Intensity-based laser distance measurement system using 2D electromagnetic scanning micromirror

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Abstract
In this research, we present the feasibility testing results of a simple distance measurement system using microfabricated scanning micromirrors. Two different configurations have been tested with different types of micromirrors. In the first configuration, Lissajous scan pattern has been generated with horizontal scan frequency of 715 Hz, and the intensity of the laser beam reflected from the object has been measured with avalanche photodiode to estimate the distance. The position of the beam has been tracked using a separate position sensitive detector. Signals from both sensors are synchronized by eliminating the signal delay, which enables the detection of the distance of a specific point in the 2-dimensional scan pattern. In the simplified configuration, faster scanning micromirror with horizontal scan frequency of 28.8 kHz has been used to increase the resolution and position sensitive detector has been removed from the system by synchronizing the driving current waveform with the avalanche photodiode signals. Distance measurement from 20 to 50 cm has been demonstrated with the developed system.

Introduction
Recently, technologies related to the optical measurement of 3-dimensional (3D) profile or distance is gaining significant research momentum due to growing needs in various fields of application. LIDAR (light detection and ranging) sensor has become a crucial component for data collection and reconstruction of the 3D space surrounding the autonomous vehicle, and facial or gesture recognition sensors are being actively deployed in hand-held smart devices and automotive vehicles. In general, three different approaches are used for optical distance measurement using the laser beam as a light source, which are TOF (time-of-flight) measurement, triangulation, and intensity measurement methods. The TOF measurement utilizes the time difference between outgoing and incoming laser pulses [1]. Although the long-distance measurement capability with high accuracy makes the technique an attractive choice for applications such as LIDAR systems for autonomous vehicles, complex and costly architecture for photon-counting and autocorrelation algorithms are required. Despite the low system complexity and fast response, utilization of triangulation is limited as the measurable distance is proportional to the reflected laser beam displacement [2]. Intensity measurement method requires a very simple system architecture, which makes it a reasonable choice for short range distance measurement and motion tracking. Laser sensing display and gesture recognition system from the University of Tokyo are good examples of the intensity-based distance measurement systems [3–5]. As the 3D measurement of distance inherently requires the scanning of laser beam in 2D (2-dimensional) space, motorized scanners are widely used in conventional systems. Recently, various approaches have been proposed to utilize MEMS (microelectromechanical systems) scanners in these applications, which can potentially provide a significant reduction of overall volume and cost of the system [1, 6].

In this research, we present the feasibility testing results of a simple distance measurement system using electromagnetic 2D MEMS scanner. In the proposed system, the intensity of the reflected laser beam is measured with APD (avalanche photodiode)
to estimate the distance and position of the beam is tracked using PSD (position sensitive detector). As shown in Fig. 1, two different types of electromagnetic 2D MEMS scanners with different scan frequency have been tested, and simplified system without the aid of PSD has also been developed [7].

**Distance measurement using a 2D low-frequency Lissajous scanner**

Block diagram and optical setup used in the experiment are shown in Fig. 2. Input beam from the laser diode (LD) is incident on the MEMS scanner to generate a 2D Lissajous scan pattern at the image plane. Half of the steered...
beam reflected from the scanner is directed towards the PSD sensor which detects the beam displacement to track the beam position on the scan pattern. The beam reflected from the object goes back to the APD via beam splitter where the intensity is measured. A 638 nm laser diode with 120 mW output power has been used as the laser source, and an electromagnetic 2D scanner with a mirror diameter of 1.2 mm and resonance frequency lower than 1 kHz for both scan axes has been used for beam scanning (Fig. 1a). The scanner was originally developed for vector-graphic scanning, but can also be used as a Lissajous scanner by providing sinusoidal input to driving coils for both scan axes [8]. To fully cover the large scan pattern, relatively large optical components have been used including the beam splitter which measured 5×5×5 cm³. A 5.08 cm-diameter bi-convex lens has been placed in front of the APD sensor to transfer the maximum amount of the reflected beam from the object into a single APD sensor (APD130A2, Thorlabs) with 1 mm-diameter. Figure 3a, b show the actual Lissajous pattern captured at the image plane and scan pattern reconstructed with PSD sensor (PDQ80A, Thorlabs) signal. Scan frequency along the x-axis is 715 Hz and that of the y-axis is 520 Hz. Applied current for the x-axis and y-axis scan are 96 mA and 88 mA, respectively. Optical scan angle is approximately 10.5° for both directions. Discrepancies between the pattern reconstructed with PSD signal and actual scan pattern can be ascribed to the optical misalignment and insufficient resolution of the PSD.

To demonstrate the target object scanning and distance measurement, a small circular mirror with a mount has been utilized as the target. To correctly detect the distance of the target object through laser scanning, signals from APD and PSD sensors have to be synchronized. To identify the possible delay between the sensor signals, a low-frequency input pulse has been applied to the LD, and the output signal from the APD and PSD sensors have been measured. As shown in Fig. 4, the APD sensor had almost no delay, while the PSD sensor had a delay of approximately 0.524 ms. Therefore, after acquiring each signal from the sensors, the delay has to be taken into account for synchronization. Figure 5 shows the typical output waveform of the APD sensor. After eliminating the delay between the two signals, the position of the measured point can be obtained by mapping the signals on the same plane as shown in Fig. 6. Distance data for each measurement point can also be acquired in the form of PSD sensor output voltage (intensity of the beam incident on the PSD). In the experimental setup, the distance between the target object (mirror) and the beam splitter is approximately 37 cm. As the intensity of the laser beam entering the PSD sensor varies depending on the position and reflectivity of the target object, distortion of the scan pattern cannot be avoided, which is evident in the scan pattern shown in Fig. 6b. In addition to the removal of the time delay between the two sensor signals, external triggering is required to maintain the scan pattern and thus the position of the measurement points. As the

![](https://example.com/image1)

**Fig. 3** a Lissajous scan pattern (area of the scan region is approximately 8 × 8 cm²), b Lissajous scan pattern reconstructed with PSD sensor signal, c scan pattern generated with 29 kHz scanner (area of the scan region is approximately 7 × 8 cm²)

![](https://example.com/image2)

**Fig. 4** LD input signal and output signals of the PSD and APD
output from the PSD has two separate signals for \( x \) and \( y \) scan axes, the frequency of the external triggering signal is adjusted to the greatest common factor, 65 Hz, of the two scan frequencies. After checking out the feasibility of simultaneously measuring the position and intensity of the laser beam reflected from the high reflectivity mirror object, additional experiments have been conducted to confirm whether it is possible to measure the distance of other low reflectivity materials. Figure 7 shows the measurement result of a paper as the object. Results shown in Figs. 6 and 7 verify that the position and distance measurement of 2D region with various reflectivity is feasible using the proposed method, although the relationship between the measured intensity and distance has to be adjusted depending on the reflectivity of the material.

![Fig. 5 Output waveform of the APD sensor](image)

![Fig. 6 Position and intensity measurement result: a mirror position inside the scan pattern, b reconstructed scan pattern and intensity measurement points, c intensity of the reflected beam vs. \( xy \) position](image)

![Fig. 7 Position and intensity measurement result of a paper located on the right side: a position of the paper, b intensity of the reflected beam vs. \( x \) position, c intensity of the reflected beam vs. \( xy \) position](image)
However, as shown in the previous results, the intensity measurement results are distributed unevenly due to the sparse scan pattern generated with a relatively slow scanner. Although not demonstrated in this work, high definition and high frame rate Lissajous scan can be achieved by appropriate selection of the scan frequency without having to increase the scan frequency dramatically [9].

Distance measurement using a 2D high-frequency scanner

To improve the resolution of the system, electromagnetic 2D scanner with a mirror diameter of 1 mm and horizontal resonance frequency of 28.8 kHz has been tested (Fig. 1b). The device was originally designed for a high-definition pico projection display system, and horizontal and vertical resonance frequencies are 28,775 Hz and 493 Hz, respectively [10, 11]. The operating frequencies are adjusted to generate a scan pattern with the desired area. Used horizontal and vertical scan frequencies are 28,761 Hz and 495 Hz, respectively. Applied current for the x-axis and y-axis scan are 68 mA and 5 mA, respectively. Optical scan angle are approximately 9.2° for the x-axis and 10.5° for the y-axis. Instead of combining the resonance mode actuation for the x-axis and forced mode actuation for the y-axis, resonance mode actuation is used for both axes for simplicity. To maintain a stable scan range, resonance mode actuation requires continuous track and trace of resonance frequency and scan angle, while forced mode actuation requires a PD (proportional-derivative) control to remove the ringing during vertical scan. As the micromirrors used in the experiment are not equipped with integrated deflection angle sensor, we have utilized resonance mode actuation for both axes without feedback control. For the development of more simple and cost-effective device architecture, PSD is removed and driving current waveform and the APD sensor signal are synchronized by 495 Hz rising edge triggering signal. As the output from the function generator passes through a voltage follower circuit to drive the 2D scanner, elimination of the time delay between the function generator and the APD sensor signals is required. The measured time delay is 0.857 ms. To compare the position and distance measurement results, previously experimented mirror object is scanned with

![Fig. 8](image_url) Position and intensity measurement result using 29 kHz scanner (mirror position inside the scan pattern (left), intensity of the reflected beam vs. xy position (middle), top view of the graph in the middle (right)): a mirror located in the center, b mirror located on the left side.
the high-frequency scanner. As shown in Fig. 8, improved results with more data points have been obtained compared to those achievable with low-frequency scanner. To estimate the actual distance of the object, the intensity of the reflected beam from the object is measured at various distances. The distance of the mirror is adjusted from 20 to 50 cm using an optical rail with a 5 cm step. In Fig. 8, measured data points indicate average values of maximum intensity point for five repeated measurements. According to the results shown in Fig. 9, measurable distance ranges from 20 to 50 cm.

Although the proposed intensity-based distance measurement system cannot provide an accurate estimation of the absolute distance, relative differences in intensity or rough estimate of the distance and position of an object in 2D space can be obtained. Therefore, the location and approximate profile of the object can be found. Also, the distance of the object at the center of the scan pattern matches relatively well with the equation derived with distance measurement experiment. When the intensity versus distance equations are established for objects located at various positions and angles, it is possible to detect the distances with more accuracy. Therefore, through more experiments and optimization of the optics, more advanced intensity-based distance sensor using a 2D MEMS scanner can be developed for motion tracking and gesture recognition.

**Conclusion**

Feasibility testing result of an intensity-based distance measurement system using 2D MEMS scanning micro-mirror has been constructed. An APD sensor has been utilized in measuring the intensity of the reflected beam, and a PSD sensor has been utilized for detecting the reflected beam position and scan pattern. By synchronizing the APD and PSD outputs, the position and distance of the object in the 2D space can be detected. Also, the PSD sensor can be removed from the optical setup by synchronizing the input waveform applied to the scanner and the APD sensor signal. Although dependence on object surface roughness and reflectivity could not be removed, detection of approximate distance and the position of the target object with simple architecture using a single APD sensor has been demonstrated. For the object with known reflectivity and position, the distance can be determined with more accuracy. Although further experimentation would be required to improve the accuracy of measurement, the feasibility of utilizing 2D MEMS scanner in an intensity-based distance measurement application has been verified successfully.

**Authors’ contributions**

KK carried out the experiments, and KK, JH, and C-HJ analyzed the experimental results, and drafted the manuscript. All the authors discussed the proposed architecture and experimental results. All the authors read and approved the final manuscript.

**Competing interests**

The authors declare that they have no competing interests.

**Funding**

This work was supported by Basic Science Research Program through the National Research Foundation of Korea (NRF) funded by the Ministry of Science, ICT & Future Planning (2017R1A2B4007830), Basic Science Research Program through the National Research Foundation of Korea (NRF) funded by the Ministry of Education (NRF-2014R1A1A2057721), and by the Center for Integrated Smart Sensors as GFP (C1SS-2013M3A6A6054204).

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Springer Nature remains neutral with regard to jurisdictional claims in published maps and institutional affiliations.

**Received:** 6 September 2018   **Accepted:** 26 November 2018   **Published online:** 30 November 2018

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