Importance of thermodynamics dependent kinetic parameters in nitrate-based souring mitigation studies

Moein Jahanbani Veshareh a,*, Jan Dolfing b, Hamidreza M. Nick a

a Danish Hydrocarbon Research and Technology Centre, Technical University of Denmark, Lyngby, Denmark
b Faculty of Engineering and Environment, Northumbria University, Newcastle upon Tyne, UK

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ABSTRACT

Souring is the unwanted formation of hydrogen sulfide (H₂S) by sulfate-reducing microorganisms (SRM) in sewer systems and seawater flooded oil reservoirs. Nitrate treatment (NT) is one of the major methods to alleviate souring: The mechanism of souring remediation by NT is stimulation of nitrate reducing microorganisms (NRM) that depending on the nitrate reduction pathway can outcompete SRM for common electron donors, or oxidize sulfide to sulfate. However, some nitrate reduction pathways may challenge the efficacy of NT. Therefore, a precise understanding of souring rate, nitrate reduction rate and pathways is crucial for efficient souring management. Here, we investigate the necessity of incorporating two thermodynamic dependent kinetic parameters, namely, the growth yield (Y), and Fₜ, a parameter related to the minimum catabolic energy production required by cells to utilize a given catabolic reaction. We first show that depending on physiochemical conditions, Y and Fₜ for SRM change significantly in the range of [0-0.4] mole biomass per mole electron donor and [0.0006-0.5], respectively, suggesting that these parameters should not be considered constant and that it is important to couple souring models with thermodynamic models. Then, we highlight this further by showing an experimental dataset that can be modeled very well by considering variable Fₜ. Next, we show that nitrate based lithotrophic sulfide oxidation to sulfate (lNRM₁) is the dominant nitrate reduction pathway. Then, arguing that thermodynamics would suggest that S⁰ consumption should proceed faster than S⁰ production, we infer that the reason for frequently observed S⁰ accumulation is its low solubility. Last, we suggest that nitrate based souring treatment will suffer less from S⁰ accumulation if we (i) act early, (ii) increase temperature and (iii) supplement stoichiometrically sufficient nitrate.

Abbreviations

SRM sulfate reducing microorganisms
oNRM organotrophic nitrate reducing microorganisms
INRM lithotrophic nitrate reducing microorganisms
laNRM lithoautotrophic nitrate reducing microorganisms
lhNRM lithoheterotrophic nitrate reducing microorganisms
laNRM₁ lithoautotrophic nitrate reducing sulfide oxidizing to sulfur microorganisms
laNRM₂ lithoautotrophic nitrate reducing sulfur oxidizing to sulfate microorganisms
laNRM₃ lithoautotrophic nitrate reducing sulfide oxidizing to sulfate microorganisms
lhNRM₁ lithoheterotrophic nitrate reducing sulfide oxidizing to sulfur microorganisms
lhNRM₂ lithoheterotrophic nitrate reducing sulfur oxidizing to sulfate microorganisms
lhNRM₃ lithoheterotrophic nitrate reducing sulfide oxidizing to sulfate microorganisms
lNRM₁ lithotrophic nitrate reducing sulfide oxidizing to sulfate microorganisms
lNRM₂ lithotrophic nitrate reducing sulfur oxidizing to sulfate microorganisms
lNRM₃ lithotrophic nitrate reducing sulfide oxidizing to sulfate microorganisms
ED electron donor
EA electron acceptor
NT nitrate treatment

* Corresponding author.
E-mail address: moein@dtu.dk (M.J. Veshareh).

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1. Introduction

Biologic hydrogen sulfide (H₂S) production due to the activity of sulfate reducing microorganisms (SRM), or the so-called souring process, is a common problem in sewer systems (Jiang et al., 2014) and secondary oil recovery by seawater flooding (Veshareh and Ayatollahi, 2019) due to the odorant, corrosive and toxic nature of H₂S. Nitrate treatment (NT) is one of the intervention methods to control souring by stimulating nitrate reducing microorganisms (An et al., 2010). Nitrate can suppress souring by various mechanisms such as activating organotrophic nitrate-reducing microorganisms (oNRM) that may outcompete SRM for the available organic matter (Agrawal et al., 2012), and reducing sulfide concentration by stimulating lithotrophic nitrate-reducing microorganisms (INRM) (Veshareh et al., 2021). Lithotrophic nitrate-reduction based sulfide-oxidation can be associated with biogenic elemental sulfur (S⁰) (Huang et al., 2015). Due to the corrosive character of S⁰ (Lahme et al., 2019; Schmitt, 1991), its accumulation can reduce the efficiency of NT (Dolfing and Hubert, 2017). Therefore, an understanding of likely nitrate reduction pathways as well as kinetics of sulfate and nitrate reduction is essential for designing promising NT plans.

Respiring prokaryotes catalyze redox reactions (called catabolic actions) to derive energy for growth and maintenance (Jin, 2012). The amount of free energy available from various redox reactions, or Gibbs free energy of catabolic reaction (ΔGcat) has been used by scientists as a method to compare the likelihood of different metabolisms/pathways. For example, Dolfing and Hubert (2017) used this method to predict nitrate reduction pathways in nitrate-based oil reservoir souring mitigation. Since under typical oil reservoir conditions -ΔGcat of nitrate reduction coupled to acetate oxidation was higher than nitrate reduction coupled to sulfide oxidation, they proposed that under realistic oil field conditions nitrate reduction is more likely to be organotrophic rather than lithotrophic. Dolfing and Hubert (2017) claimed that lithotrophic nitrate reduction coupled to partial oxidation of sulfide to sulfur is an exception and can be more favorable than organotrophic nitrate reduction as far as acetate to sulfide molar ratio is less than 0.001, or the temperature is sufficiently low. Additionally, showing that per mole of nitrate sulfide oxidation to S⁰ releases slightly more energy than sulfide oxidation to sulfate, they suggested that S⁰ accumulation is likely to occur under nitrate limiting conditions. The assessment of Dolfing and Hubert labels one metabolism/pathway as favorable and the other as unfavorable, and does not allow an energy based quantitative comparison. Some other metabolisms such as syntrophic oxidation, iron reduction, sulfate reduction and methanogenesis, Jin and Kirk (2016) and Jin and Kirk (2018) used a thermodynamic limiting factor (Fcat) that relates the rate of microbial metabolisms to ΔGcat. The Fcat coefficient is not the only term that links thermodynamics to metabolism kinetics. Growth yield (Y) is another parameter that controls the kinetics of microbial metabolisms and is a function of ΔGcat and of the Gibbs free energy of anabolic reaction (ΔGan) (Jin and Roden, 2011; Smeaton and Van Cappellen, 2018). To the best of our knowledge, no previous research work has used growth yield to relate thermodynamics of microbial reactions to their kinetics. Note that Y and Fcat have been assumed to be constant in biomass explicit microbial kinetic models used over the last decades to simulate souring and its mitigation with nitrate (Hvitved-Jacobsen et al., 2013; Sharma et al., 2008; Veshareh and Nick, 2019, 2021a; 2021b). As such, the error associated with assuming Y and Fcat parameters to be constant in simulation of souring process and nitrate-based souring mitigation measures, is unknown.

To address the abovementioned gaps, in this article, we calculate Y and Fcat to evaluate the range in which they vary under various physiochemical conditions such as electron donor (ED) and electron acceptor (EA) availability, pH and temperature, relevant to sewer systems and petroleum reservoirs. We then use Y to link thermodynamics of sulfur and nitrogen cycle to their kinetics. Using this link, we first revisit the questions raised by Dolfing and Hubert (2017) by illuminating whether nitrate reduction is more likely to be organotrophic or lithotrophic, and whether or not S⁰ accumulation during NT is due to a thermodynamic drive. Lastly, we suggest some measures to minimize S⁰ accumulation in NT of souring.

2. Theory

Lithotrophic nitrate reducers can extract their energy by (i) oxidation of sulfide to sulfur (INRM¹), (ii) oxidation of sulfur to sulfate (INRM²) and (iii) direct oxidation of sulfide to sulfate (INRM₃). Regardless of whether nitrate is reduced through INRM or oNRM, it is reduced either to nitrogen gases through denitrification or to ammonium through dissimilatory nitrate reduction (DNRA) (Callbeck et al., 2013). However, various research works (e.g. (Veshareh and Nick, 2019) and Marjetou et al., 2020) have shown that DNRA is the responsible nitrate reduction pathway in nitrate mitigation of reservoir souring. Therefore, here we do not consider redox reactions related to the denitrification pathway. Lithotrophic nitrate-reducing microorganisms can be autotrophic (lnNRM) (Hamilton et al., 2015) or heterotrophic (lnNRM) (Miroshnichenko et al., 2003). Various organic compounds can serve as the ED of SRM and oNRM; however, Dolfing and Hubert (2017) showed that the energy yield of SRM and oNRM metabolisms is independent of the type of the organic ED used. Therefore, here we only consider acetate as the ED, and as the organic carbon source for cell synthesis of organotrophic and lithoheterotrophic metabolisms. Catabolic and anabolic reactions are from, or are based on the methodology introduced by Smeaton and Van Cappellen (2018). Table 1 and 2 list the catabolic and anabolic reactions that represent various metabolisms studied in this work.

Chemical compounds in the aqueous phase can lose or obtain protons or hydroxide due to reaction with water molecules, or combine with other ions or molecules in a process called speciation (Jin and Kirk, 2018). Due to speciation, chemical compounds dissolved in water can exist in various forms or chemical species. As a result, environmental pH can affect the energetics of redox reactions directly by changing the chemical activity of protons, for redox reactions that consume or produce protons, or indirectly, by controlling the speciation of reactants and products. In this work, all reactions are written using dominant chemical species at pH 7. At a neutral pH, hydrogen sulfide (H₂S⁻) occurs in relatively equal proportions as dihydrogen sulfide (H₂S). Following Smeaton and Van Cappellen (2018), we choose HS⁻. Catabolic and anabolic reactions are written per mole ED and per mole biomass.

| Table 1 | The catabolic and anabolic reaction, Gibbs free energy and enthalpy for various metabolisms studied in this work. |
|-------------------------------|-----------------|-----------------|
| Metabolism | Reaction type | Reaction number |
| oSRM | Catabolic | 1 |
| oNRM | Anabolic | 2 |
| lnNRM₁ | Catabolic | 3 |
| lnNRM₂ | Anabolic | 4 |
| lnNRM₃ | Anabolic | 5 |
| lnNRM₄ | Catabolic | 6 |
| lnNRM₅ | Anabolic | 7 |
| lnNRM₆ | Catabolic | 8 |
| lnNRM₇ | Anabolic | 9 |

Jin and Kirk, 2018
Catabolic and anabolic reactions corresponding to various metabolisms and pathways listed in Table 1.

| Reaction number | Reaction                                      | ΔG_{298.15}^{\circ}(*) | ΔH_{298.15}^{\circ}(*) |
|-----------------|-----------------------------------------------|-------------------------|-------------------------|
| 1               | C_2H_5OH + SO_4^{2-} → 2 HCO_3^- + H^+      | -48.13                  | -359.8                  |
| 2               | 0.525 C_2H_5OH + 0.2 NH_4^+ + 0.275 H^+ → HCO_3^- + 0.4 H_2O | 18.64                  | 41.61                  |
| 3               | C_2H_5OH + H_2O + H^+ + NO_3^- → NH_4^- + 2 HCO_3^- | -530.6                | -534.5                |
| 4               | H^+ + 1.5 H^+ + 0.25 NO_3^- + 0.25 NH_4^+ + 2 S + 0.75 H_2O | -180.2                 | -180.0                 |
| 5               | S + 1.75 H_2O + 0.75 NO_3^- + 0.75 NH_4^- + 0.5 H_2O | -305.9                 | -354.3                 |
| 6               | H^+ + H_2O + H^+ + NO_3^- + 2HCO_3^- | -487.9                  | -534.2                  |
| 7               | HCO_3^- + 2.1 H^+ + 0.2 NH_4^+ + 2.9 H^+ → CH_3 COO^- + 2.1 S + 2 + 5 H_2O | -82.09                  | -55.48                  |
| 8               | HCO_3^- + 0.7 S + 0.2 NH_4^+ + 0.3 H_2O | 85.90                  | 74.22                  |
| 9               | HCO_3^- + 0.525 HS^- + 0.25 NH_4^- + 0.275 H^+ → CH_3 COO^- + 0.7 SO_4^{2-} + 0.6 H^+ | 43.91                  | 41.80                  |

$^a$kJ/mol ED for catabolic reaction and kJ/c-mol biomass for anabolic reaction respectively.

3. Methodology

According to the thermodynamically consistent rate law (Jin and Bethke, 2005; 2007), respiration rate ($r$) [mol ED·s$^{-1}$] can be written as follows:

$\frac{dX}{dt} = v_{max} X F_k F_T$ (1)

where $v_{max}$ [mol ED·(mol biomass)$^{-1}$·s$^{-1}$] is the maximum rate of a metabolism, X is the biomass concentration [mol·(kg water)$^{-1}$], $F_k$ is a kinetic limiting term and $F_T$ is a thermodynamic limiting term. According to Monod (1949) and LaRowe et al. (2014) $F_k$ and $F_T$ can be defined as follows:

$F_k = \frac{C_{ED}}{K_{ED} + C_{ED} + C_{EA}}$ (2)

$F_T = \begin{cases} \exp \left( \frac{\Delta G_{cat}}{RT} \right) & \text{for } \Delta G_{cat} \leq 0 \\ 1 & \text{for } \Delta G_{cat} > 0 \end{cases}$

Where $C$ [mol·(kg water)$^{-1}$] is concentration, K is half saturation constant, $\Delta G$ $^a$ [J·mol$^{-1}$] is the Gibbs free energy of a metabolism’s catabolic reaction under non-standard conditions, $F$ [C·mol$^{-1}$] is the Faraday constant, R [J·mol$^{-1}$·K$^{-1}$] is the gas constant, T [K$^{-1}$] is temperature, and $\Delta \psi$ [V] is the electric potential across the membrane. The subscripts ED and EA denote electron donor and electron acceptor, respectively. Even though the value of $\Delta \psi$ can be different for various low energy environments and for various metabolisms, an evaluation of investigations on several distinct organisms led to the proposition that the expression $\Delta \psi$ can be considered a representative value for $\Delta \psi$ (Dimroth et al., 2003; Kadenchab, 2003; Toei et al., 2007) and Daniels et al. (1984) reported a value of 118 mV for $\Delta \psi$. Therefore, here we assume that $\Delta \psi$ is equal to 120 mV for all the considered metabolisms.

Gibbs free energy of a reaction under non-standard condition can be calculated as follow:

$\Delta G = \Delta G^\circ + RT \ln Q$ (4)

Where $\Delta G^\circ$ is the Gibbs free energy of a reaction under biochemical standard conditions (25°C, 1 atm, pH 7 and chemical activity of unity (Jin and Kirk, 2018)) and can be calculated by subtracting the sum of Gibbs free energy of formation ($\Delta G_{f}$) of substrates from that of products. Q is the reaction quotient. For a hypothetical reaction aA + bB $\rightarrow$ cC + dD, reaction quotient is equal to:

$Q = \frac{[C]^c[D]^d}{[A]^a[B]^b}$ (5)

Where $[S]$ is the activity of a reactant/product ($S = \{A, B, C, D\}$). Chemical speciation and activity of species are calculated using LLNL Thermodynamic Database (Delany and Lundeen, 1990) and PHREEQC v.3 (pH-Redox-EQuilibrium written in the C programming language (Parkhurst and Appelo, 2013). Activity of $S_{H_2}$ is assumed to be equal to its concentration. Gibbs-Helmholz equation is used to correct $\Delta G$ for non-standard temperatures:

$\Delta G_{T} = \Delta G_{298.15}^\circ \left( \frac{T}{298.15} \right) + \Delta H_{298.15}^\circ \left( \frac{298.15 - T}{T} \right)$ (6)

Where $\Delta H_{298.15}$ is the enthalpy of a reaction in standard condition and can be calculated by subtracting the sum of enthalpies of formation of substrates ($\Delta H_f$) from that of products. The value of $\Delta G_{T}$ and $\Delta H_f$ for acetate is obtained from Shock (1995), for inorganic species from Shock et al. (1997), and for biomass from Roels (1980).

The rate of biomass (X) formation is given by:

$\frac{dX}{dt} = (\mu - b)X$ (7)

Where $\mu$ [s$^{-1}$] is the specific growth rate and b [s$^{-1}$] is the specific maintenance rate. The specific growth rate is linked to respiration rate using growth yield (Y) [mol biomass·(mol ED)$^{-1}$] through the following relationship:

$\mu = \frac{Y}{X}$ (8)

Growth yield Y is dependent on $\Delta G_{cat}$, $\Delta G_{f}$, and energy utilization efficiency of organisms (VanBriesen, 2002). In order to study the effect of changes in chemical (variation in species concentrations and pH) and physical (e.g. temperature) conditions, the Gibbs Energy Dynamic Yield Method (GEDYM) of Smeaton and Van Cappellen (2018) is employed:

$Y = \frac{a(\Delta G_{cat}^\circ)^3 - \beta \Delta G_{cat}^\circ \Delta G_{cat}}{\alpha(\Delta G_{cat}^\circ)^2 - \Delta G_{cat}(\beta \Delta G_{cat} + \alpha \Delta G_{cat} + \Delta G_{cat}) + m \Delta G_{cat}}$ (9)

Where $a$ and $\beta$ are model parameters and equal to -0.0004 and -0.0694 for a broad range of metabolisms including all major EAs, fermentation, methanogenesis and acetogenesis. Smeaton and Van Cappellen only considered hydrogen as the non-organic ED. Note that GEDYM has not been validated for nitrate-reduction, and sulfide-oxidation pathways. However, as the model is valid for all the other metabolisms mentioned above, here we assume that Y for nitrate-reduction and for sulfide-oxidation pathways follows equation 9 as well.

According to equation 7, the biomass growth depends on the thermodynamic dependent term of Y and $F_T$. Assuming that microorganisms that derive their energy from the various metabolisms (i) are all present, (ii) have the same kinetic parameters such as $v_{max}$, $K_A$ and $K_D$ and (iii) have the same initial biomass concentration (X), terms Y and $F_T$ determine which metabolism proceeds faster. For each metabolism, we consider a set of pH, temperature and concentration of reactants and products in the range observed in petroleum reservoirs and sewer systems, referred to as the base condition.

In order to analyze the temperature effect, the temperature range of...
1 to 110 °C is evaluated. This is because contrary to sewer systems, where souring occurs in a relatively narrow temperature range, in petroleum reservoirs souring can occur in a relatively broad temperature range, anywhere between the injection temperature (e.g. between 4 to 25 °C) if North Sea water is injected (CLIMATE-DATA.ORG, 2021) to the reservoir temperature. The temperature of subsurface reservoirs depends on their depth (e.g Willems & Nick 2019). Sourcing in temperatures higher than 110°C can be ignored as these temperatures preclude microbial activity (Thaysen et al., 2021).

Since chemical compounds depending on temperature and pH can appear in water in various forms, we define the base condition based on the sum of various forms. In the base condition, the water phase is saturated with $S^0$. Elemental sulfur solubility is calculated by exponential regression of data reported by Kamyshny Jr (2009). Table 3 lists the base condition. $C(\cdot)$ stands for the sum of carbonate species including carbonic acid ($H_2CO_3$), bicarbonate ($HCO_3^-$), carbonate ($CO_3^{2-}$), and dissolved carbon dioxide ($CO_2(gaq)$). $S(\cdot)$ stands for the sum of sulfide species including dihydrogen sulfide ($H_2S$), hydrogen sulfide ($HS^-$) and sulfide ($S^2-$). $N(\cdot)$ stands for the sum of ammonium ($NH_4^+$) and ammonia ($NH_3$), and $C(0)$ stands for sum of acetate and acetic acid. We investigate the variations in $Y$ and $F_T$ due to deviations from the base case by changing physical (e.g. temperature) and chemical conditions (e.g. pH and EA concentration).

4. Results

4.1. Variations in $Y$ and $F_T$ for sulfate reduction

4.1.1. Effect of substrate concentration

Fig. 1A and B show $Y$ and $F_T$ of SRM for various ED (acetate) and EA (sulfate) concentrations for the base case. The value of $Y$ changes significantly from 0.4 for EA = ED concentration of 0.028 M, to zero if EA and ED are concentration both are less than $10^{-5}$ M (Fig. 1A). This is because according to equation 4, by reducing the concentration of EA and ED (reactants of SRM catabolic reaction), and ED (reactant of SRM anabolic reaction), respectively, the energy yield of the catabolic reaction ($-\Delta G_{cat}$) decreases and the energy demand of the anabolic reaction ($\Delta G_{an}$) increases. The value of $F_T$ follows a similar trend as $Y$ and decreases from a maximum of around 0.5 when ED and EA are high (0.028 M) to around zero ($6 \times 10^{-4}$ M) when EA and ED are minimal ($10^{-10}$ M, Fig. 1B).

4.1.2. Effect of pH

Fig. 1C demonstrates the effect of pH on $Y$ and $F_T$ of SRM for the base case. In the pH range of 6.6 to 9.8, $F_T$ values are relatively low and $Y$ shows only a small reduction. Considering the catabolic reaction of SRM and equation 3, $F_T$ depends only on $\Delta G_{cat}$, and $\Delta G_{cat}$ depends on the activity of $HCO_3^-$, $HS^-$ and $CO_3^{2-}$. Since the activity of these species is relatively pH independent in the pH range of 6.6 to 9.8, $\Delta G_{cat}$ and consequently $F_T$ stay relatively constant. The value of $Y$ depends on both $\Delta G_{cat}$ and $\Delta G_{an}$. While $\Delta G_{cat}$ is relatively constant, in the range of 6.6 to 9.8 due to increase in $NH_4^+$ (Fig. 2D), $\Delta G_{an}$ increases slightly and this leads to a small reduction in $Y$ (from 0.18 to 0.14). For pH values less than 6.6 and above 9.8 decreases in the activity of $HCO_3^-$ and $HS^-$ result in increases in $Y$ and $F_T$. For pH values less than 6.6, the decrease in acetate activity cancels out the effect of reduction in $HCO_3^-$ and $HS^-$ activity. Therefore, the slope of $F_T$ (that is, the absolute value of the derivative of $F_T$) is slightly sharper for pH values higher than 9.8 (0.19 per unit pH) than pH < 6.6 (0.16 per unit pH). For pH values above 9.8, a significant decrease in $NH_4^+$ activity causes a significant increase in $\Delta G_{an}$. The increase in $\Delta G_{an}$ cancels out the decrease in $\Delta G_{cat}$ and as a result, the increase in $Y$ values due to an increase in pH above 9.8 (0.04 mol biomass per mol ED) is less than the increase in $Y$ values due to a decrease in pH below 6.8 (0.13 mol biomass per mol ED).

4.1.3. Effect of temperature

Fig. 1D illustrates the impact of temperature on $Y$ and $F_T$ for SRM for the base case. Increase in temperature increases the catabolic energy yield ($-\Delta G_{cat}$) as well as $\Delta G_{an}$. While $Y$ decreases slightly (from 0.19 to 0.17 mol biomass per mol ED) it depends on both $\Delta G_{cat}$ and $\Delta G_{an}$. $F_T$ decreases by a factor of 2 (from 0.13 to 0.26) since it is only dependent on $\Delta G_{cat}$. Fig. 1E demonstrates how $HS^-$ concentration affects $Y$ and $F_T$. As $HS^-$ is the product of the catabolic reaction of SRM, the reduction in $HS^-$ increases $\Delta G_{an}$, and as a result, both $Y$ and $F_T$ for SRM increase.

4.2. Variations in $Y$ and $F_T$ for nitrate reduction

Various nitrate reduction pathways considered in this study have a sufficiently high $-\Delta G_{cat}$ such that $F_T$ for all of them is equal to one under the conditions for which $Y$ is plotted in Fig. 3.

4.2.1. Effect of substrate concentration

Fig. 3 shows $Y$ for the various nitrate reduction pathways listed in Table 1. For the base case, when the ED concentration increases, growth yield increases for all nitrate reduction pathways. The smallest $Y$ values are associated with laNRM1 and lhNRM1 (maximum 0.12 and 0.34, respectively, Fig. 3A), since these two metabolisms have the lowest $-\Delta G_{cat}$ (181.96 kJ per mol ED). The value of $\Delta G_{an}$ for laNRM1 (82.09 kJ per mol biomass) is the smallest value among $\Delta G_{an}$ of other nitrate reduction metabolisms listed in Table 1. However, the value of $\Delta G_{an}$ for laNRM1, as function of ED concentration (HS$^-$) varies from -1.1 to 145 kJ per mol biomass. Therefore, while laNRM1 and lhNRM1 have the same $\Delta G_{cat}$, lhNRM1 has a lower $\Delta G_{an}$ compared to lhNRM1 (41.84 kJ per mol biomass) for ED concentrations greater than $2.4 \times 10^{-5}$. A smaller $\Delta G_{an}$ for lhNRM1 does not cause a higher $Y$ value compared to lhNRM1 as $Y$ decreases only in the number of moles of ED (o) that is utilized in order to synthesize 1 mol of biomass (Smeaton and Van Cappellen, 2018). In lhNRM1 the $\Delta G_{cat}$ is equal to 536.0 kJ per mol ED) than laNRM1 (487.9 kJ per mol ED). The metabolism of oNRM has also a higher $-\Delta G_{cat}$ compared to lhNRM1. However, the value of $\Delta G_{cat}$ is equal to 0.525 for oNRM and 0 for lhNRM1. That is, while $-\Delta G_{cat}$ of oNRM is equal to 536.0 kJ per mol ED, only between 50 to 74% of it (solid line, Fig. 3B) is used for energy production. As a result, the energy produced by oxidation of 1 mol ED in oNRM metabolism is in the range of 57 to 82% of that of lhNRM1 (dotted line in Fig. 3B). Therefore, for a given ED concentration (e.g. $10^{-4}$ M ED), $Y$ values for lhNRM1 (1.1 mol biomass per mol ED) are higher than for oNRM (0.77). Similar to the plot of $Y$ versus ED concentration (Fig. 3A), the plot of $Y$ versus EA concentration (Fig. 3C) has a positive slope for all nitrate reduction metabolisms. However, the slope of $Y$ versus log of EA concentration is smaller than the slope of $Y$ versus log of ED concentration. For metabolisms with $o > 0$, this is because ED is present in both catabolic and anabolic reaction, whereas EA is only present in the anabolic reaction.

| Table 3
| Base case condition. |
|----------------------|
| pH                  | 7       |
| T°C                 | 75      |
| Nitrate (mM)        | 1       |
| Sulfate (mM)        | 1       |
| CO(2) (mM)          | 1       |
| CO(3) (mM)          | 8.3     |
| N(3) (mM)           | 2.8     |
| S(2) (mM)           | 1       |
present in the anabolic reaction. For metabolisms that partially oxidize HS\(^-\), the stoichiometric coefficient of EA is a quarter of the stoichiometric coefficient of ED. Consequently, \(\Delta G_{\text{cat}}\) is a stronger function of ED concentration than of EA concentration.

4.2.2. Effect of pH

Fig. 3D illustrates that in general an increase in pH decreases Y for all the nitrate-reducing metabolisms as they are all proton consuming. However, for low pH values (from 3 to 5), the influence of increasing pH on \(\Delta G_{\text{cat}}\) is canceled out by an increase in HS\(^-\) activity (Fig. 2B) for laNRM\(_1\) and lhNRM\(_1\). The stoichiometric ratio of HS\(^-\) to H\(^+\) is bigger for complete oxidation of sulfide compared to the partial oxidation. In consequence, in the pH range of 3 to 5 the impact of an increase in HS\(^-\) concentration on \(\Delta G_{\text{cat}}\) of lhNRM\(_3\) and laNRM\(_3\) is higher than the impact of an increase in pH, leading to an increase in Y. The pH increase effect in oNRM metabolism is canceled out by the increase in acetate concentration (Fig. 2C) in the pH range of 3 to 4. The reduction in Y decreases in pH values higher than 10 for all metabolisms due to reduction of NH\(_4^+\) concentration. For oNRM metabolism, pH values higher than 10 also reduce HCO\(_3^-\) concentration. Consequently, the Y value for oNRM levels off relatively at pH 10.
increase significantly from 0.27 to 0.41, and from 0.07 to 0.14, by a
4.2.3. Effect of temperature and sulfate concentration
Fig. 2.
reduction in temperature from 110 to 4
reducing metabolisms, Y of laNRM
Fig. 2. Variation with pH in concentrations of A) carbolic acid (blue), HCO$_3^-$
(black) and CO$_2^-$ (red), B) H$_2$S (blue), HS$^-$ (black) and S$^2-$ (red), C) acetic acid
(blue) and acetate (black) and D) NH$_2$N (blue) and NH$_3$ (black), predicted by
PHREEQC v.3 for three arbitrary temperatures of 50°C (dashed line), 75°C
(solid line) and 100°C (dotted line).

4.2.3. Effect of temperature and sulfate concentration
Similar to SRM metabolism, temperature influence on Y value of
oNRM, lhNRM$_3$, laNRM$_3$ is relatively insignificant (maximum 3.6, 6.0
and 4.0 % change, respectively). The Y values of lhNRM$_1$ and laNRM$_1$
increase significantly from 0.27 to 0.41, and from 0.07 to 0.14, by a
reduction in temperature from 110 to 4°C since the decrease in temperature
reduces S$^0$ solubility (Kamyszny Jr, 2009). Among all nitrate
reducing metabolisms, Y of laNRM$_3$ and lhNRM$_3$ depend on sulfate
concentration. Fig. 3F shows that Y of laNRM$_3$ is greater than Y of oNRM
for sulfate concentrations lower than $10^{-5}$M.

5. Discussion
5.1. Importance of taking into account variations in Y and $F_T$
SRM activity has caused detrimental consequences such as corrosion and
reservoir plugging for seawater injection into oil reservoirs (Youssaf
et al., 2009). In sewer systems, the H$_2$S produced by SRM is a major
source of odor nuisance (Jiang et al., 2015) and corrosion of concrete
sewer pipes (Pikar et al., 2019). Modeling SRM activity is also essential
for mainstream anaerobic digestion technology development (Duran
et al., 2020). Microbial sulfate-reduction models have been used to
predict the extent of reservoir souring, aiming to minimize the impacts
and costs of SRM activity. To the best of our knowledge, in these models
Y has been always assumed to be a constant, and the energy that SRM
require to maintain transmembrane electric potentials has been ignored
(i.e. $F_T=1$) (e.g. Cheng et al., 2016; Haghshenas et al., 2012; Veshareh
et al., 2021)). Underestimation or overestimation of souring in seawater
injection can cause erroneous material design for injection/production
wells and surface facilities (Johnson et al., 2017). Additionally, inac-
curate estimate of souring does not allow efficient treatment design. For
example, in nitrate treatment, over usage of nitrate can lead to accumu-
lation of nitrite, which increases corrosion in production wells
(Huang and Zhang, 2006). The growth yield of SRM varies significantly
from around 0.33 when the concentration of SRM ED and EA is around
the maximum concentration observed in typical seawater flooding
processes (0.028 M) (Vigneron et al., 2017), to zero for ED and EA
concentrations smaller than 1μM (Fig. 1A). In sewer systems, petroleum
reservoirs as well as the biofilm of bioreactors, there is invariably a
gradient of substrates. As our results show, the value of Y that controls
souring in time and space domains is significantly dependent on the
substrate concentrations. Assuming a constant Y value - the value of
which depends on the laboratory conditions under which Y has been
determined – will thus cause over or underestimation of souring rates in
that given time and location. Due to the low exergonicity of SRM cata-
bolic reaction, and depending on the concentration of ED and EA, SRM
kinetics will be thermodynamically limited by 60 to around 100% ($F_T=
0 to 0.4, Fig. 1B). That is, while assuming a constant Y may over or
underestimate souring rate, ignoring $F_T$ will always lead to over-
estimation of souring. Therefore, accurate souring simulation requires

10^{-5}$M.

5. Discussion
5.1. Importance of taking into account variations in Y and $F_T$
SRM activity has caused detrimental consequences such as corrosion and
reservoir plugging for seawater injection into oil reservoirs (Youssaf
et al., 2009). In sewer systems, the H$_2$S produced by SRM is a major
source of odor nuisance (Jiang et al., 2015) and corrosion of concrete
sewer pipes (Pikar et al., 2019). Modeling SRM activity is also essential
for mainstream anaerobic digestion technology development (Duran
et al., 2020). Microbial sulfate-reduction models have been used to
predict the extent of reservoir souring, aiming to minimize the impacts
and costs of SRM activity. To the best of our knowledge, in these models
Y has been always assumed to be a constant, and the energy that SRM
require to maintain transmembrane electric potentials has been ignored
(i.e. $F_T=1$) (e.g. Cheng et al., 2016; Haghshenas et al., 2012; Veshareh
et al., 2021)). Underestimation or overestimation of souring in seawater
injection can cause erroneous material design for injection/production
wells and surface facilities (Johnson et al., 2017). Additionally, inac-
curate estimate of souring does not allow efficient treatment design. For
example, in nitrate treatment, over usage of nitrate can lead to accumu-
lation of nitrite, which increases corrosion in production wells
(Huang and Zhang, 2006). The growth yield of SRM varies significantly
from around 0.33 when the concentration of SRM ED and EA is around
the maximum concentration observed in typical seawater flooding
processes (0.028 M) (Vigneron et al., 2017), to zero for ED and EA
concentrations smaller than 1μM (Fig. 1A). In sewer systems, petroleum
reservoirs as well as the biofilm of bioreactors, there is invariably a
gradient of substrates. As our results show, the value of Y that controls
souring in time and space domains is significantly dependent on the
substrate concentrations. Assuming a constant Y value - the value of
which depends on the laboratory conditions under which Y has been
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that given time and location. Due to the low exergonicity of SRM cata-
bolic reaction, and depending on the concentration of ED and EA, SRM
kinetics will be thermodynamically limited by 60 to around 100% ($F_T=
0 to 0.4, Fig. 1B). That is, while assuming a constant Y may over or
underestimate souring rate, ignoring $F_T$ will always lead to over-
estimation of souring. Therefore, accurate souring simulation requires
considering both of these thermodynamic dependent parameters.

Among various environmental conditions, pH is a classical physiological parameter. In order to tolerate acidic or alkaline conditions, microorganisms require special surface properties that protect cells from proton or hydroxide ions (Golyshina and Timmis, 2005; Horikoshi, 1999). Very low or high pH values restrict microbial reactions due to various reasons. For example, at low pH conjugate acids become abundant and diffuse into cell membrane, destabilizing the membrane and dissipating proton motive force (Russell and Dombrowski, 1980). Our results show that in near neutral pH, with an increase in pH, the SRM rate decreases due to reduction in both $F_T$ and $Y$. The effect of pH on SRM activity has been well studied in the context of wastewater treatment since the pH of waste water can be subject to significant changes due to processes such as fermentation of organics or treatment with alkali (Sharma et al., 2013). Gutierrez et al. (2009) reported that a pH increase from 7.6 to 8.6 and 9.0 reduces the biological sulfate reduction by 30 to 50%.

To further highlight the importance of considering the effect of thermodynamics on souring kinetics, we compare our data with experimental and modelling data published by (Sharma et al., 2014). These authors conducted several batch experiments using a sewer biofilm reactor at various pH values in the range of 4.0 to 9.0 and observed that sulfate reduction rate is maximal at pH 6.3, and decreases when pH deviates from this value. In order to model the pH effect Sharma et al. (2014) used the pH inhibition expression proposed by Angelidaki et al. (1993) for pH values lower than 6.75, and for higher pH values they employed the non-competitive inhibition model of (Siegrist et al., 2002) that is focused on free ammonia. The model developed by Sharma et al. (2014) predicts that souring rate in the range of 6.4 to 8.3 is independent from pH (i.e. is constant), whereas experimental data shows that souring rate decreases with increase in pH in this range (Fig. 4A). The model of Sharma et al. (2014) ignores variations in $Y$ due to pH change and does not take into account any thermodynamic limiting factor. Since the rate of sulfate reduction in the course of Sharma et al. (2014) experiments (Fig. 2 in their work) is constant, the effect of $Y$ variations can be neglected. To evaluate whether the variations in sulfate reduction rate in the pH range of 6.4 to 8.3 is related to changes in $F_T$, we consider the value of sulfate reduction rate at a reference value and predict other sulfate reduction rates using the following equation:

$$r(pH) = \frac{F_T(pH)}{F_T(ref)}$$

Fig. 4A shows a good agreement between the values predicted using equation 10 and the experimental data. Therefore, considering $F_T$ with $\Delta\gamma = 100 \text{mV}$ can explain changes in sulfate reduction rate in the pH range of 6.4 to 8.3. The strong correlation between $F_T$ and rates is probably due to the minimal impact of physiological parameters as pH values are relatively close to neutral. Note that in pH higher than 7, $-\Delta G_{cat}$ is less than 45 kcal (Fig. 4B), i.e. the model introduced by (Jin and Bethke, 2003) would predict $F_T$ to be equal to zero. Therefore, using the thermodynamic limitation factor proposed by LaRowe et al. (2012) seems to be more appropriate for modeling souring. High pH values also decrease H$_2$S liquid to gas mass transfer, increasing the total dissolved sulfide (Ganigue et al., 2011). Higher dissolved sulfide concentrations reduce SRM activity not only due to its toxicity (Kushkevych et al., 2019; McCartney and Oleszkiewicz, 1991), but also by reducing the $-\Delta G_{cat}$ of sulfate reduction (Fig. 1E).

5.2. Is it valid to use the GEDYM for lNRM pathways?

As mentioned earlier in the methodology section, we assume that GEDYM is valid for estimating the growth yield of lithotrophic metabolisms listed in Table 1. Zeng and Zhang (2005) conducted two batch experiments and measured the growth yield for lnNRM to be 0.75 and 0.85. The growth yield values calculated in this work using GEDYM (Fig. 3E), matches these experimental values, suggesting that GEDYM holds true also for lithotrophic nitrate reduction based sulfide oxidation.

5.3. What nitrate-reduction pathway is expected to be faster thermodynamically?

Assuming (i) a diverse microbial community that can sustain the various nitrate reduction pathways considered in this study, (ii) all community members have the same kinetic parameters and initial biomass concentration, and (iii) the concentration of EA and ED is equal for all metabolisms, lhNRM$_3$ is around two times faster than oNRM pathway, for various physiochemical conditions found in typical petroleum reservoirs. This is in disagreement with the work of Dolfing and Hubert (2017) where except for special conditions such as low temperature, or low acetate to H$_2$S ratios, oNRM pathway is predicted to prevail. This is because Dolfing and Hubert (2017) consider the pathway with a higher $-\Delta G_{cat}$ as the dominant pathway, while not considering the anabolic reaction. Our results highlights that to find the dominant metabolism among metabolic pathways with high catabolic energy yields (i.e. $F_T = 1$), $-\Delta G_{cat}$ cannot be used directly to reveal the dominant pathway as it has been used for other metabolisms such as methanogenesis or acetogenesis (Jin and Kirk, 2018). Note that while the value of $Y$ allows a quantitative comparison between the rate of two metabolisms in a system at its initial condition, the relationship of respiration rate and $Y$ is not linear and rather exponential (equations 1, 7 and 8). Therefore, a two time higher $Y$ of lhNRM$_3$ compared to that of oNRM can lead to lhNRM$_3$ domination. This is in agreement with various studies available in the literature. Hubert et al. (2005) injected nitrate into a soured bioreactor (sulfide concentration of 12 mM) and observed that despite injection of 25 mM lactate, nitrate reduction was entirely coupled to sulfide oxidation to sulfate. Lambo et al. (2008) showed that lithotrophic reduction of nitrate always preceded organotrophic reduction of nitrate.

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**Fig. 4.** A) Circle markers, solid line and the dotted line show sulfate reduction rate at different pH values measured by Sharma et al. (2014), modeled by Sharma et al. (2014) and calculated by using equation 10, respectively. B) The Gibbs free energy of catabolic reaction of sulfate reducing microorganisms. C) Left y-axis, circle markers, elemental sulfur ($S^0$) solubility and right y-axis, dashed line, the kinetic limiting factor ($F_T$) that takes into account the effect of limitation of electron donor ($S^0$) on the kinetics of lithotrophic nitrate-reduction, sulfur-oxidation.
Mathioudakis et al. (2006) by conducting experiments on sour waste water samples (sulfide concentration of around 1 mM) reported that nitrate reduction is preferentially autotrophic and that heterotrophic nitrate reduction only commenced after sulfide had been completely oxidized. In another study, Okabe et al. (2003) observed that in sewer biofilm experiments, 65% of the $\text{H}_4\text{S}$ produced by SRM residing in deeper layers of the biofilm was oxidized via INRM in shallower layers. A similar observation has been reported by Garcia-de-Lomas et al. (2007).

Dolfling and Hubert (2017) discussed whether INRM$_1$ or INRM$_2$ is expected to be the dominant INRM pathways by comparing the $\Delta G$ of acetate driven reduction of sulfate and $S^0$. They proposed that because $\Delta G$ of acetate driven reduction of $S^0$ is less than acetate driven reduction of sulfate, INRM$_3$ is the dominant INRM pathway. They suggested that the dominance of INRM$_1$ is more likely at lower temperatures, as the differences between $\Delta G$ of acetate driven reduction of $S^0$ and that of acetate driven reduction of sulfate, increases with temperature. According to our results (Fig. 3), under all studied conditions, lithotrophic sulfide based nitrate reduction is envisaged to be through INRM$_1$ pathways rather than INRM$_2$ due to significantly higher Y values (1.6 to 17 times).

5.4. Why does elemental sulfur accumulation occur?

The low growth yield of lithotrophic nitrate reduction coupled to partial sulfide oxidation to sulfur (INRM$_1$ and INRM$_2$) does not imply that nitrate treatment does not cause $S^0$ production. It merely means that if all the parameters that affect various nitrate reduction pathways are equal, and if oxidation of sulfide to sulfate in a single step is possible, thermodynamically a lower fraction of nitrate reduction is coupled to partial sulfide oxidation and a higher fraction of nitrate is coupled to either complete sulfide oxidation or to oxidation of organic compounds. Veshareh et al. (2021) showed that nitrate treatment by Desulfobacterium autotrophicum and a microbial community of a production water enrichment that contained organotrophic nitrate reducing members from Delta- and Gammaproteobacteria caused $S^0$ concentrations of 17 to 22 $\mu$M. Jiang et al. (2009) observed that lithotrophic nitrate reduction based sulfide oxidation occurs first by oxidation of sulfide to sulfur (INRM$_1$), followed by oxidation of sulfur to sulfate (INRM$_2$). These authors reported that the rate of INRM$_2$ is 15% of that of INRM$_1$, Yang et al. (2005) observed that elemental sulfur was the end product of nitrate-based sulfide oxidation. The accumulation of $S^0$ due to NT has also been reported by Liang et al. (2016). Fig. 3 shows that INRM$_2$ metabolisms have higher Y values than INRM$_1$ metabolisms due to significantly higher $\Delta G_{\text{cat}}$ values, i.e. based on thermodynamics the rate of INRM$_2$ should be higher than that of INRM$_1$. Fig. 4 demonstrates why INRM$_2$ can be slower than INRM$_1$ even though it is thermodynamically more favorable. Sulfur solubility in water is extremely low and increases exponentially with temperature from $6.3 \times 10^{-9}$ at 4°C to $6.3 \times 10^{-7}$ M at 80°C (Kamyshny Jr, 2009). By considering $1.7 \times 10^{-8}$ M (Mora et al., 2015) as the half saturation constant for sulfur, and assuming that the environment is saturated with sulfur, the limiting kinetic term ($f_K$) will be between $2 \times 10^{-8}$ and $4 \times 10^{-8}$ for 4°C and 80°C, respectively. That is, if we ignore the dependency of INRM$_1$ on any other factor, reduction in temperature from 80 to 4°C, makes INRM$_1$ 20 times slower merely because of the reduction in $S^0$ solubility. Therefore, decrease in temperature does not promote $S^0$ accumulation only by increasing the growth yield of INRM$_1$ due to an increase in Y, but mainly by reducing $S^0$ solubility and thereby reducing the rate of $S^0$ oxidation to sulfate. This explains why in sewer systems where the temperature is relatively low (around ambient temperature) NT is associated with elemental sulfur production as shown by Liang et al. (2016) and Jiang et al. (2009). In reservoir souring processes, $S^0$ accumulation can be expected to occur mainly in injection tubing and near the well bore area. However, the extent of $S^0$ accumulation can spread to the production well, provided presence of fractures reduce the travel time between the injection and production wells and thereby reducing the water temperature in the production well. Given the abovementioned temperature dependence of $S^0$ accumulation, one can conclude that heating injection water can remediate the $S^0$ related corrosion associated with NT of reservoir souring. Note that in Fig. 4 only the range of 4 to 80°C has been considered because we did not have $S^0$ solubility data outside this range.

5.5. Single-step sulfide oxidation vs two-step sulfide oxidation

Single step nitrate-based oxidation of sulfide (INRM$_3$) seems to have both the thermodynamic advantage as well as the kinetic advantage as no elemental sulfur is produced as an intermediate. However, Cui et al. (2019) reported that nitrate reducers that catalyze single step sulfide oxidation to sulfate can only harvest two electrons per nitrate reduced as the nitrate reduction pathways stops at nitrite due to a lack of nitrite reductase. The nitrite produced in the single-step oxidation of sulfide to sulfate is then reduced further by nitrate reducers that oxidize sulfide in two-steps. Therefore, two-step sulfide oxidation has a physiological advantage and is expected to always co-occur with the single-step sulfide oxidation as the organisms involved can reduce nitrite. Cui et al. (2019) showed that compared to the two-step sulfide oxidation, single-step oxidation of sulfide is more sensitive to sulfide, suggesting that the physiological advantage of two-step sulfide oxidation when nitrate treatment is applied increases with the souring level. These observations have implications for souring management where (i) low temperatures, (ii) limited nitrate availability compared to sulfide, or (iii) limited travel time between the injection and production well can cause elemental sulfur accumulation. Therefore, we speculate that souring treatment efficiency by nitrate injection can be improved by (i) early treatment, (ii) increasing temperature, (iii) making sure that stoichiometrically enough nitrate is available for sulfide oxidation, and (iv) reducing injection flow rate (in the case of souring in petroleum reservoirs) such that sufficient time is given to INRM$_3$ to complete sulfide oxidation (from sulfide to sulfate). Note that half-hearted measures, that include only some of these conditions, may cause even more severe souring problems as for example increase in temperature can increase $H_2S$ emission from the liquid phase to the gas phase.

6. Caveats and future directions

Zhang et al. (2018) have shown that polysulfide formation substantially increases the rate of organotrophic sulfur reduction to sulfide. Qiu et al. (2020) showed that sulfur-based autotrophic denitrification is substantially enhanced due to polysulfide formation. This is why Zhang et al. (2021) introduced polysulfide as an “electron shuttle” that accelerates sulfur oxidation or reduction. Indeed, the polysulfide formation step should not be ignored in the simulation of sulfide/sulfur/sulfate transformations when the exact value of elemental sulfur accumulation or the rate of accumulation is to be evaluated. However, in this study, polysulfide formation from sulfide and elemental sulfur, and polysulfide oxidation to sulfide has been ignored in the sulfur cycle because rather than estimating the pool sizes of the $S^0$ species, the aim was to predict the likelihood of elemental sulfur accumulation. Future work can validate the proposed methodology in this paper for polysulfide oxidation and study whether the faster oxidation/reduction rates of polysulfide is due to the thermodynamic advantage of this species under varied physiochemical conditions.

7. Conclusions

The key findings of this study can be summarized as follows:

- Growth yield can be used to link the differences in energetics of microbial reactions with their kinetics for metabolisms that have a sufficiently high $-\Delta G_{\text{cat}}$ such that thermodynamic limiting factor is equal to one.
• Since the kinetic parameters of souring processes can be substantially affected by thermodynamics, it is essential to couple souring models to a thermodynamic model that takes into account the effect of variations in catalytic energy yield and anabolic energy demand on the metabolism rate.

• Compared to other nitrate reduction pathways such as organotrophic nitrate-reduction, based on the magnitude of growth yield, single-step lithotrophic nitrate reduction driven sulfide-oxidation to sulfate is expected to be the dominant nitrate reduction pathway in sour systems.

• Even though nitrate-reduction, sulfur oxidation to sulfate is thermodynamically expected to be faster than nitrate-reduction, sulfate oxidation to sulfur, it is slower due to the low solubility of elemental sulfur.

• Elemental sulfur accumulation associated with nitrate-reduction driven sulfide-oxidation is prevalent at lower temperatures due to the exponential decrease of sulfate solubility with temperature.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have influenced the work reported in this paper.

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