EFFECTIVE PROPERTIES OF PERIODIC TUBULAR STRUCTURES

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Abstract
A method is described to calculate effective tensor properties of a periodic array of two-phase dielectric tubes embedded in a host matrix. The method uses Weierstrass’ quasiperiodic functions for representation of the potential that considerably facilitates the problem and allows us to find an exact expression for the effective tensor. For weakly interacting tubes we obtain Maxwell-like approximation of the effective parameter which is in very good agreement with experimental results in considered examples.

1 Introduction
The problem of evaluating the effective properties (permittivity, conductivity, etc.) of periodic heterogeneous materials has been extensively investigated. Its solution for noninteracting particles was suggested by Maxwell [17], which has become ubiquitous in physics and engineering as well as an indispensable benchmark asymptotics. Despite apparent limitations, it provides a good approximation in a certain range of parameters for the estimation of optical properties of square lattice of carbon nanotubes [8],[26] as well as optical properties of artificially engineered microstructured materials [16].

The seminal paper of Rayleigh [25] predestined the development in this area for many decades to come. It contained the ideas of the multipole expansion method, relation of the potential with the elliptic functions, its application to elasticity and wave propagation. Rayleigh’s method was extended to a regular arrays of cylinders [24],[18],[23] as well as to the dynamic problems [28].

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Application of Rayleigh’s approach to arbitrary lattices, however, encounters two obstacles. The distribution of stream lines is not known for the medium whose effective properties are described by a tensor. As a result, the method used in [25] for evaluation of a scalar is not applicable for determination of the effective tensor. Next, the method entails conditionally convergent sum whose summation order is obscure. That hampers further development of the method.

The advantages of application of the elliptic and meromorphic functions to the problems of determination of the effective properties of perforated plates and shells had been clearly demonstrated in [13]. Elliptic functions were successfully employed for a rectangular lattice of circular inclusions [11] as well as in the problem of periodic fibrous composites in applications to biological tissues [6]. A method of functional equations [22], [27] employing analytic functions was used to find an expression of the permittivity tensor for small volume fraction of inclusions.

Another method was introduced in [2, 3, 4, 5] and is based on the study of the analytic properties of the effective parameters. This approach was extended in [19, 20, 21] and proved to be efficient for obtaining bounds on complex effective parameters. Its mathematical justification is given in [11, 12].

In this paper we represent the potential in terms of Weierstrass’ $\zeta$-functions and their derivatives (an analog of periodically distributed multipoles). This ensures periodicity of the electric field in the whole plane and avoids the problem of summation of conditionally convergent series. Then we determine the average electric field and electric displacement within the parallelogram of the periods. It allows us to find an explicit formula for the tensor of effective properties.

## 2 Representation of solution and compliance with the boundary conditions

We consider an infinite periodic array of parallel tubes with the periods $2\tau_1$ and $2\tau_2$ (see Figure 1) embedded in a homogeneous medium with dielectric constant $\varepsilon_{\text{ex}}$. Dielectric constant of the tubes of inner radii $b$ and outer radii $a$ is denoted by $\varepsilon_{\text{tu}}$. We also suppose that the tubes are filled with a material with dielectric constant $\varepsilon_{\text{in}}$. A homogeneous electric field $E$ is applied in the direction perpendicular to the axes of the tubes. In the plane of complex variable $z = x + iy$ we introduce the electric potential $u(z)$ which satisfies the equation

\[
\nabla \cdot [\varepsilon \nabla u] = 0, \quad \varepsilon = \begin{cases} 
\varepsilon_{\text{in}}, & 0 \leq r < b, \\
\varepsilon_{\text{tu}}, & b < r < a, \\
\varepsilon_{\text{ex}}, & r > a.
\end{cases}
\]
On the boundaries \( r = a \) and \( r = b \) of the tubes we impose continuity conditions
\[
[u] = 0, \quad (2)
\]
\[
\varepsilon \left[ \frac{\partial u}{\partial n} \right] = 0, \quad (3)
\]
where brackets \([\cdot]\) denote the jump of the enclosed quantity across the interface. In addition, we require the field \( \nabla u \) to be periodic
\[
\nabla u(z + 2\tau_i) = \nabla u(z), \quad i = 1, 2, \quad (4)
\]
and normalized in such a way that when the radius of the tubes approaches zero the field tends to the homogeneous one of intensity \( E = E_x - iE_y \)
\[
uex(z) \to -Ez \quad \text{as} \quad a \to 0. \quad (5)
\]

\begin{figure}[h]
\centering
\includegraphics[width=\textwidth]{figure1.png}
\caption{(a) A fragment of an infinite periodic array of tubes with the periods \( 2\tau_1 \) and \( 2\tau_2 \) and a fundamental period parallelogram \( ABCD \). (b) Material and geometric parameters of the tubes.}
\end{figure}

Following [10], we represent complex potential \( u(z) \) in the form
\[
uin(z) = Ea \sum_{n=0}^{\infty} \left[ A_n \left( \frac{z}{b} \right)^{2n+1} + B_n \left( \frac{\bar{z}}{b} \right)^{2n+1} \right], \quad (6)
\]
\[
uin(z) = Ea \sum_{n=0}^{\infty} \left[ C_n \left( \frac{z}{b} \right)^{2n+1} + D_n \left( \frac{\bar{z}}{b} \right)^{2n+1} + E_n \left( \frac{a}{z} \right)^{2n+1} + F_n \left( \frac{a}{\bar{z}} \right)^{2n+1} \right], \quad (7)
\]
\[
uex(z) = -Ez + Ea \sum_{n=0}^{\infty} \frac{a^{2n+1}}{(2n)!} \left[ G_n \zeta^{(2n)}(z) + H_n \zeta^{(2n)}(\bar{z}) \right], \quad (8)
\]
where \( A_n, \ldots, H_n \) are unknown complex dimensionless coefficients, \( \bar{z} \) stands for the complex conjugation, and \( \zeta^{(2n)}(z) \) is \( 2n \)-th derivative of the Weierstrass \( \zeta \)-function [15]
\[
\zeta(z) = \frac{1}{z} + \sum_{m,n} \left[ \frac{1}{z - P_{m,n}} + \frac{1}{P_{m,n}} + \frac{z}{P_{m,n}^2} \right]. \quad (9)
\]
Here $P_{m,n} = 2m\tau_1 + 2n\tau_2$. Prime in the sum means that summation is extended over all pairs $m, n$ except $m = n = 0$. Since the electric field $E$ is periodic, the potential $u(z)$ should be represented as the sum of periodic and linear functions. The Weierstrass $\zeta$-function has just that property \cite{7}

\[
\zeta(z + 2\tau_k) = \zeta(z) + 2\eta_k, \quad \eta_k = \zeta(\tau_k), \quad k = 1, 2,
\]

where constants $\eta_1$ and $\eta_2$ are related by the Legendre identity

\[
\eta_1\tau_2 - \eta_2\tau_1 = \frac{\pi i}{2}, \quad (11)
\]

Its derivatives however are periodic functions, so that condition (4) is fulfilled. Also, from (9) it follows that

\[
\oint_{ABCD} \zeta^{(n)}(z) \, dz = 0, \quad n \geq 1. \quad (12)
\]

To satisfy conditions (2)-(3) on the boundary $r = a$ we expand $\zeta(z)$ and its even derivatives in a Laurent series

\[
\zeta^{(2n)}(z) = \frac{(2n)!}{z^{2n+1}} - \sum_{k=0}^{\infty} s_{n+k+1} \frac{(2n + 2k + 1)!}{(2k + 1)!} \frac{1}{z^{2k+1}}, \quad n \geq 0, \quad s_1 = 0, \quad (13)
\]

where

\[
s_k = \sum_{n,m} P_{m,n}^{2k}, \quad k = 2, 3, \ldots \quad (14)
\]

Due to the symmetry of the lattice the only nonzero sums (14) are those with even powers of $P_{m,n}$.

Compliance with the boundary conditions (2)-(3) leads to an infinite system of linear equations

\[
H_n - \gamma_n \sum_{k=0}^{\infty} s_{n+k+1} \frac{(2n + 2k + 1)!}{(2k)! (2n + 1)!} G_k a^{2n+2k+2} = \gamma_n \delta_{n,0}, \quad (15)
\]

\[
G_n - \gamma_n \sum_{k=0}^{\infty} s_{n+k+1} \frac{(2n + 2k + 1)!}{(2k)! (2n + 1)!} H_k a^{2n+2k+2} = 0, \quad (16)
\]

where

\[
\gamma_n = \frac{\alpha - \tilde{\alpha} \nu^{4n+2}}{1 - \alpha \tilde{\alpha} \nu^{4n+2}}, \quad (17)
\]

\[
\alpha = \frac{\varepsilon_{tu} - \varepsilon_{ex}}{\varepsilon_{tu} + \varepsilon_{ex}}, \quad (18)
\]

\[
\tilde{\alpha} = \frac{\varepsilon_{tu} - \varepsilon_{in}}{\varepsilon_{tu} + \varepsilon_{in}}, \quad (19)
\]

\[
\nu = \frac{b}{a}, \quad 0 \leq \nu < 1, \quad (20)
\]
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and $\delta_{n,0}$ is the Kronecker delta. The other coefficients are expressed through $H_n$ and $G_n$ as follows:

$$
A_n = \frac{(\alpha - 1)(1 + \tilde{\alpha})\nu^{2n+1}}{\alpha - \tilde{\alpha}\nu^4n+2} H_n, \quad B_n = \frac{(\alpha - 1)(1 + \tilde{\alpha})\nu^{2n+1}}{\alpha - \tilde{\alpha}\nu^4n+2} G_n,
$$

(21)

$$
C_n = \frac{(\alpha - 1)\nu^{2n+1}}{\alpha - \tilde{\alpha}\nu^4n+2} H_n, \quad D_n = \frac{(\alpha - 1)\nu^{2n+1}}{\alpha - \tilde{\alpha}\nu^4n+2} G_n,
$$

(22)

$$
F_n = \frac{\tilde{\alpha}(\alpha - 1)\nu^{4n+2}}{\alpha - \tilde{\alpha}\nu^4n+2} H_n, \quad E_n = \frac{\tilde{\alpha}(\alpha - 1)\nu^{4n+2}}{\alpha - \tilde{\alpha}\nu^4n+2} G_n.
$$

(23)

We introduce new variables

$$
x_n = H_n + G_n, \quad y_n = H_n - G_n.
$$

(24)

Then equations (15)-(16) become independent

$$
x_n - \gamma_n \sum_{k=0}^{\infty} s_{n+k+1}s_{n+k+1} \frac{(2n + 2k + 1)!}{(2k)!(2n + 1)!} x_k a^{2n+2k+2} = \gamma_0 \delta_{n,0},
$$

(26)

$$
y_n + \gamma_n \sum_{k=0}^{\infty} s_{n+k+1}s_{n+k+1} \frac{(2n + 2k + 1)!}{(2k)!(2n + 1)!} y_k a^{2n+2k+2} = \gamma_0 \delta_{n,0}.
$$

(27)

We will analyze (26)-(27) by the approach described in [10]. First, we introduce parameter $h$

$$
h = \frac{a}{\ell}, \quad h \leq \frac{1}{2},
$$

(28)

where $\ell$ is the least distance between the centers of the tubes

$$
\ell = \min(2|\tau_1|, 2|\tau_2|, 2|\tau_1 - \tau_2|).
$$

(29)

Then we denote by $S_k$ the dimensionless lattice sums

$$
S_k = \sum_{n,m}^{'} \left( \frac{\ell}{P_{m,n}} \right)^{2k}, \quad k = 2, 3, \ldots, S_1 = 0,
$$

(30)

and represent both equations (26)-(27) as

$$
\mathbf{u} - \mathcal{G}(h)\mathbf{u} = \mathbf{v},
$$

(31)

where $\mathbf{u} = (u_0, u_1, \ldots) \in \ell_\infty(\mathbb{C})$, $\mathbf{v} = \gamma_0 \delta_{n,0}$, and operator $\mathcal{G}(h)$ is defined by

$$
(\mathcal{G}(h) \mathbf{u})_n = \gamma_n \sum_{k=0}^{\infty} G_{n,k} u_k h^{2n+2k+2},
$$

(32)

where

$$
G_{n,k} = \pm \frac{(2n + 2k + 1)!}{(2k)!(2n + 1)!} S_{n+k+1}, \quad G_{0,0} = 0.
$$

(33)

Properties of equation (31) describes the following
Theorem 1. Equation (31) has the following properties:

(a) For each \(0 \leq h \leq \frac{1}{2}\), \(G(h)\) is a bounded operator in \(l_\infty(C)\).

(b) If \(0 \leq h < \frac{1}{2}\), then operator \(G(h)\) is compact.

(c) The norm of \(G(h)\) is estimated by

\[
\|G(h)\|_\infty \leq |\gamma_0| \left( \left( \frac{h}{1 - h} \right)^2 + \left( \frac{h}{1 + h} \right)^2 \right) \sup_n |S_n|.
\]  

(34)

(d) If \(\|G(h)\|_\infty < 1\) then (31) has a unique solution \(u_0 \in c_0(C)\). Truncated solution of (31) converges exponentially to \(u_0\) and can be represented as a convergent power series in \(h\).

Proof of the theorem is almost identical to that given in [9].

We will seek for the series solution of (31) in the form

\[
u_n = \gamma_0 \delta_{n,0} + \sum_{m=0}^\infty p_{n,m} h^{2n+2m+2}.
\]  

(35)

Substitution of (35) into (31) gives a recurrence relation for the coefficients \(p_{n,m}\):

\[
p_n = \gamma_0 G_n,\]

(36)

\[
p_n = \sum_{m=0}^{\left[\frac{k-1}{2}\right]} G_{n,m} p_{m,k-2m-1},
\]  

(37)

where \([\nu]\) denotes the integral part of \(\nu\).

In the next section it will be shown that the effective properties are determined by only \(x_0\) and \(y_0\) in (26)-(27) which we denote as

\[
x_0 = \gamma_0 \lambda, \quad y_0 = \gamma_0 \mu.
\]  

(38)

From (36)-(37) one can find the series expansion for \(\mu\) and \(\lambda\). The first few terms of their expansion are given by

\[
\lambda = 1 + 3 \gamma_0 \gamma_1 S_2^2 h^8 + 5 \gamma_0 \gamma_2 S_3^2 h^{12} + 30 \gamma_0 \gamma_1^2 S_2^2 S_3 h^{14}
+ (9 \gamma_0^2 \gamma_1^2 S_2^4 + 7 \gamma_0 \gamma_3 S_2^2 S_3 h^{16} + 210 \gamma_0 \gamma_1 \gamma_2 S_2 S_3 S_4 h^{18}
+ (15 \gamma_1 S_2^2 (\gamma_0 \gamma_2 S_3^2 + 20 \gamma_0 \gamma_2^2 S_2^2) + 15 \gamma_0 \gamma_1 \gamma_2 S_2 S_3^2 + 9 \gamma_0 \gamma_4 S_2^2) h^{20} + O(h^{22})
\]  

(39)

\[
\mu = 1 + 3 \gamma_0 \gamma_1 S_2^2 h^8 + 5 \gamma_0 \gamma_2 S_3^2 h^{12} - 30 \gamma_0 \gamma_1^2 S_2^2 S_3 h^{14}
+ (9 \gamma_0^2 \gamma_1^2 S_2^4 + 7 \gamma_0 \gamma_3 S_2^2 S_3) h^{16} - 210 \gamma_0 \gamma_1 \gamma_2 S_2 S_3 S_4 h^{18}
+ (15 \gamma_1 S_2^2 (\gamma_0 \gamma_2 S_3^2 + 20 \gamma_0 \gamma_2^2 S_2^2) + 15 \gamma_0 \gamma_1 \gamma_2 S_2 S_3^2 + 9 \gamma_0 \gamma_4 S_2^2) h^{20} + O(h^{22})
\]  

(40)
3 Determination of the effective permittivity tensor

Effective permittivity tensor \( \epsilon^* \) relates the average electric displacement \( \langle D \rangle \) and the average electric field \( \langle E \rangle \)

\[
\langle D \rangle = \epsilon^* \langle E \rangle.
\]

Observe that

\[
\langle E \rangle = \frac{1}{S} \int_S E \, dS = \frac{1}{S} \int_{S_{in}} E_{in} \, dS + \frac{1}{S} \int_{S_{tu}} E_{tu} \, dS + \frac{1}{S} \int_{S_{ex}} E_{ex} \, dS,
\]

while

\[
\langle D \rangle = \frac{1}{S} \int_S D \, dS = \frac{\epsilon_{in}}{S} \int_{S_{in}} E_{in} \, dS + \frac{\epsilon_{tu}}{S} \int_{S_{tu}} E_{tu} \, dS + \frac{\epsilon_{ex}}{S} \int_{S_{ex}} E_{ex} \, dS,
\]

where \( S \) is the total area of the parallelogram \( ABCD \), \( S_{in} \) is the disk of radius \( b \), \( S_{tu} \) is the annular domain with \( b \leq r \leq a \), and \( S_{ex} \) is the part of the parallelogram outside the disk \( r \leq a \). Thus, in (21)-(25) we need to evaluate three distinct integrals.

Using the mean-value property of harmonic functions in the first integral and relations (21), (24)-(25) we get

\[
\int_{S_{in}} E_{in} \, dS = E_{in}(0,0) S_{in} = -E ab (A_0 + B_0, i(A_0 - B_0))
\]

\[
= -\pi b^2 E \frac{(\alpha - 1)(1 + \bar{\alpha})}{\alpha - \bar{\alpha} \nu^2} \left[ \begin{array}{c} x_0 \\ iy_0 \end{array} \right].
\]

Evaluation of the second integral gives

\[
\int_{S_{tu}} E_{tu} \, dS = \int_{S_{tu}} \left( \frac{\partial u_{tu}}{\partial x}, \frac{\partial u_{tu}}{\partial y} \right) \, dS = -E \int_{b}^{a} \int_{0}^{2\pi} \sum_{n=0}^{\infty} (2n + 1) \left( C_n \frac{1}{\nu} \left( \frac{r}{b} \right)^{2n} e^{i2n\phi} + D_n \frac{1}{\nu} \left( \frac{r}{b} \right)^{2n} e^{-i2n\phi} - E_n \left( \frac{a}{r} \right)^{2n+2} e^{-i(2n+2)\phi} - F_n \left( \frac{a}{r} \right)^{2n+2} e^{i(2n+2)\phi} \right) r \, dr \, d\phi
\]

\[
= -\pi a^2 E \left( \frac{1}{\nu} - \nu \right) (C_0 + D_0, i(C_0 - D_0)) = -\pi a^2 E \frac{(\alpha - 1)(1 - \nu^2)}{\alpha - \bar{\alpha} \nu^2} \left[ \begin{array}{c} x_0 \\ iy_0 \end{array} \right].
\]

To evaluate the last integral we change the variables form \( x, y \) to \( z, \bar{z} \) and apply Green’s theorem in complex form

\[
\int_{S_{ex}} E_{ex} \, dS = \int_{S_{ex}} \left( \frac{\partial u_{ex}}{\partial x}, \frac{\partial u_{ex}}{\partial y} \right) \, dS = -(1,i) \int_{S_{ex}} \frac{\partial u_{ex}}{\partial z} \, dS - (1,-i) \int_{S_{ex}} \frac{\partial u_{ex}}{\partial \bar{z}} \, dS
\]

\[
= \frac{(1,i)}{2i} \left( \oint_{\Pi} u_{ex} \, d\bar{z} - \oint_{C} u_{ex} \, d\bar{z} \right) - \frac{(1,-i)}{2i} \left( \oint_{\Pi} u_{ex} \, dz - \oint_{C} u_{ex} \, dz \right),
\]
where $\Pi$ is the perimeter of the parallelogram $ABCD$, while $C$ is the circle of radius $a$. Observe that $u_{ex} = u_{tu}$ when $r = a$, and the integrals over the circle can be evaluated directly

$$
\oint_C u_{ex} \, dz = \oint_C u_{tn} \, dz = 2\pi i a^2 E \left( \frac{1}{\nu} D_0 + E_0 \right).
$$

The use of quasiperiodicity of $\zeta$-function (10) greatly facilitates evaluation of the integrals over the parallelogram $ABCD$ (see Figure 1(b)). We have

$$
\oint_\Pi \zeta^{(2n)}(z) \, dz = \int_B^A \, dz + \int_C^D \, dz = \int_C^D \left[ \zeta^{(2n)}(z + 2\tau_2) - \zeta^{(2n)}(z) \right] \, dz
$$

$$
- \int_D^C \zeta^{(2n)}(z) \, dz + \int_D^A \zeta^{(2n)}(z) \, dz = \int_D^C \left[ \zeta^{(2n)}(z + 2\tau_1) - \zeta^{(2n)}(z) \right] \, dz
$$

$$
- \int_D^A \zeta^{(2n)}(z + 2\tau_1) \, dz + \int_D^C \zeta^{(2n)}(z) \, dz = \left(2\eta_1 \int_D^C \, dz - 2\eta_2 \int_D^A \, dz \right) \delta_{n,0}
$$

$$
= (2\eta_1 \tau_1 - 2\eta_2 \tau_2) \delta_{n,0}.
$$

In the same manner we evaluate similar integrals appearing in (6)

$$
\oint_\Pi \zeta^{(2n)}(z) \, d\bar{z} = (2\eta_1 \tau_2 - 2\eta_2 \tau_1) \delta_{n,0},
$$

$$
\oint_\Pi \zeta^{(2n)}(\bar{z}) \, d\bar{z} = (2\eta_1 \tau_2 - 2\eta_2 \tau_1) \delta_{n,0},
$$

$$
\oint_\Pi \zeta^{(2n)}(\bar{z}) \, dz = (2\eta_1 \tau_2 - 2\eta_2 \tau_1) \delta_{n,0}.
$$

Here we supposed for simplicity that all lattice sums (30) are real that is true for rectangular and rhombic lattices.

Combining the three integrals in (2) and using the Legendre identity (11) we obtain

$$
\langle E \rangle = \left( I - \frac{2a^2\gamma_0}{S} \Psi M \right) E,
$$

where $I$ is the identity matrix,

$$
\Psi = \begin{bmatrix}
\text{Re} \eta_1 \text{Im} 2\tau_2 & -\text{Im} \eta_1 \text{Im} 2\tau_2 \\
-\text{Im} \eta_1 \text{Im} 2\tau_2 & \pi - \text{Re} \eta_1 \text{Im} 2\tau_2
\end{bmatrix},
$$

and

$$
M = \begin{bmatrix}
\lambda & 0 \\
0 & \mu
\end{bmatrix}, \quad \begin{bmatrix}
1 \\
i
\end{bmatrix}.
$$

Here we made use that $\text{Im} \tau_1 = 0$. 

Similar calculations for $\langle D \rangle$ in (3) give

$$
\langle D \rangle = \varepsilon_{ex} \left( I + \frac{2\pi a^2 \gamma_0}{S} M - \frac{2a^2 \gamma_0}{S} \Psi M \right) E.
$$

Comparing (12) and (15) with (1) we find the effective dielectric tensor

$$
\varepsilon^* = \varepsilon_{ex} \left[ I + \pi \eta M (I - \eta \Psi M)^{-1} \right],
$$

where $\eta = \frac{2a^2 \gamma_0}{S}$. Note that if $\gamma_0 = 0$, that is when

$$
\frac{b^2}{a^2} = \frac{(\varepsilon_{tu} - \varepsilon_{ex})(\varepsilon_{tu} + \varepsilon_{in})}{(\varepsilon_{tu} + \varepsilon_{ex})(\varepsilon_{tu} - \varepsilon_{in})}
$$

the two-dimensional effective medium becomes isotropic with $\varepsilon^* = \varepsilon_{ex} I$ for any geometry of the lattice and any concentration of the tubes.

### 4 Maxwell’s approximation

If $a \ll \ell$ and the interaction between the tubes is weak one can approximate solution of (26)-(27) by the their right hand side

$$
x_n = y_n = \gamma_0 \delta_{n,0}. \quad (1)
$$

As a result,

$$
G_n = 0, \quad H_n = \gamma_0 \delta_{n,0}, \quad (2)
$$

and from (23)-(21) one can find expression of the potential

$$
u_{in}(z) = \frac{(a - 1)(1 + \alpha)}{1 - \alpha \tilde{\alpha} \nu^2} Ez, \quad (3)
$$

$$
u_{tu}(z) = \frac{a - 1}{1 - \alpha \tilde{\alpha} \nu^2} \left( 1 + \frac{\tilde{\alpha} b^2}{|z|^2} \right) Ez, \quad (4)
$$

$$
u_{ex}(z) = -Ez \left( 1 - \frac{\alpha - \tilde{\alpha} \nu^2 a^2}{1 - \alpha \tilde{\alpha} \nu^2 |z|^2} \right). \quad (5)
$$

The average electric field $\langle E \rangle$ in the medium and that in the core $\langle E_{in} \rangle$ and the tubes $\langle E_{tu} \rangle$ are related by

$$
\langle E \rangle = \nu^2 f \langle E_{in} \rangle + (1 - \nu^2) f \langle E_{tu} \rangle + (1 - f) \langle E_{ex} \rangle, \quad (6)
$$

where $f$ is the volume fraction of solid rods of radius $a$.

Similar relation is valid for the average electric displacement $\langle D \rangle$

$$
\langle D \rangle = \varepsilon_{in} \nu^2 f \langle E_{in} \rangle + \varepsilon_{tu} (1 - \nu^2) f \langle E_{tu} \rangle + \varepsilon_{ex} (1 - f) \langle E_{ex} \rangle. \quad (7)
$$
From (3)–(4) we find
\[
\langle E_{in} \rangle = -\frac{(\alpha - 1)(1 + \tilde{\alpha})}{1 - \alpha \tilde{\alpha} \nu^2} E,
\]
\[
\langle E_{tu} \rangle = -\frac{\alpha - 1}{1 - \alpha \tilde{\alpha} \nu^2} E.
\] (8) (9)

As for \( \langle E_{ex} \rangle \) we assume that \( \langle E_{ex} \rangle = E \). Then from (6) and (7) we obtain
\[
\langle E \rangle = (1 - \gamma_0 f) E,
\]
\[
\langle D \rangle = \varepsilon_{ex} (1 + \gamma_0 f) E.
\] (10) (11)

Comparing the two expressions we arrive at the effective dielectric constant
\[
\varepsilon^* = \varepsilon_{ex} \frac{1 + \gamma_0 f}{1 - \gamma_0 f},
\] (12)

where
\[
\gamma_0 = \frac{\alpha - \tilde{\alpha} \nu^2}{1 - \alpha \tilde{\alpha} \nu^2}.
\] (13)

Similar to the lattice case (16), \( \gamma_0 = 0 \) implies \( \varepsilon^* = \varepsilon_{ex} \). As \( \nu \to 0 \) (solid rods) the formula becomes regular Maxwell’s approximation for the two-dimensional case.

5 Regular lattices

For regular lattices (square or hexagonal) one can show [13] that \( \text{Im} \eta_1 = 0 \) and \( \text{Re} \eta_1 \text{Im} 2 \tau_2 = \frac{\pi}{2} \), so that \( \Psi = \frac{\pi}{2} I \) in (13). As a result, \( \lambda = \mu \) in (38), and \( \varepsilon^* \) becomes an isotropic tensor \( \varepsilon^* = \varepsilon^* I \) with
\[
\varepsilon^* = \varepsilon_{ex} \frac{1 + \gamma_0 \lambda f}{1 - \gamma_0 \lambda f},
\] (14)

where \( f \) is the volume fraction of solid cylinders of radius \( a \), while \( \lambda \) can be calculated either numerically form (26) and (38) or by the series expansion (39). In the latter case for the square array we obtain the following expansion
\[
\lambda = 1 + 3 \gamma_0 \gamma_1 S_2^2 \nu^8 + (9 \gamma_0^2 \gamma_1^2 S_2^4 + 7 \gamma_0 \gamma_3 S_4^2) \nu^{16} + O(\nu^{24}),
\] (15)

where
\[
S_2 = \sum' \frac{1}{(m + in)^4} \approx 3.15121, \quad S_4 = \sum' \frac{1}{(m + in)^8} \approx 4.25577.
\] (16)
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\[ 2\tau_2 = i\ell \]

\[ 2\tau_1 = \ell \]

**Figure 2:** Cross-sections of elementary cells of the square (a) and hexagonal (b) lattices. In both cases \( h = \frac{a}{\ell} \).

Similar expansion for a hexagonal array gives

\[
\lambda = 1 + 5\gamma_0\gamma_2S_3^2h^{12} + \gamma_0 \left( 25\gamma_0\gamma_2^2S_3^4 + 11\gamma_5S_6^2 \right) h^{24} + O(h^{36}). \quad (17)
\]

Here \( S_3 = \sum_{n,m}^{'} \frac{1}{(m + ne^{i\pi/3})^6} \approx 5.86303 \), \( S_6 = \sum_{n,m}^{'} \frac{1}{(m + ne^{i\pi/3})^{12}} \approx 6.00964 \).

Comparison of expansions shows that (17) decays in \( h \) faster than (15). Therefore, Maxwell’s approximation is more accurate for the hexagonal lattice. It has also been shown in [14] that (14), when used for the long wave approximation of the effective parameter of a hexagonal lattice of solid cylinders, is in a very good agreement with numerical calculations.

**Figure 3:** Dependence of the real (a) and imaginary (b) parts of the complex effective dielectric constant \( \varepsilon^* \) of a square array of tubes on the parameter \( h = a/\ell \). The solid blue line corresponds to exact numerical evaluation, red circles show result of formulas (14)–(15), and black dots represent Maxwell’s approximation (12) for \( \varepsilon_{in} = 2 - 4i \), \( \varepsilon_{tu} = 80 - 2i \), \( \varepsilon_{ex} = 5 - 4i \), and \( \nu = 0.9 \).
Figures 3-4 show dependence of the real and imaginary parts of the complex effective dielectric constant $\varepsilon^*$ of a square and hexagonal arrays of tubes on the parameter $h = a/\ell$. Formula (14) gives an excellent agreement between numerical evaluation of $\varepsilon^*$ using solution of (26) and the expansions (15), (17) for chosen material parameters. In the case of square lattice estimate (34) gives $\|G(0.5)\|_\infty \leq 1.4644$ while in fact $\|G(0.5)\|_\infty \approx 0.88035$. For the hexagonal lattice estimation through (34) yields $\|G(0.5)\|_\infty \leq 6.6122$ while direct evaluation results in $\|G(0.5)\|_\infty \approx 1.1632$. Maxwell’s formula (12) gives a good approximation as long as the norm of the operator $G(h)$ is significantly less than unity.

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