Design of CW THz Photonic Transmitter based on Low Pass-Filter and Bow-tie Wideband Antenna

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ABSTRACT
This paper presents the design of Continuous Wave Terahertz photonic transmitters which is composed from photodetector (PD) associated to a wideband antenna, low–pass filter (LPF) and DC Probe. Firstly, we have developed the bow-tie wideband antenna using an EM solver Momentum integrated in ADS “Advanced Design System”. Then we had optimized a low-pass filter which is responsible of blocking the RF signal providing from the antenna to reach the DC probe. And finally, we have validated into simulation the CW THz photonic transmitter. The three structures are based on multi-layers GaAs substrate, which is the most widely used for THz circuit design. The dimensions of the Whole circuit are 776.788 × 303.39 μm².

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1. INTRODUCTION
We remark in the recent years the big interest giving to the terahertz technology. Before the THz domain was ignored due to a lot of difficulties related to the generation and detection. But with the development of the modern Femtosecond Lasers and High-Speed Photodetectors the situation was changed. A diversity of domains such as biomedical imaging, spectroscopy, Security and telecommunications are focus now theirs applications on THz waves which presented several advantages based on interactivity with the material where it spreads and fast absorption by the atmosphere [1].

To generate the THz waves many methods are proposed but the most used is the one that relays on the coplanar waveguide (CPW) photonic transmitters [2]. The CPW technology offers in fact several advantages due to its features, like low radiation, low dispersion, easy of shunts and series connections [3]. This paper presents a new study of a THz photonic transmitter composed from a photodetector associated to the broadband antenna inserts in series with a low pass filter and a DC Probe. This paper is divided on two parts, the first one is reserved to the theory of different components of the system and the second part presents the design of devices and discussion of simulation results.

2. RESEARCH METHOD
A PD is a sensor its role is to convert an optical power into an electrical current. To generate electron-hole-pairs, the photon energy provides from the light absorbed in a PD must be at last equal to the bandgap energy Eg of the absorber material [4]. This available energy of one photon is sufficient to excite an electron from the valence band (v.b.) to the conduction band (c.b.). For this band-to-band transition, the upper
wavelength limit for photon absorption is given by [4]:

\[ \lambda_g [\mu m] = \frac{1.24}{E_g [eV]} \] (1)

A PD has different properties such as:

- Sensitivity: The ability of the photodiode to transform light absorbed into an electrical current in other term the number of charge carrier pairs generated per incident photon [4].

\[ \eta_{ext} = \frac{I_{pd}}{q} \frac{hv}{P_{opt}} \] (2)

- Responsivity: The external responsivity R is the ratio of photocurrent to the input optical power [4]:

\[ R = \frac{I_{pd}}{P_{opt}} = \eta_{ext} \frac{\lambda_{\mu m}}{1.24} A/W \] (3)

Where R depends on the state of polarization of the incoming light, the definition of the polarization dependent loss (PDL) is useful [4]:

\[ \text{PDL} = 10 \cdot \log \left( \frac{R_{max}}{R_{min}} \right) \text{dB} \] (4)

With \( R_{max} \) and \( R_{min} \) are the maximum and minimum responsivities for all states of polarization.

In order to evaluate the high-speed photodiode, the electrical 3dB bandwidth is used. It specifies the frequency range from DC to the cut-off frequency \( f_{3dB} \). The bandwidth of a lumped element photodiode, at which the device length is much shorter than the electrical signal wavelength, might be limited mainly by the RC-time constant and the carrier drift times in the depletion region. These bandwidth constraints lead to a 3dB bandwidth which can be approximated by [4]:

\[ f_{3dB} \approx \frac{1}{\sqrt{\frac{1}{f_{RC}} + \frac{1}{f_t}}} \] (5)

With the RC limited bandwidth.

\[ f_{RC} = \frac{1}{2\pi R_{tot}C_{pd}} \] (6)

And the carrier transit time limited bandwidth.

\[ f_t = \frac{3.5 \bar{v}}{2\pi d_{abs}} \] (7)

\( R_{tot} \) stands for the photodiodes’s total resistance including series and load resistances.
\( C_{pd} \) is the junction capacitance.

\[ \bar{v} = \sqrt{\frac{2(1/v_e^2 + 1/v_h^2)^{-1}}{\frac{1}{v_e} + \frac{1}{v_h}}} \] is the averaged carrier drift velocity with the electron and hole velocities \( v_e \) and \( v_h \).
\( d_{abs} \) : The absorber thickness [4].

2.1. Photodetector structures

There is a different structure of high speed detectors which are shown in Figure 1:

In our case we used the Metal Semiconductor-Metal Traveling wave Photodetector (MSM-TPD) by reason of its high power-bandwidth and coplanar-waveguide fed slot owing to its easy connection with planar devices [5]. The PD based on GaAs substrate which characterized by a succession of layers as mentioned in the Figure 2 [6]:

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2.2. THz wideband antenna

The antenna is one of the most important elements in the design of CPW photonic transmitter [7], [8]. Its role focuses on the transmission of RF signals providing from PD.

In this work we choose the Bowtie design for the antenna which is a planar version of the well known biconical antenna [2]. This antenna type gives a wideband frequency transmission in the THz domain. Figure 3 shows the proposed antenna structure.

To optimize the final antenna structure we have used Momentum integrated in ADS [9]. After many series of optimization by using many methods as Random and gradient, we have validated the structure depicted in Figure 3. The Table 1 presents different parameters of the optimized Bowtie antenna.

Figure 4 presents the reflection coefficient of the validated antenna with the matching input impedance below -10dB between 1THz and 1.25THz. That makes it suitable for THz CW photonic transmitters.

To study the radiation behavior of the antenna we have launched a 3D simulation at 1.22 THz in ADS, we obtain the radiation diagram which shows that the antenna is bidirectional as shown in Figure 5.
Table 1. Values of Design Parameters

| Parameter | Value (µm) |
|-----------|------------|
| L1        | 147.26     |
| L2        | 330        |
| L3        | 223.497    |
| W1        | 5          |
| W2        | 100.23     |
| W3        | 132.71     |
| W4        | 11.75      |

Table 2. Unit Cell of Periodic Structure CPW Low-Pass Filter Parameters

| Parameter | Value (µm) |
|-----------|------------|
| L1        | 77.61      |
| L2        | 30.28      |
| L3        | 25.70      |
| W1        | 20.77      |
| W2        | 25         |
| W3        | 5          |
| W4        | 15.5       |

2.3. Low-pass filter (LPF)

The integration of the Low Pass Filter into the CW photonic transmitter system is mandatory. It works like an inductance which role reside in blocking the RF signal providing from PD and transmitting via antenna to reach the DC probe.

In this paper we choose a several periodic structure presenting in the study [10] with the aim to increase the rejection band and to obtain a low insertion loss in the pass-band along a CPW line as demonstrated in [11]. The proposed structure is composed from three units as shown in Figure 6 and dimensions are presented in Table 2.

The idea was to validate a THz low pass filter based on this cell by enlarging the rejected band. Therefore, we have validated into simulation after the optimization of this structure in Momentum by achieving a periodic low pass filter (LPF) based on the unit cell presents in Figure 7. This final filter is mounted on a multilayers GaAs substrate [6].

Figure 3. The Bowtie antenna structure

Figure 4. Reflection coefficient versus frequency

Figure 5. The radiation pattern at 1.22 THz

Figure 6. Unit cell of periodic structure CPW low-pass Filter

Figure 7. Unit cell of periodic structure CPW low-pass Filter

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The Table 3 resumes the different dimensions of the proposed LPF.

| Parameter | Value (µm) |
|-----------|------------|
| L1        | 228.47     |
| L2        | 42.61      |
| L3        | 15.14      |
| W1        | 24.02      |
| W2        | 114.01     |
| W3        | 6          |

Table 3. Values of Filter Parameters

Figure 7. The layout of the periodic LPF THz structure

Figure 8 demonstrates that the achieved LPF presents a good low insertion loss, with a cutoff frequency of 0.67 THz and a wide rejection band until 1.35 THz, which makes the proposed “LPF” able to work in THz domain and to be insert into a THz system of CW photonic transmitters [10].

To validate the function of the “LPF” structure we have launched a 3D simulation in ADS at 0.55 THz in the frequency passband and at 1 THz in the rejection frequency band. As a result, we can see from Figure 9(a) that we have a flow of energy from port 1 to port 2 and for Figure 9(b) the energy is stopped to reach the port 2.

Figure 8. Simulation S-parameters results versus frequency

Figure 9. The current density @ (a) 0.55 THz and (b) 1 THz
2.4. CW Photonic transmitter simulation

After the simulation of the antenna and the filter separately, we have connected the photodetector to the system composed from the antenna, the filter and DC probe responsible for the polarization. The global system named CW photonic transmitter for generation of THz signal is presented in Figure 10.

Table 5 shows the values of DC probe parameters.

Table 5. Values of DC Probe Parameters

| Parameter | Value (µm) |
|-----------|------------|
| L1        | 60.74      |
| L2        | 62.91      |
| L3        | 88.77      |
| W1        | 36.88      |
| W2        | 110.64     |

Figure 10. The proposed CW photonic transmitter

As mentioned, we have associated the antenna, LPF with the DC probe having the optimized dimensions illustrated in Table 6. As shown in Figure 11, the simulation of the final CW THz photonic transmitter permits to validate this circuit between 750 GHz and 980 GHz.

Figure 11. Simulation S-Parameters results versus frequency

After the validation of this THz photonic transmitter into simulation we have done a comparison between the proposed THz antenna which is the key of the THz source and with another THz antennas validated in literature. The table below presents the comparison of the performances (dimensions, frequency bandwidth) between the proposed antenna and two others structures:

As shown in table 6, the proposed antenna presents good performances in term of bandwidth with an acceptable miniature length.

Table 6. Comparaison of the Antenna structures

| Antenna Structure | Length  | Frequency Bandwidth          |
|-------------------|---------|------------------------------|
| Proposed Antenna  | 330 µm  | [THz,1.25THz]                |
| Antenna [12]      | 200 µm  | Narrow band at 645 Ghz      |
| Antenna [13]      | 1040 µm | Narrow band at 850 Ghz      |
3. CONCLUSION

This paper presented a CW photonic transmitter used for generation of THz waves. To obtain the final target we have follow four main steps. Firstly, we have chosen the photodector, in our case we have used MSM-TPD. Secondly we have optimized the Bowtie antenna to be able to transmit and receive THz signal. In the third step, we have validated the “LPF” as an inductance to block the RF signal from reaching the DC probe. And finally, we have generated and optimized the whole CW THz photonic transmitter by using an electromagnetic solver Momentum integrated in ADS. The final circuit is mounted on a multilayers GaAs substrate and having an area around 776.788 × 303, 39 µm².

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