Applications of Gauss-Radau and Gauss-Lobatto Numerical Integrations Over a Four Node Quadrilateral Finite Element

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Abstract

In this paper Gauss-Radau and Gauss-Lobatto quadrature rules are presented to evaluate the rational integrals of the element matrix for a general quadrilateral. These integrals arise in finite element formulation for second order Partial Differential Equation via Galerkin weighted residual method in closed form. Convergence to the analytical solutions and efficiency are depicted by numerical example.

Key words: Gauss-Radau, Gauss-Lobatto, Rational Integrals, Quadrilateral Finite Element.

Introduction

Various integrals are determined numerically in the evaluation of the element/stiffness matrix, mass matrix, body force vector, initial stress vector, the surface load vector etc., arising in Finite Element Method (FEM). Since the integrals in practical situations are not always simple but rational expressions in which the lower order quadrature scheme cannot evaluate exactly. Also there is no order of Gauss quadrature that will evaluate these integrals exactly (Zienkiewicz 1977, Bickford 1990, Yagawa et al. 1990). The integration points have to be increased in order to improve the integration accuracy and it is desirable to make these evaluations by using as few Gauss points (Stroud 1974, Burden and Faires 2002, Babolian et al. 2006) as possible, from the point of view of the computational efficiency.

In this aspect, a large number of articles are available in the literature using the quadrilateral element with straight sides, which is one of the most popular elements in FEM. The complications arise from two main sources (Barrett 1999): the large number of integrations that need to be performed and the presence of the determinant of the Jacobian matrix (which will be referred to simply as the Jacobian throughout this paper) in the denominator of the element matrices. For this some researchers have been attempted to

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develop analytical integration formula (Rathod and Islam 2002, Hacker and Schreyer 1989) for limited finite elements, but a huge amount of computing time and memory space are involved. Thus numerical integration is an essential task to strike a proper balance between accuracy and efficiency commonly applied for science and engineering problems.

However, this paper describes the finite element matrix by Galerkin weighted residual method using four node quadrilateral elements. Then a brief introduction of Gauss-Radau (Masjed-Jamei et al. 2005) and Gauss-Lobatto (Eslahchi et al. 2005) quadrature rules, which are previously applied to evaluate for single integrals, is presented in the next section. These numerical methods are exploited to evaluate the double integrals of rational functions belonging to the finite element matrix in this paper. A symbolic algebra package, Mathematica is used to generate this element matrix. Numerical accuracy and efficiency are demonstrated by comparing it with the conventional Gaussian quadrature as well as analytical method through numerical example.

**Explicit formulation of element matrix**

Let us consider an arbitrary four noded linear quadrilateral element in the global system \((x, y)\) which is mapped into a 2-Square in the local parametric system \((\xi, \eta)\) as shown in the following figure. Then the isoparametric coordinate transformation from \((x, y)\) plane to \((\xi, \eta)\) plane is given by,

\[
x = \sum_{i=1}^{4} x_i N_i(\xi, \eta) \quad \text{and} \quad y = \sum_{i=1}^{4} y_i N_i(\xi, \eta)
\]

where \((x_i, y_i), i = 1-4\), are the vertices of the element in \((x, y)\)-plane and denotes the 2D bilinear basis functions (Zienkiewicz 1977, Bickford 1990) with \((\xi_i, \eta_i)\) as the natural coordinates in \((\xi, \eta)\)-plane such that

\[
N_i = \frac{1}{4}(1+\xi_i)(1+\eta_i), \quad i = 1-4
\]

Now from equation (1) we have

\[
x = \frac{1}{4}[a_x + b_x \xi + c_x \eta + d_x \xi \eta] \quad \text{and} \quad y = \frac{1}{4}[a_y + b_y \xi + c_y \eta + d_y \xi \eta]
\]

where,

\[
\begin{align*}
a_x &= x_1 + x_2 + x_3 + x_4 \\
b_x &= -x_1 + x_2 + x_3 - x_4 \\
c_x &= -x_1 - x_2 + x_3 + x_4 \\
d_x &= x_1 - x_2 + x_3 - x_4
\end{align*}
\]

\[
\begin{align*}
a_y &= y_1 + y_2 + y_3 + y_4 \\
b_y &= -y_1 + y_2 + y_3 - y_4 \\
c_y &= -y_1 - y_2 + y_3 + y_4 \\
d_y &= y_1 - y_2 + y_3 - y_4
\end{align*}
\]

Hence the Jacobian can be expressed as:

\[
J = \frac{\partial(x, y)}{\partial(\xi, \eta)} = \frac{\partial x}{\partial \xi} \frac{\partial y}{\partial \eta} - \frac{\partial x}{\partial \eta} \frac{\partial y}{\partial \xi} = \alpha_0 + \alpha_0 \xi + \alpha_0 \eta
\]
where,
\[
\begin{align*}
\alpha_0 &= \frac{1}{8}[(x_4 - x_2)(y_1 - y_3) - (y_4 - y_2)(x_1 - x_3)] \\
\alpha_1 &= \frac{1}{8}[(x_4 - x_2)(y_2 - y_1) + (x_1 - x_3)(y_4 - y_3)] \\
\alpha_2 &= \frac{1}{8}[(x_4 - x_1)(y_2 - y_3) + (x_3 - x_2)(y_4 - y_1)]
\end{align*}
\]

(4b)

In order to obtain the finite element matrix using quadrilateral elements due to second order linear Partial Differential Equation via Galerkin weighted residual formulation the integrals of the symmetric 4x4 matrix (Zienkiewicz 1977, Bickford 1990) is

\[
\int \int_\Omega \left[ \begin{array}{cccc}
  k_{1,1} & k_{1,2} & k_{1,3} & k_{1,4} \\
  k_{2,1} & k_{2,2} & k_{2,3} & k_{2,4} \\
  k_{3,1} & k_{3,2} & k_{3,3} & k_{3,4} \\
  k_{4,1} & k_{4,2} & k_{4,3} & k_{4,4}
\end{array} \right] df d\Omega = \int_\Omega k_{ij} df d\Omega
\]

(5)

where each \( k_{ij} \), after a minor simplification, is of the form

\[
\begin{align*}
  k_{ij} &= \frac{1}{64} \int_0^1 \int_0^1 \left[ B_{00}^{ij} + B_{10}^{ij} \xi + B_{01}^{ij} \eta + B_{00}^{ij} \xi^2 + B_{11}^{ij} \xi \eta + B_{02}^{ij} \eta^2 \right] d\xi d\eta \\
  i, j &= 1 - 4
\end{align*}
\]

(6)

Here each coefficient, \( B_{ij}^{m,n} \) \((0 \leq m, n \leq 2)\), of each \( k_{i,j} \) \((1 \leq i, j \leq 4)\) depends on the four vertices of the physical quadrilateral, can be written explicitly. For example, the coefficients of \( k_{1,1} \) are:

\[
\begin{align*}
  B_{11}^{00} &= (y_2 - y_4)^2 + (x_4 - x_2)^2 \\
  B_{11}^{10} &= 2\{ (y_2 - y_4)(y_4 - y_3) + (x_4 - x_2)(x_3 - x_4) \} \\
  B_{11}^{01} &= 2\{ (y_2 - y_4)(y_3 - y_2) + (x_4 - x_2)(x_2 - x_3) \} \\
  B_{11}^{11} &= 2\{ (y_2 - y_4)(y_3 - y_2) + (x_4 - x_2)(x_2 - x_3) \}
\end{align*}
\]

Numerical integration

The most common numerical integration is given by (Stroud 1974, Burden and Faires 2002)

\[
\int_a^b w(x) f(x) dx = \sum_{k=1}^n w_k f(x_k) + E[f]
\]

(7)

known as the Gaussian quadrature, where \( x_k \), \( w_k \) \((k = 1, 2, \ldots, n)\) and \( E[f] \) are called nodes (abscissas), weights, and error approximation, respectively. Since \( w(x) \), called weight function, and \( f(x) \) are integrable functions over the interval \([a, b]\), and \( x_k \) lies in \([a, b]\), the interval of integration. This gives us \( 2n \) parameters to choose. If the coefficients of a polynomial are considered parameters, the class of polynomials of degree at most \( 2n - 1 \) also contains parameters. This, then, is the largest class of polynomials for which it is reasonable to expect the formula to be exact (i.e. \( E[f] = 0 \)). With the proper choice of values and constants, exactness on this set can be obtained.

Assuming the exactness (i.e. \( E[f] = 0 \)) and for our convenient (by change of variable), and set \( w(x) = 1 \), the eqn. (7) the can be written as,

\[
\int_{-1}^1 f(x) dx = \sum_{k=1}^m w_k f(x_k) + \sum_{k=m+1}^{n+m} w_k f(x_k) \quad m \leq n.
\]

(8)
which is known as generalized Gauss quadrature rules. Particular quadratures are as follows:

1. If we put \( m=0 \), then the concluded numerical integration rule is called Gauss-Legendre (Burden and Faires 2002). Set \( f(x)=x^i \), \( i=0,1,2,\ldots,2n-1 \) in (8), which gives us \( 2n \) parameters \( (n \) weights and \( n \) nodes), and solving the nonlinear system to obtain the required nodes \( x_k \), and the corresponding weights \( w_k \) for each \( k=1,2,\ldots,n \). Since the nodes are symmetric.

2. If we put \( m=1, x_1 = -1 \) (or 1) then the concluded numerical integration rule is called Gauss-Radau (Masjed-Jamei et al. 2005). Setting \( f(x)=x^i \), \( i=0,1,2,\ldots,2n-2 \) in (8) to obtain \( 2n-1 \) parameters \( (n \) weights and \( n-1 \) nodes). Then solving the system, we can obtain required nodes \( x_k, k=2,3,\ldots,n \) and the corresponding weights \( w_k, k=1,2,\ldots,n \). Observe that the nodes are unsymmetric.

3. Rearrange the eqn. (8) as

\[
\int f(x)dx = \sum_{k=1}^{n-1} w_k f(x_k) + w_n f(x_n)
\]

and putting \( x_n = -1 \) and \( x_a = 1 \) in (9), then the numerical integration rule is called Gauss-Lobatto (Eslahchi et al. 2005). If we set \( f(x)=x^i, i=0,1,2,\ldots,2n-3 \) in (9), we get \( 2n-2 \) parameters \( (n \) weights and \( 2n-2 \) nodes). Then solving the system, we can obtain required nodes \( x_k, k=2,3,\ldots,n-1 \), and the corresponding weights \( w_k, k=1,2,\ldots,n \). In this case the nodes are symmetric.

We may summarize the nodes and corresponding weights for \( n=3,4,5 \) in Table - I, for this paper.

| \( n \) | Gauss-Legendre (G) | Gauss-Radau (GR) | Gauss-Lobatto (GL) |
|-------|------------------|------------------|------------------|
|       | Nodes \( x_k \)  | Weights \( w_k \) | Nodes \( x_k \)  | Weights \( w_k \) | Nodes \( x_k \)  | Weights \( w_k \) |
| 3     | 0.000000         | 0.888889         | -1.000000        | 0.222222         | 0.333333         |
|       | \pm0.774597      | 0.555556         | -0.289898        | 0.752806         | 1.333333         |
| 4     | \pm0.339981      | 0.652145         | 0.125000         | 0.125000         | 0.166667         |
|       | \pm0.861136      | 0.347859         | 0.080000         | 0.080000         | 0.833333         |
| 5     | 0.000000         | 0.568889         | -1.000000        | 0.446208         | 0.100000         |
|       | \pm0.538469      | 0.478629         | 0.044631         | 0.044631         | 0.544444         |
|       | \pm0.906179      | 0.236927         | 0.287427         | 0.287427         | 0.711111         |
In general, the integrals defined in eqn. (6) cannot be evaluated easily. Then each term, $k_{i,j}$ of (5) gives us rational integral. In fact, these rational integrals are evaluated by Gauss quadratures. Since the denominator (the Jacobian defined in eqn. (4)) is a function of two variables $\xi$ and $\eta$, the numerator is also a function of two variables $\xi$ and $\eta$, so we assume that the eqn.(6) can be expressed as

$$I = \int_{-1}^{1} \int_{-1}^{1} f(\xi, \eta) \, d\xi \, d\eta \quad (10)$$

In particular, for integration over the standard square, we can use the two dimensional Gaussian quadratures, which takes the form:

$$I = \sum_{p=1}^{n} \sum_{q=1}^{n} f(\xi_p, \eta_q) \, w_p \, w_q \quad (11)$$

where $(\xi_p, \eta_q)$ are the Gauss-Legendre, Gauss-Radau, and Gauss-Lobatto integration points and $w_p, w_q$ are the corresponding weighting factors independent of $f$.

Now compute the complete element matrix for a general four noded quadrilateral, described in Fig.1, on the basis of the above information using Mathematica program.

**Test Example**

In this section, we wish to compute the element matrix using closed form integration formula presented in this paper to compare with the existing solutions. For this, we consider a simple one-element example to evaluate the element matrix for two-dimensional Laplace's equation. The finite element formulation (Zienkiewicz 1977, Bickford 1990) of the Laplace's equation is

$$k_{i,j} = \iint_{R} \left( \frac{\partial N_i}{\partial x} \frac{\partial N_j}{\partial x} + \frac{\partial N_i}{\partial y} \frac{\partial N_j}{\partial y} \right) \, dx \, dy$$

$$= P_{i,j}^{x,x} + P_{i,j}^{y,y} \quad i, j = 1, 2, 3, 4 \quad (12)$$

**Fig. 2. Element geometry for Laplacian matrices**

where $R$ is the typical four-node isoparametric element shown in Fig. 2 [Bickford 1990, pp. 313-314]. In order to compare the accuracy, the complete element matrix (symmetric) for the geometry shown in Fig. 2 is given in Table II, and the error compare to the analytical method (Rathod and Islam 2002) obtained by Mathematica is also given in Table III obtained by the presented numerical integration methods.
Table II. A: Element matrix for the geometry in Fig. 2 using 3x3 order

| Integration Methods | \(i\) | 1          | 2          | 3          | 4          |
|--------------------|------|------------|------------|------------|------------|
| Legendre (G) 0.48519217 |     | 0.02221173 | -0.29072138 | -0.21668250 |
| Radau (GR) 1 0.48505441 |     | 0.02241839 | -0.29110038 | -0.21637241 |
| Lobatto (GL) 0.48662137 |     | 0.02006795 | -0.28679124 | -0.21998070 |
| Analytical 0.48521668 |     | 0.02217497 | -0.29065411 | -0.21673754 |
| G 0.71668250 |     |            | -0.31391790 | -0.42497624 |
| GR 2 0.71637241 |     |            | -0.31334942 | -0.42544137 |
| GL 0.71989807 |     |            | -0.31981314 | -0.42015288 |
| Analytical 0.71673754 |     |            | -0.31401883 | -0.42489369 |
| G |     |            |            |            |            |
| GR 0.82447395 |     |            | -0.22002414 |            |
| GL 3 0.83632409 |     |            | -0.22971971 |            |
| Analytical 0.82570118 |     |            | -0.22102824 |            |
| G |     |            |            |            |            |
| GR 4 0.86183793 |     |            |            |            |
| GL 0.86977067 |     |            |            |            |
| Analytical 0.86265947 |     |            |            |            |

Table: IIB: Element matrix using 4x4 order

| Integration Methods | \(i\) | 1          | 2          | 3          | 4          |
|--------------------|------|------------|------------|------------|------------|
| G 0.48521592 |     | 0.02217615 | -0.29065628 | -0.216735816 |
| GR 1 0.48521198 |     | 0.02218201 | -0.29066701 | -0.21672974 |
| GL 0.48521513 |     | 0.02212446 | -0.29056209 | -0.216813894 |
| Analytical 0.48521668 |     | 0.02217497 | -0.29065411 | -0.216737540 |
| G |     |            | -0.31401559 | -0.42489634 |
| GR 2 0.71673577 |     |            | -0.31399950 | -0.42490949 |
| GL 0.716815730 |     |            | -0.31415962 | -0.42478057 |
| Analytical 0.71673754 |     |            | -0.31401883 | -0.42489369 |
| G |     |            |            |            |            |
| GR 3 0.82566576 |     |            | -0.22099920 |            |
| GL 0.82596022 |     |            | -0.22123851 |            |
| Analytical 0.82570118 |     |            | -0.22102824 |            |
| G |     |            |            |            |            |
| GR 4 0.86265558 |     |            |            |            |
| GL 0.86263572 |     |            |            |            |
| Analytical 0.86283298 |     |            |            |            |
| Analytical 0.86265947 |     |            |            |            |
Table. IIC: Element matrix using 5×5 order

| Integration methods | i | j  | 1          | 2          | 3          | 4          |
|---------------------|---|----|------------|------------|------------|------------|
| G                   |   |    | 0.48521671 | 0.02217505 | -0.29065450| -0.21673770|
| GR                  | 1 |    | 0.48521651 | 0.02217518 | -0.29065448| -0.21673721|
| GL                  |   |    | 0.48521675 | 0.02217337 | -0.29065069| -0.21673944|
| Analytical          |   |    | 0.48521668 | 0.02217497 | -0.29065411| -0.21673754|
| G                   |   |    | 0.71673818 | -0.31401899| -0.42489423|            |
| GR                  | 2 |    | 0.71673715 | -0.31401818| -0.42489414|            |
| GL                  |   |    | 0.71673844 | -0.31402247| -0.42488934|            |
| Analytical          |   |    | 0.71673754 | -0.31401883| -0.42489369|            |
| G                   |   |    | 0.82570170 | -0.2210282 |            |
| GR                  | 3 |    | 0.82569977 | -0.22102731|            |
| GL                  |   |    | 0.82570736 | -0.22103421|            |
| Analytical          |   |    | 0.82570118 | -0.22102824|            |
| G                   |   |    | 0.86265934 |            |
| GR                  | 4 |    | 0.86265866 |            |
| GL                  |   |    | 0.86266299 |            |
| Analytical          |   |    | 0.86265947 |            |

Table III. Error estimation for the results in Table II

| Order n x n | Integration methods | Errors                  |
|-------------|---------------------|-------------------------|
|             | Legendre            | (0.00002445, 0.00003669, 0.00006728, 0.0000550) |
|             | Radau               | (0.00016228, 0.00024342, 0.00044627, 0.0003651) |
| 3 x 3       | Lobatto             | (0.00140467, 0.00210702, 0.0038629, 0.00316053) |
In this paper, we use the notations $G$, $GR$, and $GL$ for Gauss-Legendre, Gauss-Radau, and Gauss-Lobatto numerical integration methods, respectively.

**The error is calculated as follows**

$$Error = |(Analytical - Approximate)|$$

The computational CPU time for each matrix obtained in Table II, is also given in Table IV. We observe that the CPU time of the exact method is 300 times comparing to the numerical methods: $G$, $GR$ and $GL$, even if we use higher order quadrature points. The errors given in Table III are very negligible and the accuracy of the presented methods in this paper is excellent.
The integrals arising in finite element analysis usually involve a huge amount of computing time and memory space. In this paper, a simple and efficient method is focused on the reduction of computing time and space in the stiffness matrix for a general four node quadrilateral element through pre- and post-integration process, and by symbolic computation. For this, three types of numerical Gaussian quadrature rules are used. Here, the numerical integration methods are used for the comparison purpose but not for the integration itself. The procedures are rather simple and it may be carried out to optimize the explicit integration formulas also for the other finite elements. The comparison of the computing time also confirmed one of the main advantages of the symbolic integration approach. Thus the authors' concluding remark is that not only Gauss-Legendre quadrature rule is efficient but also Gauss-Radau as well as Gauss-Lobatto quadrature rules may be used for the evaluation of element matrices for a general four-node linear convex quadrilateral element.

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**Table IV. Comparison of CPU time for element matrix in Table II**

| Order $n \times n$ | Methods and CPU time (in s) | G | GR | GL | Exact |
|-------------------|----------------------------|---|----|----|-------|
| $3 \times 3$      |                            | 0.016 | 0.015 | 0.016 |       |
| $4 \times 4$      |                            | 0.031 | 0.031 | 0.031 | 9.437 |
| $5 \times 5$      |                            | 0.031 | 0.031 | 0.031 |       |

**Conclusion**

The integrals arising in finite element analysis usually involve a huge amount of computing time and memory space. In this paper, a simple and efficient method is focused on the reduction of computing time and space in the stiffness matrix for a general four node quadrilateral element through pre- and post-integration process, and by symbolic computation. For this, three types of numerical Gaussian quadrature rules are used. Here, the numerical integration methods are used for the comparison purpose but not for the integration itself. The procedures are rather simple and it may be carried out to optimize the explicit integration formulas also for the other finite elements. The comparison of the computing time also confirmed one of the main advantages of the symbolic integration approach. Thus the authors' concluding remark is that not only Gauss-Legendre quadrature rule is efficient but also Gauss-Radau as well as Gauss-Lobatto quadrature rules may be used for the evaluation of element matrices for a general four-node linear convex quadrilateral element.
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