Strength Analysis of Vessel Ship Type PBL Conversion From Barge

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Abstract—One of the stages in evaluating ship design is the calculation of the strength of the ship's length. So we need a support tool that can speed up the calculation process. Therefore it is necessary to develop a program for calculation, as an alternative to evaluate the strength of the ship's length. Analysis of the strength of the length of the vessel to determine the strength of the length of the ship which is the result of conversion from the barge. Lengthening strength calculations using numerical methods with the help of the maxsurf study version program. Voltage price checks are carried out on three loading conditions, namely (1) empty load conditions, (2) FWT, FOT conditions, in conditions of 50% and (3) full load conditions (working conditions). The results of this study are in the form of a calculation of the longitudinal strength of the vessel in operation. The final output of this program is in the form of a latitude and mom style curve in the longitudinal direction of the ship. The results of the calculation of the strength of the longitudinal PBL vessel results from the shear force and moment. Shear force on loadcase 2, and 3 conditions in the parallel position of the middle body of the frame frame 25 longposes 58 and 60 meters in a row. Whereas in the 1 shear force loadcase at from 26 post length 58 meters. The maximum load case 1 moment is 7,605 × 10³ tonne meters. Loadcase 2 is 10.232 × 10³ tonne meters, while in loadcase 3 is 9,974 × 10³ tonne meters.

Keywords—longitudinal strength, software, shear force, momen, PBL ship

I. INTRODUCTION

Increasing the need for transportation equipment to transport various kinds of cargo from natural resources to logistics. Sea transportation is that the ship has advantages in terms of its huge load capacity. Especially in an archipelago country like Indonesia, the way to distribute various kinds of mutants such as logistics to various islands is none other than using ships. However, as well as land and air vehicles, marine vehicles also have the possibility of experiencing damage during their use. Therefore the need for transportation equipment in the form of ships increases as the number of requests continues to grow. Increasing the need for ships can be overcome by modifying existing vessels. Like the PBL vessel which is a modification of the barge. However, as a modified barge building has a disadvantage compared to a new vessel specific to PBL vessels, the shortage is the possibility of damage to the PBL ship itself due to various types of equipment above it. Therefore it is necessary to review the longitudinal strength, which in this case is affected by the distribution of the charge which is the internal pressure of the equipment PBL ship itself and the cargo on it. Especially when the ship PBL m eniliki exceeding 102.50 meters long it is necessary to check the power of longitudinal which are also present in the class rules. In this study will be discussed how to find out how much influence the internal load in the form of cargo and equipment and the load that occurs. In addition, a longitudinal strength analysis of PBL vessels which are converted from barges will also be carried out. PBL type ships are generally made using new pontoons in this case PBL ships are barges that are already unused. Looking at the case above, it is necessary to re-check the strength extending due to different loading conditions from the barges that become PBL ships. By analyzing the load that occurs due to the influence of the PBL ship load it can be known the minimum strength required. Moreover, the different burden of each ship that will do docking is also a consideration for the need to check the lengthening strength of the floating dock so that there will be no structural failure in the future. This study uses a numerical method with the help of a computer in the stress analysis experienced by the PBL vessel.

II. METHOD

2.1 PBL Ship

PBL ships are ships used to unload coal loads. Main dimension of PBL LPP ship 102.50 meters; breadth 19 meters; breadth max 25 meters; 6.70 meters depth. This PBL vessel is equipped with a conveyor system mounted on the left side of the ship along the ship. Next the PBL ship is also equipped with a mobile crane system located on the deck of the ship. Modeling is carried out with the help of a computerized system to obtain the PBL ship model.
The models that have already been obtained are processed in the software to produce longitudinal force calculation data. After ensuring that the model meets the model, it is used to analyze various variations of loading conditions. After all loading and boundary conditions have been applied to the model, the next step is to run the modeling and analyze the results of the modeling. The voltage at working conditions is less than the permit voltage and the voltage in the condition of an empty charge is smaller than the permit voltage. Even though in the submerged condition the resulting voltage does not meet the rules of the class, but the results are acceptable because these conditions only occur for a moment in the real floating dock condition does not exceed the yield of the material used [3].

2.2 Weight Component

There are two major components of ship’s weight; they are light weight and dead weight.

a. Light Weight
   Light weight measures the actual weight of the ship with no fuel, passengers, vehicles, water, etc. on board. The light weight distribution can be seen on the calculation.

b. Dead Weight
   Dead weight is the displacement at any loaded condition minus the light weight. It includes the crew, passengers, vehicles, fuel, water, and stores.

2.3 Weight Distribution, Loading, Shearing Force and Bending Moment

The Longitudinal distribution of weight is assessed by dividing the ship into large number of intervals. Several displacement intervals (groups) are used. The weight falling within each interval is assessed for each item or group in the schedule of weights and tabulated. Total for each interval divided by the length give mean weight per unit length. It is important that the center of gravity of the ship divided up in this way should be in the correct position. To ensure this, the centers of gravity of each individual item have been checked after it has been distributed.

2.4 Loading, Shearing Force and Bending Moment

Because the weight curve has been drawn parallel to the buoyancy curve, the difference between two, which represents the net loading p’ for each interval. It comprises a series of rectangular blocks. The loading curve is integrated to obtain the distribution of shearing force along the length of the ship. The integration is a simple cumulative addition starting from one end and the shearing force at the finishing end should, of course, be zero; in practice, due to the small inaccuracies of the preceding steps, it will probably have small value. This is usually corrected by canting the base line, i.e. applying a correction at each section in proportion to its distance from the starting point. The most forcw transverse is at first integral from load f(x)[1].

2.5 Longitudinal Strength Calculation

Longitudinal strength is a calculation of the strength of a ship seen in a long way to support the load and load of the ship. When the ship sails in calm or bumpy water conditions it will experience uneven loading. The calculation of Longitudinal strength is one classification requirement. The entry category for ships that have a length of more than 65 m ether. Dimension ship and scantling (plate size and profile) will affect the calculation results. Longitudinal strength will calculate the moment inertia of scantling. This is done to get the amount of stress and moment experienced by the ship due to load and wave loads. In this condition it is considered that the curvature of the ship’s gravity distribution and the curvature of the compressive force distribution upwards as long as the ship can meet the second equilibrium requirement, namely the center of gravity and the center point of the upward force is located on a vertical line (one work line).
Three boundary conditions are divided into two pieces placed on the back of the ship and one piece is placed on the front of the ship. The first point placed behind and on starboard with the degree of freedom locked (fixed) is the direction of x, y, and z to eliminate the three translations. Then the second point is placed parallel to the front point on the portside with a different x coordinate but the y and z coordinates remain the same. At this second point the degrees of freedom that are locked (fixed) are the direction of y and z to eliminate the rotation of z and y but there is still a rotation of the x axis. The last is the third point that is placed on the front of the ship at the centerline and the degree of freedom that is locked (fixed) is the direction y to eliminate the last rotation which is the rotation of the x axis [2].

Calculation of latitude and moment forces aims to calculate the maximum force and curvature moment that occurs on the ship. Latitude or shear force is the force generated by loading. Loading is a force that weighs on the structure of the ship's construction in this case the difference between ship weight distribution with force distribution press upwards. Moments are forces acting on objects that make the object rotate because of two forces or more. In other words the moment is the amount of force that works on objects at a certain distance [4].

Maximum Permissible Shear Force and Still Water Bending Moment. The values of maximum permissible Shear Force and Still Water Bending Moments for various frames are taken as follows:

**Table 1. Equilibrium PBL Ship Each Loadcase**

| Data                  | LOADCASE 1 | LOADCASE 2 | LOADCASE 3 |
|-----------------------|------------|------------|------------|
| Draft                  | 2.248      | 2.563      | 2.642      |
| Amidships m           | 3903       | 4530       | 4692       |
| Displacement t        | 0.9        | -0.3       | -0.3       |
| Heel deg              | 2.719      | 2.701      | 2.654      |
| Draft at FP m         | 1.777      | 2.424      | 2.631      |
| Draft at AP m         | 2.255      | 2.564      | 2.642      |
| Trim (+ve by stern) m | -0.942     | -0.276     | -0.023     |
| WL Length m           | 92.568     | 93.51      | 93.859     |
| Beam max extents on WL m | 26.643    | 26.64      | 26.64      |
| Wetted Area m²        | 2319.442   | 2392.233   | 2409.8     |
| Waterpl. Area m²      | 1994.572   | 2006.84    | 2007.712   |
| Prismatic coeff. (Cp) | 0.694      | 0.768      | 0.786      |
| Block coeff. (Cb)     | 0.569      | 0.658      | 0.684      |
| Max Sect. area coeff. (Cm) | 0.837   | 0.869      | 0.871      |
| Waterpl. area coeff. (Cwp) | 0.809 | 0.806      | 0.803      |
| LCB from zero pt. (+ve fwd) m | 55.018 | 52.703      | 51.952      |
| LCF from zero pt. (+ve fwd) m | 51.896 | 51.605      | 51.577      |

### III. Results and Discussion

In this study there were three loading conditions which were analyzed using numerical methods to obtain the main response in the form of longitudinal deformation and stress. The following are three variations of loading conditions used:

1) Load Case 1: is the loading condition where PBL ships being in an empty condition that is floating without any charge on it. The workload is only in the form of the weight of the PBL ship itself and buoyancy that works on PBL’s hull at 102.50 m. Is the safest loading or in other words not bad.

2) Load Case 2: is a loading condition where PBL ships are in a non-immersing condition, i.e all PBL hulls are submerged up to the deck and the only ones left are safety decks (working decks) of non-immersed wing tanks. The workload is the weight of the vessel PBL itself, the weight of tanks and buoyancy which works on PBL’s hull on a full 6.70 m. Is the worst burden.

3) Load Case 3:

is a loading condition where the PBL vessel is in working condition that is floating in the presence of a load above it. The working load is the weight of the PBL vessel itself, the weight of the tanks, and the buoyancy that works on PBL’s hull on 6.70 m laden. Is a load requested by the class society to be calculated with a certain maximum voltage limit.

2.5 Load Case 1

Based on a calculation analysis longitudinal strenght 1 loadcase result right moment 7.605 ton.m on longitudinal position 60 meters.
IV. CONCLUSION

Based on PBL ship loading modeling that has been carried out, it can be concluded as follows:

The maximum voltage experienced by PBL ships in all three loading conditions on loadcase 1 evenly distributed throughout the ship, loadcase 2 and 3 occur in the stern area of the ship. Strength extends from PBL ships can be seen in the results of shear forces and moments. Shear force on loadcase 2, and 3 conditions in the parallel position of the middle body of the frame frame 25 longposes 58 and 60 meters in a row. Whereas in the 1 shear force loadcase at fram 26 post length 58 meters. The maximum load case 1 moment is $7,605 \times 10^3$ tonne meters. Loadcase 2 is $10.232 \times 10^3$ tonne meter, while at loadcase 3 is $9.974 \times 10^3$ tonne meter.

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REFERENCES

[1] A. Ben and E. T. Diego, “Analytical and Numerical Determination of The Hull Girder Deflection of Inland Navigation Vessels,” Master Thesis: Polytechnic University of Cartagena, Cartagena, 2015
[2] B. Santosa, “Diktat Kekuatan Kapal,” Institut Teknologi Sepuluh Nopember, Surabaya, 2013.
[3] Pramono, D.R. et.al. AnalisaKekuatanMemanjang Floating Dock Konversi Dari Tongkang denganMetodeElemenHingga. JURNAL TEKNIK ITS Vol. 5, No. 2, ISSN: 2337-3539 (2301-9271 Prat) Hal. G148-152(2016).
[4] Sitepu, G. Perangkat Lunak Perhitungan Kekuatan Longitudinal Kapal. Prosiding Volume 5. ISBN: 978-979-127255-0-6. Group Perkapalan Hal. TPG 1-8 Desember 2011.