Faulty antenna detection in a linear array using simulated annealing optimization

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ABSTRACT
Sonar, radar and communication systems solely depend on antenna arrays for signal attainment. These arrays are capable of producing directional signals which can be steered in a certain direction. Faulty elements in an array will result in distorted radiation pattern with increased sidelobe levels. Far-field faulty antenna detection is necessary due to the near field repairing at complex systems like spacecraft. This paper proposes simulated annealing (SA) optimizing method to find the faulty element’s location in a linear array. In this study, a Chebyshev array is presented with the SA optimization method to detect faulty element location with a random permutation of failure locations tested. This method can successfully detect faulty antenna in a linear array. Even though, this method is developed for linear array it can easily be adapted to a planar array.

Keywords: Beam pattern, Failed sensor, Location, Optimization, Simulated annealing

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1. INTRODUCTION
Antenna arrays play a vital role in various fields like sonar, radar and communication systems for its signal attainment which can generate directed signals that can be steered to the desired angle. Normally, the arrays are designed with a large number of elements which will eventually increase the probability of faulty elements in an array. The faulty elements ruin the symmetry of the array and rigorously distort the radiation pattern with increased sidelobe levels. The usual way is to take near field measurements of the antenna to find the failed element in an array [1–3]. It is not practical to apply this convention method in remote systems like spacecraft where the system is inaccessible by humans [4]. However, another way to detect the failed elements is to use test couplers and calibration probes which are expensive and complex to use [5]. This increases the necessity of more research on a far-field radiation pattern to find the failed element(s) in an array [6]. On the other hand, literature [7–10] suggested correction or compensation for the failed radiation pattern. However, information on the number and the position of the failed element is required to apply the corrections to the array.

Authors in the previous works have used artificial neural network [11, 12] to detect failed locations. This method maps the radiation pattern of a faulty array at different sets of combinations and trains the network. While in [13], the author has suggested a Multi-class Support Vector Classifier (SVC) for planar array failure diagnosis. These methods are limited to the on-off type of fault where antennas were considered as completely failed or completely working; no consideration was executed for partial failure or a certain percentage of failure of the elements in the array. Whereas, optimizations using the firefly algorithm [14], bacteria foraging technique [15] and fast Fourier transform [16] solves fault-finding with complete and partial failure in an array. Other than that, a Hybrid genetic algorithm with parallel coordinate descent [17] and a Hybrid cultural algorithm with differential evolution [18] is suggested by Khan S. U. et. al for a large...
number of elements in an array. The recent research is proving that an efficient algorithm to find the faulty element in an array is still continuing.

This paper presents a simulated annealing optimization method to detect the faulty element’s location and the percentage of failure in an array. Simulated annealing method is suitable in finding the lowest value during the objective function optimization which is known as global minima in the presence of other lower value known as local minima. It is an adaptation of the Monte Carlo method to generate a sample state of the thermodynamic system [19]. This method is used in various fields like solving network coverage problems [20], power system distribution [21], component location optimization [22] and solving multi-objective problems like production scheduling [23]. Previous work with this method related to failed elements in an array is to optimize the performance of the array [24]. But, no research has been done with this method to locate the failed elements in an array. A failed Dolph-Chebyshev pattern is generated with some faulty antenna in an array. Simulated annealing optimization is developed for the failed pattern to find the failed element location in the array. The method is successful in finding the failed location. The rest of the article is organized as follows. Section 2 compromises methodology while in Section 3 the SA method is provided. Section 4 discusses the simulation and results and this paper is concluded with Section 5.

2. METHODOLOGY

In order to test the proposed method, a beam pattern with failed elements is generated. A classical Dolph-Chebyshev linear array with 32 elements, λ/2 inter-element spacing and -30db constant SLL is used as the original array beam pattern and, failed elements are then randomly generated on this beam pattern. Then, the SA algorithm is developed to find the location(s) of the failed element(s). The details to generate the classical radiation pattern failed radiation pattern and simulated annealing method for failed element detection is discussed in the upcoming sections.

2.1. Beam pattern generation

The array factor of a classical Dolph-Chebyshev linear array beampattern with \( N \) elements, \( (N = 32) \) with equally spaced non uniform amplitude is given as (1) [25] below.

\[
G(\theta) = \sum_{n=1}^{N} w(n)e^{(2n-1)c} \text{arg}
\]

(1)

where

\[
\text{arg} = \pi d \left[ \sin \left( \theta - \frac{\pi}{2} - \gamma \right) \right]
\]

(2)

\( \theta \) is scanning angle,
\( \gamma \) is the steering angle
\( w(n) \) is Chebychev weights on each element
\( d \) Inter-element distance between array elements
\( N = 32, \) Array elements and \( n \) is the index

Failed radiation pattern with one or more faulty element(s) is calculated by using (1) and assigning the values for failed weights, \( w_f \) depending on the level percentage of failure. A zero weight for completely failed element, 50% of weight at a partially failed element or 75% of weight for three quarter failed element from the initial Chebyshev weights. Modified (1) for the failed radiation pattern is (3) [26] below.

\[
G_f(\theta_k) = \sum_{n=1}^{N} w_f(n)e^{(2n-1)c} \text{arg}
\]

(3)

\( G_k(\theta_k) \) will be treated as \( k \)-th radiation pattern (current) while \( G_f(\theta_k) \) will be the far-field radiation pattern. The optimization will compare far-field pattern with the current radiation pattern and minimize the objective function. The objective function is defined as

\[
\text{error} = \sum_{k=1}^{N} ((G_f(\theta_k) - G_k(\theta_k))^2
\]

(4)

Minimization in the objective function in return will give the weights or known as excitation amplitude of each element in the array.
2.2. Simulated annealing algorithm

Simulated annealing (SA) method falls under a stochastic optimization family which is similar to the Genetic Algorithm (GA) and Evolutionary Algorithm (EA). Normally, an initial design is changed using combinatorial analysis and evaluated with the objective function. SA allows the optimization to find an optimal solution to the design. The analogy of metal annealing is used in this which will reduce the objective function similar to temperature reduction in metal annealing process.

2.2.1 Simulated annealing for failed element detection

The desired calculation of SA is to detect the failed array element location in (3). The SA optimization searches are implemented by Monte-Carlo random searches. After every search, a new radiation pattern is formed and compared with reference far-field failed pattern. The error, in (4) represents the convergence of the successful detection of the failed array element. After running the optimization, the error value is checked. If error $\neq 0$, then the number of the sensor is increased by one and the procedure to find the failed location is repeated. If it is zero, the optimization ends by showing the weights at each element in the array including the failed elements. Figure 1 explains the SA optimization in flow chart representation.

![Flowchart representation of SA](image)

3. RESULTS AND ANALYSIS

The classic Chebyshev array radiation for 32 elements is generated with (1). The array pattern and its normalized weight distribution is shown in Figure 2. Then, the elements in the array are failed to test if the algorithm is able to detect the element(s) that failed in the array. For this purpose, 14th, 6th and 23rd element of an array is selected randomly. The optimization will start from one failure in the array and increases the number of element if the error after SA optimization is not equaled to zero as shown in Figure 1 earlier. The test was limited to three element failure as most of the literature has remained the number of failure to three in their works. Firstly, to test the ability to finding one or more element failure in an array, 14th element
is completely failed; then, 14th and 6th elements are failed; and lastly, 14th, 6th and 23rd elements are failed. For all the conditions, the optimization method managed to find the failed element(s) accurately. The initial Chebyshev weights and weights after running SA for all elements in the array are summarized in Table 1. It is observed that the SA managed to find the weights of completely failed elements as zero for all the specified locations and for all three conditions. Figure 3(a) shows the original Chebyshev array pattern and failed pattern for the 14th, 6th, and 23rd elements completely failed. Figure 3(b) shows its weight distribution. It is observed that the failure at three completely failed locations can severely damage the radiation pattern.

![Original Chebyshev array pattern for 32 elements and its normalized weight distribution](image)

**Table 1. Original chebyshev weights and weights obtained by simulated annealing**

| Element Number | Chebyshev Weights | 14th element Failed | 14th element & 6th element Failed | 14th element, 6th element & 23rd Failed |
|----------------|------------------|---------------------|-----------------------------------|----------------------------------------|
| 1              | 0.44             | 0.44                | 0.44                              | 0.44                                   |
| 2              | 0.24             | 0.24                | 0.24                              | 0.24                                   |
| 3              | 0.31             | 0.31                | 0.31                              | 0.31                                   |
| 4              | 0.37             | 0.37                | 0.37                              | 0.37                                   |
| 5              | 0.44             | 0.44                | 0.44                              | 0.44                                   |
| 6              | 0.51             | 0.51                | 0.0                               | 0.0                                    |
| 7              | 0.58             | 0.58                | 0.58                              | 0.58                                   |
| 8              | 0.64             | 0.64                | 0.64                              | 0.64                                   |
| 9              | 0.72             | 0.72                | 0.72                              | 0.72                                   |
| 10             | 0.78             | 0.78                | 0.78                              | 0.78                                   |
| 11             | 0.84             | 0.84                | 0.84                              | 0.84                                   |
| 12             | 0.89             | 0.89                | 0.89                              | 0.89                                   |
| 13             | 0.93             | 0.93                | 0.93                              | 0.93                                   |
| 14             | 0.97             | 0.0                 | 0.0                               | 0.0                                    |
| 15             | 0.99             | 0.99                | 0.99                              | 0.99                                   |
| 16             | 1                | 1                   | 1                                 | 1                                      |
| 17             | 1                | 1                   | 1                                 | 1                                      |
| 18             | 0.99             | 0.99                | 0.99                              | 0.99                                   |
| 19             | 0.97             | 0.97                | 0.97                              | 0.97                                   |
| 20             | 0.93             | 0.93                | 0.93                              | 0.93                                   |
| 21             | 0.89             | 0.89                | 0.89                              | 0.89                                   |
| 22             | 0.84             | 0.84                | 0.84                              | 0.84                                   |
| 23             | 0.78             | 0.78                | 0.78                              | 0.0                                    |
| 24             | 0.72             | 0.72                | 0.72                              | 0.72                                   |
| 25             | 0.65             | 0.65                | 0.65                              | 0.65                                   |
| 26             | 0.58             | 0.58                | 0.58                              | 0.58                                   |
| 27             | 0.51             | 0.51                | 0.51                              | 0.51                                   |
| 28             | 0.44             | 0.44                | 0.44                              | 0.44                                   |
| 29             | 0.37             | 0.37                | 0.37                              | 0.37                                   |
| 30             | 0.3              | 0.3                 | 0.3                               | 0.3                                    |
| 31             | 0.24             | 0.24                | 0.24                              | 0.24                                   |
| 32             | 0.44             | 0.44                | 0.44                              | 0.44                                   |

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Figure 3. The original Chebyshev array pattern and failed pattern for 14th, 6th, and 23rd elements completely failed and its normalized weight distribution.

Figure 4 shows the distribution of the weights of the array elements after running SA optimization. The SA optimization managed to find the failed element’s location similar to far-field defected radiation pattern. Other than that, failure percentage with complete failure element (100%), partial failure element (50%), and three-quarter failure element (75%) were also tested. For the next condition, 14th element three-quarter failed (75%), 6th element partial failed (50%) and the 23rd element completely failed (100%) far-field radiation pattern is simulated. Figure 5(a) shows the original radiation pattern and failed radiation pattern. Figure 5(b) shows its weight distribution throughout the array elements. Complete faulty element with zero weight, a partial faulty element with 50% of initial weight and three-quarter element failure with 25% from its initial weight can be clearly observed from the figure. Then, SA was run to locate the failed elements.

Figure 6 shows the weights of the original pattern and weights obtained after running SA. It is observed that the SA can successfully find the failed element’s location and the percentage failure precisely after the optimization. The algorithm can be modified to increase the number of failures in an array if needed.

Then, other random failure permutations were also tested with different locations and different percentages of failures to test the accuracy of the SA method. All results obtained by SA were recorded in Table 2. The results of the failed location found are bold in the table. The results prove that SA is capable of detecting the percentage failure in each element at random locations accurately.
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Figure 5(a). Original Chebyshev array pattern and failed pattern for 14th element failed 75%, 6th element failed 50% and the 23rd element completely failed (100%) Figure 5(b). Weight distribution of Original Chebyshev array pattern and Failed pattern for 14th element failed 75%, 6th element failed 50% and 23rd element completely failed (100%)

Figure 6. Original Chebyshev normalized weight distribution, Faulty elements and SA optimized weights for 14th element failed 75%, 6th element failed 50% and 23rd element completely failed (100%)

Table 2. Original chebyshev weights and weights obtained by simulated annealing for different percentage of errors

| Element Number | Chebyshev Weights | 14th element, 6th element & 23rd (100) Failed | 9th element (25%), 17th element & 29th (100) Failed | 30th element (75%), 20th element (50%) & 31st (100) Failed | 5th element (75%), 14th element (75%) & 28th (100) Failed |
|----------------|-------------------|-----------------------------------------------|-----------------------------------------------------|--------------------------------------------------------|--------------------------------------------------------|
| 1              | 0.44              | 0.44                                          | 0.44                                                | 0.44                                                   | 0.44                                                   |
| 2              | 0.24              | 0.24                                          | 0.24                                                | 0.24                                                   | 0.24                                                   |
| 3              | 0.31              | 0.31                                          | 0.31                                                | 0.31                                                   | 0.31                                                   |
| 4              | 0.37              | 0.37                                          | 0.37                                                | 0.37                                                   | 0.37                                                   |
| 5              | 0.44              | 0.44                                          | 0.44                                                | 0.44                                                   | 0.44                                                   |
| 6              | 0.51              | 0.51                                          | 0.51                                                | 0.51                                                   | 0.51                                                   |
| 7              | 0.58              | 0.58                                          | 0.58                                                | 0.58                                                   | 0.58                                                   |
| 8              | 0.64              | 0.64                                          | 0.64                                                | 0.64                                                   | 0.64                                                   |
| 9              | 0.72              | 0.72                                          | 0.54                                                | 0.72                                                   | 0.72                                                   |
| 10             | 0.78              | 0.78                                          | 0.78                                                | 0.78                                                   | 0.78                                                   |
| 11             | 0.84              | 0.84                                          | 0.84                                                | 0.84                                                   | 0.84                                                   |

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4. CONCLUSION

This paper presents simulated annealing optimization for finding failure location in an array. It is capable of finding the failed element’s location and percentage failure of a far-field defected radiation pattern successfully. Complete, partial, and 75% failure of the element in an array at different failure locations was traced out accurately by the proposed method. Far-field fault finding by SA reduces the need for near field measurements to find the failed location. When the failed location is known, it also helps to do a correction to the weights of other active elements to produce a similar radiation pattern as the original Chebyshev pattern. This method can be extended to planar arrays easily for future works.

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| Element Number | Chebyshev Weights | 14th element, 6th element & 23rd element (100%) Failed | 9th element (25%), 17th element & 29th element (100%) Failed | 30th element (75%), 20th element (50%) & 3rd element (100%) Failed | 5th element (75%), 14th element (75%) & 28th element (100%) Failed |
|----------------|------------------|----------------------------------------------------------|----------------------------------------------------------|----------------------------------------------------------|----------------------------------------------------------|
| 12             | 0.89             | 0.89                                                     | 0.89                                                     | 0.89                                                     | 0.89                                                     |
| 13             | 0.93             | 0.93                                                     | 0.93                                                     | 0.93                                                     | 0.93                                                     |
| 14             | 0.97             | 0.97                                                     | 0.97                                                     | 0.97                                                     | 0.2425                                                   |
| 15             | 0.99             | 0.99                                                     | 0.99                                                     | 0.99                                                     | 0.99                                                     |
| 16             | 1                | 1                                                        | 1                                                        | 1                                                        | 1                                                        |
| 17             | 1                | 1                                                        | 0                                                        | 1                                                        | 1                                                        |
| 18             | 0.99             | 0.99                                                     | 0.99                                                     | 0.99                                                     | 0.99                                                     |
| 19             | 0.97             | 0.97                                                     | 0.97                                                     | 0.97                                                     | 0.97                                                     |
| 20             | 0.93             | 0.93                                                     | 0.93                                                     | 0.465                                                    | 0.93                                                     |
| 21             | 0.89             | 0.89                                                     | 0.89                                                     | 0.89                                                     | 0.89                                                     |
| 22             | 0.84             | 0.84                                                     | 0.84                                                     | 0.84                                                     | 0.84                                                     |
| 23             | 0.78             | 0                                                        | 0.78                                                     | 0.78                                                     | 0.78                                                     |
| 24             | 0.72             | 0.72                                                     | 0.72                                                     | 0.72                                                     | 0.72                                                     |
| 25             | 0.65             | 0.65                                                     | 0.65                                                     | 0.65                                                     | 0.65                                                     |
| 26             | 0.58             | 0.58                                                     | 0.58                                                     | 0.58                                                     | 0.58                                                     |
| 27             | 0.51             | 0.51                                                     | 0.51                                                     | 0.51                                                     | 0.51                                                     |
| 28             | 0.44             | 0.44                                                     | 0.44                                                     | 0.44                                                     | 0.44                                                     |
| 29             | 0.37             | 0.37                                                     | 0.37                                                     | 0.37                                                     | 0.37                                                     |
| 30             | 0.3              | 0.3                                                      | 0.3                                                      | 0.075                                                    | 0.3                                                      |
| 31             | 0.24             | 0.24                                                     | 0.24                                                     | 0.24                                                     | 0.24                                                     |
| 32             | 0.44             | 0.44                                                     | 0.44                                                     | 0.44                                                     | 0.44                                                     |
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