Analysis of Climate Change’s Effect on Flood Risk. Case Study of Reinosa in the Ebro River Basin

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Abstract: Floods are one of the natural hazards that could be most affected by climate change, causing great economic damage and casualties in the world. On December 2019 in Reinosa (Cantabria, Spain), took place one of the worst floods in memory. Implementation of DIRECTIVE 2007/60/EC for the assessment and management of flood risks in Spain enabled the detection of this river basin with a potential significant flood risk via a preliminary flood risk assessment, and flood hazard and flood risk maps were developed. The main objective of this paper is to present a methodology to estimate climate change’s effects on flood hazard and flood risk, with Reinosa as the case study. This river basin is affected by the snow phenomenon, even more sensitive to climate change. Using different climate models, regarding a scenario of comparatively high greenhouse gas emissions (RCP8.5), with daily temperature and precipitation data from years 2007–2070, and comparing results in relative terms, flow rate and flood risk variation due to climate change are estimated. In the specific case of Reinosa, the MRI-CGCM3 model shows that climate change will cause a significant increase of potential affected inhabitants and economic damage due to flood risk. This evaluation enables us to define mitigation actions in terms of cost–benefit analysis and prioritize the ones that should be included in flood risk management plans.

Keywords: climate model projections; flood risk; flood hazard; Reinosa; climate change prioritization

1. Introduction

Floods are natural hazards that produce great material damage and human losses worldwide [1]. The increasing population density and infrastructure on river banks contribute to increased floodplain vulnerability, which can result in severe social, economic and environmental damage [2].

The fourth of the nine essential rules of flood risk management indicates that it should be taken into account that “The future will be different from the past. Climate and societal change as well as changes in the condition of structures can all profoundly influence flood risk” [3].

For all these reasons, it is essential to design methodologies that enable one to estimate flow regime variations and evaluate flood risk modification due to climate change. [4–6].

The technical document of the IPCC IV forecasts a probable increase in the frequency and intensity of precipitation episodes, as well as a decrease in average values in summer for mid-latitudes countries as Spain. The Fifth Assessment Report (AR5) of the IPCC (2013–14), points out that it is probable that the frequency or intensity of intense rainfall has increased in Europe, and in relation to future changes, that extreme precipitation events over most of the mid-latitude lands will most likely be more intense and more frequent [7]. Additionally, climate change can specially affect those regions in which the snow phenomenon is relevant in hydrological behavior.

As a matter of these facts, the 2019 flash flood European notifications beat the last 7 years of notifications clearly [8], and Reinosa (Cantabria, Spain) suffered two important floods on January and
December 2019, the second one being one of the worst floods in memory. This flood was caused by the Elsa storm, on December 19 and 20, which came from the southwest and was accompanied by very strong winds and very high temperatures for that time of the year, causing the melting of the snow-cover in the highest part of the catchment. A203 gauging station, recorded on 20 December 2019 at 1:00 a.m., 246 m$^3$/s instant (15 minutes period) flow, while the maximum ever recorded was 100 m$^3$/s (27 February 2010). The daily flow rate recorded by A203 for this event was 83 m$^3$/s and the return period has been estimated approximately as $Tr = 300$ years. This flood caused great damage in Reinosa, affecting residential areas (Figure 1).

![Figure 1. Reinosa (Cantabria, Spain). 20th December 2019.](image)

Reinosa (Cantabria, Spain) is located in the north of the Iberian Peninsula, in the junction of Hijar, Ebro and Izarilla rivers, immediately upstream the Ebro reservoir. Hijar catchment, with 27.6 km length and 147.6 km$^2$ surface, drains the highest area of Cantabrian mountain range that belongs to the Ebro river basin. The catchment height ranges between 865 and 2023 m above sea level, with a mean height of 1351 m. A203 gauging station is located in Hijar River, immediately upstream of Reinosa, with a time of concentration of approximately 15 hours.

The average rainfall of the head of the Ebro for the period 1920–2002 was 1190 mm/year, concentrated in autumn and winter, characteristic of an Atlantic climate, with some continental patterns producing 33 L/s/km$^2$. The average annual temperature is 8.9 °C in Reinosa. The main land uses in the catchment are forest and scrub. Figure 2 shows Hijar river basin overall and site map.

![Figure 2. Hijar river basin. (a) Overall Site map. (b) Detailed Site map.](image)

Reinosa belongs to the Hijar river basin, and had potential significant flood risk (ES091_HIJ_01_02_04_05_06) during the implementation of DIRECTIVE 2007/60/EC, as shown in Figure 3.
In order to evaluate climate change, projections of a series of climatic variables are entered as different climate models regarding a scenario of comparatively high greenhouse gas emissions (RCP8.5), with daily temperature and precipitation data.

The main aim of the work is to estimate flow and flood risk variation due to climate change by using different climate models regarding a scenario of comparatively high greenhouse gas emissions (RCP8.5), with daily temperature and precipitation data.

2. Materials and Methods

2.1. Overall Methodology

According to DIRECTIVE 2007/60/EC, Spanish hazard and flood risk maps can be downloaded at https://sig.mapama.gob.es/snczi/, regarding the following scenarios: (a) floods with a low probability, or extreme event scenarios (return period \( \geq 500 \) years); (b) floods with a medium probability (likely return period \( \geq 100 \) years); (c) floods with a high probability (return period \( \geq 10 \) years).

By relating flow rates in A203 gauging station with hazard and risk maps, correlations with flooding surface, economic damage and casualties can be achieved.

In order to evaluate climate change, projections of a series of climatic variables are entered as input data in a calibrated hydrological model in the study basin. The ASTER® model is a distributed hydrological model that calculates snowmelt and accumulation regarding energy balance [12,13].
Two global climate models (GCM), downscaled by the Spanish Meteorological Agency (AEMET), have been selected; we validated them with real flow rates from the control period (1961 to 2000) and used under the highest greenhouse gas emissions pathway (RCPs 8.5) from the Fifth Assessment Report of the Intergovernmental Panel on Climate Change.

The relationship between calculated daily flow rates and instant (15 minutes period) flow rates is not necessary for these downscaled climate models, as climate change’s effect will be calculated in relative terms comparing climate models in the calculation period in two equal length stages (2007–2038) and (2039–2070).

Once the flow rate variation for the climate projection is estimated and applied on real flow, new impacts on hazard and risk maps can be established. Figure 4 shows the overall methodology scheme.

2.2. Hazard and Risk Maps

Hazard maps are the result of two-dimensional hydraulic models, indicating flooded area, flood depths and flood velocities. Return periods were given by Spanish Authority in the framework of DIRECTIVE 2007/60/EC implementation by “Maximum Flow Maps” software, based on a regionalized gauging station study [14].
Flood risk maps shall show the potential adverse consequences associated with flood scenarios, and express, among other things, terms of the indicative numbers of inhabitants potentially affected and the type of economic activity of each area potentially affected. Additionally, economic damage can be estimated.

According to DIRECTIVE 2007/60/EC, these maps serve as a tool for establishing priorities and for making additional technical, economic and political decisions related to flood risk management. Measures to be implemented in the at-risk areas can be prioritized, depending on the results of the cost-benefit analysis. They also allow us to evaluate climate change’s effects. The risk associated with flood events is established based on the vulnerability of the threatened element and the hazard to which it is exposed. The estimation of indicative number of inhabitants potentially affected depends on updated census data. The Spanish Water Authority has also established a methodology to estimate the economic value of flood damage partially based on the PREEMPT project [15,16].

Finally, a relationship, as shown in Table 1, between flow rates for different return periods in Hijar, A203, and hazard and risk maps can be estimated, and subsequently a trend line, as shown in Figure 5, can be fitted:

| Instant Flow Rate (m$^3$/s) | Return Period (years) | Surface (km$^2$) | Inhabitants | Economic Value (€) |
|-----------------------------|-----------------------|------------------|-------------|--------------------|
| 138                         | 10                    | 2.783            | 346         | 29,194,901         |
| 214                         | 100                   | 3.843            | 982         | 56,806,383         |
| 273                         | 500                   | 4.620            | 1484        | 90,791,074         |

1 Obtained for overall ES091_HIJ_01_02_04_05_06 potential significant flood risk area, including the Spanish Public Water Domain (RDPH).

Figure 5. (a) Flood surface, (b) inhabitants potentially affected and (c) economic damage value in terms of flow rate in A203 gauging station.
2.3. Hydrological Model

2.3.1. Hijar Basin Model

A 500 by 500 m grid and daily time resolution distributed hydrological model has been built for the Hijar river basin (Figure 6), with A203 gauging station in Reinosa as the outlet and calibration point, 2014–2016 as the calibration period and 2017–2019 as the validation period.

Figure 6. ASTER hydrological model. Hijar river basin mesh (grey grid), Gauging Station (A203), rainfall stations (9008E, 9012) and temperature stations (2225, 2232).

ASTER® is a distributed hydrological model that calculates streamflow in a river using rainfall, temperature, windspeed and radiation as climate inputs. It has been applied in several countries and implemented by Spanish water authorities as an accurate model in river basins with strong snow phenomena, as in our case study (Hijar catchment) [17,18]. Figure 7 shows the snow–water equivalent for two consecutive days in Hijar model.

Figure 7. ASTER hydrological model snow accumulation (snow–water equivalent) (a) Day 1, (b) Day 2. Hijar model (ranging from 1 mm–pink to 215 mm–cyan).

2.3.2. Snow Accumulation Routine

Precipitation will be snow or water form at different temperatures depending on several atmospheric conditions. This range of temperatures can vary between −2 and 2 °C. The model sets a temperature, named rain/snow temperature, at which 50% of precipitation is snow, with a bilinear increase and decrease of snow form up to −2 and 2 °C.

2.3.3. Snowmelt Routine

As aforementioned, snowmelt is calculated using the energy balance equation. Melting takes place when air temperature is below a specific temperature ($T_{mi}$—snowmelt temperature). Snowmelt can be divided into two types: (a) rainfall snowmelt; (b) no rainfall snowmelt.
Rainfall Snowmelt

It is the snowmelt produced by rainfall energy. Assuming that the snow surface temperature is equal to 0 °C (273 K), snowmelt caused by energy from rainfall is [19]:

\[ M_r = 0.0125 \cdot P \cdot f_r \cdot T_r \]  (1)

where:
- \( P \) = Precipitation (mm)
- \( f_r \) = fraction of precipitation in the form of rain
- \( T_r \) = temperature of rain (°C)

In addition to energy from rainfall, other secondary terms as radiation and condensation energy must be added to calculate snowmelt when rain takes place.

No Rainfall Snowmelt

It is the snowmelt on a dry day. Due to difficulties estimating wind speed, hydrological models usually use non-forced convection or other empirical relations depending on air temperature. The following equation is used to estimate no rainfall melt \( M_c \) (mm) [20]:

\[ M_c = M_f \cdot (T_a - T_{mi}) \]  (2)

where:
- \( M_f \) = melt factor (mm/°C)
- \( T_a \) = air temperature (°C)
- \( T_{mi} \) = snowmelt temperature (°C)

This melt factor \( M_f \) indicates the seasonal variation, and can be represented with a sine function [21,22].

\[ M_f = \frac{MFMAX + MFMIN}{2} + \sin\left(\frac{n\cdot2\pi}{366}\right) \cdot \frac{MFMAX + MFMIN}{2} \]  (3)

where:
- \( MFMAX \) = maximum melt factor on June 21st (mm/°C/24hrs)
- \( MFMIN \) = minimum melt factor on December 21st (mm/°C/24hrs)
- \( n \) = number of days from March 21st.

2.3.4. Model Calibration and Validation

Calibration and validation have been carried out, comparing real daily flow rates, in A203 Hijar in Reinosa Gauging Station with the ASTER model daily flow rates being calculated with real meteorological data. The available continuous period for the observed daily flow rate ranges from 2014 to 2019, defining the calibration period as October 1st 2014 to September 30th 2016 and the validation period from October 1st 2017 to December 22nd 2019, including the aforementioned extraordinary event.

Figure 8, shows results during the calibration period, with a correlation coefficient of 0.90 and a Nash index (NSE) of 0.78. The maximum observed daily flow rate was 23.6 m³/s, and the maximum calculated daily flow rate was 23.5 m³/s. Total observed runoff was 189 hm³ and calculated runoff was 200.7 hm³, with 27 hm³ of overall snow–water equivalent accumulation.
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Rainfall Snowmelt

It is the snowmelt produced by rainfall energy. Due to difficulties estimating wind speed, hydrological models usually use non-forced convection or other empirical relations depending on air temperature. The main calibration parameters of the model are:

- $\text{MFMAX} = 5.5 \text{ (mm/°C/24 h)}$;
- $\text{MFMIN} = 1.46 \text{ (mm/°C/24 h)}$;
- $\text{T}_{\text{mi}} = -0.35 \text{ (°C)}$;
- $\text{Rain/Snow temperature} = -0.53 \text{ (°C)}$;
- $\text{Altimetry temperature gradient} = -3.1 \text{ (°C/1000 m)}$.

Figure 9 shows results during the validation period, with a correlation coefficient of 0.90 and a Nash index (NSE) of 0.80. The maximum observed daily flow rate was 83 m$^3$/s, and the maximum calculated daily flow rate was 69 m$^3$/s. Total observed runoff was 231 hm$^3$ and calculated runoff was 289 hm$^3$, with 20 hm$^3$ of overall snow–water equivalent accumulation.

2.4. Climate Projection

Daily rainfall and temperature data from two regionalized climate models (analog method—ANA and statistical regionalization method—SDSM) can be obtained from AEMET website (http://www.aemet.es/es/serviciosclimaticos/cambio_climat) for RCP 8.5.

Two climate models have been selected from 24, to analyze the combination of rainfall and temperature:

- ANA—BCC-CSM1-1-m (BCC);
- ANA—MRI-CGCM3 (MRI).

These two models have been pre-selected as generating the highest rainfalls. To evaluate their suitability, daily flow rates for the control period (1961–2000) have been calculated with ASTER for real
meteorological data and both climate models. Figure 10a shows that annual maximum real daily flow rates are above climate models, and the trend line shows a higher increase as well. Figure 10b shows that annual mean real daily flow rates fit the MRI better at the beginning of the control period, while a fit better with BCC is shown at the end of the control period. Supplementary Materials for rainfall stations (9008E, 9012) and temperature stations (2225, 2232) is given.

**Figure 8.** Upper level. Real (blue) and calculated (red) daily flow rates in A203. Lower level. Snow water equivalent in the catchment for the calibration period.

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**Figure 10.** Daily flow rate evolution during control period (1961–2000) for real data (blue), BCC (green) and MRI (red). (a) Annual maximum, (b) annual mean.

2.5. Calculation of Flow Rates for Different Return Periods

Daily flow rates for the calculation period (2007 to 2070) have been estimated with ASTER model for both climate projections (BCC and MRI). Calculation period has been divided in two equal length stages (2007 to 2038) and (2039–2070) and a probability distribution of extreme values has been estimated using the Gumbel distribution, presenting the best fit goodness:

\[
X = u - \beta \cdot \ln\left(-\ln\left(\frac{Tr - 1}{Tr}\right)\right)
\]

where:

- \( u \) = location parameter;
- \( \beta \) = scale parameter;
- \( Tr \) = Return period.

Finally, daily flow rates and instant (15 minute period) flow rates observed in A203 can be fitted in a linear relationship. As climate projections flow rates are being studied in relative terms with observed flow rates, transformation from daily flow rates into instant flow rates is not necessary.

3. Results

3.1. Flow Rate Evolution (RCP 8.5)

Table 2 and Figure 11 show results and trend lines from percentile analysis for both calculated climate models. For BCC-CSM1-1-m a small decrease in flow rate projection due to climate change is estimated, with small variability for different probabilities, while for MRI-CGCM3 bigger increase is predicted, showing a smooth variability for different probabilities, describing a more extreme climate.
Table 2. Return period, daily flow rate projection, 1st Stage (2007–2038); daily flow rate projection ratio, 2nd Stage (2039–2070); and flow rate ratio (2nd Stage/1st Stage).

| Tr (years) | Flow Rate Projection 2007–2038 (m$^3$/s) | Flow Rate Projection 2039–2070 (m$^3$/s) | 2039–2070/2007–2038 (%) |
|-----------|----------------------------------------|----------------------------------------|----------------------------|
| 10        | 28.13                                  | 27.00                                  | 96.0%                      |
| 25        | 31.92                                  | 30.62                                  | 95.9%                      |
| 50        | 34.73                                  | 33.30                                  | 95.9%                      |
| 100       | 37.52                                  | 35.96                                  | 95.9%                      |
| 500       | 43.96                                  | 42.11                                  | 95.8%                      |

ANA—MRI-CGCM3

| Tr (years) | Flow Rate Projection 2007–2038 (m$^3$/s) | Flow Rate Projection 2039–2070 (m$^3$/s) | 2039–2070/2007–2038 (%) |
|-----------|----------------------------------------|----------------------------------------|----------------------------|
| 10        | 27.36                                  | 31.05                                  | 113.5%                    |
| 25        | 31.99                                  | 36.51                                  | 114.1%                    |
| 50        | 35.43                                  | 40.57                                  | 114.5%                    |
| 100       | 38.85                                  | 44.59                                  | 114.8%                    |

1 Column 3 divided by column 2.

Figure 11. Flow rate projection ratio (2nd Stage (2039–2070)/1st Stage (2007–2038)) trend line in terms of return periods. (a) Analog method (ANA)—BCC-CSM1-1-m; (b) ANA—MRI-CGCM3.

3.2. Hazard and Risk Maps

After calculating the projected flow rate by entering for each return period (2nd Stage (2039–2070)/1st Stage (2007–2038)) the flow rate ratio in the trend line fitted for flood surface, economic damage and inhabitants potentially affected (Figure 5), new climate change estimations show similar results as for flow rate (Table 3).

As for flow rate, the MRI-CGCM3 climate model shows an increase in flood risk effects due to climate change, while BCC-CSM1-1-m shows a decrease. Results are enlarged for economic value and inhabitants potentially affected, while flooded surface decreases.

A logarithmic trend line is the one that best fits, and represents how the atmosphere behaves that shows in Figures 12–14.
Table 3. Projection ratio 2nd Stage (2039–2070)/1st Stage (2007–2038) for the flow rate, flood surface, inhabitants potentially affected and flood damage’s economic value.

| Flow Rate (%) | Instant Flow Rate (m³/s) | Return Period (years) | Flood Surface (%) | Inhabitants (%) | Economic Value (%) |
|---------------|--------------------------|-----------------------|------------------|-----------------|-------------------|
| −4.0          | 132.4                    | 10                    | −2.9             | −13.3           | −4.5              |
| −4.1          | 205.1                    | 100                   | −3.1             | −7.6            | −7.3              |
| −4.2          | 261.5                    | 500                   | −3.2             | −6.6            | −8.2              |

ANA—MRI-CGCM3

| Flow Rate (%) | Instant Flow Rate (m³/s) | Return Period (years) | Flood Surface (%) | Inhabitants (%) | Economic Value (%) |
|---------------|--------------------------|-----------------------|------------------|-----------------|-------------------|
| 13.5          | 156.7                    | 10                    | 9.6              | 44.8            | 17.4              |
| 14.8          | 245.6                    | 100                   | 11.0             | 27.3            | 29.7              |
| 15.3          | 314.7                    | 500                   | 11.4             | 24.2            | 33.7              |

Figure 12. Second Stage (2039–2070)/1st Stage (2007–2038) flood surface ratio trend line in terms of return periods. (a) ANA—BCC-CSM1-1-m; (b) ANA—MRI-CGCM3.

Figure 13. Second Stage (2039–2070)/1st Stage (2007–2038) economic damage ratio trend line in terms of return periods. (a) ANA—BCC-CSM1-1-m; (b) ANA—MRI-CGCM3.
Figure 12. Second Stage (2039–2070)/1st Stage (2007–2038) flood surface ratio trend line in terms of return periods. (a) ANA—BCC-CSM1-1-m; (b) ANA—MRI-CGCM3.

Figure 13. Second Stage (2039–2070)/1st Stage (2007–2038) economic damage ratio trend line in terms of return periods. (a) ANA—BCC-CSM1-1-m; (b) ANA—MRI-CGCM3.

Figure 14. Second Stage (2039–2070)/1st Stage (2007–2038) inhabitants potentially affected ratio trend line in terms of return periods. (a) ANA—BCC-CSM1-1-m; (b) ANA—MRI-CGCM3.

Flooded surface, inhabitants potentially affected and flood economic damage value can be calculated in absolute terms and are shown in Table 4 for ES091_HIIJ_01_02_04_05_06.

Table 4. Absolute terms for the flow rate, flood surface, inhabitants potentially affected and flood damage’s economic value for selected climate change projections.

| ANA—BCC-CSM1-1-m | ANA—MRI-CGCM3 |
|-------------------|----------------|
| **Flow Rate (m³/s)** | **Return Period (years)** | **Surface (km²)** | **Inhabitants** | **Economic Value (€)** |
| 132.4 | 10 | 2.703 | 300 | 27,887,407 |
| 205.1 | 100 | 3.722 | 907 | 52,640,944 |
| 261.5 | 500 | 4.472 | 1386 | 83,327,840 |
| 156.7 | 10 | 3.049 | 501 | 34,286,399 |
| 245.6 | 100 | 4.263 | 1250 | 73,649,691 |
| 314.7 | 500 | 5.145 | 1843 | 121,426,897 |

1 Obtained for overall ES091_HIIJ_01_02_04_05_06 potential significant flood risk area, including the Spanish Public Water Domain (RDPH).

4. Discussion

4.1. Climate Change Effect

Comparison between observed meteorological data and projections of climate scenarios, for a common time interval, has revealed a significant difference between the series. This means that the results must in any case be interpreted in relative terms, evaluating trends and not absolute values.

Results for both selected climate models show important differences between each other in absolute and relative terms, indicating that there is significant uncertainty in the projections, especially due to rainfall; and they suggest that for local impact studies, further analysis to regionalize outputs from global climate models still needs to be done. For the results to be reliable, climate models must adequately represent extreme phenomena, as most of them are suitable for evaluating water resource evolution.

There is a large uncertainty in climate projections that influences the estimation of future flood risk. The crucial action in the case of adaptation to floods is to carry out a detailed analysis to choose
the best climate model and use results in relative terms between the short term (1st Stage) and long term (2nd Stage) of the projection period [4].

The proposed methodology allows one to determine in terms of hazard and flood risk, the effect that climate change has on a given territory, considering both variable rainfall and temperature, and enables a fast evaluation of various climate models and a comparison of their differences.

This evaluation enables one to define actions in terms of a cost–benefit analysis and prioritize the ones that should be included in flood risk management plans due to climate change, as these management plans must contain effective actions in the short, medium and long term and cannot ignore the effect of climate change.

In the specific case of Hijar River Basin, and Reinosa, MRI-CGCM3 model trend analysis shows that climate change will increase damage to society, both economic and personal, while BCC-CSM1-1-m shows a small decrease. As the MRI-CGCM3 model fits better with annual maximum real daily flow rates than BCC-CSM1-1-m, it can be concluded that climate change will cause a significant increase of potential affected inhabitants and economic damage due to flood risk that will require mitigation actions.

This assumption might match with previous years’ observations, especially given the high number of low probability events recorded in Spain. This is the specific case of the Hijar River that in 2019 registered two floods, the one on December 2019 being the largest ever registered in Reinosa Gauging Station and related with a low probability event (300 years return period). This conclusion is consistent with the Fifth Assessment Report (AR5) of the IPCC (2013–14), which points out that it is likely that the frequency or intensity of intense rainfall has increased in Europe.

4.2. Future Research

As already mentioned, this methodology could be applied in every potential significant flood risk area through a water authority flood risk management plan in order to prioritize actions.

Firstly, all available regional climate models could be selected and evaluated. Finally, a sensitive RCP analysis with RCP 4.5 scenario could be carried out.

Supplementary Materials: The following are available online at http://www.mdpi.com/2073-4441/12/4/1114/s1.

Spreadsheet1: Climate_Models_Input_Data.xlsm.

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