Optimization of Extrusion and Sphenronization Parameters for Tolterodine Tartrate Pellets by Design of Experiment (DoE)

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Abstract: Objective: The purpose of this indicative DoE is the optimization of Screw Speed and Sphenronization Speed which may impact the final physical and chemical parameters of pellets such as aspect ratio/sphericity, PSD and dissolution which are pre-requisite for further extended release coating on immediate release pellets. From the risk assessment and Pre DoE, Aspect Ratio, Dissolution at 30 min and PSD were identified as critical quality attributes which may be potentially influenced by the factors such as Screw Speed and Sphenronization Speed and their respective levels. Methods: Immediate release pellets of tolterodine were prepared and optimized by employing extrusion spheronomization process. The experimental ranges chosen were based on the development experience and prior knowledge. Since the aim of DoE was to assess the impact of factors that would affect the product critical quality attributes (CQAs), a central composite design was chosen. Results: The optimized process parameters exhibited required dissolution, PSD and aspect ratio of immediate release pellets which are further required for successful extended release coating. DoE statistical analysis demonstrated the impacts of all factors (in the studied range) on the responses studied. Based on the observation suggested model for PSD below # 25 was Linear, for PSD above # 25 is Quadratic, for aspect ratio its Quadratic and for response Dissolution at 30 min its Quadratic. Conclusion: Based on the statistical analysis and considering the scientific rational product performance, it can be concluded that the Factor A (Screw Speed) and Factor B (Sphenronization Speed) were the significant factors which had impact on the response dissolution, aspect ratio and PSD.

Keywords: Tolterodine tartrate, Extrusion-Spheronomization, Central composite design (CCD), Dissolution, Aspect ratio, PSD

1. Introduction

Tolterodine, antimuscarinic (anticholinergic) agent is indicated for treating OAB with symptoms of urinary frequency, urgency and leakage[1, 2]. Tolterodine acts as a competitive antagonist of acetylcholine at postganglionic muscarinic receptors. Both urinary bladder contraction and salivation are mediated via cholinergic muscarinic receptors. After oral administration, tolterodine is metabolized in the liver, resulting in the formation of 5-hydroxymethyl tolterodine (5-HMT), the major pharmacologically active metabolite. 5-HMT, which exhibits an antimuscarinic activity similar to that of tolterodine, contributes significantly to the therapeutic effect. Both tolterodine and 5-HMT exhibit a high specificity for muscarinic receptors, since both show negligible activity and affinity for other neurotransmitter receptors and other potential cellular targets, such as calcium channels[3].

For urge incontinence, medications known as anticholinergics/ antimuscarinics (tolterodine, oxybutynin chloride, darifenacin, fluoxetine hydrochloride, and solifenacin succinate) can prevent bladder spasms and OAB

At the time of research, there was no alternative formulation available other than innovator which was patented and costly. The aim of the present study was to develop a formulation using simpler techniques and circumventing the technology used by the innovator product in order to have technological and commercial advantage along with benefit to society.

In the present research work tolterodine was selected for the development of an ER[4] formulation which was developed as a generic version of Detrol LA, marketed by Pfizer-Pharmacia and Upjohn Co.

The study was directed towards the development of a novel drug delivery system based on pelletization technique and was limited to the development of a formulation which can be commercially exploited for well-being of society in general and meant for the US market in particular.

Tolterodine formulation was developed in two parts where in extrusion pelletization technique is used to develop immediate release pellets of tolterodine tartrate followed by extended release coating using wruster process.

This study was carried out using QbD approach where central composite design was used for design of experiment to optimize the extrusion spheronomization parameters for
development of immediate release pellets formulation of tolterodine.

2. Literature Survey

2.1 Drug Delivery

Humankind’s efforts to confront disease dates back to early civilization. Substances taken from nature were tested and used to treat dysfunctions of physiological life processes, pain and discomfort. With the advancement of science, the active ingredients of these materials, the drugs, were identified, isolated and in many cases their mechanism of action elucidated. New drug candidates are tested even today in the quest to add increasingly effective tools against diseases.

Drug characteristics differ dramatically, even those aimed to treat the same symptoms; chemical composition, size, hydrophilicity and potency identify molecules whose function may be specific or highly complex. An increasing understanding of cellular biology at the molecular level, combined with the (decoding) of the human genome, and a technological breakthrough in the field of proteomics and DNA micro-arrays, has introduced even more applicants, like peptides and nucleic acids (gene delivery).

Drug activity is a result of molecular interaction(s) in certain cells; it is therefore easily deduced that it is necessary for the drug to reach somehow the site of action following administration (oral, intravenous, local, transdermal, etc.) at sufficient concentrations. The scientific field dealing with this issue is known as drug delivery and has essentially the following aim: to deliver the drug at the right place, at the right concentration measured in blood. Here it can be mentioned that during further production, transportation and coating of a retard capsule or a pellet is is optimal both technologically (low powder formation, quick drying, Reduced proneness to agglutination) and because of the relative quantity of the coating Material; e.g. fluidization - granules produced by spraying process - the structure of which can be compared to that of breadcrumbs’ are practically impossible to disrupt with reasonable quantity of coating material. In connection with good coating properties fraction toughness and abrasion hardness derived from the shape and form of the granules and the almost identical specific surface of the particles from successive batches can also be mentioned.

2.2 Pellet

2.2.1 Pellet as a Pharmaceutical Dosage Form:
Although the basic meaning of the word ‘pellet’ is ‘a small ball or tube-shaped piece of Any substance’, in the different branches of industry and agriculture this term is used to indicate particles or piles of particles of various shape, size and scale, which are Produced by granulation, extrusion, pelletisation, drop-frosting *hence forward according to pharmaceutical requirements and specialization. 'Pellet' is to refer to granulated pharmaceutical dosage form for per oral usage, which is characterized by $10^{-3}$ - $10^{-5}$ m in size, near-spherical form, slightly uneven surface and Compactness approximate to that of agglomerated materials (low porosity). Thus the Advantages of the pellet as a pharmaceutical dosage form are implied in the above given Definition [5]

2.2.2 Good Coating Properties
The minimum scale of surface/capacity (volume) relatively Even surface and small degree of porosity from the point of view of coating – especially Film coating - is optimal both technologically (low powder formation, quick drying, Reduced pronseness to agglutination) and because of the relative quantity of the coating Material; e.g. fluidization - granules produced by spraying process - the structure of which can be compared to that of breadcrumbs’ are practically impossible to disrupt with reasonable quantity of coating material. In connection with good coating properties fraction toughness and abrasion hardness derived from the shape and form of the granules and the almost identical specific surface of the particles from successive batches can also be mentioned.

2.2.3 Adjustable Active Ingredient Transmission:
The definite specific surface derived from the near-spherical shape (form) which can reliably influenced by modifying the size of the particles and the good coating properties ensure almost infinitely adjustable active ingredient transmission and plan able active ingredient transmission profile. Regarding the latter we should think - for example - that the ‘small balls’ can be covered by coating different in quality and thickness, and these can be arbitrarily blended together before filling capsules or compression. In this way the ingestion of the initial and the maintaining dose can happen simultaneously and safely, alongside with the elimination of the side-effects caused by top concentration and the continuous assurance of the plasma concentration.

2.2.4 Low Toxicological Risk
If the coating of a retard capsule or a pellet is incomplete/imperfect or damaged a toxic dose may enter the patient’s organism. However, in the capsule fillings or tablets a few (among several hundred or thousand) pellets with damaged coating do not cause significant rise of drug concentration measured in blood. Here it can be mentioned that during further production, transportation and dosing of the pellet - especially in the case of coated granules – the danger of dust formation is minimal, because the pile is practically free from powder and the particles have no sharp ends which, if fractured, could lead to powder formation (Their friability is low).
4. Globulation or Droplet Formation.

2. Hot Melt Extrusion Process.

1. Extrusion - Spheronization Technique or Wet Mass Extrusion.
2. Layer Building Method.
3. Globulation or Droplet Formation.
4. Cryopelletization.

6. Balling.
7. Freeze Pelletization.
8. Compression.

2.4 Extrusion – Spheronization:

ES is the most convenient method used in the pharmaceutical industry to make uniform sized spheroids. It was first reported by Reynolds, Conine and Hadley in 1970 [8]

It is a multistep process involving four steps namely mixing, granulation, extrusion, spheronization and finally drying of prepared pellets [9]. In the first step, powders are dry mixed to obtain uniform dispersion. It is usually carried out in same mixer used for granulation. The uniformity of dry mix has a significant effect on the quality of spherical particles produced.

In the next step, wet mass of sufficient plasticity is produced from the powder dispersion. It is similar to conventional granulation technique used for compressed products. The most commonly used granulator is planetary mixer or sigma blade mixer or high shear mixer and Hobart mixer.

High shear mixer brings in high amount of energy into the wet mass which is transformed into heat and causes evaporation of granulation fluid. This changes the extrusion behavior of the wet mass. This can be avoided by cooling the granulation bowl [10-16].

The next step is extrusion. It consists of shaping the wet mass into long rods termed as ‘extrudates’. It is considered as specialized wet granulation technique as well as integral part of overall spheronization process. The extrusion process is used not only in the pharmaceutical industry but also in the food, ceramic and polymer industries. The extrusion process is currently used as an alternative method for the manufacture of completely water-soluble tablets [17].

In this method, the wet mass is forced through the opening of dies and shaped into small cylindrical particles having uniform diameter. The extrudate particles break at similar lengths under their own weight. The extrudate must have enough plasticity to deform. If it is more, the particles adhere together when collected or rolled in the spheronizer. This operation is the major contributing factor in the final particle size of the pellets. The diameter of the extruder screen opening directly controls the diameter of the extrudate [18,19].

There is great variety of extruders. Extruders are classified based on the extrusion zone. In axial extruders, the wet mass is conveyed and it is forced through a flat perforated plate and extruded in same plane. In radial extruders, the wet mass is transferred perpendicular to the extrusion plane. The screw and gravity extruders are used mainly for development and manufacturing procedure.

The main difference between screw and gravity extruder is that before extrusion less compression force is applied in gravity feed extruder [20, 21].
The next step is spherization. Spherization method was first introduced by Nakahara in 1964. It is a single step process in which the extruded particles refine and form uniform sized spheres. The formation of pellets depends on the formulation of extrudates. The equipment used is spherizer, also called as merumerizer, is simple equipment consisting of a bowl with fixed side walls and fast rotating bottom plate or disk. The sphericity of the pellets depends on the frictional forces applied i.e. force generated by particle-to-particle and particle-to-equipment interaction. The spherization of a product usually takes 2-10mins [22-25]

Drying is the final step in extrusion-spherization method. In this step, prepared pellets are dried at room temperature or at elevated temperature in a tray drier/oven or in fluidized bed drier. The choice of the drier is mainly based on particle properties desired.

Applications:
1) Production of controlled release reservoir system and sustain-release pellets.
2) Useful in masking the bitter taste of an active drug and used in enhancing dissolution rates for poorly water soluble drugs.
3) Improves dissolution and bioavailability of drug by forming solid dispersions or solid solutions.

3. Materials and Methods

Chemicals and reagents
Tolterodine was procured from Cipla, Mumbai, India; hypromellose 2910 USP was procured from Colorcon India Ltd, microcrystalline cellulose and mannitol were procured from Signet chemical, Mumbai, India.

Equipments
Rapid mixer granulator (RMG) (Gansons-31), Gansons Ltd, Mumbai, India; extruder-spherodizer (USPH-60), Umang Pharmatech, India.

Methods

Preparation of immediate release core pellets of tolterodine
Trials to formulate the core immediate release pellets of tolterodine(table 1).

Table 1: Composition of immediate release pellets of tolterodine

| Ingredients               | Function | composition |
|---------------------------|----------|-------------|
| Tolterodine tartrate      | Active   | 4           |
| Microcrystalline cellulose| Diluent  | 100         |
| Mannitol                  | Diluent  | 28          |
| Hypromellose, 2910        | Binder   | 10          |
| Purified water            | Solvent  | qs          |
| Average weight(mg)        |          | 142         |

Extrusion and spheronisation was followed where tolterodine, microcrystalline cellulose and mannitol were sifted through 30 mesh sieve. The resultant material was mixed in a RMG for 10 min. Methocel E5 was dissolved in water and the dry mix was granulated with this binder solution which was followed by extrusion, spheronization and drying.

Table 2: Design Summary

| Design for formulation Component | Optimization Design |
|----------------------------------|---------------------|
| Factors                          | Unit                |
| A: Screw Speed                   | RPM                 |
| B: Spheronization Speed          | RPM                 |
| -1                               | 20                  |
| +1                               | 60                  |
| -1                               | 200                 |
| +1                               | 600                 |

Table 3: Design Layout

| Standard | Run | Space Type | Factor 1 | Factor 2 |
|----------|-----|------------|----------|----------|
|          |     | RPM        |          | RPM      |
| A: Screw Speed | 2   | 1          | 60       | 200      |
|          | 3   | 40         | 400      | 400      |
|          | 4   | 20         | 600      | 600      |
|          | 5   | 40         | 400      | 400      |
|          | 7   | 20         | 600      | 600      |
|          | 10  | 40         | 400      | 400      |
|          | 11  | 2          | 400      | 400      |
|          | 12  | 1          | 400      | 400      |
|          | 6   | 9          | 400      | 400      |
|          | 5   | 10         | 400      | 400      |
|          | 9   | 12         | 400      | 400      |
|          | 8   | 13         | 400      | 400      |

Evaluation of pellets
The pellets of all the batches were evaluated for dissolution, particle size and aspect ratio.

Table 4: Design Summary

| Response | Name             | Units | Acceptance criteria |
|----------|------------------|-------|---------------------|
| R1       | Aspect Ratio     |       | 0.95 to 1.05        |
| R2       | Dissolution at 30 min | %     | 85 to 95           |
| R3       | PSD Above #20    | %     | 5-10               |
| R4       | PSD # 20-25      | %     | 85-100             |
| R5       | PSD below #25    | %     | 5-10               |

4. Results / Discussion
Table 5: Design Layout summary table with outcome

| Standard | Run | Space Type | Factor 1 | Factor 2 | Response 1 | Response 2 | Response 3 | Response 4 | Response 5 |
|----------|-----|------------|----------|----------|------------|------------|------------|------------|------------|
|          |     |            | A:Screw Speed | B:Sphenronization Speed | Aspect Ratio | Dissolution at 30 min | PSD Above #20 | PSD # 20-25 | PSD Below#25 |
|          |     | RPM        | RPM       | %        | %          | %          | %          | %          | %          |
| 2        | 1   | Factorial  | 60        | 200      | 0.72       | 84         | 10         | 88         | 2          |
| 7        | 2   | Axial      | 40        | 200      | 0.79       | 85         | 13         | 84         | 3          |
| 3        | 3   | Factorial  | 20        | 600      | 1.2        | 92         | 2          | 88         | 10         |
| 11       | 4   | Center     | 40        | 400      | 0.89       | 84         | 6          | 90         | 4          |
| 4        | 5   | Factorial  | 60        | 600      | 1.2        | 92         | 3          | 84         | 13         |
| 10       | 6   | Center     | 40        | 400      | 0.87       | 84         | 8          | 87         | 5          |
| 1        | 7   | Factorial  | 20        | 200      | 0.78       | 89         | 15         | 81         | 4          |
| 12       | 8   | Center     | 40        | 400      | 0.89       | 85         | 5          | 91         | 4          |
| 6        | 9   | Axial      | 60        | 400      | 0.85       | 95         | 5          | 90         | 5          |
| 5        | 10  | Axial      | 20        | 400      | 0.9        | 95         | 7          | 88         | 5          |
| 13       | 11  | Center     | 40        | 400      | 0.88       | 85         | 8          | 87         | 5          |
| 9        | 12  | Center     | 40        | 400      | 0.87       | 91         | 6          | 85         | 9          |
| 8        | 13  | Axial      | 40        | 600      | 1.3        | 91         | 4          | 81         | 15         |

Response 1: Aspect Ratio

Table 6: Summary of Model selection

| Source              | Sequential p-value | Lack of Fit p-value | Adjusted R-Squared | Predicted R-Squared |
|---------------------|--------------------|---------------------|--------------------|--------------------|
| Linear              | 0.0000059          | 0.000308            | 0.828625           | 0.748851           |
| 2FI                 | 0.709164           | 0.000233            | 0.812068           | 0.64806            |
| Quadratic           | 0.000179           | 0.013486            | 0.979516           | 0.912526           |
| Cubic               | 0.42939            | 0.0057              | 0.97955            | 0.127889           |

Suggested model for response Aspect Ratio is Quadratic.

Table 7: ANOVA for Aspect Ratio

| Source                | Sum of Squares | Degree of freedom | Mean Square | F Value | p-value Prob > F |
|-----------------------|----------------|-------------------|-------------|---------|-----------------|
| Model                 | 0.3843         | 5                 | 0.0769      | 115.7629| 0.0000 Significant |
| A-Screw Speed         | 0.0020         | 1                 | 0.0020      | 3.0377  | 0.1249          |
| B-Sphenronization Speed | 0.3314         | 1                 | 0.3314      | 499.1149| 0.0000          |
| AB                   | 0.0099         | 1                 | 0.0099      | 1.3557  | 0.2824          |
| A^2                  | 0.0037         | 1                 | 0.0037      | 5.5059  | 0.0514          |
| B^2                  | 0.0493         | 1                 | 0.0493      | 74.2796 | 0.0001          |
| Residual             | 0.0046         | 7                 | 0.0007      |         |                 |
| Lack of Fit          | 0.0042         | 3                 | 0.0014      | 14.1571 | 0.0135 Significant |
| Pure Error           | 0.0004         | 4                 | 0.0001      |         |                 |
| Cor Total            | 0.3889         | 12                |             |         |                 |

The Model F-value of 115.76 implies the model is significant. There is only a 0.01% chance that an F-value this large could occur due to noise. Values of "Prob > F" less than 0.0500 indicate model terms are significant. In this case B, B^2 are significant model terms. Values greater than 0.1000 indicate the model terms are not significant. The "Lack of Fit F-value" of 14.16 implies the Lack of Fit is significant. There is only a 1.35% chance that a "Lack of Fit F-value" this large could occur due to noise.

Final Equation in Terms of Coded Factors:

\[
\text{Aspect Ratio} = 0.88897 -0.01833 \times A + 0.23500 \times B + 0.01500 \times AB -0.03638 \times A^2 + 0.13362 \times B^2
\]

Final Equation in Terms of Actual Factors:

\[
\text{Aspect Ratio} = 0.904598 -0.00165 \times \text{Screw Speed} -3.75E-06 \times \text{Sphenronization Speed} -9.1E-05 \times \text{Sphenronization Speed}^2 +3.34E-06 \times \text{Sphenronization Speed}^2
\]
DoE statistical analysis demonstrated that the impact of all factors (in the studied range) on the response studied was significant. Based on the observation suggested model for aspect ratio is Quadratic.

The Contour plot and 3 D plot showing impact of factor A (Screw Speed) and Factor B (Sphenorization speed). Although model is showing Quadratic relationship, but ANOVA and Contour plot showing Sphenorization speed is main impacting factor on the response aspect ratio. Aspect ratio depicts linear relationship i.e. as the sphenorization speed increases the aspect ratio increases. Also it was observed from the data that aspect ratio throughout the studied ranges is 0.72 to 1.0 i.e. near to 1 which is required.

Response 2: Dissolution at 30 min
Table 8: Summary of Model selection for dissolution

| Source         | Sequential p-value | p-value | R-Squared | R-Squared |
|----------------|--------------------|---------|-----------|-----------|
| Linear         | 0.255425           | 0.194311| 0.086657  | -0.17936  |
| 2FI            | 0.568413           | 0.162963| 0.023213  | -0.15898  |
| Quadratic      | 0.089581           | 0.294534| 0.369657  | -0.68872  |
| Cubic          | 0.934108           | 0.088787| 0.141256  | -22.3516  |

Suggested model for response Dissolution at 30 min is Quadratic.

Table 9: ANOVA for Dissolution at 30 Min

| Source                  | Sum of Squares | Degree of freedom | Mean Square | F Value | p-value | Prob> F |
|-------------------------|----------------|-------------------|-------------|---------|---------|---------|
| Model                   | 120.70         | 2                 | 60.3480     | 6.1341  | 0.018263| Significant |
| B-Sphenronization Speed | 48.17          | 1                 | 48.1667     | 4.8959  | 0.051328|           |
| A^2                     | 72.53          | 1                 | 72.5293     | 7.3723  | 0.021739|           |
| Residual                | 98.38          | 10                | 9.8381      |         |         |         |
| Lack of Fit             | 63.58          | 6                 | 10.5968     | 1.2180  | 0.443629| Not Significant |
| Pure Error              | 34.80          | 4                 | 8.7000      |         |         |         |
| Cor Total               | 219.08         | 12                |             |         |         |         |

The Model F-value of 6.13 implies the model is significant. There is only a 1.83% chance that an F-value this large could occur due to noise. Values of "Prob > F" less than 0.0500 indicate model terms are significant. In this case A^2 is a significant model term. Values greater than 0.1000 indicate the model terms are not significant. The "Lack of Fit F-value" of 1.22 implies the Lack of Fit is not significant relative to the pure error. There is a 44.36% chance that a "Lack of Fit F-value" this large could occur due to noise.
DoE statistical analysis demonstrated that the impact of all factors (in the studied range) on the response studied was significant. Based on the observation suggested model for dissolution is Quadratic. The Contour plot and 3D plot showing impact of factor A (Screw Speed) and Factor B (Sphenronization speed). The Sphenronization speed and screw speed showing Quadratic relationship on the response Dissolution i.e. as the sphenronization speed and screw speed increases the Dissolution increases. Also it was observed from the data that Dissolution throughout the studied ranges is 84.0% to 95.0% which is well within the defined limit.

**Response 3: Particle Size above #20**

![3D plot of Dissolution at 30 Min](image)

**Figure 4: 3 D plot of Dissolution at 30 Min**

The Model F-value of 29.54 implies the model is significant. There is only a 0.01% chance that an F-value this large could occur due to noise. Values of "Prob > F" less than 0.0500 indicate model terms are significant. In this case B, AB are significant model terms. Values greater than 0.1000 indicate the model terms are not significant. The "Lack of Fit F-value" of 0.95 implies the Lack of Fit is not significant relative to the pure error. There is a 53.44% chance that a "Lack of Fit F-value" this large could occur due to noise.
DoE statistical analysis demonstrated that the impact of all factors (in the studied range) on the response studied was significant. Based on the observation suggested model for PSD above # 20 are 2 Factorial interactions. The Contour plot and 3 D plot showing impact of Factor B (Spheronization speed). The Spheronization speed and screw speed showing slightly 2 factorial interactions on the response Particle Size distribution above # 20 i.e. as the spheronization speed and screw speed increases the PSD above # 20 increases, that might be due to agglomeration of fine particles at high speed.

Response 4: Particle Size Distribution between # 20-25

| Source     | Sequential p-value | Lack of Fit p-value | Adjusted R-Squared | Predicted R-Squared |
|------------|--------------------|---------------------|--------------------|---------------------|
| Linear     | 0.8466             | 0.1732              | -0.1607            | -0.8691             |
| 2FI        | 0.1209             | 0.2207              | 0.0273             | -0.5562             |
| Quadratic  | 0.0266             | 0.7039              | 0.5561             | 0.0646              | Suggested         |
| Cubic      | 0.5593             | 0.5849              | 0.5074             | -1.2044             | Aliased           |

Table 12: Summary of Model selection for particle size between #20-25

Figure 5: Particle Size Distribution above # 20

Figure 6: 3 D Plot of Particle Size distribution above # 20
Suggested model for response PSD #20-25 min is Quadratic.

**Table 13: ANOVA for particle size between #20-25**

| Source            | Sum of Squares | Degree of freedom | Mean Square | F Value | Prob> F | p-value |
|-------------------|----------------|-------------------|-------------|---------|---------|---------|
| Model             | 94.2854        | 5                 | 18.8571     | 4.0066  | 0.04899 | significant |
| A-Screw Speed     | 4.1667         | 1                 | 4.1667      | 0.8853  | 0.37808 |
| B-Sphenronization Speed | 0.0000 | 1 | 0.0000     | 0.0000 | 1.00000 |
| AB                | 30.2500        | 1                 | 30.2500     | 6.4273  | 0.03894 |
| A^2               | 9.3998         | 1                 | 9.3998      | 1.9972  | 0.20048 |
| B^2               | 59.8522        | 1                 | 59.8522     | 12.7170 | 0.00914 |
| Residual          | 32.9454        | 7                 | 4.7065      |         |         |
| Lack of Fit       | 8.9454         | 3                 | 2.9818      | 0.4970  | 0.70391 | not significant |
| Pure Error        | 24.0000        | 4                 | 6.0000      |         |         |
| Cor Total         | 127.2308       | 12                |             |         |         |

The Model F-value of 4.01 implies the model is significant. There is only a 4.90% chance that an F-value this large could occur due to noise. Values of "Prob > F" less than 0.0500 indicate model terms are significant. In this case AB, B^2 are significant model terms. Values greater than 0.1000 indicate the model terms are not significant. The "Lack of Fit F-value" of 0.50 implies the Lack of Fit is not significant relative to the pure error. There is a 70.39% chance that a "Lack of Fit F-value" this large could occur due to noise.

**Final Equation in Terms of Coded Factors:**

\[
\text{PSD #20-25} = 87.75862 + 0.833333 \times A - 2.75 \times AB - 4.65517 \times A^2 - 4.65517 \times B^2
\]

**Final Equation in Terms of Actual Factors:**

\[
\text{PSD #20-25} = 63.85057 - 0.0523 \times \text{Screw Speed} + 0.120603 \times \text{Sphenronization Speed} - 0.00069 \times \text{Screw Speed} \times \text{Sphenronization Speed} + 0.004612 \times \text{Screw Speed}^2 - 0.00012 \times \text{Sphenronization Speed}^2
\]

**Figure 7: Contour plot of PSD #20-25%**
DoE statistical analysis demonstrated that the impact of all factors (in the studied range) on the response studied was significant. Based on the observation suggested model for PSD above # 20-25 is Quadratic. The Contour plot and 3 D plot showing impact of Factor B (Sphenronization speed).

The Sphenronization speed and screw speed showing Quadratic interactions on the response Particle Size distribution above # 20-25.

**Response 5: PSD Below # 25**

**Table 14:** Summary of Model selection for particle size below # 25

| Source          | Sequential p-value | Lack of Fit p-value | Adjusted R-Squared | Predicted R-Squared | Suggested |
|-----------------|--------------------|---------------------|--------------------|---------------------|-----------|
| Linear          | 0.0015             | 0.3929              | 0.6715             | 0.5303              | Suggested |
| 2FI             | 0.3007             | 0.3915              | 0.6781             | 0.5072              |           |
| Quadratic       | 0.0794             | 0.7488              | 0.7993             | 0.6062              |           |
| Cubic           | 0.6012             | 0.6174              | 0.7708             | 0.1142              | Aliased   |

Suggested model for response PSD #20 min is Linear.

**Table 15:** ANOVA for particle size below # 25

| Source                      | Sum of Squares | Degree of freedom | Mean Square | F Value | p-value Prob>F | Significant |
|-----------------------------|----------------|-------------------|-------------|---------|----------------|-------------|
| Model                       | 140.3333       | 2                 | 70.1667     | 13.2647 | 0.0015         | Significant |
| A-Screw Speed               | 0.1667         | 1                 | 0.1667      | 0.0315  | 0.8627         |             |
| B-Sphenronization Speed     | 140.1667       | 1                 | 140.1667    | 26.4978 | 0.0004         |             |
| Residual                    | 52.8974        | 10                | 5.2897      |         |                |             |
| Lack of Fit                 | 35.6974        | 6                 | 5.9496      | 1.3836  | 0.3929         | Not Significant |
| Pure Error                  | 17.2000        | 4                 | 4.3000      |         |                |             |
| Corrected Total             | 193.2308       | 12                |             |         |                |             |

The Model F-value of 13.26 implies the model is significant. There is only a 0.15% chance that an F-value this large could occur due to noise. Values of "Prob > F" less than 0.0500 indicate model terms are significant. In this case B is a significant model term. Values greater than 0.1000 indicate the model terms are not significant. The "Lack of Fit F-value" of 1.38 implies the Lack of Fit is not significant relative to the pure error. There is a 39.29% chance that a "Lack of Fit F-value" this large could occur due to noise.

**Statistical Analysis Summary**

| Std. Dev. | R-Squared | Adj R-Squared | Pred R-Squared | Adeq Precision |
|-----------|-----------|---------------|----------------|----------------|
| 2.2999    | 0.7262    | 0.6715        | 0.5303         | 9.0509         |
| Mean      | 6.4615    |               |                |                |
| C.V. %    | 35.3944   |               |                |                |
| PRESS     | 90.7583   |               |                |                |
Final Equation in Terms of Coded Factors:

\[
\text{PSD Below# 25} = 6.461538 + 0.166667 \times A + 4.833333 \times B
\]

Final Equation in Terms of Actual Factors:

\[
\text{PSD Below# 25} = -3.53846 + 0.008333 \times \text{Screw Speed} + 0.024167 \times \text{Sphenronization Speed}
\]

Figure 9: Contour plot of PSD below # 25

Figure 10: 3 D Plot of PSD below # 25

DoE statistical analysis demonstrated that the impact of all factors (in the studied range) on the response studied was significant. Based on the observation suggested model for PSD below # 25 is Linear.
The Contour plot and 3 D plot showing impact of Factor B (Spheronization speed). The Spheronization increases PSD below #25 increases and vice versa.

**Optimization:**
The final ranges for factors identified through design of experiment to have optimum physical and chemical parameters need to be validated and hence an optimization study was carried out.

| Factor Criteria | Factor         | Goal    | Low    | High   |
|-----------------|----------------|---------|--------|--------|
| Screw Speed     | In Range       | 20      | 60     |
| Spheronization Speed | In Range       | 200     | 600    |

| Response Criteria | Response         | Goal    | Low    | High   |
|-------------------|------------------|---------|--------|--------|
| Aspect Ratio      | In Range         | 0.95    | 1.05   |
| Dissolution at 30 Min | Maximum        | 85      | 95     |
| PSD Above # 20    | In Range         | 5       | 10     |
| PSD # 20-25       | In Range         | 80      | 90     |
| PSD below # 25    | In Range         | 5       | 10     |

**Remark:**
Yellow zone represents all responses meet predefined criteria while grey zone showing experimental region conducted through design.

**Verification of Design Space:**
For verification of design space, following trial to be conducted and predicted results with 95% confidence interval and compare with actual result.

| Sr. No. | Factor         | Condition in RPM |
|---------|----------------|------------------|
| A       | Screw Speed    | 30               |
| B       | Spheronization Speed | 500            |

| Response | Predicted* results | 95% CI* | Actual Results |
|----------|--------------------|--------|---------------|
| Aspect Ratio | 0.95              | 0.93   | 0.94          |
| Dissolution at 30 Min | 88.32             | 86.10  | 88.14         |
| PSD Above # 20 | 6.18              | 5.09   | 6.12          |
| PSD # 20-25 | 87.86             | 85.66  | 86            |
| PSD below # 25 | 7.59              | 5.75   | 7.51          |

**Figure 11:** Design space of Screw speed and Spheronization Speed

5. **Conclusion**
This is indicative DoE performed for determination of suitable ranges for factors and to study optimization. Based on the statistical analysis and considering the scientific rational product performance, it can be concluded that the Factor A (Screw Speed) and Factor B (Spheronization Speed) are the significant factor which impact on the response dissolution, aspect ratio and PSD. Contour plot above figure shows that Optimized condition (Shown in the yellow zone) there is interaction between the factor A and B. For verification of design space, verification of design space by considering one trial conducted and predicted result if aspect ratio, dissolution at 30 Min, Particle size distribution were match with actual results with 95% confidence interval. Hence we can conclude that optimization of Factor A (Screw Speed) and Factor B (Spheronization Speed) were take place at 30 RPM and 500 RPM respectively.

6. **Future Scope**
It is of immense importance to build the quality in the product by design itself rather than testing into it upon completion. Current study outlines the importance of various factors that affects the final output of any product. This study is carried out at lab scale and it becomes imperative to check the impact of proposed parameters derived from study on a larger /commercial scale. In future the success of this study will ensure the techno-commercial feasibility of product designed with the approach studied.
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