A Workload Adaptive Haptic Shared Control Scheme for Semi-Autonomous Driving
Ruikun Luo*, Yifan Weng*, Yifan Wang, Paramsothy Jayakumar, Mark J. Brudnak, Victor Paul, Vishnu R. Desaraju, Jeffrey L. Stein, Tulga Ersal†, and X. Jessie Yang‡

Abstract—Haptic shared control is used to manage the control authority allocation between a human and an autonomous agent in semi-autonomous driving. Existing haptic shared control schemes, however, do not take full consideration of the human agent. To fill this research gap, this study presents a haptic shared control scheme that adapts to a human operator’s workload, eyes on road and input torque in real-time. We conducted human-in-the-loop experiments with 24 participants. In the experiment, a human operator and an autonomy module for navigation shared the control of a simulated notional High Mobility Multipurpose Wheeled Vehicle (HMMWV) at a fixed speed. At the same time, the human operator performed a target detection task for surveillance. The autonomy could be either adaptive or non-adaptive to the above-mentioned human factors. Results indicate that the adaptive haptic control scheme resulted in significantly lower workload, higher trust in autonomy, better driving task performance and smaller control effort.

Index Terms—Haptic shared control, workload, autonomous vehicles, adaptive control

I. INTRODUCTION
Autonomous driving technology is currently limited in its scope and reliability, giving rise to the semi-autonomous mode of driving. In this mode, the driving task is shared between the human and the autonomy. Thus, properly allocating the control authority between these two agents becomes critical for safety and performance. Managing this allocation is a challenging problem referred to as the shared control problem.

As the literature review in Sec. [A] shows, researchers have recognized this challenge and proposed many strategies for managing control authority in shared control. However, one very important consideration has been overlooked in the strategies developed to date; namely, the human operator’s workload. The human operator’s workload may change over time as the driving conditions change, or as a result of the human getting involved in secondary tasks. These variations in workload have direct implications on the management of control authority, as the human operator may or may not be ready to seize or relinquish control depending on the current workload. However, the relationship between human workload and control authority management has not yet been explored. This work aims to fill this gap by developing a shared control scheme that adapts to the human operator’s workload in real-time.

A. Background on shared control

Based on the hierarchy of authority, prior literature on shared control can be broadly classified into two categories: supervisory and co-operative.

In supervisory shared control, one agent supervises the behavior of the other agent and determines the final control input to the vehicle. One example is a vehicle with Level 2 automation [1], where the human acts as the supervisor. Human operator monitors the status of the vehicle and decides when to engage/disengage the automated driving function. On the other hand, in some schemes, the autonomy serves as the supervisor to monitor human operator’s control commands and modify them as needed [2–4]. In supervisory shared control, the control authority transfers entirely from one agent to the other in a discrete manner. Therefore, only one of the agents has the final control of the vehicle.

In co-operative shared control, both agents can affect the final control input. One type of co-operative shared control directly blends the steering angle inputs from both the human and autonomy through a designed arbitrator [5]. This scheme has the property that the loop between the human and the autonomy is closed after the steering wheel; i.e., the human will be able to feel the impact of autonomy input only after the resultant steering command takes effect and through the response of the vehicle. The other type of co-operative shared control is haptic shared control, in which the human and autonomy can negotiate the steering angle through the torques they apply to the steering wheel [6–8]. In this scheme, the human operator can directly feel the torque from the autonomy and can choose to yield to or fight with it by exerting extra torque on the steering wheel. Researchers developed and tested a haptic shared control framework, and showed that haptic control improved the driving performance while reducing visual demand or shortening the reaction time of the secondary task [9]. Others used the haptic control framework with the bandwidth guidance version and the continuous guidance version, and showed that both helped reduce driver errors [7].
The impedance of autonomy in a haptic shared control scheme can be considered as a natural tuning parameter through which adaptability can be introduced. Indeed, even though earlier haptic shared control schemes used a fixed impedance [6], [9], later works started investigating adaptive impedance schemes. Some schemes adopt vehicle-performance-based switching rules as adaptation mechanisms, such as turning shared control on when the lateral error of the vehicle exceeds a designed threshold [7]. Others consider human-performance-based metrics to adapt impedance continuously, such as human’s input torque and attention as the guideline for designing control authority allocation [9]. However, workload, an important human factor, has not yet been considered for adaptation purposes.

Therefore, in the present work, we proposed an adaptive haptic shared control scheme, which considers the human operator’s workload, eyes on road and torque input in the control authority allocation.

B. Background on workload estimation

Workload can be measured offline or online. Offline retrospective measures are commonly used after a human operator completes a task via questionnaires such as the NASA TLX (Task Load Index) [10]. Their offline nature prohibits their utilization for real-time adaptation. Online real-time measures of workload are assessed while the human operator is performing the task and thus could be used for designing adaptive systems. Online real-time measures of workload are usually based on task performance or human operator’s physiological signals. The underlying rationale for performance-based measures is that under high workload, human operator’s task performance would be harmed. Performance-based measures, however, are not applicable if the task performance is ambiguous or is not available immediately. Physiological measures rely on changes in the human physiological signals. Various types of physiological signals have been used to estimate workload, including heart rate, electroencephalogram (EEG), eye-related measures, Galvanic Skin Response (GSR) and near infrared spectroscopy (NIRS). Please refer to [11] for a review.

Among all the physiological measures, some could be intrusive (e.g., EEG [12]) or could be easily affected by body movements (e.g., heart rate [13]). Eye-tracking emerges as a less intrusive and robust technique and research efforts have been spent on using eye-related measurements to assess operators’ workload, including pupil diameter [14], [15], gaze distribution [16], gaze trajectory [17], [18], and blink rate [19].

To assess workload online using physiological measurements, previous studies largely adopted statistical methods to show the relationships between certain physiological signals and workload. Recently, researchers started to use machine learning techniques to classify mental workload into different levels. For example, some researchers used a decision tree to classify the drivers’ workload into two levels using 30 s driving data and the pupil diameter data [20]. Others proposed a deep neural network to analyze a 6 s video of the eye and classified operators’ workload into 3 categories in real-time [18]. However, such online measures of workload have not yet been incorporated into the shared control schemes.

II. PRESENT STUDY

In the present study, we developed a dual-task shared control platform. Using the experimental platform, the human operator and the autonomy shared the control of a simulated notional High Mobility Multipurpose Wheeled Vehicle (HMMWV) at a fixed speed. At the same time, the human operator performed a target detection task for surveillance. We used the Hidden Markov Model (HMM) to estimate the human’s workload by analyzing 4 s gaze trajectory data. We then designed and tested the adaptive shared control scheme by regulating the assistance level of the autonomy based on the estimated workload, and the operator’s eyes on road and input torque.

A. Workload estimation with HMM

HMM contains a set of hidden states $S = \{s_1, s_2, \ldots, s_N\}$, where $N$ is the number of hidden states, time sequence observations $o_t$, observation model $p(o_t|s_j)$, and state transition probabilities $p(s_i|s_j)$. In the present study, the time sequence observations are the gaze points, i.e., locations of where the human is looking relative to the external world coordinate. Let $O = \{o_1, o_2, ..., o_T\}$ represent a gaze trajectory captured from the eye tracker, where $o_t$ represents the gaze point at time $t$. Therefore, the hidden states are centers of the gaze points, $\mu_1, ..., \mu_N$ and the observation model is the multivariate normal distributions.

We trained two HMMs, one for the high workload and one for the moderate workload. The parameters of the HMMs were learned by the Expectation Maximization algorithm using the open source implementations from [21], [22]. The number of hidden states was determined by the Bayesian Information Criterion (BIC) [23], [24].

Given a gaze trajectory $X$, we computed the likelihood of $p(X|H_i)$ via the forward algorithm, where $H_i$ represents different learned HMMs for the high workload and moderate workload. To estimate the workload of $X$, we found the HMM with the maximum likelihood, i.e., $\arg \max_i p(X|H_i)$.

Our proposed adaptive shared control scheme is based on the human operator’s real-time workload, eyes on road and input torque. We used the gaze point data from a 4 s time window captured by the Tobii eye tracker (30 Hz sampling rate) to estimate participants’ workload and eyes on road. Thus, $T = 120$. Let $w_t$ represent a human operator’s workload at time $t$, $w_t = c_1 \arg \max_i p(O_t|H_i) + c_2$, where $c_1, c_2$ are scaling and offset factors such that $w_t = 50$ represents moderate workload, and $w_t = 100$ represents high workload. A human operator’s eye on road is defined as the percentage of time that s/he is looking at the driving task. Let $e_i$ denote the...
human operator’s eyes on road, \( e_t \) is calculated as the average number of times that a participant’s gaze points fall on the driving screen within the time window \( T \).

Due to the large mass and high center of gravity of the simulated military vehicle (see Sec. III-B), a rapid change of control commands resulting from a rapid change of \( w_t \) and \( e_t \) could trigger a rollover. Therefore, we applied a moving average filter with a 1 s time window and downsampled \( w_t \) and \( e_t \) to 10 Hz.

### B. Adaptive shared control scheme

1) **Autonomy design:** In the present work, we designed a fixed speed scenario when the vehicle travels at 15 mph. Hence, the autonomy only needed to provide the steering angle commands for reference. We used the Nonlinear Model Predictive Control (NMPC) method to generate the steering wheel commands, which can track the given centerline for the vehicle. Refs. [25] and [26] describe the formulation of the NMPC in detail. We used the same bicycle model representation of the vehicle within the NMPC framework with the same states and control constraints as [25], [26]. We tailored the cost function to fit to our problem, because unlike the scenarios for which the original NMPC formulation was developed, we limited the vehicle traveling speed to 15 mph and there were no obstacles on the path. Specifically, the cost function was defined as

\[
J = w_1 \int_{t_0}^{t_p} (y_{\text{ref}}(x(t)) - y(t))^2 dt + w_2 \int_{t_0}^{t_p} \gamma^2 dt + w_3 \int_{t_0}^{t_p} \tanh \left( \frac{a - F_{z,rl}}{b} \right) + \tanh \left( \frac{a - F_{z,rr}}{b} \right) dt
\]

The cost function comprises three terms. The first term is designed to penalize the distance from the position of the vehicle \( y(t) \) to the given position on the centerline \( y_{\text{ref}}(x(t)) \). The second term is designed to regularize the steering rate \( \gamma \), which ensures the steering angle command changes smoothly. The third term is a soft constraint that increases the cost when one of the tire vertical loads \( F_{z,rl} \) is close to the lowest allowable threshold. This soft constraint is used to prevent the vehicle from operating at its dynamic limit unnecessarily [25], [27]. The weights \( w_1 \), \( w_2 \) and \( w_3 \) are set to achieve a trade-off between the three terms in the cost function. In this formulation, \( t_0 \) is the time when the prediction horizon starts, while \( t_p \) marks the end time of the prediction horizon, \( t_p = t_0 + T_p \), where \( T_p \) is the fixed prediction horizon and it equaled 6.5 s in this work. We used the open-source nonlinear optimal control package NLOptControl [28], which uses the Legendre-Gauss-Radau collocation method to transfer the continuous optimal control problem into a nonlinear program. We then solved the nonlinear program by using the solver package IPOPT [29].

This optimization process generates a series of steering angle commands through the whole control horizon \( T_p \), and we use only the first 3 s worth of commands. While executing the previous control command series, the system formulates and solves a new optimal control problem with a receded horizon, and the resulting new command series are applied as soon as they are available.

2) **Non-adaptive haptic shared control:** Haptic shared control combines the torques applied by the autonomy and human operator. It creates a smooth control authority transfer between the human operator and autonomy. The implementation is visualized in Fig. 2 where \( \beta = 1 \) for the baseline non-adaptive case.

The torque from the autonomy comes from a proportional-integral-derivative (PID) controller, which acts on the difference between the steering commands resulting from the NMPC framework as the reference trajectory and the current steering angle measurement. When there is no input from the human operator, the autonomy follows the reference centerline it perceives. The perceived reference centerline may be different from the actual centerline. When there is an input from the human operator that deviates the vehicle from the centerline autonomy perceives, the autonomy applies extra torque to bring the vehicle back to the perceived centerline. The human operator can hence feel the intention of the autonomy and decide whether s/he would agree with it and let autonomy have more control authority (yield), or claim more control authority (fight). The resultant torque applied on the steering wheel, which is the summation of the torques from the human operator and autonomy, determines the final steering angle applied to the vehicle.

3) **Adaptive haptic shared control:** We designed our adaptive shared control scheme based on three different features: workload, torque from the human operator, and eyes on road. The resultant torque \( \tau_c \) in the adaptive scheme is \( \tau_c = \tau_h + \beta(w_t, e_t)\tau_a \), where the term \( \beta \) is referred to as assistance level and it determines the strength of assistance torque from autonomy. \( \tau_h \) is the normalized human torque that is calculated by dividing the input torque from the human operator by the maximum torque a human operator can apply. The implementation of the adaptive scheme is shown in Fig. 2. This scheme is in contrast to the direct blending of the input torques from both the human operator and autonomy as in the non-adaptive haptic shared control scheme. Specifically, \( \beta \) is always 1 in the baseline non-adaptive haptic shared control scheme, whereas it varies in the proposed adaptive scheme.

In our heuristic design for the assistance level, \( \beta \) was separated into two parts: base assistance level \( \beta_b \) and assistance level increment \( \Delta \beta \); i.e., \( \beta = \beta_b(w_t, \bar{\tau}_h) + \Delta \beta(w_t, e_t) \). The base assistance level \( \beta_b \) considers the impact from workload.
and input torque from the human operator, while the assistance level increment $\Delta \beta$ considers the combined effect of eyes on road and workload.

The base assistance level $\bar{\beta}$ was designed according to the principles illustrated in Fig. 3 and explained next. On the one hand, when the torque from the human operator is held constant, the relationship between the assistance level and workload is shown in Fig. 3a. The designed curve for assistance level matches the study of [30], which shows the assistance from the autonomy should be high when the workload is either very high (overloaded) or very low (underloaded). When the subject has a moderate workload, the assistance from the autonomy should be lower. We set the workload value $w_t$ as 0 when the subject is underloaded, $w_t$ as 50 when the subject experiences moderate workload and $w_t$ as 100 when the subject is overloaded. We heuristically set the assistance level as 0.1 for moderate workload ($w_t = 50$) and as 1 for very high workload ($w_t = 100$). We fit a sigmoid function to create the smooth transition from $w_t = 50$ to $w_t = 100$. We then mirror the function when workload $w_t$ ranges from 0 to 50 and obtain the curve for the whole workload spectrum.

On the other hand, when the workload of the human operator is held constant, the relationship between the assistance level $\beta$ and normalized human torque $\hat{\tau}_h$ is shown in Fig. 3b. There are two critical properties of the designed curve. When the human torque is small, the assistance level is kept at a high level ($\beta = 1$) to filter out some unintended input torque from the human operator. The assistance level starts to drop after the normalized human torque passes a threshold, which increases as workload increases from moderate workload ($w_t = 50$) to high workload ($w_t = 100$). The threshold value from underloaded to moderate workload mirrored the threshold value when the workload ranges from moderate to high. The threshold is smaller when workload approaches the moderate level, since we assume human would make less mistakes at this workload level based on the results in the literature that show a moderate workload level to be optimal [30]. We heuristically set the threshold value as 0.01 when the human operator experiences a moderate workload ($w_t = 50$), while this value is 0.3 when the human operator is fully overloaded and underloaded ($w_t = 100$ and $w_t = 0$). We fit a quadratic function that is symmetric about the moderate workload case ($w_t = 50$). When the input torque from the human operator becomes greater, the assistance level starts to drop to a lower level. The system is designed to let the human operator have more control authority when there is a strong intention for intervention from the human operator. The value also changes according to the workload. When the human is overloaded, the assistance level for a large torque input remains a relatively large value. We heuristically set the assistance level for maximum torque as 1 when the human operator is overloaded ($w_t = 100$) and 0.1 when the human operator experiences moderate workload ($w_t = 50$). We then use a modified sigmoid function, connecting the threshold point with the maximum torque point.

Combining those two principles, the formulation of the base assistance level $\bar{\beta}$ is obtained as

$$\bar{\beta}(w_t, \hat{\tau}_h) = 1 - \left[ 1 - \left( \frac{9e^{0.3\hat{\tau}_h}}{e^{0.3\hat{\tau}_h} + 1} \right) + 0.1 \right]$$

(2)

The corresponding 3D plot showing the relationship between the base assistance level, the workload and the normalized human torque is shown in Fig. 4.

The assistance level increment $\Delta \beta$ was designed according to the principles illustrated in Fig. 5 and explained next. On the one hand, keeping the workload constant, when the subject focuses on the driving task, i.e., $e_t$ is very close to 1, $\Delta \beta$ is very close to 0, which indicates no additional assistance level is provided based on the the eyes on road metric. When the subject directs their attention to the secondary tasks, i.e., $e_t$ is very close to 0, $\Delta \beta$ increases to a high level, which is illustrated in Fig. 5a. An exponential function is used to connect these two points. On the other hand, keeping the eyes on road constant, when workload is high, the increment $\Delta \beta$ is large, while when the workload is moderate, the increment

![Diagram](image-url)
\( \Delta \beta \) is small, which is shown in Fig. 5b. We heuristically set the value of \( \Delta \beta \) as 0.4 when the subject experiences moderate workload (\( w_t = 50 \)), and as 0.9 when the subject is overloaded or underloaded (\( w_t = 100 \) or \( w_t = 0 \)). This value is calculated through linear interpolation when the workload is between these critical values.

Combining these considerations, the formulation of assistance level increment \( \Delta \beta \) is obtained as

\[
\Delta \beta(w_t, e_t) = 0.1(0.1|w_t - 50| + 5)^{1-e_t} - 0.1
\]  

The corresponding 3D plot showing the relationship between the assistance level increment, the workload and the eyes on road is shown in Fig. 6.

### III. EXPERIMENT 1

#### A. Introduction

In Experiment 1, we aimed to estimate a human operator’s workload in real-time by analyzing his/her gaze trajectories. We conducted a human-in-the-loop experiment with 12 participants using a dual-task shared control platform. The participant and the autonomy shared the control of a simulated notional HMMWV. At the same time, the participant performed a surveillance task. The participant wore a pair of Tobii eyeglasses 2 during the experiment and his/her gazes were captured at 30 Hz. Based on the gaze trajectories, we estimated the participant’s workload using HMM.

#### B. Method

1) **Participants:** A total of 13 university students participated in the experiment. Data from one participant were discarded due to equipment malfunction. The remaining 12 participants were on average 26.7 years old (SD = 3.0 years) and had an average of 8.3 years of driving experience (SD = 4.4 years). All participants had normal or corrected-to-normal vision.

2) **Apparatus and stimuli:** A dual-task shared control simulation platform was used in Experiment 1. Participants performed two tasks simultaneously, a driving task and a surveillance task as shown in Fig. 7.

   In the driving task, a participant and the autonomy shared the control of the HMMWV at a fixed speed of 15 mph, with the goal to complete a track with minimal deviation from the centerline. To emulate degraded localization due to sensor uncertainty, an offset was introduced such that the autonomy tracked a line which deviated from the centerline by 1 m. The non-adaptive shared control scheme was used in Experiment 1. The non-adaptive shared control scheme described in Sec. II-B2 was used in Experiment 1.

   In the surveillance task, the participant received image feeds and was asked to identify potential threats (Fig. 8). If the participant identified a threat, s/he pressed the red paddle at the steering wheel to report “danger”. Otherwise, the participant pressed the green paddle to report “clear” (Fig. 7b).

   Participants received a new set of four images at a fixed time interval, with a 1 s white screen in between, and were responsible for detecting potential threats as accurately as possible. The fixed time interval was varied to manipulate the workload level (See Appendix B for more details).

3) **Experimental design:** We manipulated the workload of the experimental tasks (the driving and the surveillance task) by varying the time interval of the surveillance task. During the experiment, the participants drove on 6 different tracks, each lasting for approximately 3 min. Every track was equally segmented into 3 portions and each portion had a different time interval for the surveillance task, 1.5, or 2.5, or 6.5 s. The order of presentation for the 3 time intervals on each track is balanced by two 3 × 3 Latin squares.

4) **Measures:** Participants wore a pair of the Tobii Pro Glasses 2 and their gaze points were recorded at 30Hz.

5) **Experimental procedure:** Participants provided a signed informed consent and filled in a demographic survey. After that, they received a training. Participants were first trained on the driving task alone, followed by the surveillance task alone. After that, they performed both the driving and the surveillance task.

   After the training session, participants were assisted to wear the eye tracker and underwent the calibration. With the normal room light and without any specific tasks, the experimenter...
measured each participant’s baseline pupil diameter twice, each about 30 s. During the experiment, participants performed the driving task and the surveillance task on 6 different tracks, each lasting approximately 3 min.

C. Results

1) Data processing: Participants drove on 6 different tracks in this experiment. As mentioned above, each track was segmented into 3 portions and each portion had a different time interval for the surveillance task. The portion with the 1.5 s time interval was considered as the high workload portion, and the portion with the 6.5 s time interval the moderate workload portion. The ground truth labels were determined in two pilot studies (see Appendix A and B for details). For each track, we randomly selected 5 sequences of data and each sequence lasted 4 s.

2) Evaluation of the workload estimation performance: Due to the small dataset of 12 participants, we used the holdout method \([51]\) for cross-validation and tested the performance of our proposed method. In each run of the holdout, we randomly selected data of 3 participants as the testing dataset and data of the remaining 9 participants as the training dataset. To find the best number of hidden states, we varied the number of hidden states from 2 to 10 for the HMM and ran 100 holdouts for each number of hidden states. The results indicate that 2 was the best number of hidden states.

We then ran another 100 holdouts to evaluate the performance of the HMM for workload estimation. Precision, recall and \(F_1\) score were used as performance metrics, where precision = \(\frac{\#\text{true positives}}{\#\text{true positives}+\#\text{false positives}}\) and recall = \(\frac{\#\text{true positives}}{\#\text{true positives}+\#\text{false negatives}}\). For our multi-classification problem, the precision is the mean precision of all classes and the recall is the mean recall of all classes. \(F_1 = 2\frac{\text{precision} \cdot \text{recall}}{\text{precision} + \text{recall}}\). Table I shows the mean and standard error of each performance metric. The results show that the HMM model achieved a 0.66 \(F_1\) score, 0.67 precision and 0.66 recall.

IV. EXPERIMENT 2

A. Introduction

In Experiment 2, we tested two different haptic shared control schemes: the adaptive haptic shared control and non-adaptive haptic shared control schemes. The adaptive haptic shared control scheme adapted to the estimated real-time workload, and the participant’s eyes on road and torque input. We used the HMM learned with the data from all the 12 participants to estimate the participant’s workload in real time.

B. Method

1) Participants: A total of 13 students participated in the experiment. Data of 1 participant were discarded due to the wrong experiment setup. The remaining 12 participants were on average 22.3 years old (SD = 3.7 years) and had an average of 5.7 years of driving experience (SD = 3.9 years). All participants had normal or corrected-to-normal vision.

2) Apparatus and stimuli: The same dual-task shared control simulation platform was used in this experiment as in Experiment 1. Both the adaptive haptic shared control and the non-adaptive haptic shared control were used in this experiment.

3) Experimental design: The experiment used a within-subjects design with two independent variables. The first independent variable was the haptic shared control scheme (adaptive haptic shared control vs. non-adaptive haptic shared control). The second independent variable was the second task urgency (1.5 s vs. 6.5 s). Each participant experienced four tracks in the experiment. On each track, one type of haptic shared control scheme was used. In addition, each track was segmented into two portions, one portion with high urgency secondary task (1.5 s) and the other with low urgency secondary task (6.5 s). The resulting four test conditions are shown in Table II. The presentation of test conditions followed a 4 x 4 Latin square design to eliminate potential order effects.

4) Measures: Five dependent variables were collected in the experiment: participants’ self-reported workload and trust in the shared control autonomy, participants’ control effort, driving task performance and surveillance task performance. After each track, participants reported their workload and trust for the first and second half of the track using two uni-dimensional scales. The NASA TLX survey \([32]\) and the Moray’s trust survey \([33]\) were presented to the participants such that they understood the meaning of workload and trust. Participants’ control effort was calculated as the average torque that a participant applied on the steering wheel. Driving task performance was evaluated by lane keeping error. The lane keeping error is calculated as the mean of the absolute deviation of the vehicle’s position from the centerline. The surveillance task performance was measured using the detection accuracy.

5) Experimental procedure: Participants provided a signed informed consent and filled in a demographic survey. After that they were assisted to wear the eye tracker with calibration. With the normal room light and without any specific tasks, the experimenter measured each participants’ baseline pupil diameter twice each about 30 s before the training.

During the training session, the participants first performed two trials of driving task only, one with the non-adaptive haptic shared control and one with the adaptive haptic shared control. Each trial took approximately 1.5 min. Then the participants performed three trials of the surveillance task only. Each trial took approximately 60 s. After that, the participants performed four trials of the combined driving and surveillance task.

During the official experiment, participants performed the
driving task and the surveillance task on 4 different tracks with different test cases as described in Table III. Each trial took approximately 3 min. After each trial, the participants were asked to fill a post survey about the workload and trust during each portion of the track.

C. Experiment 2 Results

Two-way repeated measures Analysis of Variance (ANOVAs) were conducted with the shared control scheme and the surveillance task urgency as the within-subjects variables. Results are reported as significant for \( \alpha < .05 \). Table III summarizes the mean and standard error (SE) values of the participants’ self-reported workload and trust as well as driving task performance, surveillance task performance and their exerted torque.

1) Participants’ Workload: Both control scheme and surveillance task urgency influence participants’ self-reported workload. With the adaptive shared control, participants reported lower workload \((F(1, 11) = 5.18, p = .044)\). When the surveillance task was less urgent, participants reported lower workload \((F(1, 11) = 20.26, p < .001)\).

2) Trust in Automation: Participants trusted the shared control autonomy more when the autonomy was adaptive \((F(1, 11) = 12.76, p = .004)\). The effect of surveillance task urgency on trust was not significant.

3) Driving Task Performance: Results revealed that the haptic shared control scheme and the surveillance task urgency significantly affected the driving task performance. Participants had smaller lane keeping errors when using the adaptive shared control autonomy \((F(1, 11) = 7.593, p = .019)\), and when the surveillance task was less urgent \((F(1, 11) = 96.33, p < 0.001)\) (Fig. 9a). There was also an interactive effect between the control scheme and surveillance task urgency \((F(1, 11) = 6.141, p = .031)\). Using adaptive shared control led to a large reduction in lane keeping error when the surveillance task was more urgent.

4) Surveillance Task Performance: For the surveillance task, task urgency significantly influenced the detection accuracy \((F(1, 11) = 6.73, p = .025)\). Detection accuracy was higher when the task was less urgent. The effect of the shared control scheme was non-significant (Fig. 10b).

5) Participants’ Control Effort: There was a significant effect of shared control scheme on participants’ control effort \((F(1, 11) = 217.66, p < .001)\). With adaptive shared control, participants exerted significantly less control effort. The effect of surveillance task urgency on participants’ control effort was non-significant. In addition, results revealed a significant interaction effect between control scheme and surveillance task urgency \((F(1, 11) = 11.42, p = .006)\). When the surveillance task was less urgent (6.5 s), the adaptive shared control scheme led to a larger drop in torque.

D. Experiment 2 Discussion

1) Participants’ Workload: Participants’ self-reported workload decreased when using the adaptive shared control scheme and when the surveillance task became less urgent. The results could have resulted from the following reasons. First, the 6.5 s surveillance task urgency imposed a smaller temporal demand on participants. Second, the participants’ control effort was smaller with the adaptive control scheme. Third, participants’ driving task performance was higher with the adaptive control scheme and when the surveillance task was less urgent.

2) Trust in Automation: Our result is consistent with prior research that human operators’ trust in automation is determined by the autonomy’s performance \([34], [35]\). Human operators perceived both the driving and the surveillance task performance continuously, based on which they adjusted their trust in automation. As the driving task performance increased with the adaptive control scheme, trust increased accordingly.
3) Driving Task Performance: The results showed that the adaptive shared control scheme benefited the driving task performance, especially when participants were under a high workload. Based on the design of the adaptive haptic shared control scheme, with the same input torque, when the human operator has a high workload and focuses on the surveillance task, the assistance level is increased. The increment in the assistance level is expected to aid the driving task and reduce the lane keeping error. This design principle was supported by the experimental results.

4) Surveillance Task Performance: As the surveillance task became more urgent and more demanding, the surveillance task performance decreased significantly. This result is consistent with prior research that when workload increased from moderate to high level, task performance would decrease [15].

5) Participants’ Control Effort: Our results indicate that with adaptive shared control participants exerted significantly less amount of control effort in both low and high workload conditions. The results can be explained as follows: First, as the participants’ trust toward the adaptive shared control scheme is significantly higher than the non-adaptive control scheme, participants had a higher tendency to yield to the autonomy, resulting in smaller input torque. Second, according to the design of the adaptive shared control scheme, with the same input torque, when the human operator experiences moderate workload and focuses on the driving task, the assistance level is reduced. With a reduced assistance level, regardless of whether the human yields to or fights with the autonomy, the human operator’s torque is expected to be smaller.

V. GENERAL DISCUSSION AND CONCLUSION

In this study, we proposed an adaptive haptic shared control scheme by designing a heuristic function for assistance level considering human’s workload, torque and eyes on road. The results indicate that our adaptive haptic shared control scheme leads to lower self-reported workload, higher trust in automation, lower lane keeping error and lower human control effort. To our best knowledge, this is the first study in which the human operator’s workload was estimated in real-time and used as an input to an adaptive haptic shared control scheme.

The findings should be viewed in light of the following limitations. First, a group-level workload estimation model was developed in the study, ignoring potential individual differences. In this study, we assumed that participants experienced high workload when the surveillance task was more urgent and moderate workload when surveillance task was less urgent. This assumption may not hold for different individuals. In the future work, we will develop a personalized workload estimation model to account for individual differences. Second, the assistance level adaptation function is manually designed based on heuristics. In the future work, we would investigate other methods to find the optimal assistance level adaptation function.

APPENDIX A
PILOT STUDY 1 – TRACK SELECTION

In pilot study 1, we developed and selected 6 driving tracks with two considerations. First, the driving tracks should have the same difficulty. Second, along each track, the difficulty at every point should be roughly the same. The two considerations ensure that the difficulty of the dual-task mission can be easily manipulated by varying the surveillance task urgency, because the difficulty of the driving task is fairly constant.

1) Participants: 10 participants (Age: Mean = 21.8 years, SD = 2.7 years) took part in pilot study 1. All participants had normal or corrected-to-normal vision and hearing, with an average of 4.1 years of driving experience (SD = 1.7 years).

2) Apparatus and stimuli: Pilot study 1 used the same driving simulator as in Experiment 1 with driving task only and non-adaptive haptic shared control scheme.

3) Experimental design: The pilot study used a within-subjects design with 10 different candidate tracks (Fig. [12]). The presentation of tracks followed a 10 × 10 Latin square design to eliminate potential order effects.

4) Measures: Along each track, participants reported the difficulty of driving at 11 locations using a 7-point Likert scale (1: easiest; 7: most difficult). After completing each track, participants also evaluated to what extent the track had the same difficulty anywhere along it (i.e. uniformity score), using another 7-point Likert scale (1: the same; 7: significantly different). For each track, the average of the 11 reported difficulty scores was calculated to represent the overall difficulty of the track (i.e. overall difficulty score).

5) Result: One-way repeated measures Analysis of Variance (ANOVA) was conducted with the driving track as the within-subjects variable. The results showed a non-significant difference between the ten tracks in their overall difficulty scores ($F(9, 81) = 1.161, p = 0.331$) and in their uniformity score ($F(9, 81) = 0.557, p = 0.828$). Based on the results, we selected track 2, 3, 5, 6, 8, 9 to be used in Pilot Study 2 and Experiment 1, and track 2, 3, 6, 9 to be used in Experiment 2.

APPENDIX B
PILOT STUDY 2 – DESIGN OF SURVEILLANCE TASK

We aimed to manipulate the difficulty of the dual-task mission and hence the human operators’ workload by varying the surveillance task urgency. In Pilot Study 2, we selected the paces of the surveillance task, so that the difficulty and workload of the dual-task mission can be manipulated.

1) Participants: A total of 7 students participated in Pilot Study 2. Data of one participant was discarded due to equipment malfunction. The remaining 6 participants were on average 25.3 years old ($SD = 1.6$ years) and had an average of 2.7 years of driving experience ($SD = 1.6$ years). All participants had normal or corrected-to-normal vision.
2) Apparatus and stimuli: Pilot study 2 used the same dual-task shared control simulation platform as in Experiment 1. The non-adaptive haptic shared control scheme was applied.

3) Experimental design: The pilot study used a within-subject design with six different time intervals of the surveillance task: 1.5, 2.5, 3.5, 4.5, 5.5, and 6.5 s, i.e. participants had to complete the detection task within any given time interval. The six time intervals were selected based on the results from our previous study [36]. Participants performed both the driving task and the surveillance task on 6 different tracks, each with a constant different time interval. The presentation of surveillance task conditions followed a 6 × 6 Latin square design to eliminate potential order effects.

4) Measures: Participants reported their workload of the dual-task mission using the NASA TLX survey [10] and their perceived difficulty of the dual-task mission.

5) Result: One-way repeated measures Analysis of Variance (ANOVA) was conducted with the surveillance time interval as the within-subjects variable. The results showed a significant difference of time interval on workload (F(5, 25) = 10.458, p < 0.001) and difficulty (F(5, 25) = 13.423, p < 0.001). We then performed a series of t tests between different pairs of time intervals. The results revealed significant differences in workload and difficulty between 1.5 and 2.5 s (workload: p < .001, difficulty:p = .006), between 1.5 and 3.5 s (workload: p = .005, difficulty:p = .012), between 1.5 and 4.5 s (workload: p = .004, difficulty:p = .006), between 1.5 and 5.5 s (workload: p = .001, difficulty:p < .001), and between 1.5 and 6.5 s (workload: p = .004, difficulty:p < .001). The differences between any other pairs of time intervals were non-significant.

Based on the results, we selected 1.5- and 6.5-second time intervals to be used in the Experiment 1 and Experiment 2 to induce varying levels of workload. Note in Experiment 1, we also included the 2.5-second time interval, as we were interested to explore participants’ performance with a slightly larger time interval compared to the 1.5-second time interval.

REFERENCES

[1] Taxonomy and Definitions for Terms Related to Driving Automation Systems for On-Road Motor Vehicles, Sep 2016. [Online]. Available: https://doi.org/10.4277/J3016-2016009

[2] S. M. Erlien, S. Fujita, and J. C. Gerdes, “Shared steering control using safe envelopes for obstacle avoidance and vehicle stability,” IEEE Transactions on Intelligent Transportation Systems, vol. 17, no. 2, pp. 441–451, 2016.

[3] W. Schwarting, J. Alonso-Mora, L. Pauli, S. Karaman, and D. Rus, “Parallel autonomy in automated vehicles: Safe motion generation with minimal intervention,” in 2017 IEEE International Conference on Robotics and Automation (ICRA), May 2017, pp. 1928–1935.

[4] J. Storms, K. Chen, and D. Tilbury, “A shared control method for obstacle avoidance with mobile robots and its interaction with communication delay,” The International Journal of Robotics Research, vol. 36, no. 5-7, pp. 820–839, 2017.

[5] S. J. Anderson, S. C. Peters, T. E. Pihlatti, and K. Iagnemma, “Design and development of an optimal-control-based framework for trajectory planning, threat assessment, and semi-autonomous control of passenger vehicles in hazard avoidance scenarios,” in Robotics Research, C. Pradalier, R. Siegwart, and G. Hirzinger, Eds. Berlin, Heidelberg: Springer Berlin Heidelberg, 2011, pp. 39–54.

[6] P. G. Griffiths and R. B. Gillespie, “Sharing control between humans and automation using haptic interface: Primary and secondary task performance benefits,” Human Factors, vol. 47, no. 3, pp. 574–590, 2005.

[7] S. M. Petereimejer, D. A. Abbink, and J. C. F. de Winter, “Should drivers be operating within an automation-free bandwidth? evaluating haptic support systems with different levels of authority,” Human Factors, vol. 57, no. 1, pp. 5–20, 2015.

[8] A.-T. Nguyen, C. Sentouh, and J.-C. Popieul, “Sensor reduction for driver-automation shared steering control via an adaptive authority allocation strategy,” IEEE/ASME Transactions on Mechatronics, vol. 23, no. 1, pp. 5–16, 2018.

[9] M. Mulder, D. A. Abbink, and E. R. Boer, “The effect of haptic guidance on curve negotiation behavior of young, experienced drivers,” in 2008 IEEE International Conference on Systems, Man and Cybernetics, Oct 2008, pp. 804–809.

[10] G. Hart and L. E. Staveland, “Development of nasa-tlx (task load index): Results of empirical and theoretical research,” in Advances in psychology. Elsevier, 1988, vol. 52, pp. 139–183.

[11] J. Heard, C. E. Harriott, and J. A. Adams, “A Survey of workload assessment Algorithms,” IEEE Transactions on Human-Machine Systems, vol. 48, no. 5, pp. 434–451, 2018.

[12] Y. Liu, H. Ayaz, and P. A. Shewokis, “Multisubject learning for mental workload classification using concurrent eeg, firs, and physiological measures,” Frontiers in human neuroscience, vol. 11, p. 389, 2017.

[13] W. Chen, N. Jaques, S. Taylor, A. Sano, S. Fedor, and R. W. Picard, “Wavelet-based motion artifact removal for electrodermal activity,” in 2015 37th Annual International Conference of the IEEE Engineering in Medicine and Biology Society (EMBC), IEEE, 2015, pp. 6223–6226.

[14] M. A. Recarte and L. M. Nunes, “Mental workload while driving: effects on visual search, discrimination, and decision making,” Journal of experimental psychology: Applied, vol. 9, no. 2, p. 119, 2003.

[15] S. Lu, M. Y. Zhang, T. Ersal, and X. J. Yang, “Workload management in teleoperation of unmanned ground vehicles: Effects of a delay compensation aid on human operators workload and teleoperation performance,” International Journal of Human–Computer Interaction, pp. 1–11, 2019.

[16] B. Reimer, “Impact of cognitive task complexity on drivers visual tunneling,” Transportation Research Record, vol. 2138, no. 1, pp. 13–19, 2009.

[17] Y. Wang, B. Reimer, J. Dobres, and B. Mehler, “The sensitivity of different methodologies for characterizing drivers gaze concentration under increased cognitive demand,” Transportation research part F: traffic psychology and behaviour, vol. 26, pp. 227–237, 2014.

[18] L. Fridman, B. Reimer, B. Mehler, and W. T. Freeman, “Cognitive load estimation in the wild,” in Proceedings of the 2018 CHI Conference on Human Factors in Computing Systems. ACM, 2018, p. 652.

[19] M. P. Coral, “Analyzing cognitive workload through eye-related measurements: A meta-analysis,” 2016.

[20] Y. Zhang, Y. Owechko, and J. Zhang, “Driver cognitive workload estimation: A data-driven perspective,” in Proceedings. The 7th International IEEE Conference on Intelligent Transportation Systems (IEEE Cat. No. 04TH8749). IEEE, 2004, pp. 642–647.

[21] L. Rozo, J. Silverio, S. Calinon, and D. G. Caldwell, “Learning controllers for reactive and proactive behaviors in human–robot collaboration,” Frontiers in Robotics and AI, vol. 3, p. 30, 2016.

[22] S. Calinon, “A tutorial on task-parameterized movement learning and retrieval,” Intelligent Service Robotics, vol. 9, no. 1, pp. 1–29, 2016.

[23] S. Calinon and A. Billard, “Recognition and reproduction of gestures using a probabilistic framework combining pca, ica and hmm,” in Proceedings of the 22nd international conference on Machine learning. ACM, 2005, pp. 105–112.

[24] G. Schwarz et al., “Estimating the dimension of a model,” The annals of statistics, 1978.

[25] J. Liu, P. Jayakumar, J. L. Stein, and T. Ersal, “Combined speed and steering control in high speed autonomous ground vehicles for obstacle avoidance using model predictive control,” IEEE Transactions on Vehicular Technology, vol. 66, no. 10, pp. 8746–8763, 2017.

[26] H. Febo, J. Liu, P. Jayakumar, J. L. Stein, and T. Ersal, “Moving obstacle avoidance for high, high-speed autonomous ground vehicles,” in 2017 American Control Conference (ACC). IEEE, 2017, pp. 5568–5573.

[27] J. Liu, P. Jayakumar, J. L. Stein, and T. Ersal, “A nonlinear model predictive control formulation for obstacle avoidance in high-speed autonomous ground vehicles in unstructured environments,” Vehicle System Dynamics, vol. 56, no. 6, pp. 853–882, 2018.

[28] H. Febo, “Nloptcontrol,” [https://github.com/JuliaMPC/Nloptcontrol.jl] 2017.

[29] A. Wächter and L. T. Biegler, “On the implementation of an interior-point filter line-search algorithm for large-scale nonlinear programming,” Mathematical Programming, vol. 106, no. 1, pp. 25–57, 2006.
Ruikun Luo is a Ph.D. candidate at the Robotics Institute, University of Michigan, Ann Arbor. Prior to joining the University of Michigan, he obtained a M.S. in Mechanical Engineering from Carnegie Mellon University in 2014 and a B.S. in Mechanical Engineering and Automation from Tsinghua University, China in 2012. His research interest is human-robot interaction.

Yifan Weng is a Ph.D. candidate at the Mechanical Engineering, University of Michigan, Ann Arbor. He received the B.S.E. degree in mechanical engineering from Shanghai Jiao Tong University, Shanghai, China and from Purdue University, IN, US in 2016 and the M.S.E. degrees in mechanical engineering from the University of Michigan, Ann Arbor, MI, USA, in 2018.

Yifan Wang is a Ph.D. student at the electrical engineering and computer science, University of Michigan, Ann Arbor. He received the B.S. degree in electrical engineering from Xi’an Jiao Tong University, China, in 2018, and the M.S. degree in electrical and computer engineering from the University of Michigan, Ann Arbor, in 2019. His research interests include human-computer interaction, medical image processing and reinforcement learning theory.

Paramsothy Jayakumar received his M.S. and Ph.D. degrees in structural dynamics from Caltech, and B.Sc. Eng. from the University of Peradeniya, Sri Lanka. He is a Senior Research Scientist, SAE Fellow, and a member of the Analytics Team at the U.S. Army Ground Vehicle Systems Center (GVSC) in Warren, Michigan. He is a member of the U.S. Army Acquisition Corps, an Honorary Fellow of the Department of Mechanical Engineering at the University of Wisconsin Madison, and an Associate Editor for the ASME Journal of Computational and Nonlinear Dynamics.

Mark Brudnak (M04) received the B.S. degree in electrical engineering from Lawrence Technological University, Southfield, MI, in 1991, and the M.S. degree in electrical and computer engineering and the Ph.D. degree in systems engineering from Oakland University, Rochester, MI, in 1996 and 2005, respectively. He is currently an Associate Director at the U.S. Army Ground Vehicle Systems Center (GVSC), Warren, MI. In this capacity, he oversees the operation of laboratories for durability testing, vehicle characterization, and human-in-the-loop motion base simulation.

Victor Paul serves as a Team Leader in the Ground Vehicle System Centers System Ground Vehicle Simulation Laboratory (GVSL) where he has worked for 28 years. He holds extensive knowledge in the area of motion base simulation and its application in both man and hardware in the loop experiments. He is currently a senior advisor for the Crew Optimization and Augmentation Technologies Science and Technology program and is supporting the development of Crew Station and Squad interfaces for the Next Generation Combat Vehicle Mission Enabling Technology Demonstrator.

Vishnu R. Desaraju received the B.S.E. degree in Electrical Engineering from the University of Michigan, Ann Arbor, MI in 2008, S.M. degree in Aeronautics and Astronautics from the Massachusetts Institute of Technology, Cambridge, MA in 2010, and M.S. and Ph.D. degrees in Robotics from Carnegie Mellon University, Pittsburgh, PA in 2015 and 2017, respectively. He is currently a Research Scientist at the Toyota Research Institute, Ann Arbor, MI developing automated driving technologies. His research interests include real-time motion planning and control of constrained, uncertain systems.

Jeffrey L. Stein received the B.S. degree in premedical studies from the University of Massachusetts, Amherst, MA, in 1973, and the S.B., S.M, and Ph.D. degrees in mechanical engineering from the Massachusetts Institute of Technology, Cambridge, MA, in 1976, 1976, and 1983, respectively. Since 1983 he has been with the University of Michigan, Ann Arbor, MI, where he is currently a Professor of Mechanical Engineering. His research interests include computer based modeling and simulation tools for system design and control, with applications to vehicle-to-grid integration, vehicle electrification, conventional vehicles, machine tools, and lower leg prosthetics.

Tulga Ersal received the B.S.E. degree from the Istanbul Technical University, Istanbul, Turkey, in 2001, and the M.S. and Ph.D. degrees from the University of Michigan, Ann Arbor, MI USA, in 2003 and 2007, respectively, all in mechanical engineering. He is currently an Associate Research Scientist in the Department of Mechanical Engineering, University of Michigan, Ann Arbor, MI. His research interests include modeling, simulation, and control of dynamic systems, with applications to vehicle and energy systems.

X. Jessie Yang is an Assistant Professor at the Department of Industrial and Operations Engineering, University of Michigan Ann Arbor. She obtained her PhD in Mechanical and Aerospace Engineering (Human Factors) from Nanyang Technological University, Singapore in 2014.