Research Article

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Preparation of POSS-triol/wollastonite composite particles by Liquid phase mechanochemical method and its application in UV curable coatings

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Abstract: POSS-coated wollastonite composite particles were prepared by the liquid phase mechano-chemical grinding of wollastonite and POSS powder together in the high pressure homogenizer [1–4] for the first time. And then we prepare UV curable coatings of vinyl trimethoxy silane(VTMS)/butylacrylate(BA) with different content of composite particles [5]. Nuclear magnetic resonance spectroscopy, scanning electron microscopy and infrared spectra were used to investigate the microstructures and morphologies of the composite. The properties of the coatings are tested by FTIR, SEM, water contact angles and so on. The results indicate that the POSS was successfully loaded on the surface of silica fume to prepare composite particles and when the addition of the composite particles is 12%, the water contact angle of the UV curable coating reaches $151.96^\circ$, and the mechanical properties of the coating are also qualified.

Keywords: Wollastonite; composite particles; superhydrophobic; UV coating

1 Introduction

In recent years, the super-hydrophobic material has attracted much interest. Because it has the unique properties like self-cleaning, super-hydrophobic and other surface properties, and it has potential application value in the direction of construction, navigation, automobile and daily necessities [6–8]. The various methods to prepare super-hydrophobic surfaces has become a hot spot. And how to apply the super-hydrophobic surfaces in coatings, especially UV curable coatings, has become the difficulties in the field of coatings.

Many studies have shown that wollastonite [9–11], which has silica properties like mechanical properties on the surface [12, 13], is prepared by an orderly combination of silica particles and wollastonite [14], which can lead to the roughness of the wollastonite particles, eliminate the angle, improve the bonding strength of wollastonite to the matrix, and improve the application performance of wollastonite. However, the dispersivity of the silica / wollastonite composite particles prepared by the traditional solid-phase mechanochemical method [15] is poor and its performance is limited and unstable. Because of the dry system, the nuclear particles and the shell particles are combined only by the intermolecular force like the Van der Waals’ force and the electrostatic force [16, 17]. Under the condition of liquid medium (mainly water), the liquid phase mechanochemical method is a new method of preparing the coated composite particle material by activating the solid particles by mechanical grinding and finally triggering the interfacial reaction of the particles. This method can solve the problems existing in the solid-phase mechanochemical method [18, 19].

In high pressure homogenizer, the high pressure reciprocating pump is power transmission and the material conveying mechanism transfers material to the working valve part. In the process of passing through the working valve, the liquid material or solid particles with liquid as the carrier are refined under a strong shear, impact and hole action (Figure 1) [20, 21]. The effect of high pressure homogenizer on material is also a liquid mechanochemical method [22, 23]. It is rarely reported that the preparation of composite particles by high pressure homogenization mechanism. High pressure homogenizer can make the particle size fine and exposing more hydroxyl groups on the fracture surface [24], leading the hydroxyl association

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and the binding degree between the core and shell particles increased. This is a new method to prepare composite particles.

![Figure 1: Working principle of high pressure homogenizer](image)

UV curable coatings have the advantages that many traditional coatings didn’t have [25], such as high efficiency, low consumption, green pollution and so on. The UV curable coatings have achieved rapid development and attracted the attention of scientists [26, 27]. The preparation of organosilicon materials by light curing have both excellent properties of organosilicone materials [28, 29] and the characteristics of high efficiency and energy saving of light curing technology. Moreover, the organic / inorganic two phase compatibility is good, and the mechanical properties of the materials are excellent, and it has a broad application prospect [30]. However, the focus of the present study is to mix nano silica after surface modification into the light solidified organosilicon system, in order to improve the hardness, strength and wear resistance of the coatings [31, 32], and few studies have been made on the preparation of superhydrophobic coatings by UV curing. And the use of wollastonite composite particles to prepare the superhydrophobic surface has not been reported.

In this paper, POSS-triol / wollastonite composite particles are prepared by liquid phase mechanochemical method of high pressure homogenizer, and hybrid particles are added to UV curing coatings in different proportions to prepare hybrid light curing coatings. The properties of the coatings are tested by FTIR, SEM, water contact angles and so on. The influence of particle size on the properties of coatings was studied. A superhydrophobic composite particle light curing hybrid coating with good mechanical properties was prepared.

## 2 Experimental

### 2.1 Materials

Vinyltrimethoxysilane (VTMS) and phenyltrimethoxysilane were obtained from Jingzhou Jianghan Fine Chemical Co., China. Wollastonite was purchased from Guangdong wuling wollastonite co., China. 1-Hydroxycyclohexyl phenyl ketone (photoinitiator 184) was purchased from Macklin's Reagent Company. The solvents such as tetrahydrofuran (THF), acetic acid glacial, methanol, butyl acrylate were of chemically pure grade, also obtained from commercial resources. And sodium hydroxide (NaOH) were of chemically pure grade, purchased from Fuchen(Tianjin) Reagent Co., China.

### 2.2 Preparation of heptameric phenyl silsesquioxane trisilanol (POSS-triol)

195 mL tetrahydrofuran, 3.0803 g (0.077 mol) sodium oxide, 4.064 g (0.2258 mol) of distilled water and 35.258 g (0.1781 mol) phenyltrimethoxysilane were added into three flasks in turn, and then refluxed and heated for 5 hours after mixing. Then the reaction was dropped to the room temperature to continue to react to 15h. The obtained suspension was poured into the suction funnel for filtration, and the filter cake was dissolved in 115 ml methanol. After dissolved completely, then the solution neutralized by adding 115ml glacial acetic acid (3mol/L). The filtrate was removed and the filter cake was washed with deionized water for 3 times. The obtained white solid was dried in a vacuum oven for 24h, and the target product polysiloxane was obtained (Figure 2).

![Figure 2: Synthesis of POSS-triol](image)
2.3 Preparation of POSS-triol/wollastonite composite particles

The preparation process of composite particles is shown in Figure 3. After weighing wollastonite, polyesquisiloxane and water according to certain quality, they are put into plastic bottles and stirred for half an hour under magnetic stirring to prepare milky white suspension with slurry concentration of 1%. After mixing and under the liquid phase mechanochemical action of high pressure homogenizer, the turbid liquid of POSS-triol/wollastonite composite particles after treatment is obtained by adjusting the pressure of high pressure homogenizer and the number of homogenization. The filter cake after suspension filtration was dried in vacuum oven for 24h, and POSS-triol/wollastonite composite particles were obtained. The specific reaction process is as follows:

2.4 Preparation of UV curable coatings doped with POSS-triol/wollastonite composite particles

The postoptimality composite particles(homogenization pressure:12 MPa, homogenization:4 times, slurry concentration:1%, POSS content:40%). vinyl trimethoxy silane, butyl acrylate and 1-hydroxycyclohexyl benzophenone are proportioning in a certain proportion, and then it is stirred by magnetic stirring. After mixing, the hybrid solution is obtained. It is coated on the clean slide glass by roll coating and put into the UV curing box (100mw/cm^2), and it is irradiated for a certain time at a distance of 10cm from the UV lamp. Under the combined action of ultraviolet radiation and ultraviolet photoinitiator, the double bond on vinyl trimethoxy silane and the double bond on butyl acrylate were polymerized by free radical polymerization, solidified into a film, and after drying at room temperature for 24h, the composite particle hybrid superhydrophobic coating was obtained.
2.5 Characterizations

2.5.1 Fourier transform infrared spectroscopy (FTIR)

The FTIR measurements were conducted on a VERTEX 70/70v Fourier transform research spectrometer at room temperature (25°C). The sample films of UV curable coatings were prepared by dropping on the KBr tablet. The samples of POSS-triol/wollastonite composite particles were mixed with the powder of KBr and then pressed into the small flakes.

2.5.2 Nuclear magnetic resonance spectroscopy (NMR)

The $^1$H $^{13}$C and $^{29}$Si NMR measurements were carried out on a Bruker Avance III 400Hz NMR spectrometer. The samples were dissolved with deuterated chloroform and the solutions were measured with tetramethylsilane (TMS) as the internal reference.

2.5.3 Thermogravimetric analysis (TGA)

An America TA Q5000IR thermal gravimetric analyzer (TGA- Q5000IR) was used to investigate the thermal stability of the hybrids. The samples (about 10 mg) were heated under nitrogen atmosphere from ambient temperature to 800°C at the heating rate of 10°C/min. The temperature of the extrapolated onset was taken as the thermal degradation temperature.

2.5.4 X-ray diffraction (XRD)

The XRD analyses were conducted on a PANalytical X’Pert X-ray powder diffractometer (XRD, Panalytical Corporation, Holand) operated with Cu Ka radiation at 30 kV and 10 mA and with a scanning speed of 2 (2θ)/min.

2.5.5 Laser Particle Size Analyzer

The particle size of the composite particles was tested in a Beckman Coulter laser particle size analyzer. The composite particle aqueous solution was prepared at a concentration of 2% and dispersed evenly through the ultrasonic cleaning machine.

2.5.6 Scanning electron microscope

The microstructure and morphologies were investigated by scanning electron microscope (SEM, NOVA 430, FEI, Holand).

2.5.7 Contact angle measurements

The flat free surfaces of the UV curable coatings were used for the measurement of contact angle. The static contact angle measurements with the probe liquids (i.e., ultra-pure water) were carried out on a German KRUSS, DSA30 Research Contact Angle Measuring Instrument at room temperature (drop volume is 5µL). The samples were dried at 60°C in a vacuum oven for 24 h prior to measurement.

2.5.8 High pressure homogenizer

The composite particles were prepared by high-pressure homogenizer (ATS Engineering Limited AH-500). The optimum parameters of the preparation process were homogenization pressure:12 MPa, homogenization:4 times, slurry concentration:1%, POSS content:40%.

2.5.9 Hardness test

According to GB/6739-1996: Determination of film hardness by pencil test, the coating is coated on the iron, the size is 50mm*120mm* (0.2~0.3) mm, the test plate is placed on the horizontal table, the coating is fixed upwards, and the handheld pencil is about 45 angles. When the pencil is not broken, push pressure on the film surface, push about 1cm at a uniform speed of about 1cm/s ahead of the tester, scratch on the surface of the film, and repeat five repeats to the pencil of the same hardness mark. In the five scratch test, if there are two or more than two items that the film is not scratched, replace the same pencil hardness mark with the same test. Select the pencil that has been scratched two or two times, and record the hardness number of the pencil after the pencil hardness label number.

2.5.10 Adhesion determination

According to the national standard GB/T9286-1988: Paints varnishes-Crosscut test, the coating on the base material (glass) is made in a lattice, and the sample is 25mm*25mm, the number of delimit is 25*25, and the length of each lat-
tice is 1mm. Manual cutting is used for drawing, uniform force, smooth cutting speed and no chatter. After cutting, a soft hair brush is used along the two diagonal direction of the lattice and gently reciprocating several times. (the angle of the brush action is 45 degrees to the surface of the coating, and the force keeps consistent). The adhesion of the coating is characterized by observing the number of the remaining film squares remaining on the surface of the leather. The 0 class adhesion force is the best, and the 5 class adhesion force is the worst. 0, 1, 2 three grade can meet the general purpose.

3 Results and discussion

3.1 Characterization of heptameric phenyl silsesquioxane trisilanol(POSS-triol)

3.1.1 FTIR spectra of heptameric phenyl silsesquioxane trisilanol(POSS-triol)

Shown in Figure 4 are the FTIR spectra of heptameric phenyl silsesquioxane trisilanol(POSS-triol). On the infrared spectrum, it shows that the 3426 cm$^{-1}$ is the characteristic absorption peak of telescopic vibration of O-H, and the 1431 cm$^{-1}$ is the characteristic absorption peak of the flexural vibration of O-H, which indicates that the synthetic POSS-triol has a large number of hydroxyl groups; The 3062 cm$^{-1}$ is a telescopic vibration absorption peak of Ar-H, and the 1596 cm$^{-1}$ is the characteristic absorption peak of the benzenering, the 737 and 696 cm$^{-1}$ is the characteristic peak of mono substituted benzene, indicating that POSS-triol has a single substituted phenyl ring on it; The asymmetric stretching vibration peak at the width of 1069-1137 cm$^{-1}$ is Si-O-Si, indicating that the structure of Si-O-Si in the structure of POSS-triol and the 911.29 cm$^{-1}$ is the bending vibration absorption peak of Si-OH. It shows that the infrared spectra of the compounds are basically consistent with the structural peaks of POSS-triol [33].

3.1.2 NMR spectra of heptameric phenyl silsesquioxane trisilanol(POSS-triol)

Shown in Figure 5 are the $^1$H NMR spectrogram of heptameric phenyl silsesquioxane trisilanol(POSS-triol). The three peaks are corresponding to three different chemical environments of H on POSS-triol. $^1$H NMR(ppm,CDCl$_3$): 3.75(s,3.0H,-OH).5.30(dd,7.0H, para- Ar-H).7.26(m,28.0H, ortho- Ar-H, meta- Ar-H).

Shown in Figure 6 are the $^{13}$C NMR spectrogram of heptameric phenyl silsesquioxane trisilanol(POSS-triol) [34]. The four peaks are corresponding to four different chemical environments of C on POSS-triol. $^{13}$C NMR(ppm,CDCl$_3$): 127.70(dd,14.0C, ortho- C). 128.80(dd,7.0C, Si- C). 130.50(s,7.0C, para- C). 134.10(s,14.0C, meta- C).

Shown in Figure 7 are the $^{29}$Si NMR spectrogram of heptameric phenyl silsesquioxane trisilanol(POSS-triol). The three peaks are corresponding to three different chemical environments of Si on POSS-triol. $^{29}$Si NMR(ppm,CDCl$_3$): −76.88(s,1.0Si).−77.34(s,3.0Si).−78.20(s,3.0Si).

![Figure 4: FTIR spectra of heptameric phenyl silsesquioxane trisilanol(POSS-triol)](image)

![Figure 5: $^1$H NMR spectrum of heptameric phenyl silsesquioxane trisilanol(POSS-triol)](image)
3.2 Characterization of POSS-triol/wollastonite composite particles

3.2.1 Laser Particle Size Analysis of wollastonite

The comparison of wollastonite particle size before and after the action of high pressure homogenizer is shown on the Figure 8. From the comparison of the two diagrams, it can be seen that the average particle size of wollastonite decreased from 15.172 µm to 10.097 µm by the impact and fragmentation of the homogenizer, so the granularity of wollastonite decreased to a certain extent, indicating that the high pressure homogenizer has a certain dispersing and crushing effect on the wollastonite, thus making more hydroxyl groups on the broken surface. It can promote the effect of hydroxyl between wollastonite and POSS-triol, and improve its binding degree.

3.2.2 X-ray diffraction of wollastonite

Figure 9 is the XRD diagram of wollastonite and its composite particles. The XRD diagram of POSS-triol can be seen in Figure 9a), which shows the wide diffuse peak of the typical nanoscale sample, indicating that the prepared POSS-triol is a nanoscale substance. Figure 9b): the peaks of wollastonite on XRD diagram are basically matched with those wollastonite should have, and there are no other hetero peaks, so the purity of wollastonite is relatively high. Figure 8c): the composite particle XRD diagram, there are
both the broad diffuse peaks of the typical nanoscale samples and the sharp diffraction peaks of wollastonite, indicating that the composite particles contain both POSS-triol and wollastonite, and the wollastonite in the composite particles has good crystal integrity. After combination, only diffraction peaks of the wollastonite and POSS-triol appear in the XRD pattern of composite pigments and no new phase occurred, which means that the composite still kept its original phase composition. These results indicate that the reaction between wollastonite and POSS-triol only occurs on the interfaces.

3.2.3 FTIR spectra of POSS-triol/wollastonite composite particles

Figure 10 is the FTIR spectrum of POSS-triol/wollastonite composite particles increases with the content of POSS-triol (POSS-triol:wollastonite). The absorption peak at 3400 cm\(^{-1}\) represents the stretching vibration peak of O-H, which represents hydroxyl on the surface of hydroxyl and wollastonite on POSS-triol. It can be seen that the absorption peak of the position of 3400 cm\(^{-1}\) is strong in the FTIR spectrum of the composite particles. And with the increase of POSS-triol, the absorption peak of the composite particles is widening. It shows that the combination of POSS-triol and wollastonite is a strong connective between the hydroxyl groups on the surface of the two particles. For the enhancement of cooperation, it results in widening of the absorption peaks. It is inferred that this is done by con-
condensation of POSS-triol and wollastonite through the surface hydroxyl groups of each other, and the combination of them has a chemical binding nature [35].

3.2.4 The Morphology of POSS-triol/Wollastonite Composite

Figure 11 is the SEM images of the wollastonite before and after the compound. Figure 11b): the needle like wollastonite has a smooth surface and no more other particles, but Figure 11d): the surface of the needle like wollastonite in the composite particles has been attached to a large number of POSS-triol particles, making the surface of needle like wollastonite rough, which indicates that POSS-triol has been successfully loaded on the wollastonite, eliminated the angle of the wollastonite and made the surface of the wollastonite rough, and finally, wollastonite is changed from hydrophilic to hydrophobic.
Preparation of POSS-triol/wollastonite composite particles and its application

3.3 Testing of UV curable coatings doped with POSS-triol/wollastonite composite particles

3.3.1 Preparation and film formation of UV curable coatings doped with POSS-triol/wollastonite composite particles

Table 1 is the film formation of different proportions of UV curable acrylate/vinyl trimethoxy silane coatings with vinyl trimethoxy silane (VTMS) and butyl acrylate (BA). It can be seen that when VTMS:BA is 2:1, the coating is wrinkled slightly; when VTMS:BA is 1:1, the coating is wrinkled; when VTMS:BA is 4:1, the coating produces a slight crack; when VTMS:BA is 5:1, the coating produces cracks and separations; and when VTMS:BA is 3:1, the coating is smooth. Therefore, we chose the system when VTMS:BA is 3:1 as a hybrid modification system with composite particles.

3.3.2 Effect of composite particles content on thermal stability of UV curable Hybrid Coatings

Figure 12 is the thermogravimetric curve of VTMS/BA-m-composite particle hybrid coating containing different mass fraction of composite particles. The weightlessness step, which is slightly above 150°C, is caused by the weight loss of the molecular short chain in the hybrid coating. In the high temperature region, the weightlessness step of 400-550°C is the molecular long chain breaking in the hybrid coating. It can be seen from the diagram that the initial decomposition temperature of VTMS/BA-m-composite particle hybrid coatings containing 0%, 3%, 6%, 9%, 12% and 15% particles in the low temperature region is 152.9°C,
Figure 14: The SEM images of UV curable Hybrid Coatings. a) 0%; b) 6%; c) 12%

137.5°C, 126.7°C, 125.4°C, 118.8°C, and 110.5°C, and the overall presentation shows an increasing trend. The decomposition temperature in the high temperature region is 480.7°C, 408.4°C, 480.6°C, 489.2°C, 492.5°C, 502.6°C, respectively. The decomposition temperature is reduced when the 3% composite particles are added, because the added composite particles are filled in the coating to make the molecular chain of the coating be stretched and the chain [36] is easily broken at high temperature, so the decomposition temperature will decrease. When the amount of addition reaches 6%, the composite particles are the main body of the coating. The thermal stability of the coating is increased by the high temperature resistant composite particles, and the decomposition temperature is increased. The final residues in the system were 7.17%, 8.70%, 15.73%, 18.82%, 22.96% and 31.62% respectively, which basically accorded with the increasing trend of the composite particles.
3.3.3 FTIR spectra of UV curable Hybrid Coatings

In order to study the reaction mechanism of VTMS/BA-m-composite particle hybrid superhydrophobic coating, the infrared spectra of VTMS/BA-m-composite hybrid superhydrophobic coating before and after curing were compared (Figure 13). Figure a) is an infrared spectrum of a hybrid superhydrophobic coating containing 12% VTMS/BA-m-composite particles cured at different times, and Figure b) is a partial enlarged view of Figure a).

In Figure a), 2962 cm\(^{-1}\) is a stretching vibration peak of methyl C-H, 1619-1635 cm\(^{-1}\) is a stretching vibration absorption peak of C=C, and 1056 cm\(^{-1}\) is a stretching vibration absorption peak of Si-O-Si; As can be seen from the partial enlarged view of Figure b), before the curing, there is obvious stretching vibration absorption peak of carbon-carbon double bond c=c at 1619-1635 cm\(^{-1}\), which is caused by C=C on vinyltrimethoxysilane and butyl acrylate. After curing, the peak disappeared, indicating that the polymerization occurred in the system under the initiation of ultraviolet light. Ultraviolet light induced a radical polymerization reaction in the system, and the double bond disappeared after polymerization.

3.3.4 The Morphology of UV curable Hybrid Coatings

In order to observe the surface morphology of UV curable superhydrophobic hybrid coatings prepared, the hybrid coatings with different mass fraction of composite particles were analyzed by scanning electron microscope. It can be seen that the surface morphology of the coatings has changed greatly after the doping of the composite particles, and there is no obvious composite structure on the coating with no composite particles (Figure 14a)). After adding 6% composite particles (Figure 14b)), the surface of the coating formed a number of protruding structures. The composite particles formed a micro nano structure on the surface. When the amount of addition reached 12%
Figure 17: The contact angle of UV curable hybrid coatings with different composite particles content: a) 0%; b) 3%; c) 6%; d) 9%; e) 12%; f) 15%

Figure 18: The SA photos of 10µl water-drop on the hybrid coating with 12wt% composite particles

3.3.5 Analysis of water contact angle of UV curable Hybrid Coatings

Figure 16 is the influence of composite particles with different mass fractions (0%, 3%, 6%, 9%, 12%, 15%) on the contact angle of UV curable hybrid coatings. Figure 17 is the different contact angle of UV curable hybrid coatings with different composite particles content. Figure 18 is the SA photos of 10µl water-drop on the hybrid coating with 12wt% composite particles. It can be seen from Figure 16 that the influence of the content of the composite particles on the contact angle of the hybrid coating can be divided into two stages. In the first stage, with the mass fraction of the composite particles in the hybrid system changing from 0% to 12%, the contact angle of the hybrid coating has been gradually increased to 151.96° when the contact angle of the hybrid coating has never been added to the composite particles. This is due to the polymerization of vinyl trimethoxy silane and butyl acrylate when the UV curing is not added, and the addition of low surface energy active monomer vinyl trimethoxy can make the coating with a certain hydrophobicity. When the composite particles with different mass fraction were added, the composite particles formed a micro nano structure that conformed to the Cassie model on the surface of the composite particles. This is due to the polymerization of vinyl trimethoxy silane and butyl acrylate when the UV curing is not added, and the addition of low surface energy active monomer vinyl trimethoxy can make the coating with a certain hydrophobicity. When the composite particles with different mass fraction were added, the composite particles formed a micro nano structure that conformed to the Cassie model on the surface of the coating, thus increasing the contact angle of the coating water. When the addition amount reached 12%, the water contact angle reached 151.06°, the rolling angle reached 8.56°. And the water contact angle of the coating was over 150°, the rolling angle was below 10°, so the coating changed from hydrophobic-
ity to superhydrophobicity. In the second stage, the contact angle of the coated water drops slightly after the addition of more than 12%, which is due to the excessive accumulation of composite particles on the coating surface and the saturation of the surface structure, so that the water contact angle of the coating remains to a certain level or even a little drop. On the whole, when the mass fraction of the composite particles is 12%, the hybrid coating has a large water contact angle, that is, super hydrophobic.

3.3.6 Analysis of mechanical properties of UV curable Hybrid Coatings

Table 2 is the effect of composite particles with different mass fraction on the hardness and adhesion of UV curing coatings. The experimental results show that the addition of the composite particles can improve the pencil hardness of the UV curable Hybrid Coatings, because the composite particles have a certain rigidity and hardness, and they are added to the coating to support the coating and give the coating a good hardness. When the addition amount reached 6%, the adhesion of the composite particles had no significant effect on the adhesion of the coating, but the adhesion of the film was weakened when the amount of addition was over 6%. This is because the addition of the composite particles to the coating destroys the order of the coating, and the adhesion of the coating to the coating is poor, so it is easily destroyed and the adhesion is reduced.

(3) By studying the effect of different mass fraction of composite particles on the water contact angle of the coating, it is found that when the mass fraction of the composite particles rises from 0% to 12%, the contact angle of the hybrid coating increases, the highest can reach $151.96^\circ$, and the water contact angle is little changed after more than 12%. When the addition of composite particles reached 12%, the mechanical properties of the coating were relatively high and the adhesion decreased little.

(4) The raw materials used in wollastonite are large and easy to obtain. The coating has certain prospects in industrial production.

4 Conclusions

(1) In general, through characterization and performance testing, a new method of preparation of composite particles was studied. A hydrophobic composite particle was prepared by the mechanochemical effect of high pressure homogenizer on wollastonite and POSS-triol.

(2) The optimized composite particles were added to the UV curable coatings with VTMS/BA, and the super hydrophobic UV curable coatings were prepared.

(3) By studying the effect of different mass fraction of composite particles on the water contact angle of the coating, it is found that when the mass fraction of the composite particles rises from 0% to 12%, the contact angle of the hybrid coating increases, the highest can reach $151.96^\circ$, and the water contact angle is little changed after more than 12%. When the addition of composite particles reached 12%, the mechanical properties of the coating were relatively high and the adhesion decreased little.

Conflict of Interests: The authors declares that there is no conflict of interest regarding the publication of this paper.

The data availability statement: The data used to support the findings of this study are available from the corresponding author upon request.

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