Recent Advances and Challenges of Nanomaterials-Based Hydrogen Sensors

Bei Wang 1,2,* , Ling Sun 3, Martin Schneider-Ramelow 2,4, Klaus-Dieter Lang 2,4 and Ha-Duong Ngo 1,2,*

Abstract: Safety is a crucial issue in hydrogen energy applications due to the unique properties of hydrogen. Accordingly, a suitable hydrogen sensor for leakage detection must have at least high sensitivity and selectivity, rapid response/recovery, low power consumption and stable functionality, which requires further improvements on the available hydrogen sensors. In recent years, the mature development of nanomaterials engineering technologies, which facilitate the synthesis and modification of various materials, has opened up many possibilities for improving hydrogen sensing performance. Current research of hydrogen detection sensors based on both conservational and innovative materials are introduced in this review. This work mainly focuses on three material categories, i.e., transition metals, metal oxide semiconductors, and graphene and its derivatives. Different hydrogen sensing mechanisms, such as resistive, capacitive, optical and surface acoustic wave-based sensors, are also presented, and their sensing performances and influence based on different nanostructures and material combinations are compared and discussed, respectively. This review is concluded with a brief outlook and future development trends.

Keywords: hydrogen safety; hydrogen sensor; transition metals; catalytic sensing; micro and nanosensors; metal oxide semiconductors; graphene; graphene oxide; reduced graphene oxide

1. Introduction

Climate change has called people to action to create a more sustainable future. Lower CO₂ emissions have become a global target in coming decades. Applying renewable clean energies, such as wind, solar, hydropower, biomass, and hydrogen, is the first step towards carbon neutrality in line with the target agreed under the Paris Agreement in the United Nations Framework Convention on Climate Change (UNFCCC) in 2015 [1]. As one of the clean and renewable energies, the combustion of hydrogen (H₂) emits power, heat, and water, making H₂ the most promising energy carrier for our future. Moreover, in comparison with electric vehicles, hydrogen fuel cells present an enhanced driving range with the most extended range currently >300 m [2]. The energy transfer and consumption processes avoid CO₂ emissions.

Hydrogen is the lightest element in the periodic table. At room temperature, hydrogen shows the form as a gas, dihydrogen, formula H₂. It is colourless, odourless, tasteless, and combustible. The flammability property of hydrogen is the main concern about its safety. It has a wide range of flammability limits (the mixture of hydrogen and air are approximately from 4% to 77%), very low ignition energy (the ignition energy of the mixture of 23 vol% hydrogen and air is 0.017 mJ, which is only 1/10 of the other gasoline-air mixtures) [3]. The flame propagation speed can even reach a subsonic velocity (975 m/s for a 29.6 vol% H₂ in air mixture) [3]. Furthermore, hydrogen flame is nearly invisible.
Hydrogen combusts very rapidly in oxygen and air and can cause sudden explosions. In hydrogen storage applications, the interaction of hydrogen and the material directly in contact can also cause embrittlement and mechanical degradation in the containment material, which leads to hydrogen spills or leaks [4]. According to the published report of the U.S. National Renewable Energy Laboratory (NREL), for the on-board safety of fuel cells vehicles, hydrogen sensor should have the ability to respond to 1 vol% of H\textsubscript{2} within 1 s, and to achieve the lowest detection limit of 0.1 vol% of hydrogen operating in the range of temperature from −40 °C to +40 °C and relative humidity within 5% to 95% [5]. The US Department of Energy (DOE) has also published specific technical targets for hydrogen safety sensors, in terms of the measurement range (0.1–10%), operating temperature (−30–80 °C), the response time (less than 1 s), accuracy (5% of full scale), gas environment (ambient air, 10–98% relative humidity range), lifetime (10 years) and interference resistance (e.g., hydrogens) [6,7].

Therefore, future research and developments of very accurate and fast hydrogen sensors will play a crucial role in hydrogen safety. Studies in [3,4] proposed several criteria in consideration of hydrogen sensors, including response time, detection range, signal accuracy, recovery time, low cost and low power consumption, sensitivity to the environment, and so on. Regarding the efficiency of hydrogen leak detection, the gas response was mainly defined as the ratio of the electrical resistance variation in detection gas (R\textsubscript{g}) to that in the air (R\textsubscript{a}):

\[
\text{Response (\%)} = \frac{|R\textsubscript{a} - R\textsubscript{g}|}{R\textsubscript{a}} \times 100\%
\]

The sensor response time was defined as the needed time for the sensor to reach 90% signal maximum of hydrogen in the sensor environment. Together with the response time, the recovery time means the time needed to lower the signal maximum of 90%. The lower the concentration of hydrogen that a device can detect, the better it is at preventing a potential explosion.

Detection of hydrogen correlates directly to the interaction of the hydrogen with a selected sensing material. These interaction effects can be catalytic-based, thermal conductivity-based, electrical and electrochemical-based, mechanical-based, optical-based, and even acoustic-based [4]. Among them, transition metals, such as palladium (Pd) and platinum (Pt)-based materials, have been favoured and are still undergoing more in depth research due to their high sensitivity to hydrogen [8,9]. The transition metal Pd in particular has a high-affinity property with hydrogen even at room temperature, making it the most promising hydrogen detection sensor. Another kind of sensing material is the metal oxide semiconductor (MOS), such as SnO\textsubscript{2}, TiO\textsubscript{2}, and ZnO. However, most metal oxide semiconductors exhibit gas sensing performance at elevated temperatures in the range of up to 500 °C [10], due to the energy barriers for electron mobility caused by their bandgaps. Materials like graphene, graphene-oxide, and reduced graphene-oxide have been introduced to gas sensing to enhance the sensing performance because of their mechanical and chemical advantages. Many researchers investigated sensing materials by modifying their forms, sizes, and combinations, developed innovative structures and synthesis methods to improve the sensor response, sensitivity, and selectivity on the one hand, and to reduce the energy consumption and production cost on the other hand.

This work is divided into three parts. The first part mainly addresses sensing properties of transition metals, like Pd, in different forms in detection applications, including the operating theories, properties, current research, and their performances. The second part focuses on the hydrogen sensors based on metal oxide semiconductors (MOS) involving the bandgaps changes in n-type and p-type MOS during the hydrogen absorption/desorption processes and their performances when applied in hydrogen detection will be discussed. In the third part, we share insights into the applications of graphene and its derivatives-based hydrogen sensors. More interesting research will be explained and compared with performances and reliability.
We hope this work can give our readers an up-to-date overview of promising hydrogen sensors and offer some insights for future work in this area.

2. Palladium-Based Hydrogen Gas Sensors

Palladium has been one of the most promising materials for gas sensing for decades. Due to its high hydrogen affinity and catalytic properties, Pd has been widely used as thin films or nanoparticles for hydrogen leak detection or hydrogen storage. This absorption process leads to lattice/volume expansion and resistance increase during hydrogen diffusion [11,12]. Moreover, Pd’s high state density at the Fermi level makes hydrogen absorption occur even at room temperature reversibly [13].

Hydrogen molecules (H₂) dissociates into hydrogen (H) atoms during hydrogen absorption, and the H atoms diffuse into palladium, occupying the interstitial sites of the Pd lattice as shown in Figure 1a. Most metals require energy input, such as high pressure or elevated temperature, to overcome an active barrier by hydrogen absorption. On Pd surfaces, the dissociative adsorption of H₂ molecules occurs with little or no activation energy barrier, as shown in Figure 1b [14–17]. Behind this catalytic activity is a bond alternation mechanism in which the dangling bond of the Pd surface plays an essential role [14,18]. Because of the lower kinetic energy of the surface, the dissociated H atoms are distributed and bonded with the Pd surface rapidly. As the surface reaches its saturation status, the H atoms slowly begin the penetration process into the Pd bulk, during its higher kinetic energy inside the lattices. In Figure 1b, the tetrahedral sites have higher kinetic energy (≈0.097 eV) than the sites on the surface (≈0.44 eV), and the diffusion to the octahedral sites (≈0.092 eV) needs even more energy. The transition state (TS) in Figure 1b can be found by applying the complete linear synchronous transit/quadratic synchronous transit method [19] during the hydrogen diffusion process [17].

![Figure 1](image)

**Figure 1.** (a) Illustration of hydrogen adsorption in Pd (100) [16]; (b) diagram of the potential energy profile of hydrogen-absorption [17]. Copyright (2017), with permission from American Chemical Society.

Palladium that absorbs dissociated H atoms forms a metal–hydrogen system, which can be labelled as palladium hydride PdHₓ. The absorption can be described in the following forms:

\[
H_2 \rightarrow 2H \tag{2}
\]

\[
Pd + xH \rightarrow PdH_x \tag{3}
\]

Here x is hydrogen content. In many works, the hydrogen adsorption process is modelled as a kinetic process [11–14,20–23]. During this process, different phases can appear, coexist and transform from one to another at variant pressure P, temperature T, where the hydrogen composition x, i.e., H/Pd, changes consequently. Figure 2 shows such a pressure–composition–temperature (P–C–T) diagram [24,25]. When x is small, Pd and H atoms form an unsaturated solid solution, and the state of the Pd-Hₓ system reaches
α-phase like in Figure 2 (PdH$_{0.015}$ lattice constant = 0.3894 nm@298 K). Increasing the content of hydrogen $x$ up to about the $x \approx 0.7$, the PdH$_x$ presents a saturation status β-phase (PdH$_{0.607}$: lattice constant = 0.4025@298 K) solid solution, which leads to the lattice expanded [20,21]. When $x$ is in between, the Pd-H system state is in the region of the coexisting region. This region is unstable and nd it is not clear where the system will go at the next moment, either converging towards the α-phase or evolving towards the β-phase at the next moment. As shown in Figure 2, the coexisting region of two phases (α- and β-phase) covers a wide H$_2$ composition range, from about 0.01 to 0.62, while the kinetic energy in the environment (mainly, the pressure and the temperature) varies [24,26]. In the saturated state, the octahedral site of the Pd is fully filled with hydrogen atoms. This saturation can introduce about 10.9% volume expansion of the Pd material; thus, it is undesirable for the material to reach the β-phase. In a worst-case scenario, for instance, for the Pd films, the tensile stress consequently leads to the failure of sensing devices [27,28]. Additionally, previous works [28–30] have observed that some hysteretic behaviour in the resistance caused irreversible structural changes in Pd bulk and Pd films, which can lead to sensing stability problems.

![Figure 2](image_url)  
**Figure 2.** H$_2$ pressure–composition–temperature (P–C–T) phase diagram of the Pd-H system [22,23]. Copyright (2019), with permission from Chemistry Europe.

Available work went beyond the surface of the Pd material to determine how the thickness affects sensing performance. In [26], Lee et al. have examined Pd thin films’ sensitivity of variant thickness, from 5 nm to 400 nm. The results in Figure 3 show a sensitivity curve during the process of hydrogen absorption (red curve, from the bottom going towards higher H$_2$ concentration until there is a quick increase of sensitivity), and the process of hydrogen desorption (blue curve, from the most upper right side, going towards lower H$_2$ concentration until there is a sharp decrease of the sensitivity in the end). The cycle formed around the area of α- and β-phases also called hysteretic behaviour. During the interacting process of hydrogen and Pd, free electrons from hydrogen can move through and thus affect the electrical resistance within the thin film. Let $t$ be the thickness of a Pd film. As Figure 3b shows, by 5 nm thickness, the process of hydrogen absorption and desorption forms a relatively flat curve at a quite low sensitivity level. Each curve with $t$ between 20 nm and 400 nm shows a hysteretic behaviour covering a lower and an upper sensitivity range, with H$_2$ concentration ranging from 0.25% to 1.75%. Observation of these curves indicates that the range of sensitivity that can be covered increases when $t$
increases from 20 nm to 150 nm. The highest sensitivity level that a Pd thin film can reach also increases when the thickness of the film increases. These curves reach the highest sensitivity value at 150 nm, where a larger $t$ does not result in a better sensitivity level. This saturation of sensitivity can be attributed to the limited depth to which the hydrogen atoms can penetrate Pd material. This limited penetration depth also means that the phase transition occurs mainly near the surface region of the Pd thin film. However, the low sensitivity level of the 5 nm-thick films indicates that the too-small thickness can restrain the capacity of the absorption of hydrogen atoms and the Pd lattice expansion.

The response time of a hydrogen sensor is employed to describe the penetration/diffusion process of the dissociated hydrogen atoms from the surface into the sensing materials. Due to the penetration process of hydrogen atoms, hydrogen sensors based on Pd thin-film suffer from slow response and poor stability for sensing performance [31]. Instead of pure Pd, much of the literature studied palladium alloy and bilayers like Pd/Ag [32], Pd/Ni [33], Pd/Au [34], Pd/Mg [35] and Pd/ZnO [36] for faster responses or better durability.

The hydrogen diffusion rate correlates with the temperature significantly. This relation [37] is defined by diffusion coefficient $D$ as:

$$D = D_0 \exp\left(-\frac{Q}{RT}\right)$$

where $D_0$ is the diffusion constant, $Q$ is the diffusion activation energy, $R$ is the ideal gas constant and $T$ the temperature.

With Fick’s 2nd law for the case of three-dimensional diffusion, the process can be written as:

$$\frac{\partial \rho}{\partial t} = \nabla \cdot (D \nabla \rho)$$

where $\rho$ is the density of hydrogen atoms.

Liu et al. in [37] investigated the temperature dependence of Pd-based thin film, and developed a hydrogen sensor based on sputtered Pd/Ni alloy thin film with a Pt heating resistor as shown in Figure 4a. This sensor had significantly improved response and recovery time at 75 °C in comparison with the sensor based on the exact sensing mechanism [38]. Furthermore, Liu discussed the effect of different temperatures on the Pd/Ni film. At room temperature, the oxygen atoms of the environment at the grain boundary increased the resistance of the alloy film without hydrogen. When the hydrogen atoms diffused inside the film, they reacted with oxygen to form water, which removed oxygen from the film surface and caused a resistance decrease of the Pd/Ni film. The oxygen atoms were driven to leave the grain boundary by raising the working temperature, and more hydrogen atoms.

Figure 3. Hysteresis curve of sensitivity during the process of absorption and desorption of hydrogen from 0 to 2% concentration (a) for the Pd thin film with the thickness of 100 nm and (b) for the Pd thin film with thicknesses ranging from 5 to 400 nm [26]. RT means room temperature. Copyright (2010), with permission from Elsevier.
could permeate deeper into the film. This process built additional electrical pathways by filling hydrogen atoms in more lattice vacancies, thus increasing electrical conductivity and decreasing resistance in a reverse way. As the temperature rises to a specific value, like 100 °C, some absorbed hydrogen atoms on the surface are oxidized, which weakens the penetration process and leads to the sinking of the sensing response (1.85% decrease at 100 °C).

Interestingly, at 75 °C, the Pd/Ni film was reported with optimized sensing properties, such as better linearity than at 25 °C. Additionally, at a higher operating temperature, the hydrogen absorption and desorption processes rarely present hysteresis, as shown in Figure 4b, because the heating process accelerated diffusion and release of hydrogen atoms in absorption and desorption processes. On the other hand, the high operation temperature also has disadvantages. It can cause high power consumption and increase the noise signal, further limiting the performance and stability of applying Pd-film-based sensors.

By contrast with the use of the electrical resistive principle, some researchers investigated sensors by applying the surface acoustic wave (SAW) [33,39] and optical reflection principles [40,41] to improve the sensor performance at room temperature. Wang et al. in [33] developed a Pd–Ni alloy thin film-coated SAW hydrogen detection sensor with high stability. In their study, the Pd–Ni thin-film was deposited by applying an RF magnetron co-sputtering from separate Pd and Ni targets onto a SAW propagation path for sensing, and the response time of the 40 nm Pd–Ni alloy-thin-film can approach less than 10 s at room temperature. Moreover, their experiments also indicated a trade-off effect between film thickness and diffusion velocity of hydrogen atoms. As the thickness of the film increased, the diffusion of dissociated hydrogen slowed down with higher sensitivity. Another highlight of the study is the long-term stability. The sensor has been reported to have a half-year detection error of about 3.7%, which can be explained by the fact that Ni doping in Pd helps to suppress the lattice destruction in gas adsorption. In comparison to SAW sensing mechanism, sensors based on sputter-deposited Pd–Y alloy film in [40] use reflected optical signal intensity in hydrogen detection. As Song et al. reported [40], the sensor has a fast response/recovery time and sensitive signal value in hydrogen concentration ranging from 0.1% to 2% after the annealing process.

As a summary in this part, the Pd thin-film based or Pd alloy-based thin film-based hydrogen sensors could have high sensitivity due to their large contact surface. However, the thickness increase of the thin film slows down the hydrogen diffusion velocity, thus weakening the sensor performance, especially for the sensors using an electrical sensing
mechanism. Another disadvantage is of the Pd thin film is the lattice expansion. For high H₂ concentrations (more than 2%), the Pd lattice expansion leads to the Pd film buckling or collapsing, making the sensor unstable, irreversible, and unreliable. In order to improve the sensor performance accordingly, an external heater can be employed to accelerate the diffusion process. Moreover, the SAW-based and optical sensing mechanism-based sensor can also be used to enhance the sensing response of the sensors.

To better meet the requirements of high sensitivity, rapid response, and reliable performance, another small form of Pd has been investigated for decades by many researchers [42–48], the Pd nanoparticles. Due to its unique physical and chemical properties, drastic changes can be observed during the hydriding process using Pd nanoparticles, such as the H₂ pressure-composition phase diagram [42–44], hysteresis [42,49,50], vibrational density of states [45,46], structures [47,48], and so on.

It is well known that significant lattice distortions accompany the hydrogen absorption and desorption [51,52], which essentially affects the reliability and performance of devices in applications like hydrogen sensing, and hydrogen storage. Due to their thermodynamic dependence on sizes [53], palladium nanoparticles have a coherent phase transformation process during the hydrogen absorption and desorption below the critical temperature Tc [50,54]. In that transformation, the variation in hydrogen concentration leads to a modulation of the host lattice accompanying coherency stress and elastic energy contributions to the enthalpy, as shown in Figure 5a,d. The pressure-composition isotherms of coherent transformation show a significant pressure difference between absorption and desorption processes, forming a large hysteresis phenomenon.

![Figure 5. Schematic pressure-composition isotherms at temperatures above, equal and below the critical temperature Tc. The upper spinodal pressure Pₜₚ and the lower spinodal pressure Pₚₜ, together with the corresponding concentration Xₜₚ and Xₚₜ, are indicated for the gold isotherm with the red arrow.](image-url)

According to Schwarz and Khachaturyan [56,57], the hysteresis is comparable to full-spinodal hysteresis. The black line corresponds to the critical isotherm at T = Tc and the red line to a supercritical isotherm at T > Tc. [50]. Copyright (2016), with permission from Nature Publisher Group.
By contrast, the absorption and desorption in bulk palladium or larger particles are consistent with incoherent phase transformation. The dilute α-phase and the concentrated β-phase coexist at thermodynamic equilibrium with the dislocation of lattices, which leads to minimizing elastic stress and more negligible hysteresis, as illustrated in Figure 5b,c.

Several Pd-based hydrogen sensors applying micro- and nano-sensing structures have been investigated in the literature, such as Pd/Y [32], Pd/ZnO [39], Pd [58,59], Pd/TiO₂ [60], Pd/Ni [61] and Pd/SnSe [61]. As synthesis methods, the direct current (DC)- or radio frequency (RF)-sputtering methods have been used to fabricate thin-film structures for both electrical resistive [58,60,61] and SAW sensors [33]. Sensing structures based on nanowires and nanoparticles were synthesized mainly with deposition methods [39,61–82].

Hu et al. in [58] developed an innovative processing method to improve sensing properties through a new nanoporous-structure of Pd thin film for H₂ sensing applications with a specific surface-volume ratio. In their work, a nanoporous structural Pd thin film was achieved through DC sputtering and followed by annealed process under vacuum conditions. Specifically, the porous structure was formed by the competition between the melting of ultrathin Pd film and the surface tension effect during the annealing process. With the optimized annealing temperature of 300 °C, the Pd film exhibited significant sensing properties, with a response time of ~25 s, and a recovery time of about 10 s due to the sizeable reactive surface of the porous structure. The sensor had a wide concentration range of 0.04–1.6%. Additionally, as Figure 6 shows, the sensor exhibits good repeatability, and its sensitivity towards hydrogen was about 6–10 times higher than other reductive gases, like CO, NH₃, CH₃OH., at room temperature.

Figure 6. The hydrogen response of nanoporous Pd film sensors at room temperature. (a) The transient response to various concentrations of H₂ in the air; (b) the H₂ concentration-dependent response time and sensitivity; (c) repeatability; (d) selectivity [58]. Copyright (2016), with permission from Elsevier.
Liu et al. integrated a Pt micro coplanar hotplate beside a suspended Pd-film sensing layer to control the sensor’s temperature [59]. At low temperatures, e.g., 50 °C, with a low power consumption of about 7.5 mW, the suspended sensor had a response time of about 30 s, and the recovery time was 17 s for 4000 ppm H₂ concentration and sensitivity of 0.2%. As the power consumption of the Pt micro heater was increased to 65 mW, the working temperature rose to 400 °C, accordingly. This results in a significantly improved sensor response, with a more rapid response/recovery time of 10 s /15 s, a higher sensitivity of 4%, and better selectivity towards hydrogen at the same H₂ concentration. As mentioned by Liu et al., the reaction mechanism of Pd films at high temperatures is different from that at room temperature. Firstly, Pd reacts with oxygen to form PdO on the surface rather than absorbing oxygen. Once the hydrogen gas is released in the test environment, Pd is reduced from PdO by reaction with H₂. Secondly, due to the presence of PdO, the reduction reaction between hydrogen and PdO leads to a significant drop in sensor resistance, and the reaction of PdO with hydrogen produces a negative sensitivity signal, as shown in Figure 7.

Figure 7. (a) Microscope image of a hydrogen sensor sample. (b) Responses of different H₂ concentrations at 400 °C, and (c) responses of the sensor to various gases (4000 ppm) at 400 °C [59]. Copyright (2019), with permission from Elsevier.

Mao et al. [60] investigated a hydrogen gas sensor based on nanoporous palladium and titanium dioxide (TiO₂) composite film. At the interface of the Pd and TiO₂ layers, both Pd hydride and migrated H atoms react with the adsorbed oxygen on the TiO₂ surface while injecting electrons into the TiO₂. The reactions between migrated H atoms and the adsorbed oxygen can be described with Equations (6) and (7):

\[
PdH_x + \frac{x}{2}O^{\text{ads}} \rightarrow Pd + \frac{x}{2}H_2O + \frac{x}{2}e^- \tag{6}
\]

\[
O^{\text{ads}} + 2H \rightarrow H_2O + e^- \tag{7}
\]

The Pd hydride process leads to an increase in resistance on the one hand, while the reaction mechanism of TiO₂ leads to a decrease in resistance on the other. Therefore, tuning the thickness of the TiO₂ layer can adjust the sensing performance. As reported by Mao et al. in [60], the best performance was achieved with a 10 nm thickness of TiO₂. At 0.4% H₂ concentration, the recovery time of the gas sensor was 8 s, which was faster than 13 s at 0.8% H₂ concentration.

Wang et al. in [33] investigated surface acoustic wave (SAW) devices based on Pd–Ni alloy thin films due to their fast response, low cost, satisfactory stability and remarkable sensitivity when used for hydrogen sensing. As reported in [33], the operation frequency of the devices decreases with the increasing thickness of the Pd–Ni film due to the mass loading effect. Furthermore, as shown in Figure 8, the enhanced acoustoelectric coupling effect in the thicker films raises the wave attenuation as the thickness of the Pd–Ni film increases. Increasing the thickness of the Pd–Ni film can slow down the diffusion velocity, leading to a slower response, but it can also adsorb more gas molecules, and therefore a higher sensitivity can be expected. The highest sensor response observed with a 300 nm thick Pd–Ni film-coated device was about 8.7 kHz. The fastest response was obtained with
a 40 nm film with a relatively fast sensor response (2.75 kHz to 0.1% hydrogen) of ~7 s. As shown in Figure 8, the SAW-based gas sensor possesses significant working stability with a detection error of ~3.7% for six months and selectivity of 0.1%. Viespe et al. developed a SAW gas sensor by employing a Pd/ZnO bilayer for hydrogen sensing applications at room temperature [39]. The sensitive layers were deposited onto ST-X quartz substrates by pulsed laser deposition (PLD). The high laser deposition pressures enabled the sensing film to have a large porosity and a big surface area. As a result, the sensor has a fast response of 16 s at room temperature and a detection range from 2000 ppm to 20,000 ppm.

Figure 8. (a) Measured frequency responses of the proposed sensing device depending on the Pd–Ni thin-film thickness, inset: picture of the prepared sensing device; (b) measured sensor responses relating to the 40 nm Pd–Ni alloy thin-film coated sensing device to various hydrogen gas concentrations; (c) selectivity testing of the proposed Pd–Ni alloy thin-film coated sensing device [39]. Copyright (2017), with permission from MDPI.

Xu et al. investigated hydrogen gas sensors with two-dimensional (2D) layered tin monoselenide (SnSe) ultrathin films deposited on SiO2/Si substrate, which were decorated with a 15 nm-thick Pd layer on the surface [61]. The SnSe combination belongs to the IV–VI family and forms heterojunctions with enhanced electrical transporting characteristics at the interface. Figure 9 shows a typical I–V curve for the heterojunction of the sensor experimentally. The heterojunction exhibits an apparent rectifying behaviour with a large rectification ratio, indicating the formation of a high-energy barrier near the interface of the heterojunction. When H2 is released into a test environment filled with pure N2, the response (S) of the device is defined by the following equation:

\[
S = \frac{I_H}{I_N}
\]

where \(I_H\) and \(I_N\) are the currents under the H2 and N2 atmospheres. According to the calculation in the paper [62], the fabricated Pd decorated with SnSe/SiO2/Si heterojunction shows an ultra-high response to H2 at room temperature. Its response at 1 V is ~3225 with an ultra-low detection limit of 0.91 ppb, which was calculated using the equation in [60]:

\[
LD = \frac{3\sigma_{\text{noise}}}{s}
\]

where \(LD\) is the detection limit, \(\sigma_{\text{noise}}\) is the root mean square of noise, and the denominator \(s\) is the slope of the response versus concentration plot.
Figure 9. (a) The I–V curve of a SnSe/SiO₂/Si heterojunction. The inset shows a schematic illustration of the measurements. (b) Schematic illustration of the sensing behaviour of the Pd-decorated SnSe/SiO₂/Si heterojunction towards H₂. (c) The consecutive dynamic response of the heterojunction upon exposure to the above concentrations of H₂. The inset shows the dependence of the response on the H₂ concentration. (d) The sensor’s response to pure N₂, O₂, ethanol and acetone, 10,000 ppm NH₃, 80% relative humidity (RH) (H₂O) and 1000 ppm H₂ [61]. Copyright (2021), with permission from Elsevier.

As shown in Figure 9, the heterojunction responses to N₂, O₂, NH₃, humidity, ethanol and acetone are approximately 1.02, 1.11, 1.21, 1.01, 1.30 and 1.07, respectively, which are much lower than the heterojunction’s response towards H₂ (~3225). This quick response shows that the heterojunction exhibits good selectivity for H₂.

Despite having several advantages mentioned above, Pd-based thin-film hydrogen sensors also have their disadvantages. For example, the hydrogen embrittlement susceptibility caused by lattice expansion of PdHₓ intermediates may cause Pd membrane cracking [62]. As well as an irreversible structure, changes after several sensing cycles induced by multiple α-β phase transitions of the PdHₓ intermediates can cause mechanical stresses on the resistors, which in return can lead to deformation, delamination, and a reduction in sensing durability [38,63].

Many researchers have attached significance to Pd- and its composites-based nanowires and nanoparticles [64–93]. These materials have unique physical and chemical properties. Compared to the thin sensing films, these nanowires and nanoparticles have a larger surface–volume ratio, more enhanced sensitivity, lower power consumption, faster sensing response and better durability. The ratio of length to diameter is defined as the aspect ratio. The nanostructures with aspect ratios less than 10 are called nanorods (NRs), the aspect ratios more than 10 are called nanowires (NWs), and additionally, hollow NWs are called nanotubes (NTs).

Du et al. investigated PdCo NW sensors for hydrogen gas sensing over a wide range of temperatures [64]. As shown in Figure 10, the PdCo NW (diameter 60 nm) was fabricated by electrodeposition within an anode aluminium oxide (AAO) nanochannel and further integrated on the test interdigital electrodes (IDE). The sensing performance and stability can be modified by tuning the cobalt Co dopant content. Compared with different Co contents, Pd₃₃Co₆₇ has a better sensitivity of about 0.2% but a slower response/recovery
time of over 200 s/500 s, at 1% H₂ concentration at a temperature of 273 K, as shown in Figure 10d. Interestingly, the response of the PdCo NW decreases with increasing temperature. The critical temperature $T_c$ for the “reverse sensing behavior” of PdCo NWs is far below room temperature compared to the pristine Pd NWs ($T_c = 287$ K) [65], see Figure 10e. The improvement expanded the low-temperature range and stability of hydrogen sensing.

Lee et al. proposed a partially anchored Pd nanowire (PA-PdNW) to enhance the durability of Pd nanowire-based H₂ sensors. Because most of the structure was not restrained from the volume expansion, PA-PdNW could relieve the internal mechanical stress and thus improve the reliability of the sensor device even it was repeatedly exposed to high concentrations of H₂ [66]. Schematically, Figure 11a demonstrates the fabrication process of the PA-PdNW H₂ sensor. Aluminium oxide was first deposited on a silicon nanograting and then further deposited with copper (Cu) at an oblique angle during the process. After selective etching, the Cu layer was processed by Pd-deposition for the sensing, forming a partially anchored and suspended Pd nanowire structure. Then, the Cu layer was removed as the sacrificial layer. Figure 11d shows the sensing response of PA-PdNW sensors in dry and 85% relative humidity (RH) environments. However, the sensors showed no significant sensitivity difference in both cases. Although the solubility of H₂ in Pd was almost unaffected by the two different humidity levels, the α-β phase transition could still be observed at H₂ concentrations greater than or equal to 2.5%. On the other side, the response/recovery time increased significantly with increasing humidity due to the thin water layer on the surface that delays the hydrogen absorption [67]. Increasing the temperature of the nanowire by applying a heater can significantly reduce the delaying effect caused by high humidity [68].
Lee et al. proposed a partially anchored Pd nanowire (PA-PdNW) to enhance ... humidity (single nanograting pattern) [66]. Copyright (2019), with permission from Royal Society of Chemistry.

Additionally, the repeatability of the sensor properties performed stably after 50 cycles of β-phase transitions tests in Figure 11d. The SEM images in Figure 11e,f demonstrate the robustness of the partially anchored nanowire. This work in [66] provides a unique structural view for designing a Pd NW-based hydrogen sensor with high durability.

In order to improve the sensitivity while lowering the power consumption, Yun et al. [69] developed self-heating, suspended, and palladium-decorated silicon nanowires (Pd-SiNWs) for high-performance hydrogen (H2) gas sensing. The suspended SiNWs can significantly lower the power consumption by reducing the heat loss through the substrate. Surface modification with Pd can react with H2 at room temperature, but this reaction is slow and can be influenced by humidity or carbon monoxide in the environment (see Figure 12a). Figure 12b,c show the Joule-heating mechanism of the self-heating and suspended structures at lower power consumption, increasing the reaction rate and reducing the degradation caused by humidity or carbon monoxide gas. According to available studies [70,71], the sensitivities of Pd nanowires for H2 gas are lowered when applying Joule heating because of the low solubility of H2 at high temperatures. In this work [69], Yun et al. developed a Joule heating method for Pd-SiNW, which can accelerate the response to H2 gas without sacrificing sensitivity.

Figure 13 presents the H2 gas response of the suspended Pd-SiNW sensor to H2 at different Joule heating powers for H2 concentration from 0.01% to 0.5% under the varying Joule heating powers. The sensing performance of both suspended Pd-SiNW and substrate-bound Pd-SiNW is improved without sacrificing response due to the application of the Joule heating. Additionally, as shown in Figure 4e, the suspended Pd-SiNW sensor has a significantly higher response and lower conductivity than the substrate-bound Pd-SiNW sensor. In Figure 13f, the suspended Pd-SiNW at a Joule heating power of 147 µW has a similar transient response to the substrate-bound Pd-SiNW at a Joule heating power of 613 µW, indicating that at the same Joule heating power, the temperature of the suspending SiNW on the substrate is higher than that of the substrate-bound SiNW.
In order to improve the sensitivity while lowering the power consumption, Yun et al. developed a Joule heating method for Pd-SiNW, which can accelerate the reaction rate and reduce the power consumption [69]. Copyright (2017), with permission from American Chemical Society.

Figure 12. Working principle of H2 sensing of a Pd-SiNW. (a) At room temperature, (a-i) depletion of charge carrier (electron) in SiNW (n-type) by negatively charged adsorbed oxygen ions (red dots) and (a-ii) accumulation of charge carrier by desorbing oxygen with H2O formation under H2 gas exposure. (b) Faster and higher response with Joule heating of Pd SiNW because (b-i) more adsorbed oxygen causes more depletion of charge carrier and (b-ii) it has a fast reaction rate with H2, but a low interfering gas effect (H2O and CO) with Joule heating. (c) By replacing substrate-bound SiNW with suspended SiNW, the heat loss through the substrate is reduced, resulting in lower power consumption [69]. Copyright (2017), with permission from American Chemical Society.

Figure 13. H2 gas sensing of the suspended Pd-SiNW sensor: (a) normalized current with Joule heating powers of 41, 79, 115, and 147 μW. The (b) response, (c) response time and (d) recovery time for variant H2 concentrations at four Joule heating powers. Comparison between the substrate-bound and suspended Pd-SiNW sensors: (e) responses at various Joule heating powers (red arrows: direction of Joule heating power increment (from 41 to 147 μW for the suspended Pd-SiNW
Cho et al. investigated the network structure of a half-pipe palladium nanotube (H-PdNTH) by using electrospinning and e-beam evaporation for high-performance hydrogen gas sensing applications [72]. The H$_2$ gas sensing test revealed that reducing the thickness of the H-PdNTH is the main factor to improve the H$_2$ sensing sensitivity and response time. The effect of the Pt catalyst on the H$_2$ sensing performance was also investigated in the paper. In comparison, the Pt decorated H-PdNTN sensors respond nearly two times faster than that of the pristine H-PdNTN sensors. Wang et al. developed a SAW hydrogen gas sensor by employing Pd and Cu-coated nanowires (Pd/Cu NWs) as the sensitive interface [73]. The electrodeposited Pd/Cu was synthesized inside an AAO template. Their sensor was tested with fast response and recovery time within 4 s, a low detection limit of 7 ppm, and a sensitivity of 1.5 kHz/% at room temperature. Baek et al. decorated Pd on n- and p-type Si NW arrays to improve the sensing performance of H$_2$ [74]. Their experiments indicated that the p-type Si NW arrays had ultra-high H$_2$ sensitivity of 1700% at 1% H$_2$ concentration, which was higher than that of the n-type Si NW arrays of 75% at 1% H$_2$. This sensitivity difference was because the Schottky barrier in the n-type Si NW arrays changes to ohmic contact when exposed to H$_2$, and the interface effect of Pd/Si diminishes with increasing H$_2$ concentration. On the other hand, the ohmic contact in the p-type Si NW arrays changes to a Schottky barrier when exposed to H$_2$. As the H$_2$ concentration increases, the work function of PdH$_x$ decreases, increasing the height of the Schottky barrier in the p-type Si NW arrays, thereby improving its sensitivity.

Zheng et al. investigated palladium/bismuth/copper hierarchical nano architectures (Pd/Bi/Cu HNAs) for a hydrogen evolution reaction (HER) and hydrogen sensing applications [76]. In their work, the Pd/Bi/Cu NWs were synthesized by electrochemical deposition inside the nanochannels of AAO templates, forming “forest”-like crystalline microstructures, as shown in Figure 14a–c. The “trunk” of the hierarchical structure is around 2.5 µm long, and 200 nm-long secondary branches serve as a second “trunk”, generating further branches in succession. This kind of microstructures expanded the contact surface for hydrogen sensing via creating more chemical reactive sites. Furthermore, the author investigated the temperature-dependent “reversing sensing behaviour”, which changed the resistance sensing response at the critical temperature. Such a behaviour has been reported and explained by the fact that the crystalline transformation during the α-β phase transition in the hydride process generates new percolation paths that reduce the necessary distance for electrons to move through different percolation paths [65]. At the critical temperature, the sensing response appears as a negative resistance change ΔR (RH(−)).

In contrast, for the working temperature above the critical temperature, the sensing response presented itself as a positive resistance change ΔR (RH(+)), as shown in Figure 14h,i. Compared with pristine Pd nanowires (NWs, 278 K), the designed microstructure of the Pd/Bi/Cu combination reduced the critical temperature of the “reversing sensing behaviour” to about 156 K and extended the operating temperature range (about 156 to 418 K). The sensing response is illustrated in Figure 14d–i.

Pd-coated SnO$_2$ nanofiber rods (NFRs) synthesized by electrospinning and magnet sputtering were introduced by Wang et al. in 2020 [77]. The deposited Pd played a role as a catalyst to improve the sensing performance. The gas sensors enhanced the sensing response at a temperature (160 °C) lower than the SnO$_2$-based hydrogen gas sensor and obtained a fast response with a response time of 4 s at 100 ppm H$_2$ concentration. The limit of detection can be achieved at an ultra-low hydrogen concentration of 0.25 ppm.
applications [76]. In their work, the Pd/Bi/Cu NWs were synthesized by electrochemical deposition inside the nanochannels of AAO templates, forming “forest”-like crystalline microstructures, as shown in Figure 14a–c. The “trunk” of the hierarchical structure is around 2.5 μm long, and 200 nm-long secondary branches serve as a second “trunk”, generating further branches in succession. This kind of microstructures expanded the contact surface for hydrogen sensing via creating more chemical reactive sites. Furthermore, the author investigated the temperature-dependent “reversing sensing behaviour”, which changed the resistance sensing response at the critical temperature. Such a behaviour has been reported and explained by the fact that the crystalline transformation during the α-β phase transition in the hydride process generates new percolation paths that reduce the necessary distance for electrons to move through different percolation paths [65]. At the critical temperature, the sensing response appears as a negative resistance change ΔR

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Figure 14. A hydrogen sensor of Pd/Bi/Cu hierarchical nano architectures (HNAs), SEM images and elemental mapping analysis. (a) The sensor prototype. (b,c) SEM images of Pd/Bi/Cu HNAs on IDE electrode and the magnified SEM image from the dashed rectangle in (b). Response of hydrogen sensor integrated with multiple HNAs. (d–g) ΔR plots with the representative temperature at 388 K, 298 K, 273 K, and 143 K, respectively. (h,i) The summarized temperature-dependent ΔR plots of Pd/Bi/Cu HNAs sensors. The resistance modes, negative values (below T_c), corresponds to the RH(−) mode and positive ones to the RH(+) mode. Here, on: introducing Hydrogen, off: venting hydrogen, ΔR: alteration of resistance [79]. Copyright (2019), with permission from American Chemical Society.

Generally, Pd nanoparticles were deposited on the substrate to enhance sensing performance towards hydrogen. Kumar et al. in 2015 deposited Pd layers directly on the SiO_2/Si substrate by evaporating Pd for hydrogen gas detection [78]. After deposition, the samples were annealed at 400 °C for 2 h to form the isolated Pd nanoparticles. As investigated in the paper, the annealed sensor formed with Pd layers of thickness 1 nm and 5 nm had no sensing response during the release of H_2. The Pd nanoparticles were isolated after annealing, and no electrical pathways were formed to transfer sensing signals. Up to 10 nm thickness, the annealing process formed electrical “channels” on the substrate leading to a sensing performance of 51.4% response at 2% H_2 concentration in the test environment. The response time for the detection was 6 s, and the recovery time was 45 s.

In contrast, Behzadi Pour et al. in 2017 investigated a hydrogen sensor based on a capacitive sensing mechanism synthesized by depositing palladium nanoparticles on a silicon oxide surface, as shown in Figure 15 [79]. For this type of hydrogen sensor based on a capacitive sensing mechanism synthesized by depositing palladium nanoparticles on a silicon oxide surface, the capacitance can be obtained by [80]:

\[
C = \left( \frac{k_{OX}}{\varepsilon_{OX}\varepsilon_0 A} + \frac{X_{sl}}{\varepsilon_{s}\varepsilon_0 A} \right)^{-1}
\]
where $\varepsilon_{OX}$ and $t_{OX}$ are the relative permittivity and thickness of the oxide film, respectively, $\varepsilon_s$ is the relative permittivity of Si, $A$ is the area of the Pd gate, and $X_d$ is the width of the depletion region. In an ideal MOS capacitor, the $V_{FB}$ is defined as the boundary between accumulation and depletion regions as:

$$V_{FB} = \frac{W_{MS}}{q} - \frac{Q}{C_{OX}}$$ (11)

where $W_{MS}$ is the work function difference between gate and substrate, and $Q$ is the trapped charges in the $SiO_2$ film. For Pd/$SiO_2$/Si sensors, the $V_{FB}$ is 0.7 V. Thus, the capacitance of the MOS capacitor in the depletion layer can be obtained [81]:

$$C_T = \frac{C_{OX}}{\sqrt{1 + \frac{2\varepsilon_{OX}^2 \varepsilon_s |V - V_{FB}|}{qN_D t_{OX}^2}}}$$ (12)

where $N_D$ is the donor carrier density in Si, and $q$ is the charge of the electron. This gas sensor had a fast response time of 1.4 s and a recovery time of 14 s with a sensitive response of 88% at 1% $H_2$ concentration.

Figure 15. (a) Schematic diagram of the Pd/$SiO_2$/Si capacitor. (b) Experimental values of the C–V curves for the Pd/$SiO_2$/Si sensor at room temperature and the Ni/$SiO_2$/Si sensor at 100 kHz frequency in a mixture of pure nitrogen and 1% $H_2$–$N_2$ at 140 °C. (c) The response (%) of the Pd/$SiO_2$/Si and Ni/$SiO_2$/Si MOS capacitor sensors in 1% $H_2$–$N_2$ mixtures [79]. Copyright (2017), with permission from World Scientific.

Despite the advantages of employing Pd nanoparticles for hydrogen gas sensing, the low selectivity may reduce the sensor’s sensitivity towards hydrogen gas. Chen et al. in 2017 [82] investigated the $H_2$ gas sensor with Pd nanoparticles deposited on $SiO_2$/Si substrates for different target gases and gas mixtures. Without any filtration layer, this $H_2$ gas sensor cannot accurately distinguish between cross-sensitive gases and gas mixtures such as carbon monoxide (CO), water vapour and methane (CH$_4$). More importantly, CO is a highly toxic cross-sensitive gas for Pd catalysts, which causes a reduction in available dissociation sites on the Pd metal surface due to CO adsorption [83,84]. To address this issue, Lee et al. in [85] reported that an $H_2$ sensor using a hybrid structure of Pd NP/single-
layer graphene (SLG) coated with a polymer membrane achieved high selectivity towards H₂. In comparison, Chen et al. reported in [82] that H₂ sensors with a thin spin-coated layer of poly (methyl methacrylate) (PMMA) on the sensing surface deposited by Pd NP significantly improved the gas selectivity towards H₂, as shown in Figure 16e. Due to the thickness of the PMMA membrane layers, the sensor response became correspondingly slower. This retardation effect of the sensing kinetics during the sensing reaction is mainly attributed to three mechanisms: the diffusion of H₂ gas in the PMMA matrix, the nucleation and growth of the β phase in the α phase matrix of Pd hydride, and the stress relaxation at the interface between Pd NPs and the PMMA matrix. Accordingly, the response time was experimentally proved to be correlated with hydrogen pressure and the thickness of the PMMA layer, as presented in Figure 16f,g.

![Figure 16. Schematic illustration of the procedure used to fabricate the hydrogen sensor based on a poly (methyl methacrylate) (PMMA)-membrane-coated Pd nanoparticle (NP) film. (a) The deposition of Pd NPs. (b) The Pd NP film formed on the interdigital electrode substrate after the NP deposition. (c) The PMMA-membrane-coated Pd NP film fabricated by spin coating. (d) The structure of the hydrogen sensor based on the PMMA-membrane coated Pd NP film. (e) The response of sensors with and without a PMMA membrane layer to target gas mixtures. The concentration of CO/N₂, CH₄/N₂ and H₂/N₂ was 1000 ppm. The tested mixed gas of H₂, CO and CH₄ in N₂ was formed by simultaneously filling the three kinds of gas into the test chamber. (f) Response time as a function of hydrogen pressure for five samples of different thicknesses (a–e). The dashed lines indicate the boundaries of the three hydride phase regions. (g) Plots of the response time versus the thickness of the PMMA membrane layer [82]. Copyright (2017), with permission from American Chemical Society.

Even though Pd NPs can be deposited in hydrogen gas sensors as catalysts in hydrogen detection, their combination with metal oxide structures can still improve the sensing response by enhancing the electron conductive path. Much literature has discussed the use of Pd NPs decorated with various metal oxide structures for hydrogen gas sensing, such as ZnO [86], SnO₂ [87,88], WO₃ [89,90], MnO₂ [91], and MoS₂ [92].

A flexible hydrogen sensor based on ZnO nanorods (NRs) was developed by Rashid et al. in 2014 [86]. The ZnO NRs were synthesized from Ga-modified ZnO seed layers (GZO). The dopant Ga atoms were incorporated into ZnO material by replacing the Zn host atoms, releasing free electrons, and contributing to high conduction or improving carrier mobility. This kind of sensor (ZnO: 3% Ga-doped seed) is reported to have a high response factor of 91.2% and a fast response time of 18.8 s. Additionally, it also exhibits high selectivity when exposed to different target gases. In paper [93]. Weber et al. in 2019 developed an H₂ gas sensor based on ZnO NWs coated with a thin layer
of boron nitride (BN) and decorated with Pd NPs, whereas the Pd NPs help the BNs to enhance the performance of different catalytic reactions [94,95]. It has been found that the hydrogen’s lowest detection level could be 0.5 ppm with a sensitivity of 1.34 at 200 °C. The Pd/BN/ZnO NWs responded at an H₂ concentration of 100 ppm within an H₂ releasing time of 160 s and a recovery time of 90 s (R₄/R₆ = 12.28).

For the gas sensor based on the combination of SnO₂ and Pd NPs, Li et al. [87] in 2017 synthesized SnO₂-composite Pd nanoparticles with average diameters up to hundreds of nanometers via a solvothermal method. The hydrogen sensor using 10 mol% Pd-SnO₂ composites showed enhanced performance compared to pristine SnO₂. At 200 °C working temperature, the Pd-SnO₂ composite-based hydrogen sensor performed a fast response/recovery time of 4s/10s and high sensitivity (R₄/R₆ = 315.34) for 3000 ppm H₂ concentration. The lowest detection limit was achieved at an ultra-low concentration of about 10 ppm. By contrast with the work in [87], Kim et al. in 2019 synthesized in [88] Pd NPs-decorated SnO₂ NWs for hydrogen sensing applications, as shown in Figure 17. The presence of Pd on the NW surface increased the electron depletion region of SnO₂ NWs, which modulated the conduction channels inside NWs. Therefore, the initial conduction volume or initial electron concentration of SnO₂ decreased accordingly. When H₂ gas was adsorbed onto SnO₂, it raised electron concentration at the surface and assisted in further elevating the Fermi level, which increased the potential barrier at the SnO₂/Pd interface. This change at the surface made it difficult for electrons in SnO₂ to move to the Pd side, decreasing the resistance in SnO₂ and improving the sensing response, as presented in Figure 17c. The gas test results showed that the response of the decorated SnO₂ NWs to 1 ppm H₂ concentration at 300 °C increased from 6.88 to 16.95 (R₄/R₆).

![Figure 17. Field-emission scanning electron microscope (FE-SEM) micrographs of (a) bare SnO₂ NWs and (b) Pd-decorated SnO₂ NWs. Upper-right inserts are the top-view of the FE-SEM images. (c) The sensing mechanism of Pd-decorated SnO₂ NWs [87]. Copyright (2017), with permission from Elsevier.](image)

As the summary in the section of Pd-based hydrogen gas sensors, Table 1 compares the sensing performances based on different material combinations, operating temperatures, synthesis methods, low detection limits, and sensing responses (including response time/recovery time, sensitivity at target hydrogen concentration). Furthermore, the sensor performance responsible parameters are also schematically illustrated in Figure 18a,b. In general, Pd and its combination-based gas sensors can detect hydrogen gas at room temperature, and the size effect affects the sensing performance significantly. The smaller
the sensing structure/cluster is, the more significant the sensor’s reactive surface, which promises better sensing performance towards hydrogen with lower power consumption. However, the low ambient operating temperature can raise the humidity rate on the sensor surface, which reduces the sensor response and sensitivity. Additionally, the small size and discontinuity of the sensing materials also lead to a very low conductivity of the nanostructures, which induces high electrical noise, and degrades the sensor response.

Table 1. Comparison of sensing performances towards hydrogen gas of Pd-based gas sensors in literature. Unless specified, the sensor response is defined by the given Equation (1). (*) Sensor response given by the form $R_a/R_g$. (**) The recovery times were not given directly in their publications and were approximately read out from the sensing response curves. RT: room temperature, DC: direct current, RF: radio frequency, SAW: surface acoustic wave, PVD: physical vapour deposition.

| Ref. Nr. | Sensor Materials | Operating Temperature | Synthesis Methods | Low Detection Limit | Response/Recovery Time (Response) at H₂% | Literature |
|---------|------------------|-----------------------|-------------------|---------------------|------------------------------------------|------------|
| 1       | Pd film          | RT                    | DC sputtering     | 100 ppm             | 25/10 s (17%) at 1.2%                   | [58]       |
| 2       | Pd film/Pt heater| 50 °C                 | —                 | 200 ppm             | 30/17 s (0.2%) at 4000 ppm              | [59]       |
| 3       | Pd film/Pt heater| 400 °C                | —                 | 200 ppm             | 10/15 s (4%) at 4000 ppm               | [59]       |
| 4       | Pd/SnSe film     | RT                    | DC magnetron sputtering | 0.91 ppb           | 73.1/23.7 s (3225 *) at 1000 ppm        | [61]       |
| 5       | Pd/TiO₂ film     | RT                    | DC magnetron sputtering | 0.4%            | 4/8 s (−) at 0.4%                     | [60]       |
| 6       | Pd-Ni alloy thin-film | RT              | co-sputtering, SAW | 0.01%             | 7/30 s (2.75 kHz) at 0.1%               | [33]       |
| 7       | Pd/ZnO film      | RT                    | pulsed laser deposition | 0.2%         | 12/16 s (−) at 2%                      | [39]       |
| 8       | Pd/Y alloy film  | RT                    | magnetron co-sputtering | 0.1%          | 33/27 s (24.1 mV) at 1%                | [32]       |
| 9       | Pd/Co NWs        | RT                    | electrodeposition  | 0.1%             | 200/500 s (−0.2%) at 1%                | [64]       |
| 10      | PA Pd NWs        | RT                    | deposition        | 0.1%             | 70/140 s (−7%) at 1%                   | [66]       |
| 11      | Pd-Si NWs        | 200–400 °C            | PVD               | 0.01%             | 10/30 s (1.5 *) at 0.1%                 | [69]       |
| 12      | Pd NWs           | 296–336 K             | electrosyn, deposition | 314 ppm     | 12/18 s **(2.1%) at 1.8%               | [72]       |
| 13      | Pd/Cu NWs        | RT                    | electrodeposition  | 7 ppm            | 4/4 s (1.5 kHz) at 1%                   | [73]       |
| 14      | Pd/Si NWs        | RT                    | DC magnetron sputtering | 5 ppm          | −/−                                      | [74]       |
| 15      | Pd NWs@ZIF-8_2h  | RT                    | lithographically patterned nanowire, electrodeposition | 1000 ppm | 13/6 s (0.3%) at 0.1%                  | [75]       |
| 16      | Pd NWs@ZIF-8_4h  | RT                    | lithographically patterned nanowire, electrodeposition | 600 ppm | 30/8 s (0.7%) at 0.1%                  | [75]       |
| 17      | Pd NPs coated SnO₂ | 160 °C               | DC sputtering magnet sputtering | 0.25 ppm | 4 s/− (30 *) at 100 ppm                | [77]       |
| 18      | Pd NPs/SiO₂/Si   | RT                    | Deposition        | 2%               | 6/45 s (51.4%) at 2%                    | [78]       |
| 19      | Pd NPs/SiO₂/Si   | RT                    | Deposition        | 1%               | 1.4 s/14 s (88%) at 1%                  | [79]       |
| 20      | PMMA/Pd NPs / SiO₂/Si | RT                  | deposition, Spin coating | 100 ppm | −/−                                      | [82]       |
| 21      | Pd NPs/ZnO      | RT                    | RF magnetron sputtering | 0.5 ppm      | 18.8 s/− (91.2%) at 0.1%                | [86]       |
| 22      | Pd NPs/SnO₂     | 200 °C                | solvothermal method | 10 ppm         | 4/10 s (315.34 *) at 3000 ppm           | [87]       |
| 23      | Pd NPs/SnO₂ NWs | 300 °C                | chemical Deposition | 1 ppm          | 150/400 s **(27.8 *) at 100 ppm         | [88]       |
| 24      | Pd/BN/ZnO NWs   | 200 °C                | atomic layer deposition | 0.5 ppm  | 160/90 s *(7.95 *) at 10 ppm            | [93]       |
Figure 18. Regarding Table 1, schematic illustrations of the comparison of the reported Pd-based hydrogen gas sensors in literature: (a) low detection limits. The x-axis “Reference Number” represents the 1st column “Ref. Nr.” in Table 1. (b) Response time/recovery time under experimental conditions as reported in the literature.

3. Metal Oxide Semiconductor-Based Hydrogen Gas Sensors

Another classification of promising materials for gas sensing is the conductometric metal oxide semiconductor (MOS). They are generally crystalline or polycrystalline in nature and interconnected with different grains having grain boundaries. However, by contrast with transition metals, most metal oxide materials are essentially insulators at room temperature. As a result, they cannot be used directly for gas sensing due to their bandgaps between the conduction band and valence bands forming electron mobility barriers. Typically, the gas sensing suitable metal oxides have bandgap between 2.7 eV and 4 eV, like SnO\(_2\) (3.6 eV), NiO (3.5 eV), TiO\(_2\) (3.2 eV), ZnO (3.2 eV), WO\(_3\) (2.7 eV) etc. [96,97]. With an elevated temperature in the range of up to 600 °C [98], the amount of mobile electrons can be generated by electrons thermally from the valance band into the conduction band participating in the charge transfer.

Meanwhile, the interaction between the MOS sensing materials and the surrounding chemical environment also affects the mobile carrier density inside metal oxide materials and changes their resistance consequently. In their gas sensing mechanisms, depending on the target gas (oxidizing or reducing) and semiconductor type (n- or p-type), the resistance can increase or decrease during the interaction with the target gas. In the case of n-type metal oxides with electrons (e\(^-\)) as majority carriers, the resistance increases in oxidizing gases (acceptor) but decreases in reducing ones (donor), whereas the p-type metal oxide (e.g., NiO [99]) with holes as majority charge carriers has the converse resistance changes [100].

Taking n-type MOS such as SnO\(_2\) or TiO\(_2\), for instance, at elevated temperature in the air atmosphere, the oxygen molecules (O\(_2\)) are chemisorbed on the surface of the MOS, as shown in Figure 19. Since O\(_2\) molecules are oxidizing gas and act as acceptors of electrons, they are dissociated on the surface and ionized into species such as O\(_{2^-}\), O\(^-\), and O\(^2-\) by trapping electrons from the conduction band of the n-type MOS, as indicated in Equations (1)–(4). The ionizations of these chemisorbed species are temperature dependent. The O\(_{2^-}\) is dominant at temperatures lower than 150 °C, O\(^-\) has its range from 150 to 400 °C, and O\(^2-\) is at temperatures larger than 400 °C [101,102].

\[
\begin{align*}
\text{O}_2^{\text{gas}} & \rightarrow \text{O}_2^{\text{ads}} \quad (13) \\
\text{O}_2^{\text{ads}} + e^- & \rightarrow \text{O}_2^-^{\text{ads}} \quad (14) \\
\text{O}_2^-^{\text{ads}} + e^- & \rightarrow 2\text{O}^-^{\text{ads}} \quad (15)
\end{align*}
\]
Due to the decrease of electron density of the n-type MOS, an electron depletion layer has been created around the MOS with a high potential barrier. This electron depletion layer leads to an electronic core–shell configuration. As the electron conduction of the MOS decreases, its resistance is therefore increased.

When reducing gases, such as H$_2$ are exposed to the MOS, the chemisorbed oxygen ion species on the MOS surface react with H$_2$, as indicated in Equations (17)–(19) by forming H$_2$O and releasing electrons back into the electron depletion layer.

\[
O_{\text{(ads)}}^- + e^- \rightarrow O_{\text{(ads)}}^{2-}
\]  

(16)

\[
2H_2 + O_{\text{2(ads)}}^- \rightarrow 2H_2O + e^-
\]  

(17)

\[
H_2 + O_{\text{(ads)}}^- \rightarrow H_2O + e^-
\]  

(18)

\[
H_2 + O_{\text{2(ads)}}^- \rightarrow H_2O + 2e^-
\]  

(19)

Thus, the thickness of the electron depletion layer becomes thinner, accompanying the decrease of the resistance of the MOS hydrogen gas sensor [103].

In contrast, when the p-type MOS hydrogen gas sensor is exposed at elevated temperature in the air atmosphere, the electrons from the valence band are captured on the surface, and a hole accumulation layer is formed around the p-type MOS core. Consequently, the resistance of the MOS hydrogen gas sensor decreases. Similarly, the chemisorption of air oxygen and ionization process can also be described with Equations (1)–(4). With H$_2$ as the target gas releasing in the test environment, the H$_2$ molecules react with oxygen ion species similarly and release electrons back into the hole accumulation layers. The receptor site accommodates electrons from the conductance band and causes a shrink of the hole accumulation layer, which leads to a resistance increase of the MOS gas sensor, as shown in Figure 20 [104]. Similar to the case for the n-type MOS gas sensor, the Equations (17)–(19) are also used to describe the reduction process for the p-type MOS gas sensor.
Since the MOS gas sensors can exchange electrons with a wide variety of gases, the selectivity of MOS gas sensors is inherently limited. Thus, optimization measures are also required to adjust the performance, such as a mixture with noble metal catalysts on the MOS surface, like palladium and platinum [87]. Furthermore, the optimization of microstructure and nanostructure can also improve the sensibility and response of the MOS gas sensors [105–107].

A Joule effect heating element is needed to raise the oxide layer’s temperature, to promote surface reactions, and to remove water produced from these reactions [108]. SnO$_2$, with a wide bandgap of 3.7 eV at 300 K (about 26.85 °C) [109], is one of the most widely used metal-oxide-semiconductors for gas sensing applications due to its high sensitivity and good stability. However, the SnO$_2$ based gas sensors exhibited poor selectivity, long response/recovery time, and a need for high operating temperature, high power consumption and complex integration structure accordingly [110]. To resolve these issues, researchers have devoted their efforts to improve the sensing performance of SnO$_2$ by applying various methods, such as morphological modifications [105,106,111] and metallic doping [87,112–115]. Since the gas-sensing performance of SnO$_2$-based gas sensors depends strongly on the fabrication morphology, Shen et al. in [105] investigated nanofilms, nanorods and nanowires at various hydrogen concentrations at high ambient temperatures, as presented in Figure 21a,f. In their work, the SnO$_2$ nanofilms were deposited on oxidized Si substrates using the sputtering method, and the SnO$_2$ nanorods and nanowires were synthesized by the thermal evaporation method. When the sensors are exposed to H$_2$ test gas of 1000 ppm concentration at 150 °C, the nanomaterial demonstrates low sensor resistance and good reversibility due to its sizeable effective surface. The response time and recovery time become shorter as the effective surface area increases. The resistance of the SnO$_2$ nanowire is one order of magnitude lower than nanofilms and nanorods. At varying operation temperatures at the same H$_2$ concentration, the SnO$_2$ nanomaterials had their peak response at different temperatures, namely SnO$_2$ nanofilms had 2.3 at 250 °C, SnO$_2$ nanorods had 2.8 at 200 °C, and SnO$_2$ nanowires had 5.5 at 150 °C. These results revealed that, as the effective surface area of SnO$_2$ nanomaterials increases, the peak operating temperature decreases gradually, as shown in Figure 22b.
Figure 21. (a) Surface and (b) cross-sectional field of the emission scanning electron microscopy (FE-SEM) images of SnO$_2$ nanofilms. (c) Low- and (d) high-magnification FE-SEM images of SnO$_2$ nanorods. (e) Low- and (f) high-magnification FE-SEM images of SnO$_2$ nanowires [105]. Copyright (2015), with permission from Elsevier.

Figure 22. (a) Changes in the resistance of gas sensors based on SnO$_2$ nanomaterials upon exposure to 1000 ppm H$_2$ at an operating temperature of 150 °C. (b) Responses of SnO$_2$ nanomaterials upon exposure to 1000 ppm H$_2$ as a function of the operating temperature. (c) Arrhenius plots representing the electrical conductivities of SnO$_2$ nanomaterials before H$_2$ introduction versus the reciprocal of the operating temperature (1/T). (d) Relationships between the response and H$_2$ concentration for SnO$_2$ nanofilms at 250 °C, SnO$_2$ nanorods at 200 °C, and SnO$_2$ nanowires at 150 °C [105]. Copyright (2015), with permission from Elsevier.
The relation between the sensor response and operating temperature of an n-type semiconductor has been described by employing the Arrhenius equation [116,117]:

$$\sigma = \sigma_0 \exp \left( \frac{-E_a}{k_B T} \right)$$

(20)

where $\sigma$ is the electrical conductivity; $E_a$ represents the activation energy, $k_B$ is the Boltzmann constant, and $T$ is the operating temperature in Kelvin. As shown in Figure 22c, the authors calculated the activation energies from the Arrhenius plots’ slope over a temperature range of 25–150 °C with values of 0.47 eV for SnO$_2$ nanofilms, 0.31 eV for SnO$_2$ nanorods, and 0.08 eV for nanowires. These results suggest that smaller activation energy leads to more straightforward sensing reactions and faster sensor responses. Moreover, as Figure 22d shows, there is a relatively linear response for target gas concentrations at each peak response temperature. Furthermore, the response of SnO$_2$ nanofilms, nanorods, and nanowires increases sequentially at the same H$_2$ concentrations.

Zhu et al. studied the hydrogen detection response of SnO$_2$ nanostructures in a non-oxygen environment innovatively [106]. As shown in Figure 23, the three different nanostructures of SnO$_2$ were synthesized by a thermal evaporation method: SnO$_2$ solid spheres (of ~500 nm diameter) (marked as 0-SnO$_2$), the SnO$_2$ nano-urchins assembled by a nano-needle (of ~50 nm diameter and ~500 nm length) (marked as 1-SnO$_2$), and SnO$_2$ nanoflowers assembled by nanosheets (of ~50 nm average thickness) (marked as 2-SnO$_2$). Among these three nanostructures, nanoflowers had the best sensing response at 350 °C. The reason behind this is that a nanoflower has the largest effective surface for H$_2$ chemisorption in both aerobic/oxygenated and anaerobic/non-oxygenated environments, as shown in Figure 24. A similar trend can also be seen in the change in gas response of the sensors based on the nanostructures, i.e., an increase followed by a decrease with increasing operating temperature.

Figure 23. Scanning electron microscope (SEM) and transmission electron microscope (TEM) images of the SnO$_2$ samples with different morphologies: (a–c) solid spheres (S0), (d–f) nano-needle assembled nano-urchins (S1), (g–i) nanosheet-assembled nanoflowers (S2) [106]. Copyright (2019), with permission from Elsevier.
Interestingly, these sensors in a vacuum environment are more sensitive and have faster response and recovery times than those in the atmospheric environment. Furthermore, the (1 1 0) surface was the most thermodynamically stable among all the low-index SnO$_2$ surfaces [118,119]. In turn, the sensing performance of the SnO$_2$ nanostructure is strongly affected by its effective surface. Therefore, the authors in [120] investigated SnO$_2$ (1 1 0) surface-based sensors’ mechanism in the two vacuums mentioned above and atmospheric test environments. The adsorbed oxygen is widely claimed to be the primary mediator of a gas sensing reaction between reductive gases and sensing materials, and adsorbed oxygen is considered as the electron transfer pathway. However, the results show that only relatively weak electron transfer occurs between the H$_2$ and adsorbed oxygen atoms. Furthermore, the H$_2$ gas molecule is more likely to react with its oxygen atoms in the SnO$_2$ lattices on the surface than with adsorbed oxygen atoms, which is inconsistent with the conventional gas sensing mechanism of n-type semiconductors. Therefore, this discovery can probably open up a new route to improve the gas sensing properties of SnO$_2$ and even other sensing materials.

Liu et al. in 2018 developed a hydrogen gas sensor based on hydrothermal synthesized SnO$_2$ nanoflowers [111]. This nanostructure increased the effective surface significantly for oxygen adsorption. Additionally, a vacuum annealing treatment in the post-treatment process increased the surface area of SnO$_2$ nanoflowers by another 8% and decreased the sensor conductivity. As the annealing process raised the number of active sites for adsorbed oxygen remarkably, the annealed sensor exhibited a sensitivity of about 80.2% for 1000 ppm H$_2$ concentration at room temperature, compared to 27.1% for the unannealed

Figure 24. (a) Gas response of the three sensors exposed to 400 ppm H$_2$ concentration at different temperatures in an atmospheric environment. (b) The response-recovery curve of the three sensors under 400 ppm H$_2$ concentration at 350 °C in an atmospheric environment. (c) Gas response of the three sensors exposed to 400 ppm H$_2$ concentration at different temperatures in a vacuum environment. (d) The response-recovery curve of the three sensors under 400 ppm H$_2$ at 350 °C in a vacuum environment [106]. Copyright (2019), with permission from Elsevier.
one. The annealed sensor required a response time of 71 s, which was slightly slower than the annealed one, of 62 s. However, the recovery time for the annealed sensor was as long as about 500 s, compared to 130 s for the unannealed one.

The metallic doped nanoparticles (NPs), such as palladium Pd [87, 112], platinum Pt [113, 114], and gold Au [115], have also been proved to be an efficient method to improve the hydrogen sensing response of metal oxide semiconductor-based gas sensors.

SnO$_2$-composited Pd NPs with different Pd loadings (0, 2.5, 7.5, 10 mol% Pd) for hydrogen detection application were investigated by Li et al. [87]. In their work, the sensing materials were synthesized by the solvothermal method and then calcinated. At an operating temperature of 200 °C, for a hydrogen concentration of 3000 ppm, the 10 mol% Pd loaded sensor performed the highest response, with $R_a/R_g$ equal to 315.34 and a fast response/recovery time (4 s/10 s), more than eight times higher than pristine SnO$_2$-based sensors. By contrast, Yang et al. in [112] compared Pd NPs-modified SnO$_2$ thin-film hydrogen gas sensors synthesized with the sol-gel method and the magnetron sputtering method, as shown in Figure 25a–d. The hydrogen sensing properties were characterized using delay-line surface acoustic waves (SAW). The results showed that the sensor with the RF-sputtered Pd surface-modified layer and DC sputtered SnO$_2$ layer obtained the highest sensitivity to 2000 ppm hydrogen gas at 175 °C.

![Figure 25. Two kinds of hydrogen gas sensors based on SnO$_2$ films: (a) the chemi-resistive hydrogen gas sensor, (b) the micrograph of the chemi-resistive hydrogen sensor, (c) the delay-line surface acoustic waves (SAW) hydrogen gas sensor, and (d) the micrograph of interdigital transducers (IDTs) of the SAW hydrogen sensor [112]. Copyright (2017), with permission from Elsevier.](image)

A hydrogen gas sensor based on SnO$_2$ nanorods has also been fabricated using a simple hydrothermal method, with the surface of the nanorods decorated with Pt NPs through irradiated photochemical reduction method. Surprisingly, the sensor exhibited a high sensitivity of 88.35% even at room temperature with an ultra-fast sensing response of 0.4 s in time for 1000 ppm hydrogen. This type of Pt-decorated SnO$_2$ hydrogen gas sensor can efficiently reduce the power consumption [87], thus ensuring the sensor performance during the long-term operation process [21]. On the other hand, the low ambient temper-
temperature enhanced the negative impact of humidity on the sensor. As reported in [98], the entire sensor response decreased from 88.35% at 21.88% relative humidity (RH) to ~26.58% at 83.50% RH, indicating that the sensor response decreased significantly with increasing relative humidity.

Yin et al. [114] used screen-printed Pt-decorated SnO$_2$ NPs on alumina substrates for H$_2$ gas sensing. Before the screen-printing process, the decorated NPs were prepared by using sol-gel and hydrothermal methods. The results indicated that a 1 wt.% Pt-SnO$_2$ sample gave the best sensing response to 100 ppm H$_2$ at an optimum working temperature of 350 °C with the lowest detection limit of 0.08 ppm. The ideal response time for this sample was 29 s, and the recovery time was 36 s.

In 2017, Wang et al. [115] developed a hydrogen gas sensor based on Au-loaded SnO$_2$ composite NPs, (see in Figure 26a). Firstly, the Au-loaded SnO$_2$ was mixed with terpineol and ethyl cellulose, grounded with deionized water. Then, the mixture formed a sensing paste, which was coated on a ceramic tube. Next, the paste formed a functional sensing film towards hydrogen with a pair of Au electrodes and Pt wires. After analyzing the effect of Au concentration on sensing properties, it was found that the 4.0 wt.% Au-loaded SnO$_2$ gas sensor exhibited a relatively high sensing response at the optimal working temperature of 250 °C. At this temperature, the sensor’s response/recovery time (1/3 s) was fast, and a low detection limit of 1 ppb H$_2$ concentration was obtained. The paper [115] also verified the high selectivity of this sensor towards H$_2$ and its excellent long-term stability, as presented in Figure 26b.

![Figure 26. (a) Schematic diagram of SnO$_2$ gas sensing element. (b) Long-term stability of the prepared gas sensors to 100 ppm H$_2$ at their optimum temperatures [115]. Copyright (2017), with permission from Elsevier.](image)

Another widely used metal oxide semiconductor is ZnO, an n-type semiconductor with a bandgap of 3.37 eV. ZnO-based gas sensors exhibit better performance because of their wide range and direct bandgap, high electron mobility and high excitation binding energy. However, like some SnO$_2$-based gas sensors, many ZnO gas sensors require high operating temperature (up to 400 °C) in sensing applications, which causes high power consumption and thus leads to instability during long-term gas detection. Therefore, more thoughtful strategies were developed to enhance their sensitivity and selectivity with lower power consumption [107,121–127].

In 2020, Krishnakumar et al. investigated ZnO-based sensors for hydrogen sensing at a high operating temperature of 400 °C with fast response and recovery time (5 s/7 s) [107]. The sensor exhibited a relatively low sensing response (R$_a$/R$_g$ equals 10 at 2000 ppm H$_2$). Earlier in 2018, Vallejos et al. synthesized ZnO rods-based hydrogen sensors via chemical vapour deposition [121], as shown in Figure 27. Due to the large effective surface, the ZnO rods exhibited better sensitivity for 100 ppm hydrogen concentration and at a relative lower temperature of 350 °C. The low detection limit was determined to be 10–90 ppm.
Kim et al. recently investigated two-dimensional (2D) ZnO nanosheets decorated with pristine and Pd for different sensing modes to lower the power consumptions in 2021 [122]. The ZnO nanosheets with an ultrathin thickness of 1 nm were synthesized using a facile hydrothermal method and decorated with Pd NPs using the UV reduction method, as shown in Figure 28a,b. Using the thin ZnO film nanostructure, the hydrogen gas sensors exhibited high performance with reduced power consumption. When sensors based on the pristine and Pd-decorated ZnO nanosheets were exposed in hydrogen, the pristine sensor showed no significant differences with increasing H2 concentration at the optimal working temperature of 300 °C, as shown in Figure 29a. On the other hand, at 250 °C, the Pd-decorated ZnO nanosheets exhibited higher response (Ra/Rg = 2.5) to 50 ppm H2, and better selectivity towards H2 compared to other gases like CO, C6H6, C7H8, and C2H6O. The low detection limit of the Pd-decorated ZnO ultra-thin film sensor can reach 0.5 ppm (see Figure 29b–d). In self-heating mode, the Pd-decorated ZnO nanosheets exhibited relatively lower responses and poor selectivity among the test gases at the optimal applied voltage of 1 V to 20 V. In their investigations [122], the Pd-decorated ZnO thin-film sensor exhibited p-type behaviour at 25 °C, increasing resistance upon introducing H2 gas. In the range of 100–350 °C, the Pd-decorated ZnO nanosheets exhibited n-type behaviour, in which the resistance decreased during the introduction of H2 gas. Similarly, Kim et al. also developed a Pd-decorated-ZnO based gas sensor for H2 detection [123]. The sensing part was Pd-loaded ZnO nanofibers synthesized by a facile electrospinning technique. It was found that the Pd-loaded (0.6 wt%) ZnO nanofibers exhibited a high response of Ra/Rg = 74.7 at 350 °C for a low concentration of hydrogen at 100 ppb.

The sensitivity of Pt/ZnO Schottky diode-based hydrogen sensors is reduced when switching to humid ambient H2 conditions in the presence of water due to hydroxyl groups on the Pt surface. Consequently, Jang et al. [124] spin coated the PMMA on Pt/ZnO Schottky diode sensors as a protective layer to enhance hydrogen sensing performance. Due to its hydrophobicity, the PMMA layer can effectively serve as a moisture barrier and selectively filter the water vapour during hydrogen sensing. The hydrogen sensitivity of PMMA-coated diode sensors could be recovered to up to 80% under humid H2 ambient conditions at room temperature. Under dry and humid conditions, ZnO diodes exhibited relatively fast and stable on/off switching with good repeatability in each cycle.

Nakate et al. in 2019 investigated an H2 sensor-based on hollow ZnO particles that exhibited remarkable sensitivity and selectivity towards hydrogen gas by heat treatment to polystyrene@ZnO core-shell microstructure [125]. At an optimized temperature of 225 °C, the sensor showed the lowest H2 detection limit of 2 ppm with a response of 7%.
The sensitivity of Pt/ZnO Schottky diode-based hydrogen sensors is reduced when switching to humid ambient $H_2$ conditions in the presence of water due to hydroxyl groups on the Pt surface. Consequently, Jang et al. [124] spin coated the PMMA on Pt/ZnO Schottky diode sensors as a protective layer to enhance hydrogen sensing performance. Due to its hydrophobicity, the PMMA layer can effectively serve as a moisture barrier and selectively filter the water vapour during hydrogen sensing. The hydrogen sensitivity of

Other metal oxide semiconductors like TiO$_2$ [128–130], WO$_3$ [131,132] were also investigated intensively for hydrogen sensing applications. Krško et al. in 2017 fabricated a flexible TiO$_2$-based gas sensor by depositing TiO$_2$ on a 38 µm thick polyimide foil [128]. The sensor is highly sensitive at room temperature with the achieved response ($R_a/R_g$) of
about 10^4 for 1000 ppm H_2 in synthetic air. Its low detection level was found to be about 30 ppm. The authors explained that such high sensitivity is due to the meager grain size (about 10 nm), which is comparable to the width of the depletion layer. Moreover, the TiO_2 films exhibited good adhesion to the polyimide foil. The sensitivity values did not decrease after bending the sensor 1000 times, and no damage was evident. Chen et al. in 2016 in [129] presented a porous Pt-TiO_2 nanocomposite (TiO_2: P25, 80% anatase and 20% rutile; Pt power: particle sizes of ~10 nm) ceramics, synthesized by applying a pressure of about 10 MPa and sintering at 450 °C. Such sensors exhibited a high hydrogen sensitivity of about 6000 for 1000 ppm H_2 balanced in N_2 and a fast response/recovery times of 10/20 s at room temperature. Because hydrogen molecules can easily penetrate the porous nanoparticles, this leads to increased hydrogen reactivity. Furthermore, the Pt aggregates in the nanocomposites improved the dissociation of hydrogen molecules and helped the migration of hydrogen atoms to migrate onto surfaces of TiO_2 nanoparticles by spill-over process [130].

Tungsten trioxide (WO_3) exhibits chemochromic properties resulting from a change in the metal ions’ oxidation state, usually transparent crystalline oxide. With the decoration of catalytic metal NPs such as Pd or Pt, the WO_3 enable a reversible colouration process upon exposure to hydrogen. Partially, the reduced oxide turns blue or black. The chemical reactions can be described as [132]:

\[
\text{WO}_3 + x\text{H}^+ + xe^- \rightarrow \text{H}_x\text{WO}_3 \tag{21}
\]

\[
\text{H}_x\text{WO}_3 + \frac{x}{4}\text{O}_2 \rightarrow \text{WO}_3 + \frac{1}{2}x\text{H}_2\text{O} \tag{22}
\]

Lee et al. in 2021 developed a cost-effective chemochromic gas sensor based on Pd and WO_3 nanoparticles for hydrogen detection [131]. The sensing materials were fabricated via electrostatic spray deposition (ESD) of a solution of Pd and WO_3 NPs. During the processing, fine droplets of the solution were broken down into sub-micron scales via electric forces, ensuring the uniform deposition of sub-micron droplets on a target substrate. Moreover, the ESD process enabled the sub-micro-scale structure with well-defined porosity and a high aspect ratio, facilitating gas diffusion. The Pd catalyst reduced the activation energy of hydrogen adsorption and allowed hydrogen adsorption on the surface of WO_3 via the spill-over effect [133,134]. The adsorption of hydrogen ions and electrons changed the charge state of tungsten ions. Upon the reduction of W^{6+} to W^{5+}, the chemochromic colour of WO_3 changes from pale green (W^{6+}) to deep blue (W^{5+}) [135], as shown Figure 30. On these sensing layers, the chemochromic property of the WO_3-Pd sensor is determined by the surface chemical reaction of the adsorbed gas species. For the quantitative investigation of the chemochromic properties, the spectrometer was employed to measure the light beam’s colour difference (dE) injected into the sensor and reflected subsequently. As a result, the optimized sensor was found to have a WO_3:Pd molar ratio of 125:1 and a thickness of 5 µm. This chemochromic sensor demonstrated a rapid sensing response, with a colour change occurring within 15 s at room temperature. The sensor exhibited a deep blue colour in the presence of hydrogen, with the dE value of 18.5 at 1% hydrogen concentration. The lowest detection limit of the sensor could be achieved at 0.2% concentration, and the reversibility in colouration and recovery was demonstrated over 20 times with repeated exposures to hydrogen and air.

Zhou et al. investigated an optical fibre Bragg grating (FBG) hydrogen sensor based on Pt-loaded WO_3 in 2017, as shown in Figure 31 [136]. The grating structure was processed using a femto second (fs) laser with a wavelength of 780 nm, a pulse duration of 180 fs and a repetition rate of 1 kHz. Unlike the single spiral grating structure, this sensor exhibited a better sensing performance through processing a double spiral grating structure in FBG. The sensing mechanism was based on thermal optic changes caused by the reaction of hydrogen gas and Pt-WO_3 [137]. The wavelength shift induced by the temperature
variation correlates with the thermo-optic effect, thermo-expansion and elasto-optical effects on the optical fibre [138]:

\[
\frac{\Delta \lambda_B}{\lambda_B} = [\zeta + \alpha + (1 + p_e) \times (\alpha_{\text{film}} - \alpha)] \Delta T
\]  

(23)

where \( p_e \) is the elasto-optical coefficient, and \( \alpha \) and \( \zeta \) refer to thermal expansion and thermo-optic coefficients of fibre. Additionally, \( \alpha_{\text{film}} \) is the thermal expansion of film, \( \Delta \lambda_B \) is the Bragg wavelength, and \( \Delta T \) is the temperature change.

**Figure 30.** (a) Schematic of electrostatic spray deposition (ESD) process for fabricating WO\(_3\)-Pd sensor, (b) SEM image of deposited WO\(_3\)-Pd layer with a WO\(_3\):Pd ratio of 75:1, (c) TEM image of WO\(_3\)-Pd, and (d) optical images of sensors with WO\(_3\)-Pd ratios of 50:1, 75:1, 100:1, 125:1 and 150:1 before and after exposure to 1% hydrogen gas [131]. Copyright (2021), with permission from Elsevier.

**Figure 31.** (a) Morphology of double spiral microstructure after depositing Pt-WO\(_3\) film, (b) The cross-section diagram of Pt-WO\(_3\) film, (c) The SEM picture of nanostructure of Pt-WO\(_3\), (d) The energy-dispersive X-ray spectrometer (EDS) pattern of Pt-WO\(_3\) film [136]. Copyright (2017), with permission from OPTICA Publishing Group.
As reported in [139], the double spiral grating FBG structure sensor displayed 2–4 times improvement in H₂ sensing compared to that based on a single spiral grating FBG structure. At the optimized mole ratio of Pt:WO₃ 1:5, the sensor exhibited a higher sensitivity (522 pm% (v/v)) and faster response (15 s) at room temperature towards 1% H₂ concentration. The main reason for this improvement was the large reaction surface created by the double spiral grating and the inhomogeneous stress distribution caused by fs ablation, which increased the wavelength shift and further improved the sensor’s sensitivity.

Another promising strategy to enhance the hydrogen sensing properties of metal oxide-based sensors is to form a heterojunction with the “backbone” materials, such as SnO₂, TiO₂ or ZnO, due to their stability, low cost, and superior electrical properties. As a heterojunction is formed, a renewed charge distribution occurs accordingly, creating electron depletion in one material and electron accumulation in another. This redistribution dramatically changes the total number of charge carriers and leads to measurable improvements in the sensitivity and selectivity of the sensor.

Hu et al. synthesized ZnO-SnO₂ heterojunction nanofibers by electrospinning and plasma treatment for hydrogen sensing applications in 2020 [123]. Figure 32a,f show the surface morphology of the ZnO-SnO₂ nanofibers. For comparison, both plasma treated (optimized to 20 min) and the original samples (no plasma treatment) were exposed to 100 ppm H₂ concentration. At the optimized working temperature of 300 °C, the plasma-treated sensor exhibited better performance with a sensor response (R_a/R_g) of 18, compared to a response of about 10 for the original sensor at 330 °C (the optimized temperature for the sensor without plasma treatment) as shown in Figure 32g,h. Moreover, the response time of the plasma-treated sensor was shorter at 24 s, compared to 69 s for the untreated sensor. This kind of plasma-treated sensor can detect the H₂ concentration down to 10 ppm.

Lee et al. controlled the content of SnO₂ in their SnO₂/ZnO heterojunction hydrogen gas sensor and reported in their paper [127] that the sensors with the xSnO₂-loaded (x = 1) ZnO nanofiber also exhibited a high response (R_a/R_g = 50.1) to 50 ppb hydrogen at 300 °C. Furthermore, this kind of sensor showed an excellent selectivity towards the hydrogen gas sensor.

The hydrogen sensing mechanism has been illustrated graphically in Figure 33 from previous work in 2015 [140]. When ZnO-SnO₂ heterojunctions are exposed in the air, the adsorbed oxygen molecules from the air are on ZnO-SnO₂ grains and dissociated into oxygen ions. In particular, the chemisorption process takes place on vacant oxygen sites, which form a depletion layer in the grains, depleting their thickness, accompanied by an increase in grain resistance. When hydrogen is released, the adsorbed oxygen reacts rapidly with hydrogen. As a result, the depletion layer becomes thinner, and the resistance of grains is reduced accordingly. Meanwhile, ZnO grains are directly reduced to Zn metal, forming a metalized layer on the grain surface. This process significantly affects the potential heterojunction barriers and dramatically improves the range of resistance modulation in the ZnO-SnO₂ heterojunction.

In 2019, Lee et al. and their team investigated the heterojunction gas sensor based on Pd-functionalized In₂O₃-loaded ZnO nanofiber and synthesized by electrospinning and an ultraviolet irradiation method for hydrogen sensing applications [141]. Besides the hydrogen active Pd NPs, the sensor also employed heterojunctions like In₂O₃/ZnO, homojunctions like ZnO-ZnO and In₂O₃-In₂TablwO₃, and the Schottky junction Pd/ZnO, which all contribute to improved gas sensing performance. Sensors with an optimized mole ratio of 0.1 In₂O₃ have been reported to exhibit a high response of R_a/R_g = 172 for an ultra-low hydrogen concentration of 50 ppb at 350 °C.

A comparison of the MOS-based hydrogen sensors with their operating temperature, synthesis method, and performance parameters are presented in Table 2. Right after the table, Figure 34 schematically illustrates the temperature, response, and recovery time. Generally, MOS-based hydrogen sensors require a higher ambient operating temperature, which requires high power consumption. However, high temperature can also effectively reduce the weakening of sensor sensitivity by humidity, thus allowing the MOS sensor...
to reach a detection range of ppb level. On the other hand, the lifetime of the sensor is significantly reduced as high temperatures accelerate the fatigue of the sensing material.

Figure 32. (a,b) SEM images of ZnO–SnO$_2$ nanofibers, (c–f) images of area scan by EDS including the element content of Zn, Sn, and O. (g) Response and recovery at optimum operating temperature 300 °C. (h) Response curve with 10 ppm to 500 ppm H$_2$ concentrations at an optimum operating temperature [123]. Copyright (2020), with permission from Elsevier.

Figure 33. (a,b) SEM images of ZnO–SnO$_2$ nanofibers, (c–f) images of area scan by EDS including the element content of Zn, Sn, and O. (g) Response and recovery at optimum operating temperature 300 °C. (h) Response curve with 10 ppm to 500 ppm H$_2$ concentrations at an optimum operating temperature [123]. Copyright (2020), with permission from Elsevier.

Figure 33. The schematic diagram for explanation of sensing mechanism of ZnO-SnO$_2$ heterojunction [140]. Copyright (2015), with permission from American Chemical Society.
Table 2. Comparison of sensing performances towards hydrogen gas of metal oxide semiconductor (MOS)-based gas sensors in the literature. Unless specified, the sensor response is defined by the given Equation (1). (*) Sensor response given by the form \( R_a / R_g \). (**) The recovery times were not given directly in their publications and were approximately read out from the sensing response curves. RT: room temperature, DC: direct current.

| Ref. Nr. | Sensor Materials | Operating Temperature | Synthesis Methods | Low Detection Limit | Response/Recovery Time (Response) at \( H_2 \)% | Literature |
|----------|------------------|------------------------|-------------------|--------------------|-----------------------------------------------|------------|
| 1        | SnO\(_2\) NW     | 150 °C                 | DC sputtering     | 10 ppm             | –/– () at 1000 ppm                            | [105]      |
| 2        | SnO\(_2\) NPs    | 350 °C                 | thermal evaporation method | 400 ppm           | 11/17 s ** (4.5 V) at 400 ppm                 | [106]      |
| 3        | SnO\(_2\) NFs    | RT                     | hydrothermal method | 100 ppm            | 63/500 s (80.20%) at 1000 ppm                 | [111]      |
| 4        | Pd/ SnO\(_2\)    | 200 °C                 | solvothermal method | 10 ppm             | 4/10 s (315.34 *) at 3000 ppm                 | [87]       |
| 5        | Pd/ SnO\(_2\) Film | 175 °C                | magnetron sputtering method | 100 ppm          | 1/512 s (115.9 kHz) at 2000 ppm              | [112]      |
| 6        | Pt/ SnO\(_2\)    | RT                     | hydrothermal method, irradiated photochemical reduction method sol-gel and | 100 ppm          | 0.33/29.60 s (88.35%) at 1000 ppm            | [113]      |
| 7        | Pt/ SnO\(_2\)    | 350 °C                 | hydrothermal methods | 0.08 ppm          | 29/36 s (–60 *) at 100 ppm                   | [114]      |
| 8        | Au/ SnO\(_2\)    | 200 °C                 | hydrothermal method | 1 ppb             | 1/3 s (25 *) at 100 ppm                      | [115]      |
| 9        | Pd/ZnO NFs       | 250 °C                 | hydrothermal method, UV reduction method | 0.5 ppm          | 450/500 s (2.5 *) at 50 ppm                  | [122]      |
| 10       | ZnO              | 400 °C                 | Wet chemical method | 2000 ppm         | 5/7 s (10 *) at 2000 ppm                     | [107]      |
| 11       | ZnO rods         | 350 °C                 | —                   | 10 ppm            | 700/1100 s ** (–) at 100 ppm                 | [121]      |
| 12       | Hollow ZnO particles | 225 °C               | hydrothermal       | 2 ppm             | 139 s/>30 min ** (89%) at 100 ppm            | [125]      |
| 13       | ZnO NFs          | 350 °C                 | electrospinning    | 0.1 ppm           | 400/200 s ** (74.7 *) at 100 ppb             | [126]      |
| 14       | ZnO/ SnO\(_2\) NFs | 330 °C               | electrospinning    | 25 ppm            | 69/175 s (10 *) at 100 ppm                   | [123]      |
| 15       | ZnO/ SnO\(_2\) NFs | 300 °C               | electrospinning, Ar plasma | 10 ppm           | 24/165 s (18 *) at 100 ppm                   | [123]      |
| 16       | ZnO/0.1 SnO\(_2\) NFs | 300 °C              | electrospinning    | 50 ppb            | –/– (50.1 *) at 50 ppb                      | [127]      |
| 17       | TiO              | RT                     | reactive DC magnetron sputtering | 30 ppm            | (10\(^4\) *) at 1000 ppm                    | [128]      |
| 18       | Pt/TiO           | RT                     | pressing, sintering | 30 ppm            | 10/20 s (6000 *) at 1000 ppm                 | [129]      |
| 19       | Pt/WO\(_3\)      | RT                     | electrostatic spray deposition (ESD) fermto second laser, hydrothermal method | 0.2%             | 15 s/10 min (18.5 *) at 1%                   | [131]      |
| 20       | Pt/WO\(_3\)      | RT                     | hydrothermal method electrospinning, ultraviolet irradiation method | 0.02%            | 15/33 s (522 pm% (v/v)) at 1%                | [136]      |
| 21       | Pd/0.1In\(_2\)O\(_3\)/ZnO | 350 °C               | —                   | 50 ppb            | –/– (172 *) at 50 ppb                       | [141]      |
4. Graphene and Its Derivatives-Based Hydrogen Gas Sensors

As mentioned in the previous sections, despite several advantages of the Pd based hydrogen gas sensors, there are also disadvantages, for example, high cost for low H\(_2\) concentrations (less than 1\%). The Pd-film sensor has a long response time. For high H\(_2\) concentrations (more than 2\%), the Pd lattice expansion leads to the Pd film buckle or collapse, making the sensor unstable, irreversible, and unreliable [23]. For Pd-nanostructure sensors like nanowires, and nanocomposites, the very low conductance of these discontinuous nanostructures induces a high electrical noise, degrading the sensor response. In contrast, as another promising hydrogen gas sensor, most of the typical commercial MOS-based sensors have cost limitations, such as high power consumption, rare sensitivity in ppb level, limited lifetime, poor selectivity and repeatability, and difficult miniaturization. Therefore, graphene(G) and its modified derivatives have been employed as promising special materials to enhance the sensing performance due to their unique features.

Graphene has attracted attention continuously for decades [142]. Graphene has been acknowledged as a novel material for sensor applications due to its high surface-to-volume ratio, specific large surface area, fast electron-transfer kinetics, and remarkable carrier mobility [138,143–147]. Its high carrier mobility ensures the desired low electrical noise, fast response, high sensitivity, and low energy consumption [138,145]. However, the pristine graphene sheets cannot be applied directly to the hydrogen sensor [148] because pure graphene has no bandgap (see illustration in Figure 35) nor functional groups on its surface for gas adsorption, thus presenting a low adsorption behaviour. Therefore, it is suggested that functional graphene or its derivatives are combined with other substances like transition metals, metal oxide semiconductors (MOS), or even polymers in sensing applications.

As one of the derivatives of graphene, graphene oxide (GO) is mainly fabricated by a modified Hummers method via oxidizing from graphite [150], which creates different functional groups and defects (it is much easier to obtain GO using a wet chemical method from graphite as compared to producing pure graphene). These newly gained groups are located on its basal plane and edges: carboxyl (−OOH), epoxy (−O) and hydroxyl (−OH) [151,152]. Since π-bonding is weak due to its low formation energy, numerous disorder-induced localized states can present in the band tail of the π−π\(^*\) gap. With these functional groups, the electric structure of graphene changes, and a bandgap of about 2.2 eV can be achieved [149]. The sensitivity and repeatability of a sensor depend a lot on the amount of oxygen functional groups on the GO’s surface. However, the content of the oxygen functional groups is difficult to control during the synthesis process [153].
4. Graphene and Its Derivatives-Based Hydrogen Gas Sensors

As mentioned earlier, there are also disadvantages, for example, high cost for low H₂ concentrations (less than 1%). The Pd-film sensor has a long response time. For high H₂ concentrations (more than 2%), the Pd lattice expansion leads to the Pd film buckle or collapse, making the sensor unstable, irreversible, and unreliable [23]. For Pd-nanostructure-based sensors like nanowires, and nanocomposites, the very low conductance of these discontinuous nanostructures induces a high electrical noise, degrading the sensor response. Therefore, graphene (G) and its modified derivatives have been employed as promising special materials to enhance the sensing performance due to their unique features, like high carrier mobility and high sensitivity. Therefore, graphene oxide (GO) and reduced graphene oxide (rGO) [149]. Copyright (2018), with permission from Nature Publisher Group.

Due to the presence of the oxygen functional group, GO is by nature insulating. However, the electrical conductivity can be improved by removing some oxygen functional groups via a controlled reduction process and keeping some oxygen functional groups to limit electron transport. GO can be converted to another graphene derivative, reduced graphene oxide (rGO), by using a chemical reduction method. The bandgap of rGO varying between 1 eV to 1.69 eV depending on the degree of reduction [154–156]. The removal of some oxygen groups allows the bandgap to be adjusted during the reduction process, so that the oxygen presenting in rGO can be further engineered. Therefore, rGO behaves like a semi-metal or semiconductor, and its electrical conductivity can be tuned by controlling its oxygen content [155].

4.1. Transition Metals/Graphene Combinations

Knowing that graphene lacks active sites, Shao and Hayasaka et al. investigated a crumpled graphene structure-based stretchable gas sensor for hydrogen sensing [157]. The chemical vapour deposition (CVD)-grown monolayer flat graphene is first transferred on a substrate made of elastomer polymer during its fabrication. This substrate has a pre-strain of about 200% in both the x and y-direction. After the deposition of gold or palladium (Au/Pd) electrodes, it is interesting that the substrate releases pre-strain and crumples up accompanying the transferred graphene. Subsequently, this process increases the contact area, distorts π bonds and strengthens the interaction of the Au/Pd deposited surface with gas molecules. This deposition of Au/Pd electrodes works like an enhancement, and this material-based sensor has a sensitivity of 0.58% at room temperature surrounded by 0.1 vol% hydrogen concentration. It has a better sensitivity than the flat graphene on SiO₂-based sensor, which has a sensitivity of 0.18%, as reported in [157]. Another derivative to improve the sensitivity of graphene towards hydrogen is the nanoporous graphene oxide (NGO). The work [158] found that the NGO has a large surface, high content of oxygen functional groups (hydroxyl, epoxy, carbonyl, and carboxyl groups) and high electric conductivity. Shaban et al. in [159] fabricated NGO film by a modified Hummer method followed by a spray pyrolysis method for hydrogen sensing application at room temperature. During its characterization, a hydrogen gas flew at 60 SCCM (standard cubic centimetres per minute) for 5 min, the nanoporous sensor has a faster response/recovery time of 100 s/437.2 s with a sensitivity of 16.16% compared to those using pure graphene [157]. However, the selectivity of this kind of NGO gas sensor is relatively
low, since the sensitivity of CO₂ sensing surrounded by a particular concentration of released gas is higher than its sensitivity towards hydrogen [157]. Compared with graphene and its derivatives, rGO has been proved to have a better response by Wang et al. [160]. The rGO-based hydrogen gas sensor is fabricated on a micro-hotplate by dielectrophoresis (DEP) and has a good sensitivity of around 6% with a relatively fast response and recovery time of 11 s/36 s for 200 ppm hydrogen at room temperature. However, when the working temperature increases to 300 °C, the sensitivity of the rGO gas sensor could approach a higher value of about 17% towards hydrogen, and the response time is around 1 s, much faster than at room temperature.

Since Pd nanoparticles have superior hydrogen solubility at room temperature [144, 161], decoration using Pd nanoparticles can induce a change of work function of Pd with low noise and low energy consumption, thus changing the electron mobility of the Pd nanoparticles-decorated sensor [26,162–165]. In [162], Tang et al. developed a hydrogen detection gas sensor based on Pd nanoparticles-decorated graphene at room temperature, where Pd nanoparticles act as reaction sites for H₂ absorption and graphene as an electron pathway. Without releasing hydrogen, the work function of the Pd nanoparticle is larger than that of the CVD fabricated graphene [166,167], as shown in Figure 36a. This difference led to electron transfer from graphene to Pd nanoparticles. Increased hole density in graphene improves the conductivity and reduces the resistance of graphene [168]. When the gas sensor is exposed to hydrogen, the work function of the hydride PdHₓ formed has a lower work function of 3.2 eV than that of Pd [30], leading to a decrease in the hole density in graphene and hence an increase in its resistance, as shown in Figure 36b. This sensor has an extended response and recovery time of 3 min and 9 min, respectively, with a sensitivity of 5.88%. In order to improve the sensing response, Yokoyama et al. developed hydrogen sensors with suspended graphene films functionalized with Pd nanoparticles [164], which introduced self-heating changes in sensor performance. The suspended graphene film also avoids heat transfer to the substrate. With a low power consumption per unit graphene width of 0.93 mW/µm, graphene can create a working temperature of up to 180 °C.

![Figure 36. Energy band diagrams (a) for Pd decorated graphene and (b) for PdHₓ and graphene [162]. Copyright (2019), with permission from Nature Publisher Group.](image)

The sensor achieves a fast response to hydrogen with a response time of 15 s at 100 ppm hydrogen concentration. For the same purpose, Sharma et al. functionalized graphene with Pd–Ag alloy nanoparticles in their dual-gate field-effect transistor (FET) [165]. The study [169] showed that the Pd–Ag alloy nanoparticles could improve mechanical stability, hardness, chemical inertness and hydrogen permeability. The working temperature can be tuned between 25 and 254.5 °C, employing an external micro heater Pt. At 245 °C, the sensor has a rapid response time of 16 s and recovery time of 14 s at 1000 ppm hydrogen concentration, and a low detection limit at around 1 ppm is observed.

With the application of reduced graphene oxide (rGO), Mohammadi et al. in [170] investigated Pd-decorated crumpled rGO balls for hydrogen detection at room temperature by using a flame technology [171]. A rapid, continuous high-temperature reducing jet...
In recent years, since sensitive polymers have attracted interest in gas sensing research, PANI-based sensors have also been expanded to hydrogen detection by combining PANI with other nanomaterials [174,175]. Zou et al. developed a gas sensor with PANI-rGO composite doped with Pd nanoparticles [176]. Figure 38a–f present images of material blending from rGO to Pd-PANI-rGO. As shown in Figure 38, the pure PANI forms short rod-like agglomerates with an average diameter of about 80 nm before being compounded with rGO in Figure 38d. In principle, similar to rGO, the PANI-rGO exhibits p-type behaviour [177], with electron transfer from PANI-rGO to Pd resulting in a modified level charge-neutrality at the Pd-PANI-rGO interface [178]. Due to the lower chemisorption work function of PdHx formed by the release of hydrogen than that of PANI-rGO, electron transfers from PANI-rGO to PdHx decrease and the resistance of the PANI-rGO surface increases. Figure 38e demonstrates the sensing response of PANI, PANI-rGO, and Pd-PANI-rGO in an environment with 1% H2 concentration at room temperature, which shows that Pd-PANI-rGO is significantly more sensitive towards hydrogen (~25%) due to its enhanced gas diffusion capability and the high H2 absorption capability of Pd. In Figure 38f, the hydrogen sensing response of the Pd-PANI-rGO based sensor was tested in various H2 concentrations at room temperature. A low detection limit of 0.01% H2 concentration was reported. At an H2 concentration of
1%, the response time and recovery time of the Pd-PANI-rGO based sensor were 20 s and 50 s, respectively. In their study, Zou et al. compared the sensing performance towards different gases (CH$_3$OH, CO$_2$, H$_2$S) and further demonstrated the remarkable selectivity of the Pd-PANI-rGO sensor towards hydrogen.

Despite research investigating the chemi-resistive graphene-based hydrogen gas sensor, which achieved promising sensing performance, there have also been studies focusing on a Pd-decorated graphene-based optical gas sensor for hydrogen sensing application. For instance, Ma et al. in [163] demonstrated a miniature fibre-optic hydrogen sensor with Pd-decorated multilayer graphene (MLG), synthesized by the CVD method. This Pd/MLG film covered the air cavity at the optical fibre tip, forming a flexible Fabry–Pérot (FP) interferometer, as shown in Figure 39a. During H$_2$ Adsorption, the expanded Pd lattice causes stretching and defects in the Pd/MLG film, reducing the length of the FP cavity and leading to a wavelength shift in the reflection spectrum within the cavity. Figure 39b presents the response of the MLG coated with a 5.6 nm-thick Pd film and exposed to a range of hydrogen concentrations up to 3%. A low detection limit of ~200 ppm can be achieved, and a wavelength shift of ~50 pm/ppm is induced. At an H$_2$ concentration of 0.5%, the sensor can respond to H$_2$ within ~18 s.

For further enhancement of the gas sensing performance, Shin et al. developed graphene decorated with flower-like Pd nanoclusters (FPNC) by treating it with 1,5-diaminonaphene (DAN) [179], as shown in Figure 40. Due to expanded reactive sites, the gas sensor achieved an ultra-low hydrogen detection limit of 0.1 ppm at room temperature. The decorated graphene was transferred to a flexible polyethylene naphthalate (PEN) film, used as the sensor substrate. The gas sensor was, therefore, mechanically stable and stretchable. Even after 100 bending cycles, the sensing response decreased by only 2%.
For further enhancement of the gas sensing performance, Shin et al. developed graphene-based hydrogen gas sensors with a 5.6 nm Pd film for various H\textsubscript{2} concentrations [163].Copyright (2019), with permission from Royal Society of Chemistry.

Figure 39. (a) Schematic of a fibre-optic H\textsubscript{2}-sensor with Pd-decorated MLG film, and (b) temporal response of the Pd/MLG sensor with a 5.6 nm Pd film for various H\textsubscript{2} concentrations [163]. Copyright (2019), with permission from Royal Society of Chemistry.

Figure 40. (a) Illustrative diagram for the fabrication steps of flower-like Pd nanoclusters (FPNCs) on chemical vapour deposition (CVD) graphene electrode. (b) Normalized resistance changes upon sequential exposure to H\textsubscript{2} gas of various concentrations (0.1 to 100 ppm) at room temperature, and (c) response time and rate (inset) vary with H\textsubscript{2} concentration [179]. Copyright (2015), with permission from Nature Publisher Group.

In a similar effort to obtain a flexible gas sensor, Zhu et al. developed a biomimetic gas sensor based on 3D porous laser-induced graphene (LIG) decorated with Pd nanoparticles for hydrogen sensing at room temperature, inspired by the turbinate structure of the dogs' olfaction system [180]. Figure 41a shows the synthesis process of a LIG-gas sensor (LIG-GS) on PI substrate and a transferred LIG-gas sensor (TLIG-GS) on PET substrate. Pd nanoparticles were decorated on the sensing surface using an e-beam evaporation process (Figure 41b). As illustrated, LIG-GS was decorated with an e-beam evaporation process directly after the formation of the turbinate graphene, but the TLIG-GS was treated with UV light exposure before the LIG microstructure was transferred onto the PET substrate. Figure 41e shows an SEM image of the 3D porous structure of the LIG, and Figure 41f presents a cross-sectional image of TLIG with a PET substrate. As reported, with the decorated Pd nanoparticles, the sensitivity of LIG-GS was on average 20% higher than that of TLIG-GS. At 1% H\textsubscript{2} concentration, the sensing response of LIG-GS was ~3.2%, with a response time of ~6 min and a recovery time over 20 min.
As the summary of this section, current research based on graphene and its derivatives or their combinations with transition metal nanoparticles is listed and compared in detail in Table 3. As shown in the table, the graphene and its derivatives-based sensors operate mainly at room temperature, which allows for power consumption. Even sensors operating at high temperatures require a much lower power consumption than that of the transition metal-based hydrogen gas sensors in Table 1 since their maximal operating temperature is below 260 °C [165]. That difference can be observed more clearly by comparing the sensing combinations of both graphene and MOS materials in the following section. Secondly, due to the excellent chemical and physical properties, the graphene (e.g., GO, rGO)-based sensors have been proved experimentally by exhibiting a better electrical conductivity, which leads to fast sensor response and equal response/recovery time, as shown in Figure 42.

Figure 41. (a) The fabrication process of the laser-induced graphene gas sensor (LIG-GS) and transferred LIG-gas sensor (TLIG-GS). (b) Schematic of Pd NPs on LIG-GS and TLIG-GS. (c) Transferred line pattern of 3D porous LIG. (d) Image of bendable TLIG-GS. (e) Morphology of TLIG and (f) cross-sectional image of TLIG [180]. Copyright (2019), with permission from American Chemical Society.

Figure 42. Regarding Table 3, schematic illustrations of the comparison of the reported: (a) low detection limits. The x-axis “Reference Number” represents the 1st column“Ref. Nr.” in Table 3. (b) Response time/recovery time under experimental conditions in literature.
Table 3. Comparison of sensing performances towards hydrogen gas of the transition metal/graphene (e.g., GO, rGO)-based gas sensors in literature. Unless specified, the sensor response is defined by Equation (1). RT: room temperature, CVD: chemical vapour deposition, HTRJ: high-temperature reducing jet.

| Ref. Nr. | Sensor Material | Operating Temperature | Method | Low Detection Limit | Response/Recovery Time (Response) at H₂ | Literature |
|----------|----------------|-----------------------|--------|---------------------|----------------------------------------|------------|
| 1        | G              | RT                    | CVD, e-beam evaporation Modified Hummer | 200 ppm | 1/3 min (−) at 0.1% | [157]     |
| 2        | GO             | RT                    | method and spray pyrolysis method Modified Hummers’ method | 60 sccm | 100/437.2 s (16.16%) | [159]     |
| 3        | rGO            | RT                    | CVD, e-beam evaporation Modified Hummer | 200 ppm | 11/36 s (6%) at 200 ppm | [160]     |
| 4        | Pd/G           | RT                    | CVD | 1% | 3/9 min (5.88%) at 1% | [162]     |
| 5        | Pd/rGO         | RT                    | HTRJ process | 25 ppm | 73/126 s (14.8%) at 2% | [170]     |
| 6        | Pd/G           | RT                    | CVD, dip-coating process Exfoliation, Soft lithography | 200 ppm | 18/300 s (−) at 0.5% | [163]     |
| 7        | Pd/G           | 180 °C                | Deposition | 10 ppm | 15/16 s (−) at 100 ppm | [164]     |
| 8        | Pd/G           | 254 °C                | Polymer-assisted hydrothermal (HT) method | 1 ppm | 16/14 s (−) at 1000 ppm | [165]     |
| 9        | PMMA/Pd/G      | RT                    | CVD | 250 ppm | 6/7 s (−) at 1% | [185]     |
| 10       | Pd/GO          | RT                    | CVD | 0.5% | 6/7 s (−) at 1% | [181]     |
| 11       | Pt/G           | 200 °C                | Modified Hummers’ method | 10 ppm | 9/10 s (−) at 1% | [182]     |
| 12       | PEDOT:PSS/GO   | RT                    | Modified Hummers’ method | 30 ppm | 30/25 s (4.2%) at 100 ppm | [183]     |
| 13       | Pd/PANI/rGO    | RT                    | Chemical reduction | 100 ppm | 20/50 s (25%) at 1% | [176]     |
| 14       | Pt/G           | RT                    | Hummers’ method | 500 ppm | 0.97/0.92 s (1.6%) at 1% | [184]     |
| 15       | Pt/rGO         | 50 °C                 | Modified Hummers’ method | 0.3% | 63/104 s (−) at 0.5% | [185]     |
| 16       | Pt/rGO         | RT                    | Modified Hummers and Offman method | 1 ppm | −/− | [186]     |
| 17       | Pd/Ag/G        | 70–190 °C             | Spin Coating, Sputter | 100 ppm | 56 s/− (15.23%) at 500 ppm | [187]     |
| 18       | Pd/G           | RT                    | CVD | 0.1 ppm | 12/15 s (−) at 100 ppm | [179]     |
| 19       | Pd/LIG         | RT                    | Laser-induced graphene (LIG) | 600 ppm | 6/20 min (−) at 1% | [180]     |

4.2. Metal Oxide Semiconductor (MOS)/Graphene Combinations

Besides the hydrogen sensors based on transition metal-doped graphene and its derivatives, the combination of graphene (e.g., GO, rGO) with doped MOS particles offers other new possibilities to improve hydrogen detection in gas sensing applications [188–209]. Many work groups investigated the combination of graphene with n-type MOS such as ZnO [188], SnO₂ [197,199], WO₃ [208,209] and p-type MOs like NiO [196] in combinations with graphene oxide [189] and reduced graphene oxide. These enhancements can significantly improve the sensitivity and selectivity while reducing operating temperature [190–195] due to the existence of the functional groups and defects mentioned earlier. Because of the p-type property of graphene and its derivatives, the combinations with MOS x essentially forms a heterojunction, and thus they exhibit heterojunction charge transfer properties during gas absorption and desorption processes. For better selectivity towards the hydrogen, the deposition of transition metal nano components (e.g., Pd, Pt, Au, Ag, and Ni) has been used to functionalize further MOS/graphene gas sensors, and significant improvements have been achieved as in the results of [192,193,197,198,206,208,209].

Among the semiconductor metal oxide, ZnO nanostructures are widely used to functionalize graphene [188], graphene oxide [189] and reduced graphene oxide [191,192], aiming for a better gas sensing performance. Such combinations can improve the sensitivity [188–192] and reduce the working temperature [189,190]. For instance, Galstyan et al. reported in [188] that the ZnO/rGO composites responded 40–50% better to H₂.
at temperature 200 °C compared to pure ZnO sensors. As a further improvement, the transition metals like Pd, Pt, Ag were deposited on the ZnO/rGO gas sensors [192,193,197]. Innovatively, Ni-doped ZnO sensors decorated with reduced graphene oxide (rGO) for hydrogen sensing at 150 °C were investigated by Bhati et al. in [198]. As shown in Figure 43a, the Ni-doped ZnO nanoparticles were synthesized using the RF sputtering method, while rGO was synthesized using Hummer’s method. The purpose of Ni-doping is to create more active sites for the chemisorption of oxygen, thereby enhancing the sensing response at lower operation temperatures [210]. Since rGO (p-Type) and ZnO (n-Type) have different MOS types, a Schottky heterojunction is formed at the rGO/ZnO interface. As illustrated in Figure 43c, rGO has a more extensive work function than Ni-doping ZnO. Since rGO has a smaller bandgap, which makes it behave like a metal, the contact with ZnO generates a Schottky barrier at the heterojunction [200,201] due to the electron transfer from ZnO to rGO at the interface. As a result, it forms a thick depletion layer between ZnO and rGO, accompanied by a decrease in total carrier concentration and an increase in resistance. When these heterojunctions are exposed to the air, electrons are extracted from the conduction band to form oxygen ions adsorbed on the sensor surface, thus increasing the thickness of the depletion layer at the heterojunction interface, which also leads to the increase of the Schottky barrier, as shown in Figure 43d. As hydrogen is filled into the test environment, the hydrogen molecules react with the oxygen ions adsorbed on the sensor surface, and release electrons back into the heterojunction (Figure 43b), which causes the Schottky barrier to decrease, and the depletion layer to become thinner. As a consequence, the total carrier concentration rises, and the resistance falls.

Figure 43. (a) SEM image of Ni-doped ZnO nanostructure and 0.75 wt% rGO loaded ZnO. (b) Schematic diagram of the gas sensing mechanism in the presence of hydrogen. (c–e) The band diagram illustration of rGO/ZnO heterojunction before contact and after contact in air and hydrogen [198]. Copyright (2018), with permission from American Chemical Society.

As shown in Figure 44a, this heterojunction-based hydrogen gas sensor has a low detection limit of 1 ppm with a relative response of about 30% at the test temperature (150 °C), for a 0.75% wt% rGO-loaded sensor and a response time as fast as 28 s. This heterojunction-based hydrogen gas sensor has, surprisingly, a lower detection limit of 1 ppm with a relative response of about 30% at test temperature for 0.75% wt% rGO loaded sensor and fast response time 28 s, as shown in Figure 44a. Moreover, the sensor has also
better selectivity for hydrogen compared to pure ZnO [109]. The optimal rGO concentration was found at 0.75 wt% H₂ concentration, as shown in Figure 44b.

Zhang et al. investigated a 2D material for a hydrogen sensor functionalized with copper oxide (CuO) nanorods deposited on the top and bottom surfaces of rGO, forming a sandwich nanostructure as shown in Figure 45a [202]. CuO is a p-type semiconductor with a bandgap of about 1.2–1.9 eV and is reported in many gas sensor applications [203,211]. The reduced graphene oxide layer provided inherent chemical defects and functional groups, while CuO nanorods can efficiently prevent rGO nanosheets’ aggregation and generate more active sites. This CuO-rGO-CuO hybrid film sensor exhibits excellent response with a low detection limit and high sensitivity at room temperature, as Figure 45b demonstrates. At various hydrogen concentrations from 10 to 1500 ppm, the response time and recovery time were observed to be less than 80 and 60 s, respectively, and the sensitivity increased from 1% (10 ppm) to 12% (1500 ppm).

Figure 44. (a) Relative response of a 0.75 wt% rGO loaded sensor at an operating temperature of 150 °C with increasing gas concentration from 1 ppm to 100 ppm. (b) Selectivity histograms for pristine and rGO-loaded sensors with Ni-doped ZnO nanostructures [198]. Copyright (2018), with permission from American Chemical Society.

Figure 45. (a) Structure illustration of CuO-rGO-CuO hydrogen sensor, and (b) response–recovery curves for various concentrations of hydrogen [202]. Copyright (2017), with permission from Springer.
Peng et al. in [206] compared two hydrogen sensors based on Pd/rGO and Pd/SnO$_2$/rGO. The Pd/SnO$_2$/rGO nanocomposites-based sensor exhibited higher sensitivity and faster response to H$_2$ gas compared to the Pd/rGO based sensor. Over a range of H$_2$ concentrations from 100 ppm to 10,000 ppm, the Pd/SnO$_2$/rGO-based sensor has an approximate 50% advantage in response and is about 10% faster in response time and recovery time. Similarly, Dhall et al. investigated Pd-SnO$_2$ nanocomposites on a graphene surface in [197] and reported that the sensing response of Pd/SnO$_2$/G was significantly higher than that of Pd/G (~70% advantage) and SnO$_2$/G (~30 times advantage) at room temperature. Both Pd/SnO$_2$/rGO in [206] and Pd/SnO$_2$/G in [197] have good sensitivity, but the sensing response of the Pd/SnO$_2$/G-based hydrogen gas sensor is faster than the other. The possible reason for this is that graphene has better conductivity than reduced graphene oxide due to its functional groups and defects.

Since its two-dimensionality, high optical transmittance and electrical conductivity, graphene sheets can also be used as an active layer for electrons/holes separation [212,213] and optoelectronic hydrogen sensing [209]. Chen et al. reported in [209] an optoelectronic hydrogen sensor based on a gasochromic Pd-loaded WO$_3$ (Pd-WO$_3$) film and a graphene/Si heterojunction structure, as shown in Figure 46a. However, when Pd-WO$_3$ was exposed to a hydrogen gas test environment, it absorbed light through the intraband absorption due to the formation of H$_2$WO$_3$, reducing the light transmittance of the film [214]. When the sensor was exposed to hydrogen gas (4% H$_2$/Ar mixed gas) and a 10 mW laser with a wavelength of 980 nm, it had rapid response and recovery time as reported. This optoelectronic hydrogen sensor has a low detection limit at room temperature, even down to 0.05 vol%. Furthermore, as shown in Figure 37b, it exhibits good repeatability, improving the sensor’s stability and lifetime.

![Figure 46. (a) Schematic of the optoelectronic Pd-WO$_3$/Graphene sensor. (b) Cyclic performance of the device [209]. Copyright (2018), with permission from Elsevier.](image-url)

Table 4 shows a list of comparisons of the sensing performance of several current MOS/graphene (e.g., GO, rGO)-based hydrogen gas sensors. The critical parameters, such as low detection limits, operating temperature, response/recovery time, are illustrated in Figure 47 schematically. Despite their high operating temperature, the power consumption is significantly lower than that of the MOS-based gas sensor because the maximal operating temperatures are mainly lower than 250 °C. Additionally, graphene’s unique physical and chemical properties (e.g., GO, rGO) improved the sensing response both in response/recovery time and selectivity.
Table 4. Comparison of sensing performances towards hydrogen gas of metal oxide semiconductor (MOS)/graphene (e.g., GO, rGO)-based gas sensors in literature. Unless specified, the sensor response is defined by the given Equation (1). (*) Sensor response given by the form $R_s/R_0$. (**) The recovery times were not given directly in their publications and were read out approximately from the sensing response curves in the corresponding literature. RT: room temperature, CVD: chemical vapour deposition.

| Ref. Nr. | Sensor Material | Operating Temperature | Method | Low Detection Limit | Response/Recovery Time (Response) at H2% | Literature |
|----------|-----------------|-----------------------|--------|---------------------|----------------------------------------|------------|
| 1        | ZnO/G           | 150 °C                | Hummer’s method | 200 ppm | 22/90 s (3.5 %) at 200 ppm | [188] |
| 2        | ZnO/GO          | RT                    | simple wet-chemical coating technique | 4 ppm | 114/30 s (3.42 %) at 1000 ppm | [189] |
| 3        | ZnO/rGO         | RT                    | Electrochemical exfoliation | 100 ppm | 21.04/47.09 s (484.1 % %) at 100 ppm | [190] |
| 4        | ZnO/rGO         | 250 °C                | Modified Hummers method [C23] | 100 ppm | –/ – (30%) at 500 ppm | [191] |
| 5        | ZnO/Ag/Pd/rGO   | 150 °C                | Modified Hummers method | 100 ppm | 10/14 s (59%) at 100 ppm | [192] |
| 6        | ZnO/rGO         | 150 °C                | Modified Hummers method | 100 ppm | 33/19 s (46%) at 100 ppm | [192] |
| 7        | Ag/ZnO/rGO      | 150 °C                | Modified Hummers method | 100 ppm | 45/27 s (51%) at 100 ppm | [192] |
| 8        | ZrO2/ZnO/rGO    | 150 °C                | Modified Hummers method | 100 ppm | 15/16 s (52%) at 100 ppm | [192] |
| 9        | Pt/ZnO/rGO      | 100 °C                | Modified Hummers method | 50 ppm | 12/412 s (99%) at 400 ppm | [193] |
| 10       | SnO2/rGO        | 80 °C                 | Modified Hummers method | 1000 ppm | 15/61 s (15.8%) at 1000 ppm | [195] |
| 11       | Pd/SnO2/G       | RT                    | CVD | 2% | 50/100 s (11%) at 2% | [197] |
| 12       | SnO2/G          | RT                    | CVD | 2% | 18/12 s (0.35%) at 2% | [197] |
| 13       | Ni/ZnO/rGO      | 150 °C                | Hummer’s method | 1 ppm | 28/320 s (63.8%) at 100 ppm | [198] |
| 14       | CuO/rGO         | RT                    | Thermal heating from GO at 180 °C | 50 ppm | 80/60 s (12%) at 1500 ppm | [202] |
| 15       | TiO2/G          | 125 °C                | Hummers’ chemical method | 5000 ppm | 16/61 s (18%) at 5000 ppm | [204] |
| 16       | MoS2/rGO        | 60 °C                 | Modified Hummers method | 200 ppm | 261/260 s (15.6%) at 200 ppm | [205] |
| 17       | Pd/SnO2/rGO     | RT                    | Modified Hummers method | 100 ppm | 600 s / >2000 s ** (55%) at 10,000 ppm | [206] |
| 18       | SnO2/rGO        | 60 °C                 | Modified Hummers method | 200 ppm | 119.6 s/265 s (19.6%) at 1000 ppm | [207] |
| 19       | Pd/WO3/rGO      | 100 °C                | Modified Hummers method | 100 ppm | 52/35 s (150 %) at 500 ppm | [208] |
| 20       | Pd/WO3/G        | RT                    | CVD-Method | 0.1% | 13/43 s(90%) at 4% | [208] |

Figure 47. Regarding to Table 4, schematic illustrations of the comparison of the reported: (a) low detection limits. The x-axis “Reference Number” represents the 1st column “Ref. Nr.” in Table 4. (b) Response time/recovery time under experimental conditions in literature.
5. Conclusions

Nanotechnology- and nanostructure-based hydrogen gas sensors were reviewed in this article, and in particular their unique sensing mechanisms, operating environments, and sensing responses.

With ongoing technological developments in nanotechnology and synthesis methods, several materials have been employed as the sensing materials, such as conventional approaches like transit metals, metal oxide semiconductors and their combinations, and new materials like graphene and its derivatives. Furthermore, innovative nanostructures and nanocomposites are investigated in many pieces of research to improve the sensing performance and stability due to high safety requirements in hydrogen energy-based facilities and vehicles avoiding hydrogen leakages and explosion hazards.

The conventional materials, like the nanostructured transit metals or MOS, have been synthesized and dispersed on the sensor surfaces, which on the one hand reduces the power consumption and increases the sensing response. On the other hand, however, it can lead to low conductivity, inhomogeneity of hydride reaction, and noise in the sensing signals. Moreover, the requirement of an external heater for MOS to maintain high operation temperatures also means high energy consumption and thermal safety problems. Thus, other material is required to form a highly conductive surface or pathways for electrons transition during the sensing process. Transition metal oxides such as RuO$_2$, NiO, MnO$_2$, Co$_3$O$_4$, and SnO$_2$ are being studied continuously as candidate materials for gas sensing, and the metal oxide nanostructures such as SnO$_2$, ZnO and Cu$_2$O nanowires or nanorods with heterojunction structures show high sensitivity to various gases.

In comparison, graphene and its derivatives have the advantage of high sensitivity, low detection limit, and facile operation at low temperatures. Their unique structures and electronic properties also ensure high electron mobility and low electronic noise. With the help of CVD methods, the functional groups on their surfaces can be modified and engineered for sensing target gas molecules even at ppm/ppb levels. These advantages are generating a trend in the application of novel materials for nanoscale sensing performances. The application of graphene and its derivatives (e.g., GO, rGO) provides a new millstone in research towards nanoscale structures or clusters in gas sensing, achieving significant electrical conductivity and sensing selectivity through graphene functionalization. However, most research announcements fail to deliver adequate information on the chemical stability of graphene-based materials working under specific conditions required by chemical processes that occur in the sensing layer. Notably, there are still not many reliable graphene-based hydrogen leakage sensors available in the market that meet industry safety requirements.

Generally, nanomaterials-based gas sensors have obvious advantages:

1. Very high surface-to-volume ratio. Large exposed surfaces of sensing materials ensure a high density of defects for possible improvement of electron transfer, such as vacancies or dangling bonds. As reported in many works, certain optimized particle sizes can raise the sensing performance of the nanomaterial-based gas sensor;

2. The operating temperature of nanomaterials-based gas sensors is lower than traditional gas sensors based on bulk materials because of adsorption sites created by dangling bonds on the surface;

3. The unsatisfied bonds on the surface of nanosized materials also enable the surface functionalization and activation towards the target gas in sensing applications, which allows precise control and surface engineering methodologies to enhance the sensing performance in a wide range.

In conclusion, nanotechnology- and nanocomposite-based materials enable an ideal platform for hydrogen gas sensing and other sensing applications. The remarkable advantages encourage innovative sensor designs focusing on increasing catalytic activity, adsorption/desorption parameters, reducing operating temperatures, rapid sensing response, and improving sensor performance. In-depth research and understanding of the influence of the size-effect of nanomaterials on physical and chemical properties modifica-
tions can help us develop more effective methodologies in surface activation and surface functionalization in order to improve the operation of gas sensors.

**Author Contributions:** Conceptualization, B.W., L.S. and H.-D.N.; methodology, B.W.; formal analysis, L.S.; investigation, B.W.; resources, B.W., L.S. and H.-D.N.; data curation, B.W.; writing—initial draft preparation, B.W. and L.S.; writing—review and editing, M.S.-R. and K.-D.L.; visualization, B.W.; supervision, H.-D.N.; project administration, B.W.; funding acquisition, H.-D.N. All authors have read and agreed to the published version of the manuscript.

**Funding:** This research received no external funding.

**Conflicts of Interest:** The authors declare no conflict of interest.

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