Data Article

Conversion of flaxseed oil into biodiesel using KOH catalyst: Optimization and characterization dataset

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A B S T R A C T

The dataset presented here are part of the data planned to produce biodiesel from flaxseed. Biodiesel production from flaxseed oil through transesterification process using KOH as catalyst, and the operating parameters were optimized with the help of face-centered central composite design (FCCD) of response surface methodology (RSM). The operating independent variables selected such as, methanol oil ratio (4:1 to 6:1), catalyst (KOH) weight (0.40–1.0%), temperature (35 °C–65 °C), and reaction time (30 min–60 min) were optimized against biodiesel yield as response. The maximum yield (98.6%) of biodiesel from flaxseed can achieved at optimum methanol oil ratio (5.9:1), catalyst (KOH) weight (0.51%), reaction temperature (59.2 °C), and reaction time (33 min). The statistical significance
of the data set was tested through the analysis of variance (ANOVA). These data were the part of the results reported in "Optimization of process variables for biodiesel production by transesterification of flaxseed oil and produced biodiesel characterizations" Renewable Energy [1].

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### Abbreviations

| Abbreviation | Full Form |
|--------------|-----------|
| FCCD         | Face-centered central composite design |
| RSM          | Response surface methodology |
| ANOVA        | Analysis of variance |
| Std. Dev.    | Standard deviation |
| Std Err      | Standard error |
| DF           | Degree of freedom |
| Obs          | Observed |
| VIF          | Variance inflation factor |
| POE          | Propagation of error |
| FI           | Interactive factor |
| C.V          | Coefficient of variance |

### Specifications Table

| Subject                        | Energy |
|-------------------------------|--------|
| Specific subject area         | Renewable energy, sustainability and the Environment |
| Type of data                  | Table |
|                               | Graph |
|                               | Figure |
| How data were acquired        | Titration method was used for biodiesel yield estimation and the yield data were set in face centered cubic design of response surface methodology approach using Design-Expert 6.0.6 (Stat-Ease, Inc. Minneapolis, USA) |
| Data format                   | Raw (.dx6 file) |
|                               | Analyzed data |
| Parameters for data collection| Volume ratio of methanol/oil, catalyst (KOH) weight percent, reaction temperature, and reaction time. |
| Description of data collection| The biodiesel was prepared under different operating conditions, and the data were collected through titration methods for estimating the biodiesel yield. |
| Data source location          | Biodiesel synthesized in chemistry laboratory, college of Natural and Computational science, Madda Walabu University, Bale-Robe, Ethiopia |
|                               | City/Town/Region: Bale-Robe |
|                               | Country: Ethiopia |
| Data accessibility            | All data is along with this article. |
| Related research article      | T. Ahmad, M. Danish, P. Kale, B. Geremew, S.B. Adeljoju, M. Nizami, M. Ayoub, Optimization of process variables for biodiesel production by transesterification of flaxseed oil and produced biodiesel characterizations. Renewable Energy, 139 (2019) 1272–1280. DOI.org/10.1016/j.renene.2019.03.036 |
1. Data

The exponential growth of world population and its consequence on energy demand consumes the limited source of conventional non-renewable fossil fuel at much faster rate than expected. The rise of energy demand and fast depletion in fossil fuel triggered the research for finding the alternate source of energy. Biodiesel is one of the solutions to fulfill the energy demand as well as safety of the environment, because it is free from Sulphur, biodegradable, non-toxic, and renewable [2–4]. The fatty acid content of the flaxseed oil is reported elsewhere [5]. The data reported here is for the optimum production of the biodiesel from flaxseed oil.

Table 1 shows the data obtained from the face-centered composite design (FCCD) approach of response surface methodology for the independent factors (methanol to oil ratio, catalyst (KOH) weight, temperature, and reaction time) and dependent factor (actual percentage yield of biodiesel) based on design of experiments. The levels

| Std | Run | Factor 1 | Factor 2 | Factor 3 | Factor 4 | Response 1 |
|-----|-----|----------|----------|----------|----------|------------|
|     |     | A:(Methanol to oil) | B:(Catalyst wt.% to oil) | C:(Temperature) °C | D:(Reaction time) min | Yield % |
| 21  | 1   | 5 (0)   | 0.7 (0)  | 35 (−1) | 45 (0)  | 93.30      |
| 8   | 2   | 6 (1)   | 1.0 (1)  | 65 (1)  | 30 (−1) | 95.88      |
| 23  | 3   | 5 (0)   | 0.7 (0)  | 50 (0)  | 30 (−1) | 96.62      |
| 20  | 4   | 5 (0)   | 1.0 (1)  | 50 (0)  | 45 (0)  | 94.90      |
| 2   | 5   | 6 (1)   | 0.4 (−1) | 35 (−1) | 30 (−1) | 96.40      |
| 15  | 6   | 4 (−1)  | 1.0 (1)  | 65 (1)  | 60 (1)  | 92.26      |
| 10  | 7   | 6 (1)   | 0.4 (−1) | 35 (−1) | 60 (1)  | 96.84      |
| 28  | 8   | 5 (0)   | 0.7 (0)  | 50 (0)  | 45 (0)  | 94.22      |
| 11  | 9   | 4 (−1)  | 1.0 (1)  | 35 (−1) | 60 (1)  | 91.04      |
| 9   | 10  | 4 (−1)  | 0.4 (−1) | 35 (−1) | 60 (1)  | 84.14      |
| 17  | 11  | 4 (−1)  | 0.7 (0)  | 50 (0)  | 45 (0)  | 95.09      |
| 14  | 12  | 6 (1)   | 0.4 (−1) | 65 (1)  | 60 (1)  | 98.10      |
| 4   | 13  | 6 (1)   | 1.0 (1)  | 35 (−1) | 30 (−1) | 96.86      |
| 12  | 14  | 6 (1)   | 1.0 (1)  | 35 (−1) | 60 (1)  | 98.72      |
| 29  | 15  | 5 (0)   | 0.7 (0)  | 50 (0)  | 45 (0)  | 96.66      |
| 16  | 16  | 6 (1)   | 1.0 (1)  | 65 (1)  | 60 (1)  | 95.50      |
| 19  | 17  | 5 (0)   | 0.4 (−1) | 50 (0)  | 45 (0)  | 94.58      |
| 18  | 18  | 6 (1)   | 0.7 (0)  | 50 (0)  | 45 (0)  | 99.54      |
| 24  | 19  | 5 (0)   | 0.7 (0)  | 50 (0)  | 60 (1)  | 95.68      |
| 3   | 20  | 4 (−1)  | 1.0 (1)  | 35 (−1) | 30 (−1) | 94.86      |
| 6   | 21  | 6 (1)   | 0.4 (−1) | 65 (1)  | 30 (−1) | 98.41      |
| 1   | 22  | 4 (−1)  | 0.4 (−1) | 35 (−1) | 30 (−1) | 85.88      |
| 27  | 23  | 5 (0)   | 0.7 (0)  | 50 (0)  | 45 (0)  | 96.86      |
| 5   | 24  | 4 (−1)  | 0.4 (−1) | 65 (1)  | 30 (−1) | 96.48      |
| 22  | 25  | 5 (0)   | 0.7 (0)  | 65 (1)  | 45 (0)  | 94.52      |
| 13  | 26  | 4 (−1)  | 0.4 (−1) | 65 (1)  | 60 (1)  | 92.26      |
| 25  | 27  | 5 (0)   | 0.7 (0)  | 50 (0)  | 45 (0)  | 96.14      |
| 7   | 28  | 4 (−1)  | 1.0 (1)  | 65 (1)  | 30 (−1) | 89.32      |
| 26  | 29  | 5 (0)   | 0.7 (0)  | 50 (0)  | 45 (0)  | 96.18      |
and ranges of independent factors and their effect on standard deviation with measures derived from the $(X'X)^{-1}$ matrix are elaborated in Tables 2 and 3. The parameters for prediction design and the correlation matrix of regression coefficients with correlation matrix of factors are described in Table 4. The 3D interactive effects of the process variables for the percent yield of the flaxseed biodiesel is shown in Fig. 1 while deviation of input values of different parameter from reference point depicted in Fig. 2. The sequential model sum of squares and lack of fit tests and model summary statistics are discussed in Tables 5 and 6. Analysis of variance (ANOVA) table for response surface reduced quadratic model was reported elsewhere [1]. The adjustment of R-squared value parameters and coefficient estimation for final model equation along with diagnostics case statistics are illustrated in Tables 7--9. Fig. 3 shows contour plot for maximum biodiesel yield within the selected independent variables (methanol to oil ratio, catalyst (KOH) weight, temperature, and reaction time) ranges. In addition, cubic graph for the maximum percent yield of the flaxseed biodiesel against independent

| Table 2 |
| Levels and ranges of independent factors used during biodiesel production from flaxseed oil. |
| Response | Name | Units | Obs | Minimum | Maximum | Trans | Model |
|----------|------|-------|-----|---------|---------|-------|-------|
| Y1       | Yield (%) | % | 29 | 84.14 | 99.14 | None | R Quadratic |
| Factor   | Name | Units | Type | Low Actual | High Actual | Low Coded | High Coded |
| A        | Methanol/oil ratio | Numeric | 4 | 6 | –1 | 1 |
| B        | Catalyst Weight % | % | 0.4 | 1 | –1 | 1 |
| C        | Temperature C | Numeric | 35 | 65 | –1 | 1 |
| D        | Reaction Time min. | Min | 30 | 60 | –1 | 1 |

| Table 3 |
| Power at 5% alpha level for effect of following Standard Deviation. |
| Term | Std Err | VIF | Ri-Squared | ½ Std. Dev. | 1 Std. Dev. | 2 Std. Dev. |
|------|--------|-----|------------|-------------|-------------|-------------|
| A    | 0.24   | 1   | 0.0        | 16.7%       | 50.6%       | 97.6%       |
| B    | 0.24   | 1   | 0.0        | 16.7%       | 50.6%       | 97.6%       |
| C    | 0.24   | 1   | 0.0        | 16.7%       | 50.6%       | 97.6%       |
| D    | 0.24   | 1   | 0.0        | 16.7%       | 50.6%       | 97.6%       |
| A²   | 0.62   | 2.64| 0.6213     | 11.7%       | 32.2%       | 84.8%       |
| B²   | 0.62   | 2.64| 0.6213     | 11.7%       | 32.2%       | 84.8%       |
| C²   | 0.62   | 2.64| 0.6213     | 11.7%       | 32.2%       | 84.8%       |
| D²   | 0.62   | 2.64| 0.6213     | 11.7%       | 32.2%       | 84.8%       |
| AB   | 0.25   | 1   | 0          | 15.4%       | 46.1%       | 96.0%       |
| AC   | 0.25   | 1   | 0          | 15.4%       | 46.1%       | 96.0%       |
| AD   | 0.25   | 1   | 0          | 15.4%       | 46.1%       | 96.0%       |
| BC   | 0.25   | 1   | 0          | 15.4%       | 46.1%       | 96.0%       |
| BD   | 0.25   | 1   | 0          | 15.4%       | 46.1%       | 96.0%       |
| CD   | 0.25   | 1   | 0          | 15.4%       | 46.1%       | 96.0%       |

Basis std dev. = 1.

| Table 4 |
| Parameters for prediction design. |
| Parameters | Value |
|-------------|-------|
| Maximum Prediction Variance (at a design) | 0.659 |
| Average Prediction Variance | 0.517 |
| Condition Number of Coefficient Matrix | 10.655 |
| G Efficiency (calculated from the design points) (%) | 78.500 |
| Scaled D-optimality Criterion | 2.510 |
| Determinant $(X'X)^{-1}$ | 1.148x10$^{-16}$ |
| Trace of $(X'X)^{-1}$ | 2.251 |

Analysis of variance (ANOVA) table for response surface reduced quadratic model was reported elsewhere [1]. The adjustment of R-squared value parameters and coefficient estimation for final model equation along with diagnostics case statistics are illustrated in Tables 7--9. Fig. 3 shows contour plot for maximum biodiesel yield within the selected independent variables (methanol to oil ratio, catalyst (KOH) weight, temperature, and reaction time) ranges. In addition, cubic graph for the maximum percent yield of the flaxseed biodiesel against independent
Fig. 1. Interactive effects 3D of the process variables for the percent yield of the flaxseed biodiesel.
Fig. 2. Deviation of input values of different parameter from Reference point.
## Table 5
Sequential Model Sum of Squares and Lack of Fit test.

| Source     | Sum of squares | DF | Mean Square | F Value | Prob>F |
|------------|----------------|----|-------------|---------|--------|
| Mean       | 2.604x10^5     | 1  | 2.604x10^5  |         |        |
| Linear     | 178.93         | 4  | 44.73       | 6.39    | 0.0012 |
| 2FI        | 88.30          | 6  | 14.72       | 3.33    | 0.022  |
| Quadratic  | 41.5           | 4  | 10.37       | 3.81    | 0.0268 |
| Suggested  | Cubic          | 26.45 | 8  | 3.31       | 1.70    | 0.2670 |
| Aliased    | Residual       | 11.67 | 6  | 1.94       |         |        |
| Total      | 2.604x10^5     | 29 | 8991.48     |         |        |

## Table 6
Model summary statistics.

| Source     | Std. Dev. | R-Squared | Adjusted R-Squared | Predicted R-Squared | Press |
|------------|-----------|-----------|--------------------|---------------------|-------|
| Linear     | 2.65      | 0.5159    | 0.4352             | 0.1946              | 279.36|
| 2FI        | 2.10      | 0.7704    | 0.6429             | -0.0112             | 350.74|
| Quadratic  | 1.65      | 0.8901    | 0.7802             | 0.1915              | 280.43|
| Suggested  | Cubic     | 1.39      | 0.9664             | -4.1879             | 1799.46|
| Aliased    | Pure Error | 4.39      | 4                  | 1.10                |       |

## Table 7
Adjustment of R-Squared value parameters.

| Source     | Std. Dev. | R-Squared | Adj R-Squared | Pre R-Squared | Adeq Precision |
|------------|-----------|-----------|---------------|---------------|---------------|
| Mean       | 1.59      | 0.8901    | 0.7948        | 0.2014        | 14.274        |
| C.V.       | 1.68      |           |               |               |               |
| Press      | 277       |           |               |               |               |

## Table 8
Coefficient estimation for final model equation.

| Factor | Coefficient Estimate | DF | Standard Error | 95% CI Low | 95% CI High | VIF |
|--------|----------------------|----|----------------|------------|-------------|-----|
| Intercept | 96.10            | 1  | 0.52           | 95         | 97.19       |     |
| A      | 3.01                | 1  | 0.38           | 2.21       | 3.81        | 1   |
| B      | 0.35                | 1  | 0.38           | -0.45      | 1.15        |     |
| C      | 0.82                | 1  | 0.38           | 0.015      | 1.62        | 1   |
| D      | -0.34               | 1  | 0.38           | -1.14      | 0.46        |     |
| A^2    | 1.55                | 1  | 0.95           | -0.47      | 3.57        | 2.41|
| B^2    | -1.43               | 1  | 0.95           | -3.45      | 0.59        | 2.41|
| C^2    | -2.26               | 1  | 0.95           | -4.28      | -0.24       | 2.41|
| AB     | -0.72               | 1  | 0.40           | -1.57      | 0.13        | 1   |
| AC     | -0.96               | 1  | 0.40           | -1.81      | -0.11       | 1   |
| AD     | 0.53                | 1  | 0.40           | -0.32      | 1.38        |     |
| BC     | -1.91               | 1  | 0.40           | -2.76      | -1.06       |     |
| BD     | 0.40                | 1  | 0.40           | -0.45      | 1.25        | 1   |
| CD     | 0.081               | 1  | 0.40           | -0.77      | 0.93        | 1   |
variables and residual variation plots for normal and predicted value along with run and reaction time are shown in Fig. 4 and Fig. 5, respectively. The Residual variation plots with different process variables and variation in run number for the diagnostics case statistics are elaborated in Figs. 6 and 7. The criteria for desirability for constraints is shown in Fig. 8. The point prediction and optimization of independent variables for maximum biodiesel yield from the flaxseed oil are tabulated in Tables 10 and 11 respectively.

2. Experimental design, materials, and methods

2.1. Materials

The flaxseed oil was collected from the local market of Bale-Robe, Ethiopia. Methanol (CH\textsubscript{3}OH, 99.8% purity), sulfuric acid (H\textsubscript{2}SO\textsubscript{4}, 98%), and KOH were bought from Sigma Aldrich and were of analytical grade. During experiment 0.1 N sulfuric acid solution was used. All chemicals consumed during the biodiesel synthesis were of analytical grade.

2.2. Methods

Biodiesel from flaxseed oil was produced in a batch experiment. The biodiesel produced in the laboratory from flaxseed oil involved a two-step transesterification reaction accompanied with product separation, washing, and drying. The process flow chart for the biodiesel production from flaxseed oil shown in Fig. 9. A fixed quantity (50 g) of the oil was measured and poured into a conical flask. The

| Standard Order | Actual Value | Predicted Value | Residual | Leverage | Student Residual | Cook’s Distance | Outlier t | Run Order |
|---------------|--------------|-----------------|----------|----------|-----------------|----------------|-----------|-----------|
| 1             | 85.88        | 87.54           | -1.66    | 0.65     | -1.78           | 0.437          | -1.942    | 22        |
| 2             | 96.40        | 95.85           | 0.55     | 0.65     | 0.585           | 0.047          | 0.572     | 5         |
| 3             | 94.86        | 92.69           | 2.17     | 0.65     | 2.330           | 0.746          | 2.819     | 20        |
| 4             | 96.86        | 98.12           | -1.26    | 0.65     | -1.352          | 0.251          | -1.393    | 13        |
| 5             | 96.48        | 94.74           | 1.74     | 0.65     | 1.861           | 0.476          | 2.050     | 24        |
| 6             | 98.41        | 99.22           | -0.81    | 0.65     | -0.872          | 0.104          | -0.865    | 21        |
| 7             | 89.32        | 92.26           | -2.94    | 0.65     | -3.153          | 1.366          | -5.247    | 28        |
| 8             | 95.88        | 93.86           | 2.02     | 0.65     | 2.165           | 0.644          | 2.522     | 2         |
| 9             | 84.14        | 84.84           | -0.70    | 0.65     | -0.747          | 0.077          | -0.736    | 10        |
| 10            | 96.84        | 95.26           | 1.58     | 0.65     | 1.694           | 0.394          | 1.820     | 7         |
| 11            | 91.04        | 91.59           | -0.55    | 0.65     | -0.587          | 0.047          | -0.574    | 9         |
| 12            | 98.72        | 99.13           | -0.41    | 0.65     | -0.444          | 0.027          | -0.431    | 14        |
| 13            | 92.26        | 92.36           | -0.10    | 0.65     | -0.108          | 0.002          | -0.104    | 26        |
| 14            | 98.10        | 98.95           | -0.85    | 0.65     | -0.913          | 0.114          | -0.908    | 12        |
| 15            | 92.26        | 91.48           | 0.78     | 0.65     | 0.833           | 0.095          | 0.824     | 6         |
| 16            | 95.50        | 95.20           | 0.30     | 0.65     | 0.325           | 0.014          | 0.315     | 16        |
| 17            | 95.90        | 94.64           | 1.26     | 0.43     | 1.058           | 0.062          | 1.063     | 11        |
| 18            | 99.54        | 100.65          | -1.11    | 0.43     | -0.928          | 0.048          | -0.923    | 18        |
| 19            | 94.58        | 94.31           | 0.27     | 0.43     | 0.222           | 0.003          | 0.215     | 17        |
| 20            | 94.90        | 95.01           | -0.11    | 0.43     | -0.091          | 0.000          | -0.088    | 4         |
| 21            | 93.30        | 93.02           | 0.28     | 0.43     | 0.238           | 0.003          | 0.230     | 1         |
| 22            | 94.52        | 94.65           | -0.13    | 0.43     | -0.107          | 0.001          | -0.104    | 25        |
| 23            | 96.62        | 96.44           | 0.18     | 0.16     | 0.125           | 0.000          | 0.120     | 3         |
| 24            | 95.68        | 95.75           | -0.07    | 0.16     | -0.050          | 0.000          | -0.048    | 19        |
| 25            | 96.14        | 96.10           | 0.04     | 0.10     | 0.029           | 0.000          | 0.028     | 27        |
| 26            | 96.18        | 96.10           | 0.08     | 0.10     | 0.056           | 0.000          | 0.054     | 29        |
| 27            | 96.86        | 96.10           | 0.76     | 0.10     | 0.506           | 0.002          | 0.494     | 23        |
| 28            | 94.22        | 96.10           | -1.88    | 0.10     | -1.244          | 0.013          | -1.269    | 8         |
| 29            | 96.66        | 96.10           | 0.56     | 0.10     | 0.374           | 0.001          | 0.363     | 15        |

Cases(s) with IOutlierTI>3.50.
Fig. 3. Standard Error of Design at different parameters for the percent yield of the flaxseed biodiesel.
Fig. 4. Cube graph for the maximum percent yield of the flaxseed biodiesel at different parameters.
Fig. 5. Residual variation Plots for normal and predicted value along with run and reaction time.
Flaxseed oil was pre-heated at 110 °C for 30 min to remove the moisture content in oil. The process involves the catalyst KOH in different weight percentage of oil (0.40, 0.70, and 1.0%), methanol at various molar ratios of methanol/oil (4:1, 5:1, and 6:1) under different temperature (35, 50, and 65 °C) and reaction time (30, 45, and 60 min). The water washing method was used for further purification of FAME (biodiesel). The mixture was stirred gently to avoid foam formation. The mixture was left overnight to settle into two phases: a water-impurity phase and a biodiesel phase. Separating funnel was used to separate the FAME (biodiesel) from the water-impurity phase. This process was repeated three times to ensure the removal of most impurities from the biodiesel fraction. The washed biodiesel fraction was then reheated at 100 °C for 1 h to evaporate the residual water. The titration of biodiesel fraction with sulfuric acid (0.1 N) was used for the quantification of the FAME [6]. The percentage yield of flaxseed biodiesel was determined by comparing biodiesel weight with flaxseed oil weight used initially.

2.3. Design of experiment

The face-centered central composite design (FCCD) was applied to optimize the biodiesel yield. This design is most suitable approach to optimize such processed which have a quantitative independent variable, and its response can also be observed quantitatively experimental matrix. The FCCD have sufficient tool to find the optimum values of independent variables within the selected range. Two levels and four factors with five center point values were considered for this experiment, the total number of experiments suggested through this method was \(2^4 + 2 \times 4 + 5\) 29 batch experiments. The independent variables selected for optimization were methanol/oil molar ratio (A), catalyst weight percent (B), reaction temperature (D) and reaction time (E). The response chosen was the biodiesel yields produced through KOH catalyzed transesterification reaction of flaxseed oil. The actual values of

Fig. 6. The Residual variation Plots with different process parameters.
Fig. 7. Variation in run number for Diagnostics Case Statistics.

Fig. 8. Criteria for desirability for Constraints.
The independent variables are listed in Table 1. The biodiesel synthesis was conducted in batch, and each set of experimental conditions were selected randomly to minimize systematic error. All statistical parameters including analysis of variance (ANOVA) and figures were plotted with the help of Design-Expert 6.0.6 (Stat-Ease, Inc., Minneapolis, USA) [7].

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Conflict of Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Appendix A. Supplementary data

Supplementary data to this article can be found online at https://doi.org/10.1016/j.dib.2020.105225.

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