Comparison of the NIST and ENEA Air Kerma Standards

R. F. Laitano
Istituto Nazionale di Metrologia delle Radiazioni Ionizzanti, Dipartimento Ambiente, Centro Ricerche Casaccia, ENEA, c.p. 2400, Roma, Italy

P. J. Lamperti
National Institute of Standards and Technology, Gaithersburg, MD 20899-0001 USA

and

M. P. Toni
Istituto Nazionali di Metrologia delle Radiazioni Ionizzanti, Dipartimento Ambiente, Centro Ricerche Casaccia, ENEA, c.p. 2400, Roma, Italy

1. Introduction

A comparison was made between the National Institute of Standards and Technology (NIST) and the Ente per le Nuove Tecnologie l’Energia e l’Ambiente (ENEA) air kerma standards for medium energy x rays and $^{60}$Co gamma rays. The comparison took place at ENEA in June 1994. Two different transfer chambers from NIST were used for the comparison. The measurements were made at radiation qualities similar to those used at the Bureau International des Poids et Mesures (BIPM) (generating voltages of 100 kV, 135 kV, 180 kV and 250 kV, respectively) and with $^{60}$Co gamma radiation. The transfer chamber calibration factors obtained at the NIST and at the ENEA agreed with one another to 0.03 % for $^{60}$Co gamma radiation and between 0.1 % to 0.8 % for the medium energy x-ray beam codes.

Key words: air kerma; Co-60; comparison of standards; gamma-ray standards; transfer chambers; x-ray standards.

Accepted: April 23, 1998

Available online: http://www.nist.gov/jres
2. Irradiation Facilities

2.1 Radiation Beam Characteristics at ENEA

2.1.1 X-Ray Beams

A 420 kV x-ray machine is used for x-ray production at ENEA. The metal-ceramic x-ray tube has a beryllium window about 2.2 mm thick and a projected focal spot size of 4.5 mm². The high voltage can be varied between 50 kV and 400 kV. A potential divider is incorporated in the generator to monitor the actual voltage on the tube. With the addition of an electronic mains stabilizer, the average tube high-voltage deviations were within ±2% of the preset voltage.

The x-ray beam is monitored by a transmission chamber that has electrodes of polyethylene terephthalate (PTP) foils coated with aluminium and graphite so that its response as a function of energy varies by less than ±2% in the x-ray energy range of interest. The filters for the x-ray beam codes were mounted in a rotating wheel which was controlled remotely and turned pneumatically. The aluminum and copper filter materials used for the beam codes of this comparison contained less than ±0.1% impurities, and their thicknesses are known with an uncertainty of 0.01 mm. Materials for the filters used to determine half-value layers (HVLs) had the same characteristics.

The comparison measurements were made at a distance of 100 cm and the collimator aperture was chosen to give a field size of about 10 cm diameter. The uniformity of the x-ray beam intensity, measured by means of an ionization chamber, was within 0.2% out to a radius of 2.5 cm. This degree of uniformity is adequate for the comparison measurements described below. The ENEA x-ray beam codes and the other associated parameters relevant to the present measurements are given in Table 1. The mean energy values in Table 1 were experimentally determined at ENEA by means of spectra measurements [1].

2.1.2. Gamma-Ray Beams

The gamma-ray beam is produced by a therapy-Type gamma unit having an activity of about $4 \times 10^{13}$ Bq on the reference date (June 1994). The collimator of this unit was designed to minimize electron contamination. The percentage of photons scattered in the beam due to the collimator was estimated to be not greater than 3%. The largest contribution of degraded photons originates within the source and is estimated to be about 16% of the primary photons [2].

The chambers were positioned at a distance of 111 cm from the source, in a beam with an area of about 10 cm². The beam uniformity was measured using an ionization chamber whose volume was about 0.2 cm³. The uniformity of the $^{60}$Co beam was within 0.2% of the center out to a radius of 2.5 cm. Table 2 summarizes some relevant data on the $^{60}$Co irradiation system used at ENEA for this comparison.

2.2 Radiation Beam Characteristics at NIST

2.2.1 X-Ray Beams

The x-ray source at NIST is a 320 kV x-ray machine with a metal-ceramic x-ray tube. The x-ray generator is a high frequency (500 Hz), highly stabilized voltage source with an x-ray output variation of no more than

### Table 1. Medium energy x-ray beam codes at NIST and at ENEA

| Beam code | P6 | P7 | P8 | P9 |
|-----------|----|----|----|----|
| Mean energy (keV) | 44 | 68 | 93 | 139 |
| Peak voltage (kV) | 100 | 135 | 180 | 250 |

| ENEA | Inherent filtration (Be, mm) | 2.2 | 2.2 | 2.2 | 2.2 |
| Added filtration (Al, mm) | 3.49 | 4.08 | 4.06 | 4.02 |
| Added filtration (Cu, mm) | 0.17 | 0.43 | 1.48 |
| Half value layer (mm) | Al, 4.00 | Cu, 0.50 | Cu, 1.00 | Cu, 2.50 |
| Air kerma rate ($10^{-3} \text{ Gy s}^{-1}$) | 5.2 | 4.9 | 5.6 | 5.4 |
| Focus-reference plane distance | 100 cm |
| Beam diameter in reference plane | 10 cm |

| NIST | Inherent filtration (mm Be) | 3 | 3 | 3 | 3 |
| Added filtration (mm Al) | 3.024 | 1.495 | 1.518 | 1.522 |
| Added filtration (mm Cu) | 0.2413 | 0.4936 | 1.5944 |
| Half value layer (mm) | Cu, 0.145 | Cu, 0.483 | Cu, 0.967 | Cu, 2.493 |
| Air kerma rate ($10^{-3} \text{ Gy s}^{-1}$) | 0.9; 1.8 | 1.7 | 1.8 | 2.2 |
| Focus-reference plane | 100 cm |
| Beam diameter in reference plane | 7.5 cm |
Table 2. Measurement conditions at ENEA and at NIST, for 60Co gamma radiation

| Source activity (Bq) | ENEA     | NIST       |
|----------------------|----------|------------|
| 4.2 × 10^{13}        | 2.4 × 10^{14} |
| Source diameter (mm) | 20       | 20         |
| Source height (mm)   | 20       | 26         |
| Source-reference plane distance (cm) | 111 | 146 |
| Beam size at the reference plane (cm) | 10 | 6.3 |
| Air kerma rate (Gy s^{-1}) | 2.3 × 10^{-3} | 2.0 × 10^{-3} |

* Approximate value at the time of measurements

The ENEA free-air chamber for medium energy x rays is of the Attix-type and differs in geometry and mode of operation from the more conventional parallel-plate free-air chamber. One electrode of the chamber consists of two telescoping aluminum cylinders which can be independently displaced along their common axes so that the midplane of the collecting volume can remain fixed with respect to the diaphragm plane and the chamber length can be changed. An off-center aluminum rod collects substantially all the ionization produced in the chamber. Some chamber characteristics are given in Table 3. A detailed description of the chamber and its mode of operation is reported elsewhere [3, 4].

The measurement procedure is based on a subtraction method. Two ionization current readings are taken with different cylinder displacements and the difference is used to determine the x-ray air kerma or exposure (see Sec. 4). This type of chamber does not require any correction for field nonuniformity, which, in the plane-parallel free-air chambers, can constitute an important source of uncertainty [5]. On the other hand greater care in the statistical analysis of the experimental results is required for this chamber. In fact, the charge subtraction procedure can, with low signal conditions, result in greater deviations than in the case of the parallel-plate chamber.

Table 3. Principal characteristics of the ENEA medium-energy free-air ionization chamber

| Change in chamber length (collapsed and extended) | 20.00 cm |
| Aperture diaphragm diameter (mm) | 10.008 |
| Aperture diaphragm thickness (mm) | 12.75 |
| Measuring volume (cm^3) | 15.73 |
| Internal diameter (cm) | 30 |
| Polarizing potential (kV) | + 5.0 |
| Leakage current (C s^{-1}) | < 1 × 10^{-14} |
| Defining plane of aperture to chamber center distance (cm) | 40.3 |

3. Characteristics of the Air-Kerma Standards

3.1 The ENEA Standards

3.1.1 Free-Air Ionization Chamber

3.1.2 Cavity Ionization Chamber

The ENEA air kerma standard for the 60Co gamma radiation is a cavity chamber with a wall sufficiently thick to assure charged particle equilibrium for the 60Co gamma rays. The chamber geometry is cylindrical and both its walls and the collecting electrode are made of high purity graphite, greater than 99.985 %, with a density of 1.75 g/cm^3 and a porosity of 14 %. A detailed description of the chamber and its mode of operation is reported elsewhere [6]. Some relevant data of the ENEA graphite cavity chamber are reported in Table 4.
Table 4. Relevant characteristics of the ENEA graphite cavity chamber

| Characteristic                  | Value  |
|--------------------------------|--------|
| Diameter of cavity (cm)        | 1.1    |
| Height of cavity (cm)          | 1.1    |
| Collecting electrode diameter (cm) | 0.2    |
| Collecting electrode height (cm) | 1      |
| Cavity volume (cm³)            | 1.022  |
| Wall thickness (cm)            | 0.4    |
| Polarizing potential (V)       | ≥ 300  |
| Polarity effect, \( I^+ / I^- \) | 1.003  |
| Leakage current (A)            | \(6 \times 10^{-15}\) |

3.2 The NIST Standards

3.2.1 Free-Air Ionization Chamber

The NIST standard for x rays generated from 50 kV to 300 kV peak voltages is a parallel-plate free-air chamber, described by Wyckoff and Attix [7]. The chamber has a collector length of 10 cm and a plate separation of 20 cm. The tungsten alloy defining aperture is 1 cm in diameter and 1 cm long in the direction of the beam. The air-attenuation path is 30.8 cm. Table 5 summarizes the characteristics of the NIST x-ray standard.

Table 5. Principal dimensions and characteristics of the NIST free-air chamber

| Characteristic                  | Value  |
|--------------------------------|--------|
| Collecting electrode length (cm) | 10.08  |
| Aperture diaphragm diameter (mm) | 10.00  |
| Aperture diaphragm thickness (mm) | 10.00  |
| Measuring volume (cm³)         | 7.91   |
| Plate separation (cm)          | 20.0   |
| Plate height (cm)              | 26.8   |
| Polarizing potential (kV)      | −5.0   |
| Leakage current (C s⁻¹)        | < \(5 \times 10^{-14}\) |
| Defining plane of aperture to chamber center distance (cm) | 30.8 |

3.2.2 Cavity Ionization Chambers

The cavity ionization chambers used for the NIST \(^{60}\)Co gamma-ray standard were fabricated from reactor-grade high-purity graphite, following the design of Wyckoff [8]. The spherical shape was chosen in order to allow the standards to be based on a homogeneous group of six chambers of different volumes and to present a uniform, symmetrical, chamber aspect to the source. Details of the chambers, their construction, and corrections are given by Loftus and Weaver [9]. Table 6 gives the dimensions of the graphite ionization chambers.

Table 6.

4. Exposure Measurement

4.1 Free-Air Chambers

The exposure rate measured by a parallel-plate free-air chamber, like the NIST chamber, is given by [7]

\[
\dot{X} = \frac{I}{\rho S L} II_k, \quad (1)
\]

where \(I\) is the mean value of the currents measured at positive and negative chamber polarity, respectively. In the determination of \(I\), the NIST free-air chamber uses only negative polarity with respect to the collecting electrode. The polarity difference has been found to be negligible. All ionization currents are corrected to a relative humidity of 0 %, a pressure of 101 325 Pa (1 standard atmosphere), and a temperature of 0 °C. This is referred to as “reference conditions.” In Eq. (1) the quantity \(II_k\) includes all the correction factors required for this type of measurement [7]. The determination of the correction factors for the NIST free-air chamber was made by the procedure described in Ref. [7]. The factors related to this comparison are shown in Table 7.

The ENEA medium-energy free-air chamber differs in mode of operation from the parallel-plate free-air chamber (see Sec. 3.1.1). The exposure rate is given by [3]

\[
\dot{X} = \left( \frac{I_e - I_c}{\rho S \Delta L} \right) II_k, \quad (2)
\]

where \(I_e\) and \(I_c\) are the values of the ionization currents measured under conditions of collapsed and extended chamber, respectively, in dry air at reference conditions; \(\rho\) is the density of dry air at reference conditions; \(S\) is the standard chamber diaphragm area; \(\Delta L\) is the change in the free-air chamber collecting volume length from collapsed to extended chamber conditions; and the product \(II_k\) [3, 7] includes all the correction factors used with the free-air chamber measurement. The polarity effect is negligible for this type of chamber, therefore, ionization current measurements are made only at positive chamber polarity. The correction factors for the ENEA chamber, at the beam codes used for the comparison, were determined according to Ref. [4] and are shown in Table 8. At air kerma rates lower than 0.2 mGy s⁻¹ the saturation correction, \(k_{sat}\), was determined by extrapolation of the experimental curve \((I^{-1}, V^{-1})\) to \(V^{-1} = 0\), to obtain the saturation current \(I_{sat}\). A correlation coefficient very close to unity was obtained for the linear plot \((I^{-1}, V^{-2})\) confirming the predominant presence of initial recombination [10]. At air kerma rates in the range from 0.2 mGy s⁻¹ to 2 mGy s⁻¹, as used for the present comparison, a straight line was instead obtained from a \((I^{-1}, V^{-2})\) plot. This corresponds...
Table 6. Principal dimensions and characteristics of the NIST graphite cavity chambers

| Chamber code | Volume (cm$^3$) | Net volume (cm$^3$) | Outside diameter (cm) | Graphite density (g/cm$^3$) | Radial wall thickness (cm) | Graphite density (g/cm$^3$) | Radial wall thickness (g/cm$^2$) |
|--------------|----------------|---------------------|-----------------------|-----------------------------|---------------------------|-----------------------------|-------------------------------|
| 1            | 1.140          | 1.131               | 2.065                 | 1.73                        | 0.398                     | 0.688                        | 0.688                         |
| 10           | 10.088         | 10.069              | 3.428                 | 1.72                        | 0.3755                    | 0.647                        | 0.647                         |
| 30           | 30.262         | 30.24               | 4.607                 | 1.74                        | 0.3751                    | 0.653                        | 0.653                         |
| 50-1         | 51.943         | 51.634              | 5.34                  | 1.73                        | 0.3652                    | 0.632                        | 0.632                         |
| 50-2         | 50.425         | 50.089              | 5.58                  | 1.73                        | 0.5085                    | 0.880                        | 0.880                         |
| 50-3         | 50.460         | 50.155              | 5.80                  | 1.73                        | 0.6129                    | 1.060                        | 1.060                         |

Table 7. Correction factors for the NIST free-air ionization chamber

| Beam code | Air-kerma rate (mGy/s) | $k_a$ | Air scattered electron loss | $k_e$ | Aperture saturation correction | $k_{sat}$ | Field distortion | $k_d$ |
|-----------|-------------------------|-------|-----------------------------|-------|-------------------------------|-----------|------------------|-------|
| P6        | 0.878                   | 1.0106| 0.9937                      | 1.0000| 1.0018                        | 1.0012    | 1.0015           |       |
| P6        | 1.758                   | 1.0106| 0.9937                      | 1.0000| 1.0018                        | 1.0017    | 1.0015           |       |
| P7        | 1.701                   | 1.0072| 0.9951                      | 1.0010| 1.0018                        | 1.0017    | 1.0015           |       |
| P8        | 1.783                   | 1.0050| 0.9957                      | 1.0030| 1.0018                        | 1.0017    | 1.0015           |       |
| P9        | 1.476                   | 1.0049| 0.9964                      | 1.0050| 1.0018                        | 1.0015    | 1.0015           |       |
| P9        | 2.223                   | 1.0049| 0.9964                      | 1.0050| 1.0018                        | 1.0019    | 1.0015           |       |

Table 8. Correction factors for the ENEA medium-energy free-air ionization chamber

| Correction factor | P6 | P7 | P8 | P9 |
|-------------------|----|----|----|----|
| Saturation, $k_{sat}$ | 1.0017 | 1.0020 | 1.0025 | 1.0030 |
| Scattered radiation-electron loss, $k_e$ | 0.993 | 0.995 | 0.996 | 0.999 |
| Wall penetration, $k_w$ | 1.000 | 1.000 | 1.000 | 1.000 |
| Aperture penetration, $k_t$ | 1.000 | 1.000 | 1.000 | 1.000 |
| Polarity effect, $k_6$ | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Air attenuation, $k_a$ | 1.013 | 1.009 | 1.009 | 1.007 |

*At air kerma rate used for the present comparison specified in Table 1.

4.2 Cavity Chamber

The exposure rate measured by a graphite cavity chamber can be expressed by [12]

$$\tilde{X} = \frac{I}{V_p} \left( \frac{L}{p} \right)_C \left( \frac{\mu_{en}}{p} \right)^C \Pi_k, \tag{3}$$

where $I$ is the mean value of the currents measured at positive and negative chamber polarity respectively, in dry air at reference conditions; $p$ is the density of dry air at reference conditions; $V$ is the chamber collecting volume; $\left( \frac{L}{p} \right)_C$ and $\left( \frac{\mu_{en}}{p} \right)_C$ are the mass energy absorption coefficient ratio of air to that of graphite and the restricted mass stopping power ratio of graphite to that of air, respectively, and the product $\Pi_k$ includes all the corrections needed for exposure measurement with a cavity chamber [12, 13]. The correction factors (updated in 1986) for the NIST cavity chambers were determined according to Ref. [9] and are shown in Table 9.

The correction factors for the ENEA chamber were determined according to Ref. [5] and are reported in Table 10. At the air kerma rate used for this comparison (see Table 2), the saturation correction $k_{sat}$ was determined by extrapolating the experimental curve ($I^{-1}, V^{-1}$) to $V^{-1} = 0$, to obtain the current $I_{sat}$ in full saturation condition. Since this plot was linear it was assumed that initial recombination is predominant [10].

For the ENEA chamber the correction due to the field nonuniformity in the chamber volume was re-evaluated to improve the values previously used. This correction, traditionally described by the product of the two factors...
and $k_{an}$ [12,13], was replaced by the product of the factors $k_{pn}$ and $k_{npn}$ defined by Bielajew and Rogers [14, 15]. The factor $k_{pn}$ corrects for the effects due to the axial and radial non-uniformity of the field across the chamber. Only the effects due to a purely $r^{-2}$ diverging field (point source) are accounted for by $k_{pn}$. The factor $k_{npn}$ accounts for the nonuniformity of the field due to nonpoint source effects and for the scatter from the collimators and the room. For the experimental conditions at ENEA, the factor $k_{npn}$ was calculated on the basis of the Kondo and Randolph [16] and Bielajew data [14], as a function of the chamber dimensions. To determine the factor $k_{npn}$, the field uniformity across the chamber in the beam transverse direction was measured. This measurement was made by 0.13 cm$^3$ ionization chamber. The results showed a constant distribution, within the experimental uncertainty, up to radial distances of 1 cm (the outer chamber radius) from the beam axis. The results obtained also included the effects of the radial non-uniformity due to the beam divergence. These effects are not included in the definition of $k_{npn}$ and therefore should be subtracted. On the other hand, these effects cannot be detected separately when performing a measurement of field uniformity. The correction for this latter effect was then calculated according to the chamber size and to the chamber to source distance. From this calculation, the correction was found to be negligible. Thus, taking into account the above experimental results, the factor $k_{npn}$ was set equal to unity.

A specific comment should be made regarding the wall attenuation and scatter correction factor $k_{wall}$ [12, 13]. From the Bielajew and Rogers Monte Carlo calculations [15, 17], consistent differences were obtained for these factors with respect to the values resulting from the traditionally adopted extrapolation measurements. Such differences are of the same order for the NIST and the ENEA cavity chambers. Therefore the comparison results between the two standards would not substantially change if the new calculated values of $k_{wall}$ were adopted for both the standards. However, it was decided to reconsider the possibility of changing the $k_{wall}$ values only at the time when experimental confirmation of the Bielajew and Rogers theoretical results become available. To this end, an experimental research program has been initiated at ENEA.

### Table 9. $^{60}$Co correction factors for the NIST graphite cavity chamber, as of 1986

| Chamber code | Wall absorption coefficient ($k_c$) | Stopping-power ratio ($L/p_{air}$) | Energy-absorption coefficient ratio ($\mu_{air}/\mu_{C}$) | Stem scatter correction factors ($k_{cep}$) | Product of correction factors ($k_{cep}k_{wn}$) |
|--------------|-----------------------------------|-----------------------------------|----------------------------------------------|--------------------------------------------|-----------------------------------------------|
| 1            | 1.0168                            | 0.9999                            | 0.9985                                       | 0.9982                                     | 0.9950                                        |
| 10           | 1.0216                            | 0.9994                            | 0.9985                                       | 0.9992                                     | 0.9950                                        |
| 30           | 1.0220                            | 0.9992                            | 0.9985                                       | 0.9992                                     | 0.9950                                        |
| 50-1         | 1.0227                            | 0.9991                            | 0.9985                                       | 0.9990                                     | 0.9950                                        |
| 50-2         | 1.0319                            | 0.9991                            | 0.9985                                       | 0.9990                                     | 0.9950                                        |
| 50-3         | 1.0387                            | 0.9991                            | 0.9985                                       | 0.9990                                     | 0.9950                                        |

*$^a$ The product of the correction factors for beam radial nonuniformity and beam axial nonuniformity, $k_{an}$ and $k_{an}$, respectively, is unity.

### Table 10. Correction factors and physical parameters for the ENEA graphite cavity chamber

| Correction factor | Value |
|-------------------|-------|
| Saturation loss correction factor | $k_{sat}$ |
| Radiation scattered by stem correction factor | $k_{st}$ |
| Non-point source effects | $k_{npn}$ |
| Point source nonuniformity | $k_{pn}$ |
| Wall thickness correction factor | $k_{w}$ |
| Electron production origin correction factor | $k_{cep}$ |
| Wall effect correction factor | $k_{wn} = k_{w}k_{cep}$ |
| Air density correction factor | $k_{T}$ |
| Air humidity correction factor [20]$^b$ | $k_{h}$ |
| Restricted mass stopping power ratio of graphite to air [25] | $(L/p_{air})_{C}$ |
| Air to carbon mass energy absorption coefficient ratio [26, 27] | $(\mu_{air}/\mu_{C})_{air}$ |

*$^a$ At air kerma rate used for the present comparison specified in Table 2.

*$^b$ The values of correction factors $k_{w}$ and $k_{h}$ (temperature, pressure and humidity) were determined according to ambient conditions during measurements.
5. Air Kerma Determination

The air kerma values were calculated from the exposure according to the relationship [19]

\[ K_{au} = X \frac{W}{e} \frac{1}{(1 - g)} \]  

where \( W \) is the mean energy required to produce an ion pair in air; \( e \) is the elementary charge; and \( g \) is the mean fraction of the secondary electron energy that is lost to bremsstrahlung. The values used for these physical parameters are \( W/e = 33.97 \cdot 10^{-1} \) [20], \( g = 3.2 \times 10^{-3} \) for \( ^{60}\text{Co} \) gamma radiation, and \( g \) is in the range from \( 1 \times 10^{-4} \) to \( 3 \times 10^{-4} \) for x-ray beam codes used in this comparison [21].

6. The ENEA Charge Measuring System

The same type of charge-measuring system was used at ENEA, for the free-air chambers, the cavity chamber, the transfer chambers and the monitor chambers, respectively. This system was expressly designed for accurate measurements of the ionization currents produced by irradiation in ionization chambers of various volumes. Typically, these currents are in the range from \( 10^{-14} \text{ C} \) to \( 10^{-8} \text{ C} \) and can be determined with a relative standard (i.e., one standard deviation estimate) uncertainty from 0.1 % to 0.2 %. The charge measuring system is based on a high-gain negative-feedback MOSFET amplifier with a capacitive feedback element as shown in Fig. 1. The amplifier of the electrometer has an input impedance \( R > 2 \times 10^{14} \) \( \Omega \) and a gain \( A = 10^3 \). For the measurement conditions described above, the potential across the capacitance chamber, \( V_i \), is forced to be near zero and constant because \( V_i = 10^{-5} \text{ V}_u \), where \( \text{V}_u \) is the amplifier output. Therefore, the electrical field inside the chamber and the efficiency for ion collection will be constant. According to the circuit in Fig. 1, the current through the amplifier is negligible. The charge produced in the ionization chamber is transferred to the measuring system, as the values of the amplifier input resistance and gain are high (\( R > 2 \times 10^{14} \) \( \Omega \) and \( A = 10^3 \)). Under these conditions, the voltage across the feedback capacitor \( C_f \) is practically the same as the circuit output voltage, \( \text{V}_u \). Then the current through the feedback capacitor is the same as the current \( I \) to be measured, where

\[ I = \frac{C_f \Delta \text{V}_u}{\Delta t} \]  

and where \( \Delta \text{V}_u \) is the change in the feedback capacitor voltage after the time interval \( \Delta t \) and \( C_f \) is the capacitance of the feedback capacitor.

Two more features characterize the circuit shown schematically in Fig. 1. Since the change of \( \text{V}_u \) with time during chamber irradiation is linear, the slope \( \Delta \text{V}_u/\Delta t \) is constant. The input terminal, being at virtual ground, is essentially isolated from the input circuit and the magnitude of the voltage on \( C_f \) does not affect the ionization current supplied from the chamber. If this were not so, the charge build-up on \( C_f \) would be exponential. The linearity of the capacitor charge during measurements is periodically checked by linear regression. Since the stray capacitances are reduced by the gain of the electrometer, it is possible to use a long signal cable. For a signal cable length of 15 m and a capacitance typically \( 0.1 \text{ nF} \cdot \text{m}^{-1} \), the total capacitance is 1.5 nF. In the described circuit, the signal cable capacitance is decreased to about 0.015 pF, as the amplifier gain is \( 10^3 \).

The total stray capacitance due to cables, amplifier and ionization chamber was measured at ENEA and found to be less than 0.01 pF. This value is within the calibration uncertainty of the standard capacitors used. For the smaller value of the feedback capacitance, about 100 pF, the percent loss of charge trapped on the stray capacitance is about 0.01 %.

The standard capacitors used at ENEA as feedback element are high quality polystyrene capacitors with very high insulation resistance (\( R > 10^{14} \) \( \Omega \)), low fractional temperature coefficient (– 0.01 %/°C) and capacitance value that is very stable over a long time period. The capacitors are calibrated twice a year with a relative standard uncertainty of 0.05 % and the maximum fractional deviation observed over a period of 5 years is less than 0.1 %. Each capacitor is mounted in an aluminium box for electromagnetic shielding and physical protection. A number of polystyrene capacitors, of nominal capacity from 100 pF to 100 nF, are available for current measurements over the range of interest. The appropriate capacitor is selected according to the chamber volume and the air kerma rate. The standard capacitors are

![Fig. 1. Schematic diagram of the current integrator used for charge measurement at ENEA.](image)
mounted in a sealed box to keep them dry. The value of the capacitor is always corrected for temperature variations during measurements and calibration.

Typical leakage currents for the ionization standard chambers used at ENEA, are less than $5 \times 10^{-15}$ A and are subtracted from the measured currents in order to obtain the true signal. A personal computer (PC) with specially designed software was used to perform the series of measurements with the related experimental apparatus (see Figs. 2a and 2b). At the end of each series of measurements the standard capacitor is automatically discharged and after a preset time a new series of measurements is started. Computer data acquisition includes ambient temperature, pressure, and humidity data supplied by the respective probes interfaced with the computer which automatically processes the signals and calculates the appropriate corrections. The final results are presented in a printed format along with the statistical parameters. For x-ray measurements the charge measuring systems for both the standard chamber and monitor chamber are remotely controlled simultaneously.

7. Comparison Procedure

In the present comparison two NIST transfer chambers (NIST-T1 and NIST-T2, respectively) were used. Both the NIST transfer standards were spherical chambers constructed of air equivalent plastic. The nominal volume of the two chambers was the same, 3.6 cm$^3$, with an outside diameter of 1.9 cm and a wall thickness of 0.25 mm. Equilibrium caps were used for measurements with the $^{60}$Co gamma beam. A collecting voltage of $–300$ V was used for x rays, while a collecting potential of $–500$ V was used for the $^{60}$Co gamma-ray measurements.

Both the NIST transfer chambers were calibrated against the NIST and the ENEA standards. The
calibration factors determined at ENEA were compared with the calibration factors determined at NIST before and after the measurements at ENEA. The air kerma measurements using the ENEA standards were repeated before and after the NIST transfer chambers calibration. For each chamber, either the primary standard or the transfer chamber, a series of six groups of five charge measurements was made. The x-ray calibration factors determined at NIST were based on an average of 18 calibrations. The $^{60}$Co calibration factors determined at NIST were based on an average of 22 calibrations for each of the NIST transfer standards. The $^{60}$Co calibrations at NIST were made in part before and in part after the measurements at ENEA. A summary of the NIST measurements is given in Table 11.

### 7.1 Correction Factors $k_{\text{sat}}$ for the Transfer Chambers

The recombination correction factors $k_{\text{sat}}$ were determined at NIST for each transfer standard for the range of air kerma rates used during the measurements at NIST and at ENEA. For the NIST-T2 chamber, the recombination correction at – 300 V is estimated to be 1.0029.

The recombination for the NIST-T1 chamber at – 300 V is represented by the equation

$$k_{\text{sat}} = 1.0025 + (0.000689 \text{ mGy}^{-1} \text{ s}) \hat{K}_{\text{air}},$$

where $\hat{K}_{\text{air}}$ is the air kerma rate. At the collecting potential of – 500 V used for the $^{60}$Co measurements at NIST and at ENEA, the recombination was found to follow the equations below for the transfer chamber NIST-T1 and NIST-T2, respectively:

$$k_{\text{sat}} = 1.00132 + (0.000178 \text{ mGy}^{-1} \text{ s}) \hat{K}_{\text{air}},$$

$$k_{\text{sat}} = 1.00073 + (0.000177 \text{ mGy}^{-1} \text{ s}) \hat{K}_{\text{air}},$$

where $\hat{K}_{\text{air}}$ is the air kerma rate. The correction factors $k_{\text{sat}}$ for NIST transfer chambers were also determined at ENEA at the air kerma rates shown in Table 2 for $^{60}$Co gamma rays. The saturation current $I_{\text{sat}}$ was determined by extrapolating the experimental curve ($I^{-1}, V^{-1}$) to $V^{-1} = 0$. Since this plot was linear, it was assumed that initial recombination was predominant [10]. The $k_{\text{sat}}$ correction factors determined at ENEA were 1.0022 and 1.0009 for NIST-T1 and NIST-T2 chambers, respectively, as compared to 1.0017 and 1.0011, which would be predicted from Eqs. (7) and (8).

### 8. Measurement Uncertainties

The experimental uncertainties were evaluated according to the Comité International des Poids et Mesures (CIPM) recommendations [22, 23]. The combined uncertainty was obtained by summing in quadrature the uncertainties of Type A, evaluated by statistical methods, and those of Type B, evaluated by other methods. The uncertainties of Type A were evaluated as experimental standard deviations of the mean. The uncertainties of Type B were evaluated by nonstatistical methods to approximate a standard deviation.

| Transfer chamber | NIST-T1 | NIST-T2 |
|------------------|---------|---------|
| Beam no. | Cal. factor $^{a}$ | Rel. Uncert. $^{b}$ | Cal. factor $^{c}$ | Uncertainty |
| HVL, Cu, mm | 10$^{6}$ Gy $\cdot$ cm$^{-1}$ | $u_{c}$ | $U$ | $u_{c}$ | $U$ |
| P6 | 0.1455 | 18 | 7.8202 | 0.04 % | 0.09 % | 8.4071 | 0.03 % | 0.07 % |
| P7 | 0.4835 | 18 | 7.9308 | 0.04 % | 0.08 % | 8.4923 | 0.03 % | 0.07 % |
| P8 | 0.9672 | 18 | 8.0308 | 0.03 % | 0.06 % | 8.6074 | 0.03 % | 0.06 % |
| P9 | 2.4932 | 18 | 8.1216 | 0.04 % | 0.08 % | 8.7371 | 0.03 % | 0.07 % |
| $^{60}$Co | 14.9 | 22 | 8.2123$^{c}$ | 0.05 % | 0.10 % | 8.9386$^{c}$ | 0.04 % | 0.09 % |

$^{a}$ Combined before and after ENEA comparison, corrected for recombination.

$^{b}$ $u_{c}$ is the combined standard uncertainty (i.e., one standard deviation estimate) and $U = k_{u}$ is the expanded uncertainty with a coverage factor of $k = 2$ (i.e., a 95 % level of confidence estimate).

$^{c}$ Equilibrium shells added.
8.1 Uncertainties for Measurements at ENEA

For the ionization current measurements at ENEA, the standard uncertainty \( u_i \) of Type A was evaluated as the standard deviation of the mean for the series of six groups, each group consisting of five measurements. Then one has

\[
u_i = \frac{1}{\sqrt{6}} \sqrt{\frac{1}{(6 - 1)} \sum_{j=1}^{6} \left( \bar{x}_j - \bar{x} \right)^2},
\]

where \( \bar{x}_j \) is the mean of the five measurements \( (x_{ij}) \) of the \( j \)th group, and \( \bar{x} \) is the mean of the mean values of the six groups.

In order to check the existence of a possible trend within each series, two independent estimates of the variance of the mean of a group were performed. Two variances, \( S^2_s \) and \( S^2_m \), denoted as short-term and medium-term standard deviations, were determined. The Fisher-test was used to exclude significant differences between \( S_s \) and \( S_m \) and to infer the statistical independence among the measurements.

The short-term relative standard deviation of the mean of a group \( (S_s) \) is given by the mean of the relative standard deviations \( \left( \frac{u_x}{x_j} \right) \) of individual readings \( (x_j) \) within each group divided by the square root of the number of readings in a group:

\[
S_s = \frac{1}{\sqrt{5}} \sum_{j=1}^{5} \left( \frac{u_x}{x_j} \right) = \sqrt{\frac{1}{5 \times 6} \sum_{j=1}^{6} \left( \frac{u_x}{x_j} \right)^2}.
\]

The medium-term relative standard deviation of the mean of a group \( (S_m) \), is given by the relative standard deviation \( \left( \frac{u_x}{\bar{x}_j} \right) \) of the mean \( (\bar{x}_j) \) of each group. The mean values of the various groups are treated as if they were individual values:

\[
S_m = \frac{u_x}{\bar{x}} = \sqrt{\frac{1}{(6 - 1)} \sum_{j=1}^{6} \left( \bar{x}_j - \bar{x} \right)^2}.
\]

Tables 12 and 13 summarize the uncertainties evaluated for the measurements with the ENEA medium-energy free-air chamber and cavity chamber respectively. The relative combined standard uncertainty of the air kerma rates determined for medium-energy x rays using the free-air ionization chamber was 0.39 %. The relative combined standard uncertainty of the air kerma rate determined for the gamma-ray beam using the graphite ionization chamber was 0.44 %. The uncertainty of the NIST transfer chambers calibration factor determined at ENEA was evaluated in the same way (see Table 14), resulting in a relative combined standard uncertainty of less than 0.5 %, both for x- and gamma radiation.

8.2 Uncertainties for Measurements at NIST

The experimental uncertainties at NIST were evaluated according to Ref. [24]. For all the measurements made with the NIST transfer chambers (NIST-T1 and NIST-T2) with both the x-ray beam and \(^{60}\text{Co} \) gamma rays, the within-group average relative standard deviation was 0.01 %, with a range from 0.00 % to 0.03 %. The between-group relative standard deviations ranged from 0.03 % to 0.08 %, with an average of 0.05 %.

Tables 15 and 16 summarize the uncertainties associated with the NIST medium-energy free-air chamber and with the NIST graphite cavity chamber standards, respectively. The relative combined standard uncertainty of the air kerma rate for the x-ray beam codes, using the NIST free-air chamber, was 0.38 %. The relative combined standard uncertainty of the gamma-ray beam air kerma rate using the NIST graphite chamber standards was 0.41 %.

9. Results and Conclusions

The average x-ray calibration factors determined at NIST were plotted as a function of HVLs in Cu in order to account for slight differences in HVLs between NIST and ENEA. At the 100 kV beam code used at ENEA, an estimate was made for an equivalent HVL in Cu by using the ratio of Al HVLs (4.00 mm/3.896 mm). The NIST calibration factors predicted at the ENEA HVLs using these least-square fits are reported in Table 17. Table 17 also shows the percent deviations between these predicted calibration factors for the NIST transfer chambers and those determined at ENEA. The results obtained with each of the two NIST transfer chambers agree within the statistical uncertainty of the measurements. The maximum relative deviation was within the range from 0.03 % to 0.93 %, depending on the radiation quality. The percent deviations between the ENEA and NIST results do not appreciably change whether they refer to measurements with the NIST-T1 or the NIST-T2 chamber. Therefore, the mean value of these deviations was taken as the significant figure for the ENEA-NIST comparison. This is shown in Table 17 where the deviations referring to each transfer chamber are reported together with the mean deviation.
### Table 12. Relative standard uncertainties relevant to the air kerma and the exposure determination by the ENEA medium-energy free-air chamber

| Source of component of relative standard uncertainty | Air-kerma rate Type A (%) | Type B (%) | Exposure rate Type A (%) | Type B (%) |
|-----------------------------------------------------|---------------------------|------------|--------------------------|------------|
|                                                     |                           |            |                          |            |
| $k_{sat}$                                           | 0.01                      | 0.1        | 0.01                     | 0.1        |
| $k_e$                                               | 0.15                      | 0.15       |                          |            |
| $k_w$                                               | 0.06                      | 0.06       |                          |            |
| $k_t$                                               | 0.1                       | 0.1        |                          |            |
| $k_0$                                               | 0.05                      | 0.05       |                          |            |
| Leakage                                             | 0.01                      | 0.01       |                          |            |
| $V$                                                  | 0.12                      | 0.12       |                          |            |
| $\rho$                                              | 0.02                      | 0.02       |                          |            |
| $f$                                                  | 0.05<sup>b</sup>          | 0.1<sup>c</sup> | 0.05<sup>b</sup> | 0.1<sup>c</sup> |
| $({W/e})^{[21]}$                                     | 0.18                      | Not applied|                          |            |
| $g^{[21]}$                                           | 0.02                      | Not applied|                          |            |

Quadratic sum (%) 0.06 0.39 0.06 0.34

Relative combined standard uncertainty, $u_c$(%) 0.39 0.35

<sup>a</sup> The uncertainty of some correction factors that, once determined, are not currently evaluated is considered only of Type B even if a statistical component was included at the time of their experimental determination.

<sup>b</sup> Standard deviation of the mean of four series of 30 measurements, two with positive and two with negative chamber polarizing voltages, respectively.

<sup>c</sup> This value includes relative standard uncertainties for voltage (0.06 %), capacitance (0.05 %), time (0.01 %), stray capacitance (0.01 %) and was evaluated by also taking into account the deviations among absolute charge measurements by different measuring systems.

### Table 13. Relative standard uncertainties associated with the air kerma and exposure rate determinations by the ENEA graphite cavity chamber

| Source of component of relative standard uncertainty | Air-kerma rate Type A (%) | Type B (%) | Exposure rate Type A (%) | Type B (%) |
|-----------------------------------------------------|---------------------------|------------|--------------------------|------------|
|                                                     |                           |            |                          |            |
| $k_{sat}$                                           | 0.01                      | 0.1        | 0.01                     | 0.1        |
| $k_e$                                               | 0.05                      | 0.05       |                          |            |
| $k_{ep}$                                            | 0.2                       | 0.2        |                          |            |
| $k_{ep}$                                            | 0.03                      | 0.03       |                          |            |
| $k_a$                                               | 0.1                       | 0.1        |                          |            |
| $k_a$                                               | 0.1                       | 0.1        |                          |            |
| $k_t$                                               | 0.01                      | 0.03       | 0.01                     | 0.03       |
| $k_0$                                               | 0.02                      | 0.02       | 0.01                     | 0.02       |
| Leakage                                             | 0.05                      | 0.1<sup>c</sup> |                          |            |
| $V$                                                  | 0.14                      | 0.14       |                          |            |
| $\rho$                                              | 0.02                      | 0.02       |                          |            |
| $f$                                                  | 0.03<sup>b</sup>          | 0.1<sup>c</sup> | 0.03<sup>b</sup> | 0.1<sup>c</sup> |
| $({W/e})^{[21]}$                                     | 0.18                      | Not applied|                          |            |
| $g^{[21]}$                                           | 0.02                      | Not applied|                          |            |

Quadratic sum (%) 0.035 0.44 0.035 0.40

Relative combined standard uncertainty $u_c$(%) 0.44 0.40

<sup>a</sup> The uncertainty of some correction factors that, once determined, are not currently evaluated is considered only of Type B even if a statistical component was included at the time of their experimental determination.

<sup>b</sup> Standard deviation of the mean of four series of 30 measurements, two with positive and two with negative chamber polarizing voltages, respectively.

<sup>c</sup> This value includes relative standard uncertainties for voltage (0.06 %), capacitance (0.05 %), time (0.01 %), stray capacitance (0.01 %) and was evaluated by also taking into account the deviations among absolute charge measurements by different measuring systems.
Table 14. Relative standard uncertainties relevant to the procedure for calibration of the NIST transfer chambers at ENEA

| Source of relative standard uncertainty | Medium energy x-ray | 60Co gamma radiation |
|----------------------------------------|---------------------|----------------------|
|                                        | Air-kerma Type A | Type B | Exposure Type A | Type B | Exposure Type A | Type B |
| Primary standard                       | 0.06               | 0.39    | 0.06             | 0.34    | 0.035            | 0.44   |
| Current                                | 0.1<sup>a</sup>    | 0.05<sup>a</sup> | 0.1<sup>a</sup> | 0.05<sup>a</sup> | 0.1<sup>a</sup> | 0.05<sup>a</sup> |
| Recombin. loss                         | 0.1                | 0.1     | 0.1              | 0.1     |                  |        |
| Distance                               | 0.01               | 0.01    | 0.01             | 0.01    |                  |        |
| Pressure                               | 0.02               | 0.02    | 0.02             | 0.02    |                  |        |
| Temperature                            | 0.03               | 0.03    | 0.03             | 0.03    |                  |        |
| Humidity                               | 0.05               | 0.05    | 0.05             | 0.05    |                  |        |
| Leakage                                | 0.02               | 0.02    | 0.02             | 0.02    |                  |        |
| Radial nonunif.                        | 0.01               | 0.01    | 0.01             | 0.01    |                  |        |
| Quadratic sum (%)                      | 0.28               | 0.42    | 0.28             | 0.37    | 0.28             | 0.47   |
| Relative combined standard uncert. <sub>u_c</sub> (%) | 0.50 | 0.46 | 0.55 | 0.51 |

<sup>a</sup> Standard deviation of the mean of a series of 30 measurements.

<sup>b</sup> This value includes relative standard uncertainties for voltage (0.06 %), capacitance (0.05 %), time (0.01 %), stray capacitance (0.01 %) and was evaluated by also taking into account the deviations among absolute charge measurements by different measuring systems.

Table 15. Relative standard uncertainties relevant to the air kerma and exposure rate determinations using the NIST medium-energy free-air chamber

| Source of component of relative standard uncertainty | Air-kerma rate Type A (%) | Type B (%) | Exposure rate Type A (%) | Type B (%) |
|------------------------------------------------------|----------------------------|------------|--------------------------|------------|
| Volume (S.L)                                         | 0.04                       | 0.01       | 0.04                     | 0.01       |
| Charge (Cap., V)                                     | 0.03                       | 0.1        | 0.03                     | 0.1        |
| Timing (t)                                           | 0.04                       | 0.1        | 0.04                     | 0.1        |
| Air density (ρ)                                       | 0.01                       | 0.08       | 0.01                     | 0.08       |
| Recombination loss (k<sub>μ</sub>)                    | 0.1                        |            | 0.1                      |            |
| Humidity (k<sub>h</sub>)                              | 0.1                        |            | 0.1                      |            |
| Leakage current                                       | 0.01                       |            | 0.01                     |            |
| Radiation background                                  | 0.01                       |            | 0.01                     |            |
| Air attenuation (k<sub>a</sub>)                       | 0.07                       |            | 0.07                     |            |
| Scattered photons (k<sub>p</sub>)                     | 0.2                        |            | 0.07                     |            |
| Electron loss (k<sub>e</sub>)                         | 0.1                        |            | 0.01                     |            |
| Electric field distortion                             | 0.2                        |            | 0.2                      |            |
| Polarity difference (k<sub>δ</sub>)                   | 0.03                       | 0.1        | 0.03                     | 0.1        |
| Aperture penetration                                  | 0.04                       |            | 0.04                     |            |
| Penetration of chamber face (W/r) [21]                | 0.01                       |            | 0.01                     |            |
| g [21]                                                | 0.18                       | Not applied| Not applied              |            |
| Quadratic sum (%)                                     | 0.07                       | 0.38       | 0.07                     | 0.33       |
| Relative combined standard uncertainty (%)            | 0.38                       | 0.34       |                           |            |

376
Table 16. Relative standard uncertainties relevant to the air kerma and exposure rate determinations using the NIST cavities chambers

| Source of component of relative standard uncertainty | Air-kerma rate | Exposure rate |
|-----------------------------------------------------|----------------|---------------|
|                                                     | Type A (%)     | Type B (%)    | Type A (%) | Type B (%) |
| Volume \((S,L)\)                                     | 0.06           | 0.05          | 0.06       | 0.05       |
| Charge \((\text{Cap., } V)\)                        | 0.03           | 0.1           | 0.03       | 0.1        |
| Timing \((t)\)                                      | 0.04           | 0.1           | 0.04       | 0.1        |
| Air density \((\rho)\)                              | 0.01           | 0.08          | 0.01       | 0.08       |
| Recombination loss \((k_{\text{wa}})\)              | 0.1            | 0.1           | 0.1        | 0.1        |
| Humidity \((k_h)\)                                  | 0.1            | 0.1           | 0.1        | 0.1        |
| Leakage current                                     | 0.01           | 0.01          | 0.01       | 0.01       |
| Radiation background                                | 0.01           | 0.01          | 0.01       | 0.01       |
| Stopping-power ratio                                 | 0.25           | 0.25          | 0.25       | 0.25       |
| Energy-absorption coefficient ratio                 | 0.05           | 0.05          | 0.05       | 0.05       |
| Stem scatter                                        | 0.1            | 0.1           | 0.1        | 0.1        |
| Mean origin of electrons                             | 0.05           | 0.05          | 0.05       | 0.05       |
| Effective measurement point                         | 0.05           | 0.05          | 0.05       | 0.05       |
| Axial nonuniformity                                 | 0.02           | 0.02          | 0.02       | 0.02       |
| Radial nonuniformity                                | 0.01           | 0.01          | 0.01       | 0.01       |
| \((W/e)\) [21]                                      | 0.18           | Not applied   | 0.18       | Not applied |
| \(g\) [21]                                          | 0.02           | Not applied   | 0.02       | Not applied |
| Quadratic sum (%)                                    | 0.08           | 0.40          | 0.08       | 0.36       |
| Relative combined standard uncertainty (%)           | 0.41           | 0.37          |            |            |

Table 17. Results of the comparison measurements using the NIST transfer chambers NIST-T1 and NIST-T2. \(F_t\) are the transfer chambers calibration factors at reference conditions: \(T = 295.15\, \text{K}, P = 1013.25\, \text{Pa},\) and \(H = 50\, \%\). The results are reported as percent deviations, \(\Delta (\text{ENEAT-NIST})\), between the calibration factors, for each of the two NIST transfer chambers predicted from measurements made at NIST and those determined at ENEA (see text for details). For each beam code the mean values of the percent deviations are reported.

| Beam code | \(F_t (10^6 \, \text{Gy C}^{-1})\) | \(\Delta(\%)^a\) | \(\Delta_m(\%)^b\) |
|-----------|------------------------------------|------------------|---------------------|
| ENEA      | NIST                              | ENEA-NIST        | ENEA-NIST           |
| P6        | 7.772                             | 7.822            | −0.63               | −0.93               | −0.78               |
| P7        | 7.910                             | 7.935            | +0.32               | −0.53               | −0.43               |
| P8        | 8.046                             | 8.036            | +0.13               | −0.01               | +0.06               |
| P9        | 8.163                             | 8.122            | +0.50               | +0.48               | +0.49               |
| \(^{60}\text{Co}\)^c | 8.215                             | 8.212            | +0.04               | +0.03               | +0.03               |

\(a\) \(\Delta = \left\{\left[F_t(\text{ENEAT}) - F_t(\text{NIST})\right]/F_t(\text{NIST})\right\} \times 100\, \%\).

\(b\) \(\Delta_m = \text{average percent difference}\).

\(c\) Equilibrium shells added.

mentioned above. The relative mean deviations in air kerma measurements at the four x-ray beam beam codes are from 0.1 % to about 0.8 %. The relative mean deviation in air kerma measurements at the \(^{60}\text{Co}\) gamma-ray is less than 0.03 %.

The deviations between the ENEA and NIST air kerma standards are of the same order of magnitude as the combined uncertainty typical of these types of standards. The results of this ENEA-NIST comparison can therefore be considered satisfactory.

10. References

[1] R. F. Laitano, R. Pani, R. Pellegrini, and M. P. Toni, Energy distributions and air kerma rates of ISO and BIPM reference filtered x-radiations, ENEA RT/PAS(89) (1989).

[2] International Commission on Radiation Units and Measurements, Specification of high activity gamma-ray sources, ICRU Report 18 (1970).

[3] F. H. Attix, Report NRL-5646, Naval Research Laboratory, Washington, DC (1961).
[4] R. F. Laitano and M. P. Toni, The primary exposure standard of ENEA for medium energy X-ray: characteristics and measurement procedures, ENEA Report RT/PROT(83) (1983).

[5] NBS Handbook 85, Physical Aspects of Irradiation (1964).

[6] R. F. Laitano and M. P. Toni, The primary exposure standard for Co-60 gamma radiation: characteristics and measurement procedures, ENEA Report RT/PROT(83) (1983).

[7] H. O. Wyckoff and F. H. Attix, Design of free-air ionization chambers, National Bureau of Standards (U.S.) Handbook 64 (1957).

[8] International Commission on Radiological Units and Measurements, National Bureau of Standards (U.S.), ICRU Handbook 78 (1959).

[9] T. P. Loftus and J. T. Weaver, Standardization of $^{60}$Co and $^{137}$Cs Gamma-Ray Beams in Terms of Exposure, J. Res. Natl. Bur. Stand. (U.S.) 78A (4), 465–476 (1974).

[10] E. Kara-Michailova and D. E. Lea, Recombination in ionization chambers, Proc. Camb. Phil. Soc. 36, 101–150 (1940).

[11] G Mie, Ionization chambers, Ann. Phys. (Leipzig) 13, 857–933 (1904).

[12] M. Boutillon and M. T. Niatel, A study of a graphite cavity chamber for absolute exposure measurements of $^{60}$Co gamma rays, Metrologia 9, 139–171 (1973).

[13] M. T. Niatel, T. P. Loftus, and W. Oetzmann, Comparison of exposure standards for $^{60}$Co gamma rays, Metrologia 11, 17–23 (1975).

[14] A. F. Bijelaiew, An analytic theory of the point-source non-uniformity correction factor for thick-walled ionization chambers in photon beams, Phys. Med. Biol. 35 (4), 517–538 (1990).

[15] A. F. Bielajew and D. W. O. Rogers, Implications of new correction factors on primary air kerma standards in Co-60 beams, Phys. Med. Biol. 37 (6), 1283–1305 (1992).

[16] S. Kondo and M. L. Randolph, Effect of finite size of ionization chambers on measurements of small photon sources, Radiat. Res. 13, 37–66 (1960).

[17] D. W. O. Rogers and A. F. Bielajew, Wall attenuation and scatter corrections for ion chambers: measurements versus calculations, Phys. Med. Biol. 35 (8), 1065–1078 (1990).

[18] A. F. Bielajew, On the technique of extrapolation to obtain wall correction factors for ion chambers irradiated by photon beams, Med. Phys. 17 (4), 583–587 (1990).

[19] International Commission on Radiation Units and Measurements, Radiation Quantities and Units, ICRU Report 33 (1980).

[20] M. T. Niatel, Rayons X-Etude experimentale de l’influence de la vapeur d’eau sur l’ionization produite dans l’air, C. R. Acad. Sc. Paris (Seriès B) 208–221 (1969).

[21] BIPM—CCEMRI (Section I), 8 (1985).

[22] BIPM, Rapport du groupe de travail sur l’expression des incertitudes au CIPM, BIPM Proc. Verb. Com. Poids et Mesures 49, Annexe A (1981).

[23] International Organization for Standardization, Guide to the expression of uncertainty in measurement, ISBN 92-67-10188-9 (1993).

[24] B. N. Taylor and C. E. Kuyatt, Guidelines for evaluating and expressing the uncertainty of NIST measurement results, NIST Technical Note 1297 (1994).

[25] M. T. Niatel, A. M. Perrouche-Roux, and M. Boutillon, Two determinations of W, Phys. Med. Biol. 30, 67–75 (1985).

[26] J. H. Hubbell, Photon mass attenuation and mass energy-absorption coefficients for H, C, O, Ar, and seven mixtures from 0.1 keV to 20 MeV, Rad. Res. 70, 58–81 (1977).

[27] J. H. Hubbell, Photon mass attenuation and energy-absorption coefficients from 1 keV to 20 MeV, Int. J. Appl. Radiat. Isot. 33, 1269–1290 (1982).

About the authors: Dr. F. Laitano, Head of the INMRI at ENEA, works primarily in the fields of x-ray, gamma-ray, and absorbed dose standards. Dr. M. P. Toni, a physicist at INMRI-ENEA, is responsible for x-ray standards and the calibration of x-ray measuring instruments. The INMRI is the Italian Institute of Ionizing Radiation Standards and belongs to ENEA, the Italian National Agency for New Technology, Energy and the Environment. P. Lamperti, a physicist in the Ionizing Radiation Division of the Physics Laboratory at NIST, is responsible for x-ray and brachytherapy standards, calibration of brachytherapy sources, and x-ray measuring instruments. The National Institute of Standards and Technology is an agency of the Technology Administration, U.S. Department of Commerce.