Carbon fibres are a significant volume fraction of modern structural airframes. Embedded into polymer matrices, they provide significant strength and stiffness gains by unit weight compared with competing structural materials. Here we use the Raman G peak to assess the response of carbon fibres to the application of strain, with reference to the response of graphene itself. Our data highlight the predominance of the in-plane graphene properties in all graphitic structures examined. A universal master plot relating the G peak strain sensitivity to tensile modulus of all types of carbon fibres, as well as graphene, is presented. We derive a universal value of—average—phonon shift rate with axial stress of around \(-5\omega_0^{-1}\) (cm\(^{-1}\)MPa\(^{-1}\)), where \(\omega_0\) is the G peak position at zero stress for both graphene and carbon fibre with annular morphology. The use of this for stress measurements in a variety of applications is discussed.
Graphene is a one-atom-thick planar sheet of sp²-bonded carbon atoms stacked in a two-dimensional honeycomb lattice, and is the basic building block for carbon allotropes of any dimensionality, such as graphite, nanotubes and fullerenes. It can also be considered as an infinitely large aromatic molecule. Graphitic materials, including carbon fibres (CF) or multivall nanotubes (MWNNTs), are also governed in terms of their physicomechanical properties, by the anisotropy between the strong intramolecular covalent forces and the weak intermolecular (van der Waals) forces. In CF, the basic structural units (BSUs) are thought to be graphite crystals, with a lateral extension \( L \sim 2-6 \text{ nm} \) and a stacking height \( L_z \sim 1-10 \text{ nm} \) depending on the final graphitization temperature. However, this view has been challenged on the basis of the fact that the interplanar distance differs considerably from graphite, as has also been confirmed recently by high-brilliance synchrotron X-ray measurements. Single-wall nanotubes (SWNT) can also be thought of as folded graphene, whereas the MWTN morphology has both graphitic tubular (longitudinal direction) and graphitic (through thickness direction) characteristics. Therefore, the detailed knowledge of the mechanical behaviour of the basic graphitic structural unit should yield important information on the properties not only of graphitic structures, such as graphite itself and CFs, but also of tubular structures, at least in the longitudinal direction.

The entire fuselage of some modern civil aircrafts is constructed from CF composites and, in particular, polyacrylonitrile (PAN)-based CF reinforced plastic. The PAN fibre precursor, produced after wet or dry spinning of the bulk polymer, has a high degree of molecular orientation and gives greater CF yield. For this type of fibres, the prevalent notion is that the mechanical properties are governed by the structure and properties of the BSU. However, there is no agreement as to what exactly the BSU consists of. Structures comprising elongated ribbons, or crumpled and folded sheets have been proposed. Another route to CF production starts from petroleum or coal tar pitch, which is thermally treated above \( 350^\circ \text{C} \) to convert it to the well-known mesophase pitch. With reference to the development of spectroscopic stress sensors, a substantial amount of research focused on the stress-induced alterations in the Raman spectra of a range of materials, both organic and inorganic. In graphitic materials, such as CF, the variation in phonon frequency per unit of strain can provide information on the efficiency of stress transfer to individual bonds. When macroscopic stress is applied to a polycrystalline CF, the resulting deformation emanates not only from bond stretching or contraction, but also from other mechanisms, such as crystal lattice rotation and slippage, which do not change the phonon frequency. Indeed, the higher the CF crystalline order (hence the modulus), the higher is the bond deformation, and hence, the higher is the Raman shift per unit strain. The Raman G peak corresponds to the in-plane, doubly degenerate \( E_{2g} \) phonon at the graphene Brillouin zone centre and is present in all carbonaceous materials. It is thus the ideal phonon to monitor the in-plane properties of complex graphitic structures, such as CF (see Methods for more details on Raman scattering). Previous Raman work on CFs revealed that the G peak shifts linearly with macroscopic applied uniaxial stress for various CF families of quite diverse elastic moduli. Indeed, it was reported that the rate of change of G peak position with applied strain, \( \partial \omega / \partial \varepsilon \), is linearly related to the CF modulus, \( E \), \( \partial \omega / \partial \varepsilon \sim E \). Given that, by definition, \( E \) is the proportionality constant between axial stress \( \sigma \) and strain \( \varepsilon \), it follows that \( \partial \omega / \partial \sigma \) should take a constant value for specific CF families (that is, derived from an identical precursor and processing conditions). Hence, these fibres can be considered as equal stress bodies (that is, springs in series) regardless of their respective modulus. The question now is why \( \partial \omega / \partial \sigma \) varies when changes are brought about to the fibre precursor and/or to the degree of fibre drawing within the carbonization or stabilization regimes. Note that in most experiments, \( \partial \omega / \partial \sigma \) is estimated by performing direct \( \partial \omega / \partial \varepsilon \) measurements and then dividing the resulting \( \partial \omega / \partial \varepsilon \) by the CF tensile modulus. Therefore, any underestimation of the effective optical ‘skin’ modulus of 13–15 nm in depth will affect the results as it would effectively boost the value of \( \partial \omega / \partial \sigma \). However, this cannot be the only source of discrepancy as direct mechanical measurements on a PAN fibre yielded a higher value of \( \partial \omega / \partial \sigma \) than that reported by Huang and Young for fibres with approximately the same \( E \).

Axial stress applied on graphene lifts the degeneracy of the \( E_{2g} \) phonons, splitting the G peak into two distinct \( G^+ \) and \( G^- \) components. The Raman intensities of the two peaks are then given by:

\[
I(G^+) \propto \sin^2 (\theta_{\text{in}} + \theta_{\text{out}} + 3\varphi), \quad I(G^-) \propto \cos^2 (\theta_{\text{in}} + \theta_{\text{out}} + 3\varphi)
\]

where \( \varphi \) is the angle between the strain axis and the \( x \) axis, chosen to be perpendicular to the \( C-C \) bond (Fig. 1), \( \theta_{\text{in}} \) and \( \theta_{\text{out}} \) are the polarization angles of the incident and scattered light relative to the strain axis, respectively, for normal incidence of light on the graphene plane. A question that needs addressing is whether the graphene orientation in CF also leads to observable phonon splitting and stress-strain-induced shifts. This is important in view of the possible use of CF as stress/strain sensors in commercial composites, in tandem to their primary role as structural reinforcements. As the average orientation of the CF-BSU with respect to the incident light is fixed during the carbonization and drawing procedures, it follows that polarized Raman measurements could in principle determine the relative contribution of each G peak component. Indeed, it was long known that in CF, the full width at half maximum of the G peak (FWHM(G)) increases with tensile strain, in contrast to the expectation that this should decrease following the decrease of crystallite misorientation. Hence, it is reasonable to assume that the observed broadening of the G peak in CF is an indication of phonon splitting during mechanical loading.

We embarked on an experimental campaign to examine the response of the basic graphene unit present in all graphitic structures to an applied tensile stress/strain field. Two PAN-based and two pitch-derived CFs of various elastic moduli have been selected for polarized Raman measurements and the results are compared to a variety of PAN-based and pitch-based fibres reported in the literature. By plotting the G peak strain sensitivity as a function of modulus for all types of CF, we have found that all data points lie within the boundaries defined by graphene itself. A universal value of—average—phonon shift rate with axial stress of around \(-5\alpha_{\text{loc}}\) (cm\(^{-1}\) MPa\(^{-1}\)) is thus derived.

**Results**

**Strain/stress sensitivity of the G peak of graphene.** Graphene monolayers were subjected to tensile loading by means of a cantilever beam (CB) apparatus. Representative Raman spectra in the G peak spectral region of graphene at 0 and 1% of strain are plotted in Figure 2a and the fitted positions of the G subbands (Pos(G)) as a function of strain are shown in Figure 2b. Care was taken to measure flakes with zero residual strain to avoid non-linear effects. The initial stress condition of the flake depends on fabrication (mechanical cleavage) and/or on surrounding film shrinkage due to curing. The straight lines are least-squares-fits of four sets of measurements, giving an average \( \alpha_{\text{loc}} \sim 0.3 \times 10^{-17} \text{ cm}^{-1} \text{ MPa}^{-1} \). For each material, the polynomial fitting allows the determination of an effective Young’s modulus, which is given by \( E \sim \frac{1}{\alpha_{\text{loc}}} \). To derive the phonon shifts with respect to axial strain for unsupported graphene, and therefore eliminate any effect from the substrate Poisson’s ratio, we first estimate the Gruneisen and the shear deformation potential parameters for the supported case, then revert to free-standing
Figure 1 | Schematic representation of scattering geometry for onion skin and radial CFs. A simplified concept of the structure of (a) onion skin and (b) radial CFs is shown. $\vec{E}$ depicts the strain axis, whereas $e_\varphi$ and $e_\psi$ indicate the directions of incident and scattered light, respectively. $\theta_{in}$ and $\theta_{out}$ are the angles between the strain axis and the plane of the electric-field vector of incident and scattered light. The $x$ axis is taken perpendicular to the C–C bond. $\varphi$ is the angle between the strain axis and the $x$ axis (that is, orientation of the graphene lattice with respect to strain). $L_{l1}$ is the CF crystallite thickness (that is, number of graphene layers). $L_{y1}$ and $L_{z1}$ represent crystallite width in directions parallel and perpendicular to the fiber axis. $e_i$ is plotted in both directions, which were used in the experiments ($\theta_{in}=0^\circ$ and $90^\circ$). In (b), $e_p$ designates the $e$ vector projected onto the graphene plane, which is rotated around a vertical axis at an arbitrary angle. $e_p$ is plotted only at $\theta_{out}=0^\circ$.

Such procedure yields $\partial \omega_{G^+}/\partial \epsilon = -17.5 \times 10^2 \text{ cm}^{-1}$ and $\partial \omega_{G^-}/\partial \epsilon = -36.0 \times 10^3 \text{ cm}^{-1}$, which is comparable to $-18.6 \times 10^3 \text{ cm}^{-1}$ and $-36.4 \times 10^3 \text{ cm}^{-1}$, respectively, obtained earlier.

Figure 2 | Graphene under strain. (a) $G^*$ peak Raman spectra of graphene at 0% (grey) and 1% (black) strain at 785 nm excitation. The solid curves are Lorentzian fits. The insets show the eigenvectors of the $G^*$ and $G$ modes. (b) $G^*$ (empty rectangles) and $G$ (full rectangles) peak positions for graphene embedded in polymer beam in tension. The data points are averages from four different locations on the flake, with the error bars denoting the s.d. Labelled lines represent values calculated for suspended graphene (see text). The inset shows an optical microphotograph of the measured flake. Scale bar, 10 μm. The arrows indicate the strain orientation.

The secular equation for the $E_{2g}$ mode of graphene under strain is:

$$\left| \begin{array}{cc} AE_{xx} + BE_{xy} - \lambda & (A-B)E_{xy} \\ (A-B)E_{xy} & BE_{xx} + AE_{yy} - \lambda \end{array} \right| = 0$$

(2)

where $\lambda = (\omega^* - \omega_x) = 2\omega_0 \Delta \omega$ is the difference between the squared strain-dependent frequency, $\omega_0$, and the squared frequency in the absence of strain, $\omega_0$.

Solving equation (2) analytically, and ignoring terms higher than $\epsilon^4$, the $G^+$ and $G^-$ shifts in uniaxially strained graphene in the $x$ direction ($\epsilon_{xx} = \epsilon, \epsilon_{yy} = -\nu \epsilon, \epsilon_{xy} = 0$) are:

$$\frac{\partial \omega_{G^+}}{\partial \epsilon} = \frac{B - VA}{2\omega_0}$$

(3)

$$\frac{\partial \omega_{G^-}}{\partial \epsilon} = \frac{A - VB}{2\omega_0}$$

(4)

or

$$A = \frac{2\omega_0 \left( \frac{\partial \omega_{G^+}}{\partial \epsilon} + \nu \frac{\partial \omega_{G^-}}{\partial \epsilon} \right)}{1 - \nu^2}$$

(5)
When a polycrystalline (turbostratic) CF is subjected to uniaxial tension, both the type of polymer beams (CB or four-point-bending) employed and both experimental tests is excellent and does not depend on the type of polymer beams (CB or four-point-bending) employed to load the monolayer.

\[ B = 2 \omega_0 \frac{\partial \omega_{G^+}}{\partial \sigma} + VA \]  

Inserting the estimated values of \( \frac{\partial \omega_{G^+}}{\partial \sigma} \) and \( \frac{\partial \omega_{G^-}}{\partial \sigma} \) for free graphene in equations (5) and (6), we get \( A = -1.23 \times 10^7 \text{cm}^{-2} \) and \( B = -7.16 \times 10^7 \text{cm}^{-2} \) in agreement with previously obtained values.\(^{25,28}\)

We now consider the stress sensitivity. For uniaxial stress, the resulting strains are given by \( \varepsilon_{xx} = \varepsilon = S_{11} \sigma \) and \( \varepsilon_{yy} = -\nu \varepsilon = S_{12} \sigma \) or equivalently:

\[ \varepsilon = S_{11} \sigma \]  

\[ \nu = -\frac{S_{12}}{S_{11}} \varepsilon \]  

where \( S_{11} \) and \( S_{12} \) are the compliances. Following the analysis mentioned earlier, we obtain:

\[ \frac{\partial \omega_{G^+}}{\partial \sigma} = \frac{(AS_{12} + BS_{11})}{2\omega_0} \]  

\[ \frac{\partial \omega_{G^-}}{\partial \sigma} = \frac{(AS_{12} + BS_{11})}{2\omega_0} \]  

To derive the \( G \) peak stress sensitivity, we need the graphene compliance constants, \( C_{ij} \). When

\[ S_{11} = \frac{C_{11}C_{33} - C_{13}^2}{(C_{11} - C_{12})(C_{33}(C_{11} + C_{12}) - 2C_{13}^2)} = 1 \text{TPa}^{-1} \]

\[ S_{12} = -V/S_{11} = -0.12 \text{TPa}^{-1} \]  

inserting these \( S_{11}, S_{12} \) in equations (9) and (10), we obtain \( \partial \omega_{G^+}/\partial \sigma = -1.6 \text{cm}^{-1} \text{GPa}^{-1} \) and \( \partial \omega_{G^-}/\partial \sigma = -3.5 \text{cm}^{-1} \text{GPa}^{-1} \). The corresponding values from experiments on an embedded flake using the CB apparatus\(^{31,32}\) are approximately \(-1.7 \) and \(-3.6 \text{cm}^{-1} \text{GPa}^{-1} \), whereas those derived earlier on a bare flake using the four-point-bending test\(^{34,35}\) were \(-1.9 \) and \(-3.6 \text{cm}^{-1} \text{GPa}^{-1} \). The agreement between the above analysis and both experimental tests is excellent and does not depend on the type of polymer beams (CB or four-point-bending) employed to load the monolayer.

**Figure 3** | CFs under strain. Raman \( G \) band region of (a) HM fibre at 0 (G+D’, grey) and 1% (G+G’+D’, black) strain and (b) of PS5 fibre at 0 (G+D’, grey) and 0.8% (G+D’, black) strain. The lines are Lorentzian fits to the experimental spectra, in which the dashed lines stand for individual bands. The red solid line in a represents a Lorentzian fit to the HM fibre at 1% strain using only a single G peak.

**Figure 4** | Position of \( G \) band under strain in CFs. The position of the Raman \( G \) band of (a) HM and (b) PS5-CFs. The squares represent \( \text{Pos}(G) \) fitted as a single Lorentzian for \( \theta_{in} = 0^\circ \) and \( \theta_{out} = 0^\circ \). In a, the diamonds correspond to the \( G^+ \) (full) and \( G^D \) (empty) positions for \( \theta_{in} = 0^\circ \). The straight lines represent the least-squares fits to the experimental data (solid lines for \( \theta_{in} = 0^\circ \) and dashed line for \( \theta_{in} = 90^\circ \)—in the latter case the data points are not shown for the sake of clarity). The insets show the FWHM of the respective G peaks when fitted as a single Lorentzian. The error bars represent the s.d. from all measurements on the given strain level.

**Strain/stress sensitivity of the \( G \) peak of CFs.** When a polycrystalline (turbostratic) CF is subjected to uniaxial tension, both \( G^- \) and \( G^+ \) should be seen. Only for specific combinations of incident polarization/analysis directions, one of the two components can be suppressed.\(^{33}\) In almost all CF literature (see, for example, refs 4,5,18), the incident polarization is along the fibre (\( \theta_{in} = 0^\circ \)) no analyser is used and no \( G \) peak splitting is seen, but an increase in FWHM(G). We take this FWHM increase as a signature of phonon splitting. To test this hypothesis, we subject our fibres to tension and examine the peak evolution with strain for \( \theta \) \( = 0^\circ \) or \( 90^\circ \) and \( \theta_{out} = 0^\circ \).

For the high modulus (HM)-PAN-CF, the \( G \) peak is plotted in Figure 3a at 0 and 1% strain. For strains higher than 0.5–0.6%, the \( G \) peak can be fit with two Lorentzians (black line) better than a single Lorentzian (red line, Fig. 3a). The two components correspond to \( G^- \) and \( G^+ \) (Fig. 2a). For a tensile strain of 1% and \( \theta_{in} = \theta_{out} = 0^\circ \), we...
Figure 5 | Master plot of $\partial \omega_g / \partial \varepsilon$ as a function of tensile modulus. The black solid and dashed lines correspond to fits of experimental data for graphene. The black and red triangles correspond to graphene G subbands values measured in this work and in ref. 25, respectively. In red, the solid square points correspond to group A fibres, the solid circles correspond to group B, the open circles to group C, whereas the diamonds to MPP-CFs and the stars to various PAN-CFs. In black, data points for HM (empty square), IM (full circle), P25 (full diamond) and P55 (empty diamond) CFs measured in this work. The black empty triangles show the HM-CF G band splitting and its projection onto the graphene average line. The inset shows the $\partial \omega_g / \partial \varepsilon$ least-squares line fits for group A ($\partial \omega_g / \partial \varepsilon = 3 \text{ cm}^{-1} \text{ GPa}^{-1}$), B ($2.3 \text{ cm}^{-1} \text{ GPa}^{-1}$) and MPP-CFs (1.5 cm$^{-1}$ GPa$^{-1}$) as dotted lines. The other symbols in the inset have the same meaning as in the main plot. The error bars represent the s.d. from all measurements on the given fibre.

get $I(G^-)/I(G^+)=0.6$ from a number of fibres tested (Fig. 3a). From equation (1) and $\theta_{\phi g}=\theta_{\phi m}=0^\circ$, we expect $I(G^-)/I(G^+)=\tan^2(3\phi)$, implying an average $\phi=13^\circ$ (Fig. 1). However, this result should be treated with caution even for ‘onion’ skin fibres, due to the presence of a disorder that can affect the measured intensities. In contrast, for the P55-CF, there is no sign of splitting at strains just before fracture ($-0.8\%$) indicating, as argued below, the absence of the $G^-$ component in MPP-CFs.

Pos(G) as a function of strain for both the HM- and P55-CFs is plotted in Figure 4. For the HM-CF (annular morphology), FWHM(G) increases significantly for strains higher than 0.4%, whereas the P55-CF shows no increase up to fracture. Also plotted in Figure 4 is Pos(G) for both $\theta_{\phi m}=0^\circ$ and $\theta_{\phi m}=0^\circ$, with $\theta_{\phi m}=0^\circ$. For all CFs, and strains up to 0.4%, we get $\partial \omega_g = -1.12 \times 10^7 \text{ cm}^{-1}$ for $\theta_{\phi m}=0^\circ$, similar to what was reported earlier for similar fibres and $-9.5 \times 10^6 \text{ cm}^{-1}$ for $\theta_{\phi m}=90^\circ$. However, at higher strains, by fitting two Lorentzians, we get $\partial \omega_g / \partial \varepsilon$ and $\partial \omega_g / \partial \varepsilon = -18.8 \times 10^6 \text{ cm}^{-1}$ and $-6.7 \times 10^6 \text{ cm}^{-1}$ (Fig. 4a). In contrast, the P55-CF (Fig. 4b), with radial morphology, shows no appreciable FWHM(G) increase, hence no peak splitting. It is interesting to note that the average $\partial \omega_g / \partial \varepsilon$ for the P55-CF is close to that of the $G^+$ peak in the HM-CF of similar modulus. Translating this finding to the graphene plane (see Fig. 5 in ref. 25), prevalence of $G^+$ would imply that $\phi$ is close to zero, that is, the $C-C$ bond is perpendicular to the fibre axis, the so-called zig-zag configuration.

The expected shift per unit of normal stress in fibres can be derived as follows. If both components contribute equally to the measured Raman shift, using equations (9) and (10) we get:

$$\Delta \omega_c = \frac{\Delta \omega_{G^+} + \Delta \omega_{G^-}}{2} = \frac{(A + B)(S_{11} + S_{12})}{4\omega_0} \sigma \left[ \frac{S_{11}(A + B)}{4\omega_0} \right] \sigma$$

(11)

By returning to the treatment presented in the previous section for graphene, we can estimate the theoretical value of the expression in brackets as $-5\omega_0^{-1} \text{ cm}^{-1} \text{ MPa}^{-1}$. This is valid at least for annular morphology CFs (that is, most PAN-based CFs) and confirms the applicability of the fibre as stress sensors in a number of applications. As shown below, it also defines the mean value of phonon shift over a wide modulus range.

Discussion

To visualize the structural relation between graphene and CFs, a universal master plot is constructed. In Figure 5, the $\partial \omega_g / \partial \varepsilon$ for graphene, the PAN-based, HM and intermediate modulus (IM) fibres, as well as the MPP-based, P55 and P25 fibres, are plotted against their nominal—bulk—tensile Young's modulus. All these data were obtained for $\theta_{\phi m}=0^\circ$ and $\theta_{\phi m}=0^\circ$. Furthermore, we include data from PAN-based and MPP-CFs measured over the past 20 years, (see Methods for details). All CF data are contained within two boundary lines defined by the graphene $G^+$ and $G^-$ slopes $-1.7$ and $-3.6 \text{ cm}^{-1} \text{ GPa}^{-1}$.

We also note that the data points from fibres exhibiting annular structure (classical processing route) lie below the bisector (average) line $\partial \omega_g / \partial \varepsilon = -2.7 \text{ cm}^{-1} \text{ GPa}^{-1}$, also confirmed by direct stress measurements. On the contrary, PAN-CFs produced by the imposition of a higher drawing ratio at the carbonization stage and at lower ultimate firing temperature (UFT) have much smaller $\partial \omega_g / \partial \varepsilon$. A further validation of this phenomenon is given for the so-called group C fibres of approximately the same modulus but of varying draw ratio. In this case, the higher the extent of pre-graphitization drawing, thus the lower the UFT, the smaller the $\partial \omega_g / \partial \varepsilon$. It appears therefore that, as the CF morphology is altered by drawing from the annular (‘onion’) to a highly folded structure, the data shift towards the $G^+$ boundary (see Fig. 5). The PAN-CFs from ref. 18 consist of various fibres obtained from different producers and derived through different processing conditions. Yet, their data points lie within the boundaries of the $G^+$ and $G^-$ lines as the PAN fibres mentioned above. Finally, the data for MPP-CFs with radial morphology, measured in this study and those extracted from the literature, tend to conform to the $G^+$ line of slope $\partial \omega_g / \partial \varepsilon = -1.6 \text{ cm}^{-1} \text{ GPa}^{-1}$. These effects can be explained by the results of the previous sections with reference to the angle $\phi$ between strain axis and $C-C$ bond (Fig. 1). As the graphene stacks in CF rotate and $\phi$ decreases towards $0^\circ$ (radial morphology, Fig. 1), the $G^+$ peak prevails, as for equation (1) with $\theta_{\phi m}=0^\circ$. Finally, the $G^+$ and $G^-$ peaks’ strain shifts of $-18.8 \times 10^6 \text{ cm}^{-1}$ and $-6.7 \times 10^6 \text{ cm}^{-1}$ of the HM-CF (Fig. 4a), respectively, can be projected onto the average line of Figure 5 to get an estimate of the true tensile modulus of the CF optical (sampling) area. This indicates a skin modulus of some 100 GPa higher than the CF bulk modulus, in broad agreement with the previous results, obtained by X-ray measurements for CF of similar morphology.

Note that in the case of SWNTs, the overall phonon shift will also depend on chirality. In nanotubes, pure curvature splits the graphene $E_2$ mode into two components, one parallel and one perpendicular to the tube axis. Thus, by curvature only, semiconducting nanotubes will have a low frequency transverse optical $G^-$ peak and a higher frequency longitudinal optical $G^+$ peak. However, in metallic SWNTs, a further significant longitudinal optical softening takes place because of the enhanced Kohn anomaly due to electron confinement, resulting in the opposite assignment of $G^-$ and $G^+$.
**Methods**

**CFs.** The HM fibre has 7 µm diameter and 370 GPa bulk modulus. This is produced by conventional manufacturing technologies. Acrylic filaments were wet-spun and drawn in hot water and saturated steam to a total draw ratio of 14, to yield a final diameter of ~12 µm. The filaments were stabilized in hot air to a density of ~1.38–1.40 g/cm³ using a rising-ramped temperature regime (225–245 °C). Primary carbonization was carried out using a maximum temperature of 950 °C, whereas secondary carbonization and graphitization were at UFT = 2,600 °C. No additional drawing processes were carried out. During stabilization, the filaments were held at constant length. During carbonization and graphitization, a 5% shrinkage was allowed.

The IM fibre has a 5 µm diameter and 270 GPa bulk modulus. Acrylic filaments were wet-spun and drawn as described above. The filaments were then subjected to a multistage prestabilization drawing at temperatures up to 270 °C, followed by stabilization as described above. Carbonization and graphitization were carried out with the filaments held at constant length at UFT = 1,750 °C.

Two commercial MPP fibres with E = 167 GPa (P25) and 371 GPa (P55) sourced from Cytec Industries were also tested. These use MPP derived from petroleum pitch. The P55-CF is a ~25 mm diameter and 250 GPa modulus. Acrylic filaments were wet-spun and drawn as described above. The filaments were then subjected to a multistage prestabilization drawing at temperatures up to 270 °C, followed by stabilization as described above. Carbonization and graphitization were carried out with the filaments held at constant length at UFT = 1,750 °C.

**Graphene.** Graphene monolayers were prepared by mechanical cleavage from natural graphite (Nacional de Grafite) and transferred onto the poly methyl methacrylate acetate (PMMA) CB covered by a ~200 nm-thick layer of SU8 photoresist (SU8 2005, MicroChem). A thin layer of S1805 photoresist (Shipley) was coated on top. The beam has a total thickness 2.9 mm and width 12.0 mm. The graphene flake was located at 12.97 mm from the beam end. The flake's dimensions are 6.56 mm², with the shorter side parallel to the strain axis.

**Raman spectroscopy.** Apart from the G band mentioned in the main text, other Raman features can be traced in carboxenizable materials. The D peak is due to the breathing modes of sp² rings and requires a defect for its activation. It comes from the transverse optical phonon branch (TO) around the K point of the Brillouin zone. It is active by double resonance (DR) and is strongly dispersive near the Kohn Anomaly at K. DR can also take advantage of intravalley, that is, connecting two points belonging to the same Dirac cone around K or K'. This gives rise to the so-called D' peak, which appears around 1620 cm⁻¹ in defected graphene and CFs measured with visible excitation. The 2D peak is the second order of the D peak. This is a single peak in single-layer graphene, whereas it splits into four in bilayer graphene, reflecting the evolution of the band structure. The 2D peak is the second order of the D' peak. Because both 2D and 2D' originate from a process where momentum conservation is satisfied by two phonons with opposite wavevectors, q and –q, they do not require the presence of defects for their activation, and are thus always present. Indeed, high-quality graphene shows the G, 2D and 2D' peaks, but not D and D'. Unlike the G peak, the 2D band shows a significant evolution in shape with the number and orientation of the graphene layers, as well as broadening or separation, according to the uniaxial strain orientation with respect to the graphene unit cell. However, while amorphous carbons or CFs of low modulus show a broad and almost featureless 2D peak, owing to the additional effect of defects in the DR process, the G peak, even though broader compared with graphene, is always present, being due to the relative motion of carbon atoms and not requiring the presence of sp² rings. Hence, the G peak is ideal for comparative studies of in-plane stress and strain between different graphitic materials.
2. Zhi, L. J. & Mullen, K. A bottom-up approach from molecular nanographenes to ultrconventional carbon materials. J. Mater. Chem. 18, 1472–1484 (2008).
3. Morgan, P. Carbon Fibers and Their Composites (Taylor & Francis, 2005).
4. Melanitis, N., Tselov, P. L. & Galiotis, C. Characterization of PAN-based carbon fibers with laser Raman spectroscopy. J. Effect of processing variables on Raman band profiles. J. Mater. Sci. 31, 851–860 (1996).
5. Loidl, D., Peterlik, H., Muller, M., Riekel, C. & Paris, O. Elastic moduli of nanocrystallites in carbon fibers measured by in situ X-ray microbeam diffraction. Carbon 41, 563–570 (2003).
6. Oberlin, A. Carbonization and graphitization. Carbon 22, 521–541 (1984).
7. Fitzner, E. (ed.) Carbon Fibers and Their Composites (Springer, 1985).
8. Donnet, J. B. & Bansal, R. C. Carbon-Fibers. (Marcel Dekker, 1984).
9. Ruland, W. Carbon-Fibers. Adv. Mater. 2, 528–536 (1990).
10. Anastassakis, E., Pinczuk, A., Burstein, E., Pollak, F. H. & Cardona, M. Effect of static uniaxial stress on Raman spectrum of silicon. Solid State Commun. 8, 133 (1970).
11. Cerdeira, F., Buchenauer, C. J., Cardona, M. & Pollak, F. H. Stress-induced shifts of first-order Raman frequencies of diamond and zinc-blende-type semiconductors. Phys. Rev. B 5, 580 (1972).
12. Eland, J. F., Lattava, C. & Galiotis, C. Modeling of stress transfer in fiber composites. Compos. Sci. Technol. 50, 319–332 (1994).
13. Melanitis, N., Tselov, P. L., Galiotis, C. & Smith, S. B. Compressional behavior of carbon-fibers. J. Modulus softening. J. Mater. Sci. 29, 786–799 (1994).
14. Ferrari, A. C. Raman spectroscopy of graphene and graphite: disorder, electron-phonon coupling, doping and nonadiabatic effects. Solid State Commun. 143, 47–57 (2007).
15. Ferrari, A. C. et al. Raman spectrum of graphene and graphene layers. Phys. Rev. Lett. 97, 187401 (2006).
16. Tuinstra, F. & Koenig, J. L. Raman spectrum of graphite. J. Chem. Phys. 53, 1126–1130 (1970).
17. Ferrari, A. C. & Robertson, J. Raman spectroscopy of carbons from nanotubes to diamond. Philos. Trans. R. Soc. A 362, 2267–2565 (2004).
18. Huang, Y. & Young, R. J. Effect of fibre microstructure upon the modulus of PAN- and pitch-based carbon fibres. Carbon 33, 97–107 (1995).
19. Northolt, M. G., Veldhuizen, L. H. & Jansen, H. Tensile deformation of carbon-fibers and the relationship with the modulus for shear between the basal planes. Carbon 29, 1267–1279 (1991).
20. Casiraghi, C. et al. Rayleigh imaging of graphene and graphene layers. Nano Lett. 7, 2711–2717 (2007).
21. Kvatno, V. G. et al. Spectroscopic ellipsometry of graphene and an exciton-shifted van Hove peak in absorption. Phys. Rev. B 81, 155413 (2010).
22. Wada, N. & Solin, S. A. Raman efficiency measurements of graphite. Physica B+C 105, 353–356 (1981).
23. Djurisic, A. B. & Li, E. H. Optical properties of graphite. J. Appl. Phys. 85, 7404–7410 (1999).
24. Chohan, V. & Galiotis, C. Effects of interface, volume fraction and geometry on stress redistribution in polymer composites under tension. Compos. Sci. Technol. 57, 1089–1101 (1997).
25. Mohiuddin, T. M. G. et al. Uniaxial strain in graphene by Raman spectroscopy: G peak splitting, Grueneisen parameters, and sample orientation. Phys. Rev. B 79, 205343–205348 (2009).
26. Huang, M. Y. et al. Phonon softening and crystallographic orientation of strained graphene studied by Raman spectroscopy. Proc. Natl Acad. Sci. USA 106, 7304–7308 (2009).
27. Sakata, H., Dresselhaus, G., Dresselhaus, M. S. & Endo, M. Effect of uniaxial-stress on the Raman-spectra of graphite fibers. J. Appl. Phys. 63, 2769–2772 (1988).
28. Thomsen, C., Reich, S. & Ordejon, P. Ab initio determination of the phonon deformation potentials of graphite. Phys. Rev. B 65, 073403 (2002).
29. Bosak, A., Krish, M., Mohr, M., Maultzsch, J. & Thomsen, C. Elasticity of single-crystalline graphite: inelastic X-ray scattering study. Phys. Rev. B 75, 153408–153404 (2007).
30. Lee, C., Wei, X. D., Kysar, J. W. & Hone, J. Measurement of the elastic properties and intrinsic strength of monolayer graphene. Science 321, 385–388 (2008).
31. Frank, O. et al. Compression behavior of single-layer graphenes. ACS Nano. 4, 3131–3138 (2010).
32. Tsoukleris, G. et al. Subjecting a graphene monolayer to tension and compression. Small 5, 2397–2402 (2009).
33. Piscanec, S., Lazzeri, M., Robertson, J., Ferrari, A. C. & Mauri, F. Optical phonons in carbon nanotubes: Kohn anomalies, Peterls distortions, and dynamic effects. Phys. Rev. B 75, 035427–035422 (2007).
34. Jorio, A. et al. G-band resonant Raman study of 62 isolated single-wall carbon nanotubes. Phys. Rev. B 65, 155412 (2002).
35. Cronin, S. B. et al. Measuring the uniaxial strain of individual single-wall carbon nanotubes: resonance Raman spectra of atomic-force-microscope modified single-wall nanotubes. Phys. Rev. Lett. 93, 167401 (2004).
36. Cronin, S. B. et al. Resonant Raman spectroscopy of individual metallic and semiconducting single-wall carbon nanotubes under uniaxial strain. Phys. Rev. B 72, 035423 (2005).
37. Gao, B., Jiang, L., Ling, X., Zhang, J. & Liu, Z. F. Chirality-dependent Raman frequency variation of single-walled carbon nanotubes under uniaxial strain. J. Phys. Chem. C 112, 20123–20125 (2008).
38. Ferrari, A. C. & Robertson, J. Interpretation of Raman spectra of disordered and amorphous carbon. Phys. Rev. B 61, 14095–14107 (2000).
39. Piscanec, S., Lazzeri, M., Mauri, F., Ferrari, A. C. & Robertson, J. Kohn anomalies and electron-phonon interactions in graphite. Phys. Rev. Lett. 93, 185503 (2004).
40. Thomsen, C. & Reich, S. Double resonant Raman scattering in graphite. Phys. Rev. Lett. 85, 5214–5217 (2000).
41. Frank, O. et al. Raman 2D-band splitting in graphene: theory and experiment. ACS Nano, doi: 10.1021/nn103493g.
42. Huang, M., Yan, H., Heinz, T. F. & Hone, J. Probing strain-induced electronic structure change in graphene by Raman spectroscopy. Nano Lett. 10, 4074–4079 (2010).
43. Lomax, R. Statistical Concepts (Lawrence Erlbaum Associates, 2007).
44. Acknowledgments
FORTH/ICE-HT acknowledges financial support from the Marie-Curie Transfer of Knowledge program CNTCOMP (Contract No.: MTKD-CT-2005-029876). Also, G.T. gratefully acknowledges FORTH/ICE-HT for a scholarship, and A.C.F., K.S.N., A.K.G. thank the Royal Society and the European Research Council for financial support. A.C.F. acknowledges funding from EPSRC grant EP/G042357/1 and EU projects RODIN and Marie Curie ITN-GENIUS (PITN-GA-2010-264964), a Royal Society Wosfon Research Merit Award, and Nokia Research Centre Cambridge. Cytec Industries (US) are thanked for supplying the P25 and P55 fibres. We also thank D.M. Baiko, G. Savini and N. Melanitis for useful discussions.

Author contributions
Project planning, C.G.; sample preparation G.T., I.R., K.S.N., A.K.G.; spectroscopic measurements and analysis, G.T., O.F., J.P., A.C.F.; data interpretation, O.F., K.P., C.G., A.C.F.; manuscript drafting, C.G., K.P., O.F., A.C.F.

Additional information
Competing financial interests: The authors declare no competing financial interests.
Reprints and permission information is available online at http://npg.nature.com/reprintsandpermissions/
How to cite this article: Frank, O. et al. Development of a universal stress sensor for graphene and carbon fibres. Nat. Commun. 2:255 doi: 10.1038/ncomms1247 (2011).
License: This work is licensed under a Creative Commons Attribution-NonCommercial-Share Alike 3.0 Unported License. To view a copy of this license, visit http://creativecommons.org/licenses/by-nc-sa/3.0/