Double-Transmon Coupler: Fast Two-Qubit Gate with No Residual Coupling for Highly Detuned Superconducting Qubits

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Although two-qubit entangling gates are necessary for universal quantum computing, they are notoriously difficult to implement with high fidelity. Recently, tunable couplers have become a key component for realizing high-fidelity two-qubit gates in superconducting quantum computers. However, it is still difficult to achieve tunable coupling free of unwanted residual coupling, in particular, for highly detuned qubits, which are desirable for mitigating qubit-frequency crowding or errors due to crosstalk between qubits. We thus propose this kind of tunable coupler, which we call a double-transmon coupler, because this is composed of two transmon qubits coupled through a common loop with an additional Josephson junction. Controlling the magnetic flux in the loop, we can achieve not only fast high-fidelity two-qubit gates, but also no residual coupling during idle time, where computational qubits are highly detuned fixed-frequency transmons. The proposed coupler is expected to offer an alternative approach to higher-performance superconducting quantum computers.

I. INTRODUCTION

Remarkable advances have been made in the technologies for realizing quantum computers over the past decade. Nevertheless, two-qubit entangling gates, which are necessary for universal quantum computing together with single-qubit gates [1–7], are still hard to implement with high fidelity. For instance, two-qubit gates with fidelity of over 99%, which is necessary for tasks such as fault-tolerant quantum computation using quantum error correction [8–12], have been demonstrated experimentally by using only a few kinds of physical systems: laser-cooled trapped ions [13–18], superconducting circuits [19–32], and most recently silicon-based approaches such as quantum dots [33–35] and donor spins [36]. Among these, superconducting circuits may be promising in the sense that their qubits are, of course, solid-state devices and therefore do not need trapping, unlike trapped ions, and also two-dimensional qubit arrays have already been realized [21, 24, 37], which is still difficult for quantum dots, by recently developed 3D integration technologies [38–40].

Tunable couplers have recently become a key component for high-fidelity two-qubit gates in superconducting quantum computers [21–24, 27–32, 34–35, 41–48]. Some research groups have found special conditions under which the ZZ coupling in the single-transmon coupler vanishes [28, 42]. However, the vanishing points exist only in a region of small detunings between two computational qubits [28] (see Appendix E). In other words, in the single-transmon coupler, there is inevitable ZZ coupling for highly detuned qubits [28]. Thus, zero ZZ coupling in the single-transmon coupler results in qubit-frequency crowding or crosstalk between qubits [64].

In this paper, we theoretically propose a new kind of tunable coupler, which we call a double-transmon coupler. Our coupler consists of two fixed-frequency transmons coupled through a common loop with an additional Josephson junction. We can control the coupling between the two couplers by controlling the magnetic flux in the loop, and consequently tune the coupling strength between computational qubits. A remarkable feature of this coupler is that the ZZ coupling vanishes even for highly detuned computational qubits, unlike the single-transmon coupler. Our numerical simulations indicate that this coupler allows us to achieve not only high two-qubit gate fidelities of over 99.99% with a short gate time of 24 ns, but also no residual ZZ coupling during idle time for highly detuned fixed-frequency transmons with detuning of 0.7 GHz. Thus, the double-transmon coupler is expected to be promising for improving the performance of superconducting quantum computers.

II. DESIGN AND MECHANISM

Figure 1 shows a diagram of the proposed coupler. This consists of two fixed-frequency transmons [Transmons 3 and 4 in Fig. 1] coupled through a common loop with an additional Josephson junction, the critical current of which is smaller than that of the transmons. Two
computational qubits (Transmons 1 and 2 in Fig. 1) are capacitively coupled to the coupler, as shown in Fig. 1.

The mechanism of this coupler is qualitatively explained from a classical point of view under rough approximations as follows. The Lagrangian describing the total system is given by $L = K - V$ with

$$K = \sum_{i=1}^{4} C_{ii} \frac{\dot{\varphi}_{i}^2}{2} + \sum_{i=1}^{4} \sum_{j=i+1}^{4} C_{ij} \dot{\varphi}_{i} \dot{\varphi}_{j} + \sum_{i=1}^{4} \frac{C_{ii}}{2} \phi_{i}^{2},$$

$$V = -\sum_{i=1}^{5} \hbar \omega_{j_{i}} \cos \varphi_{i},$$

where $\varphi_{i}$ and $\varphi_{i}^{(0)}$ are the phase differences minimizing $V_{c}$, $\delta_{i} = \varphi_{i} - \varphi_{i}^{(0)}$, and constants have been dropped. Note that when $\Theta_{ex}$ is equal to $\Theta_{ex}^{(0)}$ satisfying $\cos(\varphi_{i}^{(0)} - \varphi_{j}^{(0)} - \Theta_{ex}) = 0$, nondiagonal elements of the matrix in Eq. (4) vanish, and consequently the coupling between the two coupler transmons is turned off, as desired. This mechanism is substantially different from that of the single-transmon coupler.

III. ZZ COUPLING

In order to accurately evaluate the properties of the double-transmon coupler, here we numerically investigate it using a fully quantum-mechanical model with finite parasitic capacitances. In this work, the qubits are assumed to be detuned. The qubit states are then well-defined by the energy eigenstates of the total Hamiltonian. However, there can be an unwanted correlated energy shift due to residual ZZ coupling. The ZZ coupling strength $\zeta_{ZZ}$ is defined as

$$\zeta_{ZZ} = \omega_{11} - (\omega_{10} + \omega_{01}),$$

where $\omega_{ij} = E_{ij}/h$ is the frequency corresponding to the energy, $E_{ij}$, of the two-qubit state $|ij\rangle$. We also set the origin of energy as $\omega_{00} = 0$. When $\zeta_{ZZ} = 0$, the two qubits are completely independent.

By numerically diagonalizing the quantum-mechanical Hamiltonian derived from the Lagrangian given by Eqs. (1) and (2) (see Appendix A), we evaluate $\zeta_{ZZ}$ for two situations: larger and smaller detunings between the qubits than the anharmonicities (Kerr coefficients) of the qubits, which are, respectively, called “out of the straddling regime” and “in the straddling regime.” The results in the two situations are, respectively, shown in Figs. 2(a) and 2(b), where the parameters are set to experimentally feasible values. From these results, it turns out that the double-transmon coupler can have the vanishing points of the ZZ coupling in both the regimes. This is a
remarkable feature of the double-transmon coupler, because for the conventional single-transmon coupler, the ZZ-coupling vanishing points exist only in the straddling regime [28] (see Appendix D). It is also interesting that the coupler-transmon frequency required for the zero ZZ coupling is lower bounded out of the straddling regime, but upper bounded in the straddling regime [69].

IV. TWO-QUBIT GATE

We evaluate two-qubit gate performance by numerical simulations with the parameter values in Fig. 2(a) and \( \omega_4/(2\pi) = 8.5 \text{ GHz} \) [indicated by the horizontal dashed line in Fig. 2(a)] [70]. The \( \Theta_{ex} \) dependence of \( \zeta_{ZZ} \) for these parameter values is shown in Fig. 3(a). As shown in the inset, the ZZ coupling vanishes at \( \Theta_{ex} \approx 0.61\pi \) and \( 0.63\pi \). We thus define the qubit states by the energy eigenstates at \( \Theta_{ex} = 0.61\pi \). In other words, we set \( \Theta_{ex} = 0.61\pi \) during idle time, as indicated in Fig. 3(a).

In Fig. 3(a), it is also notable that \( \zeta_{ZZ}/(2\pi) \) becomes as large as 40 MHz at \( \Theta_{ex} = \pi \). This property can be used for a fast two-qubit gate called the controlled-phase (CPHASE) gate including the controlled-Z (CZ) gate [23, 28, 43], where \( \zeta_{ZZ} \) is adiabatically increased and then decreased by controlling the external flux \( \Phi_{ex} \). The flux pulse shape in the present simulations is shown in Fig. 3(b), which is designed according to a technique for reducing nonadiabatic errors [71] (see Appendix C). The simulation results are shown in Figs. 3(c) and 3(d).

Figure 3(c) shows that the rotation angle, \( \theta_{\text{CPHASE}} \), of the CPHASE gate increases linearly as the gate time \( T_g \) increases. The CZ gate corresponding to \( \theta_{\text{CPHASE}} = \pi \) can be achieved when \( T_g \approx 24 \text{ ns} \), as indicated by the horizontal dashed line in Fig. 3(c). The average fidelity of the CPHASE gate is shown in Fig. 3(d) (see Appendix B), suggesting that the CZ-gate fidelity, indicated by the vertical dashed line in Fig. 3(d), will surpass 99.99\%. Thus, the double-transmon coupler allows us to simultaneously achieve fast high-fidelity two-qubit gates and no residual coupling during idle time for highly detuned qubits [72]. The infidelity is mainly due to leakage errors caused by nonadiabatic transitions from \( |01 \rangle \) and \( |11 \rangle \) to higher levels outside the qubit subspace (see Appendix C). For instance, when the gate time is 24 ns, 20\% and 73\% of the average infidelity are due to the leakage errors from \( |01 \rangle \) and \( |11 \rangle \), respectively.

V. FLUX NOISE

Although the qubits are fixed-frequency transmons, the qubit frequencies vary a little depending on the flux in the coupler (see Appendix A). Here we examine the influence of the flux noise on the qubit coherence.

The coherence time \( T_2 \) for Qubit 1 in terms of the flux noise is formulated as [68]

\[
T_2 \approx |A_\Phi \frac{\partial \omega_{10}}{\partial \Phi_{ex}}|^{-1} = 2\pi |A_\Phi \frac{\partial \omega_{10}}{\Phi_{0} \partial \Theta_{ex}}|^{-1}, \tag{7}
\]

where the coefficient \( A_\Phi \) is typically \( 10^{-5} \Phi_0 \) [69] [68] (\( T_2 \) for Qubit 2 is given similarly). Using the parameter values in Fig. 3 and \( A_\Phi = 10^{-5} \Phi_0 \), \( T_2 \) for Qubits 1 and 2 are numerically estimated to be about 260 \( \mu s \) and 430 \( \mu s \), respectively, in idle state. These long coherence times
suggest the robustness of the proposed scheme against flux noise.

During the two-qubit gate, Θ_{ex} changes from 0.61π to π. In this range of Θ_{ex}, the minimum values of T_2 estimated as above are 30 µs and 5µs, respectively, for Qubits 1 and 2. Even in the worst-case scenario where the coherence time is assumed to be 5µs, the infidelity of the CPHASE gate with the gate time of 24 ns may increase to about 0.5%, which is still small. This rough estimation suggests that the flux noise may not degrade the gate performance very much.

VI. CONCLUSIONS

We have theoretically proposed a new kind of tunable coupler for superconducting quantum computers. We call this a double-transmon coupler, because this consists of two fixed-frequency transmons coupled through a common loop with an additional Josephson junction. We have numerically found that by tuning the external flux in the loop, residual ZZ coupling vanishes even for highly detuned computational qubits, in contrast to the conventional single-transmon coupler. Numerical simulations have also shown that the proposed coupler enables two-qubit gates with high fidelity of over 99.99% and a short gate time of 24 ns. The next step is experimental realization of this proposal, where relaxation and decoherence in transmons will degrade the performance. However, from its short gate time (24 ns) and recently reported long coherence times of transmons (over 300 µs) [73, 74], the proposed coupler is expected to achieve high two-qubit gate fidelity. Another important issue in experiments is the unwanted deviation of critical currents of Josephson junctions from design values. The precision of the critical currents is known to be about 2%, though this can be reduced by laser annealing [75]. The effects of the critical-current deviation on the coupler performance are left as an important issue for future work.

Appendix A: Quantum-mechanical model

Using the constraint that φ_5 = φ_4 - φ_3 - Φ_{ex}, the kinetic energy term in Eq. (1) can be expressed as

\[ K = \frac{1}{2} \dot{\phi}^T M \dot{\phi} - q^T \dot{\phi}, \]  

where \( \dot{\phi}^T = (\dot{\phi}_1 \ \dot{\phi}_2 \ \dot{\phi}_3 \ \dot{\phi}_4), q^T = (0 \ 0 \ -C_{34} \dot{\Phi}_{ex} \ C_{34} \dot{\Phi}_{ex}), \) and M is a capacitor matrix. The canonical conjugate variables for the flux variables, namely, charge variables Q, and the Hamiltonian are obtained as

\[ Q = \frac{\partial L}{\partial \dot{\phi}} = M \dot{\phi} - q, \]  

\[ H = Q^T \phi - L = \frac{1}{2} Q^T M^{-1} Q + q^T M^{-1} Q + V. \]
Introducing the Cooper-pair number variables as \( n = Q/(2e) \) (\( e \) is the elementary charge), \( H \) is rewritten as

\[
H = 4\hbar n^T W n + \frac{\hbar}{\omega_{C34}} (0\ 0\ -1\ 1) W n + V,
\]

where \( \hbar W = \frac{e^2}{2} M^{-1} \) and \( \hbar \omega_{C34} = \frac{e^2}{2C_{34}} \) have been introduced as frequency parameters.

The variables are quantized by the commutation relation \([\hat{\varphi}_i, \hat{\eta}_j] = i\delta_{ij}\) as follows. \( \hat{n}_i \) is represented by \(-i\frac{\partial}{\partial \varphi_i}\) and the eigenfunction of \( \hat{n}_i \) is proportional to \( e^{in_i\varphi_i} \). In the basis of these eigenfunctions, we have the following matrix representation of operators:

\[
\hat{n}_i = \begin{pmatrix} -N & \cdots & \cdots & 0 \\ \cdots & \cdots & \cdots & \cdots \\ \cdots & \cdots & \cdots & \cdots \\ 0 & \cdots & \cdots & N \end{pmatrix}, \quad \cos \varphi_i = \frac{1}{2} \begin{pmatrix} 1 & \cdots & \cdots & 0 \\ \cdots & \cdots & \cdots & \cdots \\ \cdots & \cdots & \cdots & \cdots \\ 0 & \cdots & \cdots & 1 \end{pmatrix}, \quad \sin \varphi_i = \frac{1}{2i} \begin{pmatrix} 0 & \cdots & \cdots & -1 \\ \cdots & \cdots & \cdots & \cdots \\ \cdots & \cdots & \cdots & \cdots \\ -1 & \cdots & \cdots & 0 \end{pmatrix},
\]

where we have truncated the number of Cooper pairs at \( \pm N \).

Since the total system is composed of four subsystems (transmons), each operator in Eq. (A4) is represented by a tensor product of four operators, such as \( \hat{n}_i \otimes \hat{I}_2 \otimes \hat{I}_3 \otimes \hat{I}_4 \), where \( \hat{I}_i \) is the identity operator for the \( i \)th subsystem of \( \varphi_i \) and \( \hat{n}_i \). From the addition theorem, \( \cos(\varphi_i - \varphi_j - \Theta_{\text{ex}}) \) can be expressed as

\[
\cos \Theta_{\text{ex}} \left[ \hat{I}_1 \otimes \hat{I}_2 \otimes (\cos \varphi_3 \otimes \cos \varphi_4 + \sin \varphi_3 \otimes \sin \varphi_4) \right] + \sin \Theta_{\text{ex}} \left[ \hat{I}_1 \otimes \hat{I}_2 \otimes (\cos \varphi_3 \otimes \sin \varphi_4 - \sin \varphi_3 \otimes \cos \varphi_4) \right].
\]

In the matrix representation, \( \hat{I}_i \) is given by the \((2N + 1) \times (2N + 1)\) unit matrix and the tensor product \( \otimes \) is replaced by the Kronecker product of matrices. Thus, we obtain a \((2N + 1)^4 \times (2N + 1)^4\) matrix representation of the Hamiltonian in Eq. (A4). In this work, we choose \( N = 10 \) for sufficient convergence of energies.

Numerically diagonalizing the Hamiltonian matrix with \( \Theta_{\text{ex}} = 0 \), we can obtain the energies, \( E_{ij,kl} \), of the state \(|ij\rangle|kl\rangle\), where \(|ij\rangle\) and \(|kl\rangle\) denote the qubit state (Qubits 1 and 2) and the coupler state (Transmons 3 and 4), respectively. These energies lead to the ZZ-coupling strength \( \zeta_{ZZ} \) in Figs. 2 and 3(a). For example, the energies in the case of Fig. 3 are shown in Fig. 4. The qubit energies vary a little depending on \( \Theta_{\text{ex}} \). The slopes of the qubit-energy curves give the estimated values of \( T_2 \). Figure 4 also shows that the levels corresponding to the coupler excited states largely change by the flux and the other levels do not, as expected.

The simulation results of the CPHASE gate in Fig. 3 are obtained by numerically solving the Schrödinger equation with the Hamiltonian matrix. The average fidelity \( \bar{F}_{\text{CPHASE}} \) and rotation angle \( \theta_{\text{CPHASE}} \) of the CPHASE gate in Fig. 3 are obtained as explained in the next section.

**Appendix B: Average fidelity and rotation angle of the CPHASE gate**

The average gate fidelity is a standard metric for evaluating the performance of quantum gates. This is defined by averaging gate fidelities over uniformly distributed initial states. The average fidelities in Fig. 3(d) are obtained using the formula in Ref. 76, which is an extension of the formula in Ref. 77 to cases where there exist leakage errors and the norm of the qubit-subspace vector is not preserved. In the case of two-qubit gates, the formula for the average fidelity \( \bar{F} \) is given by

\[
\bar{F} = \frac{\text{tr} \left( U_{\text{id}}^\dagger U' \right)^2 + \text{tr} \left( U'^\dagger U' \right)}{20},
\]

where \( U_{\text{id}} \) is a \( 4 \times 4 \) unitary matrix corresponding to the ideal gate operation and \( U' \) is a \( 4 \times 4 \) matrix defined as follows. Suppose that we simulate the gate operation on four initial states each of which is one of the four two-qubit basis vectors denoted by \(|\psi_{ij}\rangle\) \((i, j = 0, 1)\). Using the resultant vectors \(|\psi_{ij}'\rangle\), \( U' \) is defined as \( U'_{2i+2j,2i'+2j'} = \langle \psi_{ij}' | \psi_{ij'} \rangle \). Note that \( U' \) is not a unitary matrix in general because of leakage errors. In the case of the CPHASE gate, we define \( U_{\text{id}} \)
as $U_{ij} = \text{diag}(e^{i\theta_0}, e^{i\theta_1}, e^{i\theta_2}, e^{i\theta_3})$, where diag(· · ·) represents a diagonal matrix and $e^{i\theta_k} = U_{k,k}^\dagger / |U_{k,k}|$. By eliminating the overall phase factor and single-qubit phase rotations from $U_{ij}$, we define the rotation angle of the CPHASE gate as $\theta_{\text{CPHASE}} = \theta_3 - \theta_1 - \theta_2 + \theta_0$.

**Appendix C: Flux pulse shape**

As shown in Fig. 4, higher energy levels $E_{00,10}$ and $E_{10,10}$ approach the qubit levels $E_{01,00}$ and $E_{11,00}$ respectively, around $\Theta_{\text{ex}} = \pi$. Thus, the infidelity of the CPHASE gate is mainly due to the leakage errors from $|01\rangle|00\rangle$ to $|00\rangle|10\rangle$ and from $|11\rangle|00\rangle$ to $|10\rangle|10\rangle$. To reduce these leakage errors, we design the flux pulse shape based on the technique proposed in Ref. 71. Here we explain how we designed the pulse shape shown in Fig. 3(b).

The technique is based on the two-level system, $|g\rangle$ and $|e\rangle$, with a constant coupling rate $g$ and a time-dependent detuning $\Delta(t)$, where the energy gap between the two energy eigenstates of this system is given by $h\omega_{\text{gap}} = h\sqrt{\Delta^2 + 4g^2}$. We first focus on the two levels of $|00\rangle$ and $|10\rangle$. In this case, we have $\omega_{\text{gap}} = (E_{00,10} - E_{10,00})/h$, and $2g$ is given by the minimum of $\omega_{\text{gap}}$. The energy gap is shown in Fig. 5 together with other energy gaps. From this, we obtain $g$ and the $\Theta_{\text{ex}}$ dependences of $\omega_{\text{gap}}$ and $\Delta$.

The two energy eigenstates are expressed as $\cos(\theta/2)|g\rangle - \sin(\theta/2)|e\rangle$ and $\sin(\theta/2)|g\rangle + \cos(\theta/2)|e\rangle$ with $\theta = \arctan(2g/\Delta)$. Then, the nonadiabatic error probability $P_e$ is approximately formulated as

$$
P_e \approx \frac{1}{4} \left| \int_0^{T_s} \frac{d\theta}{dt} e^{-i\int_0^t \omega_{\text{gap}}(t') dt'} dt \right|^2 = \frac{1}{4} \left| \int_0^{s_f} \frac{ds}{ds} e^{-i\omega_{\text{gap}}(s') ds'} \right|^2,
$$

where we have introduced a dimensionless time defined as $s(t) = \int_0^t \omega_{\text{gap}}(t') dt'$ [$s_f$ is defined as $s_f = s(T_g)$]. In this work, we set $\theta(s)$ as

$$
\theta(s) = \theta_0 + (\theta_1 - \theta_0)
\times \left( \frac{\cos \left( \frac{2\pi s}{s_f} \right) - 1}{\cos \left( \frac{4\pi s}{s_f} \right) - 1} \right),
\tag{C2}
$$

where $\theta_0 = \theta(0) = \theta(s_f)$ and $\theta_1 = \theta(s_f/2)$ are $\theta$ corresponding to $\Theta_{\text{ex}} = 0.61\pi$ and $\pi$, respectively, and the coefficient $A$ is set as $A = -0.17$ to achieve small $P_e$ and short $T_g$.

Using this $\theta(s)$, $t(s) = \int_0^s \omega_{\text{gap}}(s') ds'$, and the $\Theta_{\text{ex}}$ dependences of $\omega_{\text{gap}}$ and $\Delta$, we obtain the corresponding pulse shape $\Theta_{\text{ex}}(t)$.

However, we found that this pulse shape leads to relatively high leakage error probabilities from $|11\rangle|00\rangle$, though the energy gap between $|11\rangle|00\rangle$ and $|10\rangle|10\rangle$ is close to that between $|01\rangle|00\rangle$ and $|00\rangle|10\rangle$, as shown in Fig. 5. The leakage errors may be due to the smaller energy gap between $|11\rangle|00\rangle$ and $|02\rangle|00\rangle$ around $\Theta_{\text{ex}} = 0.61\pi$. Also, slower change of $\Theta_{\text{ex}}$ around $\Theta_{\text{ex}} = \pi$ may be more desirable for increasing the rotation angle, because the $ZZ$-coupling strength becomes maximum there. Inspired by these, we modified the energy gap used for $t(s) = \int_0^s \omega_{\text{gap}}(s') ds'$ as

$$
\begin{align*}
0.2 \left[ (E_{00,10} - E_{10,00}) / h - 2g \right] + 2g \cdots \Theta_{\text{ex}} \leq \Theta_{\text{ex}}^{(g)}, \\
2g \cdots \Theta_{\text{ex}} > \Theta_{\text{ex}}^{(g)},
\end{align*}
\tag{C3}
$$

which is shown by the bold solid curve (in blue) in Fig. 5, $\Theta_{\text{ex}}^{(g)}$ is $\Theta_{\text{ex}}$ satisfying $(E_{00,10} - E_{10,00})/h = 2g$. Thus, we obtain the pulse shape shown in Fig. 3(b).

**Appendix D: Parameter values in numerical studies**

The parameter values used for the present numerical studies are set as follows. Note that the present system can be regarded as a network of capacitively coupled four transmons, except for the interaction between Transmons 3 and 4 through the additional Josephson junction given by the last term in Eq. (4). The transmon network is quantized by the standard method using bosonic operators. Its Hamiltonian is given by

$$
\hat{H} = \sum_{i=1}^4 \left( \hbar \omega_i \hat{a}_i^\dagger \hat{a}_i - \hbar \frac{W_{ii}}{2} \hat{a}_i^2 \hat{a}_i^2 \right)
+ \sum_{i=1}^3 \sum_{j=i+1}^4 \hbar g_{ij} \hat{a}_i^\dagger \hat{a}_j + \hat{a}_j^\dagger \hat{a}_i,
\tag{D1}
$$

$$
\omega_i = \sqrt{\text{SW}_i \omega_j - W_{ii}},
\tag{D2}
$$

$$
g_{ij} = \frac{W_{ij}}{2} \sqrt{(\omega_i + W_{ii})(\omega_j + W_{jj})},
\tag{D3}
$$
where $\hat{a}_i$ and $\hat{a}_i^\dagger$ are the annihilation and creation operators, respectively, for the $i$th transmon. In this work, we set the transmon frequencies $\omega_i$ and capacitances as design values, as given in Fig. 2. The parasitic capacitances not shown in Fig. 1 are ideally set to zero, but this is impossible in actual experiments. Among the parasitic capacitances, $C_{34}$ is set to a relatively large value, because Transmons 3 and 4 are directly coupled via the Josephson junction with critical current of $I_{c5}$. On the other hand, the other parasitic capacitances, which comprise nonadjacent transmons, are set to small values, which may be feasible by placing the transmons as far from each other as possible. The other parameters are determined by their definitions, together with $\omega_{j5} = (\omega_{j3} + \omega_{j4})/8$ (a quarter of the mean value of $\omega_{j3}$ and $\omega_{j4}$). Table I summarizes the design values (shown in bold and resultant other parameter values used in this work. The anharmonicities (Kerr coefficients) of the transmons are given by $W_{ii}$, which are about 0.3 GHz.

**Table I.** Parameter setting for the present numerical studies. Bold values are design values. The others are calculated from their definitions using the design values.

| Parameter        | Value       |
|------------------|-------------|
| $\omega_1/(2\pi)$ (GHz) | 5           |
| $\omega_2/(2\pi)$ (GHz) | 5.7         |
| $\omega_3/(2\pi)$ (GHz) | 7.2         |
| $\omega_4/(2\pi)$ (GHz) | 8.5         |
| $C_{11}$ (fF)     | 60          |
| $C_{12}$ (fF)     | 0.025       |
| $C_{13}$ (fF)     | 6           |
| $C_{14}$ (fF)     | 0.05        |
| $C_{22}$ (fF)     | 60          |
| $C_{23}$ (fF)     | 0.05        |
| $C_{24}$ (fF)     | 6           |
| $C_{33}$ (fF)     | 60          |
| $C_{34}$ (fF)     | 1           |
| $C_{44}$ (fF)     | 60          |
| $g_{12}/(2\pi)$ (MHz) | 1.7         |
| $g_{13}/(2\pi)$ (MHz) | 239         |
| $g_{14}/(2\pi)$ (MHz) | 5.7         |
| $g_{23}/(2\pi)$ (MHz) | 6.5         |
| $g_{24}/(2\pi)$ (MHz) | 270         |
| $g_{34}/(2\pi)$ (MHz) | 57          |
| $W_{11}/(2\pi)$ (MHz) | 296         |
| $W_{12}/(2\pi)$ (MHz) | 0.19        |
| $W_{13}/(2\pi)$ (MHz) | 26.5        |
| $W_{14}/(2\pi)$ (MHz) | 0.63        |
| $W_{22}/(2\pi)$ (MHz) | 296         |
| $W_{23}/(2\pi)$ (MHz) | 0.63        |
| $W_{24}/(2\pi)$ (MHz) | 26.5        |
| $W_{33}/(2\pi)$ (MHz) | 291         |
| $W_{34}/(2\pi)$ (MHz) | 4.42        |
| $W_{44}/(2\pi)$ (MHz) | 291         |
| $\omega_{j1}/(2\pi)$ (GHz) | 11.9        |
| $\omega_{j2}/(2\pi)$ (GHz) | 15.2        |
| $\omega_{j3}/(2\pi)$ (GHz) | 24.1        |
| $\omega_{j4}/(2\pi)$ (GHz) | 33.2        |
| $\omega_{j5}/(2\pi)$ (GHz) | 7.2         |
| $I_{c1}/(2\pi)$ (nA) | 23.9        |
| $I_{c2}/(2\pi)$ (nA) | 30.6        |
| $I_{c3}/(2\pi)$ (nA) | 48.5        |
| $I_{c4}/(2\pi)$ (nA) | 66.8        |
| $I_{c5}/(2\pi)$ (nA) | 14.4        |

**Figure 6.** Single-transmon coupler. (a) Simplified diagram. (b) ZZ-coupling strength $\zeta_{ZZ}$ with $\omega_1/(2\pi) = 5$ GHz, $\omega_{j1}/(2\pi) = \omega_{j2}/(2\pi) = \omega_{j3}/(2\pi) = \omega_{j4}/(2\pi) = \omega_{j5}/(2\pi) = 250$ MHz, $g_{12}/(2\pi) = g_{23}/(2\pi) = 250$ MHz, $g_{12}/(2\pi) = 25$ MHz. The dashed yellow box indicates the region in the straddling regime.

### Appendix E: Single-transmon coupler

The conventional single-transmon coupler is shown in Fig. 6(a), in which the dc SQUID for the frequency-tunable transmon in the coupler is replaced by a single Josephson junction for simplicity. Figure 6(b) shows the ZZ-coupling strength, $\zeta_{ZZ}$, of the coupler with typical parameter values [43]. Note that ZZ-coupling vanishing points [the white region in Fig. 6(b)] exist only in the straddling regime [the dashed yellow box in Fig. 6(b)]. Thus, the single-transmon coupler cannot realize zero ZZ coupling for highly detuned qubits. This is an essential contrast to the proposed double-transmon coupler.

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Recently, couplers with a flux qubit, instead of a frequency-tunable transmon, have been proposed \[65\]. These use three or more Josephson junctions, like our double-transmon coupler. However, they are rather similar to the single-transmon coupler, and notably different from the double-transmon coupler.

This qualitative and classical explanation under rough approximations describes how we found the concept of the double-transmon coupler. While this will be helpful for intuitive understanding of the mechanism, we must investigate the coupler in a more accurate manner for evaluating its performance, which is presented later.

\[66\] \(\hbar\) and \(\phi_0 = \Phi_0/(2\pi)\) are, respectively, the reduced Planck constant and the reduced flux quantum (\(\Phi_0\) is the flux quantum).

This holds when the loop self-inductance is negligible.

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We found this fact by numerical studies. Its theoretical explanation is desirable, but left for future work.

\[69\] We choose the parameters in Fig. 2(a) (out of the straddling regime), because in this work, we are interested in highly detuned qubits. We also choose \(\omega_4/(2\pi) = 8.5\) GHz as a relatively low value among the values satisfying the zero ZZ coupling. (We avoid the lower-bound value (about 8.3 GHz), because this may be not robust against small errors in parameter values.)

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When there are more qubits, gate operations on other qubits will affect the performance, in particular, the zero ZZ coupling. This is an important issue, but its simulations need massive computations. Therefore, the study on this issue is left for future work.

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