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Effect of Montmorillonite Nanogel Composite Fillers on the Protection Performance of Epoxy Coatings on Steel Pipelines

Ayman M. Atta 1,2,*, Ashraf M. El-Saeed 2, Hamad A. Al-Lohedan 1 and Mohamed Wahby 3

1 Chemistry Department, College of Science, King Saud University, Riyadh 11451, Saudi Arabia; hlohedan@ksu.edu.sa
2 Petroleum Application Department, Egyptian Petroleum Research Institute, Nasr City, Cairo 11727, Egypt; ashrefelsaied@yahoo.com
3 Arki for advanced construction chemicals Co. Ltd., Riyadh 11451, Saudi Arabia; m.wahby@arkichem.com
* Correspondence: aatta@ksu.edu.sa; Tel.: +966-056-155-7975

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Abstract: Montmorillonite (MMT) clay mineral is widely used as filler for several organic coatings. Its activity is increased by exfoliation via chemical modification to produce nanomaterials. In the present work, the modification of MMT to form nanogel composites is proposed to increase the dispersion of MMT into epoxy matrices used to fill cracks and holes produced by the curing exotherms of epoxy resins. The dispersion of MMT in epoxy improved both the mechanical and anti-corrosion performance of epoxy coatings in aggressive marine environments. In this respect, the MMT surfaces were chemically modified with different types of 2-acrylamido-2-methyl propane sulfonic acid (AMPS) nanogels using a surfactant-free dispersion polymerization technique. The effect of the chemical structure, nanogel content and the interaction with MMT surfaces on the surface morphology, surface charges and dispersion in the epoxy matrix were investigated for use as nano-filler for epoxy coatings. The modified MMT nanogel epoxy composites showed excellent resistance to mechanical damage and salt spray resistance up to 1000 h. The interaction of MMT nanogel composites with the epoxy matrix and good response of AMPS nanogel to sea water improve their ability to act as self-healing materials for epoxy coatings for steel.

Keywords: wetting; wettability; surface and interface science; polymer composites; nanostructure; nanomaterials

1. Introduction

Montmorillonite (MMT) is one of the most important nanoclay minerals that have been widely used in several medical and industrial applications [1–3]. The exfoliation of MMT silicate layers increases their applications due to improvement of their surface activity, surface area aspect ratio and strength, as well as reduction of the material cost due to formation of MMT on nano- or micro-scales [4]. Different techniques are used to exfoliate the MMT layers such as organic modification or reactive extrusion [5,6]. The organic modifications were carried out either by cationic exchange of Na+, K+, Li+, Ca2+ cations between silicate layers or by formation of nanogels between silicate layers. The chemical modifications completed either with organic cations modifications such as cationic trialkyl ammonium bromide surfactants [7] or by formation of MMT polymer composites [8]. MMT polymer nanocomposites were obtained by using two techniques, either polymer modifications based on hyper-branched and modified nonionic polymer composites [9–11] or by polymerization of ionic monomers among MMT galleries [12]. MMT polymer composites have several drawbacks such as MMT aggregation, wide particle size distribution, swelling and hydration...
of MMT composites. The present study aims to solve these problems and to apply MMT nanopolymer composites as fillers for epoxy coatings to improve their mechanical and anticorrosion performance to protect the steel pipelines from aggressive marine environments.

Epoxy organic coatings were used to protect the pipeline steel from environmental corrosion due to their thermal resistivity, good adhesion with steel and low volatility. The major drawbacks of epoxy resins as organic coatings refer to their high moisture absorption, formation of micro-cracking and holes during their curing, their stiffness and high brittleness [13]. MMT clay has been used for the construction of gas barrier and flame retardant protective coatings [14,15]. Moreover, some of nanomaterials based on silica, titania, clay minerals, metal oxide nanoparticles were proposed to modify the epoxy drawbacks [16–18]. The exfoliated silicate layers of sodium MMT (Na-MMT) have been widely used due to their high shape-anisotropy and surface that proposed to fill the cracks and to inhibit the penetration of corrosive humidity, water and salts through epoxy coatings [19–21]. Furthermore, the Na-MMT nanocomposites improved the flame retardant and mechanical properties of epoxy resins at low contents of 2–5% by weight as compared with high contents (40 wt %) of conventional fillers [22]. In our previous works [23–25], the Na-MMT was exfoliated by crosslinking copolymerization of smart monomer based on N-isopropylacrylamide (NIPAm), ionic monomers such as (3-acylamidopropyl)trimethylammonium chloride (APTAC) and 2-acrylamido-2-methylpropane sulfonic acid (AMPS). The exfoliation of Na-MMT with nanogel composites produced amphiphilic nanocomposite materials have a great tendency to reduce the water surface tension to remove toxic organic and inorganic water pollutants [25]. The present work aims to prepare different types of Na-MMT nanogel composites for use as filler for epoxy coatings. The exfoliation of Na-MMT into epoxy coatings and its effect on mechanical and anticorrosion characteristics of epoxy coatings are another goal of the present work.

2. Results and Discussion

It was previously reported that Na-MMT consists of compressed stacked aluminosilicate galleries [26]. These galleries are composed on two silica tetrahedral layers connected to one either octahedral layer of alumina aluminosilicate or magnesia to form magnesium silicate. Every sheet has a small negative surface charges produced from an isomorphous substitution of ions in the framework. The intercalation or exfoliation of these sheets increased the surface charges and surface activity on the silicate sheets by exchange the interlayer cations Na+, K+ and Ca2+ [27]. In the present work, the exfoliation and intercalation of silicate layers can be carried out by using 2-acrylamido-2-methylpropane sulfonic acid (AMPS) copolymers to form nanogel layers between Na-MMT silicate layers. These monomers were proposed to increase the negative surface charges on MMT layers to facilitate the exfoliation of MMT into epoxy coatings to improve their mechanical and anticorrosion performances. The ionic monomers such as acrylic acid (AA) and (3-acylamidopropyl)trimethylammonium chloride (APTAC) were used to prepare anionic copolymers with AMPS. Nonionic co-monomer based on acrylamide (AAm) was used to investigate the effect of copolymer types on the intercalation or exfoliation of MMT into epoxy matrix. Moreover, the nonionic monomers (AAm and VP) are used to form nanogels between hydrophilic Na-MMT and organic modified MMT with octadecylamine sheets (HMMT) to study the effect of MMT types on anticorrosion and mechanical performance of epoxy coatings. In our previous works [23–25], PVP and ethanol/water (60/40 vol %) were used as dispersing agent and co-solvents to intercalate the silicate layer of MMT. Scheme 1 illustrates the mechanism for exfoliation of Na-MMT layers using nanogels. It is suggested that the strong interaction between the amide groups of monomers and oxygen of MMT silicate layer via hydrogen bond formation assists the adsorption of AAm, APTAC, AA, and AMPS monomers on Na-MMT sheets [28]. It is also expected that the electrostatic interaction between positively charged APTAC monomer and negatively charged Na-MMT sheets increases the adsorption of APTAC on Na-MMT sheets. The strong interaction of amido group of AMPS with Na-MMT silicates inhibits the repulsive force between sulfate negative charges and Na-MMT negative
charges to acts as a surface-active material \[29\]. The strong interaction of monomers with Na-MMT widens the distance between its sheets to form nanogels that assist to exfoliate the Na-MMT sheets as illustrated in the Scheme 1.

![Scheme 1. Preparation of MMT nanogel composites.](image)

2.1. Characterization of Na-MMT Nanogels

It is necessary to elucidate the chemical structure of the produced Na-MMT nanogels by using FTIR spectra as represented in Figure 1a–e. These confirm the crosslinking polymerization but it is difficult to determine exfoliation of Na-MMT by FTIR analysis. The spectrum of Na-MMT (Figure 1a) confirms the presence of silicate without any organic materials as elucidated from appearance of bands at 520, 470 and 1045 cm\(^{-1}\) (Si-O, stretching of silicate layers), 625 cm\(^{-1}\) (Al-O stretching of aluminate) and 3440, 3640 cm\(^{-1}\) (O-H stretching of the silicate and bound water). New bands appeared in MMT nanogels (Figure 1b–e) at 2945 and 2870 cm\(^{-1}\) (C-H stretching vibration of polymerized monomers) without appearance of vinyl or acrylate =CH stretching bands (3100–3000 cm\(^{-1}\)) confirms the polymerization of monomers.

![Figure 1. FTIR spectra of (a) Na-MMT (b) MMT-AMPS/APTAC (c) Na-MMT-AMPS/AA, (d) Na-MMT-AMPS/AAm and (e) Na-MMT-AAm/VP.](image)

Moreover, the new bands at 1685 (CONH stretching) and 1545 cm\(^{-1}\) (NH stretching) elucidate the amide groups of MBA crosslinker and polymers of AMPS/APTAC, AMPS/AA, AMPS/AAm and AAm/VP nanogels. These data confirm the formation of crosslinked nanogel on the surface or intercalate space of Na-MMT galleries.
The nanogels and MMT contents were determined from TGA-DTA data obtained from representative samples, summarized in Figure 2. The thermal degradation steps up to 650 °C of MMT nanogels are gathered in Table 1. The data (Table 1 and Figure 2a–d) confirm that the bound water between silicate layers (5.5 wt %) was reduced to 1.8 wt % by forming nanogel composites. This was caused by capping of silicate layers with nanogels with strong hydrogen bonds between the amide groups of nanogels and the oxygen groups of silicate. This bond reduces the presence of water among the silicate O− groups of MMT galleries [30]. The nanogel contents of MMT composites can be determined from degradation steps at temperature from 200–550 °C. These data also confirmed by the appearance of exothermic peaks at 324 °C and 475 °C in DTA analysis (Figure 2a–d). The remained residue above 650 °C used to determine the Na-MMT in nanogel composites. The MMT contents can be arranged in the order AMPS/APTAC > AMPS/AA > AMPS/AAm > AAm/VP. These data confirm the presence of polyampholyte (contains positive and negative charges) increase the encapsulation of MMT into nanogel networks more than polyionic nanogel composites. This observation can be referred to the presence of electrostatic repulsion forces between polyionic charges decrease the intercalation of nanogel among MMT galleries.

![Figure 2](image_url)

**Figure 2.** TGA and DTA thermograms of (a) Na-MMT; (b) MMT-AMPS/AAm; (c) MMT-AMPS/APTAC and (d) MMT-AMPS/AA nanogel composites.

| Weight Loss (%) | Na-MMT | Na-MMT Nanogels |
|----------------|--------|-----------------|
|                |        | AMPS/APTAC | AMPS/AA | AMPS/AAm | AAm/VP |
| 25–200         | 5.5    | 2.8          | 3.2     | 1.8      | 2.5    |
| 200–550        | -      | 48.2         | 52.1    | 57.3     | 59.0   |
| 550–750        | 3.5    | 4.0          | 5.0     | 4.0      | 5.3    |
| residue        | 91     | 45           | 39.7    | 36.9     | 33.2   |

The interaction between MMT layers and nanogel networks via surface morphology of nanomaterials can be determined from HR-TEM as illustrated in Figure 3a–d. It is observed that the AMPS/AA nanogel has great tendency to form exfoliated MMT galleries as observed from Figure 3a. The uncharged nanogels based on AAm/VP can intercalate with the MMT galleries without exfoliation (Figure 3b). The AMPS/AAm and AMPS/APTAC nanogels can form partially exfoliated MMT layers as observed from Figure 3c,d, respectively. The reason for exfoliation of MMT layers with charged polyionic or polyampholytic nanogel networks can be attributed to the repulsion between high charge on MMT surfaces or due to the formation of elastic networks between MMT sheets [31]. Accordingly, the AMPS can produce elastic surface charged networks when copolymerized and crosslinked with...
AA more than AAm or APTAC. It was previously reported that, the electrostatic interaction between the charged groups affected the elastic free energy and can reduce the elastic modulus of networks to form elastic gel [32]. This result can be confirmed by measuring the surface charges or zeta potential of MMT nanogel composites.

Wide-angle X-ray diffraction (WXRD) is an effective tool used to determine the intercalation or exfoliation of MMT galleries as represented in Figure 4a–c. The diffraction patterns were determined at lower 2-theta angles from 1 to 10°. In this respect, the diffractograms of MMT modified with AMPS/AA and AMPS/AAm were selected to represent the partial and complete exfoliation of MMT galleries. The data (Figure 4a,b) elucidate the partial exfoliation of MMT with AMPS/AAm nanogel which confirmed from the reduction of the intensity of peak at 2-theta of 7.9°, corresponding to a d-basal spacing of (001), and the shift of this peak to lower angles signal at 4.8° with formation of AMPS/AAm. The complete exfoliation of the MMT layers was observed with the disappearance of this peak as confirmed from incorporation of AMPS/AA nanogels (Figure 4c).

The surface charges or zeta potentials of MMT nanogel composites can be measured as reported in the experimental section at different pHs of aqueous solutions and represented in Table 2. It was
noticed that, all MMT nanogels have negative charges at different pHs even when APTAC used to form nanogels. It was also observed that from the data, listed in Table 2, the order of negativity at pH 7 increases in the order AMPS/AAm > AMPS/AA > AAm/VP > AMPS/APTAC nanogels. Moreover, this order also confirms the dispersion stability of MMT nanogel suspensions in water. High dispersed MMT suspensions can obtained for particles have zeta potentials more negative than $-25 \text{ mV}$ [33]. The reductions of negative charges of MMT layers in the presence of AMPS/APTAC can be referred to the exchange of Na cation with APTAC nanogels that intercalate or exfoliate MMT layers to equilibrate the negative charge density [25]. Finally, it can be concluded that the high surface charges on MMT nanogel composites based on AMPS/AAm and AMPS/AA will produce elastic and highly dispersed MMT nanogel networks.

| MMT Nanogels      | Solvent     | DLS: Particle Size (nm) | PDI  | *Zeta Potential (mV) at Different pHs | pH 4 | pH 7    | pH 9    |
|-------------------|-------------|-------------------------|------|-------------------------------------|------|---------|---------|
| AMPS/AA           | water       | 222 ± 10                | 0.151| −26.4 ± 5                            | −30.60 ± 4 | −31.60 ± 3 |
|                   | Sea water   | 324 ± 10                | 0.181|                                     |      |         |         |
| AMPS/AAm          | water       | 92 ± 5                  | 0.165| −30 ± 3                             | −45.4 ± 4 | −25.4 ± 2 |
|                   | Sea water   | 135 ± 15                | 0.271|                                     |      |         |         |
| AMPS/APTAC        | water       | 138 ± 15                | 0.533| −3.60 ± 4                           | −8.6 ± 2 | −11.6 ± 4 |
|                   | Sea water   | 1397 ± 45               | 0.671|                                     |      |         |         |
| HMMT-AAm/VP       | water       | 122 ± 11                | 0.403| −2.9 ± 3                            | −18.4 ± 5 | −19.4 ± 4 |
|                   | Sea water   | 1481 ± 65               | 0.971|                                     |      |         |         |
| AAm/VP            | water       | 78.2 ± 8                | 0.371| −14.60 ± 5                          | −13.7 ± 4 | −17.6 ± 2 |
|                   | Sea water   | 865 ± 35                | 0.456|                                     |      |         |         |

* The all measurements were carried out in $10^{-3}$ M KCl at pH.

The particle size diameter and polydispersity index of nanoparticles in aqueous solution can be determined to investigate the behavior of nanoparticles in aqueous solution as determined from DLS measurements in distilled and sea water as summarized in Figure 5a–j and Table 2. Sea water was filtered from the solid suspension and used to investigate the effect of sea water on the aggregation of nanogel particles to correlate their behavior when blended with epoxy and exposed to a marine environment as illustrated in the coating section. The TEM data cannot give accurate nanomaterial diameter values and their dispersions because it is determined in the dry state but it can be used to elucidate the effect of electrostatic charges on the particle dispersion. DLS data of MMT nanogels were measured in fresh distilled and filtered sea water to investigate the effect of salt on swelling of nanogels and PDI of nanomaterials.

Careful inspection of the data confirms that MMT-AMPS/AAm produced uniform nanogel composites and the particle sizes increase from 92 to 135 nm when measured in distilled and sea water, respectively (Figure 5a,b). The MMT-AAm/VP form non-uniform particles with formation of cluster aggregates which increased when hydrophobic MMT was used instead of hydrophilic MMT as observed in Figure 5c–f. The interaction of AMPS/AA nanogel with MMT produced uniform nanogel composites (Figure 5g,h) like MMT-AMPS/AAm. The particle sizes of MMT-AMPS/AA are greater than MMT-AMPS/AAm which confirms the low contents of AMPS/AAm as compared to AMPS/AA as determined from TGA data (Table 1). On the other hand, the great interaction between amide groups of AMPS/AAm and MMT sheets decreases the nanocomposite particle sizes [34]. The increment of particle sizes of MMT-AMPS/APTAC (Figure 5i,j) in sea water more than other nanogel composites can be attributed to an increment of the absorption capacity of polyampholyte networks in sea water [35]. It can also concluded that the higher surface charges on MMT nanogels of AMPS/AA and AMPS/AAm beside the high interaction of amide groups with silicate layer produce MMT nanogel composites having elastic networks and good PDI, even in the sea water. These data encourage the application of these materials in marine environment as nano-filler for epoxy resins.
2.2. Surface Characteristics of Na-MMT Nanogels

One of the most important limitations that affect the application of nano-fillers in coatings is the aggregation of the nanomaterials during the curing of coatings due to their small particle size [36]. The prepared MMT nanogel composites were mixed with different weight contents ranging from 0.1 to 3.0 wt % as illustrated in the Experimental Section. The dispersion of MMT nanogel composites into cured epoxy coatings on the glass grids can be examined from optical microscope photos as illustrated in Figure 6a–f. The photos confirm the good dispersion of MMT-AMPS/AAm and MMT-AMPS/AA nanogel composites as represented in Figure 6b,c at different weight percentages. It can be also observed that MMT-AMPS/APTAC forms aggregates even at low concentration (Figure 6d). It can also be observed that the hydrophobic modified MMT coated with AAm/VP nanogel composites (Figure 5e) were aggregated in the epoxy matrix. The MMT-AAm/VP photos (Figure 6f) showed better dispersion stability in epoxy resins than when hydophobically modified. These results are in harmony with the zeta potential and particle size data listed in Table 2. This means that the more negatively charged MMT nanogel composites can disperse into the epoxy matrix due to repulsive forces among nanogels and due to strong hydrogen bond formation between the amide groups of the nanogels with the hydroxyl groups of silicate layers or the hydroxyl groups of the cured epoxy polyamine system.

Figure 5. DLS data of particle sizes and PDI of MMT modified with (a,b) AMPS/AAm; (c,d) AAm/VP; (e,f) HMMT-AAm/VP; (g,h) AMPS/AA and (i,j) AMPS/APTAC nanogels in filtered sea and distilled water, respectively.
This speculation can also be confirmed by adhesion strength measurements between modified epoxy networks and the steel surfaces that will be illustrated in the forthcoming section.

![Figure 6.](image)

**Figure 6.** Optical microscope micrographs of glass slides coated with epoxy resins modified with MMT (a) blank; (b) AMPS/AA, (c) AMPS/AAm; (d) AMPS/APTAC; (e) HMMT-AAm/VP and (f) AAm/VP nanogels.

The wetting characteristics of epoxy films with sea water can be determined from the contact angle measurements between sea water droplets and epoxy films as summarized in Table 3. It is expected that the epoxy films having high contact angle values (low wettability) will resist the diffusion of water or salt into epoxy resins. The contact angle data (Table 3) of modified epoxy with MMT nanogel composites have high values than blank. The epoxy modified with MMT-AMPS/APTAC has lower contact angles than other modified epoxy resins. The epoxy modified with 0.1 wt % of hydrophobically modified MMT-AAm/VP and MMT-AMPS/AAm show greater contact angle data due to the hydrophobicity and high dispersion of nanogel composites, respectively. The higher dispersion efficiency of MMT nanogel composites into epoxy resins increases the contact angle data due to the strong interactions of nanoparticles at the surface reduces the formation of microcracks or holes on the epoxy surfaces and inhibits the diffusion of water into the epoxy matrix. It was also reported that the low particle size of nanomaterials reduced the contact angle data [37,38]. These data agree with the present work as summarized in Tables 2 and 3. The thermal oxidation stability of the cured epoxy resins and their MMT nanogel composites can be determined from TGA in air as represented in Table 4. The data confirmed that there are two degradation steps. The first degradation step of the blank epoxy networks shows thermal oxidation up to 240 °C. The second degradation step starts at
340 °C indicated the charring of the blank epoxy networks occurred in air at a higher yield (ca. 21% at 400 °C) which referred to catalysis by oxygen. Moreover, the complete oxidation combustion of the blank epoxy network chars occurred in air with maximum rate at 510 °C (Table 4). Careful inspection of data listed in Table 4 elucidate that the first degradation step is strongly reduced in the presence of nanogel composites embedded with the epoxy networks. The MMT nanogel epoxy composites are stable up to 280–350 °C. The TGA curves of the MMT nanocomposites show a maximum rate of weight loss at a lower temperature (345–355 °C) than the blank epoxy network resin (Table 4) which can be probably attributed to the catalytic activity of MMT as clay mineral. This was clear observed in the epoxy networks embedded with AMPS/AA networks as MMT protonic acid catalyst due to presence of sulfonic and carboxylic acid groups in its chemical structure more than other MMT nanogel composites. The thermal stability of the epoxy and their nanogel composited is estimated at the onset at 5 wt % loss (Table 4) proves that the lower thermal stability of the epoxy embedded with AMPS/AA nanogel composites as compared to the other nanogel composites. It was also observed that the yield of the charred epoxy is reduced with incorporation of nanogel composites and lowered in AMPS/AA composites. The data also confirmed that the most exfoliated MMT in the presence of AMPS/AA shows the largest shielding effect from oxygen as confirmed from increment of char oxidation temperature of epoxy that increased to 620 °C (Table 4). A lower oxidation protection for the epoxy networks is obtained with the incorporation of MMT capped with AMPS/APTAC and AAmVP that have low degree of dispersion in epoxy coat (Figure 6d,e). This observation agree with the data reported on the incorporation of intercalated or low exfoliated clay with epoxy coat do not give oxygen shielding to reduce the thermal oxidation stability of epoxy networks [39].

Table 3. Contact angles, pull-off resistance and mechanical properties of cured epoxy with different types of MMT nanogel composites.

| Cured Epoxy | Concentrations of Nanocomposites (wt %) | Contact Angles (Degree) | Pull-Off Resistance Force (MPa) | Abrasion Resistance mg/1 kg Weight for 5000 Cycles | Mechanical Properties | Impact Test (Joule) | Hardness (Newton) | Bending |
|-------------|----------------------------------------|-------------------------|--------------------------------|-----------------------------------------------|----------------------|---------------------|-------------------|---------|
| blank       | 0                                      | 49.80                   | 4.59                           | 85                                            | 5                    | 8                   | pass              |
| AMPS/AA     | 0.1                                    | 73.43                   | 9.11                           | 12                                            | 14                   | 16                  | pass              |
|             | 1.0                                    | 71.40                   | 11.5                           | 15                                            | 12                   | 14                  | pass              |
|             | 3.0                                    | 75.60                   | 8.5                            | 18                                            | 10                   | 12                  | pass              |
| AMPS/AAm    | 0.1                                    | 82.40                   | 10.5                           | 14                                            | 13                   | 14                  | pass              |
|             | 1.0                                    | 83.43                   | 12.0                           | 9                                             | 15                   | 16                  | pass              |
|             | 3.0                                    | 80.33                   | 14.0                           | 5                                             | 18                   | 12                  | pass              |
| AMPS/APTAC  | 0.1                                    | 74.07                   | 7.15                           | 22                                            | 10                   | 10                  | pass              |
|             | 1.0                                    | 69.17                   | 10.5                           | 34                                            | 8                    | 11                  | pass              |
|             | 3.0                                    | 64.20                   | 7.4                            | 20                                            | 11                   | 12                  | pass              |
| HMMT-AAm/VP | 0.1                                    | 80.33                   | 6.75                           | 19                                            | 10                   | 10                  | pass              |
|             | 1.0                                    | 79.47                   | 5.4                            | 28                                            | 9                    | 9                   | pass              |
|             | 3.0                                    | 61.13                   | 5.55                           | 20                                            | 11                   | 11                  | pass              |
| AAm/VP      | 0.1                                    | 77.23                   | 7.0                            | 20                                            | 12                   | 13                  | pass              |
|             | 1.0                                    | 81.27                   | 7.5                            | 12                                            | 14                   | 12                  | pass              |
|             | 3.0                                    | 68.03                   | 7.8                            | 18                                            | 10                   | 14                  | pass              |

Table 4. Thermal oxidation of cured epoxy with 1 wt % of different types of MMT nanogel composites.

| Cured Epoxy | Concentrations of Nanocomposites (wt %) | T5 wt % Loss (°C) | Char Yield % at 500 °C | Degradation Steps (°C) | First | Second | Char Oxidation |
|-------------|----------------------------------------|-------------------|-------------------------|------------------------|-------|--------|---------------|
| blank       | 0                                      | 240               | 21                      | 240                    | 340   | 510    |
| AMPS/AA     | 1.0                                    | 280               | 27                      | 330                    | 620   |
| AMPS/AAm    | 1.0                                    | 350               | 25                      | 350                    | 580   |
| AMPS/APTAC  | 1.0                                    | 320               | 24                      | 410                    | 540   |
| AAm/VP      | 1.0                                    | 310               | 24                      | 380                    | 530   |
2.3. Mechanical and Anticorrosion Performances of Cured Epoxy Matrix with Nanogel Composites

The strong adhesion of epoxy resins with steel substrates increases their anticorrosion performance towards corrosive environments. Moreover, the good mechanical properties of organic coatings improve their resistance to mechanical damages. In this work, the mechanical properties of epoxy resins can be improved by using modified MMT mineral with elastic networks contains amide groups to increase the adhesion of epoxy with steel substrates beside the hydroxyl groups produced from curing of epoxide rings with polyamide hardeners [40]. The strong electrostatic attraction forces between MMT nanogel composites having more negative charge increased with positive charges of steel substrate. The pull-off adhesion resistance of unmodified epoxy resin (blank) and modified epoxy resins with MMT nanogel composites were determined and summarized in Table 3. The adhesion data of epoxy modified with MMT nanogels show good adhesion performances with steel substrate more than blank. It was also observed that, the adhesion strength of epoxy resin modified with MMT nanogels with AMPS/AAm and AMPS/AA possess large adhesion values which can be referred to their high dispersion of these nano-composites. Moreover, the exfoliation of MMT sheets increases the adhesion of epoxy resins with steel substrate due to strong interaction with amide gels and steel substrate [41]. The impact, abrasion resistances, hardness force and bending tests of the epoxy coatings on the steel substrate were determined as ASTM procedure and listed in Table 3. The high abrasion and impact resistances of modified epoxy resin with MMT nanogels based on AMPS/AAm and AMPS/AA confirm the improvement of mechanical properties of epoxy coats. On the other hand, the good hardness force and pass the bending test elucidate the good dispersion of MMT nanogel into epoxy matrix to fill the holes and micro cracks of epoxy resins. The good abrasion and impact resistance confirm that the MMT nanogel composites possess elastic networks which can absorb any forces to improve the mechanical properties of modified epoxy resins.

Salt spray resistance is an alternative test used to evaluate the anticorrosion performance of organic coats in humid marine environments. It can be evaluated either by blistering or rust formation under coats. The failure of the test can referred to diffusion of water and salt into coating layers to form activated corrosive centers on the steel surfaces. The test was accelerated by deformation of coatings with X-cut. The coated steel panels were evaluated periodically at different duration times up to 1000 h. It is recommended that, the coatings pass 500 h without rust or blistering formation can be used for marine coatings of steel substrate. The results of salt spray tests of modified epoxy coats such as rust area percentages were evaluated and listed in Table 5.

| MMT Nanogel | Sample wt Ratio (%) | Exposure Time (h) | Disbonded Area % | Rating Number (ASTM D1654) |
|-------------|---------------------|-------------------|------------------|-----------------------------|
| AMPS/APTAC  | 0.1                 | 500               | 3                | 8                           |
|             | 1.0                 | 500               | 2                | 8                           |
|             | 3.0                 | 500               | 2                | 8                           |
| AAm/VP      | 0.1                 | 750               | 2                | 8                           |
|             | 1.0                 | 750               | 3                | 8                           |
|             | 3.0                 | 750               | 1                | 9                           |
| AMPS/AAm    | 0.1                 | 1000              | 3                | 8                           |
|             | 1.0                 | 1000              | 2                | 8                           |
|             | 3.0                 | 1000              | 1.5              | 9                           |
| AMPS/AA     | 0.1                 | 1000              | 1                | 9                           |
|             | 1.0                 | 1000              | 2                | 8                           |
|             | 3.0                 | 1000              | 3                | 8                           |

The photos of the modified epoxy coatings after passing the salt spray test were gathered in Figure 7a–f. The blank epoxy failed to pass the salt spray resistance above 300 h duration time. The modification of epoxy coatings with MMT nanogels based on AMPS/AA, AMPS/AAm achieved
good salt spray resistance up to 1000 h. The MMT modified with AAm/VP pass the salt spray resistance test up to 750 h and that epoxy modified with hydrophobic MMT passes the test up to 650 h. The epoxy coatings modified with polyampholye nanogels based on MMT-AMPS/APTAC achieved low duration times up to 500 h. These data agree with the contact angles and DLS dispersion data which show that the coatings modified with dispersed nanogel composites increase the salt spray resistance of epoxy coatings. Moreover, the ability of nanogel composites to fill the cracks, microscopic porosities and free volumes existed in the epoxy coating matrix leading to the increase of electrolyte pathway length due to their smaller particle sizes in sea water. The photos of coated panels (Figure 7) show that the epoxy coating modified with nanogel based on AMPS/AA (0.1%) and all AMPS/AAm nanogels can act as self-healing for epoxy modified coats due to absence of rust at X-cut. This can be refereed to salt resistances of AMPS polymers to salt [42–45]. The salt resistance and sensitivity of ionic AMPS/AAm gels increase their ability to form a self-healing layer at the damage area. The exfoliation of MMT-AMPS/AAm into the epoxy matrix and the excellent adhesion of their amide groups of nanogels to steel substrates improve their ability to inhibit the diffusion of salts or water into the epoxy matrix.

The dispersion of MMT into the epoxy nanocomposites is important parameter that increases the coating performance of epoxy networks as organic coatings for steel. In this respect, the aggregation, intercalation and exfoliation of MMT nanogels can be confirmed by TEM analysis as represented in Figure 8a–c. The incorporation of 1 wt % of MMT encapsulated with AMPS/AAm and AMPS/AA (Figure 8a,c) shows a mixture of exfoliated and intercalated silicate layer. The presence of AMPS/AMPTAC shows the formation of an intercalated structure for the silicate MMT layer that agglomerates the MMT nanogel composites into epoxy networks (Figure 8b). The TEM data showed that the larger spacing of MMT in the presence of AMPSAA (Figure 8c) confirms that the presence of sulfonate and carboxylic acid groups increased the acidity of nanogel. Consequently, the higher
acidity of MMT encapsulated with AMPS/AA increases the catalytic curing of epoxy networks and MMT exfoliation [46].

Figure 8. TEM micrographs of 1% weight percentages of MMT modified with (a) AMPS/AAm; (b) AMPS/APTAC and; (c) AMPS/AA nanogels.

Electrochemical impedance spectroscopy (EIS) measurements were used to investigate the coating performances of epoxy blank and embedded with 1 wt % of MMT encapsulated with AMPS/AA in 3.5% NaCl solution. Figure 9 represents the Bode plots of the epoxy coating blank with 0.1 wt % of MMT encapsulated with AMPS/AA at different immersion times ranged from 1 to 10 days in 3.5% NaCl aqueous electrolyte solution. The data confirmed the impedance of the coating samples increased with the incorporation of 0.1 wt % of MMT encapsulated with AMPS/AA than blank at different immersion times as confirmed from increment of the polarization resistance (Rp) [47]. The Rp are measured for blank at 1, 10 immersion days, epoxy embedded with 0.1 wt % of MMT encapsulated with AMPS/AA at 1 and 10 immersion days in aqueous electrolyte solution as $0.06186, 0.09021, 0.73743$ and $0.92071 \times 10^5$ (Ohm), respectively. Moreover, the difference in the modulus of impedance between the epoxy blank and with 0.1 wt % of MMT encapsulated with AMPS/AA increased with the immersion time. These data suggest that the 0.1 wt % of MMT encapsulated with AMPS/AA increased the barrier properties of the epoxy coatings. It seems that the exfoliated MMT could efficiently restrict the access of the aggressive ions to the underlying substrate surface through forming protective layer on the coating surface by self-healing of the scratched area. Therefore, protection performance of the coating is increased. It can be concluded that a barrier layer of epoxy coatings was released after scratching the coating containing 0.1 wt % of MMT encapsulated with AMPS/AA, which limited the access of the aggressive ions to attack the underlying substrate and provide more protection performance of the coating by self-healing effect as confirmed from the salt spray resistances.

Figure 9. The Bode plots of epoxy coating blank and embedded with 0.1 wt % of MMT encapsulated with AMPS/AA at different immersion times in 3.5% NaCl solution.
3. Materials and Methods

3.1. Materials

Hydrophobic nanoclay based on montmorillonite modified with 15 wt % octadecylamine (HMMT) with the commercial name Nanomer® clay and hydrophilic sodium montmorillonite (Na-MMT) with the commercial name Nanomer® PGV were used as the sources for MMT. 2-Acrylamido-2-methylpropane sulfonic acid (AMPS), acrylamide (AAm), acrylic acid (AA), N-vinyl pyrrolidone (VP), (3-acrylamidopropyl)trimethylammonium chloride (APTAC), N,N-methylene-bisacrylamide (MBA) crosslinker, ammonium persulfate radical polymerization initiator (APS), N,N,N′,N′-tetramethylethylenediamine radical polymerization activator (TEMED) and poly(vinyl pyrrolidone) stabilizer (PVP with molecular weight 40,000 g/mol) were used without purification to prepare crosslinked nanogel composites with MMT. All chemicals were obtained from Sigma-Aldrich Co., Darmstadt, Germany.

3.2. Preparation of MMT Nanogel Composites

Na-MMT was used to prepare nanogel composites with AMPS/AA, AMPS/AAm, AMPS/APTAC and AAm/VP using suspension radical crosslinking copolymerization surfactant free technique. In this respect, Na-MMT (3.5 g) was mixed in ethanol/water mixture (60/40 vol %, 150 mL) and PVP (1 g) under vigorous stirring for 24 h at room temperature. APS (0.125 g) was added to the reaction mixture under a nitrogen atmosphere and stirring followed by the addition of AMPS/AA, AMPS/AAm, AMPS/APTAC, or AAm/VP to the reaction mixture using a mole ratio of 1:1 and their total weights did not increase more than 3 g. TEMED (20 µL) was injected into the reaction mixture and the reaction temperature increased up to 50 °C and kept constant for 24 h. The MMT nanogel composites were separated from the solutions after ultracentrifugation at 21,000 rpm for 30 min and purified using dialysis membrane for 1 week. The same procedure was repeated and HMMT was used instead of Na-MMT to prepare HMMT-AAm/VP nanogel composite.

3.3. Preparation of MMT Epoxy Nanocomposite Coatings

Na-MMT-AMPS/AA, AMPS/AAm, AMPS/APTAC, or AAm/VP and HMMT-AAm nanogel composites were blended with epoxy resin at different weight percentages ranged from 0.1 to 3 wt % based on total weight of epoxy and hardener under sonication for 30 min. The dispersed MMT nanogel epoxy composites were mixed with polyamine hardener under vigorous stirring according to the recommended resin/hardener volume ratios (4/1). The mixtures were sprayed on blasted and cleaned steel panels to obtain dry film thickness (DFT) of 100 µm and cured for 1 week at temperature 40 °C to be sure the all epoxy films were cured.

3.4. Characterization

The chemical structure of MMT nanogel composites was determined by Fourier Transform infra-red (Varian 3100 FTIR spectrometer, Madison, WI, USA). The thermal stability and MMT contents of MMT nanogel composites were evaluated using differential thermal and thermogravimetric analysis (TGA-DTA; TGA-50, Shimadzu, Tokyo, Japan) at flow rate 50 mL/min and heating rate of 20 °C/min under an inert nitrogen atmosphere and air for epoxy embedded with MMT nanogel composites. High resolution transmission electron microscopy (HR-TEM) using a JEM-2100 electron microscope (JEOL, Tokyo, Japan) at an acceleration voltage of 200 kV was used to examine the nanogel composite surface morphology. The dispersion stability, polydispersity index (PDI) and surface charges (zeta potential; mV) of MMT nanogel composites were determined by using dynamic light scattering (DLS; Laser Zeta meter Model Zetasizer 2000, Malvern Instruments, Montereal, QC, Canada). The surface contact angles between sea water and cured epoxy panels were determined using a drop shape analyzer model DSA-100 (Krüss GmbH, Hamburg, Germany). The distribution of nanogel
composites into cured epoxy films was examined using optical microscope (DP 72, Olympus, Tokyo, Japan) after coating the glass slides with epoxy nanogel composites.

The adhesion (pull-off resistance forces), abrasion resistance, hardness, T-bending, impact resistance tests for the epoxy coatings on steel panels were carried out according standard methods ASTM procedures. A salt spray cabinet (model SF/450, manufactured by CW Specialist Equipment Ltd., Leintwardine, Craven, Arms, Shropshire, UK) was used to examine the salt spray resistance of coated panels.

The exfoliation of MMT using nanogels was investigated using wide-angle X-ray diffraction (WXRD; D/MAX-3C OD-2988N X-ray diffractometer, Rigaku, Eindhoven, The Netherlands) with a copper target and Ni filter at a scanning rate of 4°/min.

Electrochemical impedance spectroscopy (EIS) was performed using a 1470E multichannel system (Solartron, Farnborough, UK) as electrochemical interface and a Solartron 1455A Frequency Response Analyzer. The measurements were initiated applying to the electrode a sinusoidal amplitude of 10 mV on the frequency range from 10^4 to 10^−2 Hz.

4. Conclusions

The modification of MMT with nanogel composites based on AMPS produced sheets having high negative surface charges after using AMPS/AAm and AMPS/AA nanogels produced elastic and highly dispersed MMT nanogel composites. The surface charges on MMT nanogels of AMPS/AA and AMPS/AAm beside the interaction of their amide groups with silicate layer produce MMT nanogel composites having a good dispersity index in sea water. The contact angles and DLS dispersion data show that the epoxy coatings modified with dispersed MMT nanogel composites increase the salt spray resistance of epoxy coatings. The exfoliation of MMT-AMPS/AAm into the epoxy matrix and their excellent adhesion to steel substrate improve their ability to inhibit the diffusion of salts or water into epoxy matrix. The epoxy coating modified with nanogel based on AMPS/AA (0.1%) and all AMPS/AAm nanogels can act as self-healing material for epoxy modified coatings. The salt resistance and sensitivity of ionic AMPS/AAm gels increase their ability to act as a self-healing layer at damaged areas.

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