Aberrations in Structured Illumination Microscopy: A Theoretical Analysis

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In super-resolution optical microscopes, aberrations often compromise the image performances by reducing its resolution and contrast. In previous works, the aberrations in stimulated emission depletion (STED) microscopy and single-molecule localization microscopy (SMLM) have been well-investigated, while the research on the aberrations in structured illumination microscopy (SIM) is not sufficient. The researchers always poured attention into aberrations only in the detection path. In this paper, we investigate the aberrations in SIM in a comprehensive manner, and their causes and effects on both the illumination and the detection paths are discussed. The aberrations in the illumination path may distort illumination patterns, and deteriorate the final images, together with the aberrations in the detection path. In addition, several non-aberration-related factors, especially the misalignment of the incident beams with respect to the objective pupil, can also dramatically influence the performances of SIM. The analysis provides the theoretical basis and for optimizing a SIM system.

Keywords: fluorescence microscopy, structured illumination, aberrations, adaptive optics, Zernike polynomials

INTRODUCTION

Fluorescence microscopy is widely used for the visualization of microstructures and dynamic processes in cells. However, owing to the diffraction limit, the best resolution is only about a half wavelength of the fluorescence [1] when the conventional fluorescence microscope is applied. Nevertheless, the state-of-the-art super-resolution microscopy can break the diffraction limit. These methods include, but are not limited to the single-molecule localization microscopy (SMLM) that stochastically activates single molecules in the full-field [2–5], the stimulated emission depletion (STED) microscopy using a depletion doughnut focal spot to reduce the size of the effective point spread function (PSF) [6–8], and the structured illumination microscopy (SIM) illuminating the sample with a periodic pattern [9–11]. Among them, SIM is exceedingly significant for live-cell imaging, providing double spatial resolution than that of the conventional wide-field microscopy. In this method, a one-dimensional sinusoidal illumination pattern is produced in the focal plane of the objective lens. A series of images, when the sample is illuminated by the patterns with different phases and orientations, are acquired by a camera. Using the specific SIM reconstruction algorithms [12–15], the super-resolution image of the sample can be obtained.

In super-resolution optical microscopes, aberrations compromise the image performances by worsening its resolution and reducing its contrast. The aberrations in SMLM and STED microscopy have been investigated sufficiently in previous works [16–18]. However, for SIM, researchers always poured attention only into the aberrations in the detection path, or assume that the aberrations are...
identical in the two paths [19, 20]. The discussion regarding the illumination path is insufficient. Yet, the quality of the illumination pattern is also crucial for the imaging performance of SIM. To fully optimize the final images of SIM, it is essential to create a model to describe the aberrations in SIM more comprehensively and figure out how they affect both the illumination pattern and the detection PSF.

In this paper, a strategy is developed for quantifying aberration effects in SIM. We build a mathematical model to analyze how the aberrations affect the illumination pattern and the detection PSF. As the systematic aberrations can be minimized during the design, only the sample-induced aberrations are considered. In addition, several non-aberration-related factors, especially the misalignment of the incident beams with respect to the objective pupil, are also discussed.

THEORY

In SIM, a sinusoid pattern is used to excite the sample. The image obtained by a camera can be expressed as:

\[ i(r) = \mathbf{e}(r) \cdot \mathbf{o}(r) \otimes h(r) \]  

(1)

where \( \mathbf{e}(r) = 1 + \cos(\mathbf{k}_e \cdot r) \) is the intensity distribution of the illumination pattern, \( \mathbf{o}(r) \) is the spatial distribution of the sample labeled with fluorophores, and \( h(r) \) is the point spread function (PSF) of the detection path.

In the Fourier domain, Equation (1) can be expressed as:

\[ \tilde{i}(k) = [\tilde{\mathbf{e}}(k) \otimes \tilde{\mathbf{o}}(k)] \cdot \tilde{h}(k) = [\tilde{\mathbf{o}}(k) + \frac{1}{2} \tilde{\mathbf{o}}(k - \mathbf{k}_e) \cdot e^{i\varphi} + \frac{1}{2} \tilde{\mathbf{o}}(k + \mathbf{k}_e) \cdot e^{-i\varphi}] \cdot \tilde{h}(k) \]

(2)

where \( \tilde{i}(k) \), \( \tilde{\mathbf{e}}(k) \), \( \tilde{\mathbf{o}}(k) \), and \( \tilde{h}(k) \) are the Fourier transform of \( i(r) \), \( \mathbf{e}(r) \), \( \mathbf{o}(r) \), and \( h(r) \), respectively, \( \mathbf{k} \) represents the spatial frequency. Inducing structured illumination pattern, SIM can move the high spatial frequency information originally blocked by the optical system into the passband, which expands the size of the optical transfer function (OTF) of the system.

Equations (1) and (2) demonstrate that the image obtained by SIM is in close connection with the illumination pattern, the spatial distribution of the sample, and the PSF of the detection path. Therefore, we took both the illumination path and the detection path into consideration to analyze the aberrations in SIM. To simplify the discussion, only the sample-induced aberrations were considered, since the systematic aberrations are always minimized during the design. For the illumination path, the excitation pattern is generated by the interference of two beams, which can be expressed as:

\[ e(r) = |A_1 \exp(\mathbf{k}_1 \cdot r + \varphi) + A_2 \exp(\mathbf{k}_2 \cdot r)|^2 \]

(3)

where \( A_1 \) and \( A_2 \) are the amplitudes of the two coherent incident beams, respectively, \( \mathbf{k}_1 \) and \( \mathbf{k}_2 \) are the wave vectors, respectively, and \( \varphi \) is the phase difference between the two beams. To simplify the discussion, the two beams can be assumed to be s-polarized and \( \varphi = 0 \) [21], plus \( |A_1| = |A_2| \). For the detection path, the PSF can be calculated using the vectorial diffraction theory [22, 23]. Moreover, in our simulation, the illumination beam and the detection beam are both linear polarized.

A mathematical model is built to analyze the effects of the aberrations. As depicted in Figure 1, the illumination beam exits the objective, propagates into the immersion medium layer, and then passes through the coverslip into the sample medium. On the other hand, in the detection path, following the reversibility principle of the beam path, the fluorescence emitted from the sample medium can be treated as the light focused by the same objective. The refractive indices (RI) of the three layers of media (immersion liquid, coverslip, and the sample) are represented as \( n_1 \), \( n_2 \), and \( n_3 \), respectively, while the thickness of the coverslip is \( h \). The incident angles of the illumination beam on each media interface are \( \theta_1 \), \( \theta_2 \), and \( \theta_3 \), respectively, while the angles are \( \alpha_1 \) and \( \alpha_2 \) for the detection path. In our simulation, the objective is plan-apochromatic by default [24].

A Cartesian coordinate system \( (x, y, z) \) is built for the description of the position information (Figure 1A). The orientations of the unit vectors \( x \) and \( z \) are defined by the layer interface and the optical axis, respectively. The origin of the coordinate system is consistent with the position of the Gaussian focus in the absence of stratified media (no sample medium, Figure 1B), and the subscript \( i \) denotes the ideal values [24]. Following the above definitions, the lower surface of the coverslip is located at \( z = 0 \), while the upper one at \( z = -h \).

To quantitatively test the aberration effects, we set the excitation and fluorescence wavelengths as 488 and 532 nm, respectively.

Aberrations are usually measured by the deviation of the practical wavefront from its ideal shape and can be expressed as:

\[ \delta = |k| \cdot \left[-z_1 \cdot n_3 \cos \theta_3 + (z_1 - z_2) \cdot n_2 \cos \theta_2 + z_2 \cdot n_1 \cos \theta_1 - (h_1 \cdot n_2 \cos \theta_2 - h_1 \cdot n_1 \cos \theta_1)\right] \]

(4)

where \( z_1 \) and \( z_2 \) are the \( z \)-coordinates of the lower and upper surface of the coverslip for simulation, respectively. Notably, the radius of the aberration induced by the RI difference between the immersion medium and the coverslip during the objective’s design [24].

RESULTS AND DISCUSSION

The results with no aberrations are shown in Figure 1. Different numerical apertures (NA) were applied during the simulations, and the specific parameters in each simulation are presented in Table 1. Combining the excitation patterns and the PSFs of the detection path, the images of SIM were reconstructed using the inverse matrix-based phase estimation algorithm (Figure 1E) [15], and the resolution was estimated using the parameter-free image resolution estimation method [25]. As what we expect, the comparisons between Figures 1C–G illustrate that using the objective with a larger NA generates a smaller PSF and a denser...
sinusoid pattern, thereby achieving a better resolution. In our simulation, the ideal interference angle of the two beams is determined by \( \theta_{i} = \sin^{-1}(\text{NA} / n_{1}) \).

We further investigated the effects of the aberrations when the value of the RI of the coverslip deviates from the desired one, which is depicted in Figure 2. In Figures 2A,B, the incident angles \( \theta \) and \( \alpha \) change in response to the varied RI of the coverslip. Similar to the above simulations, a series of different RIs were considered to discuss the effects in a more comprehensive manner, and Figures 2C–I are simulated in \( n_{2} = 1.521 \) for detail.

As depicted in Figure 2C, the pupil functions of the detection path were calculated using the ray tracing. Moreover, to quantify the aberrations, we decomposed these pupil functions into Zernike polynomials \([26, 27]\) from 0th to 14th modes, which are shown in Figure 2D. The piston (0th) mode holds the most part, which has no visible effect on the PSF, while the remainders are the defocus mode (4th) that simply makes the PSF out of focus and the primary spherical mode (12th) which increases the size of the PSF (Figures 2E,F). The profiles (Figure 2H) indicate that the aberrations induced in Figure 2A have little effects on the excitation patterns (Figure 2G) owing to the constant NA.

FIGURE 1 | SIM with no aberrations for objectives with different NAs. (A) The illumination beam path. (B) The fluorescence is inversely collected by the same objective using the classic epifluorescence architecture. (C) The PSFs on the plane \( z = 0 \) (ideal focal plane). (D) The excitation patterns calculated from different objectives using the same parameters in (C). (E) The reconstructed images of SIM from the objectives with different NAs. From left to right, the resolutions are 164, 128, 125, 125, and 120 nm. (F,G) are profiles of the ideal PSFs in (C) on the x and y-direction, respectively.
All three cases discussed above can induce aberrations to some extent. However, these aberrations are symmetrical about the optical axis. Therefore, only the symmetric Zernike polynomials, e.g., defocus and spherical aberrations appear. The condition becomes more complicated when the symmetry is broken. As an example, we can give a small slope angle $\beta$ to the coverslip (Figures 5A,B). The direct consequence of the tilted coverslip is the re-organization of the incident angles $\theta$ and $\alpha$, which eventually results in the accumulation of the aberrations. It’s paramount to be clear that the aberrations vary with the field of view along the x-axis, as a result of the various optical length difference. Therefore, the PSF is location dependent, and the final image is blurred by these variable PSFs. During the simulation, the slope angle $\beta$ varied within a range of 0°–0.3°, and Figures 5C–I is an example when $\beta = 0.3°$. The pupil functions were then calculated and decomposed into the first 15 Zernike modes, and the major modes now are tip (2nd) and coma (8th) aberration. Notably, in our simulation, the tilted coverslip has effects on the size of pupil function when $NA = 1.4$ (Figure 5J), as a result of the TIR induced by the tilt. Moreover, the intensity of the excitation pattern decreases with $x$ increasing, and the periods of these patterns change. The scope is different from that in the above cases because the sample only exists in the side $x > 0$ on the plane $z = 0$. Subsequently, the reconstructed images were obtained with deviation from the center of the scope, and the contrast reduced.

The correlation coefficients between the distorted images and that with no aberrations are shown in Figure 5K. Generally speaking, it descends with the slope angle $\beta$ increasing. However, for $NA = 0.95$, the correlation coefficient decreases first and then increases.

Based on the above results, the aberrations induced by the mismatched RIs, the increase of the focal depth, and the biased thickness of the coverslip have little effects on the excitation patterns. However, the PSFs are more affected, which is shown in the larger size caused by the defocus and the primary spherical aberrations. The immediate effect of these aberrations is the more blurred reconstructed images of SIM. Moreover, the aberrations induced by the tilted coverslip change the period of the excitation pattern, and result in the non-uniform contrast, on the other hand, the PSF of the detection path is stretched and biased in the $x$-$y$ plane. Correspondingly, the reconstructed images of SIM are biased, and the contrasts are non-uniform, as shown in Figure 5I. In particular, as for the objective with a larger NA (e.g., $NA = 1.4$), the reduction of the coverslip thickness and the tilted case not only induce aberrations but also reduce the effective size of the pupil in the detection path.

In previous research, the aberrations on the pupil plane of the illumination path are investigated [28], however, the offset of the excitation beam with respect to the BFP of the objective, can also intensely affect the reconstructed images of SIM. In the optical system of the illumination path, the excitation pattern can be treated as the Fourier transform of two edge points on the pupil plane. As depicted in Figure 6A, one of the two edge points shifts toward the center point of the size-normalized pupil plane, $m$ represents the distance between the edge point and the center. Furthermore, the amplitude on the corresponding pupil function of the detection path is shown in

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**TABLE 1 | Parameters in the ideal case.**

| NA    | $n_{ij}$ | $n_{ij}$ | $n_{ij}$ | $z_i$ (µm) | $z_w$ (µm) |
|-------|----------|----------|----------|------------|------------|
| 0.95  | 1        | 1.515    | 1.38     | 0          | $-170$     |
| 1.3   | 1.518    | 1.515    | 1.38     | 0          | $-170$     |
| 1.33  | 1.53     | 1.515    | 1.38     | 0          | $-170$     |
| 1.35  | 1.406    | 1.518    | 1.38     | 0          | $-170$     |
| 1.4   | 1.518    | 1.518    | 1.38     | 0          | $-170$     |

The reconstructed images are shown in Figure 2I, which are blurred by the larger PSFs (Figure 2E), compared with the images in Figure 1E. In order to further detail the effects of the aberrations, the correlation coefficients of the reconstructed images are presented in Figure 2J. The simulated values of $n_2$ are set to be larger than the desired ones, otherwise, the light emitted from the sample cannot be collected by the objective effectively.

On the other hand, we investigated how the aberrations affect SIM images when the objective focuses deeper into the sample. As shown in Figures 3A,B, this case can be treated as the location shift of the coverslip along the optical axis. The $z$-coordinates of the lower and the upper surfaces ($z_l$ and $z_u$) of the coverslip change a value $a$, while the other parameters remain constant. A series of different $z_i$ are considered, and an example is given in Figures 3C–I ($z_i = -0.2$ µm). The pupil functions are shown in Figure 3C, specifically, when $NA = 1.4$, the value on the edge of the pupil function is complex due to the total internal reflection (TIR), which reduces the effective size of pupil (Figure 3J) and the effective NA. The decomposition of the pupil function (Figure 3D) shows that the main aberration modes are the piston (0th), defocus (4th), and primary spherical (12th). The aberrated PSFs and the corresponding profiles are shown in Figures 3E,F, which are larger than that in the ideal case. The excitation patterns and the local profiles are illustrated in Figures 3G,H, and as a result of TIR, the intensity of the excitation pattern for $NA = 1.4$ is lower than that in the ideal case. However, the image is well-reconstructed with satisfactory contrast, for the reason that the contrast of the excitation pattern is the same as the ideal ones. Similarly, the images of SIM and the corresponding correlation coefficients are shown in Figures 3I,K.

Similarly, the thickness change of the coverslip, which may also induce aberrations can be treated as the offset of $z$-coordinate of the upper surface, while the lower surface still locates at $z = 0$ (Figures 4A,B). For objective that $n_1$ is smaller than $n_2$, the thickness should not be thinner than the ideal value, otherwise, the light emitted from the sample cannot be collected by the objective effectively. In contrast, the thicker coverslip is not valid if $n_1$ is larger than $n_2$. To make the discussion complete, different thicknesses of the coverslip are considered, and Figures 4C–I is an example for $h = 170.8$ µm (above the black dashed line) and $h = 169.25$ µm (below the black dashed line), respectively. Figures 4J,K indicate that the offset of the thickness affects the objective for $NA = 0.95$ more critically, and the increase of thickness is more serious than the reduction of that. No visible effects are induced in objective for $NA = 1.4$ because the aberrations have little effect on the pupil function and the excitation pattern.
The aberrations induced by the deviation of the RI of the coverslip. (A,B) The RIs between the immersion medium and the coverslip mismatch for the illumination path and the detection path, respectively. (C) The pupil functions calculated from the case depicted in (B). (D) Zernike decomposition of the pupil functions shown in (C). (E) The PSFs on the plane $z = 0$, calculated from the corresponding pupil functions. (F) The profiles of the ideal (solid line) and biased (dashed line) PSFs in (E). (G) The excitation patterns affected by these biased RIs. (H) The local profiles of the corresponding excitation patterns shown in (G). The red dashed line (l) presents the biased case and the green solid line (l) presents the ideal case, respectively. The scope is $-0.5 \sim 0.5 \mu m$. (I) The corresponding reconstructed images of SIM. (J) The correlation coefficients of SIM images with different $n_2$ and NAs. The purple dashed line corresponds to $n_2 = 1.518$.

**Figure 6B.** Figures 6C–G is an example for $m = 0$, therefore, the PSFs (Figure 6C) distorted to more elliptical shapes. The excitation patterns and profiles are depicted in Figures 6E,F, in which the periods of the patterns show an intense difference from the ideal counterparts. The reconstructed images show that the images include a lot of ghost parts in higher NA objectives (Figure 6G). The correlation coefficients are calculated and plotted in Figure 6H. The quality of the images declines with the distance between the edge point and the center of the pupil plane increasing for all objectives.

The aberration modes we built include the biased working condition of the objective (as discussed above, the illumination path has a stable performance, however, the PSFs are expanded in the detection path, and the resolution of the reconstructed...
FIGURE 3 | The aberrations induced by the increase of the focal depth. (A,B) The case that objective focuses deeper into the sample medium. (C) The pupil functions calculated from the case depicted in (B). (D) Zernike decomposition of the pupil functions shown in (C). (E) The PSFs on the plane $z = 0$, calculated from the corresponding pupil functions. (F) The profiles of the ideal and biased PSFs in (E). (G) The excitation patterns affected by biased $z_l$. (H) The local profiles of the corresponding excitation patterns shown in (G), the scope is $-0.5 \sim 0.5 \mu m$. (I) The corresponding reconstructed images of SIM. (J) The effective pupil for $NA = 1.4$. (K) The correlation coefficients of SIM images with different $z_l$.

images is reduced) and the tilted coverslip, which induce the non-uniform contrast and the offset from the center of the reconstructed images. These modes are very beneficial to the analysis for the aberrations induced by the immersion medium and the coverslip, and have potential application in the adaptive optics for SIM. Additionally, the distance between the two edge points on the BFP of the objective is taken into account, which leads to a tremendous change of the excitation patterns from the ideal counterparts, and PSFs are just like being squished on the vertical direction, therefore, the reconstructed images include a lot of ghost parts. It’s necessary to comprehend these effects for further optimizing a SIM system, for example, if the reconstructed images contain ghost parts, the researchers can analyze the source of the damage by reference to the aberration mode of misaligned pupil. However, in practical experiments, the noise and background
intensity must be taken into consideration, which aggravates the quality of images more intensely. Moreover, with the increase of the imaging depth, not only do the aberrations increase, but also the influence of scattering and absorption should be paid more attention.

SUMMARY

In conclusion, we have built modes for the mismatched RIs, the increase of the focal depth, and the biased thickness of the coverslip, the tilted coverslip, and the misalignment of incident
FIGURE 5 | The diagrams of the illumination path and the detection path for a tilted coverslip, and the corresponding results for $\beta = 0.3^\circ$. (A,B) The tilted coverslip mode in the illumination path and the detection path. (C) The pupil functions calculated from the case depicted in (B). (D) Zernike decomposition of the pupil functions shown in (C), the first 15 orders of modes are used. (E) The PSFs on the plane $z = 0$, calculated with the pupil functions shown in (C). (F) The profiles of the ideal and biased PSFs in (E). (G) The excitation patterns affected by the aberrations. (H) The profiles of the excitation pattern shown in (G), the scope is 0 $\sim$ 1 $\mu$m. (I) The reconstruction images of SIM. (J) The effective pupil for NA = 1.4. (K) The correlation coefficients of the reconstructed images and the corresponding slope angle $\beta$. beams with respect to the BFP of the objective, respectively. In these modes, the excitation patterns are calculated based on the principle of two beams interference. In the first four modes, the pupil functions of the detection path are calculated using the ray tracing and are decomposed into the first 15th Zernike polynomials to obtain a quantified analysis, however, for the misalignment of incident beams, the pupil is not filled in the detection path. Consequently, the PSF of the detection path is distorted as a result of the corresponding pupil function, and combined with the excitation pattern, the reconstructed images
FIGURE 6 | Effects of the off-centered excitation beam. (A) The back focal plane (BFP) of the objectives. (B) The pupil function of the detection path. (C) PSFs on the plane $z = 0$, calculated from the pupil function in (B). (D) The profiles of the ideal and biased PSFs in (C). (E) The excitation patterns. (F) The local profiles of the corresponding excitation patterns shown in (E), the scope is $-0.5 \sim 0.5 \mu m$. (G) The reconstructed images of SIM, $m = 0$ for all objectives. (H) The correlation coefficients of the biased reconstructed images and the corresponding $m$. 
are affected at different levels in these cases. The quantified descriptions for these modes can assist in monitoring and compensating the aberrations by adaptive optics, and a more completed reference for the correction of the SIM systems can be obtained.

This model is beneficial for the estimation and the correction of the aberrations in SIM, giving a guideline to further improve the performance of the SIM microscopes. In addition, this model is generally applicable to the systems that use structured illumination, e.g., such as multi-beams interference illumination.

**DATA AVAILABILITY STATEMENT**

All datasets generated for this study are included in the article/supplementary material.

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**AUTHOR CONTRIBUTIONS**

XH conceived the idea. XiL, ST, and YX did the simulation. HS, WL, and QL gave the guide for analysis. XH, CK, and XuL supervised the project. All the authors contributed to the discussion on the results for this manuscript.

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**Conflict of Interest:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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