Effects of an Integrated Carbide Slag-Mushroom Dreg-Calcium Superphosphate Amendment on the Stabilization Process of Pb, Cu, Zn and Cd in Contaminated Soils

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Abstract: In the present study, the integrated use of organic and inorganic amendments (CS–MD–CSP) including carbide slag (CS), calcium superphosphate (CSP) and mushroom dreg (MD) are employed for the stabilization of heavy metals in contaminated soils. A response surface methodology combined with immobilization efficiency was employed to evaluate and optimize the proportion of the integration amendments on the stabilization process. The results predicted by a Box–Behnken design indicated that the maximum immobilization efficiencies of soil Pb, Cu, Zn and Cd could be achieve up to 99.88, 96.11, 99.78 and 87.88%, respectively, when the dosage of CS, CSP and MD were set as 4, 1 and 6%, respectively. European Community Bureau of Reference (BCR) speciation analysis indicated that the acid-soluble proportion of Pb, Cu, Zn and Cd in the soils decreased by 72.68, 37.03, 9.36 and 12.94%, respectively. Thus, this CS–MD–CSP integration amendment could potentially be used for the remediation of Pb, Cu, Zn and Cd in contaminated soils.

Keywords: heavy metals; stabilization; carbide slag; calcium superphosphate; mushroom dreg

1. Introduction

In recent decades, the heavy metal contamination of soil has dramatically increased globally due to the intensification of anthropogenic activities, especially in mining, smelting, chemical engineering, electroplating and the disposal of industrial wastes [1–4]. Among these heavy metals, zinc (Zn), copper (Cu), lead (Pb) and cadmium (Cd) are particularly persistent in soil environments, because of their non-biodegradable characteristic [5]. Meanwhile, these heavy metals are highly toxic in soils and can significantly inhibit seed germination, plant and crop growth, threaten food safety and disturb the ecosystem [6,7]. Moreover, the heavy metal contamination of soils has received great attention due to the fact that the toxicity poses serious threats to human and wildlife sustainability via the accumulation of the food chain, such as itai-itai disease and blood lead [8–10]. Consequently, the remediation of heavy metal contamination in soils is imperative.

Soil remediation technologies attract special attention since traditional soil reclamation practices such as landfilling, excavation, thermal treatment and chemical soil washing are typically expensive and destructive [11]. Strategies “ex situ” cause a significant deterioration of soil structure and often come at a high economic cost and an infeasible environment, limiting their use on large contaminated areas [12]. Compared to traditional soil remediation treatments, techniques “in situ” including soil amendment based-technologies such as stabilization seem to be more efficient and environmentally
friendly for heavy metal remediation because of their low cost and simple maintenance [13,14]. Chemical stabilization, a remediation technique that decreases the dissolved contaminants by sorption, precipitation/coprecipitation and chelation, is suitable for soil remediation in less polluted and larger areas [15].

Various inorganic (i.e., lime and phosphate compounds) and organic (i.e., cow or pig manure and compost) amendments have been used for the stabilization process of heavy metals in soil [16–19]. Inorganic amendments including phosphate compounds (i.e., rock phosphate, apatite and hydroxyapatite) [20,21], iron (Fe) and manganese (Mn) oxides and oxyhydroxides, Fe/Mn-bearing amendments [22,23], and lime agents. They [24] have been tested and were found to be successful in reducing the availability of heavy metals [25]. Organic amendments including sewage sludge [26,27], compost [28,29], rice straw [30], animal manures [31,32], and biosolids [33,34] are low-cost adsorbents which have received more attention due to their availability, inexpensiveness, flexibility and capability to stabilize heavy metals without additional pre-treatment [35]. Moreover, they require much less area and dosages than inorganic agents.

Generally, phosphate compounds enhance the immobilization of heavy metals in soils by direct metal adsorption/substitution with P compounds, which significantly increased surface charge and enhance anion-induced metal adsorption [36]. A range of liming materials is effectively used to neutralize soil acidity. The addition of organic amendments improves the physicochemical and biological conditions of soils. Carbide slag (CS) is a by-product of the calcium carbide industry and mainly composed of Ca(OH)\(_2\) (85–95%) and CaCO\(_3\) (1–10%) [37]. Most of the CS in China is industrial solid waste. However, recently CS has been used to replace hydrated lime to ameliorate soil acidity in the soil stabilization process due to their similar chemical compositions [38]. Mushroom dreg (MD) is a type of agricultural waste, which is produced after the cultivation of edible fungus. MD have been already widely used as an ameliorant to improve the soil fertility of farmlands in many regions of China [39]. Calcium superphosphate (CSP) is a typical phosphate compound, which is applied as a fertilizer to improve the nutrient supply in soil and enhance the immobilization of heavy metals [40].

As a new soil stabilization binder, using CS–MD–CSP integration amendment as the stabilizer has not been investigated yet. So the objectives of this study were: (1) to select and optimize the proportion of CS–MD–CSP integration amendments for heavy metal stabilization; (2) to assess heavy metal leachability before and after the stabilization process using European Community Bureau of Reference (BCR) speciation analysis.

2. Experimental

2.1. Soil and Binders

The fresh soil was obtained from the suburban area in Nanning, Guangxi province, China, which was sieved to pass through a 2.0-mm mesh after air drying at room temperature. Based on the generally soil-contaminated situation around the smelter, according to the GB 15619-1995 (National standard of soil environmental quality), the proper amount of soluble salt containing Pb, Cu, Zn and Cd was added to the fresh soil in order to obtain the experimental soil (i.e., stimulated heavy metals combining polluted soil). The water content of the experimental soil was regulated to 40%, and laboratory incubation was carried out for 30 days. Selected chemical and physical properties of the experimental soil are presented in Table 1.
Table 1. Chemical and physical properties of the experimental soil.

| Parameters          | pH  | Total Heavy Metal Content (mg kg\(^{-1}\) DW *) |
|---------------------|-----|-----------------------------------------------|
|                     |     | Zn  | Cu  | Pb  | Cd  |
| Fresh soil          | 5.22| 74.8| 38.1| 45.3| 0.77|
| Experimental soil   | 3.97| 5040| 3600| 4080| 49.6|

* DW: dry weight.

CS is a kind of industry waste, which was obtained from Nanning Chemical Plant, sieved to pass through a 0.4-mm mesh after air drying at room temperature. The main chemical composition (by % weight) of the CS is presented in Table 2. MD was obtained from the local farmers and CSP is a kind of phosphate fertilizer and is mainly composed of Ca\((\text{H}_2\text{PO}_4)_2\cdot\text{H}_2\text{O}\) and \(\text{CaSO}_4\cdot2\text{H}_2\text{O}\), with an effective content (by % weight) of \(\text{P} \geq 16\%\), \(\text{S} \geq 10\%\) and \(\text{Ca} \geq 18\%\). The leaching toxicity concentrations of heavy metals in CS, MD, CSP and experimental soil are shown in Table 3.

Table 2. Main chemical composition (by % weight) of carbide slag (CS).

| Materials           | CaO | SiO\(_2\) | Al\(_2\)O\(_3\) | FeO  | Fe\(_2\)O\(_3\) | S    | P\(_2\)O\(_5\) | MgO  | K\(_2\)O | Loss on Ignition |
|---------------------|-----|-----------|-----------------|------|-----------------|------|-------------|------|----------|-----------------|
|                     | %   | %         | %               | %    | %               | %    | %           | %    | %        | %               |
|                     | 67.8| 3.51      | 2.06            | 0.55 | 0.36            | 0.05 | <0.05       | 0.074| <0.01    | 25.4            |

Table 3. Heavy metals' leaching toxicity concentrations in CS, MD, CSP and experimental soil.

| Parameters          | pH  | Heavy Metals' Leaching Toxicity Concentrations (mg L\(^{-1}\)) |
|---------------------|-----|---------------------------------------------------------------|
|                     |     | Zn  | Cu  | Pb  | Cd  |
| Experimental soil   | 3.97| 600 | 380 | 398 | 5.33|
| CS                  | 8.84| -   | 0.031| -  | 0.002|
| Mushroom dreg (MD)  | 6.82| 0.038| 0.065| 0.016| 0.002|
| Calcium superphosphate (CSP) | 1.94 | 4.73 | 1.02 | 0.055 | 0.127 |

2.2. Total Heavy Metal Content Determination

Total heavy metal content in soil was determined by digestion with a mixture of aqua regia with \(\text{HClO}_4\). A conical flask containing 0.5 g of soil sample and 10 mL of aqua regia (\(\text{HCl}:\text{HNO}_3 = 3:1\)) was heated in a sand-bath heater, and then 2 mL of \(\text{HClO}_4\) was used for the digestion of heavy metals, only added when the liquid cooled to room temperature. Finally, 1% of \(\text{HNO}_3\) was employed to dissolve the sample. The digests were filtered into 100-mL polyethylene bottles, and the content was determined using Inductively Coupled Plasma Atomic Emission Spectroscopy (ICP-AES).

2.3. Selection of Proportion by Box–Behnken Design

Response surface methodology (RSM) based on a Box–Behnken design (BBD) was employed to select the proportion of the CS–MD–CSP integration amendments. The significant variables utilized were as follows: dosage of CS, dosage of MD and dosage of CSP. BBD was used to determine the optimum proportion of these three amendments. A total of 17 trial experiments were conducted, which are indicated in Tables 4 and 5. The central values of all variables were coded as zero. Three-dimensional surface plots were used to express the fitted polynomial equation (Figure 1). The combination of different optimized variables was determined to verify the model. The statistical software package Design-Expert, Version 8.0.6 was used for the experimental designs and to analyze the central composite design. The information of model fitting was estimated by the analysis of variance (ANOVA) and multiple linear regressions. The quality of fit explained by the model was given by the multiple coefficient of determination R squared \((R^2)\) value [41,42]. The statistical significance of the model equation was determined via the Fisher’s test \((F\)-test) value and \(p\)-value (Table 6).
Table 4. Experimental variables at different levels using Box–Behnken design.

| No. | Variables          | Level |
|-----|--------------------|-------|
|     |                    | -1   | 0  | +1 |
| X1  | Dosage of CS(by % weight) | 2    | 3  | 4  |
| X2  | Dosage of CSP(by % weight) | 1    | 2  | 3  |
| X3  | Dosage of MD(by % weight)  | 5    | 6  | 7  |

Table 5. Experimental design and results of Box–Behnken optimization experiments.

| Standard Order | Experimental Values | Immobilization Efficiency (%) |
|---------------|--------------------|--------------------------------|
|               | Observed           | Predicted                      |
| X1            | X2                | X3                | Pb | Cu | Zn | Cd | Pb | Cu | Zn | Cd |
| 1             | 2.00              | 1.00              | 6.00 | 99.7 | 85.7 | 98.9 | 68.8 | 99.7 | 85.8 | 98.8 | 68.5 |
| 2             | 4.00              | 1.00              | 6.00 | 99.9 | 96.1 | 99.8 | 87.9 | 99.9 | 96.2 | 99.7 | 88.7 |
| 3             | 2.00              | 3.00              | 6.00 | 99.9 | 82.5 | 94.8 | 65.1 | 99.8 | 82.4 | 94.9 | 64.3 |
| 4             | 4.00              | 3.00              | 6.00 | 99.9 | 90.1 | 99.3 | 85.3 | 99.9 | 99.9 | 99.4 | 85.6 |
| 5             | 2.00              | 2.00              | 5.00 | 99.8 | 83.6 | 96.5 | 60.6 | 99.8 | 82.7 | 96.6 | 61.1 |
| 6             | 4.00              | 2.00              | 5.00 | 99.9 | 93.8 | 99.6 | 83.8 | 99.9 | 93.0 | 99.7 | 83.2 |
| 7             | 2.00              | 2.00              | 7.00 | 99.9 | 84.5 | 97.2 | 67.1 | 99.9 | 85.4 | 97.2 | 67.7 |
| 8             | 4.00              | 2.00              | 7.00 | 100.0 | 92.2 | 99.6 | 87.6 | 100.0 | 93.0 | 99.5 | 87.1 |
| 9             | 3.00              | 1.00              | 5.00 | 99.8 | 87.7 | 99.8 | 77.6 | 99.8 | 88.5 | 99.9 | 77.5 |
| 10            | 3.00              | 3.00              | 5.00 | 99.8 | 85.2 | 97.7 | 73.2 | 99.8 | 86.2 | 97.5 | 73.4 |
| 11            | 3.00              | 1.00              | 7.00 | 99.9 | 93.3 | 99.6 | 82.6 | 99.8 | 92.3 | 99.8 | 82.3 |
| 12            | 3.00              | 3.00              | 7.00 | 99.9 | 85.7 | 98.1 | 78.9 | 99.9 | 85.0 | 98.0 | 79.1 |
| 13            | 3.00              | 2.00              | 6.00 | 99.9 | 89.5 | 99.2 | 78.6 | 99.9 | 89.5 | 99.1 | 78.5 |
| 14            | 3.00              | 2.00              | 6.00 | 99.9 | 89.8 | 99.1 | 78.7 | 99.9 | 89.5 | 99.1 | 78.5 |
| 15            | 3.00              | 2.00              | 6.00 | 99.9 | 89.3 | 99.2 | 78.7 | 99.9 | 89.5 | 99.1 | 78.5 |
| 16            | 3.00              | 2.00              | 6.00 | 99.9 | 89.2 | 99.2 | 78.7 | 99.9 | 89.5 | 99.1 | 78.5 |
| 17            | 3.00              | 2.00              | 6.00 | 99.9 | 89.9 | 98.9 | 77.8 | 99.9 | 89.5 | 99.1 | 78.5 |

Figure 1. Correlation of observed and predicted immobilization efficiency for Pb, Cu, Zn and Cd of the Box–Behnken optimization experiments.
Table 6. Results of the regression analysis of the Box–Behnken design for the optimization of the stabilization ratio.

| Factor | df | Sum of Squares | Pb | Cu | Zn | Cd | Pb | Cu | Zn | Cd | p-Value |
|--------|----|----------------|-----|----|----|----|----|----|----|----|---------|
| Model  | 9  | 0.071          | 227 | 29.5 | 982 | 16.5 | 28.9 | 105 | 214 | 0.0006 | 0.0001 | <0.0001 | <0.0001 |
| X₁     | 1  | 0.026          | 161 | 14.5 | 863 | 54.9 | 184 | 462 | 1690 | 0.0001 | <0.0001 | <0.0001 | <0.0001 |
| X₂     | 1  | 3.20 × 10⁻³    | 46.8 | 8.69 | 26.2 | 6.65 | 53.7 | 278 | 51.3 | 0.0366 | 0.0002 | <0.0001 | 0.0002 |
| X₃     | 1  | 0.022          | 3.50 | 0.090 | 55.4 | 45.8 | 4.01 | 2.89 | 109 | 0.0003 | 0.0852 | 0.1330 | <0.0001 |
| X₁X₂   | 1  | 1.23 × 10⁻³    | 2.12 | 3.33 | 0.35 | 2.54 | 2.43 | 107 | 0.68 | 0.155 | 0.163 | <0.0001 | 0.436 |
| X₁X₃   | 1  | 2.03 × 10⁻³    | 1.78 | 0.15 | 1.68 | 4.21 | 2.05 | 4.87 | 3.29 | 0.0794 | 0.196 | 0.0632 | 0.113 |
| X₂X₃   | 1  | 2.25 × 10⁻⁴    | 6.45 | 0.065 | 0.17 | 0.47 | 7.40 | 2.08 | 0.34 | 0.516 | 0.0297 | 0.193 | 0.579 |
| X₁²    | 1  | 1.29 × 10⁻⁵    | 0.16 | 2.37 | 26.9 | 0.027 | 0.19 | 75.7 | 52.7 | 0.875 | 0.678 | <0.0001 | 0.0002 |
| X₂²    | 1  | 0.014          | 2.30 | 0.12 | 2.68 | 29.7 | 2.64 | 3.98 | 5.26 | 0.0010 | 0.149 | 0.0861 | 0.0554 |
| X₃²    | 1  | 1.40 × 10⁻³    | 2.83 | 0.076 | 6.10 | 2.91 | 3.25 | 2.44 | 12.0 | 0.132 | 0.115 | 0.163 | 0.0106 |
| Residual | 7  | 3.37 × 10⁻³    | 6.10 | 0.22 | 3.57 | 6.10 | 2.91 | 3.25 | 2.44 | 12.0 | 0.132 | 0.115 | 0.163 |
| Lack of fit | 3  | 3.05 × 10⁻³    | 5.74 | 0.18 | 2.90 | 12.7 | 21.1 | 6.05 | 5.74 | 0.0164 | 0.0065 | 0.0573 | 0.0623 |
| Pure error | 4  | 3.20 × 10⁻³    | 0.36 | 0.040 | 0.67 | 233 | 29.7 | 986 | 0.075 | 233 | 29.7 | 986 | 0.075 |

Pb: $R^2 = 0.955$, $R^2_{adj.} = 0.897$, C.V. (%) = 0.022, Adeq Precision = 13.2. Cu: $R^2 = 0.974$, $R^2_{adj.} = 0.940$, C.V. (%) = 1.05, Adeq Precision = 19.3.

Zn: $R^2 = 0.993$, $R^2_{adj.} = 0.983$, C.V. (%) = 0.180, Adeq Precision = 36.7. Cd: $R^2 = 0.996$, $R^2_{adj.} = 0.992$, C.V. (%) = 0.930, Adeq Precision = 50.3.
The quadratic equation model for predicting the optimum value and elucidating the interaction between the factors within the specified range are expressed as Equation (1) [2]:

\[ Y = \sum_{i=1}^{n} \beta_i X_i + \sum_{i=1}^{n} \beta_{ii} X_i^2 + \sum_{i=1}^{n-1} \sum_{j=i+1}^{n} \beta_{ij} X_i X_j + B_0 \]

where \( Y \) is the predicted response; \( X_i \) and \( X_j \) are the independent variables; \( \beta_0 \) is a constant of the equation; \( \beta_i \), \( \beta_j \) and \( \beta_{ij} \) are the linearity, quadratic and interactive coefficients of the model, respectively; \( n \) is the number of variables; \( B_0 \) is the intercept term.

2.4. Speciation Identification of Heavy Metals

Sequential extraction was performed using a three-stage modified procedure recommended by the European Community Bureau of Reference (BCR) plus the residual fraction [43,44]. In the BCR sequential extraction process, there were four nominal target fractions in order to recognize the environmental behavior and bioavailability of heavy metals and potentially toxic metals effectively, which were named the acid-soluble fraction (F1), easily reducible fraction (F2), oxidizable fraction (F3), and residual fraction (F4). The steps of the sequential extraction are presented in Table 7.

| Fractions | Extraction Fluid | Steps |
|-----------|------------------|-------|
| Step1—F1 | HOAc (0.11 mol·L\(^{-1}\)) | In this step, 32 mL of HOAc was added to 0.8 g of sample in a centrifuge tube and shaken at 25 °C for 16 h. The supernatant was separated and tested. |
| Step2—F2 | NH\(_2\)OH·HCl (0.11 mol·L\(^{-1}\)) | In this step, 32 mL of NH\(_2\)OH·HCl was added to the residue from Step 1 and shaken at 25 °C for 16 h. The supernatant was separated and tested. |
| Step3—F3 | H\(_2\)O\(_2\) (30%, pH = 2) CH\(_3\)COONH\(_4\) (1 mol·L\(^{-1}\), pH = 2) | In this step, 8 mL of H\(_2\)O\(_2\) was added to the residue in Step 2, digested at 85 °C for 1 h in a water bath until the volume reduced to approximately 2–3 mL. Then, 32 mL of CH\(_3\)COONH\(_4\) was added to the tube and digested with a cover at 85 °C for another 1 h and shaken at 25 °C for 16 h. The supernatant was separated and tested. |
| Step4—F4 | HCl/HNO\(_3\) + HClO\(_4\) | In this step, the residue from Step 3 was determined by the method mentioned in 2.2. |

3. Results and Discussion

3.1. Proportion Optimization of CS–MD–CSP Integration Amendments

3.1.1. Model Fitting and Analysis of Variance (ANOVA)

The models were statistically significant with a F-value of 16.48, 28.94, 104.76 and 214.01 for Pb, Cu, Zn and Cd, respectively, while the F-value of ‘lack of fit’ was 12.71, 21.07, 6.05 and 5.74 for Pb, Cu, Zn and Cd, respectively (Table 6). The high F-value and non-significant lack of fit indicate that the quadratic model was valid for the present optimization study. Meanwhile, the p-value for the models was less than 0.05 and proved that the obtained experimental data were a good fit with the model [45]. Moreover, determination and the adjusted determination of coefficients (\( R^2 \) and \( R^2_{adj.} \)) values for all metals were close to 1.0, confirming that the models have high explanatory power. In addition, the coefficient of variation (C.V.) for all metals was less than 10%, which indicated the high degree of precision and reliability of the developed models [46]. Furthermore, the high values of Adeq. Precision. (13.222, 19.273, 36.704 and 50.325 for Pb, Cu, Zn and Cd, respectively) show the adequate signal for the developed models, since an Adeq. Precision. value higher than 4% is desirable [46,47].
The variance of observed immobilization efficiencies and validity of the regression analysis are shown in Figure 1. The predicted values of Pb, Cu, Zn and Cd immobilization efficiencies obtained from the models and the observed experimental data were split evenly at the 45° line (Figure 1), implying that the quadratic models were considered to be reasonable. Additionally, the plot of studentized residual versus the predicted immobilization efficiency for Pb, Cu, Zn and Cd exhibited a non-symmetric scatter (Figure 2), indicating that the quadratic model terms were significant ($p < 0.05$) [2]. These results discussed above demonstrate the accuracy of the Box–Behnken model when applied to examine the proportion combinations of the CS–MD–CSP integration amendments in order to enhance the immobilization efficiencies of Pb, Cu, Zn and Cd in soils.

![Plot of residuals versus the predicted immobilization efficiency for Pb, Cu, Zn and Cd](image)

**Figure 2.** Plot of residuals versus the predicted immobilization efficiency for Pb, Cu, Zn and Cd of the Box–Behnken optimization experiments.

### 3.1.2. Prediction of Immobilization Efficiency by RSM Model

The experimental data on the immobilization efficiencies of Pb, Cu, Zn and Cd in the soils under different proportion combinations of the CS–MD–CSP integration amendments were analyzed by the second-order polynomial equation based on the coded values of the three operational factors:

\[
Y_1 = 99.89 + 0.057 \times X_1 + 0.020 \times X_2 + 0.053 \times X_3 - 0.017 \times X_1 X_2 - 0.022 \times X_1 X_3 + 7.5 \times 10^{-3} \times X_2 X_3 + 1.75 \times 10^{-3} \times X_1^2 - 0.058 \times X_2^2 - 0.018 \times X_3^2
\]

\[
Y_2 = 89.53 + 4.48 \times X_1 - 2.42 \times X_2 + 0.66 \times X_3 - 0.73 \times X_1 X_2 - 0.67 \times X_1 X_3 - 1.27 \times X_2 X_3 - 0.20 \times X_1^2 - 0.74 \times X_2^2 - 0.82 \times X_3^2
\]

\[
Y_3 = 99.10 + 1.34 \times X_1 - 1.04 \times X_2 + 0.11 \times X_3 + 0.91 \times X_1 X_2 - 0.20 \times X_1 X_3 + 0.13 \times X_2 X_3 - 0.75 \times X_1^2 - 0.17 \times X_2^2 - 0.13 \times X_3^2
\]

\[
Y_4 = 78.49 + 10.38 \times X_1 - 1.81 \times X_2 + 2.63 \times X_3 + 0.30 \times X_1 X_2 - 0.65 \times X_1 X_3 + 0.21 \times X_2 X_3 - 2.53 \times X_1^2 + 0.80 \times X_2^2 - 1.20 \times X_3^2
\]
which present the immobilization efficiency of Pb (Y₁), Cu (Y₂), Zn (Y₃) and Cd (Y₄) as a function of the dosage of CS (X₁), dosage of CSP (X₂) and dosage of MD (X₃). Because the coded variables in the regression equations (Equations (2)–(5)), were in the normalized form, the coefficients gave direct measures of the contribution of each factor and its interactions [47]. The dosage of CS had the largest coefficient in all four functions, which were 0.057, 4.48, 1.34 and 10.38, respectively, implying that it is the most dominating factor that affects the metal stabilization process.

Values of \( p \) less than 0.05 indicated that the model terms were significant and values below 0.01 indicated that the model terms were very significant. So, in this case, presented in Table 6, of the individual quadratic factors, the dosage of CS (X₁) and the dosage of CSP (X₂) had a statistically significant effect on the stabilization process of Pb, Cu, Zn and Cd, while the dosage of MD (X₃) is statistically insignificant on the stabilization process of Zn. The most important operational factor was the dosage of CS, having the highest F-value (54.94, 184.28, 462.05 and 1691.37) in all four models. Among the two-factor interaction, the interactions between the dosage of CS and the dosage of CSP (X₁×X₂) were significant on the stabilization process of Cu and Zn. From the squares of individual variables, the square of the dosage of CS (X₁²) was significant on the stabilization process of Cu, Zn and Cd, while the square of the dosage of CSP (X₂²) was significant on the stabilization process of Pb. Moreover, F-values present in Table 6 indicate that the effect of individual variables is relatively more significant than that of their interactions.

3.1.3. Contour Analysis

As presented in Figure 3 (1) and (3), the oval shape contour plots indicated that there was a strong interaction between the dosage of CS and CSP, and the dosage of MD and CSP. The Pb immobilization efficiency increased steadily as the dosage of CS rose from 2.00 to 4.00%, while the dosage of CSP remained approximately 2.00%. The shape of the contour in Figure 3 (4)–(6) confirmed a weak interaction between the two independent variables. But the contour plots showed that the Cu immobilization efficiency increased when the level of the dosage of CS increased while the level of the dosage of CSP decreased. As shown in Figure 3 (7)–(9), although the flat curve confirmed a weak interaction between the two independent variables, the contour plots implied that the lower dosage of the level of CSP was helpful to improve the immobilization efficiency of Zn. Additionally, the same conclusion can be found in Figure 3 (10) and (12). The curve increased in Cd immobilization efficiency when the level of the dosage of CSP decreased.

Hence, the curves indicated that the dosage of CS and dosage of CSP substantially influence Pb, Cu, Zn and Cd immobilization efficiencies. The higher dosage of the level of CS had a positive effect on the stabilization process, while higher dosage of the level of CSP an antagonistic effect on the stabilization process. When the dosage of CS remained approximately 6%, and the dosage of CSP remained approximately 1%, immobilization efficiencies of metals occurred in the following order: Pb > Zn > Cu > Cd. Meanwhile, the intermediate dosage of the level of MD was favorable to the stabilization process.
experiments yielded the average immobilization efficiencies of soil Pb, Cu, Zn and Cd, which were 99.8, 97.1, 99.7 and 88.2%, respectively. The results were in good agreement with the predicted value. Hence, the model developed was considered to be reliable for the prediction of the optimum proportion of the CS–MD–CSP integration amendments and for the optimization of the heavy metal stabilization process.

Figure 3. The contour plots showing effects of two independent variables on the Pb, Cu, Zn and Cd immobilization efficiency (holding another variable at central values).

3.1.4. Validation of the Models

The main purpose of RSM was to obtain the maximized response value with operational independent factors. In this study, the dosage of CS, CSP and MD were utilized to determine the optimum proportion of the three amendments, willing to obtain the best heavy metal immobilization efficiency. This optimization strategy successfully enhances the heavy metal immobilization efficiency. The results predicted by Box–Behnken design indicated that the maximum immobilization efficiencies of soil Pb, Cu, Zn and Cd could be achieve up to 99.9, 96.1, 99.8 and 87.9% efficiency, respectively, when the dosage of CS, CSP and MD were set as 4, 1 and 6% (by % weight), respectively. Based on the results, to confirm the model adequacy for the prediction of the maximum immobilization
efficiency, additional experiments were conducted in triplicate. The three replication experiments yielded the average immobilization efficiencies of soil Pb, Cu, Zn and Cd, which were 99.8, 97.1, 99.7 and 88.2%, respectively. The results were in good agreement with the predicted value. Hence, the model developed was considered to be reliable for the prediction of the optimum proportion of the CS–MD–CSP integration amendments and for the optimization of the heavy metal stabilization process.

3.2. Evaluation of the Immobilization Ability Using CS–MD–CSP Integration Amendments

3.2.1. BCR Specification Analysis of Targeted Heavy Metals

The four extracted fractions were analyzed, namely, the acid-soluble fraction, easily reducible fraction, oxidizable fraction and residual fraction, which were designated as F1, F2, F3 and F4. The mobility of these fractions was in the order of acid soluble > easily reducible > oxidizable > residual. The descriptive statistic of extraction fractions for Pb, Cu, Zn and Cd in soil after the stabilization process are listed in Table 8, and the contrast between the variation of the proportion of each metal before and after the stabilization process is presented in Figure 4.

Table 8. Total concentration of four targeted metals detected in soil (mg·kg−1).

| Elements | Total Concentration | F1   | F2   | F3   | F4   | Recovery/% |
|----------|---------------------|------|------|------|------|------------|
| Pb       | 4080                | 948  | 1430 | 1650 | 28.6 | 99.5       |
| Cu       | 3600                | 2180 | 899  | 502  | 14.1 | 98.5       |
| Zn       | 5040                | 4320 | 398  | 103  | 18.9 | 95.9       |
| Cd       | 49.6                | 33.8 | 13.4 | 1.57 | 2.90 | 104        |

Figure 4. Proportion of targeted heavy metals in the soil sample determined by the European Community Bureau of Reference (BCR).

Generally, acid-soluble heavy metals were not stable and would be easily released due to their weak binding capacity, which implied this fraction of metals can be directly used biologically and impose grave risks of contamination to the environment [43,48]. As shown in Figure 4 and Table 8, the F2 fraction of Pb, Cu, Zn and Cd in the soil was 35.2, 25.0, 8.23 and 27.0%, respectively, while the F3 fraction of Pb, Cu, Zn and Cd in the soil was 40.7, 14.0, 2.13 and 3.16%, respectively. Cd showed the highest proportion of F4 fraction with a content of 5.86%.
As presented in Figure 4, compared to the Cu, Zn and Cd, the fraction of Pb changed more obviously. The F1 fraction of Pb decreased from 84.4 to 23.4% and the F2 fraction of Pb increased from 14.5 to 35.1%, while the F3 fraction of Pb increased from 0.49 to 40.7%. In contrast, the increased amplitude of Cu, Zn and Cd is 18.1, 4.05 and 11.4%, respectively in the F2 fraction, while 12.1, 1.65% and 1.66%, respectively in the F3 fraction. The stabilization process of the metallic ion (Pb$^{2+}$, Cu$^{2+}$, Zn$^{2+}$ and Cd$^{2+}$) was promoted by binder in soil. In terms of the amounts of the four metals, Pb had a higher affinity for the reactive solid phases than Cu, Zn and Cd [49]. Meanwhile, ion exchange between divalent cations (Pb$^{2+}$) in soil and calcium (Ca$^{2+}$) chelated or linked to carboxylic groups in the polymeric structure [50]. Additionally, phosphate ions in CSP-induced reactions in the presence of divalent cations (Pb$^{2+}$) in soil can easily produce phosphate precipitation/mineral, which will significantly decrease the acid-soluble fraction [51].

3.2.2. Recovery Rate of Targeted Metals

Recovery (Equation (6)) is determined by comparing the total amount of metal extracted by different reagents during the sequential extraction procedure (four fractions: F1, F2, F3 and F4) with the total concentration of heavy metal in soil, which was served as an internal check for the precision of the results and calculated as followed [44]:

$$\text{Recovery} = \frac{C_{F1} + C_{F2} + C_{F3} + C_{F4}}{C_{\text{Total concentration}}} \times 100\% \quad (6)$$

The recovery of targeted heavy metals is presented in Table 8. These results showed that the total concentration of the four fractions of metals is in good agreement with the total concentration. Meanwhile, the satisfactory recovery rate of the four targeted metals ranges from 95.9 to 104%, which indicates that the data obtained in Table 8 by using the modified BCR sequential extraction method and ICP-AES are reliable and repeatable [52].

4. Conclusions

A response surface methodology based on a Box–Behnken design was employed to optimize the proportion of the integration amendments and enhance the stabilization process. The maximum immobilization efficiency of Pb, Cu, Zn and Cd could achieve up to 99.88, 96.11, 99.78 and 87.88%, respectively, when the dosage of CS, CSP and MD were set as 4, 1 and 6%, respectively. BCR speciation analysis indicated the acid-soluble proportion of Zn, Cu, Pb and Cd in the soils decreased by 9.36, 37.03, 72.68 and 12.94%, respectively, after treatment. The repairing mechanism of CS–MD–CSP integration amendments is complex, and the heavy metal concentration also changes since the properties of the repairing objects are different. Due to the limitation of experimental conditions and evaluation criteria, the characteristics and interactions of heavy metal ions needs further study.

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