Computational Investigations of Arrhenius Activation Energy and Entropy Generation in A Viscoelastic Nanofluid Flow Thin Film Sprayed on A Stretching Cylinder

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ABSTRACT

This paper investigates the two-dimensional and incompressible flow of viscoelastic nano-liquid dynamic and axisymmetric sprayed thin film deposit on a stretched cylinder. It also looked at how activation energy and entropy evaluation affected mass and heat flow. The governing equations are transformed into nonlinear ordinary differential equations using similarity transformation techniques, which are then resolved successively using a strong semi analytical homotopy analysis method (HAM). The velocity decreases as the magnetic field strength and viscoelastic parameters are increased. The temperature rises as the Brownian motion parameter increases, while it falls as the Prandtl number, film thickness parameter, and thermophoresis parameter increase. The greater the Reynolds number and the activation energy parameter, the higher the concentration of nanoparticles. The film size increases nonlinearly with the spray rate. Entropy generation increases as the Brinkmann number, magnetic field, and thermal radiation parameters increase. A nearby agreement is signed after comparing current investigation with published results. The results obtained, possibly under ideal conditions, could be useful for determining and architecting coating applications.

Keywords: Arrhenius activation energy; Binary chemical reaction; Entropy generation; Film spray; HAM; Viscoelastic nanofluid

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1. Introduction

Non-Newtonian fluid advancement is critical for new developments and productions in many industrial sectors. The application of magnetic hydrodynamics to electrically conductive fluids is directly related to the results that can be obtained by linking any external magnetic field current and fluid momentum. Some non-Newtonian main applications investigated and reported by Albano et al., [1] include metallurgy (form control, homogenization, sample levitation material), molten steel flow, planetary science and astrophysics, and fusion reactors. The viscoelastic fluid model is essential for the type of fluid due to its remarkable behavior. Han et al., [2] studied viscoelastic fluids in conjunction with the Cattaneo–Christov heat flux model. Mrokowska and Krzto-Maziopa [3] investigated the viscoelastic and shear-thinning effects of an aqueous exopolymer solution on the disk and sphere. Li et al., [4] investigated MHD viscoelastic flow and heat transfer through a vertical stretching sheet with Cattaneo-Christov heat flow effects. There are studies that provide more information on Newtonian and non-Newtonian fluids [5-11].

Liquid cooling is improved by nano-sized particles with diameters ranging from 1 to 100 nm. These nanoparticles are mixed with the base fluid, which improves cooling by having a higher coefficient of heat transfer than normal liquids, this mixture is known as a nanofluid. Choi and Bestman [12] pioneered the concept of nanofluids at the Argonne National Laboratory in the United States. Nanotechnology is currently one of the most fascinating fields. It is frequently a special type of fluid with greater thermal conductivity than standard host fluids. Buongiorno [13] evaluated Brownian motion and thermophoretic features to determine the convective transport of nanoparticles. Chakraborty and Panigrahi [14] investigated and review the stability of nanofluid. Ellahi et al., [15] investigated the heated couple stress bi-phase fluid with spherical Hafnium particles metal. The flow bounded by two parallel plates in the paper is entirely caused by the influence of an axial pressure gradient. There are studies that provide more information about the recent studies on nanofluids [16-25].

Thin film flow is regarded as a significant area of research. Thin film fluids are used to make a variety of heat exchangers and chemical tools; however, these technologies necessitate a thorough understanding of the movement process. Among the numerous applications for thin film fluids were wire and fiber coating, polymer preparation, and other applications for thin film fluids. This motion is associated with the production of various types of sheets, whether metal or plastic. In recent years, some researchers have considered working on this type of flow. Ellahi et al., [26] studied the thin film coating on the multi-fluid flow of a rotating disk suspended with nano-size silver and gold particles. Further researches can be found in others studies [27-29].

The species does not normally respond to chemical reactions with Arrhenius activation energy, which is one of the most significant indicators. Arrhenius [30] was the first to investigate the term activation energy. The minimum energy required for the process of molecules or atoms in chemical reactions, on the other hand, is referred to as activation energy. Bestman [31] may have described a principal model that consists of a boundary layer of fluid flow problems caused by binary chemical reactions with Arrhenius activation energy for perhaps the first time. The flow of a binary chemical reacting fluid with Arrhenius activating energy and convective boundary conditions is the focus. One of several goals of this study is to see how activation energy affects fluid flow and binary chemical reactions. More such research is available in the other studies [32-36].

It has been observed that when a cylinder is stretched, adequate attention is given to the stretching of the cylinder's flow. Wang [37] was the first to investigate the steady-state incompressible viscous fluid across the expanding cylinder. Bachok and Ishak [38] examined and
found on the stretching cylinder’s numerical flow and thermal transfer solution. Further research is available in the other studies [39-44].

This research paper is supplemented by a number of intriguing studies on stretching cylinders in the literature. To the best of knowledge, no investigation into the core problems has taken place. This paper investigates the steady two-dimensional, incompressible radiative flow of the viscoelastic nanofluid and axisymmetric sprayed thin film deposition past the stretching cylinder while accounting for the effect of activation energy and entropy measured. The fluid flow problem is governed by partial differential equations, which are transformed into ordinary differential equations through the use of appropriate similarity transformations. Liao introduced HAM for the first time in 1992 [45-47]. The solution of this method is fast convergent. Due to its rapid convergence, various researchers such as Usman et al., [48] and Shah et al., [49] have used HAM to solve their fluid flow problems. The results obtained for the effects of all related parameters on all profiles are graphically presented.

2. Problem Formulation

At \( r = 0 \), the steady, two-dimensional, and incompressible flow of viscoelastic and axisymmetric sprayed thin film nanofluid is considered. \( r > 0 \), consider to be the domain of the flow and \( z - \alpha \text{axis} \) is consider to be the axis of cylinder and \( r - \alpha \text{axis} \) is consider to be the radial direction. The effects of the magnetic field are used in the radial direction. Suggesting that the effects of induced magnetic fields are negligible. A radial axisymmetric spray with velocity \( V \) condenses as a film and is drawn along the cylinder’s outer surface, see Figure 1. Let \( T \) and \( C \) represent the fluid temperature and nanoparticles concentration respectively. At the outer radius \( b \) of the film thickness with \( \beta \) as the nondimensional film thickness parameter, \( T_b \) temperature at the outer radius of the film surface, \( T_w \) temperature at the wall, \( C_w \) Nanoparticle concentration at the wall, \( C_b \) Nanoparticle concentration beyond the surface ,\( T_{ref} \) is the reference temperature, \( C_{ref} \) reference concentration, \( c, d \) are constants.

![Fig. 1. Geometry of the Problem](image)
The fluid flow governing equations that have been modelled are [11,27,37-39]

\[
\frac{\partial u}{\partial r} + \frac{u}{r} + \frac{\partial w}{\partial z} = 0, \tag{1}
\]

\[
\frac{\partial w}{\partial r} + w \frac{\partial w}{\partial z} = v \left( \frac{\partial^2 w}{\partial r^2} + \frac{1}{r} \frac{\partial w}{\partial r} \right) - \frac{\sigma B^2 w}{\rho_f} + \frac{k_0}{\rho_f} \left[ \frac{\partial^2 w}{\partial r^2} + \frac{w}{\partial z} \frac{\partial w}{\partial r} \frac{\partial^2 w}{\partial z^2} + \frac{\partial w}{\partial r} \frac{\partial^2 w}{\partial z^2} \right] + \frac{1}{\rho_f} \left[ (1-C_b) \beta(T-T_b) - (\rho_p-\rho_f)(C-C_b) \right] g \tag{2}
\]

\[
\frac{u}{r} \frac{\partial T}{\partial r} + w \frac{\partial T}{\partial z} = \alpha_t \left[ \frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} \right] + \tau \left[ D_B \frac{\partial C}{\partial r} \frac{\partial T}{\partial r} + \frac{D_T}{T_b} \left( \frac{\partial T}{\partial r} \right)^2 \right] - \frac{1}{(\rho c_p)_f} \frac{\partial (rq_r)}{\partial r} \tag{3}
\]

\[
\frac{u}{r} \frac{\partial C}{\partial r} + w \frac{\partial C}{\partial z} = D_B \frac{1}{r} \frac{\partial C}{\partial r} \left( \frac{\partial C}{\partial r} \right) + \frac{D_T}{T_b} \frac{1}{r} \frac{\partial C}{\partial r} \left( \frac{\partial T}{\partial r} \right) - k_f^2 (C-C_b) \left( \frac{T}{T_b} \right)^n \exp \left[ -\frac{E_a}{k T} \right] \tag{4}
\]

with boundary conditions

\[
w(z, r) = W_w(z), \quad u(z, r) = U_w(z), \quad T(z, r) = T_w(z), C(z, r) = C_w(z) \text{ at } r = a, \tag{5}
\]

\[
\frac{\partial w}{\partial r} = 0, \quad \frac{\partial \delta}{\partial r} = 0, \quad \frac{\partial C}{\partial r} = 0, \quad \frac{\partial T}{\partial r} = 0, \quad u = \frac{\partial \delta}{\partial z} \text{ at } r = b \tag{6}
\]

where $\delta$ is the film size, $B_0$ is the magnetic field strength, $\sigma$ is the electrical conductivity, $k_0$ is the relaxation time coefficients, $g$ is the gravity acceleration, $\rho_p$ stands for the liquid density, $\nu_f$ is the kinematic viscosity, $\mu$ dynamic viscosity, $u$ and $w$ are velocity components, the nanoparticles volume is $C$, the fluid temperature is $T$, $\rho_f$ is the density of base fluid, $\alpha_t$ is the thermal diffusivity, $D_B$ is the Brownian motion, $D_T$ is the thermophoretic diffusion coefficient, and the heat capacity ratio is $\tau$.

According to the Rosseland approximation the thermally developed flow can be expressed as a modification with $\sigma^{**}$ is represented as Stefan-Boltzmann constant and $k^{**}$ as the mean absorption coefficient [8].

\[
q_r = -\frac{16 \sigma^{**} T_b^3 \frac{\partial T}{\partial r}}{3k^{**}}, \tag{7}
\]

Introducing the transformation for non-dimensionless functions $f, \theta, \phi$ and similarity variable $\zeta$ as [27]
\[ \zeta = \left( \frac{r}{a} \right)^2, \quad u = -ca \frac{f(\zeta)}{\sqrt{\zeta}}, \quad w = 2czf'(\zeta), \quad T(z) = T_b - T_{ref} \left[ \frac{cz^2}{v_{nf}} \right] \theta(\zeta), \quad C(z) = C_b - C_{ref} \left[ \frac{cz^2}{v_{nf}} \right] \phi(\zeta). \quad (8) \]

\[ \zeta = \left( \frac{b}{a} \right)^2 = \beta_1, \quad (9) \]

Eq. (1) is satisfied through Eq. (8) whereas Eq. (2)-(6) have the following form

\[
\frac{1}{\text{Re}} (2f'' + 2\zeta f'''') - Mf^{'} + \phi f'' - f''^2 + \lambda_1 \left( 4ff'f'' + \frac{1}{\zeta} f^2f'' - 2f^2f''' - 2Mf'''' \right) + \]

\[-Gr\theta + Gm\phi = 0 \]

\[(1 + Rd)(2\theta' + \zeta\theta'') - Nb\theta'\theta' - Nt\theta'^2 + Pr(f\theta' - 2f'\theta) = 0 \]

\[Sc(\phi' + \zeta\phi'') + f\phi' - 2f'\phi + \frac{Nt}{Nb} (\theta' + \zeta\theta'') - \gamma_1 (\gamma_2 - \theta_w^2) e^{\frac{E}{(\gamma_2 - \theta_w^2)}} = 0 \quad (12)\]

with boundary conditions given by

\[f = f' = \theta = \phi = 1 \text{ at } \zeta = 1 \]

\[f' = \theta' = \phi' = 0 \text{ at } \zeta = \beta_1 \quad (13)\]

where \(Gr\) is the thermal Grashof number, \(Gm\) is the solutal Grashof number, \(\text{Re}\) is Reynolds number, \(M\) is the parameter of the magnetic field, \(Pr\) is the Prandtl number, \(Nt\) is the parameter of thermophoresis, \(Nb\) is the parameter of Brownian motion, \(Sc\) is the Schmidt number, \(Rd\) is the radiation parameter, \(\lambda_1\) is the viscoelastic parameter, \(\gamma_1\) is chemical reaction rate constant, \(\gamma_2\) is the temperature ratio, \(\theta_w\) is dimensionless wall temperature, \(E\) is the activation energy parameter, are defined as:

\[
\text{Re} = \frac{ca^2}{\nu_f}, \quad M = \frac{\sigma B_i^2}{2c\rho_f}, \quad \lambda_i = \frac{k_i c}{\rho_i}, \quad Gr = \frac{g\beta'(1-C_b)(T_w-T_b)}{4c^3 a}, \quad Gm = \frac{g(\rho_p - \rho_f)(C_w-C_b)}{4c^3 \rho_f a}, \quad Rd = \frac{32\sigma'' T_w^3}{3(\rho c) k''}, \quad \lambda_i = \alpha_i, \quad (14)\]

\[Nb = \frac{\tau D_i (C_w - C_b)}{\alpha_i}, \quad Nt = \frac{\tau D_i (T_w - T_b)}{\alpha_i}, \quad Sc = \frac{2D_y}{ca^2}, \quad \gamma_1 = \frac{k^2}{2c}, \quad \gamma_2 = \frac{T_w - T_b}{T_b}, \quad \theta_w = \frac{E_{ca}}{kT_b}, \quad \mu = \frac{\mu c_p}{k}\]

The shear stress on the surface of the outer film is zero i.e., \(f''(\beta_1) = 0\). And the shear stress on the cylinder is

\[
\tau = \frac{\rho_f v f''(1)}{a} = \frac{4cz\mu_f f''(1)}{a} \quad (15)\]
The deposition velocity $V$ in terms of film thickness $\beta_1$, Mass flux $m_1$ (interesting quantity which in connection with the deposition per axial length) and normalized mass flux $m_2$ are given respectively

$$ca \frac{f(\beta_1)}{\sqrt{\beta_1}} = V, \quad m_1 = 2\pi b V \quad \text{and} \quad m_2 = \frac{m_1}{2\pi a^c c} = \frac{m_1}{4\pi v_j \text{Re}} = f(\beta_1)$$

(16)

3. Physical Quantities

The physical quantities of interest which estimate the skin friction coefficient ($C_f$), heat transfer coefficient ($Nu$) and mass transfer coefficient ($Sh$) which are very important through the industrial application point of view are also calculated in this study. The equation defining the skin friction is

$$C_f = \frac{2\tau_{zc}}{\rho_f(W_w)^2} \bigg|_{r=a} \quad \text{with} \quad \tau_{zc} = \mu_f \left( \frac{\partial W}{\partial r} - k_o w \right)_{r=a}$$

$$C_f = \frac{2}{\text{Re}_f^2} \left( f''(1) + \frac{f'(0)}{\lambda_1} \right)$$

(17)

The equation defining the heat transfer is

$$Nu = \left( \frac{aq_h}{k(T_w - T_b)} \right) \bigg|_{r=a} \quad \text{with} \quad q_h = \left( -k \frac{\partial T}{\partial r} + q_r \right)_{r=a},$$

$$Nu = -(2+R_d)\theta'(1)$$

(18)

The equation defining the mass transfer is

$$Sh = \frac{aq_m}{D_b(C_w - C_b)} \bigg|_{r=a} \quad \text{with} \quad q_m = -D_b \frac{\partial C}{\partial r} \bigg|_{r=a},$$

$$Sh = -2\phi'(1)$$

(19)

4. Analysis of Entropy Generation

For the bio-nanofluid system, the irreversibility formulation with $R$ denotes the ideal gas constant and $D$ represents the diffusivity is

$$E^{*}_{\text{gen}} = \frac{\alpha_1}{T_b^2} \left[ 1 + \frac{16\sigma_s^*}{K(T)b} \left( \frac{\partial T}{\partial r} \right)^2 + \frac{\mu}{T_2} \left( \frac{\partial W}{\partial z} \right)^2 + \frac{RD}{C_b} \left( \frac{\partial C}{\partial r} \right)^2 + \frac{RD}{T_b} \left( \frac{\partial T}{\partial r} \frac{\partial C}{\partial z} + \frac{\partial C}{\partial r} \frac{\partial T}{\partial z} \right) + \sigma B_0^2 w^2 \right]$$

(20)

In Eq. (20), the first term represents the irreversibility due to heat transfer, the second term is entropy generation due to viscous dissipation and third to six terms are irreversibility due to diffusion effect. The seventh term stands for the entropy generation due to magnetic field. The characteristic entropy generation rate is
\[
E_0^m = \frac{\alpha_i (T_a - T_b)}{T_b^2}
\]

(21)

Notice that irreversibility \( N_G(\zeta) \) in the scaled form is

\[
N_G(\zeta) = \frac{E_{\text{gen}}}{E_0^m}
\]

(22)

where \( E_0^m \) Dimensional characteristic entropy generation, \( E_{\text{gen}}^m \) Dimensional entropy generation.

Using Eq. (8), dimensional Eq. (20) converted into the following dimensionless form

\[
N_G(\zeta) = \frac{4}{a^2} \left( 1 + \frac{4}{3} R_d \right) \theta'^2 + B_r f'^2 + B \left[ \left( \frac{\phi}{\theta} \right)' \right]^2 + a^2 \frac{\phi}{\theta} \theta'^2 + \phi \theta'' + M \Pr f'^2
\]

(23)

where \( N_G \) represents the entropy generation rate, \( B_r = \frac{4 c^2 \mu}{\alpha_i (T_w - T_b)} \), and \( B_1 = \frac{4 RDC_b}{\alpha_i} \), are respectively the Brinkman number, diffusivity constant parameter due to nanoparticle concentration and magnetic field parameter. \( \theta_w = \frac{(T_a - T_b)}{T_b} \), \( \phi_w = \frac{(C_a - C_b)}{C_b} \), are respectively the dimensionless heat and nanoparticle concentration variables.

5. Solution Procedures by HAM

Choosing the initial guesses and the corresponding linear operators as

\[
f_0(\zeta) = (1 - e^{-\zeta}), \quad \theta_0 = e^{-\zeta}, \quad \phi_0 = e^{-\zeta}
\]

(24)

\[
L_f = f''' - f', \quad L_0 = \theta''' - \theta, \quad L_{\phi} = \phi''' - \phi
\]

(25)

satisfying the properties as given below

\[
L_f \left[ C_1 + C_2 e^{\zeta} + C_3 e^{-\zeta} \right] = 0,
\]

\[
L_0 \left[ C_1 e^{\zeta} + C_2 e^{-\zeta} \right] = 0,
\]

\[
L_{\phi} \left[ C_1 e^{\zeta} + C_2 e^{-\zeta} \right] = 0
\]

(26)

With arbitrary constants \( \{C_i\}_{i=1} \).

To compute the zeroth order form of the problems. Take as follows
with $p$ as the embedding parameter and $h_f, h_\theta, h_\phi$ the non-zero auxiliary parameters. Taking $N_f, N_\theta, N_\phi$ to represent the nonlinear operators and can be obtained through Eq. (10)-(13) as follows

\begin{align}
N_f &= \frac{2}{Re} \left( \frac{\partial^2 f(\zeta, p)}{\partial \zeta^2} + \zeta \frac{\partial^3 f(\zeta, p)}{\partial \zeta^3} \right) - M \frac{\partial f(\zeta, p)}{\partial \zeta} \\
&\quad + f(\zeta, p) \left( \frac{\partial^2 f(\zeta, p)}{\partial \zeta^2} - \left( \frac{\partial f(\zeta, p)}{\partial \zeta} \right)^2 \right) + \lambda_{1} \left( 4 f(\zeta, p) \frac{\partial f(\zeta, p)}{\partial \zeta} \frac{\partial^3 f(\zeta, p)}{\partial \zeta^3} + \frac{1}{\zeta} f^2(\zeta, p) \frac{\partial^2 f(\zeta, p)}{\partial \zeta^2} \right) \\
&\quad - f^2(\zeta, p) \frac{\partial^3 f(\zeta, p)}{\partial \zeta^3} - M f(\zeta, p) \frac{\partial^2 f(\zeta, p)}{\partial \zeta^2} \right) \\
N_\theta &= \left( 2 + Rd \right) \left( \frac{\partial \theta(\zeta, p)}{\partial \zeta} + \zeta \frac{\partial^2 \theta(\zeta, p)}{\partial \zeta^2} \right) \\
&\quad - Nb \frac{\partial \phi(\zeta, p)}{\partial \zeta} \frac{\partial \theta(\zeta, p)}{\partial \zeta} - Nt \left( \frac{\partial \theta(\zeta, p)}{\partial \zeta} \right)^2 + Pr \left( f(\zeta, p) \frac{\partial \theta(\zeta, p)}{\partial \zeta} - 2 \theta(\zeta, p) \frac{\partial f(\zeta, p)}{\partial \zeta} \right) \\
N_\phi &= Sc \left( \frac{\partial \phi(\zeta, p)}{\partial \zeta} + \zeta \frac{\partial^2 \phi(\zeta, p)}{\partial \zeta^2} \right) + f(\zeta, p) \frac{\partial \phi(\zeta, p)}{\partial \zeta} \\
&\quad - 2 \phi(\zeta, p) \frac{\partial f(\zeta, p)}{\partial \zeta} + Sc \left( \frac{\partial \theta(\zeta, p)}{\partial \zeta} + \zeta \frac{\partial^2 \theta(\zeta, p)}{\partial \zeta^2} \right) - \gamma_{1} \left( \gamma_{2} - \theta(\zeta, p) \right)^{\gamma} \exp \left[ \frac{-E}{\gamma_{2} - \theta(\zeta, p)} \right] \\
\end{align}

Taking $p = 0$ and $p = 1$, the following results are obtained

\begin{align}
&f(\zeta, 0) = f_{\theta}(\zeta), \theta(\zeta, 0) = \theta_{\theta}(\zeta), \phi(\zeta, 0) = \phi_{\theta}(\zeta) \\
&f(\zeta, 1) = f(\zeta), \theta(\zeta, 1) = \theta(\zeta), \phi(\zeta, 1) = \phi(\zeta) \\
\end{align}

Obviously, when $p$ is increased from 0 to 1, then $f(\zeta, p), \theta(\zeta, p), \phi(\zeta, p)$ vary from $f_{\theta}(\zeta), \theta_{\theta}(\zeta), \phi_{\theta}(\zeta)$ to $f(\zeta), \theta(\zeta), \phi(\zeta)$. Through Taylor’s series expansion, the following can be obtained
\[ f(\zeta, p) = f_o(\zeta) + \sum_{m=1}^{\infty} f_m(\zeta) p^m, f_m(\zeta) = \frac{1}{m!} \frac{\partial^m f(\zeta, p)}{\partial \zeta^m} \bigg|_{p=0} \]

\[ \theta(\zeta, p) = \theta_o(\zeta) + \sum_{m=1}^{\infty} \theta_m(\zeta) p^m, \theta_m(\zeta) = \frac{1}{m!} \frac{\partial^m \theta(\zeta, p)}{\partial \zeta^m} \bigg|_{p=0} \]  

(33)

\[ \phi(\zeta, p) = \phi_o(\zeta) + \sum_{m=1}^{\infty} \phi_m(\zeta) p^m, \phi_m(\zeta) = \frac{1}{m!} \frac{\partial^m \phi(\zeta, p)}{\partial \zeta^m} \bigg|_{p=0} \]

The convergence of the series in Eq. (33) depends strongly upon \( h_f, h_o, h_\theta \). By considering that \( h_f, h_o, h_\theta \) are selected properly so that the series in Eq. (33) converge at \( p = 1 \), then the following simplifications are achieved

\[ f(\zeta) = f_o(\zeta) + \sum_{m=1}^{\infty} f_m(\zeta) \]

\[ \theta(\zeta) = \theta_o(\zeta) + \sum_{m=1}^{\infty} \theta_m(\zeta) \]  

(34)

\[ \phi(\zeta) = \phi_o(\zeta) + \sum_{m=1}^{\infty} \phi_m(\zeta) \]

The order \( m \) deformation of the problem can be constructed as follow

\[ L_f [f_m(\zeta) - \eta_m f_{m-1}(\zeta)] = h_f R_f^m(\zeta) \]

\[ L_\theta [\theta_m(\zeta) - \eta_m \theta_{m-1}(\zeta)] = h_o R_\theta^m(\zeta) \]  

(35)

\[ L_\phi [\phi_m(\zeta) - \eta_m \phi_{m-1}(\zeta)] = h_\phi R_\phi^m(\zeta) \]

\[ f_m(1) = f'(1) = 0, \theta_m(1) = \theta_\beta(1) = 0, \phi_m(1) = \phi_\beta(1) = 0 \]  

(36)

where \( R_f^m(\zeta), R_\theta^m(\zeta), R_\phi^m(\zeta) \) and can be obtained as

\[ R_f^m(\zeta) = \frac{2}{Rd} \left( f''(\zeta) + \zeta f''_{m-1}(\zeta) \right) - Mf'_{m-1} + \sum_{k=0}^{m-1} f_{m-1-k} f'_k(\zeta) - \sum_{k=0}^{m-1} f_{m-1-k} f'_k(\zeta) \]

\[ + \tilde{A}_f \left( 4 \sum_{k=0}^{m-1} \sum_{r=0}^{k} f_{m-1-k} f'_{k-r}(\zeta) f'_r(\zeta) + \frac{1}{\zeta} \sum_{k=0}^{m-1} \sum_{r=0}^{k} f_{m-1-k} f'_{k-r}(\zeta) \right) \]

\[ - \frac{1}{Gr} \sum_{k=0}^{m-1} \sum_{r=0}^{k} f_{m-1-k} f'_{k-r}(\zeta) f''(\zeta) - 2M \sum_{k=0}^{m-1} f_{m-1-k} f'_k(\zeta) \]  

(37)

\[ R_\theta^m(\zeta) = (2 + Rd) \left( \theta'_{m-1}(\zeta) + \zeta \theta''_{m-1}(\zeta) \right) - Nb \sum_{k=0}^{m-1} \theta_k + Nt \sum_{k=0}^{m-1} \theta_k + Pr \left( \sum_{k=0}^{m-1} f_{m-1-k} \theta_k - \sum_{k=0}^{m-1} \phi_k \right) \]  

(38)
The general solutions are given by

\[
R_m^m(\zeta) = Sc\left(\phi_{m-1}^m(\zeta) + \zeta\phi_{m-1}^m(\zeta)\right) + \sum_{k=0}^{m-1} \phi_k^m(\zeta) f_k^m(\zeta) - 2 \sum_{k=0}^{m-1} \phi_k^m(\zeta) \phi_k^m(\zeta)
\]

\[
+ Sc_b \left( \theta_{m-1}^m(\zeta) + \zeta \theta_{m-1}^m(\zeta) \right) - \gamma_1 \left( \gamma_2 - \Theta_{m}^m(\zeta) \right) \right) e^{\sigma x} \left[ \frac{-E}{(\gamma_2 - \Theta_{m}^m(\zeta))} \right]
\]

\[
\eta_m = \begin{cases} 
0, & m \leq 1 \\
1, & m > 1 
\end{cases}
\]

The general solutions are given by

\[
f_m^m(\zeta) = f_m^m(\zeta) + C_1 e^{\sigma} + C_2 e^{-\sigma}
\]

\[
\theta_m^m(\zeta) = \theta_m^m(\zeta) + C_3 e^{\sigma} + C_4 e^{-\sigma}
\]

\[
\phi_m^m(\zeta) = \phi_m^m(\zeta) + C_6 e^{\sigma} + C_7 e^{-\sigma}
\]

with \(f_m^m(\zeta), \theta_m^m(\zeta), \phi_m^m(\zeta)\) are the special solutions.

6. Results and Discussion

The graphs are prepared using the following set of parameters \(\lambda_1 = Gr = Gm = 0.3,\)
\(\beta = \gamma_1 = \gamma_2 = Re = Rd = Sc = E = M = 0.4, Nb = Nt = 0.5,\) and \(\beta_2 = 2.\) To achieve acceptable results, Liao [44-46] introduced h curves for the convergence of the series solution. Therefore, the acceptable h-curves for \(f(\zeta), \theta(\zeta)\) and \(\phi(\zeta)\) are drawn in the ranges \(-4 \leq h \leq 4, \) \(-2 \leq h \leq 2,\) and \(-4 \leq h \leq 4\) in Figure 2, Figure 3 and Figure 4 respectively.

**Fig. 2.** h-curve of \(f'(\zeta)\)
The viscoelastic nano-liquid dynamic with coolant and shielding paint or film are sprayed on a stretching cylinder. Figure 5 depicts the normalized spray rate $m_2$, which is functionally correlated with film size. The film size naturally increases with the spray rate at simultaneously in a nonlinear fashion. The film’s outer surface as observed may be harmed if the spray is not uniform. Spraying also improves cooling because it creates a thinner boundary layer.
Figure 6 shows that the velocity is a decreasing function of the magnetic field parameter $M$. In general, when a magnetic field is applied to a conduction-capable fluid flow, the momentum boundary layer becomes thin. The possible explanation for this is that throughout this process, resistance forces known as Lorentz forces are generated, which have a negative impact on fluid flow. This force slows the velocity of the nanofluid as it passes through the vertical surface.

Figure 7 depicts that by increasing the viscoelastic parameter the velocity decreases and hence momentum boundary layer thickness weakens. Figure 8 illustrates that the velocity increases with the Grashof number as a consequence of the buoyancy force's dominant effects in the core part, which causes changes in velocity and high viscous effects across the walls.
As shown in Figure 9, the velocity increased as the Reynolds number increased. This is due to the fact that as the Reynolds number increases, the inertial force dominates the flow more than the viscous forces. High viscous forces are highly resistive to fluid flow, and strong inertial forces reduce the flow of the boundary layer. When \( \text{Re} \) is small, then it means there exists small inertial effect compared to that of viscous effect. Since \( \text{Re} = \frac{ca^2}{v_f} \) so for \( \text{Re} = 0 \), the stretching rate \( c \) tends to vanishing since the cylinder radius \( a \) cannot be zero in the present case. Also, the thickness is made infinite for finite deposition rate and the steady form cannot exist.
Figure 10 shows that increasing the magnetic field parameter values raises the temperature of the nanofluid. The magnetic field parameter generates a resistive force that works in the opposite direction of the flow field and increases the thickness of the thermal boundary layer.

Figure 11 shows that as the Prandtl number increases, the temperature of the nanofluid decreases, and thus the thermal boundary layer decreases, indicating that effective cooling of the nanofluid occurs quickly. Given the small size of the motion layer, the impact of a high Prandtl number is even more obvious.
Figure 12 shows that increasing the Brownian motion parameter causes an increase in fluid temperature, resulting in a decrease in friction on the free surface of nanoparticles, this demonstrates that the thickness of the thermal boundary layer increases, indicating that nanoparticles play an important role in improving convection.

Figure 13 shows that as the Thermophoresis parameter values increase, the temperature of the nanofluid decreases. Thermophoresis is the phenomenon of particle diffusion caused by a temperature gradient effect. The force that transfers nanoparticles to the surrounding fluid as a result of a temperature gradient is known as thermophoretic force. Increased thermophoretic force results in more nanoparticles being transferred to the fluid layer.
As shown in Figure 14, the radiation parameter is used to add heat to the temperature of the nanoparticles as the temperature of the nanofluid rises. Thermal radiation analysis is essential in the cooling of the cylinder and present study incorporate with the many published results. The temperature distribution is influenced by the thin film parameter. The thermal boundary surface’s temperature is high and small, as is the transverse distance. For larger quantities, the film thickness parameter slows down the temperature, as shown in Figure 15. The heat transfer is improved by thinning the nanofluid. In the current situation, however, it is depreciating. The possible explanation for this is that as the thickness of the fluid film increases, so does the mass of the fluid, which exhausts the temperature. Mostly as consequence, heat enters the fluid and the environment cools.
Figure 16 and Figure 17 depict the effect of the activation energy parameter and the binary chemical reaction parameter on the concentration profile, demonstrating that it is increased with larger activation energy parameter values and decelerated with larger chemical reaction parameter values, respectively. The Schmidt number is related to mass diffusion and thus increases mass diffusivity values, resulting in a decrease in nanoparticle concentration due to less mass diffusion transportation, as shown in Figure 18.
Increasing the magnetic field parameter causes a slight increase in entropy generation in general. Because the magnetic field parameter has little effect on entropy generation, a large change in the magnetic field parameter results in a small change in entropy, as illustrated in Figure 19.
Figure 20 shows that as the Brinkmann number increases, so does the generation of entropy. Physically, this is of real significance since $Br = \frac{Pr}{Ec}$ is an irreversibility coefficient of fluid friction. The Prandtl number is defined as the ratio of thermal to momentum diffusivity, whereas the Eckert number is defined as the conversion of kinetic energy into heat in the flow domain via viscous dissipation. The generation of entropy increases as viscous dissipation increases.

Figure 21 depicts how the rate of entropy generation in the flow increases as the thermal radiation parameter increases. This is because the emission through the thermal radiation parameter has increased.
6.1 Table Discussion

The current work is compared to the published work by Hayat et al., [39] for various Prandtl number $Pr$ values, and the results show good resemblance, as seen in Table 1.

| $Pr$  | Hayat et al., [39] | Present work |
|-------|--------------------|--------------|
| 1.0   | -1.0000            | -1.0000      |
| 0.0   | 0.0                | 0.0          |
| 0.5832| 0.5832             | 1.0000       |
| 1.0000| 1.0000             | 1.3332       |
| 1.3332| 1.3332             | 1.3334       |
| 10    | -10.0000           | -10.0000     |
| 0.0   | 0.0                | 0.0          |
| 2.3080| 2.3076             | 3.7210       |
| 3.7207| 3.7210             | 4.7971       |
| 4.7969| 4.7971             | 4.7971       |

Table 2 shows the convergence of series solutions for different order of approximation.

| Order of Approximation | $f''(1)$ | $\theta'(1)$ | $\phi'(1)$ |
|------------------------|----------|--------------|------------|
| 1                      | 0.7331   | 0.6513       | 0.6033     |
| 10                     | 0.6282   | 0.6239       | 0.6000     |
| 20                     | 0.5121   | 0.6070       | 0.5891     |
| 21                     | 0.5001   | 0.5969       | 0.5891     |
| 25                     | 0.4990   | 0.5969       | 0.5891     |
| 30                     | 0.4990   | 0.5969       | 0.5891     |
Table 3, Table 4 and Table 5 showed the numerical values of the physical quantities accessing the effect of different parameters.

### Table 3
Variation in skin friction coefficient $-f''(1)$ for $M, \lambda_1, Re, Gr$ and $Gm$

| $M$ | $\lambda_1$ | Re | Gr | Gm | $-f''(1)$ |
|-----|--------------|----|----|----|-----------|
| 0.4 | 0.3          | 0.4| 0.3| 0.3| 0.4231    |
| 0.6 |              |    |    |    | 0.3231    |
| 0.8 |              |    |    |    | 0.2231    |
| 1.0 |              |    | 0.4|    | 0.1231    |
|     |              |    | 0.5|    | 0.1231    |
|     |              |    | 0.6|    | 0.1231    |
|     |              | 0.7|    |    | 0.1231    |
|     |              | 1.0|    |    | 0.1231    |
|     |              | 1.3|    |    | 0.1231    |
|     | 0.7          |    |    |    | 0.1031    |
|     | 0.9          |    |    |    | 0.1201    |
|     | 1.0          |    |    |    | 0.1031    |
|     | 1.3          |    |    |    | 0.1031    |
|     | 1.5          |    |    |    | 0.1230    |
|     | 1.7          |    |    |    | 0.1031    |
|     | 1.9          |    |    |    | 0.1031    |
|     | 2.0          |    |    |    | 0.1031    |

### Table 4
Variation in Nusselt number $-\theta'(1)$ for $M, \lambda_1, Pr, Nb, Nt$ and $Rd$

| $M$ | $\lambda_1$ | Pr | Nb | Nt | Rd | $-\theta'(1)$ |
|-----|--------------|----|----|----|----|---------------|
| 0.4 | 0.3          | 0.7| 0.3| 0.3| 0.4| 0.2764        |
| 0.2 |              |    |    |    |    | 0.2763        |
| 0.6 |              |    |    |    |    | 0.2755        |
| 1.0 |              |    | 0.4|    |    | 0.2745        |
|     |              | 0.5|    |    |    | 0.2725        |
|     |              | 0.6|    |    |    | 0.2715        |
|     | 1.0          |    |    |    |    | 0.2754        |
|     | 1.3          |    |    |    |    | 0.2753        |
|     | 1.6          |    |    |    |    | 0.2760        |
|     | 1.0          |    |    |    |    | 0.2761        |
|     | 1.7          |    |    |    |    | 0.2762        |
|     | 2.4          |    |    |    |    | 0.2736        |
|     | 1.0          |    |    |    |    | 0.2735        |
|     | 1.7          |    |    |    |    | 0.2734        |
|     | 2.4          |    |    |    |    | 0.2733        |
|     | 1.0          |    |    |    |    | 0.2732        |
|     | 1.6          |    |    |    |    | 0.2731        |
|     | 2.0          |    |    |    |    | 0.2730        |
Table 5

Variation in Sherwood number $-\phi'(1)$ for $\lambda_1, Pr, Nb, Nt$ and $E$

| $\lambda_1$ | $Nb$ | $Nt$ | $\gamma_1$ | $E$ | $-\phi'(1)$ |
|------------|------|------|------------|-----|-------------|
| 0.3        | 0.3  | 0.3  | 0.4        | 0.4 | 0.15479     |
| 0.5        |      |      |            |     | 0.15478     |
| 0.7        |      |      |            |     | 0.15477     |
| 0.9        |      |      |            |     | 0.15476     |
| 1.0        |      |      |            |     | 0.15475     |
| 1.7        |      |      |            |     | 0.15474     |
| 2.4        |      |      |            |     | 0.15473     |
| 0.6        |      |      |            |     | 0.15472     |
| 0.9        |      |      |            |     | 0.15471     |
| 1.2        |      |      |            |     | 0.15470     |
| 0.9        |      |      |            |     | 0.15469     |
| 1.4        |      |      |            |     | 0.15468     |
| 1.9        |      |      |            |     | 0.15467     |
| 0.8        |      |      |            |     | 0.15468     |
| 1.3        |      |      |            |     | 0.15467     |
| 1.8        |      |      |            |     | 0.15466     |

7. Conclusions

The mass and heat transfer flow of the viscoelastic nanoliquid film sprayed on the stretching cylinder taking to account the effect of activation energy and entropy measure is evaluated. The solution of the problem obtained using HAM and presented the result using graphs. These results shows that an effective flow and cooling process of heat exchange of innovative scientific and engineering are observed. The most important findings are

i. The velocity decreases as the magnetic field and viscoelastic parameters are increased.

ii. The temperature increases with the increase in Brownian motion parameter and decreases with the Thermophoresis parameter and Prandtl number.

iii. The activation energy parameter causes the nanoparticle concentration to rise, while the thermal radiation and chemical reaction parameters, as well as the Schmidt number, cause it to decline.

iv. The generation of entropy increases with the increase of all parameters such as magnetic field and thermal radiation parameters and Brinkman number.

v. The spray rate increase in a nonlinear fashion with the thickness of the film.

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