Package Reliability Verification of Vanadium Oxide Thin-film Element

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(Received June 30, 2019; accepted January 19, 2020)

Keywords: vanadium oxide, VO₂/AlN/Si, MIT, sensor, resistance, reliability

Vanadium oxide (VO₂) is a typical metal–insulator transition (MIT) material currently receiving considerable attention because of its MIT occurring at the transition temperature \( T_C \) of 67 °C. In this study, VO₂/AlN/Si MIT devices with specific temperature sensor characteristics were designed and packaged for commercial use, and their temperature resistance and humidity dependences were studied to determine whether the characteristics of the elements changed over time. Clear epoxy was used as a packaging material. Reliability tests were conducted by fabricating two oxide device package types: SMD 1608 and a 3Φ lamp package used for light-emitting diodes. In high-temperature (60 °C) storage, low-temperature (−25 °C) storage, and high-temperature (60 °C) operation tests, the resistance change was 10% compared with the initial resistance. However, in the high-temperature/high-humidity test (85 °C/85% RH), the resistance increased by 20%, and the resistance also decreased on the order of 10³. Furthermore, when epoxy was applied to each package after conducting a high-temperature/high-humidity test, the resistance increased by 22%.

1. Introduction

Vanadium oxide (VO₂) is a typical metal–insulator transition (MIT) material.\(^{(1–3)}\) MIT structures contain a very complex and diverse range of oxides including VO, V₂O₃, VO₂, and V₂O₅, whose stability depends on the oxygen content, with the Magneli phase existing between V₂O₃ and VO₂. A typical characteristic of vanadium is its MIT at around a specific temperature (68 °C) because it has a tetragonal rutile structure above its transition temperature. There is also a transition to a V–O–V junction, that is, a metal bond, accompanied by a change in monoclinic crystal structure in the covalent bond below the transition temperature.\(^{(4–7)}\) This change in crystal structure is being actively developed for use in superfast switching devices owing to its switching time of 1–10 fs.

MIT is induced by various external factors such as light, heat, electricity, pressure, and magnetic field, and its usage in sensor is increasing. It is being studied for applications in
devices such as temperature sensors, optical filters, and actuators. However, there is little research on MIT applications in commercial packaging compared with that on MIT applications in device fabrication. The development of MIT-based applications will progress further when various packaging materials are developed to suit the characteristics of oxides and the usage environment of various sensors.

In this study, MIT materials with sensor characteristics for a specific temperature were designed and packaged for commercial use, and their resistance temperature and humidity dependences were studied to determine whether the characteristics of the materials changed over time. The MIT materials comprise a VO$_2$ thin film with a thickness of 200 nm deposited on a silicon substrate with an aluminum nitride (AlN) layer thickness of more than 500 nm. The thin film with the VO$_2$/AlN/Si structure has a $T_C$ of about 80 °C and is manufactured as a material through a semiconductor element manufacturing process.

The designed device has an insulation resistance of about 50 MΩ at room temperature and a temperature resistance of less than 5 kΩ above 80 °C. The SMD1608 package process using epoxy, a clear compound packaging material, was used in reliability tests.

The effects of temperature change on the crystallinity of VO$_2$ and the electrical characteristics of the sensor, i.e., temperature resistance, were evaluated. The temperature resistance of VO$_2$ in the high-temperature, low-temperature, and high-humidity operation tests is reviewed to confirm the feasibility of these MIT materials for commercialization.

2. VO$_2$ Packaging

2.1 VO$_2$/AlN/Si thin film growth

450 μm thick N-type (100) silicon substrates were used for VO$_2$/AlN/Si thin film growth. The substrates were ultrasonically cleaned in isopropyl alcohol, acetone, and ethanol solutions for 15 min to remove organic materials and impurities from the surface of the substrate before washing them in distilled water. The first layer, an AlN thin film was deposited using an RF sputtering system at a base pressure of 1.5 × 10$^{-6}$ Torr. The argon and nitrogen flow rates were adjusted to target Al (Tasco Co.) with 99.9% purity.

AlN thin films were grown to a thickness of 500 nm at a deposition pressure of 7 mTorr, a deposition temperature of 350 °C, and an RF power of 200 W. The second layer, a VO$_2$ film, was grown at a determined ratio (1:7) of argon to oxygen using the 99.9%-purity vanadium (ProTech Co.) target, and the distance between the substrate and the target was maintained at 60 mm.

A crystalline vanadium dioxide thin film was fabricated with a thickness of 200 nm at a growth pressure of 5 mTorr, a deposition temperature of 500 °C, and an RF power of 300 W. Presputtering was performed for about 20 min to generate plasma before deposition, to remove the natural oxide film and contaminants from the target surface, and to stabilize the plasma. Figure 1 shows each layer of the wafer grown by sputtering and analyzed by TEM. Figure 1(a) shows a bright TEM image of the VO$_2$ (~200 nm in thickness) and AlN (~150 nm) layers on the Si substrate. Figure 1(b) shows a high-resolution TEM image of the VO$_2$ and AlN layers with their electron diffraction patterns (EDPs), which indicate epitaxially well grown thin films of
VO\textsubscript{2} and AlN. From the EDPs, AlN has a [100] direction normal to the Si substrate and VO\textsubscript{2} has a [020] direction normal to the AlN layer.

The VO\textsubscript{2} thin film shows good properties with a resistance variation of \( \sim 10^4 \) times in the transition temperature region when it is grown on a sapphire board (C-plane Al\textsubscript{2}O\textsubscript{3}). However, since the price and process cost of sapphire substrates are relatively high, research on VO\textsubscript{2} growth on other substrates is very important from the perspective of commercialization.

2.2 Package element manufacture

The VO\textsubscript{2} thin film was etched using a reactive-ion etching (RIE) system, and a VO\textsubscript{2} channel with a device resistance of 50 MΩ was formed. The chip was designed to be 380 \times 380 \textmu m\textsuperscript{2}, and Ti and Au electrodes of 30 and 300 nm thicknesses were formed, respectively. After cutting a cross section of 150 \mu m thickness, each chip was cut crosswise.

Figure 2 shows an optical microscopy image of the structure fabricated by an elemental manufacturing process. The final package element was completed with two products packaged using two types of commercial LED package: SMD1608 and 3Φ lamp package. Clear epoxy was used as the molding compound.

Figure 3 shows the SMD1608 package with dimensions of 1.6 \times 0.8 mm\textsuperscript{2}. This package is fabricated by the epoxy bonding of the chip to the printed circuit board (PCB) and widely used for displays and panels of small appliances.

Figure 4 shows a product that is packaged using 3Φ lamp specifications. The top of the package is flat, and only the upper part of the chip in the lead frame is molded into epoxy. This type of package is widely used for displays and sensors. The resistance of the final product, which was designed to be 50 MΩ, was measured and the required jigs were manufactured and tested for their reliability.
3. Experimental Methods and Results

3.1 Analysis of basic characteristics

VO₂ has a rutile structure (P42/mnm) at its transition temperature and above \( (T > T_C) \), but below its transition temperature \( (T < T_C) \), it has a monoclinic structure (P21/c). VO₂ shows a sharp decrease in resistance of \( \sim 10^4 \) order at around \( T_C \) as the temperature increases. The reason is that VO₂ changes from being a semiconductor to a metal with changes in crystal structure near temperatures at which resistance varies rapidly. In addition, VO₂ is affected by the microstructure of the thin film, the transition temperature due to lattice strain, the hysteresis width, and the resistivity difference from electrical and optical perspectives.\(^{(8–11)}\) The \( T_C \) of the element with the VO₂/AIN/Si structure was about 80 °C. The reason why the transition temperature of AIN/Si is higher than that of VO₂ by about 13 °C seems to be the increase in phase transition temperature induced by the lattice strain during growth.
Figure 5 shows the result of an XRD $\theta$–2$\theta$ scan of a VO$_2$ thin film grown by RF magnetron sputtering deposition on a Si (100) substrate. It was confirmed that the thin film grew at 500 °C epitaxially in the direction of the monoclinic VO$_2$ (M-VO$_2$) (020). In addition, the half-width of the peak (0.09°) in the direction of VO$_2$ (020) was found to be the same at all deposition temperatures. For the VO$_2$ (020) direction peak, the strain between the VO$_2$ film and the substrate was calculated as

$$\text{strain} = \frac{d_{\text{film}} - d_{\text{bulk}}}{d_{\text{bulk}}} \times 100\%,$$

where $d_{\text{film}}$ is the interplane distance of the film obtained from the Bragg law ($2d \sin \theta = n\lambda$) and $d_{\text{bulk}}$ (2.2585 Å) is the interplane distance of the bulk VO$_2$.\(^{(12,13)}\) It was found that 0.18% of strain was detected and that the entire film was subjected to tensile strain in the out-of-plane direction.

Figure 6 shows the result of an XRD $\omega$-rocking scan for VO$_2$ (020) directional peaks. The half-width is 0.09°, which indicates that the mosaic crystals are good.

### 3.2 Temperature resistance characteristics

To investigate the changes in the resistivity and MIT characteristics of the VO$_2$ thin film, the resistance was measured by raising and lowering the temperature. When the nonresistance, surface resistance, and thin film thickness are $\rho$, $\rho_s$, and $t$, respectively, the nonresistance in the thin film is calculated as\(^{(14)}\)

$$\rho = \rho_s \frac{V}{T} \times C \left( \frac{d}{s} \right) \times t.$$

Fig. 5. (Color online) XRD analysis of vanadium oxide thin films. Fig. 6. (Color online) $\omega$-Rocking curves of vanadium oxide thin films.
When a specimen is rectangular, $a$, $d$, and $s$ are the horizontal length of the specimen, the longitudinal length of the specimen, and the distance between the four terminals and the two terminals, respectively. $C$ is a constant value as a function of geometry. The experimental equipment used in the study (2000 DC and AC current source M3500 nanovoltmeter from Keithley Co.) was operated at 1 mA, and voltage was measured to calculate resistance. In addition, resistance was measured by raising the temperature of the chamber for measuring the element from 1 to 100 °C.

Figure 7 shows the differential curve of nonresistance according to the temperature obtained from the equation $\frac{d(\log \rho)}{dT}$, which is the correlation between temperature and resistance as temperature rises. The $T_C$ of the MIT element is determined from the minimum of this differential curve. Figure 8 shows the differential curve of nonresistance according to temperature, which is the resistivity relationship from the zone of temperature when temperature is lowered. The resistance was 50 MΩ at room temperature and less than 5 kΩ above 80 °C, which shows a resistance change of more than $10^4$ degrees at the transition temperature.

3.3 Reliability experiment

Reliability tests consist of an electrical characteristic test to evaluate the basic performance of a MIT temperature sensor, an environmental test to assess its environmental resistance, and a life test to determine its longevity.

The electrical characteristics were verified by the life and environmental tests. The life test was carried out under the conditions of high-temperature (60 °C) storage and low-temperature (−25 °C) storage. The environmental test was conducted at a high temperature (85 °C) and a high humidity (85% RH). Ten temperature sensor samples per package type were used in the reliability tests conducted for 336 h each in the high-, low-, and constant-temperature/constant-humidity chambers. The high-temperature/high-humidity tests determine whether the packaging material molded is sufficiently moisture-resistant. The polyamide series, a

![Fig. 7. (Color online) Temperature-dependent resistivity of VO$_2$/AIN/Si structure (temperature rise).](image1)

![Fig. 8. (Color online) Temperature-dependent resistivity of VO$_2$/AIN/Si structure (temperature drop).](image2)
clear compound, is vulnerable to humidity compared with conventional epoxy semiconductor molding packaging materials. It has no filler, has a relatively low expansion rate for heat, and is mainly used extensively as a packaging material for optical parts. In addition, to identify the weak points against humidity, reliability tests were carried out using the Si series epoxy material for each package type.

The temperature resistance characteristics of each sample were measured prior to the reliability tests. In general, the characteristics of MIT are such that the electrical resistance rapidly increases from $10^2$ to $10^5$ $\Omega$ from a certain temperature to higher temperatures. $\text{VO}_2$, which has a $T_C$ of 68 $^\circ$C, has a relatively high resistance at room temperature, making it difficult for the current to pass. However, when the temperature is gradually increased to above $T_C$, the resistance suddenly decreases and the current can easily pass.

Figure 9 shows the results of the high-temperature storage test of the temperature sensor. In the high-temperature (60 $^\circ$C) storage test, the initial resistance of the devices packaged with SMD1608 and 3Φ lamp was about 52 M$\Omega$. After 336 h, the resistance of the device packaged with SMD1608 increased to about 54 M$\Omega$, which was an increase of 5%. The initial resistance of the device packaged with the 3Φ lamp product was about 53 M$\Omega$, and the resistance increased by about 6%.

Figure 10 shows the results of the low-temperature (−25 $^\circ$C) storage test. The initial resistance of the devices packaged with SMD1608 and 3Φ lamp was about 51 M$\Omega$. After 336 h, the resistance of the device packaged with SMD1608 increased to about 55 M$\Omega$, which was an increase of 7%. The resistance of the device packaged with the 3Φ lamp increased to around 56 M$\Omega$ with a variation rate of 9%.

The increase in resistance may be due to the shrinkage of the molding compound during the high-temperature storage, resulting in the increase in the resistance of the inner vanadium oxide element.

As shown in Fig. 11, the device packaged with SMD1608 exhibits a 20% increase in resistance to about 65 M$\Omega$ in the high-temperature/high-humidity test (85 $^\circ$C/85% RH). The device packaged with the 3Φ lamp shows a 17% increase in resistance to 62 M$\Omega$. It was confirmed that the extent of increase was significantly greater in the high-temperature/high-
humidity test than in the high-temperature and low-temperature storage tests. This is due to the delamination of the electrodes caused by the high humidity, moisture adsorption, and oxidation of lead wires. The delamination of the polymer electrode seems to have affected its reliability owing to the increase in resistance caused by the repeated adsorption and desorption of water depending on the external stress and environment conditions. Another reason is the effect of the expansion or contraction of the package itself on the thin film, and the moisture that penetrated into the package reacts with the oxygen on the surface of the vanadium oxide thin film, resulting in the chemical conversion of VO$_2$ into VO$_x$. At present, V$_2$O$_5$ has the largest resistance among VO$_x$ compounds, so there is a possibility of using this compound instead of VO$_2$.

Figure 12 shows that the device packaged with SMD1608 had a 22% increase in resistance to 66 MΩ in the high-temperature/high-humidity test (85 ℃/85% RH), which was applied to each package prepared using silicon (Si) series epoxy. The resistance of the device packaged with the 3Φ lamp device increased to about 63 MΩ, which was an increase of about 17%. Although epoxy was applied, it was found that it did not augment the effects of humidity on resistance.

Figure 13 shows the transition order, and the resistance ratios measured at 25 and 100 ℃ for the devices packaged with SMD1608. Usually, the transition order for good-quality VO$_2$
is $\sim 10^4$. In the present study, the initial transition order denoted by a solid square at 0 h in Fig. 13 is $\sim 2 \times 10^4$, which means that the sample has good quality after packaging. After the high-temperature test for 168 h, the transition order is $\sim 1.6 \times 10^4$, which showed a slight decrease. On the other hand, after the high-temperature/high-humidity test, the transition order markedly decreased to $\sim 2 \times 10^3$. This low humidity reliability means that moisture penetrated into the epoxy package and chemically reacted with the oxygen in VO$_2$. However, more studies are required to clarify the precise mechanism underlying the decrease in the transition order of VO$_2$ caused by high humidity. Finally, for VO$_2$ devices to be commercially available, the development of packaging materials the prevent entry of air is required.

4. Conclusion

In this study, a temperature sensor was fabricated using VO$_2$, and the deterministic properties of VO$_2$ and the electrical characteristics of the device were confirmed. Also, the packages SMD1608 and 3Φ lamp were applied, and the reliability test was carried out. The results obtained were as follows. In the high-temperature (60 °C) and low-temperature (−25 °C) storage tests, the resistance increased by 10% compared with initial resistance, but the resistance increased by 20% in the high-temperature/high-humidity test (85 °C/85% RH). This 20% increase was due to the greater effect of humidity and the larger increase in resistance in the high-temperature/high-humidity test than in the high-temperature and low-temperature storage tests. To compensate for this larger increase in resistance, in the high-temperature/high-humidity tests, silicon (Si)-based epoxy was applied, but the increase was 22%, which could not compensate for the increase in resistance caused by high humidity. Thus, it is necessary to study the internal lifting phenomenon and the oxidizing action in different types of package.

Acknowledgments

This study was supported by Wonkwang University in 2019.

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