VOLUME MEASUREMENT OF SAND CARRIER USING UAV-BASED MAPPING

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ABSTRACT:

To improve the operation efficiency and reduce the risks associated with exposing surveyors to danger during on-site operations, this paper presents a volume measurement approach of the sand carrier using unmanned aerial vehicle (UAV) imagery. Instead of the efficiency and accuracy of sand volume measurement play a key role in project management (Lu, 2011; Fawzy, 2015). At present, volume measurement of sand carrier is mainly manual field measurement, which is technically complex and time-consuming because of the heavy workload, low efficiency, and empirical requirements. Also, this method is difficult to guarantee the accuracy of volume measurement.

Generally, based on the measuring instruments used, the traditional methods of volume measurement include total station measuring method and real-time kinematic global positioning system (RTK GPS) measuring method, the finely detailed surfaces of the sand carriers are reconstructed from dense point clouds derived by UAV-based mapping. Then, the volume of sand is calculated by the differential method, which multiplies the height difference between the UAV-derived 3D surfaces of the vessel and sand by the resolution of these surfaces. A total of 10 sand carriers are selected to test and evaluate the performance of the proposed approach, the absolute values of relative deviation between the volume obtained by UAV-based and the reference volume are approximately equal to 2%, which can be considered acceptable and satisfy the need of volume measurement of sand carriers. Compared with the manual field measurement and the laser scanning-based method, the proposed approach performs better in the accuracy of volume measurement or the reliability under the circumstance of a moving carrier. The overall results suggest that UAV-mapping can be used as an effective alternative to the commonly used method for volume measurement of the sand carrier.

1. INTRODUCTION

Sand is an important raw material for many engineering projects and usually transported to the construction site by ship, the efficiency and accuracy of sand volume measurement play a key role in project management (Lu, 2011; Fawzy, 2015). At present, volume measurement of sand carrier is mainly manual field measurement, which is technically complex and time-consuming because of the heavy workload, low efficiency, and empirical requirements. Also, this method is difficult to guarantee the accuracy of volume measurement.

Generally, based on the measuring instruments used, the traditional methods of volume measurement include total station measuring method and real-time kinematic global positioning system (RTK GPS) measuring method (Hamzah, 2011). Due to the limitations of viewpoint occlusion and the range of the sand carrier, the total station visibility requirements are difficult to meet. Besides, the sand carrier is difficult to keep stationary because it may often be disturbed by wind and water flow, in this case, the positions on the sand carrier may change greatly with time, which makes it difficult to be effective for time-consuming methods such as total station-based and RTK GPS-based methods. Besides, the common problem of the aforementioned measurements using traditional instruments is that they are not able to obtain sufficient three-dimensional (3D) object points to characterize the surface of the sand (Yilmaz, 2010; Bajtala, 2011). In recent years, 3D laser scanning and unmanned aerial vehicle (UAV)-based mapping have emerged as a promising techniques due to the ability to efficiently acquire a large amount of 3D point clouds and is widely used for volume measurement (Starek, 2013; Fan, 2015; Raeva, 2016; Xu, 2019). Especially, the backpack-type laser scanner with portability and flexibility is suitable to quickly measure the volume. However, the high-precision laser scanning instruments are costly and are not easily operated by surveyors in the narrow passages on the deck of the carrier. Even worse, the laser scanning may not be used to reconstruct the 3D surface of sand when the carrier is moving or shaking. Therefore, the laser scanning-based methods are not suitable for the volume measurement of sand carriers and are not popularized in this field. Recently, due to the ability to quickly obtain high-resolution remote sensing images and reconstruct high-precision 3D geometry structure, another high-tech UAV mapping technology has also been developed rapidly and broadly applied to the applications of agriculture, forestry, archaeology, resource investigation, environmental monitoring, 3D city modeling (Shahbazi, 2015; Mancini, 2017; Sluijs, 2018). In contrast to the laser scanning operation, UAV-mapping is low-cost and may offer the opportunity to measure the volume of sand under the circumstance of a moving or shaking carrier. That is, UAV-mapping can provide a new way to suit this case of volume measurement of the sand carrier.

The aim of this paper is to assess the capabilities of UAV-based mapping for measuring the volume of sand carrier. A workflow for volume measurement based on low-cost UAV...
mapping including data acquisition and processing is proposed. This involves aerial triangulation with several ground control points and dense matching with semi-global algorithm (SGM), then high-precision and dense 3D points on the surface of sand can be derived from UAV overlapping images. Overall results confirm that UAV-based mapping can significantly improve the accuracy and efficiency of volume measurement.

2. UAV MAPPING BASED SURFACE RECONSTRUCTION

UAV mapping is highly integrated with the UAV platform, sensors, remote control, communication, navigation and positioning, and image processing techniques. The overlapping images can be acquired by the airborne camera and processed by photogrammetric software, thus the geospatial information of the ground objects can be derived. In this study, a low-cost small quadcopter, namely, DJI Phantom 4 PRO, which is used to capture the overlapping images, as shown in Figure 1. This UAV has a simple structure, flexible in operation, less preparation time, and low requirements for the landing site. It can take off and land at any time according to the mission needs and is not limited by data acquisition during the revisit period. Moreover, the UAV can directly acquire overlapping images of dangerous areas and areas beyond the reach of surveyors.

Similar to traditional aerial photogrammetry, UAV mapping also requires route planning according to the requirements of the mission, and then the overlapping images are acquired through the waypoints predefined. However, route planning is generally used to obtain images of stationary ground objects and not applicable for data acquisition under the circumstance of a moving or shaking object. Because of the small operating range, in this study, we manually operated the UAV to capture the overlapping images. As a consequence of this, the overlapping range between images is irregular. In addition, unlike the traditional aerial photogrammetry, initial exterior orientation parameters obtained from the low-cost airborne GPS and inertial measurement unit (GPS/IMU) are not available to assist aerial triangulation. Therefore, Structure-from-motion (SfM) is used to recover the 3D surface of the sand carrier due to the ability to allow 3D reconstruction from the overlapping but otherwise unordered images without a prerequisite of accurate GPS/INS data (He, 2019). To minimize the systematic errors of the airborne consumer-grade camera, which is pre-calibrated. The interior orientation parameters are then optimized through self-calibrating adjustment.

To satisfy the requirements of the volume measurement of the sand carrier, the aerial photography is conducted to acquire the overlapping images of the sand carrier before (no load) and after loading (full load). Note that the surface of the sand carrier only needs to be reconstructed once. The 3D reconstruction is achieved by a serial photogrammetric process, e.g., feature extraction and matching, SfM, dense matching. Then, the volume of sand is calculated based on the differential z-value between the two sets of point clouds with no load and full load. Specifically, the technical process is shown in Figure 2, which mainly includes ground control points (GCPs) placement, overlapping images acquisition, lens distortion correction, dense point clouds generation, and volume calculation etc.

![Figure 1. UAV data acquisition.](image1)

The volume measurement of this study still requires GCPs to georeference for absolute orientation. The difference with the common GCPs acquisition is that the GCPs are measured once on a static carrier and then used for absolute orientation regardless of whether the carrier is moving or not. In other words, this study ignores the background information in the overlapping images and only treats the carrier as a relatively stationary object. The GCPs are marked on the surface of the carrier, as illustrated in Figure 3.

![Figure 2. A technical workflow of UAV-mapping volume measurement of the sand carrier.](image2)

![Figure 3. GCPs placements marked by white crosses.](image3)
in the dense matching is slightly different from the SGM to ensure the matching reliability of repetitive or weak textures (shown in Figure 4) on the surface of the sand.

Based on the SGM algorithm (Hirschmuller, 2005), let \( L_r \) denote a cost path that traverses in the direction \( r \). The minimum cost path \( L_r(p_x,d) \) for the pixel \( p_x \) at disparity \( d \) can be defined recursively as

\[
L_r(p_x,d) = C(p_x,d) + \min \left( \begin{array}{l}
L_r(p_x-r,d), \\
L_r(p_x-r,d-1) + P_1, \\
L_r(p_x-r,d+1) + P_1, \\
\min_i L_r(p_x-r,i) + P_2, \\
dist(p_x-r,p_x)
\end{array} \right)
\]

where the pixel-wise matching cost \( C(p_x,d) \) can be calculated based on mutual information (MI) (Viola, 1995). \( \text{dist} \{ \} \) denotes an operation of gradient Euclidean distance and is enforced to establish a more robust similarity measure than the original cost function, the gradient calculation is similar to the operation used in the scale-invariant feature transform (SIFT) algorithm.

### 3. VOLUME CALCULATION

The dense point clouds obtained from UAV-mapping are split into a series of grids with a size of \( d \times d \) on the \( xoy \) coordinate plane, which is shown in Figure 5. The \( z \)-value of each grid is defined as an average value of 3D points within the grid. Then, the mathematical differential method is used to calculate the volume \( V \) of the sand carrier by multiplying the \( z \)-value difference between the sand and carrier surface models. And the differential calculation can be defined as

\[
V = \sum_{i=1}^{M} \sum_{j=1}^{N} (Z_{\text{sand}}^{z(i,j)} - Z_{\text{carrier}}^{z(i,j)}) \cdot d_{i,j}^2,
\]

where \( M \) and \( N \) are the rows and columns of the grids, respectively; \( Z_{\text{sand}}^z \) and \( Z_{\text{carrier}}^z \) are the \( z \)-values on the surface of sand and vessel, correspondingly.

### 4. EXPERIMENTS AND DISCUSSION

The experimental area is located in the Pearl River, where sand carriers frequently pass through. The UAV used for data acquisition is a consumer-grade UAV, i.e., DJI Phantom 4 PRO shown in Figure 6, with 20-megapixel RGB true color obtained from 1-inch complementary metal-oxide-semiconductor (CMOS) sensor. Besides, the DJI Phantom 4 PRO has an integrated remote control with a 5.5-inch 1080p display that allows the operator to view the images captured by the drone in real-time and adjust the flight status through the high-resolution image transmission system. Other related parameters of the DJI Phantom 4 PRO are given in Table 1 (DJI, 2016), thus the UAV image acquisitions are performed under the requirements of the parameters. Because the width of the sand carrier is small, it can be photographed with a single strip, and the overlaps are set to 80%. The flight height is adjusted to ensure that the width of the carrier is no less than 60% of the image. Besides, the airborne camera is calibrated using the 2D chessboard pattern, four views are exhibited in Figure 7, and the initial camera parameters are given in Table 2.

![DJI Phantom 4 PRO](image-url)

**Figure 6.** DJI Phantom 4 PRO.

| Weight | Flight time | Flight altitude | Withstand wind |
|--------|-------------|-----------------|----------------|
| 1.388 kg | \( \leq 30 \) min | \( \leq 6000 \) m | \( \leq 10 \) m/s |

**Table 1.** Several parameters of DJI Phantom 4 PRO.
Figure 7. Four views of the 2D chessboard exhibited as examples.

| Focus $f_x$: | 3960.9648 |
| Focus $f_y$: | 3959.1806 |
| Principal Point $x$: | 2977.5390 |

Principal Point $y$: 1946.4755
Radial Distortion $k_1$: -0.048182446509599686
Radial Distortion $k_2$: 0.040056683123111725
Tangential Distortion $p_1$: -0.003868975676596164
Tangential Distortion $p_2$: -0.001025215955451131

Table 2. Parameters of the airborne camera.

Following the aforementioned requirements, the DJI Phantom 4 PRO is operated to capture the carrier before and after loading the sand in the experimental area. A total of 10 carriers (half stationary carriers No. 1-5 and a half moving carriers No. 6-10 shown in Table 2) are photographed in the cases of no-load and full load. Figure 8 shows the dense point clouds and the depth maps of an example derived by the SfM and SGM algorithms, the visualization results show that the finely detailed surfaces of vessel and sand are reconstructed.

Table 3. Comparisons of volume calculation using manual field measurement (Manual), laser scanning based and UAV-based methods.
Table 3 shows the results of volume measurement using the proposed approach, which is also compared with other methods, i.e., manual field measurement and laser scanning based methods. The relative deviation $\sigma$ of volume measurement is defined as

$$\sigma = \frac{(V_{M/L/U} - V)}{V} \times 100\%,$$

in which $V$ denotes the reference volume, $V_{M/L/U}$ represents one of the volumes obtained by manual field measurement, laser scanning-based, and UAV-based methods.

Note that the reference volume is determined by the same sand with a regular shape such as trapezoid, which is shaped on land shown in Figure 11a. Then, the volume of sand is calculated by the mathematical formula of a trapezoid. Similar to the acquisition of the true value, the sand in the carrier is generally shaped into a trapezoid (shown in Figure 11b) in the manual field measurement, and then the measuring tape is used to measure the size of the trapezoid for volume calculation (Bajtala, 2012). For the backpack-type laser scanning-based method, a Velodyne LiDAR with HDL-32E LiDAR sensor shown in Figure 9 is used to obtain the point clouds of the surfaces of vessel and sand, as shown in Figure 11c.

As can be seen from Table 2, the volumes calculated by the manual measurement have a large deviation from the reference values, some of which are more than 10%. It indicates that the reliability of this manual method is poor due to the difficulty of quality control of trapezoid. In the first five results, the total deviation of the laser scanning-based method is similar to the UAV-based method obtained, and the absolute values of relative deviation are relatively small and approximately equal to 2%. In contrast, both of the laser scanning-based and UAV-based methods are significantly better than the manual measurement, the deviation can satisfy the requirements of sand carrier measurement (Raeva, 2016; Abbaszadeh, 2017). However, the moving carrier may cause laser sensor vibration and generate invalid data, e.g., No. 6-10.

Besides, the results obtained by the dense matching of the proposed cost function are compared with that of the original SGM cost function. The statistical results of 10 sand carriers are shown in Figure 10, it can be seen that the proposed cost function performs better in terms of smaller relative deviations. It should be noted here that we did not use GCPs to evaluate the accuracy of surface reconstruction, because the sand surface is unstable and soft, and the measuring instrument placed on the sand may cause deformation of the sand surface. Besides, on the one hand, the UAV-based method can effectively avoid the influence of site obstacles without the need of boarding, the whole operation process is simple, fast and safe, and the data is presented in the form of image, which is highly intuitive; on the other hand, the DJI Phantom 4 PRO is low-cost, and there is no need for multiple operators to cooperate, which also saves manpower and financial resources. Thus, results suggest that the UAV-based method can be used as an effective alternative to the manual field measurement for volume calculation of sand carrier.
5. CONCLUSIONS

This paper presents the data acquisition and processing of volume measurement of sand carriers based on UAV mapping. Briefly, a volume measurement is performed by the differential method with the height difference between the UAV-derived dense point clouds of vessel and sand. Compared with the manual field measurement and laser scanning-based method, the following conclusions are drawn:

(1) The volume measured by the manual field method is poor and unreliable, while the laser scanning-based and UAV-based methods can obtain results close to the reference volume. However, the laser scanning-based method maybe not available to measure the volume under the circumstance of a moving carrier.

(2) Based on the advantages of UAV aerial photography, data acquisition can be completed without the need of surveyors boarding a carrier, which improves the operation efficiency and reduces the risks associated with exposing surveyors to danger during on-site operations. Besides, the UAV instrument is low-cost and easily operated, which is conducive to popularize the application of UAV-based volume measurement.

(3) The high-precision dense point clouds derived from UAV-mapping can characterize the finely detailed surface of the vessel and sand. The deviation between the volume obtained by UAV-based and the reference volume is approximately equal to 2%, thus the UAV-based method can be used as an effective alternative to the manual field measurement for volume calculation of sand carrier.

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