Scatterometry and diffractometry techniques to monitor surfaces textured by rapid ultra-short pulse laser

C Alleaume¹, S Alamri², T Kunze³, J Ziegler³, A Wilson⁴ and R Bola⁵

¹ AIMEN Technology Centre (Laser Applications Centre), Porriño, Spain
² Fraunhofer-Institute for Material and Beam Technology IWS, Dresden, Germany
³ IRIS Technology Group, Madrid, Spain
⁴ TWI Ltd, Cambridge, United Kingdom
⁵ European Federation for Welding, Joining and Cutting, Porto Salvo, Portugal

E-mail: rgbola@ewf.be

Keywords: texturing, scatterometry, diffractometry

Abstract
The overall aim of the PROMETHEUS project is to develop high power ultra-short pulse lasers and the associated optics to enable the precise periodic texturing of surfaces to impart a range of surface functionalities at unprecedented processing speeds. The project focuses upon the industrial application of ultra-short pulse lasers for manufacturing and on the development of high power ultra-short pulse laser technologies in the range of 700 ps – 10 ns. In summary, new textures will be manufactured to achieve functional surfaces utilising fewer raw materials, less energy and less waste; improve accuracy, power and control over existing technologies; increase achievable precision and minimize heat impact on sensitive materials. This article will provide the outcomes of the first results achieved from the monitoring solutions being used to assess surface textures with micrometer resolution.

1. Introduction

Among the different approaches that can be used to fabricate biomimetic structures on surfaces, short/ultra-short (S/US) laser pulses gained in the last years a high relevance [1–3]. The material removal takes place locally at the zone where the laser beam is interacting with the substrate surface which also causes limited chemical surface modification [4]. From an industrial point of view, S/US pulsed laser technologies are very flexible and allow to treat a wide range of materials, as long as the substrate absorbs the used laser wavelength (i.e. IR and VIS for metals [5, 6] and UV for polymers [7]). In addition, the scale-up of such technologies for industrial applications has been already demonstrated in several cases [8].

Although the fabrication of functional surfaces has been demonstrated on different materials, the main drawback of the traditional direct laser writing (DLW) technology is the long processing time with machining speeds in the range of minutes per square centimetre [9–11]. Multiple solutions are available for scaling-up the fabrication speed of DLW including the use of polygonal scanners and multi-beam approaches. However, the achievable feature sizes of DLW are typically limited to 5–15 µm [12, 13].

Considering the fabrication of periodic patterns with different length scales (larger or even smaller than the laser wavelength) other well-established laser technologies can be considered such as Direct Laser Interference Patterning (DLIP) [14, 15]. This method relies on the overlap of two or more coherent laser beams which results in the formation of well-defined interference patterns.

For a given laser wavelength and number of beams, the spatial period can be easily adjusted by modifying the angle of the interfering beams [15]. By changing the polarization and the geometrical configuration of the interfering beams, very different pattern geometries can be created. For instance, in a two-beam arrangement a line-like pattern is generated whereas a three-beam configuration lead to dot-like patterns.

Although the fabrication of periodic structures using DLIP has been demonstrated on different materials and employing different laser sources, the assessment of the structuring quality during the manufacturing process remains an open topic of great interest for its exploitation under industrial conditions. The aim of
the present work is therefore to demonstrate a promising method to characterize microstructured surfaces employing scatterometry and diffractometry techniques and their possible implementation in an inline process monitoring system.

1.1. Hydrophobicity and oleophobicity
Achieving super-hydrophobicity is specific to achieve water repellent surfaces. However, super-oleophobicity requires surfaces that are not wetted by organic liquids that typically have lower surface tensions compared to that of water. It has been demonstrated that the synergistic effects of re-entrant topographic features, combined with tailored surface chemistry properties, helps to promote super-oleophobicity which inherently provides super-hydrophobic properties. However, it is possible in some cases that oleophobic properties can occur alongside hydrophilic properties instead. This phenomenon is not fully understood. The PROMETHEUS project will investigate both hydrophobic properties and oleophobic properties for different materials.

In order to achieve hydrophobic/oleophobic properties, a robust Cassie wetting state must be met [16, 17]; the re-entrant feature must promote the net traction to drive the liquid/air interface to recede to the top edge of the microstructures, resulting in a three-phase (solid/air/liquid) interface. To simplify, the microstructures of the material surface can be overall be divided into two types that represent either a trapezoid (figure 1(a)) or an inverted trapezoid (figure 1(b)).

In the case of water, the trapezoid microstructures can promote a robust Cassie state for having hydrophobic surfaces.

However, according to the design constraint, oils which commonly have very low surface tension and almost all of their Young’s CAs smaller than 90°, are unable to be form a robust Cassie state. In this case, this can be realised on inverted-trapezoid textures. Thus, inverted-trapezoid surface microstructures are usually termed re-entrant textures [18].

In the PROMETHEUS laser station prototype, laser texturing processes will be based on Direct Laser Interference Patterning (DLIP) by two laser beams. In this case, the pattern generated by the two-beams interference is a line-like pattern. If a metallic or polymeric surface is patterned with the proper line-like structures, then this becomes hydrophobic or oleophobic. Figure 2 depicts the wetting behaviour of a water droplet on a patterned surface.

The water droplet sits on the top of the patterns with air trapped in between the patterns, thereby giving rise to hydrophobicity due to composite wetting as described by the Cassie-Baxter model [16, 17]. Based on previous experimental works performed [34], a line by line laser scanning process will be investigated for the generation of micro-conical structures and trapezoids on metallic and polymeric samples.

2. Materials and methods
In the scope of the PROMETHEUS project, several European partners have shown interest in the DLIP surface texturization technology, leading to a large range of materials been studied. Several metals such as
steels and aluminium are currently under investigation and are showing promising results in both the
texturization process and in the physical property obtained.

For the laser experiments, a compact diode-pumped Nd:YLF laser (Tech 1053 basic, Laser Export,
Russia) emitting 15 ns pulses with TEM\textsubscript{00} mode (Gaussian beam) at 1053 nm was used to irradiate
the materials. The main laser beam was then directed through a compact DLIP optical module (developed
at Fraunhofer IWS, Dresden) capable to fabricate line-like interference patterns with varying spatial
periods (software-controlled). The main laser beam is divided into two sub-beams by a diffractive
beam-splitting element. The two sub-beams are collimated by a prism and then overlapped by a lens
onto the sample surface resulting in a line-like interference pattern in a well-defined interference area
(denoted as DLIP pixel), as depicted in figure 3(a). By changing the distance between the beam-splitting
element and the prism, the interference period \( \Lambda \) can be selectively changed in a range of 1.5–8.5 \( \mu m \).

High precision positioning stages (AEROTECH PRO115) were used for displacing the sample
and distributing the interference pattern over a larger area both in the direction parallel and perpendicular
(hatch distance \( h \)) to the interference pattern, as highlighted in figure 3(b). The quantity \( p \) defines also the
pulse-to-pulse overlap and can be expressed as number of pulses per pixel (P/px) which also denotes the
cumulative fluence dose.

It is worth mentioning that the \( h \) value have been adjusted for the employed spatial period, in order to
match a distance equal to an entire multiple of the period. In the present work, a period of 8.5 \( \mu m \) and a
hatch distance of 25.5 \( \mu m \) have been used.

### 2.1. Characterization and selection of textures

Once a matrix of sample is manufactured, their properties are studied, in order to select the best process
parameters for a successful texturization. Two aspects are mostly looked at in this phase: on one hand, the
reproducibility of the pattern, and on the other hand the physical properties of the newly texturized material.

Regarding the reproducibility of the pattern, a valley detection algorithm was developed at AIMEN, in
order to identify each individual period and easily extract the associated geometrical parameters. An
illustration of this algorithm applied to a reproducible texture can be found in figure 4. By using this
algorithm on all samples, it becomes obvious that some strategies for texturing are not optimal. The main
parameters of the texturing process been the number of laser pulses and the energy of each laser pulse,
we can observe that if a low energy is used on the laser, the desired patterns tend not to appear correctly on
the surface. Using more pulses with lower energy does not always compensate for this issue, even with the same
total energy. To the contrary, using too much energy in the pulses leads to a degraded material, and a
non-reproducible pattern, even with less pulses.

For each texture, an optimal texturing strategy is then obtained. An illustration of this selection can be
found in figure 5 where both a ‘good’ and a ‘bad’ cases are shown side by side for comparison. Table 6 gives
the actual values found by the detection algorithm with both mean value and standard deviation for different
fabrication receipes.

The other aspect of the qualification of the textures concern the physical properties. Indeed, the
PROMETHEUS project been designed to create hydrophilic or hydrophobic materials, a contact angle
measurement is performed on the fabricated DLIP textures [19, 20]. An example of the contact angle
measurement can be found in figure 6. Note that this method is limited to the reaction with water and is
therefore not always directly linked to the requested property of the final product: for instance, if the final
product will be in contact with oil (like for the case of a car’s engine component) or oily products (like
Table 1. Results for different process recipe for the aluminium sample.

| Sample Description                     | Pitch (µm) | Pitch std (%) | Height (µm) | Height std (%) | Width (µm) | Width std (%) | Slope | Slope std (%) | Valid flag (%) |
|----------------------------------------|------------|---------------|-------------|----------------|------------|---------------|-------|---------------|----------------|
| Aluminium—target pitch 8.5 µm—03 P/px—low laser power | 8.49       | 7.31          | 2.51        | 21.37          | 4.20       | 11.63         | 0.38  | 29.30         | 100             |
| Aluminium—target pitch 8.5 µm—03 P/px—medium power      | 8.53       | 6.71          | 4.00        | 17.40          | 4.50       | 12.84         | 0.67  | 29.58         | 99              |
| Aluminium—target pitch 8.5 µm—03 P/px—high laser power   | 8.53       | 9.58          | 5.29        | 19.12          | 4.42       | 14.54         | 0.92  | 30.77         | 99              |
| Aluminium—target pitch 8.5 µm—10 P/px—low laser power    | 8.47       | 5.92          | 6.45        | 13.20          | 5.08       | 8.44          | 1.30  | 18.86         | 100             |
| Aluminium—target pitch 8.5 µm—10 P/px—medium laser power | 8.51       | 7.06          | 9.40        | 22.69          | 5.15       | 13.59         | 1.66  | 37.39         | 100             |
| Aluminium—target pitch 8.5 µm—10 P/px—high laser power   | 8.54       | 9.94          | 9.61        | 30.72          | 5.62       | 16.08         | 2.03  | 60.43         | 93              |
| Aluminium—target pitch 8.5 µm—17 P/px—low laser power    | 8.47       | 6.42          | 8.08        | 17.05          | 5.42       | 8.40          | 1.67  | 21.50         | 100             |
| Aluminium—target pitch 8.5 µm—17 P/px—medium laser power | 8.47       | 10.92         | 8.25        | 31.50          | 5.94       | 14.79         | 1.82  | 60.01         | 90              |
| Aluminium—target pitch 8.5 µm—17 P/px—high laser power   | 8.70       | 15.41         | 7.35        | 42.22          | 6.47       | 14.74         | 1.78  | 63.27         | 75              |
cosmetics product), the relation between the contact angle and the behaviour with the final product will not necessarily be linear [21]. However, as a first approach, a set of potential strategies for texturing the end-materials are selected and will be tested by the different customers in order to assess a first correlation between theoretical models and the real application. Eventually, a range of geometrical properties (such as pitch, gap width, structure height and slope) will be selected, as those properties are the ones that are responsible for the physical property of the material [19]. An ideal DLIP laser strategy will be later developed to create the line-like structures with the highest reproducibility. 

\( \theta_c > 160^\circ \)

### 2.2. Process qualification: scatterometry

During the process of characterization of the line-like structures described earlier, the geometrical characteristics of the lines are studied, and a good reproducibility of those geometrical characteristics is expected. Those values have been extensively studied with the help of a confocal microscope and a scanning laser microscope, among others. However, such technics are very time consuming and cannot be implemented in-line during the manufacturing process.
Therefore, in order to monitor the quality of the process, a different approach is being adapted: the scatterometry technology [22], in which we compare the measured reflected light on the texturized sample, with an optical model of RCWA.

For the measure of the reflected light, a preliminary setup has been mounted at AIMEN. In this setup, a white polarized and collimated light is shined into the texturized sample, as illustrated in figure 7. The sample which contains a line-like structure that acts as a diffraction grating will diffract light in a well-defined way. Each diffraction order will have a certain intensity which will depend on several parameters such as the angle of incidence, the polarization, the wavelength, the optical index of the material, the order itself (1st order, 2nd order...), and finally the geometrical parameters of the lines. This means that, since we are shining a white light onto the sample, each wavelength will reflect a different quantity of energy in 0th order, that is strongly dependent of the geometrical parameters. A spectrum of intensity of reflected light is therefore obtained experimentally for the 0th order of diffraction for different wavelengths.

This behavior of a predictable reflection/diffraction has been extensively explained and study by the scientific literature [23–25] and is only adapted in the PROMETHEUS project with the expected geometrical dimension required by hydrophobic/hydrophobic textures.

The measured reflected spectrum is directly compared with a commercial RCWA simulator. The geometrical parameters are injected directly into the simulator, along with the optical index of the material, the polarization and the angle of incidence. By changing the value for the wavelength in the simulator, the full spectrum of intensity of the reflected light for the 0th of diffraction is also obtained. Figure 8 illustrated this spectrum generation principle, where for a given experimental typical profile, we can obtain the spectrum reflected by the sample, by simulating the electromagnetic propagation of the 0th order with a RCWA simulator.

If the sample is correctly fabricated and present a good enough reproducibility, both spectrums from the measurement and from the simulator should match. This has been proven to work successfully for at least one
sample in such a way that we can successfully correlate the measured spectrum with the RCWA simulation as illustrated in figure 9.

Such a scatterometry technology offers the advantage of being easily scalable in terms of speed. Implementing a scatterometry technique has been proven very efficient in other industries such as semi-conductor [26], nanoimprint [27], grating structure [28, 29] and hologram fabrication [30], and it has been proven to be a very effective and time efficient qualification method for line-like structures.

One difficulty that is already foreseen with the proposed technique is the retrieval algorithm. In the literature, different techniques are proposed to match the measured sample with the simulated sample. The most commonly used is the direct library search [22]. This implies that a large number of samples are simulated, and an algorithm is developed in order to find a match within this library.

In the PROMETHEUS project, a slightly different approach is anticipated, and a neural network will be trained to find and match the measured spectrum, and therefore validate the parameters defining the texture (height, pitch, gap, slope...). The idea is to simulate thousands of spectra corresponding to structures within the observed standard variation of the geometrical parameters (for example, 5% height fluctuation), and to feed the neural network with those 'good' spectra. The same is done with 'bad' samples. If the neural network is successful, it should be able to identify which structures are from a 'good' sample, and therefore be able to validate the fabrication process in-line with the scatterometry techniques, eliminating the need for
time-consuming measurement. Such methodology has already been proven to be working by different studies [31, 32].

2.3. Process qualification: diffractometry
Complementary to scatterometry characterization, diffractometry is being established as optical monitoring technique in a dedicated setup at IRIS in order to obtain the necessary information on surface geometry and thus assess structure quality.

Diffractometry is an optical technique, similar to scatterometry, that analyzes the diffraction pattern produced by a microstructured surface when light interacts with it [25]. The main requirements for the illumination in the case of a diffractometry measurement are the high directionality of the light and its monochromaticity (because scattering angles depend both on the size of the scatterers and the wavelength of incident light). Those two conditions are easily fulfilled by using a laser source.

In case of periodic structures, experimental parameters such as diffraction angle separation between the orders and orientation of the diffraction orders are measured in order to deduce sample features like the period and orientation of the lines. The depth of the lines may be determined by measuring the intensity of the diffracted spots, the degree of order/disorder by measuring the relative intensity of peaks compared to background etc. This technique provides average information of all the lines illuminated. The optical analysis can be enhanced by optimizing the polarization state and direction of the light as well as its wavelength.

Preliminary measurements of the diffraction behavior from textures with line-like structures are shown in figure 11. The photograph (figure 10) displays the sample matrix with three panels (framed in green, blue and purple) of textures, all fabricated with varying process parameters. The corresponding diffractometry measurements for each texture in the respective panel were obtained by a prototype lab rig (excitation wavelength 638 nm, 30° incidence angle) and exhibit characteristic diffraction patterns. A clear dependence on the process parameters is observable. While most of the textures in the green panel do not reveal a clear diffraction pattern due to a potentially strong extinction of the incident visible light, the situation is different
in the blue and purple panels. Here, the individual diffraction orders are more pronounced and related to the different texture dimensions. Structural information will be deduced in the future from the distances between the diffraction orders and also from their shapes. Especially in the blue panel, additional features are visible, indicating a deviation from perfectly straight and regular lines on the texture. Moreover, sample structures with more complex diffraction patterns will be analyzed in forthcoming studies in order to establish a correlation to the process parameters, supported by the aid of RCWA model simulations [33].

3. Risks and challenges

In order to successfully implement the scatterometry or diffractometry technique within the PROMETHEUS project, several aspects need to be considered and accounted for. Although they have already been successfully implemented in other industries where the reproducibility of the structures is very high its implementation within the PROMETHEUS project presents some challenges.

One risk is due to the 'low' reproducibility of the line-like pattern. Indeed, even with the best initial texturing strategies, a 5% to 10% error margin can be found on the geometrical parameters of the lines (width, height, slope…). This is widely bigger than the error found in the semi-conductor or in the nanoimprint industries. Those fluctuations will yield different spectrum, which still needs to be fully identified and quantify, for the validation algorithm to successfully recognize if the patterns have properly been engraved.

Another risk comes from the fact that some structures present a strong extinction for visible and infrared wavelengths. Therefore, a very large spectrum needs to be analysed in order to successfully identify the structures. Apart from being a challenge for integration due to a more complex setup, strategies have to be developed to prevent potential limitations in case diffraction orders are hardly detectable.

The final challenge to overcome is the scalability of the spectrum/angular measurement and matching with a database in order to deduce the geometrical parameters, or at least an OK/NOK. Indeed, if it is easy to compare a given simulated spectrum with a measured spectrum offline, this is not sufficient for in-line measurement during process. A full invert model needs to be built with a large spectrum database, capable of retro-finding the geometrical parameters from a measured spectrum. Not only this model needs to accurately predict the geometrical parameters, but it also needs to do it with enough speed that it does not slow down the process, a challenge which will be approached in the near future in order to facilitate the successful implementation of an in-line monitoring technique.

4. Conclusions

Within the PROMETHEUS project, we successfully created a first surface textured using the Direct Laser Interference Patterning (DLIP) technology, which resulted in hydrophobic and hydrophilic surfaces. The used DLIP setup will be further developed with the goal of implementing it on an industry compatible and scalable prototype.

Two inline characterization approaches are currently being developed to validate the DLIP texturization process, in particular scatterometry and diffractometry. Those techniques need to be able to determine the quality of the textures with high speed and high accuracy in order to be successfully implemented inline into the DLIP prototype machine.

Both complementary techniques are currently being studied, and measured spectrum are manually compared with optical model and RCWA simulation. The preliminary results are promising, and both techniques give useful information on the texture's characteristics and quality of the texturing process.

The next steps are to match the measured spectrum with the simulated spectrum, to built-up an invert model in order to retrofit the geometrical parameters from the measured spectrum.

Eventually, the PROMETHEUS project supported by the EU Horizon 2020 project aims to create a scalable prototype that can generate and validate hydrophobic/oleophobic and hydrophilic/oleophilic structures in a way that is relevant for the industry. Such prototype would lead to a large diffusion of new products within the consumer market.

Acknowledgments

This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 825503—PROMETHEUS and from the "Photonics Public Private Partnership" www.photonics21.org.
ORCID iD

R Bola ○ https://orcid.org/0000-0001-7789-3458

References

[1] Yan Y Y, Gao N and Barthlott W 2011 Mimicking natural superhydrophobic surfaces and grasping the wetting process: a review on recent progress in preparing superhydrophobic surfaces Adv. Colloid Interface Sci. 169 80–105
[2] Wong W S Y, Stachurski Z H, Nisbet D R and Tricoli A 2016 Ultra-durable and transparent self-assembly of hierarchical interpenetrated polymer networks ACS Appl. Mater. Interfaces 8 13615–23
[3] Wermuth L, Kolb M, Mertens T, Strobll T and Raps D 2015 Superhydrophobic surfaces based on self-organized TiO2-nanotubes Prog. Org. Coat. 87 242–9
[4] Cardoso J T, García-Girón A, Romano J M, Huerta-Murillo D, Jagdheesh R, Walker M, Dimov S S and Ocaña J I 2017 Influence of ambient conditions on the evolution of wettability properties of an IR-, ns- and fs-laser textured aluminium alloy RSC Adv. 7 39617–27
[5] García-Girón A, Romano J M, Liang Y, Dashbirozog B, Dong H, Penchey P and Dimov S S 2018 Combined surface hardening and laser patterning approach for functionalising stainless steel surfaces Appl. Surf. Sci. 439 516–24
[6] Romano J-M, Guckur M, Garcia-Giron A, Martinez-Solanas E, Whiteside B R and Dimov S S 2019 Mechanical durability of hydrophobic surfaces fabricated by injection moulding of laser-induced textures Appl. Surf. Sci. 476 830–60
[7] Chen F, Zhang D, Yang Q, Yong J, Du G, Si J, Yun F and Hou X 2013 Bioinspired wetting surface via laser microfabrication ACS Appl. Mater. Interfaces 5 6777–92
[8] Jansen F, Budnicki A and Sutter D 2018 Pulsed Lasers for Industrial Applications Laser Tech. J. 46–9
[9] Arnalado D et al 2010 Picosecond laser machined designed patterns with anti-ice effect Lpm 2010 9–12
[10] Wu B, Zhou M, Li J, Ye X, Li G and Cai L 2009 Superhydrophobic surfaces fabricated by microstructuring of stainless steel using a femtosecond laser Appl. Surf. Sci. 256 61–6
[11] Long J, Fan P, Gong D, Jiang D, Zhang H, Li L and Zhong M 2015 Superhydrophobic surfaces fabricated by femtosecond laser with tunable water adhesion: from lotus leaf to rose petal ACS Appl. Mater. Interfaces 7 9858–65
[12] De Loor R 2013 Polygon scanner system for ultra short pulsed laser–micro-machining applications Physica Procedia 41 544–51
[13] Kuang Z, Liu D, Perrie W, Edwardson S, Sharp M, Fearon E, Deardern G and Watkins K 2009 Fast parallel diffractive multi-beam femtosecond laser surface micro-structuring Appl. Surf. Sci. 255 6582–8
[14] Nakata Y 2016 Interference laser processing Adv. Opt. Techn. 2016 2–6
[15] Voiisat B, Gedvils A, Indrišinas S and Picosecond-laser R G 2013 4-beam-interference ablation as a flexible tool for thin film microstructuring Physica Procedia 12 116–24
[16] Oliver J F, Huhi C and Mason S G 1976 The apparent contact angle of liquids on finely grooved solid surfaces-A SEM study J. Adhes. 8 223–34
[17] Arumugam V et al 2018 Innovative approach for suppressing corrosion of SS304 steel in saline water environment Anti-Corrosion Methods and Materials 76 484–91
[18] Tutela A et al 2007 Designing Superoleophobic Surface Science 318 1618–22
[19] Babooram S 2013 Superhydrophobic and superhydrophilic surfaces Technical Report
[20] Yuan Y et al Contact Angle and Wetting Properties Surface Science Techniques (Berlin: Springer) pp 3–34
[21] Kanna R et al 2017 Analysing contact angle of different fluids present in petroleum reservoirs international refereed J. Eng. Sci. 6 32–6
[22] Madsen M H and Hansen P E Optics Express 24 1109–17
[23] Moharam M G, Grann E B, Pommet D A and Gaylord T K 1995 J. Opt. Soc. Am. A 12 1068–76
[24] Gross H, Model R, Bär M, Wurm M, Bodermann B and Rothsfeld A 2006 Measurement 39 782–94
[25] Feidenhans’l N A 2016 Optical Characterization of Nanostructured Surfaces (Kongens Lyngby: DTU Nanotech)
[26] Raymond C 2005 Overview of scatterometry applications in high volume silicon manufacturing AIP Conf. Proc. 788 398
[27] Kreuzer M et al 2018 In-line metrology for roll-to-roll UV assisted nanoimprint lithography using diffractionpectroscopy Appl. Material 12 058502
[28] Hansen P-E, Madsen M H, Lehtolahti J and Nielsen I 2017 Traceable Mueller polarimetry and scatterometry for shape reconstruction of grating structures Appl. Surf. Sci. 421 471–9
[29] Moharam M G et al 1995 Formulation for stable and efficient implementation of the rigorous coupled-wave analysis of binary gratings J. Opt. Soc. Am. 12 1068–76
[30] Tamulevičius T et al 2018 Dot-matrix hologram rendering algorithm and its validation through direct laser interference Patterning 2 14245
[31] Robert S et al 2002 Characterization of optical diffraction gratings by use of a neural method J. Opt. Soc. Am. A 19 24–32
[32] Kallioniemi I, Saarinen J and Oja E 1998 Optical scatterometry of subwavelength diffraction gratings: neural-network approach Appl. Opt. 37 5830–5
[33] Moharam M G and Gaylord T K 1982 Diffraction analysis of dielectric surface-relief gratings J. Opt. Soc. Am. 72 1385–92
[34] Delgado García T et al 2019 Fabrication of micro/nano fluidic silicon moulds by a mix-and-match methodology Proc. ICALOE in press