THE INNOVATION MODEL OF TURBINE ENGINE COMPRESSOR TO SIMULATE THE PERFORMANCE IN OIL AND GAS INDUSTRY

Damianus Mario Ricky Fernando¹, Joko Waluyo¹
¹Magister Teknik Sistem
Universitas Gadjah Mada, Yogyakarta, Indonesia
²Departemen of Mechanical Engineering
Universitas Gadjah Mada, Yogyakarta, Indonesia
*E-mail: damianus.mario.r@mail.ugm.ac.id

ABSTRACT
In 1997s, East Kalimantan had several oil and gas fields that had reservoir pressure in the High-Pressure category. However, a few years later, the pressure continued to decrease until it reached Low Pressure, so the compressor is needed to produce high-pressure. In this study, an explanation of the process of making a turbine engine performance simulation model in 2019 is discussed and predicting turbine engine performance in the following years. This is important because the compressor is a vital tool in the oil and gas industry. Furthermore, it works continuously so that performance must be considered. In general, the simulation model equation consists of several parameters that exist in the Brayton cycle in the gas turbine in steady conditions. Simultaneous equation solving in simulation models using the Newton-Raphson method. The simulation results show that the performance of the Turbine Engine Compressor in 2019 has a net power of 20.58 MW with a cycle efficiency of 23.06%. This can be developed for plans for maintenance applications to improve efficiency changes.

Keywords: simulation, Newton-Raphson, gas turbine, pressure, compressor

INTRODUCTION
The use of compressors in the oil and gas industry is now very important, especially for supporting changes in pressure from the reservoir, which slowly decreases (Kalimattulah, 2019). In the large-scale oil and gas industry using gas turbine as the prime mover of the compressor is called the Turbo Engine Compressor. The changing of pressure in the oil and gas industry system is caused by
several things such as a decrease in pressure that occurs in the reservoir which can result in decreased gas deliverability so the pressure must be maintained by installing a compressor on the installation (INDONESIE, 2007). In addition to the delivery of gas using a very long pipeline then the possibility of a pressure drop or pressure drop caused by the existence of friction resistance to changes in the cross-section angle of the pipe through which the gas caused a large pressure loss (Mahmudin, 2018). In this case study the delivery of gas through a pipeline along 65.97 km so that the installation of a Turbine Engine Compressor is needed to help deliver gas to consumers (Total Finaelf, 2001). Pressure decrease also happened in upstream, especially in a gas well. Based on production, reservoir pressure will gradually decrease. Since 2003, this area operates in Medium Pressure mode (MP) and wellhead pressure approximately 25 until 35 bar. The other platform still operates in High-Pressure mode (HP) because it has wellhead pressure approximately 100 until 150 barg. However, in 2008 wellhead pressure gradually decreases until reach Low-Pressure mode (LP). Oil and gas industry has to install a turbine engine compressor to maintain gas deliverability of this area. Turbine engine compressor has been installed in parallel mode when normal condition both of them running together but when one of them perform scheduled maintenance or got some problem so only one of turbine engine compressor will be running. If only one turbine engine compressor running, it makes the turbine engine compressor running harder than normal condition, and if an unexpected shutdown happened there is no more turbine engine compressor standby. This condition makes the loss of production, and it is very bad (INDONESIE, 2007). That condition make a turbine engine compressor is one of the main concern in the oil and gas industry, so the condition of the turbine engine compressor have to be monitored carefully.

The role of the simulation model in predicting the performance of the Turbine Engine Compressor throughout the year is very important to evaluate the performance of the turbine. By evaluating the performance of the turbine each year, it can be further developed to optimize the maintenance of the turbine. In 2017 the turbine performance was at 17.52 MW with a cycle efficiency of 22.49% then the engine replacement was carried out so that the turbine performance changed to 19.86 MW with a cycle efficiency of 30.88% (Geasang, 2017).

Based on Stoecker’s research, it gives an example of a non-regenerative gas turbine cycle operating at constant speed 7200 rpm (120r/s) and constant energy that was added at combustion chamber (Stoecker, 2018). This research develops a new simulation model to analyze the performance of the Turbine Engine Compressor that has variable speed and load depend on gas production in the oil and gas industry throughout the year. The advantage of this simulation is that we can see the output power produced by gas turbines throughout the year with various variations in load and energy added by regulating the fuel. From the solution side, using a simulation model with Newton-Raphson can solve iterations faster when compared to using the successive substitution method (Stoecker, 2018).

**LITERATURE REVIEW**

The literature review in this research is based on Stoecker's research on the design of the thermal system. His study made a simulation of the extensive thermal system such as non-regenerative gas turbine cycle. His study introduces that system simulation can also be one step in an optimization process. For example, the effect on the output of the system, if we make a small change in the system such as the size of the combustion chamber, it will give an effect to the output (Stoecker, 2018). Stoecker's objective research to determine the power output at the shaft, if the gas turbine was added 8000 KW of energy by burning fuel and has constant operating speed at 7200 rpm (120 r/s). Figure 1 shows us about the simulation of axial flow compressor operating at 120 r/s and 101 KPa inlet pressure. Stoecker simulation based on constant speed and constant fuel rate. Based on the basic principle of stocker's research, this study will simulate the real operating parameter of the turbine engine compressor with varies load throughout 2019.
Ramadhan’s research generator gas turbine in Petrokimia Gresik before and after overhaul combustion inspection. Generator gas turbine has load 19 MW, and before performed overhaul combustion inspection, its cycle efficiency is 29.3%. Gas turbine performance increase after overhaul combustion inspection and reach 30.6%. Based on Ramadhan's research, the result of overhaul combustion inspection gives a positive effect to generator gas turbine's performance. Ramadhan's method in this research uses the basic calculation of the Brayton cycle in generator gas turbine. His calculation divide by several stages. The first stage consists of calculation in inlet guide van to find fluid enthalpy. Then second stage calculation in the compressor to calculate the parameter in the compressor. The third stage consists of a calculation in the combustion chamber that combustion happened. The fourth stage consists of expansion in power turbine until exhaust. The last stage is to calculate the performance of the generator gas turbine part by part (Ramadhan, 2018). Ramadhan's method in calculating generator gas turbine only in instantaneous time. So this study will make a simulation to calculate the performance of the turbine engine compressor the whole year in 2019.

Oil and gas industry is one of the major industry in Indonesia, one of them in East Kalimantan. This processing area main product is gas, and its delivery to Bontang, which has distance 65.97 km (TOTAL, 2002). Based on Mahmuddin's research, the pressure drop will be happened due to the length of the pipe, and the pressure drop will be greater if there are pipe bends during the trip of fluida. Not only pipe bends but also rate of fluida can affect the decrease of pressure. Figure 2 shows us Mahmuddin's research that a higher degree of pipe bend can give higher decrease of pressure and higher rate of fluida can also give a higher decrease in pressure. SD 20 mean20 degree of pipe bend and its reduce pressure until 98 Pa with flow rate 0.0003 m³/s and SD 160 mean 160 degrees of pipe bend and its reduce pressure until 431 Pa with same flow rate. So we need a Turbine Engine Compressor to increase the pressure so we can deliver gas from one place to another place (Mahmudin, 2018). The distance of gas delivery is 65.97 km, so its need to increase the pressure approximately 50 bar to deliver the product. Upstream pressure of the system is 17 bar, then turbine engine compressor will increase the pressure until reach 50 bar, then the product will be delivered. That is the main reason for the oil and gas industry have to maintain the performance of the turbine engine compressor to keep the continuity of the process. This study will simulate the performance of a turbine engine compressor to know the thermal efficiency, and for further research, it can be used to optimize the turbine engine compressor and maintenance schedule.
According to operational on-site, the gas generator has reached 24,012 hours, at which the unit will undergo a major overhaul to restore its performance and maintain its reliability. Therefore, in order to maintain the integrity of the turbo compressor package, it is decided to replace GG with a spare unit. Based on Gaesang's report, when he performed engine replacement of turbine engine compressor, we can see the difference in thermal efficiency before and after the engine replacement (Gaesang, 2017). In 2017, the turbine engine compressor had engine replacement because the performance gradually decreases and cycle efficiency reaches 22.49%, and then they perform engine replacement to increase the efficiency of the turbine engine compressor. In normal condition, two turbine engine compressors will be running in parallel mode. If one of them was performed maintenance, so only one turbine engine compressor running and reduce the capacity of gas delivery. After the engine replacement was performed, the cycle efficiency increase and reach 30.88%. That is the reason for the turbine engine compressor have to monitor the reliability of turbine engine compressor. This study will help the oil and gas industry to simulate the performance of the turbine engine compressor if any changing of the parameter happened or to optimize the performance of the turbine engine compressor.

METHODS

The main objective of this research is to create a performance simulation model of the Turbine Engine Compressor which will be used to evaluate the performance of each year. In general, this research methodology covers the following matters:

1. Data collection parameters of the gas turbine reading each day.
2. Make an equation model for the axial flow compressor and gas turbine.
3. Determine the basic equations in the simulation model
4. Determine the initial value that will be used.
5. Completion of the basic equations in the simulation model by using iterations based on the Newton-Raphson method to obtain convergent results.
6. Analyze the cycle efficiency of the Turbine Engine Compressor.

Data Parameter of Turbine Engine Compressor.

The parameter data used is obtained from direct reading in the field every day, which is then processed to create a simulation model. There are several simplifications made in this analysis, which are as follows (Stoecker, 2018):

1. It is assumed that the gas entering the system is perfect gas with a constant heat capacity at \( C_p = 1,005 \text{ KJ} / (\text{Kg.K}) \)
2. Ignores the increase in the mass of the fuel in the combustion chamber so that the mass flow rate in that enters the system is constant.
3. The pressure drop that occurs in the combustion chamber of 0.2%
4. Ignore the existence of heat transfer to the environment.
Based on this simplification, an analysis is carried out based on the parameters obtained, as shown in Figure 3 below. Figure 3 is a display shown by the Human to Machine Interface Panel (HMI Panel) with RS Logic R 5.0 type to record Turbine Engine Compressor parameter data in the field (Electric, 2001).

![Display Parameter Turbine Engine Compressor](image)

**Figure 3 Display Parameter Turbine Engine Compressor**

**Source:** (Electric, 2001)

**Basic Equation.**

The basic equation is developed from the parameter data contained in the Brayton cycle of the Turbine Engine Compressor. The basic equation is taken from two main parts. In Figures 4 and 5 the data comes from the axial flow compressor, and in Figures 6 and 7 come from the gas turbine.

Figure 4 shows the pressure data coming out of the axial flow compressor (P₂) against the mass flow rate of the incoming air (ṁ) while in Figure 5 shows the energy data required by the axial flow compressor (Wₐ) for the amount of pressure coming out of the axial flow compressor (P₂). In Figure 6 is the data obtained in the turbine by comparing the mass flow rate (ṁ) with the inlet pressure on the turbine (P₁) and in Figure 7 is a graph of the power generated by the turbine (Wₜ) against the inlet pressure on the turbine (P₁). These data were analyzed from reading parameters in the field throughout 2019.

![Outlet pressure (P₂) on the mass flow rate (ṁ)](image)

**Figure 4 Outlet pressure (P₂) on the mass flow rate (ṁ)**

**Source:** simulated by authors
Figure 5: Axial flow compressor power ($W_c$) to outlet pressure ($P_2$)  
Source: simulated by authors

Figure 6: Mass flow rate ($\dot{m}$) to turbine inlet pressure ($P_3$)  
Source: simulated by authors
Based on the data obtained from the field shown in Figure 4 through Figure 7, the equation fitting method obtained four basic equations that will be used with the Newton-Raphson simulation method. The equation obtained from the curves shown in Figures 2 through 5 is as follows:

\[
P_2 = -1.9871\dot{m}^2 + 284.06\dot{m} - 8467.4 \quad (1)
\]

\[
W_C = 0.0247P_2^2 - 57.239P_2 + 55628 \quad (2)
\]

\[
\dot{m} = -2 \times 10^{-6}P_3^2 + 0.0271P_3 + 26.332 \quad (3)
\]

\[
W_T = -0.0775P_3^2 + 297.69P_3 - 201294 \quad (4)
\]

From these four equations we add one more equation to find the \( W_{\text{nett}} \) value to find out the net power generated by the Brayton cycle in the Turbine Engine Compressor.

\[
W_{\text{nett}} = W_T - W_C \quad (5)
\]

Based on these equations, several unknown variables are obtained that will be used in the simulation (Stoecker, 2018). The unknown variable that we have to determine are \( P_2, \dot{m}, P_3, W_C, W_T \) and \( W_{\text{nett}} \).

**Newton – Raphson Method.**

After the basic equations are obtained, the next step is to solve the simulation model using the Newton-Raphson method. The advantage of using this method is that it can solve equations that have convergent values with faster iterations, by choosing an initial value that is close to (Chapra & Canale, 2006)

The fifth writing in the form of a matrix equation can be written as follows:

\[
\begin{bmatrix}
P_2 + 1.9871\dot{m}^2 - 284.06\dot{m} + 8467.4 \\
W_C - 0.0247P_2^2 + 57.239P_2 - 55628 \\
\dot{m} + 2 \times 10^{-6}P_3^2 - 0.0271P_3 - 26.332 \\
W_T + 0.0775P_3^2 - 297.69P_3 + 201294 \\
W_{\text{nett}} - W_T + W_C
\end{bmatrix} = 0
\]

(6)

Based on the matrix shown in equation (6), iterations are performed using the Newton-Raphson method for multiple equations and unknowns. The value of equation (6) is iteratively searched until the maximum percentage of errors possessed reaches the desired value.
RESULTS AND DISCUSSION

This simulation model is implemented in the Turbine Engine Compressor, which works to increase the gas pressure from 14 bar,\(g\) to 50 bar,\(g\) in 2019. In Table 1 we can see several fixed parameters used in the analysis of model calculations.

| Variable                                | Value       |
|-----------------------------------------|-------------|
| Air Heat Capacity (Cp)                  | 1.005 KJ/Kg.K |
| Lower Heating Value (LHV) fuel gas      | 47324.6 KJ/Kg |
| Pressure drop in Combustion Chamber     | 0.2%        |

**Table 1.** Turbine Parameter.

The newton-Raphson method uses an initial value of outlet pressure axial flow compressor (\(P_2\)) 1200 KPa, air mass flow rate (\(m\)) 55 Kg/s, the power used compressor (\(W_C\)) 22.5 MW, turbine gas inlet pressure (\(P_1\)) 1100 KPa, the power produced by the turbine gas (\(W_T\)) is 43 MW, and the net power (\(W_{net}\)) is 20 MW. Based on the initial value, iterations are performed as shown in Table 2 and Table 3 as follows.

| Iteration | \(P_2\) (KPa) | \(m\) (Kg/s) | \(W_C\) (KW) |
|-----------|---------------|--------------|--------------|
| 0         | 1200          | 55           | 22500        |
| 1         | 1186.96       | 55.642       | 24030.254    |
| 2         | 1191.196      | 55.722       | 21994.284    |
| 3         | 1191.234      | 55.723       | 22488.708    |
| 4         | 1191.234      | 55.723       | 22493.207    |
| 5         | 1191.234      | 55.723       | 22493.207    |
| 6         | 1191.234      | 55.723       | 22493.207    |
| 7         | 1191.234      | 55.723       | 22493.207    |
| 8         | 1191.234      | 55.723       | 22493.207    |
| 9         | 1191.234      | 55.723       | 22493.207    |

**Table 2.** Axial flow compressor parameter values in the simulation.

**Source:** Processed by authors
Table 3. The value of the turbine gas parameter in the simulation.

| Iteration | $P_3$ (KPa) | $W_T$ (KW) | $W_{nett}$ (KW) |
|-----------|-------------|------------|-----------------|
| 0         | 1100        | 43000      | 20000           |
| 1         | 1184.572    | 43169.545  | 19139.291       |
| 2         | 1188.814    | 43077.435  | 21083.150       |
| 3         | 1188.852    | 43079.233  | 20590.525       |
| 4         | 1188.852    | 43079.233  | 20586.016       |
| 5         | 1188.852    | 43079.233  | 20586.016       |
| 6         | 1188.852    | 43079.233  | 20586.016       |
| 7         | 1188.852    | 43079.233  | 20586.016       |
| 8         | 1188.852    | 43079.233  | 20586.016       |
| 9         | 1188.852    | 43079.233  | 20586.016       |

Source: Processed by authors

Figure 8 shows the $W_{nett}$ values obtained from iterations by the Newton-Raphson method. From Figure 8, it can be seen that the iteration reaches convergence at around four times iteration. Based on Table 2 and Table 3, the value of $W_T$ and $W_C$ reaches convergence first, then the value of $W_{nett}$ reaches convergence. In order to obtain a $W_{nett}$ value of 20,586 MW.

In the field conditions, the Turbine Engine Compressor works with an average fuel gas rate of around 1.89 kg / s so that based on the Lower Heating Value (LMV) the $Q_h$ results are 89.443 MW which is used in the combustion chamber. So that calculated cycle efficiency in 2019 of 23.06%
CONCLUSION

This research has developed a simulation model that can be used to predict the performance of the Turbine Engine Compressor in 2019. Based on this research, the turbine engine compressor cycle efficiency is 23.06% in the whole year. The model can accommodate the dynamics of changing parameters of the turbine cycle throughout the year because the performance of the turbine engine compressor always changes day to day depending on the change of load and condition. By using the Newton-Raphson method, it can solve iterations quickly. In this study, the fourth iteration has gotten convergent values. The results of this simulation can be used for turbine maintenance schedule because turbines are vital equipment in the oil and gas industry so that performance is a major concern. This study can help to determine the right time of scheduling maintenance depends on the performance of the turbine engine compressor for further research. The limitation of this study only analyze the performance throughout the year, and for further research, it can be used for optimization model by changing the parameter of turbine such as change the size of axial flow compressor so it will show the change of cycle efficiency too.

Nomenclature

\[ C_P \] Air heat capacity, KJ/Kg.K
\[ HMI \] Human to Machine Interface
\[ LHV \] Lower Heating Value, KJ/Kg
\[ m \] Air mass flow rate, kg/s
\[ P_1 \] Axial flow compressor inlet pressure, KPa
\[ P_2 \] Axial flow compressor outlet pressure, KPa
\[ P_3 \] Turbine gas inlet pressure, KPa
\[ P_4 \] Turbine gas outlet pressure, KPa
\[ Q_m \] Heat energy added to the combustion chamber, MW
\[ T_1 \] The air temperature at the inlet axial flow compressor, K
\[ T_2 \] The air temperature at the axial flow compressor outlet, K
\[ T_3 \] The temperature of the air at the combustion chamber outlet, K
\[ T_4 \] Air temperature at the exhaust, K
\[ W_C \] The energy used in the axial flow compressor, KW
\[ W_{net} \] Nett energy generated by the Brayton cycle, KW
\[ W_T \] Energy produced by the gas turbine, KW

REFERENCES

Boyce, M. P. (2002). *Gas Turbine Engineering Handbook Second Edition*. Houston: Gulf Publishing Company.
Boyce, M. P. (2012). *Gas Turbine Engineering Handbook fourth Edition*. Oxford: Elsevier.
Chacartegui, R., Sanchez, D., Munoz, A., & Sanchez, T. (2011). Real time simulation of medium size gas turbine. *Energy Convention and Management*, 713-724.
Chapra, S. C., & Canale, R. P. (2010). *Numerical Method for Engineers sixth edition*. New York: McGraw-Hill.
Ciggaar, J. (2010). *Training and Technical Resources Development Solar Turbine Titan 130 & Thermodyne*. Solar Turbine International.
Electric, G. (2003). *Instruction, Operation and Maintenance Manual LM 2500*. Balikpapan: Nuovo Pignone.
Gaesang, D., & Aditia. (2018). *Engine Replacement Report*. Mechanic. Balikpapan: PT. Pertamina Hulu Mahakam.
Giampaolo, A. (2006). *Gas Turbine Handbook Prinnciple and Practice Third Edition*. Lilburn: The Fairmont Press.
INDONESIE, T. E. (2007). Tunu Field Development Project Phase 11 N / EPSC 11+12. Balikpapan: TOTAL E&P INDONESIE.

Kalimattullah, A. N. (2019). Performansi Kompressor dengan Flowrate Gas Minimum pada Lapangan Tunu North - NPU PT. Pertamina Hulu Mahakam. Balikpapan: Universitas Balikpapan.

Mahmuddin. (2017). Studi Eksperimental Penurunan Tekanan Aliran Melewati Belokan Pipa Horizontal dengan Variasi Rasio R/D. Teknologi, 18, 45 - 52.

Mechanic Team. (2004). Gas Turbine GE LM 2500. Balikpapan: Total E&P Indonesie.

Oyedepo, S. (2014). Thermodynamic Analysis of a Gas Turbine Power Plant Modeled with Evaporative Cooler. International Journal of Thermodynamics (IJot), 17(1), 14-20. doi:10.5541/ijot.480

Pathirathna, K. (2013). Gas Turbine Thermodynamic and Performance Analysis Methods Using Available Catalog Data. Gavle: University of Gavle.

Pignone, N. (2001). Instruction, Operation and Maintenance Manual Gas Turbine LM 2500. Florence: Nuovo Pignone.

Ramadhan, T. A. (2018). Efisiensi Turbin Gas sebelum dan sesudah overhaul combustion inspection di GTG Utility I PT. Petrokimia Gresik. Yogyakarta: Universitas Gadjah Mada.

Stoecker, W. F. (1989). Design of Thermal Systems third edition. Singapore: McGraw-Hili Book Co.

Team, M. (2009). 8000 hr preventive maintenance general electric turbine engine compressor. Balikpapan: TOTAL E&P INDONESIE.

TOTAL. (2002). Turbines. Balikpapan: Total E&P Indonesie.

Total Finaelf. (2002). Tunu Field Development Project Phase 8. Balikpapan: Total Finaelf E&P Indonesia.

Wahzudi, T., Ariestyanti, A. P., & Pramaeda, T. D. (2017). Makalah Metode Newton-Raphson. Yogyakarta: Universitas PGRI Yogyakarta.