Spontaneous flow states in active nematics: A unified picture

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Abstract – Continuum hydrodynamic models of active liquid crystals have been used to describe dynamic self-organising systems such as bacterial swarms and cytoskeletal gels. A key prediction of such models is the existence of self-stabilising kink states that spontaneously generate fluid flow in quasi-one dimensional channels (Voituriez R. et al Europhys. Lett., 70 (2005) 404). Using simple stability arguments and numerical calculations we extend previous studies to give a complete characterisation of the phase space for both contractile and extensile particles (i.e. pullers and pushers) moving in a narrow channel as a function of their flow alignment properties and initial orientation. This gives a framework for unifying many of the results in the literature. We describe the response of the kink states to an imposed shear, and investigate how allowing the system to be polar modifies its dynamical behaviour.

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Suspensions of flagellate bacteria swim in quasi-turbulent swirls that suggest long-range collective ordering [1]. Cytoskeletal filaments and motor-proteins spontaneously form stars and spirals without any external guide [2]. These are just two examples of a class of self-organizing system that poses a novel challenge to physicists, as the ordering is intrinsically non-equilibrium in nature. The pattern formation is a dynamic phenomenon that relies on a continuous expenditure of energy by the individual particles as they actively generate forces on each other and/or the surrounding medium [3].

Convergent strands of research focused on modeling bacterial swarms [4–7] and on cytoskeletal dynamics [8–11] have suggested that the collective behaviour seen in both types of system can be described in the continuum limit by the same phenomenological, hydrodynamic model. This builds on the equations of liquid-crystal hydrodynamics, which capture the inherent directionality of the particles (e.g. bacteria, microtubules), and adds extra non-equilibrium terms to account for the activity. One of the most striking predictions of the active-liquid-crystal model has been that, under certain conditions, the uniform aligned state is unstable [4]; furthermore, when confined to a quasi-one dimensional slab geometry by flat interfaces (fig. 1) this instability can lead to the onset of a spontaneous steady flow [12,13]. Previous studies of the spontaneous flow transition in the active liquid crystal model using both analytic [12] and numerical [14–16] approaches have focused on illuminating only certain neighbourhoods of the complete phase space. To help map the phenomenological coefficients in the continuum theory onto microscopic parameters, and to aid in identifying their values for a given physical system, it is helpful to have a more complete picture of the effect of varying key coefficients. Therefore our aim in the letter is to extend and unify previous studies by carrying out a complete numerical exploration of the phase space formed by three of the most important physical characteristics of the system: the type and strength of the flow field...
generated by the individual particles, their flow alignment behaviour, and the initial orientation of the director field. We distinguish six spontaneous flow states, describe their response to an applied shear, and explain how they are modified in a system with polar symmetry.

We assume that, apart from their activity, the assembly of particles can be well approximated as nematic liquid crystal — that is, there is no difference between the two ends of an individual particle. The effect of relaxing this assumption by allowing the particles to be polar is discussed at the end of this letter. The hydrodynamics of nematic liquid crystals is well developed [17]. We adopt the Erickson-Leslie-Parodi approach [12], in which the nematic order parameter is a fixed-magnitude unit vector \( \mathbf{n} \) which evolves according to

\[
\partial_t \mathbf{n}_i + \mathbf{u} \cdot \nabla \mathbf{n}_i = \lambda D_{ij} n_j - \Omega_{ij} n_j + \Gamma h_i, \tag{1}
\]

where \( \mathbf{u} \) is the velocity field of the solvent; \( \lambda \) is the flow alignment parameter, more on which below; \( \Gamma \) is a rotational viscosity; \( h_i \) is the molecular field given by

\[
h_i = K \nabla^2 n_i \tag{2}
\]

(assuming only a single elastic constant \( K \)); and

\[
D_{ij} = \frac{1}{2} (\partial_i u_j + \partial_j u_i), \quad \Omega_{ij} = \frac{1}{2} (\partial_i u_j - \partial_j u_i). \tag{3}
\]

The first two terms on the right-hand side of eq. (1) describe alignment (or tumbling) of the director field by local shear flow. The third term accounts for the tendency of the ordered nematic to resist distortions, and arises ultimately from excluded-volume interactions between individual particles.

The flow field \( \mathbf{u} \) obeys the Navier-Stokes equation

\[
\rho (\partial_t + \mathbf{u} \cdot \nabla) \mathbf{u}_i = \partial_i (\sigma_{ij}^P) + \rho \mathbf{u}_i \cdot \nabla \mathbf{u}_i, \tag{4}
\]

where \( \rho \) is the fluid density and \( \eta \) is the viscosity. The passive part of the stress tensor \( \sigma_{ij}^P \) is

\[
\sigma_{ij}^P = -p \delta_{ij} - \frac{\lambda}{2} [n_i n_j + n_j n_i] + \frac{1}{2} [n_i n_j - n_j n_i], \tag{5}
\]

where \( p \) is the bulk pressure.

Equations (1)–(5) are generalised to describe active systems by introducing one or more terms \( \sigma_{ij}^a \) to the stress tensor, so that \( \sigma = \sigma^P + \sigma^a \). These active stresses account for the forces generated by the individual particles, as a function of the local director field, and cannot be derived from a free energy; however, their form can be arrived at from considering the symmetry of the flow field generated by the particles. It is commonly assumed that this flow field can be described to leading order as dipolar, and that higher-order contributions can be neglected, when considering far-field interactions and long time scales [4]. The appropriate active stress tensor for a suspension of force dipoles is

\[
\sigma_{ij}^a = -\zeta n_i n_j, \tag{6}
\]

where \( \zeta \) is the activity coefficient, the meaning of which is discussed below. One can also add active terms to the director equation of motion, eq. (1), to account for self-alignment effects [12], but as such terms do not play an important role in the spontaneous flow transition they are neglected here. For the same reason, we neglect active contributions to the isotropic pressure \( p \).

The two key parameters that characterise the individual particles are the activity parameter \( \zeta \) and the flow alignment parameter \( \lambda \). Both the magnitude and sign of each have an easily understood physical significance. The sign of \( \zeta \) determines whether the dipolar flow field generated by the particles is extensile \( \zeta > 0 \) or contractile \( \zeta < 0 \), as illustrated in fig. 2. In the swimmer literature, an alternative nomenclature is sometimes used, with extensile swimmers described as pushers and contractile swimmers as pullers. The magnitude of \( \zeta \) relates to the strength of the forcing, or equivalently the rate at which the particles expend energy.

The flow alignment parameter \( \lambda \) determines how the director field responds to a shear flow. A shear flow can be decomposed into an extensional and a rotational component, and the magnitude of \( \lambda \) determines their relative influence. For \( |\lambda| < 1 \), the rotational part of the flow always dominates regardless of the director orientation, and thus the director will continuously rotate under shear. This is the flow tumbling regime. In general, molecule-sized nematic liquid crystals are flow aligning and larger objects are flow tumbling, since for the extensional flow to dominate there must be enough Brownian rotational diffusion to wash out the rotational part of the flow. The sign of \( \lambda \) is also important, and relates to the shape of the individual particles. Rod-like objects have \( \lambda > 0 \); discoid objects have \( \lambda < 0 \); and \( \lambda = 0 \) corresponds to spheres.

The original analytic prediction of the spontaneous flow transition by Voituriez et al. [12] considered the
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Fig. 3: Stable states (in activity $\zeta$ vs. flow alignment parameter $\lambda$) for a one-dimensional slab of active nematic. Initial director orientation (a) parallel to the walls $\theta_0 = 0$, (b) perpendicular to the walls $\theta_0 = \pi/2$. In the shaded (unshaded) regions the initial state is unstable (stable) to small perturbations. The phase boundaries are given by eq. (7). The diagrams show the configuration of the director field $\vec{n}$ for the steady spontaneous flow state that arises in each unstable region. (c) Example flow fields $u_x(y)$ corresponding to the spontaneous flow states identified in (a) and (b). Parameters used are: for E1/C1, $\lambda = +1.5/-1.5$, $\zeta = +0.001/-0.001$, $\theta_0 = 0/\pi/2$; for E2/C2, $\lambda = +1.5/-1.5$, $\zeta = +0.001/-0.001$, $\theta_0 = 0/\pi/2$; and for E3/C3, $\lambda = 0/0$, $\zeta = +0.001/-0.001$, $\theta_0 = 0/\pi/2$. Other parameters are given in the text.

Equations (1)–(6) were solved, using a hybrid Lattice Boltzmann approach analogous to that described by Marenduzzo et al. [15], in the one-dimensional geometry of fig. 1. We follow Cates et al. [18] in using free boundary conditions for the director field ($\partial_y n_i = 0$ at the walls); the effect of fixed boundary conditions will be mentioned below. The following parameter values were used throughout: slab width $L = 100$, $K = 0.04$, $\eta = 1.27$, and $\Gamma = 0.2$ (all in simulation units). The director field was initially uniform and aligned at an angle $\theta_0$ to the walls. To break the symmetry we perturbed the uniform state by generating a small kink at the centre of the slab by rotating the director in the left half of the domain clockwise 0.1 radians and that in the right half the same amount anti-clockwise. The diagrams in fig. 3 show where the system was found to be stable (unshaded) and unstable (shaded) against the perturbation, for (a) $\theta_0 = 0$, and (b) $\theta_0 = \pi/2$. The critical value of the activity $\zeta_c$ corresponding to the phase boundary is determined analytically by linearizing the equations of motion around the initial state, and checking when a non-uniform solution exists, following Voituriez et al. [12]

$$
\zeta_c = \begin{cases} 
\frac{\pi^2 K(4\eta \Gamma + (\lambda - 1)^2)}{2L^2(\lambda - 1)}, & \text{for } \theta_0 = 0, \\
\frac{\pi^2 K(4\eta \Gamma + (\lambda + 1)^2)}{2L^2(\lambda + 1)}, & \text{for } \theta_0 = \frac{\pi}{2}.
\end{cases} 
$$

The director configurations in fig. 3 are typical numerical results obtained after the spontaneous flow state is reached in each of the unstable regions. There are six in total, three each for extensile (labeled E1, E2, E3) and contractile (C1, C2, C3) systems. In the previous work by Marenduzzo et al. [15,16], regions E1 and C3 were explored. The C2 state was predicted analytically...
perturb by increasing the director orientation slightly at
a single point, which stimulates the formation of at least
two kinks, one on either side of the perturbation. Thus the
effect state chosen by the system can depend strongly on
how the initial uniform state is perturbed. It is possible
to have the two different types of flow aligning kink (E1
and E2, or C1 and C2) coexisting in the same state, but
only if the state is specially prepared. Note that we restrict
the director to the $(x,y)$-plane, which does not allow for
twisted states, as were sometimes observed for high $|\frac{\sigma}{\kappa}|$
in [15].

Each of the states reacts differently to externally
imposed shear. For the tumbling states, E3 and C3, even
a small amount of imposed shear causes the director to
rotate continuously, and there is no steady state. Indeed
these states are only stable in the first place because they
spontaneously adopt a configuration which generates
no fluid flow, and thus no shear, outside the kink. In
contrast, the flow aligning states E1/C1 and E2/C2 can
survive in applied shear up to a certain magnitude. A
single kink of either type responds to applied shear by
moving towards the wall that is moving in the same
direction as the spontaneous flow. This is illustrated in
fig. 4 for an E1 kink. At some critical wall velocity, the
kink gets too close to the wall and becomes unstable; for
higher velocities, there is no steady kink state and the
velocity profile is standard linear shear flow.

Having catalogued this variety of states, it is important
to ask which we would predict to occur in specific physical
systems. Considering first swimming bacteria: they may be
either extensile or contractile, depending on their mode
of swimming, but most are certainly rod-like ($\lambda > 0$)
and furthermore should be flow tumbling ($|\lambda| < 1$) given their
relatively large size. Therefore, with reference to fig. 3,
one might expect to see states of type E3 for suspensions
of “pushers” (e.g. E. coli) or C3 for “pullers” (e.g. Chlamydomonas).
This is consistent with the experiments
and analytical predictions of Berke et al. [20] showing that
pushers tend to align parallel to walls, as seen in state E3,
while pullers align perpendicularly as in C3. Note however
that the existence of spontaneous flow in these states relies
on a non-zero elastic constant $K$; if $K \rightarrow 0$, the width of
the kink also goes to zero, and for the states E3 and
C3 the induced flow would vanish. Therefore attempts to
simulate suspensions of microswimmers must incorporate
liquid crystalline elasticity, for example via excluded-
volume interactions, to see steady flow-generating kinks
of this type. Previous simulations of large numbers of rod-
like swimmers in the literature [21,22] do not incorporate
excluded-volume interactions, and therefore would not be
expected to reproduce any such steady spontaneous flow
states. However, our predictions are consistent with the
instabilities of uniform aligned states observed in these
simulations. In particular, the enhancement of mixing by
pushers (extensile rods) but not by pullers (contractile rods)
[7,23] can be explained with reference to fig. 5. For
the value $\lambda = 1$ assumed by Saintillan et al. [22], an aligned

in Voituriez et al. [12] but has not yet been studied
numerically.

The six kink states are, for the geometry we consider,
related in pairs by a symmetry transformation. This
symmetry is apparent from an examination of the flow
profiles generated by each type of spontaneous flow state,
shown in fig. 3. Notice that the states naturally fall
into three pairs (E1/C1, E2/C2 and E3/C3), each with
the same type of flow profile, but director fields rotated by
$\pi/2$ radians with respect to each other. The states in each
pair have $\lambda$ and $\sigma$ values with the same magnitudes, but
opposite signs. This highlights the symmetry inherent in
the equations of motion: a change in sign of $\zeta$ is equivalent
to a change in sign of $\lambda$ together with a $\pi/2$ rotation of
the director field; an extensile rod-like particle interacts
with a flow field the same way as a contractile discoidal
particle rotated by $\pi/2$. Note that although this holds true
for the quasi-one dimensional geometry of interest, it is not
universally true; in particular the symmetry does not hold
in three dimensions.

The instabilities leading to each type of kink can
be understood from a simple pictorial model, extending
ideas from [19] (who consider the flow tumbling regime).
Figure 5 illustrates kink perturbations to the initial state
of the director field, $\theta_0 = 0$ on the left and $\theta_0 = \pi/2$ on
the right. The discontinuity in $\vec{n}$ at the centre of the
kink generates a force on the fluid due to the active term
in the stress tensor $\sigma^p$. The flow direction depends on
the sign of $\zeta$; in the figure, all kinks are drawn such
that the resulting flow is upwards. Because of the no-
slip condition at the walls, this central forcing necessarily
generates a region of uniform shear flow on either side of
the kink, illustrated by the fat vertical arrows. The wide
arrows overlaid on the director field show the effect of the
shear flow on the director in each case: depending on the
values of $\lambda$ and $\theta_0$, either the extensional flow dominates,
attempting to align the director at the Leslie angle (double
headed arrows) or the rotational flow dominates (curved
arrows) and causes the director to tumble. By reacting
to the shear flow, the director field either returns
to the initial aligned state and the induced shear flow
vanishes, or the perturbation grows until one of the stable
spontaneous flow states is reached. The same instability
mechanism applies in two dimensions, except that without
walls to restrict flow to one axis there will be no steady
spontaneous flow states. Instead, the instabilities drive
quasi-turbulent mixing flow [6,7].

2rotation of

The six stable kink states in fig. 3 are the fundamental
building blocks for more complicated states observed in
other numerical studies. For instance, if fixed boundary
conditions are used for the director field as in Marenduzzo
et al. [15], a half-kink is necessary at each wall. At higher
activities, striped states can be observed, which are simply
multiple kinks sitting side by side. We do not observe
striped states in our study, even at higher $|\zeta|$ values,
because our method for perturbing the initial state seeds
a single kink at the centre. In contrast, Marenduzzo et al.
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Fig. 4: Response of an E1-type kink to an applied shear, and the corresponding induced flow profile. The shear is generated by moving the right wall with a steady upwards velocity \( v_{\text{wall}} \). From left to right, \( v_{\text{wall}} = 0.005, 0.01, 0.02 \) in simulation units.

Fig. 5: Mechanism driving the (in)stability of an initially uniformly aligned state. Thin straight arrows show the director field, following a kink perturbation acting on a state with initial orientation \( \theta_0 = 0 \) (left) and \( \theta_0 = \pi/2 \) (right). Arrowheads pointing outwards (inwards) denote extensile (contractile). Wide vertical arrows show shear flow generated by the kink. Wide arrows superimposed on the director field show the influence of the shear flow upon it: either aligning (straight, double-headed arrows) or tumbling (curved arrows).

State of contractile rods is stable whereas one of extensile rods is unstable.

For solutions of cytoskeletal rods and molecular motors there is experimental evidence for the active stress being contractile [24], but it is not clear whether they should be treated as flow aligning or flow tumbling. Voituriez et al. [12] assumed the former, in which case the particles must be discoidal (\( \lambda < -1 \)) for spontaneous flow to occur, via states C1 or C2. If they are flow tumbling, then they could be expected to generate kinks of type C3. In either case, our results suggest that cytoskeletal components will tend to align roughly perpendicular to the walls, if the director is not otherwise pinned at the boundary.

The story changes significantly if the particles are allowed to be polar, having a preferred direction along which they will move. Polarity is accounted for in the model by including more active terms that are forbidden by symmetry in the nematic case [25]. At lowest order, these comprise an extra active contribution to the stress tensor \( a_{ij}^{\text{pol}} = \beta (\partial_i n_j + \partial_j n_i) \), and the replacement of \( \vec{u} \) in the director equation of motion (eq. (1)) with \( \vec{u} + \beta \vec{n} \) (for simplicity we assume that both these terms carry
the same polar activity coefficient \( \beta \), but in general they may be different). When \( \beta \) is allowed to be non-zero, the number of distinct kink states is doubled with respect to the nematic case (fig. 6) since each of the original kinks illustrated in fig. 3 now has two possible alignments. The nematic states for which the kink centre is parallel to the walls (E1, C2 and C3) each have “up” and “down” polar analogues; the nematic kinks with centres perpendicular to the walls (C1, E2 and E3) have “left” and “right” analogues. Numerical studies of the polar kinks show that only the “up/down” kinks remain stationary and persistent. The “left/right” kinks, by contrast, move in the direction they point until they reach a wall, and then vanish, leaving a uniformly aligned state with zero induced flow. Note that the symmetry between the three pairs of states E1/C1, E2/C2 and E3/C3 is broken by the introduction of polarity. The remaining stationary kinks can be further subdivided into two groups: those that point inwards (E1up, C2down and C3down), for which the sharpness of the peak in the induced velocity profile increases with \( \beta \), and those that point outwards (E1down, C2up and C3up) for which it decreases. If the local concentration of particles is allowed to vary, evolving via diffusion and self-advective, the particle concentration is enhanced at the centre of the kink and reduced at the walls for the inward kinks, but tends to build up at the walls for the outward kinks.

We have unified and extended previous studies of spontaneous flow in quasi-1D active nematics by numerically exploring the range of possible steady states as the activity, flow alignment characteristics and orientation are varied. We predict three qualitatively distinct types of spontaneous flow state, and examine how they respond to externally applied shear. We have also studied how the ensemble of stable states is affected when the active particles are made polar. Knowledge of the range of possible states should help match continuum and microscopic models of active materials and guide future experiments and simulations attempting to realize spontaneous fluid flow in narrow channels.

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