Behavior of Reactive Powder Concrete Beams Exposed to Fire

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ARTICLE INFO

ABSTRACT

In this paper, the effect of direct fire flame and steel fiber ratio on some mechanical properties and behavior of the relationship between load and deflection of rectangular reinforced concrete beams under the influence of fire exposure was studied. Concrete specimens were exposed to fire at temperatures ranging from (25- 400 °C). Three temperature levels of (200, 300, 400 °C) where chosen for exposure duration of 2.0 hours. After conducting the test, it was found that increasing the proportion of steel fibers in percentages 0.5% to 1% and 1.5% decreases the mid-span deflection at service load by 33%, 50% and 37.5 and increases the ultimate load by 36.36%, 41.6% and 53% respectively. After the beams are exposed to fire, it was noticed that the maximum crack width increases with increasing fire temperature.

1. Introduction

Reactive Powder Concrete (RPC) One of the latest products of the new generation of concrete It has high cement content and low water content as well as fine sand and silica dust. The results showed that the resistance of RPC samples decreases when the high temperature increases. At 400 °C, the losses in compressive strength and split tensile strength were 77.78% and 85%, respectively. [1]. Studied the effect of elevated temperatures on performance of RCC beams. Results revealed robust performance up to 550°C. The drop in flexural strength & other parameters was noticeable but not alarming up to 750°C. Around 950°C, the RCC members lost their fidelity on all counts [3]. Investigated four hybrid-fiber reinforced RPC beams protected with fire insulation exposed to fire flame. They note that the failure of the reinforced RPC beams was due to a fracture in the longitudinal armature caused by direct exposure to fire after failure of the fire insulator on the RPC beam [4]. Studied the phenomenon of fragmentation of Ultra High-Performance Concrete (UHPC) beams when exposed to high temperatures. The results showed that the fragmentation phenomenon was affected by the loading level. Under the same loading conditions, the fragmentation of beams containing steel fibers was 4% less than that of beams with a content of 2% [5]. Several results (6, 7, 8, 9, and 10) showed a deterioration in the properties of concrete under exposure to high temperatures. The degree of deterioration was affected by the type of aggregate and concrete used.

2. Experimental program

2.1. Materials

2.1.1. Cement

Portland cement grade [CEM I 52.5N] was used. [11] The properties of the cement used

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DOI: 10.24237/djes.2021.14401
are in accordance with the Egyptian Standard Specifications E.S.S. 47561/2013.

2.1.2. Fine sand

Very fine sand used according to the Egyptian Specification (E.S.S 1109/2008 requirements) [12]. Its small maximum nominal size (0.6 mm). Its grading is shown in Table (1).

Table 1: Classification of sand used according to (E.S.S. 1109/2008)

| Sieve No. | No.30 | No.50 | No.100 | No.200 |
|-----------|-------|-------|--------|--------|
| passing % | 100   | 58    | 7      | 0.7    |

2.1.3 Silica fume

In this study, silica fume was used as a mineral mixture added to RPC concrete.

2.1.4 Steel fibers

To increase RPC ductility, a steel fiber hook end is used. The steel fibers were 50 mm in length and diameter 0.5mm density of 7800 kg/m$^3$, and maximum tensile strength of 1200 MPa.

2.1.5 Water

Pure water was used to mix and treat concrete.

2.1.6 Super-plasticizer

A commercial name (Sikament 163) was used. The properties of the admixture correspond to with ASTM C494-Type A and F [13].

2.2 Concrete mix

Concrete was mixed and stirred in a large capacity mixer 0.1m$^3$. The details of concrete compositions are shown in Table 2.

Table 2: Details of concrete mix.

| Mix | Cement kg / m$^3$ | Fine sand kg / m$^3$ | Silica fume % | Steel fiber % | W/C % | Super-plasticizer % |
|-----|-------------------|----------------------|---------------|---------------|------|--------------------|
| R0  | 800               | 1100                 | 20%           | 0%            | 20%  | 4%                 |
| R0.5| 800               | 1100                 | 20%           | 0.5%          | 20%  | 4%                 |
| R1  | 800               | 1100                 | 20%           | 1%            | 20%  | 4%                 |
| R1.5| 800               | 1100                 | 20%           | 1.5%          | 20%  | 4%                 |

2.3 Details of beams

Nominal dimensions of tested beams were (1700mm) in overall length, (200mm) in depth and 120 mm width as shown in Fig. (1). the beams in the bottom direction are reinforced with (3-Ø10mm). A 6 mm diameter stirrup was used every 100 mm to prevent shearing failure and this is for sixteen beams from group (G1 to G4), A 6 mm diameter stirrup was used every 100 mm for four beams at group G5 for the failure of the beams to shear. Also, steel bars (2-Ø8mm) were used in the longitudinal direction at the top of the section.
2.4 Test methods

The test was carried out in two stages: in the first stage of the test, each beam is positioned simply supported by a two-point load the beam was gradually loaded static load until reaching the service load worth 3.25 tons which was obtained by reference beam test the apparent extension between the two loading points is 500mm as shown in Figure (1). to measure the maximum deflection of the beam under load, a dial gage was placed in the mid span so that the head of dial gage touches the bottom face of the beam. The corresponding deviation was recorded for the service load, then the fire furnace was operated at the required temperature then the beam was exposed to fire from three sides, from the bottom and from both sides until the failure of the sample or reaching the maximum test time of two hours, as shown in Figure (2). A thermo cable and Digital temperature indicator was used to measure different temperatures. Two wires of different metals are connected together at the intersection, as shown in Figure (2). then the sample was left in the air for 24 hours, then the loading was completed until the sample failed the deviation corresponding to the maximum load was recorded.
3. Results and discussion

3.1 Crack patterns and mode of failure at room temperature

The reference beams such as R0 showed the typical mode of failure under flexural load. The cracks started in the tension zone within the middle third of the beam. The cracks were then propagated along the depth of the beam. It can be noticed for beams with steel fibers played a major role, by observing the mode of failure for RPC beams container with steel fibers and without fibers. The final failure occurred due to the formed two main inclined cracks and crushed of concrete under the point of loading as shown in Fig. (3).
3-2 Crack patterns and mode of failure at different temperature exposures

Based on the results of the tests, the first crack load and the corresponding deflection are shown, as well as the maximum load and the corresponding deflection, after operating the fire furnace and direct exposure to fire for two hours as shown in table 3. Having been exposed to fire before failure, it showed that cracks had started and spread along the beam. Concrete cracking is observed at different locations. Figures (4 to 7) shows the crack patterns and mode of failure at different temperature exposures.
Table 3: Results of the tests beams

| Group No. | Mix No | Temperature of fire flame (°C) | Cracking load (kN) | Ultimate load (kN) | Deflection at cracking load (mm) | Deflection at ultimate load (mm) |
|-----------|--------|--------------------------------|--------------------|--------------------|----------------------------------|---------------------------------|
| G1        | R0     | 25                             | 2.9                | 7.3                | 6                               | 32                             |
|           | R0.5   |                                | 3                  | 7.7                | 4.6                             | 27                             |
|           | R1     |                                | 3.2                | 8.85               | 4                               | 28                             |
|           | R1.5   |                                | 3.5                | 9                  | 4                               | 27                             |
| G2        | R0     | 200                            | 1.1                | 4.4                | 12                              | 37                             |
|           | R0.5   |                                | 1.6                | 4.81               | 10                              | 34                             |
|           | R1     |                                | 1.8                | 5.5                | 9                               | 30                             |
|           | R1.5   |                                | 1.92               | 6                  | 8                               | 27                             |
| G3        | R0     | 300                            | 0.9                | 3                  | 14                              | 44                             |
|           | R0.5   |                                | 1.1                | 3.5                | 11                              | 40                             |
|           | R1     |                                | 1.65               | 3.9                | 9                               | 36                             |
|           | R1.5   |                                | 1.86               | 4.25               | 7                               | 31                             |
| G4        | R0     | 400                            | 0.83               | 2                  | 16                              | 50                             |
|           | R0.5   |                                | 0.9                | 2.2                | 14                              | 46                             |
|           | R1     |                                | 1                  | 2.65               | 12                              | 44                             |
|           | R1.5   |                                | 1.1                | 3.06               | 10                              | 35                             |
| G5        | R1     |                                | 2                  | 6.65               | 4                               | 29                             |

Figure 4. Mode of failure of beam at group 2 (G2)
Figure 5. Mode of failure of beam at group 3 (G3)

Figure 6. Mode of failure of beam at group 4 (G4)
3.3 The load–deflection relationship of beam at room temperature

The load is tested against the deflection of the booster reference RPC beams tested under two-point loading until the failure as shown in Figure (8). Effect of increasing steel fiber content on load–deflection curve is very clear in Fig. (8), as the steel fibers ratio increases the curve becomes stiffer. The largest difference is between beam R0 (beam with zero steel fibers) and beams R1.5 (beams with high ratios of steel fibers). It is generally concluded that as steel fiber content increases the failure load increases too (using 1.5% steel fiber ratio increases failure load by 23.3%).

3.4 The load–deflection relationship of beam after different temperature exposures

The deviation at the end of the heating time is displayed for all beams in table (2). When the beams are exposed to fire in the second stage of the test, a significant increase in deflection can be observed resulting from decreasing the bending strength in the beam and thus increasing the deflection. This is shown in the Figures from 9 to 14.

3.5 Fire Resistance of reinforced RPC beams

Regarding the effect of temperature on the final load, Fig. (15 and 16) shows the decrease in the final load due to the increase in temperature.
Figure 8. Load-deflection of beam at Room Temperature

Figure 9. Load-deflection of beams at group 2 (G2)

Figure 10. Load-deflection of beams at group 3 (G3)
Figure 11. Load-deflection of beams at group 4 (G4)

Figure 12. Load-deflection of beams at group 5 (G5)

Figure 13. Effect of steel fibers with different volume fractions on mid span Deflection-temperature curve of RPC beams from group (1-4)
Figure 14. Effect of steel fibers with different volume fractions on mid span Deflection-temperature curve of RPC beams at group 5

Figure 15. Effect of elevated temperature on ultimate load of RPC beams from group (1-4)

Figure 16. Effect of elevated temperature on ultimate load of RPC beams at group (5)
4. Conclusions

According to the experiments presented in this research, the following can be concluded:

1- Reactive powder concrete is the product of a new generation of high-performance concrete.
2- The proportion of steel fibers increases the overall compressive strength.
3- In the final loading stage, as the fiber content increases, the final deflection of the beams will be reduced.
4- After conducting the test, it was found that increasing the proportion of steel fibers in percentages 0.5%, 1% and 1.5% decreases the mid-span deflection at service load by 33%, 50% and 37.5 and increases the ultimate load by 36.36%, 41.6% and 53% respectively.
5- Two types of cracks appeared after the beams were exposed to direct fire, the first type was in the form of honeycomb, and the second type was the result of deflection resulting from bending.
6- Concerning the color of the concrete, the color of the concrete did not change until 200 °C, while notice the color change at higher temperatures, the pink color.

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