Study on the Corrosion Resistance of 39SiCrVTiA High strength and high toughness spring steel

Lun Nie1, *, Min Zhu 2, Shirun Tu 1, Kefeng Yuan 1, Kexin Lu 1
1 Zhejiang Meili High Technology Co., Ltd, Xinchang 312500, China
2 School of Mechanical Engineering & Automation, Zhejiang Sci-Tech University, Hangzhou 310018, China

Abstract. 39SiCrVTiA spring steel is heat-treated and compared with the existing high-strength spring steels 60Si2CrVA and SAE9254 for electrochemical impedance spectroscopy (EIS), polarization curve and slow strain rate testing (SSRT). The test results of electrochemical impedance spectroscopy (EIS), polarization curve show that the corrosion resistance of 60Si2CrVA was the best, followed by that of SAE9254 and 39SiCrVTiA. However, the test results of the SSRT test show that the three spring steels in 5% NaCl solution possess high SCC susceptibility. The SCC susceptibility of 39SiCrVTiA steel is slightly lower and the stress corrosion ability is better than the other two steels which may be related to its containing Ti, V elements and lower carbon content.

Keywords: 39SiCrVTiA, heat-treated, electrochemical impedance spectroscopy (EIS)

1 Introduction

High strength spring steel is widely used in railway, automobile, engineering machinery and other machinery manufacturing[1]. This kind of spring steel, has been implemented in the high-stress design, such as the spiral spring for automobile suspension, but the further improving the strength index of steel has been greatly restricted. With the increase of spring stress, the sensitivity of spring steel to corrosion has increased rapidly, and the problem of corrosion fatigue failure during the process has attracted attention. Therefore, higher strength and better corrosion fatigue resistance will become the main research direction of new spring materials.

According to the current high-performance, high-reliability and lightweight development trends of various types of mechanical devices, this paper develops alloy spring steel with high strength, high toughness and good corrosion resistance. In the research and development of the current high-end spring products such as automotive and rail transit damping spring and stabilizer rod, the latest concept requirements of performance are put forward, enhancing the strength and toughness of the material at the same time pay attention to improve the spring material corrosion resistance to meet the needs of high reliability and lightweight mechanical products. At present, 55SiCrA and 60Si2CrVA are used as spring steels. The 55SiCrA steel has unstable strength and poor corrosion resistance, while the 60Si2CrVA steel has the characteristics of high strength but insufficient plastic toughness, hydrogen embrittlement resistance and corrosion fatigue resistance. Therefore, the research and development of spring steel with high strength, high toughness and corrosion resistance has important practical engineering significance and good academic value. In view of the above situation, in order to improve the low-temperature toughness of the material and ensure the durability of the coil spring in the corrosive environment, the 39SiCrVTiA spring steel with high strength and toughness has been developed.

2 Test Method

This paper mainly uses various testing methods to comprehensively evaluate the various properties of the 39SiCrVTiA spring steel developed, with special attention to corrosion resistance. And compared with the high-strength spring steel 60Si2CrVA and SAE9254 commonly used today, it provides relevant reference basis and data support for the promotion and application of this material. The experimental materials are 39SiCrVTiA, 60Si2CrVA and SAE9254 spring steels with $\phi$ 15.8 mm. The material is quenched and tempered, and the structure is tempered troostite. The specific chemical components are shown in table 1. 39SiCrVTiA also contains Ni 0.22, Cu 0.23 and Ti 0.049.

Table 1. Chemical compositions of 39SiCrVTiA, 60Si2CrVA and SAE9254 spring steels (mass fraction, %)

| Steel      | C  | Si  | Mn  | Cr  | S   | P   | V   | Fe     |
|------------|----|-----|-----|-----|-----|-----|-----|--------|
| 39SiCrVTiA | 0.39 | 1.75 | 0.64 | 0.73 | 0.003 | 0.006 | 0.06 | Bal.    |
| 60Si2CrVA  | 0.56 | 1.56 | 0.62 | 1.02 | 0.009 | 0.012 | 0.16 | Bal.    |
| SAE9254    | 0.55 | 1.50 | 0.65 | 0.80 | 0.009 | 0.01  | --   | Bal.    |
The electrochemical test instrument is a PARSTAT 2273 electrochemical workstation. The sample size is φ 15.8 mm × 5 mm. Use a welding gun and a tin wire to solder the back of the test surface of the sample to the copper wire, and seal it with epoxy resin and ethylendiamine. The electrochemical test adopts a three-electrode system, saturated calomel electrode(SCE) as the reference electrode, graphite as the auxiliary electrode, and the sample to be tested is the working electrode. Before the experiment, the working electrode was first polished by SiC water abrasive paper from 150# to 1500#, then cleaned by ethanol and deionized water, and then dried by cold air for later use. The experimental medium is a 5% (mass fraction) NaCl solution at 35 ℃. During the experiment, the temperature of the medium is controlled by a constant temperature water bath with digital display. Before the test, the sample is polarized at -1000 mV for 3 minutes. The electrochemical impedance spectroscopy (EIS) test frequency range is 10^5 ~ 10^-2 Hz, and the excitation signal amplitude is 10 mV. The EIS test is performed under open circuit potential. The impedance data is shown by Nyquist and Bode diagram. The circuit component codes were used to describe the data, and the equivalent circuit was fitted and analyzed with ZSMPWLN software. When measuring the polarization curve, the potential scanning range is: -1000~450 mV (vs SCE), and the scanning rate is 0.5 mV·s⁻¹. The polarization curve results are analyzed by Tafel extrapolation.

The slow strain rate tensile test (SSRT) is carried out on the WDML-30KN material testing machine. The experiment uses a smooth plate-like tensile test specimen with a sample size prepared in accordance with GB/T 15970. Before the experiment, the surface of the sample is polished to 1500 # by SiC water-resistant sandpaper, then cleaned with acetone, deionized water, and dried for later use. The experimental solution medium is 5%NaCl (mass fraction). A three-electrode system was used, with the tensile sample as the working electrode, Pt sheet as the auxiliary electrode, and saturated calomel electrode (SCE) as the reference electrode. In SSRT experiment, the tensile samples are tested at the constant potential of -1000 mV (vs SCE). The test samples were maintained at this potential until the samples fractured during the whole experiment, and the CS350H electrochemical workstation is used to apply constant potential to the samples. The tensile strain rate is 1×10⁻⁶ s⁻¹, and the test temperature is room temperature (~25 ℃). After the SSRT experiment, Quanta250 scanning electron microscope (SEM) is used to observe and analyze the fracture morphology of tensile samples.

After the experiment, the parameters of elongation loss Iδ and section shrinkage loss Iψ are used to evaluate the SCC sensitivity of spring steel, where Iδ and Iψ are calculated according to the following formula.

\[
I_\delta = \left( 1 - \frac{\delta_E}{\delta_0} \right) \times 100\% \quad (1)
\]

\[
I_\psi = \left( 1 - \frac{\psi_E}{\psi_0} \right) \times 100\% \quad (2)
\]

In the formula, δE and ψE are the elongation and sectional shrinkage of spring steel in solution, and δ0 and ψ0 are the elongation and sectional shrinkage of spring steel in air, respectively.

### 3 Results and Analysis

#### 3.1 Electrochemical test.

Electrochemical impedance spectra test. Figure1 shows the electrochemical impedance spectra of three materials in a 5% NaCl solution. The equivalent circuit Rs (QdlRt) in Figure2 is used to fit the impedance spectrum, where Rs is the solution resistance, Qdl is the electric double layer capacitance at the non-ideal electrode/solution interface, and Rt is the charge transfer resistance. In the actual electrochemical system, the frequency response characteristics of the double-layer capacitor at the electrode/solution interface are different from that of the pure capacitor, so the constant phase angle Q is often used to represent the double-layer capacitor. Figure3 shows the fitted charge transfer resistance Rt. It can be seen from Figure3 that the value of the charge transfer resistance Rt of different materials is different. 39SiCrVTiA has the smallest Rt value, and the other two materials are closer. The smaller Rt is, the smaller the resistance during charge transfer is[2], and the lager the electrochemical reaction rate is, the lager the corrosion rate is[3]. Therefore, the order of the corrosion resistance of different materials is: 60Si2CrVA> SAE9254> 39SiCrVTiA.
Figure 1. Electrochemical impedance spectra of different materials in 5% NaCl solution

Figure 2. Electrochemical impedance spectroscopy simulation equivalent circuit

Figure 3. Fitted charge transfer resistance $R_t$

Polarization curves test. Figure 4 shows the polarization curves of different spring steels in 5% NaCl solution. Table 2 shows the corrosion potential $E_{corr}$ and corrosion current density $I_{corr}$ of different spring steels in 5% NaCl solution fitting from the polarization curves in Figure 5. From the table 2, it can be seen that the corrosion potential sequence from positive to negative is 60Si2CrVA, SAE9254 and 39SiCrVTiA, and the corrosion current density sequence from small to large is 60Si2CrVA, SAE9254 and 39SiCrVTiA. The more negative the corrosion potential is, the greater the thermodynamic tendency of corrosion is. The larger the corrosion current density is, the higher the corrosion rate is. Therefore, the higher content of element Cr and V may account for the better corrosion resistance of spring steel 60Si2CrVA.

Table 2. Corrosion potential $E_{corr}$ and corrosion current density $I_{corr}$ of three steels

| Steel      | $E_{corr}$/mV (vs SCE) | $I_{corr}$/($\mu A\cdot cm^{-2}$) |
|------------|------------------------|-----------------------------------|
| 39SiCrVTiA | -651                   | 29.8                              |
| 60Si2CrVA  | -598                   | 17.1                              |
| SAE9254    | -614                   | 23.1                              |

Stress corrosion test. Figure 5 shows the stress-strain curves of three spring steels in air and 5% NaCl solution. According to the figure, the tensile strength and yield strength 0.2 of spring steel 39SiCrVTiA, 60Si2CrVA and SAE9254 is 1855Mpa and 1767Mpa, 2127Mpa and 1900 Mpa, 2073 Mpa and 1845 Mpa respectively. It can be observed that the stress-strain behavior of samples in air and solution (applying -1v vs.SCE) is significantly different, and the elongation of samples in air is much higher than that in solution. When we carried on the slow strain rate tensile test (SSRT) of the three materials in individual test conditions, it was observed that...
5% NaCl solution, the samples fracture during the elastic deformation phase. This indicates that spring steels have a high stress corrosive cracking sensitivity under corrosion test condition.

![Stress-strain curves of three steels tested in air and 5% NaCl solution](image)

**Figure 5.** Stress-strain curves of three steels tested in air and 5% NaCl solution (a) 39SiCrVTiA; (b) 60Si2CrVA; (c) SAE9254.

Figure 6 shows the elongation loss and section shrinkage loss of three spring steels in 5% NaCl solution. From the figure, the spring steels 39SiCrVTiA and 60Si2CrVA in solution both have the very high elongation loss $\delta_0$ and area reduction loss $\psi$, while the steel SAE9254 has higher $\delta_0$ and $\psi$ that larger than 90%, and SCC parameter values are the lowest. Combining with the Figure8, we can know that three spring steels all have higher SCC sensitivity under corrosion test condition, and steel 39SiCrVTiA has a slightly lower SCC sensitivity than the other spring steels. The high brittleness coefficient indicates that three spring steels brittle fracture.

Figure 7 shows the fracture morphologies of spring steel 39SiCrVTiA in air and 5% NaCl solution. It can be seen from Figure 7(a) that the tensile fracture of steel 39SiCrVTiA in air has obvious necking and plastic deformation phenomenon. Meanwhile, Figure 7(b) shows a large number of dimples and micropores of different sizes which shows evident ductile fracture characteristics. Figure 7(c) and (d) show that the fracture morphology of spring steel in 5% NaCl solution is different from that in air. Compared with the fracture morphology in air, the fracture is more flat and there is no apparent necking phenomenon when it fractured in 5% NaCl solution. Figure 7(d) presents the typical intergranular crack morphology which looks like rock candy. The cracks extend along the grain boundary, and the grain separation phenomenon also can be observed, which are characteristics of Intergranular Stress Corrosion Crack (IGSCC) [12,13]. After observing of Figure 7(e) in detail, it can be seen that the cracks in the local region are wide and deep, and the short cracks are connected with each other to grow into long cracks, and the extension path is similar to the linear form, which are the obvious hydrogen embrittlement cracking characteristics (HE) [14]. Therefore, the SCC process presents the characteristics of intergranular brittle cracking and hydrogen embrittlement cracking at the same time, and its SCC sensitivity is relatively high.
deformation phenomenon, and large number of dimples and micropores of different sizes and depth which shows ductile fracture characteristics. Figure 8(c) and (d) show that the fracture morphology of steel 60Si2CrVA in 5%NaCl solution is significantly different from that in air. The fracture in air shows obvious ductile fracture characteristics like necking phenomenon; however, in 5%NaCl solution, the fracture shows no necking phenomenon. Figure 8(d) shows the typical ice-sugar-like intergranular cracking morphology, with many cracks extending along grain boundaries and obvious grain separation, which are obvious characteristics of Intergranular Stress Corrosion Crack (IGSCC). After observing the Figure 8(e) and 8(f) in detail, it also can be seen that apart from obvious characteristics of IGSCC, there are also existing some characteristics of Transgranular Stress Corrosion Cracking (TGSCC)[15,16,17] in the local region. Transgranular cracks are long, deep and wide when they almost extend in a continuous linear form, which show the obvious hydrogen embrittlement cracking characteristics (HE). Then, if combined with Figure 7 and 8, it can be seen that when -1v (vs.SCE) is applied in SSRT process, the spring steel 60Si2CrVA has a high SCC sensitivity in 5%NaCl solution, and presents obvious characteristics of intergranular brittle cracking and hydrogen embrittlement cracking.

Figure 7. Fracture morphologies of steel 39SiCrVTiA tested in air (a,b) and 5% NaCl solution(c-f)

Figure 8 shows the fracture morphology of spring steel 60Si2CrVA in air and 5% NaCl solution. It can be seen from Figure 8(a) and (b) that the tensile fracture of steel 60Si2CrVA in air also has obvious necking and plastic
Figure 8. Fracture morphologies of steel 60Si2CrVA tested in air (a,b) and 5% NaCl solution (c-f).

Figure 9 shows the fracture morphology of spring steel SAE9254 in air and 5% NaCl solution. It can be seen from Figure 9 (a) and (b) that it is similar to the steel 60Si2CrVA, the SAE9254 fracture in the air also presents necking and plastic deformation phenomenon, as well as a large number of dimples and micropores, which on behalf of the ductile fracture. Figure 9 (c) and (d) show that the fracture of SAE9254 steel in 5% NaCl solution is flat without necking phenomenon, and there is obvious grain separation, which are typical characteristics of hydrogen embrittlement. In addition, Figure 9 (e) also shows that long, deep and wide transgranular cracks extending in a straight line. This indicates that the fracture characteristics of steel SAE9254 both have the characteristics of intergranular brittle cracking and transgranular cracking in the form of mixture of shallow intergranular crack extension and deep transgranular crack extension. It is shown that steel SAE9254 has higher Iδ and Iψ value, and presents the obvious characteristics of hydrogen embrittlement cracking combined with Figure 8. So when we apply 1V (vs. SCE) in the process of the SSRT, the steel SAE9254 shows more SCC sensitivity in 5% NaCl solution.
3.2 Discuss

According to the polarization curve (Figure 4), when the potential reaches -1V (vs, the steels will react as the cathode as shown below.

\[ 2\text{H}_2\text{O} + 2\text{e}^- \rightarrow 2\text{H}^+ + 2\text{OH}^- \]  
\[ \text{H}^+ + \text{H} \rightarrow \text{H}_2 \]  

The partly H generated in the process of cathode hydrogen evolution will be adsorbed, then it penetrates into the steel and spreads along the grain boundary. In the SSRT process, on the influence of stress, the diffusion of H atom is intensified, and it tends to gather at the grain defect (grain boundary), which will lead to stress concentration and generate a large number of tiny grain boundary cracks in the steel (Figure 7(d), 8(d) and 9(d)). In addition, due to the stress-induced diffusion, H atom is more likely to diffuse and accumulate at the crack tip, and it will promote the rapid propagation of the crack tip, then the tendency of hydrogen embrittlement increases and it will lead to the occurrence of transgranular brittle fracture (Figure 7(e), 8(e), 8(f) and 9(e)). If we combine the brittle fracture characteristics in Figure 7, 8 and 9 with the relatively large values of section shrinkage loss and elongation loss in Figure 7, it can be inferred that when spring steel is applied to -1V (vs.SCE) in the 5% NaCl solution, the SCC mechanism is mainly hydrogen embrittlement (HE). The lower SCC sensitivity of 39SiCrVTiA steel may be related to its elements Ti, V and low carbon content. To sum up, 39SiCrVTiA spring steel is a kind of high strength and high toughness spring steel, which has excellent plastic toughness especially under low temperature condition and it also has the better hydrogen embrittlement resistance. However, its corrosion resistance remains to be improved.

5 Conclusion

The results of the long period immersion test show that the corrosion rates of the three spring steels are similar, and the steel SAE9254 has the highest corrosion rate, followed by 60Si2CrVA steels. Electrochemical ac impedance spectrum and polarization curve tests all show that the corrosion resistance sequence of spring steel materials from strong to weak was 60Si2CrVA > SAE9254 > 39SiCrVTiA. When -1V (vs.SCE) was applied in SSRT process, all three spring steels had high SCC sensitivity in 5% NaCl solution. The SCC sensitivity of steel SAE9254 was slightly lower, while the SCC sensitivity of steel SAE9254 was largest. The SCC mechanism is mainly hydrogen embrittlement (HE). The lower SCC sensitivity of 39SiCrVTiA steel may be related to its elements Ti, V and low carbon content.

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