Metamodelling Techniques for the Optimal Design of Low-Noise Amplifiers

Amel Garbaya, Mouna Kotti, Mourad Fakhfakh and Esteban Tlelo-Cuautle

1 Department of Electronics, ENET’com and University of Sfax, Sfax 3018, Tunisia; amelgarbaya11@gmail.com (A.G.); kot.mouna@gmail.com (M.K.); fakhfakhmourad@gmail.com (M.F.)
2 Department of Electronics, Electrotechnics and Control, ISSIG, University of Gabes, Gabes 6032, Tunisia
3 INAOE, Tonantzintla, Puebla 72840, Mexico
* Correspondence: etlelo@inaoep.mx; Tel.: +522222663100

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Abstract: In this article we deal with the optimal sizing of low-noise amplifiers (LNAs) using newly proposed metamodeling techniques. The main objective is to construct metamodels of main performances of the LNAs (namely, the third intercept point (IIP3), the scattering parameters ($S_{ij}$)), and the noise figure (NF)) and use them inside an optimization kernel for maximizing the circuits’ performances. The kriging surrogate modelling technique is used for constructing these models. The particle swarm optimization (PSO) technique is considered as the optimization metaheuristic. Two CMOS amplifiers are considered: a UMTS LNA and a multistandard LNA. Obtained results show that, at the considered working frequencies, the first LNA exhibits at 2.14 GHz a noise figure of 1.30 dB, an $S_{21}$ of 16.01 dB, an $S_{11}$ of $-12.60$ dB, and an IIP3 of 8.30 dBm. At 2 GHz, the second LNA has a noise figure of 1.24 dB, an $S_{21}$ of 17.16 dB, an $S_{11}$ of $-13.74$ dB, and an IIP3 of 4.30 dBm. Comparisons between results obtained using the constructed models and those of the simulation are presented to show the perfect agreement between them.

Keywords: surrogate models; kriging technique; RF; LNA; CMOS; IIP3; scattering parameters; noise figure; optimization

1. Introduction

The optimal design of analogue circuits has long been, and continues to be, a tedious and complicated task that depends significantly on the designer’s experience. It is indeed a subject of great interest to designers, engineers, researchers, etc. This is mainly due to the lack of dedicated design automation tools. Moreover, and as is well known, for radio frequency applications such a task is greatly complicated by the fact that additional parasitics/performances/constraints have to be taken into consideration in the design process (the most constraining being arguably the third intercept point).

In this work we are interested in the optimal design of low-noise amplifiers (LNAs).

The literature offers a plethora of research works that have dealt with the design of such amplifiers. Different approaches have been considered, mainly:

- The use of the conventional equation-based techniques, see for instance [1–3];
- The in-loop based approaches, see [4–6].

The majority of these works deal with the optimization of the scattering parameters that are introduced within an optimization kernel as performances and/or constraints. Only a few papers have considered the maximization of the third intercept point (IIP3) due to its high complexity [4,5,7,8]. Actually, IIP3 is generally considered as a circuit performance that is computed a posteriori, see for instance [4,8–11]. In [11], the authors have dealt with a symbolic approach for obtaining an approximation of the IIP3.
expression. In [8] a graphical technique is used. It depicts the intercept point based on measurements of the fundamental and third-order intermodulation distortion amplitude for an input power sweep. Automating this measurement takes long computation times. The authors in [4] use another method: when the IIP3 is related to the direct current (DC) power consumption, the IIP3 is calculated in the region where the DC power consumption is below 60 dB (this region guarantees a linear relationship between the input and the output powers).

Recently, a new modelling technique has been proposed. It is known as ‘metamodelling’ or ‘surrogate modelling’. It has been shown and proven that such a technique can faithfully model complicated ‘non-linear’ phenomena using a relatively reduced input database [12–17]. It has overcome limitations and errors of the conventional modelling techniques [12]. Moreover, these metamodelling approaches offer additional very interesting features, namely the estimation of the error at the interpolation points. Different variants are available in the specialized literature:

- The polynomial regression model [13];
- The artificial neural network model [14];
- The kriging model [15];
- The radial basis function model [16];
- The support vector machine model and the support vector regression model [17].

Nowadays, metamodelling is used in many engineering domains: aeronautics [18], mechanics [19], electronics [20–24], telecommunication [25], and management science [26], to name a few. The authors have already focused on the use of such techniques and have shown the efficiency of these modelling approaches for the design of some analogue circuits, see [20–22].

In this work we are interested in the design of high-performance low-noise amplifiers. The main objective is to model these circuits’ performances (namely IIP3, scattering parameters ($S_{ij}$), and noise figure (NF)) using the kriging technique. The constructed metamodels are then used within a particle swarm optimization (PSO)-based optimization kernel to generate the optimal values of the circuits’ parameters.

The rest of the paper is organized as follows. In Section 2, we provide an overview on the metamodelling techniques. In Section 3, we present the considered amplifiers and we deal with the construction and the validation of these circuits’ performance models. In Section 4, we consider the optimization approach, highlight the performances reached, and give comparisons with the simulation results. In Section 5, we conclude the work and underline some perspectives.

2. Overview of Surrogate Models

Surrogate modelling is a kind of an interpolation technique that, in contrast with the conventional approaches that focus on the linear regression term, deals with the error term by considering the correlation between the instances. It has rapidly become a popular method to solve the computation time problems related to constraint and performance evaluations [20–31]. Actually, it offers a very interesting advantage since, in many engineering applications, particularly in analogue circuit design, such evaluations/measures can be very time consuming, mainly when using an in-loop technique. For example, in [32] the sizing of integrated inductors is considered, and it is shown that, due to the electromagnetic simulations, it takes around two weeks to generate the Pareto front of three performances (Inductance/Area/Quality factor) of a square integrated inductor.

This new technique is capable of approximating very complex non-linear functions by a simple and an accurate model. A large number of works have used this method for modelling complex performances of analogue circuits, for example, in [30] the kriging model was used within a multi-objective robust optimization of electromagnetic devices. In [21], the authors have used the kriging modelling technique for the accurate approximation of several performances of a couple of circuits. In [22] the kriging model was combined with the PSO for optimizing the sizing of a current conveyor and a unity gain voltage amplifier. In [33], the response surface methodology is used within
the multi-objective optimization in the aim to implement an accurate solution for the optimization of RF-MEMS switches. In [34], the authors used the support vector machine for standby statistical leakage estimation of CMOS circuits using sampling based methods, which your aim is to replace SPICE simulation with your proposed surrogate models.

In metamodelling, the interpolation function can be simplified and expressed as follows [27,32,35]:

\[ Y(x) = \sum_{j=1}^{N} \beta_j f_j(x) + Z(x) \]  

(1)

where \( N \) is the number of sample points. \( f_j(x) \) represents the \( j^{th} \) regression function model, \( \beta_j \) is the corresponding weighting coefficient, and \( Z(x) \) is a stochastic process. The latter has a mean value equal to zero, and the covariance between two sampling points \( x_i \) and \( x_j \) is expressed as [27,30,35]:

\[ \text{Cov}(Z(x_i), Z(x_j)) = \sigma^2 R(R(\theta, x_i, x_j))_i, j = 1, \ldots, N \]  

(2)

where \( \sigma^2 \) is the variance coefficient of \( Z(x) \). \( R(\theta, x_i, x_j) \) is the correlation function.

The most renowned correlation functions are:

- The spline correlation function:

\[ R(\theta, x_i, x_j) = \prod_{k=1}^{N} \max(0.1 - \theta_k |x_i - x_j|_k) \]  

(3)

- The exponential correlation function:

\[ R(\theta, x_i, x_j) = \prod_{k=1}^{N} e^{-\theta_k (|x_i - x_j|_k)^2} \]  

(4)

- The Gaussian correlation:

\[ R(\theta, x_i, x_j) = \prod_{k=1}^{N} e^{-\theta_k (|x_i - x_j|_k)^2} \]  

(5)

where \( |x|_k \) is the distance between \( x_i \) and \( x_j \) in direction \( k \). \( \theta_k \) is the \( k^{th} \) element of the correlation parameters [27,30,35].

The best linear prediction of \( Y(x^*) \) is defined as follows [27]:

\[ \hat{Y}(x^*) = \hat{\beta}^* (\theta) + r(x^*, \theta) R(\theta)^{-1} (Y - f \beta^* (\theta)) \]  

(6)

where \( x^* \) is the new sample, \( \hat{\beta}^* \) is the estimator of \( \beta \), and \( Y \) is the \( (N^*1) \) vector of the samples’ values, \( f \) is a unit vector \( (N^*1) \), \( R \) is the correlation vector between \( x^* \) and the \( N \) samples. The maximum probability estimation of \( \hat{\beta} \) is defined as follows:

\[ \hat{\beta}^* (\theta) = (f^T R(\theta)^{-1} f)^{-1} (f^T R(\theta)^{-1} Y) \]  

(7)

The accuracy of the prediction is expressed by the MSE predictor [26] (MSE stands for mean square error):

\[ s(x^*) = \hat{\delta}^2 (\theta)(1 - rR^{-1}r^T + \frac{(1 - f^T R^{-1}r^T)^2}{f^T R^{-1} f}) \]  

(8)
3. On the Modelling of Low-Noise Amplifiers’ (LNAs) Performances

Radio frequency (RF) systems and circuits are key elements in various application domains such as mobile wireless communication, wireless local area network applications, mobile cellular, etc. [9,37].

In RF receivers, LNAs are arguably the most important circuits because their performances can considerably alter those of the rest of the system [2,38–40].

An LNA is characterized by several performances, principally its gain, its input and output matching (which can be evaluated via the scattering parameters $S_{21}$, $S_{11}$ and $S_{22}$), its noise figure (NF), and its third-order intercept point (IIP3).

As introduced above, two LNAs are considered in this work.

In the following, we present these circuits, deal with constructing models of the aforementioned performances, and present a comparison with Hspice [41] results for models’ validation purposes.

3.1. An UMTS LNA

Figure 1 presents a CMOS LNA, which topology was developed for UMTS applications, see [1,42]. $R_1$, $R_2$ and $M_3$ form the bias circuitry. $M_2$ forms the isolation stage between the input and the output of the circuit. $L_L$, $R_L$, and $C_L$ form the circuit’s output impedance [1].

![Image of a CMOS LNA](image)

Figure 1. An UMTS CMOS low-noise amplifier (LNA).

The kriging modelling technique is used for constructing models of the scattering parameters $(S_{21}$, $S_{11}$, $S_{22}$), the noise figure, and the third-order intercept point. Below, the models’ results are presented and compared with the Hspice simulation.

The adopted modelling approach encompasses four steps:

(1) **Design of Experiments**: It consists of establishing a database that serves as an input for the kriging technique. This database is composed of the geometric variables of the considered circuits. The Latin hypercube sampling technique (LHS) is used for this purpose [43]; 1400 valid points were considered: 1200 samples for constructing the model and 200 test samples for checking/validating the model. Table 1 gives details corresponding to the handled input variables, viz. MOS transistors channel widths and passive components values.

$$
\delta^2 = \frac{(Y - f\hat{\beta})^TR^{-1}(Y - f\hat{\beta})}{n}
$$

(9)

It is to be mentioned that, when compared to the other modelling techniques, the kriging approach offers several advantages, such as the simplicity of its implementation, its accuracy, and the fact that it is able to provide an estimation of the model’s error [32,36]. The kriging technique using a Gaussian correlation function is adopted in this work.

| Components Variation | Ranges             |
|----------------------|--------------------|
| W1, W2              | [400 µm, 700 µm]   |
| LL, L1              | [0.1 nH, 1 nH]     |

Table 1. Parameters’ ranges.
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Table 1. Parameters’ ranges.

| Components | Variation Ranges |
|------------|------------------|
| W₁, W₂     | [400 µm, 700 µm] |
| L, L₁      | [0.1 nH, 1 nH]   |
| L₂         | [5 nH, 10 nH]    |
| C_L, Cₛ    | [5 pF, 10 pF]    |

(2) **Performance Evaluation**: Hspice simulator was used to evaluate the samples, check the constraints, and establish both databases. (.MEAS instruction within HSpice-RF was used to measure S_{ij} and NF values within the considered frequency range (it is to be mentioned that 30 models have constructed for each working frequency, in the range of 1 GHz to 3 GHz)).

(3) Kriging associated to the Gaussian correlation function is used to construct the model.

(4) **Model Construction**: It consists of applying the Gaussian correlation functions-based kriging technique to construct a model for each performance (S_{11}, S_{22}, S_{21}, NF and IIP3), using the established databases.

(5) **Model Validation**: Both the root mean square error (RMSE) and the maximum absolute error (MAE) were considered to evaluate the accuracy of the constructed models. Corresponding equations are given by (10) and (11), where y_i and Y_i are the measured and the estimated performance values, respectively [44].

\[
RMSE = \sqrt{\frac{1}{N} \sum_{i=1}^{N} (y_i - Y_i)^2} \quad (10)
\]

\[
MAE = \max |y_i - Y_i| \quad (11)
\]

It is important to mention that one model has been generated for each working frequency (in the range of 1 GHz to 3 GHz). 30 models were constructed. Tables 2 and 3 give the errors’ values between the constructed models and Hspice results for five working frequencies. Figures 2–6 depict the corresponding models and simulation results.

Table 2. Root mean square error (RMSE) for scattering parameters (S_{ij}) and noise figure (NF) of the UMTS LNA.

| Frequency | S_{11}   | S_{22}   | S_{21}   | NF       |
|-----------|----------|----------|----------|----------|
| 1 GHz     | 0.0012 × 10^{-11} | 0.0001 × 10^{-11} | 0.0578 × 10^{-12} | 0.0386 × 10^{-13} |
| 1.5 GHz   | 0.0188 × 10^{-11} | 0.0037 × 10^{-11} | 0.0579 × 10^{-12} | 0.0208 × 10^{-13} |
| 2.14 GHz  | 0.6182 × 10^{-11} | 0.2809 × 10^{-11} | 0.1410 × 10^{-12} | 0.0369 × 10^{-13} |
| 2.5 GHz   | 0.1942 × 10^{-11} | 0.0514 × 10^{-11} | 0.1691 × 10^{-12} | 0.0652 × 10^{-13} |
| 3 GHz     | 0.0497 × 10^{-11} | 0.0046 × 10^{-11} | 0.0875 × 10^{-12} | 0.1328 × 10^{-13} |

Table 3. Maximum absolute error (MAE) for S_{ij} and NF of the UMTS LNA.

| Frequency | S_{11}   | S_{22}   | S_{21}   | NF       |
|-----------|----------|----------|----------|----------|
| 1 GHz     | 0.0003 × 10^{-10} | 0.0003 × 10^{-11} | 0.1683 × 10^{-12} | 0.0822 × 10^{-13} |
| 1.5 GHz   | 0.0062 × 10^{-10} | 0.0133 × 10^{-11} | 0.1616 × 10^{-12} | 0.0488 × 10^{-13} |
| 2.14 GHz  | 0.3052 × 10^{-10} | 0.7127 × 10^{-11} | 0.3908 × 10^{-12} | 0.1066 × 10^{-13} |
| 2.5 GHz   | 0.0729 × 10^{-10} | 0.1689 × 10^{-11} | 0.5791 × 10^{-12} | 0.1910 × 10^{-13} |
| 3 GHz     | 0.0181 × 10^{-10} | 0.0156 × 10^{-11} | 0.3066 × 10^{-12} | 0.3730 × 10^{-13} |
Regarding the third-order intercept point, one model was generated for each working input power (in the range of −50 dBm to 0 dBm). 10 models were constructed. Table 4 shows RMSE and MAE error values for the IIP3 in input powers.

Table 4. RMSE and MAE error for third intercept point (IIP3) of the UMTS LNA.

| Input Power | RMSE    | MAE     |
|-------------|---------|---------|
| −50 dBm     | 5.4793 $\times 10^{-13}$ | 3.1646 $\times 10^{-12}$ |
| −40 dBm     | 4.1372 $\times 10^{-13}$ | 1.4415 $\times 10^{-12}$ |
| −30 dBm     | 4.1928 $\times 10^{-13}$ | 1.4451 $\times 10^{-12}$ |
| −20 dBm     | 3.9675 $\times 10^{-13}$ | 1.3305 $\times 10^{-12}$ |
| −10 dBm     | 3.7601 $\times 10^{-13}$ | 1.3900 $\times 10^{-12}$ |

Figure 2. S11: Hspice simulations vs. the kriging model (the UMTS LNA).

Figure 3. S22: Hspice simulations vs. the kriging model (the UMTS LNA).
Figure 2. $S_{11}$: Hspice simulations vs. the kriging model (the UMTS LNA).

Figure 3. $S_{22}$: Hspice simulations vs. the kriging model (the UMTS LNA).

Figure 4. $S_{21}$: Hspice simulations vs. the kriging model (the UMTS LNA).

Figure 5. NF: Hspice simulations vs. the kriging model (the UMTS LNA).

Figure 6. IIP3: Hspice simulations vs. the kriging model (the UMTS LNA).

3.2. A Multistandard CMOS LNA

Figure 7 presents the CMOS transistor level schematic of a LNA for multistandard applications in the frequency range 1.5–2.5GHz [1]. The proposed LNA design encompasses a cascade architecture for reducing the Miller effect and uses the reverse isolation. $M_3$, $R_2$, and $R_1$ form the biasing circuitry of the input transistor. $L_2$, $C_1$, and $C_2$ allow the input matching [1]. We refer the reader to [40] for further details regarding the LNA topologies and characteristics.
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![Figure 7. A multistandard CMOS LNA.](image)

Constructing models of different performances of the multistandard-LNA are generated using the same approach adopted for the first application example. The database is composed of 10 input variables. Ranges of the geometric variables were set as indicated in Table 5.

| Components | Variation Ranges |
|------------|------------------|
| W1, W2     | [100 µm, 1000 µm]|
| L_L        | [0.5 nH, 0.9 nH]  |
| L1         | [0.01 nH, 0.9 nH]  |
| L2         | [1 nH, 10 nH]  |
| C_L, C_s   | [1 pF, 10 pF]  |
| C1, C2     | [0.1 ff, 20 ff]  |
| R_L        | [0.1 Ohm, 10 Ohm]  |

The kriging model was constructed using the Gaussian correlation function. 30 models were established. Tables 6 and 7 show the obtained error values for RMSE and MAE, respectively. Table 8 shows RMSE and MAE for IIP3 in input powers.

| Frequency | S_11  | S_22  | S_21  | NF    |
|-----------|-------|-------|-------|-------|
| 1 GHz     | 0.0385 × 10^{-12} | 0.0244 × 10^{-12} | 0.0526 × 10^{-11} | 0.1767 × 10^{-13} |
| 1.5 GHz   | 0.3384 × 10^{-12} | 0.1694 × 10^{-12} | 0.0132 × 10^{-11} | 0.0953 × 10^{-13} |
| 2 GHz     | 0.7082 × 10^{-12} | 0.5271 × 10^{-12} | 0.0364 × 10^{-11} | 0.0881 × 10^{-13} |
| 2.5 GHz   | 0.8602 × 10^{-12} | 0.7183 × 10^{-12} | 0.1135 × 10^{-11} | 0.1729 × 10^{-13} |
| 3 GHz     | 0.7436 × 10^{-12} | 0.4882 × 10^{-12} | 0.0617 × 10^{-11} | 0.3702 × 10^{-13} |
Table 7. MAE for $S_{ij}$ and NF of the multistandard-LNA.

| Frequency | $S_{11}$      | $S_{22}$      | $S_{21}$      | NF          |
|-----------|---------------|---------------|---------------|-------------|
| 1 GHz     | $0.0184 \times 10^{-11}$ | $0.0081 \times 10^{-11}$ | $0.1692 \times 10^{-11}$ | $0.0995 \times 10^{-12}$ |
| 1.5 GHz   | $0.1908 \times 10^{-11}$ | $0.0740 \times 10^{-11}$ | $0.0448 \times 10^{-11}$ | $0.0535 \times 10^{-12}$ |
| 2.14 GHz  | $0.2519 \times 10^{-11}$ | $0.1986 \times 10^{-11}$ | $0.1430 \times 10^{-11}$ | $0.0264 \times 10^{-12}$ |
| 2.5 GHz   | $0.6047 \times 10^{-11}$ | $0.3219 \times 10^{-11}$ | $0.3684 \times 10^{-11}$ | $0.0728 \times 10^{-12}$ |
| 3 GHz     | $0.3300 \times 10^{-11}$ | $0.2938 \times 10^{-11}$ | $0.1963 \times 10^{-11}$ | $0.1559 \times 10^{-12}$ |

Table 8. RMSE and MAE for IIP3 of the multistandard-LNA.

| Input Power | RMSE Error | MAE Error |
|-------------|------------|-----------|
| −50 dBm     | $2.8713 \times 10^{-12}$ | $6.9952 \times 10^{-12}$ |
| −40 dBm     | $3.6393 \times 10^{-12}$ | $7.6232 \times 10^{-12}$ |
| −30 dBm     | $3.9481 \times 10^{-12}$ | $10.7478 \times 10^{-12}$ |
| −20 dBm     | $1.4343 \times 10^{-12}$ | $4.5812 \times 10^{-12}$ |
| −10 dBm     | $1.8178 \times 10^{-12}$ | $5.8903 \times 10^{-12}$ |

Figures 8–12 show comparisons between simulation and model results.

![Figure 8](image1.png)

Figure 8. $S_{11}$: Hspice simulations vs. the kriging model (the multistandard-LNA).

![Figure 9](image2.png)

Figure 9. $S_{22}$: Hspice simulations vs. the kriging model (the multistandard-LNA).
4. The Optimization Kernel

As introduced in Section 1, the constructed and validated metamodels of the LNAs’ performances are used within an optimization kernel for the optimal sizing of these circuits.
Figure 13 depicts the flowchart of the corresponding approach where the particle swarm optimization (PSO) metaheuristic is used as the optimization engine.

![Flowchart of the kriging-particle swarm optimization (PSO) technique.](image_url)

We briefly recall that PSO is a swarm intelligence technique. It has already been used in a plethora of applications in electronics engineering. It is a simple, robust and rapid metaheuristic. It mimics the behaviour of animals within swarms, namely fishes and birds [2,45–47]. Its mechanism works on updating each particle’s velocity and position at each iteration, according to the following equations:

\[
\begin{align*}
\mathbf{v}_i(t+1) &= \omega \mathbf{v}_i(t) + c_1 \text{rand}(0,1)(\mathbf{x}_{Pbesti}(t) - \mathbf{x}_i(t)) \\
&\quad + c_2 \text{rand}(0,1)(\mathbf{x}_{Gbest}(t) - \mathbf{x}_i(t)) \\
\mathbf{x}_i(t+1) &= \mathbf{x}_i(t) + \mathbf{v}_i(t)
\end{align*}
\]  

(12)

(13)

where \(x_{Pbesti}\) is the best position of particle \(i\), \(x_{Gbest}\) is the global best position, \(\omega\) is the inertia weight of the particle. \(c_1\) and \(c_2\) are the constriction parameters.

In the following we provide optimization results for both circuits presented in the previous section. The considered working frequencies are 2.14 GHz and 2 GHz for the UMTS LNA and the multistandard LNA, respectively (AMS 0.35 µm CMOS technology (Level 49 model) is used.)

The optimization task consists of maximizing the third-order intercept point while imposing threshold constraints on the noise figure and on the \(S_{ij}\) parameters: \(NF < 4 \text{ dB}, S_{21} > 16 \text{ dB}, S_{11} < -10 \text{ dB} \) and \(S_{22} < -10 \text{ dB}\).
Regarding the PSO routine, the following parameters have been considered: 100 generations, 200 particles. The inertia weight is equal to 1, and both constriction parameters are equal to 2.

Tables 9 and 10 give the optimal values obtained for the circuits’ components. Obtained performances are summarized in Tables 11 and 12.

### Table 9. Optimal parameters for the UMTS LNA.

|    | \( W_1 \) (\( \mu \)m) | \( W_2 \) (\( \mu \)m) | \( L_1 \) (nH) | \( L_2 \) (nH) | \( L_3 \) (nH) | \( C_s \) (pF) | \( C_L \) (pF) |
|----|-------------------|-------------------|--------------|--------------|--------------|-------------|-------------|
|    | 482.30            | 620.61            | 0.948        | 7.432        | 0.244        | 8.648       | 5.187       |

### Table 10. Optimal parameters’ values for the multistandard-LNA.

|    | \( W_1 \) (\( \mu \)m) | \( W_2 \) (\( \mu \)m) | \( L_1 \) (nH) | \( L_2 \) (nH) | \( C_s \) (pF) | \( C_1 \) (fF) | \( C_2 \) (fF) | \( R_L \) (Ohm) | \( C_L \) (pF) |
|----|-------------------|-------------------|--------------|--------------|-------------|-------------|-------------|--------------|-------------|
|    | 574.57            | 494.82            | 0.859        | 7.910        | 0.303       | 2.903       | 9.865       | 2.074       | 0.346       | 6.731       |

### Table 11. Optimal performances for the UMTS LNA with \( P_{in} = -50 \) dBm.

| Performances | Specification | Kriging model-PSO | Hspice Simulation |
|--------------|---------------|-------------------|------------------|
| \( S_{21} \) (dB) | \( >16 \)     | 16.013            | 16.093           |
| \( S_{11} \) (dB) | \( <-10 \)  | -12.600           | -12.770          |
| \( NF \) (dB)    | \( <4 \)      | 1.300             | 1.307            |
| \( IIP3 \) (dBm) | To be maximized | 8.300             | 8.306            |

### Table 12. Optimal performances of the multistandard-LNA with \( P_{in} = -50 \) dBm.

| Performances | Specification | Kriging model-PSO | Hspice Simulation |
|--------------|---------------|-------------------|------------------|
| \( S_{21} \) (dB) | \( >16 \)     | 17.165            | 17.164           |
| \( S_{11} \) (dB) | \( <-10 \)  | -13.735           | -13.737          |
| \( NF \) (dB)    | \( <4 \)      | 1.246             | 1.246            |
| \( IIP3 \) (dBm) | To be maximized | 4.307             | 4.307            |

Regarding computation time, it is to be mentioned that for each constraint, namely, the scattering parameters and the noise figure, about 1 h 18 min was needed to evaluate the 1200 LHS samples and prepare the input database, and around 2 s for constructing the kriging model. The kriging-based PSO optimization routine took 44 s to maximize IIP3, which input database required 2 h 15 min to be prepared. For the sake of comparison, an inloop PSO-based optimization routine was considered to maximise the same performance under the same conditions, and it took 11 h 3 min 4 s to converge. (An Intel core i3-1.8 GHz-4Go RAM-64 bits PC was used).

### 5. Conclusions

An efficient approach to maximizing the IIP3 of low-noise amplifiers was presented. It consists of the use of surrogate models to construct models of circuits’ performances. This allows us to alleviate the burden related to the very long computation time when using the conventional in-loop optimization sizing processes where the simulator is used as the performance (and constraint) evaluator. The kriging metamodelling technique was used to construct accurate models of the IIP3, the noise figure and the scattering parameters. These models were used within a PSO-based optimization kernel for the optimal sizing of the LNAs. Comparisons with Hspice results were provided to show the perfect agreement between the simulated results and the expected ones.

The main objective of the paper is to present a fast way to evaluate LNA performances, particularly IIP3. The proposed approach can be extended to use complex models of integrated inductors such as those proposed in [32], and also sensitivity and yield analysis.
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