Performance Analysis of Vapour Compression Refrigeration System Using HC Refrigerant Mixtures for Water Chiller

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Abstract: The use of HC refrigerant mixtures has been a topic of current research in view of the concerns related to global warming and Ozone depletion problems caused by CFCs and HFCs. The HC mixture as an alternate refrigerant has been reported to be a promising one in addressing the global warming and Ozone depletion problems. In the present work an experimental setup is built up to test Vapour Compression Refrigeration (VCR) system with different refrigerants. The aim of this work is to investigate the performance analysis of Vapor Compression Refrigeration system with alternate refrigerants such as Hydrocarbon (HC) refrigerants mixture and compare with Hydro Fluoro Carbon (HFC) refrigerant (R134a) under the similar operating conditions. The alternate refrigerant mixture is selected in the combination of Propane (R290) and Isobutene (R600a). The refrigeration system variables considered for the investigation of performance are evaporating temperature, condensing temperature and power consumption. The HC refrigerant mixture is observed to give superior performance compared to HFC refrigerant in terms of global warming.

I. INTRODUCTION

A lot of experimental investigations are happening on the replacement of refrigerants that has negative impact on environment. The most common refrigerants being used is tri fluoro ethane, R-410A, R-404A. They have a huge Global Warming Potential (GWP) and negligible Ozone depletion potential (ODP). Refrigerants such as Dichlorodifluoromethane, difluoro mono chloro methane are banned because of the harm they cause in depleting the Ozone layer. The investigation is being made on replacement of these refrigerants with the Hydrocarbons (HC) mixtures to reduce the GWP. Ching-Song Jwo et al reported Efficiency Analysis of Home Refrigerators by Replacing the R-134a refrigerant with Hydrocarbon Refrigerants. They used varying strengths of HC refrigerant mixtures with R-290 and R-600a in the ratio 50%. The results were shown to be encouraging in terms of improved refrigerating effect and reduced power consumption. A.S. Dalkilic and S. Wongwises studied the Performance Comparison of Vapor-Compression Refrigeration System Using Various Alternative Refrigerants based on hydro carbon and hydro flor carbon refrigerants with varying mixture ratios. The results were compared with the performance of Dichlorodifluoromethane, difluoro monochloro methane and tri fluoro ethane. The results were shown that all the alternate refrigerants investigated in this analysis have a slightly lower coefficient of performance than Dichlorodifluoromethane, difluoromonochloromethane and trifluoroethane for the condensation temperature of 50ºC and evaporating temperature ranging between -30ºC and 10ºC. Propane/Isobutene (40/60 weight %) mixture was reported to give superior performance and is suggested as an alternative to Dichlorodifluoromethane. Similarly the propane/ Propylene (20/80 by28weight %) mixture was suggested as an alternative in the place of difluoromonochloromethane. QiqiTian, DehuaCai et al conducted experimental Investigation of Refrigerant Mixture Difluoromethane /propane as an alternative to HFC410a. They reported reduced power consumption by 34.1%, increased cooling capacity by 64.4% and increased COP by 6.8%. S. Wongwises and N.Chimires (2005,) conducted Experimental Studies with HC Refrigerants propane, butane, Isobutene and compared with trifluoroethane as baseline refrigerant. Experimental results showed that the mixture of propane and Isobutene (60% & 40%according to mass respectively) was the most appropriate alternative compared with trifluoroethanethey reported a reduced power consumption by 86% and reduction charge by approximately 50%. ShridharVasantRaskar, SachinVyasMutalikdesai presented the analysis of vapour compression system with alternative refrigerants Difluoroethane. The performance of alternative refrigerant Difluoroethane is evaluated through evaporating pressure, pressure ratio, compression work, coefficient of performance etc. It showed that difluoroethane would be better replacement for trifluoroethane. Arthur Heleno Pontes Antunes and EnioPedoneBandarraFilho conducted Experimental Investigation on the Performance and Global Environmental Impact of a Refrigeration System Retrofitted with alternative refrigerants. This paper presents associate experimental investigation of the drop-in method for difluoromonochloromethane in a 5-ton cooling system. The original refrigerant was replaced by different halogenated refrigerants like HFC-438A, HFC-404A, HFC-410A and Difluoromethane and also with hydrocarbons propane and Propylene. Results showed that the natural refrigerants presented the best coefficient of performance compared to HFCs, except for Difluoromethane which remained below that of difluoromonochloromethane. Regarding the environmental impact the parameter TEWI, the simplest results were reached with hydrocarbons; in the meantime the refrigerant HFC-404A gave the best environmental impact. Selection of a refrigerant is a critical process involving analysis of environmental, thermo physical and safety
property. Ozone depletion potential, Global Warming Potential and atmospheric life are the significant factors of refrigerant that affect the environment. Ozone depletion potential of a refrigerant is the measure of its ability to destroy ozone layer of the atmosphere. Global Warming Potential is an indicator of potential of refrigerant to warm the planet by its action in contributing to greenhouse gases. Propane and Isobutane are considered to be non-Ozone depletion potential refrigerants and have a very low Global Warming Potential as compared to trifluoroethylene. It has very less adverse effect on the environment.

### Table 1: Environmental Properties of refrigerants

| Refrigerant      | Chemical formula | Atmospheric life in year | GWP 0.1 | ODP |
|------------------|------------------|--------------------------|---------|-----|
| Iso Butane       | C4H10             | 1<                       | 8       | 05  |
| Propane          | C3H8              | 0.041                    | 20      | 0   |
| Trifluoroethane  | CH3FC             | 13.8                     | 1300    | 0   |

The heat energy required for evaporation of propane, iso butane and Trifluoroethane is less than difluoromonochloromethane by 80% at normal boiling point. The amount of refrigerant charge required is inversely proportional to the latent heat of evaporation.

### Table 2 Physical properties of refrigerants

| Refrigerant      | Molecular Weight (Kg/Km ol) | Normal Boiling point (°C) | Critical Temperature (°C) | Critical Pressure (bar) | Latent Heat of Evaporation (kJ/Kg) |
|------------------|-----------------------------|---------------------------|---------------------------|--------------------------|----------------------------------|
| Iso Butane       | 58.1                        | -11.6                     | 135                       | 3                        | 367                              |
| Propane          | 44.1                        | -42.2                     | 96.7                      | 425                      | 425                              |
| Trifluoroethane  | 102.03                      | -26.1                     | 101.1                     | 4.06                     | 377                              |

The thermophysical properties of the charge influence the performance of the system. The mass density of propane and Iso-Butane is less than Trifluoro-methane. The mass density and refrigerant charge flow rate are directly proportional to each other. Therefore propane exhibits less frictional losses and enhanced heat transfer in the condenser and evaporator. Butane and propane have lower viscosity when compared with Trifluoroethane resulting in higher heat transfer rates.

### Table 3: Thermo-physical properties of the refrigerants

| Property            | R600a (23°C liquid) | R290 (25°C liquid) | R134a (11°C liquid) |
|---------------------|---------------------|--------------------|----------------------|
| Pressure (MPa)      | 3.3                 | 8.4                | 1.9                  |
| Density (Kg/m3)     | 8.6                 | 21.8               | 943.9               |
| Viscosity (µPa-s)   | 15.4                | 8.5                | 18.1                |
| Thermal Conductivity (W/mK) | 0.0                 | 0.0                | 0.1                  |
| Specific heat (kJ/Kg°C) | 1.7                 | 1.8                | 2.7                 |

### II. EXPERIMENTAL SETUP

Figure 1 shows a photographic view of vapour compression refrigeration test rig made with 30 liter capacity for cooling water. The evaporator coil is submerged in water made with a metal container insulated with polymer foam. Filter-drier is set up before the capillary tube to absorb any moisture that may be present within the refrigerant circuit so that the refrigerant condensed inside the condenser flows via the filter-drier right into a capillary tube. The test rig used for the experiment is a vapour compression refrigeration system designed to work with R134a and blend mixture of R600a and R290. It consists of an evaporator, cord mesh air cooled condenser and a hermatically sealed reciprocating compressor. Four pressure gauges are hooked up at compressor inlet and outlet, condenser outlet and evaporator inlet. Five calibrated temperature sensors (thermocouples) are mounted at the evaporator inlet, evaporator outlet, compressor outlet, condenser outlet and inside the water container. The supply voltage and the current are measured from the display unit. A Digital Energy meter is used to measure the actual power consumption. Service ports are provided at the pinnacle aspect of the compressor for charging and recuperating the refrigerant. The evacuation of moisture within the device was executed via the carrier port to start with. The device is flushed with nitrogen fuel to eliminate air, impurities, moisture and other particles in the device, which may additionally affect the overall performance of the system. The rig is charged with the assistance of charging machine and evacuated with the help of a vacuum pump to a pressure of -30mm of Hg. Figure indicates a schematic diagram of the measurement machine used inside the experimental setup. The most crucial specifications of the fridge are summarized within the below Table 4. Measured quantities with their range and accuracy are indexed in the below table. An electronic weighing device of 1 gram decision become used to degree the quantity of refrigerant to be charged to the rig during.
examine. A digital data logger along with HMI device was used to collect the experimentally measured values.

Fig.1 Vapour compression Test Rig

Table 4 Technical specifications of Vapour compression Test unit

| Quantity            | Value                          |
|---------------------|--------------------------------|
| Storage Volume      | 30L                            |
| Current rating      | 1.1 max                         |
| Voltage             | 220-240V                       |
| Frequency           | 50Hz                           |
| Refrigerant type    | R134a & Blend(R600a+R290)      |
| Mass of charge      | 0.140 kg                       |
| Capillary tube length | 1.5m                        |
| Capillary tube inner diameter | 1.2mm                  |
| Refrigeration capacity | 240 W                      |

Table 5 Measured quantities with their range and accuracy

| Quantity          | Range                  | Accuracy   |
|-------------------|------------------------|------------|
| Temperature       | -0.1°C to 35°C         | +0.1°C     |
| Power consumption | 0 to 1000 watts        | 1 watts    |
| Voltage           | 0 to 240Volts          | 0.1 Volts  |
| Current           | 0 to 10Amps            | 0.1Amps    |
| Pressure          | 0 to 21bars            | +0.7bars   |

In this test, the freezer is completely loaded, and the thermostat is hooked up to the circuit at complete load condition. Because the temperature reaches maximum set freezing temperature the compressor stops that's referred to as the cut-off time, and because the temperature in the cabinet reaches the lowest set freezing temperature, the compressor starts off evolved that is known as the reduce-in- time, taking the strength retaining the temperature within the cupboard at stabilized condition. Significance of this test is to find out how an awful lot time is needed by using the loaded product to gain the desired temperature at full load circumstance additionally indicates how energy is required by way of the compressor at reduce-in and cut-off positions. From the experimental system with the intention to discover the refrigeration effect, C.O.P, and work completed on the system the above may be received by way of using p-h chart. The subsequent experimental values are plotted on the p-h to realize the behavior of the easy vapour compression cycle with and without low receiver.

III. RESULTS AND DISCUSSION

The basis for present work is the result reported by M. Mohanraj et.al [18] for selection of combination of refrigerant mixture. Firstly the vapour compression test is carried out with R-134a to assess the parameters like evaporator temperature, coefficient of performance, power consumption, refrigerating effects. Later the experiment is repeated with alternate blended mixture R290 and R600a (50:50 weight proportions). Figure 2 shows the Evaporator temperature drop for R-134a refrigerant and the blended refrigerant mixture. The lowest Evaporator temperature achieved is 0.1ºC with 135g of R134a and 0.05ºC with 135g of blend. It is observed that as the time increases the cooling capacity also increases and reaches 200 W at 0.05ºC with hydrocarbon blend and 0.1ºC for R-134a.

Fig.2 Variation of Evaporator Temperature of Vapour compression refrigeration system with respect to time

Figure 3 shows the variation of power consumption for134a and the blend of R600a/R290. The power consumption with R134a is observed to be 25% higher than the blend of R600a/R290, due to larger amount of charge. Maximum power consumption is noted as 0.10 kWh for R134a and 0.07 kWh for HC blend. Figure 4 shows that the coefficient of performance of blend is higher than R-134a.

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butane (R600a). The test rig is suitably modified by adopting different lengths of liquid line suction line heat exchanger.

1. The combination of propane and isobutane in equal proportions as a blend can be used in the place of trifluoroethane.
2. A least mass of refrigerant charge for the above blend of 134 g is recorded which is considerably lower than the trifluoroethane as charge.
3. The Coefficient of Performance for the combination of propane and isobutane in equal proportions is observed to be higher at all operating conditions when compared with trifluoroethane.
4. Also the cooling rate is noted to be higher for the above blend when compared with trifluoroethane.
5. The condenser temperature, during the condensation process for the blend is less. It shows that it doesn’t require any external energy for condensation.
6. Also the above blend is seen to consume lower power than with trifluoroethane.
7. It is evident that the combination of propane and isobutane in equal proportions as a blend is superior in performance than trifluoroethane hence a better choice.
8. The global warming potential for blended mixture is less when compare with the trifluoroethane.

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IV. CONCLUSIONS

In the present work experimental investigation is carried out to investigate the performance of vapour compression refrigeration system for water chiller of 30 liters capacity, with R134a and blended mixture of propane (R290) and Iso

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