Thermal Annealing and Laser Treatment of Sol-gel Derived Zirconia Thin Films

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Abstract
Soluble precursor powders were prepared from zirconium propoxide and acetylacetone by evaporation of volatile products directly after the hydrolysis step. Dissolution of the solid residue resulted in solutions that were further processed by dip coating on glass substrates. One set of as-dried films was thermally annealed in an oven at temperatures between 300 and 600°C. In parallel, samples were irradiated by a CO₂ laser, in doing so laser power density and beam feed rate were varied. The thermally cured and laser treated film series were characterized with respect to film thickness, refractive index, phase content, crystallite size and film microstructure.

Keywords ZrO₂ · Thin films · Thermal curing · Laser processing · Microstructure

Introduction
The preparation of inorganic thin films by sol-gel processing has proven to be a flexible and cost-efficient alternative to vacuum-based technologies such as sputtering [1, 2]. The development of wet-chemical coating solutions with a sufficient stability under industrial conditions, however, is a challenging task. In this context the use of soluble precursor powders has been established for film compositions ranging from Al₂O₃ [3], TiO₂ [4], ZrO₂ [5] to lead zirconate titanate (PZT) [6]. As usual for such inorganic compositions film densification and crystallization were performed by thermal annealing.

As an alternative to oven treatment, sol-gel derived films may be annealed by irradiation with a laser source. Different lasers such as ArF [7, 8], KrF [7, 9–14], HeCd [15] and frequency tripled NdYAG [16, 17] operating at wavelengths below 1 μm have been used. In these cases, selective energy transfer to the film material is assumed which may enable the use of polymer substrates that may not withstand thermal sintering above 150°C. Even though this objective is commonly claimed, in most of
the above studies inorganic substrates were used. This is so because organic residues were removed from the films by thermal treatment up to 500°C before the final laser irradiation.

For sintering of sol-gel films on glass and silica substrates the use of CO₂ lasers with a wavelength of 10.6 μm has been reported [18–21]. As these glasses strongly absorb in this spectral range [22, 23], an indirect heating of the above sol-gel films can be assumed. The local temperatures may well exceed the respective softening point of the glass substrate. Therefore, crystal phases that are not accessible by oven treatment may become accessible [19, 24–26].

In a previous publication [27] we systematically compared the CO₂ laser treatment of TiO₂ films derived from soluble precursor powders to parallel thermal annealing experiments. Laser power density could well be correlated to furnace temperatures in terms of film thickness and refractive index. However, whereas conventional thermal heating resulted in the anatase phase, exclusively rutile was found in films after laser treatment. In this manuscript we extend these systematic investigations to sol-gel derived coatings of zirconia (ZrO₂) composition.

**Experimental Procedure**

**Film Preparation**

Soluble ZrO₂ precursor powders were prepared similar to a procedure previously established for TiO₂ [4, 27]: By slow addition of 103.5 g (1.0 mol) acetylacetone to 485.6 g (1.0 mol) zirconium (IV)-propoxide a clear honey yellow solution was obtained which was heated up to 80°C for one hour. Subsequently, 54.0 g (3.0 mol) deionized water was added. Without any further delay all volatile components were separated from the reaction mixture by rotational evaporation at reduced pressure (< 40 mbar) with a maximum bath temperature of 80°C.

The coating solution was prepared by dissolution of this amorphous precursor powder in a mixture of 90 mass % ethanol and 10 mass % 1,5-pentanediol to result in an oxide yield of 6 mass % respective to crystalline ZrO₂. After stirring for 12 h it was filtered through a 0.45 μm membrane.

Thin films were deposited by dip coating of borosilicate glass (Schott, Borofloat®, 3.3 * 100 * 100 mm³) that was pre-cleaned in a laboratory dishwasher using an alkaline detergent. Coating experiments were performed within 8 h after cleaning. Directly before film deposition the substrates were additionally cleaned with compressed air.

Thin film preparation was carried out in clean room atmosphere at 24°C. The coating was made with a withdrawal rate resulting in a film thickness of 120 nm after sintering at 600°C. The as-coated plates remained in a fume hood for at least two minutes before they were dried in a vented furnace at 80°C for one hour.

**Thermal Annealing**

Directly after the drying, calcinations of the sol-gel films were achieved by rapid thermal annealing (RTA) for 10 min using a vented oven pre-heated to temperatures between 300 and 600°C.)
Laser Treatment

The films dried at 80°C were shipped from Fraunhofer ISC Würzburg to LZH Hanover where laser treatment was performed. A CO$_2$ laser with the wavelength of 10.6 μm (Firestar ti-60, Synrad, Inc.) with a maximum power of 35 W was used. The quasi-continuous mode operated with a repetition rate of 10 kHz. The beam with a diameter of approximately 200 μm was focused on the samples by a galvanometer scanner and a f-theta lens with a focal length of 324 mm. Feed rates ranging from 500 mm/s to 3000 mm/s and a hatch of 200 μm between the laser lines were applied. Using these parameters the laser power density was varied between 64 W/mm$^2$ and 605 W/mm$^2$ by varying the duty cycle.

Material Characterization

Reflection curves were measured with a UV-Vis-spectrometer (Shimadzu UV-3100, Kyoto, Japan) in the range of 300 nm − 1700 nm. Analysis of the single layers was achieved using the Fresnel equations for vertical incidence and the interference law. So refractive index and layer thickness could be calculated by regarding the evaluable extremes of reflection. Details about this technique can be found in [28].

The films were characterized by X-ray diffractometry (XRD; Empyrean, Malvern Panalytical Ltd, United Kingdom) with regard to phase development. Grazing incidence X-ray diffractometry was performed at an incidence angle of 1°. Crystallite sizes were calculated using the Scherrer equation.

For microstructural analysis, scanning electron microscopy (SEM), (Supra 55VP, Carl Zeiss AG, Oberkochen, Germany) was used. Some samples were mechanically fractured in order to take images of cross-sections. All specimen were sputtered with platinum prior to the examination.

Results and Discussion

Thin films in ZrO$_2$ composition were deposited on borosilicate glass substrates by dip coating. After thermal annealing their thickness and refractive index was measured. From Fig. 1 it can be seen that up to 450 ° a steady consolidation from 350 nm to 125 nm is induced, up to 600°C a constant level is maintained. In parallel the refractive index of the film rises from 1,55 to 1,95 as the annealing temperature is increased.

In Fig. 1b the SEM cross-sectional view of a ZrO$_2$ coating that had been thermally annealed at 600°C is given. The granular microstructure is very similar to those of its alumina [3] and titania [27, 29] counterparts. Obviously, despite their different compositions and crystallinity sol-gel processing of soluble precursor powders results in comparable textural film features.

With a constant feed rate of 500 mm/s the laser power density was varied for the irradiation of ZrO$_2$ films that only had undergone drying at 80°C. In Fig. 2a the resulting film thickness is given along with the values for the parallel thermal treatment experiments. The course of the respective data can well be correlated with each other: For a laser power density of 65 W/mm$^2$ the shrinkage is similar to samples that only had been dried at 80°C. For 415 W/mm$^2$ a densification equal to thermal annealing at
600°C is observed. For the evaluation of the refractive index (Fig. 2b) a similar good correspondence between the two experimental series can be seen: Values of 1.95 are measured for a laser power density of 415 W/mm² corresponding to annealing temperatures of 500 to 600°C.

It has to be emphasized that the laser irradiation in our study is done on as-dried sol-gel coatings and the removal of residual organics as well as densification/crystallization is done in a single irradiation step. In contrast to that most of the previous reports in the literature perform laser sintering on coatings that had experienced pre-treatment in a furnace at temperatures between 300 and 500°C [7, 10, 15, 17, 19, 20, 25, 26].

X-ray diffraction (XRD) experiments were performed on the films in order to determine the crystal phases present. After furnace treatment (Fig. 3a) up to 400°C the coatings remain amorphous, at 450°C first diffraction pattern corresponding to the tetragonal phase of ZrO₂ become apparent. At 500°C the peak intensity increases, above 550°C a saturation is observed. No monoclinic ZrO₂ is observed which corresponds to other sol-gel derived...
coatings after annealing at 500°C [30]. In contrast to that report, however, our films remain free from cracks throughout thermal processing.

Laser treatment at 64 W/mm² results in the first appearance of tetragonal ZrO$_2$ (Fig. 3b), above that laser power density this phase coexists with monoclinic ZrO$_2$. The appearance of this thermodynamically more stable modification takes place in sol-gel derived films at temperatures exceeding 600°C [31, 32]. It therefore can be concluded that the local temperatures during laser sintering well exceed 600°C as suggested by theoretical simulations [19, 23] where surface temperatures exceeding 1000°C were calculated. In addition, it has been found that the crystallization of monoclinic ZrO$_2$ is favored by high heating rates [33].

As an intermediate result, it has to be noted, that different crystalline phases and thus differences in microstructure result from thermal annealing and CO$_2$ laser treatment, even though the film thickness and refractive index (Fig. 2) on first sight suggested matchable trends.

In our previous investigation on TiO$_2$ films, a similar behavior was observed: Laser treatment resulted solely in formation of the thermodynamically stable rutile phase, whereas in conventional thermal annealing only phase-pure anatase was found [27].

It appears from Fig. 3b that the peak intensity decreases when the laser power density is raised to 605 W/mm². This observation may indicate the removal of film material by ablation at high energies as previously reported [34].

The crystal sizes as calculated from the peak width of Fig. 3 by the Scherrer equation are given in Fig. 4. Thermal annealing between 500 and 600°C results in crystallites of tetragonal ZrO$_2$ with sizes between 15 nm and 20 nm. These diameters basically conform to the size of granular structures found in Fig. 1b. For laser annealing with power densities below 300 W/mm² tetragonal grains in the same order of magnitude are found. Above 300 W/mm² tetragonal and monoclinic ZrO$_2$ coexist with grain sizes exceeding the values measured for films that had undergone thermal treatment. This observation supports the assumption that the local temperatures during laser irradiation significantly exceed 600°C.
For a given laser power density the beam feed rate determines the photon fluence, in a manner of speaking the local energy input to the substrate: The faster a given beam traverses, the smaller the power delivered to the surface.

With a power density of 414 W/mm² and a feed rate of 500 mm/s a film densification similar to that of thermal sintering at 600°C was obtained (Fig. 2). With this given power output the feed rate of the laser beam was varied from 500 mm/s to 4000 mm/s. In Fig. 5a the resulting ZrO₂ film thickness is compared to that resulting from conventional furnace processing. It can be seen that the laser irradiation can precisely emulate the thermal film densification. The same applies for the refractive index of the ZrO₂ coatings (Fig. 5b).

XRD phase analysis was performed on this sample series. From Fig. 6a it can be seen that a feed rate of 500 mm/s results in a certain ratio of monoclinic to tetragonal reflex intensity, that is shifted to tetragonal ZrO₂ at higher feed rates. At 1500 mm/s the tetragonal phase is detected almost exclusively. Obviously, the energy input under these conditions does not facilitate the formation of the thermodynamically more stable monoclinic phase any more. When the feed rate is raised to 3000 mm/s, the diffraction signal corresponding to tetragonal ZrO₂ is transformed to a broad hump indicating a low level of crystallinity.

Crystallite size analysis reveals that for feed rates of 500 mm/s and 1000 mm/s tetragonal and monoclinic grains with diameters exceeding 30 nm coexist. For thermal treatment between 500 and 600°C only tetragonal crystallites with diameters between 15 nm and 20 nm were found.

Structural uniformity is a key feature for the technical application of thin films. In Fig. 7a representative SEM image for a laser-processed ZrO₂ film is given. In general, no distinctive border between adjacent laser lines (hatch 200 μm) can be distinguished.
Within the beam center, some defects are located inside a zone of 70 μm width. The cross-sectional view reveals that in this region the ZrO$_2$ film spans bubbles that extend into the substrate. The defects obviously result from partial flaking of such ZrO$_2$ film domes. This observation suggests that the glass substrate is substantially liquefied by the high temperatures that is induced by laser processing. The bubbles are presumably generated by gaseous products that result during the pyrolysis of the sol-gel film. Outside the central defective zone, however, the ZrO$_2$ film appears homogeneous and uniform similar to samples that have been thermally annealed (Fig. 1b).

Some similar features have been observed for laser-treated TiO$_2$ films previously studied [27]. In contrast to that report, however, no evidence for partial ZrO$_2$ removal...

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**Fig. 5** Thickness (a) and refractive index (b) of ZrO$_2$ films that had undergone thermal annealing (black) and laser treatment (blue). The laser power density was fixed at 414 W/mm$^2$ whereas the beam feed rate was varied as indicated.

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**Fig. 6** X-ray diffraction pattern of ZrO$_2$ films treated with a laser power density fixed at 414 W/mm$^2$ and a beam feed rate varied as indicated (a). In (b) the resulting crystal sizes (blue) are compared to values observed after thermal annealing (black).
by ablation could be observed here even though identical laser parameters have been applied. In the whole the ZrO$_2$ material seems to be more damage resistant than TiO$_2$ [27].

**Conclusions**

ZrO$_2$ sol-gel coatings can successfully be processed by conventional thermal annealing and CO$_2$ laser treatment. Film properties such as film thickness, refractive index and grain size systematically correlate with laser power density and beam feed rate. Results indicate that laser irradiation locally induces substrate temperatures by far exceeding 600°C that lead to the coexistence of the monoclinic and tetragonal phase of ZrO$_2$.

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Compliance with Ethical Standards  

Conflict of Interest  The authors declare that they have no competing interests.

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