Introduction

Gait analysis has been proposed as an alternative for evaluating the functionality of lower limbs during daily living tasks (Baker, 2006). The basic instrumentation usually recommended is a motion analysis system (MAS), force plates and electromyography. All these instruments have high costs, which makes it difficult to implement a gait service in the clinical practice context, outside the academic laboratory. Therefore, alternatives for low-cost equipment have been proposed. Inertial sensors have been used to replace the MAS (Favre et al., 2009) and seem to be a promising technology. Several studies have already shown the clinical applicability of these systems to collect kinematic data (Fasel et al., 2015; Peruzzi et al., 2011).

However, little effort has been made to replace force plates to acquire ground reaction force (GRF). So far, there is no means of directly measuring these forces during walking. Computational mathematical systems have been developed to estimate these forces by optimization algorithms based on ground reaction forces and kinematic data (Lewis & Garibay, 2015). Usually, data from optoelectronic motion analysis systems and force plates are used to calculate inverse and forward dynamics. However, these devices limit the performance of the gait analysis to a laboratory environment - besides its high cost (Baker, 2006) - reducing the application of quantitative biomechanical tests in the clinical practice.

Some studies have proposed a model to predict GRF based on insole plantar pressure measurements (Fong et al., 2008; Jung et al., 2014), presenting promising results. Despite the advance, the required insoles still have an elevated cost and do not allow the analysis to be done barefoot, which can influence the outcome (Chen et al., 2015). Accelerometers attached to the tibia, on the other hand, are lightweight and have already been used to...
simulate some discrete force variables, using regression analysis (Elvin et al., 2007). The limitation of these latter models is that they do not estimate the complete GRF signal. To overcome these limitations, some studies have used artificial neural networks to predict moment of force data during different tasks (Favre et al., 2012; Oh et al., 2013).

Therefore, the aim of this study was to predict 3D ground reaction force signals based on accelerometer data during gait, using a feed-forward neural network (MLP). The hypothesis of this study was that 3D accelerometer data from the distal tibia would allow an adequate simulation of GRF, with prediction errors comparable to other studies using a plantar pressure device.

Methods

Seventeen healthy subjects (11 males; 27.1 ± 3.4 years old; 84.3 ± 4.5 kg) participated in the study. All of them provided written consent, approved along with the experimental protocol of the Institutional Ethics and Research Committee. Inclusion criteria were: (i) to have no history of ligament injuries, nor pain at the time of the tests; (ii) to be between 20 and 40 years old; and (iii) to walk independently, without the need of any orthoses or braces.

Subjects were instructed to walk at a self-selected speed along an eight m long walkway. Each subject performed six laps with a 3D accelerometer (± 6 g, model MMA7260Q, Freescale, USA) attached to the distal and anterior part of the shank. A force plate (AccuGait, AMTI, USA) was embedded into the middle of the walkway. The first two laps were not collected to allow familiarization with the task. The last four laps were collected in order to capture, during four gait cycles the acceleration of the shank. All data were collected simultaneously using a BIOPAC system (UIM, MP100 Systems, BIOPAC, USA) with a sample rate of 1 kHz.

After collection, the data were filtered by a 2nd order Butterworth low pass filter, applied in the direct and reverse directions to avoid phase shift. The cutoff frequency for GRF and accelerometer data was 25 Hz. Stance phase was defined when vertical ground reaction forces were above 10 N.

To fit anteroposterior (AP), vertical (Vert) and mediolateral (ML) GRF curves, fourteen inputs were selected based on previous studies (Favre et al., 2012; Liu et al., 2009), as follows:

i to iii: the 3D leg acceleration data normalized by body weight;
iv to vi: the 3D leg velocity, represented by the single integration of the acceleration curve;
vii to ix: 3D leg displacement, represented by the double integration of the acceleration curve;
x to xii: the first derivate of the 3D accelerometer signal
xiii: the stance duration (s); and
xiv: time point of the stance phase of gait (%), expressed as a percentage of the stance time.

Multilayer perceptron (MLP) neural networks with one hidden layer and three output layers were selected to simulate the 3D GRF. The number of neurons in the hidden layer was chosen by testing the fitting of signals with different sizes, always seeking the most parsimonious model, i.e. few hidden neurons and good generalization power. Networks were modeled using from five to 12 neurons in the hidden layer.

To assess the network fitting, a leave one out cross-validation strategy was used. The network was trained using the Levenberg-Marquardt backpropagation algorithm according to Favre et al. (2012) and Liu et al. (2009).

Hyperbolic tangent and linear activation transfer functions were used in the hidden and output layers, respectively. These typologies were used in previous biomechanical studies which showed that these transfer functions produced the best signal prediction (Favre et al., 2012; Liu et al., 2009). To avoid overfitting, the generalization error obtained for the validation set during the training process, and the minimum gradient were used as stop criteria.

The network with the lowest mean absolute deviation (MAD) among all subjects was selected as the best number of neurons in the hidden layers. MAD was calculated as:

\[
MAD = \frac{1}{N} \sum_{t=1}^{N} \|GRF(t) - \hat{GRF}(t)\| \\
\]

where \(GRF(t)\) represents the simulated ground reaction force, \(\hat{GRF}(t)\) corresponds to the collected GRF and \(N\) is the vector size.

The normalized mean absolute deviation (MAD%) was also calculated as [8]:

\[
MAD\% = \frac{MAD}{\text{range}(GRF(t))} \times 100 \\
\]

Data from each gait cycle were interpolated into 51 values, representing 0% to 100% of the stance phase. To test significant differences between the simulated and measured signals, the 136 GRF curves, 68 measured and 68 simulated, were inserted into a matrix \(D\) [136 x 51],
where each row corresponded to a gait cycle and each column corresponded to the interpolated signals.

Principal Component (PC) analysis was applied to three independent matrices $D$, each one corresponding to a different GRF component (Jolliffe, 2002). Initially, the mean was subtracted, the covariance matrix $S$ [51 x 51] was calculated and, finally, the eigenvectors and eigenvalues were estimated from $S$, based on a singular value decomposition algorithm (Jolliffe, 2002). The number of PC retained in the analysis represented approximately 80% of the original data variance. The scores of the retained PCs were compared between the simulated and measured signals using a paired t-test. The correspondent eigenvectors of the statistically significant PC scores were analyzed in temporal correspondence to the original signals to identify the location where the variance between them could be explained (Leporace et al., 2012). The locations where eigenvectors deviate from zero indicate increased differences between the simulated and collected signals.

The correlation between the simulated and collected signal was also calculated for each GRS component, using the Pearson’s correlation coefficient. The significance level was set at 0.05. The effect size was also calculated based on Cohen (1988). Values higher than 0.8 were considered large and values lower than 0.5 were considered small.

### Results

The number of neurons in the hidden layer with the lowest MAD was ten. The vertical ground reaction forces showed the lowest errors, followed by the anteroposterior and, with the greatest errors, the mediolateral forces. The correlation between the simulated and collected signals was high, with values above 0.8 (Table 1).

The simulation of the signal showed good qualitative results, with all the simulated signals resembling the original data (Figures 1 to 3). Four, five and four PCs were retained for the vertical, anteroposterior and mediolateral GRF comparison between the signals, respectively. The vertical GRF showed no significant differences ($p > 0.05$), with low effect size (Table 2, Figure 2). The anteroposterior GRF showed significant differences in the fifth PC ($p = 0.009$) (Table 2, Figure 3), and the mediolateral forces presented differences in the second ($p = 0.01$) and third ($p = 0.02$) PCs (Table 2, Figure 3). The loading factors indicated that the variance was higher in the first 15% of the stance phase, representing the impact phase and the first active peak.

| Component     | MAD (± sd) | % MAD (± sd) | $r$  |
|---------------|-----------|--------------|------|
| Anteroposterior| 4.5 ± 1.1%BW | 4.0 ± 0.8% | 0.98 |
| Vertical      | 4.5 ± 1.1%BW | 4.0 ± 0.8% | 0.98 |
| Mediolateral  | 1.4 ± 0.3%BW | 10.5 ± 3.3% | 0.80 |

**Table 1.** Mean absolute deviation (MAD) and normalized mean absolute deviation (%MAD), expressed as mean (± standard deviation), and Pearson Correlation Coefficient ($r$).

![Figure 1. Vertical Ground Reaction Forces.](image1)

![Figure 2. Anteroposterior Ground Reaction Forces.](image2)

**Figure 1.** Vertical Ground Reaction Forces. The black continuous line represents the collected signal and the magenta dashed line represents the simulated signal. The area surrounding the averages represents 95%CI for each group.

**Figure 2.** Anteroposterior Ground Reaction Forces. Above: The black continuous line represents the collected signal and the magenta dashed line represents the simulated signal. The area surrounding the averages represents 95%CI for each group. Below: Fifth principal component, and the arrows represent the locations where there is higher variance, representing differences between signals.
Discussion

The purpose of this study was to predict 3D ground reaction forces during gait based on a lightweight and low cost accelerometer attached to the distal tibia. The results showed that the neural network model achieved success to simulate the shape of the 3D GRF curves, although the PC analysis still discriminated some differences between the simulated and collected signal.

The MAD and MAD% were equal or lower than other studies that used plantar pressure insoles to calculate GRF. The MAD from AP GRF simulation from studies using plantar pressure insoles ranged from 1.6 to 5.8%BW, while the %MAD ranged from 7.3% to 10.1% and the correlation coefficient ranged from 0.85 to 0.98 (Fong et al., 2008; Forner-Cordero et al., 2004; Jung et al., 2014; Liedtke et al., 2007; Rouhani et al., 2010; Savelberg & Lange, 1999). The MAD, MAD% and correlation coefficient found in the present study were 1.8%BW, 4.6% and 0.97, respectively. Vert GRF simulation in the literature has error values ranging from 6.6%BW to 13.8%BW; the relative error ranging from 7.3% to 10.1%, while the present study showed values of 4.5%BW and 4.0%. The correlation coefficient of all studies is close, ranging from 0.97 to 0.99, similar to the neural network simulation (Barnett et al., 2001; Fong et al., 2008; Forner-Cordero et al., 2004; Jung et al., 2014; Liedtke et al., 2007; Oh et al., 2013; Rouhani et al., 2010).

Similar to other studies, ML GRF presented lower correlation and higher error than AP and Vert GRF (Liedtke et al., 2007; Oh et al., 2013). The ML error of this study was similar to Oh et al. (2013), showing a relative error of 10%. This should be due to the greater variability of this signal (John et al., 2012). Maybe, with a higher sample size this variability could be captured by the neural network model, decreasing the error.

Despite the similarity of the error, none of the studies have validated their models, making it difficult to discuss the fitness of the model, not allowing to confirm if the model is well fitted or that it cannot be improved without a validation process. In a previous study (Leporace et al., 2015), it has been shown, through a residual analysis, the closeness of the model proposed in the present study to a normal probability distribution, confirming the data is suitable.

Additionally, this is the first study to compare the simulated and collected GRF using a statistical technique that is more sensitive to differences than more traditional ones (Leporace et al., 2012; Muniz et al., 2010). The advantage of using PCA is that it allows the analysis of the entire time series, not just discrete values extracted from them (Jolliffe, 2002).

The simulated and collected vertical ground reaction forces (Figure 2) showed no differences, suggesting that the use of this curve in clinical practice is acceptable.

Table 2. P value and effect size (ES) of the comparison between the collected and simulated ground reaction forces.

|                  | Anteroposterior |          | Vertical |          |          | Mediolateral |          |
|------------------|----------------|----------|----------|----------|----------|--------------|----------|
|                  | p value | ES | p value | ES | p value | ES | p value | ES |
| PC1              | 0.07    | 0.44  | 0.48    | 0.12  | 0.31    | 0.50         |
| PC2              | 0.95    | 0.01  | 0.93    | 0.02  | 0.01**  | 1.04         |
| PC3              | 0.08    | 0.63  | 0.71    | 0.09  | 0.02*   | 1.06         |
| PC4              | 0.50    | 0.20  | 0.98    | 0.01  | 0.24    | 0.46         |
| PC5              | 0.009** | 0.94  | -       | -     | -       | -            |

*p ≤ 0.05; **p ≤ 0.01. PC = Principal Component; ES = Effect Size.

Figure 3. Mediolateral Ground Reaction Forces. Above: The black continuous line represents the collected signal and the magenta dashed line represents the simulated signal. The area surrounding the averages represents 95%CI for each group. Below: Second (continuous line) and third (dashed line) principal components, and the arrows represent the locations where there is higher variance, representing differences between signals.
This result is very important, since some variables extracted from vertical GRF have already been linked with injury risk (Zadpoor & Nikooyan, 2011) and disease progression (Houck et al., 2011); and this system is low cost and does not need a highly instrumented biomechanics laboratory to collect data. On the other hand, PCA showed that AP and ML curves still present differences that could influence the use of these signals in clinical practice. The loading factor from the AP and ML GRF found differences in 5% and 15% of the stance phase, representing a decreased impact peak and first active peak.

The impact forces’ peak had a higher frequency range (10 to 20 HZ) and represents the rapid deceleration of the leg and foot just after the initial contact with the ground, while the active peak had a lower frequency range (4 to 8 Hz), representing voluntary lower extremity motion and the deceleration of the center of mass (CoM) (Gruber et al., 2014). It is possible that the deceleration of the CoM and foot could not be captured, since in the present study only one accelerometer was attached to the shank. It was proposed, for future studies, the inclusion of sensors on the sacrum, representing the acceleration of the CoM, and on the foot, providing more information for the neural networks to simulate the GRF signals.

This study confirmed that multilayer perceptron neural network can predict the highly non-linear relationship of shank acceleration parameters and ground reaction forces in healthy young individuals, as well as other studies have done using plantar pressure devices. The greater advantages of this device are the low cost and the possibility of use outside the laboratory environment. Although the error rates were low, ranging from 4 to 10%, some improvements must be made, regarding the management of input parameters and number of sensors used, prior to application in clinical settings.

The results of this study must be only applied to level walking of healthy individuals. Although it is known that straight-line level walking is actually not common in real-world activities (Orendurff et al., 2008), usually level gait with self-selected speed is the most used task in clinical biomechanical gait assessments aimed at identifying lower limb dysfunctions. Future studies must be performed applying this algorithm to different orthopedic and neurologic conditions.

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