Interfacial reactions in thermoelectric modules

Hsin-jay Wu\textsuperscript{a}, Albert T. Wu\textsuperscript{b}, Pai-chun Wei\textsuperscript{c} and Sinn-wen Chen\textsuperscript{d}

\textsuperscript{a}Department of Materials and Optoelectronic Science, National Sun Yat-sen University, Kaohsiung, Taiwan; \textsuperscript{b}Department of Chemical and Materials Engineering, National Central University, Taoyuan, Taiwan; \textsuperscript{c}Computer, Electrical, and Mathematical Sciences and Engineering Division, King Abdullah University of Science and Technology (KAUST), Thuwal, Saudi Arabia; \textsuperscript{d}Department of Chemical Engineering, National Tsing Hua University, Hsinchu, Taiwan

**ABSTRACT**

Engineering transport properties of thermoelectric (TE) materials leads to incessantly breakthroughs in the $zT$ values. Nevertheless, modular design holds a key factor to advance the TE technology. Herein, we discuss the structures of TE module and illustrate the inter-diffusions across the interface of constituent layers. For Bi\textsubscript{2}Te\textsubscript{3}-based module, soldering is the primary bonding method, giving rise to the investigations on the selections of solder, diffusion barrier layer and electrode. For mid-temperature PbTe-based TE module, hot-pressing or spark plasma sintering are alternative bonding approaches; the inter-diffusions between the diffusion barrier layer, electrode and TE substrate are addressed as well.

**ARTICLE HISTORY**

Received 8 January 2018

**KEYWORDS**

Thermoelectric (TE) material and module; interfacial reaction; Bi\textsubscript{2}Te\textsubscript{3}; PbTe

---

1. Introduction

In cope with the increasing energy demand, thermoelectric technology has attracted growing attentions, due to its capability in converting waste heat into useable electricity via the Seebeck effect [1]. The conversion efficiency of a thermoelectric (TE) material is guided by a dimensionless figure-of-merit ($zT = S^2\sigma/\kappa$), whereas the $S$ refers to the Seebeck coefficient, $\sigma$ is the electrical conductivity, $T$ is the absolute temperature and $\kappa$ is the thermal conductivity that comprises two contributors from the traveling phonons ($\kappa_L$) and the transporting electrons ($\kappa_e$), respectively. Strategies for $zT$ enhancement have been enormously reported in the past decade, including the maximization of $S$ thorough the band structure engineering [2], the reduction of $\kappa$ via the nanstructuring [3] while maintaining high $\sigma$ by increasing the carrier mobility. Accordingly, improving the electronic transport (i.e. power factor $PF = S^2\sigma$) is one of the approaches, as the combinational effects of the convergence of heavy valence/conduction band [2], quantum effect [4,5], etc.

The TE technology specializes in converting the waste heat below 800 K through Seebeck effect, so-called the thermoelectric generator (TEG). For the waste heat higher than 800 K, the thermal stability of TE material might be degraded. Peltier cooler (or referring as thermoelectric cooler, TEC) is a solid state heat pump used in various industrial applications, which provides cooling for lasers, diodes, refrigerators and automobiles or acts as temperature stabilizer for equipment and chips [6]. Figure S1(a) and S1(b) show the schematic illustrations for the TEG and TEC, respectively. In this review paper, we discuss the state of art TE materials for TEC and TEG applications, and place great emphasis on the interfacial reactions between the TE materials, solders and diffusion barrier layers.
2. Low-temperature Bi$_2$Te$_3$-based modules

2.1. Bi$_2$Te$_3$-based materials

Since 1960s, the Bi$_2$Te$_3$-based materials have been the most well-established TE cooler, which reached $zT > 1$ in $p$-type (Bi$_2$(Sb$_{1-x}$Te$_x$)) [7–11] and $zT > 0.6$ for $n$-type (Bi$_2$(Te$_x$Se$_{1-x}$)$_3$) [12–14]. The Bi$_2$Te$_3$ is a narrow-bandgap layered semiconductor with a trigonal unit cell, in which the van der Waal bonding between neighboring tellurium atoms in adjacent quintuple layers of Te($^{(1)}$)$\text{-Bi-Te}^{(2)}$-$\text{Bi-Te}^{(1)}$, which makes it cleave easily along the trigonal axis. Such layered structure results in the highly anisotropic transportation of free electrons and phonons. e.g. $\sigma$ is approximately four times greater perpendicular to the trigonal axis than in the parallel orientation, $\kappa$ is about two times greater perpendicular to the trigonal axis than that parallel to it, and $S$ is nearly isotropic [12]. Therefore, the maximum $zT$ occurs in the parallel orientation. Approaches for tuning the inter-related thermolectric parameters of Bi$_2$Te$_3$-based materials including alloying or doping, to optimize power factor and/or to reduce thermal conductivity. For example, alloying equal mole of Sb and Se into Bi$_2$Te$_3$ makes $\kappa_1$ reduce from 0.7 to 0.47 (W/mK) at 400 K [11]. By additional Ag doping, an enhanced $S$ and reduced $\kappa_1 \sim 0.29$ (W/mK) can be achieved in Bi$_2$Te$_{1.5}$Se$_{1.5}$ [11]

Nanostructuring has been considered as an effective way to reduce $\kappa_1$, as a result of enhancing phonon scattering at grain boundary, and to improve the thermoelectric performance and mechanical strength in various material systems. To reach a high bulk density and high thermoelectric performance, various methods such as spark plasma sintering (SPS) [8], ball-milling following by hot-pressing [9] or mechanical alloying (MA) [10], are conducted to sinter Bi$_2$Te$_3$ powders into bulks, and are subsequently assembled together with their electrical interconnects into thermoelectric modules.

2.2. Solders in Bi$_2$Te$_3$-based modules

Solder is commonly used as a metallurgical junction between Cu electrodes and thermoelectric materials for low-temperature TE modules. Sn [15, 16] and Sn-based alloys, such as Sn–Bi [17–19], Sn–Cu [20], Sn–Ag [21], Sn–Sb [22] and Sn–Ag–Cu [23] are promising solders for Bi$_2$Te$_3$ modules. Several studies have depicted the interfacial reaction and the resultant microstructures at the junction between solders and Te substrate. For example, the interfacial reaction between pure Sn and pure Te leads to a very unique cruciform pattern [15, 18] (Figure S2(a)), owing to the fast reaction-limit growth of SnTe IMC. In the Sn/Te couple, the Te acts as the dominant diffusion species, while the Sn also diffuses across the reaction region, to react with Te and form the duplex structure [15]. The similar cruciform pattern (Figure S2(b)) can be observed in Sn–Bi/Te [18]. As known, the SnTe forms mainly at the interface between Sn-based solder and Te-based TE substrate, and it is weak in mechanical strength and likely deteriorating the reliability of the thermoelectric module. That directs the selection of solders towards the alloys which could be self-diffusion barriers. In addition to the SnTe IMC, the interfacial reactions between Sn–Cu, Sn–Ag or Sn–Sb solders and Te substrate result in the formation of multiple reaction layers, such as the CuTe IMC in Sn–Cu/Te [20], Ag$_2$Te IMC in Sn–Ag/Te [21], or SnSb IMC in Sn–Sb/Te [22], respectively.

The above-mentioned IMCs creates extra interfaces, increases the contact resistance and possibly degrades the thermoelectric performance. A metal-based diffusion barrier is typically added, between the solder and TE substrate, to inhibit the formation of IMCs while ensuring good electrical contact [23–26]. The barrier layer also creates extra interfaces and possibly form new IMCs with either the TE substrate or the solders. Sputtering and electroless-plating are the two common methods for depositing the diffusion barrier layers. The interfacial reaction between the barrier metals, solders and TE substrate will be discussed.

2.3. Diffusion barrier in Bi$_2$Te$_3$-based modules

A layer of Ni could be an effective diffusion barrier for Bi$_2$Te$_3$-based modules [27–31]. The NiTe IMC is commonly observed. However, the bonding strength between the Ni layer (electroless-plated or sputtered) and Bi$_2$Te$_3$ substrate is less than 10 MPa, which fail to meet the requirement for practical application. Another promising candidate for diffusion barrier is Co, owing to the slow inter-diffusion between Co and Te [32, 33]. After aging, only the CoTe$_2$ grows slowly at the interface of Co/TE substrate.

Figure 1(a)–(c) summarize the inter-diffusion between $p$-type (Bi$_2$(Sb)$_x$)$_2$Te$_3$ and the SAC305 (Sn$_3$Ag$_{0.5}$Cu) solder, with (Figure 1(b) and 1(c)) or without (Figure 1(a)) the incorporation of diffusion barrier layer. As shown, the incorporation of various diffusion barriers, such as Ni–P (Figure 1(b)) and Co–P (Figure 1(c), not only alter the type of IMCs, but prohibit the inter-diffusion between the (Bi$_2$(Sb)$_x$)$_2$Te$_3$ and SAC305. The IMCs transform from the SnTe (Figure 1(a)) to (Cu,Ni)$_3$Sn$_5$ (Figure 1(b)) or CoSn$_{3+x}$ (Cu,Co)$_6$Sn$_5$ (Figure 1(c)), with thickness less than 5 $\mu$m.

In addition to the metal Ni and Co, metallic thin films, including Pd, Pt, binary Ni–7 at% V and ternary Ta–Si–N, are effective diffusion barriers for Bi$_2$Te$_3$-based modules [34]. Among them, the ternary Ta–Si–N (100 nm in
(a) (b) (c)

![Figure 1. SAC305 reflow on (Bi,Sb)₂Te₃ substrate at 250°C (a) without diffusion barrier for 30 min (b) with Ni–P (c) with Co–P diffusion barrier and aging at 150°C for 15 days.](image1)

**Figure 1.** SAC305 reflow on (Bi,Sb)₂Te₃ substrate at 250°C (a) without diffusion barrier for 30 min (b) with Ni–P (c) with Co–P diffusion barrier and aging at 150°C for 15 days.

(a) (b) (c) (d)

![Figure 2. n-type PbTe bonded on Cu [43] (a) without (b) with Co–P diffusion barrier. n-PbTe bonded on Ni (c) without (d) with Co–P diffusion barrier, at 650°C for 60 min.](image2)

**Figure 2.** n-type PbTe bonded on Cu [43] (a) without (b) with Co–P diffusion barrier. n-PbTe bonded on Ni (c) without (d) with Co–P diffusion barrier, at 650°C for 60 min.

thickness) successfully prevents the out-diffusion of constituent elements in Bi₂Te₃, and acts as effective diffusion barrier layer [34].

3. Mid-temperature PbTe-based modules

3.1. PbTe-based materials

Since 1950s, the PbTe has been utilized in TEG [35–40]. The Sb-doped PbTe shows n-type semiconducting with a peak $zT$ of 0.62 at 723 K [35], while the addition of Ag in PbTe leads to a degenerate p-type PbTe due to the formation of interstitial Ag [39]. Moreover, composites comprising nanosized Ag₂Te precipitates and Ag-doped PbTe matrix exhibit exceptionally high $zT$ ($zT > 1.3$ at T > 725 K), owing to the combined effects of carrier concentration optimization and phonon scattering [37].

3.2. Bonding in PbTe-based modules

Hot-pressing or SPS are major bonding methods to fabricate the PbTe-based TE modules. Both methods require high operation temperature and may induce severe inter-diffusion. Alternatively, a solid–liquid inter-diffusion provides a low-temperature bonding, through the incorporation of low-melting-point interlayers, such as the Sn or In [41–43]. Those interlayers (Sn or In) are consumed by the metal layers (such as Ag), resulting in the high-melting-point IMCs (such as Ag₃Sn and Ag₃In), which might enhance the bonding strength.

Various metals or alloys are selected for the electrodes, while the diffusion barrier layer or interlayer are inserted in between the TE substrate (e.g. PbTe) and the electrodes, to prevent the severe inter-diffusion. Figure 2(a)–(d) interpret the inter-diffusion of n-type PbTe/Cu and n-type PbTe/Ni couples [43], where the diffusion barrier layer (e.g. Co–P) is introduced or not. After aging (650°C for 60 min), the formation of IMCs and interfacial irregularity in Figure 2(a) and 2(c) (i.e. free of diffusion barrier) reveal the joint failure, in contrast to flat interface as introducing the Co-P diffusion barrier layer (Figure 2(b) and 2(d)). Moreover, the mismatch in coefficient of thermal expansion (CTE) between the TE substrate, diffusion barrier layer and electrode is likely to induce the joint failures. Table S1 collects the CTE of the electrodes, the diffusion barrier layer/interlayer, the IMCs formed between the electrodes and PbTe substrate and the bonding methods.

Fe is an ideal electrode for the n-type PbTe [44]. As for p-type (Na-doped) PbTe, an interlayer (SnTe) is typically introduced between the PbTe and Fe electrode, to form a completely graded solid solution. Instead, an interlayer of Ni with CTE of $13.4 \times 10^{-6}$/K should be inserted to minimize the CTE mismatch between PbTe ($19.8 \times 10^{-6}$/K) and Fe ($11.7 \times 10^{-6}$/K), in order to reduce thermal stress during the thermal cycling. Further investigations upon the interfacial reactions between PbTe and Ni is therefore of interests [45, 46]. In the beginning of aging (600°C), the $\beta₂$ phase (Ni₃±xTe₂) precipitates out from the PbTe nearing PbTe/Ni interfaces, and grows as a continuous
layer with increasing aging time. Attention needs to be drawn that the $\beta_2$ acts as a self-diffusion barrier layer. As elevating the temperature to 650°C, a ternary Ni$_3$Pb$_2$Te$_3$ forms between the PbTe and Ni layer.

Mo is another candidate for metal electrode, and the corresponding diffusion barrier is of NiFeMo layer (82Ni–15Fe–3Mo (wt%) [47]). While bonding, the liquid Pb forms inside the PbTe, and penetrates into NiFeMo film, which leads to the joint failure. As switching to Nb electrode, two reaction products, which are of Nb$_3$Te$_4$ and Pb, are observed at the interface of Nb/PbTe [48]. However, the large mismatch in CTE between Nb (7.3 × 10$^{-6}$/K) and PbTe (19.8 × 10$^{-6}$/K) limits the use of Nb in the PbTe-based modules.

For temperature lower than 400°C, Ag and Cu could be ideal electrodes, owing to the similarity in CTE (see Table S1). As bonding (400°C), both Ag and Cu atoms diffuse into PbTe, and form Ag$_2$Te and Cu$_2$Te IMC, respectively [49, 50]. An increase in bonding temperature (~550°C) leads to the formation of liquid Pb that induces voids and cracks. Nevertheless, both Ag and Cu are not suitable in bonding p-type (Pb$_{0.6}$Sn$_{0.4}$)Te, due to the fact that the Ag or Cu reacts with Sn to form Ag$_4$Sn and Cu$_3$Sn, respectively, and thus depletes the Sn in (Pb$_{0.6}$Sn$_{0.4}$)Te.

In addition to the pure metals, the eutectic Ag–Ge is a promising electrode [51]. With the incorporation of Co or Ni diffusion barrier layer, a sandwich-like couple of PbTe/(Co,Ni)/Ag–Ge depicts a prototype for TEG. The inter-diffusion of the reaction couple is thereupon of interest. After aging at 400°C, the interface of PbTe/Co remains free of IMCs, while that of Co/Ag–Ge shows two IMCs, which are of the $\beta$-Co$_5$Ge$_3$ and CoGe, respectively. The inter-diffusion upon the Ni/Ag–Ge is even more severe; multiple IMCs (e-Ni$_3$Ge$_3$ and Ag) are formed, reflecting that both Ni and Ge are fast diffusion species. Consequently, Co acts as an much more appropriate diffusion barrier layer as compared to Ni, in the bonding of PbTe and Ag–Ge.

4. Conclusions

The interfacial reactions between the electrode, the solder and the TE materials, are of great importance for a reliable module that can undergo a long-term operation with a constantly high performance at elevated temperature. In this review, the solders and diffusion barriers used for state-of-the-art Bi$_2$Te$_3$ and PbTe-based TE modules are discussed. The maximum/average $zTS$ in various TE materials are still on the rise, showing an upward tendency at presen as well as in the future. Against this backdrop, progressive advances in bonding techniques are essential to develop the next-generation TEG and TEC.

Disclosure statement

No potential conflict of interest was reported by the authors.

Funding

The authors acknowledge the financial support from the Ministry of Science and Technology, Taiwan [grant number 106-2221-E-110-025-MY3].

References

[1] Goldsmid HJ. Applications of thermoelectricity. London (UK): Methuen & Co Ltd.; 1960.
[2] Tang Y, Gibbs ZM, Agapito LA, et al. Convergence of multi-valley bands as the electronic origin of high thermoelectric performance in CoSb$_3$ skutterudites. Nat Mater. 2015;14:1223–1228.
[3] Zhang SN, Zhu TJ, Yang SH, et al. Improved thermoelectric properties of AgSb$_2$Te$_2$ based compounds with nanoscale Ag$_2$Te in situ precipitates. J Alloys Compd. 2010;499:215–220.
[4] Hicks LD, Dresselhaus MS. Effect of quantum-well structures on the thermoelectric figure of merit. Phys Rev B. 1993;47:12727–12731.
[5] Paul B, Kumar A, Banerji VP. Embedded Ag-rich nanodots in PbTe: enhancement of thermoelectric properties through energy filtering of the carriers. J Appl Phys. 2010;108:064322–064325.
[6] Zhao L, Tan G, Hao S, et al. Ultrahigh power factor and thermoelectric performance in hole-doped single-crystal SnSe. Science. 2016;351:141–144.
[7] He W, Zhang G, Zhang X, et al. Recent development and application of thermoelectric generator and cooler. Appl Energy. 2015;143:1–25.
[8] Jeon H, Ha H, Hyun D, et al. Electrical and thermoelectrical properties of undoped Bi$_2$Te$_3$-Sb$_2$Te$_3$ and Bi$_2$Te$_3$-Sb$_2$Te$_3$-Sb$_2$Se$_3$ single crystals. J Phys Chem Solids. 1991;52(4):579–585.
[9] Bulat LP, Drabkin IA, Karatayev V, et al. Structure and transport properties of bulk nanothermoelectrics based on Bi$_3$Sb$_2$...Te$_3$ fabricated by SPS method. J Electron Mater. 2013;42:2110–2113.
[10] Poudel B, Hao Q, Ma Y, et al. High-thermoelectric performance of nanostructured bismuth antimony telluride bulk alloys. Science. 2008;320:634–638.
[11] Li H, Jing H, Han Y, et al. Microstructure and transport properties of copper-doped p-type BiSbTe alloy prepared by mechanical alloying and subsequent spark plasma sintering. J Alloy Compd. 2013;576:369–374.
[12] Son JH, Oh MW, Kim BS, et al. Effect of ball milling time on the thermoelectric properties of p-type (Bi,Sb)$_2$Te$_3$. J Alloy Compd. 2013;566:168–174.
[13] Fan Z, Wang H, Wu Y, et al. Thermoelectric high-entropy alloys with low lattice thermal conductivity. RSC Adv. 2016;6:52164–52170.
[14] Yan X, Poudel B, Ma Y, et al. Experimental studies on anisotropic thermoelectric properties and structures of n-type Bi$_2$Te$_{2.7}$Se$_{0.3}$. Nano Lett. 2010;10:3373–3378.
