The paper deals with a modeling and simulation of the direct AC-AC propulsion system and compares two matrix converter concepts with five-phase traction induction motors (IM) for the hybrid electric vehicle (HEV). The simulation results of \([3\times 5]\) matrix converter and 4Q-converter are done using Matlab-Simulink environment. Part I deals with a theoretical study of converter concepts for hybrid electric vehicle, since the configurations of \([3\times 5]+[0\times 5]\) matrix converters with five-phase motor(s) have not been analyzed so far. Based on simulation results the comparison and evaluation of the property and quality of the quantities of different type of the matrix powertrain are discussed in Part II.

**Keywords:** AC/AC powertrain, 3x5 matrix converter, 0x5 matrix converter, five-phase induction motor, electric drive, 4QC converter, modeling and simulation, HEV vehicle

The article is a continuation of Part I [1].

1 Introduction

The paper [2] compares a \([3\times 3]\) matrix converter (MxC) and 3-phase VSI converter with an active front end for a 7.5 kW induction motor drive. It has been shown that the matrix converter’s semiconductor losses are smaller at full load operation for the same silicon area in both converters. A one-third reduction of the device current rating of the MC is possible, resulting in comparable thermal device stress. The overall passive component count and rating are only slightly better for the MxC but the absence of bulky smoothing capacitor is evident what emphases also work [3].

A novel enhanced AC/AC series/parallel HEV powertrain has been introduced in Part I of [1], Figure 1. An indirect space-vector modulated three-phase AC-DC matrix converter for hybrid electric vehicles in [4], and with improved efficiency in [5]. The configurations of \([3\times 5]+[0\times 5]\) matrix converters with five-phase motor(s) are not analyzed in available literature so far.

2 Comparing simulation results of both concepts of MxC propulsion powertrain

Modeling approach of PMSG generator was taken from [6] and [7]. Modeling of matrix converter with indirect control and supposing multi-phase commutation was adapted for five-phase from [8-11] without special IM control. Model of five-phase IM can be found and taken from [12]. The connection of the control scheme of AC/AC powertrain with internal-combustion engine and synchronous generator together with a five phase induction machine and matrix converter are depicted in Figure 2.

The simulation results of the proposed powertrain are shown in Figures 2-4. Autonomous drive mode of HEV powered by ICE/SG is shown in Figure 3a-e. It can be seen as waveforms of input/output quantities of \([3\times 5]\) MxC as phase motor current/voltage and generator current/voltage, respectively. The entire control scheme in Matlab/Simulink environment is shown in Figure 2 - where matrix converter is presented by block 3x5 MxC.

There are simulation results of the start-up of AC/AC powertrain in Figure 3a and 3c. After start-up of ICE/SG during 0-2 sec with one no-load IM, the IM is loaded by torque equal 20 Nm. Steady-state results of voltages and currents of SG and IM are given in Figure 3b and Figure 3d-e. They show a good quality of the quantity waveforms, mainly of phase-current of IM. Any special control of IM has not been used.

Autonomous drive mode of HEV powered by AB accu-battery using 4QC and \([3\times 5]\) MxC is shown in Figure 4. Wave-forms of input/output quantities of 4QC and \([3\times 5]\) MxC can be seen there.

There are results of the start-up of AC/AC powertrain powered by accu-battery and 4QC converter in Figure 4a-c and Figure 4f-g. The total course of the start-up is similar to the previous one (in Figure 3c) but DC current is taken from accu-battery AB and input currents of \([3\times 5]\) MxC are different due to 4QC operation. During start-up, the IM is no-loaded. The steady-state voltage of 4QC, phase-voltage, and current IM are given in Figure 4e and Figure 4h. Phase-current of IM (Figure 4h) is similar to that of IM powered by AB without 4QC (Figure 5e - the next). Any special control of IM has not been used.
Figure 1 Novel enhanced AC/AC series/parallel HEV with one MxC converter and two traction motors M1, M2 with independent control.

Figure 2 The control scheme of AC/AC powertrain with ICE/SG unit, [3x5] matrix converter and 5-phase IM in Matlab/Simulink environment.

Figure 3a Start-up of SG - phase-currents.

Figure 3b The SG - phase-voltage/current in details.

Figure 3c Start-up of IM - phase-currents.

Figure 3d The IM phase-voltages of IM.
Figure 3e The IM phase-current and voltage in steady-state in detail

Figure 4a The current taken from accu-battery

Figure 4b The accu-battery voltage

Figure 4c Start-up 4QC currents of traction mode

Figure 4d The 4QC phase-currents in detail

Figure 4e The 4QC phase-voltages in detail

Figure 4f Start-up currents of IM
**Figure 4g** Start-up voltages of the IM motor

**Figure 4h** The phase voltage and current in detail

**Figure 5a** The current taken from AB accu-battery

**Figure 5b** The accu-battery voltage

**Figure 5c** The stator currents in details

**Figure 5d** The stator voltages of the IM motor

**Figure 5e** The phase voltage and current of the IM motor in details

**Figure 5f** Time course of motor torque
Autonomous drive mode of HEV powered by AB accu-battery using [0x5] MxC is shown in Figure 5a-g. The waveforms of input/output quantities of [3x5] MxC operated as [0x5] MxC converter can be seen there.

The start-up of IM supplied by accu-battery AB is shown in Figure 5a, Figure 5c and Figure 5e. After start-up of ICE/SG, in time of 1, 2 and 3 sec, the IM has been loaded with torque 5, 10 and -10 Nm, respectively. Steady-state of phase voltages and currents are presented in Figure 5d and Figure 5e. Comparison to previous result mode (Figure 4a-c) shows that start-up of IM is faster, and shape of phase-voltage of IM slightly different one but the phase-current is slightly better. Torque and angular speed circumstances are depicted in Figure 5f-g.

Comparison of autonomous modes in Figure 4 and Figure 5 shows that the concept of AC/AC powertrain with 4QC features:
- worse quality of quantities waveforms as accu-battery current and output phase current and voltage of the IM motor
- worse energetic efficiency because of adding of 4QC into the power chain.

A similar situation is regarding to charging of accu-battery by concept with 4QC, and starting-up of ICE/SG module using the 4QC unit or [0x3] and [5x3] MxCs, respectively. Comparison of autonomous modes in Figure 4 to previous Figure 2 and Figure 3 it should be noted that 4QC converter and input - 3-phase - LC filter in front of matrix converter are not necessary, therefore, the efficiency can be better.

3 Conclusion

Regarding comparison of [3x5] matrix converter system with auxiliary 4QC and auxiliary [0x5] MxC the second one is clearly better in the:
- batter autonomous traction and a braking regime where 4QC should be completed by [3x5] MxC since auxiliary [0x5] MxC should not be,
- also, charging mode from ICE/SG unit with 4QC needs either control by ICE engine or further DC/DC converter since auxiliary [0x5] MxC is not needed.

Total comparison and evaluation can be done until when all operation modes of both concepts (with 4QC and with [0x5] MxC) will be simulated and their result known. Both of those concepts make possible to also combine (parallel) modes of the HEV powertrain.

Proposed paper provides detailed study of the functionality of ac-ac matrix converter serving within the modified power train of the HEV vehicle concept. Due to high degree of complexity, the presented approach shows mostly the simulation analysis and comparison between front-end VSI propulsion system and ac-ac matrix converter system, and comparison of two variants MxC: with- and without 4QC battery converter.

Experimental verification will be realized within future research tasks based on the received results of expected behavior [13-14]. These results will be consequently published as a separate scientific paper.

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