Observing binary inspiral in gravitational radiation: One interferometer

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Abstract

Close binary systems of compact objects with less than ten minutes remaining before coalescence are readily identifiable sources of gravitational radiation for the United States Laser Interferometer Gravitational-wave Observatory (LIGO) and the French-Italian VIRGO gravitational-wave observatory. As a start toward assessing the full capabilities of the LIGO/VIRGO detector network, we investigate the sensitivity of individual LIGO/VIRGO-like interferometers and the precision with which they can determine the characteristics of an inspiralling binary system. Since the two interferometers of the LIGO detector share nearly the same orientation, their joint sensitivity is similar to that of a single, more sensitive interferometer. We express our results for a single interferometer of both initial and advanced LIGO design, and also for the LIGO detector in the limit that its two interferometers share exactly the same orientation.

We approximate the secular evolution of a binary system as driven exclusively by its leading order quadrupole gravitational radiation. Observations of a binary in a single interferometer are described by four characteristic quantities: an amplitude $A$, a chirp mass $M$, a time $T$, and a phase $\psi$. We find the amplitude signal-to-noise ratio (SNR) $\rho$ of an observed binary system as a function of $A$ and $M$ for a particular orientation of the binary with respect to the interferometer, and also the distribution of SNRs for randomly oriented binaries at a constant distance To assess the interferometer sensitivity, we calculate the rate at which sources are expected to be observed and the range to which they are observable. Assuming a conservative rate density for coalescing neutron star binary systems of $8 \times 10^{-8} \text{yr}^{-1} \text{Mpc}^{-3}$, we find that the advanced LIGO detector will observe approximately 69 yr$^{-1}$ with an amplitude SNR greater than 8. Of these, approximately 7 yr$^{-1}$ will be from binaries at distances greater than 950 Mpc.
We give analytic and numerical results for the precision with which each of the characteristic quantities can be determined by interferometer observations. For neutron star binaries, the fractional one-sigma statistical error in the determination of $A$ is equal to $1/\rho$. For $\rho > 8$, the fractional one-sigma error in the measurement of $M$ in the advanced LIGO detectors is less than $2 \times 10^{-5}$, a phenomenal precision. The characteristic time is related to the moment when coalescence occurs, and can be measured in the advanced detectors with a one-sigma uncertainty of less than $3 \times 10^{-4}$ s (assuming $\rho > 8$).

We also explore the sensitivity of these results to a tunable parameter in the interferometer design (the recycling frequency). The optimum choice of the parameter is dependent on the goal of the observations, e.g., maximizing the rate of detections or maximizing the precision of measurement. We determine the optimum parameter values for these two cases.

The calculations leading to the SNR and the precision of measurement assume that the interferometer observations extend over only the last several minutes of binary inspiral, during which time the orbital frequency increases from approximately 5 Hz to 500 Hz. We examine the sensitivity of our results to the elapsed time of the observation and show that observations of longer duration lead to very little improvement in the SNR or the precision of measurement.

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I. INTRODUCTION AND MOTIVATION

Both the United States Laser Interferometer Gravitational-wave Observatory (LIGO [1,2]) and the French/Italian VIRGO gravitational-wave observatory [3] are expected to begin operation in the late 1990s. Inspiralling binary systems of compact objects — either neutron stars or stellar mass black holes with orbital frequencies ranging from $5 \, \text{s}^{-1}$ to $500 \, \text{s}^{-1}$ — are currently regarded as the most certain observable source for these detectors: the density of sources [4,5] suggest event rates of several per year and the radiation they emit can be calculated unambiguously [6,7,8,9,10,11,12]. In support of the LIGO/VIRGO observational effort, theoreticians must combine refined calculations of the radiation from binary inspiral with the anticipated detector properties to deduce the instrument sensitivity. These calculations will, in turn, play an important role in the final design and ultimate use of the instruments. In this paper, we begin a detailed analysis of binary inspiral as a source of gravitational radiation for a LIGO/VIRGO-like interferometric detector.

Our goal in this work is to estimate the sensitivity of LIGO/VIRGO-like interferometers and the LIGO detector by determining the rate at which inspiralling binary systems can be detected, the range to which they can be observed, and the precision with which they can be characterized in a single interferometer. We also explore the compromises that must be made as different questions are asked of the observations. The optimal design and operation of these interferometers depends on a detailed understanding of the nature of the detector response to the radiation, the detector noise power spectral density (PSD), and the questions the observation is meant to resolve. For example, we show in §V that the goal of observing as many sources as possible (without necessarily being able to characterize them precisely) leads to a different optimal interferometer configuration than the goal of characterizing observed sources as precisely as possible (while allowing that weak sources may be missed entirely).

The ultimate goal of our assessment of binary inspiral is to determine the ability of a single interferometer (or a network of such interferometers) to

1. Detect the gravitational radiation from the last few minutes of inspiral of a binary neutron star or black hole system, and

2. Measure the parameters describing the detected binary system from the observed gravitational radiation.

By detection we mean the determination of the presence or absence of a signal characteristic of an inspiralling binary system in the output of a detector, irrespective of the particular parameters that might characterize the observed binary system. By measurement we mean the determination of the parameters that characterize the signal presumed to be present in the detector output. In a real detector noise can mask or distort a signal present in the detector output; alternatively, it can conspire to appear as a signal characteristic of a binary system. Consequently, any conclusion we draw from observations (e.g., that we have detected an inspiralling binary system) is associated with a probability that characterizes our certainty in its validity.

As a practical matter, reliable detection of gravitational radiation will initially require coincident observation between two or more interferometers so that non-Gaussian noise events can be differentiated from gravitational radiation signals. When completed, the
LIGO detector will consist of two interferometers: one in Hanford, Washington and one in Livingston, Louisiana \cite{2}. The relative orientation of the two interferometers has been chosen to maximize their sensitivity to a single polarization state of the gravitational radiation impinging on the Earth\cite{13}; consequently, the two interferometers act together like a single interferometer whose sensitivity will be greater than that of either of its components. This analogy is not exact: combining the interferometers in this way ignores the different arrival times of the signal at the two distinct interferometers. Nevertheless, our single-detector analysis is directly relevant to the actual LIGO configuration, and we discuss our results in the context of (i) single LIGO/VIRGO-like interferometers of the proposed initial and advanced designs, and (ii) the LIGO detector in the limit that its two independent interferometers share exactly the same orientation and ignoring the difference in the signal arrival times.

In principle, simultaneous observation of an inspiralling binary system in three interferometers of different orientations is sufficient to measure (among other characteristics) the binary’s luminosity distance \(d_L\), its position in the sky, and a function \(\mathcal{M}\) that depends only on the masses of its components and its cosmological redshift \cite{14,15}. If the position is known through other observations, then \(\mathcal{M}\) and \(d_L\) can be measured from observations with only two interferometers of different orientations. Observation of an inspiralling binary in a single interferometer can measure \(\mathcal{M}\) and a waveform “amplitude” \(\mathcal{A}\), which depends on the luminosity distance and orientation of the binary with respect to the detector. Even this limited information is of astrophysical significance, however: from observations of the distribution of \(\mathcal{A}\) and \(\mathcal{M}\) among the observed binaries one can determine the distribution of the component masses of inspiralling binary systems, find the Hubble constant and deceleration parameter, and test cosmological models \cite{16}.

The study of binary systems as sources of gravitational radiation began in 1963 when Peters and Mathews \cite{6} made the first detailed calculation of the gravitational radiation luminosity from inspiralling binary systems, focusing on the leading order quadrupole radiation from two point particles in circular and elliptical orbits. Clark and Eardley \cite{17} explored how gravitational radiation (among other effects) drives the orbital evolution of binary systems. Clark \cite{18} suggested inspiralling binary systems as an important source of gravitational radiation for modern interferometric detectors; however, he considered only the burst of radiation from the coalescence event itself. Thorne recognized the importance of the gravitational radiation from the final few minutes of inspiral. Since 1987 a number of investigators have worked with increasing sophistication on problems related to the observation of inspiralling binaries in interferometric detectors. Some have focused on understanding and refining interferometer detector technology \cite{19,20,21,22,23,24}, others have focused on the data analysis problems of detecting or determining the characteristics of a binary system from the radiation \cite{25,26,27,28,29,30}, and still others have focused on refining our understanding of the gravitational radiation waveform from these systems \cite{7,8,9,10,11,12,31,32,33}.

\footnote{While primarily sensitive to a single polarization state of the radiation field, LIGO will, with more limited sensitivity, be capable of observing both polarizations simultaneously. In a subsequent paper we will take the exact detector orientations into account in our analysis.}
or their rate of occurrence in the Universe [4,5].

The remainder of this paper is organized as follows. In §II we review how the precision with which the parameterization of a signal, observed in a noisy detector, is determined. In §III, we apply these techniques to the particular problem of finding the precision with which the parameters of an inspiralling binary system can be measured. These results depend only on the detector noise power spectral density (PSD) and not on the type of detector (e.g., interferometer or bar). In §IV we apply the results of §III to both the initial and advanced proposed LIGO/VIRGO-like interferometers. We discuss the astrophysical implications of these results in §V and present our conclusions in §VI.

II. MEASUREMENT AND UNCERTAINTY

In this section we review the techniques we use to determine the statistical uncertainties in observations of binary inspiral. A complete discussion is found in Finn [34]. The techniques developed there are closely related to those associated with signal analysis by optimal filtering. For more information on optimal filtering and signal analysis we direct the reader to Oppenheim, Willsky, and Young [35], the review by Davis [36] and references therein, Wainstein and Zubakov [37], and Hancock and Wintz [38].

A. Introduction

Consider a deterministic (i.e., not stochastic) source of gravitational radiation (e.g., an inspiralling binary system) and a detector (e.g., a laser interferometer). We write the response of the detector to the radiation as a superposition of noise \( n(t) \) and signal \( m(t; \mu) \), where \( \mu \) is a minimal set of parameters that uniquely characterizes the detector response (absent the noise) to the radiation for the entire duration of the observation (in §III we show that for an inspiralling binary system observed by a single interferometric detector \( \mu \) is a four dimensional vector). Let the source of radiation be characterized by \( \tilde{\mu} \). In analyzing the output of the detector, we have two goals:

1. To determine whether a signal is present in the detector output, and

2. To find the precision with which we can determine \( \tilde{\mu} \) (assuming a signal is present).

Owing to the detector noise, we cannot determine with certainty either the presence of a signal or (assuming it present) \( \tilde{\mu} \). Instead, we find the probability that the detector output is consistent with the presence of a signal, and represent our uncertainty in \( \tilde{\mu} \) by a set of volumes \( V(P) \) in parameter space, such that \( \tilde{\mu} \) is in \( V(P) \) with probability \( P \). The volumes \( V(P) \) are a measure of the sensitivity of the detector. Throughout this section, we will assume that we have determined that a signal is present so that the probability \( P \) associated with \( V(P) \) is a conditional probability. In a later paper, we will discuss the determination of the probability that a signal of the form \( m(t; \mu) \) is present in the detector output.

Each observed signal is immersed in its own realization of the detector noise; consequently we cannot know in advance of an observation what the volumes \( V(P) \) will look like. We can,
however, determine what the most likely volumes are for a given observation, and that is what we do here. In this section we review briefly the procedures used to find the most likely volumes \( V(P) \). These procedures are developed in Finn [34], and we refer the interested reader there for more information.

B. The probability volumes \( V(P) \)

We characterize the observed output of our detector as a time series \( g(t) \), which is a superposition of noise \( n(t) \) and (perhaps) a signal \( m(t; \tilde{\mu}) \):

\[
g(t) \equiv \begin{cases} 
n(t) + m(t; \tilde{\mu}) & \text{signal present} \\
n(t) & \text{signal absent}. 
\end{cases} \tag{2.1}
\]

The parameter \( \tilde{\mu} \) is fixed but unknown, and we assume the noise is drawn from a stationary process. The probability density that a signal with parameterization \( \mu \) is present in the detector output \( g(t) \) is

\[
P(\mu | g) \equiv \begin{pmatrix} 
\text{The conditional probability that a} \\
\text{signal characterized by } \mu \text{ is present} \\
given the detector output } g(t).
\end{pmatrix} \nonumber
\]

\[
= \frac{\Lambda(\mu)}{\Lambda + P(0)/P(m)} \tag{2.2}
\]

where

\[
P(0) \equiv \begin{pmatrix} 
\text{The a priori probability} \\
\text{that the signal is absent}
\end{pmatrix}, \tag{2.3a}
\]

\[
P(m) \equiv \begin{pmatrix} 
\text{The a priori probability} \\
\text{that the signal } m(\mu) \\
\text{(for undetermined } \mu) \text{ is present}
\end{pmatrix}, \tag{2.3b}
\]

\[
\Lambda \equiv \int d^N \mu \Lambda(\mu), \tag{2.3c}
\]

\[
\Lambda(\mu) \equiv p(\mu) \exp \left[ 2 \langle g, m(\mu) \rangle - \langle m(\mu), m(\mu) \rangle \right], \tag{2.3d}
\]

\[
p(\mu) \equiv \begin{pmatrix} 
\text{The a priori probability density that the signal} \\
\text{parameterization is } \mu.
\end{pmatrix} \tag{2.3e}
\]

\[
\langle r, s \rangle \equiv \int_{-\infty}^{\infty} df \frac{\bar{r}(f) \bar{s}^*(f)}{S_h(|f|)}, \tag{2.3f}
\]

\[
\bar{r}(f) \equiv \int_{-\infty}^{\infty} dt e^{2\pi i ft} r(t), \tag{2.3g}
\]

\[
S_h(f) \equiv \begin{pmatrix} 
\text{One-sided detector noise} \\
\text{power spectral density (PSD)}
\end{pmatrix}. \tag{2.3h}
\]

The likelihood ratio \( \Lambda \) (eqn. 2.3c) is proportional to the a posteriori probability that a signal is present in the observed \( g(t) \). When that probability exceeds a given threshold
we assume a signal is present and try to determine $\tilde{\mu}$. We characterize an observation of $g(t)$ in terms of the mode (i.e., the maximum) of the distribution $P(\mu|g)$, denoted $\hat{\mu}$. The mode of $P(\mu|g)$ is also the mode of the odds ratio $\Lambda(\mu)$. In terms of $\hat{\mu}$ the observation’s signal-to-noise ratio (SNR) $\rho^2$ is

$$\rho^2 = 2 \langle m(\hat{\mu}), m(\hat{\mu}) \rangle. \quad (2.4)$$

Assuming that $\Lambda(\mu)$ is smooth and that its global maximum is a local extremum, $\hat{\mu}$ satisfies

$$2 \left\langle m(\hat{\mu}) - m(\hat{\mu}), \frac{\partial m}{\partial \mu_j}(\hat{\mu}) \right\rangle + \frac{\partial \ln p}{\partial \mu_j}(\hat{\mu}) = -2 \left\langle n, \frac{\partial m}{\partial \mu_j}(\hat{\mu}) \right\rangle. \quad (2.5)$$

We assume that the noise $n(t)$ is a normal random variable with zero mean; consequently, so are each of the $\langle n, \partial m/\partial \mu_j \rangle$ on the righthand side of equation 2.5. Denote these random variables $\nu_i$:

$$\nu_i \equiv 2 \left\langle n, \frac{\partial m}{\partial \mu_i}(\hat{\mu}) \right\rangle. \quad (2.6)$$

Since the $\nu_i$ are normal, their joint distribution is a multivariate Gaussian, characterized by the means $\nu_i$, which vanish, and the quadratic moments

$$\nu_i \nu_j = 4 \left\langle n, \frac{\partial m}{\partial \mu_i}(\hat{\mu}) \right\rangle \left\langle n, \frac{\partial m}{\partial \mu_j}(\hat{\mu}) \right\rangle = 2 \left\langle \frac{\partial m}{\partial \mu_i}(\hat{\mu}), \frac{\partial m}{\partial \mu_j}(\hat{\mu}) \right\rangle \equiv C^{-1}_{ij}. \quad (2.7a)$$

Here we have used an overbar to indicate an average over all instances of the noise $n(t)$. Since we have assumed that the noise is normal these averages can be evaluated using the ergodic theorem (cf. Finn [34] for more details). In terms of $C_{ij}$ (i.e., the inverse of $C^{-1}_{ij}$), the joint distribution of the $\nu_i$ is given by the probability density

$$p(\nu) = \frac{\exp \left[ -\frac{1}{2} \sum_{i,j} C_{ij} \nu_i \nu_j \right]}{[(2\pi)^N \det ||C_{ij}||]^{1/2}}. \quad (2.8)$$

This is also the joint distribution of the quantities that appear on the lefthand side of equation 2.5. In Finn [34] it was stated that for an observation characterized by $\hat{\mu}$, the probability volumes $V(P)$ are given implicitly by

---

\footnote{Note that $\rho^2$ is quadratic in the signal strength. In the literature SNR is often used to refer to both $\rho$ and $\rho^2$. We avoid this ambiguity by using either $\rho$ or $\rho^2$ as appropriate.}
\[ K^2 \geq \sum_{i,j} C_{ij} \left[ 2 \left\langle m(\mu) - m(\mu), \frac{\partial m}{\partial \mu_i}(\mu) \right\rangle + \frac{\partial \ln p}{\partial \mu_i}(\mu) \right] \times \left[ 2 \left\langle m(\mu) - m(\mu), \frac{\partial m}{\partial \mu_j}(\mu) \right\rangle + \frac{\partial \ln p}{\partial \mu_j}(\mu) \right], \] (2.9)

where

\[ P = \int_{\sum_{i,j} C_{ij} \nu_i \nu_j \leq K^2} d^N \nu \frac{\exp \left[ -\frac{1}{2} \sum_{i,j} C_{ij} \nu_i \nu_j \right]}{(2\pi)^N \det ||C_{ij}^{-1}||}^{1/2} \] (2.10)

and \( \tilde{\mu} \in V(P) \) with probability \( P \) (recall that \( P \) is conditional on the assumption that a signal is in fact present in the detector output). *This is correct only when \( \Lambda(\mu) \) has a single extremum, or near \( \hat{\mu} \). In the most general case only a Monte Carlo analysis can determine the probability volumes \( V(P) \). No other results of Finn [34] are affected by this correction.

C. The strong signal approximation

The volumes \( V(P) \) are representations of a cumulative probability distribution function. Denote the corresponding probability density by \( P(\delta\mu|\tilde{\mu}) \):

\[ P(\delta\mu|\tilde{\mu}) \equiv \begin{cases} \text{The conditional probability} \\ \text{density that } m \text{ is characterized} \\ \text{by } \tilde{\mu} + \delta\mu, \text{ given that } \Lambda(\mu) \\ \text{has mode } \hat{\mu} \end{cases} \] (2.11)

In the limit of large \( \rho^2 \), \( P(\delta\mu|\tilde{\mu}) \) becomes sharply peaked about \( \hat{\mu} \) and the determination of \( V(P) \) is greatly simplified. Suppose that \( \rho^2 \) is so large that for \( \tilde{\mu} \in V(P) \) for all \( P \) of interest the difference \( m(\tilde{\mu}) - m(\hat{\mu}) \) can be linearized in \( \delta\mu \), where

\[ \delta\mu \equiv \tilde{\mu} - \hat{\mu}. \] (2.12)

We then obtain in place of equation (2.5)

\[ \sum_{i,j} \delta\mu_i C_{ij}^{-1} = -2 \left\langle n, \frac{\partial m}{\partial \mu_j}(\hat{\mu}) \right\rangle - \frac{\partial \ln p}{\partial \mu_j}(\hat{\mu}) \] (2.13)

The random variables \( \delta\mu \) are related to the \( \nu \) by a linear transformation,

\[ \delta\mu_i = -\sum_{i,j} C_{ij} \left[ \nu_j + \frac{\partial \ln p}{\partial \mu_j}(\hat{\mu}) \right]; \] (2.14)

consequently, the \( \delta\mu \) are normal with means

\[ \overline{\delta\mu_i} = -\sum_{i,j} C_{ij} \frac{\partial \ln p}{\partial \mu_j}(\hat{\mu}), \] (2.15)
and quadratic moments

\[
(\delta \mu_i - \bar{\delta \mu}_i)(\delta \mu_j - \bar{\delta \mu}_j) = C_{ij}.
\] (2.16)

The probability distribution \( P(\delta \mu | \bar{\mu}) \) is thus a multivariate Gaussian (cf. eqn. 2.8):

\[
P(\delta \mu | \bar{\mu}) = \exp \left[ -\frac{1}{2} \sum_{i,j} C_{ij}^{-1} (\delta \mu_i - \bar{\delta \mu}_i) (\delta \mu_j - \bar{\delta \mu}_j) \right] \frac{1}{(2\pi)^N \det ||C_{ij}||}^{1/2}.
\] (2.17)

Note that the matrix \( C_{ij} \) has now acquired a physical meaning: in particular, we see that the variances \( \sigma_i^2 \) of the \( \delta \mu_i \) are

\[
\sigma_i^2 \equiv (\delta \mu_i - \bar{\delta \mu}_i)^2 = C_{ii} \tag{2.18}
\]

and the correlation coefficients \( r_{ij} \) are given by

\[
r_{ij} \equiv \sigma_i^{-1} \sigma_j^{-1} (\delta \mu_i - \bar{\delta \mu}_i) (\delta \mu_j - \bar{\delta \mu}_j) = \frac{C_{ij}}{\sigma_i \sigma_j} \tag{2.19}
\]

In this sense we say that \( C_{ij} \) is the covariance matrix of the random variables \( \delta \mu \).

In the strong signal approximation, the surfaces bounding the volume \( V(P) \) are ellipsoids defined by the equation

\[
\sum_{i,j} (\delta \mu_i - \bar{\delta \mu}_i) (\delta \mu_j - \bar{\delta \mu}_j) C_{ij}^{-1} = K^2,
\] (2.20)

where the constant \( K^2 \) is related to \( P \) by

\[
P = \int_{\sum_{i,j} C_{ij}^{-1} x^i x^j \leq K^2} d^N x \exp \left[ -\frac{1}{2} \sum_{i,j} C_{ij}^{-1} x^i x^j \right] \frac{1}{(2\pi)^N \det ||C_{ij}||}^{1/2} \tag{2.21}
\]

Finally we come to the question of when the linearization in equation 2.13 is a reasonable approximation. Three considerations enter here:

1. The probability contours of interest (e.g., 90\%) must not involve \( \delta \mu \) so large that the linearization of \( m(\bar{\mu}) - m(\hat{\mu}) \) is a poor approximation;
2. The probability contours of interest must not involve \( \delta \mu \) so large that for \( \delta \mu \in V(P) \), \( \Lambda(\delta \mu + \hat{\mu}) \) has more than one extremum or inflection point; and
3. The condition number of the matrix \( C_{ij}^{-1} \) must be sufficiently small that the inverse \( C_{ij} \) is insensitive to the linearization approximation in the neighborhood of \( \hat{\mu} \).\(^3\)

\(^3\)Recall that the relative error in \( \delta \mu \) is the condition number times the relative error in \( C_{ij}^{-1} \); for a large condition number, small errors in \( C_{ij}^{-1} \) introduced by the linearization approximation can result in large errors in \( \delta \mu \) (cf. Golub & Van Loan [39]).
If the validity of the linearization procedure for a particular problem is doubtful owing to
the violation of any of these conditions, then we must fall-back on either equations 2.5, 2.9
and 2.10 (if $\Lambda(\mu)$ has a single extremum), or a Monte Carlo analysis.

III. PRECISION OF MEASUREMENT:
BINARY INSPIRAL

In this section we apply the techniques described in §II to the problem of measuring the
characteristics of an inspiralling binary system in an interferometric gravitational radiation
detector. We determine the gravitational radiation from an evolving binary system in the
quadrupole approximation and evaluate the corresponding detector response. The amplitude
of the response is a function of the (unknown and unknowable) relative orientation of the
source and the detector, and we evaluate its mean square amplitude and a priori cumulative
probability distribution. We also discuss the validity of describing binary evolution using
the quadrupole approximation, arguing that while the result is certainly not good enough
for use in actual data analysis, it is sufficient for the purpose of exploring the precision
with which we will ultimately be able to characterize a binary system through gravitational
radiation observations in LIGO/VIRGO-like interferometers.

The general interferometer response to the gravitational radiation from an inspiralling
binary system is a sinusoid with slowly varying amplitude and frequency. Using the station-
ary phase approximation, we obtain an analytic expression for the Fourier transform of the
response. We find that the SNR $\rho_2$ and the covariance matrix $\mathcal{C}_{ij}$ can be expressed simply
in terms of several moments of $S_h^{-1}(f)$, the inverse of the interferometer noise PSD.

A. Parameterization of the radiation waveform

In order to express the response of a single interferometer to the gravitational radiation
from a binary system (or any source), we define two coordinate systems: the source co-
dordinate system and the radiation coordinate system. The binary system is most simply
described in the source coordinate system. The $e^S_x$-axis of this coordinate system is along the
binary system’s angular momentum. We choose the axes $e^S_x$ and $e^S_y$ of the source coordinate
system to make the expression of the radiation directed toward the interferometer simple:
the $e^S_x$ axis is chosen so that the unit vector $n_I$ in the direction of the interferometer is in
the $e^S_x \wedge e^S_y$ plane and in the positive $e^S_y$ direction (if the interferometer is along the polar
axis, then there is no preferred direction for the $e^S_x$ axis).

The radiation coordinate system has its $e^R_z$ axis in the direction $n_I$, and its $e^R_x$ and $e^R_y$
axes are projections of the $e^S_x$ and $e^S_y$ coordinate axes normal to $n_I$:

\[
\begin{align*}
    e^R_y &= e^S_y, \\
    e^R_x &= e^S_y \times n_I.
\end{align*}
\] (3.1a) (3.1b)

In the radiation coordinate system, the radiation propagating toward the interferometer is
described by
where

\[ h = h_+ e_+ + h_\times e_\times \]  

(3.2)

where

\[ e_+ = e_x^R \otimes e_x^R - e_y^R \otimes e_y^R \]  

(3.3a)

\[ e_\times = e_x^R \otimes e_y^R + e_y^R \otimes e_x^R. \]  

(3.3b)

### 1. The quadrupole waveform

In the quadrupole approximation,

\[ h_+ \equiv 2 \frac{\mathcal{M}}{d_L} \left(1 + \cos^2 i\right) (\pi \mathcal{M} f)^{2/3} \cos (\Phi + \Psi) \]  

(3.4a)

\[ h_\times \equiv 4 \frac{\mathcal{M}}{d_L} \cos i (\pi \mathcal{M} f)^{2/3} \sin (\Phi + \Psi) \]  

(3.4b)

where

\[ d_L \equiv \text{(Luminosity distance to binary)} \]  

(3.5a)

\[ \cos i \equiv n_I \cdot e_s^x, \]  

(3.5b)

\[ i \equiv \begin{pmatrix} \text{Inclination angle of orbital} \\ \text{angular momentum to line of} \\ \text{sight toward the interferometer.} \end{pmatrix}, \]  

(3.5c)

\[ \mathcal{M} \equiv \text{(Chirp mass)}, \]  

(3.5d)

\[ = (1 + z) \mu^{3/5} M^{2/5}, \]  

(3.5d)

\[ \Phi \equiv -2 \left(\frac{T - t}{5\mathcal{M}}\right)^{5/8}, \]  

(3.5e)

\[ f \equiv \frac{1}{2\pi} \frac{\partial \Phi}{\partial t} \]  

(3.5f)

\[ = \frac{1}{\pi \mathcal{M}} \left[\frac{5}{256 T - t}\right]^{3/8}. \]  

(3.5f)

\( \Psi \) is the phase of the binary system at \( t = T \), \( T \) is the Newtonian “moment of coalescence,” \( z \) is the cosmological redshift of the binary system, and \( \mathcal{M} \) and \( \mu \) are the binary system’s total and reduced mass \([340]\). The gravitational radiation frequency \( f \) is twice the systems orbital frequency.

\(^{4}\)Here and henceforth we adopt units where \( G = c = 1 \)
2. The interferometer response

The response of an interferometer to the gravitational radiation field is a linear combination of $h_+$ and $h_\times$:

$$m = F_+ h_+ + F_\times h_\times,$$

where the antenna patterns $F_+$ and $F_\times$ depend on the orientation of the interferometer with respect to the binary system [40]. We make no assumptions regarding the relative orientation of the interferometer and the binary; consequently, the general interferometer response is

$$m(t; \mathcal{A}, \mathcal{M}, \psi, T) \equiv \mathcal{A} \mathcal{M} (\pi f \mathcal{M})^{2/3} \cos (\Phi + \psi),$$

where $\psi$ is a constant (distinct from $\Psi$ in equations 3.4a and 3.4b), and $\Phi$ and $f$ are given above in equations 3.5c and 3.5d. We will return in §III E to discuss how $\mathcal{A}$ depends on the orientation angles through $F_+$ and $F_\times$.

3. Radiation reaction and the quadrupole approximation

LIGO/VIRGO-like interferometers are most sensitive to gravitational radiation with frequencies in the range 30–1000 Hz. This corresponds to binary orbital frequencies of 15–500 Hz. In this regime gravitational radiation reaction is the most important factor in determining the evolution of a binary system’s orbit [31,32]. In §II IA 1, where we describe the evolution of the binary systems orbit, only backreaction owing to the leading-order quadrupole radiation is taken into account [31]. This approximation neglects higher order effects (in both $v/c$ and $M/r$) that contribute to the gravitational radiation luminosity and, consequently, the evolution of $f$. This has serious ramifications for the construction of the model detector response [41].

The detector response to binary inspiral is a sinusoid of slowly varying amplitude and frequency. The determination of the characteristics of the binary system is equivalent to finding the “template” response that is most closely correlated to the detector response. If the phase of the template drifts from that of the signal by as little as $\pi$ radians over the course of the observations, then the correlation will be insignificant. Neutron star binary inspiral observations in LIGO/VIRGO-like interferometers will last for on order $2\pi \times 10^4$ radians in phase; consequently, the phase advance can be determined to better than 1 part in $10^4$. The errors we have made in our template $m(\mu)$ (eqn. 3.7) by neglecting the post-Newtonian contributions to the evolution of the binary system lead to phase differences significantly greater than $2\pi$ radians over $10^4$ cycles observed. Consequently, the waveform model used in actual data analysis must be more accurate than that given by the quadrupole approximation [42,41].

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5Cutler, Finn, Poisson, and Sussman [12] have shown that successive post-Newtonian approximations to the evolution and waveform converge very slowly upon the fully relativistic solution. Consequently, it may require an impractically high order post-Newtonian expansion to predict correctly the advance of the phase over the course of the LIGO/VIRGO observations.
Nevertheless, for the particular purpose of exploring our ability to detect and characterize binary systems by their gravitational radiation signature, we believe the quadrupole approximation waveform is a useful substitute for a more accurate waveform. The determination of the anticipated sensitivity of a LIGO/VIRGO-like interferometer to binary inspiral depends on the $\rho^2$ and $C_{ij}$, and we expect that the quadrupole approximation provides good lower bounds on these. The predominant observable effect of the inclusion of post-Newtonian corrections is to change the rate that the wave frequency $f$ advances, thus changing the elapsed phase of the wave over the period of the observation. The SNR $\rho^2$ depends approximately on the elapsed phase and the corrections, while large compared to $2\pi$, change this by only a small fraction of the total. Similarly, in the quadrupole approximation the rate at which $f$ advances depends exclusively on $M$ (cf. eqn. 3.5f); consequently, to the extent that the corrections to the quadrupole formula depend on characteristics of the binary other than $M$ (e.g., component masses and spins) these characteristics are observable and affect the precision with which $M$ can be measured. In this way we expect that the use of a more accurate waveform in our analysis will increase the estimated $\sigma_M$ but have little effect on our estimates of $\sigma_A$, $\sigma_\psi$, and $\sigma_T$ made using the quadrupole waveform and corresponding binary evolution.

B. The stationary phase approximation

In order to evaluate the SNR $\rho^2$ (eqn. 2.4) and the covariance matrix $C_{ij}$ (eqn. 2.7b) we must find the Fourier transform $\tilde{m}$ of $m$ (eqn. 3.7). We approximate $\tilde{m}$ using the method of stationary phase. Given a real function of the form

$$k(t) = A(t) \cos \hat{\Phi}(t),$$

where $\partial \hat{\Phi}/\partial t$ is a monotonically increasing function of $t$, the stationary phase approximation to the Fourier transform $\tilde{k}(f)$ is

$$\tilde{k}(f) = \int_{-\infty}^{\infty} dt \, k(t) e^{2\pi i ft}$$

$$\simeq \begin{cases} 
\frac{1}{2} A[T(f)] \left[ 2\pi / \partial^2 \hat{\Phi} / \partial t^2 [T(f)] \right]^{1/2} 
\times \exp \left[ i \left( 2\pi f T(f) - \hat{\Phi}(T(f)) + \pi/4 \right) \right] & \text{for } f > 0 \\
\tilde{k}^*(-f) & \text{for } f < 0,
\end{cases}$$

where

$$T \left[ \frac{1}{2\pi} \frac{\partial \hat{\Phi}}{\partial t} (t) \right] = t.$$
\[ \frac{\partial \ln A}{\partial t} \ll 1 \quad \text{and} \quad \frac{\partial^2 \hat{\Phi}}{(\partial \hat{\Phi} / \partial t)^2} \ll 1. \]  

(3.11a)  

(3.11b)

For the interferometer response \( m \) given in equation 3.7 these two relations are equivalent to the single condition

\[ \frac{T - t}{M} \gg \left( \frac{3\pi}{8} \right)^{8/5} \left( \frac{256}{5} \right)^{3/5} \simeq 14, \]  

(3.12)

or, alternatively,

\[ fM \ll \frac{1}{\pi} \left( \frac{5}{256 \pi} \right)^{3/5} \simeq \frac{1}{37}. \]  

(3.13)

For binary systems that will be observable by LIGO/VIRGO-like interferometers,

\[ fM = 6 \times 10^{-4} \frac{f}{100 \text{ Hz}} \frac{M}{1.2 M_\odot} \ll \frac{1}{37}; \]  

(3.14)

consequently, the stationary phase approximation is a good one for our purposes. We thus have

\[ \tilde{m}(f) \simeq \begin{cases} A M^2 \left[ \frac{5\pi}{384} \right]^{1/2} (\pi f M)^{-7/6} \\ \times \exp \left\{ i \left[ 2\pi f T + \frac{3}{128} (\pi f M)^{-5/3} - \psi + \frac{\pi}{4} \right] \right\} \text{ for } f > 0, \\ \tilde{m}^*(-f) \text{ for } f < 0. \]  

C. The signal-to-noise ratio

Now suppose that we have analyzed the output \( g(t) \) of an interferometer for the signal \( m \) and found that the likelihood function is maximized for the parameterization \( \{ \hat{A}, \hat{M}, \hat{\psi}, \hat{T} \} \). The SNR \( \rho^2 \) is then given by (cf. eqn. 2.4)

\[ \rho^2 = 2 \langle m(\hat{\mu}), m(\hat{\mu}) \rangle = \frac{5}{96\pi^{1/3}} \hat{A}^2 \hat{M}^{5/3} f_{7/3}, \]  

(3.16)

where, if we assume that we have access to \( g(t) \) for all \( t \),

\[ f_{7/3} = \int_0^\infty df \left[ f^{7/3} S_h(f) \right]^{-1}. \]  

(3.17)

In practice, of course, data analysis is limited to a finite length sample of the interferometer output. During this limited interval, the signal “frequency” \( f \) (eqn. 3.5f) of an inspiralling binary system ranges from \( f_l \) to \( f_h \). We assume that the minimum of \( S_h(f) \) occurs in this
interval and not too near the endpoints. Then, just as the slowly varying amplitude and frequency of \( m \) permitted us to estimate \( \tilde{m}(f) \) using the stationary phase approximation, so it allows us to approximate \( \rho^2 \) for a finite duration observation by replacing the lower and upper limits in the integral expression for \( f_{7/3} \) (eqn. 3.18) by \( f_l \) and \( f_h \). The lower bound \( f_l \) is determined by the duration of the data stream being analyzed while the upper bound \( f_h \) is determined by the coalescence of the binary components. We further assume that the \( f_{7/3} \) does not change significantly as \( f_h \to \infty \); thus, we have

\[
f_{7/3} = \int_{f_l}^{\infty} df \left[ f_{7/3} S_h(f) \right]^{-1}.
\]

(3.18)

We discuss our choice of low-frequency cut-off \( f_l \) in §IV A 6 and again in §V D.

**D. The covariance matrix**

Turn now to the calculation of the covariance matrix \( C_{ij} \) (cf. eqn. 2.7b). Instead of a parameterization in terms of \( A \) and \( M \), it is more convenient to introduce \( \eta \) and \( \zeta \) defined by

\[
\tilde{A}(1 + \eta) \equiv A
\]

(3.19a)

\[
\tilde{M}(1 + \zeta) \equiv M,
\]

(3.19b)

where \( \tilde{A} \) and \( \tilde{M} \) are the modes of the observed distribution of \( A \) and \( M \).

Given our expression for \( \tilde{m}(f) \), we can evaluate all of the elements of the symmetric matrix \( C_{ij}^{-1} \) in terms of the frequency moments \( \tilde{f}_{\beta} \) defined by

\[
\tilde{f}_{\beta} \equiv f_{7/3}^{-1} \int_{f_l}^{\infty} df \left[ f_{\beta} S_h(f) \right]^{-1}.
\]

(3.20)

To express \( C_{ij} \), only \( \tilde{f}_{\beta} \) for \( \beta \in \{17/3, 4, 3, 7/3, 1/3\} \) are needed. In terms of these moments,

\[
C_{ij}^{-1} = \rho^2 \left( \begin{array}{ccc}
1 & \frac{5}{6} \left[ 1 + \frac{9}{4096} \left( \frac{\tilde{f}_{17/3}}{\pi M} \right)^{10/3} \right] & 0 \\
\frac{25}{36} \left[ 1 + \frac{9}{4096} \left( \frac{\tilde{f}_{17/3}}{\pi M} \right)^{10/3} \right] & \frac{5}{128} \left( \frac{\tilde{f}_4}{\pi M} \right)^{5/3} & -\frac{5\pi}{64} \left( \frac{\tilde{f}_3}{\pi M} \right)^{5/3} \\
0 & -\frac{2\pi}{f_{4/3}} \left( \frac{\tilde{f}_{4/3}}{f_{1/3}} \right) & 1
\end{array} \right),
\]

(3.21)

where the indices are ordered \( \eta, \zeta, \psi, \) and \( T \). We have inverted equation 3.21 to find \( C_{ij} \) and so the variances and correlation coefficients describing the distributions of \( \eta, \zeta, \psi, \) and \( T \) (cf. eqns. 2.18 and 2.19). The variances are

\[
\sigma_{\eta}^2 = \frac{\sigma_A^2}{A^2}
\]

\[
= \left[ 1 + \frac{4096}{9\Delta} \left( \pi \tilde{M} \right)^{10/3} \left( \tilde{f}_{1/3} - \tilde{f}_{4/3} \right) \right] \rho^{-2}
\]

(3.22a)
\[ \sigma_\zeta^2 = \frac{\sigma_\mathcal{M}^2}{\mathcal{M}^2} = \frac{16384}{25\Delta \rho^2} (\mathcal{F}_{1/3} - \mathcal{F}_{4/3}^2) (\pi \hat{\mathcal{M}})^{10/3} \qquad (3.22b) \]

\[ \sigma_\psi^2 = \frac{\mathcal{F}_{17/3} \mathcal{F}_{1/3} - \mathcal{F}_3^2}{\Delta \rho^2} \qquad (3.22c) \]

\[ \sigma_T^2 = \frac{\mathcal{F}_{17/3} - \mathcal{F}_4^2}{4\pi^2 \Delta \rho^2} \qquad (3.22d) \]

and the correlation coefficients are

\[ r_{\eta \zeta} = r_{\mathcal{A} \mathcal{M}} = \frac{64 (\mathcal{F}_{1/3} - \mathcal{F}_1^2) (\pi \hat{\mathcal{M}})^{10/3}}{\left\{ \left[ 9\Delta + 4096 (\pi \hat{\mathcal{M}})^{10/3} (\mathcal{F}_{1/3} - \mathcal{F}_{4/3}^2) \right] (\mathcal{F}_{1/3} - \mathcal{F}_{4/3}^2) (\pi \hat{\mathcal{M}})^{10/3} \right\}^{1/2}}, \quad (3.23a) \]

\[ r_{\eta \psi} = r_{\mathcal{A} \psi} = \frac{64 (\mathcal{F}_{1/3} \mathcal{F}_{1/3} - \mathcal{F}_{4/3}^2) (\pi \hat{\mathcal{M}})^{5/3}}{\left\{ \left[ 9\Delta + 4096 (\pi \hat{\mathcal{M}})^{10/3} (\mathcal{F}_{1/3} - \mathcal{F}_{4/3}^2) \right] (\mathcal{F}_{17/3} - \mathcal{F}_{3}^2) \right\}^{1/2}}, \quad (3.23b) \]

\[ r_{\eta T} = r_{\mathcal{A} T} = \frac{64 (\mathcal{F}_4 \mathcal{F}_{1/3} - \mathcal{F}_{3}^2) (\pi \hat{\mathcal{M}})^{5/3}}{\left\{ \left[ 9\Delta + 4096 (\pi \hat{\mathcal{M}})^{10/3} (\mathcal{F}_{1/3} - \mathcal{F}_{4/3}^2) \right] (\mathcal{F}_{17/3} - \mathcal{F}_4^2) \right\}^{1/2}}, \quad (3.23c) \]

\[ r_{\zeta \psi} = r_{\mathcal{M} \psi} = \frac{(\mathcal{F}_{1/3} \mathcal{F}_{1/3} - \mathcal{F}_4^2)}{\left\{ (\mathcal{F}_{1/3} - \mathcal{F}_{4/3}^2) (\mathcal{F}_{17/3} - \mathcal{F}_3^2) \right\}^{1/2}}, \quad (3.23d) \]

\[ r_{\zeta T} = r_{\mathcal{M} T} = \frac{\mathcal{F}_3 - \mathcal{F}_4 \mathcal{F}_{1/3}}{\left\{ (\mathcal{F}_{1/3} - \mathcal{F}_{4/3}^2) (\mathcal{F}_{17/3} - \mathcal{F}_4^2) \right\}^{1/2}}, \quad (3.23e) \]

\[ r_{\psi T} = \frac{\mathcal{F}_{17/3} \mathcal{F}_{4/3} - \mathcal{F}_3 \mathcal{F}_{17/3}}{\left\{ (\mathcal{F}_{17/3} \mathcal{F}_{4/3} - \mathcal{F}_3^2) (\mathcal{F}_{17/3} - \mathcal{F}_4^2) \right\}^{1/2}}, \quad (3.23f) \]

where

\[ \Delta \equiv (\mathcal{F}_{1/3} - \mathcal{F}_{4/3}^2) \mathcal{F}_{17/3} - \mathcal{F}_{1/3} \mathcal{F}_{17/3} + (2\mathcal{F}_4 \mathcal{F}_{4/3} - \mathcal{F}_3) \mathcal{F}_3 > 0. \quad (3.24) \]

**E. Properties of \( \mathcal{A} \)**

Despite the fact that we cannot measure the orientation angles relating the interferometer to the source, we still need them in order to assess the interferometer’s sensitivity. Recalling that
\[ m = F_+ h_+ + F_\times h_\times, \quad (3.25) \]

we express \( F_+ \) and \( F_\times \) according to the following convention:

1. Assume that the interferometer arms are the same length and that they meet in right angles.

2. Define a right-handed coordinate system with one interferometer arm along the \( x \)-axis and the other along the \( y \)-axis. Denote the unit vector in the direction of the \( x \) arm by \( \mathbf{l} \) and the unit vector in the direction of the \( y \) arm by \( \mathbf{m} \).

3. Let the position of a source in the sky be given by the polar angle \( \theta \) and the azimuthal angle \( \phi \), and denote the unit vector pointing toward the source by \( \mathbf{n}_S \) (i.e., \(-\mathbf{n}_I\)).

4. The interferometer responds linearly to the radiation field \( \mathbf{h} \), so its response \( m \) can be represented by a tensor \( \mathbf{R} \) such that

\[ m = \mathbf{R} : \mathbf{h}. \quad (3.26) \]

For our interferometric detector

\[ \mathbf{R} \equiv \frac{1}{2} (\mathbf{l} \otimes \mathbf{l} - \mathbf{m} \otimes \mathbf{m}). \quad (3.27) \]

5. Assume that axis \( \mathbf{e}_x^R \) makes an angle \( \zeta \) with the axis \( \mathbf{l} \), i.e.,

\[ \mathbf{e}_x^R = \mathbf{l} \cos \zeta + \mathbf{m} \sin \zeta. \quad (3.28) \]

With these conventions, the antenna patterns are given by [10]

\[
F_+ \equiv \mathbf{R} : \mathbf{e}_+ \\
= \frac{1}{2} \cos 2\zeta \left( 1 + \cos^2 \theta \right) \cos 2\phi - \sin 2\zeta \cos \theta \sin 2\phi \quad (3.29a)
\]

\[
F_\times = \mathbf{R} : \mathbf{e}_\times \\
= \frac{1}{2} \sin 2\zeta \left( 1 + \cos^2 \theta \right) \cos 2\phi + \cos 2\zeta \cos \theta \sin 2\phi \quad (3.29b)
\]

and the amplitude \( \mathcal{A}^2 \) may be written

\[
\mathcal{A}^2 = \frac{4}{d_L^2} \left[ F_+^2 (1 + \cos^2 \theta)^2 + 4F_\times^2 \cos^2 \theta \right]. \quad (3.30)
\]

It is convenient to denote the angular dependence of \( \mathcal{A}^2 \) by \( \Theta^2 \):

\[
\Theta^2 = 4 \left[ F_+^2 (1 + \cos^2 \theta)^2 + 4F_\times^2 \cos^2 \theta \right]. \quad (3.31)
\]

The range of \( \Theta^2 \) is \( 0 \leq \Theta^2 \leq 16 \).
The SNR $\rho^2$ and covariance matrix $C_{ij}$ (eqns. 2.4 and 2.7b) both depend on $A^2$, which is in turn a function of the (unknown) relative orientation of the source and interferometer through $\Theta^2$. In order to evaluate the expected $\rho^2$ (or the expected $C_{ij}$) of a source at a given distance $d_L$ we need to know some properties of the probability distribution of $\Theta^2$.

Since $\Theta^2$ depends on the angles $\theta$, $\phi$, $i$, and $\zeta$ (cf. eqn. 3.31), the a priori distribution of $\Theta^2$ depends on the a priori distribution of these angles. These distributions are all known: in particular, $\cos \theta$ and $\cos i$ are uniformly distributed over the range $[-1, 1]$ and $\phi$ and $\zeta$ are uniformly distributed over the range $[0, 2\pi)$. Making use of the definitions of $F_+$ and $F_x$ (eqns. 3.29a and 3.29b), we find that the mean square of $\Theta$ is

$$\Theta^2 = \frac{64}{25}.$$  \hspace{1cm} (3.32)

The distribution of $\Theta^2$ is not symmetric, however: in fact, its mode is zero and larger values of $\Theta^2$ are much less likely to occur than smaller ones. We have determined the cumulative distribution function of $\Theta^2$ using a Monte Carlo analysis; we give the percentiles of the distribution in table I. In performing these calculations, we used Knuth’s portable random number generator [13] as implemented by Press et al. [14] (i.e., their RAN3). The results in table I are based on a sample of $10^7$ points in the $\{\cos \theta, \cos i, \phi, \zeta\}$ parameter space. The corresponding values of $\Theta^2$ were sorted into bins and the reported percentiles are the rounded bin centers.

Note from table I that significantly more than half (i.e., approximately 65%) of the inspiralling binary systems will have $\Theta^2$ less than $\Theta^2$. The skew of the distribution toward smaller $\Theta^2$ plays a significant role when we estimate the range of the interferometer (cf. §5B).

IV. APPLICATION TO LIGO

In §IV we found expressions for the SNR, the variance, and correlation coefficients corresponding to the detection of a signal characterized by $\hat{A}$, $\hat{M}$, $\hat{\psi}$, and $\hat{T}$. In this section we join those expressions with the design characteristics of LIGO/VIRGO-like interferometers to obtain estimates for the sensitivity of a realistic interferometric detector to inspiralling binaries.

A. Noise and the LIGO interferometers

The characteristic of the interferometers enter our analysis solely through the strain noise PSD $S_h(f)$. The dominant contributions to $S_h(f)$ for the interferometer configurations that will be used to search for inspiralling binaries are from seismic, thermal, and photon shot noise. In this subsection we summarize these contributions to the overall noise PSD that we use in our calculations.
1. Photon shot noise

At high frequencies $S_h(f)$ is dominated by photon shot noise. The shot noise depends on the interferometer arm lengths, laser power and wavelength, mirror reflectivities and configuration in a complicated fashion. In all of our calculations we have assumed that LIGO/VIRGO will be equipped with Fabry-Perot cavity interferometers, and we have used the analysis of Krolak, Lobo, and Meers [28, cf. their eqns. 2.11-22] to describe the photon shot noise. This analysis is general enough to encompass non-recycling, standard recycling, and dual recycling interferometers. Except in §IV B we always assume that the instrumentation makes use of standard recycling techniques. For standard recycling, the photon shot noise is given approximately by Thorne [10, eqn. 117c] or Krolak, Lobo, and Meers [28, eqn. 3.5]

$$S_{\text{shot}}^h(f) = \frac{\hbar \lambda A^2}{\eta I_0 L f_c} \left[ 1 + \left( \frac{f}{f_c} \right)^2 \right], \quad (4.1)$$

where $A^2$ describes the mirror losses, $I_0$ is the laser power, $\eta$ is the quantum efficiency of the photo-detector, $\lambda$ is the laser wavelength, $L$ is the length of interferometer arms, and $f_c$ is the recycling “knee” frequency.

The simplest way in which the observer can change the noise characteristics of the LIGO/VIRGO instrumentation is by changing the recycling knee frequency $f_c$. The general trend is that, as the recycling frequency increases the bandwidth increases while the sensitivity across the bandwidth decreases [10, fig. 9.13].

2. Thermal noise

At lower frequencies, off-resonance thermal excitations of the test mass suspensions and internal modes of the pendulum masses either dominate or provide important contributions to the noise. We approximate the suspension noise by focusing only on the pendulum mode (ignoring both torsional and violin modes). If the dissipative force in the pendulum suspension is due to friction, then the strain PSD of a single test mass $m$ with resonant frequency $f_0$ and quality factor $Q_0$ at temperature $T$ is given by

$$S_{\text{pend}}^h(f) = \frac{k_B T f_0}{2\pi^3 m Q_0 L^2 \left[ (f^2 - f_0^2)^2 + (f f_0/Q_0)^2 \right]} \quad (4.2)$$

(note that we use $T$ for both the temperature and the Newtonian “moment of coalescence;” nevertheless, the meaning of the symbol in any given context should be clear). Each arm of the interferometer has a pendulum degree of freedom at each end and the noise from each degree of freedom is independent; thus, the total noise PSD is a factor of four greater than this (note that Dhurandhar, Krolak and Lobo [22, eqn. 2.10] neglect this factor of four in their analysis and have several typographical errors in their formulae). The total thermal suspension noise PSD is given by

$$S_{\text{susp}}^h(f) = 4 S_{\text{pend}}^h(f). \quad (4.3)$$
The primary dissipative force acting on the pendulum may not be friction, however: it has been suggested [23] that the dissipation is due instead to a phase lag between the stress and the strain in the pendulum suspension. If this is the case, then the noise PSD is different than that given above. This is not an issue for the initial interferometers, but will be for the advanced ones [13]. The nature of the dissipation is far from settled, and in the absence of a consensus we have used the form given in equation 4.3.

Off-resonance thermal excitations of the vibrational modes of the test masses will also be a significant source of noise in the LIGO/VIRGO interferometers. Here we consider only the fundamental vibrational mode of each test mass. The contribution to the noise PSD has the same form as the thermal suspension noise $S_{\text{susp}}(f)$ (and is subject to the same controversy), only now the resonant frequency and oscillator quality that enter are those of the test masses:

$$S_{\text{int}}^h(f) = \frac{2k_B T f_{\text{int}}}{\pi^3 m Q_{\text{int}} L^2 \left[(f^2 - f_{\text{int}}^2)^2 + (f f_{\text{int}}/Q_{\text{int}})^2\right]}.$$  \hfill (4.4)

3. Seismic noise

Seismic noise will dominate $S_h(f)$ at low frequencies. Saulson [45] has surveyed the literature on the seismic displacement noise PSD $S_x(f)$ and finds that it is roughly proportional to $f^{-4}$ in the range $1/10$ Hz $\lesssim f \lesssim 10$ Hz. Consequently, if the LIGO/VIRGO test mass suspensions were coupled directly to the Earth, then

$$S_{h}^{\text{seismic}}(f) = \frac{S'_0 f^{-4}}{(f^2 - f_0^2)^2 + (f f_0/Q_0)^2}$$ \hfill (4.5)

where $f_0$ is the pendulum mode frequency, $Q_0$ is pendulum quality, and $S'_0$ is a proportionality constant with units of Hz$^7$. Note that at frequencies above the pendulum frequency $f_0$ the seismic strain noise is proportional to $f^{-8}$ while below $f_0$ is is proportional to $f^{-4}$.

In the actual LIGO/VIRGO interferometers, the pendulum suspensions will be isolated from the Earth by a mechanical circuit that is a series of several highly damped oscillators [46, 47]. Each oscillator in this series circuit will introduce four poles in the strain noise PSD near the pendulum frequency; consequently, the actual seismic noise contribution will be much steeper than $f^{-8}$ at frequencies greater than $f_0$ and much more complicated near the resonant frequencies of the mechanical circuit. It is proposed that seismic isolation in the initial interferometers be provided by a five stage circuit (where the final stage of isolation is the pendulum suspension itself) [10, §V 3 b and appendix D]: consequently, for frequencies much greater than $f_0$ the seismic strain noise PSD is expected to be proportional to $f^{-24}$. Nearer the resonant frequencies of the isolation circuit the dependence is quite complicated as the poles in the response function are not at zero frequency, but at complex frequencies with real parts near 1 Hz. The strain noise PSD below the resonant frequencies of the isolation circuit remains proportional to the displacement noise PSD $S_x(f)$.

In our calculations we use the following crude estimate for the seismic strain noise PSD:

$$S_{h}^{\text{seismic}}(f) = \frac{S_0 f^{-4}}{(f^2 - f_0^2)^{16}}.$$ \hfill (4.6)
The proportionality constant $S_0$ has units of Hz$^{23}$. This estimate scales correctly with frequency above and below $f_0$, though it fails near $f_0$. This failure is unimportant since (except in §\text{V.D}) we assume that $f_l > f_0$ (the choice of cut-off $f_l$ is discussed in §\text{V.A}).

The amplitude of the noise (as reflected by the proportionality constant $S_0$) depends on the detailed nature of the seismic isolation circuit and the properties of the seismic displacement noise at the interferometer site. The LIGO design goals for the initial and advanced interferometers are [46]

\begin{align}
S_h^{\text{seismic}}(40 \text{ Hz}) &= S_h^{\text{susp}}(40 \text{ Hz}) + S_h^{\text{int}}(40 \text{ Hz}) \quad \text{(initial interferometers)} \quad (4.7a) \\
S_h^{\text{seismic}}(10 \text{ Hz}) &= S_h^{\text{susp}}(10 \text{ Hz}) + S_h^{\text{int}}(10 \text{ Hz}) \quad \text{(advanced interferometers).} \quad (4.7b)
\end{align}

We fix $S_0$ by these relationships. Where we discuss the advanced LIGO detectors, we use the same condition on the seismic noise as for the advanced interferometers.

4. Quantum noise

In addition to the primary noise sources discussed above, we have also included a contribution whose origin is quantum mechanical and rooted in the Heisenberg uncertainty principle. When we observe a signal of frequency $f$ in an interferometer, we are measuring the periodic motion of the end-masses at that frequency. Since the motion is periodic, this is equivalent to a simultaneous measurement of the momentum and localization of the end masses, and the precision with which we can make this measurement is subject to the usual quantum mechanical limits. In our calculations, we use the form of the quantum noise given by Thorne [40, eqn. 121]:

\[ S_h^{\text{quant}}(f) = \frac{8\hbar}{m (2\pi f)^2 L^2}, \]  

(4.8)

where $m$ is the mass of the LIGO pendulum bobs.

5. Noise source summary

In table 2 we give the instrument characteristics we have assumed in our calculations. Two sets of values are given, corresponding to estimates for LIGO initial and advanced instrumentation. These estimates have been culled from the literature [42], the LIGO proposal [46], and personal communication with members of the LIGO project [43,48]. In terms of the noise sources discussed in the previous subsections, the noise PSD $S_h(f)$ we use in our calculations is

\[ S_h(f) = S_h^{\text{shot}}(f) + S_h^{\text{int}}(f) + S_h^{\text{susp}}(f) + S_h^{\text{seismic}}(f) + S_h^{\text{quant}}(f). \]  

(4.9)

As a companion to table 2 and as a graphical illustration of how all of the noise sources discussed above act in concert to determine an interferometer’s noise characteristics, we show our approximation to the anticipated $S_h(f)$ for both the initial (fig. 1) and advanced (fig. 2)
instrumentation. The contributions to $S_h(f)$ from each of the influences discussed above are shown as dashed lines and $S_h(f)$ is shown as a solid line. Both figures show interferometers configured to operate in standard recycling mode. In figure 1, corresponding to the initial interferometers, the recycling frequency $f_c$ is 300 Hz, while in figure 2 (corresponding to the advanced interferometer design) it is 100 Hz.

6. Choosing the low frequency cut-off $f_l$

The elements of the covariance matrix $C_{ij}$ depend on the moments $f_{7/3}$, $\mathcal{T}_{17/3}$, $\mathcal{T}_4$, $\mathcal{T}_3$, $\mathcal{T}_{4/3}$, and $\mathcal{T}_{1/3}$. In turn, these depend on $S_h(f)$ and the low frequency cut-off $f_l$ (see eqns. 3.18 and 3.20). Our calculations of these moments have assumed a low frequency cut-off of 10 Hz, corresponding to the last several minutes in the inspiral of a binary neutron star system. In table III we give the frequency moments $f_{7/3}$, $\mathcal{T}_{17/3}$, $\mathcal{T}_4$, $\mathcal{T}_3$, $\mathcal{T}_{4/3}$, and $\mathcal{T}_{1/3}$ for two cases of interest.

7. The LIGO detector

The two LIGO interferometers, though separated by several thousand miles, share nearly the same orientation in space: the planes defined by the detector arms are nearly parallel, and the arms themselves are nearly parallel. Consequently the network acts like a single interferometer of greater sensitivity than either of its components. If the noise in the two component interferometers of the LIGO detector is uncorrelated and described by $S_h^{(0)}(f)$, then the effective PSD of the more sensitive single interferometer is $S_h(f) = S_h^{(0)}(f)/2$. Consequently, the effective PSD for the LIGO detector in the limit that the interferometers share the same orientation is also given by figure 2, but with the scale reduced by a factor of $2^{-1/2}$. In making this approximation we are ignoring the differences in arrival time of the gravitational radiation signal at the two interferometers. In the following sections when we refer to the LIGO detector (as opposed to a LIGO/VIRGO-like interferometer) we are actually referring to a single interferometer whose noise PSD is 1/2 that of the advanced interferometer design.

B. Signal-to-noise ratio

As discussed in §II B, we decide whether or not a signal is present in the output of the detector by comparing the likelihood ratio $\Lambda$ to a pre-determined threshold. In this regard, the SNR $\rho^2$ is an acceptable surrogate for $\Lambda$; i.e., we can choose a threshold $\rho_0^2$ (which may be a function of $\hat{\mu}$) to compare with $\rho^2$. Then, if $\rho^2 \geq \rho_0^2$ we assert the presence of a signal while if $\rho^2 < \rho_0^2$ we conclude that the detector output is only noise. The choice of threshold is a delicate matter: on the one hand we want a high threshold to minimize the probability that we misidentify noise as signal; on the other hand, we want a low threshold to minimize the probability that we misidentify a real signal as noise. We will consider the proper choice of the threshold $\rho_0^2$ in a later paper; now, however, we assume only that the threshold depends weakly on the detection strategy and $\hat{\mu}$.
The amplitude SNR $\rho$ may be expressed

$$\rho = 8 \left( \frac{M}{1.2 M_\odot} \right)^{5/6} \left( \frac{\Theta}{\Theta_{50\%}} \right) F_{7/3}$$

$$\times \begin{cases} 
(17.0 \text{ Mpc}/d_L) & \text{initial interferometers} \\
(308. \text{ Mpc}/d_L) & \text{advanced interferometers} \\
(436. \text{ Mpc}/d_L) & \text{advanced LIGO detector}
\end{cases} \quad (4.10)$$

where

$$F_{7/3}(f_c, f_i) \equiv \left[ \frac{f_{7/3}(f_c, f_i)}{f_{7/3}(100 \text{ Hz}, 10 \text{ Hz})} \right]^{1/2}$$

$$\times \begin{cases} 
(f_{7/3}/5.331 \times 10^{42} \text{ Hz}^{-1/3})^{1/2} & \text{initial interferometers} \\
(f_{7/3}/1.747 \times 10^{45} \text{ Hz}^{-1/3})^{1/2} & \text{advanced interferometers} \\
(f_{7/3}/3.493 \times 10^{45} \text{ Hz}^{-1/3})^{1/2} & \text{advanced LIGO detector}
\end{cases} \quad (4.11a)$$

In figure 3, we show $F_{7/3}$ for both the initial and advanced LIGO instrumentation. Two curves are shown: one for the initial interferometers and one for the advanced interferometers. Each curve assumes a low-frequency cutoff $f_i$ of 10 Hz (corresponding to the last several minutes of binary neutron star inspiral). For the advanced instrumentation, the detection strategy that maximizes $\rho$ has $f_c = 100$ Hz (where $F_{7/3} = 1$), while for the initial instrumentation $f_c = 300$ Hz (where $F_{7/3} = 1.3$). These correspond to the choice of $f_c$ in figures 1 and 2 showing the detailed breakdown of $S_h(f)$ for the initial and advanced interferometers.

Now consider the case of resonant dual recycling [19,21,24]. The photon shot noise in an interferometer operating in a resonant dual recycling mode is proportional to (cf. [28] eqn. 3.7 but note that their approximate expression has several errors; see also [19,24])

$$S_{\text{dual}}(f) \propto \left[ 1 + \left( \frac{f - f_n}{\Delta f} \right)^2 \right], \quad (4.12)$$

where $\Delta f$ and $f_n$ depend on the reflectivities of certain mirrors in the experimental apparatus. This shot noise PSD is large except in a narrow band about $f_n$ where it is very small. The bandwidth $\Delta f$ and the central frequency $f_n$ of this “notch” can be adjusted, and the size of $S_{\text{dual}}$ in and out of the notch will vary depending on the $f$ and $\Delta f$. In comparison, an interferometer operating in standard recycling mode has a nearly constant shot noise PSD for frequencies below the knee frequency $f_c$, with the noise PSD increasing as $f^2$ for frequencies greater than $f_c$ (cf. eqn. 4.1 and figs. 1 and 2). For $|f - f_n| \lesssim \Delta f$, dual recycling cuts a notch in $S_{\text{dual}}$. Elsewhere, $S_{\text{shot}}$ is lower than that for dual recycling (assuming $f_0 \simeq f_c$). On the basis of numerical investigations of the interferometer response and the waveform of inspiralling binary systems, Krolak, Lobo, and Meers [28] suggested that dual recycling with $f_n = 100$ Hz and $\Delta f \simeq 6$ Hz is superior to standard recycling for the observation of binary systems. Their analysis assumed that $S_h(f)$ is infinite below 100 Hz and that only photon shot noise is important above 100 Hz: in particular, they did not consider the noise owing to the thermal excitations of the test mass vibrational modes (cf. §IIVA2). When $S_{\text{int}}^n(f)$
is included in the analysis, then the advantage of dual recycling in this regime is lost: the notch is “filled in” by the thermal noise almost to the level of standard recycling photon shot noise (cf. their fig. 5 and our figs. 1 or 2), and everywhere else the noise is much greater than is the case for an interferometer operated in standard recycling mode.

Dual recycling may still be useful at much higher frequencies where the photon shot noise is a standard recycling configuration is much larger than the thermal noise (e.g., 1.5 KHz). Observations at such high frequencies may prove useful for detecting the actual coalescence event [12].

V. ASTROPHYSICAL IMPLICATIONS

A. Source rate

Chernoff and Finn [16] have shown that the observed differential rate \(d\hat{N}/dM dA\) of inspiralling binary systems depends on the cosmological model; consequently, it can be used to determine the Hubble constant \(H\), the deceleration parameter \(q\), and otherwise distinguish between cosmologies. Here we are interested in the total rate of observed binary inspiral as an estimate of the sensitivity of an interferometer, and in this subsection we estimate that rate ignoring cosmological effects. We refer the reader interested in a rate calculation consistent with an expanding universe and taking into account evolution of the binary population and distribution of \(M\) in binaries to Chernoff and Finn [14].

Assume that the rate density (number per unit co-moving cosmological volume per unit time) of inspiralling neutron-star binary systems is a constant \(\dot{N}\) and that the variation in neutron star masses is small so that \(M\) is approximately equal to 1.4 \(M_\odot\) (corresponding to two 1.4 \(M_\odot\) neutron stars). The expected total rate \(\dot{N}\) of systems whose SNR \(\rho^2\) is greater than \(\rho_0^2\) is

\[
\dot{N} = \int_0^\infty dr \, 4\pi \dot{N} r^2 P \left[ \rho^2(r) > \rho_0^2 \right]
\]

\[
= \int_0^\infty dr \, 4\pi \dot{N} r^2 P \left( \Theta^2 > \frac{r^2}{r_0^2} \right)
\]

\[
= 4\pi \dot{N} r_0^3 \int_0^\infty dx \, x^2 P \left( \Theta^2 > x^2 \right)
\]

\[
\equiv \frac{4\pi}{3} \dot{N} R^3,
\]

(5.1)

where

\[
P \left( \Theta^2 > x^2 \right) \equiv \text{The probability that } \Theta^2 \text{ is greater than } x^2 \] (5.2a)

\[
r_0 \equiv \left( \frac{5M^{5/3}f_{7/3}}{96\pi^{4/3}\rho_0^2} \right)^{1/2}
\]

\[
= \left( \frac{M}{1.2M_\odot} \right)^{5/6} \left( \frac{8}{\rho_0} \right)^{7/3}
\]

(5.2b)
\[ R \equiv r_0 \left[ 3 \int_0^\infty dx x^2 P (\Theta^2 > x^2) \right]^{1/3} \]  \tag{5.2b}

[recall that we have ignored cosmological effects (cf. Chernoff and Finn [16]) in eqn. 5.1a]. Using the cumulative distribution function for \( \Theta^2 \) (cf. § III E and tbl. I), we find that
\[ \int_0^\infty dx x^2 P (\Theta^2 > x^2) = 1.84; \]  \tag{5.3}

\[ R = \left( \frac{\mathcal{M}}{1.2 M_\odot} \right)^{5/6} \left( \frac{8}{\rho_0} \right) F_{7/3} \]
\[ \times \begin{cases} 
13.0 \text{ Mpc} & \text{initial interferometer} \\
236. \text{ Mpc} & \text{advanced interferometer} \\
334. \text{ Mpc} & \text{advanced LIGO detector,} 
\end{cases} \]  \tag{5.4}

Phinney [4] has given estimates for the number density of sources per unit time (\( \dot{N} \)) based on observational and theoretical arguments. These estimates range from an ultra-conservative \( 6 \times 10^{-10} \text{ Mpc}^{-3}\text{yr}^{-1} \), to a conservative \( 8 \times 10^{-8} \text{ Mpc}^{-3}\text{yr}^{-1} \), to an upper limit of \( 6 \times 10^{-5} \text{ Mpc}^{-3}\text{yr}^{-1} \). They are based on the statistics of local populations of binary pulsars and type Ib supernovae, and the large range reflects both the small size of the local sample, uncertainties in our understanding in the evolution of binary systems, and uncertainties in the selection effects at work in determining the fraction of the local systems we have direct knowledge of. If we take the typical threshold \( \rho_0 \) to be 8, then we find that expected rate of detections of inspiralling binary systems is
\[ \dot{N} \simeq \frac{\dot{\mathcal{N}}}{8 \times 10^{-8} \text{ Mpc}^{-3}\text{yr}^{-1}} \left( \frac{\mathcal{M}}{1.2 M_\odot} \right)^{5/2} \left( \frac{8}{\rho_0} \right)^3 F_{7/3}^3 \]
\[ \times \begin{cases} 
4.1 \times 10^{-3} \text{ yr}^{-1} & \text{initial interferometer} \\
24. \text{ yr}^{-1} & \text{advanced interferometer} \\
69. \text{ yr}^{-1} & \text{advanced LIGO detector.} 
\end{cases} \]  \tag{5.5}

As commented earlier, to maximize the rate at which binaries are detected we need to choose \( f_c \) in order to maximize \( F_{7/3} \).

For a binary system consisting of a 10 M\(_\odot\) black hole and a neutron star, \( \mathcal{M} \simeq 3 \), and for a binary system consisting of two 10 M\(_\odot\) black holes, \( \mathcal{M} \simeq 9 \) (recall that we are neglecting cosmological effects). Consequently, for these neutron-star/black-hole (black-hole/black-hole) binaries \( R_{90\%} \simeq 2 \text{ Gpc} \) (5 Gpc) for the advanced LIGO detector. The situation for determining the rate at which such systems will be detected is a bit more complicated. Phinney argues that black-hole/black-hole and black-hole/neutron-star binaries form at rates comparable to the neutron-star/neutron-star merger rate; however, the fraction which merge depends on the model dependent details that vary greatly [4], so no reliable estimate of the coalescence rate is available for use with eqn. 5.5.

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B. Range

An important measure of the sensitivity of a LIGO/VIRGO-like interferometer is its "range," i.e., the distance to which sources can be observed. The definition of the range is subtle. Not all inspiralling binaries within, e.g., a distance \( R \) will be identified as such: for some, \( \Theta \) will be less than \( R/r_0 \), the corresponding SNR \( \rho^2 \) will be less than the threshold \( \rho_0^2 \), and the signal will be dismissed as noise. Similarly, not all inspiralling binaries outside a distance \( R \) will fail to be identified by the interferometer: for some \( \Theta \) will be greater than \( R/r_0 \), the SNR \( \rho^2 \) will be greater than \( \rho_0^2 \), and the signal will be identified as coming from a binary system. Since the range is a slippery concept, we define a range function \( R_\gamma \) such that a fraction \( \gamma \) of the observable sources fall within the distance \( R_\gamma \):

\[
\gamma = \frac{\int_0^{R_\gamma/r_0} dx \frac{x^2 P(\Theta^2 > x^2)}{P(\Theta^2 > x^2)}}{\int_0^\infty dx \frac{x^2 P(\Theta^2 > x^2)}{P(\Theta^2 > x^2)}}. \tag{5.6}
\]

The quantity

\[
\frac{\int_0^z dx \frac{x^2 P(\Theta^2 > x^2)}{P(\Theta^2 > x^2)}}{\int_0^\infty dx \frac{x^2 P(\Theta^2 > x^2)}{P(\Theta^2 > x^2)}} \tag{5.7}
\]

is tabulated in the third column of table I, and we show \( \gamma \) as a function of \( R_\gamma/R \) in figure 4. Note that

\[
R_{90\%} = \left( \frac{\mathcal{M}}{1.2 \, M_\odot} \right)^{5/6} \left( \frac{8}{\rho_0} \right) F_{7/3} \times \begin{cases} 37.2 \text{ Mpc} & \text{initial interferometer} \\ 673. \text{ Mpc} & \text{advanced interferometer} \\ 952. \text{ Mpc} & \text{advanced LIGO detector,} \end{cases}
\tag{5.8}
\]

i.e., for the advanced LIGO detector approximately 7 sources per year will be observed whose distance is greater than 950, Mpc. Like the rate, the range is sensitive to the detection strategy so that if we wish to maximize the sensitivity of the interferometer to either we need to choose a detection strategy that maximizes \( F_{7/3} \).

C. Standard deviation and correlation coefficients

First consider the measurement of \( A \). For all \( \mathcal{M} \) and \( f_c \) relevant for both the initial and advanced LIGO/VIRGO-like interferometers, the fractional standard deviation \( \sigma_A \) (cf. 3.22a) of the waveform amplitude \( A \) is \( \rho^{-1} \); consequently, the maximum fractional one-sigma uncertainty in the determination of \( A \) is

\[
\frac{\sigma_A}{A} = 0.125 \frac{8}{\rho_0} \tag{5.9}
\]

for both the initial and advanced interferometers. Additionally, the correlation coefficients \( r_{Ai} \) all have magnitude less than \( 10^{-4} \), indicating that \( A \) is statistically independent of \( \mathcal{M} \),
ψ and T (i.e., the random errors in measurements of $A$ owing to detector noise are not correlated with the corresponding errors in the measurement of $M$, $\psi$, or $T$).

Now turn to the measurement of $M$. Before discussing the exact results obtained with equation 3.22b, we give a heuristic derivation of the precision with which $M$ can be determined. Recall that the phase $\Phi$ of the gravitational wave signal is given by

$$\Phi = -2 \left( \frac{\bar{T} - t}{5\bar{M}} \right)^{5/8}. \quad (5.10)$$

The observation encompasses approximately the last ten minutes in the life of the binary system, during which time the phase advances by

$$\Delta \Phi = 7.4 \times 10^4 \left( \frac{\Delta t}{10\text{ m}} \right) \frac{1.2 M_\odot}{\bar{M}} \frac{5}{8} \text{ rad}. \quad (5.11)$$

The argument of the exponential in the odds ratio (eqn. 2.3d) is

$$2 \langle n, m(\mu) \rangle + 2 \langle m(\bar{\mu}), m(\mu) \rangle - \langle m(\mu), m(\mu) \rangle. \quad (5.12)$$

The contribution owing to the term $2 \langle m(\bar{\mu}), m(\mu) \rangle$ is much greater than that owing to the noise; consequently, to a good approximation the odds ratio will be maximized where this quantity is maximized. Ignoring the frequency dependence of $S_h(f)$ the term $\langle m(\bar{\mu}), m(\mu) \rangle$ is the correlation between two sinusoidal functions of the phase, and is large only as long as the advance in phase of $m(\mu)$ is within approximately $\pi$ radians of the advance in phase of $m(\bar{\mu})$ over the course of the observation. Since $\Delta \Phi$ depends only on $M$, we have $\pi \gtrsim |\Delta \bar{\Phi} - \Delta \Phi|$ or

$$\frac{\delta M}{\bar{M}} \lesssim \frac{4\pi}{5} \left( \frac{\bar{M}}{\Delta t} \right)^{5/8} \lesssim 10^{-4} \left( \frac{\bar{M}}{1.2 M_\odot} \frac{10\text{ m}}{\Delta t} \right)^{5/8}, \quad (5.13)$$

where $\delta M$ is $\bar{M} - M$.

Return now to consider the exact results. Equation 3.22b gives the fractional standard deviation $\sigma_M/\bar{M}$ in terms of the frequency moments $f_\beta$ and $\rho$:

$$\frac{\sigma_M}{\bar{M}} = \left( \frac{\bar{M}}{1.2 M_\odot} \right)^{5/3} \left( \frac{\beta}{\rho} \right) \Sigma_M$$

$$\times \begin{cases} 2.08 \times 10^{-4} & \text{initial interferometer}, \\ 2.20 \times 10^{-5} & \text{advanced interferometer} \end{cases} \quad (5.14)$$

where

$$\Sigma_M = \left[ \left( \frac{f_{1/3}^2 - f_{4/3}^2}{\Delta} \right) / \left( \frac{f_{1/3}^2 - f_{4/3}^2}{\Delta} \right) \right]_{f_c=100\text{ Hz}, f_l=10\text{ Hz}}^{1/2}. \quad (5.15)$$

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Given a threshold $\rho_0$ such that $\rho \geq \rho_0$ for all observed sources, equations 5.14 and 5.15 give the maximum fractional standard deviation in the measurement $\mathcal{M}$ for any binary system observed with LIGO/VIRGO-like interferometers — a phenomenal precision. In interpreting eqn. 5.14, note that $\sigma_{\mathcal{M}}/\hat{\mathcal{M}}$ is inversely proportional to $\rho$, and recall that the SNR $\rho$ of a binary system observed in an interferometer of the advanced design is approximately 26 times greater than the SNR of the same binary observed in a detector of the initial design (cf. eqn. 4.10). The results for the advanced LIGO detectors are identical to those for the advanced interferometers, except that the amplitude SNR $\rho$ for a binary observed in the advanced detector is $2^{1/2}$ greater than that for the same binary observed in a single advanced interferometer.

In figure 5 we show $\Sigma_{\mathcal{M}}$ for both the initial and advanced interferometers. For the advanced interferometer the total variation of $\Sigma_{\mathcal{M}}$ is approximately 20% as $f_c$ ranges from 50 Hz to 1 KHz, while for the initial interferometer the variation is approximately 15%. The optimum recycling frequency for measurement of $\mathcal{M}$ is that which minimizes $\Sigma_{\mathcal{M}}$, and we see that this is very different than the choice which maximizes the number of binaries observed (cf. § IV B and fig. 3): in fact, the optimal choice of $f_c$ for the detection of binaries (in either the initial or advanced interferometers) is close to the worst possible choice of $f_c$ for the precise measurement of $\mathcal{M}$.

As we have pointed out, with observations in a single gravitational wave interferometer the location of the source on the sky cannot be determined. If, as has been suggested, some coalescing binaries result in $\gamma$-ray bursts [49, 5], then burst observations may be used to localize the binary system in the sky. The identification between a gravitational wave burst from orbital decay (which takes place before actual coalescence of the binary components) and a $\gamma$-ray burst (which takes place at the time of coalescence) depends on the accuracy with which we can measure the time of arrival of the $\gamma$-ray burst and the "moment of coalescence" $T$: in all events, $T$ will be within seconds of the actual moment of neutron star disruption and the emission of the $\gamma$-ray burst. Consequently, we need to know $T$, the rate of detected binary coalescence, and the rate of $\gamma$-ray bursts (the latter both assumed to be Poisson distributed in time) in order to evaluate the probability that a correlation in time between a $\gamma$-ray burst and a gravitational wave burst is coincidental. The accuracy with which we can determine $T$ is given by $\sigma_T$ (cf. 3.224):

$$\sigma_T = \left(\frac{8}{\rho}\right) \Sigma_T \times \begin{cases} 1.54 \times 10^{-4} \text{s} & \text{initial interferometer,} \\ 3.00 \times 10^{-4} \text{s} & \text{advanced interferometer,} \end{cases}$$

(5.16)

where

$$\Sigma_T = \left[ \frac{T_{17/3} - T_{4}^2}{\Delta} / \left( \frac{T_{17/3} - T_{4}^2}{\Delta} \right) \right]_{f_c=100 \text{ Hz}, f_l=10 \text{ Hz}}^{1/2}.$$  

(5.17)

The results for the advanced LIGO detector are the same as those for a single advanced interferometer. The factor $\Sigma_T$ varies by approximately a factor of 2.5 over the range 50 Hz < $f_c$ < 1000 Hz, and is shown (for both the initial and advanced interferometers) in figure 6.
Again, the optimal interferometer configuration for precision measurements of $T$ is very different than that for detection of inspiralling binaries.

The parameter $\psi$ depends on the orientation of the source and the detector and the phase of the binary systems orbit at $t = 0$. For completeness, we also give the precision with which $\psi$ can be measured:

$$
\sigma_{\psi} = \left( \frac{8}{\rho} \right) \Sigma_{\psi} \times \begin{cases} 
0.257 \text{ rads} & \text{initial interferometer,} \\
0.338 \text{ rads} & \text{advanced interferometer,}
\end{cases}
$$

where

$$
\Sigma_{\psi} \equiv \left[ \left( \frac{f_{17/3} - \mathcal{F}_{4}^2}{\Delta} \right) / \left( \frac{f_{17/3} - \mathcal{F}_{4}^2}{\Delta} \right) \right]_{f_c=100 \text{ Hz}, f_l=10 \text{ Hz}}^{1/2}.
$$

The results for an advanced detector are the same as those for a single advanced interferometer.

The correlation coefficients $r_{M\psi}, r_{MT},$ and $r_{\psi T}$ are nearly independent of $f_c$ for both the initial and advanced LIGO-like interferometers. As mentioned above, the statistical error in $\mathcal{A}$ is essentially uncorrelated with that in $\mathcal{M}, \psi,$ or $T$ (i.e., the correlation coefficients $r_{\mathcal{A}i}$ are for all $\lesssim 10^{-4}$). Figure 7 shows the remaining correlations coefficients $r_{M\psi}, r_{MT},$ and $r_{\psi T}$ for the initial and advanced interferometers.

**D. The low frequency cut-off**

In order to evaluate the covariance matrix we needed to compute the six frequency moments $f_{7/3}, \mathcal{F}_{17/3}, \mathcal{F}_{4}, \mathcal{F}_{3}, \mathcal{F}_{4/3}$, and $\mathcal{F}_{1/3}$. The evaluation of all of these is straightforward; however, the calculation of $\mathcal{F}_{17/3}$ deserves special attention: at frequencies below the pendulum frequency of the LIGO masses the seismic noise PSD is proportional to $f^{-4}$ (cf. eqn. 4.5); consequently, $\mathcal{F}_{17/3}$ diverges as $f_l$ approaches 0 (cf. eqn. 3.20).

For any particular application we never encounter the divergence: there is always a low frequency cut-off in the integral corresponding to the finite period of the observation. Even if we had access through an interferometer to the entire life history of a binary system, our model for its evolution is relevant during only a small part of its lifetime: for example, we have assumed that the orbit is circular for all times (when in fact gravitational radiation may be responsible for circularizing it), that the evolution of the orbit is due exclusively to the gravitational forces acting between the two components, and that the two bodies are bound in a binary into the infinite past. Similarly, our model of the detector noise PSD $S_h(f)$ is not necessarily valid at very low frequencies. Nevertheless, the divergence of $\mathcal{F}_{17/3}$ tells us something interesting about the observation of a binary system in gravitational radiation and it is worthwhile to spend a few moments understanding its origin. So, for the purpose of understanding this divergence we assume that we know $S_h(f)$ as $f$ tends to 0, that our
model for the waveform from a binary is correct throughout its life history, and that the lifetime of a binary extends into the infinite past.

Turn first to the related example of a strictly monochromatic signal of frequency $f_0$:

$$m(t) = A \cos 2\pi f_0 t$$

for all $t$. The noise PSD of the detector is given by $S_h(f)$. If we observe the signal for a finite period of time $\tau$, the SNR $\rho^2$ is

$$\rho^2 = \frac{\tau A^2}{S_h(f_0)}. \quad (5.21)$$

No matter how small $A^2$ is compared to the power in the noise, the signal can always be discerned given a long enough observation time. The situation with binary inspiral is similar: consider the transformation of the time coordinate

$$t' \equiv -\frac{M}{(T - t) 5/8} \quad (5.22)$$

In terms of $t'$, the signal can be expressed

$$h(t) = \frac{AM}{4} \left( -\frac{M}{t'} \right)^{5/32} \cos(\Phi + \varphi) \quad (5.23a)$$

$$\Phi(t') = 2\pi f't' \quad (5.23b)$$

$$f' = \frac{1}{2\pi M}. \quad (5.23c)$$

Thus, the signal from an inspiralling binary is very much like that from a monochromatic source of radiation, save that

1. The signal amplitude tends to zero as the stretched time $t'$ tends to $-\infty$;
2. The detector noise amplitude tends to $\infty$ as the stretched time $t'$ tends to $-\infty$; and
3. The signal ends at $t' = 0$.

As a result, as long as the ratio of the signal amplitude to the noise PSD does not decrease too rapidly with decreasing frequency (the precise rate determined by the rate at which the frequency changes with time), then $\rho^2$ for a inspiralling binary system should increase without bound as the observation period extends into the infinite past. This is the role that the moment $f_{7/3}$ plays in equation 2.4 for $\rho^2$: if the detector noise PSD increases as or less rapidly than $f^{-7/3}$ as $f \to 0$, then $f_{7/3}$ diverges as the observation period is extended into the infinite past (i.e., as the cut-off frequency $f_l$ tends to zero) and the SNR increases without bound. In the case of LIGO, the PSD owing to seismic noise increases as $f^{-4}$ at frequencies below the suspension pendulum frequency, so that even an infinite observation period leads to a finite SNR.

Like the SNR, the frequency $f_0$ of a truly monochromatic signal (i.e., eqn. 5.20) can be determined to arbitrary precision given a sufficiently long observation period. By analogy,
this is equivalent to the determination of the mass parameter $M$ of a inspiralling binary system (cf. eqn. 5.23d). Consequently, we expect that as long as the ratio of the signal amplitude to the noise PSD does not increase too rapidly, the variance in the $M$ decreases to zero as the observation period extends into the infinite past. Too rapidly, in this case, is $f^{-17/3}$. Thus, even though the signal power in a given bandwidth may be much lower than the noise power in the same bandwidth, the information present can still play an important role in determining the precision with which the parameterization of the signal can be determined.

Again, we emphasize that these conclusions refer only to the idealized case of a circular binary system of two point masses evolving exclusively owing to the emission of quadrupole gravitational radiation. The relevance of these conclusions is that the limit $f_l \to 0$ (i.e., $f_{17/3} \to \infty$), which may seem far from the reality of observation, is in fact very close to that which can be attained in LIGO operating in a regime where all our approximations are valid.

In the limit $f_l \to 0$ ($f_{17/3} \to \infty$), the variance $\sigma^2_\zeta$ and the correlation coefficients $r_{i\zeta}$ vanish, corresponding to the determination of $M$ to infinite precision. The remaining variances are (cf. eqns. 3.22a, 3.22c, 3.22d)

\begin{align}
\infty \sigma^2_\eta &= \rho^{-2} \\
\infty \sigma^2_\psi &= \frac{f_{1/3}}{f_{1/3} - f_{4/3}} \frac{1}{\rho^2} \\
\infty \sigma^2_T &= \left[4\pi^2 \rho^2 \left(f_{1/3} - f_{4/3}^2\right)\right]^{-1},
\end{align}

and the remaining correlation coefficients are (cf. eqns. 3.23b, 3.23c, 3.23f)

\begin{align}
\infty r_{\eta \psi} &= 0 \\
\infty r_{\eta T} &= 0 \\
\infty r_{\psi T} &= \frac{f_{4/3}}{f_{1/3}^{1/2}}.
\end{align}

In this limit, the moments $f_{7/3}$, $f_{4/3}$, and $f_{1/3}$ describe completely the precision with which $A$, $\psi$, and $T$ can be measured. For LIGO/VIRGO-like interferometers, these moments change negligibly when we pass from $f_l = 10$ Hz to the limit of $f_l = 0$ Hz [recall that we are assuming $S_h(f) \propto f^{-4}$ at frequencies below the resonant frequencies of the seismic isolation circuit]; consequently, in observing more than the last several minutes of binary inspiral the SNR of the observed signal is unchanged, and the variances and correlation coefficients are independent of the details of the ultralow frequency behavior of the interferometers.

By analogy with $\Sigma_\psi$ and $\Sigma_T$ we define $\infty \Sigma_\psi$ and $\infty \Sigma_T$:

\begin{align}
\infty \sigma_\psi &= 8 \left(\frac{\rho}{8}\right) \infty \Sigma_\psi \begin{cases} 
0.232 \text{ rads} & \text{initial interferometer,} \\
0.190 \text{ rads} & \text{advanced interferometer,}
\end{cases} \\
\infty \sigma_T &= 8 \left(\frac{\rho}{8}\right) \infty \Sigma_T \begin{cases} 
1.32 \times 10^{-4} \text{ s} & \text{initial interferometer,} \\
2.71 \times 10^{-4} \text{ s} & \text{advanced interferometer,}
\end{cases}
\end{align}
\[ \infty \Sigma \psi = \left[ \frac{\left( f_{1/3} - f_{2/3}^2 \right)}{\left( f_{1/3} - f_{2/3}^2 \right)} \right] \left( f_{1/3} - f_{2/3}^2 \right) \]  
(5.26c)

\[ \infty \Sigma_T = \left\{ \left[ \frac{\left( f_{1/3} - f_{2/3}^2 \right)}{\left( f_{1/3} - f_{2/3}^2 \right)} \right] \right\}^{1/2} \]  
(5.26d)

The factor \( \infty \Sigma_T \) is shown together with \( \Sigma_T \) in figure 6 for both the initial and advanced interferometers. Over the range \( 50 \text{ Hz} < f_c < 1 \text{ KHz} \) the differences between \( \infty \Sigma_i \) and \( \Sigma_i \) are small.

Since the SNR is unchanged as the observation period expands from the last several minutes of binary insiripal to include the entire lifetime of the binary, observations over more than the last several minutes of the lifetime of a binary system will have an insignificant effect on the number of binaries observed (cf. eqn. 5.3). Comparing the expressions given above for \( \infty \sigma_i \) with those for \( \sigma_i \) (cf. eqns. 3.22a–3.22d) shows that increasing the observation period increases the precision with which \( T \) can be determined by approximately 10% and the precision with which \( \psi \) can be measured a factor of two.

VI. CONCLUSIONS

Inspiralling binary systems of compact objects are regarded as the most certain observable source of gravitational radiation for the Laser Interferometer Gravitational-wave Observatory (LIGO). As a start toward understanding the capabilities of the LIGO instruments in observations of inspiralling binary systems, we have investigated the sensitivity of a single interferometer of the LIGO type to the gravitational radiation from inspiralling binary systems in the quadrupole approximation.

Observation of binary inspiral in a single LIGO/VIRGO-like interferometer can, in principle, determine a characteristic mass \( \mathcal{M} \), signal amplitude \( \mathcal{A} \), time \( T \), and phase \( \psi \). The mass \( \mathcal{M} \) is a function only of the masses of the system’s components and its cosmological redshift. The amplitude \( \mathcal{A} \) is inversely proportional to its luminosity distance and depends also on a function of four angles describing the relative orientation of the binary and the interferometer. The time \( T \) is related to the moment of binary coalescence. Finally, \( \psi \) is related to the phase of the binary system at a fixed moment of time and is also a function of the relative orientation angles.

The probability that the detector response is consistent with the presence of a signal from an inspiralling binary system is related to the signal-to-noise ratio (SNR) \( \rho \) that characterizes the observation. In practice, a threshold \( \rho_0 \) is chosen and we assert that a signal is present in the detector output only if \( \rho \geq \rho_0 \). We characterize our uncertainty in the parameters \( \hat{\mu} = \{ \hat{\mathcal{A}}, \mathcal{M}, \hat{\psi}, \hat{T} \} \) that describe the detected binary system by defining volumes \( V(P) \) in parameter space such that \( \hat{\mu} \in V(P) \) with probability \( P \).

When \( \rho^2 \) is large, the probability density from which \( V(P) \) is constructed is a multivariate Gaussian. Consequently, the determination of \( V(P) \) is equivalent to the determination of the several variance and correlation coefficients that describe the Gaussian. These coefficients
in turn describe the statistical uncertainty in the determination of $A$, $M$, $\psi$, and $T$, and the correlation in the errors in each.

For observations of binary systems in LIGO/VIRGO-like interferometers, the expected SNR, variance, and correlations coefficients may be expressed in terms of the mode of the probability distribution $P(\mu)$ and several moments of the noise PSD of the interferometer. We have used a detailed model of the PSD for both the initial and advanced LIGO interferometers configured for standard recycling, and have evaluated the moments of the PSD, the expected SNR, variances, and correlation coefficients as functions of the recycling knee frequency.

The two interferometers of the LIGO detector share nearly the same orientation. Consequently, they will act similarly to a single, more sensitive interferometer. In addition to providing results for a single interferometer of the LIGO/VIRGO type (either initial or advanced), we also express our results for the LIGO two-interferometer network in the limit that the interferometers share exactly the same orientation.

From the expected SNR and an estimate for the cosmological rate density of inspiralling binary systems, we have calculated the rate of observed binary inspiral events as a function of the SNR threshold. We find that for the advanced LIGO detector a conservative estimate of the rate of observed binary neutron star inspiral events is $69\,\text{yr}^{-1}$, of which 7 per year will be from binaries at distances greater than 950 Mpc. This is important for observational cosmology, since the differential rate (i.e., $d\dot{N}/dA dM$) depends on the Hubble constant and other cosmological parameters.

For observed binary systems, the fractional standard deviation in the characteristic waveform amplitude is equal to $1/\rho$: if the threshold $\rho$ is 8, then the fractional one-sigma uncertainty in the measured amplitude will be less than 12.5% for sources observed in either LIGO or LIGO-like interferometers. The chirp mass can be measured to phenomenal precision: again, if the threshold $\rho$ is 8, then the fractional one-sigma uncertainty in $M$ will be less than $2.2 \times 10^{-5}$ for binary neutron star systems observed in the advanced LIGO detector.

We have also calculated the precision with which $T$ and $\psi$ can be determined.

The optimum detector configuration for the observation of binary inspiral depends sensitively on the goal of the observation. For example, if the object is to maximize the rate of observed binary systems without constraining the uncertainties in $A$, $M$, $T$ and $\psi$, then one detector configuration is clearly favored. On the other hand, if the object is to be able to characterize as precisely as possible one of the observables (e.g., $M$), while allowing that some otherwise observable sources may be missed entirely, then another detector configuration is preferred. We have given a concrete formulation to the question of optimum interferometer configuration and answered it in the context of our model for the interferometer noise PSD.

The quadrupole approximation is useful for our LIGO/VIRGO appraisals; however, the neglect of post-Newtonian contributions (including spin-orbit and spin-spin interactions) to the gravitational radiation luminosity and waveform is a weakness of our estimates and should be remedied in a more detailed appraisal of interferometer sensitivity.

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6Preliminary Monte Carlo investigations by Cutler suggest that the inclusion of some of the
these interactions will increase the information that can be extracted from gravitational radiation observations of binaries over that described here. The formalism that we have developed — where the SNR, variances, and correlation coefficients are all expressed in terms of moments of the interferometer noise PSD — should prove valuable in that regard: it is readily extended to encompass an arbitrarily more sophisticated gravitational radiation waveform that is richer in information regarding the source than the one we have studied here.

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terms neglected in our analysis increase the fractional one-sigma uncertainty in $M$ by no more than a factor of ten over our estimate, and have a much smaller effect on $A$, $T$, and $\psi$.  

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FIG. 1. The noise power spectral density (PSD) \( S_h(f) \) for the (anticipated) initial LIGO interferometers configured for standard recycling with a knee frequency of 300 Hz. The solid line shows the total PSD, while the dashed lines show the important physical limits and environmental influences that contribute to the total. For more detail, see Sec. IV A and table I.

FIG. 2. The noise power spectral density (PSD) \( S_h(f) \) for the (anticipated) advanced LIGO interferometers configured for standard recycling with a knee frequency of 100 Hz. The solid line shows the total PSD, while the dashed lines show the important physical limits and environmental influences that contribute to the total. In the limit that the two LIGO interferometers have identical orientations and we ignore the information available owing to gravitational wave burst arrival time differences, the (advanced design) LIGO detector noise PSD \( S_h(f) \) is \( \frac{1}{2} \) the value shown here. For more detail, see Sec. IV A and table I.

FIG. 3. The sensitivity of a LIGO-like interferometer to the gravitational radiation from a coalescing binary system depends on the detailed characteristics of the interferometer through several moments of the inverse of the its power spectral density (PSD) \( S_h(f) \). In particular, the signal-to-noise ratio (SNR) \( \rho^2 \) depends on a moment of \( S_h^{-1}(f) \). Here we show how this moment (normalized to its value at a recycling frequency of 100 Hz) varies with the choice of interferometer recycling frequency. To maximize the rate at which sources are detected this quantity should be maximized. For more details see IV B.

FIG. 4. We define the range function \( R_\gamma \) of a LIGO-like interferometer as the distance \( d_L \) within which a fraction \( \gamma \) of the observable sources are expected to lie. We also define a characteristic distance \( R_\gamma \), such that the total rate of observable sources is \( 4\pi R_\gamma^3 \dot{N} / 3 \), where \( \dot{N} \) is the rate density of sources (which we assume to be uniform). A conservative estimate of \( R_\gamma \) for an advanced LIGO-like interferometer is 420 Mpc. Here we show \( \gamma \) as a function of \( R_\gamma / R_\gamma \). For further discussion see Sec. V B.

FIG. 5. The fractional standard deviation \( \sigma_M/ \Hat{M} \) of the measured mass \( M \) depends on the distance to the source, the relative orientation of the source and the interferometer, and a factor \( \Sigma_M(f_c) \) that depends on the interferometer configuration (i.e., the recycling frequency \( f_c \); cf. eqn. 5.13 and Sec. V C). Here we show \( \Sigma_M \) as a function of \( f_c \) for initial and advanced LIGO-like interferometers. In order to maximize the precision with which \( M \) can be determined, the recycling frequency should be chosen to minimize \( \Sigma_M \). The corresponding recycling frequency differs from that which should be chosen to maximize the rate of sources detected (cf. fig. 3). For more details, see Sec. V C.
FIG. 6. The characteristic time $T$ (related to the moment when coalescence occurs) can be determined from pre-coalescence observations. The precision with which it can be determined depends on (among other things) a factor $\Sigma_T$ (defined in Sec. V C) that encapsulates all dependence of the precision on the duration of the observation and the characteristics of the detector noise. The duration of the observation will typically be several minutes, during which time the radiation frequency will sweep from 10 Hz to approximately 1 KHz, and $\Sigma_T$ assumes that the observation period is limited in this way. Here we show $\Sigma_T$ as a function of the detector recycling frequency for both initial and advanced LIGO-like interferometers. An interferometer optimized to measure $T$ as precisely as possible should minimize $\Sigma_T$. Also shown are factors $\infty\Sigma_T$ for initial and advanced interferometers. These are defined identically to $\Sigma_T$ except that they assume an observation period that extends over the entire life of an idealized binary system evolving only owing to the emission of gravitational radiation. The small differences between $\infty\Sigma_T$ and $\Sigma_T$ show that the characteristics of the interferometer do not change significantly as the observation period is lengthened beyond the last several minutes of binary inspiral. For more details, see Sec. V D.

FIG. 7. The correlation coefficients describe correlations among the statistical errors in the measurements of the parameters describing an inspiralling binary system. There is no correlation between errors in the measurement of the waveform characteristic amplitude $A$ and any of the other measurable parameters. The remaining correlation coefficients are shown here, for both initial and advanced LIGO-like interferometers, as a function of the interferometer recycling frequency. For more details, see Sec. V C.
TABLE I. The amplitude of the gravitational radiation waveform observed in a single detector depends on the relative orientation between the source and the detector through the function $\Theta^2$ (cf. eqn. [3.31]). The orientation angles are unknown and cannot be ascertained by observation; however, their a priori distribution is known and consequently the a priori distribution of the signal amplitude for binaries at a fixed distance from the detector is also known. In this table we give the cumulative probability distribution of $\Theta^2$, and also a function of $P(\Theta^2 > x^2)$ that arises when we evaluate the number of sources within a given distance whose signal amplitudes exceed a given threshold. For more details, see Sec. III E, V A, and V B.

| $P(\Theta^2 > x^2)$ | $x^2$ | $\int_0^x dz z^2 P(\Theta^2 > z^2)$ |
|----------------------|-------|---------------------------------|
| 90.0%                | 0.240 | 2.00%                           |
| 80.0%                | 0.542 | 6.32%                           |
| 75.0%                | 0.707 | 9.06%                           |
| 70.0%                | 0.878 | 12.06%                          |
| 60.0%                | 1.250 | 18.82%                          |
| 50.0%                | 1.709 | 27.11%                          |
| 40.0%                | 2.283 | 36.98%                          |
| 30.0%                | 3.020 | 48.29%                          |
| 25.0%                | 3.485 | 54.54%                          |
| 20.0%                | 4.063 | 61.37%                          |
| 10.0%                | 6.144 | 79.48%                          |
| 9.0%                 | 6.471 | 81.59%                          |
| 8.0%                 | 6.832 | 83.75%                          |
| 7.0%                 | 7.239 | 85.94%                          |
| 6.0%                 | 7.701 | 88.18%                          |
| 5.0%                 | 8.233 | 90.42%                          |
| 4.0%                 | 8.857 | 92.64%                          |
| 3.0%                 | 9.614 | 94.82%                          |
| 2.0%                 | 10.589| 96.91%                          |
| 1.0%                 | 11.985| 98.77%                          |
| 0.5%                 | 13.054| 99.52%                          |
| 0.4%                 | 13.350| 99.65%                          |
| 0.3%                 | 13.682| 99.77%                          |
| 0.2%                 | 14.091| 99.87%                          |
| 0.1%                 | 14.284| 99.95%                          |
TABLE II. The sensitivity of LIGO depends in large measure on the details of the instrumentation, and this is expected to evolve over the lifetime of the physical plant. We consider the two extremes of detector technology that have been cited by the LIGO team in their reports [1,2]: the instrumentation that is expected to be available when the facilities first come online (initial interferometers), and that expected to be available much later (advanced interferometers).

|                    | Initial interferometers | Advanced interferometers |
|--------------------|-------------------------|--------------------------|
| Temperature (T)    | 300 K                   | 300 K                    |
| Pendulum frequency ($f_0$) | 1 Hz                  | 1 Hz                     |
| Suspension Quality ($Q_0$) | $10^7$               | $10^9$                   |
| End mass (m)       | 10 Kg                   | 1000 Kg                  |
| End mass fundamental mode ($f_{int}$) | 23 KHz                | 5 KHz                    |
| End mass quality ($Q_{int}$) | $10^5$               | $10^5$                   |
| Effective laser power ($I_0\eta$) | 5 W                  | 60 W                     |
| Laser wavelength ($\lambda$) | 5139 Å                | 5139 Å                   |
| Mirror losses ($A^2$) | $5 \times 10^{-5}$     | $2 \times 10^{-5}$       |

TABLE III. The signal-to-noise ratio, the variances, and the correlation coefficients all depend on the characteristics of the interferometer through the moments of its inverse noise power spectral density (cf. Sec. [VA]). Here we give those moments for the initial and advanced LIGO instrumentation for the two cases where the standard recycling “knee” frequency $f_c$ is 100 Hz and 500 Hz. In both cases, the low-frequency cut-off (determined by the duration of the observation) is 10 Hz.

| $f_c$ [Hz] | Initial Interferometers | Advanced Interferometers |
|-----------|-------------------------|--------------------------|
|           | 100                     | 500                      |
| $f_{7/3}$ [Hz$^{-1/3}$] | 5.331×10$^{42}$         | 6.520×10$^{42}$          |
| $f_{17/3}$ [Hz$^{-5/3}$] | 9.540×10$^{-8}$         | 7.704×10$^{-8}$          |
| $f_4$ [Hz$^{-2/3}$] | 2.059×10$^{-4}$         | 1.721×10$^{-4}$          |
| $f_3$ [Hz] | 3.056×10$^{-2}$         | 2.775×10$^{-2}$          |
| $f_{4/3}$ [Hz$^{1/3}$] | 2.346×10$^{2}$          | 2.939×10$^{2}$           |
| $f_{1/3}$ [Hz$^{2/3}$] | 7.765×10$^4$            | 1.394×10$^5$             |
|           | 100                     | 500                      |
| $f_{7/3}$ [Hz$^{-1/3}$] | 1.747×10$^{45}$         | 1.353×10$^{45}$          |
| $f_{17/3}$ [Hz$^{-5/3}$] | 6.758×10$^{-6}$         | 8.267×10$^{-6}$          |
| $f_4$ [Hz$^{-2/3}$] | 1.562×10$^{-3}$         | 1.720×10$^{-3}$          |
| $f_3$ [Hz] | 6.615×10$^{-2}$         | 6.741×10$^{-2}$          |
| $f_{4/3}$ [Hz$^{1/3}$] | 8.423×10$^4$            | 9.536×10$^4$             |
| $f_{1/3}$ [Hz$^{2/3}$] | 1.248×10$^4$            | 2.282×10$^4$             |

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Noise Contributions

- □ = Shot noise
- ○ = Thermal noise
- △ = Seismic noise
- + = Quantum noise
$F_{\gamma/3}$ vs. $f_c$ (Hz)

- $\square$ = Initial interferometers
- $\circ$ = Advanced interferometers
\[ \sum_{x} \] = Initial interferometers

\[ \circ \] = Advanced interferometers

\( f_c \) (Hz)
\[ r_{\mu\phi} \] (initial interferometers)
\[ r'_{\mu\phi} \] (initial interferometers)
\[ r_{\mu T}\phi \] (initial interferometers)
\[ r'_{\mu T}\phi \] (advanced interferometers)
\[ r_{\mu T}\phi \] (advanced interferometers)
\[ r'_{\phi T} \] (advanced interferometers)