Temporal focusing microscopy combined with three-dimensional structured illumination

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Temporal focusing microscopy provides the optical sectioning capability in wide-field two-photon fluorescence imaging. Here, we demonstrate temporal focusing microscopy combined with three-dimensional structured illumination, which enables us to enhance the three-dimensional spatial resolution and reject the background fluorescence. Experimentally, the periodic pattern of the illumination was produced not only in the lateral direction but also in the axial direction by the interference between three temporal focusing pulses, which were easily generated using a digital micromirror device. The lateral resolution and optical sectioning capability were successfully enhanced by factors of 1.6 and 3.6, respectively, compared with those of temporal focusing microscopy. In the two-photon fluorescence imaging of a tissue-like phantom, the out-of-focus background fluorescence and the scattered background fluorescence could also be rejected. © 2017 The Japan Society of Applied Physics

1. Introduction

Super-resolution microscopy has become a powerful tool for investigating biological phenomena.1–11 However, there is a trade-off between the spatial resolution and penetration depth in optical imaging techniques. If the spatial resolution is enhanced by a factor of N, the signal intensity is reduced by a factor of \( N^2 \) due to the decreased signal volume. The lower intensity signal is easily buried in the background fluorescence generated in the out-of-focus regions. Thus, it is difficult to use super-resolution microscopy for the deep imaging of biological tissue. In contrast, two-photon excited fluorescence (TPEF) microscopy has attractive advantages over confocal microscopy including decreased background fluorescence and deeper penetration into thick specimens.12,13 On the other hand, the spatial resolution of TPEF microscopy is lower than that of confocal microscopy utilizing visible light due to the use of near-infrared light. Recently, super-resolution microscopy was combined with TPEF microscopy to perform deep imaging.14–19 In general, as stimulated emission depletion (STED) microscopy12,15 employs a tightly focused beam as an excitation light, it can be easily coupled with laser scanning TPEF microscopy.14,15 In contrast, structured illumination microscopy (SIM)3,4 saturated SIM,5,7 and single-molecule localization microscopy (SMLM)8–11 require a wide-field illumination scheme. Temporal focusing (TF), which provides wide-field two-photon excitation with optical sectioning capabilities,20,21 allows SIM17 and SMLM40 to operate in deep imaging. In a wide-field microscope, the fluorescent photons generated in the focal plane must be imaged in their conjugate positions on a two-dimensional (2D) detector. Thus, if the emitted photons are scattered within the sample, the scattered photons become the background fluorescence. This problem has been solved by applying non-super-resolution SIM, which enables the rejection of the scattered background fluorescence.22 To TF microscopy,17,23 To obtain a large field-of-view, the excitation power must be increased. As TF microscopy does not require laser scanning, it can utilize an amplifier, which operates at low repetition rates (lower than megahertz), as an excitation light source. Therefore, by using amplified pulses at a low average power, TPEF video-rate imaging over large areas in the 5000–20000 \( \mu \text{m}^2 \) range has been achieved.24,25 By using the time multiplexing technique,26,27 the out-of-focus background fluorescence generated in the TF microscope has been suppressed.28,29 The multifocal TPEF technique30,31 can also be combined with SIM.18,19 However, in multifocal SIM, multiple foci must be scanned. Thus, to increase the imaging speed, the repetition rate of the pulses must be more than several tens of megahertz.

Since the spatial resolution of super-resolution SIM is enhanced in the periodic pattern direction, a periodic illumination pattern in the axial direction as well as the lateral direction allows the enhancement of the spatial resolution in both the axial and lateral directions.32 However, in TF microscopy combined with super-resolution SIM ever reported, only laterally structured illumination, which is produced by the interference between two TF pulses, has been used.17 In this paper, we demonstrate three-dimensional (3D) interferometric TF (ITF) microscopy in which periodic patterns are generated in the lateral and axial directions by the interference between three TF pulses. The three TF pulses is generated by employing a digital micromirror device (DMD), which can be utilized both as a phase grating to generate TF pulses33 and an amplitude grating to achieve 3D structured illumination.34 Thus, the use of DMD can also enable us to simplify a complex ITF microscope, which includes a grating for TF and a beamsplitter or another grating for structured illumination.17 TF microscopy combined with SIM using the DMD has already been reported.35 But the 3D structured illumination has been treated incorrectly as a 2D periodic
pattern only in the lateral direction. The required pattern images for 3D structured illumination is different from that for 2D structured illumination. In Sect. 2, we start with an explanation of the concept of 3D-ITF microscopy and show an experimental setup for it. In Sect. 3, we report and discuss the experimental results of 3DF-ITF microscopy. In Sect. 4, we summarize this paper.

2. Methods

2.1 Theory

We first show the principle of 3D-ITF microscopy. As shown in Fig. 1, in TF microscopy, all the spectral components in a spectrally dispersed pulse are recombined only at the focal plane of an objective lens. As a result, the pulse duration decreases as the distance from the focal plane decreases and becomes the shortest at the focal plane. Thus, although the wide field illumination is used, the TF effect provides the suppression of the out-of-focus TPEF. The focal plane is imaged onto a 2D detector, which is used to record a wide-field image. A 3D image is obtained by scanning the sample along the axial direction. Therefore, the detected image \( D(x, y, z) \) can be expressed as

\[
D(x, y, z) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} S(x', y', z') P_0^2(x', y', z - z') h(x - x', y - y', z - z') \, dx' \, dy' \, dz',
\]

where \( S(x, y, z) \) is the density distribution of the fluorophore in the sample, \( I_{ex}(x, y, z) \) is the time-averaged intensity distribution of a TF pulse, and \( h(x, y, z) \) is the point spread function (PSF) of the detection system. \( A_{TF}(z) \) is the axial response for two-photon excitation by the TF pulse, which is described by \( 36,37 \)

\[
A_{TF}(z) = \frac{1}{[1 + (z/z_p)^2]^{1/2}}.
\]

Here, \( z_p \) is related to the optical sectioning capability by the TF effect, which depends on the numerical aperture. We assume that the sample is illuminated by an excitation light with a periodic pattern, which is generated by the interference of three TF pulses, as shown in Fig. 1. If we represent the time-averaged electric field of the excitation light as

\[
E_{ex}(x, y, z) = E_0(e^{j \omega_0 z} + \alpha e^{jka(y \sin \theta + z \cos \theta + \phi_0)} + \alpha e^{jka(-y \sin \theta + z \cos \theta - \phi_0)}),
\]

the square of the time-averaged intensity can be written as

\[
I_{ex}(x, y, z) = (|E_0|^2)^2 \sum_{j=-4}^{4} A_{TF}^{(2j)}(z) e^{jka(y \sin \theta + z \cos \theta + \phi_0)},
\]

where \( A_{TF}^{(2j)}(z) = 1 + 8z^2 + 6\alpha^2 + 4\alpha^2 \cos(2k_0 z), A_{TF}^{(4j)}(z) = 8\alpha^2 (1 + \alpha^2) \cos(k_0 z), \)

\[
A_{TF}^{(2j)}(z) = 2\alpha^2 [2 + 2\alpha^2 + \cos(2k_0 z)],
\]

\[
A_{TF}^{(4j)}(z) = \alpha^4,
\]

\[
k_0 = k_0 \sin \theta,
\]

\[
k_{m} = k_0 (1 - \cos \theta).
\]

Here, \( \alpha \) is a modulation depth, \( k_0 \) is the wavevector of the pulse center wavelength, \( \theta \) is the angle between the central and outer beams, and \( \phi_m \) is the phase shift of the periodic pattern. By using Eqs. (1) and (4), the detected image can be rewritten as

\[
D_m(x, y, z) = (|E_0|^2)^2 \sum_{j=-4}^{4} S(x, y, z) e^{jka(y \sin \theta + z \cos \theta + \phi_0)} \otimes [A_{TF}(z) A_{TF}^{(2j)}(z) h(x, y, z)],
\]

where \( \otimes \) denotes a convolution. The detected image in Fourier space is given by

\[
D_m(k_x, k_y, k_z) = (|E_0|^2)^2 \sum_{j=-4}^{4} \tilde{S}(k_x, k_y - jk_0, k_z) e^{j\phi_m} \times [\tilde{A}_{TF}(k_z) \otimes \tilde{A}_{TF}^{(2j)}(k_z) \otimes \tilde{h}(k_x, k_y, k_z)]
\]

\[
= \sum_{j=-4}^{4} \tilde{F}(j, k_x, k_y, k_z) e^{j\phi_m},
\]

where

\[
\tilde{F}(j, k_x, k_y, k_z) = (|E_0|^2)^2 \tilde{S}(k_x, k_y - jk_0, k_z) \times [\tilde{A}_{TF}(k_z) \otimes \tilde{A}_{TF}^{(2j)}(k_z) \otimes \tilde{h}(k_x, k_y, k_z)].
\]

As shown in Eq. (7), the detected image includes nine Fourier components, \( F(j, k_x, k_y, k_z) \), at spatial frequencies of around \(-4k_0, -3k_0, -2k_0, -k_0, 0, +k_0, +2k_0, +3k_0, \) and \(+4k_0 \) in the k\(_x\)-direction. In each Fourier component, the high spatial frequency sample information \( S(k_x, k_y, k_z) \) is down-converted to the lower frequency information \( S(k_x, k_y - jk_0, k_z) \) in the k\(_z\)-direction. In addition, the detectable bandwidth in the k\(_z\)-direction is broadened by the convolution of the optical transfer function (OTF) of the detection system with the excitation effects of the TF and the periodic pattern illumination along the axial (z) direction. By shifting the down-converted components \( F(j, k_x, k_y, k_z) \) back to their true positions \( F_j(k_x, k_y + jk_0, k_z) \) in Fourier space and by recombining them, the effective OTF of the microscope is broadened.\( 8 \) As a result, the cut-off spatial frequencies in the k\(_x\) and k\(_y\)-directions are extended to \( k_{or} + 4k_0 \) and \( k_{or} + k_{TF} + 2k_0 \), respectively. Here, \( k_{or} \) and \( k_{or} \) are the cut-off spatial frequencies of the detection system OTF in the k\(_x\)-
and \( k_x \)-directions, and \( k_{TF} \) is the cut-off spatial frequency of the TF effect. Thus, in order to reconstruct the super-resolution images, each Fourier component \( F_i(k_x, k_y, k_z) \) must be separated. To separate each Fourier component, we take nine images, \( D_m(x, y, z) \), at phase shifts \( \phi_m = \phi_0 + m\phi_s \) from \( m = 0 \) to \( 8 \), and use the principle of homodyne detection:

\[
F_i(k_x, k_y, k_z) = \frac{1}{N} \sum_{m=0}^{N-1} D_m(k_x, k_y, k_z) e^{-i\phi_m}.
\] (9)

Here the phase step \( \phi_s = 2\pi/9 \), and \( \phi_0 \) is the offset phase. After shifting the separated Fourier components back to their true position, they are recombined with the exception of the Fourier component at the spatial frequency of around 0, \( F_0(k_x, k_y, k_z) \). As the scattered background fluorescence and the out-of-focus background fluorescence do not produce the periodic pattern on the 2D detector, they are contained in \( F_0(k_x, k_y, k_z) \). Thus, to reject the background fluorescence, \( F_0(k_x, k_y, k_z) \) is not used. The super-resolution image can be acquired by the inverse Fourier transform of the recombined image in Fourier space. In order to enhance the spatial resolution in 3D, the orientation of the periodic pattern must be rotated in the lateral direction.

2.2 Experimental setup

Figure 2(a) shows a schematic diagram of the system used for 3D-ITF microscopy. As an excitation light source, an Yb-fiber chirped-pulse amplifier (CPA) was utilized. The output pulse from an Yb-fiber oscillator (Onefive Origami-10), which produced 152 fs pulses at a central wavelength of 1061 nm, a bandwidth of 8.1 nm, and a repetition rate of 40 MHz, was used as a seed pulse. In the CPA, the input pulse with an average power of 15 mW was stretched to 203 ps using a fiber stretcher with a group delay dispersion (GDD) of 7.5 ps2 and a third order dispersion (TOD) of −0.087 ps3. The output spectrum from the stretched fiber was broadened to the bandwidth of 19 nm by self-phase modulation. The stretched pulse was amplified to an average power of 330 mW by the first Yb-fiber amplifier. After the first amplification, the repetition rate was reduced to 200 kHz by using an acousto-optic modulator (AOM). The output pulse from the AOM was amplified to an average power of 252 mW by a second Yb-fiber amplifier. The amplified pulse was compressed using the combination of a pulse shaper with a liquid-crystal spatial light modulator (SLM) and a pair of 1600 lines/mm transmission gratings with a separation of 12 cm at an incident angle of 59.1°. The pulse shaper was used to compensate for the higher order dispersion of the system, while the grating pair was used for the simultaneous GDD and TOD compensation. The output pulse from the CPA was reflected by a DMD (Texas Instruments DLP4500NIR) with a micromirror pitch of 10.8 µm and a micromirror tilt angle of ±12°. As shown in Fig. 2(b), the DMD can operate both as an amplitude grating and as a phase grating. In the x-direction, all the micromirrors on the DMD were tilted by +12° or −12°, which indicated on or off states, respectively. As the tilt angle of the micromirror on the DMD is regarded as the blaze angle of a blazed grating along the x-direction, the spectrally dispersed pulse for the TF was generated using the DMD as the phase grating. To avoid the tilt of the TF plane on the sample, the diffraction angle of the central wavelength must be zero. Considering the blaze condition to maximize the diffraction efficiency, we chose a fourth order diffraction light at an angle of incidence of 23.1°. Under this condition, the diffraction efficiency was 54%. Conversely, in the y-direction, the periodic pattern with on and off states were produced at a period of 18 micromirrors. The periodic pattern was utilized as an amplitude grating along the y-direction, which gave zero and ±1 order diffraction lights as three TF pulses. The periodic pattern on the DMD was imaged at the focal plane of a water-immersion objective lens with a numerical aperture (NA) of 1.2 (OB; Olympus UPLSAPO60×W) by a factor of 1/125×. The periodic pattern near the focal plane was observed not only in the lateral direction but also in the axial direction. By blocking the zero-order diffraction beam, the periodic pattern was only produced in the lateral direction. The pulse duration at the focal plane was 103 fs and the input power was 9 mW on the sample surface. The generated TPEF signal was collected by the same objective lens and was separated from the excitation pulses using a dichroic mirror (DM; Thorlabs DMLP900). To remove the residual excitation pulses, a short-pass filter (SPF; Semrock FF01-890/SP-25) and a bandpass filter (BPF; Semrock FF01-550/88-25) were used. Wide-field TPEF images were obtained by a CMOS camera (Hamamatsu Photonics ORCA-Flash2.8) with an exposure time of 10 ms. In order to achieve the resolution enhancement in all the lateral directions, the orientation of the periodic pattern on the DMD was rotated by 45, 90, and 135°. By scanning the sample in the axial (z) direction with a stepping motor-driven stage with a step size of 100 nm, the 3D image was obtained. By replacing the DMD with a reflective diffraction grating with a groove density of 830 grooves/mm, TPEF images for the TF microscope were acquired.

3. Results and discussion

In order to obtain the fundamental spatial frequency of the
The 3D images were reconstructed from 2001 cross-sectional images at penetration depths of 45 and 162 µm. The line profiles in Fig. 5 clearly show the separation of the neighboring beads due to the improved resolution of 3D-ITF microscopy.

Using TF and 3D-ITF microscopy, we imaged fluorescently labeled beads in a tissue-like phantom. The phantom consisted of a low-melting-point agarose gel containing 200-nm and 2-µm fluorescent polystyrene beads at concentrations of 2.3 × 10^11 beads/mL and 2.1 × 10^12 beads/mL, respectively. The observed images are depicted in Fig. 6. In the image obtained by TF microscopy, the TPEF signals from the 200-nm beads are buried in the large background fluorescence, which originated from periodic pattern \( k_{0b} \), a TPEF image of the Rhodamine B solution was recorded under a structured illumination. From the measured fringe pattern, the fundamental spatial frequency of the periodic pattern in the lateral direction, \( k_{y0} \), was evaluated to be 4.1 rad/µm, which was used to reconstruct the 3D-ITF image. The signal-to-noise ratios of the Fourier components, \( F_{±4}(k_x, k_y, k_z) \), at the spatial frequencies of around \(-4k_{0d}+4k_{y0}\) and \(+4k_{0d}+4k_{y0}\) were too low to be used in the reconstruction of the 3D-ITF image.

We characterized the optical sectioning capability of 3D-ITF microscopy. Figure 3 shows the measured signal intensity distribution along the axial direction near the interface between the coverslip and the Rhodamine B solution. The full width at half maxima (FWHMs) of the smoothed first derivatives of the signal distributions for TF and 3D-ITF microscopies were 2.6 and 0.72 µm, respectively. We found that the optical sectioning capability of 3D-ITF microscopy was 3.6 times higher than that of TF microscopy. Compared with the optical sectioning capability of 2D-ITF microscopy with the periodic pattern illumination only in the lateral direction, which was reported to be 0.89 µm,\(^{17}\) that of 3D-ITF microscopy was also enhanced by a factor of 1.2. This improvement is due to the periodic pattern illumination along the axial direction.

In order to investigate the spatial resolution of 3D-ITF microscopy, we obtained a 3D image of 200-nm fluorescent polystyrene beads (Molecular Probes F8809) with a concentration of 2.3 × 10^11 beads/mL in a low-melting-point agarose gel. The emission wavelength of the beads was 560 nm. From the cut-off spatial frequencies of the OTF in the lateral and axial directions, \( k_{y0} \) and \( k_{z0} \) were theoretically calculated to be 26.9 and 8.4 rad/µm, respectively. As the fundamental spatial frequency of the periodic pattern in the lateral direction, \( k_{y0} \), was 4.1 rad/µm, the third harmonic spatial frequency of the periodic pattern in the lateral direction, \( 3k_{y0} \), and the second harmonic spatial frequency of the periodic pattern in the axial direction, \( 2k_{z0} \), were experimentally evaluated to be 12.3 and 2.3 rad/µm, respectively. From the FWHM of 2.6 µm for the characterization of the optical sectioning capability, the cut-off spatial frequency in the axial direction by the TF effect, \( k_{TF} \), was evaluated to be around 2.4 (= 2π/2.6) rad/µm. Thus, the cut-off spatial frequencies of the effective OTF in the lateral and axial directions should be extended to 39.2 rad/µm (= \( k_{y0} + 3k_{y0} \)) and 13.2 rad/µm (= \( k_{z0} + k_{TF} + 2k_{z0} \)), which results in the 0.16-µm lateral FWHM and 0.48-µm axial FWHM of the effective PSF, respectively. Compared with the minimum FWHM at the diffraction limit, the measured FWHMs are slightly broadened due to the wavefront distortion. However, the 3D spatial resolution is improved by 3D-ITF microscopy. Figure 5 illustrates the cross-sectional images at penetration depths of 45 and 162 µm. The line profiles in Fig. 5 clearly show the separation of the neighboring beads due to the improved resolution of 3D-ITF microscopy.

and 0.22 µm with the fluorophore distribution in a 200-nm bead, to be 0.30 and 0.18 µm, respectively. The axial FWHMs for TF and 3D-ITF microscopies were 0.82 ± 0.050 and 0.66 ± 0.059 µm, respectively. We found that the FWHMs in the lateral and axial directions were enhanced by factors of 1.6 and 1.2, respectively. For the diffraction-limited detection system at a wavelength of 560 nm and an NA of 1.2, the cutoff frequencies were 12.3 and 2.3 rad/µm, respectively. From the FWHM of 2.6 µm for the characterization of the optical sectioning capability, the cut-off spatial frequency in the axial direction by the TF effect, \( k_{TF} \), was evaluated to be around 2.4 (= 2π/2.6) rad/µm. Thus, the cut-off spatial frequencies of the effective OTF in the lateral and axial directions should be extended to 39.2 rad/µm (= \( k_{y0} + 3k_{y0} \)) and 13.2 rad/µm (= \( k_{z0} + k_{TF} + 2k_{z0} \)), which results in the 0.16-µm lateral FWHM and 0.48-µm axial FWHM of the effective PSF, respectively. Compared with the minimum FWHM at the diffraction limit, the measured FWHMs are slightly broadened due to the wavefront distortion. However, the 3D spatial resolution is improved by 3D-ITF microscopy. Figure 5 illustrates the cross-sectional images at penetration depths of 45 and 162 µm. The line profiles in Fig. 5 clearly show the separation of the neighboring beads due to the improved resolution of 3D-ITF microscopy.

Using TF and 3D-ITF microscopy, we imaged fluorescently labeled beads in a tissue-like phantom. The phantom consisted of a low-melting-point agarose gel containing 200-nm and 2-µm fluorescent polystyrene beads at concentrations of 2.3 × 10^11 and 9.0 × 10^8 beads/mL, respectively. The observed images are depicted in Fig. 6. In the image obtained by TF microscopy, the TPEF signals from the 200-nm beads are buried in the large background fluorescence, which originated from
the out-of-focus TPEF of the 2-µm beads and the scattered TPEF. In contrast, the 200-nm beads are clearly visualized by 3D-ITF microscopy. The large background fluorescence could be successfully rejected by 3D-ITF microscopy.

4. Conclusions

We have demonstrated that 3D-ITF microscopy combining TF microscopy with 3D structured illumination allows the improvement of 3D spatial resolution and the elimination of background fluorescence. A 3D structured illumination was achieved by the interference between three TF pulses, which were easily generated by using a DMD both as an amplitude grating and as a phase grating. The lateral and axial FWHMs of the effective PSF was enhanced by factors of 1.6 and 1.2, respectively, compared with those of TF microscopy. The optical sectioning capability was improved by a factor of 3.5. This approach can be applied to super-resolution deep imaging. The amplified pulses used in these demonstrations can be used to induce TPEF saturation. The nonlinearity of the saturation effect provides the possibility of further enhancement to the spatial resolution. By employing saturation nonlinearity in one-photon excited fluorescence (OPEF), the spatial resolution of SIM was improved.\(^5\)\(^-\)\(^7\) However, OPEF saturation generates large out-of-focus background fluorescence and induces photobleaching due to the high excitation intensity. TPEF and photobleaching in out-of-focus excited images can be reduced by using a modified illumination technique.\(^8\)\(^-\)\(^11\) Furthermore, the large optical sectioning capability allows the use of sub-diffraction-limited spatial frequencies of PSF for super-resolution imaging.\(^12\)\(^-\)\(^14\)

Fig. 5. (Color online) Cross-sectional (a, c) TF and (b, d) 3D-ITF images of 200-nm fluorescent beads at penetration depths of (a, b) 45 µm and (c, d) 162 µm. The signal intensities were normalized by the maximum intensity in each image. Normalized signal profiles of TF (•) and ITF (×) microscopies along the lateral direction indicated by arrows in (e) a and b, and (f) c and d.

Fig. 6. (Color online) (a) 3D TF and (b) 3D-ITF images of the tissue-like phantom including 200-nm and 2-µm fluorescent beads. The signal intensities in a and b were normalized by the maximum intensity in each 3D data set. Cross-sectional (c) TF and (d) 3D-ITF images in a and b. The signal intensities in c and d were normalized by the maximum intensity in each image. (e) Normalized signal profiles of TF (•) and ITF (×) microscopies indicated by arrows in c and d.
focus regions can be decreased by using the TF effect. In-focus photobleaching can additionally be reduced by decreasing the repetition rate of the amplified pulse to several hundreds of kilohertz.39)

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