Estimating Dynamic Model Parameters for Adaptive Protection and Control in Power System

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Abstract—This paper presents a new approach in estimating important parameters of power system transient stability model such as inertia constant $H$ and direct axis transient reactance $x_d'$ in real time. It uses a variation of unscented Kalman filter (UKF) on the phasor measurement unit (PMU) data. The accurate estimation of these parameters is very important for assessing the stability and tuning the adaptive protection system on power swing relays. The effectiveness of the method is demonstrated in a simulated data from 16-machine 68-bus system model. The paper also presents the performance comparison between the UKF and EKF method in estimating the parameters. The robustness of method is further validated in the presence of noise that is likely to be in the PMU data in reality.

Index Terms—Power system dynamic model, parameters estimation, unscented Kalman filter, measurement-based, phasor measurement units, synchrophasors

NOMENCLATURE

$x(t), x_k$ Continuous and discrete state variables, respectively,

$y(t), y_k$ Continuous and discrete output variables, respectively,

$u(t), u_k$ Continuous and discrete input variables, respectively,

$v(t), v_k$ Continuous and discrete process noise variables, respectively,

$w(t), w_k$ Continuous and discrete measurement noise variables, respectively,

$f(\cdot), h(\cdot)$ State update and measurement function, respectively,

$\hat{x}_k$, $P_{x_k}$ Estimated mean and covariance of the state,

$Q$, $R$ Process and measurement noise covariance, respectively,

$x_k^o$, $X_k$ Augmented state variables,

$\hat{X}_k$, $P_{X_k}$ Estimated mean and covariance of augmented state, respectively,

$\psi$ Parameters vector,

$\Delta t$ Time step,

$L$ Dimension of state vector,

$\chi$, $\chi^-$ Sigma points and predicted sigma points of state vector, respectively,

$n, W$ Length and associated weight of sigma points, respectively,

$\hat{X}_k^-, P_{X_k^-}$ Weighted mean and covariance of predicted sigma points, respectively,

$\gamma^-$ Sigma points of predicted measurement,

$\hat{y}_k^-, P_{y_k^-}$ Weighted mean and covariance of sigma points of predicted measurement, respectively,

$P_{x_k^-y_k^-}$ Cross-correlation matrix,

$K_k$ Kalman gain,

$\delta$, $\omega$, $\omega_0$, $\omega_B$ Rotor angle (rad), rotor speed (pu), synchronous speed (pu) and base speed (rad/s), respectively,

$P_m$ Mechanical power (pu),

$P_g$, $Q_g$ Active power (pu) and reactive power (pu), respectively,

$V_g$, $\theta_g$ Voltage magnitude (pu) and phase angle (rad), respectively,

$E_g$, $x_d'$, $H$ Generator internal voltage (pu), transient reactance (pu) and inertia constant (s), respectively,

$V_g^u$, $P_g^u$ Pseudo input for voltage magnitude $V_g$ and active power $P_g$, respectively,

$V_g^w$, $P_g^w$ Pseudo process noise for voltage magnitude $V_g$ and active power $P_g$, respectively.

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I. INTRODUCTION
The objective of dynamic model parameters estimation is to provide an accurate representation of the dynamic behaviour of the system for simulation studies. Conventionally, short-circuit test on unloaded machine represented the standard measure of transient performance and various commonly accepted approximations formed the basis of model parameter derivation. However, due to its limitation on providing q-axis transient and sub-transient constant, several alternative tests, such as enhanced sudden short circuit test, stator decrement test and standstill frequency response test have been proposed to obtain better representation of the dynamic model [4]. Although accurate, these approaches are not economically feasible because the generator under investigation must be offline.

Online methods have been proposed to address the pitfall of the staged test approach to identify the dynamic model parameters. The approaches underlying these methods are diverse, e.g., trajectory sensitivity [5], extended Kalman filter (EKF) [6], non-linear least square technique [7], Newton Raphson [8] and Euler [9]. Despite having advantages over offline methods, these techniques have some limitations. The methods assume the availability of accurate rotor angle and speed; field voltage and current; terminal voltage and current; and active and reactive power measurements. In practice, it is not always possible to have all these measurements time-stamped.

PMU measurements driven model parameters estimation has been proposed in the literature. The PMU provides the data across the network with time synchronous stamping. The maximum likelihood estimation (MLE) is proposed to estimate the dynamic model parameters of the system in [10]. The method requires a priori additional information of the state variable to estimate the parameters accurately. Other effort integrates hybrid dynamic simulation, trajectory sensitivity, parameter correlation analysis and minimum variance criterion to solve the estimation problem [11]. It is non-recursive and computationally exhaustive. Another approach, inter-area model estimation (IME), is reported in [12] and [13] to estimate the parameters. The proposed method extrapolates system impedance and inertia using the inter-area oscillation components in the voltage variables after disturbance. Besides being non-recursive, the complexity of the method increases with the number of generators in the system.

Numbers of research groups exploit variants of EKF [14], [15]. The EKF works on the assumption that all non-linear transformations are quasi-linear. Hence, EKF simply linearizes all non-linear transformations and substitutes Jacobian matrices for linear transformation. Although the EKF maintains an elegant and computationally efficient recursive update, it
III. DYNAMIC MODEL PARAMETER ESTIMATION USING UKF

Generally, power system dynamics is represented using a set of continuous-time nonlinear equation, given in (1).

\[ \dot{x}(t) = f[x(t), u(t), v(t)] \quad (1a) \]
\[ y(t) = h[x(t), u(t), v(t)] + w(t) \quad (1b) \]

where the \( x(t) \) vector represents the state variables, the \( y(t) \) vector represents the output variables, and \( u(t) \) is the input variables. Equations (1) are rewritten in discrete form with a time step of \( \Delta t \), given by (2).

\[
x_k = x_{k-1} + f[x_{k-1}, u_{k-1}, v_{k-1}]\Delta t
\]
\[ y_k = h[x_k, u_k, v_k] + w_k \quad (2a) \]

The state \( x_k \) is considered as a random variables with an estimated mean \( \hat{x}_k \) and an estimated covariance \( P_{\Delta k} \). The process noise \( v_k \) in (2) is assumed to be non-additive, while the measurement noise \( w_k \) is assumed to be additive. The covariance matrix for \( v_k \) and \( w_k \) are denoted by \( Q \) and \( R \), respectively. Both are assumed to be constant. Assume that (2) is parameterised by the unknown vector \( \psi_k \). The state \( x_k \) and the set of model parameters \( \psi_k \) need to be estimated simultaneously. If \( \psi \) is also treated as a state, then it may be augmented with \( x_k \) to give an augmented state vector \( x_k^a \), i.e. \( x_k^a = [x_k^T, \psi_k^T]^T \). The state-space model in (2) is reformulated as:

\[
x_k^a = f[x_k^a-1, u_k-1, v_k-1] \quad (3a)
\]
\[ y_k = h[x_k^a, u_k, v_k] + w_k \quad (3b) \]

Using the same approach in (3), the process noise \( v_k \) may also be concatenated with \( x_k^a \), resulting higher-dimensional state random variables \( X_k = [x_k^a^T, v_k] \) with an estimated mean \( \hat{X}_k \) and covariance \( P_{X_k} \). Hence, the state random variable is redefined as the augmentation of the original state \( x_k \), the set of unknown model parameter \( \psi_k \) and the process noise \( v_k \) given in (4):

\[
X_k = \begin{bmatrix} x_k^a \\ \psi_k \\ v_k \end{bmatrix} \quad (4)
\]

In a similar manner, the corresponding augmented state covariance is built up from the individual covariance matrices of \( x_k \), \( \psi_k \) and \( v_k \) given in (5):

\[
P_{X_k} = \begin{bmatrix} P_{x_k} & 0 & 0 \\ 0 & Q_{\psi_k} & 0 \\ 0 & 0 & Q_{v_k} \end{bmatrix} \quad (5)
\]

Hence, the state-space model in (3) is rewritten as follows,

\[
X_k = f[X_{k-1}, u_{k-1}] \quad (6a)
\]
\[ y_k = h[X_k, u_k] + w_k \quad (6b) \]

Consequently, given that the system differential equations (DEs), the measured signals from PMU and all noise covariances are available, the unknown parameter vector \( \psi_k \) is estimated using recursive algorithm by finding the real-time estimates of the mean and covariance of the augmented state \( X_k \).

A. Unscented Kalman Filter (UKF)

The idea of UKF is the propagation of the statistical distribution of state through the non-linear equations. This is realised by obtaining a set of vectors called sigma points, which capture the mean and covariance of the state \( X \) distribution. A set of sigma points, denoted as \( \chi_i \), are selected in such a way that the mean and covariance of these points are
\( \hat{X} \) and \( P_X \). Consequently, these points are transformed into a set of transformed points by applying \( \chi_i \) into a non-linear function. This process is described as follows:

\[
\gamma_i = h(\chi_i)
\]

(7)

Next, the mean \( \hat{y} \) and covariance \( P_y \) of the transformed points are calculated. The mean \( \hat{y} \) is the weighted average of the transformed points while the covariance \( P_y \) is the weighted outer product of the transformed points. For \( l \) numbers of sigma points, \( \hat{y} \) and \( P_y \) are calculated as follows:

\[
\hat{y} = \sum_{i=0}^{l} W_i \gamma_i \\

P_y = \sum_{i=0}^{l} W_i (\gamma_i - \hat{y})(\gamma_i - \hat{y})^\top
\]

(8a)

(8b)

To provide an unbiased estimate, the weight \( W_i \) used to calculate \( \hat{y} \) and \( P_y \) must be set such that:

\[
\sum_{i=0}^{l} W_i = 1
\]

(9)

In this paper, for \( L \) number of state, a set of \( l = 2L + 1 \) points is used to distribute the sigma points. The following set of points satisfied the condition described above:

\[
\begin{align*}
\chi_0 &= \hat{X} \\
W_0 &= 1 - \frac{L}{3} \\
\chi_i &= \hat{X} + \sqrt{\frac{l}{2} W_0 P_X}_{ji} \\
W_i &= \frac{1}{2L} W_0 \\
\chi_{i+L} &= \hat{X} - \sqrt{\frac{l}{2} W_0 P_X}_{ji+L} \\
W_{i+L} &= \frac{1}{2L} W_0
\end{align*}
\]

(10a)

(10b)

(10c)

(10d)

(10e)

(10f)

The set of sigma points described in (10) able to exploit any additional known information about the error distribution associated with an estimate and maintain the mean \( \hat{X} \) and covariance \( P_X \). This set of sigma points provides approximations accurate to a third order of Gaussian probability density functions, regardless of the forms of non-linear transformation function used in the estimation [21]. The weight associated with the new sigma point, \( W_0 \) provides a parameter for controlling some aspect of the higher moments of the distribution of sigma points without affecting the mean of the covariance. In this paper, the value of \( W_0 \) is set such that the fourth order error for a Gaussian is minimized [21]. Consequently, each sigma points is passed through the model of state evolution to obtain the predicted-state sigma points given as:

\[
\chi_k^- = f(\chi_{k-1}, u_{k-1})
\]

(11)

Subsequently, the weighted mean and covariance of the predicted sigma points \( \chi_k^- \) defined as \( \hat{X}_k^- \) and \( P_{X_k^-} \), respectively, are calculated using (12):

\[
\begin{align*}
\hat{X}_k^- &= \sum_{i=0}^{2L} W_i (\chi_{i,k}^-) \\
P_{X_k^-} &= \sum_{i=0}^{2L} W_i (\chi_{i,k}^- - \hat{X}_k^-)(\chi_{i,k}^- - \hat{X}_k^-)^\top
\end{align*}
\]

(12a)

(12b)

Subsequently, the predicted sigma points \( \chi_k^- \) are instantiante through the measurement equation to generate the predicted-measurement sigma points \( \gamma_k^- \) as follows:

\[
\gamma_k^- = h(\chi_k^-, u_k)
\]

(13)

Consequently, the weighted mean of the predicted measurement \( \bar{y}_k^- \), the corresponding covariance matrix \( P_{y^-} \) and the cross-correlation matrix \( P_{\chi^- y^-} \) are computed as shown in (14). The matrix \( P_{\chi^- y^-} \) represents the cross-correlation between the difference of the predicted-state sigma points \( \chi_{i,k}^- \) and the difference of predicted-measurement sigma points \( \gamma^- \) with the corresponding predicted-measurement \( \bar{y}_k^- \):

\[
\begin{align*}
\bar{y}_k^- &= \sum_{i=0}^{2L} W_i (\gamma^-_{i,k}) \\
P_{y^-} &= \sum_{i=0}^{2L} W_i (\gamma^-_{i,k} - \bar{y}_k^-)(\gamma^-_{i,k} - \bar{y}_k^-)^\top + R \\
P_{\chi^- y^-} &= \sum_{i=0}^{2L} W_i (\chi^-_{i,k} - \hat{X}_k^-)(\gamma^-_{i,k} - \bar{y}_k^-)^\top
\end{align*}
\]

(14a)

(14b)

(14c)

Finally, the Kalman gain matrix \( K_k \) is calculated to find the mean \( \hat{X}_k \) and covariance matrix \( P_{X_k} \) as given in (15):

\[
\begin{align*}
K_k &= P_{\chi^- y^-}(P_{y^-})^{-1} \\
\hat{X}_k &= \hat{X}_k^- + K_k (y_k - \bar{y}_k) \\
P_{X_k} &= P_{X_k^-} - K_k P_{y^- y^-} K_k^\top
\end{align*}
\]

(15a)

(15b)

(15c)

B. Implementation of UKF for dynamic model parameters estimation

Power system first swing dynamics is represented as follows:

\[
\begin{align*}
\frac{d\delta(t)}{dt} &= (\omega(t) - \omega_\delta) \omega_s \\
\frac{d\omega(t)}{dt} &= \frac{1}{2H} (P_m - P_g(t) - D(\omega(t) - \omega_s))
\end{align*}
\]

(16a)

(16b)

where \( \delta(t) \), \( \omega(t) \), \( \omega_\delta \) and \( \omega_s \) are rotor angle, rotor speed, synchronous speed and base speed, respectively. Neglecting the damping coefficient \( D \), the discrete form of (16) is given by:

\[
\begin{align*}
\delta_{k} &= \delta_{k-1} + (\omega_{k-1} - \omega_\delta) \omega_s \Delta t \\
\omega_{k} &= \omega_{k-1} + \frac{\Delta t}{2H} (P_m - P_{g(k-1)} - D(\omega(t) - \omega_s)) \\
&= \omega_{k-1} + G_{k-1} (P_m - P_{g(k-1)})
\end{align*}
\]

(17a)

(17b)

Since \( \Delta t \) and \( H_k \) are constant, \( \omega_k \) is simplified by substituting the term \( \frac{\Delta t}{2H} \) with \( G_k \) to reduce the nonlinearity of the
equation. Consequently, the state vector of the system given in (17) is defined as $x_k = [\delta_k \ \omega_k]^\top$ and is parameterized by inertia constant $H$, transient impedance $x'_d$ and generator internal voltage $E_q$. These parameters and variable are unknown and represented by the vector $\psi_k = [E_{q_k} \ x'_d \ G_k]^\top$.

As described in (3), the state $x_k$ and the unknown parameter vector $\psi_k$ are simultaneously estimated by augmenting these two vectors into a higher-dimensional state variables $x^*_k = [\delta_k \ \omega_k \ E_{q_k} \ x'_d \ G_k]^\top$. Hence, to accommodate this change, the state evolution equation in (17) is reformulated as:

\begin{align}
\delta_k &= \delta_{k-1} + (\omega_{k-1} - \omega_0) \omega_0 \Delta t \\
\omega_k &= \omega_{k-1} + G_{k-1} (P_m - P_{g_{k-1}}) \\
E_{q_k} &= E_{q_{k-1}} \\
x'_{d_k} &= x'_{d_{k-1}} \\
G_k &= G_{k-1}
\end{align}

(18a)-(18e)

In (18), the mechanical input power $P_m$ is assumed to be known. It is approximated to the electrical power measured at the generator terminal bus prior to a disturbance in the system. The dynamic behaviour of one generator unit can be analysed independently from the dynamic behaviour of the rest of the network. This is realised by separating the signals at the terminal bus into two groups: inputs and measurements. It is assumed that PMU provides time-tagged voltage magnitude $V_g$, phasor angle $\theta_g$, active power $P_g$ and reactive power $Q_g$ measurements at the generator terminal bus to monitor the dynamic behaviour of the generators. Hence, $V_g$ and $P_g$ at the terminal bus are treated as the input signal, while $\theta_g$ and $Q_g$ are treated as the measurement to decouple one generation unit from the rest of the system. The equations for the measurement quantities, $\theta_g$ and $Q_g$ of a generation unit are:

\begin{align}
\theta_{g_k} &= \theta_{g_{k-1}} - \tan^{-1} \left( \frac{P_{g_k} \ x'_{d_k}}{\sqrt{(E_{g_k} V_{g_k})^2 - (P_{g_k} x'_{d_k})^2 - V_{g_k}^2} \ x'_{d_k}} \right) \\
Q_{g_k} &= \sqrt{(E_{g_k} V_{g_k})^2 - (P_{g_k} x'_{d_k})^2 - V_{g_k}^2} \ x'_{d_k}
\end{align}

(19a)-(19b)

In the presence of noise in the measured signals, dealing with $V_g$ and $P_g$ may cause a problem to the UKF algorithm. Hence, the actual values of $V_g$ and $P_g$ have to be redefined to include the effect of noises in the estimation algorithm. Consequently, the actual inputs ($V_g$ and $P_g$) are equal to the differences of their measured values ($V_{g}^u$ and $P_{g}^u$) and the associated noises ($V_{g}^w$ and $P_{g}^w$). The associated noises $V_{g}^w$ and $P_{g}^w$ also drive the system modelled in the UKF algorithm. They are modelled as in (17) and given below:

\begin{align}
V_{g_k} &= V_{g_k}^u - V_{g_k}^w \\
P_{g_k} &= P_{g_k}^u - P_{g_k}^w
\end{align}

(20a)-(20b)

Hence, $V_{g_k}^u$ and $P_{g_k}^u$ formed a pseudo input vector $u_k$ while $V_{g_k}^w$ and $P_{g_k}^w$ formed a pseudo process noise vector $w_k$. As derived in (4), the process noise $v_k$ is concatenated with the state vector and the unknown parameters $\psi_k$ vector to form an augmented state $X_k$. This formulation incorporates the process noises $v_k$ into the predicted state vector with the same level of accuracy as the propagated estimation errors without the needs to calculate the Jacobian, Hessian or other numerical approximation [16]. Therefore, the UKF algorithm as described in the preceding subsection will be directly applied to estimate $X_k$.

IV. APPLICATION, RESULTS AND ANALYSIS

The 16-machine 68-bus system model is considered as the test system. The bus data, line data and dynamic characteristics of the systems are available in [22]. Fig. 1 shows the single line diagram of the system. Nonlinear simulations of the test system model are performed in MATLAB Simulink. The synchronous generators in the test system are modelled as classical models. The mechanical power input to the generators is assumed to be constant. The disturbance considered for this study is a three-phase bolted fault at bus 21. The fault is applied at $t = -0.9s$ and cleared by removing line 21-22 after 100 ms. The proposed method is applied on the measured data 800 ms following the clearance of the fault to avoid transient error of the PMU estimation during the transition period from pre-fault to post-fault condition [2]. For parameter estimation, the proposed method is applied to the voltage magnitude $V_g$, phase angle $\theta_g$, active power $P_g$, and reactive power $Q_g$ signals from 16 machines.

The main aim of the proposed methodology is to provide a parameter estimation tool for adaptive protection and control application, mainly for adaptive out-of-step protection. Therefore, the scope is focused on the dynamic in power swing time scale (0.5 to 0.8 Hz) [23]. In this time scale, the speed voltage $E_q$ is relatively constant because of large field circuit time constant (constant flux linkage situation). Transient reactance $x'_d$ and inertia constant $H$ will not be affected by the inclusion of sophisticated electromagnetic dynamics model. Therefore, a classical model (speed voltage behind a transient reactance) is adequate for the purpose of this investigation. The choice of sampling frequency is important. In this paper, 120 Hz was used as recommended for 60 Hz system in the recent IEEE Standard for Synchrophasor Measurements for Power System C37.118.1-2011 [24].
Fig. 2 illustrates the signals measured from Generator #4 terminal bus. Fig. 2a-2d display the measured data of $V_g$, $\theta_g$, $P_g$, and $Q_g$, respectively. All other generators are measured but not shown because of the lack of space. As described in Section III, $V_g$ and $P_g$ are used as the input, while $\theta_g$ and $Q_g$ are used as the measurements for the UKF. The proposed method is applied to the whole set of measured data and the parameters are estimated. The initial parameters for UKF algorithm used in this paper are described as follows:

$$X_0 = [x_0 \psi_0 v_0]^T$$
$$= [\delta_0 \omega_0 \ E_{q_0} \ x'_{d_0} 
 H_0 
 0 
 0]^T$$

$$= 1 \pi/2 
 1.0 
 0.5 
 5.0 
 0 
 0]^T$$

$$P_{x_0} = \text{diag} \{[1 1]\}$$
$$Q_{\psi_0} = \text{diag} \{[1 1 1]\}$$

$$Q_{v_0} = \text{diag}\{[1 \times 10^{-4} 
 1 \times 10^{-3}]\}$$

$$P_{x_0} = \text{diag}\{[P_{x_{q_0}} \ Q_{\psi_0} \ Q_{v_0}]\}$$

$$R = \text{diag}\{[1 \times 10^{-4} 
 1 \times 10^{-3}]\}$$

The values of initial parameters influence the convergence rate of the proposed method. The closer the value of initialised parameters with the actual value of the parameters, the faster is the convergence of the proposed method in estimating the dynamic model parameters of the system. However, the work presented in this paper assumes that the initial parameters are unknown. Therefore, the proposed method is initialised at the same value to provide an unbiased assumption in estimating the dynamic models parameters using UKF. The initial values for the covariance matrix of $P_{x_0}$ and $Q_{\psi_0}$ are not important. It will be updated throughout the UKF iteration process and its value will become zero if the algorithm converged. On the hand, the values of $Q_{v_0}$ and $R$ represent the process and measurement noise covariance matrix and their values are assumed to be known. Fig. 3 shows the results of the dynamic model parameters estimation for the 16-machine 68-bus test system model.

Fig. 3a, 3b and 3c display the convergence of $E_q$, $x'_d$ and $H$, respectively. The dashed line indicates the convergence of estimated parameters obtained using the proposed method, while the solid line represents the actual parameters of the test system. In this application, the parameters are assumed to be unknown. The initial parameters were set arbitrarily. All the results in the figure converged to their actual value. $E_q$ is initialised arbitrarily at 1.0 per unit. After first iteration, $E_q$ increased before it became constant at 1.1250 per unit after 1.0 s. On the other hand, the initial value of $x'_d$ is set to 0.5 per unit arbitrary. After 1.0 s, $x'_d$ is converged to 0.3868 per unit. Similar observation can be made for $H$, where the value is initially set at 5.0 s and consequently converged at 4.1627 s after 1.0 s.

Fig. 4 shows the estimation of rotor angle and speed of Generator #4. The dashed line indicates the estimated state, while the solid line represents the simulated state. The estimated rotor angle and speed match very well with the simulated rotor angle and speed of the machine.

Table I summarises the results of the dynamic model parameters estimation for 16-machine 68-bus test system model. $E_q$, $x'_d$ and $H$ for all machines were initialised to 1.0 pu, 0.5 pu and 5.0 s, respectively. From the table it can be observed that the estimated parameters are very close to the actual
value of the dynamic model parameters for all machines. The maximum percentage errors in estimation for $E_q$, $x_d'$ and $H$ are 0.29%, 3.26% and 0.21%, respectively. This indicates that the results obtained using dynamic model parameters estimation technique proposed in this paper are accurate and consistent for all machines in a large interconnected power system context.

The proposed method is able to estimate the dynamic model parameters of the systems without prior knowledge of system model. The UKF method requires a time window of 1.0 s to estimate the parameters accurately. Therefore, the method requires 120 iterations to precisely estimate the parameters using the measured data sampled at every 8.33 ms. The speed of computation of UKF method recorded in this paper is 281.2 μs per iteration. Hence, considering the time windows required for estimation and the computation time of UKF, it only requires 1.0337 s for the proposed method to precisely estimate $E_q$, $x_d'$ and $H$ at real time. Typically, a power swing oscillates with the frequency of 0.5-0.8 Hz [23], which gives a time windows of 1.25-2.0 s to analyse the oscillation as it develops. Thus, the speed of estimation using the proposed method is sufficient for adaptive out-of-step protection application which focuses only on the first few swings of the system.

V. COMPARISON AND PERFORMANCE ROBUSTNESS

In this section, the accuracy of the dynamic model parameters estimated using the proposed method is compared with the results obtained using the EKF approach [14], [15]. The performance of the proposed method and the EKF method is also evaluated in the presence of noise in the measured signals. Using identical operating condition, the 16-machine 68-bus test system model is used for this evaluation.

A. Parameter estimation using EKF

The details of the EKF method for dynamic model parameter estimation are reported in [14], [15] and is briefly discussed here to extend the discussion of the idea presented in this paper. The EKF is formulated as a two-step prediction-correction process. The prediction step is a time update using the discretized differential equations as follows:

\[
\delta_k = \delta_{k-1} + (\omega_{k-1} - \omega_0) \Delta t \\
\omega_k = \omega_{k-1} + \frac{\Delta t}{2H} P_m \ldots
\]

\[
E_{q_k} = E_{q_{k-1}} \\
x_d'_{k} = x_d'_{k-1} \\
H_k = H_{k-1}
\]

The discretized differential equations in (22) predict the state and measurement variables of the next time step using the estimated values of the state and measurement variables of the previous time step. $E_q$, $x_d'$ and $H$ are the unknown parameters that need to be estimated. Apart from the state variables, the process also estimates priori error covariance matrix corresponding to the state variables. Consequently, the estimated measurement is calculated using the following equations:

\[
P_{g_k} = \frac{E_{q_{k-1}} V_{q_{k-1}}}{x_{d_k-1}'} \sin \left( \delta_{k-1} - \theta_{g_{k-1}} \right)
\]

\[
Q_{g_k} = -V_{g_k}^2 + E_{q_k} V_{q_k} \cos \left( \delta_k - \theta_{g_k} \right) x_{d_k}'
\]

Next step involves the calculation of the Kalman gain, which corrects the error of the estimated state variables based on the discrepancy between the estimated and the actual measurement. The following set of equations summarized the prediction-correction process of EKF.

**Prediction:**

\[
x_k^- = f(x_{k-1}, u_{k-1}, 0)
\]

\[
P_k^- = A_k P_{k-1} A_k^\top + W_k Q_{k-1} W_k^\top
\]

**Correction:**

\[
K_k = P_k^- H_k^\top (H_k P_k^- H_k^\top + V_k R_k V_k^\top)^{-1}
\]

\[
x_k = x_k^- + K_k [y_k - h(x_k^-, u_{k-1}, 0)]
\]

\[
P_k = (I - K_k H_k) P_k^-
\]

where,

\[
A_k = \frac{\partial f(x_{k-1}, u_{k-1}, 0)}{\partial x}, \quad W_k = \frac{\partial f(x_{k-1}, u_{k-1}, 0)}{\partial w}
\]

\[
H_k = \frac{\partial h(x_{k-1}, u_{k-1}, 0)}{\partial x}, \quad V_k = \frac{\partial h(x_{k-1}, u_{k-1}, 0)}{\partial w}
\]

Using this process, the unknown parameters $E_q$, $x_d'$ and $H$ estimation will approach their actual values.

### TABLE I

| i | $E_q^{est}$ | $E_q^{act}$ | $x_d'^{est}$ | $x_d'^{act}$ | $H^{est}$ | $H^{act}$ |
|---|---|---|---|---|---|---|
| 1 | 1.1867 | 1.1871 | 0.2480 | 0.2485 | 3.4000 | 3.4030 |
| 2 | 1.1176 | 1.1194 | 0.4253 | 0.4296 | 4.9494 | 4.9540 |
| 3 | 1.1232 | 1.1250 | 0.3831 | 0.3868 | 4.9623 | 4.9673 |
| 4 | 1.0629 | 1.0606 | 0.2995 | 0.3081 | 4.1629 | 4.1627 |
| 5 | 1.1227 | 1.1224 | 0.3600 | 0.3595 | 4.7667 | 4.7769 |
| 6 | 1.1611 | 1.1607 | 0.3543 | 0.3534 | 4.9107 | 4.9303 |
| 7 | 1.1145 | 1.1144 | 0.2990 | 0.2987 | 4.3267 | 4.3344 |
| 8 | 1.0489 | 1.0485 | 0.3533 | 0.3519 | 3.9150 | 3.9221 |
| 9 | 1.0932 | 1.0930 | 0.4872 | 0.4867 | 4.0365 | 4.0427 |
| 10 | 1.0307 | 1.0305 | 0.4868 | 0.4846 | 2.9106 | 2.9133 |
| 11 | 1.0093 | 1.0093 | 0.2531 | 0.2536 | 2.0053 | 2.0068 |
| 12 | 1.1527 | 1.1523 | 0.5525 | 0.5515 | 5.1791 | 5.1827 |
| 13 | 1.0398 | 1.0405 | 0.3345 | 0.3454 | 4.0782 | 4.0786 |
| 14 | 1.0030 | 1.0029 | 0.2850 | 0.2837 | 3.0000 | 3.0004 |
| 15 | 1.0023 | 1.0022 | 0.2850 | 0.2781 | 3.0000 | 2.9974 |
| 16 | 1.0233 | 1.0231 | 0.3590 | 0.3572 | 4.4500 | 4.4460 |
In order to evaluate the performance of the proposed method, the dynamic model parameters estimated using the proposed method is compared with the results obtained using EKF. For this evaluation, 16-machine 68-bus test system model is used to simulate the measurement of \( V_g, \theta_g, P_g \) and \( Q_g \) for every generator sampled at 120 Hz. The disturbance considered for this evaluation is similar to the disturbance considered in Section IV. Using identical initialization of the parameters, the estimation of \( E_q, x_q' \) and \( H \), for Generator #4 obtained using UKF and EKF is illustrated in Fig. 5.

The results in Fig. 5 show that \( E_q, x_q' \) and \( H \) estimated using UKF and EKF converged to its actual value of 1.0 pu, 0.5 pu and 5.0 s, respectively. This implies that both UKF and EKF are able to estimate the dynamic model parameters in the system. However, it is observed from the results that the proposed method shows better performance in estimating the parameters, especially for the estimation of \( x_q' \). The EKF requires about 3.5 s while the proposed method only requires about 1.0 s to converge to its actual value of \( x_q' \). This is because the proposed method has a better approximation of nonlinear process in each iteration compared to the EKF approach.

It is also necessary to compare the computational speed of UKF and EKF, formulated to estimate the dynamic model parameters. The computational speed of EKF is 497.6 \( \mu \)s per iteration while the computational speed of UKF is 281.2 \( \mu \)s per iteration to estimate \( E_q, x_q' \) and \( H \). The difference in computational speed of EKF and UKF is related to the computational load at each iteration for both methods. The EKF algorithm requires to update the Jacobian matrix at every step of computation to estimate \( E_q, x_q' \) and \( H \). On the other hand, the UKF method does not need the calculation of the Jacobian matrix. This finding is consistent with the discussion reported in [25]. This implies that the EKF consumes more computing power compared to the proposed method in estimating the dynamic model parameters of the system.

### C. Performance robustness

1) Performance under noise: It is well known that the presence of noise in the data influences the quality of any measurement-based method. This subsection evaluates the performance of the proposed technique in the presence of noise in the measured signals. For this evaluation, the measured data illustrates in Fig. 2 is added with white Gaussian noise and the proposed technique is applied on this data to estimate \( E_q, x_q' \) and \( H \) of the generator. The presence of noise affects the quality of the PMU measurements. It is assessed by the Total Vector Error (TVE) of the PMU measurements described as follows:

\[
\text{TVE} (n) = 100 \times \sqrt{\frac{[X_i(n) - X_r(n)]^2 + [x_r(n) - X_r(n)]^2}{[X_r(n)]^2 + [x_r(n)]^2}}
\]  

(25)

As recommended in [24], the TVE of PMU measurement should be less than 1%. However, in order to validate the robustness of the proposed method in filtering out the effect of noise, TVE less than 3% is used in this analysis. The plots of the data are given in Fig. 6a-6d represent \( V_g, \theta_g, P_g \), and \( Q_g \) for Generator #4. Fig. 7 displays the result obtained from the application of the UKF method using the measured signals with noise.

The estimation of \( E_q, x_q' \) and \( H \) using the measured data with noise are illustrated in Fig. 7a-7c. The green lines represent the 99% confidence interval of the estimated parameters. The results clearly show that the UKF method has a fast convergence rate even with the presence of noise in the measured data. All parameters converged to the actual value in about 1.0 s. \( E_q, x_q' \) and \( H \) converged to 1.0627 pu, 0.2998 pu and 4.2278 s, respectively. It is also observed that the actual values of the parameters lie between the upper and lower bounds for the 99% confidence interval of the estimated parameters.
The convergence of $E_q$, $x_d'$, and $H$ using both methods are plot in Fig. 8a-8c, respectively.

The results displayed in Fig. 8 show that both methods are able to estimate $E_q$ accurately using the measured signals with noise. The EKF method requires about 5.0 s while the proposed method only requires about 0.2 s to estimate $E_q$ accurately. The estimation of $x_d'$ and $H$ using EKF approach shows that the presence of noise in the measured data influences the accuracy of the dynamic model parameter estimation technique. The EKF method shows limitation in estimating $x_d'$ and $H$ even with the presence of noise in the measured data. This may be due to the fact that the approach proposed in this paper accurately approximate the posterior mean and covariance up to the third order of the Taylor series expansion for any non-linear system while the EKF method only achieved first-order accuracy [21]. The results imply that the proposed method outperforms EKF in estimating the dynamic model parameter in the system, particularly in the presence of noise in the measured data. These attributes are important for any data-driven estimation tools as the presence of the noise in measured data is inevitable.

3) Performance in coloured noise: Coloured noise covers a wide range of intensities and bandwidths for a variety of flow fluctuation during power system operation [26]. Since it may be present in the measured data, hence influencing the accuracy of any data-driven method, it is necessary to assess the operation of the proposed method in the presence of coloured noise in the measured signals. The coloured noise used for this evaluation is generated by filtering the white Gaussian noise used to produce signals in Fig. 6 through a low pass finite impulse response (FIR) filter of order 31 with normalized cut-off frequency of 0.5 [27]. The measured signals illustrated in Fig. 2 are added with the coloured noise and the UKF method is applied to estimate the dynamic model parameters. As depicted in the table, the estimated value of $E_q$, $x_d'$ and $H$ are very close with the actual value of the dynamic model parameters, even with the presence of noise in the measured signals.

The proposed algorithm is applied to all machines in the test system model and the results are shown in Table II. In Table II, the results obtained using the UKF method is validated by comparing the estimated results with the actual value of the dynamic model parameters. As depicted in the table, the estimated value of $E_q$, $x_d'$ and $H$ are very close with the actual value of the dynamic model parameters, even with the presence of noise in the measured signals.

2) Comparison with EKF under noise: Both UKF and EKF require measured signal from PMU to estimate $E_q$, $x_d'$ and $H$ of the system. It is worthwhile to assess the performance of UKF and EKF in the presence of noise in the measured signals. In this investigation, the UKF and EKF are applied to the measured signals with TVE of 3% illustrated in Fig. 6.

The convergence of $E_q$, $x_d'$ and $H$ using both methods are plot in Fig. 8a-8c, respectively.

The results displayed in Fig. 8 show that both methods are able to estimate $E_q$ accurately using the measured signals with noise. The EKF method requires about 5.0 s while the proposed method only requires about 0.2 s to estimate $E_q$ accurately. The estimation of $x_d'$ and $H$ using EKF approach shows that the presence of noise in the measured data influences the accuracy of the dynamic model parameter estimation technique. The EKF method shows limitation in estimating $x_d'$ and $H$ even with the presence of noise in the measured data. This may be due to the fact that the approach proposed in this paper accurately approximate the posterior mean and covariance up to the third order of the Taylor series expansion for any non-linear system while the EKF method only achieved first-order accuracy [21]. The results imply that the proposed method outperforms EKF in estimating the dynamic model parameter in the system, particularly in the presence of noise in the measured data. These attributes are important for any data-driven estimation tools as the presence of the noise in measured data is inevitable.

### Table II

| i | $E_q^{\text{act}}$ | $E_q^{\text{est}}$ | $x_d'^{\text{act}}$ | $x_d'^{\text{est}}$ | $H^{\text{act}}$ | $H^{\text{est}}$ |
|---|------------------|------------------|------------------|------------------|----------------|----------------|
| 1 | 1.1867           | 1.1803           | 0.2480           | 0.2354           | 3.4000         | 3.5498         |
| 2 | 1.1176           | 1.1207           | 0.4253           | 0.4335           | 4.9494         | 5.0670         |
| 3 | 1.1232           | 1.1158           | 0.3831           | 0.3668           | 4.9623         | 5.0914         |
| 4 | 1.0629           | 1.0627           | 0.2995           | 0.2998           | 4.1629         | 4.2278         |
| 5 | 1.1227           | 1.1234           | 0.3600           | 0.3558           | 4.7667         | 4.6444         |
| 6 | 1.1611           | 1.1669           | 0.3543           | 0.3714           | 4.9107         | 4.7569         |
| 7 | 1.1145           | 1.1117           | 0.2990           | 0.2997           | 4.3267         | 4.3902         |
| 8 | 1.0489           | 1.0529           | 0.3538           | 0.3659           | 3.9150         | 3.7245         |
| 9 | 1.0932           | 1.0858           | 0.4872           | 0.4633           | 4.0365         | 4.2310         |
| 10| 1.0307           | 1.0345           | 0.4868           | 0.5073           | 2.9106         | 3.0081         |
| 11| 1.0093           | 1.0091           | 0.2531           | 0.2556           | 2.0053         | 2.0931         |
| 12| 1.1527           | 1.1485           | 0.5525           | 0.5456           | 5.1791         | 5.1894         |
| 13| 1.0398           | 1.0430           | 0.3345           | 0.3618           | 4.0782         | 4.0552         |
| 14| 1.0030           | 1.0034           | 0.2850           | 0.3025           | 3.0000         | 2.9742         |
| 15| 1.0023           | 1.0024           | 0.2850           | 0.3056           | 3.0000         | 3.0075         |
| 16| 1.0233           | 1.0218           | 0.3590           | 0.3559           | 4.4500         | 4.5790         |

The proposed algorithm is applied to all machines in the test system model and the results are shown in Table II. In Table II, the results obtained using the UKF method is validated by comparing the estimated results with the actual value of the dynamic model parameters. As depicted in the table, the estimated value of $E_q$, $x_d'$ and $H$ are very close with the actual value of the dynamic model parameters, even with the presence of noise in the measured signals.

The results displayed in Fig. 8 show that both methods are able to estimate $E_q$ accurately using the measured signals with noise. The EKF method requires about 5.0 s while the proposed method only requires about 0.2 s to estimate $E_q$ accurately. The estimation of $x_d'$ and $H$ using EKF approach shows that the presence of noise in the measured data influences the accuracy of the dynamic model parameter estimation technique. The EKF method shows limitation in estimating $x_d'$ and $H$ even with the presence of noise in the measured data. This may be due to the fact that the approach proposed in this paper accurately approximate the posterior mean and covariance up to the third order of the Taylor series expansion for any non-linear system while the EKF method only achieved first-order accuracy [21]. The results imply that the proposed method outperforms EKF in estimating the dynamic model parameter in the system, particularly in the presence of noise in the measured data. These attributes are important for any data-driven estimation tools as the presence of the noise in measured data is inevitable.
parameters of the system. Fig. 9 depicts the UKF estimation trace of $E_q$, $x_d'$ and $H$ in the presence of coloured noise in the measured data. For the purpose of comparison, the UKF estimation in the presence of white noise is also plotted in the same figure.

From the figure, it is observed that the UKF estimation of $E_q$, $x_d'$ and $H$ in the presence of white and coloured noise demonstrate good convergence to the actual value of parameters. The performance of the proposed method in the presence of coloured noise is similar to that of the proposed method in the presence of white Gaussian noise. Therefore, this implies that the proposed method is able to estimate $E_q$, $x_d'$ and $H$ of the system in the presence of coloured noise in the measured data. This is an important feature for any data-driven method as the fluctuation of power flows is inevitable during power system operation.

VI. MODEL VALIDATION

An accurate dynamic model should be able to replicate the system dynamic behaviour for any type of disturbance. The results obtained in Table I and II are substituted into the 16-machine 68-bus test system model. Three cases with different types of disturbances were considered in this study. The disturbances considered in this analysis are as follows,

Case 1 - Fault at bus 61, line 61-30 is removed to clear the fault after 50 ms,
Case 2 - Fault at bus 67, line 67-68 is removed to clear the fault after 100 ms,
Case 3 - Fault at bus 46, line 38-46 is removed to clear the fault after 100 ms.

Fig. 10 displays the response of the systems with this study. For all cases, the blue line indicates the response from the test system model using the parameters estimated in the presence of noise in measured data. The small difference between the response of the test system models for all cases indicate that the results obtained using UKF are able to represent the dynamic response of the system, even with the presence of noise in the measured data. Thus, the dynamic model parameters estimation technique proposed in paper is accurate, consistent and robust in filtering out the effect of noise in the measured signals.

VII. CONCLUSIONS

A measurement-based dynamic model parameter estimation for power system has been proposed. The approach is based on the application of augmented UKF based technique to estimate
the dynamic model parameters from wide-area voltage magnitude, voltage angle, real power and reactive power signals. The dynamic model parameters are estimated by augmenting the unknown states (rotor angle and speed) and parameters (inertia constant, transient reactance and internal voltage) into a single higher-dimensional state vector. Subsequently, the dynamic model parameters are estimated by using the proposed UKF on the augmented state vector.

The accuracy of the estimation is validated by comparing the estimated results with the actual dynamic model parameters of the system. The presence of noise always affects the performance of any data driven method. Nevertheless, the UKF method accurately estimates the dynamic model parameters even with the presence of noise in the measured data. The results demonstrate that the proposed method outperforms EKF in estimating the dynamic model parameter in the system, particularly in the presence of noise in the measured data. The method is simple, fast and does not require a priori details of the system information. Finally, estimating the value of the dynamic mode parameters in real time is essential to ensure appropriate operation of power system protection. This will be pursued as immediate future activity by adapting the relay characteristic to suit the current system operating condition.

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