Preparation of a magnetic reduced-graphene oxide/tea waste composite for high-efficiency sorption of uranium

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The preparation and application of adsorptive materials with low cost and high-efficiency recovery of uranium from nuclear waste is necessary for the development of sustainable, clean energy resources and to avoid nuclear pollution. In this work, the capacity of tea waste and tea waste hybrids as inexpensive sorbents for uranium removal from water solutions was investigated. Composites of graphene oxide (GO) and tea waste (TW) exhibited a promising adsorption performance for uranium from aqueous solutions. The composites GOTW and magnetic rGO Fe3O4/TW show high adsorption capacities (\( Q_m (TW) = 91.72 \) mg/g, \( Q_m (GOTW) = 111.61 \) mg/g and \( Q_m (rGO/Fe3O4/TW) = 104.95 \) mg/g) and removal rates (~99%) for U(VI). The equilibrium sorption of the adsorbents fitted well to the Langmuir model, and the sorption rate fitted well to a pseudo-second-order kinetic model. The thermodynamic parameters indicated that sorption was spontaneous and favourable. The prepared adsorbents were used for the removal of uranium from real water samples as well. The results revealed that GOTW and rGO/Fe3O4/TW can be used to remediate nuclear industrial effluent as a potential adsorbent.

To significantly reduce the emission of the greenhouse gas CO2 from burning fossil fuels and avoid air pollution-related deaths, nuclear power from fission currently accounts for ~10% of the global electricity supply. Uranium is the main nuclear fuel of fission power reactors. However, uranium released into the environment and water results in serious hazards for various organisms, including humans, due to its high chemical toxicity, radioactivity and long half-life. The US Environmental Protection Agency has established a maximum contaminant level for uranium in drinking water to be 30 \( \mu \)g/L. Consequently, researchers have investigated methods for the efficient removal and recovery of uranium from aqueous solutions to protect the environment and control nuclides pollution. At present, various methods have been developed to address uranium in water, including membrane separation, photoelectrochemical reduction, biological treatment, solvent extraction, ion exchange and adsorption. Adsorption is the most extensively used approach for uranium removal because of its high efficiency, low cost, simple operation and low production of secondary pollution.

Different types of adsorbents have been successfully used for uranium removal from aqueous solutions, including natural polymers, inorganic compounds, carbon nanomaterials, metal–organic frameworks and biomass. The economy of the adsorbents used is of great importance to reduce wastewater treatment costs. Many researchers have focused on the removal of various pollutants by low-cost adsorbents derived from agricultural wastes. The re-utilization of agricultural wastes is increasingly becoming a significant concern due to their unique structures and outstanding physicochemical properties.

Tea has been the most widely consumed beverage in many countries due to its reported positive health benefits. The largest amount of production and consumption of tea is in China. The large amount of tea waste (TW) produced each year will inevitably result in severe environmental problems if not fully utilized. Tea leaves contain an abundance of active chemical constituents, including flavonoids, phenolic compounds, alkaloids and methylxanthines. Additionally, TW has several salient advantages such as being inexpensive, easy to handle and having wide availability. Therefore, it is necessary to take full advantage of TW to avoid environmental pollution and resource waste. TW has been widely investigated for the removal of various pollutants such as dyes.
oxytetracycline, ethylene, As and Ni, Cu, Pb and Hg. To the best of our knowledge, few studies have applied TW as an adsorbent for the adsorption of uranium from aqueous solutions, and the maximum sorption capacities (\(Q_m\)) for uranium loading by TW obtained in these reports are low (< 150 mg/g). Moreover, there is no literature available on the adsorption of uranium onto a magnetic reduced graphene oxide/Fe\(_3\)O\(_4\)/TW (rGO/Fe\(_3\)O\(_4\)/TW) composite adsorbent.

At present, the development and applications of graphene and its derivatives have been hot research topics in various fields such as electronic devices, electrochemical capacitors, catalysts and environmental remediation, thanks to their unusual properties. Graphene oxide (GO) has been shown to be an excellent adsorbent for heavy metal ions (e.g., As, Eu, Cr, Pb, Cu and U). GO has numerous active functional groups fixed on the surface including carboxyl, lactone, hydroxyl and phenolic hydroxyl. TW is rich in cellulose, whose hydroxyl groups can be combined with GO to form an ester linkage, introducing carboxyl groups to TW. In the present study, we prepared two novel composites, GOTW and rGO/Fe\(_3\)O\(_4\)/TW, and explored their application as an adsorbent for uranium(VI) from aqueous solutions. Moreover, the adsorptive performance for U(VI) was tested in a solution containing other cationic ions and in practical low-radioactive uranium-bearing nuclear wastewater.

The results presented in this work reveal that the composite GOTW and magnetic rGO/Fe\(_3\)O\(_4\)/TW are promising adsorbents for the removal of uranium from nuclear industrial effluent.

**Results and Discussion**

**Characterization of the products.** The FT-IR spectra of GO, Fe\(_3\)O\(_4\), TW, GOTW and rGO/Fe\(_3\)O\(_4\)/TW are shown in Fig. 1. The IR spectrum of GO was similar to that of GO in the reference and had characteristic peaks at 3345~3229, 1725, 1618, 1387, 1227 and 1061 cm\(^{-1}\), corresponding to the stretching vibrations of O-H, carbonyl and carboxyl C=O, aromatic C=C and H\(_2\)O, carboxyl O=C-O, and alkoxy C-O-C stretching vibrational modes, respectively. In the IR spectrum of TW, the broad peaks at 3328 cm\(^{-1}\) could come from the -OH of absorbed H\(_2\)O or N-H stretching. The double peaks at 2920 and 2852 cm\(^{-1}\) were attributed to aliphatic carbons. The strong peaks at 1627 and 1026 cm\(^{-1}\) indicated the carbonyl stretching of -COOH groups and stretching vibration of the C-O groups of polysaccharides, respectively. These characteristic peaks of the prepared TW were similar to that of tea wastes reported previously. However, compared to that of GO, the double peaks at 2920 and 2852 cm\(^{-1}\) attributed to aliphatic carbons appeared in the IR spectrum of GOTW, and the intensity of the characteristic peaks at 3286 cm\(^{-1}\) ascribed to O-H was significantly lower, which suggests that the composite GOTW was prepared successfully. In the IR spectrum of rGO/Fe\(_3\)O\(_4\)/TW, there were characteristic peaks at 400 cm\(^{-1}\) belonging to the Fe-O stretching vibration, and similar absorption peaks as TW, whereas the characteristic peaks assigned to the stretching vibrations of O-H, carbonyl and carboxyl C=O, aromatic C=C and H\(_2\)O, carboxyl O=C-O, and alkoxy C-O-C disappeared. Moreover, the stretching vibrations of C=C and epoxy C-O at 1550 and 1014 cm\(^{-1}\) of rGO functional groups were present in the IR spectrum of rGO/Fe\(_3\)O\(_4\)/TW. These results implied that GO is reduced to rGO and that, simultaneously, Fe(II) is oxidized to Fe(III). The results showed that the magnetic composite rGO/Fe\(_3\)O\(_4\)/TW was prepared successfully.

The XRD patterns of the crystal phase of the prepared GO, Fe\(_3\)O\(_4\), rGO/Fe\(_3\)O\(_4\)/TW, and TW are presented in Fig. 2. No obvious diffraction peaks at 20=10° and 42° attributed to the crystal planes of GO were observed, confirming the reduction of GO to rGO. The XRD pattern of TW indicated that TW was successfully attached to the surface of GO. The XRD peaks at 20 values of approximately 29.94°, 35.30°, 42.98°, 53.38°, 56.84°, 62.46° and 74.54° of the purchased Fe\(_3\)O\(_4\) are shown in Fig. 2b. The diffraction peaks of the composite rGO/Fe\(_3\)O\(_4\)/TW (Fig. 2c) are consistent with those of Fe\(_3\)O\(_4\), but the peak intensities were significantly lower with the addition of rGO and TW.

The morphologies of GO, TW and GOTW were observed by SEM. The morphology of rGO/Fe\(_3\)O\(_4\)/TW was analysed by AFM because of its magnetic properties. Figure 3a shows that GO exhibited a wrinkled lamellar...
structure, and the sheets of GO stacked together due to strong inter-planar interactions. As shown in Fig. 3b, an irregular layered structure with a smooth surface without pores was observed in the SEM image of TW. However, the surface of GOTW (Fig. 3c) presented many tiny pores which could be propitious to adsorb heavy metal ions. In the AFM image of rGO/Fe₃O₄/TW (Fig. 3d) we observed that many Fe₃O₄ particles were attached to the surface of GOTW. Moreover, as seen in the insets of Fig. 3, a significant difference in the macroscopic morphology of the prepared sorbents was observed.

Magnetic analysis of Fe₃O₄ and rGO/Fe₃O₄/TW using a vibrating sample magnetometer (VSM) is shown in Fig. 4. The magnetization saturation values for Fe₃O₄ and rGO/Fe₃O₄/TW were 100 and 10 emu/g, respectively. A nonlinear, reversible magnetization curve with no hysteresis exhibited characteristic super-paramagnetic behaviour. The reduced saturation magnetization was mainly due to the presence of diamagnetic GOTW surrounding
the Fe$_3$O$_4$ cores. However, as seen in the inset of Fig. 4, the composite rGO/Fe$_3$O$_4$/TW can be completely separated from the solution by a conventional magnet.

**XPS analysis of the samples.** The chemical composition of Fe$_3$O$_4$, TW, GOTW and rGO/Fe$_3$O$_4$/TW was investigated by XPS. The XPS survey spectra of rGO/Fe$_3$O$_4$/TW (Fig. 5a) showed evident characteristic peaks at approximately 289, 557, 715 and 729 eV, which were attributed to C1s, O1s and Fe2p, respectively. In the high-resolution spectrum of Fe 2p (Fig. 5b), the peaks of Fe 2p$_{3/2}$ and Fe 2p$_{1/2}$ were located at 713.75 and 723.70 eV, respectively, indicating the presence of Fe$_3$O$_4$ in the composite rGO/Fe$_3$O$_4$/TW. The C1s and O1s

Figure 4. Magnetization curve of Fe$_3$O$_4$ and rGO/Fe$_3$O$_4$/TW. Inset is the separation application from the solution of rGO/Fe$_3$O$_4$/TW by an external magnetic field.

Figure 5. XPS survey spectra of Fe$_3$O$_4$, TW, GOTW and rGO/Fe$_3$O$_4$/TW (a), the high-resolution Fe 2p spectra of Fe$_3$O$_4$ and rGO/Fe$_3$O$_4$/TW (b), the high-resolution C1s spectra of TW and rGO/Fe$_3$O$_4$/TW (c) and the high-resolution O1s spectra of rGO/Fe$_3$O$_4$/TW and Fe$_3$O$_4$ (d).
XPS peaks of TW and rGO/Fe3O4/TW were deconvoluted (Fig. 5c,d). Figure 5c shows the C1s spectra with three deconvoluted peaks at 283.8, 285.1 and 287.5 eV associated with C–C, C–O and C=O bonds, respectively. Figure 5(d) shows the O1s spectrum, and the three peaks at 529.6, 531.2 and 532.7 eV belong to Fe–O, C=O and C–O, respectively. The fit results are presented in Table 1. The oxygen-containing groups C-O and C=O were significantly more abundant after combination, implying that TW was successfully loaded onto the surface of GO.

Based on the results described above, a possible reaction mechanism for the composite rGO/Fe3O4/TW is illustrated in Fig. 6. First, GO combines with TW to form GOTW, and then Fe2+ ions react with GOTW by a redox reaction to form rGOTW as shown in Eq. (2) in which GO is as an oxidant. Because the hydrolysis of Fe3+ results in the formation of Fe(OOH), as shown in Eq. (3), the composite rGO/Fe3O4/TW was obtained after the addition of ammonia solution, as shown in Eq. (4).

$$\text{GO} + \text{TW} \rightarrow \text{GOTW}$$  (1)

$$\text{GOTW} + \text{Fe}^{2+} \xrightarrow{\text{redox reaction}} \text{Fe}^{3+} + \text{rGOTW}$$  (2)

$$\text{Fe}^{3+} + \text{H}_2\text{O} \rightarrow \text{Fe(OOH)}$$  (3)

$$\text{rGOTW} \cdot \text{Fe}^{n+} (n = 2, 3) + \text{Fe(OOH)} + \text{NH}_3 \cdot \text{H}_2\text{O} \rightarrow \text{rGO/Fe}_3\text{O}_4/\text{TW}$$  (4)

**Influence of pH on adsorption.** The solution pH affects the speciation of uranium in solution and significantly influences the uranium adsorption process. The effect of pH on the adsorption of uranium (VI) by the synthesized adsorbents is presented in Fig. 7. The results showed a substantial impact of pH on uranium adsorption. The adsorption of U(VI) on TW, GOTW and rGO/Fe3O4/TW significantly increased with increasing pH from 2.0 to 5.0. At pH = 5, the removal rate of uranium of TW, GOTW and rGO/Fe3O4/TW reached the highest value. At pH < 4.0, uranium exists mainly in the form of UO2^{2+}. The competition between H3O+ and UO2^{2+} for binding sites on the adsorbent surface results in a low sorption efficiency 61. At pH = 5.0~7.0, the prominent species of uranium in the solution are UO2^{2+}, UO2(OH)+, (UO2)2(OH)2^{2+}, (UO2)3(OH)3^{2+} and (UO2)3(OH)5^{2+}. As seen in Fig. 7, the removal rate of uranium significantly increases at pH > 5.0, which can be attributed to electrostatic interactions of these complex uranium ions with negatively charged groups on the surface of TW, GOTW and rGO/Fe3O4/TW. The sorption behaviour of UO2^{2+} on GOTW and rGO/Fe3O4/TW at pH 2.0~7.0 is similar to that reported by Wang et al. 13. Additionally, the sorption efficiency of uranium by GOTW and rGO/Fe3O4/TW was higher than that for TW, indicating that the composite of GO and TW had more efficient adsorption of uranium. Consequently, the optimum pH for U(VI) adsorption by TW, GOTW and rGO/Fe3O4/TW was 5.0.

**Influence of contact time and kinetic study.** The adsorption dynamics data 63,64 were analysed based on Eqs (5) and (6). Figure 8(a) presents the time-dependent adsorption over a contact time ranging from 1 to 120 min of U(VI) by TW, GOTW and rGO/Fe3O4/TW. As seen in Fig. 8(a), the removal rate of the prepared adsorbents exceeded 96% within 1 min, and the adsorption equilibrium time was 60 min. Adsorption kinetic data of the pseudo-first-order and pseudo-second-order model at different temperature are given in Table 2. The correlation coefficient of pseudo-second-order model (R2 = 0.9999 and 1.0000) was superior to the pseudo-first-order model, which indicated that the adsorption of U(VI) onto TW, GOTW and rGO/Fe3O4/TW fitted the pseudo-second-order model better. The fit results demonstrated that a chemical reaction played a significant role in the rate-controlling steps. The surface functional groups of the prepared adsorbents might form strong electrostatic and chemical interactions with U(VI) ions 65. Moreover, the kinetic model fits results and parameters of rGO/Fe3O4/TW at different temperature are shown in Fig. 8(b) and Table 2, respectively. The result shows that temperature has no evident effect on the adsorption rate of rGO/Fe3O4/TW.

$$\lg(Q_e - Q_t) = \lg Q_e - \frac{k_1}{2.303}t$$  (5)

$$\frac{t}{Q} = \frac{1}{k_2Q_e^2} + \frac{t}{Q_e}$$  (6)

where k1 (min^{-1}) is the Lagergren rate constant of adsorption, and k2 (g/(mg-min)) is the rate constant of pseudo-second-order adsorption.
Adsorption isotherm. The Langmuir and Freundlich isotherm models are expressed in Eqs (7) and (8), respectively. The fit results of Langmuir and Freundlich isotherm models of GO, TW, GOTW and rGO/Fe$_3$O$_4$/TW at 298 K are shown in Fig. 9(a). The Langmuir and Freundlich isotherm models of rGO/Fe$_3$O$_4$/TW at different temperature are shown in Fig. 9(b). The isotherm parameters calculated from fitting processes at different temperature are listed in Table 3. The Langmuir equation of the adsorbents fitted the experimental data well, with a higher correlation coefficient ($R^2$).
\[ Q_e = \frac{Q_m \cdot K_L \cdot C_e}{1 + K_L C_e} \]  
\[ Q_e = K_F \cdot C_e^{1/n} \]

where \( Q_e \) (mg/g) is the equilibrium adsorption capacity, \( C_e \) (mg/L) is the uranium concentration at equilibrium, \( Q_m \) (mg/g) is the maximum adsorption capacity, \( K_L \) (L/mg) and \( K_F \) (mg\(^{1-n}\) L\(^n\)/g) are the Langmuir and Freundlich constants, respectively, and \( n \) is the Freundlich adsorption exponent.

Moreover, the Dubinin–Radushkevich (D–R) isotherm is applied to estimate the U(VI) adsorption behaviour (chemical or physical) onto the sorbent. The D–R equation is written as follow:

Table 2. Parameters of pseudo-first-order and pseudo-second-order kinetic models for U adsorption by TW, GOTW and rGO/Fe\(_3\)O\(_4\)/TW at different temperature.

| Sorbents         | Temperature (K) | Pseudo-first-order model | Pseudo-second-order model |
|------------------|-----------------|--------------------------|---------------------------|
|                  |                 | \( Q_e \) (mg/g) | \( k_1 \) (min\(^{-1}\)) | \( R^2 \) | \( Q_e \) (mg/g) | \( k_2 \) (g/(mg·min)) | \( R^2 \) |
| TW               | 298             | 1.026                    | 0.0002                    | 0.7400 | 19.88 | 0.2321 | 1.0000 |
| GOTW             | 303             | 5.677                    | 0.0500                    | 0.9796 | 20.00 | 0.3135 | 1.0000 |
| rGO/Fe\(_3\)O\(_4\)/TW | 313     | 0.104                    | 0.0594                    | 0.9328 | 19.80 | 0.3985 | 1.0000 |
|                  | 323             | 0.082                    | 0.0350                    | 0.9510 | 19.80 | 0.4305 | 1.0000 |
|                  | 333             | 0.083                    | 0.0364                    | 0.5729 | 19.92 | 0.2083 | 0.9999 |

Table 3. Langmuir, Freundlich and D–R model parameters for uranium adsorption on GO, TW, GOTW and rGO/Fe\(_3\)O\(_4\)/TW at different temperature.

| Sorbents         | Temperature (K) | Langmuir model | Freundlich model | D–R model |
|------------------|-----------------|----------------|------------------|-----------|
|                  |                 | \( Q_m \) (mg/g) | \( k_L \) (L/mg) | \( R^2 \) | \( n \) | \( k_F \) (mg\(^{1-n}\) L\(^n\)/g) | \( R^2 \) | \( Q_m \) (mg/g) | \( \beta \) (mol\(^2\)/J\(^2\)) | \( R^2 \) |
| GO               | 298             | 79.108          | 0.3856           | 0.9901 | 2.89 | 26.3486 | 0.9134 | 59.369 | 10\(^{-7}\) | 0.7866 |
| TW               | 298             | 91.719          | 0.2151           | 0.9797 | 3.42 | 21.5161 | 0.9320 | 56.165 | 10\(^{-7}\) | 0.9278 |
| GOTW             | 298             | 111.614         | 0.4828           | 0.9682 | 3.84 | 38.4609 | 0.9006 | 78.830 | 10\(^{-8}\) | 0.9227 |
| rGO/Fe\(_3\)O\(_4\)/TW | 303     | 103.840         | 0.7519           | 0.9892 | 4.07 | 40.2672 | 0.8838 | 72.341 | 5 \times 10\(^{-8}\) | 0.8664 |
|                  | 313             | 104.130         | 0.8218           | 0.9899 | 4.13 | 41.6600 | 0.8808 | 72.756 | 4 \times 10\(^{-8}\) | 0.8664 |
|                  | 323             | 107.210         | 0.8096           | 0.9912 | 4.17 | 42.7600 | 0.8887 | 73.821 | 4 \times 10\(^{-8}\) | 0.8632 |
|                  | 333             | 108.220         | 0.8689           | 0.9924 | 4.20 | 44.0200 | 0.8911 | 73.056 | 3 \times 10\(^{-8}\) | 0.8521 |
|                  | 333             | 109.160         | 0.9188           | 0.9934 | 4.27 | 45.2600 | 0.8899 | 73.831 | 3 \times 10\(^{-8}\) | 0.8557 |
\[ \beta = -\frac{Q}{\ln m} \]

\[ \varepsilon = RT \ln \left( \frac{1}{\theta} + \frac{1}{C_e} \right) \]

where \( \beta \) (mol²/J²) is activity coefficient depending on the mean free energy of adsorption and \( \varepsilon \) is the Polanyi potential (J/mol). 

R and T represent the gas constant (8.314 J/mol K) and absolute temperature (K), respectively.

The D–R isotherm fit parameters of GO, TW, GOTW and rGO/Fe₃O₄/TW at different temperature are listed in Table 3. The D–R isotherm usually used the mean free energy \( E \) (kJ/mol) to assess the type of adsorption mechanism. The \( E \) value can be calculated according to Eq. (11). A value higher than 8 kJ/mol is considered to indicate chemical adsorption while it is less than 8 kJ/mol for the physical adsorption.

\[ E = \frac{1}{\sqrt{2/\theta}} \]  

A comparison of the \( Q_m \) of different adsorbents is presented in Table 4. Table 4 shows that the \( Q_m \) of the prepared rGO/Fe₃O₄/TW indicated a promising adsorbent for the treatment of uranium-bearing wastewater.

\[ \ln Q_c = \ln Q_m - \beta \varepsilon^2 \]  

where \( \beta \) (mol²/J²) is activity coefficient depending on the mean free energy of adsorption and \( \varepsilon \) is the Polanyi potential (J/mol).

Table 4. Comparison of \( Q_m \) of as-obtained adsorbents in this study with the reported tea wastes for U(VI) adsorption.

| Sorbents        | pH  | c/V (g/L) | \( Q_m \) (mg/g) |
|-----------------|-----|-----------|-----------------|
| Tea wastes⁷¹     | 4   | 1.2       | 29.41           |
| Tea waste⁷²      | 6   | 0.2       | 142.21          |
| Pyrolyzed tea waste⁷³ | 3   | —         | 59.50           |
| Green tea⁶⁸      | 4–6 | 5         | 8.12            |
| Tea waste⁷⁰      | 6   | —         | 43.19           |
| Black tea scrap⁷⁴ | 5   | 4         | 62.51           |
| TW (This work)⁷⁵ | 5   | 0.5       | 91.72           |
| GOTW (This work) | 5   | 0.5       | 111.61          |
| rGO/Fe₃O₄/TW (This work) | 5   | 0.5       | 104.95          |

Table 5. Thermodynamic parameters of U(VI) adsorption on TW, GOTW and rGO/Fe₃O₄/TW.

| Sorbents         | \( \Delta H^0 \) (kJ/mol) | \( \Delta S^0 \) (J/(mol·K)) | \( \Delta G^0 \) (kJ/mol) |
|------------------|---------------------------|-------------------------------|--------------------------|
|                  | 303 K                     | 313 K                         | 323 K                     | 333 K                     |
| TW               | 45.24                     | 183.91                        | −10.48                    | −12.32                    | −14.16                    | −16.00                    |
| GOTW             | 28.71                     | 123.16                        | −10.61                    | −11.83                    | −13.07                    | −14.30                    |
| rGO/Fe₃O₄/TW     | 21.31                     | 106.83                        | −11.06                    | −12.13                    | −13.20                    | −14.26                    |

**Effect of temperature and adsorption thermodynamics.** The enthalpy (\( \Delta H^0 \)), entropy (\( \Delta S^0 \)) and standard free energy (\( \Delta G^0 \)) from 303 K to 333 K in the adsorption process were calculated from the slope and intercept of the linear line of \( \ln K_d \) versus 1/T using Eqs (12)–(14). The thermodynamic parameters and the plots of \( \ln K_d \) versus 1/T onto TW, GOTW and rGO/Fe₃O₄/TW are shown in Table 5 and Fig. 10, respectively. The negative value of \( \Delta H^0 \) indicated that the adsorption reaction was endothermic. The positive \( \Delta S^0 \) and negative \( \Delta G^0 \) suggest that the adsorption process was spontaneous.

\[ K_d = \frac{c_{ad}}{c_e} \]

\[ \ln K_d = -\frac{\Delta H^0}{RT} + \frac{\Delta S^0}{R} \]

\[ \Delta G^0 = \Delta H^0 - T\Delta S^0 \]

where \( K_d \) (mL/g) is the distribution coefficient of U(VI), \( c_{ad} \) (mg/L) is the concentration of metal ions on the adsorbent at equilibrium, \( c_e \) (mg/L) is the equilibrium concentration of metal ions in solution.
Real wastewater sample analysis. To evaluate the applicability of the prepared adsorbents in this study for real uranium-bearing wastewater samples, the removal efficiency of U(VI) from four different batches of wastewater samples under the optimum adsorption conditions was investigated. The measured parameters of real nuclear wastewater and adsorption experiment results are presented in Table 6 and Fig. 11, respectively. As shown in Fig. 11, co-existing ions had no effect on the removal efficiency of GOTW and rGO/Fe₃O₄/TW for uranium, and they can to be applied in the treatment of uranium-containing nuclear waste effluents as potential adsorbents.

![Figure 10](https://example.com/image10)

**Figure 10.** Plots of $\ln K_d$ versus $1/T$ for U(VI) adsorption onto TW, GOTW and rGO/Fe₃O₄/TW. pH = 5.0, $C_{(U)initial} = 10$ mg/L, $C_{sorbent} = 0.5$ g/L, $T = 303$ K, 313 K, 323 K and 333 K, and contact time = 24 h.

![Figure 11](https://example.com/image11)

**Figure 11.** Column chart of adsorption efficiency of TW, GOTW and rGO/Fe₃O₄/TW for real uranium-bearing nuclear waste effluents. pH = 5.0, $C_{sorbent} = 0.5$ g/L, contact time = 1 h, and $T = 298$ K.

| Wastewater parameters | Measured parameter values | Wastewater parameters | Measured parameter values |
|-----------------------|---------------------------|-----------------------|---------------------------|
| pH                    | 7.0~8.0                   | U                     | 0.3~3.0 mg/L              |
| Al                    | ≤0.05 mg/L                | Ca                    | 0~5.00 mg/L               |
| B                     | ≤0.05 mg/L                | Be                    | ≤0.05 mg/L                |
| Cu                    | 0~0.04 mg/L               | Fe                    | ≤0.34 mg/L                |
| Mn                    | 0~0.04 mg/L               | Mg                    | 0~1.38 mg/L               |
| Si                    | 0~2.71 mg/L               | Mo                    | ≤0.05 mg/L                |
| Ni                    | 0~0.02 mg/L               |                       |                           |

**Table 6.** Measured parameter values of real uranium-bearing wastewater samples.
Materials and Methods

Materials. Stock solutions of uranium (5–150 mg/L) were prepared by dissolving UO₂(NO₃)₂·6H₂O (Xi’er Dingtian Chemical Reagent Co.) in deionized water (DW) and acidifying with a small amount of concentrated HNO₃. The green tea used in this work originated from Sichuan Pingwu in China. All reagents used were of analytical grade and were used without further purification. DW was used throughout the experiments.

Preparation of tea wastes (TW). Green tea was washed with DW several times to remove all dirt substances. It was then boiled in DW at 80 °C for 1 h to remove coloured and soluble components, and then washed with DW until virtually colourless. The obtained TW was dried in an oven at 100 °C for 24 h. Finally, the products were crushed to powder in a pulveriser.

Preparation of the composite GOTW. GO was prepared from natural graphite by the modified Hummers method. GOTW was prepared using GO and TW under ultrasonic treatment. Briefly, the mixture of GO (0.5 g) and TW (0.5 g) was dispersed in 100 mL DW under ultrasonication for 3 h. Then, 25% dilute ammonia solution was added drop-wise to the solution until the pH reached 11. Then, 1.25 g of FeCl₃·4H₂O was added very slowly to the mixture with continuous magnetic stirring. After stirring for 3 h, black rGO/Fe₃O₄/TW product was obtained by filtration and washed with DW and ethanol. Finally, rGO/Fe₃O₄/TW was dried at 50 °C under vacuum.

Preparation of the magnetic composite rGO/Fe₃O₄/TW. The rGO/Fe₃O₄/TW composite was synthesized using a previously reported method. First, a mixture of GO (0.25 g) and TW (0.25 g) was dispersed in 100 mL DW under ultrasonic treatment for 3 h. Then, 25% dilute ammonia solution was added drop-wise to the solution until the pH reached 11. Then, 1.25 g of FeCl₃·4H₂O was added very slowly to the mixture with continuous magnetic stirring. After stirring for 3 h, black rGO/Fe₃O₄/TW product was obtained by filtration and washed with DW and ethanol. Finally, rGO/Fe₃O₄/TW was dried at 50 °C under vacuum.

Characterization of the products. Fourier transform infrared (FTIR) spectra of as-prepared adsorbents were obtained using an FTIR spectrometer (Bruker VERTEX 70, Germany). The crystal phases of the samples were characterized by X-ray diffractometer (XRD) (2700 model, China). The surface morphology of the products was determined using a scanning electron microscope (SEM; FEI Helios 600i, USA). The magnetic measurements of Fe₃O₄ and rGO/Fe₃O₄/TW were conducted at 300 K under a varying magnetic field (PPMS-9 ECII, USA Quantum Design Co.). X-ray photoelectron spectroscopy (XPS) was studied using an ESCALAB 250 X-ray photoelectron spectroscopy (Thermo fisher, USA).

Adsorption experiments. The influence of pH, contact time, initial uranium concentration, and temperature on the removal efficiency of uranium were investigated. The solution pH was adjusted using NaOH and HCl. The prepared adsorbent was added to 20 mL U(VI) solution and shaken in a shaker (Kangshi, China). After filtration, residual uranium concentrations were measured by a micro-quantity uranium analyser (MUA model, China). The removal rate R (%) and the adsorption capacity of U(VI) Q (mg/g) were calculated according to Eqs (15) and (16), respectively:

\[
R(\%) = \frac{c_0 - c_t}{c_0} \times 100
\]  

(15)

\[
Q(\text{mg/g}) = \frac{(c_0 - c_t)}{W} \times V
\]  

(16)

where \(c_0\) (mg/L) is the initial uranium (VI) concentration, \(c_t\) (mg/L) is the uranium concentration at time \(t\), \(V\) (L) is the solution volume and \(W\) (g) stands for the weight of adsorbent.

Conclusion

In summary, four adsorbents GO, TW, GOTW and rGO/Fe₃O₄/TW were fabricated for the adsorption of uranium from aqueous solutions. The adsorption data of U(VI) by TW, GOTW and rGO/Fe₃O₄/TW were consistent with the Langmuir isotherm model and pseudo-second-order kinetics. The composites GOTW and rGO/Fe₃O₄/TW exhibited higher adsorption capacities and faster adsorption kinetics than did GO and TW. The results showed that GOTW and rGO/Fe₃O₄/TW could be utilized effectively as promising sorbents to remove uranium from real multi-component uranium-containing nuclear waste effluents. Furthermore, due to the advantageous magnetic properties, rGO/Fe₃O₄/TW can be easily separated from aqueous solutions, thus enhancing post-treatment efficiency for further practical applications.

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Author Contributions
Author contributions were as follows: Aili Yang designed the research. Aili Yang, Yukuan Zhu and Ping Li performed the experiments. Aili Yang analyzed the data and wrote the paper. C.P. Huang guided the experiments and revised the paper.

Additional Information
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