The Effect of Co-Additives (Biochar and FGD Gypsum) on Ammonia Volatilization during the Composting of Livestock Waste

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Abstract: The effectiveness of co-additives for improving livestock waste composting (reduction of air pollution and conservation of nutrients) was investigated. Biochar and Flue gas desulphurization gypsum (FGD gypsum) were used to supplement the composting of a mixture of slaughter waste, swine slurry, and sawdust. Different compositions of additives (0% or 5% each, 10% biochar or FGD gypsum) were tested in triplicate on the laboratory scale. In addition, the effects of two different aeration schemes (continuous and intermittent) were also investigated. Ammonia volatilization, physicochemical characteristics, and compost maturity indices were investigated. The results indicated that the use of the co-additive (Biochar and FGD gypsum) during composting of livestock waste led to a reduction of ammonia volatilization by 26–59% and to a 6.7–7.9-fold increase of nitrate accumulation. The total ammonia volatilization of intermittent aeration treatment was lower than that of continuous aeration using co-additives treatment. It was concluded that co-additives (biochar and FGD gypsum) might be utilized in livestock waste composting to reduce ammonia volatilization and improve nutrient conservation.

Keywords: livestock waste; composting additives combination; ammonia; volatilization

1. Introduction

The livestock sector globally is highly dynamic and is organized in long market chains that employ at least 1.3 billion people worldwide and directly support the livelihoods of 600 million poor smallholder farmers in the developing world [1]. However, the waste from livestock industrial activities (for example manure, slaughter waste), is the major source of negative environmental impacts (that is, the release of greenhouse gases or excess nutrients, salt accumulation, growth of pathogenic microorganisms, odor, and so on), which are capable of influencing both humans and animals [2,3]. Composting is an effective technology for treatment and disposal of livestock and agricultural waste. This is because it can be converted to sanitary and marketable organic fertilizer [4,5]. The stabilization process during composting kills most parasites, pathogens, and viruses contained in the livestock waste [6,7].

Nevertheless, the process of aerobic composting can cause problems. Several chemical compounds (for example, hydrogen sulfide (H2S), trimethylamine (TMA), ammonia (NH3), 2-pentanone, 1-propanol-2-methyl, dimethyl sulfide, dimethyl disulfide, dimethyl trisulphide, and acetophenone) were identified as the main potential odor contributors from composting, which were correlated with
both the aeration rate and the ratio of bulking agent to waste during composting [8,9]. Among the potential odor compounds, ammonia (NH₃) is a major component that causes odors nuisance and toxicity to humans and plants [10]. Nitrogen losses that occurred during composting resulted in the emission of ammonia (NH₃) gas (ammonia volatilization) accounted for 24–33% of the initial N in household waste [11], 46.8–77.4% of the initial N of a mixture of straw and manure [12], 62% of the initial N was during composting of poultry layer manure [13], and 24–64% of the nitrogen was in organic waste [14]. The volatilization of ammonia deteriorating both human health and the environment would reduce the fertilizer value of the organic waste. Barrington et al. [15] reported that carbon availability, bulking agent, particle size, moisture content, and aeration regime are the factors that determine whether composting results in N volatilization as odor or N immobilization into organic components. The odor emission rate was correlated with both the aeration rate and the ratio of bulking agent to waste when composting [8].

The utilization of chemical and biological additives to mitigate ammonia volatilization and nitrogen loss during the composting process has been extensively studied. These additives have included wood fly ash, lime, phosphor-gypsum, polyethylene glycol, jaggery [16], zeolite [17], bentonite [18], superphosphate [19], and microbial inoculants [20]. Among these additives, biochar was popular to be amended in the composting mixture. Biochar is a carbon rich material produced by the thermal decomposition of biomass, was effective for reducing volatilization of ammonia during the composting of a mixture of sewage sludge and wood chips [21]. The faster decomposition process in the bio-oxidative phase led to lower greenhouse gas emissions being observed when biochar was added at the beginning of the composting process [22,23]. Reduction in readily available P was observed when biochar was applied during compost storage [22]. Biochar addition at 3% could reduce the composting time by 20% [24]. As a composting additive, biochar favored microbial activity [25,26]. Jindo et al. [26] reported a higher diversity of fungi in biochar-amended compost. Biochar materials strongly sorb polycyclic aromatic hydrocarbons (PAHs) and are thus characterized by very high sorption coefficients (K_D) for PAHs [27].

It was also reported that the N loss was mitigated by adding FGD gypsum to composting materials [28,29]. Flue gas desulphurization gypsum (FGD gypsum) is a by-product of wet gas desulphurization in coal-fired power stations and generally has a high purity, low heavy metal content, and is rich in essential mineral nutrients for plants such as S, Si and Ca [30,31]. The volatilization of ammonia and N loss were reduced by combining organic N-rich organic waste with FGD gypsum during the composting process [29]. The nitrogen compounds of humic substance in compost with FGD gypsum was higher than that in compost without FGD gypsum [30]. Gypsum has been known as an effective product used in the remediation of sodic soils, by greatly reducing the exchangeable Na, K, and Mg cation concentrations in the sodic soils [32,33]. Approximately 1–2 wt % of FGD gypsum was used to reclaim the sodic soil which resulted in no obvious heavy metal contamination [31]. Guo et al. [30] suggested adding 10% FGD gypsum to compost material to reduce nitrogen loss during composting. Information is still limited on the co-additive means of more than one additive supplemented together when applied with different aeration methods during the composting of livestock waste. Accordingly, the objectives of this research were to investigate the effect of co-additives (FGD gypsum and biochar) and the different aeration schemes (Continuous and Intermittent) on the performance of livestock waste composting and on its product.

2. Materials and Methods

2.1. Feedstock Preparation and Experimental Setup

The mixture of swine slurry and slaughter waste were utilized as livestock waste in this study. Mixtures of swine slurry and slaughter waste for composting trials were not commonly applied yet in South Korea. The swine slurry was obtained from the swine farm station of Seoul National University. The slaughter waste was obtained from a local slaughter house in Yeongcheon City (North Gyeongsang
Province, Korea). These livestock wastes functioned as the main substrate for the composting process. Sawdust was utilized as a bulking agent and was obtained from the local municipality. The Biochar was obtained from the local producer in Gyeonggi province, South Korea. It was produced from combination of hardwood (80%) and softwood (20%) by the pyrolysis process at 550 °C. FGD gypsum was obtained from the KEPCO coal-fired power plant of South Korea. Prior to composting, the physicochemical properties of the raw materials were given in Table 1.

Table 1. Properties of raw materials used for composting experiment.

|                  | Swine Slurry | Slaughter Waste | Sawdust | Biochar | FGD Gypsum |
|------------------|-------------|-----------------|---------|---------|------------|
| pH               | 8.09        | 6.23            | 7.59    | 10.99   | 8.54       |
| EC (µS/cm)       | 22.25       | 6.85            | 0.15    | 0.73    | 2.69       |
| BD (g/L)         | 1059.75     | 1133.92         | 243.57  | 515.29  | 703.33     |
| TS (%)           | 6.27        | 26.11           | 81.49   | 90.35   | 77.75      |
| VS (%TS)         | 72.13       | 94.91           | 98.99   | 65.90   | 3.04       |
| Ash (%)          | 27.85       | 5.09            | 0.94    | 34.10   | 96.06      |
| TOC (%TS)        | 41.85       | 55.05           | 57.42   | 38.23   | 2.41       |
| TKN (%TS)        | 6.74        | 6.26            | 0.37    | 0.36    | n.d        |
| C/N              | 6.21        | 8.79            | 155.18  | 105.02  | n.d        |

EC = Electrical conductivity; BD = Bulk density; TS = Total solid; VS = Volatile solid; TOC = Total organic carbon; TKN = Total Kjeldahl Nitrogen; C/N = C/N ratio.

The experiment was prepared with eight different sets of composting mixtures with different co-additive combinations and aeration schemes labelled CC, BC, FG, FB, CC-I, BC-I, FG-I, and FB-I respectively (Table 2). Mixed raw materials of an amount of 5 kg were composted in 15 L cylindrical laboratory scale composter reactors (height 30 cm × inner diameter 25 cm) covered with polyurethane insulation material to prevent heat loss (Figure 1). The experiment was conducted for 28 days. The compost pile was stirred on Day 7, 14, and 21. Samples of approximately 150 g each were collected just after the materials were stirred; then were kept at 4 °C for later physicochemical analysis. The aeration rate of 0.75 L/min·kg VS was set to keep the oxygen concentration above 15%, as suggested by References [33] and [34]. For the intermittent aeration, the air pump was left off for 135 min. then a timer switched on the high flow air pump for 15 min. to provide air at about 0.75 L/min·kg VS. The composition ratio of raw material was considered to reach the initial moisture content of about 55–60% as most suitable condition for the composting process.

Table 2. Feedstock composition ratio of treatment compost.

| Treatment | Feedstock Ratio (% Wet Weight) | Additive (% Raw Feedstock on Wet Weight) | Aeration       |
|-----------|--------------------------------|------------------------------------------|----------------|
|           | Slaughter Waste (%) | Swine Slurry (%) | Sawdust (%) | FGD Gypsum (%) | Biochar (%) |                  |
| CC        | 41.7              | 16.7            | 41.6        | -              | -          | continuous       |
| BC        | 41.7              | 16.7            | 41.6        | -              | 10         | continuous       |
| FG        | 41.7              | 16.7            | 41.6        | 10             | -          | continuous       |
| FB        | 41.7              | 16.7            | 41.6        | 5              | 5          | continuous       |
| CC-I      | 41.7              | 16.7            | 41.6        | -              | -          | intermittent     |
| BC-I      | 41.7              | 16.7            | 41.6        | -              | 10         | intermittent     |
| FG-I      | 41.7              | 16.7            | 41.6        | 10             | -          | intermittent     |
| FB-I      | 41.7              | 16.7            | 41.6        | 5              | 5          | intermittent     |
2.2. Physicochemical Parameter Analysis

Samples of the raw materials and treatment mixtures were air dried, ground up into small particles using porcelain mortar, and passed through a 2-mm sieve. The sieve samples were analyzed for physicochemical properties. The physicochemical characteristics of samples and raw materials were analyzed using methods on dry weight basis [35]. The moisture content was determined by drying fresh samples at 105 °C until the mass loss in 24 h was less than 0.5% relative to the previous day. Volatile solid was measured by dry combustion of dried samples (550 °C for 4 h). The pH and electrical conductivity (EC) were determined using a pH meter (Inolab, WTW, GmbH, Weilheim, Germany) and an EC214 conductivity meter (Hanna Instruments, Ltd., Sarmeola di aarubano, Italy) respectively. The sample was suspended in distilled water in a ratio of 1:10 (w/v). This suspension was shaken in a mechanical shaker at 230 rpm for 30 min and allowed to stand for an hour prior to pH and EC measurement. Bulk density of compost material was defined as its weight per unit volume according to Thompson [36]. The Kjeldahl Nitrogen (TKN) content was determined according to the Kjeldahl digestion method [37]. The TOC was determined by the Walkley Black method [38]. C/N ratio was estimated by divided the TOC to the TKN. Inorganic nitrogen NH$_4^+$, NO$_3^-$, and NO$_2^-$ were extracted using 2 mol/L KCL (10:1 V/m), and then analyzed using DR 5000 UV-Vis spectrophotometry (Hach Co., Loveland, CO, USA). The ambient temperature and compost temperature in the center of the composting mixture were recorded hourly by a temperature sensor and data logger (T&D recorder TR52i, Shinagawa, Japan). NH$_3$ was measured by washing bottle according to the method presented by Ren et al. [39]. Ammonia gas released during composting was captured in boric acid and was determined by the spectrophotometric method (Hach Co., Loveland, CO, USA).

The phytotoxicity was evaluated according to the method proposed by Sellami et al. [40] with modification. The Germination Index (GI) was determined by extracting 20 g (dry weight) of compost with 200 mL of distilled water, stirring for 2 h, and then centrifuging at 9000 r/min. Ten Raphanus sativus (white radish) seeds were evenly distributed on filter paper in Petri dishes (10 cm diameter) and moistened with 5 mL of compost extract. Three replicate dishes for each sample were incubated at 25 °C for three days. The number of seeds that germinated was recorded. As a control, 5 mL of distilled water was used to replace the compost extract. The GI was calculated according to the Equation (1):

\[
GI\% = \frac{\text{seed germination} \times \text{root length of treatment}}{\text{seed germination} \times \text{root length of control}} \times 100\%
\]  

(1)
Elemental analysis (that is, P, K, Na, Ca, Mg, Fe, Mn, Cu, Zn, and S) of the samples were performed according to standard nitric acid-hydrochloric acid digestion (3030 F, APHA) [35] and using inductively coupled plasma (ICP) atomic emission spectroscopy (AES) (ICPS-7510; Shimadzu Corp., Kyoto, Japan).

2.3. Statistical Analysis

The physicochemical parameter data reported in this study were analyzed by ANOVA using the statistical package SPSS 21. The average values of the quantitative factors under evaluation were compared by means of Tukey’s test.

3. Results and Discussion

3.1. The Effect on Temperature, pH, and EC

The temperature change during composting is associated with many biological reactions that take place [41]. The increase of temperature has been widely reported to correlate with microbial activities [22,23]. The composting temperature during this experiment is shown in Figure 2A,B. Initially, the temperature in the piles was about 23 °C. On the first day, the temperature increased rapidly in all treatments. The temperature remained above 55 °C for 1–2 days. According to the temperature profiles, the compost with the continuous aeration scheme reached a higher temperature than that of the compost with intermittent aeration. Composting with continuous aeration reached a temperature of 55–60 °C for two consecutive days, while the temperature in the intermittently aerated compost reached 50–55 °C for almost three consecutive days. The composting temperature with intermittent aeration was lower than that with continuous aeration, likely because the oxygen supplied was not constantly adequate for complete bio oxidation [42,43]. The longer thermophilic phase that occurred with intermittent aeration composting was likely a result of the slower degradation of partially decomposed materials transferred from the anaerobic areas to aerobic areas, as explained by Jiang et al. [44]. The fact that the composting temperature remained above 55 °C for three days was adequate to provide standard sterilization of the compost [45]. This phase was followed by a mesophilic phase. This condition corresponded to a typical composting temperature profile at the laboratory scale. According to the temperature profiles, the FGD gypsum additive supplementation did not disturb the composting process. This result was in accordance with the results of Li et al. [18] who reported that composting supplemented with bentonite did not show any stimulatory or inhibitory effects on the composting temperature profile. In this study, the highest temperature was reached in the biochar additive treatment. López-Cano [46] reported that the addition of biochar favored activation of the composting process.

![Figure 2. Cont.](image-url)
The pH change throughout the composting process is shown in Figure 2C. The pH of all treatments showed gradually decrease. The decline of pH is linked to natural acidification as a result of nitrification during the composting process [47]. The co-additives of FGD gypsum and biochar had a significant effect on the compost pH ($p < 0.05$). FGD gypsum supplementation had a greater influence on lowering pH, which was shown by the pH decline from 8.10–8.60 to 5.45–6.93 within 28 days of composting. The gradual decline of the pH was likely due to the formation of low-molecular-weight organic acids and CO$_2$ during the decomposition of organic matter, volatilization of ammonia, and nitrification during the composting process [26,28]. The pH decrease was also attributed to the replacement of Na$^+$ by Ca$^{2+}$ from the FGD gypsum, by which the reaction CO$_3^{2-}$ + HCO$_3^{-}$ generated deposits of CaCO$_3$ [48]. The pH of the compost supplemented with biochar only remained higher. This was probably attributable to the initially high pH. In addition, the rate of ammonia released due to ammonification was higher in this treatment. The pH increase was a result of ammonification and mineralization during composting [42]. The different aeration schemes resulted in no significant difference on the compost pH in this study.
Soluble salt contents were estimated through electrical conductivity (EC). The EC values throughout the composting process are presented in Figure 2D. The initial EC of the treatment with only FGD gypsum was higher. Supplementation with FGD gypsum significantly increased the initial EC of the compost substrate and was likely due to the contribution of the high mineral concentration in FGD gypsum. Possible phytotoxic effects could result in compost with high EC values, which indicates high salinity in the composting product. In this study, we observed that EC values decreased with the composting time in all treatments. The decrease of EC could be caused by the volatilization of ammonia and the precipitation of mineral salts during the composting process [42]. The results observed in this study suggested that the FGD gypsum supplementation did not have a negative effect on the composting process.

3.2. The Effect on Ammonia Volatilization

The results of ammonia emission throughout composting in all treatments are shown in Figure 3. Compared with the control, the cumulative ammonia emitted from composting with FGD gypsum was significantly less with both the continuous or intermittent aeration scheme. Biochar addition resulted in higher ammonia emission than did the addition of FGD gypsum. Intermittent aeration resulted in lower cumulative ammonia emission. In composting with continuous aeration, 90% of the ammonia was emitted during the first ten days after commencement of composting whereas with intermittent aeration, the ammonia emission was distributed over 20 days after the composting start. The higher ammonia emission with the biochar additive could be attributed to higher pH and temperature. Tiquia and Tam [49] reported that the loss of N by NH$_3$ volatilization was significant at pH levels above 7.0 and higher temperatures (>40 °C) [49]. Furthermore, at a higher pH, non-volatile ammonia ions were converted to the volatile ammonia form [50]. The highest NH$_3$ volatilization rates in the present study occurred at 50 °C. It was likely because the high temperature affects ammonia volatilization by inhibiting the nitrification process [51].

The reduction of ammonia volatilization in this experiment could be attributed to a lower pH and to ammonia absorption affected by the addition of FGD gypsum. Jeong and Kim [52] found that using amendments such as bauxite residues or biodegradable plastics could control compost pH. Guo et al. [30] reported that FGD gypsum has the ability to absorb ammonia. In addition, gypsum addition converts the ammonium carbonate to ammonium sulfate along with the formation of calcium carbonate [30]. The N in ammonium carbonate is much more apt to be lost as ammonia than when it is in the form of ammonium sulfate [29]. We observed that by FGD gypsum supplementation, NH$_3$ volatilization could be reduced by 75.46% with continuous aeration, in comparison to the control. Co-additive supplementation with FGD gypsum and biochar reduced the ammonia volatilization by 58.93% with continuous aeration, in comparison to the control. Supplementation by biochar increased the ammonia volatilization by about 22.17% in comparison to that of the control. By intermittent aeration, FGD gypsum alone and co-additive supplementation reduced the ammonia volatilization by 52.64% and 25.87%, respectively. These results were in accordance with the results of Koenig et al. [51] who demonstrated that aluminum sulfate; chloride salts of aluminum, calcium and magnesium; gypsum; and surface-applied sodium bisulfate reduced the NH$_3$ volatilization by 0–87%, depending on the rate and intervals of incubation. We observed in the present study that the lower NH$_3$ volatilization rates mostly related to the reduction in the pH of the substrate. The results of the present study show that ammonia volatilization after biochar treatment was significantly higher than that of other treatments. Biochar supplementation increased ammonia volatilization by 63.24% in comparison to that of the control. These results contrast with earlier findings that suggested that co-composting with biochar might reduce ammonia emission and increase nitrification [53]. The possible explanation of this result is that the high initial pH and temperature of the composting substrate induced the higher volatilization of ammonia. Schomberg et al. [54] found that biochar and biochar mixed with ash have the potential to raise the substrate pH. Mandal et al. [55] explained the significant linear relationship between the soil pH values and the cumulative NH$_3$ volatilization from soils. Ammonia volatilization
is favored at alkaline pH and when a high concentration of NH$_4^+$ is present. When NH$_4^+$ and OH$^-$ are present in the substrate, the OH$^-$ ions readily react with NH$_4^+$ ions, thereby resulting in the release of NH$_3$ gas [56], as described in Equation (2).

\[
\text{NH}_4^+ + \text{OH}^- \rightarrow \text{NH}_3 \uparrow + \text{H}_2\text{O}
\]  

Equation (2)

Schomberg et al. [38] demonstrated that NH$_3$ volatilization increased when biochar with a high pH was applied. This was because at high pH, the ammonification process accelerated, thereby increasing the NH$_3$ volatilization. A corresponding increase in NH$_3$ volatilization was observed as a result of the higher pH (increased OH$^-$ concentration) during the first seven days of composting unless treatment with FGD gypsum occurred along with continuous aeration. The high ammonification process seems to have stopped after the first seven days of composting, and the nitrification process started with a corresponding decline in NH$_3$ volatilization and compost pH. The decline of the compost pH could be attributed to the nitrification reaction. NH$_4^+$ ions oxidized directly to NO$_3^-$ ions and released H$^+$ ions, which subsequently reduced NH$_3$ volatilization. The slow mineralization of N was reported to be one possible reason for the low NH$_3$ volatilization [55]. The explanation of low NH$_3$ and high NH$_4^+$ with FGD gypsum treatment could be that acidic surfaces (low pH) can protonate NH$_3$ gas to form NH$_4^+$ ions, as in Equation (3).

\[
\text{NH}_3 + \text{H}^+ \rightarrow \text{NH}_4^+
\]  

Equation (3)

The treatment with intermittent aeration shows many peaks of ammonia emission even after 14 days composting (Figure 3B). According to Tiquia and Tam [49] and Liang et al. [57], the occurrence of several NH$_3$ emissions peaks could be explained in three ways. (1) Part of the organic N was first degraded to some simple N-containing compounds and stored in the compost. These compounds were mineralized after biodegradation slowed down; (2) A slowly degradable fraction with high content of biodegradable N was mineralized; (3) NH$_4^+$ released from ammonification at the beginning of the treatment was first immobilized in the biomass; then, the remineralization of the biomass was responsible for the next peak of NH$_3$ emissions. Furthermore, it was explained that during incomplete nitrification, under the effect of ammonia monoxygenase, NH$_3$ is oxidized sequentially to hydroxylamine (NH$_2$OH) and nitroxyl (NOH) by hydroxylamine oxidoreductase, which can be converted to N$_2$O [58]. Koenig et al. [51] also reported that the increase of NH$_3$ volatilization could be due to the physical effects from changes in materials and pore-space causing enhanced ventilation, as well as of improved aerobic decomposition during composting. In later work, de Guardia et al. [59] demonstrated that NH$_3$ emissions were much higher at higher aeration rates and suggested the importance of the mineralization of organic N.

![Figure 3. Cont.](image-url)
3.3. The Effects on Organic Matter, TKN, C/N, NH$_4^+$, NO$_3^-$, NO$_2^-$, NH$_4^+$/NO$_3^-$

The effects of treatments on TOC throughout the composting are shown in Figure 4A. TOC content slightly decreased in all treatments. There was no significant effect from the aeration schemes on the decrease of TOC during the composting in this experiment, however by co-additive treatment, the decrease in TOC was 4.98% during the 28 days composting. This could be due to the ability of FGD gypsum and biochar to increase the porosity of the compost substrate. Li et al. [18] reported that the decomposition of organic matter was enhanced by the addition of bentonite, clinoptilolite, and zeolite. Gao et al. [42] reported a decrease of 15.4% in 60 days of composting chicken manure. Tiquia and Tam [49] reported 9% organic matter loss during 120 days of chicken manure composting.

The variation of TKN during the composting process is presented in Figure 4B. The TKN content improved by the addition of bentonite during swine manure composting. The TKN increase can be attributed to a concentration effect as a consequence of the degradation of organic compounds because composting biomass is reduced faster than nitrogen [47]. The loss of TKN during the first week of composting was likely because of the loss of ammonia due to the volatilization at a relatively high temperature. TKN increased the most in co-additive treatment (5% FGD gypsum and 5% biochar). This result was likely associated with the additive combination speeding up the degradation rate during the composting process. The large specific surface area of the biochar was more favorable for microbial attachment. In addition, the porosity of the biochar made air and moisture available to the compost material, which is favorable for the decomposition process in composting [47]. On the other hand, FGD gypsum supplied more mineral nutrient sources for microbial growth, which accelerated the decomposition of organic matter.

The mineralization of organic matter during composting led to the gradual decrease of the C/N ratio (presented in Figure 4C). The C/N ratio of the control and biochar treatment slightly increased in the first week of composting; then gradually decreased as the composting progressed. The slight increase of the C/N ratio in the first week of the composting process could be due to vigorous ammonia volatilization [49]. Organic matter degradation and nitrogen compound mineralization then responded to the reduction of the C/N ratio during composting [18]. The C/N ratio in all treatments during composting in this experiment decreased from around 34.64 to 25.36. These results were in accordance with those in another reported by Tiquia et al. [43], in which the decline of the C/N ratio from 28 to 17 was reported during the composting of chicken manure.

The ammonification and nitrification processes were also monitored by determining the concentrations of NH$_4^+$ and NO$_3^-$. The ammonification reaction is indicated by the release of NH$_4^+$, while nitrification is indicated by the production of NO$_3^-$ [35]. The NH$_4^+$ variation throughout the
The composting process is shown in Figure 4D. The \( \text{NH}_4^+ \) content in all treatments decreased gradually during composting. We observed the \( \text{NH}_4^-\text{N} \) decrease rapidly only in the treatments of composting with biochar (BC and BC-I) either by continuous and intermittent aeration (Figure 4D). Reduction of the ammonification rate could be attributed to the alkalinity and high absorptive capacity of the biochar \([31,40]\). Chen et al. \([60]\) reported that the application of alkaline biochar with a high absorptive capacity played a major role in maintaining the soil pH, enhanced the adsorption of \( \text{NH}_4^+ / \text{NH}_3 \), and thereby reduced the \( \text{NH}_3 \) volatilization.

The treatment with Co-additives and continuous aeration showed a rapid decrease of \( \text{NH}_4^+ \). In biochar additive treatment, \( \text{NH}_4^+ \) decreased rapidly after the second week of composting while other treatments showed rapid decreases after the third week of composting (Figure 4D). The increase of \( \text{NH}_4^+ \) during the first week of composting could be due to the decomposition of nitrogen-containing organic matter to form ammonia. The decrease of \( \text{NH}_4^+ \) during composting was attributed to assimilation by microorganisms, to volatilization, and to nitrification \([42]\).

![Figure 4. Cont.](image-url)
As the composting progressed to the cooling phase, the autotrophic nitrifying bacteria increased and the high EC or pH of the additive might disrupt nitrification by inhibiting the growth of nitrifying bacteria [47]. We observed that biochar might serve to overcome the limitation of adding FGD gypsum alone in composting. The NH4+/NO3− ratio is a desirable candidate indicator for compost maturity [30]. The NH4+/NO3− ratio of all treatments in the present study decreased gradually. The NH4+/NO3− ratio of FG-I increased in the first week of composting, which could be due to the inhibition of nitrification and accumulation of NH4+. The addition of FGD gypsum increased the soluble salt, as indicated by the higher EC. The high EC or pH of the additive might disrupt nitrification by inhibiting the growth of nitrifying bacteria [12,15]. Because the presence of biochar provides benefits that induce nitrifying bacteria growth [47], we observed that biochar might serve to overcome the limitation of adding FGD gypsum alone in composting. We also observed a similar pattern of NH4+/NO3− decrease during composting by both continuous and intermittent aeration.

Figure 4. TOC (A); TKN (B); C/N ratio (C); NH4-N (D); NO3+NO2 (E); NH4/NO3 (F) throughout the composting process.

The NO3− + NO2− transformation during composting are shown in Figure 4E. Different aeration schemes showed a different pattern of NO3− + NO2− transformation. In continuous aeration, NO3− + NO2− accumulation started rapidly from the second week of composting, while rapid NO3− + NO2− accumulation under intermittent aeration started after three weeks of composting. Late accumulation of NO3− + NO2− in intermittent aeration treatments could be due to the late activation of nitrifying bacteria. The growth and activity of nitrifying bacteria are inhibited during the temperature conditions of more than 40 °C [42]. The temperature goes down slowly under intermittent aeration, thus the condition in which nitrifying bacteria could actively proliferate was delayed. Co-additives treatment of FGD gypsum and biochar (FB and FB-I) showed the highest NO3− + NO2− accumulation rate (6.72 and 7.90-fold) during the 28 days composting. As the composting progressed to the cooling phase, the autotrophic nitrifying bacteria increased and oxidized NH4+ to NO2−, which was further oxidized to NO3− by nitrite-oxidizing microorganisms. During the intermittent aeration treatment, the presence of biochar increased the porosity of the compost pile, which may induce oxygen penetration and accelerate the nitrification or conversion of NH4+ to NO3− + NO2−. Furthermore, absorption via the transfer of NO3− along with soil pore solution into biochar pores could also be possible. The adsorption of NO3− (an anion) to biochar may also be related to its anion exchange capacity [53].

Figure 4F shows the NH4+/NO3− ratio throughout the composting process. The NH4+/NO3− ratio is a desirable candidate indicator for compost maturity [30]. The NH4+/NO3− ratio of all treatments in the present study decreased gradually. The NH4+/NO3− ratio of FG-I increased in the first week of composting, which could be due to the inhibition of nitrification and accumulation of NH4+. The addition of FGD gypsum increased the soluble salt, as indicated by the higher EC. The high EC or pH of the additive might disrupt nitrification by inhibiting the growth of nitrifying bacteria [12,15]. Because the presence of biochar provides benefits that induce nitrifying bacteria growth [47], we observed that biochar might serve to overcome the limitation of adding FGD gypsum alone in composting. We also observed a similar pattern of NH4+/NO3− decrease during composting by both continuous and intermittent aeration.
3.4. The Effects on Macro-, Micronutrients and Maturity Indices

The effects of the co-additive treatment and aeration scheme on the concentrations of macro- and micro-mineral nutrients are summarized in Tables 3 and 4, respectively. FGD gypsum treatment tends to increase the concentrations of P, Ca, Mg, and S in the compost \( (p < 0.05) \), whereas compost with biochar had elevated amounts of Fe and Mn \( (p < 0.05) \). These high concentrations of minerals can be explained by the nature of the additives and the slaughter waste substrate. In addition, the mineralization process during composting increased the concentration of mineral nutrients. Hu et al. [61] suggested that mature compost should contain a variety of nutrients such as phosphorus \( (2.15 \text{ g/kg}) \), potassium \( (0.79 \text{ g/kg}) \), calcium \( (12.9 \text{ g/kg}) \), magnesium \( (8.0 \text{ g/kg}) \), sulphur \( (3 \text{ g/kg}) \), sodium \( (1.15 \text{ g/kg}) \), iron \( (1.2 \text{ g/kg}) \), along with trace amounts of zinc \( (24.9 \text{ mg/kg}) \), manganese \( (80.4 \text{ mg/kg}) \), copper \( (5.7 \text{ mg/kg}) \), and boron \( (5.7 \text{ mg/kg}) \). The balance of macro and micro nutrients of compost observed in the present study was achieved by the co-additive treatment (combined FGD gypsum and biochar). The compost treated with the co-additive contained no extremely high macro- and micro-mineral concentrations. The observed results show that compost aerated by continuous aeration mostly contains comparatively higher macro- and micro-mineral nutrient concentrations. This indicated that a higher rate of mineralization occurred under continuous aeration than under intermittent aeration. The high mineral concentration of the compost could also be the effect of the mineral content in the raw materials (slaughterhouse and pig slurry), which initially contained a high concentration of minerals.

The maturity indices from the composting test are presented in Table 5. The pH of the compost derived from the present study varied in a range of about 5.50–8.69. The lowest pH was achieved in FG-I (5.50) while the highest pH was achieved in BC-I (8.69). These were significantly different \( (p < 0.05) \) from the controls CC (7.05) and CC-I (6.64). Hogg et al. [62] reported that in most European national standards, compost should have a pH value within the range of 6.0–8.5 to ensure the safety of most plants. Hu et al. [61] suggested that the mature compost was slightly acidic. Most of the compost in this study was within the safe range limit of pH except the treatments with only FGD gypsum additive (FG-I) and only the biochar additive (BC-I). The pH of FG-I (5.5) was slightly more acidic, whereas the pH of BC-I (8.69) was slightly more alkaline. This condition could be attributable to the nature and effect of the additive treatments used in this study. FGD gypsum might induce low pH while biochar might induce high pH in the compost product. The acidic compost has potential use for horticultural growing media because of its pH of 5–6.5, as suggested by Careces et al. [63]. Several elements such as phosphorus, calcium, and magnesium are likely 25–75% available under acidic conditions, as reported by Hu et al. [61].

The EC varied across the eight observed composting treatments (Table 5). FGD gypsum and biochar (as co-additives) significantly altered the EC concentration of livestock waste during composting \( (p < 0.05) \). Compost derived from slaughter waste/slurry/sawdust mix with FGD gypsum and biochar supplementation, had a higher EC \( (p < 0.05) \) (Table 5). The high EC value of treatment FG, FB, FG-I, and FB-I might be attributable to the nature of FGD gypsum, which initially has high EC [64], and the high EC from amendments applied to soils might induce phytotoxic effects in plants. However, the EC of all the compost produced still could be considered as acceptable for nursery production, the limit of which is about 3000 \( \mu \text{S/cm} \), as suggested by Careces et al. [63]. The C/N ratios in the product from all the compost treatments are shown in Table 5. Different additive and aeration schemes did not have a significant effect on the C/N ratio of the compost produced in this study. The compost produced in the present study had a higher C/N ratio than that established by Hu et al. [61] of about 14.6, and by Hogg et al. [62] (<25).
The germination index may reflect the toxicity level of the final compost; a low germination index indicates the potential for the presence of toxic substances. The increase of the germination index during composting is indicative of highly stabilized compost. Low rates of respiration are indicative of highly stabilized compost. Table 3 shows the concentration of macronutrients after 28 days composting in this experiment. Table 4 shows the concentration of micronutrients—after 28 days composting in this experiment. Table 5 shows the characteristic of maturity indices from the composting test.

3.5. The Effect on Germination and Respiration Rate

The germination index of all treatments gradually increased during composting (Figure 5A). The germination index may reflect the toxicity level of the final compost; a low germination index equals to high toxicity contained by the compost, and a high germination index means low toxicity. Because this compost substrate originated from slaughterhouse waste and pig slurry, there is some potential for the presence of toxic substances. The increase of the germination index during composting indicated that the toxicity was decreased. The decline of the toxic level was associated with the decomposition of organic matter and conversion of toxic matter to non-toxic matter. This involved the release of toxic substances (for example, ammonia and low-molecular-weight short chain volatile fatty acids, primarily acetic acid) [65]. We observed from the present study that the co-additive and aeration scheme treatments did not have any significant effect on the germination index and respiration rate of the composting process.

Figure 5B shows the respiration rate in all the composting treatments. According to the results, the rate of respiration of composting with continuous aeration decreased more rapidly than with intermittent aeration treatments. Low rates of respiration are indicative of highly stabilized compost. It was reported that the final compost has a CO₂ respiration rate in a range 0.3–0.6 mg CO₂/g substrate,
which was reached after 80–90 days of composting [66]. We observed that for the compost products from the present study, the CO₂ respiration rate values were in the range of 8.03–13.83 mgCO₂/g-TS after 28 days of composting, which indicated the need for more time to be more stabilized. However, the use of co-additives did not have any negative effects on the compost respiration rate.

![Figure 5](image)

Figure 5. Change in (A) Germination index; (B) CO₂ respiration rate during composting.

4. Conclusions

According to the results of this study, it can be concluded that co-additives treatment using FGD gypsum and biochar did not give adverse effect during the 28 days livestock waste composting process. The selection of appropriate additives needs to be adjusted for the purpose of composting. FGD gypsum supplementation may reduce ammonia volatilization more than biochar supplementation however biochar supplementation may give a faster biodegradation process during composting, thus co-additive treatment during composting might be an alternative method to reduce ammonia volatilization as well as induce the biodegradation process.

Supplementation of livestock waste composting with the co-additives FGD gypsum and biochar reduced ammonia loss and enhanced nutrient recovery. The utilization of these co-additives led to the reduction of ammonia volatilization by 26–59% and to an increase in the nitrate (NO₃⁻) accumulation by 6.7–7.9 fold compared to the initial value. The total ammonia volatilization of the intermittent aeration treatment was lower than that of continuous aeration using co-additive treatments. The macro- and micro-nutrient content were enhanced by the supplementation with these co-additives. The use of co-additives did not have any negative effect on the compost respiration rate and reduced the phytotoxic effect. Some parameter showed that livestock waste composting using co-additives during the 28 days results in waste that is safe to be discharged to the environment, however, the waste will not have matured yet to be utilized as a compost fertilizer. Studies on the co-additive application
on the pilot and large-scale composting are necessary to investigate the effectiveness and economic viability of this method.

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