Stress Distribution in Implant-Supported Overdenture and Peri-Implant Bone Using Three Attachment Systems: A Finite Element Analysis

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Abstract

**Background:** This finite element analysis (FEA) evaluated stress distribution in implant-supported overdenture (ISO) and peri-implant bone using one extracoronal (ball) and two intracoronal (locator and Zest Anchor Advanced Generation (ZAAG)) attachment systems.

**Methods:** In this in vitro study, the mandible was modelled in the form of an arc-shaped bone block with 33 mm height and 8 mm width. Two titanium implants were modelled at the site of canine teeth, and three attachments (ZAAG, locator, and ball) were placed over them. Next, 100 N load was applied at 90° and 30° angles from the molar site of each quadrant to the implants. The stress distribution pattern in the implants and the surrounding bone was analyzed, and the von Mises stress around the implants and in the crestal bone was calculated.

**Results:** While minimum stress in peri-implant bone following load application at 30° angle was noted in the mesial point of the locator attachment, maximum stress was recorded at the distal point of the ball attachment following load application at 90° angle. Maximum stress around the implant following load application at 90° angle was noted in the lingual point of the ball attachment while minimum stress was recorded in the lingual point of the locator attachment following load application at 90° angle.

**Conclusions:** According to the results, the locator attachment is preferred to the ZAAG attachment, and the ball attachment should be avoided if possible.

**Background**

Implant-supported overdenture (ISO) is an efficient treatment plan due to its simplicity, non-invasiveness, and affordability (1,2). It is particularly suitable for patients who are not satisfied with their complete dentures. Overdentures are preferred for use in patients with severe resorption of the alveolar ridge or those who cannot afford placement of several dental implants. Different attachment systems are used to connect implants to overdentures such as the bar, ball, and magnet attachment systems (3,4). Using implants to support the overdenture significantly increases its retention and stability. Biomechanical factors play an important role in preservation of the peri-implant bone. Loads applied to the overdenture are transferred to the implants and subsequently to the peri-implant bone. Bone tissue undergoes remodeling in response to mechanical loads. The stresses applied through the implants to the bone may be constructive or destructive. Very low stress can lead to disuse atrophy of bone while excessive pressure can cause compression necrosis and subsequent implant failure (5,6). ISOs should be designed such that they uniformly distribute the stress to implants and peri-implant bone (7-9).

Selection of the appropriate attachment type for overdenture is challenging for many prosthodontists because attachments transfer the stress and loads applied to the overdenture to the abutments, and subsequently to the bone (10,11). The generated stress is affected by a number of factors such as the type of load, the material of attachments, the design of attachments, and the quality of bone surrounding the abutments. Considering the increasing use of overdentures, selection of the...
appropriate attachment type can help benefit from the advantages of overdentures (12-14). The attachments increase the overdenture retention over the implants. However, they also transfer vertical and/or horizontal loads to the implants (15-17).

Several methods are available for assessment of stress distribution around dental implants such as photoblastic methods, finite element analysis (FEA), and measurement of strain in bone. FEA has advantages such as accurate reconstruction of complex geometrical shapes, enabling simple manipulation and alteration of patterns, and simulation of internal stress patterns and other mechanical quantities (18). Considering the gap of information regarding stress distribution patterns in use of intracoronal and extracoronal attachments following load application from different angles, this study aimed to assess stress distribution in ISO and peri-implant bone in use of three attachment types including one extracoronal (ball) and two intracoronal (locator and Zest Anchor Advanced Generation (ZAAG)) attachment systems using FEA.

Materials and Methods
This in vitro experimental FEA was conducted on three models. First, the mandible was modelled in the form of an arc-shaped bone block with 33 mm height and 8 mm width. Two titanium implants (D3 BioHorizons implant system) with 12 mm height and 3.8 mm diameter were modelled at the site of canine teeth in this block. The implants had 8 mm distance from the midline. Three models were designed for the three attachment systems. The Zest Anchor Advanced Generation (ZAAG) intracoronal attachment system (Zest Anchor, CA, USA) was used on implants bilaterally in the first model. The locator intracoronal attachment system (Zest Anchor, CA, USA) was used on implants bilaterally in the second model; and the ball extracoronal attachment (Rhein 83; Bologna, Italy) was used bilaterally on implants in the third model. An overdenture with 0.5 mm height from the ridge crest was placed over the attachments.

Characteristics of the Attachments
ZAAG attachment (Zest Anchor, CA, USA): Length of male component: 2.7 mm, diameter of male component: 4.2 mm, abutment thread height: 2.9 mm, thread radius: 1.1 mm
Locator attachment (Zest Anchor, CA, USA): Length of male component: 1.35 mm, diameter of male component: 2.1 mm, length of female component: 2 mm, diameter of female component: 0.52, cap height: 1 mm.
Ball attachment (Rhein 83, Bologna, Italy): Length of male component: 2.85 mm, diameter of male component: 1.2 mm, diameter of cap: 5 mm, length of cap: 2.5 mm
The ABAQUS software was used to design the geometrical shapes. A total of 45 solid elements were used for all items with three degrees of freedom for stress calculation. Similar to previous studies, the Poisson's ratio and the modulus of elasticity were used for better simulation of clinical setting by the models.

The jawbone was divided into two segments: the top 3 mm of crestal bone was considered as the cortical bone while the rest of the bone block (to the bottom) was composed of spongy bone. It should be noted that all modeled materials were isotropic, homogenous, and linearly elastic.

In this study, the number of elements and nodes was about 30 000 and 40 000, respectively based on previous studies. Eventually, 100 N load was applied to the models at 30° and 90° angles. The loads were applied from the site of molar teeth at each quadrant. Next, the stress distribution pattern in implants and peri-implant bone was analyzed. The von Mises stress around the implants and in the crestal bone was also calculated.

Results
The von Mises stress in all three models at the buccal, lingual, mesial, and distal points of the implant platform and crestal bone was calculated following load application at 30° and 90° angles.

Comparison of the von Mises stress in the peri-implant bone in use of the three attachment types revealed maximum stress in the ball attachment (6598) followed by the ZAAG (5455) and locator (4760) attachments after load application at 90° angle.

Maximum stress was noted in the ball attachment (6254) followed by the ZAAG (5330) and locator (4551) attachments after load application at 30° angle.

Comparison of the von Mises stress in the implants in the three attachment systems revealed maximum stress in the ball attachment followed by the locator and ZAAG attachments after load application at 90° angle. Maximum stress was noted in the ball attachment followed by the ZAAG and locator attachments after load application at 30° angle. Figure 1 compares the magnitude of stress in the peri-implant bone in the three attachment systems following load application at 30° and 90° angles.

Comparison of stress in the peri-implant bone in the three attachment systems following load application at 30° and 90° angles revealed minimum stress at the mesial point of the locator attachment following load application at 30° angle; meanwhile, maximum stress was noted at the distal point of the ball attachment following load application at 90° angle (Figure 1).

While the load application at 30° and 90° angles revealed maximum stress at the lingual point of the ball attachment following the application of 100 N load at 90° angle, minimum stress was noted at the lingual point of the locator attachment following load application at 90° angle (Figure 2).

Assessment of stress at different points of the three
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The following results were obtained:

1. The ball attachment transferred greater stress to the implants and the peri-implant bone at all points and at both load application angles.
2. The locator attachment transferred lower level of stress to the implants and the peri-implant bone compared with the other two attachments at both load application angles.
3. A higher level of stress was recorded at all points following load application at 30° angle compared with 90° angle.
4. A higher level of stress was noted in the peri-implant bone and lingual point of all attachments in load application at 30° angle compared with 90° angle.
5. In total, the level of stress transferred to the implants was greater than the level of stress transferred to the bone, especially in the lingual region.

Our findings were similar to those of Ibrahim and Radi (19) in Cairo University. They assessed the changes in bone and peri-implant bone atrophy in 14 completely edentulous patients using ball and locator attachments. After 18 months, the bone loss in patients who had the ball attachment indicated a higher level of stress in the ball attachment compared with the locator attachment. Also, the level of stress in both ball and locator attachments was greater at the distal compared with the mesial surface, which indicates higher stress accumulation at the distal point. This finding was in agreement with our results.

El-Anwar et al (20) evaluated the effects of number of implants and attachment type on stress distribution in ISO of the mandible and concluded that the attachment deformity and stress distribution in the locator attachment were insignificant compared with the ball attachment. This finding indicates higher survival rate and less need for repair of this attachment. Their results were in accordance with our findings. Similarly, El-Anwar et al (21) reported that the level of stress applied to the peri-implant bone was greater at the distal compared with the mesial surface. Cakarer et al (22) reported that 14 patients were dissatisfied with the ball attachment, and seven patients were dissatisfied with the bar attachment. However, no dissatisfaction with the locator attachment was reported. They concluded that use of locator attachment is associated with higher patient satisfaction; their findings were in accordance with our results.

Saboori et al (23) found that overdentures with the bar attachment experienced greater stress following vertical load application to both the implant at the side of load application and the contralateral implant compared with other attachment systems. The level of stress in implants was greater in oblique load application than vertical load application. In use of ball and ZAAG attachments, stress was applied to the implants and the edentulous ridge following vertical load application. However, in oblique load application, greater stress was applied to the implants.

Discussion

This FEA evaluated three overdenture attachment systems including one extracoronal and two intracoronal implant attachments. Considering the pattern of von Mises stress distribution at the four points of buccal, lingual, mesial, and distal of the ZAAG (Model 1), locator (Model 2), and ball (Model 3) attachments and in peri-implant bone following load application at 30° and 90° angles, the attachment systems revealed that all three attachment systems had maximum stress accumulation at their distal point. Minimum stress was noted at the mesial point of the locator and ZAAG attachments and at the buccal point of the ball attachment.
while no stress was recorded in the edentulous ridge. The bar attachment transfers greater stress to the implants following vertical and oblique load applications compared with the ball and ZAAG attachments. Comparison of the ball and ZAAG attachments revealed that the ZAAG attachment transferred greater stress to the implant body compared with the ball attachment, which was different from our findings; this controversy may be due to the different directions of load application.

Mericske-Stern and Zarb (4) performed a piezoelectric test and observed that vertical load application resulted in greater stress in the implant body in use of a single telescopic attachment compared with the ball attachment, which was inconsistent with our findings. Such a controversy in the results can be due to the different designs or applied loads. Our literature review yielded no study comparing the ball, ZAAG, and locator attachments to compare our results with. The majority of previous studies focused on ball attachment or compared two attachment systems.

Conclusions
Within the limitations of this study, it may be concluded that the locator attachment (Model 2) is preferred to the ZAAG attachment (Model 1) for ISOs in terms of stress distribution, and the ball attachment (Model 3) should be avoided if possible.

Conflict of Interest Disclosures
The authors declare that they have no conflict of interests.

Ethical Statement
The Research Ethics Committee of Hamadan University of Medical Sciences approved this study.

Authors’ Contribution
AI: Conceived and designed the analysis, supervised the paper
FV, AS: Conceived and designed the analysis; collected the data; contributed data or analysis tools; wrote the paper
MTMV: performed the analysis; wrote the paper

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