Enhancing scour protection in river bends: a novel slotted bank-attached vane
Mohamad Azizipour, Farshid Amirsalari Meymani and Mohammad Mahmoodian Shooshtari

ABSTRACT
One of the most effective approaches for bank control erosion is using bank-attached vanes. In spite of the superiority of the bank-attached vanes to spur dikes, the vanes’ tips are still vulnerable to local scour caused by flow-structure interaction. In this study, slotted bank-attached vanes are proposed to reduce local scour at the tip of the triangular submerged vane. For this, a rectangular slot is created parallel to the chord of the vane with an area of ten percent of the effective area of the vane surface. Two types of conventional vanes and slotted vanes were installed at different angles of attack of 23, 30, 40 and 60 degrees in an arch flume. Experiments were carried out in clear water conditions with different flow regimes with Froude numbers of $F_r = 0.287, 0.304$ and $0.322$. The results show that the slotted vane outperforms the conventional vane by reducing maximum scour depth by about 70, 20, 17 and 54 percent for different angles of attack of 23, 30, 40 and 60 degrees, respectively. The proposed slotted vane also resulted in reduction of scour hole volume around the vane and formed the scour hole away from the outer bank.

Key words | erosion, local scour, slotted vane, submerged vane

HIGHLIGHTS
- Slotted submerged vanes are introduced.
- Performance of slotted vanes are investigated.
- The conventional and slotted vanes are compared.

INTRODUCTION
Bank erosion is a great challenge in meandering rivers and typically occurs in outer river bends. Although limited lateral channel migration could be beneficial for some ecosystems (e.g., Piégay et al. 2005), unrestricted bank erosion may demolish an existing riparian ecosystem. To cope with this issue, stabilization of river banks is of great importance. There are many studies in the literature proposing different methods for bank erosion protection including spur dikes (Copeland 1985), riparian vegetation (Croke et al. 2017) and different types of vanes (Bhuiyan et al. 2010; Pagliara et al. 2014; Odgaard 2015, 2017).

In recent years, submerged vanes for the protection of riverbanks have increasingly been used because of their fast and easy way of installation compared with other traditional methods like dikes and groins (Biswa & Barbhuiya 2019). As an environment-friendly structure, submerged vanes are designed for habitat improvement as well. Various studies have been undertaken on vanes. The effectiveness of vanes in reducing near-bank velocity considering different angles of attack was investigated by Odgaard & Kennedy (1983), concluding that for a greater angle of attack than $20^\circ$, a scour hole is formed at the upstream edge of the vane. Odgaard & Spoljaric (1986) developed a
rational method for design of a system of submerged vanes to control depth in alluvial rivers. Odgaard & Mosconi (1987) proposed that the secondary flow in bends is modified by use of vanes, resulting in redistribution of sediment within the channel cross-section and consequently reduction of scour at the bends. A detailed numerical study was done by Sinha & Marelius (2000) to analyze flow past a submerged vane. Tan et al. (2005) conducted experiments in a large flume to investigate the flow and sedimentation characteristics around a submerged vane. They concluded that the success of a submerged vane in sediment diversion depends on the optimum skew angle to the approach flow for the purpose of sediment diversion, the vane shape and vane alignment to the approach flow. Gupta et al. (2010) used a collar at the leading edge of the vane and indicated that the scour at the leading edge of the collar was reduced to zero. The effects of log-vanes on the scour in straight rivers were studied by Pagliara et al. (2015) resulting in obtaining an equation to determine the scour parameters and morphology. Results of a study on bank erosion and protection using a submerged vane carried out by Dey et al. (2017) showed that a 15° vane angle produces the best results in reducing outer bank scour in a parabolic-shaped channel. More recently, Biswas & Barbhuiya (2019) carried out a series of experiments in a 180° bend to explore the effects of submerged vanes on the flow field and subsequent scour morphology in a river bend.

As is mentioned by many researchers, the shape of a submerged vane plays an important role in its performance improvement (e.g. Ouyang 2009; Shafai Bejestan & Azizi 2012; Teronpi & Misra 2015). Shafai Bejestan & Azizi (2012) compared the efficiency of rectangular and triangular vanes showing that the triangular vane outperforms rectangular vanes in scour reduction. In another study, the comparison of scour depth for both triangular shape vanes (TSV) and rectangular shape vanes (RSV) proved that the scour depth for TSV is 80 percent less than the scour depth of RSV (Badri 2014). Teronpi & Misra (2015) proposed that the maximum scour depth among rectangular, trapezoidal and curved submerged vanes takes place in the case of rectangular vanes.

Despite the rich literature in the field of rectangular submerged vanes, there are only a few studies in the field of triangular submerged vanes. In a laboratory investigation, Bhuiyan et al. (2010) installed low-angle and bank-attached triangular vanes in a mobile bed channel, concluding that when a single vane or an array of vanes is installed, the scour hole at the base of the outer bank is filled and the thalweg is relocated toward the center of the river. Moreover, the deposition is formed at the downstream side of the vanes, due to plunging flow over the crest of the vanes. The components of flow velocity in a 90° mild bend were experimentally studied by Bahrami Yarahmadi & Shafai Bejestan (2015), for cases of both with and without a submerged vane. The results showed that the location of the maximum depth-averaged velocity was shifted from the near-outer bank toward the channel midpoint after installing a single triangular vane. Also, the single vane decreased the depth-averaged velocity near the outer bank both upstream and downstream of the vane.

The main drawback associated with using submerged vanes is the local scour around their tips which may cause destruction of the structure. This paper aims at introducing a novel approach to reduce the local scour around the vane’s tip and to increase the effectiveness of the triangular submerged vane in protecting riverbank erosion. This is achieved through creating a slot in the structure to modify the flow pattern around the submerged vane. Although using a slot to control local scour around a bridge pier was first introduced by Chiew (1992), to the best of our knowledge, there is no study in the literature investigating the effect of the slot on scour around a submerged vane. In this study, the effect of a slot in a submerged vane on bed topography and its skew angle is experimentally investigated. Results show that the proposed slotted vanes are superior to conventional vanes in protecting a bank from erosion by reducing the maximum scour depth.

**MATERIALS AND METHODS**

The experiments were conducted in a single-bend flume with 90 degrees of curvature. Since the ratio of the bend radius to the flume width $\left(\frac{R}{B} = \frac{2.8}{0.7}\right)$ is equal to 4, according to (Rozovskii 1957), the flume falls into the category of a mild bend. The length and width of the flume are 12.4 and 0.7 metres, respectively. The length of the straight
reaches at the upstream of the bend is 5 m while the downstream part of the bend is 3 m long. It is notable that the flume’s side walls are made of transparent Plexiglas providing a rectangular cross-section. The schematic representations of the flume and vanes are illustrated in Figures 1 and 2, respectively.

The discharge \( Q \) to the flume is adjusted via an ultrasonic flowmeter with an accuracy of \( \pm 0.01 \) l/s, installed on the entrance pipe to the flume. At the outlet section, the flow is drained into a reservoir and the water is recycled to the system, as shown in Figure 1. The flume bed is covered by uniform sand with median diameter (\( d_{50} \)) of 1.5 mm and geometric standard deviation \( \sigma \) of 1.22 for all the experiments. As shown in Figure 2 (a1), the depth of the sediment bed layer is fixed at 20 cm. A fixed slide gate at the end of the flume is employed to control the flow depth (\( h \)). The flow depth is kept constant, for all experiments, at 14 cm from the bed level, which is equal to the vane crest level at the outer bank in the bend.

The triangular vanes are made of Plexiglas with a thickness of 4 mm. To investigate the effect of a vane, a single vane was installed at the section 72° from the beginning of the bend on the outer bank in which the maximum scour usually occurs (Bahrami Yarahmadi & Shafai Bejestan 2016). All experiments were carried out for both cases of conventional and slotted triangle vanes. The conventional and proposed slotted triangular vanes are shown in Figure 2. As shown in Figure 2 (a2), a rectangular slot is created on the vane parallel to the chord. The slot surface is equal to ten percent of the effective surface of the vane, which is defined as the surface that is exposed to the approaching flow. The ratio of length to width of the slot is considered as 4 (\( \frac{a}{b} = 4 \)). As illustrated in Figure 1, the effective length is the perpendicular distance between the vane’s tip to the outer bank, which is taken as 14 cm (\( L_e = 14 \) cm), for all experiments.

A total number of 24 experiments were carried out for both cases of conventional and slotted vanes. Different angles of attack of 23°, 30°, 40° and 60° were considered for both cases, with different Froude numbers of \( Fr = 0.287, 0.304 \) and 0.322. Table 1 summarizes characteristics of all tests conducted in this study. Each test takes about three hours to be completed and the water is then gradually drained out of the flume to avoid any disturbance in the bed topography. The bed profile is then measured by using a laser distance meter (Bosch GLM 30) with an accuracy of 1 mm, which is installed on a rail on the top of the flume.

![Figure 1](http://iwaponline.com/ws/article-pdf/20/6/2175/766554/ws020062175.pdf)
RESULTS

Scour morphology

The bed morphology and contours of the scoured beds for both cases of slotted and conventional vanes, for a constant Froude number of 0.322, are illustrated in Figure 3.

As shown in the figure, for an angle of attack of $23^\circ$, there is no scouring at the upstream of the vane and the scour hole is completely transferred to the downstream of the vane. Experimental observations showed that regardless of the value of the Froude number, the scour hole is only formed at the downstream of the vane. It should be mentioned that the minimum scour volume is obtained when using a vane with an angle of attack of $23^\circ$.

It is clearly seen in Figure 3 that for all angles of attack, the scour depth around the slotted vane is much less than the case of using a conventional vane. Creating a slot in the vane also caused scour hole volume reduction around the vane for different angles of attack. Moreover, the scour hole around the tip of the structure in the slotted vane is less developed in comparison with the conventional vane.

The bed morphology contours for $40^\circ$ and $60^\circ$, presented in Figure 3, reveal that the scour around the conventional vanes reached to the outer bank for all cases considered in this study, while by using $40^\circ$ and $60^\circ$ slotted vanes, the scour only reached to the outer bank in the case of the largest Froude number, and the scour depths were much less than those of conventional vanes.

The scoured bed profile for different angles of attack and constant Froude number of 0.322 is presented in Figure 4 for the cross-section in which the maximum scour depth occurred. The dashed and continuous lines represent the scour bed for slotted and conventional vanes, respectively. The outer bank is considered to be at $x = 0$, while $x = 70$ cm is the location of the inner bank in the bend. Figure 4

\begin{figure}[h]
\centering
\includegraphics[width=\textwidth]{figure2.jpg}
\caption{The single vane that was installed at an angle of 30 degrees, without slot (b1), with slot (b2).}
\end{figure}
indicates that the slotted vane has superior performance to conventional vanes in decreasing scour, regardless of angle of attack. The superiority of slotted vanes to conventional vanes was observed not only for $Fr = 0.322$, but also for all hydraulic conditions considered. It is also obviously seen from Figure 4 that the maximum scour depth is reduced by using the slotted vane for all cases.

**Characteristics of scour hole**

Determining maximum scour depth is of great importance in design of in-stream structures. This, therefore, necessitates the careful investigation of the location and the depth of maximum scour. However, prediction of maximum scour depth and its location is complicated especially in river bends where helical flow is formed due to the presence of centrifugal forces.

Table 2 summarizes the results of maximum scour depth for all experiments carried out in this study, for slotted and conventional vanes. The maximum scour depth reduction which is obtained by using the slotted vane rather than the conventional vane is also reported in Table 2. Although the percentage of maximum scour depth reduction varies by different angle of attack and different hydraulic conditions, the slotted vane outperforms the conventional vanes in all tests. The average reductions of maximum scour depth for different Froude numbers are 70, 20, 17 and 54 percent for angles of attack of 23°, 30°, 40° and 60°, respectively. The best performance of the slotted vane is achieved while the angle of attack is set to 23°. As shown in the table, regardless of the angle of attack, the maximum scour depth is proportionate to Froude number, which coincides with previous research in the literature (e.g. Bahrami Yarahmadi & Shafai Bejestan 2015).

Since the maximum scour depth plays an important role in the stability of the in-stream structures, it could be concluded that the slotted vane is much more stable than the conventional vane.

The location of maximum scour depth and its distance from the bank of the river are also crucial parameters needing to be considered besides the maximum scour depth. A closer scour hole to the bank endangers the safety of in-stream structures. The closeness of the scour hole to the bank was investigated for the proposed slotted vane and the results are illustrated in Figure 5. The figure shows the dimensionless distance of maximum scour depth ($d/h$) versus different angles of attack, in which $d$ is the distance of the maximum scour depth from the outer bank of the bend. This figure indicates that increasing Froude number moves the scour hole away from the outer bank. Moreover, it is clearly seen from Figure 5 that there is an angle of attack, between 30° and 40°, in which the furthest scour hole is formed.

**Characteristics of deposition zone**

The process of scouring the outer banks in river bends is always associated with deposition of point bars on the

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**Table 1 | Details of conducted tests**

| Test number | Vane type     | $\alpha$ (degree) | Fr  |
|-------------|---------------|-------------------|-----|
| 1           | Conventional vane | 23                | 0.287 |
| 2           | Conventional vane | 23                | 0.304 |
| 3           | Conventional vane | 23                | 0.322 |
| 4           | Conventional vane | 30                | 0.287 |
| 5           | Conventional vane | 30                | 0.304 |
| 6           | Conventional vane | 30                | 0.322 |
| 7           | Conventional vane | 40                | 0.287 |
| 8           | Conventional vane | 40                | 0.304 |
| 9           | Conventional vane | 40                | 0.322 |
| 10          | Conventional vane | 60                | 0.287 |
| 11          | Conventional vane | 60                | 0.304 |
| 12          | Conventional vane | 60                | 0.322 |
| 13          | Slotted vane    | 23                | 0.287 |
| 14          | Slotted vane    | 23                | 0.304 |
| 15          | Slotted vane    | 23                | 0.322 |
| 16          | Slotted vane    | 30                | 0.287 |
| 17          | Slotted vane    | 30                | 0.304 |
| 18          | Slotted vane    | 30                | 0.322 |
| 19          | Slotted vane    | 40                | 0.287 |
| 20          | Slotted vane    | 40                | 0.304 |
| 21          | Slotted vane    | 40                | 0.322 |
| 22          | Slotted vane    | 60                | 0.287 |
| 23          | Slotted vane    | 60                | 0.304 |
| 24          | Slotted vane    | 60                | 0.322 |

$\alpha$ – angle of single vane to the upstream bank; $Fr$ – Froude number.
Figure 3 | Bed morphology around the conventional and slotted vanes at different angles ($Fr = 0.322$).
Figure 4 | Scoured bed profile for slotted and conventional vanes at maximum scour depth cross-section ($Fr = 0.322$).

Table 2 | Results of maximum scour depth for conventional and slotted vanes

| $\alpha$ (degree) | $Fr$ | Conventional vane | Slotted vane | Maximum scour depth reduction (%) |
|------------------|-----|-------------------|--------------|----------------------------------|
| 23               | 0.287 | 3.2               | 0.8          | 75                               |
|                  | 0.304 | 5.2               | 1.3          | 75                               |
|                  | 0.322 | 6.5               | 2.6          | 60                               |
| 30               | 0.287 | 4.3               | 3.3          | 23                               |
|                  | 0.304 | 6.2               | 5.4          | 13                               |
|                  | 0.322 | 9.3               | 7.1          | 24                               |
| 40               | 0.287 | 8.2               | 7.2          | 12                               |
|                  | 0.304 | 10.3              | 8.8          | 15                               |
|                  | 0.322 | 12.4              | 9.5          | 23                               |
| 60               | 0.287 | 10.6              | 4.8          | 55                               |
|                  | 0.304 | 11.4              | 5.9          | 48                               |
|                  | 0.322 | 18.4              | 7.4          | 60                               |

Figure 5 | Variations of normalized maximum scour depth distance from the outer bank versus angle of attack at different Froude numbers.
inner banks. Characterizations of point bars including prediction and control of how much and where the sediment deposition occurs are as important as scour hole considerations, for efficient design of in-stream structures.

Figure 6 displays the effect of orientation of the proposed slotted vane on dimensionless maximum point bar height ($H_{\text{max}}/h$). As shown in the figure, the maximum height of the point bar takes place at an angle of attack between 30° and 40°, which matches with the scour hole maximum depth, shown in Figure 5. The figure also indicates that increasing Froude number leads to forming a point bar with larger $H$.

Vane performance

The bank of the river in meanders is protected by vanes such that the flow is diverted from the river banks toward the middle of the river. The flow diversion is associated with formation of a highly turbulent rotational zone which is developed around the vane tip. The scour, therefore, occurs around the tip and scoured bed particles are deposited downstream of the vane. Although the local scour is considered a threat to the stability, durability, and function of the vane, the river banks at the downstream of the vane are naturally protected by sediment deposition. The performance of the proposed slotted vane structures is therefore evaluated considering both scour and deposition values. For this, the performance of the vane is defined as the ratio of maximum deposition ($H_{\text{max}}$) to maximum scour ($Z_{\text{max}}$), which can be mathematically formulated as $P_v = H_{\text{max}}/Z_{\text{max}}$. The higher the value of $P_v$, the better the performance of the vane.

The results of performance evaluation of the proposed slotted vane are presented in Table 3 and compared with those obtained for conventional vanes, for different angles of attack ($\alpha$) and various hydraulic conditions. The table indicates that the proposed slotted vane performs more efficiently than conventional vanes regarding the value of $P_v$ for all cases considered in this study. In other words, the slotted vanes have been able to deposit the eroded sediments with proper height at the outer bank.

### Table 3 | Results of performance index for conventional and slotted vanes

| $\alpha$ (degree) | Fr  | Conventional vane | Slotted vane |
|------------------|-----|-------------------|--------------|
| 23               | 0.287 | 1.03              | 1.50         |
|                  | 0.304 | 0.96              | 1.46         |
|                  | 0.322 | 0.80              | 1.38         |
| 30               | 0.287 | 1.02              | 1.52         |
|                  | 0.304 | 0.77              | 1.20         |
|                  | 0.322 | 0.85              | 0.96         |
| 40               | 0.287 | 0.90              | 0.93         |
|                  | 0.304 | 0.63              | 0.77         |
|                  | 0.322 | 0.39              | 0.74         |
| 60               | 0.287 | 0.47              | 0.63         |
|                  | 0.304 | 0.46              | 0.59         |
|                  | 0.322 | 0.19              | 0.49         |

DISCUSSION

The presented results show that by using the slotted vane the scouring potential is significantly reduced. The performance of the slotted vane in decreasing scour potential can be attributed to either diverting downflow away from the bed, or creating an upward flow pattern.

There are three types of approaching streamlines to the vane illustrated in Figure 7. The streamlines with higher elevation than slot elevation collide with the vane forming a downflow which has the main impact on scouring potential. A part of such streamlines is deflected to the downstream of the vane through the slot, before hitting the bed, and the

![Figure 6](http://iwaponline.com/ws/article-pdf/20/6/2175/766554/ws020062175.pdf)
scouring potential is, therefore, reduced. The streamlines with the same elevation as the slot can directly transfer to the downstream without colliding with the vane and forming downflow. The approaching streamlines to the vane with lower elevation than the slot create an upward flow. The appearance of the upward flow can neutralize a part of the downflow leading to scour potential reduction. It can be concluded that creating a slot in the vane redistributes the flow pattern such that the effect of critical shear stress as well as destructive vortices are lessened and the scour potential is consequently decreased. This in fact is vindicated by the experimental results presented in the previous sections.

As was investigated by various researchers (e.g., Bhuiyan et al. 2010; Dey et al. 2017), the smaller the angle of attack, the better the performance of the vane, which is matched by the observations in this study. However, considering the fixed effective length of the vane, the smaller angle of attack leads to a longer vane, which is not efficient from an economic point of view. The proposed slotted vane provides an alternative to the conventional vane while economically outperforming the conventional vane. The performance of the 23° conventional vane is approximately equal to the 60° slotted vane in decreasing scour depth, while the surface area of the conventional vane is 2.2 times greater than that of the slotted vane. This implies that using a slotted vane decreases the size of the vane by up to 55% in comparison with the conventional vane.

More numerical and experimental research could extend the current research to understand the effect of size and location of the slot and how it could be optimized for different hydraulic conditions.

**CONCLUSION**

A modified submerged vane was proposed for local scour protection with a rectangular slot in the effective surface of the vane. Experiments were carried out in two stages of with and without a slot on the vane, and four different angles of attack of flow were considered. The results of the experiments show the capability of the proposed slotted vane in decreasing scour depth as well as scour volume. The angle of attack of flow with 23, 30, 40 and 60 degrees led to decreasing scour depth of 70, 20, 17 and 54 percent, respectively, of those of the conventional vane. It is also noteworthy that the maximum scour depth around the tip of the slotted vanes has the lowest and highest value at the angles of 23 and 40 degrees, respectively. The slotted vanes also performed better than the conventional vanes in creating a balance between maximum scour depth and maximum point bar height.
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