Effect of the ammonia concentration on the performance of wetland microbial fuel cells

Li Wang¹*, Jiafeng Fu², Wenlei Wang¹, Yutong Song¹, and Yan Li¹

¹Harbin Institute of Technology, School of Energy Science and Engineering, 150001, Harbin, China
²Harbin Guanghan Gas Turbine Co., Ltd, 150070, Harbin, China

Abstract. This work explores the effect of the ammonia concentration on the wetland synthesis of microbial fuel cell (MFC) and on the production and the efficiency of sewage purification. Four ammonia concentrations from 1 to 30 mg/L have been selected. Under the fixed condition of a chemical oxygen demand (COD) concentration of 200 mg/L, a constructed wetland microbial fuel cell (CW-MFC) could be built. The results show that by selecting the optimum ammonia concentration the production of the CW-MFC could be promoted; a higher ammonia concentration (>20 mg/L) is found to inhibit the production activity of CW-MFC. In the optimum conditions, Cathode and anode thickness is 10 cm, the ammonia concentration is 10 mg/L, the COD concentration of 200 mg/L, the maximum power density of the battery is 13.6 W/m², the corresponding current density is 148.6 A/m² and the battery internal resistance is 270 Ω. At the ammonia nitrogen concentration of 10 mg/L, the removal rates of ammonia nitrogen and COD were up to 89.7% and 98.47% respectively. As the ammonia nitrogen concentration increased to 30 mg/L, the ammonia nitrogen and COD removal rates decreased to 74.6% and 90.69% respectively. That is, when the ammonia nitrogen concentration is 10 mg/L, CW-MFC can exhibit the best performance.

1 Introduction

The wetland microbial fuel cell is a new type of water purification device, which combines an artificial wetland with a microbial fuel cell; the anaerobic oxidation of organic matter at the anode is promoted by a microbial metabolism under electrical bias [1-3]. When the plant root is located at the cathode region, the bio-cathode composite electrode material forms a plant-microbial-electrode material; the use of plant rhizosphere oxygen at the cathode provides for the reduction reaction of electron acceptors, and an oxidizing microenvironment is formed in the reduced matrix around the root system [4,5]. To reduce the operating costs there is an urgent requirement for developing improved cathodic aeration devices. At the same time, the use of plant composite bio-cathodes instead of precious metal cathodes as in the conventional CW-MFC, would allow to greatly reduce the electrode material costs, possibly improve the catalytic activity of the electrode and allow for the large-scale production of CW-MFCs [6-8].

For the development of large-scale CW-MFC, the high cost of the infrastructure and the too low power generation are the two main problems; the cathode material plays a key role in these problems, because of its high cost and slow redox reaction. In order to overcome these bottlenecks, it is necessary to develop suitable cathode based on an easy preparation method, cheap and ensuring a high catalytic activity. Recently, it has been shown that aerobic biofilms are capable of efficiently catalyzing redox reactions [9], while ensuring low cost, self-regeneration of the catalyst, sustainability and good activity at neutral pH; for these reasons, the study of biological cathodes has attracted a wide interest [10]. Compared with inorganic cathodes, the bio-cathode is promising in the CW-MFC application.

Many previous studies have shown that when the rhizosphere is located in the anode chamber of the CW-MFC, the plant root exudates (sugar, organic acid, polymeric carbohydrates, dead cell material, etc.) can be used as organic matter to generate electricity [5,11]. In addition, the plant has the unique ability to release oxygen and root exudates into the rhizosphere and the oxygen secreted by the plant roots can be used as an electron acceptor for the CW-MFC to undergo redox reactions [12,13].

Researchers have also carried out studies on water quality parameters; Qian Dandan [14] found that at the optimum glucose concentration of 60 mg/mL, they could obtain the best battery performance with a maximum voltage and power density of 224.8 mV and 505 mW/m². Jin Xiaojun [15] studied on the influence of chemical oxygen demand (COD), shown that an anodic denitrifying MFC (MFC-D) exhibited better COD removal capability and power density than MFC without denitrification (MFC-C), and MFC-D obtained the highest coulombic efficiency of electricity generation and anodic denitrification when the value of COD/N ratio is about 5:1; Kong Xiaoying [16] studied the effects of different substrates on the electricity production performance of microbial fuel cells. The experiment found that the simpler the substrate, the smaller the

* Corresponding author: liwanghit@126.com
internal resistance and the higher the output power. However, few reports have been devoted to the study of the ammonia concentration on the performance of the MFC and of the sewage treatment; the purpose of this study is thus to clarify the effect of the ammonia concentrations on the battery performance. Because the addition of ammonia nitrogen affects the electron-capacitating ability of the cathode of CW-MFC, the cathode electrons accumulate in a large amount, which is not conducive to MFC operation. So this experiment studied the COD variation and ammonia removal for wastewater treatment, and evaluated the output voltage output, power density, current density and coulomb efficiency of the battery.

There are many factors that affect the performance, including Substrate concentration, COD concentration, substrate type, etc. In this paper, carbon felts and a copper net have been used as the cathode, bamboo as the wetland plant, allowing to build a single chamber vertical flow of microbial fuel cells. We have determined the optimum ammonia concentration in the substrate for the microbial fuel cell to provide guidance to next research materials.

2 Materials and methods

2.1 Experimental equipment and materials

The CW-MFC system used in this work is made of plexiglass cylinders with an inner diameter of 19 cm, a total height of 58 cm; Below is the anode part, above is the cathode part, the total volume of the reactor is 14.75 L, the effective storage capacity is 7.1L, set the sampling port at the bottom 20cm, 30cm, 40cm, the upper part contains the water outlet; the filling matrix stacks and the electrode materials are: (from the bottom to the top) a 10 cm thick ceramic, and three repeated cycles of a 5 cm thick quartz sand layer and a 5 cm thick activated carbon particles embedded in a carbon felt electrode. Planting rich bamboo in the cathode. The average size of the activated carbon particles is 4 mm, the specific surface area of the ceramic is 900-1000 m²/g the ceramic particle size is 3-5 mm and the quartz sand particle size is 3-6 mm. Before filling the electrode material, all materials have been washed with water and dilute hydrochloric acid (1mmol/L) [17]. From the bottom of the filled barrel there are three anodes and then a cathode: the area of the anode is 78.5 cm². Electrode materials are based on carbon felt and copper mesh, combined with a copper wire. The Copper mesh number is 25, with a 3 mm diameter copper wires which are connected to an external 1 kΩ resistor to form a closed circuit. In the reactor, the temperature is controlled at 27 ± 3 °C. The schematic diagram of the setup is shown in Figure 1. The physical map is shown in Figure 2.

2.2 Wastewater treatment and inoculation of the sludge

The composition of the artificial wastewater at the device starting conditions and during normal operation is shown in Table 1; during the operation the pH value is adjusted between 7.0 and 7.5 by adding NaHCO₃. The
sewage through the peristaltic pump (BT100M) is continuously delivered to the CW-MFC reactor, from bottom to top, with a water flow of 4.93 mL/min and a hydraulic retention time of 24h. When the system is blocked or the system is backwashed every 6 months, the sludge will be flushed out and the biofilm needs to be re-attached, during which there will be biomass loss. The CW-MFC receives the sludge from the Harbin sewage. 1.5 L of sludge are injected into the reactor for the culture of the system biofilm. For the device filled with water, the water was stopped for 1 day, so that the sludge and the carrier could fully mix.

### Table 1. Composition of the synthetic wastewater

| Reagent name | concentration (mg/L) |
|--------------|----------------------|
| Glucose      | 250                  |
| KNO₃         | 252.5                |
| K₂PO₄·3H₂O   | 26.32                |
| NaHCO₃       | 224                  |
| NaCl         | 330                  |
| (NH₄)₂SO₄    | -                    |
| MgSO₄·7H₂O   | 0.2                  |
| CaCl₂        | 0.015                |
| FeCl₃·3H₂O   | 0.001                |
| MnSO₄·H₂O    | 0.202                |
| CoCl₂·6H₂O   | 0.0001               |
| ZnSO₄·7H₂O   | 0.00005              |

2.3 Testing and calculation methods

The output voltage (U) is measured with a multimeter. The current (I) in the circuit is calculated by using Ohm’s law: the current density, where V is the effective volume of the anode area within the reaction column. The power output of the reactor is, the power density is, the polarization curve is obtained by plotting the power density versus the current density. The power output of the reactor is, the power density is, the polarization curve is obtained by plotting the power density versus the current density. The polarization curve is measured by the steady-state discharge method, the internal resistance is measured by the power density peak method and the polarization curve method.

The Coulomb efficiency is expressed as follows, M is the relative molar mass (calculated based on oxygen as the electron acceptor, i.e. 32 g/mol), F is a Faraday constant (96485 C/mol), b is the number of electrons transferred by the oxidation of 1 mol of organic matter, △COD is COD change (g/L), V is the effective volume of the anode area of the reaction column (L), q is the inlet flow rate (L/s). The COD was determined by the potassium dichromate oxidation method, and the ammonia nitrogen was determined by the ultraviolet spectrophotometer method of TU-1810 model of Beijing Pu Analysis General Instrument Co., Ltd. [18].

3 Results and discussion

3.1 Effect of the ammonia concentration on the fuel cell performance

In this paragraph we investigate the influence of the different kinds of plants, different electrode spacings and different electrode thicknesses on the battery performance. Rich bamboo is used as the wetland plant, the fuel cell electrode spacing is 10 cm, the electrode thickness is 3 mm, study the effect of different ammonia nitrogen concentrations on the electricity production performance of microbial fuel cells. Because C/N in the medium has a significant effect on the growth and reproduction of microorganisms and product synthesis. Chen Wei [19] analyzed the effect of carbon-nitrogen ratio on the water quality of the reactor. It was found that the best nitrogen and phosphorus removal effect was obtained when C/N was 15, but the stability of the system was poor. The removal effect of N is inhibited at high C/N, but the C/N is too low to obtain the effect of nitrogen and phosphorus removal. Therefore, the optimum C/N is below 15 and the C content of this experiment is 132 mg, so it is reasonable. The N content is below 8.8 mg, so the ammonia nitrogen content of the selected experiment is 1-30 mg. Therefore, the effects of different ammonia nitrogen concentrations of 1, 10, 20, and 30 mg/L on the electricity production performance were investigated. The COD was fixed at 200 ± 20 mg/L. The ammonia concentration values at the end of production are reported in Fig. 3, showing that when the starting ammonia concentration is 10 mg/L, the maximum output voltage of 550 mV is obtained; at higher ammonia concentration of 30 mg/L, the maximum output voltage of the CW-MFC decreased significantly and at the concentration of 1 mg/L, CW-MFC output voltage decreases to is only 345 mV. Figure 3 shows that ammonia will promote the production of CW-MFC at low concentrations, however at too high concentrations it will affect the activity of the CW-MFC microbes, thereby inhibiting their production, which agrees with previous studies from Nam [20]. At low ammonia concentration of 1 mg/L, the voltage generation lowers respect to 10 mg/L, indicating that a such a small concentration, inhibits the activity of anaerobic microorganisms, reducing the electrical performance of the cell.

![Fig. 3. The battery voltage varies with time at different ammonia nitrogen concentrations](image-url)
internal resistance is 200, 270, 300 and 400 Ω, respectively. It can be seen from Figure 3 that the optimum ammonia concentration is 10 mg/L, resulting in a power density which is 1.6, 1.9 and 5.3 times higher respect to what is obtained with of 1, 20, 30 mg/L ammonia.

![Fig. 4. Polarization curve and power density curve of battery under different ammonia nitrogen concentration](image)

Figure 5 shows the Coulomb efficiency diagrams obtained at different ammonia concentrations. The ammonia concentration results to strongly affect the battery efficiency: at the ammonia concentration of 1, 10, 20 and 30 mg/L the Coulomb efficiency is 2.5%, 3.4%, 2.7% and 2.4%, respectively. We conclude that the Kurun efficiency of the fuel cell decreases with the increase of the ammonia concentration under certain conditions and the Coulomb efficiency is maximum when the ammonia concentration is 10 mg/L. The possible reason for the efficiency reduction at low ammonia concentration is that by using a carbon felt thickness of 1 mm, the COD removal efficiency is high, and the efficiency of Coulomb is inversely proportional to the variation of the COD, so that the Coulomb efficiency is relatively low.

![Fig. 5. The coulomb efficiency of battery under different ammonia nitrogen concentration](image)

### 3.2 Ammonia removal rate under different ammonia concentrations

The nitrification and denitrification are two major industrial processes for ammonia treatment [21-23]. The nitrification is the oxidation of NH$_4^+$ to NO$_2^-$ and NO$_3^-$, denitrification reaction formula: $NO_3^- + C_6H_{12}O_6 \rightarrow N_2 + CO_2 + H_2O + OH^-$, so the final N element is discharged as nitrogen. In the process of ammonia nitrogen nitration and denitrification, NO$_2^-$ and NO$_3^-$ will be produced. It can be seen from Table 2 that the NO$_2^-$ content is not measured in the whole process, although there is a high content of NO$_3^-$ because NO$_3^-$ is present in the configured sewage, but the NO$_3^-$ content decreases with time and is lower than the NO$_3^-$ at the inlet. The content is so good that the denitrification process works well. The removal rate of ammonia is strongly related to the amount of oxygen in the system, since oxygen is required to support the growth of nitrifying bacteria. According to Grady [24], nitrification may also occur at low levels of DO, however, the response rate is significantly reduced compared to DO levels higher than 2 mg/L. In this experiment, the DO content at the outlet was about 4 mg/L, the anaerobic zone of the cell was at the bottom of the cell (near the anode), and the aerobic zone was at the top of the cell root (cathode zone).

![Table 2. Composition of the NO$_3^-$-N, NO$_2^-$-N](image)

| Time                  | Effluent concentration (mg/L) |
|-----------------------|-------------------------------|
| NO$_3^-$-N            | 15 days from the start         |
|                       | 270-289                       |
|                       | First month                   |
|                       | 240-255                       |
|                       | Second month                  |
|                       | 233-245                       |
|                       | Third month                   |
|                       | 188-186                       |
| NO$_2^-$-N            | All time                      |
|                       | Null                          |

In order to study the effect of the ammonia concentration on a single chamber CW-MFC, we have placed the initial external resistance of 1 kΩ, and explored different ammonia concentrations of 1, 10, 20 and 30 mg/L. The concentration of ammonia in the battery outlet was measured with a spectrophotometer to deduce the ammonia removal rate as shown in Figure 6.

![Fig. 6. Removal rate of ammonia nitrogen under different ammonia nitrogen concentration](image)

From the Fig. 6, for the inlet concentration of 1, 10, 20 and 30 mg/L the removal rate of ammonia results 89.7%, 81.3%, 78.9% and 74.6% respectively. The higher is the ammonia concentration, the lower is the removal rate. This is because the nitrification process relies on the oxygen content. When the oxygen content is constant, the ammonia nitrogen removal amount is constant, so as the ammonia nitrogen concentration increases, the removal rate decreases. It is also possible
that the ammonia nitrogen concentration is too high and the activity of the microorganism is suppressed. This suggests that when the dissolved oxygen in the cathode chamber cannot be controlled, an appropriate amount of ammonia has to be introduced to avoid that the dissolved oxygen impacts on the denitrification yield at the CW-MFC cathode, while for optimizing the nitrification and denitrification at the same time in a single reaction chamber, the cathode itself has to produce enough electrons for the denitrification, and to achieve a balance between the nitrification and denitrification, one should avoid the remaining dissolved oxygen to affect the cathodic indoor denitrification, while the denitrification should be sufficiently strong to provide the anode needs in electrons, so that a high electrons current flow through the external circuit; this will be the next step in our research objectives.

3.3 COD removal rate at different ammonia concentrations

In order to study the effect of the ammonia concentration on the COD removal rate of a single-chamber CW-MFC, we applied an initial external resistance of 1 kΩ, and varied the ammonia concentration from 1, 10, 20 and 30 mg/L. The outlet COD concentration in the battery is measured by the potassium dichromate method to finally calculate the COD removal rate; the results are shown in Figure 7.

Fig. 7. COD removal rate at different ammonia nitrogen concentration

It can be seen from Fig. 7 that at 1, 10, 20 and 30 mg/L ammonia, the corresponding COD removal rates are 98.5%, 95.6%, 94.5% and 90.7%, respectively. The higher is the ammonia nitrogen concentration at the inlet, the lower is the removal rate; this is ascribed to the fact that a too high ammonia content results in the sludge denitrification, which can cause the activated sludge to float, and thus lowering the microbial population in the activated sludge, thereby reducing the COD removal efficiency.

4 Conclusions

In this paper, we mainly studied the effects of the ammonia concentrations on the electricity generation performance and wastewater treatment performance of a microbial fuel cell; the following conclusions apply:

1. The ammonia promotes the efficiency of the CW-MFC at low concentrations. However, above a certain concentration the ammonia will lower the activity of CW-MFC microbes, thereby inhibiting the energy production of the cell. When the ammonia concentration is 1 mg/L, the voltage generation is suppressed; this is due to the fact that at too low ammonia concentration the anaerobic activity microorganisms is inhibited, which reduces the electricity generation performance.

2. The ammonia concentration affects the power density delivered from the battery; at the ammonia concentration of 1, 10, 20 and 30 mg/L, the maximum power density is 8.3, 13.6, 6.9 and 2.5 W/m², corresponding to the current density of 8.9, 148.6, 69.4 and 38.2 A/m², and the calculated internal resistance of 200, 270, 300, 400 Ω respectively. When the ammonia concentration is 10 mg/L, the battery provides for the best performance, with a power density 1.6, 1.9 and 5.3 times higher respect of 1, 20 and 30 mg/L.

3. The removal rate for the inlet ammonia concentration 1, 10, 20 and 30 mg/L is 89.7%, 81.3%, 78.9% and 74.6% respectively, thus the higher is the ammonia nitrogen concentration, the lower is the removal rate.

4. When the inlet ammonia concentration is 1, 10, 20 and 30 mg/L, the corresponding COD removal rates are 98.5%, 95.6%, 94.5% and 90.7% respectively, thus the higher is the ammonia concentration, the lower the COD removal rate.

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