Composition of molding material for ceramic tiles

Vladimir Adamyan¹, Svetlana Kalashnikova¹, Victoria Burlakova¹, Luiza Seferyan²*, and Galina Sergeeva¹

¹Don State Technical University, 344002, Rostov-on-Don, Russia
² Rostov-on-Don College of Communication and Informatics, 344000, Rostov-on-Don, Russia

Abstract. This article discusses the problems of creating new compositions for ceramic tiles. There are two ways to process the composition of the molding material - dry and wet. A description of the wet processing method is given. The molding of the plastic mass is carried out by pressing to obtain a tile with a size of 50 x 150 mm. The molded product goes through the following stages of the technological regime: blowing in a drying stove with an increase in temperature from 25 °C to 700 °C for 3-4 hours. Further, at a speed of 15-20 degrees per minute, the temperature rises to 1050 °C and then the heat treatment continues for 30 minutes. After annealing, the product is cooled and tested.

1 Introduction

Various sectors of the national economy use ceramic products - bricks, tiles for wall and floor cladding, sanitary and technical ceramics.

One of the most important stages for the formation of ceramics is the initial composition and mass of the materials processed by various methods. The main processing methods are dry and wet. Due to the high energy consumption, the wet method is more expensive but gives better results [1].

Various minerals can be used in the line mass. For example, according to the requirements of GOST (GOST R 56828.20-2017 Best available technologies. Production of ceramic tiles. Aspects of increasing energy and environmental efficiency), for the production of ceramic tiles, a composition that includes clay to ensure the plasticity of the molding mass, quartz sand, which forms the structure and the skeleton of the product is used, as well as feldspars and carbonates, which impart viscosity to the product and a glassy surface [2, 3].

2 Material and research methods

The composition of the molding material considered in this article differs from the standard one in respect that the molding material composition for ceramic tiles, including bentonite
clay, calcium silicate, aluminum potassium sulphate and calcium oxide in the following ratios of components (wt%)

- Bentonite clay: 35-50
- Calcium silicate: 25-30
- Aluminum potassium sulphate: 15-20
- Calcium oxide: 10-15

In the manufacture of facing tiles, the molding of products was carried out in a plastic way. The clay was crushed and mixed in a mixer with the pre-crushed remaining components in the calculated mass ratios. The mixture has acquired the appearance of a homogeneous plastic mass [4, 5].

The molding of the plastic mass is carried out by pressing to obtain a tile with a size of 50 x 150 mm.

### 3 Research results and their discussion.

Shaped product - tiles - in a drying plant at an initial temperature 25 °C are blown with air with a gradual increase in temperature to 700 °C within 3-4 hours. At the same time, moisture forms on the surface of the semi-finished product, which quickly evaporates and is removed by the ventilation system. In addition, by this time, complete desulfurization of aluminum potassium sulphate is achieved [6, 7].

Alum-aluminum potassium sulphate is converted into aluminum oxide as a result of stepwise thermal dissociation (1).

\[
K_2SO_4·Al_2(SO_4)3 \rightarrow K_2SO_4 + Al_2O_3 + 3SO_2
\]  

![Fig. 1. Kinetic curves of aluminum potassium sulphate dehydration at a temperature, °C: 1 – 40; 2 – 50; 3 – 60; 4 – 70; 5 -150; 6 – 200; 7 – 350.](image)

At a temperature 680-700 °C the kinetics of the desulfurization rate reaches its maximum value K=0.06 min^{-1} (Fig. 2)
As it can be seen from Figure 2, desulfurization rate starts increasing sharply already at a temperature 600 °C, reaching its maximum value at 700 °C. Further, the rate of desulfurization of aluminum potassium sulphate is reduced to a decrease, and complete desulfurization is achieved at a temperature 900 °C. Further heating of the system leads to insignificant (up to 6%) aluminate formation [8, 9].

After the desulfurization process at a speed of 15-20 degrees per minute, the temperature rises to 1050 °C and then heat treatment continues for 30 minutes. Under these conditions, a polymorphic transition of the metastable form of aluminum oxide to aluminum oxide occurs C – δ-Al₂O₃, with a strong oxidative-catalytic effect.

Aluminum oxides are usually obtained by dehydration of aluminum hydroxide at a temperature 300 °C. At a temperature 500-600 °C metastable forms of various crystalline modifications are formed (γ-Al₂O₃, η-Al₂O₃, χ-Al₂O₃). The resulting metastable forms are fairly stable to heat treatment, without changing their crystalline modification, up to 800-900 °C. With a further increase in temperature to 1100 °C received modifications γ-Al₂O₃, η-Al₂O₃, χ-Al₂O₃ pass, respectively, in the modifications δ-Al₂O₃, θ-Al₂O₃ and υ-Al₂O₃. At a temperature 1100-1200 °C all modifications go to α-Al₂O₃ [10, 11].

Alumina C contributes to the formation of a highly developed specific surface of the molded article and is a catalyst on the tile surface. In this case, a self-cleaning effect is created on the tile surface, the mechanism of which is that water flows under the dirt on the tile surface, washing it off, and in addition, when quanta are absorbed, a reaction occurs that splits the dirt on the tile. When absorbing quanta (ultraviolet radiation), it exhibits disinfecting properties [12].

Calcium oxide determines the finished molded material’s strength.
Calcium oxide CaO is a white crystalline compound (GOST 8677-76). In terms of physical and chemical parameters, calcium oxide must comply with the standards specified in Table 1.

**Table 1. Physical and chemical parameters of calcium oxide**

| Indicator name                                      | Norm                                      |
|-----------------------------------------------------|-------------------------------------------|
| 1. Mass fraction of calcium oxide (CaO), %, not less | Clean (c) RCP 26 1121 0351 06             |
|                                                     |                                          | 96.0                                      |
| 2. Mass fraction of calcium carbonate (CaCO₃), %, no more |                                          | 2.5                                       |
3. Mass fraction of substances insoluble in hydrochloric acid, %, no more & 0.02
4. Mass fraction of total nitrogen (N), %, no more & 0.06
5. Mass fraction of sulfates (SO₄), %, no more & 0.05
6. Mass fraction of chlorides (Cl), %, no more & 0.010
7. Mass fraction of iron (Fe), %, no more & 0.02
8. Mass fraction of heavy metals (Pb), %, no more & 0.010
9. Mass fraction of the sum of potassium and sodium (K + Na), %, no more & Not standardized

The content of calcium oxide in the molding material increases with the decomposition of calcium silicate - a source of silicon oxide in the general composition. [13]

The work uses carbonate-palygorskite bentonite clay with a chemical composition (Table 2):

| Name                      | SIO₂ | TIO₂ | Al₂O₃ | Fe₂O₃ | MgO | CaO | Na₂O | K₂O | P₂O₅ | SO₃ | FeO | H₂O |
|---------------------------|------|------|-------|-------|-----|-----|------|-----|------|-----|-----|-----|
| Carbonate-palygorskite clay | 46.79 | -    | 8.63  | -     | 2.74 | 10.08 | -    | 1.60 | 1.99  | -   | 3.41 | 24.33 |

### 4 Conclusion

After ignition, the product is cooled and tested [14, 15].

After cooling, the tiles do not need to be coated with an oxide-ceramic coating, since the entire internal structure of the product is similar to the external one.

The test results are shown in Table 3.

| No. of ceramic tiles composition | Components of the original mixture | Physical indicators                          |
|---------------------------------|-------------------------------------|-----------------------------------------------|
|                                 | Calcium silicate | Aluminum potassium sulphate | Calcium oxide | Flexural strength, MPa | Breaking strength, kg | Water absorption, % | Contact angle of wetting with a drop of water with a volume 10 mlcl | Specific surface in the range, m²/g |
| 1                               | 60   | 20   | 12   | 8   | 60.3 | 130.2 | -   | 149 ⁰ | 110 |
| 2                               | 50   | 25   | 15   | 10  | 63.7 | 155.1 | -   | 142 ⁰ | 120 |
| 3                               | 42   | 27   | 18   | 13  | 60.4 | 187.2 | -   | 155 ⁰ | 140 |
| 4                               | 35   | 30   | 20   | 15  | 62.4 | 149.6 | 0.1 | 130 ⁰ | 113 |
| 5                               | 30   | 32   | 22   | 16  | 61.3 | 151.3 | -   | 145 ⁰ | 113 |
References

1. Yu.I. Goncharov, V.S. Lesovik, M.Yu. Goncharova, V.V. Stroko, Mineralogy and petrography of raw materials for the production of building materials and technical ceramics, 2001.
2. V.S. Lesovik, Laboratory workshop on building materials, 2004.
3. A.S. Boldyrev, P.P. Zolotov, A.N. Lyusov et al., Building materials (Stroyizdat, Moscow, 1989).
4. K.V. Chaus, Yu.D. Chistov, Yu.V. Labzina, Manufacturing technology of building materials, products and structures (Stroyizdat, Moscow, 1998).
5. G.A. Sergeeva, V.L. Adamyan, Intelligent systems in production 1 (32), 114-117 (2017).
6. G.A. Sergeeva, L.L. Volobueva, E.A. Krivosheeva, Debris flow hazard of the Karachay-Cherkess Republic, Western Caucasus, Monograph, Palmarium Akademic Publishing, 2015.
7. S.G. Sheina, L.V. Girya, Innovative methods of monitoring for deformations of man-made loaded areas, MATEC Web of Conferences. International scientific and technical conference "Modern directions and prospects for the development of processing technologies and equipment in mechanical engineering 2017", (ISSN: 2261-236X, France).
8. G.A. Sergeeva, V.L. Adamyan, Serious areas in the Pshekha river basin, Ecology and life safety. Collection of articles of the XVII International Scientific and Practical Conference 135-138 (2017).
9. L.A. Seferyan, V.E. Chubarov, K.V. Chubarova, IOP Conf. Series: Materials Science and Engineering 1083, 012049 (2021). doi:10.1088/1757-899X/1083/1/012049
10. V.L. Adamyan, G.A. Sergeeva, L.A. Seferyan, N.Y. Gorlova, IOP Conf. Series: Materials Science and Engineering 1083, 012050 (2021). doi:10.1088/1757-899X/1083/1/012050.
11. S.B. Yazyeva, L.A. Seferyan, L.A. Oparina, A.Y. Golubeva, Materials Science Forum 931, 883-888 (2018).
12. L.A. Seferyan, T.N. Kondrateva, V.E. Morozov, I.V. Leusenko, IOP Conference Series: Materials Science and Engineering 698 (5), 055004 (2019)
13. S.G. Sheina, K.V. Yudina, Materials Science Forum 931, 822-826 (2018). URL: https://www.scientific.net/MSF.931.822.
14. V.L. Adamyan, G.A. Sergeeva, N.V. Kondratenko, D.V. Totskiy, V.O. Boyko, Science perspective 10, 7-9 (2016).
15. V.L. Adamyan, S.B. Kalashnikova, Patent RU 2 730 140. The composition of the molding material for ceramic tiles. Published by 19.08.2020. Bul. No. 23.