1, \ldots, 4 \quad (50)
\]

\(c_i^{(p)}, \chi_i, \dot{Q}_i\) being the heat capacity \([J/(kg^\circ K)]\), thermal conductivity \([W/(m^\circ K)]\) and EM-induced power density \([W/m^3]\). For simplicity, we shall average [28] the source term and the temperature distributions with respect to the angular variable \(\vartheta\). The heat diffusion equation in the angle-averaged quantities becomes (using the same symbols \(\bar{\bar{\Theta}}, \dot{Q}\) for the angle-averaged quantities, for notational ease)

\[
\eta_i c_i^{(p)} \frac{\partial \bar{\bar{\Theta}}_i}{\partial t} - \frac{\chi_i}{\rho^2} \frac{\partial}{\partial \rho} \left( \rho^2 \frac{\partial \bar{\bar{\Theta}}}{\partial \rho} \right) = \dot{Q}_i. \quad (51)
\]

Equation (51) can be solved numerically, starting from the initial conditions

\[
\Theta_i(\rho, 0) = \Theta_0, \quad \forall \rho \quad (52)
\]

under the following boundary conditions:

\[
\begin{aligned}
\Theta_i(\rho, t) \big|_{\rho=R_i} &= \Theta_{i+1}(\rho, t) \big|_{\rho=R_i}, \\
\chi_i \frac{\partial \Theta_i}{\partial \rho} \bigg|_{\rho=R_i} &= \chi_{i+1} \frac{\partial \Theta_{i+1}}{\partial \rho} \bigg|_{\rho=R_i}, \quad i = 1, \ldots, 4 \quad (53)
\end{aligned}
\]

expressing the continuity of temperature and heat flux across the material boundaries in Figure 2. The domain where the solution is numerically sought is truncated using the further boundary condition

\[
\frac{\partial \Theta}{\partial \rho} \bigg|_{\rho=R^*} = 0, \quad (54)
\]

where \(R^*\) is the radius of the cell-centered spheres in the tissue which touch without intersecting (e.g., \(R^* = 2^{-3/2}d_{att}\) for the fcc lattice cubic.) Equation (54) expresses the reasonable requirement that no heat flux exists between individual (neighboring) cells in the tissue. This is due to the negligible temperature diffusion on the typical EM pulses time scale.

### V. NUMERICAL RESULTS

In this section we illustrate some representative results based on numerical solution of the heat diffusion problem in Sect. III, obtained by using a finite element simulation code (COMSOL). The thermal response of a separate cell is azimuthally invariant. Due to the dipolar nature of EM excitation in the quasistatic approximation (on both inner and outer membranes) the thermal distribution takes the simple shape of \(\cos^2 \vartheta\) (with reference to Fig. 2 for the angular variable). The membranes average values (that are the most relevant quantity) of these distributions are displayed in Figs 4, 5, 6, 7.

In our simulations we assume \(R_p = 10^{-3} m, R_n = 3 \cdot 10^{-4} m, \delta_p = \delta_n = 10^{-8} m\). The electromagnetic and thermal parameters, from [24] and [23], respectively, are reported in Tables I and II. The host extracellular medium is modeled as a saline solution, using Stogryn formulas [25], including fixes from [26]. With reference to Section IIIA (case a), the temperature increase in the plasma cell membrane of a single multilayer cell model is shown in Fig. 4. for two different pulse widths (1ns and 10ns represented with a solid and dashed line, respectively) and a fixed Specific Absorption Dose (1 J/kg). As it can be seen, increasing the pulse duration at constant pulse energy produces a slower temperature rise. The corresponding temperature raise in the cytoplasm (shown in the inset) is in both cases negligible compared to the membranes temperature. The temperature increase in the nuclear cell membrane is displayed in Fig. 5 for two
TABLE I: Electromagnetic parameters of a multilayered living cell [24].

| Conductivity [S/m] | Permittivity [As/V m] |
|-------------------|-----------------------|
| Extracellular medium | 1.24 | 6.4 - 10^{-10} |
| Plasma and Nuclear membrane | 3 - 10^{-7} | 4.4 - 10^{-11} |
| Cytoplasm Nucleoplasm | 0.3 | 6.4 - 10^{-10} |

TABLE II: Thermal parameters of a multilayered living cell [23].

| Heat capacity [J/(kgºK)] | Mass density [kg/m³] | Thermal conductivity [W/(mºK)] |
|---------------------------|----------------------|-----------------------------|
| Extracellular medium | 4 - 10³ | 10³ | 0.577 |
| Plasma and Nuclear membrane | 2 - 10³ | 9-10² | 0.2 |
| Cytoplasm Nucleoplasm | 4-10³ | 10³ | 0.577 |

different pulse durations and in the inset the corresponding temperature increase in the nucleoplasm. As it can be seen, the temperature increase in the nuclear membrane is several orders of magnitude lower than that in the plasma membrane, while the temperature increase in the nucleoplasm and cytoplasm is negligible compared to the membranes temperature. The same analysis performed in Figs. 4 and 5 is reported in Figs. 6 and 7 respectively, but specialized to the case b) discussed in Section III A. It is interesting to note that the temperature increase in both the membranes is well below the threshold where biological damage occurs, even if the nuclear membrane temperature increase is about two orders of magnitude higher than that of the plasma membrane.

So, adopting a dispersive model for both the plasma and nuclear cell plasma and nuclear cell membrane, a localized heating effect is observed only on the plasma membrane while the nuclear membrane remains essentially unaffected. Such results suggest that although pulsed fields of nanosecond-subnanosecond duration interact mostly with the inner organelles, possible heating effects could be observed on the outer cell membrane.

Also in this more complicated but more realistic case, a steep relatively large temperature raise occurs in the membranes, without any significant temperature variation in the cytoplasm.

VI. CONCLUSIONS

We have presented a simple model of interaction between a bio tissue modeled as an assembly of multilayer cells and a pulsed EM field, by solving the coupled EM and thermal problem and including frequency dispersion in the nuclear and plasma membrane capacitances. The
FIG. 6: Increase of the (average) outer membrane temperature of a spherical multilayer-cell model (case b) Section III A) versus time, for an incident (rectangular) pulse with a Specific Absorption Dose of 1 J/kg, applied at t=0. (Full line) Pulsewidth = 1ns. (Dashed line) Pulsewidth = 10ns. This membrane is non dispersive. The cells volume fraction is $f_c = 0.64$. The corresponding temperature increase in the cytoplasm is shown in the inset.

FIG. 7: Increase of the (average) inner membrane temperature of a spherical multilayer-cell model (case b) Section III A) versus time, for an incident (rectangular) pulse with a Specific Absorption Dose of 1 J/kg, applied at t=0. (Full line) Pulsewidth = 1ns. (Dashed line) Pulsewidth = 10ns. Dispersion parameter for nuclear membrane is $C_0 = 10^{-2}$ F/m², $C_\infty = 10^{-9}$ F/m², $\omega_0 = 2\pi 10^8$ Hz, $\Delta\omega = 2\pi 10^7$ Hz. The cells volume fraction is $f_c = 0.64$. The corresponding temperature increase in the nucleoplasm is shown in the inset.

Complex permittivity of the tissue has been obtained using EMT via the classical Rayleigh formula, after computing the effective (complex) permittivity of each individual cell using the Lindell-Sihvola (closed form) EMT formula for stratified spheres. Once the effective permittivity of the tissue is known, we have computed the field in each spherical cell region in the quasi-static approximation, and then used the field solution to deduce the time-dependent temperature distribution in all cell constituents, by solving numerically the related heat diffusion problem. The model considers densely but separated (no geometric/electric contact) cells in the tissue. The short duration (nanosecond) of the pulsed EM field results in a negligible spatial diffusion of the temperature field. In this approximation, cells can be considered thermally independent and the condition (54), ensuring absence of thermal flow, can be consistently used. A more accurate thermal evolution, taking into account also transport phenomena (due to thermoregulation), and the study of the cells geometric disposition effect on the thermal tissue dynamic, are out of the scope of this paper and will be faced in future works. It is interesting to note in this simplified model that by using short, large-amplitude pulses, whose spectral content overlaps significantly the membrane capacitance dispersion band, and whose duration is shorter than the membrane thermal diffusion time, one may observe fast membrane localized heating (the cytoplasm and nucleoplasm temperatures being essentially unaffected). Membrane heating may thus occur in the absence of macroscopic heating of the whole cell (i.e., in a nonthermal exposure regime) and may affect the membrane physiology. The direct measurement of the membrane local temperature raise is, admittedly, a difficult issue. One possibility could be to use a laser beam to probe the mechanical normal modes of the membrane before and after pulsed excitations, to check the expected permanent change in membrane stiffness due to membrane protein denaturation. Whether the above findings may bear any relevance to explain, even in part, any of the observed biophysical effects in living cells exposed to subnanosecond MV/m pulsed fields remains to be investigated and makes the case for strong interdisciplinary cooperation.

VII. APPENDIX: FORMULA DERIVATION

In this appendix we give further details on the derivation of (30)-(37). This is accomplished for equations (33) and (37) starting from (28), similar calculations can be applied to the other cases. The (28) equation is

$$\frac{P_4}{|E_{loc}|^2} = \frac{2\pi}{3} R_p^3 \text{Re}[\tilde{\sigma}] |1 - \Xi|^2,$$

where $\Xi$ is reported in (18) and the definition of the coefficient $\Gamma$ (contained in the expression for $\Xi$) is given in (22). These expressions can be simplified by noting that $R_n \ll R_p$, resulting in the approximation $R_p^3 - R_n^3 \sim R_p^3$. In addition, the (complex) membrane specific admittances defined in (16) and (17) depending on the capacitance, drop to their lower values in presence of strong membrane dispersion. Taking into account these assumptions, after a lengthy but straightforward calculations we find in the cases a) (both membranes are dispersive):

$$\Gamma = 4\sigma_c^2 \sigma_{eff} R_p^3.$$
The same computation gives in the case b) (only the nuclear membrane is dispersive) the result:
\[ \Gamma = 4\sigma_c R_c^4 \gamma_1 (\sigma_c + 2\sigma_{eff}). \]

The simplified expression of \( \Gamma \) substituted in (28), after some simple algebra, gives the equations (33) and (37) of the paper.

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[27] For an homogeneous material whose density, thermal conductivity, heat capacity and thermal diffusion length are denoted as \( \eta, \chi, c^{(p)} \) and \( \tau_D = D^2 \eta c^{(p)}/\chi \) [22].

[28] Doing so, we neglect the possible relevance of spatial temperature gradients in the membrane [23].