Sub-micronter plasma-enhanced chemical vapor deposition using an atmospheric pressure plasma jet localized by a nanopipette scanning probe microscope

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Abstract
We developed a localized plasma-enhanced chemical vapor deposition (PE-CVD) technique to deposit silicon oxide with a sub-micrometer width on a substrate using an atmospheric pressure plasma jet (APPJ) irradiated from a nanopipette nozzle. To realize fine material deposition, hexamethyldisiloxane (HMDSO) vapor was blown into the localized helium APPJ irradiated from the sub-micrometer aperture of the nanopipette with the jet length limited to the aperture size of the nanopipette. The irradiation distance was controlled using a shear-force positioning technique using scanning probe microscopy (SPM). The proposed system successfully deposited silicon oxide dots with sub-micrometer width on a substrate. After the deposition, the topography of the deposited surface was observed by scanning the nanopipette, which can be used as an SPM probe. The localized PE-CVD properties were systematically investigated by varying the deposition parameters. The amount of deposited material could be controlled by the flow rate of the carrier gas of the HMDSO vapor, APPJ irradiation time, and nanopipette–substrate surface irradiation distance.

Keywords: atmospheric pressure plasma jets, scanning probe microscope, material deposition, plasma enhanced chemical vapor deposition, nanopipette

(Some figures may appear in colour only in the online journal)
1. Introduction

Atmospheric pressure plasmas (APPs) have attracted significant attention as plasmas that can be generated in the atmosphere; thus, their applications are expected to be used in various fields, such as physics [1–7], medicine [8–11], biology [12–17], and engineering [18–27]. In particular, an APP jet (APPJ), which is a jet-like plasma injected from the tip aperture of a tube nozzle under atmospheric pressure [28, 29], has recently been applied to surface material processing and modification. As APPJ does not require a vacuum environment, a simple and inexpensive device configuration can be realized. In general, APPJ is generated in a dielectric tube and irradiated as a plasma bullet through a tube aperture [29]. Therefore, the irradiation area can be localized at a high density, which is useful for maskless fabrication processes. Plasma etching techniques using APPJ have been developed for material removal processing [30–33]. By irradiating the silicon surface with APPJ doped with the etching gas of SF$_6$, localized dot etching with sub-millimeter widths was achieved. A nozzle with a smaller aperture should be used to realize finer processing using a smaller APPJ. In a previous study, specially designed microcantilevers for localized plasma generated at a pyramidal tip nozzle were proposed [34, 35]. These microcantilevers require complex microfabrication processes and are difficult to use owing to their high manufacturing costs. Previous studies have developed localized APPJs using a nanopipette that can be easily and inexpensively prepared by thermally pulling a capillary glass tube [36–39]. A nanopipette with a tip aperture of sub-micrometer diameter was used not only as a nozzle to generate localized APPJs but also as a probe for scanning probe microscopy (SPM). This allows us to move the tip of the nanopipette close to a material surface with nanometer-scale accuracy using the positioning technique of the SPM and subsequently irradiate the localized APPJ on the material surface. Using this system, we etched sub-micrometer-wide dots and lines on the surface of the photoresist [38] and polymethylmethacrylate [39, 40].

APPJ can be used not only for material removal processing, but also for material deposition techniques, called plasma-enhanced chemical vapor deposition (PECVD). PECVD techniques have been reported for silicon oxide (SiO$_2$) and tungsten oxide [41–44]. However, the processing width of PECVD is still in the sub-millimeter order. Therefore, to apply APPJ as a microdeposition process for the fabrication of microdevices, such as microelectromechanical systems (MEMS), the processing width should be further reduced.

In this study, we developed a sub-micrometer-sized PE-CVD using the nanopipette positioning technique based on SPM to improve the localization of the material deposition process using APPJ. Hexamethyldisiloxane (HMDSO) was used as the precursor gas. SiO$_2$, which is used in various applications owing to its excellent properties, such as electrical insulation, wear resistance, hardness, optical transparency, and chemical inertness [45–47], was deposited on the substrate by reacting it with the oxygen radicals generated by the APPJ, which break the chemical bonds of HMDSO. The amount of deposited SiO$_2$ dots was investigated by systematically varying the processing parameters, such as the amount of added HMDSO, plasma irradiation time, and irradiation distance, using the localized PE-CVD system based on the nanopipette SPM.

2. Experimental methods

2.1. Generation of the localized APPJ for PE-CVD of silicon oxide

Figure 1 shows a schematic of the localized APPJ generated using a nanopipette. The nanopipette was fabricated using a capillary borosilicate glass tube (G-1, Narishige, Tokyo, Japan) with an inner and outer tube diameter of 0.6 and 1.0 mm, respectively. The capillary tube was thermally pulled using a commercial laser puller (P-2000, Sutter Instrument Company, USA). The APPJ used in this study was generated using dielectric barrier discharge. The source gas was first introduced into the nanopipette. A tungsten wire inserted in the nanopipette was connected to a high-voltage power supply. When a high-voltage pulse wave was applied to the inner electrode, the He source gas was ionized as the plasma was jetted out from the aperture of the nanopipette tip. As shown in figure 1, the HMDSO vapor (Tokyo Chemical Industry, Tokyo, Japan) with O$_2$ carrier gas was blown into the APPJ irradiated from the tip of the nanopipette through a nozzle. The CH$_3$ bonds in HMDSO were broken by APPJ, and oxygen radicals were generated. As a result, a SiO$_2$ film was locally deposited on the substrate via a chemical reaction with oxygen radicals.

2.2. Scanning nanopipette probe microscope for local deposition and observation

Figure 2 shows the experimental setup of the local deposition system using an APPJ based on SPM with a nanopipette. The system consists of a nanopipette positioning system with nanometer-scale accuracy relative to the substrate and a material deposition system using the APPJ ejected from the nanopipette aperture. Shear force feedback control, a probe positioning technique of SPM, was employed to position the nanopipette in the vicinity of the substrate surface. Shear force is an interactive force between the horizontally oscillating probe tip and the sample surface, which is caused by van der Waals forces and viscous resistance due to the meniscus in the atmosphere [48]. When the nanopipette tip approached the substrate surface while oscillating the tip horizontally at its resonance frequency, the resonance frequency shifted because of the shear force acting between the tip and surface. By detecting a slight frequency shift and maintaining it at a pre-set constant value through the feedback system, the distance between the pipette tip and substrate surface can be maintained at a constant nanometer level. In the experimental system, the tip of the nanopipette oscillated at the resonance frequency using a piezoelectric (PZT) oscillator. The oscillated tip was projected with a focused beam from a laser diode (LDV167S,
Takenaka Optronic Co., Ltd, Kyoto, Japan), and the tip oscillation was detected using a photodiode (S4602, Hamamatsu Photonics, Hamamatsu, Japan). The oscillation signal from the photodiode was sequentially detected using an I–V converter, an arithmetic circuit, and a self-oscillation circuit. The shift in the resonance frequency due to the shear force was detected by a phase-locked loop (PLL) circuit (OC4, Nanonis/SPECS, Zurich, Switzerland). The output signal of the PLL circuit, corresponding to the frequency shift, was fed to a feedback controller (SC4, Nanonis/SPECS, Zurich, Switzerland) connected to a personal computer. The feedback control system maintained a predefined value of the frequency shift by driving a PZT tube scanner through a PZT driver (HVA4, Nanonis/SPECS, Zurich, Switzerland) to maintain a constant distance between the pipette tip and the material surface with nanometer-scale accuracy. During the material deposition process, the pipette tip was raised to a set distance (irradiation distance) from the position where the pipette tip detected the substrate surface using a pipette edge positioning technique. Subsequently, the deposition process was performed at a constant pipette-tip height. Immediately after the deposition process, the nanopipette was placed close to the surface for detection, and sequential topographic imaging of the deposited structures was performed after deposition under feedback control.

For the local deposition function using APPJ, the flow rate of He gas introduced into the nanopipette was controlled by a mass flow controller (Model 8500MC, Kofloc, Kyoto, Japan). To prevent damage to the nanopipette tip by the localized pressure, a leak orifice with a diameter of 1 mm was fabricated and installed before the inflow of the nanopipette. The pulse wave output from the function generator was amplified to a voltage of several kilovolts using a high-voltage amplifier (HVA4321, NF Electronic Instruments, Tokyo, Japan). By applying the amplified pulse voltage between the inner electrode of the nanopipette and the ground electrode wound outside the nanopipette, APPJ was generated by the dielectric barrier discharged between the electrodes.

To carry the HMDSO vapor, the O₂ carrier gas was also controlled by another mass flow controller (KOFLOC 8500MC) and was subsequently injected into the HMDSO container to introduce the HMDSO vapor to the APPJ using the nozzle. HMDSO temperature was maintained at 25 °C. The deposited SiO₂ is chemically stable and physically adsorbed on the substrate; therefore, the dependence on the substrate material is considered to be low. Therefore, in this study, only the slide glass was used as the substrate material, except for the EDX analysis.

3. Results

3.1. EDS analysis of the deposition film

The surface morphology and elemental composition of the deposited film were investigated using a computer-controlled digital scanning electron microscope (SM-7001 F, JEOL, Tokyo, Japan) attached to an energy dispersive x-ray spectrometer (EDS). Here, a nanopipette with an aperture diameter of 100 µm was used for easy analysis, and a gallium arsenide (GaAs) wafer, instead of glass, was used as the substrate to prevent component overlap with the deposit composition. The flow rates of the He source gas and O₂ carrier gas were 400 and 5 sccm, respectively. For the APPJ discharge, the amplitude of the applied pulse voltage was 4 kV_p–p, the frequency was 7 kHz, and the pulse duty ratio was 50%. The APPJ irradiation time was set to 20 s.

Figure 3 shows the electron microscopy, EDS spectra, and composition mapping images of the deposited film. The results confirmed the formation of the deposited film in the APPJ irradiation region. The EDS spectra and compositional mapping indicate that the deposit is composed of Si and O, and a small amount of C. Therefore, HMDSO was decomposed by the APPJ, and a fine SiO₂ film was formed through localized PE-CVD.

3.2. Sub-micrometer scale deposition of SiO₂ using the nanopipette SPM

The sub-micrometer-scale PE-CVD technique was performed using SPM with a nanopipette probe. For the sub-micrometer-scale deposition, a nanopipette with an aperture diameter of 400 nm was employed, and slide glass was used as the substrate. The flow rates of the He source gas and O₂ carrier gas were 400 and 10 sccm, respectively. HMDSO temperature was maintained at 25 °C. For the APPJ discharge, the applied voltage was 3.5 kV_p–p, the frequency was 7 kHz, and the pulse duty ratio was 50%. The distance between the pipette tip and substrate surface was 600 nm. The APPJ irradiation time was set to 1 s. Figures 4(a)–(c) show the 2D and 3D images of the topography and line profile of the dots deposited on the substrate, respectively. Four dots with half-bandwidths of approximately 300 nm were deposited on the substrate surface. These results indicate that the local deposition by He-APPJ with HMDSO vapor could be realized with sub-micrometer-scale fabrication. As shown in figure 4, the nanopipette can be used as a nozzle for the APPJ and probe for SPM. Thus, in situ observations and evaluations were performed immediately after the deposition process.
Figure 2. Schematic of the experimental setup of the localized PE-CVD system coupled with the nanopipette SPM.

Figure 3. EDS analysis of the locally deposited film formed on GaAs substrate. (a) Electron microscopy image. (b) EDS spectra of the deposited dot. (c)–(f) Compositional mapping images of Si, O, Ga, and As, respectively.

3.3. Dependence of the deposition height on the HMDSO flow rate

As SiO$_x$ deposits are formed by the decomposition of HMDSO, the flow rate of the O$_2$ carrier gas in the HMDSO vapor was increased from 2 to 10 sccm in 2 sccm increments to evaluate the dependence of the deposit height on the amount of added HMDSO. The flow rate of the He source gas was 400 sccm. For the discharge of the APPJ, the amplitude of the applied pulse voltage was 3.5 kV$_{p-p}$ and the frequency was 7 kHz with a pulse duty ratio of 50%. The APPJ irradiation time was set to 15 s. The distance between the pipette tip and the substrate surface was 600 nm. Figure 5 shows the SPM images and line profiles of the deposited dots when the flow rates of the carrier gas were 0, 4, 6, and 10 sccm. As shown in figure 5(a), there were no deposits formed within the white circles, which represent the irradiation area of the APPJ with a carrier gas flow rate of 0 sccm.
The dependence of the deposition rate on the irradiation time was investigated by varying the APPJ irradiation time from 1 to 8 s. The flow rates of the He source gas and O₂ carrier gas were 400 and 10 sccm, respectively. For the APPJ discharge, the amplitude of the applied voltage was 3.8 kV_{p-p}, the frequency was 7 kHz, and the pulse duty ratio was 50%. The distance between the pipette tip and substrate surface was 600 nm.

At irradiation times of less than 3 s, the growth rate of the deposition height was approximately 100 nm s⁻¹. In contrast, the growth rate of the deposition height was less than 30 nm s⁻¹ for irradiation times longer than 3 s. In this deposition method, HMDSO vapor was added to the APPJ from outside the nanopipette. Hence, the concentration distribution of the HMDSO vapor might be lower in the immediate vicinity of the pipette tip aperture because of the strong flow of the He source gas ejected from the pipette aperture. In addition, at irradiation times of less than 3 s, the top of the deposit is located far from the aperture of the nanopipette and the HMDSO vapor was sufficiently mixed in this region for efficient deposition. However, at an irradiation time of approximately 3 s, the height of the deposit reached approximately 400 nm, and at longer irradiation times, it tended to saturate. As mentioned above, HMDSO was not sufficiently mixed near the pipette aperture; thus, the efficiency of HMDSO deposition significantly decreased after irradiation for more than 3 s. Even after increasing the irradiation time, the deposition height remained saturated at a position of approximately 100–200 nm below the pipette tip. As discussed in sections 3.2, 3.3, and 3.5, the irradiation time was set to 15 s to ensure that the deposition height settled at the saturated value with less dispersion.

3.5. Dependence of the deposition height on the distance between pipette tip and sample

As the APPJ length emitted from the small aperture of the nanopipette was short, we evaluated the changes in the deposition height when the distance between the nanopipette and substrate surface was varied. The distance between the nanopipette and substrate, that is, the plasma irradiation distance, was varied from 200 to 1400 nm with 200 nm increments. The flow rates of the He source gas and O₂ carrier gas were 400 and 10 sccm, respectively. For the APPJ discharge, the amplitude of the applied pulse voltage was 3.8 kV_{p-p}, the frequency was 7 kHz, and the pulse duty ratio was 50%. The APPJ irradiation time was 15 s.

Figures 7(a)–(d) show the SPM images and line profiles of the deposits at irradiation distances of 200, 600, 1000, and 1400 nm, respectively. Figures 7(e) and (f) show the dependence of the deposition height and width on the nanopipette tip–sample distance, respectively. The error bars show the maximum and minimum values, and the plots indicate the mean values (n = 3). The height of the deposit increased with increasing irradiation time. This indicates that the amount of deposits can be controlled by varying the irradiation time. However, the rate of increase in the deposition height gradually decreased with a further increase in the irradiation time. At irradiation times of less than 3 s, the growth rate of the deposition height was approximately 100 nm s⁻¹. In contrast, the growth rate of the deposition height was less than 30 nm s⁻¹ for irradiation times longer than 3 s. In this deposition method, HMDSO vapor was added to the APPJ from outside the nanopipette. Hence, the concentration distribution of the HMDSO vapor might be lower in the immediate vicinity of the pipette tip aperture because of the strong flow of the He source gas ejected from the pipette aperture. In addition, at irradiation times of less than 3 s, the top of the deposit is located far from the aperture of the nanopipette and the HMDSO vapor was sufficiently mixed in this region for efficient deposition. However, at an irradiation time of approximately 3 s, the height of the deposit reached approximately 400 nm, and at longer irradiation times, it tended to saturate. As mentioned above, HMDSO was not sufficiently mixed near the pipette aperture; thus, the efficiency of HMDSO deposition significantly decreased after irradiation for more than 3 s. Even after increasing the irradiation time, the deposition height remained saturated at a position of approximately 100–200 nm below the pipette tip. As discussed in sections 3.2, 3.3, and 3.5, the irradiation time was set to 15 s to ensure that the deposition height settled at the saturated value with less dispersion.

3.4. Dependence of the deposition rate on the irradiation time

The dependence of the deposition rate on the irradiation time was investigated by varying the APPJ irradiation time from 1 to 8 s. The flow rates of the He source gas and O₂ carrier gas were 400 and 10 sccm, respectively. For the APPJ discharge, the amplitude of the applied voltage was 3.8 kV_{p-p}, the frequency was 7 kHz, and the pulse duty ratio was 50%. The distance between the pipette tip and substrate surface was 600 nm. Figures 6(a)–(d) show the SPM images and line profiles at irradiation times of 1, 3, 6, and 8 s, respectively. Figures 6(e) and (f) show the dependence of the deposit height and width on the APPJ irradiation time, respectively. The error bars show the maximum and minimum values, and the plots depict the mean values (n = 3). The height and width of the deposit increased with increasing irradiation time. This indicates that the amount of deposits can be controlled by varying the irradiation time. However, the rate of increase in the deposition height gradually decreased with a further increase in the irradiation time. At irradiation times of less than 3 s, the growth rate of the deposition height was approximately 100 nm s⁻¹. In contrast, the growth rate of the deposition height was less than 30 nm s⁻¹ for irradiation times longer than 3 s. In this deposition method, HMDSO vapor was added to the APPJ from outside the nanopipette. Hence, the concentration distribution of the HMDSO vapor might be lower in the immediate vicinity of the pipette tip aperture because of the strong flow of the He source gas ejected from the pipette aperture. In addition, at irradiation times of less than 3 s, the top of the deposit is located far from the aperture of the nanopipette and the HMDSO vapor was sufficiently mixed in this region for efficient deposition. However, at an irradiation time of approximately 3 s, the height of the deposit reached approximately 400 nm, and at longer irradiation times, it tended to saturate. As mentioned above, HMDSO was not sufficiently mixed near the pipette aperture; thus, the efficiency of HMDSO deposition significantly decreased after irradiation for more than 3 s. Even after increasing the irradiation time, the deposition height remained saturated at a position of approximately 100–200 nm below the pipette tip. As discussed in sections 3.2, 3.3, and 3.5, the irradiation time was set to 15 s to ensure that the deposition height settled at the saturated value with less dispersion.
Figure 5. Dependence of the deposition height on the $O_2$ carrier gas flow rate of the HMDSO vapor. (a)–(d) SPM images and line profiles of the deposited dots when the flow rate of the $O_2$ carrier gas was 0, 4, 6, and 10 sccm, respectively. (e) Deposition height of the dots as a function of the carrier gas flow rate. (f) Deposition width (FWHM) of the dots as a function of the carrier gas flow rate.

is less than 1000 nm, the plasma jet reaches the substrate, which is produced by the decomposition of HMDSO in the plasma, is deposited on the substrate surface, and the deposits grow close to the nanopipette aperture. However, when the irradiation distance was more than 1000 nm, the plasma jet could not reach the substrate. As a result, the decomposition products are blown away and widely scattered by the gas flow, and subsequently deposited, resulting in a significant decrease in the deposition efficiency. Therefore, to control the amount of material deposited on the substrate, the plasma irradiation distance should be precisely controlled using the SPM system.

4. Discussion

As described above, the amount of $SiO_x$ deposition depends on several parameters, such as the flow rate of the carrier gas of the HMDSO vapor, irradiation time of the APPJ, and irradiation distance from the nanopipette, indicating that the material deposition rate can be controlled by varying these parameters.

The irradiation distance that can be deposited can be slightly extended by increasing the He flow rate of the plasma source gas. However, on increasing the He flow rate, the gas did not mix with the HMDSO gas near the pipette aperture because of the strong gas flow, resulting in a decrease in the processing accuracy of the deposited film. In addition, when the flow rate was excessively low, the plasma became unstable. Therefore, to ensure stable plasma and relatively accurate deposition near the pipette tip, a He flow rate of 400 sccm was set as the optimal flow rate in this experiment.

As for the deposition rate compared with existing methods, the deposition rate of the $SiO_x$ films by PE-CVD using general low-pressure plasma is several tens of nm/min, with a power consumption of several tens to several hundred watts [49, 50]. In the case of the APP, the deposition rate is several tens of nm/s, with a power consumption of several hundred watts [51–53]. By contrast, in the proposed method, as shown in figure 7, the deposition height reached 700 nm when the irradiation distance was 1000 nm, which corresponds to an average deposition rate of 46 nm s$^{-1}$ for an irradiation time of 15 s. The power consumption of the local irradiation of APPJ...
using the nanopipette in this system was estimated to be 0.8 W based on the measured current and voltage; this is consistent with the reported power consumption of less than 1 W for similar APPJ irradiation systems using nanopipettes [54]. Thus, the proposed method can achieve a high deposition rate with low power consumption.

With regard to the processing accuracy of the deposition using this method, the error bars shown for the deposition heights in figures 5(e)–7(e) show that the difference between the average value and the maximum or minimum value is approximately 10%. However, some of the differences were as large as 30%. This may be due to the variability in the plasma intensity. It is difficult to adjust the flow rate of the He source gas introduced into the nanopipette, and the amount of irradiation from the pipette tip aperture is likely to vary slightly, resulting in variations in the plasma intensity. It has also been reported that the O₂ used for the addition of HMDSO destabilizes plasma operation [55]. In addition, factors that cause SiO₂ microcrystals to be blown off the substrate (without adhering to it) by the gas flow may also cause variations in the amount of deposition. Therefore, to improve the processing accuracy, it is necessary to optimize various parameters within the range of stabilizing the plasma intensity.

The sub-micrometer-scale PE-CVD technique based on the nanopipette SPM developed in this study can be used to develop fine deposition methods for various materials using other additive gases and is expected to be applied to various fields, such as maskless patterning of microdevices. One of the potential applications of the proposed method is post-fabrication technology to compensate for the process variations in MEMS manufacturing. Process variations, such as the structural material not being deposited uniformly or not being etched accurately, often occur in MEMS manufacturing. As a result, the mechanical and electrical characteristics differ from the design specifications. Therefore, to improve the yield rate and manufacture devices that meet the design specifications, it is necessary to deposit materials locally on a part of the positioned structure as a post-processing modification. For example, tuning the resonant frequency of a MEMS resonator [56–58], which is widely used in sensors, filters, and vibration...
power generation, via local deposition on the vibrating body, is an effective application of the proposed technique.

5. Conclusion

We developed a sub-micrometer-scale PE-CVD technique using a nanopipette as a nozzle for APPJ and a probe for SPM. By adding HMDSO vapor to the APPJ irradiated from the nanopipette aperture, HMDSO was decomposed and deposited on the substrate. EDS analysis and compositional mapping of the locally deposited film showed that the deposited film was mainly composed of Si and O, confirming the decomposition of the HMDSO vapors by the APPJ and their deposition as SiO$_x$. The deposition process using the nanopipette with a sub-micrometer aperture demonstrated reproducible material deposition with a sub-micrometer width using the proposed method. The deposit height increased with an increase in the flow rate of the O$_2$ carrier gas of the HMDSO vapor and the irradiation time of the APPJ. When the distance between the pipette and substrate was varied, the deposition height increased with an increase in the irradiation distance up to 1000 nm, where the APPJ emitted from the nanopipette aperture reached the substrate. Therefore, by optimizing these parameters, the proposed method could enable fine patterning with a controllable amount of material deposition.

Data availability statement

All data that support the findings of this study are included within the article (and any supplementary files).

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