Abstract: In recent years, worldwide research has been focused on clean and sustainable energy sources that can respond to the exponentially rising energy demands of humankind. The harvesting of unused heat in relation to automotive exhaustion, industrial processes, and home heating is one possible way of enabling the transformation from a fossil fuel-based society to a low-carbon socioeconomic epoch. Thermoelectric (TE) generators can convert heat to electrical energy thanks to high-performance TE materials that work via Seebeck effects when electricity appears between the cold part and the hot part of these materials. High figure of merit ($ZT$) TE material is characterized by high electrical conductivity and Seebeck coefficient, together with low thermal conductivity. This article aims to summarize $ZT$ values reported for chalcogenides, skutterudites, and metal oxides with graphene (G) or reduced graphene oxide (rGO), and intends to understand the relationship between the addition of G-rGO to composites and $ZT$ variation. In a majority of the publications, $ZT$ value increases with the addition of G/rGO, although the relative growth of $ZT$ varies for different material families, as well as inside the same group of materials, with it often being related not to a G/rGO amount but with the quality of the composite.

Keywords: graphene; reduced graphene oxide; thermoelectrics; chalcogenides; skutterudites; oxides; figure of merit; thermal conductivity; electrical conductivity; Seebeck coefficient

1. Introduction

In view of the current climate change problem, thermoelectric (TE) energy conversion is considered particularly attractive for harvesting electricity from solar heat or for recovering waste heat [1–4]. The use of waste heat as source of electrical energy in vehicles is also an attractive option for major automotive manufacturers, who actively pursue this technology to implement thermoelectric generators (TEGs) in car exhaust systems [5]. Moreover, it can significantly reduce the amount of CO$_2$ in industrial production processes. Furthermore, silent, reliable, and versatile TEGs without moving parts [6] can be used to power portable electronic devices as additional sources of energy.

Thus, TEGs hold a tantalizing promise of greater energy efficiency by providing a robust and clean option for waste heat recovery and its conversion into useful electrical energy through the Seebeck effect [7–10]. Moreover, their size can be easily varied, since TEGs consist of TE modules, which include multiple n- and p-type semiconductor couples connected electrically in series and thermally in parallel [11]. Both types of TE materials are widely studied and characterized by the dimensionless figure of merit at the absolute temperature, $T$:

$$ZT = \frac{\sigma \times S^2 \times T}{k}$$

Accordingly, efficient TE materials should possess a great Seebeck coefficient, $S$, and a high electrical conductivity, $\sigma$, but a low thermal conductivity, $k$. Then, a high voltage
related to the Seebeck coefficient can be generated by TE material placed in a temperature gradient. Electrical conductivity, $\sigma$, should be high to reduce the internal resistance of the material. Thermal conductivity of material, $k$, should be low to create a large temperature difference between the ends of the TE material.

However, $\sigma$ is directly proportional to the carrier concentration, $n$, but Seebeck coefficient $S$, being proportional to $n^{-2/3}$, according to the Pisarenko relation for doped semiconductors [12], depends on the carrier concentration in the opposite way. Moreover, there is a direct relationship between $\sigma$ and the electronic contribution to thermal conductivity following from $\sigma/k \sim T$ [13,14]. Thus, an enhancement of the conversion efficiency is a major challenge for the implementation of TE energy conversion. Moreover, TE materials should also be stable under operating conditions, as well as having long life cycles, greater cost efficiency, and compatibility with existing technologies.

Nowadays, both p- and n-type of TE materials can show a high value of $ZT$ that strongly depends on the material properties, such as stoichiometry/doping level, charge carrier concentration, and prevailing scattering mechanisms, as well as on processing methods/conditions [15,16]. The top $ZT$ values are up to ~2.8 at 773 K [17] and ~2.6 at 923 K [18], reported for n-type Br-doped and p-type nanostructured SnSe, respectively. $ZT$ up to ~2.2 at 915 K for n-type PbTe [19] and ~1.9 at 320 K for n-type Bi$_{0.5}$Sb$_{1.5}$Te were also reported [20]. All these systems belong to the family of chalcogenide TE materials. However, typically, $ZT$ reported for other chalcogenides such as Bi$_2$Te$_3$ or Sb$_2$Te$_3$ [21], or for skutterudites such as CoSb-family materials [22], or for metal oxides, which are promising for high-T applications due to their robustness, is lower (<1.8) [23]. Among them, metal oxide TE materials possess a considerably smaller figure of merit so far, but they are more cost-effective and high-T stable than heavy metal alloys [24–26].

From the other side, graphene (G), a one-atom-thick sheet of carbon with a high electron mobility of 230,000 cm$^2$ V$^{-1}$ s$^{-1}$ and 125,000 cm$^2$ V$^{-1}$ s$^{-1}$ at 4.2 K and room $T$, respectively [27], is widely considered as a functional additive [28]. Moreover, its composites with different TE materials, particularly with polyaniline, poly(3,4-ethylenedioxythiophene) and other polymers are also studied [28]. However, typically, much less agglomerative graphene oxide (GO) that can be easily reduced by chemical or heat treatment, or already reduced graphene oxide (rGO), are used in a majority of reported composites because they are cheaper and easier to prepare than high quality monolayer graphene.

Moreover, 3D network wrapping structures (or core-shell nanocomposites) with a shell layer of a few nm have been theoretically shown [29] and experimentally confirmed to strengthen the phonon scattering that could suppress thermal conductivity, and, thus, enhance $ZT$ [30]. According to this model, if the secondary phase could be dispersed as a nanoscale shell layer on the grains of the matrix phase (core), the heat-carrying phonons would be effectively scattered; this is because of the enhanced interparticle and intraparticle boundary scattering with an increased number of interfaces [30]. An additional $ZT$ enhancement is expected if the 3D network nanocomposite contains a wrapping phase that can scatter the phonons but maintain high electron transport. Furthermore, high electrical conductivity of the wrapping phase should be accompanied by a suitable band gap, matching with that of the matrix, to enhance the Seebeck coefficient, thus realizing an energy filtering effect in such a 3D wrapping structure. Zong et al. have shown that these demands can be satisfied using rGO as the wrapping phase because of its low thickness, high electrical conductivity (electron mobility), and band gap that can be tuned by the reduction degree (the oxygen ratio in rGO after chemical or/and thermal reduction of GO) [30]. In addition, besides the charge carrier mobility, a charge carrier density can also be enhanced in oxide TE materials by the carbon stimulated formation of oxygen vacancies [31]. Thus, a number of works were published over the last few years on G-rGO modified TE materials. In this article, a literature overview and discussion of TE performance on chalcogenides, skutterudites, and metal oxides with G-rGO additives are presented.
2. Current Achievements for Thermoelectric Materials with Graphene or Reduced Graphene Oxide

2.1. Chalcogenides

Among the chalcogenide family, Bi- and Te-based alloys are the most studied p- and n-type TE materials used in both bulk and thin film commercial applications [32]. That is because they possess a combination of relatively high Seebeck coefficient with great electrical conductivity and low thermal conductivity, which results in an elevated TE figure of merit (ZT).

In 2013, Liang et al. [33] and Dong et al. [34] first fabricated chalcogenide Bi$_2$Te$_3$ with G, and PbTe with rGO. Both research groups used a spark plasma sintering (SPS) process for the densification of the obtained TE materials. Moreover, in both cases the studied composites presented slightly decreasing relative densities when the G or rGO contents increased. Moreover, the grain sizes of the pristine ceramics were found to be larger than those of the composites, as can be seen in the scanning electron microscopy (SEM) images in Figure 1 for Bi$_2$Te$_3$, without and with graphene [33]. At the same time, the decrease in the grain size enhances the grain boundary phonon scattering, which is beneficial for the reduction in thermal conductivity [33]. The maximum ZT values were reported to increase from 0.16 to 0.21 at 475 K, with 0.2 vol.% G addition to Bi$_2$Te$_3$ [33], and from 0.12 to 0.7 at 670 K, with 5 wt.% GO addition to PbTe [34].

![Figure 1. SEM images of bulk Bi$_2$Te$_3$ with 0 (a) and 2 vol.% (b) graphene addition [33].](image)

At the same time, in 2013, Chen et al. first studied Cu-based chalcogenide TE material CuInTe$_2$ in composite, with G obtained from expanded graphite with mass ratios of 80:1 and 40:1 [35]. The authors reported that, in incorporating G sheets into the CuInTe$_2$ matrix, thermal conductivity was successfully decreased, thus leading to an enhanced ZT of 0.4 at 700 K for CuInTe$_2$ composite, with G in 80:1 ratio, compared to 0.39 at 700 K for pristine CuInTe$_2$ [35]. Further, two Cu-based chalcogenide TE materials such as Cu$_2$SnSe$_3$ [36] and Cu$_2$ZnSnS$_4$ [37] were modified by G with different concentrations. The lattice thermal conductivity of these chalcogenides decreased in composites with a low G amount, effectively resulting from the phonon scattering by the graphene interface, similar to Bi$_2$Te$_3$ with G [33] or PbTe with GO [34]. However, when the fraction of graphene exceeds a certain value, the thermal conductivity of the composites starts to increase; this is because of an increase in the interface thickness instead of interface area due to the tendency to aggregation of graphene nanosheets reported in both these works [36,37]. The maximum figure of merit for Cu$_2$SnSe$_3$ with 0.25 vol.% G was 0.44 at 700 K [36], and ZT of 0.5 at 623 K was obtained for Cu$_2$ZnSnS$_4$ with 0.75 wt.% G [37].

Besides the SPS Bi$_2$Te$_3$ reported in 2013 by Liang et al. [33], in 2016, Agarwal et al. used simple mixing and pressing of commercial Bi$_2$Te$_3$ with 0.05 wt.% commercial G without sintering or other processing [38]. Investigating obtained composites by nanoscale atomic force microscopy, conductive atomic force microscopy, Kelvin probe force microscopy and
scanning thermal microscopy, $ZT$ was reported to be up to 0.92 at 402 K according to these local technique studies [38].

In addition to pristine $\text{Bi}_2\text{Te}_3$, its alloys $\text{Bi}_x\text{Sb}_y\text{Te}_3$ ($x = 0.36–0.5, y = 1.5–1.64$) [39–44] and $\text{Bi}_2\text{Te}_2\text{Se}_0.3$ [45] were also modified by G or rGO and studied. All of them have shown enhanced $ZT$ after the addition of G or GO, up to certain concentrations. $ZT$ values for chalcogenides with G or rGO are presented in Table 1 and in Figure 2 for comparison. Table 1 shows also their thermal and electrical conductivities, as well as their Seebeck coefficient values.

Table 1. The composite preparation methods and conditions. The highest value of $ZT$ ($ZT_{\text{max}}$) at the corresponding temperature ($T_{ZT_{\text{max}}}$), as well as the thermal conductivity ($k$), electrical conductivity ($\sigma$) and Seebeck coefficient ($S$) at that temperature reported for composites of chalcogenide TE materials with graphene or reduced graphene oxide.

| TE Material | G or rGO, Method | $T$ Range, K | $ZT_{\text{max}}$ (at $T_{ZT_{\text{max}}}$, K) | $k$ at $T_{ZT_{\text{max}}}$, W/(m × K) | $\sigma$ at $T_{ZT_{\text{max}}}$, $\Omega$ cm | $S$ at $T_{ZT_{\text{max}}}$, $\mu$V/K | Ref. |
|-------------|-----------------|--------------|--------------------------------|-----------------|-----------------|-----------------|----|
| $\text{Bi}_2\text{Te}_3$ ingots | GO com. 0–2 vol.% SPS 350 °C 6 min 80 MPa | 300–472 | 0.21 (472)/0.2 vol.% | 2.2 | 75 | −114 | [33] |
| $\text{Bi}_2\text{Te}_3$ beads | GO by HM 0–10 wt.% HP 350 °C 10 min 50 MPa | RT | 0.3 (RT)/1 wt.% | 0.56 | 33 | −160 | [46] |
| $\text{Bi}_2\text{Te}_2$ NWs by WCSR | GO by HM 0–10 wt.% HP 350 °C 10 min 50 MPa | RT | 0.4 (RT)/1 wt.% | 0.48 | 41 | −180 | [46] |
| $\text{Bi}_2\text{Te}_3$ com. | G com. 0, 0.05 wt.% Mix, press 7 min, 2 MPa | 300–480 | 0.92 (402)/0.05 wt.% | 0.95 | 80 | −145 | [38] |
| $\text{Bi}_2\text{Te}_3$ ingots | G com. 0.1 wt.% SPS 420 °C 2 min, 30 MPa | 300–523 | 0.75 (360)/0.05 wt.% | 1.1 | 75 | −170 | [45] |
| $\text{Bi}_2\text{Te}_3$ ingots | G 0–0.8 vol.% SPS 480 °C 3 min, 60 MPa | 300–473 | 1.16 (393)/0.4 vol.% | 1.26 | 1 | 195 | [42] |
| $\text{Bi}_2\text{Te}_3$ ingots | G by exf. 0–0.4 vol.% HP 350 °C 1 h, 600 MPa | 293–498 | 1.54 (440)/0.4 vol.% | 0.8 | 74 | 200 | [41] |
| $\text{Bi}_2\text{Te}_3$ ingots | GO com. 0–2 wt.% SPS 480 °C 5 min, 50 MPa | 300–480 | 1.0 (400)/0.1 wt.% | 1.1 | 75 | 190 | [43] |
| $\text{Bi}_2\text{Te}_3$ ingots | G com. 0–1 vol.% HFIHS 370 °C 35 MPa | 300–500 | 1.2 (375)/0.5 vol.% | 0.7 | 55 | 215 | [44] |
| $\text{Bi}_2\text{Te}_3$ ingots | G com. 0–0.15 wt.% SPS 420 °C 10 min, 60 MPa | 300–550 | 1.25 (320)/0.05 wt.% | 1.1 | 100 | 230 | [40] |
| $\text{Bi}_2\text{Te}_3$ ingots | G by MW-EGt, 0–0.5 vol.% SPS 390 °C 3 min, 70 MPa | 300–473 | 1.13 (360)/0.1 vol.% | 0.7 | 55 | 200 | [39] |
| $\text{Bi}_2\text{Te}_3$ ingots | G by MW-EGt 0–0.1 vol.% SPS 480 °C 3 min, 70 MPa | 300–473 | 1.24 (360)/0.1 vol.% | 0.8 | 57.5 | 230 | [39] |
| $\text{Cu}_2\text{SnSe}_2$ ingots | GO com. 0–0.1 vol.% SPS 587 °C 8 min, 50 MPa | 300–700 | 0.44 (700)/0.25 vol.% | 1.0 | 0.125 | 220 | [36] |
| $\text{CuInTe}_2$ ingots | G from EGt 1.2, 2.4 wt.% SPS 500 °C 10 min, 60 MPa | 300–700 | 0.40 (700)/1.2 wt.% | 1.25 | 13.5 | 225 | [35] |
| $\text{Cu}_2\text{ZnSnS}_3$ ingots | G com. 0–1 wt.% HP 350 °C 15 min, 80 MPa | 300–700 | 0.5 (623)/0.75 wt.% | 0.5 | 30 | 120 | [37] |
| PbTe in-situ | GO by HM 0–10 wt.% SPS 580 °C 5 min, 30 MPa | 300–670 | 0.7 (670)/5 wt.% | 0.7 | 1.25 | −250 | [34] |

Here WCSR—wet-chemical synthetic route; com.—commercial; exf.—exfoliation; US—ultrasonication; MW—microwave (synthesis); STS—solvothermal synthesis; HM—Hummer’s method; Get—expanded graphite; SPS—spark plasma sintering; HP—hot-pressing; HFIHS—high frequency induction heated sintering.
Here WCSR—wet-chemical synthetic route; com.—commercial; exf.—exfoliation; US—ultrasonication; MW—microwave; HP—hot-pressing; HFIHS—high frequency induction heated sintering.

As it turned out, the method of TE material preparation can also affect the ZT value. Particularly, Bi$_{0.5}$Sb$_{1.5}$Te$_3$ made using microwave-induced solvothermally synthesized Bi$_2$Te$_3$ and Sb$_2$Te$_3$ nanoplates with 0.1 vol.% G have shown a maximum ZT of 1.13 at 360 K, in comparison to ZT of 1.24 at 360 K for the same Bi$_{0.5}$Sb$_{1.5}$Te$_3$ obtained by a ball-milling process with the same amount of G [39].

At the same time, the composite of Bi$_2$Te$_3$ nanowires (NW) fabricated by a wet-chemical synthetic route (WCSR) with rGO can have slightly higher room-temperature ZT of 0.4 than that of 0.3 for a composite made of Bi$_2$Te$_3$ powder with the same 1 wt.% rGO [46], as can be seen in Table 1. Performance enhancement was connected to higher electrical conductivity and lower thermal conductivity of G-rGO composites with nanowires. Smaller dimensions of the NWs, and, thereby, a higher interface/boundary number in Bi$_2$Te$_3$-NW composite with G than this number in the Bi$_2$Te$_3$-powder composite with G, was suggested as an explanation for the low thermal conductivity [46].

As can be seen from Figure 2, the highest ZT of 1.54 at 440 K was reported by Li et al. for Bi$_{0.4}$Sb$_{1.6}$Te$_3$ with 0.4 vol.% exfoliated G [41]. Other p-type Bi$_{x}$Sb$_y$Te$_3$ chalcogenides with G-rGO have shown lower ZT values with a visible peak at a relatively low T, up to 400 K [39,40,42–44], in contrast to p-type composites of Cu-based chalcogenides (Cu$_2$SnSe$_3$, CuInTe$_2$ and Cu$_2$ZnSnS$_4$) and G-rGO [35–37], with ZT continuously increasing up to the limit of the measured T range of 650–700 K. At the same time, reported n-type chalcogenide TE materials with G-rGO have also shown dissimilarities in the temperature variation of ZT. Evident low-T peak is detected for Bi$_2$Te$_2.7$Se$_{0.3}$ [45] and for Bi$_2$Te$_3$ [38], while no peak is seen for SPS densified Bi$_2$Te$_3$ with G [33], or for PbTe with GO [34].

2.2. Skutterudites

Skutterudites with a general formula of MX$_3$ (M = Co, Rh, or Ir; X = P, As, or Sb) have an open frame (“cagey”) structure with a body-centered cubic unit cell and a network of corner-sharing octahedra, each of which consists of one M atom in the center and six X atoms vertices [47,48]. Such a structure has motivated works on filling the cages with diverse atoms, in conjunction with the routine substitutional doping efforts, to tailor specific application functions described in many articles, including reviews [22,49]. Another
strategy to enhance the TE performance of materials such as skutterudites involves the incorporation of a secondary phase, particularly 2D graphene or reduced graphene oxide, into the core-shell nanocomposites with 3D network wrapping structures [30]. Among the composites of skutterudites with G or rGO, materials such as pristine CoSb$_3$ [50] and related Yb$_{0.27}$Co$_4$Sb$_{12}$ [30], Ce$_{0.85}$Fe$_3$Co$_4$Sb$_{12}$ [51], and La$_{0.8}$Ti$_{0.1}$Ga$_{0.1}$Fe$_3$Co$_4$Sb$_{12}$ [52] were reported.

In 2013, Feng et al. first reported p-type nanocomposite with GO added to CoSb$_3$ during the solvothermal process, performed at 290 °C for 12 h [50]. After hot pressing under 80 MPa at 600 °C for 2 h, the CoSb$_3$ bulk hybrid with rGO has shown homogeneously embedded graphene in the nanostructured CoSb$_3$ matrix (see Figure 3a,b). The obtained $ZT$ value of 0.81 at 800 K for CoSb$_3$ with 1.5 wt.% GO was found to be more than twice as high as that of bare CoSb$_3$ [50]. Reported enhancement of $ZT$ for CoSb$_3$ with the addition of a small G amount was attributed to significantly increased carrier’s concentration and their mobility, and, thereby, electrical conductivity. Moreover, the well dispersed graphene in the nanostructured CoSb$_3$ matrix prepared by solvothermal route also contributed to the diminished lattice thermal conductivity [50]. In addition, $ZT \approx 0.45$ at 650 K was reported for CoSb$_3$ also prepared by a solvothermal process with 1 wt.% commercial G, but at lower temperature of 240 °C during 24 h, with further sintering at 500 °C by Yadav et al. [53].

![Schematic illustration of the formation mechanism and SEM image of (a) CoSb$_3$/G bulk sample after hot pressing (reprinted from [50] with permission from Royal Society of Chemistry). Morphology and structure of the Yb$_{0.27}$Co$_4$Sb$_{12}$/rGO composite: (c) SEM image of the fractured surface of the sintered skutterudite/rGO composite and (b) high magnification TEM image showing the rGO nanolayer of ~3–5 nm thickness for the 0.72 vol.% rGO sample (reprinted from [30] with permission from Royal Society of Chemistry).](image)

The highest $ZT$ of 1.52 at 850 K was reported by Zong et al., for SPS densified composite of n-type Yb$_{0.27}$Co$_4$Sb$_{12}$ skutterudite, prepared by conventional solid-state melting method and 0.72 vol.% GO [30]. SEM (see Figure 3c) and transmission electron microscopy (TEM) analysis (see Figure 3d) revealed that rGO embedded in boundaries of Yb$_{0.27}$Co$_4$Sb$_{12}$ was wrapped and 3–5 nm thick. Thus, 3D-rGO network wrapping architecture dramatically reduced the lattice thermal conductivity due to enhanced interparticle and intraparticle phonon scattering effects, and simultaneously enhanced the Seebeck coefficient.
due to the energy filtering effect of the grain boundary semiconductive rGO layer with nanometer thickness, resulting in high ZT [30]. Moreover, both when GO was added to Ce₀.₈₅Fe₃CoSb₁₂ [51] and when G was grown in-situ by plasma-enhanced chemical vapor deposition (PECVD) in La₀.₄₅T₀.₅₅Gaₐ.₁Fe₃CoSb₁₂ [52], the values of ZT increased in comparison to pure CoSb₃ or CoSb₃ with G or rGO, as can be seen in Table 2 and in Figure 4.

Table 2. The composite preparation method and conditions, the highest value of ZT (ZTmax) at the corresponding temperature (T ZTmax), as well as the thermal conductivity (k), electrical conductivity (σ) and Seebeck coefficient (S) at that temperature reported for composites of skutterudite TE materials with graphene or reduced graphene oxide.

| TE Material | G-rGO Used Amount | Method | T Range | ZTmax (at T ZTmax) | k at T ZTmax | σ at T ZTmax | S at T ZTmax | Ref. |
|-------------|-------------------|--------|---------|--------------------|--------------|--------------|---------------|-----|
| CoSb₃ by STS | GO by HM 0.1, 1.5 wt.% | HP 600 °C 2 h, 80 MPa | 300-850 | 0.61 (800)/1.5 wt.% | 1 | 4.5 | 100 | [50] |
| CoSb₃ by STS | G 1 wt.% | CSM, 500 °C 5 h, 10⁻³ Torr | 300-700 | 0.45 (650)/2 wt.% | 1.75 | 11.9 | 45 | [53] |
| Ce₀.₈₅Fe₃CoSb₁₂ ingots | GO by HM 0–2.8 vol.% | SPS 600 °C 15 min, 35 MPa | 300-800 | 1.06 (700)/1.4 vol.% | 1.85 | 80 | 180 | [51] |
| La₀.₄₅T₀.₅₅Gaₐ.₁Fe₃CoSb₁₂ ingots | G by PECVD | HP 650 °C 1 h, 90 MPa | 300-800 | 1 (723) | 2 | 70 | 190 | [52] |
| Yb₀.₂₇Co₄Sb₁₂ ingots | Wrapped rGO 0–3.6 vol.% | SPS 627 °C 10 min, 60 MPa | 300-850 | 1.52 (850)/0.72 vol.% | 3 | 150 | −195 | [30] |

Here STS—solvothermal synthesis; CS—chemical synthesis; HM—Hummer’s method; PECVD—plasma-enhanced chemical vapor deposition; HP—hot-pressing; CSM—conventional sintering method; SPS—spark plasma sintering.

Figure 4 presents that all the reported skutterudite materials combined with G-rGO show increase of ZT with the temperature. Moreover, p-type materials can show a peak of ZT at 700–800 K in contrast to the only reported n-type skutterudite Yb₀.₂₇Co₄Sb₁₂ with rGO that presented no peak or saturation up to 850 K. In addition, the highest ZT reported for p-type (Ce,Fe)CoSb₁₂ with rGO (ZT of 1.06 at 700 K for Ce₀.₈₅Fe₃CoSb₁₂ [51]) is very close to ZT obtained for more complex multicomponent p-type skutterudites without addition.

Figure 4. The figure of merit ZT of p- and n-type skutterudite TE materials adapted from the references presented in Table 2.
of G or rGO such as \((\text{La,Ce,Fe})\text{CoSb}_{12}\) \((ZT)\) of 1.15 at 748 K in \(\text{La}_{0.68}\text{Ce}_{0.22}\text{Fe}_{3.5}\text{Co}_{0.5}\text{Sb}_{12}\) \([54]\) or \((\text{Ca,Ce,Nb,Fe})\text{CoSb}_{12}\) \((ZT)\) of 1.1 at 748 K for \(\text{Ca}_{0.35}\text{Ce}_{0.35}\text{Nd}_{0.35}\text{Fe}_{3.5}\text{Co}_{0.5}\text{Sb}_{12}\) \([55]\). Moreover, the highest \(ZT\) value of 1.52 at 850 K reported for unique n-type skutterudite \(\text{YP}_{0.27}\text{Co}_{4}\text{Sb}_{12}\) with rGO \([45]\) is not far from \(ZT\) of 1.8 at 823 K reported for the more complicated n-type \((\text{Sr,Ba,Yb})\text{CoSb}_{12}\) with 0.91 wt.% \(\text{In}_{0.1}\text{CoSb}_{12}\) \([56]\). Thus, TE performance similar to that of complex skutterudites can be obtained by adding G or rGO to simpler structures.

### 2.3. Metal Oxides

In contrast to chalcogenides, skutterudites or other TE materials, metal oxides are not so deeply studied yet and there are only few well known p-type materials such as \(\text{Na}_{x}\text{CoO}_{2}\) and \(\text{Ca}_{3}\text{CoO}_{4+y}\), which have been found very promising especially in high \(T\) range, benefiting from their layered structure. \(\text{BiCuSeO}\) as well as n-type \(\text{CaMnO}_{3-}\) and \(\text{SrTiO}_{3}\)-based materials are also among the most studied TE oxides \([57–59]\), summarized in Table 3 and presented in Figure 5, but there is no available report on p-type metal oxide TE materials modified by G-rGO.

#### Table 3. The composite preparation method and conditions. The highest value of \(ZT (ZT_{\text{max}})\) at the corresponding temperature \((T_{ZT_{\text{max}}})\), as well as the thermal conductivity \((k)\), electrical conductivity \((\sigma)\) and Seebeck coefficient \((S)\) at that temperature, reported for composites of metal oxide TE materials with graphene or reduced graphene oxide.

| TE Material | G-rGO Used Amount | Method | \(T_{\text{Range}}\) | \(ZT_{\text{max}}\) at \(T_{ZT_{\text{max}}}\) | \(k\) at \(T_{ZT_{\text{max}}}\) | \(\sigma\) at \(T_{ZT_{\text{max}}}\) | \(S\) at \(T_{ZT_{\text{max}}}\) | Ref. |
|-------------|------------------|--------|------------------|-------------------------------|-------------------|-------------------|-------------------|-----|
| \(\text{SrTiO}_{3}\) com. | G by HM, 0.64 vol.% | SPS 1200 °C 5 min, 60 MPa | 300–760 | 0.09 (760)/0.64 vol.% | 3 | 3 | −375 | \([31]\) |
| \(\text{SrTiO}_{3}\) by SSS | G | SPS 1300 °C 15 min, 60 MPa | 300–723 | 0.05 (723)/0.7 wt.% | 3.5 | 2.5 | −350 | \([60]\) |
| \(\text{La}_{0.10}\text{Sr}_{0.90}\text{TiO}_{3}\) by SSS | G by exfoliation, 0–1 wt.% | CSM 1457 °C 24 h | 273–1033 | 0.42 (273)/0.6 wt.% | 1.8 | 200 | −120 | \([61]\) |
| \(\text{SrTiO}_{3}\text{Nb}_{0.10}\text{O}_{3}\) by SSS | G by HM, 0.6 wt.% | CSM 1570 °C 10 h | 315–1160 | 0.24 (1160)/0.6 wt.% | 3.5 | 5 | −200 | \([62]\) |
| \(\text{Sr}_{0.85}\text{Ti}_{0.15}\text{Nb}_{0.10}\text{O}_{3}\) by SSS | G by HM, 0.6 wt.% | CSM 1570 °C 10 h | 315–1160 | 0.29 (1160)/0.6 wt.% | 3 | 5 | −200 | \([62]\) |
| \(\text{Sr}_{0.85}\text{Ti}_{0.15}\text{Nb}_{0.10}\text{O}_{3}\) by HTS | G by HM, 0.6 wt.% | CSM 1570 °C 10 h | 315–1160 | 0.27 (1160)/0.6 wt.% | 3.1 | 10 | −180 | \([62]\) |
| \(\text{Sr}_{0.85}\text{Ti}_{0.15}\text{Nb}_{0.10}\text{O}_{3}\) by SSS | G by HM, 0.6 wt.% | SPS 1300 °C 80 MPa | 300–800 | 0.22 (800)/0.6 wt.% | 3 | 0.2 | −200 | \([63]\) |
| \(\text{Sr}_{0.85}\text{Ti}_{0.15}\text{Nb}_{0.10}\text{O}_{3}\) by SSS | G by HM, 0–2 wt.% | SPS 1427 °C 7 min, 50 MPa | 300–1200 | 0.5 (1200)/1.5 wt.% | 3.5 | 45 | −190 | \([64]\) |
| \(\text{Sr}_{0.85}\text{La}_{0.15}\text{Ti}_{0.15}\text{Nb}_{0.10}\text{O}_{3}\) by SSS | G by exfoliation, 0–1 wt.% | SPS 1200 °C 5 min, 50 MPa | 300–1000 | 0.07 (1000)/1 wt.% | 2.2 | 2 | −220 | \([65]\) |
| \(\text{ZnO}\) com. | G com., 0–2 wt.% | SPS 900 °C 5 min, 70 MPa | 273–1073 | 0.04 (1073)/1 wt.% | 7 | 4 | −220 | \([66]\) |
| \(\text{Zn}_{0.85}\text{Al}_{0.15}\text{O}\) by CS | G by HM, 0–3.5 wt.% | HP 900 °C 2 h, 75 MPa | 273–1173 | 0.28 (1173)/1.5 wt.% | 2.5 | 75 | −95 | \([67]\) |
| \(\text{TiO}_{2}\) com. | G com., 0–4 wt.% | SPS 900 °C 5 min, 50 MPa | 300–1100 | 0.064 (1050)/4 wt.% | 1.2 | 5 | −100 | \([68]\) |
| \(\text{BaTiO}_{3}\) com. | G by HM, 1.5–4 wt.% | SPS 1100 °C 1 min, 80 MPa | 300–600 | 0.08 (600)/1.7 wt.% | 2.5 | 0.25 | −380 | \([69]\) |

Here com.—commercial; SSS—solid-state synthesis; HTS—hydrothermal synthesis; CS—chemical synthesis; HM—Hummer’s method; exf.—exfoliation; SPS—spark plasma sintering; CSM—conventional sintering method; HP—hot-pressing.
A composite of commercial powder of pure SrTiO$_3$ with rGO densified by SPS was studied by Feng et al., which reported a ZT value of 0.09 at 760 K for 0.64 vol.% GO [31]. That is higher than the ZT of 0.05 at 673 K reported for the similar composite densified by SPS, but with SrTiO$_3$ powder obtained by conventional solid-state reaction method and mixed with 0.7 wt.% GO by Rahman et al. [60]. However, in both cases, the authors reported significantly enhanced ZT after the addition of GO. Feng et al. also reported that room-T electrical conductivity of SrTiO$_3$ densified in vacuum by SPS increases from 18 S/m to 1633 S/m, after the addition of rGO and without any additional reducing process [31]. Based on electron energy-loss spectroscopy analysis and low-angle annular dark field imaging, Feng et al. concluded that rGO in composite with SrTiO$_3$ serves as a carbon source that promotes the formation of oxygen vacancies via a mild reaction with oxygen atoms on the surface of SrTiO$_3$ grains, and that is the reason behind the highly increased carrier density for SrTiO$_3$ with rGO [31].

Moreover, although the pristine SrTiO$_3$ was doped by many different elements, such as La, Nd, Sm, Gd, Dy, Y, Er Pr, Yb, Ta, Nb, etc., to enhance ZT [57,59], the G-rGO effect on ZT was studied only on SrTiO$_3$ doped by La, incorporated at Sr-site [61], or by Nb in Ti-position [62,63], or simultaneously doped by La and Nb [65]. In general, the ZT of Nb- and simultaneously La,Nb-doped SrTiO$_3$ composites with G-rGO were found to increase with the temperature, and the highest ZT values were reported at the highest measured T of these composites without an obvious peak (see Figure 5).

The addition of 0.6 wt.% GO to SrTi$_{0.90}$Nb$_{0.10}$O$_3$, prepared by the conventional method, leads to ZT of 0.24 at 1160 K, as was reported by Okhay et al. [62]. At the same time, almost zero ZT was detected by Dey et al. for SPS SrTi$_{0.85}$Nb$_{0.15}$O$_3$ with 0.5 wt.% GO; that was significantly enhanced, however, to 0.5 at 1200 K by further increase of GO amounts up to 1.5 wt.% [64]. Considering Sr vacancy as a defect that can serve for phonon scattering, and thus decrease thermal conductivity and increase ZT, Okhay et al. studied composites of G-rGO with nonstoichiometric Nb-doped SrTiO$_3$ with 2 mol.% Sr vacancies, achieving the highest ZT of 0.29 at 1160 K for Sr$_{0.98}$Ti$_{0.90}$Nb$_{0.10}$O$_3$ with 0.6 wt.% GO [62]. Following that direction, Wu et al. increased Sr deficiency to 7 mol.%, thus obtaining a ZT of 0.22 at 800 K for Sr$_{0.93}$Ti$_{0.90}$Nb$_{0.10}$O$_3$ + 0.6 wt.% GO nominal composition [63]. However, such high Sr...
deficiency should result not only in the formation of Sr vacancies but in the segregation of the titanium oxide secondary phase [70].

On the other hand, a $ZT$ of 0.36 at 1023 K was reported by Lin et al. for Sr-deficient La-doped strontium titanate $La_{0.067}Sr_{0.9}TiO_3$ with 0.6 wt.% G, obtained by exfoliation of graphite [61]. The high $ZT$ value is accompanied by the highest electrical conductivity and the lowest thermal conductivity in Table 3. The observed enhancement of electrical conductivity in La-doped $SrTiO_3$ with graphene loading was explained by the formation of a percolation network and the graphene-facilitated reduction of La-doped $SrTiO_3$ at the grain boundaries, resulting in faster electronic transport. Similar to other TE materials, Lin et al. also posited that the introduction of G lead to significant reduction in grain size of the nanocomposites from 2.2 $\mu$m for pristine La-doped $SrTiO_3$ to 0.12 nm when 0.6 wt.% G was added. Such nanotexturing introduces significant lattice scattering and, hence, reduces the thermal conductivity of the composite [61]. However, the reason for the decrease in thermal conductivity on cooling below 500 K reported by Lin et al., for $La_{0.067}Sr_{0.9}TiO_3$ with 0.6 wt.% G, and thereby for room temperature $ZT$ with a value of 0.42, is still unclear, since no other report on graphene-modified $SrTiO_3$-based TE materials, including that from the same group [65], has presented such variation.

Moreover, although both La-doped $SrTiO_3$ and Nb-doped $SrTiO_3$ with G-rGO present in Figure 5 and Table 3 rather high $ZT$, from 0.22 to 0.5, either the addition of solvent-derived flakes of graphene nanoplatelets to or the mixing GO prepared by the modified Hammer method with $Sr_{0.8}La_{0.067}Ti_{0.8}Nb_{0.2}O_{3-\delta}$ composition, was reported to lead to $ZT$ that does not exceed 0.07 at 1000 K [65].

In addition to the described above metal oxide TE materials, Chen et al. reported a $ZT$ of 0.28 at 1173 K for Al-doped $ZnO$ with 1.5 wt.% GO [67], which is much higher than 0.04 at 1073 K reported for pure $ZnO$ with 1 wt.% G [66], or even 0.064 at 1050 K for TiO$_2$ with 4 wt.% GO [68] and 0.08 at 600 K for BaTiO$_3$ with 1.7 wt.% GO [69].

In summary, according to the aforementioned reports, the $ZT$ of TE materials tends to be enhanced by G-rGO addition. However, the systematic studies of the G-rGO concentration influence on the TE performance of composite materials show that $ZT$ decreases after the application of a certain concentration of G or rGO, for all material types. Such an optimal concentration of G-rGO, at which the highest $ZT$ can be achieved, is individual for each composite and is reported to be between 0.1 and 1.4 vol.% (for chalcogenide $Bi_{0.5}Sb_{1.5}Te_3$ [37] and for skutterudite $Ce_{0.85}Fe_3CoSb_{12}$ [51], respectively) or from 0.05 to 4 wt.% (for chalcogenide $Bi_2Te_2.7Se_{0.3}$ [45] or $Bi_{0.48}Sb_{1.52}Te_3$ [40] and for metal oxide TiO$_2$ [68], respectively). However, the trend is general, and it deserves a comparative consideration involving all $ZT$ components in the next section.

3. Relationship between the Thermoelectric Performance of Materials and the Presence of Graphene or Reduced Graphene Oxide

According to Equation (1) for the dimensionless figure of merit, $ZT$ depends on electrical and thermal conductivity, as well as on the value of the Seebeck coefficient. As it was described above, the Seebeck coefficient decreases with increase in charge carrier concentration. Thus, a high $S$ can be observed in dielectric materials, such as undoped metal oxide, particularly $SrTiO_3$. After the addition of G-rGO to insulating pure $SrTiO_3$, its electrical conductivity increases and absolute value of $S$ decreases as can be seen in Figure 6a, as reported by Rahman et al. [60] and supported by Wu et al. [63]. However, $\sigma$ of $SrTiO_3$ can be significantly increased not only by the addition of G-rGO but also by Nb or La doping process [61,62,64]. Then, the addition of G-rGO to an already semiconductive material, such as heavily doped $SrTiO_3$, chalcogenides and skutterudites, does not lead to serious variations of $S$, as shown in Figure 6b–d, respectively, although they could be slightly enhanced in the case of $Yb_{0.27}Co_{0.4}Sb_{12}$ skutterudite (see Figure 6d) due to the energy filtering effect [30].
In accordance with the abovementioned statements, the electrical conductivity $\sigma$ of rather resistive metal oxides is significantly enhanced after G-rGO addition, as can be seen in Figure 7a, in comparison to less notable changes of $\sigma$ for initially conductive chalcogenides or skutterudites, as shown in Figure 8a. Moreover, there are several studies on chalcogenides ($\text{Bi}_{0.44}\text{Sb}_{1.56}\text{Te}_3$ [43], $\text{Bi}_{0.35}\text{Sb}_{1.5}\text{Te}_3$ [44]) and skutterudites ($\text{Yb}_{0.27}\text{Co}_4\text{Sb}_{12}$ [30], $\text{Ce}_{0.85}\text{Fe}_3\text{CoSb}_{12}$ [51]), with a reported decrease in electrical conductivity after the addition of G-rGO. In these articles, the authors stressed that the G-rGO nm-layer located between the grains can grow and form agglomerates, with increasing rGO content that leads to decreased charge carrier mobility and, thereby, electrical conductivity because of the boundary scattering effect. At the same time, both the carrier concentration and its mobility were typically increased with the addition of G-rGO in the metal oxides (see Figure 7b,c, respectively). However, in the case of the chalcogenides or skutterudites, the carrier concentration was reported only to change insignificantly, while the mobility of the carriers was not strongly raised in general with the increase of rGO content (see Figure 8b).
According to Figure 9, reported values of the thermal conductivity tend to decrease at least until a certain amount of G-rGO as for undoped SrTiO3 (see Figure 9a) [60] as for donor-doped SrTiO3 (see Figure 9b) [62], chalcogenide (see Figure 9c) [42] or skutterudite (see
Figure 9d) [30] composites. Such a decrease can be related to the enhanced interface phonon scattering, which is due both to the secondary phase of G-rGO at the grain boundaries of TE materials and to the enlarged number of grain boundaries caused by grain growth inhibition by G-rGO addition. Thus, thermal conductivity shows rather common behavior with G-rGO addition for all three TE material systems overviewed here, in contrast to electrical conductivity and the Seebeck coefficient.

ZT was also found to be usually enhanced by G-rGO addition until a certain amount, as shown in Section 2. For further analysis, we have used the published data to calculate the relative increase of ZT as a ratio between the figure of merit difference for TE material without G-rGO ($ZT_{\text{max without G-rGO}}$), and its composite with G-rGO ($ZT_{\text{max with G-rGO}}$) in relation to $ZT_{\text{max without G-rGO}}$:

$$\text{Relative increase of ZT} = \frac{ZT_{\text{max with G-rGO}} - ZT_{\text{max without G-rGO}}}{ZT_{\text{max without G-rGO}}} \times 100\%$$

Figure 9. Thermal conductivity of (a) undoped SrTiO$_3$, with 0, 0.3, 0.5, 0.7, 1, 2 and 4 wt.% rGO (from bottom to top) [60]; (b) SrTiO$_3$ doped by Nb as SrTi$_{0.90}$Nb$_{0.10}$O$_3$ (STN10), nonstoichiometric Sr$_{0.96}$Ti$_{0.90}$Nb$_{0.10}$O$_3$ (nSTN10) and Sr$_{0.96}$Ti$_{0.85}$Nb$_{0.15}$O$_3$ (nSTN15) and their composites with 0.6 wt.% GO, indicated, respectively, as STN10 + rGO, nSTN10 + rGO and nSTN15 + rGO (reprinted from [62] with permission from Elsevier); (c) Bi$_{0.36}$Sb$_{1.64}$Te$_3$ with 0, 0.1, 0.4, 0.8 vol.% GO (black, red, blue, and magenta dots and lines, respectively) (reprinted from [42] with permission from Elsevier); and (d) Yb$_{0.27}$Co$_4$Sb$_{12}$ with addition 0, 0.72, 1.8, and 3.6 vol.% rGO (reprinted from [30] with permission from Royal Society of Chemistry).
Calculated values of the increment of $ZT$ for chalcogenide, metal oxide and skutterudite TE materials are presented in Tables 4–6 and summarized in Figure 10.

**Table 4.** The highest $ZT$ values of chalcogenide materials before and after G-rGO addition, ordered from the lowest to highest $ZT$ values of TE materials without G-rGO, and calculated relative increase of $ZT$.

| TE Material          | $ZT_{\text{max}}$ without G-rGO | $ZT_{\text{max}}$ with G-rGO | Relative Increase of $ZT$, % | Ref. |
|----------------------|----------------------------------|-------------------------------|-----------------------------|------|
| Cu$_2$ZnSnS$_4$      | 0.11                             | 0.5                           | 355                         | [37] |
| PbTe                 | 0.12                             | 0.7                           | 483                         | [34] |
| Bi$_2$Te$_3$         | 0.145                            | 0.21                          | 44                          | [33] |
| Cu$_2$SnSe$_3$       | 0.24                             | 0.44                          | 83                          | [36] |
| Bi$_2$Te$_3$         | 0.68                             | 0.92                          | 23                          | [38] |
| Bi$_2$Te$_2$Se$_0.3$ | 0.65                             | 0.8                           | 15                          | [45] |
| Bi$_2$Te$_2$Se$_0.3$ | 0.65                             | 0.75                          | 35                          | [45] |
| Bi$_0.5$Sb$_{1.5}$Te$_3$ | 0.78                         | 1.13                          | 45                          | [39] |
| Bi$_0.48$Sb$_{1.52}$Te$_3$ | 0.9                         | 1.25                          | 39                          | [40] |
| Bi$_0.5$Sb$_{1.5}$Te$_3$ | 0.98                         | 1.24                          | 27                          | [39] |
| Bi$_0.44$Sb$_{1.56}$Te$_3$ | 1.0                         | 1.0                           | 0                           | [43] |
| Bi$_0.36$Sb$_{1.64}$Te$_3$ | 1.01                         | 1.16                          | 15                          | [42] |
| Bi$_0.4$Sb$_{1.6}$Te$_3$ | 1.4                            | 1.54                          | 15                          | [41] |
| Bi$_0.48$Sb$_{1.52}$Te$_3$ | 1.04                         | 1.2                           | 10                          | [44] |

**Table 5.** The highest $ZT$ values of skutterudite materials before and after G-rGO addition, ordered from the lowest to highest $ZT$ values of TE materials without G-rGO, and calculated relative increase of $ZT$.

| TE Material          | $ZT_{\text{max}}$ without G-rGO | $ZT_{\text{max}}$ with G-rGO | Relative Increase of $ZT$, % | Ref. |
|----------------------|----------------------------------|-------------------------------|-----------------------------|------|
| CoSb$_3$             | 0.26                             | 0.61                          | 135                         | [50] |
| La$_0.05$Ti$_0.1$Ga$_0.1$Fe$_3$CoSb$_{12}$ | 0.75                         | 1                             | 33                          | [52] |
| Co$_0.05$Fe$_3$CoSb$_{12}$ | 0.8                          | 1.06                          | 33                          | [51] |
| Yb$_{0.125}$Co$_4$Sb$_{12}$ | 1.25                         | 1.52                          | 22                          | [30] |

**Table 6.** The highest $ZT$ values of metal oxide materials before and after G-rGO addition, ordered from the lowest to highest $ZT$ values of TE materials without G-rGO, and calculated relative increase of $ZT$.

| TE Material          | $ZT_{\text{max}}$ without G-rGO | $ZT_{\text{max}}$ with G-rGO | Relative Increase of $ZT$, % | Ref. |
|----------------------|----------------------------------|-------------------------------|-----------------------------|------|
| SrLa$_{0.67}$Ti$_{0.9}$Nb$_{0.2}$O$_3$ | 0.0002                        | 0.07                          | 34900                       | [65] |
| TiO$_2$              | 0.0003                           | 0.064                         | 21233                       | [60] |
| ZnO                  | 0.005                            | 0.04                          | 700                         | [66] |
| SrTiO$_2$            | 0.009                            | 0.09                          | 900                         | [31] |
| SrTiO$_3$            | 0.02                             | 0.05                          | 150                         | [60] |
| Sr$_0.6$La$_{0.4}$Ti$_{0.8}$Nb$_{0.2}$O$_3$ | 0.02                         | 0.07                          | 250                         | [65] |
| SrTi$_{0.98}$Nb$_{0.12}$O$_3$ | 0.02                          | 0.05                          | 2400                        | [64] |
| Zr$_{0.98}$Al$_{0.02}$O$_3$ | 0.035                          | 0.28                          | 700                         | [67] |
| Sr$_0.6$La$_{0.4}$Ti$_{0.8}$Nb$_{0.2}$O$_3$ | 0.12                         | 0.22                          | 83                          | [63] |
| La$_{0.08}$Sr$_{0.9}$TiO$_3$ | 0.12                          | 0.42                          | 250                         | [61] |
| SrTi$_{0.98}$Nb$_{0.12}$O$_3$ | 0.17                          | 0.24                          | 41                          | [62] |
| Sr$_{0.98}$Ti$_{0.02}$Nb$_{0.18}$O$_3$ | 0.22                          | 0.27                          | 23                          | [62] |
| Sr$_{0.98}$Ti$_{0.02}$Nb$_{0.10}$O$_3$ | 0.27                          | 0.29                          | 7                           | [62] |
It is obviously seen in Figure 10 that the lowest relative increase of $ZT$ is calculated for the composites with the highest initial $ZT$ before the addition of G-rGO and vice versa. In the case that the materials have shown very low $ZT$ before the addition of G-rGO, their composite with graphene or reduced graphene oxide can show a high increment of $ZT$. Moreover, such a tendency can be found in all chalcogenide, skutterudite or metal oxide TE materials (see Figure 10). Thus, the fabrication of TE composites using the addition of up to 5 wt.% or 1.4 vol.% G or rGO can be an alternative, but not incremental method, for the preparation of high-performance TE materials.

4. Conclusions

Analyzing the available data on chalcogenide-, skutterudite- and metal oxide-based composites with graphene or reduced graphene oxide, it is possible to conclude that the addition of rather low amount of G-rGO is able to increase their final $ZT$, mainly enhancing the phonon scattering at grain boundaries of all these materials and increasing the charge carrier concentration and mobility in some of them, particularly in oxide thermoelectrics. However, that is mainly valid in the case of TE materials with low initial $ZT$. When TE material is already nanostructured and possesses high electrical conductivity, such an addition does not enhance $ZT$ significantly. Thus, G-rGO works mainly as an optimizer of the intrinsic performance of TE materials.

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Glossary

Com. commercial  
CS chemical synthesis  
CSM conventional sintering method  
EGt expanded graphite  
exf. exfoliation  
G graphene  
HFIHS high frequency induction heated sintering  
HM Hummer’s method  
HP hot-pressing  
HTS hydrothermal synthesis  
MW microwave (synthesis)  
NW nanowire  
PECVD plasma-enhanced chemical vapor deposition  
rGO reduced graphene oxide  
SEM scanning electron microscopy  
STS solvothermal synthesis  
SPS spark plasma sintering  
SSS solid-state synthesis  
TE thermoelectric  
TEG thermoelectric generator  
TEM transmission electron microscopy  
US ultrasonication  
WCSR wet-chemical synthetic route

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