Integral Reinforcement Learning Control for a Class of High-Order Multivariable Nonlinear Dynamics With Unknown Control Coefficients

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ABSTRACT

This paper develops an integral reinforcement learning (IRL) controller for a class of high-order multivariable nonlinear systems with unknown control coefficients (UCCs). A new long-term performance index is first presented, and then the critic neural network (NN) and the action NN are presented to estimate the unobtainable long-term performance index and the unknown drift of systems, respectively. By combining the critic and action NNs with Nussbaum-type functions, the IRL controllers for high-order, nonsquare multivariable systems are proposed to cope with the problem of UCCs. The analysis are given to illustrate that the stability of the closed-loop system can be obtained, and the signals of the closed-loop systems are semiglobally uniformly ultimately bounded (UUB). Finally, one simulation example is provided to show the effectiveness of the proposed IRL controllers.

INDEX TERMS
Nussbaum-type functions, integral reinforcement learning, unknown control coefficients, nonsquare multivariable systems.

I. INTRODUCTION

Adaptive control of multivariable systems has attracted significant attention in the last several decades, where the design of control laws is much more challenging than the single-input systems due to the dynamic couplings of the high-frequency gain matrix [1], [2]. In general, the high-frequency gain matrix of these works are known in advance to design controllers. However, some practical systems cannot possess the knowledge of the high-frequency gain matrix priori, see for example, in [3]–[5]. Hence, one of fundamental problems of multivariable systems is how to deal with the unknown high-frequency gain matrix known as UCCs, which makes the extension from single-input systems to multivariable systems far from trivial.

To address the problem of UCCs, one of effective methods is employing Nussbaum-type functions, which was first proposed in [6] to deal with single-input systems with UCCs, and then extended to deal with various single-input dynamics [7]–[10]. However, when multiple control inputs with UCCs are considered, i.e., in multivariable systems, one critical challenge is how to deal with the problem of multiple Nussbaum-type functions, where the effects of Nussbaum-type functions may counteract each other. Attempts to cope with this problem, the work of [11] proposed an adaptive control scheme for the strict-feedback system, where a new designed Nussbaum-type function was introduced to allow multiple Nussbaum-type functions in a single inequality. However, the method of [11] still cannot be directly extended to multivariable systems. Furthermore, the authors in [12] suggested to construct a partial Lyapunov function for each control input where only one Nussbaum-type function exists. Inspired by this idea, some extended results were applied to multi-agent systems with UCCs [13]–[15]. Although the whole multi-agent system can be regarded as a multivariable system, it still needs more efforts to make an extension to the case of general multivariable systems. To completely solve this issue, the work of [16] designed a novel adaptive control algorithm for uncertain multivariable systems by using the backstepping control technique. In addition to employ Nussbaum-type functions, there are some other methods to
A. PRELIMINARIES

Definition 1 [61]: A function \( N(\cdot) \) is the Nussbaum-type function if

\[
\begin{align*}
\lim_{k \to \infty} \sup \left( \frac{1}{k} \int_0^k N(\tau) d\tau \right) &= +\infty \\
\lim_{k \to \infty} \inf \left( \frac{1}{k} \int_0^k N(\tau) d\tau \right) &= -\infty.
\end{align*}
\]

Lemma 1 [31]: Suppose \( V(\cdot) \) and \( k(\cdot) \) are smooth functions over \([0, t_f]\) satisfying \( V(t) \geq 0 \ \forall t \in [0, t_f] \), \( N(\cdot) \) is the Nussbaum-type function, and \( \phi \) is some nonzero constant. If we have

\[
V(t) \leq \int_0^t \left( \phi N(k(\tau)) + 1 \right) k(\tau) d\tau + c, \quad \forall t \in [0, t_f]
\]

where \( c \in \mathbb{R} \) is a constant, then \( V(t) \), \( k(t) \) and \( \int_0^t \phi N(k(\tau)) d\tau \) are bounded on \([0, t_f]\).

We will present some basic knowledge on radial basis function neural network (RBFNN), and by which we can approximate any continuous nonlinear functions. In view of [32], we can use the RBFNN to approximate a continuous function \( h(x) : \mathbb{R}^q \to \mathbb{R} \) by

\[
h_{\text{RBF}}(x) = W^T \Psi(x),
\]

where \( x \in \Omega_\epsilon \subset \mathbb{R}^q \) is the vector of input, \( W \in \mathbb{R}^l \) is the vector of weight, \( l \geq 1 \) is the node number of neural network, and \( \Psi(x) = [\psi_1(x), \psi_2(x), \ldots, \psi_l(x)]^T \) with \( \psi_i(x), i = 1, 2, \ldots, l \) being the Gaussian function as

\[
\psi_i(x) = \exp \left[ -\frac{(x - \mu_i)^T (x - \mu_i)}{\eta_i^2} \right],
\]

where \( \mu_i = [\mu_{i1}, \mu_{i2}, \ldots, \mu_{il}]^T \) is the center of receptive field and \( \eta_i \) is the width of the Gaussian function. It is known [33] that if \( l \) is sufficiently large, (3) can approximate any continuous nonlinear functions on \( \Omega_\epsilon \subset \mathbb{R}^q \) with any accuracy

\[
h(x) = W^*^T \Psi(x) + \epsilon, \quad \forall x \in \Omega_\epsilon,
\]

where the ideal weight is \( W^* \) and \( \epsilon \) is the approximation error. Furthermore, there exist ideal unknown, constant weights \( W^* \) such that \( |\epsilon| \leq \epsilon^* \) with constant \( \epsilon^* > 0 \) for all \( x \in \Omega_\epsilon \). Furthermore, let \( \hat{W} \) be the estimate of \( W^* \), then the weight estimation error can be defined as \( \hat{W} = \hat{W} - W^* \).

In order to derive main results of this study, the following lemmas are needed:

Lemma 2 [29]: For any two matrices \( A = (a_{ij})_{m \times n} \in \mathbb{R}^{m \times n} \) and \( B = (b_{ij})_{m \times n} \in \mathbb{R}^{m \times n} \), one has \( \text{tr}(AB) \leq ||A||_F ||B||_F \). Furthermore, it is known that \( \text{tr}(A^T A) = ||A||_F^2 \) and \( ||A^T B||_F \leq ||A||_F ||B||_F \). For any \( a \in \mathbb{R}^m \) and \( b \in \mathbb{R}^n \), one has \( a^T b \leq ||a|| ||b|| \) and \( ||Aa||_F \leq ||A||_F ||a|| \).

Lemma 3 [34]: Let \( S \in \mathbb{R}^{m \times m} \) be a matrix, and \( x \in \mathbb{R}^m \) is a nonzero vector. If we define \( \kappa = \frac{x^T S x}{x^T x} \), then at least one eigenvalue of matrix \( S \) is in \((-\infty, \kappa]\) and at least one in \([\kappa, +\infty)\).
B. PROBLEM FORMULATION

Consider a continuous-time high-order nonlinear system with nth-order \( (n \geq 1) \) as

\[
\dot{x}(t) = f(\bar{x}(t)) + g(\bar{x}(t)) u(t) + d(t)
\]

where \( \bar{x}(t) = [x(t), \dot{x}(t), \ldots, x^{(n-1)}(t)]^T \) with \( x(t) \in \mathbb{R}^k \), \( x^{(m)}(t) \in \mathbb{R}^l \), \( m = 1, 2, \ldots, n - 1 \) being the mth derivative of the system state. The smooth function \( f(\bar{x}(t)) \in \mathbb{R}^k \) represents an unknown nonlinear drift, \( g(\bar{x}(t)) \in \mathbb{R}^{k \times l} (k \leq l) \) is the high-frequency gain, \( d(t) \in \mathbb{R}^k \) is the unknown, bounded disturbance, and \( u(t) \in \mathbb{R}^l \) represents the control input.

The aim is to design IRL controllers for high-order nonlinear system (6) such that the stability is guaranteed, i.e.,

\[
\begin{align*}
\lim_{t \to \infty} x(t) &= 0_{k \times 1} \\
\lim_{t \to \infty} x^{(m)}(t) &= 0_{k \times 1}
\end{align*}
\]

for \( m = 1, 2, \ldots, n - 1 \). Furthermore, all the signals of the closed-loop system are semiglobally UUB.

III. MAIN RESULTS

In this section, we present IRL controllers for high-order nonlinear system with UCCs. To facilitate the design procedure, we first introduce the following state variables,

\[
\theta(t) = \left( \beta + \frac{d}{dt} \right)^{n-1} x(t)
\]

and

\[
\vartheta(t) = \left( \beta + \frac{d}{dt} \right)^{n-1} \dot{x}(t) + \left( \beta + \frac{d}{dt} \right)^{n-2} \ddot{x}(t) + \cdots + C_{n-1}^n \beta x^{(n-2)}(t) + C_{n-1}^n x^{(n-1)}(t)
\]

where \( \beta > 0 \) is a constant, and \( C_i^j \) is coefficients of the binomial expansion.

In what follows, the following assumption is needed.

Assumption 1: The matrix \( g(\bar{x}(t)) \) is nonsquare and partially unknown with

\[
g(\bar{x}(t)) = g_0(\bar{x}(t)) g_a(\bar{x}(t)),
\]

where the matrix \( g_0(\bar{x}(t)) \in \mathbb{R}^{k \times l} \) is known, bounded with full row rank, and the matrix \( g_a(\bar{x}(t)) \in \mathbb{R}^{l \times l} \) is unknown. Furthermore, the matrix \( g_0(\bar{x}(t)) [g_a(\bar{x}(t)) + g_0^T(\bar{x}(t))] \)

\[
g_0^T(\bar{x}(t)) \) is either positive or negative definite.

According to Lemma 3 with Assumption 1, we have

\[
\rho(t) \| \sigma(t) \|^2 = \frac{1}{2} \| g_0(\bar{x}(t)) \|_F^2 \sigma^T(t) g_0(\bar{x}(t)) \times (g_a(\bar{x}(t)) + g_0(\bar{x}(t))) g_a^T(\bar{x}(t)) \sigma(t)
\]

where \( \lambda_{\min} \leq \rho(t) \leq \lambda_{\max} \), \( \lambda_{\min} \) and \( \lambda_{\max} \) are respectively the minimum and maximum eigenvalues of the matrix \( g_0(\bar{x}(t)) [g_a(\bar{x}(t)) + g_0^T(\bar{x}(t))] g_0^T(\bar{x}(t)) \), and \( \sigma(t) \) is defined in (8). From Assumption 1 and the definition of (11), we know that the sign of \( \rho(t) \) is nonzero, constant but unknown.

1) CRITIC NN DESIGN

A long-term performance index is proposed as

\[
J_s(t) = \int_t^\infty \gamma^{t - t_0} \rho(\sigma(t)) \rho(t) dt,
\]

where \( \rho(\sigma(t)) = [\rho(\sigma_1(t)), \rho(\sigma_2(t)), \ldots, \rho(\sigma_k(t))]^T \) with \( \rho(\sigma_i(t)) = \tanh(\sigma_i^2(t)) \). To construct the Bellman error for system (6), we define

\[
J_s(t - T) = \int_t^{t - T} \gamma^{t - t_0} \rho(\sigma(t)) \rho(t) dt = \int_t^{t - T} \gamma^{t - t_0} \rho(\sigma(t)) \rho(t) dt
\]

with

\[
\rho_{sc} = \int_t^{t - T} \gamma^{t - t_0} \rho(\sigma(t)) \rho(t) dt,
\]

where \( \rho_{sc} \) represents the value cost on \( [t - T, t] \). It is known that \( \rho_{sc} = \rho_{sc_1}, \rho_{sc_2}, \ldots, \rho_{sc_k} \) \( \rho_{sc} = \int_t^{t - T} \gamma^{t - t_0} \rho(\sigma(t)) \rho(t) dt \leq \int_t^{t - T} \gamma^{t - t_0} \rho(\sigma(t)) \rho(t) dt \]

which implies \( \| \rho_{sc} \| \leq d_{\rho_{sc}} \) with a positive constant \( d_{\rho_{sc}} \). Furthermore, it is seen from (12) that \( J_s(t) \) contains future dynamical information. Then, the RBFNN is adopted to approximate it, i.e.,

\[
J_s(t) = W_{sc}^T \Psi_{sc}(x_{sc}(t)) + \epsilon_{sc}(x_{sc}(t)), \quad \forall x_{sc} \in \Omega_{x_{sc}},
\]

where the bounded ideal weight is \( W_{sc}^* \) satisfying \( \| W_{sc}^* \|_F \leq d_{w_{sc}} \). The RBF vector \( \Psi_{sc}(x_{sc}(t)) \) is bounded with \( \| \Psi_{sc}(x_{sc}(t)) \| \leq d_{\psi_{sc}} \), and the approximation error \( \epsilon_{sc}(x_{sc}(t)) \) is bounded with \( \| \epsilon_{sc}(x_{sc}(t)) \| < d_{\epsilon_{sc}} \). In general, the weight \( W_{sc}^* \) is unknown. Therefore, we have to estimate \( J_s(t) \) by

\[
\hat{J}_s(t) = \hat{W}_{sc}^T \hat{\Psi}_{sc}(x_{sc}(t))
\]

and \( J_s(t - T) \) is estimated by

\[
\hat{J}_s(t - T) = \hat{W}_{sc}^T \hat{\Psi}_{sc}(x_{sc}(t - T)),
\]

where \( x_{sc}(t) = \hat{x}(t) \). In what follows, we design the updated law of weight \( \hat{W}_{sc} \). A difference error of the long-term performance index is defined as

\[
e_{sc} = \hat{J}_s(t) - \gamma \hat{J}_s(t - T) - \rho_{sc} = \hat{W}_{sc} \Delta \Psi_{sc}(t) + \rho_{sc} + W_{sc}^* \Delta \Psi_{sc}(t),
\]

where \( \Delta \Psi_{sc}(t) = \Psi_{sc}(x_{sc}(t)) - \hat{\Psi}_{sc}(x_{sc}(t) - T) \) and \( \hat{\Psi}_{sc} = \hat{W}_{sc} - W_{sc}^* \). Then, \( \hat{\Psi}_{sc} \) is updated by

\[
\hat{\Psi}_{sc} = -\Pi_{sc} \Delta \Psi_{sc}(t) [\hat{W}_{sc}^T \Delta \Psi_{sc}(t) + \rho_{sc}]^T - \delta_{sc} \Pi_{sc} \hat{\Psi}_{sc},
\]

where \( \Pi_{sc} > 0 \) and \( \delta_{sc} > 0 \) is to be prescribed. The first term of (19) is to minimize the critic error \( \| \epsilon_{sc} \| \), and the second term is a modification term to make (19) robust to the disturbances [35].
2) ACTION NN DESIGN
To design the action NN, the RBFNN is first established to approximate the unknown function \( f(\tilde{x}(t)) \), i.e.,

\[
f(\tilde{x}(t)) = W_{sa}^{*T} \psi_{sa}(x_{sa}(t)) + \epsilon_{sa}(t), \quad \forall x_{sa} \in \Omega_{x_{sa}}, \tag{20}
\]

where the ideal weight is \( W_{sa}^{*} \) satisfying \( \| W_{sa}^{*} \| = d_{sa} \), the RBF vector \( \psi_{sa}(x_{sa}(t)) \) satisfies \( \| \psi_{sa}(x_{sa}(t)) \| \leq d_{sa} \), and \( \epsilon_{sa}(t) \) with \( \| \epsilon_{sa}(x_{sa}(t)) \| < d_{sa} \) is the approximation error. Since the weight \( W_{sa}^{*} \) is unknown, we must estimate \( f(\tilde{x}(t)) \) by

\[
\hat{f}(\tilde{x}(t)) = \hat{W}_{sa}^{T} \psi_{sa}(x_{sa}(t)), \tag{21}
\]

where \( x_{sa}(t) = \tilde{x}(t) \). Then, \( N \) is designed and \( J_{i}(t) \) approach to zero, which implies the state \( x(t) \) and its derivatives \( x^{(m)}(t) \), \( m = 1, 2, \ldots, n-1 \) converge to zero. In this way, we define the action error as

\[
e_{sa} = \sigma(t) + J_{i}(t) = \sigma(t) + \hat{W}_{sc}^{T} \psi_{sc}(x_{sa}(t)). \tag{22}
\]

Then, \( \hat{W}_{sa} \) is updated by

\[
\dot{\hat{W}}_{sa} = \Pi_{sa} \psi_{sa}(x_{sa}(t)) \left[ (\sigma(t) + \hat{W}_{sc}^{T} \psi_{sc}(x_{sa}(t)))^{T} - \delta_{sa} \Pi_{sa} \hat{W}_{sa} \right], \tag{23}
\]

where \( \Pi_{sa} > 0 \) and \( \delta_{sa} > 0 \) is to be designed. Define \( \hat{W}_{sa} = \hat{W}_{sa} - W_{sa}^{*} \). Similarly, the first term of (23) is to minimize the action error \( \| e_{sa} \| \), and the second term is a modification term to make (23) robust to the disturbances [35].

Based on the above critic and action NNs, the IRL controller for nonsquare multivariable systems with UCCs can be proposed as

\[
u(t) = N(\chi(t)) g_{0}(\tilde{x}(t)) \sigma(t) \sigma^{T}(t) \tilde{u}(t) + \mu(t) \tag{24}
\]

with

\[
\begin{align*}
\dot{\chi}(t) &= \sigma^{T}(t) \tilde{u}(t) \\
\tilde{u}(t) &= \tilde{x}(t) + \tilde{\varphi}(t) + \hat{W}_{sc}^{T} \psi_{sc}(x_{sa}(t))
\end{align*} \tag{25}
\]

and

\[
\begin{align*}
\dot{\varphi}(t) &= \psi(t) \tanh(\sigma(t) \lambda_{1}) + \sigma(t) \\
\varphi(t) &= \sigma^{T}(t) \tanh(\sigma(t) \lambda_{1})
\end{align*} \tag{26}
\]

where \( \lambda_{1} = 1 + t^{2} \), and \( \tanh(\cdot) \) is the hyperbolic tangent function. Then, the stability results for the controller (24) are summarized as follows:

**Theorem 1:** Consider a continuous-time nonsquare multivariable system with UCCs given in (6) satisfying Assumption 1. The IRL controller (24), (25) and (26) with the critic NN (16) and (19), and the action NN (21) and (23) can achieve the objective (7) if the designed parameters are properly chosen, i.e.,

\[
\begin{align*}
\delta_{sa} &\geq d_{\psi_{sa}}^{2} \\
\delta_{sc} &\geq d_{\psi_{sc}}^{2}
\end{align*} \tag{27}
\]

Furthermore, all signals of the closed-loop system are semiglobally UUB.

**Proof:** Considering the following positive definite function

\[
V_{i}(t) = \frac{1}{2} \sigma^{T}(t) \sigma(t) + \frac{1}{2} \text{tr} \left( \hat{W}_{sa}^{T}(t) \Pi_{sa}^{-1} \hat{W}_{sa}(t) \right) + \frac{1}{2} \text{tr} \left( \hat{W}_{sc}^{T}(t) \Pi_{sc}^{-1} \hat{W}_{sc}(t) \right) + \frac{1}{2} \dot{\varphi}^{2}(t), \tag{28}
\]

where we have defined \( \hat{W}_{sa}(t) = \hat{W}_{sa}(t) - W_{sa}^{*}, \hat{W}_{sc}(t) = \hat{W}_{sc}(t) - W_{sc}^{*}, \hat{\varphi}(t) = \varphi(t) - (D + d_{sa}) \) and \( D > 0 \) is the unknown upper bound of the two-norm of \( \| \dot{d}(t) \| \). Furthermore, the elements of vector \( \sigma(t) \) are defined as \( \sigma_{i}(t) \) for \( i = 1, 2, \ldots, k \).

Let define \( V_{1}(t) = \frac{1}{2} \sigma^{T}(t) \sigma(t) + \frac{1}{2} \dot{\varphi}^{2}(t) \), \( V_{2}(t) = \frac{1}{4} \text{tr} \left( \hat{W}_{sa}^{T}(t) \Pi_{sa}^{-1} \hat{W}_{sa}(t) \right) \) and \( V_{3}(t) = \frac{1}{4} \text{tr} \left( \hat{W}_{sc}^{T}(t) \Pi_{sc}^{-1} \hat{W}_{sc}(t) \right) \). By employing (24), (25) and (26) with the critic NN (16) and (19), and the action NN (21) and (23), we have

\[
\begin{align*}
\dot{V}_{1}(t) &= \sigma^{T}(t) \dot{\sigma}(t) + \dot{\varphi}(t) \dot{\varphi}(t) \\
&= \sigma^{T}(t) \left[ f(\tilde{x}(t)) + g(\tilde{x}(t)) u(t) + d(t) + \sigma(t) \| \dot{d}(t) \| \right] \\
&= \sigma^{T}(t) \left[ (\rho(t) N(\chi(t)) + 1) \dot{\chi}(t) - \sigma^{T}(t) \sigma(t) \\
&- \sigma^{T}(t) \hat{W}_{sa}^{T}(t) \psi_{sa}(x_{sa}(t)) \right] \\
&+ \sigma^{T}(t) [d(t) + \epsilon_{sa}(t)] \\
&- \sigma^{T}(t) \tanh(\sigma(t) \lambda_{1}) (D + d_{sa}) \\
&\leq [\rho(t) N(\chi(t)) + 1] \dot{\chi}(t) \\
&- \sigma^{T}(t) \hat{W}_{sa}^{T}(t) \psi_{sa}(x_{sa}(t)) + (D + d_{sa}) \\
&\times \sum_{i=1}^{k} \| \sigma(t) \| \tanh(\sigma(t) \lambda_{1}) \\
&\leq [\rho(t) N(\chi(t)) + 1] \dot{\chi}(t) + \frac{0.285}{\lambda_{1}} k (D + d_{sa}) \\
&- \sigma^{T}(t) \hat{W}_{sa}^{T}(t) \psi_{sa}(x_{sa}(t)),
\end{align*} \tag{29}
\]

where we have used \( |y| - y \tanh(\gamma_{1}y) \leq 0.2785/\gamma_{1} \). Furthermore, we have from \( V_{2}(t) = \frac{1}{2} \text{tr} \left( \hat{W}_{sa}^{T}(t) \Pi_{sa}^{-1} \hat{W}_{sa}(t) \right) \) that

\[
\begin{align*}
\dot{V}_{2}(t) &= \text{tr} \left( \hat{W}_{sa}^{T}(t) \Pi_{sa}^{-1} \dot{\hat{W}}_{sa}(t) \right) \\
&= \text{tr} \left( \hat{W}_{sa}^{T}(t) \Pi_{sa}^{-1} \hat{W}_{sa}(t) \right) \\
&- \delta_{sa} \text{tr} \left( \hat{W}_{sa}^{T}(t) \hat{W}_{sa}(t) \right) \\
&+ \text{tr} \left( \hat{W}_{sa}^{T}(t) \Pi_{sa}^{-1} \hat{W}_{sa}(t) \right) \\
&\leq \text{tr} \left( \hat{W}_{sa}^{T}(t) \Pi_{sa}^{-1} \hat{W}_{sa}(t) \right) \\
&+ d_{\psi_{sa}} d_{\psi_{sc}} \left\| \hat{W}_{sa}(t) \right\| \left\| \hat{W}_{sc}(t) \right\| \tag{30}
\end{align*}
\]
where \( \phi_{V_3} = \frac{d\phi}{dt} \frac{d\phi}{d\psi} \frac{d\psi}{dW} - \delta_3 \psi \phi_{W_3} \). In addition, we have from \( V_3(t) = 2 \left( W_3(t) \right)^{-1} \psi \phi_{W_3} \) that
\[
V_3(t) = 2 \left( W_3(t) \right)^{-1} \psi \phi_{W_3} \\
= 2 \left( W_3(t) \right)^{-1} \psi \phi_{W_3} \\
- \delta_3 \psi \phi_{W_3} \\
\leq - \delta_3 \psi \phi_{W_3} = - \frac{dV_3}{dt} \left( W_3(t) \right) \| \psi \phi_{W_3} \| F 
\] (31)

where \( \psi = (1 + \gamma) \frac{d\phi}{dt} \frac{d\phi}{d\psi} \frac{d\psi}{dW} - 1 + \gamma \frac{d\phi}{dt} \frac{d\phi}{dW} \). Then the derivative of \( V_3(t) \) is given as
\[
\dot{V}_3(t) = \dot{V}_1(t) + \dot{V}_2(t) + \dot{V}_3(t) \\
\leq [\rho(t)N(\chi(t)) + 1] \chi(t) + \frac{0.285}{\lambda_t} k (D + d_e) \\
- \frac{1}{2} \left( \delta_{sa} - \frac{d^2}{d\psi} \right) \left( \psi \phi_{W_3} \right)^2 + \left( \frac{d^2}{d\psi} \right)^2 F \\
- \frac{1}{2} \left( \delta_{sc} - \frac{d^2}{d\psi} \right) \left( \psi \phi_{W_3} \right)^2 + \left( \frac{d^2}{d\psi} \right)^2 F \\
- \frac{1}{2} \left( \psi \phi_{W_3} \right) \left( \psi \phi_{W_3} \right)^2 F \\
\leq [\rho(t)N(\chi(t)) + 1] \chi(t) + \frac{0.2785}{\lambda_t} k (D + d_e) \\
+ \frac{\frac{d^2}{d\psi} + \frac{d^2}{d\psi}}{\lambda_t}, \] (32)

where we have used \( \delta_{sa} \geq \frac{d^2}{d\psi} \) and \( \delta_{sc} \geq \frac{d^2}{d\psi} \) given in (27). Since \( V_3(t) \) and \( \dot{V}_3(t) \) are smooth functions on \([0, T_f]\) with \( V_3(T_{f}) \geq 0 \), using Lemma 1 we have
\[
V_3(t), \dot{V}_3(t), \int_0^t [\rho(t)N(\chi(t)) + 1] \chi(t) dt 
\] (33)
are semiglobally UUB on \([0, T_f]\).

If the designed parameters of the closed-loop system are properly chosen, i.e., the inequality (27), there exists a compact set \( \Omega \) being the domain of attraction. Note that the compact set can be made to include any initial conditions by designing parameters. Therefore, the signals of the closed-loop system are semiglobally UUB.

It is seen that \( \sigma_T(T) \sigma(t) \in L_{\infty}, \sigma(t) \in L_{\infty}, \left( W_{sa}(t) \right)_{F} \in L_{\infty}, \left( W_{sc}(t) \right)_{F} \in L_{\infty}, \) and \( \varphi(t) \in L_{\infty}, \) which implies \( \sigma_T(t) \sigma(t) \) and \( \varphi(t) \in L_{\infty}. \) Thus, we have
\[
\frac{d\sigma_T(T) \sigma(t)}{dt} = \frac{2 \sigma_T(t) \dot{\sigma}(t)}{2 \sigma_T(t) \dot{\sigma}(t)} \\
= \frac{2 \dot{V}_1(t) - \dot{\varphi}(t) \dot{\varphi}(t)}{L_{\infty}, \text{ which means } \sigma_T(t) \in L_{\infty}. \text{ Meanwhile, it is seen from (29) that } \int_0^T \sigma_T(t) \sigma(t) dt \in L_{\infty}, \text{ which implies } \int_0^T \sigma_T(t) \sigma(t) dt \in L_{\infty}. \text{ Therefore, by using Barbalat’s lemma with } \sigma_T(t), \dot{\sigma}(t), \int_0^T \sigma_T(t) \sigma(t) dt \in L_{\infty}, \text{ we have } \lim_{t \to \infty} \sigma_T(t) = 0 \text{ for } i = 1, 2, \ldots, k. \]

Let \( x_i(t), i = 1, 2, \ldots, k \) be the elements of \( x(t) \). Similarly, let \( x_i^{(m)}(t), m = 1, 2, \ldots, n, i = 1, 2, \ldots, k \) be the elements of \( x^{(m)}(t) \), \( m = 1, 2, \ldots, n \). Suppose \( \partial_i(t), i = 1, 2, \ldots, k \) are the elements of \( \partial_i(t) \). It is seen from (8) and (9) that the elements \( \sigma_i(t) \) and \( \partial_i(t) \) are represented as
\[
\sigma_i(t) = \left( \beta + \frac{d}{dt} \right)^{n-1} x_i(t) \\
= \sum_{n=1}^N \beta^{n-1} x_{i}^{(n-1)}(t) + \cdots \\
+ \sum_{n=1}^N \beta^{n-1} x_{i}^{(n-1)}(t) 
\] (34)
and
\[
\partial_i(t) = \sum_{n=1}^N \beta^{n-1} x_{i}^{(n-1)}(t) + \cdots \\
+ \sum_{n=1}^N \beta^{n-1} x_{i}^{(n-1)}(t). \] (35)

Therefore, according to Lemma 3 in [36], since \( \lim_{t \to \infty} \sigma_i(t) = 0 \) for \( i = 1, 2, \ldots, k \), the elements \( x_i(t), i = 1, 2, \ldots, k \) and its derivatives \( x_i^{(m)}(t), m = 1, 2, \ldots, n-1, i = 1, 2, \ldots, k \) converge to zero as \( t \to \infty \), i.e., the objective (7) is achieved.

Remark 1: Compared with existing results [29], where the IRL controller is designed for tracking control of second-order, square multivariable dynamics, in this paper, the proposed controllers are developed for high-order, nonsquare multivariable systems.

In what follows, we will consider the system (6) in a special case, namely, the \( g(\bar{x}(t)) \) is assumed to be a square matrix. In this case, the following assumption is needed.

Assumption 2: The matrix \( g(\bar{x}(t)) + g^T(\bar{x}(t)) \) is either positive or negative definite.

According to Lemma 3 with Assumption 2, we define
\[
\frac{1}{2} \sigma_T(t) \left( g^T(\bar{x}(t)) + g(\bar{x}(t)) \right) \sigma(t) = \rho(t) \| \sigma(t) \|^2, \] (36)
where \( \lambda_{\min}(t) \leq \rho(t) \leq \lambda_{\max}(t) \) and \( \lambda_{\min}(t) \) and \( \lambda_{\max}(t) \) are respectively the minimum and maximum eigenvalues of matrix \( \frac{1}{2} (g^T(\bar{x}(t)) + g(\bar{x}(t))) \) and \( \sigma(t) \) is defined in (8). From Assumption 2 and the definition of (36), we know that the sign of \( \rho(t) \) is nonzero, constant but unknown.

It is easy to see that the Assumption 2 can be regarded as a special case of Assumption 1. Therefore, following the similar design procedure of nonsquare multivariable systems, the IRL controller for the square multivariable system with UCCs can be proposed as
\[
u(t) = N(\chi(t)) \sigma(t) \sigma_T(t) \dot{\gamma}(t) \left( \| \sigma(t) \|^2 \right)^{-1} \] (37)
with (25) and (26) Then, the stability results are summarized as follows:

**Corollary 1:** Consider a continuous-time square multivariable system with UCCs given in (6) satisfying Assumption 2. The IRL controller (37), (25) and (26) with the critic NN (16) and (19), and the action NN (21) and (23) can achieve the objective (7) if the designed parameters are properly chosen, i.e., the conditions (27) are satisfied. Furthermore, all signals of the closed-loop system are semiglobally UUB.

**Proof:** It is seen that the Assumption 2 can be regarded as a special case of Assumption 1. Therefore, the result of this corollary is a direct consequence of Theorem 1.

**IV. SIMULATION EXAMPLES**

In this section, one example is adopted to illustrate the effectiveness of the proposed controllers. We consider a system with second-order dynamics \(k = 2\) described by (6), where

\[
g(\overline{x}(t)) = g_0(\overline{x}(t)) g_u(\overline{x}(t)),
\]

in which

\[
g_0(\overline{x}(t)) = \begin{bmatrix} 1 & 2 & 0 \\ -2 & 0 & 1 \end{bmatrix}
\]

is the known, bounded matrix with full row rank, and

\[
g_u(\overline{x}(t)) = \begin{bmatrix} 2 & 0 & 0 \\ 0 & 4 - \cos(x_1) & 1 \\ 0 & 1 & 3 - \sin(x_2) \end{bmatrix}
\]

is the unknown matrix. It is seen that \(g(\overline{x}(t)) \in \mathbb{R}^{2\times3}\) is a nonsquare and partially unknown matrix. Let \(d(t) = [\sin(t), \sin(2t) + 1]^T\). Therefore, this is a nonsquare multivariable system satisfying all the imposed conditions in Section III. The initial condition of the system is \(x(0) = [-1, 3], \dot{x}(0) = [2, -5], \gamma = 0.8\) and \(T = 0.4\). The NN terms \(\hat{W}_{sa}(\dot{x})\) and \(\hat{W}_{sc}(\dot{x})\) with input vector \(\ddot{x} = [x(t), \dot{x}(t)]^T\) have 21 nodes with centers \(\mu_l, l = 1, 2, \ldots, 21\), evenly spaced in \([-4, 4] \times [-4, 4] \times [-4, 4] \times [-4, 4]\), and widths \(\eta_l = 4, l = 1, 2, \ldots, 21\). Furthermore, to satisfy the conditions in Theorem 1, let the parameters \(\delta_{sa} = \delta_{sc} = 2\). The Nussbaum-type function is \(N(x(t)) = x(t)^2 \cos(x(t))\), the initial states of \(x(t)\) and \(\dot{W}_{sa}(t)\) are zero, the initial state \(\dot{W}_{sc}(0) = I_{21 \times 2}\), and the parameters \(\Pi_{sa} = \Pi_{sc} = 0.3I_{21}\).

The simulation results are given in Fig. 1-4, where it is shown that the objective (7) can be achieved. Moreover, the signals of the closed-loop system are all bounded.

**REFERENCES**

[1] S. S. Ge, F. Hong, and T. H. Lee, “Adaptive neural control of nonlinear time-delay systems with unknown virtual control coefficients,” *IEEE Trans. Syst. Man, Cybern. B, Cybern.*, vol. 34, no. 1, pp. 499–516, Feb. 2004.
[2] G. Tao, “Multivariable adaptive control: A survey,” Automatica, vol. 50, no. 11, pp. 2737–2764, Nov. 2014.

[3] Y. Liu, G. Tao, and S. M. Joshi, “Modeling and model reference adaptive control of aircraft with asymmetric damage,” J. Guid., Control, Dyn., vol. 33, no. 5, pp. 1500–1517, Sep. 2010.

[4] A. Astolfi, L. Hsu, M. S. Netto, and R. Ortega, “Two solutions to the adaptive visual servoing problem,” IEEE Trans. Robot. Autom., vol. 18, no. 3, pp. 387–392, Jun. 2002.

[5] J. Du, C. Guo, S. Yu, and Y. Zhao, “Adaptive autopilot design of time-varying uncertain ships with completely unknown control coefficient,” IEEE J. Ocean. Eng., vol. 32, no. 2, pp. 346–352, Apr. 2007.

[6] R. D. Nussbaum, “Some remarks on a conjecture in parameter adaptive control,” Syst. Control Lett., vol. 3, no. 5, pp. 243–246, Nov. 1983.

[7] Y. Zhang, C. Wen, and Y. C. Soh, “Adaptive backstepping control design for systems with unknown high-frequency gain,” IEEE Trans. Autom. Control, vol. 45, no. 12, pp. 2350–2354, 2000.

[8] W. Chen, X. Li, W. Ren, and C. Wen, “Adaptive consensus of multi-agent systems with unknown identical control directions based on a novel nussbaum-type function,” IEEE Trans. Autom. Control, vol. 59, no. 7, pp. 1887–1892, Jul. 2014.

[9] Z. Ding, “Adaptive consensus output regulation of a class of nonlinear systems with unknown high-frequency gain,” Automatica, vol. 51, pp. 348–355, Jan. 2015.

[10] Z. Yu, S. Li, Z. Yu, and F. Li, “Adaptive neural output feedback control for nonstrict-feedback stochastic nonlinear systems with unknown backlash-like hysteresis and unknown control directions,” IEEE Trans. Neural Netw. Learn. Syst., vol. 29, no. 4, pp. 1147–1160, Apr. 2018.

[11] J. Huang, W. Wang, C. Wen, and J. Zhou, “Adaptive control of a class of strict-feedback time-varying nonlinear systems with unknown control coefficients,” Automatica, vol. 93, pp. 98–105, Jul. 2018.

[12] J. Peng and X. Ye, “Cooperative control of multiple heterogeneous agents with unknown high-frequency-gain signs,” Syst. Control Lett., vol. 68, pp. 51–56, Jun. 2014.

[13] Q. Wang, H. E. Psilakis, and C. Sun, “Adaptive cooperative control with guaranteed convergence in time-varying networks of nonlinear dynamical systems,” IEEE Trans. Cybern., early access, Jun. 3, 2019, doi: 10.1109/TCYB.2019.2916563.

[14] Q. Wang, “Distributed control of higher-order nonlinear multi-agent systems with unknown non-identical control directions under general directed graphs,” Automatica, vol. 110, Dec. 2019, Art. no. 108559, doi: 10.1016/j.automatica.2019.108559.

[15] Q. Wang and C. Sun, “Adaptive consensus of multiagent systems with unknown high-frequency gain signs under directed graphs,” IEEE Trans. Syst., Man, Cybern. Syst., early access, Mar. 13, 2019, doi: 10.1109/TSMC.2019.2916641.

[16] C. Wang, C. Wen, and L. Guo, “Multivariable adaptive control with unknown signs of the high-frequency gain matrix using novel nussbaum functions,” Automatica, vol. 111, Jan. 2020, Art. no. 108618.

[17] R. Ortega, A. Astolfi, and N. E. Barabanov, “Nonlinear PI control of uncertain systems: An alternative to parameter adaptation,” Syst. Control Lett., vol. 47, no. 3, pp. 259–278, Oct. 2002.

[18] H. E. Psilakis, “An extension of the Georgiou–Smith example: Boundedness and attractivity in the presence of unmodelled dynamics via nonlinear PI control,” Syst. Control Lett., vol. 92, pp. 1–4, Jun. 2016.

[19] Q. Wang, H. E. Psilakis, and C. Sun, “Cooperative control of multiple agents with unknown high-frequency gain signs under unbalanced and switching topologies,” IEEE Trans. Autom. Control, vol. 64, no. 6, pp. 2495–2501, Jun. 2019.

[20] C. Wang, H. E. Psilakis, and C. Sun, “Consensus in networks of agents with unknown high-frequency gain signs and switching topology,” IEEE Trans. Autom. Control, vol. 62, no. 8, pp. 3993–3998, Aug. 2017.

[21] Q. Wang, H. E. Psilakis, and C. Sun, “Cooperative control of multiple high-order agents with nonidentical unknown control directions under fixed and time-varying topologies,” IEEE Trans. Syst., Man, Cybern. Syst., early access, May 27, 2019, doi: 10.1109/TSMC.2019.2916641.

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