Electro-magneto-hydrodynamic flow of couple stress nanofluids in micro-peristaltic channel with slip and convective conditions

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Abstract  This study explores the effects of electro-magneto-hydrodynamics, Hall currents, and convective and slip boundary conditions on the peristaltic propulsion of nanofluids (considered as couple stress nanofluids) through porous symmetric micro-channels. The phenomena of energy and mass transfer are considered under thermal radiation and heat source/sink. The governing equations are modeled and non-dimensionalized under appropriate dimensionless quantities. The resulting system is solved numerically with MATHEMATICA (with an in-built function, namely the Runge-Kutta scheme). Graphical results are presented for various fluid flow quantities, such as the velocity, the nanoparticle temperature, the nanoparticle concentration, the skin friction, the nanoparticle heat transfer coefficient, the nanoparticle concentration coefficient, and the trapping phenomena. The results indicate that the nanoparticle heat transfer coefficient is enhanced for the larger values of thermophoresis parameters. Furthermore, an intriguing phenomenon is observed in trapping: the trapped bolus is expanded with an increase in the Hartmann number. However, the bolus size decreases with the increasing values of both the Darcy number and the electroosmotic parameter.

Key words  peristalsis, magnetohydrodynamics (MHD), nanofluid, Hall current, porous medium, thermal radiation

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Peristalsis is a systematic mechanism for carrying and moving fluids. This mechanism is based on the relaxation and contraction of waves in the channel containing the fluid. This phenomenon is typically encountered in physiological systems through mechanical contraction of extensible vessel walls. It is also encountered in industry and physiology, including transport of food through the esophagus[1], embryonic lung morphogenesis[2], transport of chyme in the intestine[3], propulsion of bile in the bile duct, motion of corrosive fluids, and transport of sanitary fluids. Numerous experimental investigations have been performed on the peristaltic motion[4–5]. However, a greater focus is still needed on this phenomenon from the mathematical and computational perspectives. In previous studies, many parameters were considered, such as the types of synchronous vessel oscillation, various physiological fluids, and wall properties. Moreover, recent studies can be found in the references[6–14] about the direction of peristaltic flows. Earlier, Hlew et al.[15] started working on some physiological transport phenomena by studying fluid propulsion by peristalsis of the small intestine. For this purpose, a mathematical model was developed for a viscous fluid in a tube geometry. Tripathi[16] developed a model to analyze the peristaltic chyme (viscoelastic fluid) flow in the small intestine using a cylindrical tube. The peristaltic propulsion of a rigid spherical bolus in a contractile membrane was numerically performed by Bertuzzi et al.[17]. Moradi et al.[18] numerically investigated the peristaltic motion of Newtonian incompressible liquids in annular geometries. The surface waves were superposed with the flow in the annulus by forming axisymmetric waves to achieve the peristaltic effect. Tsui[19] used a multi-dimensional calculation method to simulate peristaltic micro-pump flows. Kumar and Naidu[20] employed a nonlinear streamline quadrature up-winding non-iterative method to solve a two-dimensional (2D) peristaltic flow. A numerical simulation intended to model a soft-acting peristaltic pump was presented by Natarajan and Mokhtarzadeh[21]; this model is useful in the design of blood pumping systems. Radhakrishnamacharya and Srinivasulu[22] analyzed the peristaltic propulsion of viscous liquids in a 2D uniform channel. The hydrodynamic stability of peristaltic waves in a deformable conduit was presented by Chu[23]. The electrostatically peristaltic micro-pump design and simulation were investigated by Lin et al.[24]. Several investigations on peristaltic pumping simulation, analysis, and design were conducted[25–27]. Afifi and Gad[28] employed a mathematical model based on a viscous incompressible fluid flow between infinite parallel walls to analyze the peristaltic motion with a porous medium.

It is normally observed that nanofluids have higher thermal conductivities. In view of this, traditional nanoliquids with base liquids, such as water, oil, and ethylene glycol mixtures have been used to enhance the heat transfer. Metals (e.g., iron, copper, and zinc) typically have higher thermal conductivities than pure liquids. The mixing of nanoparticles into the base liquids generates better transport and thermophysical properties for the nanoliquids. Nanofluids significantly increase the capability of heat transfer owing to their amplified thermal diffusivity and thermal conductivity[29]. Several investigations examined the exclusive features of nanofluids under different flow configurations owing to their useful utility in many engineering and industrial applications. Few studies[30–40] for various situations can be found in the field of nanofluids. The peristaltic motion of nanoliquids is vital in current medication conveyance frameworks in which attractive transitions are utilized to manage the nanoparticles in the circulation system to the tumor site. Among many challenges, the peristaltic propulsion of nanoliquids is now focused on certain endeavors. For example, Hayat et al.[41] investigated the slip consequences on the peristaltic motion of nanofluids using Buongiorno’s model (BM). The same methodology was used to investigate the peristaltic motion of nanoliquids in the studies conducted by Abbasi et al.[42] and Shehzad et al.[43]. The aforementioned studies paid less attention to the direction of magnetic nanoparticles. A nanofluid flow under the influence of magnetohydrodynamics (MHD) plays a crucial role in industrial manufacturing and biomedical...
Electro-magneto-hydrodynamic flow of couple stress nanofluids processes. Noreen et al.\textsuperscript{[44]} discussed the propulsion of MHD nanofluids in a peristaltic channel. Hayat et al.\textsuperscript{[45]} used Carreau nanofluids to discuss the fluid flow in peristalsis under radial MHD effects. Hayat et al.\textsuperscript{[46]} discussed the effects of MHD, slip, and Joule heating on the propulsion of hyperbolic tangent nanomaterials. Shehzad et al.\textsuperscript{[47]} investigated the effects of MHD, thermophoresis, and Joule heating on the peristaltic motion of nanoliquids. The effects of MHD, Joule heating, and wall characteristics on the peristaltic flow of nanoliquids were studied by Hayat et al.\textsuperscript{[48]}.

Among the previous studies mentioned above, there have been no studies addressing the simultaneous influences of magnetic and electrical fields of couple stress nanofluids in micro-peristaltic channels under convective and slip boundary conditions with the Runge-Kutta integration scheme. To fill this gap, we propose a new model to discuss the propulsion of couple stress nanofluids through peristaltic micro-channels. The effects of the electrical field, magnetic field, Hall currents, porous medium, thermal radiation, and slip and convective boundary conditions have been considered. The consequences of pertinent factors on the characteristics of flow, such as nanoparticle concentration and heat and mass transfer coefficients, are presented.

2 Mathematical modeling

2.1 Problem formulation

We analyze the propulsion of couple stress nanofluids through a peristaltic micro-channel of the width 2\(d\). The effects of the electric field, magnetic field, Hall currents, thermal radiation, heat source/sink, and convective and slip boundary conditions are considered. The Cartesian coordinate system is assumed for the proposed analysis, with the \(X\)-axis parallel to the wave propagation and the \(Y\)-axis transverse to the flow situation. The uniform magnetic field \(B_0\) is considered to be in the opposite direction of the flow. The complete geometry of the micro-peristaltic channel is shown in Fig. 1.

![Geometry of symmetric peristaltic channel](color online)

The walls of the aforementioned problem can be expressed as\textsuperscript{[49]}

\[
  H(X, t) = \pm \left( d - a \cos^2 \left( \frac{\pi}{\Lambda}(X - ct) \right) \right).
\]

(1)

Here, \(d\), \(a\), \(\lambda\), \(c\), and \(t\) are the channel’s half-width, channel’s wave amplitude, wavelength, wave speed, and time, respectively. The governing equations can be expressed for a couple stress nanofluid flow as follows\textsuperscript{[49–51]}:

\[
  \frac{\partial U}{\partial X} + \frac{\partial V}{\partial Y} = 0,
\]

(2)
\[ \rho_i \left( \frac{\partial U}{\partial t} + U \frac{\partial U}{\partial X} + V \frac{\partial U}{\partial Y} + W \frac{\partial U}{\partial Z} \right) = -\frac{\partial P}{\partial X} + \mu_i \left( \frac{\partial^2 U}{\partial X^2} + \frac{\partial^2 U}{\partial Y^2} \right) - \eta \left( \frac{\partial^4 U}{\partial X^4} + 2 \frac{\partial^3 U}{\partial X^2 \partial Y^2} + \frac{\partial^2 U}{\partial Y^4} \right) \\
- \frac{\sigma_i B_0^2 U}{1 + m^2} - \frac{\mu_i \phi_i U}{k_0} + \rho_c E_X + (1 - C_0) \rho_i g \beta_i (T - T_0) - (\rho_p - \rho_i) g \beta_i (C - C_0), \quad (3) \]

\[ \rho_i \left( \frac{\partial V}{\partial t} + U \frac{\partial V}{\partial X} + V \frac{\partial V}{\partial Y} + W \frac{\partial V}{\partial Z} \right) = -\frac{\partial P}{\partial Y} + \mu_i \left( \frac{\partial^2 V}{\partial X^2} + \frac{\partial^2 V}{\partial Y^2} \right) - \eta \left( \frac{\partial^4 V}{\partial X^4} + 2 \frac{\partial^3 V}{\partial X^2 \partial Y^2} + \frac{\partial^2 V}{\partial Y^4} \right) \]

\[ (\rho' c')_T \left( \frac{\partial T}{\partial t} + U \frac{\partial T}{\partial X} + V \frac{\partial T}{\partial Y} + W \frac{\partial T}{\partial Z} \right) = \alpha_1 \left( \frac{\partial^2 T}{\partial X^2} + \frac{\partial^2 T}{\partial Y^2} \right) - \left( \frac{\partial q_r}{\partial X} + \frac{\partial q_r}{\partial Y} \right) \\
+ \left( \rho' c' \right)_p \left( D_B \left( \frac{\partial C}{\partial X} + \frac{\partial C}{\partial Y} \right) \right) \\
+ \frac{D_T}{T_m} \left( \left( \frac{\partial T}{\partial X} \right)^2 + \left( \frac{\partial T}{\partial Y} \right)^2 \right) + Q_0 (T - T_0), \quad (5) \]

\[ \left( \frac{\partial C}{\partial t} + U \frac{\partial C}{\partial X} + V \frac{\partial C}{\partial Y} + W \frac{\partial C}{\partial Z} \right) = D_B \left( \frac{\partial^2 C}{\partial X^2} + \frac{\partial^2 C}{\partial Y^2} \right) + \frac{D_T}{T_m} \left( \frac{\partial T}{\partial X} \right)^2 + \left( \frac{\partial T}{\partial Y} \right)^2 \right), \quad (6) \]

where the parameters \( U \) and \( V \) are the velocities in the flow and transverse directions, respectively. \( \rho_i \), \( \rho_c \), and \( \rho_p \) represent the density of fluids, the electrical charge density, and the density of nanoparticles, respectively. \( P \) is the dimensionless fixed frame pressure. \( \mu_i \) is the effective dynamic viscosity of the nanofluids, and \( \eta \) is the dimensional couple stress fluid parameter. \( \sigma_i \) and \( m \) denote the effective electric conductivity and the Hall current parameter, respectively. \( \phi_i \) is the porosity of the medium, and \( k_0 \) is the permeability. \( E_x \) is the electric field. \( C_0 \) and \( C \) are the ambient and nanoparticle concentration of the nanofluids, respectively, and \( g \) is the gravitational acceleration due to the gravity. \( \beta_i \) and \( \beta_c \) are the effective thermal expansion coefficient of the nanoliquid and the expansion coefficient of the nanofluid with concentration, respectively. \( T \) and \( T_0 \) are the dimensionless temperature and the ambient temperature, respectively. \( T_m \) is the mean temperature, and \( Q_0 \) is the volumetric rate of heat source. Equation (5) can be reduced with the help of the Rosseland approximation, which is given by \( q_r = \frac{4 \sigma T^4}{3 K_B} \). The difference in temperature may be expanded in the form of Taylor's series such as \( T^4 \) about \( T_0 \), and after neglecting the higher terms, we obtain \( T^4 \equiv 4 T_0^4 - 3 T_0^4 \), where \( \alpha \) and \( \alpha^* \) represent the Stefan-Boltzmann constant and the mean absorption coefficient of the nanofluids, respectively.

### 2.2 Electro-hydrodynamics

Poisson’s equation of the electric potential \( \Phi \) can be expressed as

\[ \frac{\partial^2 \Phi}{\partial X^2} + \frac{\partial^2 \Phi}{\partial Y^2} = -\frac{\rho_e}{\varepsilon_d}, \quad (7) \]

where \( \rho_e \) and \( \varepsilon_d \) are the electrolyte net charge density in the presence of an electric double layer and the dielectric constant, respectively.

The electric charge density is given by

\[ \rho_e = -2 n_0 e \varepsilon_d \sinh \left( \frac{e \varepsilon \Phi}{K_B T_e} \right), \quad (8) \]

where \( n_0 \), \( e \), \( z \), \( K_B \), and \( T_e \) represent the bulk concentration, the electric charge, the charge balance, the Boltzmann constant, and the absolute temperature, respectively.
With the help of Debye-Hückel linearization, Eq. (7) is reduced to
\[
\frac{\partial^2 \Phi}{\partial X^2} + \frac{\partial^2 \Phi}{\partial Y^2} = \frac{2n_0\varepsilon^2\gamma^2}{\varepsilon_{ef}K_B T_e} \Phi. \tag{9}
\]

### 2.3 Wave frame transformations and scaling of governing equations

The transformations of fixed and wave frames of reference can be introduced as follows:
\[
x = X - ct, \quad y = Y, \quad u = U - c, \quad v = V, \quad p = P, \quad \overline{T} = T, \quad \overline{C} = C. \tag{10}
\]

The scaling parameters for the current governing equations can be expressed as
\[
\begin{aligned}
\bar{x} &= \frac{x}{X}, \quad \bar{y} = \frac{y}{d}, \quad \bar{u} = \frac{u}{c}, \quad \bar{v} = \frac{v}{c^2}, \quad \bar{\sigma} = \frac{\sigma}{\mu c}, \quad \bar{\theta} = \frac{\theta}{\lambda}, \quad \bar{c} = \frac{c}{\mu c}, \quad \bar{\phi} = \frac{\phi}{\mu c}, \\
\bar{\rho} &= \frac{\rho}{\rho f}, \quad \bar{\mu} = \frac{\mu}{\mu f}, \quad \bar{\lambda} = \frac{\lambda}{\lambda f}, \quad \bar{D} = \frac{D}{D f}, \quad \bar{\gamma} = \frac{\gamma}{\gamma f}, \quad \bar{\tau} = \frac{\tau}{\tau f}, \\
\bar{G}_{r_t} &= \frac{(1 - C_0)c^2 \mu_c g \beta T_0}{\mu c}, \quad \bar{G}_{r_c} = \frac{(1 - \rho_{f}^2) \mu_c g \beta C_0}{\mu_c}, \quad \bar{K} = \frac{d}{\varepsilon_{ef}K_B T_e}, \quad \bar{\Phi} = \frac{\Phi}{\xi}, \\
\bar{U}_{hs} &= \frac{\varepsilon_{ef} \xi E X}{\mu c}, \quad \bar{N_b} = \frac{\rho_f (\rho_c') \mu_c D_B C_0}{\mu c}, \quad \bar{N_i} = \frac{\rho_f (\rho_c') \mu_c D_c T_0}{\mu c}, \quad \bar{R_n} = \frac{16\alpha^2 T_0^3}{3\alpha^2 \mu c^2}, \\
\bar{P_r} &= \frac{\mu c^2}{\alpha_1}, \quad \bar{\gamma} = \frac{Q_0 d^2}{\mu c^2}.
\end{aligned}
\tag{11}
\]

Under the above wave transformations (see Eq. (10)), scaling parameters (see Eq. (11)), and the assumptions of long wavelength and lubrication, Eqs. (3)–(6) and Eq. (9) (after dropping the bars) are reduced to
\[
\begin{aligned}
\frac{\partial p}{\partial x} &= \frac{\partial}{\partial y}\left(\frac{\partial u}{\partial y} - a^2 \frac{\partial^2 u}{\partial y^2}\right) - \left(\frac{M^2}{1 + m^2} + \frac{1}{D_a}\right)(u + 1) + k^2 U_{hs} \Phi + G_{r_t} \theta + G_{r_c} \sigma, \\
\frac{\partial p}{\partial y} &= 0, \\
\left(\frac{1 + R_n Pr}{Pr}\right) \frac{\partial^2 \theta}{\partial y^2} + N_b \left(\frac{\partial \theta}{\partial y}\right)^2 + \frac{\gamma \theta}{\gamma} &= 0, \\
\frac{\partial^2 \sigma}{\partial y^2} + \frac{N_i}{N_b} \frac{\partial^2 \theta}{\partial y^2} &= 0, \\
\frac{\partial^2 \Phi}{\partial y^2} &= k^2 \Phi. \tag{16}
\end{aligned}
\]

By introducing non-dimensional stream functions for both velocity components such as \( u = \frac{\partial \psi}{\partial y} \) and \( v = -\frac{\partial \psi}{\partial x} \) in Eqs. (12) and (13), we obtain
\[
\begin{aligned}
\frac{\partial^2 (\partial^2 \psi - a^2 \partial^4 \psi)}{\partial y^2} - \left(\frac{M^2}{1 + m^2} + \frac{1}{D_a}\right) \frac{\partial^2 \psi}{\partial y^2} + k^2 U_{hs} \frac{\partial \Phi}{\partial y} + G_{r_t} \frac{\partial \theta}{\partial y} + G_{r_c} \frac{\partial \sigma}{\partial y} &= 0, \tag{17}
\end{aligned}
\]

where \( \alpha \) is the couple stress nanofluid parameter. \( M \) is the Hartmann number. \( D_a \) and \( k \) are the Darcy number and the electo-osmosis parameter, respectively. \( U_{hs} \) is the Helmholtz-Smoluchowski velocity. \( G_{r_t} \) and \( G_{r_c} \) are the thermal Grashof number and the concentration Grashof number, respectively. \( R_n \) is the radiation parameter, and \( Pr \) is the Prandtl number. \( N_b \) and \( N_i \) are the Brownian motion parameter and the thermophoresis parameter, respectively. \( \gamma \) is the heat generation parameter, and \( u \) is the non-dimensional velocity. \( p \) is the dimensionless pressure gradient. \( \theta \) and \( \sigma \) are the dimensionless temperature and the non-dimensional nanoparticle concentration, respectively, and \( \Phi \) is the dimensionless electric potential.
2.4 Boundary conditions and volumetric flow rate

In the wave frame, the corresponding non-dimensional boundary conditions are

\[
\begin{align*}
\psi &= \frac{F}{2} \frac{\partial \psi}{\partial y} + \alpha \left( \frac{\partial^2 \psi}{\partial y^2} - a^2 \frac{\partial^4 \psi}{\partial y^4} \right) = -1, \quad \frac{\partial^3 \psi}{\partial y^3} = 0, \quad \frac{\partial \theta}{\partial y} + B_h \theta = 0, \\
n \psi &= 0 \text{ at } y = h, \\
\partial \sigma - B_m \sigma &= 0 \text{ at } y = -h,
\end{align*}
\]  

where \( F, \alpha, B_h, \) and \( B_m \) are the instantaneous average volume rate, the dimensionless slip parameter, the thermal Biot number, and the concentration Biot number, respectively. The dimensionless walls are defined as \( y = \pm (1 - \phi \cos^2(\pi x)) \). The flow rate is defined between the fixed and wave frames of reference as follows:

\[
Q = F + 1 - h - \frac{\phi}{2},
\]

where \( F = \int_0^h u dy \), \( Q \) and \( F \) are the non-dimensional flux rates in the fixed and wave frames, respectively, and \( \phi \) is the wave amplitude ratio.

2.5 Physical parameters of engineering interest

The expressions for the non-dimensional skin friction, the nanoparticle heat transfer coefficient, and the nanoparticle concentration coefficient at the walls are given by

\[
\begin{align*}
C_l &= \frac{\partial h}{\partial x} \left( \frac{\partial u}{\partial y} - a^2 \frac{\partial^3 u}{\partial y^3} \right)_{y=h}, \\
Nu &= \frac{\partial h}{\partial x} \left( \frac{\partial \theta}{\partial y} \right)_{y=h}, \\
Sh &= \frac{\partial h}{\partial x} \left( \frac{\partial \sigma}{\partial y} \right)_{y=h}.
\end{align*}
\]

3 Results and discussion

The governing equations (12)–(17) are solved using a numerical procedure with the help of NDSolve MATHEMATIC under suitable boundary conditions. This section is focused on the influence of various quantities on the axial velocity \( u \), the nanoparticle temperature \( \theta \), the nanoparticle concentration \( \sigma \), the skin-friction coefficient \( C_l \), the nanoparticle heat transfer coefficient \( Nu \), the nanoparticle concentration coefficient \( Sh \), and the trapping phenomenon.

Figures 2–6 show the effects of the Hartmann number \( M \), the Darcy number \( D_a \), the couple stress parameter \( a \), the electro-osmotic parameter \( k \), and the velocity slip parameter \( \alpha \) on the velocity distributions. The velocity decreases near the middle of the channel, and the trend is reversed near the walls with an increase in the Hartmann number. This reduction is caused by the Lorentz force, which is a resistive force that leads to a reduction in the velocity at the centre of the channel (see Fig. 2). Figures 3–4 illustrate the influences of the Darcy number and the couple stress parameter on the velocity profiles. It is clear that, the velocity decreases near the channel walls and is enhanced in the center part of the channel. A higher Darcy number provides a nearly clear medium, whereas a lower Darcy number provides a porous medium with more voids. For this reason, higher velocities are observed near the center of the channel. Moreover, note from Fig. 4 that higher velocities are observed for the couple stress nanofluid than for the viscous nanofluid. Figure 5 shows that the velocity increases near the channel walls, and decreases near the center of the channel with an increase in the electro-osmotic parameter. This is due to the electrical double layer (EDL) effect, and the EDL acts as a resistive...
agent for the fluid flows. For this reason, the velocity decreases in the middle of the channel. Figure 6 depicts the effect of different slip parameters on the velocity. It is shown that the velocity increases near the walls of the channel, and the trend is reversed in the middle of the channel. This situation is realistic, because the fluid velocity is no longer equal to that near the walls, and larger velocities will be noticed near the walls when the slip occurs at the walls.

Figure 7–11 show the impacts of $\gamma$, $N_t$, $N_b$, $R_n$, and $B_h$ on the nanoparticle temperature distributions. Figure 7 shows that the nanoparticle temperature decreases when the value of $\gamma$ increases. Figures 8–11 show the effects of $N_t$, $N_b$, $R_n$, and $B_h$ on the nanoparticle temperature distributions, respectively. Note that the nanoparticle temperature increases with higher values of $N_t$, $N_b$, $R_n$, and $B_h$. The thermophoresis parameter is directly affected by the thermophoresis diffusion coefficient, which enhances the movement of nanofluids, and consequently the particles gain kinetic energy, resulting in an increase in the nanoparticle temperature of nanofluids (see Fig. 8). An increase in Brownian motion increases the random motion of the nanoparticles. This increment in random movement causes the particles to gain energy, and thus there will be an increase in the nanoparticle temperature with the increment in the Brownian motion parameter (see Fig. 9). Figure 12 illustrates the effect of $N_t$ on the nanoparticle concentration. The thermophoresis parameter tends to enhance the nanoparticle concentration in the channel. Figure 13 shows that the concentration diminishes when the Brownian motion parameter increases.

The skin-friction coefficient distributions on the right wall of a symmetric channel for different values of $D_a$, $M$, and $k$ are presented in Figs. 14–16. These figures show that the shear stress behavior is oscillatory, which may be due to peristalsis. With increasing values of the Darcy number, the skin friction decreases to a certain range of $x$, and then the skin friction
Fig. 6  Effects of $\alpha$ on $u$ (color online)

Fig. 7  Effects of $\gamma$ on $\theta$ (color online)

Fig. 8  Effects of $N_t$ on $\theta$ (color online)

Fig. 9  Effects of $N_b$ on $\theta$ (color online)

Fig. 10  Effects of $R_n$ on $\theta$ (color online)

Fig. 11  Effects of $B_h$ on $\theta$ (color online)

Fig. 12  Effects of $N_t$ on $\sigma$ (color online)

Fig. 13  Effects of $N_b$ on $\sigma$ (color online)
Electro-magneto-hydrodynamic flow of couple stress nanofluids increases (see Fig. 14). From Figs. 15–16, the skin friction increases for a particular range of $x$, and then the trend is reversed with an increase in the Hartmann number and electro-osmosis parameter. Figures 17–19 depict the impacts of various parameters such as $R_n$, $N_t$, and $N_b$ on the magnitudes of the nanoparticle heat transfer coefficient. The graphical results of the nanoparticle heat transfer coefficient are oscillatory in nature owing to the peristaltic motion of walls. Figure 17 shows that the heat transfer rate decreases for larger radiation parameters. Figure 18 shows the heat transfer coefficient for larger values of the thermophoresis parameter. Figure 19 shows that the heat transfer coefficient decreases with larger values of the Brownian motion parameter. The nanoparticle concentration coefficient $Sh$ on the right wall of a symmetric channel for different values of $N_t$ and $N_b$ is presented in Figs. 20–21. These
figures exhibit an oscillatory behavior, which may be due to peristalsis. The absolute value of shear stress increases with increasing values of $N_t$ whereas different behaviors are observed for $N_b$ in Figs. 20–21. An intriguing phenomenon in the transport of fluid is trapping. It is presented through streamline sketches in Figs. 22–24. The trapped bolus is found to expand by increasing $M$, as shown in Figs. 22(a)–22(d). However, the size of the bolus decreases owing to the rising effects of $D_a$ and $k$, as shown in Figs. 23–24.

4 Conclusions

A mathematical model is used to analyze the combined effects of the transverse magnetic field and the axial electrical field on two-dimensional micro-peristaltic channels with different
Fig. 23  Streamlines for (a) $U_{hs} = 2.0$, $D_a = 0.1$, (b) $U_{hs} = 2.0$, $D_a = 1.0$, (c) $U_{hs} = -2.0$, $D_a = 0.1$, and (d) $U_{hs} = -2.0$, $D_a = 1.0$ (color online)

Fig. 24  Streamlines for (a) $U_{hs} = 2.0$, $k = 1.0$, (b) $U_{hs} = 2.0$, $k = 5.0$, (c) $U_{hs} = -2.0$, $k = 1.0$, and (d) $U_{hs} = -2.0$, $k = 5.0$ (color online)
peristaltic wave propagations at the left and right channel walls (complex wavy scenario) of a couple stress nanofluid. Additionally, the effects of Hall currents, porous medium, thermal radiation, heat source/sink, and slip convective boundary conditions are studied and evaluated. The governing equations are solved using a numerical procedure with the help of NDSolve MATHEMATICA under suitable boundary conditions. The key findings of this study are summarized as below.

(i) The velocity decreases for the increasing values of the Hartmann number.
(ii) An increment in the Darcy number leads to an enhancement in the velocity in the core region.
(iii) Stronger electro-osmosis yields an enhancement in the velocity.
(iv) Nanoparticle concentration increases for the thermophoresis parameter.
(v) A downfall phenomenon is observed in nanoparticle concentration for the Brownian motion parameter.
(vi) Nanoparticle heat transfer decay is recorded for a larger radiation parameter.
(vii) A larger thermophoresis parameter causes an increment in the heat transfer coefficient of nanoparticles.
(viii) The magnetic field tends to enhance the size of the bolus.

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