PREPARATION OF GEOTHERMAL SILICA GLASS COATING FILM THROUGH MULTI-FACTOR OPTIMIZATION

S. Silviana*, Gelbert Jethro Sanyotob, Adi Darmawanb

aDepartment of Chemical Engineering, Faculty of Engineering, Diponegoro University, 50275, Tembalang, Semarang, Indonesia
bMaster Program of Chemical Engineering, Faculty of Engineering, Diponegoro University, 50275, Tembalang, Semarang, Indonesia

1.0 INTRODUCTION

The “lotus leaf effect” has attracted the attention of many researchers around the world to develop self-cleaning glass technology. In addition to a variety of applications, this technology is useful in reducing maintenance costs by eliminating tedious manual cleaning work [1]. This potential has encouraged efforts to replicate the lotus leaf effect. The surface design of a lotus leaf consists of a micro/nano hierarchical structure, that creates low free-surface energy, thereby preventing water from wetting the surface of the leaf [2]. To produce self-cleaning properties on glass surfaces, previous studies have attempted to modify the glass surface by using nanoparticles such as ZnO, SiO2, TiO2 [3–5] and carbon or polymer particles [6, 7].

As one of the most abundant minerals from the earth’s crust, SiO2 has the highest potential to be produced as a glass coating. However, silica is present as mined mineral sand, and it can be formed naturally in rice husk [8], bamboo leaf [9, 10],...
bagasse ash [11, 12], rice husk [13], and coal ash [14]. In various geothermal power plants, silica can also be applied as scale in piping equipment [15]. For example, silica can be released from the geothermal power plant in Dieng generating a huge amount of solid waste. This condition has been a problem because waste accumulation in the form of saltwater solution has reached 10 tons/day and generates approximately 10% of solid silica scale waste [16]. However, many observations of the geothermal silica have been conducted in several researches [17-20].

Surface modification of silica nanoparticles originates from the behavior of hydroxyl groups on the surface of silica. These hydroxyl groups can be substituted by other functional groups. The product can have completely different behavior such as surface hydrophobicity. The hydroxyl group can be substituted into other groups, such as trimethylsilyl producing hydrophobic materials [21]. This modification can be achieved by using silica precursors reacted with several silylating agents, including trimethylchlorosilane (TMCS) [22-24], hexamethyldisilazane (HMDS) [25, 27], methyltrimethoxysilane (MTMS) [27, 28], or polydimethylsiloxane (PMDS) [21, 29].

However, optimization and multifactorial testing should be conducted to limit the usage of silane agents and the possibility of interaction between many variables. Limiting the use of materials, especially the silane agents, can minimize the product cost and increase the potential for commercialization. Therefore, in this study, a multifactor optimization is applied to prepare glass coating film using a precursor derived from geothermal power plant silica. Design Expert 8.0.6 software is used in the design process. This study revealed that the contact angle of distilled water on the coated glass with a higher contact angle can be achieved.

2.0 METHODOLOGY

2.1 Preparation of Silica Precursor

Geothermal Silica Pre-treatment

Silica from geothermal power plant was treated by drying with the temperature of 105°C, followed by size reduction through high-energy milling for 10 min and screened using Vibratory Sieve Shaker of the series AS 200, 325 mesh (45 micrometer). The procedure had used previous research with slight modification such as ratio of silica over sulfuric acid [17,30]. The geothermal silica was mixed with sulfuric acid through leaching process at temperature of 100°C. The leaching process allowed for 1 h 45 min. Pretreated silica soaked in acidic solution sulfuric acid at 1:5 (w/v) was prepared at temperature of 100°C with constant stirring. After the slurry was formed, the solution mixture was screened through filter paper, and it was neutralized by washing and then dried using oven at 105°C until a constant weight was obtained. Therefore, 2 N NaOH solution was added to the silica solids obtained with a ratio of silica over sodium hydroxide about 1:6 (w/v) and stirred until all silica was dissolved to generate a solution of Na2SiO3. Then, hydrochloric acid (HCl) 1 N was dropped to Na2SiO3 solution gradually until colloidal condition at acidic conditions and left by aging for 18 hours. Finally, demineralized water was used to wash the silica gel to remove residual salt and impurity. After that silica gel was introduced ambient pressure drying at 105°C.

Synthesis of Silica Precursor

In this study, the silica precursor used was water glass (sodium silicate) obtained through sol-gel method using NaOH and HCl. These steps were conducted to eliminate the impurity of geothermal silica. The NaOH used in the sol process was 6 N with silica to NaOH solution ratio being 1:6 (w/v). After filtration, the filtrate as water glass solution was administered with HCl 1 N at various ratios (1:5, 1:8, 1:10 v/v) to form a gel at room temperature. Then, the solution was aged for 18 h to yield silica gel. Distilled water was used to wash silica gel, and then silica gel was dried at 105°C. Dry silica was synthesized to produce a water glass precursor or sodium silicate.

2.2 Glass Coating Preparation

Experimental Design

Experiment design and optimization were conducted using statistical method with Design Expert 8.0.6 by applying a regular two-level factorial design to estimate main effects and interactions. The experiment two factors with 12 runs. Sodium silicate and silane agent concentration as the numeric factors were conducted with a low level of 2% and a high level of 8%, while silane agent type as categorical factors were MTMS, HMDS, and PMDS. Initially, the sodium silicate was dissolved in water, and the surfactant of cetyltrimethylammonium bromide (CTAB) was dissolved in ethanol. The response would be recorded as a contact angle in six measurements.

Sodium silicate and silane agent solutions at the predetermined concentrations were adjusted to pH = 2.0 using HCl 1 N to obtain a sol solution, while the gel formation was approximately to pH 5.0. The sol solution was then mixed with ratio 1:1 (V/V) and added with 0.1 gram of CTAB under constant stirring for 1 h. The sol solution was adjusted to reach pH = 5.0 using NaOH 1 N to form gel. The original randomized runs are presented in Table 1. Design Expert software automatically lists the runs in randomized order, protecting against any lurking factors through the standard order (Std) function.
Table 1 Randomized $2^5$ factorial experiment design generated from Expert 8.0.6. The same process is applied for each silane agent type

| Run | Factor 1 A: Sodium Silicate (%) | Factor 2 B: Silane Agent (%) |
|-----|---------------------------------|-------------------------------|
| 1   | 8                               | 2                             |
| 2   | 2                               | 2                             |
| 3   | 2                               | 2                             |
| 4   | 8                               | 8                             |
| 5   | 8                               | 2                             |
| 6   | 2                               | 8                             |
| 7   | 8                               | 2                             |
| 8   | 2                               | 2                             |
| 9   | 2                               | 8                             |
| 10  | 8                               | 8                             |
| 11  | 2                               | 8                             |
| 12  | 8                               | 8                             |

Coating Application

The mixed solution was applied to an alcohol-washed glass substrate by spray method. The coated glass was dried by ambient air and its contact angle was analyzed.

2.3 Characterization

All response data of coated glasses was analyzed contact angle using Race Contact angle. The other characterization have been conducted by doing analysis of BET-BJH (Autosorb IQ of Quantachrome Instrument, Austria), FTIR (IRPrestige21of Shimadzu, Japan), SEM EDX (Thermo Fischer Scientific, USA), and AFM (Park System XE-70, USA) to confirm the results.

3.0 RESULTS AND DISCUSSION

3.1 Preparation of Silica Precursor

Initially, silica from geothermal solid waste was treated by acid leaching using sulfuric acid. Table 2 shows the conditions before and after acid leaching based on composition analysis using XRF.

Through acid leaching, the treated silica consisted of reduced components due to cut of ionic bonds of metal impurities with $O_2$ from the interaction between $H_2SO_4$ and metal oxides. Furthermore, binding of $SO_4^{2-}$ ions with metal elements released metal sulfate compounds while binding of $H^+$ ions with oxygen released $H_2O$. Meanwhile, high-concentration $H_2SO_4$ can inhibit itself by in-situ deposition on metal surface [31].

3.2 Effect on Acid Ratio in Gelation

Preparation of the glass coating film was closely related to the surface modification step. In this study, surface modification aims to replace the hydrophilic hydroxyl group of silica with a hydrophobic trimethylsilyl group. Figure 1 shows an example of reaction following the surface modification.

![Figure 1 Surface modification using HMDS [32]](image)

Although the surface of silica itself contains many hydroxyl groups, surface modification depends on the surface area of a specific material. Therefore, higher surface area is preferable to maximize the substitution of hydroxyl groups. A previous study stated that the silica surface area was related to the ratio of silica sol to acid volume in the gelation step of the sol-gel method [33]. Thus, the HCl volume varies to 1:5, 1:8, and 1:10 (v/v). Figure 2 shows the result of Brunauer-Emmett-Teller (BET) analysis. BET analysis is used to calculate the surface area and pore distribution of the geothermal silica [34].
Overall surface area, pore volume, and pore radius data are summarized in Table 3.

### Table 3 BET analysis of geothermal silica

| Parameter                  | Raw | HCl 1:5 | HCl 1:8 | HCl 1:10 |
|----------------------------|-----|---------|---------|----------|
| Surface area (m²/g)        | 40.90 | 73.53   | 165.4   | 96.99    |
| Pore volume (cc/g)         | 0.13  | 0.179   | 0.097   | 0.084    |
| Pore radius (Å)            | 19.83 | 15.30   | 19.11   | 17.05    |

As shown in Table 3 and Figure 3, the sol-gel method may increase the silica surface area. This finding is similar to that of other studies [35]. Nevertheless, the ratio of silica sol-to-HCl also relates to the surface area in which the addition of HCl at 1:8 (v/v) results in the highest surface area compared with 1:5 and 1:10. A possible explanation of this result is the property of silica gel itself, which is influenced by solution pH. Silica is soluble in basic solution as sodium silicate sol. By adjusting the pH to neutral, silica sol may transform into a condensed structure known as silica gel [36]. Failure to reach this neutral pH (lower HCl addition) may hamper the gelation. However, by adding more HCl (1:10), lower pH makes the solution acidic, which may hinder the silica condensation rate [37], thereby creating less surface area. The mean radius is 17.8 Å, with a low deviation (±1.78 Å), which indicates that the variation of additional HCl does not have a significant effect on the pore radius. Pore volume values for the three samples are shallow and indicate that only a small portion of this material is porous. Most of this material is porous and non-dense. This characteristic is good because the resulting silica thin layer produces a dense surface and tends to be non-porous.

### 3.3 Glass Coating Statistical Optimization

Table 4 presents the contact angle measurement of 36 coated glass samples.
Table 4 Contact angle measurement results of coated glass

| Run | Category: Silane agent type | Factor 1 A: Sodium silicate (%) | Factor 2 B: Silane agent (%) | Response: Contact angle (°) |
|-----|-----------------------------|---------------------------------|-------------------------------|----------------------------|
| 1   | MTMS                        | 2                               | 2                             | 134.5 ± 2.3                |
| 2   | MTMS                        | 2                               | 2                             | 132.9 ± 1.3                |
| 3   | MTMS                        | 2                               | 2                             | 125.7 ± 2.9                |
| 4   | MTMS                        | 8                               | 2                             | 98.5 ± 5.1                 |
| 5   | MTMS                        | 8                               | 2                             | 105.3 ± 6.1                |
| 6   | MTMS                        | 8                               | 2                             | 109.7 ± 4.7                |
| 7   | MTMS                        | 2                               | 8                             | 90.7 ± 0.9                 |
| 8   | MTMS                        | 2                               | 8                             | 89.7 ± 0.7                 |
| 9   | MTMS                        | 2                               | 8                             | 86.4 ± 2.6                 |
| 10  | MTMS                        | 8                               | 8                             | 79.3 ± 2.3                 |
| 11  | MTMS                        | 8                               | 8                             | 93.8 ± 1.8                 |
| 12  | MTMS                        | 8                               | 8                             | 91.4 ± 4.2                 |
| 1   | HMDS                        | 2                               | 2                             | 72.3 ± 5.1                 |
| 2   | HMDS                        | 2                               | 2                             | 74.4 ± 3.8                 |
| 3   | HMDS                        | 2                               | 2                             | 93.0 ± 5.4                 |
| 4   | HMDS                        | 8                               | 2                             | 86.5 ± 3.3                 |
| 5   | HMDS                        | 8                               | 2                             | 93.1 ± 2.8                 |
| 6   | HMDS                        | 8                               | 2                             | 105.1 ± 1.3                |
| 7   | HMDS                        | 2                               | 8                             | 49.6 ± 4.0                 |
| 8   | HMDS                        | 2                               | 8                             | 69.1 ± 3.3                 |
| 9   | HMDS                        | 2                               | 8                             | 38.3 ± 1.7                 |
| 10  | HMDS                        | 8                               | 8                             | 31.1 ± 1.4                 |
| 11  | HMDS                        | 8                               | 8                             | 40.9 ± 2.1                 |
| 12  | HMDS                        | 8                               | 8                             | 36.8 ± 2.7                 |
| 1   | PDMS                        | 2                               | 2                             | 75.8 ± 4.5                 |
| 2   | PDMS                        | 2                               | 2                             | 106.1 ± 1.9                |
| 3   | PDMS                        | 2                               | 2                             | 108.3 ± 5.8                |
| 4   | PDMS                        | 8                               | 2                             | 53.8 ± 5.8                 |
| 5   | PDMS                        | 8                               | 2                             | 45.6 ± 4.6                 |
| 6   | PDMS                        | 8                               | 2                             | 35.2 ± 3.7                 |
| 7   | PDMS                        | 2                               | 8                             | 78.1 ± 0.5                 |
| 8   | PDMS                        | 2                               | 8                             | 57.5 ± 2.5                 |
| 9   | PDMS                        | 2                               | 8                             | 106.9 ± 2.7                |
| 10  | PDMS                        | 8                               | 8                             | 40.5 ± 4.6                 |
| 11  | PDMS                        | 8                               | 8                             | 52.9 ± 3.5                 |
| 12  | PDMS                        | 8                               | 8                             | 32.9 ± 2.0                 |

Based on Table 4, half-normal plots of data can be derived for each type of silane agent, i.e., Figure 4 for MTMS, HMDS, and PDMS, respectively.

Figure 4, where factor A is sodium silicate, and factor B is a silane agent from a half-normal plot, shows that the concentration of sodium silicate and silane agent has a negative effect on the response. However, factors A and B (AB) show positive effects that indicate the possible interaction between the two variables for MTMS and PDMS. This AB interaction shows a negative effect on HMDS. Further studies of these interactions are analyzed using ANOVA to determine the significance of the model and are presented in Table 5.
Table 5: ANOVA for silane type of factorial model (i = MTMS, ii = HMDS, iii = PDMS) with all significant models

| Source       | F-value | Prob>F   | Significance |
|--------------|---------|----------|--------------|
| Model        | 40.6    | <10^-4   | <9.10^-4     |
| A-Na-Si      | 18.8    | 2.510^-3 | 1.610^-3     |
| B-Silane     | 86.2    | <10^-4   | 10^-4        |
| AB           | 16.7    | 3.510^-3 | 3.810^-2     |
| R^2          | 0.93    | 0.86     | 0.74         |
| Adj R^2      | 83      | 74       | 26           |
| Pred R^2     | 0.86    | 0.70     | 0.42         |
| Adeq. Precision | 13.6 | 9.26     | 5.61         |

The ANOVA of the factorial model shows that the p-value of all the models is below 0.05. Thus, the model is considered statistically significant. Consequently, the interaction patterns of these findings tend to generalize a broader data range. The interaction between variables (sodium silicate and silane agent concentration) and resulting response (contact angle) can be observed in Figure 5.

Based on optimization using objective criteria in the form of contact angles at maximum levels, optimal use of sodium silicate and silane agents can be observed. The optimization results based on design expert software compared with those of uncoated glass are shown in Table 6 with range low level of 2 and high level of 8 for each variable.

Table 6: Optimization results of silica glass coating film and contact angle result of uncoated glass

| Silane Agent Type | Sodium Silicate (%) | Silane Agent (%) | Contact Angle from DE statistic (°) | Desirability | Contact Angle measurements (°) |
|-------------------|---------------------|------------------|-----------------------------------|--------------|--------------------------------|
| MTMS              | 2.000               | 2.000            | 130.94                            | 94.0%        | 130.94                         |
| HMDS              | 8.000               | 2.000            | 94.89                             | 86.2%        | 94.89                          |
| PDMS              | 2.000               | 2.000            | 96.72                             | 84.7%        | 96.72                          |
| Uncoated          | -                   | -                | 18.6                              | -            | -                              |

Figure 5: Model graph of interaction between sodium silicate and silane agent

Figure 6: Ramp result for the optimization

Moreover, confirmation of this optimization have been confirmed the analysis of 3 (six) samples with duplicate contact angle analysis. The optimization data from design expert software can be seen from ramps graphs in Figure 6.
Table 6 shows that the silica glass coating film, which uses 2% sodium silicate and 2% silane agent of MTMS, produces the highest contact angle at 130° with desirability of 0.94. However, coatings using surface-modified silica can provide glass with hydrophobic properties (contact angle > 90°) compared with uncoated glass substrates. Glass plates without any coating, only have a contact angle of 18.58°, which indicates as hydrophilic.

Table 7 The roughness parameter of coated glass of the silane agent by the AFM analysis

| Sample   | The height of surface (nm) | of | Ra (nm) |
|----------|---------------------------|----|---------|
| MTMS     | 48-76                     |    | 29-57   |
| HMDS     | 9-20                      |    | 5-13    |
| PDMS     | 25-73                     |    | 16-19   |

Coated glass using silane agent of MTMS resulted rougher surface, and higher contact angle (more hydrophobic). It was confirmed by the contact angle measurement and the AFM analysis result in Table 6 and Figure 8.

In addition, Figure 7 visualizes morphology and elemental analysis as basic surface analysis based on SEM-EDX mapping for samples among uncoated and coated glasses (samples with sodium silicate of 8% and silane agents of 8%) regardless the optimum variables in Table 6. The SEM-EDX mapping was used to distinguish the effect of three silane agents. Silica content of uncoated glass (33.6%) remained less than that of coated glass with several modifying agents. Through the same procedure, the highest increase of silica content can be achieved when silica coating is modified with MTMS (37.88%). Meanwhile, the roughness of coated glass with HMDS resulted in a smoother surface and contact angle less than MTMS due to reduced roughness. Moreover, the hydrophobicity can be affected by modification agent ratios in releasing a contact angle [38].

3.4 The Surface Roughness Analysis

Table 7 summarizes the height surface of coated glass regard with height of surface (nm) and root average (Ra, nm). The height of surface silica from modified silica coating by MTMS, PDMS, and HMDS released the height surface approximately 48-76, 25-73, and 9-20 nm, respectively. Moreover, the Ra of coated by MTMS, PDMS, and HMDS about 29-57, 16-19, and 5-13 nm, respectively. It confirmed the contact angle report (Table 6) that the silane agent of MTMS generated higher contact angle higher the height of surface and the Ra. The silane agent of MTMS on glass coating given a constructive effect on the surface roughness [38].

4.0 CONCLUSION

Considering the results of this study, we can conclude that the manufacture of silica glass coating films from geothermal waste using the sol-gel method obtained the best results with the silica sol-to-HCl ratio at 1/8 (v/v). The conditions obtained a surface area of 165.44 m²/g, which was higher than that obtained with other ratios. Based on contact angle
measurements, the glass coating using a modified thin layer of silica produced a hydrophobic glass surface with a contact angle of >90°. However, after optimization, the highest contact angle achieved was 130.9° with desirability of 94.0% obtained by using of 2% sodium silicate concentration and 2% MMSs.

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