Controllable Thermal Conductivity in Twisted Homogeneous Interfaces of Graphene and Hexagonal Boron Nitride

Wengen Ouyang, Huasong Qin, Michael Urbakh,* and Oded Hod

ABSTRACT: Thermal conductivity of homogeneous twisted stacks of graphite is found to strongly depend on the misfit angle. The underlying mechanism relies on the angle dependence of phonon–phonon couplings across the twisted interface. Excellent agreement between the calculated thermal conductivity of narrow graphitic stacks and corresponding experimental results indicates the validity of the predictions. This is attributed to the accuracy of interlayer interaction descriptions obtained by the dedicated registry-dependent interlayer potential used. Similar results for h-BN stacks indicate overall higher conductivity and reduced misfit angle variation. This opens the way for the design of tunable heterogeneous junctions with controllable heat-transport properties ranging from substrate-isolation to efficient heat evacuation.

KEYWORDS: Interfacial thermal conductivity, graphite, h-BN, twisted interface, misfit angle, phonon–phonon coupling, registry-dependent interlayer potential

Graphene is considered to be one of the most promising heat dissipating materials in nanoelectronics due to its ultrahigh in-plane room-temperature thermal conductivity of \( \approx 3000 \text{–} 5000 \) W \( \text{m}^{-1}\text{°K}^{-1} \). This, however, can be hindered by graphene–substrate interactions that may lead to a substantial reduction of the heat-transport due to phonon leakage across the graphene–substrate interface and strong interfacial scattering of flexural phonon modes. Such undesirable substrate effects can be reduced by considering multilayer graphene stacks. These are expected to effectively isolate the top graphene layers from the substrate due to the considerably lower cross-plane thermal conductivity (\( \approx 6.8 \) W \( \text{m}^{-1}\text{°K}^{-1} \)) while exhibiting high in-plane conductivity that can be tuned via the stack thickness.

Anisotropic thermal conductivity is also observed for bulk hexagonal boron nitride (h-BN) with in-plane and cross-plane thermal conductivities in the range of \( 390 \text{–} 420 \) and \( 2.5 \text{–} 4.8 \) W \( \text{m}^{-1}\text{°K}^{-1} \), respectively.

Efficient in situ tuning of the thermal conductivity of such graphitic structures can be achieved by controlling the twist angle between adjacent layers within the stack. This has been recently computationally demonstrated for finite-sized nanoscale few-layer graphene junctions. Two factors, however, limit the applicability of these results: (i) the simulations were performed using simplistic isotropic interlayer potentials that are known to be inaccurate for simulating the interlayer interactions in layered materials, and (ii) the relevance of the results for large-scale interfaces is questionable due to significant edge scattering effects inherent to the small finite-sized model systems studied.

To address these issues, we use anisotropic potentials to investigate the interlayer thermal conductivity of periodic graphene and h-BN stacks of varying thicknesses and twist angles. This allows us to gain fundamental understanding of the heat transport mechanisms in layered materials stacks and identify feasible means to control it. Our model system consists of two contacting identical AB (AA’)-stacked graphite (h-BN) slabs, whose interfacing graphene (h-BN) layers are twisted with respect to each other to create a stacking fault of misfit angle \( \theta \) (see Figure 1). Recent experiments demonstrated fine control over the misfit angle in such setups. The thickness of the entire construction is varied between 2.7–35 nm (8–104 layers), and periodic boundary conditions are applied in all directions. Heat transport simulations are performed using state-of-the-art anisotropic interlayer potentials (ILP) applied to the twisted stacks. These potentials were shown to capture well the structural, dynamic, and frictional properties of graphitic and h-BN layered systems, as well as their phonon spectra. A thermal bias is induced by applying Langevin thermostats with different temperatures to two layers residing on opposite sides away from the twisted...
Figure 1. Schematic representation of the simulation setup. Two identical AB-stacked graphite slabs (gray and orange) are twisted with respect to each other to create a stacking fault of misfit angle \( \theta \). A thermal bias is induced by applying Langevin thermostats to the two layers marked by dashed red (\( T_{\text{hot}} \)) and green (\( T_{\text{cold}} \)) rectangles. The arrows indicate the direction of the vertical heat flux. Since periodic boundary conditions are applied also in the vertical direction, two twisted interfaces are shown across which heat flows in opposite directions.

Figure 2. Twist-angle dependence of the cross-plane thermal conductivity of the entire stack (a,b), and the interfacial thermal resistance (c,d) of the twisted contact formed between the optimally stacked slabs of graphite (a,c) and bulk h-BN (b,d), respectively. Red circles and black triangles correspond to the results obtained using 8 and 16 layer models, respectively. The insets in panels c and d show the ratio between the twist angle-dependent ITR results obtained using 8 and 16 layer models. Error bars estimation procedure is discussed in Section 1 of the Supporting Information.

The thermal conductivity of both graphite and h-BN stacks is found to increase when doubling their thickness. To identify the source of this thickness dependence we plot in Figure 2c,d the interfacial thermal resistance (ITR) (see Section 1.2 of Supporting Information) associated with the twisted junction formed between the contacting graphene or h-BN layers of the two optimally stacked slabs. Note that unlike \( \kappa_{\text{CP}} \), which measures the conductivity of the entire stack, the ITR corresponds to the heat transport resistance of the two adjacent layers forming the twisted interface. Two important observations can be made: (i) The ITR, which measures only the resistance of the twisted interface, weakly depends on the slab thickness for any twist angle larger than zero (see insets of Figure 2c,d) indicating that the thickness dependence mainly arises from the conductivity of the optimally stacked slabs residing above and below the interface. Specifically, in the thickness range considered, the thinner the sample, the smaller the number of phonon modes that contribute to the thermal conductivity. This is because phonons of wavelength larger than the system thickness are eliminated. This reduction in density of vertical heat carrying phonon modes results in a decrease of the overall thermal conductivity with decreasing thickness.\(^{32-34}\) (ii) The ITR strongly depends on the twist angle demonstrating a \(~10\)-fold (4-fold) increase when the twist angle at the graphene (h-BN) interface is varied from 0° to 15°. This clearly indicates that the twist angle can be utilized to control the cross-plane thermal conductivity of hexagonal two-dimensional (2D) materials and to effectively thermally isolate the top layers from the underlying substrate.

The strong dependence of the cross-plane thermal conductivity of graphene and h-BN on the stacking fault twist angle is related to the degree of coupling between the phonon modes of the two contacting layers at the twisted interface. Note that the term “coupling” used herein is not related to the standard notion of phonon–phonon couplings due to anharmonic effects. Instead, we regard to the off-diagonal terms of the Hessians when represented in the basis of the harmonic phonon modes of the isolated layers. To demonstrate this, we write the dynamical matrix (the mass-reduced Fourier transform of the force constant matrix) in block form as follows

\[
\Phi(q) = \begin{pmatrix}
\Phi_{11}(q) & \Phi_{12}(q) \\
\Phi_{21}(q) & \Phi_{22}(q)
\end{pmatrix}
\]

(1)

where \( \Phi_{11}(q) \) and \( \Phi_{22}(q) \) are the block matrices relating to the first and second layer and \( \Phi_{12}(q) \) and \( \Phi_{21}(q) = \Phi_{12}^\dagger(\mathbf{q}) \) are evaluated at wavevector \( \mathbf{q} \). The interlayer phonon–phonon couplings are obtained by diagonalizing separately \( \Phi_{11}(q) \) and \( \Phi_{22}(q) \) such that \( \Phi_{11}(q) = U_{11}^\dagger(q)U_{11}(q) \) and \( \Phi_{22}(q) = U_{22}^\dagger(q)U_{22}(q) \).
frequencies ($\omega_i$) of the phonon modes of the two layers and $U_i(q)$ and $U_j(q)$ are unitary matrices of the corresponding eigenvectors. We now construct a global block diagonal transformation matrix of the form

$$U(q) = \begin{pmatrix} U_1(q) & 0 \\ 0 & U_2(q) \end{pmatrix}$$

and transform the full dynamical matrix as follows

$$U(q)^\dagger \Phi(q) U(q) = \begin{pmatrix} \Phi_{11}(q) & \Phi_{12}(q) \\ \Phi_{21}(q) & \Phi_{22}(q) \end{pmatrix}$$

where $\Phi_{12}(q) = U_1(q) \Phi_{12}(q) U_2(q)$ and $\Phi_{21}(q) = \Phi_{12}(q)$ are the interlayer phonon–phonon coupling blocks. Naturally, when the two layers are infinitely separated, these coupling blocks vanish and the diagonal blocks converge to those of the isolated layers.

The overall coupling between the two layers can be obtained from the individual phonon–phonon coupling matrix elements via Fermi’s golden rule, which reads as (see Section 7 of the Supporting Information for a detailed derivation):

$$\Gamma_{\text{tot}} = \frac{\pi \hbar}{2} \sum_{q_i} e^{-2|E_{q_i}|} Z \rho(E_{q_i}) |V_{\lambda,\lambda+3r/2}(q)|^2$$

where $Z = \sum_q e^{-2|E_q|}$ is the partition function, $E_{q_i}$ is the energy of phonons at branch $\lambda$ with wavevector $q_i$, $\rho(E_{q_i})$ is the density of states (DOS) at $E_{q_i}$, and $|V_{\lambda,\lambda+3r/2}(q)|^2$ is the coupling matrix element between branches of phonons of similar energy in the two layers, whose number of atoms in one unit cell is $r$. Note that Fermi’s golden rule derived in Section 7 of the Supporting Information and presented in eq 4 is closely related to the equivalent electronic transport expression derived from the Landauer–Büttiker approach within the nonequilibrium Green’s function formalism.

Using eq 4, we can rationalize the misfit angle dependence of the heat flux across the twisted interface from the calculated interphonon coupling. To that end, we performed room-temperature (300 K) simulations (technical details can be found in Section 5 of the Supporting Information) for tBLG with different misfits angles using the Green’s function molecular dynamics (GFMD) approach developed by Kong et al. as implemented in LAMMPS. The simulations allow us to evaluate the dynamical matrix from which the phonon–phonon couplings can be extracted (see details in Section 5 of the Supporting Information) and the overall heat transfer rate calculated. Figure 3 shows the resulting heat transfer rate (normalized to the value obtained for the aligned contact ($\theta = 0$)) as a function of the misfit angle compared to the interfacial thermal conductivity (ITC) defined as the inverse of the ITR presented in Figure 2c, ITC $\equiv 1/ITR$. The agreement between the calculated ITC and the Fermi’s golden rule results indicates that the dependence of the interlayer phonon–phonon couplings on the misfit angle is responsible for the strong angle dependence of the interfacial conductivity. Notably, the sharp heat conductivity drop at misfit angles in the range of $0^\circ$–$5^\circ$ as well as the small conductivity for larger misfit angles are well captured by Fermi’s golden rule.

To correlate our results with experimentally measured thermal conductivities that are often obtained for thick samples, we repeated our calculations for increasing stack thicknesses at fixed misfit angles. Figure 4 presents results for the calculated heat conductivity of graphite (panel a) and h-BN (panel b) stacks either aligned (open red circles) or twisted by $30.16^\circ$ (open black diamond symbols) as a function of the number of layers in the stack. The green dashed and black dash-dotted lines represent experimental results measured for graphite (a) (refs 9 and 42) and bulk h-BN (b) (refs 18 and 19). Panels (c) and (d) show the thickness dependence of the ITR extracted, using eq S1.2 in Section 1.3 of the Supporting Information, from the $\kappa_{\text{CP}}$ results for the graphic and h-BN junctions as presented in panels (a) and (b), respectively, using the same color code. Note that both axis scales are logarithmic. Error bars estimation procedure is discussed in Section 1 of the Supporting Information.
Comparing our calculated heat conductivities for the aligned contact (open red circles) to available experimental data for \( \sim 35 \) nm thick graphite slabs\(^1^2\) (dashed green line), we find that at the thickest model system considered of 104 graphene layers (\( \sim 35.4 \) nm thick) the calculated value of \( 0.85 \pm 0.05 \, \text{W/m·K} \) is in agreement with the measured value of \( \sim 0.7 \, \text{W/m·K} \). Furthermore, experimental values for bulk graphite\(^8\) indicate that the thermal conductivity continues to grow up to \( \sim 6.8 \, \text{W/m·K} \) (black dash-dotted line), which is consistent with the general trend of the calculated heat conductivity that does not saturate for the thickest model system considered. These results support the validity of our force-field and model systems to study the heat conductivity of twisted layered material interfaces. Available experimental results for the heat conductivity of bulk h-BN are marked by the dashed-dotted black and dashed-green lines in Figure 4b. In line with our findings for the graphitic interface, our calculated finite slab heat conductivities for the aligned interface (open red circles) continue to grow with the number of layers and are consistently below the bulk value.

Another important factor that may affect the interlayer thermal transport properties of 2D material stacks is the average temperature of the system, which was taken to be \( \sim 300 \, \text{K} \) in all above-mentioned simulations. To evaluate the sensitivity of our results toward this parameter, we repeated the heat conductivity and interfacial resistance calculations of optimally stacked graphite and h-BN stacks for an average temperature of \( 400 \, \text{K} \). The results, presented in Section 6 of the Supporting Information, indicate that the thickness dependence of \( \kappa_{\parallel} \) exhibits qualitatively similar behavior also at an average temperature of \( 400 \, \text{K} \) with a nearly uniform decrease in magnitude.

We note that previous calculations of the heat conductivity of twisted graphitic interfaces relied on LJ potentials describing the interlayer interactions.\(^1^2\)–\(^1^4,1^7\) To demonstrate the effect of using registry-dependent interlayer potentials, we have repeated our calculations of the heat conductivity of graphite slabs with the REBO intralayer potential augmented by LJ interlayer interactions\(^1^3\) (\( \varepsilon = 2.84 \, \text{meV}, \, \sigma = 3.4 \, \text{Å} \)). We find that the calculated heat conductivities obtained using the LJ interlayer potential are consistently higher than those obtained by our ILP and that the difference between them grows with the model system thickness. Notably, the heat conductivity obtained using the LJ potential for a graphitic slab of thickness \( \sim 35.4 \, \text{nm} \) is \( 1.54 \, \text{W/m·K} \), overestimating the experimental value by more than a factor of 2. However, it should be noted that the absolute value of the thermal conductivity might be quite sensitive to the simulation protocol used\(^4^4\) (see Section 4 of the Supporting Information), thus close attention should be paid when calculating it for nanoscale structures from MD simulations (see details in Section 2 of the Supporting Information).

The agreement between our ILP calculations of the thermal conductivity and phonon spectrum of nanoscale graphitic stacks (see Section 3 of the Supporting Information) with the corresponding experimental data, therefore, demonstrates the reliability of our predictions for the strong interfacial misfit angle dependence of cross-layer thermal conductivity in graphite and h-BN. The observed sharp conductivity decrease of twisted graphitic interfaces at misfit angles \( < 5^\circ \) opens the way to control the thermal evacuation rate and thermal isolation of active layers in graphene-based electronic and mechanical devices. The revealed underlying mechanism suggests that design rules can be obtained by carefully tailoring the phonon–phonon couplings across the twisted interface. While the misfit angle dependence of h-BN is found to be weaker than that of graphite, the overall thermal conductivity of the former is found to be higher. This may be utilized to achieve higher conductivity and controllability in twisted heterogeneous junctions of layered materials.

Finally, we note that quantum effects\(^4^5,4^6\) on thermal transport properties are not considered within our classical MD simulations. However, it should be noted that the contribution of such effects to the calculated thermal conductivity was found to be important only below the Debye temperature.\(^5^7,5^8\) For instance, two recent studies found that the quantum corrected in-plane thermal conductivity of graphene nanoribbons is close to the value obtained by classical MD simulations above the Debye temperature of \( 322 \, \text{K} \).\(^9,5^0\) In the case of cross-plane thermal conductivity, the relevant Debye temperature is \( 180.5 \, \text{K} \), \(^9\) well below the temperatures used in our simulations. Therefore, we expect quantum corrections to have a minor effect on the quantitative nature of our results and a negligible effect on the qualitative conclusions.

## ASSOCIATED CONTENT

### Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acs.nanolett.0c02983.

Methodology; convergence tests; comparison of the phonon spectrum and density of states calculated using the ILP and the Lennard-Jones potential; thermal conductivity of twisted bilayer graphene; theory for calculating the phonon coupling of twisted bilayer graphene; temperature dependence of the cross-plane thermal conductivity, and derivation of Fermi’s golden rule (PDF)

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The authors declare no competing financial interest.

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