Fully conservative, density-based SPH with improved partition of unit and better estimation of gradients

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ABSTRACT

Context. The correct evaluation of gradients is at the cornerstone of the smoothed particle hydrodynamics (SPH) technique. Using an integral approach to estimate gradients has proven to enhance accuracy substantially. Such approach retains the Lagrangian structure of SPH equations and is fully conservative. But, in practice, it is difficult to make the Lagrangian formulation totally consistent to an exact partition of unit.

Aims. In this paper we study, among other things, the connection between the choice of the volume elements (VEs), which enters in the SPH summations, and the accuracy in the gradient estimation within the integral approach scheme (ISPH). A new variant of VEs are proposed which improve the partition of unit and is fully compatible with the Lagrangian formulation of SPH, including the grad-h corrections.

Methods. Using analytic considerations, simple static toy models in 1D, and a few full 3D test cases, we show that any improvement in the partition of unit also leads to a better calculation of gradients when the integral approach is used jointly. Additionally, we propose an easy-to-implement modification of the ISPH scheme, which makes it more flexible and better suited to handle sharp density contrasts.

Results. The ISPH code built with the proposed scheme has been validated with a good number of standard tests, some of them involving contact discontinuities. The performance of the code was excellent in all of them, always showing that an improvement in the partition of unit is not detrimental of the good conservation of energy, momentum, and entropy typical of Lagrangian schemes.

Conclusions. We managed to build a new ISPH scheme on Lagrangian basis, which is fully conservative, and compatible with self-consistent grad-h terms and a better partition of the unit. The ensuing code is able to successfully cope with the tensile instability and has been validated with a number of hydrodynamic tests with good results.

Key words. Methods: numerical -hydrodynamics

1. Introduction

The smoothed particle hydrodynamics (SPH) is a firmly settled numerical technique, able to successfully simulate many cutting-edge problems in physics, astrophysics, and engineering. This technique has undergone a sustained enhancement since its original formulation Lucy (1977); Gingold & Monaghan (1977) and it is still evolving at a good pace (e.g. Springel 2010; Monaghan 2012; Rosswog 2015a; Wadsley et al. 2017; Cabezón et al. 2017; Price et al. 2018; Rosswog 2020b). A landmark in that evolution concerns the estimation of derivatives and gradients, which can be done by many different approaches.

The standard way of calculating gradients by directly taking the analytic derivative of the interpolating kernel function leads to E0-errors, even in the presence of constant pressure fields in non-uniform particle distributions (Agertz et al. 2007; Zhu et al. 2015). An alternative adapts the moving-least squares technique (MLS) to SPH (Dilts 1999) to ensure an exact interpolation of linear functions. In the MLS methods, the SPH kernel is replaced by a new interpolant, built by combining the original kernel with a linear operator. Such techniques ensure the linear consistency of the interpolations but it requires the solution of a linear system of \(d + 1\) equations (where \(d\) is the dimension) for each particle at each integration step. Alternatively, adding renormalization corrections to both the kernel and the gradient of the kernel has proved to enhance the accuracy in the calculation of gradients and to reduce the tensile instability (Bonet 1999). Tensile instability often arises at boundaries in the flow, separating fluid regions with different densities. The inconsistency in the treatment of gradients induces an nonphysical surface tension of numerical origin, which inhibits fluid mixing and suppresses hydrodynamic instabilities. A variational principle, jointly with a kernel renormalization, was used by Oger et al. (2007) to reduce the tensile instability and simulate fluid systems with free surfaces. Nevertheless, these MLS and renormalization techniques, in general, do not guarantee the perfect conservation of the whole set of physical laws governing the motion of the fluid, which are at the foundations of the SPH technique. A recent proposal was the Conservative Reproducing Kernel SPH method (CRKSPH) by Frontiere et al. (2017) which, although not derived from a Lagrangian, it still enforces perfect linear interpolation and retains the linear momentum and energy conservation properties.

An alternative way to estimating gradients was devised by García-Senz et al. (2012). In their proposal, gradients are cal-
culated from an integral expression, so that there is no need to explicitly calculate the analytic derivative of the kernel function. They also proved that such integral approach can be completely compatible with the Lagrangian formulation of the SPH equations, leading to the Integral Smoothed Particle Hydrodynamics (ISPH) scheme, named IAD in the seminal paper by García-Senz et al. (2012). It was shown that the ISPH formulation has the same conservation properties as the standard, Lagrangian-born SPH (Springel & Hernquist 2002). In particular, a remarkable feature of ISPH is that it reduces the E0-error in the derivatives (García-Senz et al. 2012; Rosswog 2015a; Valdarnini 2016).

In this work we dig further into the conditions that the ISPH scheme should meet in order to improve the calculation of gradients, which can become exact for linear functions. We found out that these conditions are connected with another basic SPH requirement: the correct partition of unit volume. Using one-dimensional numerical experiments we make clear the link between these two basic properties: any enhancement in the partition of unit leads to a better gradient estimation within the ISPH framework. The results of these 1D toy models are confirmed by detailed 3D hydrodynamic simulations of explosions, collisions, and instabilities.

A new kind of volume elements (VEs), leading to a better partition of unit is proposed and discussed. The ISPH equations of density, movement and energy are consequently reformulated, within the Lagrangian framework, so that they become fully compatible with the particular choice of the VEs. The resulting scheme is not only fully conservative, but it also enhances the density estimation and the gradient of linear functions with practically no computational overload.

Thus, the present work is a natural extension of that discussed in Cabezón et al. (2017), hereafter Paper I, where the code SPHYNX was introduced and verified. We focus here in modifying the proposal in Paper I, so that the new ISPH scheme (Appendix A) incorporates an implicit treatment of the VEs, being now fully compatible with the Lagrangian derivation of SPH equations, with a consistent treatment of grad-h terms. A second improvement is the use of a novel self-adaptive scheme to surgically reduce the tensile instability in regions with large density gradients. Unfortunately, suppressing that instability needs to abandon the Lagrangian formulation (Read et al. 2010; Wadsley et al. 2017; Wissing & Shen 2020). In our proposal, the departure from such formulation is minimal and limited to regions hosting significant density contrasts. Additionally, we show that our formulation leads to a better behavior of entropy in shocks than other schemes that suppress the tensile instability.

In Section 2, we review the main features of the ISPH scheme. We discuss the choice of the generalized volume elements used to compute the summations in Section 3. The link between the performance of the ISPH calculation of gradients and the adequate choice of the VEs is highlighted in Section 4. Section 5 presents the resulting ISPH equations, while in Section 6, we apply our code to several standard tests calculated in three dimensions, and analyze the results under the light of the VE choice. A summary of our findings and prospects for future work are given in the conclusions section.

2. The ISPH formulation

The classical way to evaluating gradients in SPH takes the multidimensional derivative of a function \( f \) as,

\[
\nabla f = \int_V f(r') \nabla W(|r' - r|, h) \, dr'^3 ,
\]

where \( W(|r' - r|, h) \) is commonly a Dirac \( \delta \)-like function named interpolating kernel which is continuous and derivable, and \( h \) is the smoothing length. In the classical SPH formulation, the gradient of the function is estimated by: 1.- approaching the integral of Eq. (1) by summations, 2.- taking the analytic derivative of the kernel, and 3.- assuming that the volume element \( dr'^3 \) is adequately represented by \( m/\rho \). Namely,

\[
\langle \nabla f \rangle_a = \sum_b m_b f_b \nabla W(|r_b - r_a|, h_a) ,
\]

where \( a \) and \( b \) refer to neighbouring particles with masses \( m_a \) and \( m_b \), respectively. Alternatively, in ISPH the gradient is calculated from an integral approach (IA), which does not require the explicit analytic derivative of \( W(|r - r'|, h) \). A vector integral \( I(r) \) is defined as (García-Senz et al. 2012):

\[
I(r) \equiv \int_V [f(r') - f(r)] (r' - r) W(|r' - r|, h) \, dr'^3 .
\]

The integral \( I(r) \) can be used to find the gradient of a function \( f(r) \) in a similar way that the Laplace operator is usually approached from another integral expression in standard SPH (Brookshaw 1985; Monaghan 2005). The IA interpretation of SPH is the consequence of approximating Eq. (3) with summations, along with approaching the function \( f(r) \) by a Taylor expansion around the evaluated point,

\[
f(r_b) - f(r_a) = \nabla f_b \cdot (r_b - r_a) ,
\]

with \( \nabla f_b \) defined below. The RHS in the integral expression in Eq. (3) becomes,

\[
I(r_a) = \sum_b m_b f_b (r_b - r_a) W(|r_b - r_a|, h_a) - [f(r_a) \langle \nabla r_a \rangle] ,
\]

where,

\[
\langle \nabla r_a \rangle = \sum_b m_b (r_b - r_a) W(|r_b - r_a|, h_a) .
\]

Putting Eqs. (4) and (5) into Eq. (3) allows to obtain the gradient \( \nabla f_a \),

\[
\begin{align*}
\frac{\partial f}{\partial x_1} &= \left[ \begin{array}{c} \tau_{11} & \tau_{12} & \tau_{13} \\ \tau_{21} & \tau_{22} & \tau_{23} \\ \tau_{31} & \tau_{32} & \tau_{33} \end{array} \right]^{-1} I_1 , \\
\frac{\partial f}{\partial x_2} &= \left[ \begin{array}{c} \tau_{11} & \tau_{12} & \tau_{13} \\ \tau_{21} & \tau_{22} & \tau_{23} \\ \tau_{31} & \tau_{32} & \tau_{33} \end{array} \right]^{-1} I_2 , \\
\frac{\partial f}{\partial x_3} &= \left[ \begin{array}{c} \tau_{11} & \tau_{12} & \tau_{13} \\ \tau_{21} & \tau_{22} & \tau_{23} \\ \tau_{31} & \tau_{32} & \tau_{33} \end{array} \right]^{-1} I_3 ,
\end{align*}
\]

where,

\[
t_{i,j,a} = \sum_b m_b (x_{i,b} - x_{i,a})(x_{j,b} - x_{j,a}) W_{ab}(h_a) ; i, j = 1, 3 ,
\]

1. Admittedly, this is not the most used implementation of the derivative in SPH. The most commonly used version is a variation involving differences of the derived function. Nevertheless, it is formally the same as Eq. (2).
where the spatial coordinates are represented by \( x \) with sub-indexes \( i \) or \( j \). From now on, \( W_{ab}(h_a) \equiv W(\mathbf{r}_b - \mathbf{r}_a), h_a \) for the sake of clarity.

It was shown in García-Senz et al. (2012) that Eq. (7) leads to perfect linear interpolation. Unfortunately, the price to pay is losing full conservation of linear and angular momentum. The exact conservation of the SPH Euler equations and perfect linear interpolation can only be retrieved simultaneously when \( \langle \mathbf{A}\rangle_a \rightarrow 0 \). We will refer to ISPH as the conservative scheme which simply neglects the term \( f(\mathbf{r}_j)\langle \mathbf{A}\rangle_j \) in Eq. (5). This is justified because \( \langle \mathbf{A}\rangle \) is in fact the indefinite integral of an odd function, which is zero\(^2\).

On the other hand, the complete integral approach, which takes into account the \( f(\mathbf{r}_j)\langle \mathbf{A}\rangle_j \) term in the RHS of Eq. (5), leads to perfect linear interpolation but is not fully conservative. We refer to it as non-conservative ISPH (ncISPH, hereafter). As commented above, both schemes, ISPH and ncISPH, converge to the same outcome when \( \langle \mathbf{A}\rangle_a \approx 0 \). Having both, a perfect partition of unit and \( \langle \mathbf{A}\rangle_a = 0 \), has been identified for a long time as the main constraint to ensure complete linear consistency in SPH (Liu & Liu 2006).

### 3. The choice of the volume elements

A common choice of the volume elements in SPH is \( V_a = m_a/\rho_a \), which leads to the widely used density equation,

\[
\rho_a = \sum_{b=1}^{m_a} V_b \rho_b W_{ab}(h_a) = \sum_{b=1}^{m_a} m_b W_{ab}(h_a),
\]

which works well provided that the density does not change too much within the kernel range. Nevertheless, the density may appreciably be miscalculated in the presence of shocks and density discontinuities. In these cases, the partition of unit condition is not fully satisfied,

\[
\sum_{b=1}^{m_a} m_b W_{ab}(h_a) \neq 1.
\]

The errors in the normalization constraint would introduce a level of uncontrolled errors in the remaining SPH equations. To reduce the normalization errors the most obvious recipe is to renormalize the kernel itself,

\[
\rho_a = \sum_{b} m_b \left( \frac{W_{ab}(h_a)}{\sum_{c} W_{ac}(h_a)} \right),
\]

where \( \rho_a^0 = \sum m_b W_{ch}(h_a) \) is the standard density. A more clever, albeit more complex, variation of that scheme was developed by Colagrossi & Landrini (2003) within the MLS approach, which exactly reproduces the linear variation of a density field (see Gomez-Gesteira et al. (2010) for a review of these topics). Nevertheless, none of those SPH schemes are totally compatible with the Lagrangian formulation of SPH. The Lagrangian formulation of the equations of movement has the advantage that the grad-h terms can be consistently incorporated to the scheme, so that complete preservation of mass, linear and angular momentum, energy, and entropy is guaranteed. Most MLS applications belong to the realm of computational fluid dynamics (CFD), which usually works with incompressible or weakly-compressible fluids. Having an almost constant density field for the entire simulation implies that the smoothing length also remains constant and the grad-h corrections are negligible (except at the boundaries, which are usually handled with special techniques). For that reason the MLS methods are mostly used in CFD simulations, but in the case of astrophysical scenarios, where density contrasts of orders of magnitude are not rare, the Lagrangian approach with a self-consistent treatment of the grad-h terms is preferable. Nevertheless, due to its properties, we are convinced that the methods presented in this paper can be also of use for CFD simulations.

Other options for the volume elements, \( V_a \), may be of interest to address specific problems. The code SPHYNX\(^3\) from Cabezón et al. (2017), makes use of the concept of generalized volume elements (Hopkins 2013; Saitoh & Makino 2013). First a scalar estimator \( X_a \) is defined so that the particle volume is,

\[
V_a = \frac{X_a}{k_a},
\]

with \( k_a = \sum X_b W_{ab}(h_a) \). The density of the particle is then calculated as \( \rho_a = m_a/V_a \). Current choices for the estimator that can be found in the literature are \( X_a = 1, m_a, P_a \), where \( P \) is the pressure and \( k \leq 1 \). There is however a particular choice which, according to Paper I, provides a better partition of the unit. Namely,

\[
X_a = \left( \frac{m_a}{\rho_a} \right)^p \quad \text{with} \quad X_a^{-1} = \left( \frac{m_a}{\rho_a^{p-1}} \right)^p.
\]

Setting \( p \) produces the standard volume element for particles with identical mass, whereas \( 0 < p \leq 1 \) gradually improves the kernel normalization when \( p \rightarrow 1 \).

There are two ways to implement the estimator in Eq. (13):

- Making use of the density calculated in the previous time-step, \( \rho_a^{n-1} \), to estimate the volume elements and density at the current iteration \( n \):

\[
\rho_a^n = m_a \frac{\sum X_b^{n-1} W_{ab}(h_a)}{X_a^{n-1}} \quad \text{with} \quad X_a^{n-1} = \left( \frac{m_a}{\rho_a^{p-1}} \right)^p.
\]

- Making use of the density calculated in the standard way in the current time-step, \( \rho_a^n = \sum m_b W_{ab}(h_a) \), to estimate \( X_a \) and then \( \rho_a^n = m_a/V_a^n \) (\( V_a^n \) calculated with Eq. 28). That is:

\[
X_a = \left( \frac{m_a}{\rho_a^n} \right)^p.
\]

We refer hereafter to the first method as an explicit procedure driven by \( X_{1,n} \) (Eq. 14), an to the second as an implicit method, driven by \( X_{2,n} \) (Eq. 15).

In the simple, static, toy models discussed below, \( X_{1,n} \) convergence is achieved after a few iterations. Once the estimator has converged, there is always an enhancement of the partition.

\(^2\) Interestingly, this argument has been used for the whole history of SPH to justify that it is a second order method, which is true in the continuum limit, but not always numerically ensured.

\(^3\) https://astro.physik.unibas.ch/sphynx
of unit, which is almost perfect when the exponent \( p \to 1 \). Because of its simplicity and good results \( x_{1,a} \) was the estimator chosen in Paper I. It has, however a couple of drawbacks which are worth commenting. Firstly, because of the explicit nature of Eq. (14), a complete Lagrangian consistency is never achieved. Therefore, \( p = 1 \) is too sensitive to particle noise and not recommended. Therefore, \( p = 0.7 - 0.8 \) were the recommended values, which slightly degrades the performance of \( x_{1,a} \) and introduces an undesirable free parameter (the particular value of the exponent \( p \)). These issues can be overcome with the second procedure to implement \( x_a \) which, in the end, was the one chosen in this work. Therefore, hereafter \( x_a \) refers always to \( x_{2,a} \). 

In the second method, the calculation of the VEs makes use of \( \rho_a^0 \) calculated in the current integration step. As we will see in the static toy models (Sect. 4), the explicit option \( x_{1,a} \) leads to a better partition of unit and interpolations than \( x_{2,a} \) for identical values of the \( p \) exponent, but the former is less numerically robust and not totally compatible with the Lagrangian formulation of the SPH equations. On the contrary, the estimator \( x_{2,a} \) allows to build a Lagrangian-consistent scheme (Appendix A), which incorporates the grad-h terms, provided that the exponent \( p \) in Eq. (15) is chosen equal to one \( (p = 1) \), allowing us to eliminate a parameter.

In the following sections we show that reducing the error in the kernel normalization \( E_1 \), (hereafter) of particle \( a \),

\[
E_1 = \left[ \sum_b V_b W_{ab}(h_a) - 1 \right],
\]

usually improves the requirement,

\[
E_2 \cdot h_a = |\langle \Delta r \rangle_a| = \left| \sum_b V_b (r_b - r_a) W_{ab}(h_a) \right| \to 0,
\]

where \( E_2 \) is the normalized error module \( |\langle \Delta r \rangle_a|/h_a \) of particle \( a \). The error reduction is the consequence of using the estimators \( x_{1,2} \) to evaluate the volume elements. Any reduction in both errors \( E_1, E_2 \) will potentially improve the dynamic evolution of the simulated physical system.

### 4. Estimating the errors \( E_1 \) and \( E_2 \) for different particle distributions

A good control of errors \( E_1 \) and \( E_2 \) is of utmost importance to the SPH technique. This is so because the quality of both, the interpolated function \( f(r) \),

\[
\langle f(r) \rangle \approx f(r) \sum_b V_b W_{ab}(h_a) + \nabla f \sum_b V_b (r_b - r_a) W_{ab}(h_a),
\]

and its gradient \( \nabla \langle f(r) \rangle \) (Eq. 7), are very sensitive to these errors (Rosswog 2015a). Nevertheless, both errors are correlated, as it can be inferred from the following argumentation in one dimension. We first take the kernel normalization condition as a function of the spatial coordinate,

\[
G(x_a) = \sum_b V_b W_{ab}(h_a).
\]

Using the Gaussian kernel \( W_{ab}(h_a) = \frac{C}{h_a} \exp[-(\frac{x_a - x_b}{h_a})^2] \), the standard SPH derivative of \( G(x) \) writes,

\[
\frac{dG}{dx} = \frac{1}{h^2} \sum_b V_b (x_b - x_a) W_{ab}(h_a),
\]

thus,

\[
\sum_b V_b (x_b - x_a) W_{ab} = -\frac{h^2}{2} \left( \frac{dG}{dx} \right)_{\|a}.
\]

We note that the LHS of Eq. (21) is in fact \( E_2 \), suggesting that having a good partition of unit \( (G \approx 1, i.e., E_2 \to 0) \) makes \( dG/dx \approx 0 \) and, as a consequence, the \( E_2 \) error is suppressed. An independent proof of the link between \( E_1 \) and \( E_2 \) obtained with an exponential kernel (Fulk & Quinn 1996), was given in the Appendix A of Paper I.

It should be recognized, however, that the proof above is only indicative because, unlike the interpolators widely used in practical calculations, the Gaussian and the exponential kernels are functions without compact support. Moreover, it could happen that even when \( G(x) \) is close to one, it shows fluctuations around the particles and its derivative may significantly differ from zero.

In this regard, additional insight about the impact of the VE choice in the errors \( E_1 \) and \( E_2 \) can be obtained by studying a handful of static particle distributions and using kernels with compact-support. These errors are expected to be large close to discontinuities, which in SPH are usually spread over a few times the smoothing-length distance \( (h) \). We have chosen three representative discontinuities which often appear in practical calculations: a Gaussian (model A), an inverted-Gaussian (model B), and a wall (model C). These are given by the following mathematical expressions:

\[
\rho(x) = \rho_0 + \Delta \rho \exp\left(\frac{-x}{a}\right), \quad (A)
\]

\[
\rho(x) = \rho_0 - \Delta \rho \exp\left(\frac{-x}{a}\right), \quad (B)
\]

\[
\rho(x) = \rho_0 + \Delta \rho \frac{\exp\left(\frac{-x}{a}\right) - \exp\left(\frac{-x}{b}\right)}{\exp\left(\frac{-x}{a}\right) + \exp\left(\frac{-x}{b}\right)}, \quad (C)
\]

where the values of the parameters \( \rho_0, \Delta \rho, \) and \( \delta \) are specified in Table 1.

We arranged these profiles into a 1D distribution of \( N = 100 \) particles with equal mass and distributed according to the density profile, with reflective boundary conditions. We used an interpolating sinc-kernel with exponent \( n = 5 \) (Cabezón et al. 2008), which has a shape similar to the \( M_6 \) spline. The different profiles of errors \( E_1 \) and \( E_2 \) at each point, for the estimators \( X_1 \) and \( X_2 \), are depicted in Fig. 1. As we can see, \( X_1 \) leads to a clear improvement in the kernel normalization condition as \( p \) increases. For \( p \approx 1 \) the \( E_1 \) error becomes negligible, hence it is not shown. Interestingly, the estimator \( X_2 \) with \( p = 1 \) (black crosses) leads to similar \( E_1 \) and \( E_2 \) errors as \( X_1 \) with \( p = 0.8 \) in all profiles. The normalized error \( E_2 \approx |\langle \Delta x \rangle|/h \) follows a similar trend, suggesting that having a good partition of unit is not only beneficial to approach the density, but also to calculating the gradient of any magnitude of interest with ISPH.
4.1. Impact of VE in estimating gradients

We can use our simple sharp profiles above to gain insight into the relationship between $E_1$, $E_2$ in Eqs. (16, 17), and the accuracy of the first derivative. To do that, we assume that the density of the test particle distribution follows profile A, Eq. (22), so that it totally determines the VEs through Eq. (13). Let us also assume that we wish to obtain the SPH derivative of a generic wall-like function $f$ given by profile $D$ in Table 1, Eq. (24). Such derivative, $\frac{df}{dx}$, is sensitive to the choice of the estimator $X$ to compute the VEs. We can thus compare the analytic and the numerical value of $\frac{df}{dx}$ and carry out the $L_1$ analysis of the results with Eq. (26).

Figure 2 depicts the wall-like function $f(x)$ (black solid line) and its analytical gradient of $df/dx$ (light-blue line). Although

4 This test would, mimic for example, a thermal wave passing through a star.
decreasing the errors in almost a factor ten when at larger $p$ values, it still provides a significant reduction of $L$ or the quantitative details again depend on the type of estimator, decreases as the exponent $p$ increases, as expected. Nevertheless, the panel on the right in Fig. 3 shows the averaged $L_1$ error of $\frac{df}{dx}$ normalized to $\left(\frac{df}{dx}\right)_{\text{analytic}}$.

$$L_1 = \frac{1}{N} \left( \frac{df}{dx}\right)_{\text{analytic}} \sum_{b=1}^{N} \left( \frac{df}{dx}_{\text{analytic}} - \left( \frac{df}{dx}_{\text{sph}} \right)_{b} \right),$$  

and how both schemes (ISPH and ncISPH) converge in light of the flavor used for the estimator $X$ ($X_1$ solid blue line and $X_2$ solid magenta line). We note that because the ncISPH scheme (Eq. 5) is making exact linear interpolations, the results (black line) are not sensitive on the adopted value of $p$. On the other hand, the results of the conservative scheme, ISPH (blue and magenta lines), show a clear dependence on the choice of the volume element, as expected. The profile of $L_1(p)$ decreases linearly, achieving the same accuracy as the ncISPH scheme when $p > 0.9$ for $X_1$ or close to it for $X_2$.

Fig. 2. Wall-like function $f(x)$ (black line) and its analytical gradient $df/dx$ (light-blue solid line). The solid lines in magenta and blue were obtained with $X_1$ and $p = 0.0, 0.9$ respectively, while the black points are for $X_2$ with $p = 1$.

the value around the maximum of $\frac{df}{dx}$ is similar for $p = 0.0$ (magenta solid line) and $p = 0.9$ (blue solid line), the last option fits better the derivative around the coordinate $x = 0.6$, which is in turn similar to that obtained using the estimator $X_2$ with $p = 1$ (black dots).

The panel on the left in Fig. 3 shows the averaged $L_1$ value for $E_1$ (Eq. 16) and $E_2$ (Eq. 17),

$$L_1(E_{1,2}) = \langle |E_{1,2}| \rangle,$$  

(25)
calculated in the interval $0.3 \leq x \leq 0.7$, for the test presented above. The $L_1$ values for the partition of the unit and $\langle \Delta x \rangle \times h$ decreases as the exponent $p$ increases, as expected. Nevertheless, the quantitative details again depend on the type of estimator, $X_1$ or $X_2$. As the figure shows, there is a factor ten reduction of the $L_1$ errors for $X_1$ and $p \approx 0.9$. The errors become negligible when $p \approx 1$. Although the option $X_2$ shows a lower convergence rate at larger $p$ values, it still provides a significant reduction of $L_1$, decreasing the errors in almost a factor ten when $p = 1$.

4.2. The quest for fully implicit VEs

In principle, the best procedure to calculate the volume elements would be to directly obtain them from the inversion of the kernel normalization matrix. Unlike the indirect methods described in the previous section, a fully implicit implementation of the VEs has the advantage of always leading to the perfect partition of unit. Previous attempts to build implicit SPH schemes (Knapp 2000; Escartín 2016), made use of advanced techniques to efficiently invert large sparse matrices, as for example the PAR-DISO library\(^5\). This type of libraries could also be used to implicitly find the volume elements $V_b$ by solving large linear systems with $N \times N$ equations and unknowns,

$$\sum_{b=1}^{m} V_b W(h_a) = 1.$$  

(27)

Unfortunately, finding the VEs with such direct approach produces, in general, non-physical results. We have calculated, in a fully implicit manner, the VEs of the Gaussian function (Eq. 22), by solving the linear system above and found that the volume elements strongly oscillate around the explicit solution given by Eq. 14 with $p = 1$ (see Fig. 4). Even worse, in many points the volume elements become negative which is non-physical. Therefore, we have discarded the fully implicit route to find the VEs in this work.

5. ISPH equations

Here we summarize the set of ISPH equations used to compute the 3D tests on the following section. We provide two sets of momentum and energy equations, one corresponding to a 'standard'\(^5\) The widely used Intel MKL PARDISO library function is based on a legacy version of this project: \url{https://www.pardiso-project.org/}
Fig. 3. $L_1$ calculation of the errors in the numerical experiments shown in Fig. 2. Left: averaged value of $L_1$ for the partition of unit (solid lines) and $(\Delta x)/h$ (dotted lines). Blue lines are for the estimator $X_1$ and magenta lines for $X_2$. Right: averaged value of $L_1$, obtained with Eq. (26), for the derivative of the wall function calculated with $X_1$ (solid blue line) and $X_2$ (solid magenta line). The black line is the calculation with the non-conservative ISPH which is independent of the particular value of the exponent $p$. Note that when $p \approx 1$ both schemes (ISPH and ncISPH) converge, albeit faster for estimator $X_1$ than for $X_2$.

Fig. 4. Implicit versus explicit estimation of the volume elements, $V_b$, in the numerical experiments with the Gaussian curve (Eq. 22).

5.1. Description of the ISPH equations

- Density equation:
  \[ \rho_a = \frac{m_a}{V_a}, \tag{28} \]
  with $V_a$ defined by Eq. (12).

- Momentum equation:
  \[
  \ddot{x}_{a,i} = -\frac{m_a}{\rho_a} \sum_b m_b \left[ \frac{X_{a,b}P_a}{\Omega_{a,b} \sigma_{a,b}} A_{a,b}(h_a) + \frac{X_{b,a}P_b}{\Omega_{b,a} \sigma_{a,b}} A_{b,a}(h_b) \right];
  \]
  \[
  \begin{align*}
  \dot{x}_{a,i} &= -\frac{m_a}{\rho_a} \sum_b m_b \left[ \frac{X_{a,b}X_{b,a}P_a}{\Omega_{a,b} \sigma_{a,b}} A_{a,b}(h_a) + \frac{X_{b,a}X_{a,b}P_b}{\Omega_{b,a} \sigma_{a,b}} A_{b,a}(h_b) \right];
  \end{align*}
  \tag{29}
  \]
  with $\rho_a = \sum_b m_b W_{ab}(h_a)$, and $\Omega_{a,b}$ is given in Appendix A. We have introduced a parameter, $0 \leq \sigma \leq 1$, which allows to choose between the pure Lagrangian scheme developed in the Appendix A ($\sigma = 0$) and a progressive deviation of it, which suppresses the tensile instability when $\sigma \to 1$ (see Section 5.2 for more details on $\sigma$). Moreover,

\[ A_{a,b}(h_a, h_b) = \sum_{j=1}^{d} c_{ja}(h_a)(x_{ja} - x_{ja}) W_{ab}(h_{a,b}), \tag{30} \]

being $c_{ja}$ the coefficients of the inverse matrix in the 1A given by Eq. (7), and $d$ is the number of dimensions. Any expression of standard SPH can indeed made compatible generally used VEs (i.e. $X_a = m_a$) and another one to our suggested VEs, which are the equations used to perform the comparisons in the tests of Sect. 6. We also provide the details of the procedure used to build these equations in Appendix A.
with the IA by taking the kernel derivative as (Cabezón et al. 2012):
\[
\frac{\partial W_{ab}(h_a)}{\partial x_{ia}} = \mathcal{A}_{ia}(h_a); \quad i = 1, d.
\]

- Energy equation:
\[
\dot{u}_{ab} = \begin{cases} 
\text{For } X_{a,b} = m_{a,b} : \\
\frac{X_a}{m_{a,b}} \sum_{i \in \{a,b\}} \left[ (v_{i,a} - v_{i,b}) \mathcal{A}_{ia}(h_a) \right]; \\
\text{For } X_{a,b} = \rho_{a,b} : \\
\frac{X_a}{\rho_{a,b}} \sum_{i \in \{a,b\}} m_i X^0_i \left[ (v_{i,a} - v_{i,b}) \mathcal{A}_{ia}(h_a) \right]; 
\end{cases}
\]

The necessary terms of artificial viscosity (AV) are added to the right of the equations above as in Paper I, but explicitly including a quadratic term in the signal velocity:
\[
v^{sig}_{ab} = \hat{\alpha}_{ab} \dot{e}_{s,ab} - \beta \omega_{ab},
\]

where \( \omega_{ab} = \nabla \cdot \mathbf{v}_{ab} \) (Monaghan 1997; Price et al. 2018). The parameter \( \beta \) is kept constant with a default value \( \beta = 2 \). The AV coefficient \( \alpha \) is controlled with the switches scheme described in Read et al. (2010) so that \( \alpha \approx 1 \) in strong shocks but it decays to a minimum value of \( \alpha \approx 0.05 \) away from them. Finally, \( \hat{\alpha}_{ab} \) and \( \dot{e}_{s,ab} \) are the average \( \alpha \) and speed of sound between neighboring particles. According to Monaghan (1997), the AV contribution to the energy equation should include a heat-conduction term which smooths the pressure in wall-shock conditions. The precise form of such heat-conduction term is:
\[
\frac{d u_{ab}}{dt}^{AV}_{cond} = \sum_{i} \frac{m_i}{\rho_{ab}} \dot{v}^{sig}_{ab,cond}(u_{a} - u_{b}) \bar{v}_{iab} \mathcal{A}_{ia}(h_a, h_b),
\]

with \( \mathcal{A}(h_a, h_b) = 0.5(\mathcal{A}(h_a) + \mathcal{A}(h_b)), \) which in the SPHYNX code is implemented as:
\[
\frac{d u_{ab}}{dt}^{AV}_{cond} = \sum_{i} \frac{1}{2} \alpha_a \dot{v}^{sig}_{ab,cond}(u_{a} - u_{b}) \left\{ v_{a} m_a \frac{r_{ab}}{\rho_{ab}} \mathcal{A}_{ia}(h_a) + v_{b} m_b \frac{r_{ab}}{\rho_{ab}} \mathcal{A}_{ia}(h_b) \right\}.
\]

The signal velocity \( \dot{v}^{sig}_{cond} \) used in our tests is (Price 2008):
\[
\dot{v}^{sig}_{ab,cond} = \sqrt{\frac{P_a - P_b}{\rho_{ab}}},
\]

The results of the tests below suggest that adding a small amount of conductive heat by Eq. (35) is beneficial, because it contributes to reduce the tensile instability and the numerical noise. Nonetheless, the value of the constant \( \alpha_a \) should not be high, otherwise the density-peak in strong shocks may be underestimated (see Section 6.4). We have chosen \( \alpha_a = 0.1 \), which is low and in agreement with the choice by other authors, e.g. Tricco (2019). The equation of state (EOS) is that of an ideal gas with \( \gamma = 5/3 \).

5.2. Obtaining the value of \( \sigma \)

When using the SPH equations deduced from the Euler-Lagrange formulation a drawback appears wherever \( \nabla \rho \) becomes large as, for example, around contact discontinuities. In these cases, the incorrect estimation of gradients may lead to numerical artifacts, being the tensile instability one of the most harmful and common. Several solutions have been postulated to cope with this problem, all of them requiring some departure from the exact Lagrangian formulation. For example, Ritchie & Thomas (2001) proposed to estimate the density by averaging over the internal energies so that the ensuing density field is smooth. A similar approach was described in Saitoh & Makino (2013), who suggested to redefine the volume elements so that they depend on pressure rather than on density. Another solution was proposed by Read et al. (2010), where a typical element within the summations of the momentum and energy equations is changed from the standard \([P_i/\rho_i^5]\) to \([P_i/(\rho_0 \dot{\rho})]\). Although not totally Lagrangian compatible, such simple change is mathematically consistent with the standard derivation of the SPH equations (Monaghan 1992; Price 2005)\(^6\) and totally suppresses the tensile instability. All these SPH variants have in common that the main magnitudes in the movement equation are somehow "crossed" for particles \( a \) and \( b \) (i.e. \( \dot{u}_i/\rho_i \) in Ritchie & Thomas (2001) or \( P_i/(\rho_0 \dot{\rho}) \) in Read et al. (2010)).

Here we propose a similar procedure as in Read et al. (2010), but allowing a self-adaptive crossing of indexes in the original Lagrangian equations derived in the Appendix A. The resulting SPH equations whereas that 0 \( \sigma \) was already suggested by J. Monaghan (1992) in his popular review, but \( \sigma \) was thought to be a constant real number.\(^7\)

Specifically, it can be shown that the scheme in Paper I involve terms such as \( P_i/(\rho_i^5 - \rho_0^5) \), with \( p = 0.7 \) being the exponent of the explicit estimator (Eq. 14) considered in that work.

6. Tests

In this section, we analyze the results of four well-known tests, that require the solution of the full system of Euler equations in

\(^6\) The possibility of working with \( P_i/(\rho_i^5 - \rho_0^5) \) (with some preference for \( \sigma = 0 \)) was already suggested by J. Monaghan (1992) in his popular review, but \( \sigma \) was thought to be a constant real number.

\(^7\) Specifically, it can be shown that the scheme in Paper I involve terms such as \( P_i/(\rho_i^5 - \rho_0^5) \), with \( p = 0.7 \) being the exponent of the explicit estimator (Eq. 14) considered in that work.
three dimensions. The first test deals with the hydrostatic equilib-rium of a two-phase fluid. It aims to analyze the abilities of our Lagrangian scheme to handle sharp density discontinuities. Then, we apply this scheme to the study of the interaction of a supersonic wind with an isothermal, high-density spherical cloud (the wind-cloud test), to the growth of the Kelvin-Helmholtz (KH) instability, and to simulate the evolution of a point-like explosion (the Sedov test). The simulations were carried out using the ISPH code SPHYNX and the outcomes have been compared to well-known solutions. Tests are run with various parameters to disentangle the effects of IA, VE, heat transport in the AV, and \(\sigma\). Special emphasis is put in the comparison among models with different choices of \(\sigma\) and volume elements, namely the standard choice\(^8\) \(X_c = m_a/\rho_a^0\) and the improved VEs with \(X_c = m_a/\rho_a^0\) 

Conservation properties are excellent. We found that linear momentum is preserved to almost machine precision in all tests. The angular momentum, with respect to the center of mass, de-viates in less than \(10^{-5}\) from the initial value. The relative deviation, \(|\Delta E|/E_0|\) in the total energy was lesser than \(10^{-5}\), except in the isobaric two-fluid test (Sect. 6.1) where it was \(10^{-2}\) at late times.

6.1. The isobaric two-fluid test

The simulation of the hydrostatic evolution of a two-phase system with very different densities and internal energies is far from being trivial with SPH codes. We consider a system of two fluids separated by a contact discontinuity but in pressure equilibrium:

\[
\rho = \begin{cases} 
4 & 0.25 \leq x, y, z \leq 0.75, \\
1 & \text{otherwise}.
\end{cases}
\]  

(38)

The system is isobaric with \(P = 2.5\) and we use \(N = 110^3\) equal-mass particles spread in two nested body-centred cubic (bcc) lattices. The EOS is \(P = (\gamma - 1)\rho u\) with \(\gamma = 5/3\), the number of neighbors is set to \(n_n = 100\) and the sinc \((n = 5)\) kernel (Cabezón et al. 2008) is used to interpolate. If the density around the contact discontinuity is not adequately smoothed, the two phase system evolves non-physically when the full Lagrangian scheme (Eqs. 29, 32, with \(\sigma = 0\)) is applied. The reason is that the error in \(\nabla P\) becomes too large at the contact discontinuity, in-ducing the tensile instability. This is just the kind of simulation where the use of the magnitude \(\sigma\) (see Section 5.2), defined by Eq. (37), becomes really helpful.

The results of applying Eqs. (29) and (32) to the hydrostatic square test are summarized in Table 2 and Fig. 5. Only models with \(X_c = m_a/\rho_a^0\) are shown in Fig. 5, calculations with \(X_c = m_a\) give similar results, albeit with higher L1 values. The density colormap slices depicted in Fig. 5 show that the behavior of the square is primarily controlled by the value of \(\sigma\). In the case of the full Lagrangian formulation (models \(H_5, H_6\)), calculated with \(\sigma = 0\), the system completely loses its shape in half of the sound-crossing time, \(\tau_{sc} \approx 0.9\ s\). Nevertheless, increasing the conductivity in the AV (model \(H_6\)) slightly delays the deformation, although, in the end, it is not able to prevent it. Model \(H_7\), calculated with \(\sigma = 1\), leads to the best results. The cube keeps its profile at \(\xi/\tau_{sc} = 1.7\) (last snapshot in third row in Fig. 5) and beyond. Such behavior is in fair agreement with the results of other density-based schemes (Read et al. 2010; Wad-sley et al. 2017) calculated in 2D and 3D respectively. It also matches the 2D calculation in Paper I (first row in their Fig. 4, with \(0 \leq \xi/\tau_{sc} \leq 2\) ) calculated with the explicit \(X_{IA}\) given by Eq. (14) with \(p = 0.7\) (see the footnote 7). It is worth noting that model \(H_6\), calculated with \(\sigma[0 - 1]\), preserves the shape of the square until \(\xi/\tau_{sc} \approx 1\) and still does at the last snapshot in Fig. 5 at \(\xi/\tau_{sc} = 1.7\), although not so well as in model \(H_7\). As shown in Fig. 6 (upper panel), the algorithm (Eq. 37) which self-adapts \(\sigma\) as a function of the local density contrast, works splendidly, increasing the value of \(\sigma\) only where it is needed.

Table 2. \(L_1\) values for errors \(E_1\) and \(E_2\) at \(\xi = 1.5\) in the hydrostatic square test. The meaning of the columns are: \(\sigma\) is the magnitude defined in Eq. (29), \(\alpha_u\) controls the amount of heat transport in the AV (Eq. (34)), \(X\) is the estimator connected to the VE choice and \(L_1(E_1), L_1(E_2), L_1(d)\) are the averaged \(L_1\) values of the partition of unit, the \(|\Delta r|/|\Delta h|\) condition, and the deviations of the SPH particles from their initial position, respectively.

| Model | \(\sigma\) | \(\alpha_u\) | \(X\) | \(L_1(E_1)\) | \(L_1(E_2)\) | \(L_1(d)\) |
|-------|---------|-----------|------|-------------|-------------|-------------|
|       | \(\times 10^{-3}\) | \(\times 10^{-3}\) | \(\times 10^{-2}\) | \(\times 10^{-3}\) | \(\times 10^{-3}\) | \(\times 10^{-2}\) |
| \(H_1\) | 0.0 | 0.1 | \(m\) | 3.0 | 2.5 | 3.2 |
| \(H_2\) | 0.0 | 1.0 | \(m\) | 3.0 | 2.6 | 3.1 |
| \(H_3\) | 1.0 | 0.1 | \(m\) | 4.4 | 3.2 | 1.6 |
| \(H_4\) | [0 - 1] | 0.1 | \(m\) | 5.0 | 3.5 | 2.0 |
| \(H_5\) | 0.0 | 0.1 | \(m/\rho_a^0\) | 2.1 | 2.7 | 3.2 |
| \(H_6\) | 0.0 | 1.0 | \(m/\rho_a^0\) | 2.5 | 2.9 | 3.0 |
| \(H_7\) | 1.0 | 0.1 | \(m/\rho_a^0\) | 2.5 | 3.2 | 1.5 |
| \(H_8\) | [0 - 1] | 0.1 | \(m/\rho_a^0\) | 2.7 | 3.3 | 2.0 |

\(H_7\), calculated with \(\sigma = 1\), leads to the best results. The cube keeps its profile at \(\xi/\tau_{sc} \approx 1.7\) (last snapshot in third row in Fig. 5) and beyond. Such behavior is in fair agreement with the results of other density-based schemes (Read et al. 2010; Wad-sley et al. 2017) calculated in 2D and 3D respectively. It also matches the 2D calculation in Paper I (first row in their Fig. 4, with \(0 \leq \xi/\tau_{sc} \leq 2\) ) calculated with the explicit \(X_{IA}\) given by Eq. (14) with \(p = 0.7\) (see the footnote 7). It is worth noting that model \(H_6\), calculated with \(\sigma[0 - 1]\), preserves the shape of the square until \(\xi/\tau_{sc} \approx 1\) and still does at the last snapshot in Fig. 5 at \(\xi/\tau_{sc} = 1.7\), although not so well as in model \(H_7\). As shown in Fig. 6 (upper panel), the algorithm (Eq. 37) which self-adapts \(\sigma\) as a function of the local density contrast, works splendidly, increasing the value of \(\sigma\) only where it is needed.

\(^8\) Actually, any constant magnitude is a suitable choice as \(X_c\), but taking the mass of the particle allows for the fine tuning of the den-sity (if needed) by slightly modifying the mass of the particles. In nearly isobaric systems, with shallow pressure gradients, the choice \(X_c = P_a, k = 1\) could also be appropriate.

\(^9\) Very similar results for H1-H3 models, calculated with standard VEs, can be found in plots in previous work. (Cabezón et al. 2017, their Fig. 4)
To investigate the dependence of the errors $E_{1,2}$ (Eqs. 16 and 17) with respect to the VE estimator and $\sigma$ we calculated the $L_1$ values (Eq. 25) in a rectangular shell with width 0.3 around the contact discontinuity.

The column $L_1(d)$ of Table 2 is defined by the average error of the absolute displacement of the SPH particles located in the shell, with respect to their initial positions:

$$L_1^d(t) = \frac{1}{N} \sum_{b=1}^{N} \sqrt{(x_b(t) - x_{b,0})^2 + (y_b(t) - y_{b,0})^2 + (z_b(t) - z_{b,0})^2},$$

(39)

where $x$, $y$, and $z$ are the Cartesian coordinates of the $b$th particles while $x_{b,0}$, $y_{b,0}$, and $z_{b,0}$ coordinates represent their initial position. Sub-index $b$ runs from 1 up to the $N$ particles contained in the rectangular shell.

The full Lagrangian models $H_1$, $H_2$, $H_5$, and $H_6$, calculated with $\sigma = 0$, give the worst results, with $L_1(d) \geq 3 \times 10^{-2}$ at $t = 1.5$. The minimum value of $L_1(d)$ corresponds to model $H_7$ ($L_1(d) = 1.5 \times 10^{-2}$), calculated with $\sigma = 1$ and improved VEs. However, model $H_6$ calculated with the self-adaptive $\sigma[0-1]$ and improved VEs, also displays a similarly good behavior, while keeping full Lagrangian consistency ($\sigma = 0$) in a large fraction of the domain (see Fig. 6, upper panel).

The lower panel in Fig. 6 depicts the evolution of the averaged estimator $L_1$ of the partition of unit (solid lines) and $\langle \Delta r \rangle / h$ (dashed lines) for models $H_5$, $H_7$, and $H_8$ in Table 2. Comparing $H_3$ to $H_7$ highlights the relevance of the VEs, while comparing $H_7$ to $H_8$ shows the impact of a variable $\sigma$. Is it clear that the partition of unit is enhanced with the choice $X = m/\rho^3$, nevertheless the behavior of $\langle \Delta r \rangle / h$ is less defined. The error $L_1(E_2)$ remains lower for models $H_5$ and $H_8$ than model $H_1$ until $t \approx 0.2$. Afterwards the error grows to eventually reach a similar value to that of model $H_1$, calculated with $X_a = m_a$. Thus, we expect a degradation in the behavior $\langle \Delta r \rangle / h$ with respect the results shown in Figs. 1 and 3 whenever the disorder of the particles is high. To sum up, the dominant parameter for the dynamic evolution of the system is $\sigma$, which basically determines the stability of the square. Using $X = m/\rho^0$ improves the partition of unit at any time, but the magnitude $\langle \Delta r \rangle / h$ does not show a definite enhancement in this test.

### 6.2. The Kelvin-Helmholtz instability

The correct simulation of the evolution of the contact layer between fluids with different densities is of capital importance for the adequate growth of the Kelvin-Helmholtz (KH) instability. García-Senz et al. (2012) proved that the use of ISPH improves the evolution of gradients overall (and in particular in the contact layer). Provided the density contrast is not very high, it prevents the appearance of tensile instabilities that otherwise suppress the growth of the KH instability. Because SPHYNX uses ISPH by default, all KH simulations presented here show no signs of tensile instability and have growth rates close to the reference calculation by McNally et al. (2012) with the code PENCIL. Nevertheless, using a volume element that better fulfills conditions (16) and (17) should additionally improve the accuracy of ISPH and, as a consequence, obtain a better KH growth rate.

We run this test in a thin three-dimensional layer of size $[1 \times 1 \times 0.0625]$ with $4.2 \times 10^6$ equal-mass particles, distributed in a ratio 2:1 between the high and low density regions. For the initial setting we have three stratified layers, being the central layer the high-density one. Each region was generated from a
random particle distribution relaxed to a glass-like configuration. The equation of state, initial velocities, and initial pressure are the same as those in Sect. 5.4.1 in Paper I. Times are normalized to the characteristic Kelvin-Helmholtz growth time $t_{KH}$, as defined in Agertz et al. (2007), which results in $t_{KH} = 1.06$ in our models. According to the discussion at the end of Sect. 6.4 we take a low value, $\alpha_0 = 0.1$, of the AV conductive parameter.

We used two different VEs (the standard $X_a = m_a$ and the enhanced version proposed here $X_a = m_a/\rho_i^0$) and, for each case, we performed two simulations: one fixing $\sigma = 0$, hence ensuring fully Lagrangian compatibility, and another one allowing $\sigma$ to vary according to Eq. (37). All simulations are summarized in Table 3.

In Fig. 7 we represent the particles distributions for each simulated model (each snapshot corresponds to one model, from $KH_1$ to $KH_6$) at $t = 2$. The color represents density. As it can be seen, there are very few differences among all simulated models. In all cases, the KH billows are able to develop, with small differences among simulations, mostly at the extremes of the billows.

We can also explore the growth of the amplitude mode for the $v_x$ field and compare it with a reference evolution taken from the PENCIL code (McNally et al. 2012). Figure 8 (left) shows this evolution and it is clear that there are very little differences among both VEs implementations, in agreement with the results in Paper I. These results are in good match with those by Frontiere et al. (2017) and Rosswog (2020a) for similar resolution and initial conditions, provided that the Cullen & Dehnen (2010) AV trigger is chosen to steer dissipation in the last case.

Figure 9 presents the time evolution of the averaged $L_1$ value for errors $E_1$ and $E_2$. To average the $L_1$ values we restricted to those particles that had $\sigma \geq 0.025$. This condition returns all those particles that are found in the inter-phase (see Fig. 10), which is the region where the error comes from and where the accurate evaluation of the VEs is more critical. It is clear that whenever the improved VEs are used (dashed lines in Fig. 9), these errors decrease, independently of the scenario being simulated. The last two columns of Table 3 show the numerical value of $L_1$ for all simulated tests at $t = 2$, where we can see that the choice $X = m/\rho^0$ reduces both, the $L_1(e_1)$ and the $L_1(e_2)$ errors.

From these results, we can conclude that, despite decreasing the errors $E_1$ and $E_2$, the VEs choice has little influence in the growth of the KH instability when the density contrast is moderate. The most important element here is having the IA implementation to calculate gradients, as shown in Paper I. Additional improvement in the conditions (16) and (17) via using improved VEs is subdominant. The dominant source of error at this level is the artificial viscosity. To test this we performed two additional simulations, $KH_3$ and $KH_6$, with an artificially increased $\alpha_{\text{min}}$ in our AV switches. This $\alpha_{\text{min}}$ controls the amount of dissipation when the AV switch is off. Therefore, is the minimum dissipation present in the whole system. Our standard value is $\alpha_{\text{min}} = 0.05$, while for $KH_3$ and $KH_6$ we used $\alpha_{\text{min}} = 0.5$. To have a reference, traditional AV without switches employ a global value $\alpha_{\text{min}} = 1 - 1.5$. The amplitude growth of the $v_x$ field is also shown in the left panel of Fig. 8 (dashed lines). It is clear that the AV has a major effect in the development of the instability. Still the VEs have a negligible impact when the IA formalism is used.

Our final test was to explore if the VEs can have an influence when the density contrast is higher. To do that we decreased the density of the low-density regions by a factor 4, simply by generating a new relaxed model with 4 times less particles, and repeated simulations $KH_3$ and $KH_6$ with this new density jump of a factor 8 (simulations $KH_7$ and $KH_8$). We present the evolution of the amplitude growth of the $v_x$ field in the right panel of Fig. 8. In this case, the growth is more irregular and there is a clear difference between the VEs in the linear regime. The improved VEs are able to grow faster than the standard VEs in the initial stages of the development of the KH instability, despite converging later, in the non-linear phase. The IA formalism still does a good job evaluating gradients even with a density jump of a factor 8. Nevertheless, using improved VEs at this density contrast shows to have a noticeable effect.

In summary, if there is a mild density contrast, the IA implementation is good enough to make the choice of VEs subdominant. The most relevant parameter in these situations is to keep the dissipation at its lowest possible value, so that random noise is still dissipated, but it doesn’t affect the shear between the different fluid layers. In this respect, improved handling of the AV would be welcomed, such as that presented in Rosswog (2020a) based on the instantaneous numerical entropy generation rate. If there is a bigger density contrast, the IA formalism can be further improved by using a VE that better fulfills conditions (16) and (17) along with $\sigma[0 - 1]$.

6.3. The wind-cloud collision

The wind-cloud collision scenario, also called “blob” test (Agertz et al. 2007) is a challenging test for SPH, involving several pieces of physics such as strong shocks and mixing due to the KH instability, amidst a two-phase medium with a large density contrast. In this test, a spherical cloud of cold gas, initially at...
Fig. 8. Amplitude growth of the $v_y$ field in the KH instability test for all calculated models. Solid lines correspond to $\alpha_{\min} = 0.05$, while dashed lines are from the models with increased AV ($\alpha_{\min} = 0.5$). Those with a density jump of two are compared with the reference PENCIL simulation in the left panel. The right panel shows two simulations with a density jump of eight for both choices of the VEs.

Fig. 9. $L_1$ evolution of errors $E_1$ and $E_2$ for the KH models. Solid lines correspond to $X = m$, while dashed lines are those of $X = m/\rho^s$.

Fig. 10. Colormap of $\sigma$ (Eq. 37), in a thin slice around $Z = 0$ for model $KH_4$ at $t = 2$.

rest, is swept by a low-density stream of gas (the wind) moving supersonically. As a consequence, the cloud deforms and, after a while, it is fragmented and mixed with the background owing to the combined effect of ablation and hydrodynamic instabilities. This scenario has been extensively studied during the last years (Agertz et al. 2007; Read et al. 2010; Saitoh & Makino 2013; Hopkins 2013; Frontiere et al. 2017), where the tensile instability appearing at the wind-cloud contact was identified as the main difficulty to overcome.

We want to check the ability of our numerical scheme to handle this test. The initial conditions were those described in Paper I, except that the calculation is now carried out in 3D with approximately $N_w = 11.23 \times 10^6$ and $N_c = 1.23 \times 10^5$ particles for the wind and the cloud, respectively. The initial particle distribution for both was that of a stable glass-like configuration. The box has a size $[0.25 \times 0.25 \times 1]$ with periodic boundary conditions. The high-density cloud is initially located at $(0.125, 0.125, 0.125)$ with a radius $R = 1/40$ and a density $\rho_c = 10$, ten times bigger than the surrounding wind. The internal energy of the wind and the cloud are $u_w = 3/2$ and
proves the capabilities of our algorithm to track density jumps. A series of snapshots where the color represents the value of a quantity generated by the particles in the inter-phase. In Fig. 12 we show a cloud, albeit more efficiently, if \( \sigma \neq 0 \). Figure 14 shows the maximum density attained in the cloud during the first stages of the interaction. Because of the strong impact of the wind a shock-wave is born which moves through the dense cloud compressing its matter. The density jumps from the original value of \( \rho_0 = 10 \) and tends to the limiting value \( \rho = 4\rho_0 \), characteristic of a strong shock in a gas with \( \gamma = 5/3 \). All models show a similar behavior but the profile from models calculated with \( X = m/\rho^0 \), give in general larger values than models calculated with \( X = m \).

In order to characterize the destruction of the high-density cloud, we tracked the percent of surviving cloud mass (criteria: \( \rho \geq 0.64\rho_c \), and \( u \leq 0.9u_c \)) in function of \( t/t_{\text{KH}} \) in Fig. 15. From this result we can see that the choice of the VE is less relevant than using a crossed formulation of the equations (i.e. variable term in the \( \Delta \) equation). Nevertheless, the surviving fraction of the cloud decreases faster and to lower values provided we don’t use \( \sigma = 0 \), independently of the VE choice. The slight delay in the evolution of the surviving fraction with \( X = m/\rho^0 \) simply reflects the fact that the ensuing VEs better track the density peak at the forward shock moving through the cloud. Such

Table 4. Simulated models in the wind-cloud test. The columns present the following: \( \sigma \) is the magnitude defined in Eq. (37), \( X \) is the estimator connected to the VE choice, and \( L_1(E_1) \) and \( L_1(E_2) \) are the averaged \( L_1 \) values of the partition of unit and the \( (\Delta r)/d \) condition, respectively, at \( t/t_{\text{KH}} = 3 \).

| Model | \( \sigma \) | \( X \) | \( L_1(E_1) \times 10^{-2} \) | \( L_1(E_2) \times 10^{-2} \) |
|-------|-------------|-------|-----------------|-----------------|
| \( W_1 \) | 0 | \( m \) | 3.84 | 2.17 |
| \( W_2 \) | 1 | \( m \) | 2.79 | 1.43 |
| \( W_3 \) | \([0-1]\) | \( m \) | 2.60 | 1.35 |
| \( W_4 \) | 0 | \( m/\rho^0 \) | 1.39 | 1.76 |
| \( W_5 \) | 1 | \( m/\rho^0 \) | 0.93 | 1.12 |
| \( W_6 \) | \([0-1]\) | \( m/\rho^0 \) | 0.92 | 1.12 |

Fig. 11. \( L_1 \) values for \( E_1 \) (solid lines) and \( E_2 \) (dashed lines) in the wind-cloud collision tests. Using the improved VEs reduces both \( L_1 \) values for the whole simulation.

\( u_c = 3/20 \), respectively, so that both regions are in pressure equilibrium. The wind has an initial velocity \( (2c/3)^{3/2} \) and tends to the limiting value \( \rho \).

\( \tau_{\text{KH}} = 0.0937 \).

In Table 4 we present the \( L_1 \) values of errors \( E_1 \) and \( E_2 \) for the simulated models. Both errors are clearly lower when the improved VEs are used, independently of the value of \( \sigma \). This trend is constant during the whole evolution of the simulation as it can be seen in Fig. 11. In particular, it is clear that the models with \( \sigma = 0 \) lead to the largest \( L_1 \) errors in the long run, proving that the pure Lagrangian scheme is the most sensitive to tensile instability with such large density gradients. As in the case of the KH test, we make use of a variable \( \sigma \) to track the \( L_1 \) error generated by the particles in the inter-phase. In Fig. 12 we show a series of snapshots where the color represents the value of \( \sigma \) and proves the capabilities of our algorithm to track density jumps.

The density colormap at \( t/t_{\text{KH}} = 1.5 \) is shown in Fig. 13 for both choices of VEs. We see here that, independently of the VE choice, mixing is taking place, which will eventually destroy the cloud, albeit more efficiently if \( \sigma \neq 0 \). Figure 14 shows the maximum density attained in the cloud during the first stages of the interaction. Because of the strong impact of the wind a shock-wave is born which moves through the dense cloud compressing its matter. The density jumps from the original value of \( \rho_0 = 10 \) and tends to the limiting value \( \rho = 4\rho_0 \), characteristic of a strong
density enhancement results in the slight delay in crossing the above threshold condition $\rho \geq 0.64 \rho_i$. The disintegration rate of the cloud depicted in Fig. 15 when $\sigma \neq 0$ is in close agreement with that obtained with the CRKSPH scheme by Frontiere et al. (2017).

In summary, when large density contrasts are present, better accuracy is achieved by the proposed generalized volume elements, while the suppression of the tensile instability is handled via a surgical departure of the Lagrangian scheme, using a variable $\sigma$.

### 6.4. The Sedov explosion

We simulated this test in a three-dimensional square box of side $L = 1$ and total number of particles $N = 10^3$ settled in a glass-like configuration. The mass of all the particles was the same, resulting in an homogeneous initial density profile with $\rho = 1 \pm 0.005$. The explosion was initiated at the center of the box by depositing an amount of energy $\Delta U = 1$. That energy was spread following a Gaussian profile with characteristic width $\delta = 0.1$.

To investigate the dependence of the errors $E_{1,2}$ (Eqs. 16 and 17) with respect the VE estimator choice and $\sigma$, we calculated the $L_1$ errors in the shocked region\(^{10}\) with Eq. 25.

The outcome of the simulations is summarized in Table 5 and Figs. 16, 17, and 18. The best results were obtained in those models which incorporate the improved VEs. Unlike in the hydrostatic square test, the particular value adopted for the magnitude $\sigma$ plays a secondary role in the Sedov test. Figure 16 shows the profiles of density at $t = 0.09$ for models $S_4$ and $S_8$ in Table (5). Top row: density profiles at $t = 0.09$ calculated with $X_\sigma = m_\sigma$ (model $S_4$, standard VEs) and $X_\sigma = m_\sigma/\rho_i^0$ (model $S_8$, improved VEs). The black line is the analytical solution. Note that the spherical symmetry is well preserved in both cases and that the density peak is very well reproduced with the improved VEs. Bottom row: same but with the partition of unit.

All particles are represented in the plots.

\begin{table}[h]
\centering
\begin{tabular}{|c|c|c|c|c|c|}
\hline
Model & $\sigma$ & $\alpha_\sigma$ & $X$ & $\rho_{\text{max}}$ & $L_1(E_1)$ & $L_1(E_2)$ \\
& & & & & [$\times 10^{-2}$] & [$\times 10^{-2}$] \\
\hline
$S_1$ & 0 & 0.1 & $m$ & 3.34 & 3.10 & 2.20 \\
$S_2$ & 0 & 0.5 & $m$ & 3.16 & 2.85 & 1.96 \\
$S_3$ & 1 & 0.1 & $m$ & 3.33 & 3.05 & 2.20 \\
$S_4$ & [0 - 1] & 0.1 & $m$ & 3.35 & 3.10 & 2.20 \\
$S_5$ & 0 & 0 & $m/\rho_i^0$ & 3.71 & 1.53 & 1.72 \\
$S_6$ & 0 & 0.5 & $m/\rho_i^0$ & 3.47 & 1.33 & 1.52 \\
$S_7$ & 1 & 0.1 & $m/\rho_i^0$ & 3.70 & 1.45 & 1.67 \\
$S_8$ & [0 - 1] & 0.1 & $m/\rho_i^0$ & 3.71 & 1.45 & 1.63 \\
\hline
\end{tabular}
\caption{Summary of all calculated Sedov tests stating the values of $\sigma$, heat transport constant in the AV, VE choice, density peak, and $L_1$ errors at $t = 0.09$.}
\end{table}

\begin{figure}[h]
\centering
\includegraphics[width=\textwidth]{fig14}
\caption{Evolution of the maximum density in the cloud at $t/t_{KH} \leq 1.6$ for all models in Table 4.}
\end{figure}

\begin{figure}[h]
\centering
\includegraphics[width=\textwidth]{fig15}
\caption{Percent of surviving cloud in function of $t/t_{KH}$ for the wind-cloud collision tests.}
\end{figure}

\begin{figure}[h]
\centering
\includegraphics[width=\textwidth]{fig16}
\caption{The Sedov explosion 3D for models $S_4$ and $S_8$ in Table (5). Top row: density profiles at $t = 0.09$ calculated with $X_\sigma = m_\sigma$ (model $S_4$, standard VEs) and $X_\sigma = m_\sigma/\rho_i^0$ (model $S_8$, improved VEs). The black line is the analytical solution. Note that the spherical symmetry is well preserved in both cases and that the density peak is very well reproduced with the improved VEs. Bottom row: same but with the partition of unit. All particles are represented in the plots.}
\end{figure}

\(^{10}\) Defined as the volume with specific internal energy $\dot{u}(t) \geq 0.1$
tive errors of the maximum density with respect to the analytical value at $t = 0.09$ are $\approx 16\%$ and $\approx 7\%$ for the standard ($S_1$) and improved VEs ($S_8$), respectively. Figure 17 shows the distribution of the averaged $\sigma$ in a thin slice along the system for model $S_8$. As it can be seen, the value of $\sigma$ self-adapts so that it approaches to 1 across the shock front, goes down to $\approx 0.5$ in the post-shock region and vanishes in the central region.

The profile of the normalization function $\sum_b V_b W_{ab}(h_{ab})$ at $t = 0.09$ is also shown in Fig. 16, bottom row. As it can be seen, the choice $X_a = m_a/\rho_a^0$ substantially improves the partition of unit with respect the standard choice $X_a = m_a$. Such assessment is quantitatively confirmed by the temporal evolution of the error estimators $L_1(E_1, E_2)$ shown in Fig. 18. The enhancement is especially good in the case of the partition of unit, although less pronounced in the $(\Delta r)/h$ condition. Therefore, we conclude that combining ISPH with the VEs obtained with $X_a = m_a/\rho_a^0$ reduces both errors and improves the simulations.

The impact of increasing the conductive term in the AV was also analyzed. Raising the parameter $\alpha_a$ from our default choice, $\alpha_a = 0.1$ to $\alpha_a = 0.5$ substantially reduces the density peak from $\rho_{\max}(t = 0.09) = 3.34$ in model $S_1$, to $\rho_{\max}(t = 0.09) = 3.16$ in model $S_2$. In light of these results, it is advisable to choose a not too high value for $\alpha_a$.

6.5. The choice of $\sigma$ and entropy evolution in a shock

Under the light of the results of the tests presented here, the question of why do we need a variable $\sigma$ at all might arise. Obviously the case $\sigma = 0$ would be the most desirable one, as it is fully Lagrangian compatible. Nevertheless, it is clear that the crossed $\sigma = 1$ scheme leads to a more efficient removal of the tensile instability, but the price to pay is that there is not a complete compatibility between the Euler-Lagrangian formulation and the standard density equation (Eq. (28)). Such weakness of the crossed scheme is highlighted in the following test, which considers the behavior of entropy in weak and strong shocks. We want to prove that the entropy is not so well evolved when $\sigma \neq 0$. We additionally show that the new volume elements have a positive impact on the evolution of entropy.

Our numerical experiment is the same as in the Sedov test above but with an additional case where the initial energy of the explosion has been reduced in a factor of ten to simulate the case of a weak explosion. During the evolution of the explosion the contribution to the entropy of the gas is separated in two components: those arising from pressure forces $\Delta s_p$ and those from the artificial viscosity $\Delta s_{AV}$. Ideally $\Delta s_p \approx 0$, because the dissipation is basically driven by the AV.

The second law of thermodynamics states:

$$T \, ds = du - \frac{P}{\rho^2} \, d\rho,$$

where $T$, $s$, $u$ are temperature, specific values of entropy and internal energy, and pressure respectively. For an ideal gas with specific heat at constant volume, $c_v,$

$$\frac{ds}{c_v} = \frac{du}{u} - (\gamma - 1) \frac{d\rho}{\rho},$$

with $u = c_v \, T$. Thus, integrating on both sides:

$$\frac{\Delta s}{c_v} = \ln\left(\frac{u}{u_0}\right) - (\gamma - 1) \ln\left(\frac{\rho}{\rho_0}\right),$$

where $\rho_0, u_0$ are the initial values of density and temperature. To obtain the evolution of entropy of the ideal gas, without
the $AV$ contribution, we first calculate the increment of entropy $(\Delta s)_{AV}/c_v$ due to the $AV$. Subtracting $(\Delta s)_{AV}/c_v$ from (42) gives the ideal gas contribution, which should remain negligible during an adiabatic evolution.

The $AV$ contribution to the entropy in a process involving an energy/heat variation $dQ$ is:

$$\frac{dQ}{T} = (ds)_{AV} \rightarrow \frac{c_v dQ}{u} = (ds)_{AV} \rightarrow \frac{ds_{AV}}{c_v} = \frac{dQ}{u},$$

which, integrating on both sides, leads to

$$\frac{(\Delta s)_{AV}}{c_v} = \int \frac{dQ}{u} = \int \frac{1}{u} \left( \frac{du}{dt} \right)_{AV} dt,$$

where $\left( \frac{du}{dt} \right)_{AV}$ is directly obtained from the SPH code. The variation of the entropy of the gas, due to pressure forces $(\Delta s)_P/c_v$, and excluding the $AV$ contribution, is determined subtracting Eq (44) from Eq (42):

$$\frac{(\Delta s)_P}{c_v} = \Delta s - \frac{(\Delta s)_{AV}}{c_v}. \quad (45)$$

In absence of heat transport and providing that there are neither entropy sources (for example nuclear reactions) nor entropy sinks, $(\Delta s)_P/c_v = 0$.

In Fig. 19, we show the radial profile of $(\Delta s)_P/c_v$ for the different calculated models. First of all, we note that there is a spurious variation of entropy in all cases. Nevertheless, the combination $(X_0 = m_a/p_0^0; \sigma = 0)$ shown in the fourth panel leads to the best behavior of entropy in the shocked region (magenta lines). Not surprisingly, the worst cases are for $\sigma = 1$ (blue lines). These results clearly prove that Lagrangian compatibility is of utmost relevance to keep the entropy variations at low levels in adiabatic flows. Even more, upgrading the partition of unit with a Lagrangian-compatible estimator, such as $X_0 = m_a/p_0^0$, substantially improves the results. The mixed option with $\sigma = [0 \ldots 1]$ (black lines) is, for most of the cases, closer to $\sigma = 0$ or in between both curves, as expected. It therefore represents a balanced solution between Lagrangian-compatibility and suppression of the tensile instability.

The profiles of the total entropy variation is shown in Fig. 20. The strong shock dissipates much more entropy than the weak. Thus, the spurious generation of entropy in weak shocks, as shown in the upper panels in Fig. 19, is comparatively more acute.

The results of this test support the idea that working with an adaptive $\sigma$ is an useful option, which allows to suppress the tensile instability across shocks and contact discontinuities, while reducing the unwanted growth of entropy in the post-shock regions.

7. Conclusion

The main goal of this work is to devise and check an SPH scheme which fulfills as many as possible of the basic physical and numerical constraints demanded to modern hydrodynamic codes. The former include conservation of mass, linear and angular momentum, energy, and entropy. The latter requires a good depiction of gradients and shocks besides a correct numerical representation of basic kernel properties, as for example, the kernel normalization. The proposed scheme strongly relies in the ISPH method plus enhanced volume elements described in Cabezón et al. (2017) but with an improved Lagrangian compatibility and a better treatment of sharp density gradients.

To this end, we introduce an easy scheme to improve the partition of unit in SPH, with especial emphasis in the connections between the partition of unit and the accuracy in estimating the gradients. By combining analytical reasoning with simple 1D toy
models and full 3D simulations, we have shown that improving the constraint \( \sum V_i W_{ab}(h_a) = 1 \) automatically leads to an enhancement of the condition \( \langle \Delta r \rangle = \sum V_i (r_i - r_a) W_{ab}(h_a) = 0 \).

When gradients are approached with an integral expression (the ISPH scheme via Eq. 7), the fulfillment of the \( \langle \Delta r \rangle \) constraint is a sufficient condition to perform exact linear interpolations.

One of the novelties of this work, is the improvement of the partition of unit, without leaving the Lagrangian formulation of ISPH, so that the enhancement is totally compatible with the inclusion of grad-h terms in the momentum and energy equations. To do that the volume elements, \( V_a \), have been redefined so that \( V_a = \bar{X}_a / h_a \) with \( \bar{X}_a = m_a / \rho_a^0 \), \( h_a = \sum X_b W_{ab}(h_a) \) and \( \rho_a^0 = \sum m_b W_{ab}(h_a) \). That particular choice of \( V_a \) results in the new set of ISPH equations described in the Appendix A. These ISPH equations not only are Lagrangian-compatible, displaying perfect conservation properties, but manifestly improve the partition of unit which translates into a better estimation of gradients. The computational cost of including these improved VEs, mainly due to the implicit search of the coupled \( h_a \) and \( \rho_a^0 \) magnitudes with a Newton-Raphson algorithm, is subdominant. The behavior of the new ISPH scheme has been checked with a number of standard 3D tests which involve large density jumps and contact discontinuities.

A second novelty in the present work has to do with the correct handling of abrupt density jumps. The numerical handling of fluid regions with large density contrasts usually requires to abandon the Lagrangian formulation of the SPH equations in favor of other schemes. We propose here a self-adaptive scheme, steered by a single parameter \( 0 \leq \sigma \leq 1 \) (see Eqs. 29, 32, and 37), which selectively chooses the optimal integration scheme. When \( \sigma = 0 \) the Lagrangian-compatible scheme is recovered while \( \sigma \approx 1 \) is more adequate to handle large gradients.

The proposed scheme with \( \sigma = \lfloor 0 \rfloor \) gets rid of the tensile instability around contact discontinuities, being the closest possible to the compatibility with the Lagrangian formalism, because the fraction of particles with a significant \( \sigma \) value is usually low. It is therefore expected a better depiction of the entropy evolution in shocks than in completely crossed schemes (i.e with \( \sigma = 1 \)). According to Eq. (37), a value \( \sigma \leq 0.1 \) is taken in those fluid regions with \( 22 \% \leq \Delta r / a \), meaning that acoustic waves and weak shock-waves can be handled with, or bordering, the uncrossed option \( \sigma = 0 \). Such moderate density ratios over the kernel domain are also found in self-gravitational structures in equilibrium and in subsonic turbulence experiments.

Table 6 presents a summary of the above-mentioned contributions and contrasts them with our previous works, which puts into context the current extension. After García-Senz et al. (2012); Cabezón et al. (2012), our chosen method is ISPH which uses the integral approach to the derivatives, IAD, to implement the equations. Further developments were bounded to the inclusion of generalized volume elements which improved the partition of unit.

The results of the hydrodynamic tests unambiguously support the conclusions of the analytical arguments and simple toy models described in Section 4. Namely, that the proposed volume elements improve both the partition of unit and the \( \langle \Delta r \rangle \) condition in all studied cases. Nevertheless, the level of enhancement in the hydrodynamic simulations is lower than that promised by the toy model experiments, especially those concerning the \( \langle \Delta r \rangle \) constraint. Such degradation is attributable to the larger particle disorder in the real three-dimensional simulations, but still the results with the improved VEs are valuable. On another note, the novel self-adaptive \( \sigma \) scheme works very well, providing much better results in the hydrostatic and wind-cloud tests than the \( \sigma = 0 \) calculation. The results of the Kelvin-Helmholtz test suggest that the artificial viscosity algorithm plays a central role here, with the VEs and \( \sigma \) choice being subdominant. Finally, the Sedov test clearly shows the best performance of the proposed VEs, which allow to reproduce the correct density jump across the shock even in three-dimensional calculations with moderate number of particles. Interestingly, the better evolution of entropy in shocked regions when the \( \sigma = \lfloor 0 \rfloor \) scheme is used (see Sect. 6.5), reinforces the recent proposal by Rosswog (2020a) of using the entropy as a useful variable to build physically motivated AV triggers in SPH.

As an immediate prospect, we plan to use our improved ISPH code to numerically reproduce the isothermal, sub- and supersonic turbulence. Implementing the ISPH scheme to handle magneto-hydrodynamics effects is also under way.

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References
Agertz, O., Moore, B., Stadel, J., et al. 2007, MNRAS, 380, 963
Bonet, J. 1999, Computer Methods in Applied Mechanics and Engineering, 180, 97
Brookshaw, L. 1985, Proceedings of the Astronomical Society of Australia, 6, 207
Cabezon, R. M., Garcia-Senz, D., & Escartin, J. A. 2012, A&A, 545, A112
Cabezon, R. M., Garcia-Senz, D., & Figueira, J. 2017, A&A, 606, A78
Cabezon, R. M., Garcia-Senz, D., & Relafo, A. 2008, Journal of Computational Physics, 227, 8523
Colagrossi, A. & Landrini, M. 2003, Journal of Computational Physics, 191, 448
Cullen, L. & Dehnen, W. 2010, MNRAS, 408, 669
Dilts, G. A. 1999, International Journal for Numerical Methods in Engineering, 44, 1115
Escartin, J. 2016, PhD thesis, Polytechnical University of Catalonia. http://hdl.handle.net/10803/384002
Frontiere, N., Raskin, C. D., & Owen, J. M. 2017, Journal of Computational Physics, 332, 160
Fulk, D. A. & Quinn, D. W. 1996, Journal of Computational Physics, 126, 165
Garcia-Senz, D., Cabezon, R. M., & Escartin, J. A. 2012, A&A, 538, A9
Gingold, R. A. & Monaghan, J. J. 1977, MNRAS, 181, 375
Gomez-Gesteira, M., Rogers, B., Dalrymple, R., & Crespo, A. J. 2010, Journal of Hydraulic Research, 48, 6
Hopkins, P. F. 2013, MNRAS, 428, 2840
Knapp, C. E. 2000, PhD thesis, Los Alamos national Laboratory. https://www.osti.gov/biblio/754046
Liu, M. & Liu, G. 2006, Applied Numerical Mathematics, 56, 19–36
Lucy, L. B. 1977, AJ, 82, 1013
McNally, C. P., Lyra, W., & Pasoy, J.-C. 2012, ApJS, 201, 18
Monaghan, J. J. 1992, ARA&A, 30, 543
Monaghan, J. J. 1997, Journal of Computational Physics, 136, 298
Monaghan, J. J. 2005, Reports on Progress in Physics, 68, 1703
Monaghan, J. J. 2012, Annual Review of Fluid Mechanics, 44, 323
Oger, G., Doring, M., Alessandrini, B., & Ferrant, P. 2007, Journal of Computational Physics, 225, 1472
Price, D. 2005, PhD thesis, University of Cambridge, https://ui.adsabs.harvard.edu/abs/2005PhDT.........295P
Price, D. J. 2008, Journal of Computational Physics, 227, 10040
Price, D. J., Wurster, J., Tricco, T. S., et al. 2018, PASA, 35, e031
Read, J. I., Hayfield, T., & Agertz, O. 2010, MNRAS, 405, 1513
Ritchie, B. W. & Thomas, P. A. 2001, MNRAS, 323, 743
Rosswog, S. 2015a, MNRAS, 448, 3628
Rosswog, S. 2015b, Living Reviews in Computational Astrophysics, 1, 1
Rosswog, S. 2020a, ApJ, 898, 60
Rosswog, S. 2020b, MNRAS, 498, 4230
Saitoh, T. R. & Makino, J. 2013, ApJ, 768, 44
Springel, V. 2010, ARA&A, 48, 391
Springel, V. & Hernquist, L. 2002, MNRAS, 333, 649
Tricco, T. S. 2019, MNRAS, 488, 5210
Valdarnini, R. 2016, ApJ, 831, 103
Wadsley, J. W., Keller, B. W., & Quinn, T. R. 2017, MNRAS, 471, 2357
Wissing, R. & Shen, S. 2020, A&A, 638, A140
Zhu, Q., Hernquist, L., & Li, Y. 2015, ApJ, 800, 6
Appendix A: The SPH and ISPH formalisms with generalized VE

According to the Euler-Lagrange formulation of SPH (Springel 2010) and references therein) the movement equations are written as,

\[ m_a \ddot{r}_a = - \sum_b m_b P_b \frac{\partial p_b}{\partial r_a} = \sum_b P_b \frac{\partial V_b}{\partial r_a}, \tag{A.1} \]

where \( V_b \) is the characteristic volume occupied by the particle, and \( \rho_b = m_b/V_b \). The derivative on the RHS embodies the effect of h-gradients. The spatial part of the derivative can be performed in the standard way, \( \nabla W_{ab} \) or, better, with the integral approach given by Eq. (31).

We first calculate the value of \( \partial V_b / \partial r_a \) in Eq. (A.1),

\[ \frac{\partial V_b}{\partial r_a} = \nabla_a V_b = \sum \frac{\partial V_b}{\partial h_b} \frac{\partial h_b}{\partial r_a}, \tag{A.2} \]

The grad-h part of equation above can be estimated differentiating the constraint \( h_b V_b^{-1} = C \) with respect \( r_a \) which, after some algebra, gives:

\[ \frac{\partial V_b}{\partial h_b} \frac{\partial h_b}{\partial r_a} = \left[ 1 - \frac{3V_b}{h_b} \frac{\partial V_b}{\partial h_b} \right] \frac{\partial V_b}{\partial r_a}, \tag{A.3} \]

which combined to expression (A.2) gives

\[ \frac{\partial V_b}{\partial r_a} = \nabla_a V_b \left[ 1 - \frac{h_b}{3V_b} \frac{\partial V_b}{\partial h_b} \right]^{-1}, \tag{A.4} \]

where \( \nabla_a V_b \) refers to the spatial gradient whereas the grad-h effects are included in the term in brackets.

To estimate \( \nabla_a V_b \), the precise form of the volume elements has to be known. A general form for these elements is Hopkins (2013):

\[ V_b = \frac{X_b}{k_b} \quad \text{with} \quad k_b = \sum_X W_{bc}(h_b), \tag{A.5} \]

where \( X_b \) is a scalar estimator. Here we have considered two different estimator families, leading to slightly different expressions of the movement and energy equations:

a) Constant \( X_b \), as for example \( X_b = m_b \) and \( X_b = 1 \) both reproducing the standard volume elements \( V_b = m_b/\rho_b \). Other choice is \( X_b = P^2 \) where \( P \) is the pressure and \( k \leq 1 \). In this case, the estimator is strictly constant only in isobaric systems.

\[ \nabla_a V_b \rightarrow \nabla a V_a = \nabla a \left( \frac{X_b}{k_b} \right) = -\frac{X_b^2}{k_b^2} \nabla_b W_{ab}(h_a), \tag{A.6} \]

\[ \nabla_a V_b \rightarrow \nabla a V_b = \nabla a \left( \frac{X_b}{k_b} \right) = -\frac{X_b^2}{k_b^2} \nabla_b W_{ab}(h_b). \tag{A.7} \]

Combining expressions (A.4), (A.6), and (A.7) with Eq. (A.1), and making use of Eq. (31) to carry out the IA approach of the kernel gradient, the i-component of the acceleration of particle \( a \) is finally obtained:

\[ \ddot{x}_{i,a} = -\frac{X_a}{m_a} \sum_b \left[ \frac{X_b P_a}{\Omega_a \rho_a^2 k_b^2} \mathcal{A}_{i,ab}(h_a) + \frac{x_b P_b}{\Omega_b \rho_b^2 k_b} \mathcal{A}_{i,ab}(h_b) \right], \tag{A.8} \]

with

\[ \Omega_a = \left[ 1 - \frac{h_a}{3V_a} \frac{\partial V_a}{\partial h_a} \right] = \left[ 1 + \frac{h_a}{3V_a} \frac{\partial V_a}{\partial h_a} \right]. \tag{A.9} \]

b) Adaptive \( X_b = m_b / \rho_b^2 \), being \( \rho_b^2 = \sum c m_c W_{bc}(h_b) \) the standard SPH density. Because of the normalization condition, this choice leads to constant \( k_b = \sum_X X_b W_{bc}(h) \). Now we have

\[ \nabla a V_b \rightarrow \nabla a V_a = \nabla a \left( \frac{X_a}{k_a} \right) = -\frac{m_a}{\rho_b^2 k_a} \nabla_b \rho_b^2 = -\frac{m_a}{\rho_b^2 k_a} \sum_b m_b \nabla_b W_{ab}(h_a), \tag{A.10} \]

\[ \nabla a V_b \rightarrow \nabla a V_b = \nabla a \left( \frac{X_b}{k_b} \right) = -\frac{m_b}{\rho_b^2 k_b} \nabla_b W_{ab}(h_b). \tag{A.11} \]

Combining expressions (A.4), (A.10), and (A.11) with Eq. (A.1), and making use of Eq. (31) to compute the IA approach of the kernel gradient, the i-component of the acceleration of particle \( a \) is obtained,

\[ \ddot{x}_{i,a} = -\sum_b m_b \left[ \frac{X_b^2 P_a}{\Omega_a \rho_a^2 k_b^2} \mathcal{A}_{i,ab}(h_a) + \frac{x_b^2 P_b}{\Omega_b \rho_b^2 k_b} \mathcal{A}_{i,ab}(h_b) \right]. \tag{A.12} \]

According to expression (A.9), to estimate \( \Omega_a \) it is necessary to know the derivative of the density with respect the smoothing-length (\( \partial \rho / \partial h_a \)). The result relies in the choice the estimator \( X_a \) used to compute the density.

– For constant \( X_a \), as for example (but not necessarily), the standard choice \( X_a = m_a \):

\[ \frac{\partial \rho_a}{\partial h_a} = \frac{m_a}{X_a} \sum_b X_b \frac{\partial W_{ab}(h)}{\partial h_a}. \tag{A.13} \]

– The choice \( X_a = (m_a / \rho_b^2) \) requires a bit more algebra:

\[ \frac{\partial \rho_a}{\partial h_a} = \frac{m_a}{X_a} \left( \frac{\partial X_a}{\partial h_a} \right) - \frac{m_a k_a}{X_a^3} \left( \frac{\partial X_a}{\partial h_a} \right). \tag{A.14} \]
with:

\[
\frac{\partial k_a}{\partial h_a} = \sum_b \frac{\partial}{\partial h_a} \left( \frac{m_b}{\rho_0^a} \right) W_{ab}(h_a) + \sum_b X_b \frac{\partial W_{ab}(h_a)}{\partial h_a} \\
= - \left( \frac{m_a}{(\rho_0^a)^2} \right) W_{aa}(h_a) \frac{\partial \rho_0^a(h_a)}{\partial h_a} + \sum_b X_b \frac{\partial W_{ab}(h_a)}{\partial h_a} ,
\]

(A.15)

and,

\[
\frac{\partial X_a}{\partial h_a} = \frac{\partial}{\partial h_a} \left( \frac{m_a}{\rho_0^a} \right) \frac{\partial \rho_0^a(h_a)}{\partial h_a} = - \left( \frac{m_a}{(\rho_0^a)^2} \right) \sum_b m_b \frac{\partial W_{ab}(h_a)}{\partial h_a} .
\]

(A.16)

Putting expressions (A.15) and (A.16) into Eq. (A.14) and manipulating,

\[
\frac{\partial \rho_a}{\partial h_a} = \left[ \frac{\rho_a}{\rho_0^a} - X_a W_{aa}(h_a) \right] \sum_b m_b \frac{\partial W_{ab}(h_a)}{\partial h_a} + \frac{m_a}{X_a} \sum_b X_b \frac{\partial W_{ab}(h_a)}{\partial h_a} .
\]

(A.17)