Nonplanar Geometry Dust –Ion Acoustic Shocks in an adiabatic Dusty Plasma with Nonthermal Electrons

Louis E. Akpabio* and Akaninyene D. Antia
Theoretical physics Group, Department of Physics, University of Uyo, Uyo, Nigeria.

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ABSTRACT

An unmagnetized dusty plasma consisting of static negatively charged dust fluid, nonthermal distributed electrons, and adiabatic ion fluid has been considered. Basic properties of the dust-ion-acoustic shock waves have been made by the reductive perturbation method to derive the Burgers’ equation for nonplanar geometry. The solution of modified Burgers’ equation in nonplanar geometry is numerically analyzed and it has been found that, the nonplanar geometry effects have a very vital role in the development of shock waves. We also discovered that; the inclusion of the nonthermal electron distribution significantly modifies the shock wave profile. The change of the DIASW structure due to the effect of ion temperature and dust density is studied.

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Introduction

The interplay between charged dust grains and plasmas has lead to much interest in new research area called dusty (or complex) plasma. Linear as well as nonlinear collective processes in dusty or complex plasma have received special attention due to the realization of their occurrence in planetary rings, interstellar clouds and cometary environment [1-6]. There has been a rapidly growing interest in nonlinear phenomena (such as shocks, solitons and vortices) in dusty plasma (plasmas with extremely massive and negatively charged dust grains), because of its crucial role in understanding electrostatic disturbances in space and laboratory dusty plasmas [7-11]. Now, it is a well known fact that the presence of static charged dust grains modifies the existing plasma wave spectra [12-14].

Dust ion acoustic shocks in unmagnetized dusty plasma may arise when there is a balance between the nonlinearity (associated with the harmonic generation) and the kinetics viscosity, introduced by the dust ion drag. The formation of dust ion acoustic shock wave (DIASWs) was observed by Nakamura et al. [15]. They found out that in the linear regime, the phase velocity of the Dust Ion Acoustic (DIA) waves increases while the wave suffers heavy damping when the dust number density in an electron –ion plasma is considerably increased. On the other hand, they found out that an oscillatory ion-acoustic shock wave in usual argon plasma transforms into a monotonic shock front when it travels through the dusty plasma column. A number of studies have been made on the propagation of DIASWs in dusty plasma by several investigators [16 – 19].

Recently, several theoretical investigations [20 – 24] on the properties of dust-ion acoustic and dust acoustic solitary waves in nonplanar geometry had been carried out. Likewise, of recent, a theoretical investigation has been done by Sahu [25] to study the effect of nonplanar DIASWs in adiabatic dusty Plasma. Moreover, in real dusty plasma, the effect of finite ion temperature cannot be neglected and the electron behaviour can be strongly modified by nonlinear potential of the localized DIA structures by generating a population of fast energetic electrons. Therefore; in our present paper, we wish to study how finite ion temperature combined with electron non-thermality effects can be expected to modify the results arrived at in Sahu [25]. The manuscript is organized as follows; section 2 deals with the basic equations governing the adiabatic dusty plasma system under consideration, section 3 presents the investigation of nonplanar DIASWs by the reduction perturbation method (RPM). In section 4, we present the numerical results and discussion, while section 5 is the conclusion.

Governing Equations

We consider an unmagnetized plasma comprising static negatively charged dust fluid, nonthermal distributed electrons and adiabatic ion fluid. The dynamics of the DIASWs in nonplanar geometry for such dust plasma is governed by the following normalized fluid equations:

\[
\frac{\partial n_i}{\partial t} + \frac{1}{r^*} \frac{\partial}{\partial r} \left( r^* n_i u_i \right) = 0
\]

\[
\frac{\partial u_i}{\partial t} + n_i u_i \frac{\partial u_i}{\partial r} = -n_i \frac{\partial \phi}{\partial r} - \alpha \frac{\partial p_i}{\partial r} + \eta_i n_i \left[ \frac{1}{r^*} \frac{\partial}{\partial r} \left( r^* u_i \right) \right] - \nu u_i
\]

\[
\frac{\partial p_i}{\partial t} + u_i \frac{\partial p_i}{\partial r} + 3p_i \frac{1}{r^*} \frac{\partial}{\partial r} \left( r^* u_i \right) = 0
\]
\[ \mu \exp(\phi) \left[ 1 - \beta \phi + \beta \phi^2 \right] - n_i + (1 - \mu) = 0 \]  

(4)

\[ \beta = \frac{4\alpha_i}{1 + 3\alpha_i} \]

where \( \alpha_i \) is a parameter determining the number of nonthermal electrons present in our plasma model. In the above equation, \( n_i \) is the ion number density normalized by its equilibrium value \( n_{i0} \), \( u_i \) is the ion fluid speed normalized by \( \phi \), \( \alpha_i \) is the ion thermal pressure normalized by \( \phi \), \( \mu = n_{e0} \) and \( \eta_i \) is the viscosity coefficient of ion fluid normalized by \( w_{p_i} \). Note that in equation (4), we assumed the quasi-neutrality condition.

**Derivation of Nonplanar Burgers’ Equation**

We derive the Burgers’ equation from equations (1) – (4) by employing the reductive perturbation method (RPM) [26] and the stretched coordinates \( \xi = \epsilon \frac{1}{2} (r - V_0 t) \) and \( \tau = \epsilon \frac{3}{2} t \), where \( \epsilon \) is a smallness parameter measuring the weakness of the nonlinearity and \( V_0 \) is the phase speed of DIASWs normalized by \( c_i \). Equations (1) – (4) can be expressed in terms of \( \xi \) and \( \tau \) as follows:

\[ \epsilon^3 \partial_\xi n_i - V_0 \frac{3}{2} \partial_\xi n_i + \frac{\epsilon^2}{2} \partial_\xi (n_i u_i) + \epsilon^3 \frac{\epsilon}{V_0} \left( \frac{1+\epsilon}{V_0} \right) (n_i u_i) = 0 \]  

(5)

\[ \epsilon^3 n_i \frac{1}{2} \partial_\xi u_i - V_0 \frac{3}{2} n_i \frac{1}{2} \partial_\xi u_i + \frac{\epsilon^2}{2} n_i \frac{1}{2} \partial_\xi u_i = \epsilon^2 \frac{1}{2} n_i \partial_\xi \phi - \epsilon^3 \frac{1}{2} \partial_\xi n_i \]

(6)

\[ \epsilon^3 \partial_\xi u_i - V_0 \frac{3}{2} \partial_\xi u_i + \frac{\epsilon^2}{2} \partial_\xi u_i - \frac{\epsilon^3}{V_0} \left( \frac{1+\epsilon}{V_0} \right) \partial_\xi u_i = 0 \]  

(7)

\[ \mu \left( 1 + \phi + \frac{1}{2} \phi^2 + \ldots \right) \left[ 1 - \beta \phi + \beta \phi^2 \right] + (1 - \mu) = n_i \]  

(8)

where \( \eta = \epsilon^2 \eta_0 \) is assumed [16]. We can expand the dependent variables \( n_i, u_i, p_i \) and \( \phi \) in power series of \( \epsilon \) as follows:

\[ n_i = 1 + \epsilon n_{i1} + \epsilon^2 n_{i2} + \ldots \]

\[ u_i = 0 + \epsilon u_{i1} + \epsilon^2 u_{i2} \]

\[ p_i = 1 + \epsilon p_{i1} + \epsilon^2 p_{i2} \]  

(9)
Now, substituting equation (9) into equations (5) – (8), we obtain the lowest order of the coefficient of $\varepsilon$ as:

$$n_{i1} = \mu \phi_i (1 - \beta)$$  \hspace{1cm} (10)

$$u_{i1} = \mu V_0 (1 - \beta) \phi_i$$  \hspace{1cm} (11)

$$p_{i1} = 3 \mu (1 - \beta) \phi_i$$  \hspace{1cm} (12)

$$V_0 = \sqrt{3 \alpha + \frac{1}{\mu (1 - \beta)}}$$  \hspace{1cm} (13)

The next higher order in $\varepsilon$, is given as the following set of equations,

$$\partial_z n_{i1} - V_0 \partial_z n_{i2} + \partial_z \left( n_{i1} u_{i1} \right) + \partial_z u_{i1} + \frac{\nu u_{i1}}{V_0} = 0$$  \hspace{1cm} (14)

$$\partial_z u_{i1} - V_0 \partial_z u_{i2} + u_{i1} \partial_z u_{i1} - V_0 n_{i1} \partial_z u_{i1} + \alpha \partial_z p_{i2} = -\partial_z \phi_2 - n_{i1} \partial_z \phi_1 + \eta_0 \partial_z^2 u_{i1}$$  \hspace{1cm} (15)

$$\partial_z p_{i1} - V_0 \partial_z p_{i2} + u_{i1} \partial_z p_{i1} + 3 \partial_z u_{i2} + 3 p_{i1} \partial_z u_{i1} + \frac{3 \nu u_{i1}}{V_0} = 0$$  \hspace{1cm} (16)

$$n_{i2} = \mu (1 - \beta) \phi_2^2 + \frac{1}{2} \mu \phi_1^2 - \mu \phi_2^2$$  \hspace{1cm} (17)

Now, using equations (10) – (17) and eliminating $n_{i2}, n_{i2}, p_{i2}$ and $\phi_2$, we finally obtain a modified Burgers’ equation

$$\partial_z \phi_i + \frac{\nu}{2 \tau} \phi_i + A \phi_i \partial_z \phi_i - C \partial_z^2 \phi_i = 0,$$ \hspace{1cm} (18)

where

$$A = \frac{12 \mu^2 \alpha (1 - 2 \beta + \beta^2) - (1 + \mu) (2 \beta + 1 - \beta^2) + 2 \mu (2 - \beta)}{2 \mu \left( \sqrt{3 \alpha + \frac{1}{\mu (1 - \beta)}} \right) (1 - \beta)^2}$$ \hspace{1cm} (19)

$$C = \frac{\eta_0}{2}$$ \hspace{1cm} (20)

**Numerical Results and Discussion**

Equation (18) is the modified Burgers’ equation describing the nonlinear propagation of the DIASWs in unmagnetized dusty plasma consisting of adiabatic ion fluid, nonthermal distributed electrons and static negatively charged dust fluid. The stationary DIASWs of this modified Burgers’ equation for planar geometry ($v = 0$) is

$$\phi_i = \frac{V}{A} \left[ 1 - \tanh \left( \frac{V (\xi - V \tau)}{2C} \right) \right]$$

Where $V$ is a constant velocity normalized by $c_i$. For nonplanar geometry, an exact analytical solution of equation (18) is not possible, hence it is solved numerically.

Figure 1, shows the variation of shock wave structure with $\xi$ for the different given parameters in different geometries. It is interesting to point out that the inclusion of non-thermal electron distribution gets the shock profile modified in terms of the shock height and shock steepness for the different geometry. The height and steepness of one-dimensional shock wave are larger than that of cylindrical shock wave, which in turn is larger than that of the spherical shock wave. The shock height is found to be decreasing monotonically with $V$ (the geometry).
Fig 1. Showing how the shock profile $(\phi, V, \xi)$ curves) varies in different geometries for $\tau = -5, \eta_0 = 0.5, \alpha = 0.5, \beta = 1.0$ and $\mu = 0.4$.

In figures 2 and 3, we present the effect of several values of $\tau$ for both cylindrical $(\nu = 1)$ and spherical $(\nu = 2)$ geometries respectively. It can be observed that as the value of $\tau$ increases, the shock wave structures look like that of the one-dimensional geometry of fig. 1. This is due to the fact that the nonplanar geometrical effect is no longer prominent for larger values of $\tau$. The nonplanar geometrical effects given by $\left(\frac{\nu}{2\tau}\right)$ will become effective as the value of $\tau$ decreases and the shock wave profiles differs from each other in both cylindrical and spherical geometry respectively.

Fig 2. Variation of $\phi$ with respect to $\xi$ at different values of $\tau$ for the cylindrical geometry $(\nu = 1)$ and the other parameters being the same as figure 1

Fig 3. Variation of $\phi$ with respect to $\xi$ at different values of $\tau$ for the spherical geometry $(\nu = 2)$ and the other parameters being the same as figure 1

The shock wave structures for different values of the nonthermal electron parameter $(\beta)$ are investigated in both cylindrical and spherical geometries as shown in figures 4 and 5 respectively. It is found that; small variation, in the magnitude of $\beta$ significantly affects the shock wave profile. The shock height is found to be increasing monotonically with $\beta$. This effect is more pronounced in cylindrical geometry when compared to the spherical geometry.
Fig 4. Variation of $\phi_1$ with respect to $\xi$ at different values of nonthermal electron parameter ($\beta$) for the cylindrical geometry ($\nu = 1$) and the other parameters being the same as figure 1.

Fig 5. Variation of $\phi_1$ with respect to $\xi$ at different values of nonthermal electron parameter ($\beta$) for the spherical geometry ($\nu = 2$) and the other parameters being the same as figure 1.

The effects of ion temperature ($\alpha$) and dust density ($\mu$) on the shock wave structures are also studied. The dust density can be expressed by the variation of $\mu$ owing to $1 - \mu = Z_d n_{d_0} / n_{i_0}$. Figure 6 shows how the steepness of the shock wave structure is also modified by dust density and it decreases with dust density. While from fig. 7, it can be observed that the ion temperature has a weak effect on the steepness of shock wave structure.

Fig 6. Variation of $\phi_1$ with respect to $\xi$ at different values of $\mu$ for the cylindrical geometry ($\nu = 1$) and the other parameters being the same as figure 1.

Fig 7. Variation of $\phi_1$ with respect to $\xi$ at different values of $\alpha$ (ion temperature) for the cylindrical geometry ($\nu = 1$) and the other parameters being the same as figure 1.
Conclusion

We have derived the cylindrical and spherical Burgers’ equation for Dust-ion acoustic shock waves in unmagnetized adiabatic dusty plasmas comprising static negatively charged dust fluid, nonthermal distributed electrons and adiabatic ion fluid. Employing the standard reductive perturbation method to derive the Burgers’ non-planar geometry equation, the choice of non-thermal distribution for energetic electrons used in our model is due to its convenience rather than as a precise fitting model of what is observed.

We have found out that, the propagation of Dust ion acoustic shock wave in nonplanar geometry with the inclusion of non-thermal electrons distribution gets the shock wave modified as the shock profile is found to vary significantly with the nonthermal parameter $\beta$. This effect is more prominent in cylindrical as compared to the spherical geometry. It is also observed that, the shock height decreases monotonically with the geometry. We realize that for large negative values of $\tau$, the nonplanar geometry approaches the planar geometry. Finally, the amplitude and steepness of the one-dimension shock waves are larger than that of the cylindrical shock waves, which in turn is larger than that of the spherical shock waves. We have also shown that the ion temperature and the dust density will modify the properties of DIASWs. These are also confirmed by experiments. This work could further throw more light on the understanding of the nonlinear propagation characteristic of DIASWs that are necessary in laboratory plasma as well as in plasma application.

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