Influence of curing age on high-temperature properties of additive manufactured geopolymer mortar

Xiaohong Yin 1,2, Xiaodong Wang 1,2,3,*, Yuan Fang 1,2,*, Zhu Ding 1,2

1Guangdong Provincial Key Laboratory of Durability for Marine Civil Engineering, Shenzhen University, Shenzhen, Guangdong, 518060, China
2College of Civil and Transportation Engineering, Shenzhen University, Shenzhen, Guangdong, 518060, China
3Centre for Smart Infrastructure and Digital Construction, Faculty of Science, Engineering and Technology, Swinburne University of Technology, 3122 Melbourne, Australia

Abstract. Some researches have been conducted on the application of geopolymer in 3D printing. However, there is no publication about the high-temperature properties of 3D printed geopolymer made from fly ash, slag, and metakaolin. This paper presents the experimental research on the mechanical properties of 3D printed geopolymer after being exposed to elevated temperatures. The effects of curing age on high-temperature properties are analyzed. The heating temperatures were 300 °C, 600 °C, and 900 °C, and the holding time was one hour. After exposure to temperatures, the flexural strength of 3D printed geopolymer exhibited different change trends with increasing curing age for different exposure temperatures. Before and after exposure to elevated temperature, the 3D printed geopolymer experienced significant anisotropic compressive strengths. The change trends of compressive strength at different exposure temperatures wit hincreasing curing ages were different from each other on different loading directions.

1 Introduction

The application of 3D printing technique in construction and building is attracting more and more attentions, and some researches and engineering projects have been conducted[1-10]. Geopolymer that is green, sustainable, and alternative to Portland cement has been formed as 3D printable cementitious materials[11-13]. Previous studies on 3D printable/printed geopolymer mainly focused on the preparation, fresh properties, interlayer adhesive strength, and hardened properties at ambient temperature.

Panda et al. [14] carried out an evaluation of the application potential of fly ash-based geopolymer for 3D printed large scale construction elements. The experimental results show that mechanical properties of 3D printed geopolymer exhibits anisotropic characters. Alghamdi et al. [15] prepared and characterized 3D-printed foamed fly ash-based geopolymer for thermal insulation. Bong et al. [11] optimised 3D printable geopolymer cured at ambient temperature by investigating the impacts of type of hydroxide solution, type of silicate solution, and the mass ratio of silicate solution to hydroxide solution on workability, extrudability, shape retention ability, and mechanical properties. The experimental results show that the combination of sodium hydroxide and sodium silicate solutions with a SiO$_2$/N$_2$O ratio of 3.22 exhibited the most effective activating action for Slag-fly ash-based geopolymer. Lim et al. [16] created a hybrid reinforcement by entraining continuous steel cable into extruded mortar, and the experimental results show that the flexural strength of 3D printed geopolymer is increased by 290%. Nematollahi et al. [17] found that only the compressive strength on perpendicular direction of additive manufactured fly ash-based geopolymer mortar can be improved by adding polypropylene fibres, and the flexural strength was improved due to the addition of fibres. Ohno and Li [18] designed fly ash-based Engineered Geopolymer Composite b integrating Design of Experiment, micro-mechanical modelling, and Material Sustainability Indices. Panda et al. [10] investigated the influences of printing time gap between layers, nozzle speed and nozzle standoff distance on the tensile bond strength of 3D printed fly ash-slag-silica fume-based geopolymer, and found that the bond strength is influenced by materials strength development rate and printing parameters. Panda et al. [19] investigated the fresh and hardened properties of 3D printed fly ash-slag-silica fume-based geopolymer, and found that silica fume significantly affected the fresh properties, and slag resulted in higher early strength.

The mechanical properties of cementitious materials after high temperature exposure are important aspects of concern for application in the building and construction. However, no publication about the high-temperature properties of 3D printed geopolymer is found. This paper investigates the flexural and compressive strengths of different loading directions after exposure to 300 °C, 600 °C, and 900 °C.
2 materials and methods

2.1 Materials

The chemical compositions of fly ash (FA), slag and metakaolin used to prepare geopolymer in this study are listed in Table 1. The chemical compositions are measured using X-ray Fluorescence Spectrometer (XRF). The activator was commercial sodium silicate solution with a modulus of 2.0 and solid content of 40.1% by weight.

| Composition | SiO$_2$ | CaO | Al$_2$O$_3$ | MgO | SO$_3$ | TiO$_2$ | Fe$_2$O$_3$ | K$_2$O | MnO | Others |
|-------------|---------|-----|-------------|-----|--------|---------|------------|-------|------|--------|
| Fly ash     | 52.09   | 5.18| 33.07       | 1.22| -      | 0.88    | 3.56       | 1.88  | -    | 2.12   |
| Slag        | 27.5    | 44.60| 13.20       | 8.72| 2.05   | 1.36    | 0.76       | 0.43  | 0.43 | 0.95   |
| Metakaolin  | 47.4    | 0.39| 41.6        | -   | 0.085  | 1.88    | 2.89       | -     | 0.28 | 5.475  |

2.2 Preparation of 3D printed geopolymer specimens

First, 3D printable geopolymer mortar was prepared by mixing fly ash, slag, metakaolin, sodium silicate solution, water, superplasticizer, and hydroxypropyl methylcellulose (HPMC). The ratio of binder composition by mass is fly ash : slag : metakaolin = 3 : 4 : 3. The sand-to-binder ratio is 1.75 by mass. The sodium silicate solution and water dosage are 0.36 and 0.112 respectively by the total mass of binder. Both the HPMC and superplasticizer dosage is 0.01 by the mass of binder.

Once prepared, the 3D printable geopolymer mortar was placed into feed bin of 3D printer. Then the 3D printer was controlled by computer, and the mortar was extruded and deposited according to the model. The layer height was set as 14 mm, and the extruded and deposited layers had a width of 52 mm. The 3D printed geopolymer had three layers. After finishing printing, the printed samples were covered with plastic film. After cured for 23 hours, 40 mm × 40 mm × 160 mm specimens were extracted from printed filaments. Then, the specimens were cured at 20 ± 2 °C, and ≥ 95% relative humidity.

2.3 High temperature exposure

A electric resistance furnace was used to conduct the high temperature exposure test. The heating temperatures were set up to 300 °C, 600 °C, and 900 °C, and the holding time was one hour. The furnace was heated at the target temperature in advance. Then, the 3D printed geopolymer specimens cured for 1d, 3d, 7d, and 28d were placed into furnace.

2.4 Flexural and compressive strength

The 3D printed geopolymer specimens before and after high temperature exposure were subjected to flexural and compressive strength. The loading rate was 50 N/s during flexural strength test. The loading rate of compressive strength test was 2.4 KN/s. The compressive strength of 3D printed geopolymer was measured on three loading directions, in terms of perpendicular to interface plane, longitudinal and lateral (Fig. 1).

3 Results and discussion

3.1 Flexural strength

Fig. 2 plots the flexural strength before and after exposure to high temperature against curing age. As shown in Fig. 2, curing ages exhibit different influences on flexural strength after exposure to different temperatures. For specimens ta 20 °C without exposure to elevated temperature, the flexural strength increased with increasing curing ages, and a very slow increase rate was observed during curing age between 3d and 7d. After exposure to 300 °C, the flexural strength first increased from 1d to 7d, and then slightly decreased at 28d. After exposure to 600 °C, the flexural strength increased with increasing curing ages, and a very slow increase rate was observed during curing age between 3d and 7d. After exposure to 300 °C, the flexural strength first increased from 1d to 7d, and then slightly decreased at 28d. After exposure to 600 °C, the flexural strength increased with increasing curing age with a decreasing growth rate. After exposure to 900 °C, the flexural strength increased first from 1d to 3d, and then decreased from 3d to 28d. It is notable that, from 3d to 7d, flexural strength had a significant increase after exposure to 300 °C and 600 °C, but decreased after exposure to 900 °C. After exposure to 300 °C, 600 °C, and 900 °C, the flexural strength decreased from 7d to 28d.
3.2 Compressive strength

Fig. 3 shows the plots of compressive strength measured on three loading directions before and after high temperature exposure against curing age. As shown in Fig. 3, the influences of curing age on compressive strength depend on exposure temperatures and compression loading directions.

For 3D printed geopolymer specimens at 20 °C before exposure to high temperature, the increase rate was different on different loading directions. On perpendicular direction, the compressive strength experienced a slight increase between 1d and 3d, and a significant increase from 3d to 7d. In contrast, on longitudinal direction, compressive strength showed a significant increase from 1d to 3d, and a slight increase between 3d and 7d. However, on lateral direction, compressive strength experienced a significant increase both from 1d to 3d and from 3d to 7d.

Fig. 3. Compressive strength of 3D printed geopolymer on different loading directions: perpendicular, longitudinal, and lateral.

For 3D printed geopolymer specimens at 300 °C, the compressive strength exhibited similar change trends on perpendicular and longitudinal directions, by showing increase between 1d and 7d, and decrease between 7d and 28d. However, on lateral loading direction, the compressive strength increased between 1d and 3d, then decreased between 3d and 7d, after that an increase was observed between 7d and 28d.

After exposure to 600 °C, the compressive strength increased continuously from 1d to 28d on perpendicular direction. However, on longitudinal direction, the compressive strength decreased first between 1d and 7d, and then increased between 7d and 28d. On lateral direction, a complex change trend in compressive strength was observed by showing increase between 1d and 3d, decrease between 3d and 7d, and increase between 7d and 28d.

For 900 °C, the compressive strength on perpendicular direction increased first between 1d and 7d, then increased slightly between 7d and 28d. However, on longitudinal direction, the compressive strength increased continuously between 1d and 28d. On lateral direction, the compressive strength experienced an increase from 1d to 3d, a drastic decrease from 3d to 7d, and a slight increase from 7d to 28d.
4 Conclusions
The flexural strength and compressive strength tested on three directions of 3D printed geopolymer before and after exposure to high temperature, the 3D printable geopolymers mortar were prepared from fly ash, slag, and metakaolin, activated by sodium silicate solution. The 3D printed geopolymers were cured for 1d, 3d, 7d, and 28d. The 3D printed geopolymers were heated at 300 °C, 600 °C, and 900 °C for one hour. The compressive strength shows significant anisotropy for specimens cured for all designed ages and heating at all questioned temperatures. The flexural strength exhibits different change trends with curing age before and after exposure to different temperatures. The change trends of compressive strength with increasing curing ages is dependent of heating temperatures.

References
1. Agusti-Juan, I.; G. Habert, Environmental implications and opportunities of digital fabrication. In Sustainable Built Environment (SBE) Regional Conference, Habert, G.; Schlueter, A., Eds. Zurich, SWITZERLAND, 2016; pp 304-308,10.3218/3774-6.49.
2. Alghamdi, H.; S. A. O. Nair; N. Neithalath. (2019)Insights into material design, extrusion rheology, and properties of 3d-printable alkali-activated fly ash-based binders. Materials & Design, 167.
3. Bajpayee, A.; M. Farahbakhsh; U. Zakira; A. Pandey; L. Abu Ennab; Z. Rybkowski; M. K. Dixit; P. A. Schwab; N. Kalantar; B. Birgisson; S. Banerjee. (2020)In situ resource utilization and reconfiguration of soils into construction materials for the additive manufacturing of buildings. Frontiers in Materials, 7.
4. Barnett, E.; C. Gosselin. (2015)Large-scale 3d printing with a cable-suspended robot. Additive Manufacturing, 7: 27-44.
5. Beyhan, F.; S. A. Selcuk, 3d printing in architecture: One step closer to a sustainable built environment. In Proceedings of 3rd international sustainable buildings symposium, Firtat, S.; Kimuthia, J.; AbuTaib, A., Eds. 2018; Vol. 6, pp 253-268.
6. Camacho, D. D.; P. Clayton; W. J. O'Brien; C. Seepersad; M. Juenger; R. Ferron; S. Salamone. (2018)Applications of additive manufacturing in the construction industry - a forward-looking review. Automat Constr, 89: 110-119.
7. Ding, Z.; X. Wang; J. Sanjayan; P. X. W. Zou; Z.-K. Ding. (2018)A feasibility study on hpme-improved sulphoaluminate cement for 3d printing. Materials, 11.
8. Yin, X.; K. Liu; S. Zheng; K. Zhuang; X. Wang; Y. Fang; Z. Ding. (2020)3d printable 'just-add-water glass and water'geopolymer-an experimental research based on extrusion-based 3d printing practices. MS&E, 780: 042044.
9. Sun, X.; Q. Wang; H. Wang; L. Chen. (2020)Influence of multi-walled nanotubes on the fresh and hardened properties of a 3d printing pva mortar ink. Constr. Build. Mater., 247: 118590.
10. Panda, B.; S. C. Paul; N. A. N. Mohamed; Y. W. D. Tay; M. J. Tan. (2018)Measurement of tensile bond strength of 3d printed geopolymer mortar. Measurement, 113: 108-116.
11. Bong, S. H.; B. Nematollahi; A. Nazari; M. Xia; J. Sanjayan. (2019)Method of optimisation for ambient temperature cured sustainable geopolymers for 3d printing construction applications. Materials, 12.
12. Li, Z.; L. Wang; G. Ma. (2020)Mechanical improvement of continuous steel microcable reinforced geopolymer composites for 3d printing subjected to different loading conditions. Compos Part B-Eng, 187.
13. Ma, G.; Z. Li; L. Wang; G. Bai. (2019)Micro-cable reinforced geopolymer composite for extrusion-based 3d printing. Mater. Lett., 235: 144-147.
14. Panda, B.; S. C. Paul; L. J. Hui; Y. W. D. Tay; M. J. Tan. (2017)Additive manufacturing of geopolymer for sustainable built environment. Journal of Cleaner Production, 167: 281-288.
15. Alghamdi, H.; N. Neithalath. (2019)Synthesis and characterization of 3d-printable geopolymeric foams for thermally efficient building envelope materials. Cem. Concr. Compos., 104.
16. Lim, J. H.; B. Panda; P. Quang-Cuong. (2018)Improving flexural characteristics of 3d printed geopolymer composites with in-process steel cable reinforcement. Constr. Build. Mater., 178: 32-41.
17. Nematollahi, B.; P. Vijay; J. Sanjayan; A. Nazari; M. Xia; V. N. Nerella; V. Mechtcherine. (2018)Effect of polypropylene fibre addition on properties of geopolymers made by 3d printing for digital construction. Materials, 11.
18. Ohno, M.; V. C. Li. (2018)An integrated design method of engineered geopolymer composite. Cem. Concr. Compos., 88: 73-85.
19. Panda, B.; C. Unluer; M. J. Tan. (2018)Investigation of the rheology and strength of geopolymer mixtures for extrusion-based 3d printing. Cem. Concr. Compos., 94: 307-314.