Bayesian optimization for goal-oriented multi-objective inverse material design

Highlights
- Multi-objective (MO) problems with predefined goals for all objectives were studied.
- Fully probabilistic Bayesian optimization (BO) for goal achievement was proposed.
- The proposed method clearly outperformed a baseline in goal achievement efficiency.
- Goal-oriented BO simplifies MO problems and works with small number of experiments.
Bayesian optimization (BO) (Greenhill et al., 2020; Shahriari et al., 2015) is one of the major approaches to inverse material design and involves gradually optimizing material-design parameters through repeated experiments (Balachandran et al., 2016; Doan et al., 2020; Lookman et al., 2017, 2019). Although the process resembles human-based trial-and-error, design parameters in BO are determined based on a machine-learning model, which is updated after each experiment and gets smarter through repeated updates (Shahriari et al., 2015). Accordingly, BO can effectively accelerate difficult optimization problems and is useful, particularly for material-design problems involving time-consuming experiments. Currently, there are many computational material design studies that utilize BO (Bassman et al., 2018; Fukazawa et al., 2019; Hashimoto et al., 2020; Herbol et al., 2018; Okamoto, 2017; Sakurai et al., 2019; Seko et al., 2015), and several recent real-world experimental studies have actually realized inverse material design using BO (Balachandran et al., 2018; Homma et al., 2020; Langner et al., 2020; Rouet-Leduc et al., 2016; Wakabayashi et al., 2019; Xue et al., 2016; Yuan et al., 2018). However, the targets for most such real-world inverse design studies were single properties, despite most material-design problems requiring the optimization of multiple target properties. This type of optimization problem is known as multi-objective (MO) optimization. Nowadays, the most popular class of method for MO optimization is genetic algorithm-based (Deb et al., 2002; Jung et al., 2017; Lee et al., 2017; Menou et al., 2018; Niu et al., 2018; Shrivastava et al., 2018), while the real-world implementation of more efficient BO based MO inverse material design remains in its nascent stages.

The challenge with MO optimization relative to single-objective optimization comes from the number of possible solutions arising. In single-objective optimization a single optimal solution is usually obtained after running the optimization, while MO optimization elicits many optimal solutions, as in the following. Consider MO optimization, where two objective properties, A and B were minimized by tuning design parameters, X. Figure 1 shows a schematic mapping of properties A and B corresponding to the optimal design parameters obtained by this optimization task (blue circle). Optimal design parameters achieving minimum values for both properties A and B may be preferable. However, usually the best design parameters for properties A and B (X1 and X2 in Figure 1, respectively) are not the same. For that reason, in MO optimization, optimal solutions are defined as design parameters where it is impossible to improve any properties without negatively affecting others. Such design parameters are called Pareto optimal solutions. For example, the design parameter X3, which corresponds to the red circle in Figure 1, is not Pareto
optimal, because there are blue circles with lower values of both properties A and B (blue box in Figure 1). Conversely, parameter X1 and X2, which corresponds to blue circles, are Pareto optimal solutions, because reducing properties A and B is impossible without causing the other to increase. According to this definition, design parameters corresponding to all blue circles, which balance dual objectives in differing ways, also constitute Pareto optimal solutions. Because no general criteria exist to compare the quality of the Pareto optimal solutions, various balances of Pareto optimal solutions should be sought, but many experiments have to be performed to find them.

Most popular MO inverse design approaches comprise finding the whole Pareto optimal solution, from which the best-balanced solution is then chosen (Figure 2A). In this paper, this inverse design approach is called “many-solution-inverse-design”. Some recent computational material design studies used MO BO in many-solution-inverse-design to accelerate the finding of the Pareto optimal solutions (Janet et al., 2020; Karasuyama et al., 2020; Solomou et al., 2018; Talapatra et al., 2018; Wang et al., 2020b). However, as schematically shown in Figure 2A, finding many Pareto optimal solutions requires an excessive number of experiments, which is difficult to execute with time-consuming real-world experiments. Accordingly, this makes applying many-solution-inverse-design to real-world material design infeasible.

There are alternative MO inverse design approaches, whereby only a few Pareto optimal solutions are searched without the time-consuming need to search the entire space of Pareto optimal solutions (Figure 2B). In this paper, this inverse design approach is called “few-solution-inverse-design”. Most few-solution-inverse-design solutions use scalarization functions (SFs), which convert multiple objective properties to a single score, which, in turn, can be optimized using any single-objective optimization methods (Cummins and Bell, 2016; Wang et al., 2020a; Wheatle et al., 2020; Yamawaki et al., 2018). Among them, weight summation of multiple objective properties is most popular one. In the weight-summation SF, predefined weights for weight summation determine the balance of objective properties in the Pareto optimal solution. Using this weight-summation SF, several studies have successfully performed inverse material designs using machine-learning-based optimization (Cummins and Bell, 2016; Wang et al., 2020a; Wheatle et al., 2020). However, because, the predefined weight is not directly reflected in the optimized solution, it is difficult to balance objective properties using weight-summation SF exactly as required. Conversely, there are studies using ad hoc SFs where the preference of the experimenter in terms of the balance of Pareto optimal solutions can be directly reflected (Hase et al., 2018; Walker et al., 2017). This class of methods for few-solution-inverse-design is promising, but comparing the performance of optimization methods for few-solution-inverse-design remains difficult because different optimization methods elicit different Pareto optimal solutions, and there is no quantitative measure available to fairly compare the quality of these different Pareto solutions. Therefore, an SF-method suitable for each application is unclear.

Figure 1. Schematic mapping of Pareto optimal solutions
Blue circles represent Pareto optimal solutions. The red circle represents a non-Pareto optimal design. Blue circles in the blue box have better values in both properties A and B than that with the design parameter X3.
Furthermore, it is often difficult to find even one Pareto optimal solution with time-consuming real-world experiments. Although finding Pareto optimal solutions represents a common goal of MO optimization studies (Gopakumar et al., 2018; Harada et al., 2020; Mannodi-Kanakkithodi et al., 2016; Del Rosario et al., 2020), for real-world material designs with limited budget and available time, it is often difficult to find a true Pareto optimal solution and efforts to optimize the material property will be stopped after finding materials having properties acceptable for each application but not Pareto optimal solutions. However, although optimization methods studied in both many- and few-solution-inverse-design would also work with such a realistic design problem, the performance of BO in such realistic design problem has not been studied well and efficiency of MO BO in real-world material design requiring time-consuming experiments remains unclear.

In this study, we show that by focusing on finding a design parameter of materials achieving predefined goal values rather than the best design parameters, MO BO can efficiently accelerate realistic MO inverse design problem with small number of experiments. We considered a realistic process of MO inverse material design named goal-achievement-inverse-design. The first step of goal-achievement-inverse-design is to define quantitative goals for all target properties, then conduct goal-oriented MO BO. Finally, optimization is completed when the objective values have reached these goals rather than Pareto optimal solutions having been found (Figure 2C). Note that a similar design process is often seen in human-based real-world material design, especially when experimenters do not want to pay much experimental cost after finding a material that achieves the goals and already has properties acceptable for each application.

First of all the following section, a fully probabilistic MO BO method for goal-achievement-inverse-design is provided by extending a well-studied BO method, lower confidence bound (LCB) (Srinivas et al., 2010). Next, a rigid benchmark method capable of evaluating the performance of BO methods in the goal-achievement-inverse-design is also provided. With this benchmark method and toy problems, the
performance of the proposed MO BO method was compared with a classical SF-based baseline. Finally, to
demonstrate the application of goal-oriented-inverse-design using the proposed method, virtual experi-
ments of MO inverse material design were conducted.

RESULTS AND DISCUSSION

Goal-oriented MO BO

Underpinning BO are the machine-learning model and the acquisition function, and the role of the former
is straightforward. Learning from past experimental results allows the BO method to recommend better
design parameters for the next experiment. You may anticipate recommendations with design parameters
featuring the best of such predicted objective properties. However, what is an excessively conservative
strategy spawns locally optimal design parameters because even if better design parameters exist far
from the current design parameters learned, the machine-learning model itself remains unaware of such
design parameters. Conversely, an excessively challenging strategy, which always selects design param-
eters far from those existing, is also inefficient. Accordingly, mastering the balance of conservative and chal-
lenging experiments is crucial. Note that in the field of BO, conservative, and challenging experiments are
referred to as exploitative and explorative experiments, respectively. To attack this problem in BO, the
scoring function of next-design parameters, known as the acquisition function, is constructed using the ma-
chine-learning model mentioned previously, and the next-design parameters are obtained by optimizing
the acquisition function. The role of the acquisition functions involves balancing the exploitative and
explorative regions of design parameters based on the machine-learning model.

Among them, LCB is one of the most well-studied and used acquisition functions (Srinivas et al., 2010). Note
that, this acquisition function is called the LCB for minimization problems, and also called upper confidence
bound for maximization problems. As its name indicates, LCB is a function that maps design parameter X
into an (100-α)% LCB for the objective property value with design parameter X, where α is a predefined
parameter controlling the balance of exploitative and explorative experiments. By considering the LCB,
BO can be aware of not only exploitative design parameters with better expected properties but also
explorative design parameters that show considerable potential for improving the objective property.

Formally, (100-α)% LCB for objective values Y, under the design parameter X is written as follows:

\[
\text{LCB}(X) = \text{ICDF}_X(\alpha / 100) \quad \text{(Equation 1)}
\]

where ICFF\(_X\) is the inverse cumulative distribution function of Y under the design parameter X. For
simplicity purpose, a one-dimensional normal distribution defined by a mean \(\mu\) and standard deviation
\(\sigma\) obtained by a regression model is assumed.

\[
Y \sim N(\mu(X), \sigma(X)) \quad \text{(Equation 2)}
\]

where Y and X are the single objective value and design parameter, respectively. In this case, using the in-
verse cumulative distribution function of the standard normal distribution \(\Phi^{-1}\), Equation 1 can also be writ-
ten as:

\[
\text{LCB}(X) = \mu(X) + \Phi^{-1}(\alpha / 100)\sigma(X) \quad \text{(Equation 3)}
\]

\[
\text{LCB}(X) = \mu(X) - \sigma(X), \quad \text{(Equation 4)}
\]

where \(\alpha = -\Phi^{-1}(\alpha /100)\). Equation 4 is well used definition of LCB acquisition function, while in the
following Equations 1 and 3 is assumed in order to discuss the probability \(\alpha\).

In the following, the LCB is first extended to the goal-achievement-inverse-design, then further still to the
MO setting. The \(\alpha\) in Equations 1 and 3 is the only tunable parameter of the LCB and tuning \(\alpha\) according to
the probability of goal achievement (PA) is a natural way of extending LCB to goal-achievement-inverse-
design. Note that with smaller \(\alpha\), optimization strategy will be more explorative (Figure 3A, LCB minimum
is different from the model prediction minimum.), whereas larger \(\alpha\) will be more exploitative (Figure 3B,
LCB minimum is same to the model prediction minimum.). Accordingly, it is possible to extend the LCB
to the goal-achievement-inverse-design by controlling the parameter \(\alpha\) depending on the distance from
the goal as follows: If the predefined goal is far away from current designs explored i.e. the PA is small
and exploitative experiments spawning small improvements are not promising, \(\alpha\) should be set smaller.
This makes optimization policy more exploitative. In contrast, if the goal is proximal to current designs
explored i.e. the PA is high and explorative experiments are wasteful, \(\alpha\) should be set larger. This makes
optimization policy more exploitative. Indeed, such tuning of $\alpha$ can be easily realized by replacing the LCB acquisition function with the PA. Although LCB and PA are distinct functions, the design parameters obtained by minimizing LCB and maximizing PA are the same. This can be easily confirmed as follows: Assume, $X^*$ is the optimal design parameter obtained by maximizing the PA and the goal achievement probability with $X^*$ is $a^\%$ (Figure 3C) (See, Equivalence between maximization of PA and minimization of LCB in STAR Methods for the formal description).

Note that the $(100-a^\%)$ LCB under the design parameter $X^*$ is the value where the probability of the observed property $Y$ falling above this point under the design parameter $X^*$ is $(100-a^\%)$, whereas the probability of the observed objective property $Y$ falling above the goal value under the design parameter $X^*$ is also $(100-a^\%)$.

Accordingly, the $(100-a^\%)$ LCB under the design parameter $X^*$ is equal to the goal value. Figure 4 shows the relation between the goal value and LCB. The goal is achieved and not achieved below and above the red line indicating the goal value in Figure 4, respectively. As mentioned above, under design parameter $X^*$, the red line in Figure 4 also indicates the $(100-a^\%)$ LCB. If there is a design parameter $X^{**}$ that results in a lower value than $X^*$ in the $(100-a^\%)$ LCB, as shown in Figure 4, the $(100-a^\%)$ LCB of $X^{**}$ is also lower than the red line indicating the goal, and the PA with design parameter $X^{**}$ exceeds $a^\%$ by a probability $\varepsilon^\%$, which contradicts the assumption that the maximum value of the goal achievement probability is $a^\%$.

Accordingly, the $(100-a^\%)$ LCB contacts the line of the goal value with design parameter $X^*$ (Figure 3D), and the true solution of minimizing LCB and maximizing PA are the same. Namely, using PA as an acquisition function corresponds to LCB with an automatically controlled $\alpha$. And using the PA, as targeted, $\alpha$ will be smaller and the optimization strategy more explorative if the predefined goal is far from current designs.

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**Figure 3. Schematic illustration of the optimization of acquisition functions**

Green lines indicate optimal solutions for acquisition functions. An orange line indicates both the optimal solution and goal value.

(A) Minimization of the LCB with smaller $\alpha$. LCB minimum is different from the model prediction minimum.

(B) Minimization of the LCB with larger $\alpha$. LCB minimum is same to the model prediction minimum.

(C) Maximization of the PA. $X^*$ is the optimal design parameter

(D) Minimization of the LCB with $\alpha^*$. 

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explored. Conversely, \( \alpha \) will be larger and the optimization strategy more exploitative if the goal is proximal to current designs explored.

Extending the PA to a MO problem is simple, by leveraging the joint probability of all objective properties achieving the predefined goals. Assuming observed values of \( M \) objective properties with design parameter \( X \) are independent, the MO PA can be written as the product of the goal achievement probability for \( m \)-th property, \( P_{Am} \):

\[
PA(X) = \prod_{m=1}^{M} P_{Am}(X) \quad \text{(Equation 5)}
\]

This acquisition function can automatically balance the objectives according to the joint probability of each objective property achieving the predefined goal and no ad hoc rules or parameters are used to balance multiple objective properties. Accordingly, the LCB was extended to the MO goal-achievement-inverse-design, in a fully probabilistic manner using the PA acquisition function.

**Benchmark method for goal-achievement-inverse-design**

To examine the PA performance in the goal-achievement-inverse-design, a rigid benchmark method for goal-achievement-inverse-design was also developed. As things stand, the performance of optimization algorithms often depends on setting of problems. For example, an algorithm that is suitable for achieving a goal A may be unsuitable for achieving another goal B. Accordingly, evaluating the performance of algorithms for a single setting of goals is insufficient. To overcome this problem, the performance of algorithms was evaluated using optimization results obtained from 1,000 random samples of setting of balance of goals, where goals were sampled from uniform distribution with minimum and maximum values of each objective property in Pareto optimal solutions obtained by a genetic algorithm-based-MO optimization.

To evaluate the performances of optimization algorithms, a quantitative measure of quality of optimization results is also required. In goal-achievement-inverse-design, this can be simply defined as the number of experiments performed before achieving the predefined goals. Accordingly, in the following benchmarks, the performances of optimization algorithms were compared by the average number of experiments performed before achieving the predefined goals or rate of optimization trajectories that achieved goals within the same time.

**Benchmarks with toy problems**

In benchmarks, for comparison, the performances of an SF-based approach that employs the achievement function which is capable of treating predefined goals (Hakanen and Knowles, 2017; Wierzbicki, 2007) were
also evaluated as a baseline. The achievement function have been used in the field of the operations research. By scalarizing multiple objective properties using the achievement function, the single-objective BO can be applied for the value of the achievement function. LCB acquisition was used for this single-objective BO of the achievement function. See Calculation of the achievement function in STAR Methods for details about how the achievement function weights and merges multiple objectives, and how the LCB acquisition was calculated.

The performances of the proposed BO method with the PA and the achievement baseline were evaluated for six mathematical MO toy functions (Figure 5) with 1,000 randomly sampled predefined goals. These functions have been used to evaluate the performances of MO optimization methods (Huband et al., 2006). The toy functions included relatively simple low dimensional problems, Fonseca, Kursawe, and Viennet and also include complex high-dimensional problems, ZDT1, ZDT2, and ZDT3. Although, the goal-achievement-inverse-design will be finished after achieving the goal, 200 steps of BOs were performed for all optimization runs for comparison purposes.

Figure 6 shows the rate of optimization runs having achieved goals for each step in 200 steps of optimizations, which is referred to as the goal achievement rate (GAR) in this study. See Performance metrics in STAR Methods for formal definition of the GAR. As expected for all six benchmarks, the PA dramatically reduced the optimization steps required to achieve the goals relative to the achievement baseline. For easier problems, Fonseca and Kursawe, the BO with the PA achieved most of the goals in the early stage of optimization, far outpacing the achievement baseline. For more difficult problems, Viennet, ZDT1, ZDT2, and ZDT3, even with the PA, the GAR did not reach 1, indicating that some of the randomly sampled goals remained unachieved within 200 steps of BO. However, the GAR after 200 steps of BO using the PA far exceeds that using the achievement baseline, particularly for high-dimensional problems ZDT1, ZDT2, and ZDT3, where the number of design parameters is 30 and the achievement baseline cannot be achieved most of goals randomly sampled for these high-dimensional problems.

There are two possible reasons explaining these significant performance gaps. The first possible reason is that BO did not work well with LCB and the achievement function and the second is the difficulty in properly balancing the objective properties with the achievement function, particularly with complex and high-dimensional design parameters. To investigate the first possible reason, convergences of optimization trajectories to the Pareto optimal solutions are monitored alongside optimization steps. Note that this analysis corresponds to evaluating the performances of optimization methods from the point of view of few-solution-inverse-design.

Figure 7 shows the time evolutions of the average minimum distances (AMDs) between the objective values of Pareto optimal solutions and current designs explored in log scale. See Performance metrics in STAR Methods for the formal definition of the AMD.

Unlike performance evaluation according to the goal-achievement-inverse-design shown in Figure 6, the performances of both methods in the few-solution-inverse-design compete. Although, for the Viennet, ZDT1, and ZDT3, the PA converged to the Pareto optimal solutions faster relative to the achievement baseline, for Fonseca, Kursawe, and ZDT2, the achievement baseline showed better convergence relative to the PA. It is notable that from the point of view of few-solution-inverse-design, the achievement baseline performed far better relative to the PA for the high-dimensional ZDT2 problem, while from the point of view of goal-achievement-inverse-design, the achievement baseline showed much worse performance relative to the PA for this problem (Figure 6). Accordingly, at least, for Fonseca, Kursawe, and ZDT2, the main reason for improved GAR on the part of PA relative to the achievement baseline is attributable to the exquisite balancing between multiple objective properties made possible by the fully probabilistic approach. And the benchmarks clearly showed that by focusing on finding a design parameter of materials achieving pre-defined goal values rather than the Pareto optimal solutions, BO with the PA can efficiently accelerate MO optimization problems.

Virtual MO inverse material design
Next, to demonstrate an application of goal-achievement-inverse-design by using the BO with the PA for realistic material design problem, virtual material-design experiments were conducted using regression models constructed from experimental data as a substitute for time-consuming real-world experiments.
The regression models were obtained from a recent MO material-design study conducted by Wang et al. (Wang et al., 2020a), where a high-performance oil sorbent material was developed by a method resembling BO with the weight-summation SF. The use of oil sorbent materials helps remove oil spilled on bodies of water, such as at sea, to mitigate ecological damage, for which materials with high contact angles, high oil absorption capacity, and high mechanical strength are known to be preferable. Wang et al. (Wang et al., 2020a) used these three parameters as objective properties in the optimization and seven design

| Problem | Pareto optimal solutions |
|---------|-------------------------|
| **Fonseca** | 
Minimize $$\begin{cases} 
 f_1(X) = 1 - \exp \left( - \sum_{d=1}^{D} \left( x_d - \frac{1}{\sqrt{D}} \right)^2 \right) \\
 f_2(X) = 1 - \exp \left( - \sum_{d=1}^{D} \left( x_d + \frac{1}{\sqrt{D}} \right)^2 \right) \\
 -4 \leq x_d \leq 4, \quad D = 2 
\end{cases}$$ |
| | ![Image 1] |
| **Kursawe** | 
Minimize $$\begin{cases} 
 f_1(X) = \sum_{t=1}^{3} \left[-10\exp \left(-0.2 \left(x_1^2 + x_2^2\right)\right) \right] \\
 f_2(X) = \sum_{t=1}^{3} \left[20x_1^{0.1} + 5 \sin x_2^2 \right] \\
 -5 \leq x_d \leq 5 
\end{cases}$$ |
| | ![Image 2] |
| **Viennet** | 
Minimize $$\begin{cases} 
 f_1(X) = 0.5(x_1^2 + x_2^2) + \sin(x_1^2 + x_2^2) \\
 f_2(X) = \frac{x_1^2}{27} + \frac{1}{x_1^2 + x_2^2 + 1} + 1.1 \exp[-(x_1^2 + x_2^2)] \\
 -30 \leq x_1, x_2 \leq 30 
\end{cases}$$ |
| | ![Image 3] |
| **ZDT1** | 
Minimize $$\begin{cases} 
 g(X) = 1 + \frac{9}{D-1} \sum_{d=3}^{D} x_d \\
 f_1(X) = x_1 \\
 f_2(X) = g(X) \left( 1 - \frac{x_1}{g(X)} \right) \\
 0 \leq x_d \leq 1, \quad D = 30 
\end{cases}$$ |
| | ![Image 4] |
| **ZDT2** | 
Minimize $$\begin{cases} 
 g(X) = 1 + \frac{9}{D-1} \sum_{d=3}^{D} x_d \\
 f_1(X) = x_1 \\
 f_2(X) = g(X) \left( 1 - \frac{x_1}{g(X)} \right) \\
 0 \leq x_d \leq 1, \quad D = 30 
\end{cases}$$ |
| | ![Image 5] |
| **ZDT3** | 
Minimize $$\begin{cases} 
 g(X) = 1 + \frac{9}{D-1} \sum_{d=3}^{D} x_d \\
 f_1(X) = x_1 \\
 f_2(X) = g(X) \left( 1 - \frac{x_1}{g(X)} - \frac{x_1}{g(X)} \sin 10\pi x_1 \right) \\
 0 \leq x_d \leq 1, \quad D = 30 
\end{cases}$$ |
| | ![Image 6] |

**Figure 5. Mathematical toy problems used in the benchmarks**
Objective values, $f_1$ and $f_2$, for Pareto optimal solutions obtained by NSGA are also shown. All the Pareto optimal solutions used in this study are also provided as Data S1.
The design parameters include three parameters related to compositions of materials, polystyrene/polyacrylonitrile ratio, mass fraction of solute, and mass fraction of SiO2 nanoparticles in solute and also include four parameters related to fabrication process, feed rate, receiving distance, applied voltage, and inner diameter of needle. In the following virtual material-design, the same objectives and design parameters are used. The regression models used here and further details of design parameters can be obtained from the work of Wang et al. (Wang et al., 2020a).

The goal-achievement-inverse-design started from defining the goal values of objective properties. In our virtual oil sorbent material design, five sets of goals, 1, 2, 3, 4, and 5, with different design objectives were defined using the oil sorbent material designed by Wang et al. in the previous study (Wang et al., 2020a) as a reference. Figure 8 shows values of the five sets of the goals scaled by the values of each property in the reference, and Table 1 shows the unscaled values of sets of properties for the five goals with short descriptions on their design objectives. The design objective of the goal 1 is to achieve same level of values relative to the reference in all the three properties. On the other hand, the design objective of the goal 2, 3, and 4 are to achieve higher values than the reference in the contact angle, oil-absorption capacity and mechanical strength, respectively. Finally, the design objective of the goal 5 is to achieve higher values in all the three properties relative to the reference. Table 1 also includes the number of random experiments.
required to achieve each goal, which indicates the difficulty of each goal, and even for the easiest goal, 1, over 100 experiments are needed to achieve the goals in average. Furthermore, for the most difficult goal, 5, over 10,000 experiments are needed to achieve the goals, which is inaccessible for real world experiments.

Next, virtual experiments for ten randomly chosen design parameters were conducted, which is needed to initialize the machine-learning model. And MO BO steps were repeated pending achievement of the pre-defined goals. For statistical purposes, these processes were repeated 100 times by randomly changing the initial ten design parameters. Note that, randomly chosen design parameters that achieve the goals were not used as initial design parameters for BO. The performance of BO with the PA in the goal-achievement-inverse-design was evaluated by calculating average number of BO steps required to achieve goals, and comparison between the obtained results and the performance of random sampling, which is also shown in Table 1, are summarized in Figure 9A in log scale. The bar graphs clearly showed that the BO with the PA can efficiently achieve the goals within small numbers of experiments (5–12). Even for the easiest goal, 1, BO with the PA achieved it over 30 times faster than random experiments, while for the most difficult goal, 5, BO with the PA achieved the goal over 1,000 times faster than random experiments. Accordingly, using the PA in goal-achievement-inverse-design can pave the way for efficiently solving MO inverse material design problems that are difficult for the random experiment.
In order to reconfirm the superiority of the PA relative to the achievement baseline in realistic inverse design problems, the performances of the BO using the PA and the achievement baseline were also compared and summarized in Figure 9B. As with the benchmarks using the mathematical toy functions, BO with the PA clearly outperformed the achievement baseline for all five settings of goals, and consistently showed around 2 times acceleration relative to the achievement baseline.

Finally, in order to demonstrate the reason why the goal-achievement-inverse-design is suitable for real-world material design problems, experimental costs for finding a Pareto optimal solution were compared with that for achieving the goals, by extending the BO steps for all the virtual experiments, and evaluating numbers of optimization steps required to find a first Pareto optimal solution. In this analysis, only the Pareto optimal solutions that achieve the predefined goals were regarded as the solutions, and therefore the obtained Pareto optimal solutions have equivalent or better values in all the objective properties compared to the goal values. See, Judgment of Pareto optimal solutions in STAR Methods for details about how to judge whether obtained objective properties reached Pareto optimal solutions. Because, the achievement baseline showed better performances than the PA in finding the Pareto optimal solutions for this virtual experiment system (Table S3), the results for the achievement baseline were used in the following comparison.

Average numbers of experiments required to find a first Pareto optimal solution using the achievement baseline are shown in Figure 9C with that required to achieve the goals using the PA. As expected, even with the BO, finding of Pareto optimal solutions is much more difficult than achieving the goals. Finding of Pareto optimal solutions required over two times more experiments than achieving the goals in all the setting of goals. Furthermore, for easier goals (goals 1 and 2) gaps between the difficulty of achieving the goals and finding Pareto optimal solutions were especially large, and finding Pareto optimal solutions required around four times more experiments than achieving the goals. Such differences in the required numbers of experiments are critical when budget and time available for the material development are limited and experimenters do not want to pay much experimental cost after finding a material that achieves the goals and already has properties required for

| Goal | Contact angle (°) | Oil-absorption capacity | Mechanical strength (Mpa) | Design objective | Required number of random experiments* |
|------|------------------|-------------------------|--------------------------|-----------------|---------------------------------------|
| Goal 1 | 140.1 | 83.7 | 4.1 | Same level of the reference | 158.6 (149.7-168.0) |
| Goal 2 | 160.0 | 83.7 | 4.1 | Higher contact angle | 256.1 (240.5-271.9) |
| Goal 3 | 140.1 | 100 | 4.1 | Higher oil-absorption capacity | 333.6 (313.4-354.1) |
| Goal 4 | 140.1 | 83.7 | 8.0 | Higher mechanical strength | 5499.6 (5136.9-5876.7) |
| Goal 5 | 160.0 | 100.0 | 8.0 | Improve all properties | 13760.8 (12946.5-14632.8) |

*Average number of experiments required to achieve the each set of goals was evaluated by 1000 sequences of random experiments. 95% confidence intervals estimated by bootstrap resampling are shown in parentheses.
applications. And such situations often occur in materials design processes requiring time-consuming real-world experiments, especially when experimenters are in competition with others and the speed of material design is important. Therefore, the goal-achievement-inverse-design using the PA, which efficiently accelerate solving the realistic design problem, goal achievement, is expected to be attractive for such situations. Indeed, in this demonstration, around 10 experiments were required to achieve the goals and design high-performance oil sorbent materials, and this experimental cost should be acceptable for many actual material design problems with time-consuming real-world experiments.

It is worth to mention that another merit of the goal-achievement-inverse-design compared with other methods intending to find Pareto optimal solutions is its simplicity in the criterion for stopping the optimization. In other words, experimenter conducting the goal-achievement-inverse-design can stop optimization efforts immediately after the goal achievement. While, even if methods intending to find Pareto optimal solutions are employed, it is often difficult to use the Pareto optimality as a criterion for stopping the optimization, because whether obtained solutions reached near the true Pareto optimal solutions can only be confirmed when whole the Pareto optimal solutions have been found after massive experiments. And there are no common reasonable criteria for stopping the optimization in such a situation.

Figure 9. Average number of steps required to achieve the goals
(A) Comparison between the PA and random sampling in log scale. For random sampling, average number of experiments required to achieve the each set of goals was evaluated by 1,000 sequences of random experiments.
(B) Comparison between the PA and achievement baseline.
(C) Average number of steps required to achieve the goals by using the PA is compared with that required to find a first Pareto optimal solution by using the achievement baseline. Error bars indicate the 95% confidence interval of the average number of steps estimated by bootstrap resampling.
See also Tables S2 and S3.
Conclusion
In this study, the goal-achievement-inverse-design for the MO material design was introduced with the fully probabilistic acquisition function, PA and the rigid benchmark method. In the benchmarks, using the six mathematical functions, the performances of the PA and the achievement baseline were compared and the benchmark results showed that by focusing on finding a design parameter achieving predefined goal values rather than the Pareto optimal solution, BO with the PA dramatically outperformed the achievement baseline for all the six mathematical functions in the rate of optimization runs that achieved the goals. And performance improvement of the PA relative to the achievement baseline were much larger for complex optimization problems with more objectives or more design parameters. In addition, the application of goal-achievement-inverse-design with the PA was demonstrated using more realistic virtual material-design problems to achieve the five goals with different design objectives, where the BO with the PA again outperformed the achievement baseline, and the BO with the PA achieved the goals over 1,000 times faster than the random sampling for the most difficult case. Furthermore, in this virtual inverse material design, number of experiments required to achieve the goals were around ten, which is over two times smaller than that required to find Pareto optimal solutions and would be acceptable for most real-world material design problems with time-consuming experiments. The proposed inverse design method that works with small number of possible experiments will precede the real-world implementation of MO inverse material design, where time-consuming experiments are often required.

Limitations of the study
The inverse design approach proposed in this study can only be applied for design problems, where a quantitative and reasonable goal can be defined for each objective. And the proposed approach is not suitable for design problems where it is difficult to set reasonable goals. Additionally, the goal-achievement-inverse-design is also not suitable for the design problems, where massive number of experiments can be conducted and experimenter want to find as good solutions as possible. A typical example of such a design problem is computational materials design using molecular simulation approaches with low computational cost.

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Supplemental information can be found online at https://doi.org/10.1016/j.isci.2021.102781.

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AUTHOR CONTRIBUTIONS

The work was done by a single author.

DECLARATION OF INTERESTS

The author applied for patents related to this work and declares no other competing interest.

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STAR METHODS

KEY RESOURCES TABLE

| REAGENT or RESOURCE | SOURCE | IDENTIFIER |
|---------------------|--------|------------|
| Deposited Data      |        |            |
| Regression model for oil sorbent materials | Wang et al., 2020a, 2020b, supplemental information | https://pubs.acs.org/doi/abs/10.1021/acsami.0c11667 |

Software and algorithms

| SOFTWARE | SOURCE | IDENTIFIER |
|----------|--------|------------|
| GPy version 1.9 | Sheffield Machine Learning Software | https://github.com/SheffieldML/GPy |
| GpyOpt version 1.2 | Sheffield Machine Learning Software | https://github.com/SheffieldML/GPyOpt |
| Platypus version 1.0 | Platypus - Multiobjective Optimization in Python | https://platypus.readthedocs.io/en/latest/ |
| SciPy version 1.5 | Virtanen et al., 2020 | https://www.scipy.org/ |
| Python version 3.6 | Python Software Foundation | https://www.python.org |
| Code for multi-objective Bayesian optimization using the PA and achievement baseline | This paper; Mendeley Data | https://data.mendeley.com/datasets/fg5ngjsm79/1 |

RESOURCE AVAILABILITY

Lead contact

Further information and requests for resources and reagents should be directed to and will be fulfilled by the lead contact, Kyohei Hanaoka (hanaoka.kyohei.xicmq@showadenko.com).

Materials availability

This study did not generate new reagents.

Data and code availability

The code required to reproduce the results of this study is available at Mendeley Data: https://data.mendeley.com/datasets/fg5ngjsm79/1. This code can be freely used for scientific purposes.

METHOD DETAILS

Equivalence between maximization of PA and minimization of LCB

In the following, Y is assumed to be a random variable whose cumulative distribution function is strictly monotonically increasing. Note that the cumulative distribution function of the well-used normal distribution is also strictly monotonically increasing. And X is a set of design parameters that determines the shape of the cumulative distribution function of the random variable Y. For clarity, random variable Y under design parameter X is written as Y_X.

Assume, X* is the optimal design parameter obtained by maximizing the PA and the goal achievement probability with X* is \( \alpha^\ast \)%. That is, the probability that random variable Y_X falls below the predefined goal g is given by

\[
P(Y_{X^*} < g) = \alpha^\ast/100 \quad \text{(Equation 6)}
\]

From the definition of the LCB, the probability that random variable Y_X falls below the \((100-\alpha^\ast)\)% LCB under design parameter X* is given by

\[
P(Y_{X^*} < \text{LCB}_{\alpha^\ast}(X^*)) = \alpha^\ast/100 = P(Y_{X^*} < g) \quad \text{(Equation 7)}
\]

where LCB_{\alpha^\ast} represents \((100-\alpha^\ast)\)% LCB. From Equation 7, because, cumulative distribution function of Y is strictly monotonically increasing,

\[
\text{LCB}_{\alpha^\ast}(X^*) = g \quad \text{(Equation 8)}
\]
If there is a design parameter \( X^{**} \) that results in a lower value than \( X^* \) in the \((100-a)^\% \ LCB\),

\[
\text{LCB}_{\alpha}(X^{**}) < \text{LCB}_{\alpha}(X^{*}) = g
\]

(Equation 9)
because the cumulative distribution functions of \( Y \) is strictly monotonically increasing, from Equation 9,

\[
P(Y_{X^{**}} < \text{LCB}_{\alpha}(X^{**})) < P(Y_{X^{*}} < g)
\]

(Equation 10)

Again, from the definition of the LCB,

\[
P(Y_{X^{**}} < \text{LCB}_{\alpha}(X^{**})) = \alpha^*/100
\]

(Equation 11)

Therefore,

\[
\alpha^*/100 < P(Y_{X^{*}} < g)
\]

(Equation 12)

This contradicts the assumption that the maximum value of the goal achievement probability is \( \alpha^\% \). Therefore, \( X^{**} \) cannot exist, and the solution of minimizing \((100-a)^\% \ LCB\) is also \( X^* \).

### Performance metrics

Goal achievement rate (GAR) in T-th optimization step (Figure 6) is defined as follows:

\[
\text{GAR}(T) = \frac{\text{Number of BO runs achieving the goals within T steps}}{\text{Total number of BO runs}}
\]

(Equation 13)

The minimum distances from the Pareto optimal solutions (Figure 7) were calculated by evaluating the distances of all the current designs explored and all approximated true Pareto solutions obtained by NSGA-II (Deb et al., 2002). Formally, the average minimum distance (AMD) from the Pareto optimal solutions in T-th step for 1,000 randomly sampled optimization trajectory is defined as follows:

\[
\text{AMD}(T) = \frac{\sum_{n=1}^{1000} \text{mindist}_n(T)}{1000}
\]

(Equation 14)

\[
\text{mindist}_n(T) = \min_{t=1, \ldots, T; m=1, \ldots, M} D_2(Y_{n,t}, P_m)
\]

(Equation 15)

where \( D_2 \) is a function mapping a pair of vectors to Euclidean distance, \( P_m \) is a vector comprising the objective values of m-th Pareto optimal solution and \( Y_{n,t} \) is a vector comprising the objective values of n-th Bayesian optimization run in t-th step. \( M \) is a total number of the Pareto optimal solutions and was set to 1000. Before calculating AMD, objective values were scaled by dividing by the difference between the maximum and minimum values of each objective in the Pareto optimal solutions.

### BAYESIAN OPTIMIZATION

The initial design parameters for Bayesian optimization were randomly selected. For benchmarks using mathematical toy functions, the number of the initial design parameters for each toy problem was set according to the number of design parameter dimensions plus 1. All Bayesian optimizations were performed using a GpyOpt library by implementing multi-objective functionalities, with default GpyOpt settings used unless otherwise stated. Gaussian process regression with the Matern52 kernel implemented in GPy and the normal distribution noise model were used for the machine learning model driving Bayesian optimization. Since the noise model assumed in the Gaussian process regression is the normal distribution, the probability distribution of the objective property with design parameter \( X \), predicted by Gaussian process regression, also follows the normal distribution and acquisition functions were calculated using mean and standard deviation of this normal distribution.

### CALCULATION OF THE PROBABILITY OF ACHIEVEMENT

Optimizations of the probability of achievement (PA) were performed following the logarithmic transformation. Given design parameter, \( X \), the log of the PA for \( M \) objective properties can be obtained as follows:

\[
\text{LogPA}(X) = \sum_{m=1}^{M} \log \left[ 1 - \Phi \left( \frac{\mu_m(X) - g_m}{\sigma_m(X)} \right) \right]
\]

(Equation 16)

where, \( g_m, \mu_m, \) and \( \sigma_m \) are the predefined goal, predicted mean and predicted standard deviation for the m-th objective property, respectively. \( \Phi \) is the cumulative distribution function of the standard normal distribution. Note that a classical experiment navigation method for the robust product design with noisy measurements called Nakazawa method also uses a similar scoring function based on the joint probability
Calculation of the achievement function
Given the predefined goal $g_m$ for each objective property $y_m$, the achievement function for $M$ objectives is defined as follows:

$$\text{Achieve}(Y) = \sum_{m=1}^{M} y_m w_m + \max_{m=1\ldots M} [(y_m - g_m) w_m]$$  (Equation 17)

where $w_m$ and $\rho$ are predefined parameters. Note that the need for $w_m$ arises from scale difference in objective properties. According to previous studies in the operational research field, (Hakanen and Knowles, 2017) $\rho$ was set to 0.05 and $w_m$ was calculated as the reciprocal number of differences between maximum and minimum values in Pareto optimal design within the design parameters explored.

Bayesian optimization with LCB acquisition, implemented in GPyOpt was used to optimize the achievement function. In GPyOpt, the LCB acquisition is implemented as Equation 4, and default value of the parameter $a$ ($a=2$) was used.

Optimization of the acquisition function
Acquisition function optimizations were performed using the default protocol implemented in GPyOpt. In this protocol, the putative global minimum (maximum for the PA) of the acquisition functions is searched by 1000 initial random searches and subsequent optimization of the top-5 local minimum using quasi-Newton method, L-BFGS-B, implemented in SciPy. (Virtanen et al., 2020) Finally, a design parameter with the minimum searched-for value is selected for the next experiment.

Calculation of pareto optimal solutions
The multi-objective optimization methods that efficiently and thoroughly find the Pareto optimal solutions have been well studied in the field of the operations research. Among them, Non-dominated Sorting Genetic Algorithms-II (NSGA-II) (Deb et al., 2002) is one of the standard methods for optimization problems with a few objectives. In order to obtain the Pareto optimal solutions, NSGA-II implemented in Platypus library was used with sufficient number of optimization steps. The number of the obtained Pareto optimal solutions for the six mathematical benchmark problems was set to 1000, while that for the virtual inverse material design problem was set to 10000 in order to accurately evaluate experimental costs of finding Pareto optimal solutions.

Regression models for virtual material design experiment
For the virtual material design experiment, regression models constructed from experimental data were used as a substitute for time-consuming real-world experiments. The regression models can be obtained from the work of Wang et al. (Wang et al., 2020a; https://pubs.acs.org/doi/abs/10.1021/acsami.0c11667)

Judgment of Pareto optimal solutions
For the virtual material design experiment, average numbers of experiments before finding a first Pareto optimal solution were evaluated (Figure 9C). A set of objectives is judged as Pareto optimal when it is not Pareto-dominated by any of 10000 Pareto optimal solutions obtained by NSGA-II. Because, finding of exact Pareto optimal solutions is unnecessarily difficult, a small value $\delta$ was added to each objective value obtained by the Bayesian optimization before Judgment of Pareto optimal solutions. The small value $\delta$ for each objective was calculated as difference between the maximum and minimum values of each objective in the true Pareto optimal solutions multiplied by 0.005.

QUANTIFICATION AND STATISTICAL ANALYSIS
Performance evaluations of the Bayesian optimization methods for mathematical multi-objective toy functions were repeated 1000 times using randomly sampled settings of goals, and averages and 95% confidence intervals obtained by bootstrap resampling were reported.
Performance evaluations of the Bayesian optimization methods for the virtual material-design experiment were repeated 100 times using randomly sampled initial design parameters, and averages and 95% confidence intervals obtained by bootstrap resampling were reported.

Performance evaluations of the random sampling for the virtual material-design experiment were repeated 1000 times, and averages and 95% confidence intervals obtained by bootstrap resampling were reported.