Three decades of tropospheric ozone lidar development at Garmisch-Partenkirchen, Germany

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Abstract. Since 1988 two ozone lidar systems have been developed at IMK-IFU (Garmisch-Partenkirchen, Germany). A stationary system, operated at the institute, has yielded about 5000 vertical profiles of ozone from next to the ground to typically 3 km above the tropopause and has contributed data for a large number of scientific investigations. A mobile system was successfully operated in a number of field campaigns after its completion in 1996, before it was destroyed in major flooding in May 1999. Both systems combine high data quality with high vertical resolution dynamically varied between 50 m in the lower troposphere and 250–500 m below the tropopause (stationary system). The stationary system has been gradually upgraded over the years. The noise level of the raw data has reached about \( \pm 1 \times 10^{-6} \) of the input range of the transient digitizers after minor smoothing. As a consequence, uncertainties in the ozone mixing ratios of 1.5 to 4 ppb have been achieved up to about 5 km. The performance in the upper troposphere, based on the wavelength pair 292–313 nm, varies between 5 and 15 ppb depending on the absorption of the 292 nm radiation by ozone and the solar background. In summer it is therefore planned to extend the measurement time from 41 s to a few minutes in order to improve the performance to a level that will allow us to trust automatic data evaluation. As a result of the time needed for manual refinement the number of measurements per year has been restricted to under 600. For longer time series automatic data acquisition has been used.

1 Introduction

Lidar measurements of tropospheric ozone have resulted in important contributions to atmospheric research. Large variations of the concentrations on timescales of less than 1 h may be observed, which have led to insight into a number of tropospheric transport processes (see Table A1 for a large number of examples). In addition, measurements with ozone lidar systems have contributed to numerous air-quality studies (Table A2). Due to considerable technical progress, rather small changes in the volume mixing ratio of just a few parts per billion (ppb) can currently be resolved, which is necessary for also distinguishing the influence of minor contributions and for reliable trend studies.

Still, important tasks in tropospheric ozone research exist, such as a clarification of the positive ozone trend observed until 2003 at high-altitude observational sites in Europe (Scheel, 2003; Ordoñez et al., 2007) despite the pronounced reduction of ozone precursors over Europe (Jonson et al., 2006; Vautard et al., 2006), a detailed analysis of the rather complex contributions of different sources to long-range transport, and the influence of vertical mixing on free-tropospheric layers, in particular on stratospheric air intrusions (Trickl et al., 2014, 2015, 2016). Although vertical sounding, including lidar measurements of complementary quantities such as aerosols and water vapour (e.g. Trickl et al., 2014, 2015, 2020; Strawbridge et al., 2018; Fix et al., 2019), can yield key information for the understanding of the role of the underlying atmospheric processes, for a long time there was no significant growth in the number of tropospheric ozone lidar stations towards something like an international network. By contrast, more and more ozone lidar systems have even been shut down. Opposite to
this development, the Tropospheric Ozone Lidar Network (TOLNet, https://www-air.larc.nasa.gov/missions/TOLNet/, last access: 19 November 2020) with seven lidar stations was recently established in North America (e.g. Newchurch et al., 2016; Wang et al., 2017; Leblanc et al., 2018). It is important to note that even vertical profiles from the impressive MOZAIC (Measurements of Ozone and Water Vapor by Airbus In-Service Aircraft) (Marenco et al., 1998) database are not able to resolve the fine-scale temporal variability of the vertical distribution of trace constituents because of the rather confined time slots for aircraft departures and arrivals at the individual airports. Satellite measurements cannot yield the necessary information because of presently insufficient spatial resolution and global coverage within a day.

With a few exceptions, mostly ultraviolet (UV) differential-absorption lidar (DIAL) systems for tropospheric applications have been proposed and developed since 1975 (Papayannis et al., 1990; Table A3). Here, the advantages of high Rayleigh backscattering and strong absorption cross sections are combined. In Europe, the TESLAS (Tropospheric Environmental Studies by Laser Sounding) subproject of EUROTRAC (EUREKA Project on Transport and Chemical Transformation of Environmentally Relevant Trace Constituents in the Troposphere over Europe; EUROTRAC, 1997) has resulted in the coordinated development of several state-of-the-art ozone lidar systems (TESLAS, 1997). Lidar sounding of tropospheric ozone is a demanding technical task (Weitkamp et al., 2000) because of the considerable dynamical range of the backscatter signal covering up to about 8 decades, the presence of aerosols and clouds, interfering trace gases such as SO2 and NO2, and the solar background (stratospheric ozone measurements are normally made during night-time), all necessitating an elaborate optical and electronic design. The data evaluation is based on derivative formation that is particularly sensitive to signal perturbations that set limitations to resolving the frequently rather small changes in free-tropospheric ozone.

At IFU (Fraunhofer-Institut für Atmosphärische Umweltforschung; now Karlsruher Institut für Technologie, IMK-IFU), a differential-absorption lidar (DIAL) with a particularly wide operating range from next to the ground to the upper troposphere was completed in 1990 in the framework of TESLAS and subsequently applied for a full year (1991) within the TOR (Tropospheric Ozone Research; Kley et al., 1997) subproject of EUROTRAC (Carnuth et al., 2002). The operating range of this system was extended to roughly 15 km by introducing three-wavelength operation (Eisele and Trickl, 1997). Due to thorough upgrading of the data acquisition system an uncertainty level of 1.5 to 4 ppb has been achieved up to the mid-troposphere (slightly higher in the upper free troposphere, depending on the ozone concentration and solar background).

In the mid-1990s a mobile ozone DIAL was additionally built in cooperation with OHB System (Bremen, Germany; Brenner et al., 1997). This system, which was completed in spring 1996 and exhibited at the 1996 International Laser Radar Conference, could be operated in a vertical range between 0.2 and more than 4 km with a similar accuracy as our stationary system at low altitudes. It was used in a number of field campaigns before it was destroyed by 2 m of water during major flooding in southern Bavaria in May 1999 while waiting for the VOTALP Munich field campaign (VOTALP II, 2000).

In this paper we review the experience gained with these two lidar systems. The development of these two systems has significantly contributed to the state of the art in this field. Meanwhile, even the dream of meaningful automatic data evaluation looks feasible due to the technical progress made. Most approaches and instruments used are the same in both lidar systems, which simplifies the description.

Most of the paper is devoted to the stationary DIAL. We describe only deviating design properties of the much compact mobile system such as the laser approach and the wavelength separation technique chosen. This system has been extensively used over 3 decades, but no full-size technical description has been given. We do not want to give a full description of all the technical improvements made over the years. Just the decisive steps are reported.

Most of the approaches of the ozone DIAL systems have also been successfully transferred to the other lidar systems of IMK-IFU.

2 General design considerations

In both IFU DIAL systems, fixed-frequency lasers and stimulated Raman shifting in H2 and D2 have been used for generating suitable “on” and “off” wavelengths (see de Schoulepinov et al., 1997; Milton et al., 1998, for general overviews). In this way just a single high-power laser source is needed. Both systems are three-wavelength lidars with two on wavelengths and one off wavelength. This offers the opportunity for wide-range operation starting below 0.3 km above the ground, with stronger absorption and accuracy as well as good vertical resolution for the shorter of the two on wavelengths and a range extension with lower vertical resolution for the longer on wavelength. In addition, the comparison of ozone profiles obtained from two separate wavelength pairs allows for internal quality control. In fact, as described in Sect. 6, for an optimum alignment and sufficient backscatter signal the agreement between the different ozone profiles is almost perfect. Apart from the wavelength separation methods, the basic optical layout principles and detection electronics are mostly the same. Both systems feature automatic data acquisition.

The stationary system (Fig. 1) is operated in two separate, rather large laboratories at IFU (47.477° N, 11.064° E; 740 m a.s.l.). This offers several advantages such as a simple optical layout, good alignment control due to long beam paths, reduced thermal drifts because of no direct exposure of
the laser system to outside air, and the long distance between detection electronics and the interfering laser system. Two separate power systems are used for the laser and electronics. The laser PC is connected to the cleaner power system for the electronics and controls the laser system via optical fibres. Remote control of the laser is achieved via RS232.

Due to the clean-air conditions prevailing at this rural site the wavelength choice is less critical. The ambient concentrations of SO$_2$ and NO$_2$, species with absorption bands in the spectral range of ozone DIAL systems, are low, which is known from the local long-term monitoring stations. Thus, the choice of the laser source was determined by high power in order to achieve a short measurement time. Krypton fluoride lasers have been used (Kempfer et al., 1994; Eisele and Trickl, 1997); since 1994 this has been a model with a maximum available average power of 54 W at 248.5 nm (all wavelengths in this paper are given for vacuum).

The laser choice was different for the mobile system (Fig. 2). A frequency-quadrupled Nd:YAG laser with up to 4.2 W of average power at 266.1 nm served as the basic source of ultraviolet (UV) light. This approach was preferred for several reasons: due to the expected operation in heavily polluted areas at least one wavelength combination (266–299 nm) reduces the cross-sensitivity with respect to SO$_2$ and NO$_2$ to about 0.01 ppb of ozone per part per billion of these species. Under such conditions, the perspective of low interference by aerosols is also important, which is fulfilled for short on wavelengths (Völger et al., 1996; Eisele and Trickl, 2005). Thus, wavelength combinations involving 266 nm are favourable. Finally, due to the choice of a solid-state laser source the dangerous gas handling in an excimer laser could be avoided, an issue for the mobile operation.

A clear design goal for the mobile system was a vertical range significantly exceeding the boundary layer by a few kilometres. This requirement was seen as crucial for meaningful investigations during air pollution field campaigns. The mobile ozone DIAL was mounted inside an air-conditioned truck (Fig. 2) and was designed for autonomous operation with an on-board power generator, batteries, automatic positioning (GPS), and detailed safety control management including rain and wind sensors, shutter control of the laser, and many interlocks. Critical safety conditions immediately overrode any other action. The operator could be automatically informed about incidents during night-time via telephone. After rain, the system could be restarted automatically, unless the laser was shut down (see Sect. 3.2).

The detection system of this DIAL was much simpler, with a less demanding optical set-up (single telescope for both near- and far-field detection, simple filter polychromator) and with fewer electronic components due to a sequential emission of two of the three operating wavelengths. All this resulted in a considerable reduction of costs, which at that time was an attractive perspective in view of the goal of our industrial partner of an affordable commercial system.

Overall specifications of the two systems are listed in Tables 1 and 2. All optical components and dielectric coatings have been provided by Laseroptik GmbH (Garbsen, Germany) unless otherwise specified.

3 Transmitter design

3.1 Stationary lidar

The transmitter of the system (Fig. 1, Table 1) is based on a KrF excimer laser (Lambda Physik, LPX 250, maximum repetition rate 100 Hz) consisting of a tunable narrowband oscillator and a three-pass power amplifier. CaF$_2$ is used for transmitted optics. CaF$_2$ is not birefringent, and thus polarization effects (Kempfer et al., 1994) and ageing are avoided. The energy was considerably enhanced by anti-reflection (AR) coating on the outer side windows of the amplifier gas cell and the beam splitter in front of the energy monitor. A pulse energy of up to 540 mJ was measured several metres away from the laser where divergent components also emerging from the amplifier can be separated and blocked by an aperture. For the lidar measurements the laser energy is usually set to 400 mJ. The unstable cavity of the amplifier yields a highly collimated rectangular beam with a divergence of 0.2 mrad. The wavelength was set for maximum output and the prism-grating combination never touched again. In 2010 measurements with a HighFinesse WS6 ($\Delta \lambda = 0.6$ pm) wavelength meter carried out over several days yielded 248.5078 nm $\pm 0.0060$ nm, in agreement with the results of Kempfer et al. (1994). The spectral bandwidth is specified as 0.2 cm$^{-1}$ (6 GHz). Locking the amplifier to the oscillator can be nicely verified by an enhancement of the pulse energy by up to 70 mJ under our standard operating conditions.

The output of the KrF laser is split by a 50 % beam splitter and focused into two Raman cells with $f = 1.0$ m AR-coated plano-convex CaF$_2$ lenses. One cell is filled with hydrogen and the other one with deuterium, and the same pulse energy per cell as previously used for a single cell (Kempfer et al., 1994) is ensured (almost 0.2 J). A total of six Stokes components are generated in hydrogen, just 277.124 nm (S1) and 313.188 nm (S2) are taken (Table 1). For deuterium the second Stokes (S2) component (291.838 nm) is used. The outer surfaces of the CaF$_2$ windows of the Raman cells are AR-coated. The inner ones are not coated because of the possibility of ageing in the presence of photolysed hydrogen. The pump radiation leaving the evacuated Raman cells is of the order of 160 mJ. The output of the Raman cells is combined with a pair of dichroic beam combiners and collimated with an $f = 5$ m, 150 mm diameter concave spherical mirror. The beam combiners reflect 99 % of the 292 m radiation at 45° and transmit 88 to 90 % of all the other relevant spectral components. Overlap and pointing of the 292 nm beam are optimized by placing a wire cross in front of the D$_2$ cell or

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Figure 1. Overview of the IFU stationary ozone DIAL system; the system covers two separate laboratories for the laser and the telescopes. Abbreviations are as follows. M1, M2: dielectric high-reflecting mirrors for 248 nm; SM: spherical mirror (M3), high-reflecting for 248 to 313 nm; \( f = 5 \) m; M4, M5: dielectric mirrors, high-reflecting for 248 to 313 nm; BS: 50 % beam splitter; BC: wavelength-selective beam combiner, reflecting 99 % at 292 nm for an incidence angle of 45\( ^\circ \) and transmitting all the other lidar wavelengths with losses not exceeding 12 %. A: rectangular sand-blasted aluminium apertures for blocking divergent parts of the amplifier emission that would otherwise hit and evaporate the black surfaces of the optics holders, leading to more rapid ageing of the optics.

Table 1. Transmitter details (the numbers are given for normal operating conditions).

| | Stationary system | Mobile system |
|---|---|---|
| Laser source | KrF laser | frequency-quadrupled Nd:YAG laser |
| Wavelength | 245.50 nm | 266.12 nm |
| Pulse energy | 400 mJ | 70 mJ |
| Pulse repetition rate | 9 Hz | 30 Hz |
| Operating wavelengths (nm) | 277.124\(^a\), 291.838\(^b\), 313.188\(^a\) | 266.12, 289.10\(^b\), 299.21\(^a\) |
| Emission | simultaneous | 289 and 299 nm sequential, 266 nm for each pulse |
| Beam expansion | 5 : 1 | 6 : 1 |
| Beam divergence | \(< 0.75 \) mrad | \(< 0.5 \) mrad |

\(^a\) \(Q_1\) line of first Stokes shift in \(H_2\) (Bragg et al., 1982; Dickensen et al., 2013): 4155.2521 cm\(^{-1}\). \(^b\) \(Q_2\) second Stokes shift in \(D_2\) (Jennings et al., 1986): 2987.289 cm\(^{-1}\).

behind the second beam combiner by watching the images of the cross in front of mirror M4.

The Raman conversion efficiency obtained with the LPX 250 laser system is lower than that previously published (Kempfer et al., 1994). We ascribe this to the smoother energy distribution in the beam profile of the new laser. As an example, Fig. 3 shows the conversion efficiencies obtained for hydrogen for a laser pulse energy of almost 200 mJ per Raman cell, attenuated by the optics, in particular by the single-side AR-coated cell entrance windows. The sum of all conversion efficiencies is less than 1.0 starting at already low pressures. This loss of overall energy is tentatively ascribed to optical breakdown. Above 3 bar the loss starts to level off. The non-negligible fourth Stokes emission (Kempfer et al., 1994) was not determined. The maximum second Stokes conversion efficiency for deuterium is approximately 17 % (at 11 bar). The operating pressures have been chosen at around 3.3 and 11 bar for \(H_2\) and \(D_2\), respectively.

The conversion efficiency was determined for a laser repetition rate of 10 Hz in order to avoid damage to the power meter used. During the lidar measurements it turned out that the second Stokes output may increase when selecting a rep-
Table 2. Receiver details (latest version only).

|                      | Stationary system                                      | Mobile system                                    |
|----------------------|--------------------------------------------------------|--------------------------------------------------|
| Primary mirrors      | 0.13 m diameter, $f = 0.72$ m                         | 0.36 m diameter, $f = 1.56$ m                    |
| Wavelength separation| two 1.1 m grating spectrographs                       | sequential detection of 289 nm, 299 nm, 266 nm optically separated |
| PMTs                 | Hamamatsu 7400 modified by RSV                       | Hamamatsu 5600                                   |
| Pre-amplifiers       | gain 1–10, bandwidth 4 MHz                            |                                                   |
|                      | (1996–2011)                                            |                                                   |
| Transient digitizers | 6 units, 12 bit, 20 MHz ground-free input stages      | 4 units, 12 bit, 20 MHz                          |
| Photon counting      | 10 GHz time bins                                      |                                                   |
| Measurement time     | 41 s                                                   | 10 min                                           |

Figure 2. Overview of the mobile ozone DIAL: the laser and the Raman-shifting components were mounted on optical tables at two different levels of a shock-isolated frame. The Newtonian telescope was located in a separate tower, with the secondary mirror directing the beam into a polychromator perpendicularly to the plane formed by the telescope and the outgoing laser beam. The covers of the Raman compartment (jalousies on both sides) and the telescope (door) were removed in this simple view. The laser power supply was delivered in two units custom-made to fit under the lower laser table. The entire frame was rolled into the lorry through the rear doors.

Figure 3. Raman conversion efficiency ($f = 1.0$ m) as a function of pressure for shifting the 248.5 nm radiation in hydrogen; the top curve (dark green) represents the sum of the residual pump energy and the first three Stokes emissions normalized to the pump energy at zero pressure. The less important higher Stokes emissions were not measured here but may contribute above 4 bar, which would shift the sum to higher values.

Linear polarization is important for single-line output of the Raman shifters (Kempfer et al., 1994). Thus, we placed a Glan prism and a Fresnel rhomb (both from Halle) in the beam between the oscillator and amplifier. All mirrors and beam splitters of the transmitter section were manufactured with minimum polarization sensitivity. The Fresnel rhomb is rotated for optimum backscatter signal (Fig. 4). The strong modulation of the lidar signal in Fig. 4 is mainly caused by the holographic gratings used in the receivers (Sect. 3).

Due to the high average power of the laser system the time for a single ozone measurement, carried out with a repetition rate of 99 Hz, is as short as 41 s.
3.2 Mobile lidar

The pump laser of the mobile DIAL was a frequency-quadrupled Nd:YAG laser with a 30 Hz repetition rate and pulse energies of up to 140 mJ at 266 nm (Continuum, Powerlite 9030). The laser was selected because of a remote control option. The manufacturer promised external control of warm-up and rotation of the frequency doubling and quadrupling crystals. The 1064 and 266 nm powers were measured by two Molectron power meters for a PC-based power optimization. However, the computer control never worked properly: automatic warm-up of the laser was never achieved. The reason was a conflict with “keep-alive” pulses that had to be sent by the external control.

The quadrupling was achieved by using BBO (beta barium borate). This approach yielded high conversion efficiency and moderate thermal loading. However, after more than 1 year of infrequent operation of the lidar the surface of the crystal started to degenerate. This turbid layer did not strongly reduce the UV emission and polishing was therefore postponed.

At maximum pump energy (1.6 J at 1064 nm) the 266 nm radiation exhibited a ring-shaped mode at a pulse-energy level of 140 mJ. We reduced the pulse energy to 1.1 J. Still, 120 mJ could be produced, now with a filled beam profile. However, a hot spot formed that focused in the Raman-shifting compartment and we reduced the UV output to about 70 mJ for safety reasons. This hot-spot problem was solved by the manufacturer in a later (“precision”) version of the laser.

A ceramics shutter was added to the exit holes of the Powerlite laser that was controlled by both the safety system and the lidar PC. Closing the shutter was preferred to switching off the laser oscillator in order to maintain stable thermal conditions in the laser during an interruption.

A side view of the lidar including the entire transmitter is given in Fig. 2, which is the lower level of the frame in Fig. 5. Figure 5 shows the Raman-shifting compartment that also contained a 6 : 1 beam expander used for reducing the beam divergence. Rotating beam splitters were used for directing the laser pulses into the H2 and D2 cells. These beam splitters were based on circular quartz plates differently coated on the two halves of the surface: high-reflecting for the lidar wavelengths on one half and high-transmitting on the other one. The rotation was synchronized to the laser pulses. The control unit issued pulses for identifying the Raman cell actually passed for the data acquisition system. Two precision motors with measured out-of-axis rotation of just about ±2 and ±40 µrad, respectively, were chosen (KaVo, model EWL 4025; with custom-made electronic control).

Due to high thermal sensitivity the emission wavelengths of Nd:YAG lasers may vary considerably from model to model. We derive a guess of the unknown pump wavelength of our Powerlite laser model from Trickl et al. (1989; 2007) and wavelength measurements for three other injection-seeded Nd:YAG lasers in our laboratory. The average pump wavelength is 266.120 nm ± 0.011 nm. This yields first-Stokes-shifted wavelengths of 289.103 nm (in D2) and 299.209 nm (in H2).

By focusing the 266 nm beam with an f = 1.0 m plano-convex lens we reached maximum first Stokes (S1) conversion efficiencies of almost 50 % in both hydrogen and deuterium at pressures as low as 0.9 and 1.6 bar, respectively. This is remarkable in two respects: the theoretical Raman conversion efficiency reaches 50 % at higher pressures and...
the Raman gain of deuterium is substantially smaller than that of hydrogen (de Schoulepnikov et al., 1997). A total of 5 Stokes orders and 1 anti-Stokes order were visually observed for hydrogen, with fewer orders for deuterium. There was some contribution of the second Stokes order (particularly low at 1 bar due to gain competition with S1), but those for the higher orders were below the 1 mW detection threshold of the power meter used. Starting at pressures below the threshold for Raman conversion absorption was realized and, in H\textsubscript{2}, the conversion efficiency rapidly dropped to zero above about 1 bar. The same effect was also observed in pure helium and argon. Thus, we ascribe these observations to laser-induced breakdown. The role of the hot spot in igniting this breakdown could not be examined. Quite obviously, the Stokes emission was emitted prior to the breakdown maximum (see also Trickl, 2010a). In any case, the high conversion efficiency achieved was more than enough for the lidar operation.

Motivated by the hot-spot problem the focusing lens was replaced by a pair of crossed \( f = 1.0 \text{ m} \) cylindrical lenses during the final phase of operation of this lidar system. As suggested by Perrone and Piccinno (1997) this may result in a softer focus, a larger focal volume, and higher Raman conversion. The maximum possible distance between the two lenses was about 12 cm and was chosen for the lidar operation. In Fig. 6 the conversion efficiencies as a function of cell pressure for this distance and also for the minimum possible distance of about 5 cm is given. A clear change in behaviour was seen. The transmitted pump energy no longer dropped to zero above 1 bar. As one would expect the depletion for pressures up to 2 bar is smaller for the larger distance between the two lenses. Quite interestingly, the pump depletion in D\textsubscript{2} was much less pronounced than that in H\textsubscript{2}. Despite these obvious improvements, the maximum conversion efficiency just rose for H\textsubscript{2} (to 61 \%, comparable to the results by de Schoulepnikoff et al., 1997).

The rectangular beam-steering mirror was mounted on two mutually orthogonal rotation stages (OWIS). The beam pointing angle was set on the lidar PC.

4 Receiver design

4.1 Design principles

The optical layout of the IFU lidar systems built or modernized since 1990 is based on several design principles:

1. the use of Newtonian telescopes for a less critical alignment than in the case of a Cassegrain telescope and for an easier discrimination of the near-field signal; and

2. separate detection in near-field and far-field channels in order to reduce the giant dynamical range of the backscatter signal covering roughly 8 decades.

3. No optical elements or detectors must be placed close to the focal points in order to avoid a modulation of the backscatter signal by the near-field scan of the focal point across inhomogeneously transmitting or detecting surfaces. A severe example for a photomultiplier tube (PMT) is given by Simeonov et al. (1999). In particular, this principle also strongly prohibits the use of optical fibres because of their unknown input surface quality (apart from the coupling losses).

4. Particularly inhomogeneous surfaces must be placed in or very close to image planes (exit pupils) where the image spots and the light bundle as a whole stay stable in space. As a result even very long beam paths do not matter as long as no aperture is hit due to an excessive pointing drift of the laser beam. In this way a stable performance is achieved over long periods of time. Also, the diameter of the light bundle reaches its minimum in the exit pupil, and it is important to place components with limited diameter in (or very close to) this plane, such as detectors, optical filters, gratings, or beam splitters.

5. All lenses with focal lengths below 0.2 m must be anti-reflection-coated in order to avoid angle-dependent transmittances. Anti-reflection coating was applied to all lenses in IFU lidar systems after 1995 to avoid transmission losses.

In most of our lidar systems we have chosen a modular design composed of a series of relay-imaging pairs of equal lenses (distance 2f) with beam splitters or filters close to the centre between the lenses (Vogelmann and Trickl, 2008; Giehl and Trickl, 2010; Klanner et al., 2020). This approach is also implemented in the receiver of the stationary ozone DIAL but with a holographic grating instead of optical filters. However, in the mobile system a convergent beam path was chosen behind the ocular of the telescope in order to save space.

4.2 Telescopes

4.2.1 Stationary system

The large dynamical range of the backscattered light of about 8 decades is reduced by using two separate Newtonian telescopes (Kempfer et al., 1994) as shown in Fig. 1 (manufacturers: Vehrenberg for the entire small telescope and Lichtenknecker for the mirrors only). The primary mirrors have diameters of 0.13 and 0.5 m and focal lengths of 0.72 and 2.0 m, respectively. The axes of the two telescopes are in plane with the outgoing laser beam and located about 0.2 and 1.8 m from that of the beam, respectively.

The solar background was reduced by both black surfaces and a black circular baffle around the input path of the backscattered radiation. This turned out to be insufficient af-
ter introducing new detectors in 2012 that are more susceptible to the background (Sect. 4.4).

The approximate vertical range is 0.2 to 2.5 km above the ground for the small near-field telescope and 1.5 to 3–5 km above the tropopause for the large far-field telescope with a dynamically adjusted vertical resolution of 50 to 300–500 m. Both telescopes are combined with 1.1 m grating spectographs. This led to a much better daylight rejection in comparison with Kempfer et al. (1994).

The alignment of the small telescope is very difficult, given the very long beam paths through the polychromator (Sect. 3.3). It was highly difficult to avoid nonlinearities of the results on the first few hundred metres. The signal had to be attenuated by a factor of 10. The solution was found a few years ago. During the routine four-quadrant (“telecover”) testing (Freudenthaler et al., 2008) introduced for quality assurance within EARLINET (European Aerosol Research Lidar Network; e.g. Amodeo et al., 2006; http://www.earlinet.org/, last access: 19 November 2020), it turned out that almost the entire near-field return passed through the quadrant on the side of the outgoing laser beam (named the “north” sector). This explains the observed sensitivity to misalignment.

The north sector of the telescope was subsequently covered by a triangular piece of cardboard. After this, the alignment sensitivity of the near-field receiver (including the spectrograph, see below) disappeared, a stable linear performance was obtained, and the signal was attenuated to an acceptable level due to the missing north quadrant. Another important consequence was that no additional attenuators had to be used after this change. Most importantly, after the design change a very reliable diurnal variation of ozone could be retrieved in the boundary layer with a morning minimum and an afternoon maximum.

The alignment of the far-field receiver has remained stable during the past 24 years. The only parameters routinely optimized have been the laser-beam pointing and the overlap of the two partial laser beams from the two Raman shifters. Slight deviations in the overall beam pointing do (inside the slits in the focal planes) not matter (despite the long distances in the receivers) due to the imaging principles applied: the final and the intermediate images of the primary mirrors are not shifted.

4.2.2 Mobile system

A single Newtonian telescope with an \( f = 1.56 \text{ m} \), 317.5 mm diameter principal mirror (Intercon Spacetec) was used. The distance between the laser and the telescope axes was 0.5 m. The exit of the telescope towards the detection polychromator was (horizontally) perpendicular to these two axes.

4.3 Wavelength separation

4.3.1 Stationary system

After 1994, wavelength separation for the stationary system was achieved with two identically built 1.1 m grating spectrographs, one per telescope (Figs. 1 and 7). A grating spectrograph has the advantage of the transverse near-field–far-field beam walk and the spectral separation taking place in separate, mutually orthogonal planes. As explained in more detail by Kempfer et al. (1994), a near-Wadsworth configuration was chosen in order to reduce the astigmatism to an acceptable level. The Wadsworth angle for a given wavelength is defined by an exit of the first diffraction order along the grating normal. As shown by ray tracing the spectral resolution is also close to optimum for this approach and was expected to be 0.2 nm. The design described by Kempfer et al. (1994) was extended by placing \( f = 80 \text{ mm} \) lenses in front of the detectors for imaging the primary mirrors of the telescopes onto the photocathode of the PMT. The spherical grating (Carl Zeiss, \( r = 1995 \text{ mm} \)) was also placed in an image plane of the primary mirror to minimize the diameter of the radiation bundle. Detailed numbers are given by Eisele (1997).

The true spectral resolution was determined with a mercury lamp to be about 0.35 nm, achieved with low-intensity emission lines not exhibiting line broadening due to absorption in the lamp prior to emission. Due to the defocusing caused by the beam walk the effective spectral range for the components of the integrated lidar return is 1.0 nm (full-width at half-maximum, f.w.h.m.), but with sharp edges. The grating efficiency was specified as 70 % by the manufacturer (Carl Zeiss, Oberkochen) in auto-collimation, which may be different for the Wadsworth configuration.

An aperture with four adjustable blades (custom-made by OWIS) was placed at the entrance of each spectrograph in the focal plane of the primary mirror for reducing the level background light. In the large receiver the vertical blades were adjusted to block the near-field return and to transmit the return from all longer distances. These vertical blades were never touched again, and the laser-beam-steering mirror was always set for a peak signal at 8.0 \( \mu \text{s} \). The horizontal blades are set for a slit width of 2–3 mm, alignment with a narrow slit. The minimum slit width possible for S1 radiation is 0.7 mm (0.35 mrad), with more being needed for the S2 components. The consequence of the small spot size is a low susceptibility to typically observed laser pointing drifts, and the 277 nm return always yields correct ozone values.

Further adjustable slits (widely open) were placed in the secondary focal planes in front of the PMTs. However, this was just for occasionally controlling the alignment since no cross-talk between the different wavelength channels was observed. As mentioned, no alignment drifts were found.

As already mentioned in Sect. 3.1 the lidar signal varies with the polarization angle of the laser (Fig. 4). An approx-
Figure 6. Raman conversion efficiencies and pump beam depletion for a pair of crossed $f = 1.0 \text{ m}$ cylindrical lenses: (a) S1 and S2 in hydrogen; (b) S1 and S2 in deuterium; (c) normalized transmitted pump energy in both $\text{H}_2$ and $\text{D}_2$.

Figure 7. Layout of the two grating spectrographs; $\alpha = 35^\circ$ is the Wadsworth angle chosen, corresponding to a wavelength of 240.0 nm. The choice of angle was limited by the space available in the housing of the spectrograph, also considering the big PMTs initially used.

imate 5 : 1 sinusoidal modulation is seen. The polarization angle was set for optimum signal.

4.3.2 Mobile system

The polychromator design for the mobile system is quite different and is based on dielectric mirrors, beam splitters, an edge filter, and adjustable-slit apertures (Fig. 8). The 289 and 289 nm returns were separated by temporal discrimination, triggered by the rotating beam splitters described in Sect. 3.2. The data were stored in different areas of the transient digitizers. The separation of the larger gap between 266 nm and the two longer wavelengths could be conveniently achieved by pairs of dielectric beam splitters (BS3), each of them transmitting just 3% of the longer wavelengths and fully reflecting the 266 nm component at an incidence angle of 45°. In this way, two 266 nm channels were available for both the near- and far-field sections of the polychromator. As seen in Fig. 8, the entire arrangement is highly symmetrical and almost identical for the near- and far-field parts. A 1 : 100 beam splitter and an o.d. 1.0 neutral density filter (Andover) were used to separate and to attenuate the near-field return. In the far-field section the signal was first adjusted to perfectly match the near-field signal for low PMT gain. After this procedure, OWIS adjustable-blade apertures (see above), placed in the focal planes in front of the PMTs, were used to cut off the strong near-field return that was shifted horizontally (due to the perpendicular geometry of the outgoing laser beam, the telescope axis, and the telescope output axis). Finally, the PMT gain was increased to maximize the
far-field signal. This approach is a rather simple alternative to the use of two telescopes as done in our stationary system and is also applied in our water vapour DIAL (Vogelmann and Trickl, 2008). However, it requires very constant pointing of the outgoing laser beam in order to avoid changes in signal level. This was not exactly the case for the laser used here but could be verified for the more recent (precision) version of the Powerlite laser of the H$_2$O DIAL.

An OWIS adjustable-slit aperture was also placed in the focal plane of the telescope (top of Fig. 8) for the reduction of the solar background. To account for the changing position of the “focus” as a function of the changing position of the outgoing laser pulse the orientation of the slit was horizontally tilted (i.e. perpendicular to the orientation in the stationary system due to the 90° rotation of the telescope exit). The vertical blades of the aperture could be closed to 1.7 mm (corresponding to an acceptance angle of 1 mrad) without a loss of signal but were set slightly wider during normal operation.

Each of the four detection channels principally looked the same, apart from the different surfaces of the components (HR1, high reflector for 266 nm; BS3). As mentioned, the set-up deviates from the conventional modular set-up with relay-imaging lenses. The $f_1 = 100$ mm ocular (L1) does not collimate the lidar return: it directly refocuses the radiation to an intermediate focal point. In this way, the overall distance to the detectors could be shortened. Just one additional lens ($L_2$, $f_2 = 50$ mm) was used for exactly imaging the principal mirror of the telescope onto the photocathodes of the PMTs. Most optical components were placed in the vicinity of the intermediate images of the primary mirror (green dots in Fig. 8).

One deficiency that was never overcome before the destruction of the system was that just a single PMT was for both on and off channels in the far-field section. Since the on signal peak is already rather small at the beginning of the far-field signal, the off component should be attenuated e.g. by rotating quartz plates with two differently coated halves similar to those next to the Raman shifter. This would allow the off signal to be reduced to about the same level as the on signal, and a higher PMT gain could be used.

### 4.4 Detectors

The detectors are key components of our lidar development, which calls for an explicit description. As suggested by Kempfer et al. (1994), we exclusively used the 14-stage EMI 9893B photomultiplier tubes (PMTs) between 1994 and April 1996. For linear performance the 9893B detectors were operated with maximum analogue signal levels below 10 mV (50 $\Omega$ termination). This means that the very high gain of this 14-dynode PMT (up to 8 decades) is completely unnecessary. The big plus was range gating (Kempfer et al., 1994), lifting the far-field signal level to values mostly well above the electronic imperfections of the signal processing system. The range-gating circuit was further improved for repetition rates of more than 20 Hz.

However, after very positive testing in 1995, we introduced Hamamatsu H5783P-06 PMT modules to both DIAL systems in spring 1996 (Brenner et al., 1997; Eisele and Trickl, 1997). The miniature PMT features a built-in Cockroft–Walton power supply, an 8 mm diameter photocathode, and six mesh dynodes, leading to a maximum current gain of $3 \times 10^5$. This gain is sufficient for obtaining a very big lidar signal. This module is extremely linear over at least 5 decades for analogue signals up to at least 100 mV (50 $\Omega$ termination) in the operating voltage range around the most recommended 800 V. Fluorescence-free Corion SB-300-F short-pass filters were placed on the PMTs and efficiently removed radiation for wavelengths beyond 320 nm.

The small size of the modules allowed us to achieve a very compact design of the polychromators of the two lidar systems. In particular, side-by-side operation of all three PMTs in the spectrographs of the stationary DIAL became possible. These modules were used in our stationary system for more than 15 years without discernible signs of ageing.

Finally, driven by the hope for further improvement, we replaced the Hamamatsu H5783P-06 modules in 2012 with an actively stabilized version optimized for us in 1999 for our three-wavelength aerosol lidar (Kreipl, 2006) by Romanski Sensors (RSV). This device had to be based on the follow-up PMT version Hamamatsu R7400U-03 because the 5600 series was longer available. The socket was further modified to deliver optimized single-photon spikes without the ringing of the original PMTs (Fig. 9a and b). The power connection cable is shielded, but the shield is grounded just on one side.

Similar to the Hamamatsu module the RSV socket generates a clean reference voltage (5 V). This voltage is produced from the 15 V supply voltage. The 5 V reference, corresponding to a PMT voltage of 1000 V, is then returned to the power supply where it is divided to the adjustable final control voltage level (0 to 5 V) that is sent back to the detector (Fig. 3.12 of Kreipl, 2006). This loop was necessary to clean the lidar signals to a level below $10^{-5}$ of the peak signal. SENDING in just an external control voltage resulted in an unacceptable baseline crossing of about $10^{-4}$ of the peak lidar signal.

The diameter of these detector modules, 50 mm, was too large for operating the PMTs for 277 and 292 nm side by side in the spectrograph of the stationary system. In order to make this possible, RSV delivered four of the modules with the small PMT tubes mounted off-axis.

Testing of the PMTs in our three-wavelength aerosol lidar showed that above peak signals of 40 mV signal-induced nonlinearities become observable that are attributed to photocathode overload (Fig. 3.10 of Kreipl, 2006; English version: http://www.trickl.de/PMT.PDF, last access: 19 November 2020). However, this result was obtained for a PMT supply voltage of the order of just 450 V and therefore corresponded to an excessive photon flux (see Fig. 10 for a gain curve). For voltages around 800 V (maximum: 1000 V), as
Figure 8. Polychromator of the mobile ozone DIAL: the opto-mechanical components were mounted on a rail system attached to a black optical table with a 25 mm × 25 mm hole pattern (M6 threads, not shown). The two green dots mark the intermediate image planes of the primary mirror of the telescope (the secondary image planes coincide with the PMT cathodes). Abbreviations are as follows. A: rectangular aperture with four adjustable black blades; BS1: beam splitter for reflecting 532 or 1064 nm out of the received radiation for aerosol measurements (not implemented); BS2: 1:100 beam splitter for near-field–far-field separation; BS3: dichroic beam splitter with \( T < 4 \% \) for 289 and 299 nm; HR1: high-reflecting mirror (45°); EF: dielectric edge filter, blocking the radiation above 299 nm; NDF: \( T = 10 \% \) neutral density filter; L1: \( f = 100 \) mm lens; L2: \( f = 50 \) mm lens; AL: alignment laser.

Recommended for photon counting, the incident radiation levels for creating the same signal are roughly 100 times lower. As a consequence, much higher signal levels can be afforded, and in recent years we have routinely set the peak signals in the far-field receiver to 70 mV, this being a rather conservative choice. This setting was motivated by the decision to stay within the 100 mV input range of the transient digitizer (Sect. 4.5).

We ascribe this unprecedented performance to the mesh layers of the dynode stages that likely act as electrostatic kinetic energy filters for the electrons. A pulse-height spectrum of one of the PMTs for the recommended operating voltage of 800 V is shown in Fig. 11. This spectrum was derived from a time scan with a 1 GHz digital oscilloscope (Tektronix, DPO 7104). No rise in photon counts towards 0 V pulse height is seen that would indicate signal-induced cathode emission, this result being limited by the chosen trigger level of the scope of \(-1.5 \) mV. It is important to mention that the pulse-height distribution does not end at \(-23 \) mV. As can be concluded from Fig. 9a and b, much higher pulses exist that can reach almost \(-200 \) mV. For 1 h measurements with our Raman lidar (Klanner et al., 2020) we did not ob-
serve dark counts in 7.5 m bins for discriminator thresholds of 4 mV and PMT supply voltages beyond 900 V.

In the far-field receiver we found that a high number of photons is more important than a high peak analogue voltage because the photon noise dominates the signal at large distances. Thus, we no longer attenuate the signals and irradiate the photocathode with all the light emerging from the spectrograph. For compensation we reduce the PMT voltage to about 700 V. Now, the 70 mV signal level corresponds to about 2.5 times more photons per time interval than before. This change has resulted in considerable lowering of the ozone noise for the 292–313 nm wavelength combination in recent years. Photon counting at 700 V, along with the resulting much lower single-photon amplitudes, has not been tested so far (Sect. 4).

A really bad surprise was that the 7400 PMT is more than 1 order of magnitude more susceptible to daylight than the old modules. The H5783P-06 modules stayed linear up to about 12 mV of constant-background analogue signal. Now, the constant signal background must be kept below 1 mV. This task is demanding at 313 nm during the brightest part of

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**Figure 9.** (a) Single-photon pulse from a Hamamatsu 5600 or 7400 PMT, measured with a 500 MHz digital oscilloscope (Tektronix, TDS 3045 C). (b) Single-photon pulse from a Hamamatsu R7400P-03 PMT with the most recent version of the Romanski (RSV) socket, measured with a 1 GHz digital oscilloscope (Tektronix, DPO 7104).

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**Figure 10.** Peak lidar signal measured with an R7400P-03 PMT as a function of the supply high voltage. The measurement was made for different attenuations of the incoming radiation by calibrating the data to the results for the standard settings. Signal-induced nonlinearities were only observed for very high photon fluxes, for which the supply voltage had to be reduced to 450 V to ensure signals below 100 mV (Kreipl, 2006).

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**Figure 11.** Pulse height distribution of a Hamamatsu R7400-03 PMT (RSV module) for 800 V of operating voltage determined from a long time scan with a 1 GHz digital oscilloscope (sign of the pulse amplitudes inverted).
the day, aggravated by the degraded surface of the primary mirror and in the presence of clouds. In spring and summer signal undershoot to below the signal baseline has even been observed during the hours around noon. We added a 5.7 nm (f.w.h.m.) filter from Laseroptik for additional background blocking. Still, mathematical corrections had to be made, which were particularly important for optimum aerosol retrievals. A filter with a 0.5 nm flat top and very steep edges is needed. Additional solutions could be an additional light baffle above the telescope and replacing the aged primary mirror of the telescope.

4.5 Transient digitizers

For the digitization of the analogue signal a 12 bit transient digitizer was found to be sufficient for avoiding the influence of single-bit steps since the shot-to-shot noise is larger than a least significant bit (LSB). This was anticipated by numerical simulations with artificial noise before the 1994–1995 upgrading of the stationary system that demonstrated the absence of steps for a noise amplitude of 4 LSBs. A sawtooth generator built for randomizing the single-bit steps turned out to be unnecessary. By contrast, Langford (1995) reported a significant improvement in his system achieved by modulating the signal.

In the upgraded stationary system, a 12 bit, 20 Hz system from DSP Technology was used until 2003. Since the mobile system was built 1 year later, the first 12 bit, low-noise 20 Hz transient digitizers systems from Licel became available and were used. The performance was excellent with lower noise than in the DSP system. In 2013, the Licel transient digitizers were upgraded at our request by introducing custom-made ground-free input amplifiers. This latest version has led to an unprecedented performance with a relative noise level of about \(10^{-4}\) of the full 100 mV voltage range after minor smoothing (Sect. 7.1), also yielding highly sensitive aerosol measurements at 313 nm despite the short wavelength. This unprecedented performance has made it possible to operate the system without photon counting with very little loss of quality.

Though being much noisier, the DSP Technology system was more linear than that of Licel as resolved down to a level of \(2 \times 10^{-5}\) of the full scale (Kreipl, 2006; Fig. 3.10: http://www.trickl.de/PMT.PDF, last access: 19 November 2020). When firing the laser of our mobile aerosol lidar nearly horizontally onto a rock at a distance of 9 km, where the peak equaled the signal maximum, the return from beyond the rock instantaneously and exactly returned to zero. By contrast, the Licel system yields a small undershoot for distances beyond remote clouds that is larger for larger signal areas. Of course, the performance is perfect in the absence of clouds that generate very pronounced spikes. The performance of the most recent version of the Licel system is discussed further in Sect. 7.1.

4.6 Pre-amplifiers

In order to lift the PMT output, typically around 10 mV for the old PMTs and 70 mV for those from Hamamatsu (into 50 Ω), to the coarsest range of the transient digitizers, adjustable-gain pre-amplifiers were used until 2011 (Analog Modules, model 351, bandwidth 4 MHz, gain-adjustable between 1 and 10). In two of the far-field channels (on wavelengths) these pre-amplifiers produced some very small ringing. Between 1997 and 2003 these problems were overcome by using photon-counting data. For many years of exclusively using analogue data the ringing had to be removed by mathematical corrections. The ringing and the additional noise finally completely disappeared after disconnecting the zero voltage. After introducing the latest (ground-free) version of the Licel input stage the pre-amplifiers were removed.

4.7 Photon counting

In the stationary ozone DIAL single-photon counting was applied between spring 1997 and 2003 with an FDC700 1 GHz photon-counting system from Optec. The signals were fully linear starting in the middle troposphere but produced extra counts at lower altitudes, presumably due to pile-up effects of the PMT ringing (Fig. 9a). The signal for photon counting was separated from the analogue output by an impedance-matched junction containing an adjustable discriminator custom-made by RSV. In the first version the discriminator level could not be reduced to below 11 mV. This level had to be chosen to ensure linear performance and maximum signal (Fig. 11). The unit was upgraded several years ago for picosecond time resolution and discriminator levels down to 2 mV.

The new PMT units delivered by RSV are free of the ringing of the original Hamamatsu tubes (Sect. 4.4) and feature pulse widths of about 1.5 ns (Fig. 10). In order to benefit from this considerable time resolution we recently purchased MCS6 and MCS6A five-channel high-speed photon-counting systems from Fast Comtec for several of our lidar systems. The signals are scanned for selectable pulse edges at intervals of 100 ps, which means a maximum count rate of about 5 GHz for equidistant picosecond pulses. For both reasons a highly linear photon-counting performance was achieved that is presented in detail in the parallel publication on our Raman lidar for water vapour and temperature (Klanner et al., 2020).

The simultaneous analogue and photon-counting measurements from a single PMT lead to a deterioration of the analogue signal with an artificial perturbation of the signal of the order of \(10^{-4}\) of the peak voltage. This could be reduced by 1 order of magnitude by adding an optocoupler to the trigger input of the counting system. However, the shape of the perturbation was somewhat complex and thus difficult to correct mathematically. In addition, we do not have experience with photon counting at the currently preferred PMT voltages of
around 700 V or less (see above). At this time the simultaneous application of photon counting is postponed until a better solution becomes available.

4.8 System control

All connections between electronic components of the two DIAL systems are ground-free. The trigger pulse is derived from a photodiode and subsequently distributed into numerous output channels via optocouplers (Ingenieurbüro W. Funk). The supply voltages for the PMTs, pre-amplifiers, and discriminators (Ingenieurbüro W. Funk) are generated through high-quality DC–DC converters (TRACO POWER, models TYL 05-05S30 and TYL 05-15W05). They are transferred to the different devices in shielded cables. The shields of the cable leading to the PMTs are open on the side of the detectors. The supply voltage can be set by the lidar PC via an I²C bus, but this option has never been used in the stationary system because of the rather stable clean-air conditions at Garmisch-Partenkirchen. Also, the opening and closing of the flap in the roof was initiated via an I²C bus.

Electromagnetic interference from outside (e.g. the laser) has been kept at a negligible level by using doubly shielded signal cables (Suhner, G03332; the outer shield is left open on one side) and ground-free circuits. The trigger pulses were obtained from photodiodes and then distributed via optocouplers.

The firing of the XeCl laser was initiated via RS232 remote control of the computer of the excimer laser. The power for the high-voltage circuits of the laser is supplied by a separate source. The laser PC was connected to the clean power in the lidar laboratory. The laser itself is controlled by its computer via optical fibres. Finally, both cables connecting the lidar laboratory and the laser PC are shielded, which successfully removed any interference from the high-voltage pulses (Eisele and Trickl, 1997).

4.9 Automatic operation

Both DIAL systems have been extensively operated under automatic control by the lidar PC. In the mobile system an external start and warm-up of the laser was not possible due to issues in the programmes delivered by Continuum. The laser output was continuously controlled: the measurements were interrupted if the 1064 and 266 nm power levels were below maximum.

Among the various error conditions the most important ones are rain and high wind speed. This results in an immediate closing of the flap in the roof. As to the KrF laser the high-voltage is shut down, and as to the Nd:YAG laser the output shutter is closed, with the laser continuing to fire in order to maintain thermal equilibrium of the frequency-doubling crystals.

Time series under automatic control have been extended for the stationary system to up to 4 d. In this way, numerous atmospheric transport studies could be made, with the first 4 d series leading to the first detection of North American ozone over Europe (Eisele et al., 1999; Trickl et al., 2003).

5 Data processing

The number density of ozone, \(n_{O_3}\), is obtained by computing the DIAL equation,

\[
n_{O_3}(r) = -\frac{1}{2\Delta\sigma} \frac{d}{dr} \ln \left( \frac{P(\lambda_1, r)}{P(\lambda_2, r)} \right) + \frac{1}{2\Delta\sigma} \frac{d}{dr} \ln \left( \frac{\beta(\lambda_1, r)}{\beta(\lambda_2, r)} \right) - \frac{1}{\Delta\sigma} \left( \alpha_r(\lambda_1, r) - \alpha_r(\lambda_2, r) \right),
\]

with the difference

\[
\Delta\sigma = \sigma_{O_3}(\lambda_1) - \sigma_{O_3}(\lambda_2)
\]

of the absorption cross sections of ozone. \(P\) is the power returning from the atmosphere (“lidar signal”), \(\beta\) the total backscatter coefficient, and \(\alpha_r\) the residual extinction coefficient that includes Rayleigh and particle scattering as well as absorption by molecules other than ozone. In the absence of aerosols and interfering gas Eq. (1) reduces to

\[
n_{O_3}(r) = -\frac{1}{\Delta\sigma} \frac{d}{dr} \ln \left( \frac{P(\lambda_1, r)}{P(\lambda_2, r)} \right) + \left( \alpha_R(\lambda_1, r) - \alpha_R(\lambda_2, r) \right),
\]

with the subscript R denoting “Rayleigh”. The Rayleigh extinction coefficients can be calculated in the ultraviolet spectral region with relative uncertainties less than 1 % if radiosonde data are used for deriving the atmospheric density. For short on wavelengths (266 nm, 277 nm) the absorption of aerosols and interfering gas Eq. (2) is a mostly reasonable approximation.

Under the clean-air conditions prevailing at Garmisch-Partenkirchen Eq. (2) is a mostly reasonable approximation. However, occasionally aerosol corrections must be made. Due to the large wavelength separation in UV ozone DIALs, the inference by aerosols may contribute more seriously than in DIAL systems measuring species with a well-resolved line structure allowing the use of neighbouring wavelengths. Operational procedures based on an iterative parameter search were developed that are described in detail in our preceding publication (Eisele and Trickl, 2005). For calculating ozone in the presence of structured aerosol distributions the lowest errors have been obtained for the wavelength pair 277–292 nm, followed by 277–313 nm and 292–313 nm. The most important factor is a strong absorption cross section of ozone and then a minimum (but finite) wavelength difference (Völger et al., 1996; Eisele and Trickl, 2005), in contrast to a frequently heard, but obviously wrong, opinion.

Our numerical approach was significantly modified with respect to that published earlier (Kempfer et al., 1994). Previously, the derivatives in the DIAL equation were calculated...
by fitting third-order polynomials to the backscatter profiles within a given evaluation interval. This method worked rather well but was slow. A faster modified approach resulted in small steps in the generated ozone profiles, requiring the application of some moderate data smoothing in addition (Kempfer et al., 1994).

From the point of view of numerical filter theory polynomials are not ideal because their transfer functions expose ringing. We decided to calculate the derivative with a simple linear least-squares fit of just a short interval, keeping the vertical resolution (see further below) at about 50 m, followed by optimized numerical filtering. A five-step algorithm is applied, consisting of

1. data pre-smoothing at a level roughly corresponding to the chosen minimum vertical resolution of 50 m (important for smooth aerosol retrievals for the near-field telescope),
2. calculation of the derivative with a constant number of data points in a sliding interval,
3. range-dependent data smoothing with a vertical resolution of about 50 m at low altitudes and 250 to 500 m in the tropopause region, depending on the noise level of the respective measurement,
4. truncation of the uppermost ozone profiles at an altitude below the onset of diverging noise, in summer sometimes even below the tropopause, and
5. final minor smoothing of the composite ozone profile put together from the best segments of the partial ozone profiles from different wavelength combinations and the two telescopes.

The smoothing intervals in step 3 have been mostly minimized in order not to suppress existing ozone structures.

For a linear fit and equidistant data points the result of the fits may be expressed in a rather simple formula, resulting in the following solution of the DIAL equation for the i-th data point (Vogelmann and Trickl, 2008). Selecting a fit interval between data point \( i - k \) and \( i + k \), one obtains

\[
\frac{d}{dr} \ln q_i \approx \frac{3}{\Delta r} \sum_{j=-k}^{i+k} \frac{(j-i)q_j}{q_i > \Delta r \, k(k+1)(2k+1)}.
\]

with the signal ratio

\[
q_i = \frac{P(\lambda_{off}, r_i)}{P(\lambda_{on}, r_i)} \quad \text{and} \quad \frac{1}{2} \sum_{j=-k}^{i+k} q_j \left( \begin{array}{c}
\sum_{j=-k}^{i+k} q_j \\
2k + 1
\end{array} \right)
\]

with \( \Delta r \) being the size of the range bin of the transient digitizer or photon-counting system. Application of Eq. (3) allows a fast computation of the derivative, in particular for constant \( k \), when only the sum in the numerator must be calculated for each step. In Eq. (3) \( < q_i > \) is written instead of \( q_i \) as by Vogelmann and Trickl (2008). This is explained further below.

Another important advantage of Eq. (3) is that the least-squares fit is not applied to the logarithm, but to the signal ratio itself, due to the transformation

\[
\frac{d}{dr} \ln q_i = q_i^{-1} \frac{d}{dr} q_i.
\]

In contrast to the noise of the logarithm of \( q_i \) the noise of the signal ratio is symmetrical and fulfills a key prerequisite of least-squares fitting. A negative density ozone bias is therefore avoided.

However, the application of Eq. (3) has limitations. Its application to simulated lidar profiles revealed that there are numerical biases with growing interval sizes \( 2k \). This is further discussed below.

The linear approach in Eq. (3) is reasonable for interval sizes \( L = 2k \Delta r \) not exceeding a scale representing the ozone distribution. Equation (3) is a reasonable choice for data smoothing, but it is not a perfect frequency filter and transmits residual high-frequency noise. Therefore, we have used a combination of Eq. (3) in a limited interval and numerical low-pass filtering.

Numerical low-pass filtering of data points \( y_i \) is based on the general equation (Eisele, 1997, and references therein)

\[
y_i' = \sum_{j=-k}^{i+k} a_j y_{i-j},
\]

with the smoothed value \( y_i' \) and the coefficients

\[
a_j = a_{-j} = N \frac{\sin(2\pi j \cdot f_c f_s^{-1})}{j \pi},
\]

with \( f_c \) and \( f_s \) being the cut-off and sampling frequencies, respectively, and \( N \) a normalization factor. The interval width is \( L = 2k \Delta r = 2k c f_s^{-1} \). One general problem with numerical low-pass filtering is the occurrence of ringing. This can be minimized by introducing window functions \( w_j \),

\[
y_i' = \sum_{j=-k}^{k} a_j w_j y_{i-j}.
\]

After comparing several listed window functions a Blackman-type window (Blackman and Tukey, 1959) was chosen:

\[
w_j = 0.42 + 0.50 \cos \left( \frac{\pi j}{k} \right) + 0.08 \cos \left( \frac{2\pi j}{k} \right).
\]

The best performance was achieved by selecting

\[
f_c = \frac{f_s}{2k} = \frac{c}{2k \delta r}.
\]
with \( c \) being the speed of light. The response function obtained for applying Eqs. (5)–(7) with \( k = 25 \) is depicted in Fig. 12 together with that for a sliding arithmetic mean over \( 2k + 1 = 51 \) symmetrically arranged data points. A linear least-squares fit is equivalent to the arithmetic mean. These linear operations, though suitable for smoothing, are not perfect frequency filters and therefore transmit residual high-frequency noise. More details on the frequency transfer functions for some filters are given by Eisele (1997) and, more recently, by Iarlori et al. (2015) and Leblanc et al. (2016).

The vertical resolution can be defined in a number of ways (Iarlori et al., 2015; Leblanc et al., 2016). For practical reasons the German Engineering Society (Verein Deutscher Ingenieure, VDI, 1999) introduced a definition of the range resolution as the interval between 25 % and 75 % of the rise in the response to a Heaviside step (Fig. 12). Here, the response reaches a signal level of 100 % at large distances from the step. Since the VDI guideline was published we have preferred to apply this definition. In spectroscopy, the spectral resolution is preferentially defined as the full-width at half-maximum of the response to a delta peak. As we can see in Fig. 12, without normalization the delta response is much smaller than the original one, which looks strange in practice.

From Fig. 12 we derive for the Blackman filter a VDI vertical resolution of 19.2 % of the full filtering interval \( L \). The response of the Blackman filter to a single-channel (“delta”) peak (5 \( \times 10^{17} \) m\(^{-3} \) to 1 \( \times 10^{18} \) m\(^{-3} \)) was found to exhibit a full-width at half-maximum of 34.3 % of \( L \) (Fig. 12). This fraction looks surprisingly large in comparison with the step response. The fractions for the pure Blackman filter (Eqs. 5, 6) are also valid for much smaller smoothing intervals than in this example.

We also give in Fig. 3 an example for numerical differentiation of a simulated lidar measurement based on Eq. (3). The DIAL equation was synthesized for the wavelength pair 277–313 nm based on the artificial ozone density step between bins 999 and 1000 and on an air density profile calculated from the U.S. Standard Atmosphere (1976). The absence of particles and absorbing molecules other than ozone was assumed. The application of Eq. (3) yields a similar step (Fig. 3) that matches that for the Blackman filter within most of the rise if one selects \( k = 27 \). In contrast to an ideal filter the derivative filter transmits some residual noise. The VDI vertical resolution is about 45 % of the filtering interval (\( k = 10 \) to 30, presumably in a wider \( k \) range).

It is important to note that due to the curvature of the backscatter profiles Eq. (3) yields a bias that is absent in the case of missing Rayleigh scattering. This bias grows with \( k \) and is negative for Eq. (3) (for \( k = 27: -0.0050 \times 10^{17} \) m\(^{-3} \) (−0.10 %) ahead of the step and −0.0033 \( \times 10^{18} \) m\(^{-3} \) (−0.33 %) behind it). This bias is small, and it even becomes negligible for e.g. \( k = 10 \) (and less). However, it grows with \( k \). Thus, it is reasonable to use moderate values of \( k \) for the derivative and subsequent numerical filtering with Eqs. (5) and (6) to remove the residual noise. Finally, the use of \( q_i \) instead on \( < q_i > \) in the denominator of Eq. (3) yields a positive bias larger than the negative one for using Eq. (3). This justifies the choice of \( < q_i > \). One could think about an empirical mathematical correction interpolating between \( q_i \) and \( < q_i > \).

The filter interval for the smoothing is dynamically enhanced with height by applying a linear relation for simplicity (a quadratic dependence might be better). The coefficients \( c_1 \) and \( c_2 \) are preselected for each wavelength pair:

\[
k = c_1 + c_2 \cdot i \text{ for bin } i.
\]  

For example, for the large telescope of the stationary lidar \( c_1 = 0 \) ad \( c_2 = 0.125 \) for the pair 277–313 nm and \( c_1 = 0 \) and \( c_2 = 0.156 \) for 292–313 nm. This results in filtering intervals 2 \( k \) of the order of 250 and 500 near the upper end of the respective useful range (VDI vertical resolutions of 360 and 720 m, respectively). These preset coefficients are used for the initially automatically produced set of quick-look profiles but are afterwards reduced in size in some subranges if allowed by the noise level. In ranges with clearly distinguishable ozone gradients (e.g. stratospheric intrusion peaks or tropopause) or strong narrow features, the vertical resolution is also reduced as far as reasonable. In particularly noisy subranges in the upper troposphere sometimes homogeneously distributed ozone is fitted to the corresponding density seg-
ments. The different segments are pasted into the actual overall ozone profile.

As a consequence of this complexity, a solution for automatically deriving uncertainties for all partial data segments has been postponed. In the early 1990s uncertainties for the much less sophisticated evaluation procedure was calculated from the least-squares fitting approach applied (Kempfer, 1992).

The calculation of mixing ratios and the retrieval of aerosol backscatter coefficients require knowledge of the atmospheric density. Within the troposphere this is not extremely important and simple annual average density profiles do not contribute more than a few percent to uncertainty (Carnuth et al., 2002). However, with growing data quality and a range reaching the stratosphere the incorporation of a better density profile became mandatory. This is achieved by importing the radiosonde data for the nearest station of the German Weather Service, Munich or Stuttgart, from the University of Wyoming database (http://weather.uwyo.edu/upperair/sounding.html, last access: 19 November 2020).

313 nm aerosol backscatter coefficients have been routinely calculated for each measurement since 2007 based on the methods mentioned above (Eisele and Trickl, 2005). They are publicly available for all years starting in 2007 from the EARLINET database (https://data.earlinet.org/, last access: 19 November 2020).

The quality of the aerosol backscatter coefficients for the latest period of lidar operation is extremely high during most of the day, as can be seen in Trickl et al. (2015) and in Sect. 7.1. This has served as an additional quality criterion for the ozone retrieval, together with the comparison of the DIAL profiles for different wavelength combinations and the single-wavelength ozone retrieval for 292 nm. In the absence of aerosol this single channel is extremely reliable and, in summer, less noisy than the DIAL solution for 292–313 nm. However, the Rayleigh backscatter coefficients must be calculated from radiosonde data in order to achieve good quality.

After the introduction of the 7400 PMTs, a slight correction of the far-field 313 nm profiles became necessary during the hours around noon (Sect. 4.4). The overshoot of the normally negative signal is particularly pronounced in summer due to the PMT overload effects in the presence of a daylight background exceeding 1 mV. Aerosol retrievals are mostly perfect during nighttime; just a constant displacement of the order of 10⁻⁷ m⁻¹ sr⁻¹ must be corrected. As the 313 nm PMT starts to exhibit overshoot for large distances, a mathematical correction becomes necessary, in summer even before 10:00 CET. In the absence of aerosol in the upper troposphere and the lower stratosphere the corrections can be nicely verified by comparing the DIAL ozone with the 292 nm single-signal ozone retrieval.

6 System validation and measurements

6.1 Calibration

Since the first measurement series in 1991 the ozone data have been calibrated by using the absorption cross sections from the University of Reims (Daumont et al., 1992; Malicet et al., 1995). The motivation for this is described by Kempfer et al. (1994). Most importantly, the measurements account for the decomposition of ozone during the absorption measurements by precise pressure measurements. The cross sections have measured again and again (e.g. Gorshelev et al., 2014; Serdyuchenko et al., 2014, and references therein), but no improvement has been achieved, except for perhaps the temperature dependence. Very recently, four new cross sections measured between 244 and 254 nm at an uncertainty level of 0.1% have been provided by Viallon et al. (2015). In view of the choice for our ozone DIALs it is extremely satisfactory that the agreement with the corresponding values in the Reims data is within ±0.06%.

The temperature dependence as a function of altitude is obtained by interpolation of the cross sections from Reims measured for different temperatures.

6.2 Validation

For the convenience of data users, the system performance is summarized in Table 4 for the different periods of operation. The uncertainties have been derived from validation exercises, sensitivity studies in low-signal ranges, and noise estimates and reproducibility of the ozone densities during diurnal series of measurements.

The lidar system has been systematically validated (since 2007 on each sounding day) by using the in situ data from the nearby mountain stations Wank (1780 m a.s.l.) and Zugspitze (2962 m a.s.l.) until the measurements at these sites were discontinued (evaluated data are available until 2010). Afterwards, the ozone values of the Schneefernerhaus (UFS) Global Atmosphere Watch station have been used for occasional comparisons (Trickl et al., 2014, 2020). UFS is located on the southern face of Zugspitze at a distance of 9 km from the ozone DIAL at IFU. The gas inlet is at 2670 m. The average ozone mixing ratios are about 1% lower than those at the summit (Ludwig Ries, personal communication). The lidar data agree similarly well with those from UFS as previously with the Zugspitze ozone.

In addition, a large number of successful comparisons have been made with the Hohenpeißenberg ozonesondes (distance: 38 km); a few examples were given by Eisele et al. (1999). A more extensive comparison is planned for the 2018 data, accompanied by a highly successful comparison with a sonde launched by colleagues from Jülich directly at IMK-IFU in February 2019. The latter side-by-side comparison for mixing ratios of about 50 ppb yielded a rather con-
stant bias of the sonde of 2 to 3 ppb up to 7 km and, above this, a slightly higher variability of the differences.

These comparisons have certain limitations. In the case of the Hohenpeißenberg sondes the air-mass difference matters in certain altitude ranges due to a 48 km distance between the two stations. Under comparable conditions the differences between the profiles have been between 5 % and 10 %.

The lidar has shown a slightly positive bias with respect to the Wank site, mostly not exceeding 5 ppb. This bias is not present during night-time but mostly forms in the morning under warm conditions. It has therefore been ascribed mostly to slope winds (Carnuth and Trickl, 2000, Fig. 5) venting morning-type low-ozone air from the valley up this rather isolated summit that acts like a chimney. Frequently the summertime morning values agree better with the 05:00 CET measurement than with the Wank mixing ratio for the true data acquisition time. Until 2011 some alignment issues occasionally exist that enhanced the uncertainty for distances below 0.5 km. The Wank site has been invaluable for verifying good alignment of the near-field telescope, until 2011 with some resulting problems.

The comparisons with the Zugspitze in situ data have been mostly very convenient. The differences of the mixing ratio have rarely exceeded 2 ppb, with exceptions typically occurring if there is a pronounced ozone gradient around 3000 m. In the absence of an extended comparison since 2012 an example from a 4 d series in May 1999 (Trickl et al., 2003, 2011) is shown in Fig. 13 that exhibits more noise than recent comparisons. The data are compared for two lidar altitudes, 2970 and 2786 m. The lower altitude accounts for the air-mass rise during the final approach towards the high mountain. The results for 2970 m show a few positive departures that result in a positive average difference between the lidar and station of 0.82 ppb (standard deviation: 2.15 ppb). For the lower altitude the “bias” is just 0.34 ppb (standard deviation: 1.61 ppb). These values are all small in comparison with the average Zugspitze mixing ratio, but the sign agrees with the expectation for the 1.8 % bias of the in situ measurements obtained in the recent cross-sectional study by Viallon et al. (2015).

The performance of the mobile system is discussed in Sect. 5.5.

6.3 Interference by other gases

Important species absorbing in the typical wavelength range of ozone DIAL systems are SO$_2$, NO$_2$, and some hydrocarbons. Under the clean-air conditions prevailing at the Alpine site Garmisch-Partenkirchen and in the free troposphere, spectral interference from these constituents should be very rare. As mentioned, the mobile DIAL retrievals for the wavelength pair 266–299 nm are almost insensitive with respect to SO$_2$ and NO$_2$.

Oxygen must also be considered in the wavelength region below 285.66 nm (Krupenie, 1972; Jeunouvrier et al., 1999). The absorption cross sections of O$_2$ in this region (Herzberg bands) are rather low, but absorption cannot be completely neglected due to the high concentration of this molecule. We found some approximate coincidences with non-relevant high rotational levels and an approximate coincidence of the 277.11 nm emission with $J = 5–7$ components of the extremely weak $A' \rightarrow X$ (2.0) band. 266.12 nm is slightly outside a group of O$_2$ lines. In summary, absorption of the emissions used in the two DIAL systems in oxygen can be neglected, in agreement with the good validation results.

7 Measurements

7.1 Examples for the stationary system

After the first upgrading of the stationary DIAL in 1994 and 1995, the system yielded greatly improved sensitivity and a much larger vertical range up to about 15 km due to the three-wavelength operation. The number of measurements per year grew and time series under automatic control were extended up to 4 d, the first 4 d series being the well-documented one in May 1996 published by Eisele et al. (1999), Stohl et al. (2000), Cristofanelli et al. (2003), and Trickl et al. (2003). However, until 2003 the operation was limited to funded projects and focused research topics. After the second major system upgrading routine measurements were started in 2007. Almost 5000 ozone profiles were obtained from 1991 to February 2019, and numerous examples can be found in our publications (see the Appendix; the most recent one for the period 2007 to 2016 can be found in Trickl et al., 2020).

A summary of the work done is given in Table 3. Uncertainties estimated for the different periods and altitude ranges are specified in Table 4 as a guide for potential data users.
The ozone hump between 3.0 and 4.7 km is caused by a very dry layer (1% minimum relative humidity at 4.2 km for the Munich radiosonde, roughly 100 km to the north; 1% is an artificial cut-off in the listings for the RS92 radiosonde; Trickl et al., 2014). 315h backward trajectories calculated with the HYSPLIT model (Draxler and Hess, 1998; http://ready.arl.noaa.gov/HYSPLIT_traj.php, last access: 19 November 2020), selecting reanalysis meteorological data, suggest a long-range descent from the stratosphere over western Canada. The Munich thermal tropopause for both standard launch times is significantly higher than the onset of the ozone rise. It is well-known, also from our measurements, that the thermal tropopause does not perfectly coincide with the onset of the ozone rise (Hoerling et al., 1991; Pan et al., 2004).

In general, as pointed out in Sect. 4.2, the near-field receiver yields reasonable ozone typically up to at least 2 km above the ground (2.74 km a.s.l.). The quality is limited due to the rapid drop of the backscatter signal. The useful range for 277 nm of the far-field receiver is 6.5 to 8 km in winter (40 to 50 ppb). 292 nm is rarely used in the lower troposphere because of the lower sensitivity for ozone and the stronger sensitivity to aerosol (Eisele and Trickl, 2005). However, the 277–292 nm profiles are preferred in the presence of pro...
Table 3. Measurement periods of the stationary DIAL.

| Period          | Measurements                                                                 | Comments                                      |
|-----------------|------------------------------------------------------------------------------|-----------------------------------------------|
| Jan–Dec 1991    | 580 measurements (just about 60 within TOR re-evaluated)                     |                                               |
| 1993            | a few measurements                                                           | within TOR                                    |
| Jan 1996–Feb 1998 | 1122 evaluated measurements                                            | within VOTALP 1 + 2                           |
| May 1999        | 86 evaluated measurements                                                   | within VOTALP 2                               |
| Aug 2000–Aug 2001 | 520 evaluated measurements                                            | within STACCATO                                |
| Jul 2003        | 37 evaluated measurements                                                   | within ATMOMFAST                               |
| 2007–2018       | 2959 evaluated measurements                                                | routine measurements; gaps due to repairs    |

* Kley et al., 1997, b Wotava and Kromp-Kolb, 2000; VOTALP II, 2000, c Stohl et al., 2003, d ATMOMFAST, 2005.

Table 4. Uncertainties of the stationary ozone lidar.

| Altitudes: above sea level (a.s.l.); E: EMI PMTs, H: Hamamatsu PMTs | Period           | 1–2.3 km | 2.3–5 km | 5–8 km | 8 km to tropopause | Electronics |
|-------------------------------------------------------------------|-----------------|----------|----------|--------|-------------------|-------------|
|                                                                  | 1991–1993       | 5 ppb    | 2–4 ppb  | 4–8 ppb | not reached       | 8 bit DSP, E |
|                                                                  | 1996–Apr 1996   | 5 ppb    | 2–4 ppb  | 4–8 ppb | up to 10 ppb (winter) up to 20 ppb (summer) | 12 bit DSP, E |
|                                                                  | May 1996–Apr 1997 | 5 ppb    | 2–4 ppb  | 4–8 ppb | unknown*          | 12 bit DSP, H |
|                                                                  | May 1997–2003   | 5 ppb    | 2–4 ppb  | 4–8 ppb | best: 7 ppb; up to 10 ppb (winter) best: 7–10 ppb; up to 20 ppb (summer) | 1 Ghz Optec |
|                                                                  | 2007–2011       | 5 ppb    | 2.5–4 ppb| 3–7 ppb | best: 7 ppb; up to 10 ppb (winter) best: 7–10 ppb; up to 20 ppb (summer) | 12 bit Licel, H |
|                                                                  | 2012–2019       | 2–4 ppb  | 1.5–4 ppb| 3–7 ppb | best: 5 ppb; up to 8 ppb (winter) best: 5–8 ppb; up to 15 ppb (summer) | 12 bit Licel, H |

* Sometimes there are artefacts in the upper troposphere due to pre-amplifier ringing, which are corrected for important examples.

nounced aerosol structures because of a less critical aerosol correction. The typical range for 292 nm is roughly 3 km above the tropopause, which can vary with the slope of ozone rise. In summer, when ozone in the free troposphere can exceed 100 ppb, sometimes the range is limited to 10 to 11 km and the seasonally higher tropopause is not reached due to the strong loss of radiation.

Due to the short measurement time of just 41 s the reproducibility of the data can be easily verified. In Fig. 16 we show the profiles for three measurements under complex conditions (Saharan dust up to 4 km and a stratospheric air intrusion around 5.7 km) obtained within less than 3 min on 18 June 2013. The intrusion originated at 10 km or more higher the United States at least 13 d backward in time (Trickl et al., 2020). The layer descended to southern Spain and then turned north-eastward towards the Alps, slightly rising. Due to the long travel the minimum relative humidity was as high as 6 %, as measured by both our water vapour DIAL and the Munich radiosonde (Trickl et al., 2020).

Due to elevated ozone mixing ratios (50 to 80 ppb) the radiation loss results in an increase in the short-term variability of the ozone profiles in the upper troposphere, which indicates a level of uncertainty of about ±10 ppb. The noise
Figure 15. Selection of partial ozone profiles from both receivers of the stationary system: the near-field result can be used here to more than 2 km above the lidar due to low ozone density. The ozone hump between about 3.0 and 4.8 km is caused by a remote stratospheric air intrusion. The lidar measurement agrees with that at the nearby Schneefernerhaus station (UFS, 2670 m; 0.7 ppb below blue curve). The altitude of the tropopause is taken from the Munich radiosonde.

Figure 16. Example for reproducibility testing during a period of elevated ozone: the on wavelengths used are 277 nm (channel 1, near-field telescope, up to 2.23 km), 277 nm (channel 6, up to about 6 km), and 292 nm (channel 5, up to the top). The lidar measurement perfectly agrees with that at UFS if the altitude is shifted to that of the Zugspitze summit (2962 m), justified by the southerly advection. Above 5 km the signal in channel 6 becomes low due to the high ozone values in the lower troposphere, and a weighted average of the 277–292 nm ozone profile with that for 292–313 nm was applied for the final few hundred metres below 6 km. Above 9 km the 292 nm signal starts to become noisy, resulting in reduced reproducibility. The altitude of the tropopause is taken from the Munich radiosonde.
Figure 17. Ozone measurement with the stationary DIAL on 13 February 2014; the variability is low apart from the two dry layers at below 4 km and at 6.1 km that are also visible in the 01:00 CET Munich radiosonde data and that seem to erode after 08:35 CET. The agreement with the in situ measurements at UFS is perfect.

Figure 18. 313 nm aerosol backscatter coefficients for 12 June 2015.

Figure 19. Ozone measurement with the mobile DIAL during the brightest part of the day, after all modifications had been made (about 10^4 laser shots); the vertical axis is the height above the lidar site (IFU, 730 m a.s.l.), and up to 2.7 km above the ground 266–299 nm wavelength pairs were taken (near-field: up to 1.5 km). Up to 3.7 km the combination 289–299 nm was used. Above this, ozone was obtained from a single-trace evaluation for 299 nm, slightly recalibrated at the lower end of that range. For comparison, in situ ozone values from the three local monitoring stations IFU (745 m a.s.l.), Wank (1780 m a.s.l.), and Zugspitze (2962 m a.s.l.) are shown for 11:30 CET (red squares). Additional values from these stations are marked with open circles for 05:00 CET, 09:30 CET, 14:00 CET, and 17:00 CET (labelled in some cases). For the interpretation of the complicated meteorological situation, the corresponding relative humidity of the Zugspitze summit and the noon operational ascent of the Munich radiosonde are also included. Outside the most reliable part of the operating range a few representative error bars are drawn.

Starting in late 2012, the aerosol backscatter coefficients were archived in the EARLINET database, mostly with a delay of less than 1 d after the measurements.

7.2 Examples for the mobile system

7.2.1 29 April 1999

The final performance of the mobile system was achieved shortly before its destruction in late May 1999 (Fig. 19). It turned out that a daylight signal background of more than 12 mV was present in the 299 nm channel, which lead to signal distortion (Sect. 4.4). Due to inserting a 300 nm cut-off filter, bridging the gap to the 320 nm edge of the Corion filter, the 299 nm channels became linear and the planned operating range of the DIAL of 4 km could be reached. As mentioned, further range extension would be possible if a rotating attenuator could be used for 299 nm to get roughly equal maxi-
mum far-field returns for 289 and 299 nm. Below a distance \( r \) of 2.7 km, 266–299 nm pairs were taken.

In the example in Fig. 19 the range could be extended to a distance \( r = 8.3 \text{ km} \) (9.0 km a.s.l.) by evaluating ozone from the much stronger (less noisy) 299 nm signal alone. A slight adjustment of that partial profile had to be made based on the DIAL results for lower altitudes, which resulted in elevated uncertainties. As can be seen from the edges of the isolated structures, smoothing over several hundred metres was applied here.

The validation is based just on comparisons with the in situ measurements at the three local stations operated by IFU. The small deviations from the 11:30 CET Wank and Zugspitze in situ data also shown in the figure suggest an uncertainty of 2 ppb in this altitude range. For the higher altitudes a comparison is missing because the measurement was made on a Thursday, too early for the Friday morning Hohenpeißenberg ozonesonde ascent.

As can be concluded from the rich structure of the ozone profile and the pronounced ozone changes in the in situ data (in Fig. 19 we select the data for 05:00, 09:30, 11:30, 14:00, and 17:00 CET), the meteorological situation was complex. The situation was characterized by prefrontal advection of North American air via Algeria at most altitudes, where the minimum altitude of about 1.5 km was reached. Up to \( r = 3.5 \text{ km} \) the ozone profile is difficult to interpret. The ozone peak between 2.5 and 3.0 km is not necessarily caused by a subsiding stratospheric air intrusion: the relative humidity (RH) at the Zugspitze summit rose from 38% to 66% until 17:00 CET, when the Zugspitze ozone reached the mixing ratio of the 11:30 peak above the summit. Subsidence is not very likely under prefrontal conditions anyway (Trickl et al., 2020). Also, contributions from northern Italy could have been picked up.

Above 3.5 km we clearly see a pronounced stratospheric intrusion layer. This view is supported by the very high peak ozone of 113 ppb, the minimum RH of 1% in the 13:00 CET ascent of the Munich radiosonde, and HYSPLIT backward trajectories. The HYSPLIT trajectories revealed descent over more than 10 d from the north-western part of North America or beyond.

The low upper-tropospheric ozone values are in agreement with the calculated source region 2 km above the Pacific south of Hawaii. Directly above the remote Pacific almost zero ozone has been found (Kley et al., 1996), which justifies the assumption of 20–30 ppb 2 km above the surface.

### 7.2.2 Milano field campaign

The second example is chosen from the VOTALP II (Vertical Ozone Transport in the Alps) Milano field campaign in 1998, in a joint effort together with the PIPAPO (Pianura Padana Produzione di Ozono) air-quality campaign around Milano (Italy) (more details on the measurements: Trickl, 2010b). The mobile ozone DIAL was operated at Barni (Provincia di Como) within the first mountain range of the Alps, about 40 km north of Milano between 1 and 5 June 1998. On the first 4 d a day-by-day increase in the afternoon peak ozone advected from the Milano metropolitan area to Barni by the daytime up-valley wind was observed. During each night the \( \text{O}_3 \) mixing ratio dropped to roughly 60 ppb due to the reversal of the orographic wind direction.

Figure 20 shows the situation for the day with the highest ozone values, 4 June. The behaviour of the ozone rise was surprisingly similar to that on the previous days, including the bimodal profile at 13:36 CET (Central European Time = UTC +1 h). In the late afternoon 120 ppb of ozone was reached, exactly verified by side-by-side measurements with ozonesondes launched by a team from the Swiss Paul-Scherrer Institute. This high mixing ratio turned out to be the very limit for retaining an overlap between the near-field and the far-field 266 nm “on” detection channels for the chosen position of the far-field apertures (blades) and PMT settings. The comparison of the DIAL and the sonde measurements also indicates some air-mass lifting towards the main part of the lake since the boundary layer height (defined here by elevated ozone) grew as the sonde drifted northward during its ascent. It is interesting to note that the 19:10 CET DIAL profile next to the ground would agree with the sonde profiles for some average position of the two sonde maxima.
8 Discussion and conclusions

Differential-absorption lidar systems for trace-gas measurements have proved to be an invaluable tool for atmospheric studies (Trickl, 2010b). Despite this fact the application of DIAL systems is rather limited, in particular combined approaches. Despite promising developments in Europe within TESLAS in the early 1990s no continental-scale ozone lidar network could be established. Ozone measurements have been mostly limited to Haute Provence (Gaudel et al., 2015; Tarasick et al., 2019), Garmisch-Partenkirchen, and Athens (Kalobakas et al., 2012; Mytilinaios et al., 2018). By contrast, the ozone lidar network TolNET was implemented in North America (Newchurch et al., 2016).

At IMK-IFU (Garmisch-Partenkirchen, Germany) three DIAL systems have been developed since 1988, two for ozone and one for water vapour (Vogelmann and Trickl, 2008). The ozone systems were used for a large number of focused investigations until 2003 (e.g. Carnuth et al., 2002; Eisele et al., 1999; Stohl and Trickl, 1999; Trickl, 2003; Trickl et al., 2003, 2010, 2011). The stationary ozone and water vapour lidars have been used for routine measurements since 2007 (e.g. Trickl et al., 2014, 2015, 2016, 2020). The measurements with the stationary ozone DIAL have yielded a total of almost 5000 evaluated ozone profiles since 1991. In the absence of interruptions in the measurement programme, the typical annual number of evaluated measurements has been of the order of 500. This number will grow with further increasing reliability of the automatically produced quick-look ozone and 313 nm aerosol profiles due to a diminishing requirement for manual optimization. Manual corrections are still required in the presence of high ozone levels due to the residual daytime issues at 313 nm and in the presence of pronounced aerosol and cloud structures.

In the course of 3 decades of ozone DIAL development at IMK-IFU we have gradually optimized the technology to a state in which even small variations in tropospheric ozone can be sensed with a high level of credibility. A full restriction to analogue data acquisition is possible due to the large dynamic range of the 5600 and 7400 Hamamatsu PMTs. Automatic operation was introduced in 1996 (for both systems), although it has been limited to clear-weather situations. Thus, the largest effort has been devoted to data evaluation. The results of automatic data evaluation have rarely been directly adopted and careful manual corrections have been made. These corrections include the selection of the best partial profiles based on comparisons and optimizing the vertical resolution in relation to the changing signal-to-noise ratio or when zooming into interesting ozone features. As a consequence of the excellent data quality the full use of automatic data evaluation is now coming within reach, at least under conditions of low to moderate aerosol.

The quality of the retrieved 313 nm aerosol backscatter coefficients almost matches that traditionally obtained in the green spectral region. Baseline corrections are needed during daytime due to signal distortions caused by the high daylight sensitivity of the 7400 PMTs. Spectral filtering must be improved. Perhaps one of the old 5400 PMTs must return to the far-field 313 nm channel.

Quite a number of lessons have been learnt.

– Three-wavelength operation is mandatory: it provides a wide vertical range and internal quality assurance; the aerosol retrieval yields an additional quality control of the 313 nm backscatter profiles.

– Use of at least one short on wavelength below 280 nm is an important base for high accuracy and for a low to moderate level of interference by aerosols that can be readily corrected for. Even for 266 nm a range up to about \( r = 2.5 \) km above the lidar was demonstrated.

– A short measurement time of 41 s was achieved with the stationary system, whereas for the mobile system about 10 min were necessary. This longer signal accumulation is in part due to the slower repetition rate of 15 Hz per wavelength for the longer wavelengths and also in part to the strong signal decay for 266 nm (30 Hz repetition rate) that necessitates longer averaging to achieve a reasonable signal-to-noise ratio at larger distances. For the stationary system, longer averaging (e.g. 5 min) will yield better results in the upper troposphere in summer. In principle, the free-tropospheric capability (i.e. without significant amounts of aerosol) can be driven close to the uncertainty limit set by the absorption cross sections.

– Current-day transient digitizers make single-photon counting in an ozone DIAL almost superfluous, except for very long measurements in a dark environment.

– Simultaneous analogue and PC counting out of a single PMT is possible but has so far led to a deterioration of the analogue signal that cannot easily be corrected mathematically (see Klandner et al., 2020). Single-photon counting will be resumed if the residual signal distortions can be removed. However, an operation for low PMT supply voltages must be ensured to avoid signal attenuation and excessively long averaging.

– The application of the small Hamamatsu PMTs has allowed the use of higher signal voltage levels (100 mV or more) than in the traditionally used phototubes. A photon flux as high as possible should be applied in the far-field channels since the signal noise is strongly influenced by the photon noise\(^1\). This is an issue if both analogue and photon counting from the same PMT are

\(^1\)In the case of the mobile lidar this would have required enhancing the 266 nm pulse energy of the Powerlite 9030 laser to the full 120 mJ or using a larger receiver (see first example in Sect. 7.2).
chosen because photon counting requires elevated supply voltages of the order of 800 V, too high for strong irradiation.

- A problem with the Hamamatsu 7400 PMTs not yet fully solved is the high sensitivity with respect to daylight: the background signal must not exceed 1 mV in order to avoid undershot, which can be minimized by higher laser pulse energy (improving the peak-signal-to-background ratio), careful spectral filtering, reducing the slit width at the polychromator entrance, adding another black baffle for the incoming radiation just below the entrance flap in the roof, and a very clean surface of the primary mirror of the telescope. Also, for 313 nm, a return to a 5600 PMT can be considered in the far-field receiver.

- The use of two spatially separated telescopes for near-field–far-field separation is superior to cutting off the near-field portions in the far-field channels as done in the mobile system (and the water vapour DIAL; Vogelmann and Trickl, 2008), unless a rotating signal attenuator is used for reducing the stronger off return.

- An operational calculation of uncertainties is planned, an important requirement for archiving data in international databases.
Appendix A

Table A1. List of citations for atmospheric transport studies including ozone lidar systems.

| Browell et al. (1987) | Ancellet et al. (1991) | Ancellet et al. (1994) | Browell et al. (1996) |
|----------------------|------------------------|------------------------|----------------------|
| Lamarque et al. (1996) | Langford et al. (1996) | Newell et al. (1997) | Ravetta et al. (1999) |
| Eisele et al. (1999) | Stohl and Trickl (1999) | Grant et al. (2000) | Baray et al. (2000) |
| Seibert et al. (2000) | Kowol-Santen and Ancellet (2000) | Browell et al. (2001) | Carnuth et al. (2002) |
| Zanis et al. (2003) | Roelofs et al. (2003) | Trickl et al. (2003) | Galani et al. (2003) |
| Papayannis et al. (2005) | Leclair De Bellevue et al. (2006) | Ravetta et al. (2007) | Liang et al. (2007) |
| Trickl et al. (2010) | Trickl et al. (2011) | Kuang et al. (2012) | Trickl et al. (2014) |
| Trickl et al. (2015) | Ancellet et al. (2016) | Granados-Muñoz and Leblanc (2016) | Sullivan et al. (2016) |
| Kuang et al. (2017) | Granados-Muñoz et al. (2017) | Langford et al. (2018) | Trickl et al. (2020) |

Table A2. List of citations for air-quality studies including ozone lidar systems.

| Durieux et al. (1998) | Fiorani et al. (1998) | Zhao et al. (1998) | Banta et al. (1998) |
|----------------------|------------------------|-------------------|-------------------|
| Valente et al. (1998) | Senff et al. (1998) | Thomasson et al. (2002) | Kourtidis et al. (2002) |
| Duclaux et al. (2002) | Couach et al. (2003) | Dufour et al. (2005) | Simeonov et al. (2005) |
| Langford et al. (2009) | Senff et al. (2010) | Trickl (2010b) | Langford et al. (2012) |
| Dreessen et al. (2016) | Langford et al. (2017) | Sullivan et al. (2017) | Yates et al. (2017) |

Table A3. List of citations for papers describing ozone DIAL systems.

| Grant et al. (1975) | Browell (1982) | Pelon and Mégie (1982) | Browell et al. (1983) |
|----------------------|----------------|----------------------|----------------------|
| Uchino et al. (1983) | Ancellet (1989) | McDermid (1991) | Zhao et al. (1992) |
| Uthe and Livingston (1992) | Sunesson et al. (1994) | Kempter et al. (1994) | Bucreev et al. (1994) |
| Bucreev et al. (1996) | Grabbe et al. (1996) | Reichardt et al. (1996) | Bucreev et al. (1994) |
| Brenner et al. (1997) | Ancellet and Ravetta (1997) | Wallinder et al. (1997) | Eisele and Trickl (1997) |
| Ancellet and Ravetta (1998) | Alvarez et al. (1998) | Vescovskii and Barchunov (1999) | Profitt and Langford (1997) |
| Matthias (2000) | Lanzarotto et al. (2001) | McDermid et al. (2002) | Fix et al. (2002) |
| Nakazato et al. (2007) | Machol et al. (2008) | Burlakov et al. (2010) | Alvarez et al. (2011) |
| Kuang et al. (2011) | Kuang et al. (2013) Uchino et al. (2014) | Sullivan et al. (2014) | Fix et al. (2019) |
| De Young et al. (2017) | Strawbridge et al. (2018) | | |
Data availability. Data and information on the lidar systems can be obtained on request from the corresponding author of this paper (thomas@trickl.de as of February 2020). The 313 nm aerosol backscatter coefficients are archived in the EARLINET database, which is accessible through the ACTRIS data portal at http://actris.nilu.no/ (last access: 19 November 2020, ACTRIS, 2020).

Author contributions. TT carried out most lidar measurements after spring 1997, following U. Kempfer and H. Eisele, assisted by HG and MP. He has led the technical development of both ozone DIAL systems since 1990. FN was responsible for the technical infrastructure of the mobile system. HG, MP, and HV have been involved in the system upgrading since 2007.

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