Discriminant Feature Extraction for Centrifugal Pump Fault Diagnosis

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This work was supported in part by the Korea Institute of Energy Technology Evaluation and Planning (KETEP), and in part by the Ministry of Trade, Industry, and Energy (MOTIE), South Korea, under Grant 20181510102160.

ABSTRACT Raw statistical features can imitate the amplitude, average, energy and time, and frequency series distribution of a raw vibration signal. However, these raw statistical features are either not very sensitive to weak incipient faults or are unsuitable for more severe faults, thus affecting the fault detection and classification accuracy. To tackle this problem, this paper proposes a discriminant feature extraction method for Centrifugal Pump (CP) fault diagnosis. In order to obtain the discriminant feature pool, the proposed method is divided into three phases. In the first phase, a healthy baseline signal is selected. In the second phase, the healthy baseline signal is cross-correlated with the CP vibration signals of different classes, and a set of new features are extracted from the resulting correlation sequence. In the third phase, raw hybrid features in time, frequency, and the time-frequency domain are extracted from both the healthy baseline signals and the CP vibration signals of different classes. The correlation coefficient is calculated between the raw hybrid feature pools, which results in a new set of discriminant features. Discriminant features help the machine learning classifiers to effectively detect and classify the data into its respective classes. Furthermore, the proposed method combines all these features into a single feature vector that forms a vulnerable feature pool. The vulnerable feature pool describes the CP’s vulnerability to a fault and is provided as an input to a multiclass support vector machine (MSVM) for CP fault detection and classification. The experimental results illustrate that the accuracy obtained from the proposed method shows promising improvements over the state-of-the-art conventional methods.

INDEX TERMS Centrifugal pump, cross-correlation, correlation coefficient, fault classification, mechanical faults, vulnerable feature pool.

I. INTRODUCTION
CP’s have become an essential part of everyday business. It has been estimated that around 20% of the energy generated worldwide is dedicated to driving pumping systems [1]. CP’s likely account for the highest percentage of pumps used in industry [2]. CP’s are simple in construction, reliable in operation, and cheap in cost. However, the consequences of their unexpected failure include costly repairs, long downtime, economic losses, and reduced safety of operating staff. For this reason, health management has been attracting increasing attention to ensure the efficiency and reliability of pump operation.

A survey made by major organizations shows that with an investment of 10,000 – 20,000 dollars in health management, one can save up to 500,000 dollars per year [3]. In the past decades, several health management strategies have been developed, out of which predictive maintenance, also recognized as condition-based maintenance (CBM) is the most beneficial one. CBM suggests maintenance action based on the information collected through condition monitoring and allows the machine to have maximized running time with minimum maintenance costs [4]. As such, this paper uses the condition-based maintenance strategy for CP fault diagnosis.

Faults in the CP can be divided into mechanical faults (MF) and fluid flow related hydraulic faults (FHF) [5]. In S.M. Chittora’s thesis [6], he mentioned that 39% of pump failures occur due to mechanical seal faults. Another study [7],
explains that impeller imbalance can result in MF or FHF. To avoid CP failure, the early fault detection of both mechanical seal and impeller faults is of great significance. Hence, in this study, MF, which include mechanical seal and impeller faults, are taken into consideration.

MF or failures occurring in a CP result in abnormal vibration. Hence, vibration signals are commonly used for diagnosing MFs [8],[9]. However, abnormal vibration and impact signals with low amplitudes can be disguised by heavy background noise. Many signal processing approaches in the time, frequency, and time-frequency domain have been previously developed to extract appropriate fault features from raw vibration signals in order to detect MFs.

MFs in CP produce shocks resulting in variation of the vibration signal’s amplitude and distribution [10]. The time-domain statistical features are utilized to capture these variations [11]–[15]. However, they are not sensitive to the changing severity of faults and result in less discriminative features. The frequency spectrum is more sensitive to faults, since an undetectable change will produce a spectrum line in the corresponding frequency spectrum. Rapur and Tiwari [16] used frequency domain features for CP fault diagnosis. However, the fault vibration signals acquired from CP are highly non-stationary and Fourier Transforms (FT) are appropriate for stationary processes only [17],[18]. Moreover, interpreting the characteristic frequency components from the spectrum requires both mathematical and experimental validation. To overcome the non-stationary behavior of CP vibration signal, time-frequency domain methods have been introduced in the past few decades. References [19]–[22],[23] utilized wavelet transform (WT) to process CP vibration signals and extract discriminant features for CP fault segregation through machine learning models. However, selecting an optimal mother wavelet function for non-stationary vibration signals is still a problem. Further, determining the proper wavelet requires many experiments and subjective judgments in the experimental processes [24],[25]. Empirical Mode Decomposition (EMD) introduced in [26], a self-adaptive signal decomposition technique can overcome the shortcomings of the wavelet transform. EMD has been effectively used to extract discriminant information from the signal for the fault diagnosis of rotating machinery such as rotors, bearings, and gears [27] and CP faults [28]. Yet, the EMD technique has limitations that can cause problems when it is used to discern the nature of extracted information for machinery fault diagnosis. Particularly, mode-mixing can pose problems for the non-orthogonal components of decomposition. Ensemble Empirical Mode Decomposition (EEMD), a variant of EMD, was proposed to solve the problem of mode-mixing [29]. However, the selection of important intrinsic mode functions (IMFs) is a major challenge in EEMD [30]. Although EMD and its variants show outstanding performance in processing complex non-stationary and nonlinear signals, they suffer from the problem of extreme interpolation, sifting stop criterion, end effects, and a limited theoretical foundation [31].

In the light of the presented literature, vibration signal preprocessing and discriminant feature extraction are of primary importance for fault diagnosis. Discriminant features help the machine learning classifiers to classify the data effectively into respective classes. Considering the shortcomings of existing signal analysis techniques, most recent fault diagnosis studies have focused on extracting hybrid feature space from the vibration signals [32]–[36]. Prosvirin et al. [34] preprocessed the vibration signal using EEMD and extracted hybrid features for the diagnosis of rub-impact faults with an accuracy of 99.8%. Sohaib et al. [35] used a hybrid feature pool with a stacked sparse autoencoder based on deep neural networks and perform diagnosis of bearing faults having multiple severities with an accuracy of 99.10%. Hybrid feature space helps to overcome the effects of common fluctuations and random impulses in the vibration signal. However, the limited understanding of deep learning-based methods makes it difficult to define features and perform vibration signal preprocessing, and these methods are also computationally expensive.

To overcome the above challenges, a correlation function based feature extraction technique is proposed in this paper. Two types of correlation functions have been considered, namely, cross-correlation and correlation coefficient. The cross-correlation represents similarities between two signals, in the time domain and bears a low computational cost [37]. The correlation operation has been widely used for Brain Computer Interface oriented signals, such as EMGs and EEGs for human brain disease classification with an accuracy of 100% [38]–[40]. On the other hand, correlation coefficient finds the relationship between variables. Shi [41] performed bearing fault diagnosis using correlation coefficient and simplified neutrosophic sets.

Despite the good discrimination information extraction capabilities and low computational cost of cross-correlation, to the best of our knowledge, preprocessing the time-domain vibration signal using cross-correlation for CP fault diagnosis has not been reported so far. This could be due to the fact that for cross-correlation, a baseline healthy signal is required to which the CP vibration signals obtained during different CP operating conditions can be compared. Further, the random fluctuations caused by multiple severity faults in the CP cannot be addressed by analyzing the signal only in the time or frequency or time-frequency domain. However, hybrid features that are extracted from the vibration signal in time, frequency, and the time-frequency domain combined together can provide enough information for CP fault classification. Yet, as far as our knowledge is concerned, CP fault diagnosis using hybrid features has been reported rarely. This is because the hybrid features are extracted separately in time, frequency, and time-frequency domain and then combined into a single feature vector forming a high-dimensional feature space. The high-dimensional feature space may produce poor diagnosis results if the features are not sufficiently separable. Thus, further preprocessing is needed to obtain highly discriminant features from the high-dimensional feature space.
To address the above problems, this study proposes a new feature extraction method that considers, (i) preprocessing the vibration signals using cross-correlation function to extract correlogram features and (ii) preprocessing the features extracted from CP vibration signals using correlation coefficient. The proposed method results in discriminant feature extraction based on correlations is explained in Section IV. The proposed method for discriminant feature preprocessing: This paper analyzes both of the health baseline and CP vibration signals in time, frequency, and the time-frequency domain and extracts raw statistical hybrid features in each domain. As a result, two hybrid feature pools were created, one for the healthy baseline signal, and the other one for the CP vibration signal obtained after a different operating condition. This work then calculates the correlation coefficient between the two hybrid feature pools, which results in a new set of discriminant features from the correlogram sequences.

II. TECHNICAL BACKGROUND

A. REVIEW OF CROSS-CORRELATION

A cross-correlation is a mathematical operation that describes the mutual relationship that exists between two signals [37] [45]. This mutual relationship or similarity between the signals is represented by a sequence called correlogram. If a signal is correlated with itself, the resultant correlogram is called the autocorrelation. Assume that, $p(n)$ and $q(n)$ are two finite energy signals. The cross-correlation of the two signals are given by Eq.1.

$$R_{xy}(m) = \begin{cases} \sum_{n=0}^{N-1} p_{n+m}q_n & m \geq 0 \\ \sum_{n=0}^{N-1} p_{n+m}q_n & m < 0 \end{cases}$$ (1)

where $m = -(N - 1), \ldots, -2, -1, 0, 1, 2, \ldots, (N - 1)$. The variable $m$ denotes the time shift, also known as the lag, and $R_{xy}(m)$ represents the correlation between two signals $p$ and $q$ with a time shift of ‘$m$’. For $m \geq 0$, signal $p(n)$ leads the signal $q(n)$ by ‘$m$’ positions. And for $m < 0$, $p(n)$ lags behind the signal $q(n)$ by ‘$m$’ positions. If the signals $p(n)$ and $q(n)$ have a finite number of samples $N$ then the resultant correlogram has $2N - 1$ samples.

B. REVIEW OF WAVELET PACKET TRANSFORM

The WT provides multiresolution analysis of a signal in independent frequency bands. The wavelet packet transform (WPT) is derived from the basic WT which decomposes a given signal into $k$ levels. The WPT splits the input signal using low-pass and high-pass filters and creates $2^k$ nodes at each level. In this manner, the WPT overcomes the poor resolution of the WT because it provides a comprehensive time-frequency analysis of the input signal at both the high and low frequencies. Each level of the WPT provides a frequency range that is twice as wide as the proceeding level and half as wide as the preceding level. Fig. 1 shows the WPT structure having three levels. Eqs. 2 and 3 show the mathematical description for WPT coefficients.

$$c_{k+1}^j(n) = c_k^j \times h(-2n), \quad 0 < j < 2^k - 1$$ (2)

$$d_{k+1}^{2j+1}(n) = d_k^j(n) \times g(-2n), \quad 0 < j < 2^k - 1$$ (3)

where $h$ and $g$ in eqs. 2 and 3 are the low pass and high pass filters associated with the mother wavelet. In WPT, the nodes (frequency parameters) are denoted by $2j$ and $2j + 1$, and the levels (scale parameters) are denoted by $k$.

C. REVIEW OF SUPPORT VECTOR MACHINE

A SVM is a supervised machine learning model that is based on statistical learning theory. Fundamentally, the SVM is used for the classification of data into binary classes. As the SVM is a supervised classification technique, it uses a set of training data or/input data to create a hyperplane that classifies the data into two classes. Once the SVM is trained, any new set of data, called the testing data, is mapped into the same space and are characterized based on which side
of the margin it belongs to. Practically, there are numerous possibilities for classifying the data using a linear boundary, as shown in Fig.2a. But the Support Vector Classifier (SVC) places the boundary such that the margin is maximized and that’s why the SVM is also called a large margin classifier. If the input training data \( T = \{ (l_1, v_1), \ldots, (l_i, v_i) \} \), where \( l_i \in \mathbb{R}^N \) is the training data and \( v_i \in \{-1, +1\} \) gives the class labels, The SVC places the boundary between the classes such that the margin is maximized. The margin can be defined as the Euclidean distance between the separating hyperplanes and the data points, also called support vectors, of every class. Fig. 2b. shows an SVC classifying data into two classes. Thus, the hyperplane optimization problem can be specified as,

\[
\begin{align*}
\text{Minimize} & \quad \frac{1}{2} \|w\|^2 + C \sum_{i=1}^{B} \xi_i \\
\text{Subject to} & \quad v_i \left[ w^T \phi(l_i) + b \right] \geq 1 - \xi_i \\
& \quad \xi_i \geq 0, \quad i = 1, 2, \ldots, S
\end{align*}
\]

In Eq. 4, \( \xi \) is the slack variable that accounts for false classification, \( B \) is the number of training points, \( b \) is the bias, \( w \) is the weight vector, and \( C \) is the cost function which explains a tradeoff between the model complexity and learning error. If the data is not linearly distinguishable, then it is transformed to a higher dimensional feature space from the input space by using a nonlinear mapping \( \phi \), in which the data becomes linearly distinguishable. These kinds of transformations are computationally expensive. To solve this problem, a kernel function can be used for such a transformation. The kernel function is given by \( K(x_i, x_j) = \phi^T(x_i) \phi(x_j) \). In the present study, a Gaussian Radial Basis Function (RBF) kernel is used.

A detailed literature review for the SVM can be found in [46]. The SVM was fundamentally developed as a binary classifier. However, in practice, there can be more than two classes of the data to be classified. Thus, the data is converted into multiple binary classes and One Against All (OAA) or Direct Acyclic Graph or One Against One techniques may be used for multiclass classification. In this work, the OAA strategy is adopted.

III. TEST RIG SETUP AND EXPERIMENTAL PROCEDURE

For experimental purposes, a test rig has been developed that consists of different parts: the CP (PMT-4008 a widely used pump in the industry) that is driven by a 5.5kW motor, a control panel with an ON/OFF switch, speed controller, flowrate controller, temperature controller, water supply controller, and display screens; pressure gauges, clear steel pipes, and two tanks (main tank and buffer tank). To maintain the net...
positive suction head (NPSH) at the pump inlet for normal operation of the CP, the water tank was placed at a sufficient height. The test rig setup, as well as a schematic of the setup, are shown in Fig. 3a and 3b. After establishing the main setup, the test rig was operated for circulating water in a closed loop. The CP vibration data were collected at a constant speed of 1,733 rpm using four accelerometers, two of which were on the pump casing using adhesive, and for the other two, one was mounted close to the mechanical seal and the other was mounted near the impeller. Each sensor records the vibration of the pump using an independent channel. The recorded vibration signal was then passed to a signal monitoring unit, where the signal passes through a National Instruments 9234 device, which digitizes the acquired vibration signal. Details for the collection of data are specified in Table 1.

Data is acquired for a period of 300 sec at a sampling rate of 25.6 kHz. The sampling rate was kept high because of the mechanical seal excitation frequencies, which occur in between the 2nd and 3rd mode of vibration. A total of 1,200 samples, each with a sample length of 25,600, were collected from the CP under different operation conditions.

In the present study, the pump was operated under normal and different simulated fault conditions. The simulated faults are:

(A) Mechanical seal fault.
   (i) Mechanical seal hole.
   (ii) Mechanical seal scratch.

(B) Impeller fault.

These faults are simulated one at a time and the signals were obtained. The measurement noises were calculated for the obtained signals in each condition with respect to healthy baseline vibration signal. The measurement noises for mechanical seal hole, mechanical seal scratch and impeller

| TABLE 1. Specifications for data collection. |
|---------------------------------------------|
| Accelerometer (622b01)                     |
| Frequency range: 0.42 to 10 kHz             |
| Sensitivity: 100 mV/g (10.2mV/(m/s²)) ± 5 % |
| DAQ System (NI 9234)                       |
| Frequency range: 0 to 13.1 MHz              |
| Generator: 4 analog input channels 24 bits |
| ADC resolution                             |
fault vibration signals were found to be -69.10, -62.07, and -63.78 dB respectively.

A. MECHANICAL SEAL FAULT
The most common seal fault occurs because of excessive pressure. To avoid leakage from the pump during the installation, the rotating part of the mechanical seal is kept in contact with the stationary part by means of a spring or a combination of springs. These springs must be compressed by a predetermined amount of pressure. Whenever this pressure is exceeded it exerts excessive pressure on the mechanical seal faces. As a result, this may cause overheating and, in turn, the thin lubricating film of liquid in between the sealing faces converts into vapors. Dirt is one of the greatest enemies of the mechanical seal. Any trace of dirt trapped between the sealing faces can lead to holes, scratches, and can make the seal faces hard and brittle during operation because of the excessive pressure of the springs in the absence of a lubricating film. These kinds of premature seal failures are very dangerous and result in catastrophic failures of the pump. To avoid afflictions because of these premature seal failures, in this study, hole and scratch faults are seeded in the mechanical seal and vibration signals were taken.

1) MECHANICAL SEAL HOLE
A mechanical seal is made up of two parts: a rotating seal part and stationary seal part. In this study, two seals of a 38 mm inner diameter are used. In the two seals, the stationary part was defectless and in the rotating part, a hole was created, as shown in Fig. 4. the diameter of the hole was 2.8 mm and the depth was 2.8 mm. This was used as a defective seal to study the weak incipient fault under a mechanical seal hole defect.

B. IMPELLER FAULT
Crevice corrosion is one of the common reasons for an impeller fault. Crevice corrosion results in an irregular surface with numerous holes of different sizes that overlap and look as if the surface of the impeller has been eaten away by insects. These holes of different sizes may become severe cracks due to the shear on the material and lead to fatigue which can result in catastrophic failure. In this paper, a similar fault was seeded on the impeller and vibration signals of the defective impeller were recorded.

In this study three cast iron impellers, with 161 mm diameters, were used. Two impellers were new impellers without any defects. In the third impeller, a defect was created by removing some portion of the metal, as shown in Fig. 6. The diameters of the fault were 2.5 mm with a length of 18 mm and a depth of 2.8 mm. Fig. 7. shows the vibration signal obtained from the defective impeller while keeping all the other components in normal condition.

IV. PROPOSED METHOD
As explained in Section I, for discriminant feature extraction, both the vibration signal and feature preprocessing are important. Discriminant features help the subsequent classifier to classify the data effectively. This paper proposes a new method for CP fault diagnosis that preprocess both the vibration signal and raw statistical features based on the similarity. The workflow of the proposed method is presented in Fig. 8. As the proposed method is based on similarity, which means that the proposed method needs a baseline for comparison with the CP vibration signal and features of different classes. For this purpose, the proposed method can be divided into three phases. In the first phase, healthy baseline signals were selected. As the correlation measures the similarity in shape between the two signals, in the second phase, the vibration signal obtained from the CP under different operating
conditions is preprocessed by taking the cross-correlation between the healthy baseline signal and the CP vibration signal. The cross-correlation results in a correlogram signal in the time domain. The correlogram signal carries similarity information between the healthy baseline signal and the CP vibration signal. The proposed method extracts a new set of...
discriminant features from the resultant correlogram. Feature preprocessing helps in overcoming the effects of likely fluctuations and random impulses in the vibration signals. In the third phase, raw statistical features are preprocessed. Raw statistical features are extracted from both the healthy baseline signal and the CP vibration signal in time, frequency, and the time-frequency domain. Raw statistical features are preprocessed by calculating the correlation coefficient between the healthy baseline signal features and the raw statistical features of the CP. The correlation coefficient results in a similarity measure. This similarity measure is a discriminant and is used as a new feature for CP fault diagnosis. After extracting the features, the proposed method combines all the features and creates a vulnerable feature pool. Furthermore, the vulnerable feature pool is provided as an input to the MSVM for CP fault segregation. The various steps involved in the proposed method are as follows:

**PHASE I: SELECTION OF HEALTHY BASELINE SIGNAL**

The selection of a healthy baseline signal plays a vital role in performing cross-correlation and calculating the correlation coefficient for the vibration signal and features preprocessing. Thus, in this study, a proper approach has been adopted for the selection of a healthy baseline signal. The steps involved in the healthy baseline signal selection are as follows:

1) **STEP 1: FINDING PUMP PEAK EFFICIENCY POINT**

The Pump peak efficiency point (PEP) is very important for the determination of the value of the flow rate and the NPSH at which the pump performs most efficiently. With a change in flowrate, the head, power consumption, and efficiency of the pump change, as well. Plotting these quantities against the flowrate gives the pump characteristic curve. The PEP is the measure that shows at which point in the characteristic curve the pump performs most efficiently. Fig. 9. shows the PMT-4008 pump characteristic curve with the PEP.

![FIGURE 9. PMT-4008 pump characteristic curve.](image_url)

The efficiency was calculated after measuring the head, power, and flow using Eq. 5.

$$\eta = \frac{Q \rho g H}{P} \tag{5}$$

where $Q$ is the flowrate, $g$ is the gravity, $\rho$ is the density, $H$ is the total head, and $P$ is the power consumption.

After finding the PEP, the pump was operated at the PEP and a total of twenty PEP healthy samples of vibration signals were obtained.

2) **STEP 2: HEALTHY BASELINE SIGNAL SELECTION**

Selecting a healthy baseline signal randomly from the healthy samples of vibration signals collected at the pump PEP does not ensure the accuracy. After careful examination, we note that a signal among the PEP healthy samples of vibration signals obtained at the pump PEP, whose sample mean is near to the sample mean of the pump healthy vibration signals but farthermost from the sample mean of the other classes (mechanical seal hole, mechanical seal scratch, impeller fault), is selected as a healthy baseline signal. The healthy baseline signal obtained after this condition results in better accuracy while a random selection of a healthy baseline signal degrades the classification accuracy. It is to be noted that the pump healthy vibration signals are those samples which were collected from the pump under the normal operation of the pump. Fig. 10. shows the selected healthy baseline signal.

![FIGURE 10. Healthy baseline signal.](image_url)

**PHASE II: PREPROCESSING CP VIBRATION SIGNAL IN TIME DOMAIN AND DISCRIMINANT FEATURES EXTRACTION**

After selecting the healthy baseline signal, the healthy baseline signal is correlated with the CP vibration signals of different classes. The different classes of vibration signals collected from the CP are normal, mechanical seal hole fault, mechanical seal scratch fault, and impeller fault, as discussed in Section III. The cross-correlation between the healthy baseline signal and the CP vibration signals result in a correlogram which carries similarity information, as shown in Fig.11. Therefore, a new set of discriminant features are extracted from the correlogram. The features are peak correlogram value, instant of peak occurrence, correlogram value, and other statistical features.
centroide, correlogram equivalent width and correlogram mean square abscissa (MSA). The peak and the time-instant of the peak can be easily extracted from the correlogram. The other three features can be computed using Eqs. 6, 7 and 8:

Let the correlogram sequence be represented by $R(m)$.

Correlogram centroid

$$\text{Correlogram centroid} = \frac{\sum_{m=-M}^{M} mR(m)}{\sum_{m=-M}^{M} R(m)}$$

(6)

Equivalent width

$$\text{Equivalent width} = \frac{\text{Peak value of } R(m)}{\sum_{m=-M}^{M} mR(m)}$$

(7)

MSA

$$\text{MSA} = \frac{\sum_{m=-M}^{M} m^2R(m)}{\sum_{m=-M}^{M} R(m)}$$

(8)

**PHASE II: RAW STATISTICAL FEATURES PREPROCESSING FOR DISCRIMINANT FEATURES EXTRACTION**

After extracting discriminant features from the correlogram sequence, in this phase, raw statistical features obtained from the vibration signal in time, frequency, and the time-frequency domain are preprocessed based on similarity and discriminant information and are extracted from the raw features in each domain. Feature preprocessing is important because it helps in overcoming the likely effect of random impulses and fluctuations in the vibration signal. The steps involved in features preprocessing are as follows.

1) **STEP 1: RAW STATISTICAL FEATURES EXTRACTION IN THE TIME DOMAIN**

In this step, the time-domain raw statistical features are extracted from both the healthy baseline signal and CP vibration signals of different classes. The time domain statistical features adopted in this study are mentioned in [31]. The representative set of statistical features that are extracted from both the healthy baseline signal and CP vibration signals of different classes are the root amplitude, mean value, peak, root mean square, skewness, kurtosis value, crest factor, clearance factor, shape factor, and impulse factor. These statistical features are listed in Table. 2, along with the mathematical formulas.

2) **STEP 2: TIME-DOMAIN RAW STATISTICAL FEATURES PREPROCESSING AND DISCRIMINANT INFORMATION EXTRACTION**

After extracting time-domain features from both the healthy baseline and CP vibration signal of different classes, these features are combined into different vectors. These vectors are the healthy baseline features vector, CP healthy features vector, CP mechanical seal hole fault features vector, CP mechanical seal scratch fault features vector, and CP impeller fault features vector. The correlations between healthy baseline features and each CP feature vector are calculated using Eq. 9 and used as a new discriminant feature, as shown in Fig. 8.

$$r_{fg} = \frac{\sum_{j=1}^{k} (f_i - \bar{f})(g_i - \bar{g})}{\sqrt{\sum_{j=1}^{k} (f_i - \bar{f})^2 \cdot \sum_{j=1}^{k} (g_i - \bar{g})^2}}$$

(9)

Eq. 9, is the Pearson correlation coefficient equation, which inspects the correlation between two variables $f$ and $g$. In this equation $r_{fg}$ is the correlation between $f$ and $g$. After calculating the correlation coefficient between the healthy baseline features vector and CP feature vectors of different classes, $r_{fg}$ is used as a new feature for CP fault diagnosis.

3) **STEP 3: RAW STATISTICAL FEATURES EXTRACTION IN THE FREQUENCY DOMAIN**

A fault in the CP component adds a weak fault signature to the vibration signal of the CP that can be explored using the frequency spectrum. Fault symptoms identification in the frequency spectrum helps in the detection of faulty components.
TABLE 2. Set of statistical features in time-domain.

| Feature         | Equation                                                                 |
|-----------------|--------------------------------------------------------------------------|
| Mean            | $X_m = \frac{\sum_{n=1}^{N} x(n)}{N}$                                  |
| Root amplitude  | $X_{\text{root}} = \left(\frac{\sum_{n=1}^{N} |x(n)|}{N}\right)^2$     |
| Peak            | $X_{\text{peak}} = \max \{x(n)\}$                                      |
| Standard        | $X_{sd} = \sqrt{\frac{\sum_{n=1}^{N} (x(n)-X_m)^2}{N-1}}$               |
| Root mean square| $X_{\text{rms}} = \left(\frac{\sum_{n=1}^{N} (x(n))^2}{N}\right)^{1/2}$ |
| Skewness        | $X_{sk} = \frac{\sum_{n=1}^{N} (x(n)-X_m)^2}{(N-1)X_{sd}^2}$            |
| Kurtosis        | $X_{\text{kurtosis}} = \frac{\sum_{n=1}^{N} (x(n)-X_m)^4}{(N-1)X_{sd}^4}$ |
| Crest factor    | $X_{\text{crest}} = \frac{X_{\text{peak}}}{X_{\text{rms}}}$           |
| Clearance factor| $X_{\text{clearance}} = \frac{X_{\text{peak}}}{X_{\text{root}}}$      |
| Shape factor    | $X_{\text{shape}} = \frac{X_{\text{rms}}}{\left(\frac{1}{N} \sum_{n=1}^{N} |x(n)|\right)}$ |
| Impulse factor  | $X_{\text{impulse}} = \frac{1}{N} \sum_{n=1}^{N} X(n)$               |

Several experimental attempts have been made in the past for CP fault frequencies identification. However, mathematical proofs are not provided for such frequencies. Without proper mathematical equations, it is very hard to utilize the fault frequencies identification methods based on experimental results in industry, as well as in research.

Before extracting features from the frequency spectrum, in this study, the defect frequencies will first be theoretically calculated for the CP mechanical seal fault and impeller fault.

There are three sources of frequencies in machines. These sources are generated frequencies, excitation frequencies, and electronic frequencies. In this study, the generated and excitation frequencies are considered. The generated frequencies are the frequencies generated by the CP. In this study, concerned generated frequencies are imbalance. These frequencies can be easily explored in the spectrum if the speed and geometry of the machine is known.

For an impeller fault the source frequencies are the generated frequencies. whenever an impeller fault occurs in the CP, an impeller imbalance usually appears in the vibration signature [7], [47]. Eq. 10. shows the formulation for an impeller imbalance frequency.

$$IF = n \times Z$$

Excitation frequencies, also referred to as natural frequencies, are a property of the system. An excitation frequency is a single frequency present in the spectrum that represents amplified vibration of the system. When a CP is operated under a mechanical seal defect, this excitation frequency then represents the mechanical seal defect in the spectrum.

For a mechanical seal defect, the source frequency is the excitation frequency. It can be calculated from the theory of ‘vibration of a circular ring’, as described in [48].

Assume, that $r$ represents the radius of the centerline of the ring and $u$ shows the radial displacement and $A$ is the cross-sectional area of the ring.

In circumferential direction, the unit elongation of the ring is given by $\frac{u}{r}$. The potential energy of deformation is given by

$$PE = \frac{AEu^2}{2r^2} \times 2\pi r$$

(11)

In Eq.11, $E$ is the modulus of elasticity.

The kinetic energy of the vibration is given by,

$$KE = \left(\frac{\rho A}{2}\right) (u')^2 \times 2\pi r$$

(12)

In Eq.12, $\rho$ is the material density.

By applying the conservation of energy method,

$$\frac{d(PE + KE)}{dt} = 0$$

(13)

As a result, equation of motion will be,

$$\left(\frac{E}{\rho r^2}\right) u = 0$$

(14)

Eq.14. can be written as,

$$\left(\frac{E}{\rho r^2}\right) u = 0$$

(15)
where $\omega_n$ is the angular frequency. By solving Eq. 15, we can obtain the ring fundamental frequency,

$$f_r = \left(\frac{1}{2\pi r}\right) \sqrt{\frac{E}{\rho}} \tag{16}$$

As vibration is not random, there are proper modes of vibration.

In the case of a mechanical seal, the torsional vibration mode, or in-plane bending mode, can be defined as the vibration mode in which the centerline of the ring remains undeformed and all the cross sections rotate during vibration at the same angle. The natural frequency and its corresponding modes of vibration can be determined by Eq. 17.

$$f_0 = \left(\frac{2n (n^2 - 1)}{\pi}\right) \left(\frac{h}{d^2}\right) \frac{E}{\rho} \left(\frac{12n^2}{(12n^2 + 1)}\right) \left(\frac{2n^3(1+\nu)}{c}\right) \tag{17}$$

where $n = 1,2,3,4,5$ represent the modes of vibration, $h$ is ring cross-sectional height, $d$ is the diameter of the ring, $t$ is the ring cross-sectional thickness, $\nu$ is Poisson’s ratio and $c$ is the torsion constant in Eq.17.

For the mechanical seal, the flexural vibration can be defined by Eq. 18,

$$f_0 = \left(\frac{n (n^2 - 1)}{\pi d^2 \sqrt{n^2 + 1}}\right) \sqrt{\frac{E t^2}{3\rho}} \tag{18}$$

where $n = 1,2,3,4,5$ represent the modes of vibration, $d$ is the diameter of the ring, and $t$ is the ring cross-sectional thickness in Eq. 17.

The mechanical seal fundamental, in-plane and out-of-plane vibrations and their consecutive modes can be calculated using Eqs. 16, 17, and 18. It is noted that the fundamental and in-plane vibrations usually have high frequencies and much lower frequencies will be found if out-of-plane vibrations of the ring are considered [48].

Next, the mechanical seal fundamental, in-plane, and out-of-plane vibrations and their consecutive modes are calculated using Eqs. 16, 17, and 18. It can be seen from Fig. 13(a), Fig. 13(b), and Fig. 13(c), that the system excitation...
frequency appears in between the 2nd and 3rd out-of-plane modes of vibration, with almost twice the amplitude when the CP is operated under mechanical seal defect conditions.

As already mentioned, the CP faults can be explored via frequency spectrum analysis, as shown in Fig. 13 and 14. Raw statistical information can be extracted from the frequency domain, as it provides enough discriminant information. Therefore, in this phase, raw statistical frequency domain features are extracted from the healthy baseline signal and CP vibration signals of different classes. The raw statistical frequency domain features considered in this study are presented in Table 3.

4) STEP 4: FREQUENCY DOMAIN RAW STATISTICAL FEATURES PREPROCESSING AND DISCRIMINANT INFORMATION EXTRACTION

The next step follows the extraction of frequency domain features from the both the healthy baseline and CP vibration signals of different classes. Next, these features are combined into different vectors, namely, a healthy baseline frequency features vector, CP healthy frequency features vector, CP mechanical seal hole fault frequency features vector, CP mechanical seal scratch fault frequency features vector, and CP impeller fault frequency features vector. The correlations between the healthy baseline frequency features vector and each CP frequency features vector are calculated using Eq. 9 and used as a new discriminant feature, as shown in Fig. 8.

5) STEP 5: FEATURES EXTRACTION IN TIME-FREQUENCY DOMAIN

Existing methods based on the WPT for CP fault diagnosis consider the energy, standard deviation, and entropy as input features to the classification model. Among these features, wavelet packet energy is an intuitive approach for fault types classification. Each node in the WPT contains a great
deal of information about the energy variations and fault types in a specific node can be helpful in segregating fault types.

In this study, both the healthy baseline signal and CP vibration signals of different classes are decomposed up to \( k = 3 \) levels. This results in \( 2^k \) nodes. After decomposition, the WPT energy is calculated using Eq. 19.

\[
\text{Energy} = \left( \sum_{p=1}^{S} \sqrt{C_j(p)^2} \right) / S
\]

(19)

where \( S \) is the number of samples at the node, \( k \) is level of decomposition, nodes (frequency parameters) \( j \) at WPT coefficient \( c \) in Eq. 19 as explained in [35].

6) STEP 6: TIME-FREQUENCY DOMAIN FEATURES PREPROCESSING AND DISCRIMINANT INFORMATION EXTRACTION

The next step follows the extraction wavelet packet energy features from both the healthy baseline and CP vibration signals of different classes. These features are combined into different vectors, namely, a healthy baseline energy features vector, CP healthy energy features vector, CP mechanical seal hole fault energy features vector, CP mechanical seal scratch fault energy features vector, and CP impeller fault energy features vector. The correlations between healthy baseline energy features and each CP energy features vector are calculated using Eq. 9 and are used as a new discriminant feature, as shown in Fig. 8.

PHASE III: VULNERABLE FEATURE POOL CREATION

A vulnerable feature pool is formed by combining the extracted discriminant features: after preprocessing the vibration signal in the time domain, discriminant features are obtained after preprocessing raw statistical time-domain features, frequency-domain features, and after preprocessing WPT energy features. This feature pool is named vulnerable because the discriminant feature obtained after preprocessing the vibration signal and features are based on similarity. The more the feature or signal is like a healthy baseline feature or signal the less vulnerable. Similarly, the less the feature or signal is similar to the healthy baseline feature or signal the more vulnerable. The vulnerable feature pool provides detailed and particular information about the complex nonstationary and nonlinear signals obtained from the CP with multiple fault severities. The dimension of the vulnerable feature pool is \( 5 + 1 + 1 + 1 = 8 \). After constructing the vulnerable feature pool, it is provided as an input to the MSVM for CP fault segregation. This procedure is explained in the next section.

V. RESULTS AND DISCUSSION

The effectiveness of the proposed CP fault diagnosis method is presented in this section.

A. DATA CONFIGURATION FOR TRAINING AND TESTING

An appropriate dataset configuration for testing and training is very important in order to determine the comprehensive quality of the proposed CP diagnosis method. In this study, CP MFs were simulated. In total, 3 different faults were simulated in the CP, namely, a mechanical seal hole fault, mechanical seal scratch fault, and impeller fault. The fault severities vary from weak incipient faults to severe faults in the CP. A 300 sec long signal was acquired from the CP under each normal and faulty condition. Therefore, the created dataset is comprised of 1,200 signals in total. In this study, the features extracted from the dataset consist of \( CP_c \times CP_s \times CP_f \) features in total. Where \( CP_c \) is the CP conditions simulated in this paper, \( CP_s \) is the signal instances for each simulated condition, and \( CP_f \) is the total number of extracted features.

In this study, a k-fold cross-validation of \( k = 3 \) strategy was adopted for validating the proposed method during each experimental trail. In the k-fold cross-validation strategy, the whole dataset is divided randomly into k-folds, where each fold must be used once as a testing subset to a classifier trained on the remaining \( k - 1 \) subsets. In this study specifically, 200 randomly chosen samples from each class were used as a training subset and the remaining 100 samples from each class were used to construct the testing subset. Thus, in total, each training set contains 800 samples and each testing set contains 400 remaining samples for classification.

B. PERFORMANCE EVALUATION OF PROPOSED CP FAULT DIAGNOSIS METHOD

To evaluate the quality of the new features obtained from preprocessing the raw vibration signal and raw statistical features for CP fault diagnosis, this study compares the proposed method of feature extraction with two time-frequency domain feature extraction methods, one time-domain feature extraction method, and one hybrid feature extraction method. The first time-frequency domain method (WPT-PCA-MSVM) used a WPT for preprocessing the time-domain vibration signal and utilized Principal Component Analysis (PCA) to select the WPT bases for statistical feature extraction [5]. The second time-frequency domain method (WPT-BE-MSVM) used a WPT for preprocessing the time-domain vibration signal and utilized the best energy criteria to select the best bases for feature extraction [5]. In the third time-domain feature extraction method, statistical features are extracted from the vibration signal for CP fault diagnosis [9]. In the fourth method, hybrid features in time and frequency domain are extracted from the vibration signal for CP fault diagnosis [36]. In this study, the MSVM classifier is used to perform the comparison between the proposed method and the above existing methods. To ensure repeatability in the results and to overcome the effects of randomness, the experiments are performed 20 times with random combinations of testing and training data.
The classification accuracy for each class of samples is computed using Eq. 20.

$$TPR_m = \frac{1}{k} \sum_{j=1}^{k} \left( \frac{N_{j,m}^{TP}}{N_{TP}^{m} + N_{FN}^{m}} \right) \times 100(\%) \quad (20)$$

Eq.20. is the True Positive Rate index (TPR), where $k$ represents the number of cross-validation $k$ folds, $(N_{j,m}^{TP})$ is the number of samples in each class $m$ that are accurately segregated as class $m$, $N_{FN}^{m}$ is the number of samples in each class $m$ that are not accurately recognized as class $m$, $j$ indicates the iterations of the k-fold cross-validation. The final TPR is calculated for each class as an average of the TPR achieved after 20 trails.

The Classification Accuracy (CA) for each trail is calculated using Eq. 21.

$$CA = \frac{1}{k} \sum_{j=1}^{k} \left( \sum_{m=1}^{L} \frac{N_{j,m}^{TP}}{N_{samples}} \right) \times 100(\%) \quad (21)$$

In Eq.21, $L$ represents the total number of classes and $N_{samples}$ is the total number of samples in a specific testing subset. The final classification accuracy showed in the results is the Average Classification Accuracy (ACA) obtained after 20 trails.

The experimental results are presented in Table 4, Fig. 14 and Fig 15. The results reveal that the proposed correlation analysis based feature extraction method for CP fault diagnosis outperforms the existing methods in terms of the ACA, error rate (ER), precision with macro-averaging ($P_M$) and recall with macro-averaging ($R_M$) with an ACA of 98.4%, ER of 3%, $P_M$ of 98.4% and $R_M$ of 98.4%. ER shows the average per-class miss classification, the $P_M$ shows the average per-class agreement of the class labels with those of the classifiers and the $R_M$ shows the per class efficiency of classifiers for the identification of class labels [49]. Table 4 also reflects that the average TPR values of the proposed method are over 95% for each class. The results can be explained as follows. Multiple faults with different levels of severity caused random fluctuations and impulses in the vibration signal. These random fluctuations and impulses in the vibration signal make the time or frequency domain analysis ineffective for such kinds of vibration signals. However, preprocessing the vibration signal can overcome the effect of random fluctuations and impulses in the vibration signal. On the other hand, raw statistical features obtained from the time and frequency domain are either not very sensitive to weak incipient faults or unsuitable for more severe faults and may result in less discriminate information. To overcome this issue, a proper preprocessing of raw statistical features is required, which can result in more discriminating information. This can be seen from results that are based on correlation preprocessing of the vibration signal as well as the hybrid features, which taken together results in discriminant features. Therefore, the proposed method outperforms the reference methods in terms of the ACA, $P_M$ and $R_M$ for CP fault diagnosis. The underperforming reference methods for CP fault diagnosis result in ACAs of 96.3%, 94%, 81.1% and 75.22%, ER of 7.5%, 10.5%, 25.4% and 29.4%, $P_M$ of 95.6%, 93.8%, 79.8% and 75.1% and $R_M$.

**TABLE 4. Experimental results. comparisons between the proposed method and reference methods (true positive rate(TPR), average classification accuracy (ACA)).**

| Methods         | Normal Condition | Mechanical seal defect (hole) | Mechanical seal defect (scratch) | Impeller fault | ACA (%) |
|-----------------|------------------|------------------------------|----------------------------------|----------------|---------|
| Proposed        | 100              | 96.2                         | 98.9                             | 98.4           | 98.4    |
| WPT-PCA-MSVM    | 100              | 97.72                        | 98.8                             | 88.6           | 96.3    |
| WPT-BE-MSVM     | 100              | 91.2                         | 90.2                             | 94.5           | 94      |
| Rapur et al. [9]| 68.9             | 83.6                         | 91.5                             | 80.4           | 81.1    |
| Nasiri et al [36]| 82.1             | 68.3                         | 70.5                             | 79.7           | 75.22   |

![FIGURE 15. Evaluation of proposed method and reference methods for CP fault diagnosis.](image)
the average TPR of the reference method is slightly less than that of the proposed method in the case of impeller defect.

Rapuri and Tiwari [9], extract time-domain statistical features for CP fault diagnosis using SVMs. After extracting the same time-domain features and repeating the analysis with our experimental data, we obtained an ACA of 81.1%, $P_M$ of 79.8% and $R_M$ of 81.1, which is less than the ACA of 98.4%, $P_M$ of 98.4% and $R_M$ of 98.4% achieved by our proposed method. This is because the raw vibration signal obtained for the CP contains random fluctuations caused by the fault. The features obtained from the raw vibration signal without preprocessing the raw vibration signal result in less discriminant information, which can be seen in Table 4 and Fig. 14(a) and (d).

Regarding Nasiri et al. [36], for cavitation detection in CP, he extracted two features in time and two features in the frequency domain from the vibration signal. The hybrid feature pool is used as an input to the neural network for the detection of cavitation in the CP. To make the comparison fair we used the MSVM for classification instead of a neural network. After using his feature extraction method, we obtained ACA of 75.22%, $P_M$ of 75.1% and $R_M$ of 75.1% which is less than the ACA of 98.4%, $P_M$ of 98.4% and $R_M$ of 98.4% obtained by our proposed method. This is because, the dimension of the feature vector is very small, and the features are not sufficiently discriminant. The miss classification of [36] can be seen from Fig 14(e). Although he used frequency domain features, the frequency harmonics of CP MFs show only a minute change in the amplitude from the healthy signal, as shown in Fig. 12. This method cannot be used for classification when it uses only two statistical features. Furthermore, the ER of the proposed method is less than that of the reference methods as can be seen from Fig. 15.

The MFs in the CP can result in to two main kinds of failure phenomena’s namely hard failure and soft failure. Hard failure can be detected by simple analysis of the CP however soft failure causes CP performance degradation, but the CP remains in function [50]. MFs such as mechanical seal hole, scratch and impeller crack may result in soft failures of the CP. Soft failure in CP are not obvious enough to be diagnosed without a well-designed diagnosis technique. Our proposed method will help the decision makers to address these soft failures. Thus, after detecting and classifying the fault by our proposed method, the decision maker will only replace that specific component in the CP and bring the CP back to operation. Through this way the CP will remain healthy, take less time and minimum cost for maintenance. It is highly recommended for the decision makers to follow the guidelines provided by the pump manufacturers for replacing components in the CP. After replacing the components in CP, the net positive suction head and discharge head of the CP must be compared with the one provided by the manufacturers.

Overall, the proposed method of discriminant feature extraction is very useful for the diagnosis of CP faults with varying severities. The effectiveness is explained through the proposed method’s main idea: preprocessing the vibration
signal and raw hybrid statistical features based on their correlation/similarity. The proposed method is very easy to implement with less computational complexity. These properties of the proposed method make it worthy for industrial purposes.

VI. CONCLUSION

This paper proposed a new discriminant feature extraction method for CP fault diagnosis based on correlations. The proposed method is divided into three phases. In the first phase, healthy baseline signals were selected. In the second phase, vibration signals are preprocessed in the time domain and a set of new features are extracted from the preprocessed vibration signal. In the third phase, raw statistical features are preprocessed by calculating the correlation coefficients between the healthy baseline signal features and the CP raw statistical features. Each correlation coefficient results in a similarity measure. This similarity measure is discriminant and is used as a new feature for CP fault diagnosis. After extracting the features, the proposed method combines all of the features into a single feature vector for each class and creates a vulnerable feature pool. In the experimental part of this study, the vulnerable feature pool was used to segregate different CP MF’s using the MSVM classifier. The experimental results show that the proposed method of the new discriminant feature extraction outperforms state-of-the-art reference methods with an ACA of 98.4%.

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Z. Ahmad et al.: Discriminant Feature Extraction for CP Fault Diagnosis

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