Data Descriptor

Data-Sets for Indoor Photovoltaic Behavior in Low Lighting Conditions

Mojtaba Masoudinejad
TU Dortmund University, 44227 Dortmund, Germany; mojtaba.masoudinejad@tu-dortmund.de

Received: 29 February 2020; Accepted: 24 March 2020; Published: 28 March 2020

Abstract: Analysis of voltage–current behavior of photovoltaic modules is a critical part of their modeling. Parameter identification of these models demands data from them, measured in realistic environments. In spite of advancement in modeling methodologies under solar lighting, few analyses have been focused on indoor photovoltaics. Lack of accurate and reproducible data as a major challenge in this field is addressed here. A high accuracy measurement setup for evaluation and analysis of indoor photovoltaic modules is explained. By use of this system, different modules are measured under diverse environmental conditions. These measurements are structured in data-sets that can be used for either analysis of physical environment effects and modeling or development of specific parameter identification methods in low light intensity conditions.

Dataset: https://doi.org/10.5281/zenodo.3697105

Dataset License: CC-BY-SA

Keywords: energy harvesting; photovoltaic; indoor lighting; low light intensity; light measurement

1. Introduction

Photovoltaic (PV) systems under solar lighting have a long history dating back to the 18th century [1]. Long-term research has led to the maturity of this type of energy harvesting with different fields of application [2]: from power production and heating [3] to outer space energy supply [4]. Due to growing enthusiasm for the Internet of Things and Industry 4.0 revolution [5], a new application domain has been opened in recent years to supply embedded devices and cyber-physical systems [6]. The addition of a small PV module to supply an ultra-low power device has shown promising results [7]. This combination can be used to build energy neutral and battery-less systems for long lasting operation even in remote locations [8].

Integration of PV in new applications shows both similarities and differences with the classic solar PV energy harvesting. In contrast to the quest for optimal operation as a shared goal for both types, embedded device applications aim for energy neutrality as a key aspect. This requires specific analysis of a PV module in the application environment. Although some embedded devices are being used outdoors under solar light, others are restricted to indoor conditions. Some examples such as in [9] even take these conditions to an extreme by use of PV harvesting in environments with low light intensity such as a warehouse [10,11]. In these environments, artificial lighting is dominant while temperature is much more limited compared to the outdoor environment. Moreover, the small size of PV modules and low intensity artificial light leads to a much lower scale of harvested energy than the solar counterpart.

Different aspects of solar PV systems have been analyzed intensively, from electrochemical design [12], parameter estimation [13], and maximum power point tracking [14] to light analysis [15]. Even Standard Testing Condition (STC) AM1.5 is proposed as a part of the IEC60904-3 standard [16],
explaining a specific lighting situation to enable comparison of PV modules’ performances. In contrast, there are a limited number of works on the indoor performance and analysis of small scale PV modules [2]. In addition to smaller physical size of indoor PV device than a typical solar module, light absorbed by them has a different spectrum [17]. Moreover, the artificial lighting spectrum is extensively dependent on the type of light source, manufacturer, and physical structure of operational environments. This makes the definition of a unique standard measurement condition for indoor lighting measurement impossible. Hence, evaluation of developed methods and models cannot be simply guaranteed. Consequently, available analyses are limited to case-studies that are only reliable in their respected environments. Researchers prove and analyze their system in a very limited range of lighting because controlling their environmental conditions is hard, if not impossible. Not only are these experiments not reproducible, but also changes in the lighting are mostly not controlled and measured randomly.

Therefore, this work addresses this issue by providing not only multiple data-sets collected in a controlled environment, but also presents a setup for collection of this type of data. These data can be used for analysis of the indoor PV in different environmental conditions and also for the evolvement of methodologies from solar energy to adapt to the indoor conditions as well. Therefore, this paper is structured in a way that the physical structure of the measurement platform is explained first. Next, the developed measurement board including different sensors and their signaling is introduced. Afterwards, a procedure of measuring voltage–current curve of a PV module in low lighting is described. Finally, data collection and distribution of data in data-sets are discussed. In addition to this paper, data-sets can be accessed publicly from [18].

2. Measurement Platform

To assure reliable, constant, and reproducible lighting, a structure is required separating measurement environment from the general lighting. A cabinet sized 1100 × 660 × 660 mm is used as the structure with its interior coated with professional dark colored, light absorbing materials. Not only does this coating add a layer of protection against uncontrolled light, but it also prohibits light reflections inside the cabinet that can cause heterogeneous lighting. Although similar physical structure for the measurement of indoor light has been suggested in [17,19], they address issues on providing a homogeneous lighting when the light intensity has to be changed.

To enable smooth and accurate light intensity control, light source is an integration sphere here with a diameter of 500 mm coated with a Barium Sulfate layer. This sphere is connected on top of the cabinet with an opening of size 190 mm as the light output of sphere to the cabinet. The integration sphere has five entry openings, each with a 40 mm diameter as the light entry point to the sphere. Design of this integration sphere is in a way that the light provided by each source reflects multiple times (in theory infinite times) before passing through the output to the cabinet. Each entry opening is equipped with a mechanical diaphragm that can control the amount of light into the sphere. To avoid overheating of light sources during long measurement sessions, light entries are cooled using a water circulation system. The overall structure of this measurement system can be seen in Figure 1.

The main benefit of using an integration sphere is that the outcoming light has a homogeneous distribution at each height. This is critical while it is not possible to mount all measuring devices at an exact similar point—specially because, in addition to the PV module, light intensity has to be measured as well. By mounting all measuring elements on a single measurement board and putting it in the measurement cabinet at a flat surface, they will receive the same light intensity.

Although this cabinet isolates measurement environment from its surroundings, heat from light sources and operation of devices inside the cabinet can still increase the internal temperature. As the cabinet does not include an air conditioning system, a ventilation system pushes fresh air from the bottom of the cabinet. However, this air passes through a light maze to avoid any changes in the lighting. In this way, the temperature of the cabinet will be constantly equal to the room temperature which is a common office space with air conditioning, changing only in a limited range.
3. Measurement Board

In addition to the PV module that has to be evaluated during each measurement, environmental data including light intensity and temperature are required. Temperature measurement principles are well established and multiple sensors are available for its measurement. In this setup, a MCP9808 sensor [20] produced by Microchip as a digital sensor with I2C interface is used, delivering a good accuracy measurement with high resolution.

In contrast to the temperature measurement, light can be measured in different types including spectroscopy and integrative form. In spectroscopy, the intensity of each wavelength in the visible light range is measured separately. In contrast, integrative measurements are a summation of the intensity of the whole range presented by a single value. Although it is possible to extract the integrative value from a measured spectrum, this conversion is not reversible due to the nature of spectroscopy measurement. In addition to the representation form of measurement, there are two concepts of measuring light, namely: radiometry and photometry. Their difference is in the sensitivity of the measurement at each wavelength. Radiometry is the measurement in its pure form, which has to be scaled according to the human eye sensitivity curve to find the photometry data [21]. Irradiance with the unit of \( \text{W m}^{-2} \) is to address the radiometry data, while illuminance is for the photometry with the unit of \( \text{lm m}^{-2} \) or [lx].

Both radiometry and photometry data can be measured with a single spectrometer. While integration of spectrum data provides integrative values, use of spectrometers is not feasible for most applications because of their complexity, cost, weight, and size. Therefore, specific sensors are available which cater to integrative measurement directly. Pyranometers are very common for solar applications, used for irradiance measurement. However, their size and cost makes them not feasible for indoor embedded systems. On the contrary, there are multiple small size integrative photometry sensors available with reasonable size and price. This is mainly due to their usage in consumer electronic devices such as mobile phones and home TV setups.

A BLACK-Comet spectrometer from Stellar Inc. is used here. It has a wavelength range of 200 nm to 1100 nm and can be governed by a control PC via a USB connection. To have an accurate measurement, light is being probed with a 2-inch StellarSphere IC2 integration sphere with a 180° field of view and a wavelength range of 200 nm to 1700 nm. This integration sphere transfers the light probe to the spectrometer through a fiber optic connection. Both types of spectroscopy data can be measured directly using this combination in the whole desired indoor range of light.
For the integrative data, energy of spectrum can be simply accumulated. However, due to common use of integrative photometry sensors in embedded systems, two digital light measurement sensors are integrated in the system. First, Max44009 [22] is an ultra-low power sensor produced by Maxim Integrated. The secondary sensor that has a higher accuracy and resolution is TSL2561 [23] from AMS AG. It has two channels to deliver measurements in separate ranges. However, the whole range measurement is used here. Similar to the temperature sensor, these light sensors use I2C protocol to communicate.

A Raspberry Pi is used for communication and setting of integrative light and temperature sensors while connected to the control PC as well. The reason for using a separate system rather than the main control PC is the ability of on-site measurement for those systems that does not require spectroscopy data. In these cases, Raspberry pi can control the measurement without a higher controlling unit. Before each measurement experiment, Raspberry Pi initializes all sensors to measure in a periodic manner with a constant sample time.

Regardless of homogeneous light from the integration sphere on top of the measurement cabinet, all of these devices are mounted on a single board (shown in Figure 2) near the PV module to reduce chance of difference in the absorbed light.

![Figure 2. Developed board for measurement of data, including all sensors, light sampling integration sphere and a PV module.](image)

All measuring components are positioned in a circle with a diameter of less than 100 mm which can be simply located in the center of light cylinder of integration sphere output with a diameter of 190 mm. However, it has to be noted that this applies a restriction on the maximum size of a possible PV module that can be measured in this setup. While both probe hole and farthest sensor subsequently have distances of about 30 mm and 20 mm from the edge of the PV module, the longest side of module has to be shorter than 170 mm. Furthermore, the diagonal distance of the PV module has to be inside the circular area of homogeneous light surface, leading to a 154 mm diagonal limitation on the PV module as well.

The PV module is fixed to the board using a double-sided tape while two jumpers are used for its electrical connection. Therefore, the PV module can be simply changed in a very short time period.

4. Voltage–Current Curve Measurement

The typical curve of a PV cell is commonly known and formulated based on its physical semiconductor structure. It has a double source form both bent and connected to each other at the Maximum Power Point (MPP) as shown in Figure 3.
This curve changes based on light intensity and type in addition to the temperature. Consequently, measurement of this curve has to be repeated for different environmental conditions. A common method of measuring this curve is to change a variable impedance connected to the PV module. This is commonly starting from zero to measure the short circuit current ($I_{sc}$) value or the cross point from the $y$-axis in Figure 3. By increasing the value of this impedance, the curve can be spanned until the crossing point from the $x$-axis to measure the open circuit voltage ($V_{oc}$).

For this measurement, a Keysight B2902A Source Measurement Unit (SMU) [24] is used that is able to operate in all four quadrants. This device has a resolution of 10 fA and 100 nV, making it a perfect candidate for high accuracy measurements in low light conditions. To assure non-destructive measurement, SMU is connected to the PV module using a 4-wire (Kelvin) connection. This SMU is connected to the control PC on the other side, using a USB connection. The overall signaling of the measurement system can be seen in Figure 4.

SMU uses a shunt resistor for the current measurement that changes according to the maximum passed current. Hence, proper peak current has to be set to reach the best possible resolution. To avoid sudden automatic change of shunt resistor during measurement, peak current value has to be set before measurement starts. From the voltage–current curve in Figure 3, $I_{sc}$ is the highest possible current for a measurement experiment as long as light intensity and temperature does not change. Therefore, before the beginning of the experiment, this current is measured by setting the SMU to a zero impedance and measuring the current. Next, according to internal limits of SMU, the proper shunt resistor is set.

For changing the impedance, it is simply possible to set the SMU as a voltage source and measure the delivered current because of its 4-quadrant identity. However, selection of the voltage range has to be done carefully, especially near the open circuit section to avoid damaging the PV module. On the other hand, some PV parameter estimation methods require knowledge of the curve slope at the axis crossing points. Measurement with a small region beyond the axis would be beneficiary for better calculation of the derivation. Consequently, voltage source starts from a marginally small negative value, growing slowly while the current is being measured simultaneously. Voltage sweeping proceeds until the current reaches a small negative value. According to the lighting intensity, the scale of current can be different. Hence, stopping current limit has to be relative to the $I_{sc}$ to avoid a change in the
shunt resistor. Considering all of these steps, the procedure of voltage–current curve measurement can be summarized in Algorithm 1.

**Algorithm 1:** Process of measuring a voltage–current curve of a PV module

Build connection between control PC and SMU;

\[V_{\text{source}} \leftarrow 0;\]

\[I_{sc}= \text{measure current};\]

Set over-current relay to \(I_{sc} + \epsilon\) (for shunt resistor selection);

\[V_{\text{source}} \leftarrow -100 \text{mV};\]

\[I_{h}= \text{measure current};\]

\[\text{while } I_{h} \geq -0.05 \times I_{sc} \text{ do}\]

\[V_{\text{source}} \leftarrow V_{\text{source}} + \epsilon;\]

\[I_{h}= \text{measure current};\]

\[\text{end}\]

Turn voltage source off;

Transfer data to the control PC;

Disconnect SMU from the control PC;

---

5. Data Collection

For a complete experiment, three sets of measurements have to proceed in parallel, namely:

- Environmental data measurement, including temperature and integrative photometry
- Spectroscopy, both radiometry and photometry
- Measurement of voltage–current curve

Hence, a MATLAB program running a script on the control PC orchestrates the procedure as presented in Algorithm 2:

**Algorithm 2:** Process of a complete experiment of PV data collection

Connect to the Raspberry Pi and initialize sensors;

Initialize SMU, measure \(I_{sc}\) and set initial values;

Initialize spectrometer;

Start sensors measurement through the Raspberry Pi;

Start spectrometry and voltage–current measurement in parallel;

\[\text{while voltage–current measurement or spectrometry not finished do}\]

\[\text{wait } ;\]

\[\text{end}\]

Stop sensors measurement through the Raspberry Pi;

Read all measurements into the control PC;

Clean sensor data and find average value for each;

Structure and store data;

---

While this process will be called an experiment, it has to be repeated in different environmental conditions. Therefore, after setting the lighting condition, each experiment is repeated three times to control and reduce the noise in data. In case of no clear discrepancy in the data, the average value of each parameter from all experiments is stored. Those experiments with large differences between trials are removed to avoid any doubt in the data-set.

For the collection of data-set, three different indoor PV modules with dissimilar technologies are selected with specifications presented in Table 1 when \(N_s\) and \(N_p\) subsequently present number of series and parallel cells in each module.
Table 1. Specifications of used PV modules for measurements.

| Manufacturer | Model          | Technology     | N_s | N_p |
|--------------|----------------|----------------|-----|-----|
| Solems       | 07/072/048     | Amorphous Silicon | 7   | -   |
| IXYS (IXOLAR)| SLMD960H12L    | Monocrystalline | 12  | -   |
| Conrad       | YH-75x90       | Polycrystalline | 18  | 2   |

For each of these modules, light has been manipulated in a range. All modules have been measured under a warm (W) white LED light source from CXM-32 series of LUMINUS [25]. For analysis of the effect of light type, the Solems module has been measured under another light from the same series and specification only with a cold (C) tune of light. To include the effect of temperature on the behavior, this module has been measured multiple times in different temperatures as well. At the end, four data-sets are collected for which an abstract representation of their light intensity and temperature can be seen in Figure 5.

Figure 5. Distribution of light intensity and temperature of measurements.

6. Real World Low Light Measurement

All data-sets until now have been measured in the cabinet that assures stable and controlled lighting conditions and can be used for systematic analysis. However, real case indoor scenarios are more complex with reflections from different objects and surfaces. Therefore, the measurement system has been taken into the PhyNetLab [10], which is a warehouse for experimental tests. These types of data can be used for the evaluation of methods and models from data-sets in the controlled environment in real case scenarios. In spite of LED lighting from ceiling, the industrial nature of the environment makes the lighting more complex. A data-set measured in different positions and height of this environment are also included which can be used for the evaluation of real case scenarios.

An abstract overview of all available data-sets can be seen in Table 2.
Table 2. Specifications of measured data-sets.

| Name       | Module | Lighting Type | Light [lx]         | Temperature [K] | No. of Experiments |
|------------|--------|---------------|--------------------|-----------------|--------------------|
| Solems-W   | Solems | Warm          | 10.8 to 240.5      | 298.8 to 304.9  | 130                |
| IXYS-W     | Ixys   | Warm          | 23.1 to 240        | 299 to 299.5    | 25                 |
| Conrad-W   | Conrad | Warm          | 29.7 to 241.5      | 298.9 to 299.1  | 23                 |
| Solems-C   | Solems | Cold          | 19.3 to 608.5      | 299.3 to 299.6  | 45                 |
| Solems-H   | Solems | Warehouse hall| 141.7 to 494.0     | 298.0 to 301.8  | 122                |

There are different reasons for fluctuation in the number of experiments in data-sets. At first, cold white LED light sources have a higher maximum power than their warm light counterparts, which enable measurements in a larger range of intensities, leading to a larger Solems-C data-set. The Solems-W data-set is larger than others with warm white LED because experiments are repeated in different temperatures to include its effect as well. Finally, Solems-H has more experiments while it is from measurements in different physical points in the warehouse with more than a 500 m² surface.

7. Structure of Data-Sets

All five data-sets use the same structure, although they have different numbers of experiments. Two data formats are available in these data-sets. On one hand, each data-set (including all its experiments) is stored as a MATLAB structure. On the other hand, data about each experiment are available in the CSV format.

The MATLAB structure is made of multiple rows with each row representing a single measurement experiment. Each experiment includes:

- **Name**: a unique identifier of experiment made as a combination of the PV module name, lighting type, temperature and light intensity
- **Temperature**: in Kelvin
- **TSL**: Integrative photometry from TSL sensor in [lx]
- **Maxim**: Integrative photometry from Maxim sensor in [lx]
- **Radiometry**: which is the spectrometry of irradiance as a table with columns of wavelength in [nm] and intensity in [W m⁻²]
- **Photometry**: which is the spectrometry of illuminance as a table with columns of wavelength in [nm] and intensity in [lm m⁻²]
- **VI**: a table including measured voltage in [V] and current in [A]

For the naming of each experiment, only the manufacturer name is included while warm and cold white LED types are shown subsequently by W and C; and H is used for the real case scenario in the warehousing hall. To distinguish experiments from each other, both temperature and intensity are multiplied by ten to build a four digit value. It should be noted that, for the light intensity, the value from a TSL sensor is used here. For instance, a measurement of the Conrad module in warm white LED at 298.9156 K and intensity of 37.6356 lx is named: Conrad_W_2989_0376.mat

To enable usage of this data for researchers without access to the MATLAB software, data from each experiment are stored in a single folder including different CSV files. Folder naming of experiments uses the same protocol as MATLAB data naming. All folders from a data-set (one PV module under a type of lighting) are collected together, leading to five main folders. Each experiment folder includes four pieces of CSV data including:
General including data name, temperature in [K], value from Maxim and TSL sensors in [lx] in addition to the integrative irradiance and illuminance from spectroscopy data

Photometry spectrometry of illuminance as a table with columns of wavelength in [nm] and intensity in [lm m$^{-2}$]

Radiometry spectrometry of irradiance as a table with columns of wavelength in [nm] and intensity in [W m$^{-2}$]

$VI$ measured voltage in [V] and current in [A]

In addition to this information, figures of radiometry, photometry, and voltage–current curves are stored in PNG format for visual review. An example of measured curves for the experiment “Solems_W_2993_2401” are shown in Figures 6–8 subsequently for radiometry, photometry and voltage–current curves.

![Figure 6. Example of radiometry spectrum from warm white LED light in experiment “Solems_W_2993_2401”.

![Figure 7. Example of the photometry spectrum from warm white LED in experiment “Solems_W_2993_2401”.

Figure 8. Example of a voltage–current curve from Solems module under warm white LED light in experiment “Solems_W_2993_2401”.

8. Conclusions

Within this work, a physical structure, electrical platform, and algorithms for measuring the behavior of small scale PV modules for indoor lighting is discussed, in addition to providing the collected data. The suggested setup separates the measurement platform from the environment, enabling control of the light intensity. Light is measured both in spectroscopy and integrative form for either radiometry and photometry. Furthermore, the voltage–current curves of PV modules are measured with high accuracy. Four different data-sets each with multiple experiments are measured, providing information for different modules, light intensities, and temperatures. Moreover, another data-set provides similar measurements from a warehouse as a real world application for integration of indoor PV modules in industrial ultra-low power embedded systems.

Funding: Part of this work has been funded by Deutsche Forschungsgemeinschaft (DFG) within the Collaborative Research Center SFB 876 “Providing Information by Resource-Constrained Analysis”, project A4. In addition, part of the work was funded by the Federal Ministry of Education and Research of Germany within the “competence center for machine learning ML2R” (01IS18038A).

Acknowledgments: The author hereby acknowledges and appreciates help from A. Riesner for the production of the measurement board; D. Kossmann, A. Korolev, and J. Emmerich during the design of the measurement cabinet, and, finally, A. Abouelkhair and M. Ansari for the data collection.

Conflicts of Interest: The author declares no conflict of interest. The funders had no role in the design of the study; in the collection, analyses, or interpretation of data; in the writing of the manuscript, or in the decision to publish the results.

References

1. Green, M. Photovoltaics: Coming of age. In Proceedings of the IEEE Conference on Photovoltaic Specialists, Kissimmee, FL, 21–25 May 1990; Volume 1, pp. 1–8, doi:10.1109/PVSC.1990.111582.
2. Masoudinejad, M.; Kamat, M.; Emmerich, J.; ten Hompel, M.; Sardesai, S. A gray box modeling of a photovoltaic cell under low illumination in materials handling application. In Proceedings of the 3rd International Renewable and Sustainable Energy Conference (IRSEC), Marrakech & Ouarzazate, Morocco, 10–13 December 2015; pp. 1–6, doi:10.1109/IRSEC.2015.7455081.
3. Padmanathan, K.; Govindarajan, U.; Ramacharamurthy, V.K.; Jeevarathinam, B. Integrating solar photovoltaic energy conversion systems into industrial and commercial electrical energy utilization—A survey. J. Ind. Inf. Integr. 2018, 10, 39–54, doi:10.1016/j.iii.2018.01.003.
4. Chen, Z.; Zhu, L.; Li, W.; Fan, S. Simultaneously and Synergistically Harvest Energy from the Sun and Outer Space. Joule 2019, 3, 101–110, doi:10.1016/j.joule.2018.10.009.
5. Masoudinejad, M.; Magno, M.; Benini, L.; ten Hompel, M. Average Modelling of State-of-the-Art Ultra-low Power Energy Harvesting Converter IC. In Proceedings of the 2018 International Symposium on Power Electronics, Electrical Drives, Automation and Motion (SPEEDAM), Amalfi, Italy, 20–22 June 2018; pp. 99–104, doi:10.1109/SPEEDAM.2018.8445303.
6. Heo, J.; Park, M. Simulation analysis of power management techniques for a solar-powered embedded device. In Proceedings of the 2017 2nd International Conference on Power and Renewable Energy (ICPRE), Chengdu, China, 20–23 September 2017; pp. 845–848, doi:10.1109/ICPRE.2017.8390653.
7. Frezzetti, A.; Manfredi, S.; Pagano, M. A design approach of the solar harvesting control system for wireless sensor node. Control Eng. Pract. 2015, 44, 45–54, doi:10.1016/j.conengprac.2015.07.004.
8. Raghunathan, V.; Kansal, A.; Hsu, J.; Friedman, J.; Srivastava, M. Design considerations for solar energy harvesting wireless embedded systems. In Proceedings of the IPSN 2005. Fourth International Symposium on Information Processing in Sensor Networks, Boise, ID, USA, 15 April 2005; pp. 457–462, doi:10.1109/IPSN.2005.1440973.
9. Masoudinejad, M.; Ramachandran Venkatapathy, A.K.; Emmerich, J.; Riesner, A. Smart Sensing Devices for Logistics Application. In Sensor Systems and Software; Magno, M., Ferrero, F., Bilas, V., Eds.; Springer International Publishing: Berlin, Germany, 2017; Volume 205, pp. 41–52, doi:10.1007/978-3-319-61563-9_4.
10. Falkenberg, R.; Masoudinejad, M.; Buschhoff, M.; Venkatapathy, A.K.R.; Friesel, D.; Hompel, M.t.; Spinczyk, O.; Wi etfeld, C. PhyNetLab: An IoT-based warehouse testbed. In Proceedings of the Federated Conference on Computer Science and Information Systems (FedCSIS), Prague, Czech Republic, 3–6 September 2017; pp. 1051–1055, doi:10.15439/2017F267.
11. Masoudinejad, M.; Venkatapathy, A.K.R.; Tondorf, D.; Heinrich, D.; Falkenberg, R.; Buschhoff, M. Machine Learning Based Indoor Localisation Using Environmental Data in PhyNetLab Warehouse. In Proceedings of the European Conference on Smart Objects, Systems and Technologies (SmartSysTech), Munich, Germany, 12–13 June 2018; pp. 1–8.
12. Giraldo, S.; Jehl, Z.; Placidí, M.; Izquierdo-Roca, V.; Pérez-Rodríguez, A.; Saucedo, E. Progress and Perspectives of Thin Film Kesterite Photovoltaic Technology: A Critical Review. Adv. Mater. 2019, 31, 1806692, doi:10.1002/adma.201806692.
13. Kumari, P.A.; Geethanjali, P. Parameter estimation for photovoltaic system under normal and partial shading conditions: A survey. Renew. Sustain. Energy Rev. 2018, 84, 1–11, doi:10.1016/j.rser.2017.10.051.
14. Pakkiraiah, B.; Sukumar, G.D. Research Survey on Various MPPT Performance Issues to Improve the Solar PV System Efficiency. J. Solar Energy 2016, doi:10.1155/2016/8012432.
15. Anagha, M.J.; Rao, S.N.; Bennaceur, K. A Survey of Solar Irradiance Measurement Techniques. In Proceedings of the 2018 IEEE International Conference on Computational Intelligence and Computing Research (ICICC), Madurai, India, 13–15 December 2018; pp. 1–4, ISSN 2471-7851, doi:10.1109/ICICC.2018.8782393.
16. IEC. IEC 60904-3:2019 | Water Management, Smart City, Rural Electrification, Solar Power, Solar Panel, Photovoltaic, PV, LVDC; IEC 60904-3:2019; IEC: Geneva, Switzerland, 2019.
17. Masoudinejad, M.; Emmerich, J.; Kossmann, D.; Riesner, A.; Roidl, M.; ten Hompel, M. Development of a measurement platform for indoor photovoltaic energy harvesting in materials handling applications. In Proceedings of the 6th International Renewable Energy Congress, Sousse, Tunisia, 24–26 March 2015; pp. 1–6, doi:10.1109/IREC.2015.7110938.
18. Masoudinejad, M. Data-sets for Indoor Photovoltaic Behavior in Low Lighting condition. 2020, doi:10.5281/zenodo.3697105.
19. Masoudinejad, M.; Emmerich, J.; Kossmann, D.; Riesner, A.; Roidl, M.; ten Hompel, M. A measurement platform for photovoltaic performance analysis in environments with ultra-low energy harvesting potential. Sustain. Cities Soc. 2015, 25, 74–81, doi:10.1016/j.scs.2015.09.006.
20. Microchip Technology Inc. MCP9808 Digital Temperature Sensor Datasheet; Microchip Technology Inc.: Chandler, AZ, USA, 2011.
21. McCluney, W.R. Introduction to Radiometry and Photometry; Artech House: Norwood, MA, USA, 2014.
22. Maxim Integrated. MAX44009 Ambient Light Sensor Datasheet; Maxim Integrated: San Jose, CA, USA, 2011.
23. ams AG. TSL2561 Ambient Light Sensor Datasheet; ams AG: Steiermark, Austria, 2018.
24. Keysight. *Keysight B2900A Series Precision Source/Measure Unit Datasheet*; Keysight: Santa Rosa, CA, USA, 2017.
25. Luminus Devices, Inc. *CXM-32 COB Arrays White LED Datasheet*; Luminus Devices, Inc.: Sunnyvale, CA, USA, 2015.