Long-Term Results of Cell-Free Biodegradable Scaffolds for In Situ Tissue-Engineering Vasculature: In a Canine Inferior Vena Cava Model

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Abstract

We have developed a new biodegradable scaffold that does not require any cell seeding to create an in-situ tissue-engineering vasculature (iTVE). Animal experiments were conducted to test its characteristics and long-term efficacy. An 8-mm tubular biodegradable scaffold, consisting of polyglycolide knitted fibers and an l-lactide and ε-caprolactone copolymer sponge with outer glycolide and ε-caprolactone copolymer monofilament reinforcement, was implanted into the inferior vena cava (IVC) of 13 canines. All the animals remained alive without any major complications until euthanasia. The utility of the iTVE was evaluated from 1 to 24 months postoperatively. The elastic modulus of the iTVE determined by an intravascular ultrasound imaging system was about 90% of the native IVC after 1 month. Angiography of the iTVE after 2 years showed a well-formed vasculature without marked stenosis or thrombosis with a mean pressure gradient of 0.51±0.19 mmHg. The length of the iTVE at 2 years had increased by 0.48±0.15 cm compared with the length of the original scaffold (2–3 cm). Histological examinations revealed a well-formed vessel-like vasculature without calcification. Biochemical analyses showed no significant differences in the hydroxyproline, elastin, and calcium contents compared with the original scaffold (2–3 cm). The use of foreign materials is necessary to repair complex heart defects. However, the materials that are commonly used are not biocompatible with the host tissue and do not have the ability to change their shape as the host grows. In addition, long-term studies of the efficacy of these materials have revealed several material-related failures, such as stenosis, thromboembolization, and calcium deposition. To solve these problems and to improve the treatment of children who require implantation of materials possessing growth potential, we have been pursuing the development of optimal biocompatible materials.

Introduction

The use of foreign materials is necessary to repair complex heart defects. However, the materials that are commonly used are not biocompatible with the host tissue and do not have the ability to change their shape as the host grows. In addition, long-term studies of the efficacy of these materials have revealed several material-related failures, such as stenosis, thromboembolization, and calcium deposition. To solve these problems and to improve the treatment of children who require implantation of materials possessing growth potential, we have been pursuing the development of optimal biocompatible materials.

We previously reported the advantages of using biodegradable scaffolds seeded with autologous cells as tissue-engineered vascular autografts (TEVAs) in canine models [1,2,3] and in a human clinical study [1,4,5]. The key benefit of utilizing such scaffolds is that the scaffold degrades in vivo, thereby avoiding the long-term presence of foreign materials, while the seeded cells proliferate to form new tissue [2,6]. We also reported that the seeded cells are able to differentiate into cells that compose the vessel wall and may act as cytokine producers [6]. However, the contributions of the seeded cells remain uncertain [6]. There was no graft-related mortality and no evidence of aneurysm formation, graft rupture, graft infection, or ectopic calcification in the late-term results for TEVAs in 25 patients (mean follow-up, 5.8 years) [4]. However, 4 of the 25 patients had graft stenosis and underwent successful percutaneous angioplasty [4]. To overcome the graft stenosis of TEVAs, we explored a new scaffold without cell seeding, and achieved acceptable long-term results as evaluated by new techniques involving an intravascular ultrasound imaging system. This new scaffold can be implanted by a simple cost-effective procedure, because no cell preparation and seeding are necessary.

In the present study, we evaluated the long-term outcomes, usefulness, and basic characteristics of an in-situ tissue-engineering vasculature (iTVE) constructed through cell-free and direct implantation of the new biodegradable scaffold in a canine model.
Results

Overview, the mechanical properties and degradation of a newly developed biodegradable scaffold

Shown as an overview in Figure 1A, this scaffold degraded by hydrolysis after implantation. Changes over time in the scaffold’s mechanical strength and molecular weight in vivo are shown in Figures 1B and 1C. Most of the scaffold’s strength was lost within a month and molecular weight decreased within 6 months, suggesting that the scaffold was almost entirely degraded and resorbed into the body during the 6-month implantation.

Biomechanical changes of biodegradable scaffolds

The mechanical properties of biodegradable scaffolds in vitro were evaluated by soaking in phosphate buffered saline (PBS) at 37°C and testing with a tensiometer, and it was found that the scaffold degraded by hydrolysis, losing half of its tensile strength in 2–3 weeks and entirely within 10 weeks. The scaffold’s tensile strength per cm width at 0, 1, 2, 3, 4, 6, and 9 weeks in vitro were 9.3, 6.9, 5.3, 2.1, 1.2, 0.4, and 0.1 N, respectively (Fig. 1B). The scaffold’s molecular weight changes under these conditions decreased with time, decreasing by 0, 1, 2, 4, 6, 8, 13, 20, and 25 weeks to 194267, 163566, 124383, 82709, 51737, 32867, 8655, 6190, and 4387 daltons, respectively (Fig. 1C).

Macroscopic and histological findings of iTEV

All animals remained alive and well without any serious complications until euthanasia at 1 (n = 3), 2.5 (n = 3), and 24 months (n = 7). Vessel-like iTEVs were recovered at 2 years by dissection and examined (Fig. 2A, black arrow, distance between suture sites at implantation). Internal iTEV sections showed completely endothelialized surfaces and thin vessel walls (Fig. 2B). Implanted scaffold lengths and iTEVs after explantation from individual dogs showed that all iTEVs increased in length over the 2-year period, ranging from 0.1 to 1.0 cm (mean ±SEM, 0.48 ±0.15 cm, Fig. 2C). When explanted at 2 years, the mean diameters of iTEVs sited close to the diaphragm and the atrium were 11.8 ±0.7 and 8.7 ±0.8 mm, respectively (Fig. 2D). All iTEV diameters increased during the 2-year period compared with the initial implanted 8 mm tubular-shaped scaffold. The iTEV sections at 1 month showed the presence of P(GA/CL) monofilaments (Fig. 2E), but they appeared to be resorbed in iTEV sections at 2.5 months (Fig. 2F). Immunohistological study revealed endothelialization (factor VIII-positive) and smooth muscle cell (alpha smooth muscle cell actin [ASMA]-positive) proliferation in iTEV sections at 1 and 2.5 months (Fig. 2G). The components of the four basic vascular layers, endothelial cells (Factor VIII-positive), smooth muscle cells (ASMA-positive), elastic fibers, and collagen fibers, were observed in iTEV sections at 2 years (Fig. 3A–E); no calcified lesions were observed (Fig. 3F). As the biodegradable materials were entirely degraded within 6 months, these findings suggested that the application of P(GA/CL) monofilaments to the scaffold did not cause calcification. A comparison of the wall thicknesses of native inferior vena cava (IVC) and iTEV showed that native IVC and iTEV walls were 0.31±0.01 and 0.29±0.01 mm thick, respectively, and were not significantly different (p = 0.311, Fig. 3G).

Angiographic and biomechanical findings using the IVUS

Seven animals were evaluated by angiography while in a right lateral position and an intravascular ultrasound imaging system (IVUS) employed in a catheter laboratory to confirm the iTEV characteristics, pressure gradient, and elastic modulus. Time-course changes of the smallest internal diameters of iTEVs measured by angiography revealed that the iTEV diameters at 1, 2.5, 6, 12, and 24 months were 5.53±0.62, 4.06±1.12, 5.20±1.02, 6.92±1.75, and 7.98±1.86 mm, respectively (Fig. 4A). The smallest internal diameters iTEVs increased the most in diameter during the 2-year period (Kruskal–Wallis tests; p<0.001). It should be noted that diameter decreased during neointimal growth on the scaffold, the tissue remodeled within 6 months into native tissues with concurrent material degradation, and the internal diameter tended to increase and adapt its shape as the living body required. The smallest internal diameter of the dog native IVCs (6.81±0.52; n = 6) showed remarkable differences from those of the 1, 2.5, and 6-month iTEVs, but no significant differences from the 12 and 24-month iTEVs (Mann–Whitney U test; native IVCs versus 1- or 2.5-month iTEVs, p>0.001, native IVCs versus 6-month iTEVs, p<0.05). Angiogram data showed some feature changes during the iTEV remodeling and scaffold degradation processes (Fig. 4B), and following the angiograms, pressure studies were performed using a Millar pressure catheter system, which showed that the pressure gradient between the iTEV proximal and distal sites was 0.51±0.19 mmHg at 24 months (Fig. 4C).

IVUS images showing iTEV changes over time indicated that the scaffold was located between the neointima and adventitia during tissue development (Fig. 5, 1, and 2.5 months).

Data for the pressure-to-strain (P-S) loops of the iTEV and native IVC at 2 years and of a control (scaffold itself) showed that the ratios of the elastic modulus of the iTEV to native IVC at 0 (control), 1, 2.5, 6, 12, and 24 months were 7.3±0.5, 2.3±0.7, 1.1±0.2, 1.0±0.2, 1.4±0.2, and 1.1±0.2, respectively (Fig. 6). The elastic modulus of the iTEV decreased over time and was almost the same as the native IVC after 2.5 months. Also, there were significant differences between the control scaffold and the

Figure 1. Overview of the new biodegradable scaffold and its degradation. A, biodegradable scaffold 8 mm in diameter; bar, 1 cm. B, tensile strength changes in biodegradable scaffolds in vitro; scaffold strength diminished remarkably over 4 weeks. C, Mw changes in scaffold immersed in 37°C PBS; gradual hydrolysis decreased Mw.

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other samples, and no significant differences among the samples at 1, 2.5, 6, 12, and 24 months.

Finally, elastic moduli data were used to calculate iTET regeneration scores at 1, 2.5, 6, 12, and 24 months and found to be 90.3±2.9%, 93.8±1.7%, 95.8±1.1%, 93.7±0.8%, and 92.7±2.5%, respectively (Fig. 6C). There were no significant differences among these samples (p = 0.836).

Biochemical findings

There were no significant differences in the protein content of iTETs and native IVCs at 2 years, with the densitometry ratios of
CD146 protein to beta-actin in native IVCs and iTEVs at 4.2 ± 0.4 and 5.0 ± 0.4, respectively (p = 0.193) and the densitometry ratios of ASMA protein to beta-actin in IVCs and iTEVs at 1.1 ± 0.1 and 1.2 ± 0.1, respectively (p = 0.907, Fig. 7).

There were also no significant differences in the elastin, hydroxyproline, and calcium contents between normal IVCs and iTEVs (Fig. 8A–C), with elastin content of native IVCs and iTEVs at 52.6 ± 9.1 and 57.9 ± 5.1 µg/g wet tissue weight, respectively (p = 0.615). Based on hydroxyproline concentration, the collagen...
concentrations of native IVCs and iTEVs were 150±15 and 142±19 μmol/g wet tissue weight, respectively (p = 0.750). And finally, the calcium content of native IVCs and iTEVs were 0.21±0.05 and 0.27±0.05 μg/g wet tissue weight, respectively (p = 0.165).

Discussion

In the present study, evaluation of the long-term results from iTEVs, produced by tubular composite scaffold implantation without cell seeding in a canine model, revealed their efficacy in terms of patency and in their histological, biomechanical, and biochemical similarities to native vessels. It was clearly demonstrated that the morphology of the implanted biodegradable scaffold was remodeled. Previously here, clinical applications of tissue-engineered vascular autographs (TEVs) have been successful, using cultured venous cell mixtures as a cell source with seeding onto a biodegradable scaffold prior to implantation [1]. However, this protocol proved difficult to manipulate, as bovine serum was necessary and the cell preparation process took several weeks. Thus, the procedure was altered to incorporate mononuclear bone marrow cells (MN-BMCs) as the cell source, as they can be easily prepared on the day of procedure [1]. MN-BMC-seeded TEVs have regenerated vessel-like structures with good results in animal studies and human clinical trials [1,2,4–6,8]. However, this protocol still requires complex cell preparation processes [9], which represents a critical barrier for broad clinical applications. Consequently, development of a scaffold for tissue engineering of vasculature that does not require cell seeding is in development here.

Although various types of scaffolds have been examined in this laboratory, successful patency rates did not differ between scaffolds with or without cell seeding (unpublished observations). Histological observations in a previous study here suggested that tissue regeneration was chiefly dependent on neighboring cells and not on seeded cells [6]. Furthermore, seeded MN-BMCs contributed as producers of cytokines, which induce cell recruitment for constructing mature tissues, rather than differentiating into mature vasculature components [10]. Therefore, it was concluded that seeding of autologous cells onto a scaffold is not a promising strategy and that it might be possible to create an iTEV with an optimized biodegradable scaffold without cell seeding.

Although the late-term results of TEVs are acceptable, the problem of graft stenosis generation in some patients still exists [4]. Such stenotic changes may cause tissue regeneration disorders, such as blood flow disturbance, thrombogenesis, or graft occlusion. Graft stenosis was also found to occur within a few months after implantation and a graft was never occluded or suffered from stenosis after complete endothelial coverage (unpublished observations), suggesting that scaffold reinforcement during the relatively early period of tissue development is essential.

The focus here was on the design of a biodegradable scaffold with optimal mechanical properties and degradation time. It should maintain its shape during early endothelialization after implantation to avoid blood flow disturbances and overgrowth of fibrotic tissue. From previous studies here, neointimal growth with optimal mechanical properties and degradation time. It should maintain its shape during early endothelialization after implantation to avoid blood flow disturbances and overgrowth of fibrotic tissue. From previous studies here, neointimal growth with optimal mechanical properties and degradation time.

![Figure 6. Biomechanical analyses of IVC and iTEV at 2 years. A, representative P–S loop data for control scaffold and iTEV and native IVC at 2 yr; P–S loops from time-dependent strain and pressure measurements {ε, p}, used to calculate sample elastic moduli. B, elastic moduli ratios of iTEV to native IVC at 0 (control), 1, 2.5, 6, 12, and 24 months (n = 7); significant differences between control and samples (p < 0.0001 by ANOVA); ***, p < 0.001, control vs. 1 month and **, p < 0.01, control vs. 2.5–24 months by Dunnett’s post hoc test. C, iTEV RS at 1, 2.5, 6, 12, and 24 months (n = 7); RS maintained by scaffold while tissue in infancy; data show iTEV elasticity not affected by time after implantation; Note, P(GA/CL) monofilament and P(LA/CL) sponge scaffold lose strength within ~2.5 and 6 months, respectively (p = 0.443 by ANOVA); NS, not significant.](doi:10.1371/journal.pone.0035760.g006)

![Figure 7. Protein densitometry of endothelial cells and smooth muscle cells of the iTEV and IVC. Bar graphs of CD146 and ASMA protein densitometry normalized by beta-actin concentrations; all results from native IVC and iTEV samples at 2 years (n = 7 each); ratios of ASMA and CD146 to beta-actin, means ±SEM; no significant differences (CD146, p = 0.193 and ASMA, p = 0.907 by unpaired Student’s t-test); NS, not significant.](doi:10.1371/journal.pone.0035760.g007)
month after implantation (unpublished data). During this initial period, if fibrotic tissues massively proliferated, stenotic changes in the iTEV would have been observed (unpublished observations). Thus, a material that maintains its shape during the endothelialization period is considered able to avoid graft stenosis and a novel biodegradable scaffold was developed that was reinforced with P(GA/CL) monofilaments on the outer surface, to maintain iTEV shape for the initial crucial period following implantation. These monofilaments, however, decreased in strength within a month and then degraded within 2 months, with the PLLA/CL spongy scaffold concurrently but more slowly degrading in the iTEV to create a relatively constant elasticity in the iTEV during the tissue-remodeling process. As a result, this new P(GA/CL) monofilament-reinforced scaffold prevented graft stenosis and allowed complete endothelialization of the graft inner surface. Furthermore, these iTEVs reached optimal elasticity after a month, judged from RS values. Consequently, tissue regeneration was also attained without complications, resulting in long-term iTEV patency. These findings suggested that the new biodegradable scaffold possessed significant potential for reducing the incidence of graft stenosis observed in previous clinical trials.

As the mechanical properties of a scaffold are closely related to biocompatibility, maturity, and structural integrity of grafted materials, the iTEV elastic modulus has been evaluated [11,12]. Although mechanical tests of the excised tissue samples from euthanized animals indicated the immediate iTEV character, it has been impossible to determine the course of continuous changes in the elastic modulus in vivo [2]. In the present study, a novel in vivo system for tracking elastic moduli is proposed which uses an IVUS and a pressure catheter for evaluating the iTEV mechanical properties [7]. This technique enabled assessment of iTEV elasticity changes as well as reduction of the number of animals required. The chosen scaffold degraded and changed its elastic moduli during tissue development and regeneration to form mature vasculature, such that, at 1–2.5 months, when the tissue was still in its infancy, iTEVs revealed adequate RSs and elastic moduli ratios. At 1–2 years, after scaffolds resorption, iTEVs showed RSs and elastic moduli ratios similar to native IVCs, which suggested significant remodeling of iTEVs.

The IVUS images showed changes in iTEV wall characteristics in vivo, in which neointima developed on the scaffold interior surfaces, the internal diameter reduced in the early phase, and the internal diameter increased, during which time the scaffold was resorbed and tissue developed.

It is widely known that artificial grafts are reliable, stable, and in common use throughout the world. However, concerns still remain regarding non-biocompatibility, such as calcification [13], thrombosis [14,15,16], and decreased diameter due to pseudo-intimal peel formation [16,17,18]. Although an iTEV is initially an artificial material when implanted, the scaffold resorbs over time, allowing regeneration of “native vessels.” The iTEV is a promising alternative to artificial grafts, particularly in venous positions, and have benefits, such as avoidance of anticoagulation therapy and reductions in the incidence of thromboembolic complications and calcification [2,6], and the potential to remodel into an appropriate size in response to vessel flow or patient’s growth [5]. Thus, in the field of congenital heart diseases, this novel strategy could provide great benefits for children who require anatomical repair using an artificial graft. Surgeons tend to implant oversized grafts in pediatric patients, increasing the chance of thrombosis in the prosthetic graft. Therefore, an ideal graft that adapts to the child’s growth is desired, as more suitable future-sized grafts cannot be implanted in pediatric patients. The present findings have shown that an iTEV undergoes remodeling to meet the body’s requirements, evidenced by changes in iTEV diameter and length over time. Furthermore, iTEVs managed to maintain their original features and mechanical properties, while avoiding stenosis and calcification. All these findings supported the realistic possibility of applying iTEVs to pediatric cardiovascular surgery. At present, iTEVs are envisioned for use in systemic venous reconstruction, such as modified Fontan operations (extracardiac total cavo-pulmonary connection) and modified Warden procedures for partial anomalous pulmonary venous connection. These iTEVs are biocompatible, anti-thrombogenic, and have the remodeling potential required by pediatric patients with congenital heart diseases as they grow. For extended applications of iTEVs, further studies of the scaffold under high-pressure circumstances should be conducted.

In conclusion, an iTEV with good long-term results can be constructed by direct implantation of this new biodegradable scaffold. As the scaffold degraded and autologous tissue developed in vivo, the new “regenerated”, “reconstructed”, and “adapted” vasculature possessed biocompatible characteristics, thereby avoiding unwanted calcification. Based on the present findings, the protocol for iTEV development can be simplified and made more versatile. We think that this novel “Cell-Free Tissue Engineering for Vasculature” can easily be applied to treatments of patients who require surgical interventions with artificial grafts to provide them a better quality of life.
Materials and Methods

Ethics statement
The ethical committee of Tokyo Women’s Medical University reviewed and approved the study protocol (Permit Number: 07-68).

Newly developed biodegradable scaffold for cell-free iTEV
A composite tubular scaffold has been previously developed, consisting of polyglycolide (PGA) knitted fibers and an L-lactide and ε-caprolactone copolymer (P[LA/CL]) sponge with outer glycolide and ε-caprolactone copolymer (P[GA/CL]) monofilament reinforcement. The PGA fibers and P[LA/CL] sponge were the same as those used in previous studies to create TEVs [1,2]. The P[GA/CL] monofilament (0.45 mm diameter) was wound around the scaffold outer surface with a pitch of 3 mm (Fig. 1A). As the P[GA/CL] monofilament will lose its strength within 2 months owing to non-enzymatic hydrolysis, it was used to provide reinforcement during the crucial tissue construction period. The new scaffold possessed 27 times higher compression strength than previous scaffolds and was sterilized with ethylene oxide gas prior to implantation.

Mechanical and degradation tests of biodegradable scaffolds in vitro
Biodegradable scaffolds were cut in 1–1 cm width rings and soaked in PBS at 37°C for 0–25 weeks. For assessment, the tensile strength [N] of sample scaffolds at 0–9 weeks were measured on a tensiometer (EZTest, Shimadzu, Kyoto, Japan) at a crosshead speed of 50 mm/min. The molecular weight (Mw) was determined by gel permeation chromatography using a Shimadzu GPC-System equipped with a pump, degasser (LC-10AT VP) at 1.0 ml/min and a refractive index detector (RID-10A, Shimadzu). The Mw was determined by injecting a sample of the scaffold into the system and eluting with trichloromethane at 1.0 ml/min at 40°C and calibrated with polystyrene standards over an Mw range of 4,000–1,600,000 daltons.

Animal experiments
Thirteen healthy adult female beagles (NARC, Tomisato, Japan) with a mean weight of 9.3 kg (7.0–11.5 kg) were obtained for this study, with six animals euthanized for histological examinations at 1 (n = 3) and 3 (n = 3) months, and seven animals euthanized at 24 months for histological and biochemical analyses. For surgeries, animals were anesthetized with pentobarbital (1 mg/kg body weight) and atropine sulfate (0.08 mg/kg body weight), with heparin (500 U/kg body weight) administered intravenously for anticoagulation during anastomoses. Each scaffold (8 mm diameter and 2–3 cm long) was implanted into the IVC, as described previously [2,6], and the animals followed by IVUS until 24 months (1 (n = 11), 2.5 (n = 11), 6 (n = 8), 12 (n = 7), and 24 (n = 7) months). Aspirin (2 mg) was orally administered for the first month after surgery as an anticoagulation therapy and subsequently maintained without anticoagulants until euthanasia.

After dissection, the iTEV length was measured directly between the two suture lines and the iTEV then longitudinally dissected to allow histological and biochemical analyses. For each assay, samples of native IVC and iTEV were dissected, rinsed with PBS, and stored at −20°C until analysis.

Histological examination
Longitudinally incised iTEV and native IVC samples as controls were fixed in 4% paraformaldehyde in pH 7.0 PBS, embedded in paraffin, and sectioned at 4–5 μm. Some sections were subjected to hematoxylin and eosin (H&E), Masson’s trichrome, Victoria blue–van Gieson, or modified von Kossa staining, as previously described [2,6]. Immunostaining of other sections was performed with antibodies against factor VIII (1:1000) and ASMA (clone 1A4; 1:1000; Dako Japan Inc., Tokyo, Japan). iTEV wall thicknesses were measured at 10 different sites in these sections and all histological examinations and measurements performed using a microscope (Biozero BZ-8000; Keyence Corp., Osaka, Japan) and accompanying analytical software (BZ-Analyzer; Keyence Corp.).

Angiography and biomechanical analyses using IVUS
Subject animals were anesthetized using the protocol described above and placed in sterilized conditions for femoral vein dissection. An 8 Fr long catheter sheath (Terumo Corp., Tokyo, Japan) was placed through the femoral vein adjacent to the IVC, close to the diaphragm. An X-ray fluoroscope was used to identify sheath and catheter locations and for digital angiography. Approximately 5 ml of angiographic agent was injected to evaluate iTEV features and to measure the smallest iTEV internal diameter during the regeneration process and in native IVCs of control dogs. Next, a 2-Fr Millar Mikro-Tip catheter pressure transducer (Millar Instruments Inc., Houston, TX) and a 2.5-Fr IVUS (Terumo Corp.) were inserted through the long catheter sheath. Simultaneously, a Millar Mikro-Tip catheter was used to measure the pressure gradient between iTEV proximal and distal sites.

The elastic moduli of iTEVs and native IVCs were analyzed based on the P-S loops obtained using synchronized ultrasonic B-mode images and pressure signals recorded in the lumen, acquired using ultrasound and pressure sensor catheters [7]. Vessel wall deformation induced by circumferential stress was analyzed using successive ultrasonic B-mode images reconstructed using RF data. Repeat imaging of the lumen on ultrasonic B-mode images enabled calculation of the time-dependent luminal circumferential length \( \langle \text{l} \rangle \) and circumferential strain \( \varepsilon_c \). Plotting of the time-dependent pressure \( \langle \text{p} \rangle \) and circumferential strain \( \varepsilon_c \) values allowed calculation of the P-S loop and the dynamics of the iTEV wall and native IVC. The elastic modulus \( \mu \) was calculated using the measured parameters that make up the P-S loop \( \varepsilon_c \langle \text{p} \rangle \) as follows:

\[
\mu = \frac{1}{N-1} \sum_{i=0}^{N-2} \frac{\text{p}_{i+1} - \text{p}_i}{\varepsilon_c^{i+1} - \varepsilon_c^i}
\]

Using the elastic moduli of the iTEVs and IVCs, the RS was calculated by comparing the elastic moduli of native IVCs with...
that of iTEVs using the following formula, which predicts the degree of iTEV regeneration:

\[
RS = 100 \times \left(1 - \frac{\mu_N - \mu_T}{\mu_{ND} - \mu_{TD}}\right) (%)
\]

where \(\mu_N\) and \(\mu_T\) indicate the elastic moduli of native IVC and iTEV at any time, respectively, and \(\mu_{ND}\) and \(\mu_{TD}\) indicate the elastic moduli of native IVC and iTEV immediately after implantation, respectively. In other words, the difference between the elastic moduli of iTEV and native IVC at any time was normalized by that observed immediately after implantation. Based on this formula, RSs of 0\% and 100\% indicated incomplete and complete regeneration, respectively.

Biochemical analyses of protein, elastin, hydroxyproline, and calcium content

After thawing, iTEV and native IVC samples were weighed and homogenized at a 1/20 (w/v) ratio of tissue to Tissue Protein Extraction Reagent (Thermo Fisher Scientific Inc., Rockford, IL) for protein extraction, and the total protein content determined using the Bradford assay. Samples of the denatured proteins, at 15 \(\mu\)g per lane, were separated in 4–12% polyacrylamide gels (NuPAGE Novex® Bis-Tris [Bis (2-hydroxyethyl) imino-Tris (hydroxymethyl) methane-HCl] Midi Gels; Invitrogen, Carlsbad, CA) and transferred to polyvinylidene difluoride membranes using an iBLOT dry blotting system (Invitrogen). As primary antibodies, an anti-ASMA antibody (1:1000, clone 1A4; Dako) and an anti-Cd45 antibody (1:1000; Epitomics, Inc., Burlingame, CA) were used to detect endothelial cell proteins in iTEVs, with an anti-human beta-actin antibody (1:2000; Abcam, Cambridge, MA) used as an internal control. A WesternBreeze® Chemiluminescence Immunodetection Kit and a BenchPro™ 4100 system (Invitrogen) were used for detection of antigen-antibody complexes immobilized on polyvinylidene difluoride membranes, according to the manufacturer’s protocol. After membrane enhancement by treatment with the kit chemiluminescent reagent, chemiluminescence images were acquired using a cooled CCD camera (LAS-3000 Mini; Fujifilm Corp., Tokyo, Japan) and analyzed using image analysis software (Multi Gauge; Fujifilm Corp.).

A commercially available elastin assay kit (Fastin Elastin Assay Kit; Biocolor, Ltd., Belfast, Northern Ireland) was used to quantify the elastin content of iTEV and native IVC samples. Insoluble tissue elastin was solubilized by hot oxalic acid treatment, precipitated, and mixed with the Fastin dye reagent. The elastin-dye complex was collected by centrifugation, dye bound to the elastin pellet solubilized with the Destain reagent, and the recovered dye concentration measured at 513 nm.

Sample hydroxyproline contents were measured by high-performance liquid chromatography (HPLC). In preparation, tissue samples were weighed and digested with 12 N HCl for 24 h, the resulting suspensions hydrolyzed with 0.5 ml of 12 N HCl for 20 h at 100°C, and after neutralization and centrifugation, a 0.1-ml aliquot of each supernatant was mixed with 1.5 ml of 0.3 N lithium hydroxide solution for analysis by HPLC.

The calcium concentrations of the tissue samples were determined using a Zeeman polarized atomic absorption spectrophotometer (Model Z-6100; Hitachi Co., Ltd., Tokyo, Japan). Tissue samples were weighed and digested with nitric acid and concentrated hydrogen peroxide (ratio, 4/1) and a model MLS1200 microwave system (Milestone Inc., Monroe, CT) was used to achieve sample decomposition. Subsequently, 25 \(\mu\)l of each sample was added to 2 ml of 10% lanthanum chloride and calcium content measured by reference to a standard calcium solution (Wako Pure Chemical Industries, Ltd., Osaka, Japan).

Statistical analysis

An unpaired Student’s \(t\)-test or the Mann–Whitney \(U\) test was used to compare the results from the control and time groups depending on each group’s data variance. One-way analysis of variance (ANOVA) followed by Dunnett’s \(post hoc\) analyses or the Kruskal–Wallis test were used when the variances were not appropriate. All data were expressed as means ±SEM, and probability values of \(p<0.05\) considered to indicate statistical significance. IBM SPSS Statistics 19 (IBM Japan, Ltd., Tokyo, Japan) was used for statistical analyses.

Author Contributions

Conceived and designed the experiments: GM SM NN. Performed the experiments: GM NN NI SM YS YI. Wrote the paper: GM SM KY YI.

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