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Fast time-scale average for a mesoscopic high cycle fatigue criterion

Stefano Bosia a,b,*, Andrei Constantinescu a

a Laboratoire de Mécanique des Solides, CNRS – Ecole Polytechnique, 91128 Palaiseau cedex, France
b Dipartimento di Matematica “F.Brioschi”, Politecnico di Milano, Piazza Leonardo da Vinci 32, 20133 Milano, Italy

The paper discusses the lifetime prediction of structures in high-cycle fatigue based on the two-scale fatigue criteria of Dang Van type and several of its extensions in finite lifetime regime. The main assumptions for this criterion are (i) the material is polycrystalline and undergoes localised plasticity in one of the misoriented grains and (ii) crack initiation arises as a consequence of cumulated plasticity in this grain.

The novelty of the presented approach is twofold. On the one hand a generalisation of mesoscopic plasticity model is presented, on the other a fast time scale average is introduced for tracking the cyclic material behaviour and the subsequent evolution of damage. The tracking method is based on the split between a quick quasi-periodic response of the system to the cyclic load and a slow evolution of the internal hardening and damage parameters of the material at the mesoscopic scale. The proposed method can be extended to a large class of local material behaviours involving not only plasticity, but also crack and damage evolution.

The paper proposes a simplified plasticity-based model for the mesoscopic material behaviour and presents a comparison between predicted and experimental lifetimes. The results are discussed in terms of prediction capabilities and also in terms of the identification procedure of parameters of the mesoscopic model.

1. Introduction

A series of fatigue prediction models for the cyclic behaviour of structures is based on multiscale analysis. These try to bridge the gap between the fine evolution of the defects at the scale of the microstructure and the load transmitted from the macroscopic scale of the structure. The analysis usually involves homogenisation techniques for the smaller scales and is based on the concept of shakedown. This amounts to characterising the cyclic behaviour through an asymptotic limit cycle, which is either plastic or elastic denoting respectively presence or absence of dissipation.

This paper addresses the question of finite lifetime in the high cycle fatigue (HCF) regime for metallic polycrystalline materials. Within HCF, it is common to assume that the structure is in elastic shakedown at the macroscopic scale but undergoes elastic or plastic shakedown at the mesoscale (i.e. scale of the grains) for infinite or finite lifetime respectively. In the case of finite lifetime, we will refer to the time to failure of the material with the expression lifetime.

In this general framework, the initial fatigue criterion proposed by Dang Van (DVK) in [6] (and extended in [21–25]) has been highly successful in predicting the infinite lifetime of structures. The DVK fatigue criterion decides whether or not the structure will have an infinite lifetime by considering the shakedown limit of the stress system in the different grains. This approach was expressed later in a more general term through the Melan–Koiter shakedown theorem (see [7,19] and references therein). The hydrostatic stress is considered in order to account for the local heterogenous structure. This has only recently been justified using a precise homogenisation procedure [3,15].

In order to give quantitative estimates of the lifetime, several extensions of the DVK criterion have been proposed. Among others we recall the models of Morel [16,17] and of Maitournam et al. [11,13]. In the first case, a simple mesoscopic plastic model is introduced. The evolution of the cumulated plastic strain up to final failure at the mesoscopic level is evaluated to effectively predict lifetime under cyclic and variable loading. The second model differs from this approach by (i) proposing a mesoscopic plastic model depending on the hydrostatic stress component to account for the damage process; (ii) estimating the plastic shakedown cycle at the mesoscopic scale using a classical fatigue criterion based on the range of plastic strain.

The extension discussed in this paper is constructed under similar assumptions to those of Morel’s model [16,17]. However, it is grounded on a generalisation of the mesoscopic plasticity model and introduces a new fast time scale average for tracking the cyclic
material behaviour and the subsequent evolution of damage. This separation of time scales is justified by the great number of cycles usually considered in HCF experiments \((10^4 \text{–} 10^7 \text{ cycles})\). The cyclic material behaviour can be viewed as the succession of (a) a short hardening (or softening) transient up to a saturation point, (b) a long phase close to a stable cycle and (c) a final brief softening predicting failure. The long transient observed in the second phase above can be described through the theory of dynamical systems as the presence of a saddle-node ghost (see [26] and references therein) and is therefore amenable to precise analytical study.

The paper starts with a short presentation of the two scale model used in the HCF theory. We then introduce three different constitutive laws and the relative techniques to compute lifetimes. In particular we discuss: (i) Maitournam’s et al., (ii) Morel’s, and (iii) the present model. Sections 2 and 3 discuss the main analytical tools from dynamical systems theory, namely separation of time-scales and saddle-node ghost estimates. In Section 4 the identification method for the parameters of the model is detailed. Finally Sections 5 and 6 present the prediction capabilities for experiments extracted from literature and conclusions. An appendix completes the presentation with an extended computation of the lifetime using the saddle-node ghost estimates.

### 2. The models at the mesoscopic scale

In the framework of HCF for metallic polycristalline materials, one can assume that only a few grains of the material undergo plastic deformations whilst most of the material remains elastic. We can therefore consider the material point at the macroscopic scale as a representative elementary volume (REV) at the mesoscopic scale. This volume is a non-homogeneous medium, which can be assimilated under the given assumptions to an elastic matrix and an elasto-plastic inclusion (grain).

The loading of the REV, i.e. macroscopic stresses \(\Sigma\) and strains \(E\), can be computed in the framework of the standard continuum theory (macroscale) and will be considered as given in this work. In order to evaluate the mesoscopic state, i.e. mesoscopic stresses \(\epsilon\) and strains \(\epsilon\), several homogenisation techniques have been considered in the literature. The models of Bui, Lin–Taylor, Kröner–Budansky–Wu and Sachs have been described in relation with the DVK fatigue criterion for example in [2,7,11,13].

Without restraining the generality, we shall adopt here the Lin–Taylor's homogenisation scheme, which is based on the equality of macroscopic and mesoscopic strain:

\[ \epsilon = E. \]

As pointed out by Dang Van (see [5,7] and references therein), when dealing with the description of HCF, Lin–Taylor’s approximation is particularly effective as it permits to accept the existence of mesoscopic plastic strain and residual stress fields. Therefore, we will limit the presentation to this particular case.

Let us denote by \(C\) and \(c\) the macroscopic and mesoscopic elasticity tensor, and by \(I\) and \(l\) the macroscopic and mesoscopic compliance tensors. For completeness reasons we also introduce both the mesoscopic plastic strain tensor \(\epsilon^p\) and the macroscopic plastic strain tensor \(E^p\). However, as in HCF the structure is in elastic shakedown at the macroscopic level, it follows that (see Fig. 1)

\[ E^p = 0. \]

With this notation the main assumptions of Lin–Taylor’s model are equality of macroscopic and mesoscopic elasticity tensors and equality of the respective strains:

\[ C = c \quad E = \epsilon. \]

Assuming that the behaviour at the macroscopic scale is purely elastic, from the expressions of the elastic Hooke’s law at the macroscopic and mesoscopic scale we deduce

\[ \sigma = \Delta \Sigma - AC(\epsilon^p - E^p) \]

where the fourth-order tensor \(A\) is the localisation tensor defined by \(A = c : L\).
The next step in the modelling is the introduction of a suitable material behaviour at the mesoscale in order to take into account fatigue. The experimental evidence leads to consider a three-phase model involving an initial hardening (or softening) phase, followed by a stable saturation phase and a final softening [18,16,17] as schematically displayed in Fig. 2. Under these assumptions, failure corresponds to vanishing mesoscopic yield limit. As the yield limit is directly related to the cumulated plastic mesostrain, denoted by $\Gamma$ hereafter (see Eq. (8) below), one can also express failure as limit of plastic strain denoted by $\mathcal{C}$.

Assuming further that only one glide plane is active for any plastically deforming inclusion of the medium (grain), it has been to be a concave function increasing when cyclic material behaviour previously introduced, one has to require $\mathcal{C}$ to be a concave function increasing when $\mathcal{F}$ is small and decreasing for larger values of the mesoscale shear plastic strain. Moreover there will be a unique value for the cumulated plastic mesostrain denoted by $\mathcal{F}$ for which the following hold:

$$G(\mathcal{F}) = 0, \quad G(\mathcal{F})' < 0.$$  

In this terms, the lifetime defined as the failure of the REV, or equivalently as the initiation of a macroscopic crack is defined as the unique time instant $\mathcal{T}$ for which $\Gamma(\mathcal{T}) = \Gamma$. As a consequence of the definition of $\Gamma$, one can equally express the lifetime by a vanishing plastic yield at the mesoscale (see (4)).

A large panel of choice for the definition of the yield function $f$ and for the evolution of the yield limit $\tau_y$ is possible. Among the different models proposed in the literature, we shall only recall the proposals of Maitournam et al. and the one of Morel.

2.1. Maitournam’s model [13]

The proposal of this model is to consider a plastic material behaviour at the mesoscale with a dependence of the yield function not only on the deviatoric part of the stress but also on the hydrostatic part. A kinematic hardening under the assumptions of associative plasticity is also considered. The mesoscopic yield function can therefore be written as

$$f(\mathbf{\sigma}, \mathbf{e}_p, \tau) = \frac{1}{2} (\mathbf{\sigma} - h \mathbf{e}_p) : (\mathbf{\sigma} - h \mathbf{e}_p) - k(p)$$

with

$$k(p) = \beta - \gamma p(t) \quad \text{or} \quad k(p) = \begin{cases} 
\beta - \gamma p & \text{if } p \geq 0 \\
\beta - \gamma p & \text{if } p < 0
\end{cases}$$

and where $p$ is the mesoscopic hydrostatic stress, $\mathbf{e}_p$ is the deviatoric part of the mesoscopic plastic strain tensor and $\alpha, \beta, \gamma$ and $h$ are suitable parameters.

The underlying hypothesis of this model consider that the mesostructure can be computed from the macroscopic structure. Failure will then be determined from the plastic shakedown cycle and from a phenomenological fatigue law linking lifetime and cumulated mesoscopic plastic strain ($\mathcal{C}$):

$$N = g(\mathcal{C})$$

which is a Manson–Coffin type fatigue criterion.

2.2. Morel’s model [16,17]

This model considers a complete description for the mesoscopic plastic yield limit as introduced above. Three sharply separated phases account for the hardening of the mesoscopic inclusion. The dependence of the yield limit on plastic strain is piece-wise linear (see Fig. 3). Moreover, the yield function is defined in terms of the resolved shear stress and has both isotropic and kinematic hardening terms:

$$f(\mathbf{\tau}, \mathbf{b}, \tau_y) = (\mathbf{\tau} - \mathbf{b}) : (\mathbf{\tau} - \mathbf{b}) - \tau_y^2.$$  

In this case, the three phase of the plastic inclusion are defined as:

$$\tau_y = \begin{cases} 
\gamma & \text{during hardening:} \\
0 & \text{during the saturation phase:} \\
-h & \text{during softening:}
\end{cases}$$

$$\mathbf{b} = c\mathbf{\tau}$$

where $\mathbf{\tau}$ is the mesoscopic shear plastic strain and $\mathcal{F}$ is the cumulated plastic mesostrain given by

$$\mathcal{F} = \sqrt{\gamma^2 + \mathbf{\tau}^2}.$$
2.3. Power law model

The model used in this work replaces the piecewise-linear dependence in the evolution of the yield limit with a power law. When compared with the model of Morel, one immediately notices the advantages arising from the piecewise-linear description. Indeed, in this latter case, for periodic macroscopic loadings it is possible to obtain explicitly the lifetime (see [16]). However, the hardening rule (7) is a rough approximation of the actual behaviour of materials, for which the sharp transitions between hardening and saturation regimes as well as from saturation to softening regimes are difficult to justify.

An alternative model is given by the following constitutive power law

\[ G(\Gamma) = \frac{\Delta T_0}{2} - \frac{|\Gamma - \Gamma_0|^{\alpha}}{\beta} \]  

(9)

with \( \alpha > 1 \), which naturally satisfies the constraints of concavity and monotonicity introduced above (see Fig. 3).

When compared with the piecewise linear model of Morel, one cannot hope to retrieve exact lifetime estimates for this model. However, as we shall see below, precise a priori analytical estimates can be derived in this setting under mild regularity assumptions on the behaviour of the function \( G \), which are satisfied by the power law (9). Before delving into the details of such estimates, we will derive a suitable approximation for the just introduced constitutive laws in the case of periodic loadings. In particular, we now want to consider a time-average over each cycle of the loading.

3. Separation of time scales

In the regime of HCF we can distinguish between a quick quasi-periodic response of the system to the cyclic charge and a slow evolution of the inner parameter describing the hardening and damage of the material itself. This separation of time scales is justified by the great number of cycles usually considered in HCF experiments (10^4–10^7 cycles). It seems therefore sound to look for a slowly-varying approximation for this internal variable and for the cumulated plastic mesostrain \( \Gamma \), by averaging out the periodic behaviour of the system. This process is also known as “time-homogenisation” (see [1,10]).

By differentiating the yield function (6) with respect to time we obtain:

\[ \dot{\Gamma} = 2(\tau - b) \cdot \dot{\tau} + 2(b - \tau) \cdot b - 2\tau_y \dot{\tau}_y. \]

Since during plastic deformations the yield function \( f \) is constant \((f = 0)\), by recalling relation (2), we deduce

\[ \dot{T} - \mu^p \dot{\eta} - c^p \eta = g(\Gamma) \dot{\Gamma} \]

where we have set \( \eta = \eta^p \mathbf{m} \).

From definition (8) we have

\[ \dot{\Gamma} = \frac{|\dot{\tau}|}{g(\Gamma) + c + \mu} \]

and therefore

\[ \dot{\Gamma} = \frac{\eta}{g(\Gamma) + c + \mu} \]

which represents the evolution law for the cumulated plastic mesostrain during plastic deformations. Obviously \( \dot{\Gamma} \) is constant during the elastic part of the loading so that we can deduce the following ordinary differential equation describing the evolution of the cumulated plastic mesostrain

\[ \dot{\Gamma} = \begin{cases} \frac{\eta}{g(\Gamma) + c + \mu} & \text{when } f = 0, \\ 0 & \text{when } f < 0. \end{cases} \]

(10)

We recall that the cumulated plastic mesostrain \( \Gamma \) is a nondecreasing function of time also if the resolved plastic mesostrain \( \eta^p \) oscillates. Indeed, \( \Gamma \) accounts for all the plastic deformations the material has endured up to the current time.

We now want to simplify the evolution law (10) in the special case of cyclic loadings. By the above discussion it is easy to see that under a periodic loading of equivalent amplitude comparable to \( \Delta T_0 \), the plastic mesostrain changes only slightly during one charge/discharge cycle. Therefore, the increase per cycle of the cumulated plastic mesostrain is small when compared with the variation of the mesoscopic strain. This justifies us stating that the evolution of cumulated plastic strain is slow with respect to the evolution of the mesoscopic strain. As a consequence, we can assume that \( \dot{\Gamma} \) constant during each cycle.

By considering \( \dot{\Gamma} \) constant during one period of the forcing term, we can decouple the quick dynamic of the elasto-plastic response of the material to the external loading and the slow evolution of the internal damaging mechanism (i.e. the slow drift of \( \Gamma \)). We denote by \( \Delta T \) the amplitude of the macroscopic resolved shear stress. In order to integrate (10) on a single cycle, we observe that during a complete unloading–loading phase from \( -\Delta T/2 \) to \( \Delta T/2 \), the mesoscopic inclusion will be in elastic regime \( f < 0 \) up to \( T = -\Delta T/2 + 2\tau_y \), therefore, we obtain (see Fig. 4 and [17, Appendix A])

\[ \int_{f=0}^{\Delta T/2} \dot{T} = \frac{\Delta T}{2} - \left( -\frac{\Delta T}{2} + 2\tau_y \right) = \Delta T - 2\tau_y. \]

By taking into account the second half of the loading cycle (i.e. the transition of \( f \) from \( \Delta T/2 \) to \( -\Delta T/2 \)), and using this result in (10) we finally have

\[ \dot{\Gamma} = \begin{cases} \frac{\eta}{g(\Gamma) + c + \mu} & \text{when } f = 0, \\ 0 & \text{when } f < 0. \end{cases} \]

(10)
We now want to particularise the above results by choosing as con-
ting parameter the “flatness” of the hardening law (see [16,17]). Indeed, we obtain
\[ g(\Gamma) = -\frac{\pi}{\beta} |\Gamma - \Gamma_0|^{\frac{1}{4}} \sin^2 \frac{\pi}{2} \]
so that our model (11) reduces to
\[
\begin{cases}
\Gamma' = \frac{4}{\beta + c + g(\Gamma)} \left( \frac{\Delta T}{2} - \tau_y(\Gamma) \right) \\
\tau_y = g(\Gamma) j 
\end{cases}
\]
and
\[
\Gamma(0) = 0.
\]
From the mathematical theory of dynamical systems an explicit lower (i.e. conservative) estimate can be deduced for the lifetime of the material (see Appendix A):
\[
\tau \geq \frac{\gamma_{\text{opt}}}{\gamma_{\text{opt}}} + \frac{\pi (\mu + c)}{2 \alpha \sin^2 \frac{\pi}{2}} \frac{(\Delta T - \Delta T_0)}{2} - \frac{1}{4(\alpha - 1)} \frac{1}{\gamma_{\text{opt}}} - 1
\]
where \( \gamma_{\text{opt}} \) is given by
\[
\gamma_{\text{opt}} = \frac{\pi (\mu + c)}{2(\mu + c) - \mu c} \left( \frac{2}{2} \frac{(\mu + c)}{\mu + c} \right) \sin^2 \frac{\pi}{2}
\]
In order to get some insight in this expression, we can consider its limit for great values of \( \alpha \), that is when the plateau of the saturation phase becomes flat. This corresponds to the setting of Morel’s works (see [16,17]). Indeed, we obtain
\[
\lim_{\alpha \to \infty} \gamma_{\text{opt}} = 2 \left( 2 - \frac{\alpha}{4(\alpha - 1)} \right) \approx 1
\]
and
\[
\lim_{\alpha \to \infty} \Gamma = \frac{\gamma_{\text{opt}}}{\gamma_{\text{opt}}} + \frac{\mu + c}{\Delta T - \Delta T_0} - 4 \frac{1}{\gamma_{\text{opt}}} - 1 \approx 2 \frac{(\mu + c)}{\Delta T - \Delta T_0}
\]
where the approximations at the end of the previous computations hold for small \( \Delta T - \Delta T_0 \). This estimate corresponds to [17, Equation (A9)].

Unfortunately, no simple and efficient expression could be derived for an analytical upper bound on the lifetime for our model.
5. Identification of the parameters from fatigue experiments

In the constitutive relation (9) for $G(T)$ and in Eq. (11), five different parameters appear: namely $\mu + c, \Delta T_0, f_0, \alpha$, and $\beta$. Moreover, since our model is essentially one-dimensional, $\Delta T$ has also to be evaluated starting from each 3D macroscopic loading state of interest.

In order to evaluate $\Delta T$ and $\Delta T_0$ we adopt the same approach used by Morel in [16]. Starting from the Dang Van criterion (see [5,6]), we assume that the material undergoes elastic shakedown if

$$\Delta T + S_{\text{max}}^m \leq B,$$

where $S_{\text{max}}^m$ is the maximum value reached by the mesoscopic (and macroscopic) hydrostatic stress during the periodic loading, while $\Delta T$ is a suitable measure of the resolved shear stress acting along the most solicited slip direction plane. In particular, we will use the following definition (see Morel [16] and Papadopoulos [22])

$$\Delta T = \max_{T(\theta, \phi)} T_{\sigma}(\theta, \phi)$$

where

$$T_{\sigma}(\theta, \phi) = \sqrt{\int_0^{2\pi} T_{\sigma}\left(\theta, \phi, \psi \right) \text{d}\psi}.$$  

Here $\theta$ and $\phi$ are angular variables used to identify the plane orthogonal to the versor

$$\mathbf{n} = \left(\sin \theta \cos \phi, \sin \theta \sin \phi, \cos \theta \right),$$

in the physical space, $\psi$ is an angle parametrizing all possible directions $\mathbf{m}$ in the slip plane identified by $\mathbf{n}$ and $T_{\sigma}(\theta, \phi, \psi)$ is the amplitude of the variation of the mesoscopic resolved shear stress $\sigma$ defined above.

The material parameters $A$ and $B$ can be related to the fatigue limits under fully reversed tension compression $f_{-1}$, and under fully reversed torsion $t_{-1}$:

$$A = \sqrt{\pi \left( t_{-1} - \frac{4}{9} \right)}, \quad B = \sqrt{\pi t_{-1}}.$$

In the simple case of sinusoidal loading, that is for loadings in the form

$$\Sigma = \begin{pmatrix} \sigma_{xx}^m + \sigma_{yy}^m \sin(\omega t) & \tau_{xy}^m \sin(\omega t + \phi) & 0 \\ \tau_{xy}^m \sin(\omega t + \phi) & \tau_{yy}^m \sin(\omega t + \phi) & 0 \\ 0 & 0 & 0 \end{pmatrix} \tag{15}$$

for a suitable reference frame, where $\sigma_{xx}^m$ is the mean normal stress in the $x$ direction, $\sigma_{yy}^m$ and $\tau_{xy}^m$ are the amplitude of the normal and shear stresses, $\Delta T$ and $\Delta T_0$ can be explicitly computed and are given by the following expressions:

- **In phase tension and torsion ($\phi = 90^\circ$)**

$$\Delta T_0 = \frac{t \cdot f_{-1} - (t_{-1} - \frac{4}{9}) \sigma_{xx}^m}{f_{-1} + (t_{-1} - \frac{4}{9}) \sqrt{\frac{\sigma_{yy}^m}{\tau_{xy}^m}}},$$

$$\Delta T = \frac{t \cdot f_{-1} - (t_{-1} - \frac{4}{9}) \sigma_{xx}^m}{f_{-1} \left( (\sigma_{xx}^m)^2 + (\tau_{xy}^m)^2 \right) + 2 \left( t_{-1} - \frac{4}{9} \right) \left( \tau_{xy}^m \right)^2} \cdot \sqrt{\frac{(\sigma_{xx}^m)^2 + (\tau_{xy}^m)^2}{2} \left( (\sigma_{yy}^m)^2 + (\tau_{xy}^m)^2 + (\tau_{xy}^m)^2 - 3 \left( \tau_{xy}^m \right)^2 \right)}}.$$

We now consider the other modelling parameters. We observe that the kinematic hardening parameter $c$ and the Lamé shear modulus $\mu$ may in principle be considered material constants already known from other experiments. However, in this work, we will identify them together with the other material constants appearing in (9) and (11): $G_0, \alpha$, and $\beta$. We note, moreover, that $\mu$ and $c$ always appear together in the above expressions (in particular, see Eq. (11)) so that only a joint estimate of the sum $\mu + c$ can be obtained with this model. The identification of these four remaining parameters will be achieved through optimisation of a suitable cost function (see e.g. [13]). Two choices seem natural in this context:

- minimising the sum of the squared errors between the experimental lifetimes and the simulated ones;
- minimising the sum of the squared relative errors between the experimental lifetimes and the simulated ones.

These two approaches have led to very similar results in the experimental validation of our model of the next sections. Following [13], we will therefore report only the results using the first of the two approaches.

6. Results and discussion

In order to assess the efficiency of the estimate for the predicted lifetime obtained above, we compared the numerical solution of system (11) describing the evolution of the cumulated mesoscopic plastic strain, to the analytical approximation of lifetime given by estimates (13) and (14). The complete integration of (11) was performed using a high-order Runge–Kutta scheme (in particular a Runge Kutta (4,5) method was used—see [14, routine ode45]). We emphasise that the estimate (13) is a lower bound for the lifetime and therefore it is a theoretical conservative estimate.

On account of the many different tests done, we report in Fig. 6 the results of some numerical experiments showing a good agreement of approximation (13) for physically meaningful parameters, when the "flatness" parameter $\alpha$ is large enough. In order to assess the efficiency of the analytical approximation deduced previously, we introduce the following efficiency ratio

$$\eta \equiv \text{lifetime obtained by numerical integration of (12)}.\tag{16}$$

We observe that values of $\eta$ near 1 correspond to efficient estimates and that if $\eta < 1$ the analytical bound is conservative. In particular, as soon as $\alpha$ is greater than 4 or 5, the approximation is efficient for all the values of $\Delta T - \Delta T_0$, which arise in experiments and which can be accounted for with this kind of model (usually $\Delta T - \Delta T_0 \approx 10^3 \div 10^4$ MPa for metallic materials). In order to keep the discussion as simple as possible, only integer values of $\alpha$ were considered here. However, $\alpha$ can be any real number greater than 1.

In Fig. 6 the behaviour of $\eta$ with respect to the load $\Delta T - \Delta T_0$ is shown. The different lines correspond to the representative values for $\alpha$, $\alpha = 2, 3, 4$ and 6. All other parameters are physically relevant and have been kept constant to ease comparison. In particular we have considered $T_0 = 66, \mu + c = 2,800,000$ MPa, $\beta = 70,000$ MPa$^{-1}, \Delta T_0 = 445$ MPa. The horizontal line at height 1 represents a
Moreover, a estimate (13) and the lifetime obtained by numerical integration of (12), see text (see [8,11,12,18,20]). In each case, we have used the data coming from simple tension compression tests (called training points in the sequel) to fit the parameters of the model and to make predictions for the other observations. The results of these experiments (predicted endurance limit vs. experimental values) can be found in Fig. 7. Data used to fit the model (training points) are highlighted in red, while the remaining observation used to check the model (control points) are in blue. In this plot the diagonal represents perfect agreement between the model and the experimental values, whereas the two dashed limes represent a factor 2 acceptable tolerance.

As can be seen from Fig. 7, the agreement between estimated and observed lifetimes is quite satisfactory. Most of the experimental points fall between the two dashed tolerance limes for a wide range of the experimental parameters and a variety of materials considered. Scatter of experimental data up to 3–5 times that of the fatigue curve is indeed typical of HCF, which is due to individual properties of the material local zones. That is why scatter of data presented in Fig. 7 can be considered as regular if individual properties of the specimen are not taken into account.

7. Conclusions

We have proposed a new model for the lifetime of materials in the HCF regime. This model is a refinement of the one introduced by Morel in [17] based on the DVK criterion. In particular, it provides a more thorough understanding of the basic phenomena and gives an explanation of the long transient behaviour observed in material between the initial accommodation and the final breakdown (or crack initiation).

Our approach allows us to consider a richer mesoscopic hardening rule than already done in the literature. As in [16,17] our model involves an initial hardening, a long saturation phase and a final softening leading to failure. The nonlinear power law proposed depends on five different parameters. The a priori analysis and the numerical tests reveal that the most relevant among the parameters is α, which describes the “flatness” of the hardening law. Moreover, α is directly related to the lifetime estimate (13). All the parameters of the mesoscopic model can be estimated using a simple and efficient least-square optimisation procedure. Nevertheless, study of the relations between more refined microscopic models and the parameters should be performed in the future.

The additional detail of description introduced has only a minor impact on the computational cost of the model. Indeed, when studying crack initiation problems, the main computational tasks are related to the solution of stresses and strains on the whole structure of interest. Therefore, any algebraic criterion for failure detection (in opposition to more complex local relations) is practically equivalent from the point of view of computational costs. The lifetime estimates obtained account well for the experiments. The residual unpredicted variability is consistent with the usual scattering of HCF experimental data.

The main advantage of the proposed method based on dynamical systems techniques is the possibility of extending it to a large class of local material behaviour involving not only plasticity, but also crack and damage evolution, while keeping a simple closed-form formula for the prediction of the lifetime.

Finally we note that the extension of this approach to more complex periodic and quasi-periodic multiaxial loadings and to a larger base of materials constitute interesting fields of research, which are relevant for applications and which remain still largely unexplored.

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Appendix A. A priori estimates

In this section we will derive the bound (13) and (14) for the dynamical system (12). In order to simplify the notation and focus on the main analytical argument, we will consider the following equivalent Cauchy problem

\[
\begin{align*}
\dot{y} &= h(y) \frac{c - Ay^\alpha}{1 - By^\alpha}, \\
y(0) &= y_0.
\end{align*}
\]
with \(y_0 \leq 0\). We observe that all the results of this section can be readily adapted to our original model (12) by setting:

\[
\epsilon = \frac{4}{\mu + \epsilon} \frac{\Delta T - \Delta T_0}{2}
\]

\[
A = \frac{4}{\mu + \epsilon} \frac{1}{B}
\]

\[
B = \frac{1}{\mu + \epsilon} \frac{1}{B}
\]

\[
y_0 = -T_0.
\]

We start by rigourously defining the lifetime of our system.

**Definition 1.** The lifetime for system (A.1) is the time \(t_{\infty}^a\) that is necessary for any solution to travel from \(y_0\) to \(\xi\), where \(\xi\) is the vertical asymptote of \(t\) given by the (unique) real root of

\[
1 - B|\xi|^{\alpha-1} \text{sgn} \xi = 0.
\]

Before stating the main estimate, we recall an elementary result, which will be very important in the following. (see [26, Exercise 4.3.10]).

**Theorem 2.** The time required for a solution of the differential equation

\[\dot{y} = \epsilon + Ay^2\]

to go from \(-\infty\) to \(+\infty\) is given by

\[t_{\infty}^a = \frac{\pi}{2 \sin \frac{\pi}{2} A^{-1} e^{\frac{\pi}{2}}}.\]

Consider now Eq. (A.1). In order to estimate the lifetime from below (conservative estimate of the endurance of the material) we will consider the following approximation from above of \(h\):

\[h(y) \leq \bar{h}(y) = \begin{cases} \epsilon + A|y|^\alpha & \text{if } y \leq 0 \\ \gamma(\epsilon + A|y|^\alpha) & \text{if } 0 \leq y \leq x_1 \\ +\infty & \text{otherwise} \end{cases}\]

where \(x_1\) is defined by:

\[\gamma(\epsilon + Ax_1^\alpha) = h(x_1), \quad x_1 \in (0, \xi) \quad \text{i.e.} \quad x_1 = \left(\frac{\gamma - 1}{B_0}\right)^{\frac{1}{\alpha}} \tag{A.2}\]

and \(\gamma\) will be determined later. Since solutions of the dynamical system associated to \(h\) travel slower than those of (A.1), we immediately deduce that

\[t_{\infty}^a = t_{\infty}^0 + t_{\infty}^0 + t_{\infty}^0 \geq t_{\infty}^0 + t_{\infty}^0 + t_{\infty}^0\]

where with \(t_{\infty}^0\) we denote the time required by a solution of the dynamical system

\[\dot{y} = \bar{h}(y)\]

to travel from \(a\) to \(b\).

We start by estimating \(t_{\infty}^0\), always from below. We consider the further approximation

\[\tilde{y} = \bar{h}_a(y) = A|y|^\alpha. \tag{A.3}\]

Reasoning as above, we deduce

\[t_{\infty}^0 = \tilde{t}_{\infty}^0 - P_{\infty}^a \geq \tilde{t}_{\infty}^0 - P_{\infty}^a.\]

By symmetry, Theorem 2 implies (see Fig. A.1).

\[t_{\infty}^0 = \frac{\pi}{\alpha \sin \frac{\alpha}{2} A^{-1} e^{\frac{\alpha}{2}}}
\]

whereas a direct integration of Eq. (A.3) gives

\[\int_{y_0}^{y_0} \frac{1}{A^{1/\alpha} e^{1/2}} - \frac{1}{\alpha \sin \frac{\alpha}{2}} \]

from which we deduce

\[t_{\infty}^0 \geq \frac{\pi}{\alpha \sin \frac{\alpha}{2}} A^{1/\alpha} e^{1/2} - \frac{1}{\alpha \sin \frac{\alpha}{2}} \frac{1}{\gamma A} x_1^{1-\alpha}\]

We now consider the lower approximation of the travelling time \(\tilde{t}_0\) from 0 to \(\xi\) (failure). Arguing as before we deduce:

\[\tilde{t}_0 \geq \tilde{t}_0 - \tilde{t}_0 = \frac{\pi}{\alpha \sin \frac{\alpha}{2}} A^{1/\alpha} e^{1/2} - \frac{1}{\alpha \sin \frac{\alpha}{2}} \frac{1}{\gamma A} x_1^{1-\alpha};\]

using the definition of \(x_1\) given above (see (A.2)) we finally get

\[\tilde{t}_0 \geq \frac{\pi}{\alpha \sin \frac{\alpha}{2}} A^{1/\alpha} e^{1/2} - B \frac{1}{\alpha (\alpha - 1)} \gamma - 1\]

which is minimised when

\[\gamma = \gamma_{opt} = \frac{\pi}{\alpha \sin \frac{\alpha}{2}} - \frac{1}{\alpha \sin \frac{\alpha}{2}} B \sin \frac{\alpha}{2}\]

for \(\epsilon\) small enough.

Putting all the above results together we finally obtain the following estimate from below to the lifetime of our model:

\[t_{\infty}^0 \geq \frac{\gamma_{opt} + \frac{1}{\alpha \sin \frac{\alpha}{2}} A^{1/\alpha} e^{1/2} - \frac{1}{\alpha (\alpha - 1)} \gamma_{opt} - B}{1 - \frac{1}{\alpha \sin \frac{\alpha}{2}} B \sin \frac{\alpha}{2}} \frac{1}{\alpha \sin \frac{\alpha}{2}} \frac{\alpha}{\alpha - 1} |y_0|^{1-\alpha}.\]

After substitution of the values for \(A, B, \epsilon\) and \(y_0\) arising in our model, we finally deduce the desired estimate on the lifetime.

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