Effect of Incorporation of Rice Husk Ash Instead of Cement on the Performance of Steel Fibers Reinforced Concrete

Osama Zaid**, Jawad Ahmad**, Muhammad Shahid Siddique¹ and Fahid Aslam²

¹ Department of Civil Engineering, Military College of Engineering, Risalpur, Sub Campus of National University of Science and Technology, Islamabad, Pakistan, ² Department of Civil Engineering, College of Engineering in Al-Kharj, Prince Sattam Bin Abdulaziz University, Al-Kharj, Saudi Arabia

The production of rice is significant worldwide; the husk produced is generally used as a combustible material for the preparation of paddies, delivering energy through direct combustion as well as by gasifying. Annually, 7.4 million tons of Rice Husk Ash (RHA) is produced and poses an incredible danger to the environment, harming the land and the encompassing zone where it is unloaded. In the transformation of rice husk to ash, the ignition cycle eliminates the natural products, leaving silica-rich remains. These silica-rich remains have proven to have potential to be utilized in concrete as a limited substitution of cement to enhance the concrete compressive strength. Steel fibers’ incorporation increases the concrete tensile strength, balances out concrete samples, and changes their brittle behavior to a more ductile response. In the current study, the influence of various doses of Rice Husk Ash (RHA) used in concrete in the presence and absence of steel fibers and concrete performance has been examined. A total of nine mixes have been designed: one was a control, four were without steel fibers containing only RHA, and the last four mixed RHA with steel fibers from 0.5 to 2%. Tests with 5, 10, 15, and 20% percentages of RHA replacing the concrete have been targeted. Results have been compared with the reference samples and the reasonability of adding Rice Husk Ash to concrete has been studied. From the results, it was noted that about 10% of cement might be replaced with Rice Husk Ash mixed in with steel fibers with almost equal compressive strength. Replacing more than 15% of cement with RHA will produce concrete with a low performance in terms of strength and durability.

Keywords: concrete, steel fibers, rice husk ash, compressive strength, superplasticizer

INTRODUCTION

Concrete is a frequently used construction and building material, which is sufficiently strong, impermeable, and durable. Among the ingredients of concrete, cement is an expensive material, and its demand is persistently increasing all over the globe. Hence, to control the cost of construction, it is important to utilize modern waste materials, mineral admixtures, and other materials to accommodate the increasing use of concrete. Agricultural waste, such as rice husk ash (RHA), can be used instead of cement in concrete making, producing efficient concrete with improved...
concrete properties like impermeability, workability, strength, and corrosion of steel reinforcement. For reasonable improvement of concrete, increasing the use of cement raw materials must be preserved. RHA is an exceptionally responsive pozzolanic material used as an Ordinary Portland Cement substitution. It is a good option to utilize RHA in concrete because it will increase concrete workability.

A lot of studies have been performed to examine the possible use of Rice Husk Ash in concrete. Tay (1990) confirmed a reduction in concrete compressive strength which is nearly relative to the amount of ash in the mixed cement (Udoeyo and Dashibil, 2002). Concrete samples with sawdust ash (SDA) substitution from 20 to 25% demonstrated a compressive strength, with strength diminishing with higher ash content (Jaturapitakkul and Roongreung, 2003). It was also shown that mortar of CaC2 residue compressive strength and Rice Husk Ash can be more than 16.5 Mpa after 28 days of curing days and expand to 20.2 Mpa after 180 days of curing (Qing-ge et al., 2004). Further studies have demonstrated that, in the substitution of cement with Rice Husk Ash, concrete compressive strength is clearly increased (Sakr, 2006). It was also showed that ilmenite concrete had the highest compressive strength when blended in with 10% steel fibers (Tangchirapat et al., 2009). One study replaced 10% cement with palm ash and showed palm oil fuel ash mortar compressive strength was 100–102% of cement Type I mortar after curing for 90 days (Ferraro et al., 2010). Using white cement, up to 15% of RHA may be well mixed (Xu et al., 2012). It was also demonstrated that that about 20% of Rice Husk Ash, Fine Aggregate, Palm oil fuel ash, or wheat straw ash can be utilized to replace cement without influencing the physical properties of glass fiber reinforced concrete (GFRC) (Zain et al., 2011). A final study examined the concrete compressive strength over varying fineness of RHA replacing cement at about 15% and indicated that the concrete strength was enhanced.

Rice husk is a significant agricultural by-product and is produced during the husk removal cycle of paddy rice. In a 2002 environmental review, it was shown that the yearly worldwide formation of paddy was 0.579 billion tons (Xu et al., 2012). India is close to China in terms of paddy production, making up 31.2% of the globe's creation. Removal of rice husk is a significant problem as inappropriate removal causes natural issues (Zain et al., 2011). One technique is using the rice husk as a replacement for concrete. In concrete, RHA could be utilized as a mineral admixture due to its profoundly siliceous nature if the rice husk is kept at a constrained temperature between 700 and 800°C (James and Rao, 1986). Through this consuming cycle, the carbon amount in rice husk is burnt off and all that is left is silica residue (O’Connell et al., 2007). The huge pozzolanic behavior is an important quality for utilizing it as a replacement or an admixture (mineral) in concrete (Ahmad et al., 2021). The viable use of Rice Husk Ash in concrete relies upon its particle size (Kishore et al., 2011). Given the checking electron magnifying lens contemplates, it has been proven that Rice Husk Ash is a permeable pozzolanic material and includes a huge number of sets of size 1–10 μm (Mehta, 1992; Uduweriya et al., 2010). Fine grains work as a filler on the pore structure and more confine enhancement of RHA particles produces more hydration. Adding Rice Husk Ash to concrete improves the strength. However, when a low water/cement ratio is used, a weak performance is seen in Rice Husk Ash concrete (Giaccio et al., 2007; Vijai et al., 2012).

Various research shows that mechanical and durability characteristics considerably improved with the incorporation of fibers (Ahmad et al., 2020a). The impact of polypropylene fibers and silica fume improved the mechanical properties of expansive-cement concrete (Toutanji, 1999). According to Toutanji (1999), characteristics considered include those of the change of length, fresh mix properties, rapid chloride permeability, flexural conduct, compressive strength, and bond of hardened concrete. The silica fume amount utilized was 7 and 9% and volume of fiber amount was 0.15, 0.20, and 0.30%. Results display that utilization of 7% silica fume joined with 0.20 percent volume of fiber volume fraction brings about an optimum mix design for repair applications from the angles of length change, workability, strength, bond, and permeability (Nuruuddin et al., 2011). Researchers examined the impacts of sodium hydroxide molarity and superplasticizer on the workability, compressive strength, and microstructure of (SCGC) Self Compacting Geopolymer Concrete. Outcomes

### TABLE 1 | Physical and chemical property of OPC.

| Chemical property | Percentage (%) | Physical property | Results |
|-------------------|----------------|-------------------|---------|
| CaO               | 62.7           | Size              | ≤75 μ |
| SiO₂              | 25.9           | Fineness          | 92%    |
| Al₂O₃             | 8.4            | Normal            | 28%    |
| Fe₂O₃             | 1.7            | Initial setting   | 38 min |
| MgO               | 2.5            | Final setting     | 412 min|
| SO₃               | 1.9            | Specific surface  | 322 m²/kg |
| K₂O               | 2.4            | Soundness         | 1.7%   |
| Na₂O              | 0.2            | 28-days compressive | 42 Mpa |

### TABLE 2 | Physical property of steel fibers.

| Physical property | Results |
|-------------------|---------|
| Length            | 35 mm   |
| Diameter          | 0.55 mm |
| Aspect ratio (L/d) | 64     |
| Tensile strength  | 415 Mpa |
| Young’s Modulus   | 3.66 GPa|

### TABLE 3 | Physical properties of fine and coarse aggregate.

| Physical property | Fine aggregate | Coarse aggregate |
|-------------------|----------------|-----------------|
| Bulk density (kg/m³) | 1.596          | 1.535           |
| Moisture content   | 1.8%           | 1.25%           |
| Absorption capacity| 5.28%          | 2.13%           |
| Fineness modulus   | 2.93           | 4.7             |
| Particle size      | 4.75–0.75 mm   | 30–4.75 mm      |
showed that workability and performance enhanced with the increase in superplasticizer content. The Rice Husk Ash produced from the consumption of husk in heater at controlled temperature satisfies the actual qualities and compound piece of mineral admixtures. The pozzolanic behavior of Rice Husk Ash relies on the silica crystallization stage, silica percentage, and surface zone and size of ash. The measure of carbon amount in RHA should be small. In the event that the carbon content is more in RHA, the strength of concrete will be less.

In the current study, lab tests were performed to analyze the use of Rice Husk Ash alongside superplasticizer (with the presence and absence of steel fibers with 0%, 0.5%, 1.0%, 1.5%, and 2.0%) as a cement substitution ingredient in

![Gradation Curve of Fine Aggregate](image1.png)

![Gradation Curve of Coarse Aggregate](image2.png)

**FIGURE 1** (A) Gradation Curve of Fine Aggregate, (B) Gradation curve of Coarse Aggregate.
Concrete. The use of steel fibers might increase the cement stabilized samples and change concrete brittle behavior to ductile behavior. The impact of the various ratios of RHA incorporated into concrete which contains superplasticizer with and without steel fibers on concrete performance has been studied. Tests with 0, 5, 10, 15, and 20% percentage of Rice Husk Ash replacing the cement have been tried. The outcomes have been compared with the control samples and the feasibility of adding Rice Husk Ash to concrete has been contemplated. From studying previous literature, it is concluded that incorporation of steel fibers affects concrete workability, so using a superplasticizer was important to keep concrete in a flowable state.

**TABLE 4 | Chemical composition of rice husk ash.**

| Chemical     | Rice husk ash (%) |
|--------------|-------------------|
| CaO          | 12.56             |
| SiO$_2$      | 62.3              |
| Al$_2$O$_3$  | 10.11             |
| Fe$_2$O$_3$  | 6.48              |
| MgO          | 3.5               |
| SO$_3$       | 0.61              |
| K$_2$O       | 2.09              |
| Na$_2$O      | 0.049             |

**TABLE 5 | Physical property of superplasticizer.**

| Property          | Result                          |
|-------------------|---------------------------------|
| Color             | Brown liquid                    |
| Air entrainment   | 1.48 at 25°C                    |
| Chloride content  | Nil to BS 5075/BS: EN934        |
| Specific gravity  | 1.18 @ 25°C                     |

**TABLE 6 | Quantification of materials.**

| Mix ID | Mix proportion (%) | Cement (Kg/m$^3$) | RHA | Steel fibers (kg) | Water (kg) | Sand (kg/m$^3$) | Coarse aggregate (kg/m$^3$) | Superplasticizer (kg) |
|--------|--------------------|-------------------|-----|------------------|------------|-----------------|-----------------------------|-----------------------|
| Mix 1  | 100% 0% 0%         | 375               | –   | –                | 165        | 650             | 1,310                       | 0%                    |
| Mix 2  | 95% 5% 0%          | 365.25            | 18.75 | –                | 165        | 650             | 1,310                       | 0%                    |
| Mix 3  | 90% 10% 0%         | 337.5             | 37.5 | –                | 165        | 650             | 1,310                       | 0%                    |
| Mix 4  | 85% 15% 0%         | 318.75            | 56.25 | –                | 165        | 650             | 1,310                       | 0%                    |
| Mix 5  | 80% 20% 0%         | 300               | 75   | –                | 165        | 650             | 1,310                       | 0%                    |
| Mix 6  | 95% 5% 0.5%        | 365.25            | 18.75 | 1.875            | 165        | 650             | 1,310                       | 2.50                  |
| Mix 7  | 90% 10% 1.0%       | 337.5             | 37.5 | 3.75             | 165        | 650             | 1,310                       | 2.50                  |
| Mix 8  | 85% 15% 1.5%       | 318.75            | 56.25 | 5.625           | 165        | 650             | 1,310                       | 2.50                  |
| Mix 9  | 80% 20% 2.0%       | 300               | 75   | 7.5             | 165        | 650             | 1,310                       | 2.50                  |

**FIGURE 2 | Compressive strength (without steel fibers and superplasticizer).**
FIGURE 3 | Relative analysis compressive strength (without steel fibers and superplasticizer).

FIGURE 4 | Compressive strength (with steel fibers and superplasticizer).

FIGURE 5 | Relative analysis of compressive strength (with steel fibers and superplasticizer).
EXPERIMENTAL PROGRAM

Methods and Materials

Cement

The primary binder that was used in all mixes was Ordinary Portland Cement, which is type I general-purpose cement as per ASTM C 150 [22]. The chemical and physical properties of Ordinary Portland Cement are displayed in Table 1.

Steel Fibers

Hook end steel fibers with a length of 35 mm were glued together and were used in different percentages. Their properties are given in Table 2.

Aggregates

For fine aggregates, typical natural sand, obtained from Lawrancepaur, was utilized in saturated surface dry conditions in entire blends. The coarse aggregate used in this study was obtained from Margalla in saturated surface dry condition and was used in all blends; the maximum size of the coarse aggregate was 30 mm. Tests were performed to determine aggregate physical parameters, which are shown in Table 3, while gradation curves of fine and coarse aggregate as per ASTM C 33 (ASTM C 33/C33M, 2008) are shown in Figures 1A,B, respectively.

Rice Husk Ash

Rice husk is obtained from the rice milling industry because it is a byproduct. Research has demonstrated that heating rice husk at a temperature of 700°C makes a powder that has a sufficient structure for pozzolanic materials. Research has also indicated that, because of RHA’s high surface area, the Rice Husk Ash can be used in concrete as a mineral admixture. RHA reduces the permeability of concrete when used as a mineral admixture. Rice Husk Ash utilized in the present study was gray, had a pH of 7.4,
and contained silica of 62.3%. The typical chemical composition is shown in Table 4.

**Water**
The study revealed that the pH of water for mixing in concrete should be in the range of 6 and 8 (Zain et al., 2011). In this study, clean drinking water was used, which was obtained from commercial tube well.

**Superplasticizer**
In the present research, Conplast SP 430 superplasticizer was used. It is included commonly in the scope of 0.6–1.3% by cement weight. The utilization of a superplasticizer makes pumpable concrete and concrete which is more workable. In the current investigation, a 0.8% superplasticizer was utilized to control test samples. Conplast SP430 meets with BS 5075, BS: EN 934-2 (ENTS, 2009), and with ASTM C494 as Type A and Type F [25], contingent upon the measurements utilized. In Table 5 its physical properties are provided.

**Test Mixing Procedure and Size of Specimen**
The complete investigation program was planned so that it was done within 30 days from the date of acquisition of cement to diminish the negative effects on properties of concrete as a result of storing cement. A 1:1.5:3 ratio was used for concrete making. First, the cement, sand, and coarse aggregates were dry mixed for 60 seconds, and then water was added along with RHA, and then the mixture was mixed again for 2 min. The aggregates used to manufacture concrete were used in saturated surface dry conditions. For concrete, 1:1.5:3 ratios were used as per ASTM C 39 (Materials ASFTA, 2012). For sampling standard size of cylinders, 6 inch × 12 inches were utilized to

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**FIGURE 8** | Split tensile strength (with steel fibers and superplasticizer).

**FIGURE 9** | Relative analysis split tensile strength (with steel fibers and superplasticizer).
determine the concrete compressive strength as per ASTM C 39 (C39/C39M A, 2003) and split tensile strength as per ASTM C 496 (Designation, 1976). Water absorption tests as per ASTM C 642-13 (C642-13 A, 2013), density as per ASTM C 642-13 (C642-13 A, 2013), and volume of voids test as ASTM C 642-13 (C642-13 A, 2013) of concrete were performed at 7, 21, and 28 days after curing. During sampling, concrete was packed with 3 layers, with each layer being compacted 25 times. Adding of RHA to concrete with varying dosages (0, 5, 10, 15, and 20%) with and without steel fibers of different percentage (0%, 0.5%, 1.0%, 1.5%, and 2.0%) and keeping the dose of superplasticizer same were compared with normal control mixes, as shown in Table 6.

**RESULTS AND DISCUSSION**

**Compressive Strength Test on Concrete Cylinders With Cement Substituted With Rice Husk Ash (Without Steel Fibers and Superplasticizer)**

The results of the compressive strength test on concrete cylinders as per ASTM C 39 (C39/C39M A, 2003) with cement substituted with Rice Husk Ash (without superplasticizer and steel fibers) are displayed below in Figure 2.

It is a known fact that concrete strength increases with an increase in curing days. For normal concrete with 0% RHA,
Concrete compressive strength was 2,554 psi after 7 days of curing, 2,750 psi after 21 days of curing, and 2,910 psi after 28 days of curing. General trends show that compressive strength decreases with the addition of RHA (Mehta, 1992; Nehdi et al., 2003). For 5% of cement replaced with RHA, the strength decrease was 5.4, 3.6, and 3.9% after 7, 21, and 28 days of curing, respectively, as in comparison to control samples. For 10% cement replaced with Rice Husk Ash, the strength decrease was 12.1, 13.2, and 13.5% after 7, 21, and 28 days of curing, respectively, as in comparison to control samples. For 15% cement replaced with Rice Husk Ash, the strength decrease was 20.3, 21.7, and 23.4% after 7, 21, and 28 days of curing, respectively, as in comparison to control samples. For 20% cement replaced with Rice Husk Ash, the strength decrease was 25.4, 26.1, and 28.5% after 7, 21, and 28 days of curing, respectively, as compared to control samples. From the outcomes, it is seen that increasing the amount of RHA used as a cement replacement decreases the concrete compressive strength. Upon replacement of 10% RHA with cement, about a 12% decrease in compressive strength was noted. By further increasing doses of RHA, concrete strength would be affected significantly. Consequently, Rice Husk Ash up to 10% as replacement of cement is allowed in concrete without considerable change in compressive strength.

A relative analysis was carried out in which the 28-days curing age compressive strength of the control mix was considered the relating mix, and from this, different blends with changing percentages of RHA are compared, as shown in Figure 3. At
7 days of curing, compressive strength was about 19% less than that of the control (28 days) at 10% substitution with RHA (optimum dosage). As compared to the control, 10% substitution with RHA (optimum dosage) showed 18% less compressive strength at 21 days of curing. On day 28 of curing, compressive strength was only 9.0% less than that of the control (28 days) at 10% substitution with RHA (optimum dosage). As compared to the control, 20% substitution with RHA showed 31% less compressive strength at 7 days. On day 21 of curing, compressive strength was about 28% less than that of the control (28 days) at 20% substitution with RHA. At 28 days of curing, compressive strength was about 24% less as compared to control mix. It can be concluded that 10% substitution shows only 9.0% less as compared to control; this is not too much of a reduction in compressive strength and hence can be successfully utilized in concrete. Therefore, it is recommended to substitute up to 10% of cement with RHA.

Compressive Strength Test on Concrete Cylinders With Cement Substituted With Rice Husk Ash (With Steel Fibers and Superplasticizer)

Figure 4 illustrates the different concrete compressive strengths in which the cement is substituted with changed doses of Rice Husk Ash (with steel fibers and superplasticizer) with the curing age of concrete. Normal concrete with 0% Rice Husk Ash showed concrete compressive strength was 2,554 psi after 7 days curing,

FIGURE 14 | Voids Volume (without steel fibers and superplasticizer).

FIGURE 15 | Voids Volume (with steel fibers and superplasticizer).
2,750 psi after 21 days curing, and 2,910 psi after 28 days of curing. RHA reduces the strength due to its porous nature which creates porous concrete and leads to less packing density, which in turn results in less strength. RHA reduces workability due to its fineness and porous nature which increases compaction, leading to pore voids in hardened concrete, resulting in less split tensile strength. Also, RHA absorbs more water which affects the hydration process due to lack of water (Nehdi et al., 2003), superplasticizer (Machnnis and Racic, 1986), and steel fiber (Vairagade and Kene, 2012; Ahmad et al., 2020a) increased strength. For 5% cement substituted with Rice Husk Ash (RHA), and also incorporating steel fibers and superplasticizer in concrete, the decrease in strength was 4.6, 3.3, and 3.0% after 7, 21, and 28 days of curing, respectively, as in comparison to control sample (with superplasticizer and steel fibers).

For 10% substitution of cement with Rice Husk Ash including steel fibers and superplasticizer in concrete, strength was reduced 9.4, 10.1, and 10.5% after 7, 21, and 28 days of curing, respectively, as compared to control sample (with superplasticizer and steel fibers). For 15% cement substituted with Rice Husk Ash including steel fibers and superplasticizer in concrete, the decrease in strength was 15.2, 17.0, and 17.3% after 7, 21, and 28 days of curing, respectively, as compared to the control sample (with superplasticizer and steel fibers). When 20% cement replaced with Rice Husk including steel fibers and superplasticizer in concrete, the decrease in strength was 22.4, 24.2, and 25.5% after 7, 21, and 28 days of curing, respectively, as compared to reference samples (with superplasticizer and steel fibers).

A relative analysis was carried out in which the 28-days curing age compressive strength of the control mix was considered the relating mix, and from this, different mixes with varying percentages of RHA and steel fiber (SF) were compared, as displayed in Figure 5. On day 7 of curing, compressive strength was about 21% less than that of the control (28 days) at 10% substitution with RHA and 1.0% SF. On day 21 of curing, compressive strength was about 13% less than that of the control (28 days) at 10% substitution with RHA and 1.0% SF. On 28 days of curing, compressive strength was about 4.0% less than that of the control (28 days) at 20% substitution with RHA and 1.0% SF.

It was observed from the test outcome that by adding superplasticizer and steel fibers the concrete compressive strength improved by a significant margin. For 10% cement replaced with Rice Husk Ash and also using steel fibers and superplasticizer, on average about 4.0% strength was reduced. Thus, up to 10% replacement of cement with Rice Husk Ash is allowed in concrete without a noticeable effect in compressive strength.

Split Tensile Strength Test on Concrete Cylinders With Cement Substituted With Rice Husk Ash (With the Absence of Steel Fibers)

Split tensile strength test is carried out as per ASTM C 496 (Designation, 1976). Results of the split tensile strength test on concrete cylinders with Rice Husk Ash substituted with cement (without steel fibers) are displayed in Figure 6. It is recognized that concrete strength increases with an increase in curing days. Split tensile strength values followed the same strength reduction pattern in concrete. It has been also reported that split tensile strength behaves in a similar pattern with the incorporation of RHA (Sakr, 2006). For normal concrete with 0% RHA, concrete split tensile strength was 265 psi after 7 days of curing, 295 psi after 21 days of curing, and 335 psi after 28 days of curing. For 5% of cement replaced with RHA, the strength decrease was 4.4, 4.2, and 3.8% after 7, 21, and 28 days of curing, respectively, as in comparison to control specimens. For 10% cement substituted with RHA, the strength decrease was 9.6, 11.9, and 13.0% after 7, 21, and 28 days of curing, respectively, as compared to reference samples. For 15% cement replaced with Rice Husk Ash, the decrease in strength was 16.1, 17.2, and 19.4% after 7, 21, and 28 days of curing, respectively, as compared to control samples. For 20% replacement of cement with Rice Husk Ash, the strength decrease was 25.2, 26.3, and 26.9% after 7, 21, and 28 days of curing, respectively, as compared to control samples. From the results, it is noted that with the increase in dosage of RHA with cement replacement, the concrete split tensile strength was continuously reduced. On substitution of 10% cement with RHA on average a 12% decrease in compressive strength was seen. By further increasing the dose of RHA, concrete strength would be affected significantly. Thus, up to 10% substitution of RHA with cement is allowed in concrete without a notable effect in split tensile strength. RHA reduces split tensile strength due to its porous nature, which creates porous concrete, leading to less packing density and, in turn, less strength. It is worth mentioning here that RHA affects split tensile strength more than compressive strength; compressive strength reduced only 9.0% while split tensile strength reduced about 14% at 10% substitution of RHA. Steel fiber improves split strength but RHA reduces it, which results strength approximately equal to the control. Furthermore, both steel and RHA reduce workability which also results in lower strength. But overall, the results show that strength is comparable to control with the incorporation of RHA. Thus, it is a good choice to use RHA instead of cement.

A relative analysis was carried out in which the 28-day split tensile strength of the control mix was considered the reference mix, and from this, different mixes with varying percentages of RHA and SF were compared, as shown in Figure 7.

On 7 days of curing, split tensile strength was about 29% below that of the reference specimen (28 days) at 10% substitution with RHA. As compared to the control, 20% substitution with RHA showed 41% less split tensile strength. On day 21 of curing, split tensile strength was about 32% below that of the reference specimen (28 days) at 10% substitution with RHA. As compared to the control, 20% substitution with RHA showed 36% below split tensile strength at 21 days curing. On day 28 of curing, split tensile strength was about 14% below that of the reference specimen (28 days) at 10% substitution with RHA.

Split Tensile Strength Test on Concrete Cylinders With Cement Substituted With Rice Husk Ash (With Steel Fibers and Superplasticizer)

Figure 8 illustrates various concrete split tensile strengths in which the cement is replaced with varying doses of RHA (with steel fibers and superplasticizer) with the 7, 21, and 28 days of curing age.
Normal concrete with 0% Rice Husk Ash demonstrated a concrete split tensile strength of 258 psi after 7 days of curing, 279 psi after 21 days of curing, and 294 psi after 28 days of curing. For 5% cement substituted with RHA, the strength decrease was 3.5, 3.8, and 3.0% after 7, 21, and 28 days of curing, respectively, as in comparison to control specimens. For 10% cement substituted with RHA, the strength decrease was 7.2, 7.6, and 6.8% after 7, 21, and 28 days of curing, respectively, as compared to reference samples. For 15% of cement replaced with Rice Husk Ash, the depression in strength was 14.3, 14.9, and 15.3% after 7, 21, and 28 days of curing, respectively, as in comparison to control specimens. For 20% substitution of cement with RHA, the strength reduction was 21.9, 22.8, and 23.3% after 7, 21, and 28 days of curing, respectively, as compared to control samples.

A relative analysis was conducted in which the 28-day split tensile strength of the control mix was considered the reference mix, and varying percentages of RHA and steel fiber (SF) are compared, as shown in Figure 9.

On day 7 of curing, split tensile strength was about 33% below that of the reference mix (28 days) at 10% substitution with RHA and 10% of SF. On day 21 of curing, split tensile strength was about 19% below that of the reference mix (28 days) at 10% substitution with RHA and 2.0% SF. On 28 days of curing, split tensile strength was only 6.0% less than that of the control (28 days) at 10% substitution with RHA and 1.0% SF.

From the outcomes, it is perceived that by increasing the percentage of cement substitution with RHA, the concrete split tensile strength continuously decreased. On substitution of 10% RHA with cement, on average a 6.0% decrease in split tensile strength at 28 days was noted. Further increasing the percentage of RHA, concrete strength would be affected significantly. Thus, up to 10% substitution with cement RHA is allowed in concrete without a notable effect in split tensile strength.

**Durability**

**Water Absorption**

Water absorption is an indirect measurement of concrete durability and is carried out as ASTM C 642-13 (C642-13 A, 2013). Most harmful chemicals are present in water. These chemicals react with concrete constituents, which changes the properties of concrete. Extra water present in the pores of concrete undergo a freeze and thaw effect because of changes in temperature, which results in cracks in the concrete (Kurda et al., 2019). The water absorption test was performed on those samples which were only cured in water for 28 days, the results of which are shown in Figure 10. General trends show that the water absorption increased as the percentages of RHA increased from 0 to 20%. It has also been reported that water absorption increases with the addition of RHA (Kishore et al., 2011).

According to test observation, maximum water absorption was 6.55% which increased to 8.39% when 20% Rice Husk Ash (RHA) was utilized in place of cement without adding steel fibers and superplasticizer.

The water absorption considerably decreased with the incorporation of steel fibers and superplasticizer, as shown in Figure 11. The reduction in water absorption is because of the rise in workability superplasticizer (Alsadey, 2015) as well as the crack prevention of steel fibers resulting in fewer voids. It has been reported that SF reduces water absorption due to crack prevention (Ahmad et al., 2020b). An increase in water absorption signifies lower durability of concrete when adding higher percentages of RHA without the addition of steel fibers and superplasticizer.

**Density**

The density test of concrete is carried out as per ASTM C 642-13 (C642-13 A, 2013). Figure 12 illustrates concrete density in detail, which is determined by using concrete cylindrical samples made with varying percentages of RHA, steel fibers, and superplasticizer.

Density decreases as the percentage of RHA increases, with a maximum density of 0% substitution of RHA while minimum density was obtained at 20% substitution of RHA. This is due to the physical nature of RHA, which is porous in nature, as well as the larger surface area (Bui et al., 2005) which results in decreased workability resulting in porous concrete, which ultimately decreases density.

Steel fibers and superplasticizer are added to offset this negative effect of (decreasing density) RHA, as shown in Figure 13. Superplasticizer enhances the workability of concrete (Alsadey, 2015) by creating an opposite charge on the particles which repel each other and, as a result, create more dense concrete. Also, steel fibers prevent the creation of cracks (Chang and Chai, 1995), resulting in a reduction in void content which leads to enhanced density of concrete. So, the addition of SFs would lead to increased tensile properties of concrete, and as a result, it would restrict the formation and development of initial cracks (Huang and Xie, 2011).

Overall, the diminishing value of density indicates that an increase in void content in concrete causes less durable and lower strength as compared to normal concrete. But by replacing cement with RHA and adding steel fibers enhances the strength value of concrete, which is both economical and environmentally friendly.

**Volume of Voids**

The results of the volume of voids are evaluated using concrete cylinders as per ASTM C 642-13 (C642-13 A, 2013) with different percentages of RHA and the result was then compared to control samples as shown in Figure 14. Voids in concrete indirectly measure the durability of concrete (Ahmad et al., 2020a). The value of voids’ volume in the normal concrete mix was 14.62%, which then increased to 21.42% with the replacement of cement with 20% RHA with no steel fibers. Furthermore, the addition of steel and superplasticizer showed some improvement with the reduction of voids in concrete as shown in Figure 15.

The volume of voids increased from 14.62 to 18.45%. This is due to fact that steel fibers act as crack arresters and prevent the propagation of a crack in hardening concrete (Ahmad et al., 2020b). It has also been reported that, with the addition of superplasticizer, the workability of concrete improved, results in decreased voids in concrete (Borsoi et al., 2000;
Ahmad et al., 2020b). Increasing voids’ volume depicts lower bonding in concrete and can raise the ultrasonic pulse velocity of concrete (Ahmad et al., 2020b).

CONCLUSION

The current research was intended to analyze the impact of the utilization of changing doses of RHA as a fractional substitution of cement in concrete blends. For this, 0, 5, 10, 15, and 20% RHA was presented in cement blends. Properties of the concrete mix, like its compressive and split tensile strength, density, water absorption, and the volume of voids, were evaluated at 7, 21, and 28 days. The aftereffects of these experiential examinations have been dissected and the significant findings of this investigation are introduced as follows.

- The compressive strength of concrete decreased considerably with an increasing percentage of RHA. Therefore, adding steel fibers and superplasticizer was important because steel fibers provide ductility to concrete and, while RHA and steel fibers diminish concrete workability, superplasticizer helps concrete to be flowable and easy to work with.
- Concrete tensile strength is around 10–15% of its compressive strength. Adding steel fibers with superplasticizer in concrete, in which cement is replaced with RHA in different percentages, improved concrete tensile strength remarkably as compared to concrete compressive strength.
- An increase in volume voids and water absorption and decrease in concrete density was detected when RHA was added up to 20%.
- 10% replacement of cement with RHA was considered good, as it did not affect concrete that much, and the introduction of steel fibers and admixtures like superplasticizer can make concrete a more economically viable option for the construction industry.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/supplementary material, further inquiries can be directed to the corresponding author/s.

AUTHOR CONTRIBUTIONS

OZ has written the main text, JA revised the paper, MSS secured the funding and helped in methodology. FA has helped in data collection.

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**Conflict of Interest:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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