Quantitative assessment of breast density using transmission ultrasound tomography

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Purpose: Breast density is important in the evaluation of breast cancer risk. At present, breast density is evaluated using two-dimensional projections from mammography with or without tomosynthesis using either (a) subjective assessment or (b) a computer-aided approach. The purpose of this work is twofold: (a) to establish an algorithm for quantitative assessment of breast density using quantitative three-dimensional transmission ultrasound imaging; and (b) to determine how these quantitative assessments compare with both subjective and objective mammographic assessments of breast density.

Methods: We described and verified a threshold-based segmentation algorithm to give a quantitative breast density (QBD) on ultrasound tomography images of phantoms of known geometric forms. We also used the algorithm and transmission ultrasound tomography to quantitatively determine breast density by separating fibroglandular tissue from fat and skin, based on imaged, quantitative tissue characteristics, and compared the quantitative tomography segmentation results with subjective and objective mammographic assessments.

Results: Quantitative breast density (QBD) measured in phantoms demonstrates high quantitative accuracy with respect to geometric volumes with average difference of less than 0.1% of the total phantom volumes. There is a strong correlation between QBD and both subjective mammographic assessments of Breast Imaging - Reporting and Data System (BI-RADS) breast composition categories and Volpara density scores — the Spearman correlation coefficients for the two comparisons were calculated to be 0.90 (95% CI: 0.71–0.96) and 0.96 (95% CI: 0.92–0.98), respectively.

Conclusions: The calculation of breast density using ultrasound tomography and the described segmentation algorithm is quantitatively accurate in phantoms and highly correlated with both subjective and Food and Drug Administration (FDA)-cleared objective assessments of breast density.

Key words: breast density, image segmentation, medical imaging, transmission ultrasound, ultrasound tomography

1. INTRODUCTION

Dense breast tissue is an independent predictor of increased breast cancer risk.1–3 Women demonstrate a natural continuum of breast density, and the presence of dense fibroglandular breast tissue is estimated to increase the risk of breast cancer by four- to sixfold.4,5 The only factors associated with greater increases in breast cancer risk are age and certain genetic mutations, such as those in the BRCA genes.6–9 In this era of precision medicine, risk models for screening based on breast density have increasingly been proposed as an alternative to risk models based on age.10–12 For risk-based screening using breast density to be effective, the methods to assess breast density must be reliable, robust, accessible, and consistent.

Breast density refers to the percentage of breast tissue that is relatively opaque to mammography.13 The fourth edition of the Breast Imaging-Reporting and Data System (BI-RADS) developed by the American College of Radiology and published in 2003 incorporated a quantitative component of density percentages to the four quartile breast density categories. More recently, the fifth edition of BI-RADS published in 2013 removed the quantitative component and instead pushed forth ordinal categories (A, B, C, and D) with more emphasis placed on the masking effects of the dense tissues. The overall result has been a shift toward higher density assessments for all women.14 Following publication of the fifth edition of BIRADS, it has also been demonstrated in the literature that the use of categorical mammographic density scales rather than continuous percent mammographic density measures results in a significant loss of information. For example, the use of a categorical scale can force very different clinical decisions based on an arbitrary category cut-off that may not be clinically relevant or meaningful. The more precise continuous density measures have been shown to better capture the density–risk relationship, resulting in more personalized and accurate risk assessments.15

There is currently no gold standard method to accurately estimate breast density. Currently utilized methods range from (a) qualitative to quantitative and from (b) visual to fully automated. The vast majority of subjective and automated assessments of breast density rely on two-dimensional (2D)
images. These 2D images are derived from either 2D mammographic images or synthesized from three-dimensional (3D) digital breast tomosynthesis (DBT). The challenge with using 2D mammographic images or 2D synthesized mammographic images as a means to assess breast density is that the 3D heterogeneity of fibroglandular breast tissue is not captured. Additionally, challenges exist with the subjective assessment of breast density, as multiple studies have demonstrated significant inter- and intra-reader variability.\textsuperscript{16,17}

Transmission ultrasound imaging is an emerging technology that has a long history\textsuperscript{18–29} that provides a 3D representation of tissue characteristics. The purpose of the work described in this paper was twofold: (a) to establish an algorithm for quantitative assessment of breast density using full-wave 3D transmission ultrasound imaging\textsuperscript{28} and (b) to determine how these quantitative assessments relate to both subjective mammographic assessments of BI-RADS breast composition categories and objective measures provided by FDA-cleared VolparaDensity software. We believe that the high resolution and quantitative accuracy of full-wave 3D inverse scattering ultrasound tomography\textsuperscript{28} should improve the accuracy of estimates of breast density.

2. MATERIALS AND METHODS

2.A. Transmission ultrasound scanning of the breast

All scans were performed on a multimodality transmission and reflection ultrasound imaging system (QT Ultrasound, LLC, Novato, CA; Fig. 1). The scanner consists of a water bath in which the breast (or phantom) is immersed, a transmitter and receiver array set for transmission imaging, and three reflection arrays for reflection imaging. This is an investigational use of this device. The scanner and the imaging algorithms have been fully described in previous literature.\textsuperscript{29–31}

2.B. Segmentation algorithm

In contrast to other manual segmentation techniques, we segment using a fully automated approach. The algorithm for automatic quantitative breast density (QBD) measurement performs the following steps in sequence:

1. Segmentation of the whole breast from surrounding water.
2. Segmentation of the relatively high-speed breast tissue from the total breast tissue volume.
3. Segmentation and removal of the skin from the high-speed breast tissue.
4. Calculation of the breast density as a ratio of high-speed breast tissue volume to the total breast tissue volume. The final output is expressed as a percentage (QBD value).

The details of segmentation of high-speed breast tissue from skin and fat are as follows:

1. The attenuation image information is used to determine the breast volume. For each 1 mm vertical level (moving from the nipple to the chest wall):
   a. From the border of the image space, the algorithm moves inward horizontally until pixels with nonzero attenuation are encountered. It is assumed that the breast has nonzero attenuation whereas the attenuation of the water bath can be considered zero.
   b. From the surface of the breast (i.e., the point at which the attenuation changes from zero to nonzero) to the midpoint of the image space, the pixels are labeled “breast tissue.” It is assumed that everything from the surface of the breast to the center of the breast is breast tissue.
   c. To account for the vertical convexity of the breast, the algorithm moves upward until pixels with nonzero attenuation are encountered. From these pixels onward, the pixels are labeled “breast tissue.”
   d. Pixels labeled “breast tissue” that are close to the border between the breast tissue and the water bath are labeled “border pixels.”

2. The speed of sound image is then segmented on the basis of speed and the pixel information from the attenuation segmentation carried out above. This is valid since the speed of sound image is coregistered with the attenuation image. This yields the separation of fibroglandular tissue and skin from fat. Fibroglandular tissue and skin are segmented together from the total breast tissue volume since they both have higher speed of sound (>1510 m/s) than that of fat (<1480 m/s).

3. In the last step, the skin is segmented and removed by exclusion of the border pixels as defined in step 1(d).

In the above algorithm, attenuation is used initially because attenuation in water is almost zero, whereas it is approximately two to three orders of magnitude larger in breast tissue. The speed of sound (SOS) and reflection images were also used to constrain the total breast volume based on \textit{a priori} known SOS of skin and lack of reflecting objects in water. The reflection image gives an accurate delineation of the skin. Note, however, that the segmentation of
the SOS is critical for distinguishing fibroglandular tissue. This requires high-resolution speed images that are obtained by modeling refraction and diffraction effects in 3D, which are required to avoid artifacts and volume averaging effects.\(^{28}\) Presently, we used a SOS of 1489 m/s as a threshold to distinguish fibroglandular from fat tissue. This was a universal value used for all image sets in this study, since the quantitative values for the SOS at each voxel should be independent of the breast type, and only dependent on the tissue type at that voxel.\(^{32}\) This multistep automatic method utilizes the information from both the attenuation and the speed of sound images in an intelligent manner specifically adapted to the breast and yields segmented speed of sound and attenuation images. The algorithm is summarized in Fig. 2.

### 2.C. Phantom studies

The algorithm was tested on multiple phantoms, the first and simplest of which was a cylindrical polyurethane phantom with cylindrical inclusions (Metropolis Design and Prototyping, North Salt Lake, UT). It consisted of an outer cylinder of polyurethane 40.5 mm wide with two cylindrical holes, each 9.25 mm in diameter, and a third cylindrical hole, 7.2 mm in diameter (Fig. 3). The outer cylinder background SOS is 1440 m/s, with attenuation 0.9 dB/cm. One of the cylindrical holes was filled with a high speed plug (1540 m/s, attenuation 1.6 dB/cm), the second larger hole and the smaller hole were filled with background material, so that only one cylindrical hole was segmented out as in Fig. 6.

The algorithm was also tested on a cylindrical polyurethane phantom, three inches tall and three inches in diameter, with spherical inclusions (Fig. 4). The spherical inclusions had a SOS of 1560 m/s and attenuation 1.6 dB/cm. The background cylinder had a SOS of 1470 m/s, and attenuation 0.9 dB/cm. The spherical inclusions were constructed to be 1 cm in diameter, and the dimensions were verified with a caliper. The volume of these spheres was measured (a) by direct calculation using the formula for the volume of a sphere and (b) by volume displacement in a graduated cylinder filled with water. The graduated cylinder was filled to 4 cc. Addition of six spheres to the water raised the volume to 7.20 cc; thus, the estimated volume of each sphere was 3.20 cc/6 = 0.53 cc. This agrees well with the volume calculated using the formula \(V = \frac{4}{3}\pi r^3\), which gave \(V = 0.52\) cc, for a sphere of radius 0.50 cm.

The algorithm was also tested on a calibration phantom consisting of a polyurethane cylinder 60 mm tall and 80 mm in diameter containing four 8-mm-diameter water-filled holes, four 15-mm-diameter spheres, two 1-mm-diameter rods, and two 5-mm-diameter rods (Fig. 5) Half of the spheres and half of the rods were made of high-speed material: 1540 m/s speed of sound and 1.7 dB/cm attenuation at 1.3 MHz. The remaining inclusions had a SOS of 1440 m/s and 0.9 dB/cm attenuation. The background material had a SOS of 1480 m/s and attenuation of 0.9 dB/cm. A calculation based on the geometry of the phantom and standard formulas for the volumes of spheres and cylinders indicates that high speed material corresponding to fibroglandular tissue accounts for 18.70% of the breast volume.

### 2.D. Correlation of QBD with BIRADS and Volpara density scores

The clinical feasibility of the algorithm was first tested by applying the algorithm to transmission ultrasound images from 17 volunteers. QBD values calculated by the algorithm were compared to BI-RADS\(^{33}\) breast composition categories assigned by four board-certified breast radiologists following review of the corresponding two-view mammograms. The radiologists were blinded to the QBD scores.

To compare the QBD values with the BI-RADS breast composition categories,\(^{34}\) it was necessary to convert the BI-RADS mammographic composition categories to breast density (BD) scores. We therefore used the values in Table I. These values are subjective\(^{17}\) estimates, but are used consistently, to quantify the BIRADS score. We also compared and correlated the QBD values with quantitative density scores provided by VolparaDensity\(^{35}\) software, for a cohort of 25 volunteers. We opted to assess the correlation with the Spearman \(\rho\), since we do not know \(a\ priors\), that the relationship between QBD and Volpara is linear.
3. RESULTS

3.A. Verification with phantoms

The results of segmentation for the cylindrical phantom with cylindrical inclusions are shown in Fig. 6. The density value based on geometry was 3.96%, whereas the QBD value was 4.09%. The results are summarized in Table II.

The results of segmentation for the cylindrical phantom with spherical inclusions are shown in Fig. 7. The density value based on geometry was 0.92%, whereas the QBD value was 1.00% (Table II).

The total volume of the phantom was calculated as 347.50 cubic centimeters (cc). The spheres had a total volume of $6.53 \text{ cc}$. The ratio $(6.53)/347.50$ gives 0.92%.

For the calibration phantom (Fig. 5), the density value based on geometry was 18.70% in comparison to the QBD value which was 18.66%. The corresponding image set is shown in Fig. 8 (along with a supplementary media file showing 3D segmentation of the relatively high-speed regions within the phantom).

See also Video, Supplemental Digital Content 1, which shows a rotating segmentation of the calibration phantom showing the high-speed rods and spheres segmented out from the entire phantom. This shows the high resolution of our method and avoidance of 2D artifacts. There has been a great deal of research toward ultrasound tomography. However, these methods generally rely on 2D (not 3D) full-wave methods or ray-based forward models in the

![Fig. 3. Photograph (left) and schematic (right) of the cylindrical phantom with cylindrical inclusions. On the schematic, the label Ø symbol indicates diameter (not radius) of the associated holes. All measurements are in millimeters. [Color figure can be viewed at wileyonlinelibrary.com]](image1)

![Fig. 4. Photographs of (a) polyurethane phantom with spherical inclusions (left) and (b) isolated spherical inclusions (right). [Color figure can be viewed at wileyonlinelibrary.com]](image2)

![Fig. 5. Isometric (left) and planar (right) views of the calibration phantom. On the planar view, the label Ø indicates diameter and THRU indicates through holes. There are four (4 × ) through holes in the phantom which are filled with water upon placement of the phantom in water. All dimensions are in millimeters.](image3)

![Table I. Conversion of BI-RADS breast density categories to quantitative scores.](image4)

| BI-RADS category | BD score |
|------------------|----------|
| a                | 6.0      |
| b                | 14.8     |
| c                | 51.2     |
| d                | 78.4     |

![Fig. 6. Segmented transmission ultrasound images (coronal and axial views) of the cylindrical phantom with cylindrical inclusions for geometric comparison. Top row: segmented total volume, middle row shows segmented peripheral capsule and internal cylinder. Bottom row: segmented internal cylinder without the peripheral capsule (representing skin). Quantitative breast density score is volume in bottom row divided by volume in top row.](image5)
inversions. Thus, they may have 2D artifacts or lower resolution, which may affect the segmentation process adversely.

### 3.B. Verification on volunteers

A typical automatically generated result from a clinical volunteer subject is shown in Fig. 9. First, a comparison of the speed of sound image (top row) with the segmented image (middle row) shows a clear correlation. Second, the bottom row shows that the “skin removing” part of the algorithm effectively removes the tissue corresponding to skin.

There was high correlation between the QBD values and the categorical BIRADS breast density scores (Fig. 10). There was also high correlation between QBD and scores determined by Volpara, as shown in Fig. 11 which shows the scatter plot of QBD values against Volpara density scores for a sample size of 25. The nonparametric Spearman coefficient for this correlation was $r = 0.96$ (95% CI: 0.92–0.98, $P < 0.0001$). The correlation equation is $y = 0.52x - 0.023$.

Figures 12–14 show application of the QBD algorithm to three different classes of breast densities: a fatty breast with QBD of 10.9%, a heterogeneously dense breast with QBD of 29.5%, and a very dense breast with QBD of 62.5%. Taken together, these figures show the effectiveness of the QBD algorithm on a variety of breast densities. We emphasize that these SOS images are the standard images that come from the scanner. The attenuation and reflection images are not shown since they are used only to accurately determine the breast volume, which is clearly seen in the images. We note that Case 2 in Fig. 10 is an outlier which we believe indicates the coarseness of the BIRADS composition score. Note that the SOS threshold value chosen in the segmentation is consistent for all image sets. One value is used for all breasts, since our image is a high-resolution 3D map of intrinsic tissue characteristics, independent of the scanner. This value (1489 m/s) was determined empirically. Further studies are ongoing to optimize this threshold value.

The algorithm uses the attenuation image as well as the speed of sound image. The attenuation and reflection images are used only to determine the whole breast volume and so are not shown. Once the breast volume is isolated, we use the quantitative estimate of the tissue SOS at each particular voxel for the critical segmentation operation to distinguish between fibroglandular and other tissue. This operation requires lack of artifacts and high resolution which requires modeling and reconstruction incorporating both refraction and diffraction effects in full 3D. The voxels are 0.4 mm $\times$ 0.4 mm $\times$ 1 mm in size and the image space is 531 $\times$ 531 pixels in the coronal view of the breast. The vertical extent of the image space varies with the size of the breast, with each level representing a 1-mm-thick slice.

### Table II. High speed material as a proportion of phantom volume: QBD value vs geometry-based value.

| Phantom                        | QBD value, % | Geometry-based value, % |
|-------------------------------|--------------|-------------------------|
| Cylindrical phantom with cylindrical inclusions | 4.09         | 3.96                    |
| Cylindrical phantom with spherical inclusions | 1.00         | 0.92                    |
| Calibration phantom (with rods and spheres) | 18.66        | 18.70                   |

**Fig. 7.** Top row, speed of sound images of the cylindrical phantom with spherical inclusions; Bottom row, high-speed spheres segmented out.

**Fig. 8.** Quantitative breast density segmentation algorithm applied to calibration phantom; (left) speed of sound image, (middle) segmented peripheral capsule and high-speed spheres and rods. The segmentation is based on speed of sound > 1489 m/s.
See Video S2, which shows the rotating fibroglandular tissue of a human breast segmented out based on the present algorithm and SOS, attenuation, and reflection values. Part of the skin is shown for perspective, and a subcutaneous vein is visible.

Finally, we also demonstrate that there is a psychovisual tendency to overestimate 3D volumes from projections. This disparity is particularly relevant in the case of solid objects with convex or concave margins. As seen in Fig. 15, the light gray 3D object appears to cover almost 50% of the cross-sectional area. This is approximately true independent of the azimuthal view. However, it can be shown through geometric considerations that the fraction of the volume of the cube occupied by the light gray volume is given by Eq. (1), where \( d/a \) is the ratio of the width, \( d \), of the light gray cross to the

![Fig. 9. Steps in the quantitative breast density algorithm: Top row, speed of sound images. Middle row, breast separated from the water bath with skin and fibroglandular tissue segmented from the total breast tissue volume. Bottom row, remaining fibroglandular tissue following the segmentation and removal of skin. The segmentation is based on speed of sound > 1489 m/s.](image)

![Fig. 10. Comparison of quantitative breast density (QBD) values and BI-RADS-based subjective breast density scores. The vertical axis is the percentage of total breast volume that is fibroglandular tissue — either the QBD value or the subjective value assigned to BI-RADS composition categories. [Color figure can be viewed at wileyonlinelibrary.com](image)

![Fig. 11. Comparison of quantitative breast density and Volpara density scores. The Spearman rank correlation \( r \) is 0.96](image)
length of the side of the cube, \( a \), and \( h \) is the height of the light gray region above the bottom of the cube.

\[
f = \frac{d}{a} \left( 1 - \frac{h}{a} \right) \quad (1)
\]

\[
d/a = h/a = 1/7 \quad (2)
\]

Hence, for the case shown in Fig. 15, (where \( d/a = h/a = 1/7 \)), the volume fraction is only \( \sim 12\% \), whereas a projection from any side view would imply a much larger volume fraction of \( \sim 49\% \) (ratio of the area of the light gray region to the square on the right panel of Fig. 15).

4. DISCUSSION

We observed that the QBD algorithm was quantitatively accurate for simple phantoms with both 2D (cylindrical) and true 3D (spherical) inclusions. Specifically, we verified the quantitative accuracy of the QBD algorithm against theoretically calculated values. This establishes the importance and accuracy of the high resolution and quantitative accuracy of the segmentation. We note that some research groups have skipped this important first step — validation. In the clinical setting, upon evaluation of images from volunteer subjects, the fibroglandular tissue volume segmented by the QBD algorithm showed high visual correlation with the speed of sound image.

There is known 3D heterogeneity within fibroglandular breast tissue, which we refer to as topological diversity. The key point in this analysis is that the fibroglandular tissue is nonconvex and contains voids. Consequently, two 2D projections as in mammography can misrepresent the true 3D
Our QBD algorithm, when used in conjunction with quantitative transmission ultrasound tomography, is accurate regardless of the 3D heterogeneity in the fibroglandular breast tissue. We also note that our images are unique in their high resolution, reduction of 2D artifact, and reduction of “volume averaging” which may affect any segmentation yielding a QBD score. Sak et al. obtained a Spearman correlation coefficient of 0.568 between k-means segmented and 0.715 between threshold segmented volumes based on ultrasound tomography and mammographic breast density. Our comparison yielded a correlation of 0.96 and the value appears to remain high over larger cohorts, as future publications will establish. It may be that the value differs due to differences in the SOS images used in the segmentation. Our 3D algorithm (utilizing diffraction) appears to avoid some artifacts and volume averaging that may arise with 2D reconstruction algorithms, especially if the model is based on refraction only, as in the case of ray-based inversions. Note that Sak et al. observed better correlation when segmentation was based on thresholding (which we use here) rather than k-means clustering. This may be because transmission ultrasound tomography yields characteristic estimates of the tissue itself, independent of the imaging system and surrounding tissue.

In consideration of frequently used imaging modalities in breast imaging, it becomes clear that 3D techniques are advantageous over 2D methods. Kopans has argued with respect to breast density determination: “Future investigations need to use 3D information,” and that “Radiologists can guesstimate the percentage of breast tissue that is dense, but they are still using 2D information to assess a 3D phenomenon.” To this end, volumetric measurement of breast density from intrinsically 3D imaging modalities is considered more accurate due to their scientific validity. Recently, 3D-segmented magnetic resonance (MR) images have been used to assess breast density and appear to be robust to positioning issues and give reproducible results. However, MR imaging is relatively costly and requires specialized expertise to run and operate.

More recently developed breast imaging modalities such as breast computed tomography (CT) have the advantage of being intrinsically volumetric. Vedantham has analyzed the use of dedicated breast CT to determine the mean and range of “volumetric glandular fraction” in a related context. They carried out a validation step and observed that their algorithm was accurate to within ±1.9% in determining the volume of an irregular shaped phantom. The calculation of breast density via automated breast ultrasound (ABUS) images has also been correlated with MR imaging (MRI) — Chen et al. found a correlation ($R^2 = 0.825$) for breast percent density (similar to our QBD), as measured with ABUS vs MRI, which are both volumetric measures.
Digital breast tomosynthesis (DBT) also provides a 3D image stack. Breast densities from DBT, MRI, and digital mammography (DM — a 2D image) were pairwise correlated in Moon et al. They indicated some correlation between breast volumes for all three modalities. However, the correlation between the estimate of breast density from DBT and DM (R = 0.789) was substantially higher than that between DBT and MRI (R = 0.482), which was the same as the correlation between DM and MRI (R = 0.482).

Prior to the work in this paper, ultrasound tomography had been explored as well for assessment of breast density although some of these methods provide a surrogate for QBD and not a direct percentage measure. Initial work using ultrasound tomography utilized images made from 2D-based algorithms, wherein 2D images are concatenated together to yield 3D images. O’Flynn et al., Glide, and Duric et al. calculated volume-averaged SOS (VASS) derived from ray-based ultrasound tomography as a means to ascertain breast density. Similarly, Sak et al. used median and mean values of the SOS image and correlated with mammographic breast density as determined by Cumulus software. However, their ray-based methods account for refraction, but not diffraction wave phenomena. Consequently, their images would be potentially subject to volume averaging resulting in lower quantitative accuracy.

Glide-Hurst et al. used a volumetric ultrasound percent density (UPD) as determined by segmenting high sound speed areas from each image slice using a k-means clustering routine and integrating these results over all the slices of the breast. Hence, their comparison of the phantom was based on integrated areas, whereas ours was based on a segmented volume. They observed a moderate Spearman correlation of 0.69 between the BI-RADS assessment of composition and UPD. However, their segmentation was semi-automatic and carried out slice by slice, which is appropriate, since their ultrasound tomograms were reconstructed in the same manner. In particular, they manually determined the first and last levels, which bound the segmented slices. Similarly, the segmentation methods utilized by O’Flynn on the ultrasound tomography images were not automatic — the posterior and anterior limiting levels were chosen manually. In our algorithm, the segmentation was totally automatic to prevent bias across multiple breasts. This characteristic is important to insure lack of bias and consistency in the proposed QBD score. Also, the segmentation threshold we chose is empirical, but universal for all breasts. We can do this because our image gives the intrinsic tissue characteristics of a particular voxel. Ours is a model-based inversion of the governing partial differential equation and thus is independent of the data collection apparatus (up to noise and numerical conditioning considerations). The VASS (SOS) images in O’Flynn show volume averaging in comparison to the images shown here. The VASS score will, in part, compensate for the volume averaging. However, the segmentation contained here geometrically isolates the fibroglandular tissue from other breast tissue, which is not only more intuitively appealing but also opens the possibility to understand more completely, why dense breasts are a cancer risk factor.

It is noted in literature that Volpara and Quantra tend to underestimate mammographic density. This also corroborates our findings. This can be attributed to the fact that although the Highnam equation and similar formulas are useful to estimate the total thickness of the fibroglandular tissue, it is an ill-conditioned inversion problem and highly susceptible to noise. The presence of multiple voids in the fibroglandular tissue can be difficult to account for when estimating density from projection images. These limitations can affect all automated breast density methods. However, Volpara seems to provide a better correlation with visual assessment of breast density as noted by Duffy et al. who analyzed both Volpara and Quantra software, which helps to justify our choice of comparison in this research. Vinnicombe also prefers Volpara to Cumulus.

Our results on volunteers demonstrate a correlation between the BI-RADS breast composition category assigned by the board-certified breast radiologists and the QBD value. In addition, our images indicate that the QBD value is geometrically accurate across a range of breast densities. We also demonstrated a significant correlation (Spearman r = 0.96) with Volpara density scores derived from VolparaDensity software which FDA cleared to provide both volumetric breast density measurements and a breast density category. The volume fraction of physiologically “dense” tissue is an intuitively appealing score to use. We established here the accuracy of the segmentation with known phantoms (validation) and showed statistical correlation with FDA-approved breast density estimation methods with small cohorts. This essential first step will be followed with future research using the quantitative nature of our images to facilitate further differentiation of glandular from connective tissue, and utilization of larger cohorts and MR images to further substantiate the correlation observed here.

In conclusion, this work demonstrates that the QBD algorithm has promise as a viable method to accurately and consistently quantify breast density. Additional work is required to further define the utility of the QBD algorithm in a clinical setting.

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CONFLICTS OF INTEREST

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**SUPPORTING INFORMATION**

Additional supporting information may be found online in the Supporting Information section at the end of the article.

**Video S1:** Video which shows a rotating segmentation of the calibration phantom showing the high-speed rods and spheres segmented out from the entire phantom. mp4

**Video S2:** Video that shows a rotating segmentation of the fibroglandular tissue of a human breast. Wmv