Intrinsic Zero-Linear and Zero-Area Compressibility over an Ultra-Wide Pressure Range within a “Gear-Spring” Structure

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Article

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Abstract

Materials with zero-linear compression (ZLC) and zero-area compression (ZAC) hold great promises for specific applications retaining constant in specific directions or planes under external impaction. Up to now, no more than ten ZLC/ZAC materials have been reported, most of which are of very limited working pressure ranges (< 10 GPa). Herein, we report the observation of concurrent ZLC and ZAC in Li$_2$Ti(IO$_3$)$_6$ with a “Gear-Spring” type structure over an ultra-wide pressure range (0 ~ 40 GPa). Structure analysis reveals that the rotatable metal coordination polyhedra (gears) and extremely compressible metal chains (springs) work together to form an exquisite mechanical unloading device with intrinsic ZLC and ZAC behavior. Moreover, Li$_2$Ti(IO$_3$)$_6$ sets a record-wide ZLC/ZAC working pressure range (up to 40 GPa) among anisotropic compression materials. The demonstration of intrinsic and long-lasting ZLC/ZAC with a “Gear-Spring” mechanism paves the way to shock-resistant precision optics applied under extreme conditions.

Introduction

Substances normally contract under external hydrostatic pressure, just as they expand with heat and contract with cold.\textsuperscript{1,2} From the perspective of thermodynamics, it is impossible for a given material exhibiting negative volume compressibility.\textsuperscript{3} Nevertheless, there are several types of materials possessing negative compressibility in specific crystalline directions or planes, while the overall cell volume keeps decreasing under compression.\textsuperscript{4-6} In the past decades, materials with negative linear compressibility (NLC) and negative area compressibility (NAC) have been widely explored with specific mechanisms, such as “wine-rack”, honeycomb networks, and Lifshitz model.\textsuperscript{7-9} In general, zero linear compressibility (ZLC) and zero area compressibility (ZAC) can be easily achieved by finding a balance between negative and positive compressibility, and the linear and area compressibility of diamond and Os are used as standard to classify a ZLC or ZAC material.\textsuperscript{10-13} ZLC and ZAC materials are ideal candidates for precision instruments applied under extreme environments, such as submarine fiber-optic communication and shock-resistant optical windows.\textsuperscript{1,14,15} Surprisingly, material with ZLC or ZAC has been rarely discovered compared with those of NLC and NAC property.\textsuperscript{9,10,16-19} Meanwhile, there lacks clear structure-property mechanism for the rational design of ZLC/ZAC materials.

In the decade’s exploration of materials with abnormal compressibility, remarkable findings have been concentrated in two types of materials: metal-organic frameworks (MOFs) and all-inorganic frameworks.\textsuperscript{4} The most important strategy to achieve materials with abnormal compressibility is to establish clear and instructive structure-property relationship. The diverse organic units endow MOFs the ability to exhibit flexible mechanical responses under compression,\textsuperscript{20-23} including both large NLC and near-ZLC. The “wine racks” structure model is the most popular mechanism describing the NLC and near-ZLC behaviors in MOFs. Particularly, “molecular gears and torsion springs” structure model is proposed to describe the NLC and extreme compressibility of $LnFe(CN)_6$ ($Ln = Ho, Lu$ or Y), which benefit from the $LnN_6$ torsion springs and the rigid Fe(CN)$_6$ gears.\textsuperscript{24} However, MOFs are soft and usually show above-mentioned abnormal
compressibility within a very narrow pressure range, typically no more than 10 GPa, which greatly limits their potential applications. Comparatively, all-inorganic frameworks such borates possessing covalently-bonded frameworks are less compressible. Although up to now the highest pressure of ZLC is 8 GPa in (Ca,Sr)B$_2$O$_4$, from the viewpoint of structural chemistry, they are still good candidates with abnormal compressibility in a relatively wide pressure range. In addition, all-inorganic frameworks can have good chemical/physical stability and excellent optical performances, which makes them potential for next-generation shock-resistant optical windows and fiber communications. Unfortunately, there lacks clear mechanism for the rational design of all-inorganic frameworks with abnormal compressibility. An exception is the recently reported “Lu-Ban Stool”-like model for (Ca,Sr)B$_2$O$_4$, in which the subtle counterbalance originated from the expansion and contraction effect between the rotation of the [BO$_3$] “planks” and the shrinkage of Ca-O “legs” attributes to an excellent ZLC property.

We are aiming at exploring all-inorganic optical materials with both excellent ZLC/ZAC properties and good chemical/physical stabilities by structure design strategy. Numerous known inorganic compounds in the ICSD database have been screened to look for framework-like structures, among which a unique family of transition metal iodates with metal-metal bonding and chains are identified potential for ZLC/ZAC behavior. Herein, we report the anomalous mechanical responses of Li$_2$Ti(IO$_3$)$_6$ to external pressure as a representative of inorganic framework structure. The anisotropic compressibility of Li$_2$Ti(IO$_3$)$_6$ was examined by using in-situ X-ray diffraction (XRD), Raman spectra, and first-principles calculations. A "Gear-Spring" mechanism was proposed responsible for the emerging intrinsic ZLC/ZAC properties, which sheds light on the future structure design of all-inorganic materials with anomalous compressibility.

**Results And Discussion**

**Material and Ambient Crystal Structure.** Phase-pure Li$_2$Ti(IO$_3$)$_6$ were obtained by hydrothermal method as both white powders and transparent single crystals. At ambient conditions, Li$_2$Ti(IO$_3$)$_6$ crystallizes in the hexagonal space group $P\overline{6}$_3 with cell parameters of $a = 9.372$ Å, $c = 5.113$ Å (Fig. S1). Fig. 1a shows the crystal structure of Li$_2$Ti(IO$_3$)$_6$ consisting of face-sharing TiO$_6$ chains along the $c$-axis, distorted IO$_3$ units and LiO$_6$ octahedra. The structure is noncentrosymmetric with a very strong second harmonic generation (SHG) efficiency of $\sim 500 \times \alpha$-SiO$_2$, comparable to those of BaTiO$_3$ (400 $\times \alpha$-SiO$_2$) and LiNbO$_3$ (600 $\times \alpha$-SiO$_2$). Both the Ti$^{4+}$ and I$^{5+}$ cations are located within asymmetric coordination environments due to the second-order Jahn-Teller effects. The parallel alignment of the lone pair electrons on the I$^{5+}$ cations contributes mostly to the macroscopic polarity of Li$_2$Ti(IO$_3$)$_6$ (Fig. S2). Notably, each TiO$_6$ octahedron links with six IO$_3$ polyhedra to form a large anionic $[(\text{TiO}_{6/2})^2-6(\text{IO}_{1/2}\text{O}_{2/1})^0]^2-$ “cylinder” in the $ab$ plane, and these nano-cylinders are separated by six-coordinated Li$^+$ cations to achieve charge balance. In such an inorganic framework, the “cylinders” are expected to have the ability to “rotate” around the Ti-Ti axis since the connection manner between (TiO$_{6/2}$)$^2-$ and six (IO$_{1/2}$O$_{2/1}$)$^0$ is corner-sharing. Thus, one can
consider the anionic \([\text{TiO}_{6/2}]^{2-} \cdot 6(\text{IO}_{1/2} \text{O}_{2/1})^0\] to be a rigid “roller”. Previous studies have preliminarily verified the anomalous compressibility of similar metal iodates such as Fe(\text{IO}_3)_3 and Zn(\text{IO}_3)_2.\textsuperscript{28,29} We have enough reasons to expect peculiar mechanical responses of \(\text{Li}_2\text{Ti(\text{IO}_3)_6}\) to external pressure.

**Structure Evolution of \(\text{Li}_2\text{Ti(\text{IO}_3)_6}\) under High Pressure.** *In-situ* high-pressure XRD measurements were conducted to study the compressibility of \(\text{Li}_2\text{Ti(\text{IO}_3)_6}\) with the “inorganic-framework” structure (Fig. 1b). No obvious structural phase transition is observed under compression up to 40.2 GPa since there is only peak shift instead of new peak emerging or disappear, and the pressure effect on the crystal structure is reversible (Fig. S3). Different Bragg peaks exhibit obviously distinct shift behaviors under compression, implying an extremely anisotropic compressibility along different crystallographic axes. Among them, the \((hk0)\) peaks such as \((20)\) and \((300)\) basically keep their \(2\theta\) values unchanged, indicating an incompressibility or minimal compressibility along the \(a\) and \(b\) axes. Specifically, the \((hk0)\) peaks shift slightly to lower \(2\theta\) angle first in the 0~8 GPa range \((i)\), and then slightly to higher \(2\theta\) angle in the 8~19 GPa \((ii)\), and finally to lower \(2\theta\) angle again above 19 GPa \((iii)\) (Fig. S4). By contrast, the \((hkl)\) peaks such as \((21)\) with \(l \neq 0\) shift quickly to higher \(2\theta\) angle under compression up to 40 GPa, indicating a large compressibility along the \(c\) axis.

Fig. 1c and Table S1 displays the refined cell parameters of \(\text{Li}_2\text{Ti(\text{IO}_3)_6}\) as functions of applied pressure. The extremely anisotropic compression behavior is evident. The evolution of the \(a\) axis has gone through three pressure regions in accordance with the peak shift of the \((hk0)\) planes. Notably, the overall change of the \(a\) axis \((\Delta a)\) in the 0~40.2 GPa region is as low as 0.97%, a low enough value to be regarded as ZLC. Due to the hexagonal symmetry of space group \(P\overline{6}_3\) with \(a = b\), the \(ab\) plane exhibits similar compression behavior with individual \(a\) and \(b\) axes, i.e. the overall area change of the \(ab\) plane \((\Delta s)\) in the 0~40.2 GPa is as low as 1.95%, which is also a low enough value to be ZAC. Comparatively, \(c\) axis exhibits tremendous compressibility with \(\Delta c = 28.69\%\) at 40.2 GPa, and a normal \(V-P\) curve is obtained in the whole pressure range.

**Table 1.** The compressibility and pressure range in all reported ZAC/ZLC materials.
| Material                  | Mechanism       | $K_l$(TPa$^{-1}$) | $K_s$(TPa$^{-1}$) | $P$(GPa) | Ref. |
|---------------------------|-----------------|-------------------|-------------------|----------|------|
| MIL-122(In)               | “Wine-rack”     | 0                 | /                 | 0~10.5   | [18] |
| [C(NH$_2$)$_3$][Cd(HCOO)$_3$] | “Wine-rack”     | 0.75              | 1.51              | 0~0.5    | [17] |
| SrB$_2$O$_4$              | “Lu-Ban Stool”  | -0.47             | /                 | 0~8.0    | [10] |
| CaB$_2$O$_4$              | “Lu-Ban Stool”  | 0.34              | /                 | 0~8.1    | [10] |
| LiBO$_2$                  | “Corrugated-graphite” | 1.54            | /                 | 0~2.5    | [16] |
| RbBe$_2$BO$_3$F$_2$       | “Lifshitz”      | 0.05              | 0.1               | 0~2.6    | [9]  |
| CsBe$_2$BO$_3$F$_2$       | “Lifshitz”      | -0.03             | -0.07             | 0~3.2    | [9]  |
| GeO$_2$                   |                 | 0.08              | /                 | 0~8.0    | [19] |
| Dimond                    | Superhard       | 0.62              | 1.23              | 0~45.0   | [11] |
| Os                        | Superhard       | 0.60$^a$          | 1.02              | 0~63.8   | [13] |
|                           |                 | 0.54$^c$          |                   |          |      |
| Li$_2$Ti(IO$_3$)$_6$       | “Gear-Spring”   | 0.24              | 0.48              | 0~40.2   | This work |

**ZLC and ZAC of Li$_2$Ti(IO$_3$)$_6$.** The linear compressibility ($K_l$) has been defined as $-\Delta l/l\Delta p$ to evaluate the strength of mechanical response to external pressure of a given material. Fig. 1d represents the pressure-dependent linear compressibilities ($K_{a/b}$ and $K_c$) of Li$_2$Ti(IO$_3$)$_6$, derived using the online PASCaI package and within three above-discussed pressure ranges ($i$, $ii$, $iii$). It is interesting to see that $K_{a/b}$ keeps very small values throughout the whole pressure range. The calculated values for individual pressure ranges are: $K_a = 1.06$ TPa$^{-1}$ and $K_c = 10.54$ TPa$^{-1}$ for $i$, (0~8 GPa); $K_a = -1.88$ TPa$^{-1}$ and $K_c = 14.84$ TPa$^{-1}$ for $ii$, (8~19 GPa); $K_a = 0.58$ TPa$^{-1}$ and $K_c = 1.78$ TPa$^{-1}$ for $iii$, (19~40.2 GPa), respectively (Fig. S5). Notably, the positive $K_a$ in the $i$ (0~8 GPa) range and the negative $K_a$ in the $ii$ (8~19 GPa) range yield a very small $K_a$ value of -0.23 TPa$^{-1}$ in the $i$+$ii$ region (0~19 GPa). According to the previous definition, compounds with absolute value of $K_l$ less than those of diamond (0.75 TPa$^{-1}$) and Os (0.70 TPa$^{-1}$) can be considered as ZLC materials. Thus, Li$_2$Ti(IO$_3$)$_6$ is a novel ZLC material in both $a$ and $b$ directions in the pressure range of 0~40.2 GPa. Of course, Li$_2$Ti(IO$_3$)$_6$ is also a novel ZAC material since the area change of the $ab$ plane ($\Delta s$) is as low as 1.95% within 0~40.2 GPa.

The online PASCaI package is found only applicable to those cases with either a positive or a negative $K_l$. To calculate the total $K_f$ for our case with both positive and negative linear compressibilities in a pressure range, we simply use the most primitive formulas ($K_f = -\Delta l/l\Delta p$ and $K_s = -\Delta s/s\Delta p$) to evaluate the linear and area compressibilities, where $l$ represents the length of the starting unit cell, $s$ represents the area of [28x4393]
the initial crystal plane, $\Delta l$, $\Delta s$ and $\Delta p$ represents the changes of linear, area and pressure, respectively. The recalculated $K_l$ and $K_s$ in the pressure range of 0~40.2 GPa are provided in Fig. S6, and the compressive properties of representative ZLC/ZAC materials including the superhard diamond and Os as references are concluded in Table 1.

First of all, Li$_2$Ti(IO$_3$)$_6$ possesses relatively small $K_l$ (0.24 TPa$^{-1}$) and $K_s$ (0.48 TPa$^{-1}$) within these materials including diamond ($K_l = 0.62$ TPa$^{-1}$, $K_s = 1.23$ TPa$^{-1}$) and Os metal ($K_l = 0.54/0.60$ TPa$^{-1}$, $K_s = 1.02$ TPa$^{-1}$), making it worthy of ZLC and ZAC material. Remarkably, inorganic ceramics or crystalline materials with both ZAC property and transparency in important wavelengths are rather rarely reported up to now, which holds great promise for practical shock-resistant optical usages. Secondly, Li$_2$Ti(IO$_3$)$_6$ exhibits ZLC and ZAC in an ultra-wide pressure range, i.e. 0~40.2 GPa, compared with ZLC/ZAC MOFs and metal borates. 40.2 GPa may not be the highest pressure value for Li$_2$Ti(IO$_3$)$_6$ to survive, nevertheless, this value still refreshes the world record of ZLC/ZAC material (except diamond and Os). At last, as we know, there are several structural mechanisms for previously discovered ZLC/ZAC materials, such as “Wine-rack” for MOFs, “Lu-Ban Stool”/”Corragated graphite”/”Lifshitz” for some borates, and superhard for diamond and Os, respectively. However, Li$_2$Ti(IO$_3$)$_6$ does not belong to any of the above-mentioned mechanisms.

**Intrinsic ZLC/ZAC in “Gear-Spring” structures.** The crystal structure of Li$_2$Ti(IO$_3$)$_6$ can be vividly regarded as a “Gear-Spring” type. As shown in Fig. 2a, the visualized “Gear-Spring” model of Li$_2$Ti(IO$_3$)$_6$ comprises of Gear-A (the anionic [(TiO$_6/2^2\cdot6$(IO$_1/2O_2/1)^0]^2$), Gear-B (LiO$_6$ octahedra), and an extremely compressible spring (Ti-Ti distances or $c$). This model is completely derived from the real crystal structure and can describe and explain the ZLC/ZAC phenomena of Li$_2$Ti(IO$_3$)$_6$ perfectly.

The parameters of the “Gear-Spring” model, gear radii (r(Gear-A), r(Gear-B)), spring length ($c$) and rotation angles ($\theta$(Gear-A), $\theta$(Gear-B)) were derived from structure optimization using the experimental cell parameters of Li$_2$Ti(IO$_3$)$_6$ under various pressures. As rigid “gears”, the sizes of “Gear-A” and “Gear-B” should basically remain unchanged, which has been perfectly validated by the calculation results (Fig. 2b). In the meantime, the spring length ($c$) decreases rapidly along with the increasing of applied pressure, working together as real springs. It is really amazing that the two gears (A and B) can rotate synergistically either in the direction or angles (Fig. 2c). A little different from the previously derived three pressure regions ($i$, $ii$, $iii$) of the cell parameter evolution, four rotation processes are observed under compression: ($i$) A$^+$ (counterclockwise)B$^-$ (clockwise) in 0~9 GPa, ($ii$-a) A$^+$B$^+$ in 9~14 GPa, ($ii$-b) A$^+$B$^+$ in 14~17 GPa, and ($iii$) A$^0$B$^0$ in 17~40 GPa, respectively. It is reasonable to believe that the rotation of the gears can convert the external pressure to the compression direction of the spring.

Fig. 2d displays the representative structures of the TiO$_6$-chain at 0 GPa and the highest pressure 40.2 GPa. The working mechanism of the “spring” is clear from the dramatic changes of the Ti-Ti distances and Ti-O-Ti bond angles. The $c$ value (spring length) is reduced from 5.07 Å to 3.63 Å, together with highly flattened Ti-O-Ti angle (from 81.3° to 52.4°) but almost unchanged Ti-O bondlengths (from 1.92/2.01 Å
to 2.04/2.07 Å). The detailed changes of individual bondlengths during the “Gear-Spring” working process under compression are displayed in Fig. 2e, 2f. Both the Ti-Ti distances and Ti-O-Ti angles exhibit similar changes under compression up to 40 GPa, and there is no distortion from the Ti-O bondlengths within TiO$_6$ octahedra. The average bondlengths of I-O and Ti-O also show cooperative changes under high pressure to maintain the size of Gear-A unchanged. In brief, the emerging ZLC/ZAC phenomena in Li$_2$Ti(IO$_3$)$_6$ can be perfectly explained by the “Gear-Spring” mechanism. Materials with such a “gear” and “spring” cooperation structure are expected to have intrinsic ZLC/ZAC properties, and also in an ultra-wide pressure range.

The local structure evolution of Li$_2$Ti(IO$_3$)$_6$ during ZLC/ZAC processes are probed by in-situ high-pressure Raman spectra (Fig. S7). Firstly, the Raman profile basically remains unchange under compression except gradual shifts of the peaks, indicating the absence of structural phase transition. The peaks located in the ranges of 400-600 and 600-850 cm$^{-1}$ can be assigned to the stretching vibration modes of [TiO$_6$] octahedra and [IO$_3$] pyramids, respectively. The softening of the [IO$_3$] peaks (shift continuously to lower wavenumber) indicates the elongation of the I-O bonds. Besides, we also measured the SHG efficiency of Li$_2$Ti(IO$_3$)$_6$ powders under high pressure (Fig. S8). It is interesting to find that Li$_2$Ti(IO$_3$)$_6$ keeps to be SHG-active up to 40.2 GPa. The long-lasting SHG functionality combined with intrinsic ZLC/ZAC properties within an ultra-wide pressure range makes Li$_2$Ti(IO$_3$)$_6$ a unique candidate for optically sensitive devices under extreme conditions.

**Conclusion**

In summary, we report intrinsic ZLC and ZAC properties in an all-inorganic iodate material Li$_2$Ti(IO$_3$)$_6$. The ultra-wide working pressure range (0~40.2 GPa) of Li$_2$Ti(IO$_3$)$_6$ sets a new record for artificial ZLC or ZAC materials (except diamond and Os). Based on structure analyses, we proposed a novel “Gear-Spring” mechanism that can describe and explain the anomalous compression behavior of Li$_2$Ti(IO$_3$)$_6$ perfectly. We are confident to predict anomalous compression properties (including intrinsic ZLC and ZAC) in compounds with such a “Gear-Spring” structure. Moreover, Li$_2$Ti(IO$_3$)$_6$ maintains its nonlinear optical functionality along with ZLC/ZAC behavior to high pressure, which makes it promising for special optical devices under extreme environments.

**Methods**

**Sample preparation.** Reagents: Li$_2$CO$_3$ (Aladdin, 99.99%), TiO$_2$ (Aladdin, 99.99%), HIO$_3$ (Aladdin, 99.99%). Powders and single crystals of Li$_2$Ti(IO$_3$)$_6$ were synthesized by hydrothermal method. Li$_2$CO$_3$ (0.30 g, 4.06 × 10$^{-3}$ mol), TiO$_2$ (0.300 g, 3.76 × 10$^{-3}$ mol), HIO$_3$ (5.00 g, 2.84 × 10$^{-2}$ mol) and water (10 mL) were put in a 23 mL Teflon-lined stainless steel autoclave and heated to 230 °C for 4 days followed by cooling to room temperature with the rate of 3 °C/h. Transparent, colorless crystals and white powder of Li$_2$Ti(IO$_3$)$_6$ were washed by water and ethanol, and dried at 70 °C overnight.
High-pressure generation. A symmetric diamond-anvil-cell (DAC) was used to produce high pressure. T301 steel gaskets were pressed to the thickness of about 35 μm, and then 180 μm holes were drilled as the sample chambers. Compact sample and a ruby ball were thrown into the sample chamber. Silicone oil was employed as the pressure medium. The pressure was calibrated based on the fluorescence peak of ruby ball.\textsuperscript{31}

High-pressure XRD measurement. \textit{In-situ} high-pressure XRD experiments were recorded at the 4W2 High Pressure Station in Beijing Synchrotron Radiation Facility (BSRF) with a beam wavelength of 0.6199 Å at room temperature. A Mar345 image plate was used to record the \textit{in-situ} high-pressure XRD patterns, and CeO\textsubscript{2} was chosen as the calibration standard. DIOPTAS software was used to execute the data reduction.\textsuperscript{32} Cell parameters under different pressures were refined by Rietveld method using the FULLPROF software.\textsuperscript{33} The compressibility was calculated by the empirical function $l = l_0 + \lambda (p - p_c)\nu$ via the online program PASCal (http://pascal.chem.ox.ac.uk/).\textsuperscript{30}

High-pressure Raman measurement. \textit{In-situ} high-pressure Raman spectra were recorded on a Renishaw Raman microscope using a 532 nm laser. The system was calibrated by the Raman signal of Si, and spectra were collected in the range of 100-1100 cm\textsuperscript{-1}.

High-pressure SHG measurement. \textit{In-situ} high-pressure SHG experiment was measured in a home-designed optical system. A fiber laser (NPI LASERCo., Ltd, 1064 nm, 20MHz, 15 ps) was used as the exciting light source, and the laser spot was focused to 40 μm. A photomultiplier tube (Thorlabs, Inc., PMT1000) was employed to collect the SHG signal. The high-pressure SHG measurement is based on the ambient powder SHG measurement extended by Kurtz and Perry.\textsuperscript{34}

First-principles calculation. The first-principles calculation was performed using the CASTEP package.\textsuperscript{35} Structure optimization at various pressure points was performed adopting the experimental cell sizes with all the atomic positions relaxed.

Data availability

The data that support the findings of this study are available in the Supplementary Information (experimental data and characterization data). All raw data and analysis files used in the study are available upon request from the authors.

Declarations

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Author contributions

D.J., T.W. and Y.W. conceived the idea and led the project. D.J. and H.S. conducted the synthesis, crystal growth and structure refinement. Z. J. and W.T. performed high-pressure XRD measurement. C.L. and K. L. performed high-pressure Raman and SHG measurements. D.J., T.W. and Y.W. wrote the manuscript with help from W.Y. and H.M. All authors discussed and revised the manuscript.

Competing interests

The authors declare no competing interests.

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**Figures**
Figure 1

Crystal structure and compression behavior of Li$_2$Ti(IO$_3$)$_6$. (a) Hexagonal structure of Li$_2$Ti(IO$_3$)$_6$ at ambient conditions, consisting of face-sharing TiO$_6$ chain (dark gray) along the c-axis, distorted IO$_3$ units (light gray) and LiO$_6$ octahedra (blue). (b) XRD patterns of Li$_2$Ti(IO$_3$)$_6$ at high pressures. The anisotropic compressibility is evident without structural phase transition. (c) Cell parameters and volume as functions of pressure, showing intrinsic ZLC and ZAC behavior along the a/b directions and in the ab plane, respectively. The dotted lines represent the change of cell parameters and volume within a very small range (±1%). (d) Pressure-dependent linear compressibilities (Ka/b and Kc) of Li$_2$Ti(IO$_3$)$_6$, calculated using the online PASCAL package.30
Figure 2

“Gear-spring” mechanism for ZLC/ZAC under compression. (a) Visualized “Gear-spring” structure of Li$_2$Ti(IO$_3$)$_6$, comprising of Gear-A (the anionic [(TiO$_6$/2)$^2-$·6(IO$_{1/2}$O$_{2/1}$)$_0$]$^2-$), Gear-B (LiO$_6$ octahedra), and the extremely compressible spring-length (Ti-Ti distances or c). (b) Evolutions of the size and length of Gear-A, Gear-B, and spring under compression. The “gears” are expected to keep their sizes and the “springs” are expected to exhibit extreme large compressibility. (c) Pressure-dependent rotations of Gear-A and Gear-B. “+” indicates anticlockwise and “−” indicates clockwise. (d) Representative structures of the TiO$_6$-chain at 0 GPa and 40.2 GPa, showing the working mechanism of the “spring”. (e, f) Bond-length and bond-angle evolutions in the “Gear-Spring” structure of Li$_2$Ti(IO$_3$)$_6$ under compression.

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