Low-Temperature Preparation of β-C$_2$S from Sand/Lime Mixture: Influence of Sodium Hydroxide

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Abstract
The low-temperature preparation of belite (β-C$_2$S) from a mixture of lime and white sand (Ca/Si=2) in presence of 0.5-5 M NaOH solution was investigated by hydrothermal treatment in a stainless steel capsule at 135°C for 3 hours followed by calcination at 1000°C for 3 hours. All materials were analyzed by FTIR, SEM-EDX, and XRD with semi-quantitative phase analysis calculation. The addition of NaOH changed the composition of the hydrothermal and calcination products. Different percent of β-C$_2$S and other calcium and sodium silicate phases were produced with increasing the concentration of NaOH. In presence of 0.5M NaOH, 32.6% of β-C$_2$S formed with the formation of calcium silicate with mole ratio CaO/SiO$_2$=1.5 (rankinite, 30.9%) and sodium-calcium silicate (combeite, 8.6%). Whereas, in the presence of 5M NaOH, the hydrothermal reaction between lime and silica was effectively deactivated i.e. 32.9% of β-C$_2$S formed. The formation of sodium silicate (31%), rankinite (15.4%) and sodium-calcium silicate (16.7%) phases were encouraged. The optimum condition for preparation of low-temperature β-C$_2$S rich cement from lime and sand under these conditions can be achieved by the addition of 2M NaOH were, 77.7% of β-C$_2$S formed and 12.4% combeite.

Keywords: White sand; Lime; Hydrothermal treatment; Calcination

The Common Phases that Appeared in the study and their Formula

| Phase            | Formula                                      |
|------------------|----------------------------------------------|
| Afwillite        | Ca$_3$Si$_2$O$_8$(OH)$_2$(H$_2$O)$_2$         |
| Alite, C$_3$S    | Ca$_3$SiO$_5$                                |
| Belite (β-C$_2$S)| Ca$_2$SiO$_4$                                |
| Calcite          | CaCO$_3$                                     |
| Combeite         | Na$_4$Ca$_4$(Si$_6$O$_{18}$)                 |
| Dellaite         | Ca$_3$[SiO$_4$]$_2$[Si$_2$O$_7$]$_2$[SiO$_4$]$_2$[OH]$_2$ |
| α-Dicalcium silicate hydrate | Ca$_3$(SO$_2$O$_7$)OH$_2$/4 |
| Gehlenite        | Ca$_2$Al[AlSiO$_4$]                           |
| Hillebrandite (dicalcium silicate hydrate) | Ca$_3$(SiO$_3$)OH$_2$/3 |
| Kaolinite        | Al$_2$Si$_2$O$_5$(OH)$_4$                    |
| Lime             | CaO                                          |
| Mayenite         | Ca$_2$Al$_2$O$_7$                            |
| Portlandite      | Ca(OH)$_2$                                   |
| Quartz           | SiO$_2$                                      |
| Rankinite        | Ca$_3$SiO$_3$                                 |
| Sodium-calcium silicate | Na$_2$Ca$_2$(Si$_3$O$_9$)                  |
| Sodium-hydrogen silicate hydrate | Na$_2$[H$_2$SiO$_4$]$_2$.7H$_2$O |
| Xonotlite        | Ca$_3$SiO$_7$(OH)$_2$                         |
**Introduction**

Cement industry consumes large amounts of limestone and clay raw materials. About 1.5ton of limestone and 0.3ton of clay are needed for the production of 1ton of cement [1]. In addition, the cement industry consumes large amounts of energy (3100-3600 kJ/kg clinker) and produces significant quantities of CO₂ from the combustion of fuel and decomposition of limestone in cement manufacture (0.83 ton of CO₂/ton of cement). CO₂ contributes to global warming by increasing the greenhouse effect [2]. The world cement industry contributes about 8% of the global quantity of CO₂ emitted into the atmosphere [3]. Both the reduction of energy consumption as well as CO₂ emission in the cement production can be achieved by reducing the lime saturation factor (LSF) of the raw meal, which leads to the production of belite-rich clinker because the formation of belite occurs at a lower temperature than that for alite [4,5]. Alite is the most important component of Portland cement, though its formation needs high temperature and consumes comparatively large amounts of energy compared to belite. The enthalpy of formation of alite and belite is -1810kJ/kg and -1350kJ/kg respectively [6]. The decrease of the clinkering temperature belite cement during the production of belite cement results in energy savings up to 16% [7] and reduction of CO₂ emissions (up to 6-10%) [8].

This is the reason of great efforts towards the development of belite cement. Nevertheless, a slow hydration process and low strength after 28 days are disadvantages of the belite-rich cement. However, this kind of cement is suitable for long term sustainable materials [9].

C₃S exists in several polymorphic forms (α, α′, α″, β, and γ), that are stable in different temperature ranges with different hydraulic properties [9]. The γ-form is considered as inert and has poor hydraulic properties [10]. The α, α′, and β-C₃S have a reactivity similar to that of alite [11]. The reactive forms of dicalcium silicate can be stabilized by rapid cooling of the belite clinker, at least 500 °C/min in the temperature range 1300-700°C [12], or by inclusion of an appropriate stabilizer oxides into the crystal lattice of C₃S, which stabilize α and β polymorphs of C₃S such as B₂O₃, Na₂O, K₂O, P₂O₅, MgO, and BaO [10,13]. β-phase of belite cement is considered as one of the favorable constituents in industrial Portland cement clinker because it has a slow rate of hydration at early ages). Accordingly, it has a lower rate of heat evolution during cement hydration and it has improved mechanical strength [14]. Belite cement is also used in the production of refractory materials [15], heat resistant coatings [16], bioactive self-setting materials [17] and electrical insulators [18].

![Figure 1: Thermal transformation relationship of belite Polymorphs.](image)

Traditionally, belite is readily prepared from limestone and sand by solid-state reaction at high temperature by using different chemical stabilizing agents [19]. Whatever, this method leads to the formation of non-homogeneous products with impurity [20]. Alternatively, belite is readily prepared from CaO and SiO₂ by various routes at relatively lower temperatures such as hydrothermal-calcination process at 700-1000 °C [21-25], sol-gel synthesis [26], Pechini process [27] and hydrothermal-mechanochemical process [28-31]. However, the application of such methods on an industrial scale is complicated due to the high purity requirements of the starting material and complex equipment [32].

The reactive low energy belite cement represents great economic and environmental value due to the use of wastes and by-products such as fly ash [33,34]. It should be emphasized that the synthesis of belite by a hydrothermal-calcination method is one of the energetically cost-effective routes, because the temperature of hydrothermal synthesis does not exceed 200 °C and the temperature of the thermal activation is lower than 1000 °C [32]. One of the older trials for preparation of β-C₃S by hydrothermal-calcination route was done by Nanru [35] when they prepared β-C₃S by heating the hydrothermally produced dicalcium silicate hydrate (hillebrandite) at 950 °C with the molar ratio C/S=2. The obtained β-C₃S had a high specific surface and reacted with water as quickly as tricalcium silicate but starting from the 14th day of hydration [35]. Then Ishida as well as and Sasaki [36-38] obtained β-C₃S by heating hillebrandite at 600 °C. Those researchers showed that the intermediate phases after the hydrothermal process are very crucial to obtain various types and characteristics of products after calcinations. From these previous works, the α-dicalcium silicate hydrate, hillebrandite and deltaxite phases as intermediate phases were obtained by hydrothermal treatment at temperatures between 100-250 °C. Hillebrandite phase is recommended to produce more reactive C₃S than α-dicalcium silicate hydrate and deltaxite phases. Kurdowski [39] heated the mixture of C-S-H phase with C/S molar ratio about 1.6 and CH at 800 °C, producing practically pure β-C₃S having a very high specific surface.
Sodium and potassium ions form solid solutions with dicalcium silicate, which imparts higher hydraulic activity and, especially in case of sodium, give much higher heat of hydration [39]. Other researchers have studied the formation of reactive belite by a hydrothermal-calcination method using coal combustion fly ash [40-50]. During the hydrothermal treatment, the pozzolanic reaction of fly-ash with lime is strongly activated, thus leading to the formation of hydraulic precursors. The dehydration of the hydraulic precursors at higher temperature 700-1000 °C, leads to the formation of reactive belite (αₗ and β-Ca₂SiO₅) and mayenite. The compressive strength of this cement at 28 days reaches similar values to those for Portland cement CEM I 32.5 type [42] and has good resistance to sulfate attack [46]. Cement with αₗ-C₂S was prepared from fly ash in KOH solution (0.6M) at 5h at 100 °C, followed by burning at a minimum temperature of 800 °C and air-cooling produced reactive belite cement containing between 79% and 86% of C₂S (αₗ and/or β polymorphs), the rest being C₃A (5-8%), C₃AF (7-11%) and free lime (2%) [48,50]. Filkova [49] proved that the bottom ash with high CaO content fixed in anhydrite form (44.1%) is not suitable as raw material for synthesizing belite cement. Because the formation of gehlenite phase was observed at 900 °C, that is known as a retarder of cement hydration, and therefore undesirable for the cement [49]. Highly reactive β-belte is obtained with relatively high surface area (4.073 m²/g) from lime sludge (a pulp and paper industry residue) and silica fume in a molar ratio of calcined at 2.0 by hydrothermal method followed by calcination at 1000 °C for 2h [21]. Also, β-C₂S was prepared from different siliceous raw materials such as silica fume, white sand, rice husk ash, silica, and amorphous silica under various hydrothermal conditions with lime in presence in stabilizer such as BaCl₂ followed by calcination of the product at 650 °C-1000 °C [24,51-55]. The aim of this work is to investigate the influence of NaOH concentration on the preparation of belite cement from lime and white sand hydrothermally treated and calcined at low temperatures.

Materials and Experimental Techniques

The raw materials that are used in this study are high-grade lime and white sand. The lime was produced by calcination of limestone powder in a muffle furnace at 950 °C, cooled to room temperature in a desiccator, milled to a fine powder and stored in a tightly closed plastic bag to avoid carbonation. The white sand was also milled to a fine powder. Figure 2 illustrates the procedure of the low-temperature synthesis of belite. A mixture of lime and white sand with a mole ratio (Ca/Si=2) and distilled water was added to obtain the water/solid ratio of 5/1 by weight. NaOH pellets were added to obtain 0.5, 2 and 5M concentration. The mixture was placed in a stainless-steel capsule keeping the occupied volume equals 67% of total volume capacity. The capsule was tightly closed, shacked vigorously, and hydrothermally treated at 135 °C for 3 hours in an electric oven. The capsule was removed from the oven and cooled to room temperature.

Figure 2: Procedure of low temperature synthesis of belite.

The hydrated product was filtered, washed with distilled water and dried in an electric oven overnight at 80 °C. The hydrated product was calcined in the muffle furnace at 1000 °C for 3 hours and cooled to room temperature in a desiccator, milled and stored in tightly closed plastic bags. The raw materials were analyzed by XRF techniques whereas the raw materials and calcined product were analyzed by FTIR, XRD, TGA/Dr TGA/DSC, and SEM-EDX techniques. X-ray fluorescence analysis (XRF) was measured by Philips PW1606 x-ray fluorescence spectrometer. X-ray diffraction analysis (XRD) was measured by Philips x-ray diffractometer PW 1370, Co. with Ni-filtered CuKₐ radiation (1.5406 Å). Semi-quantitative phase analysis was calculated using the Bruker AXS configuration program. Fourier transform infrared analysis (FTIR) was measured by spectrometer Perkin Elmer FTIR System Spectrum X in the range 400-4000cm⁻¹. Thermogravimetric analysis/differential scanning calorimetry analysis (TGA/DrTGA/ DSC) were measured by Netzsch STA 409 C/CD analyzer with 2 °C/ min heating rate from room temperature up to 1000 °C, under air atmosphere at 50ml/min flow rate, the hold time at the appropriate temperature is zero. Scanning electron microscope with energy dispersive X-ray analysis (SEM-EDX) was measured by Jeol-Dsm 5400 LG apparatus.
Results

Table 1 illustrates the chemical composition of lime and white sand determined by XRF analysis. The lime composes of 86.64% CaO and the white sand composes of 98.27% SiO$_2$. Figure 3 illustrates the FTIR spectra of raw materials as well as the hydrothermally treated and calcined products. In the case of lime, the absorption band at 3644 cm$^{-1}$ is attributed to the vibration of OH-associated with hydrated lime present as partial hydration of lime [53]. The absorption bands at 876 and 1468 cm$^{-1}$ are attributed to the v$_2$ and v$_3$ vibration of carbonate (CO$_3^{2-}$) present as a result of the partial carbonation of lime [56]. The absorption band at 458 cm$^{-1}$ is attributed to the Ca-O stretching vibration [57]. The absorption bands at 1630 and 3425 cm$^{-1}$ are attributed to the stretching and bending vibrations of structural hydroxyl groups and water [58]. The absorption band at 1420 cm$^{-1}$ is attributed to the Ca-OH vibration band of lime [59]. In case of sand, the absorption bands at 1087, 787, 472 cm$^{-1}$ are attributed to the Si-O-Si asymmetric stretching vibration, Si-O-Si symmetric stretching vibration and O-Si-O bending vibration of quartz [60]. The absorption bands at 689, 540 cm$^{-1}$ are attributed to the Si-O vibration of kaolinite. The absorption band at 1032 cm$^{-1}$ is attributed to the Si-O stretching (in-plane) vibration of kaolinite.

![FTIR spectra](image)

**Figure 3:** FTIR spectra of (a) lime and sand, (b) hydrothermally treated and (c) calcined products. (A afwillite, ββ-C2S, C calcite, Co combeite, H calcium silicate hydrate, L lime, P portlandite, Q quartz, R rankinite, W water and X xonotlite).

| Oxide, Wt % | SiO$_2$ | Al$_2$O$_3$ | CaO | Fe$_2$O$_3$ | MgO | SO$_3$ | Na$_2$O | K$_2$O | TiO$_2$ | Cl$^-$ | LOI* | Total |
|-------------|--------|-------------|-----|------------|-----|--------|--------|-------|--------|-------|------|-------|
| Lime        | 1.90   | 0.67        | 90.64 | 0.32       | 0.71 | 0.44   | 0.24   | 0.08  | 0.04   | 0.05  | 4.24 | 99.58 |
| Sand        | 98.20  | 0.95        | 0.31 | 0.08       | 0.11 | 0.07   | 0.10   | 0.02  | 0.05   | 0.05  | 99.88 |

*LOI is the loss on ignition.

The absorption band at 918 cm$^{-1}$ is attributed to the AlAlOH vibration of kaolinite [61]. The absorption bands at 3694, 3623 cm$^{-1}$ are attributed to the stretching vibrations of surface OH groups and stretching vibrations of inner hydroxyl groups [62]. In the case of the hydrothermally treated products, the absorption band at 965 cm$^{-1}$ is attributed to the characteristic vibration of calcium silicate hydrate. The absorption bands at 796, 1070 cm$^{-1}$ are attributed to the residual quartz. The absorption band at 3642 cm$^{-1}$ is attributed to residual portlandite. The absorption band at 1424 cm$^{-1}$ is attributed to calcite formed due to partial carbonation of portlandite. The absorption band at 3382 cm$^{-1}$ is attributed to the vibration band of water molecules. The absorption bands at 480, 875, 965 cm$^{-1}$ are attributed to the characteristic vibration bands of afwillite. The absorption bands at 449, 480, 668, 965 cm$^{-1}$ are attributed to the stretching vibrations of structural hydroxyl groups and water [58].
attributed to the characteristic vibration bands of xonotlite. In the case of the calcined products, the absorption bands at 1006, 876, 520 cm\(^{-1}\) are attributed to the characteristic vibration bands of \( \beta \)-C\(_2\)S\(_3\) [63].

The absorption band at 917 cm\(^{-1}\) is attributed to the characteristic vibration band of combeite. The absorption bands at 846, 998 cm\(^{-1}\) are attributed to the characteristic vibration bands of rankinite. The absorption bands at 796, 1070 cm\(^{-1}\) are attributed to the residual quartz and the absorption band at 877 cm\(^{-1}\) is attributed to the residual lime. Figure 4 illustrates the XRD diffraction patterns of raw materials as well as the hydrothermally treated and calcined products. Lime composes mainly of CaO and sand composes of quartz. The main crystalline phases that were detected in the hydrothermally treated products are the afwillite and xonotlite minerals in addition to residual portlandite and quartz. The main crystalline phases that were detected in the calcined products are the rankinite, \( \beta \)-C\(_2\)S\(_3\), combeite, sodium-hydrogen silicate hydrate, sodium-calcium silicate minerals in addition to residual calcite, portlandite, lime, and quartz. Table 2 illustrates the semi-quantitative phase analysis derived from XRD results. The addition of NaOH markedly affects the rate of hydrothermal reaction between lime and silica as well as the formation of \( \beta \)-C\(_2\)S and other phases such as rankinite (calcium silicate with mole ratio CaO/SiO\(_2\)=1.5), combeite, sodium-calcium silicate, and sodium silicate.

![Figure 4: XRD diffraction patterns of (a) lime and sand, (b) hydrothermally treated and (c) calcined products. (An afwillite, \( \beta \)-C\(_2\)S, C calcite, Co combeite, L lime, P portlandite, Q quartz, R rankinite, S sodium-hydrogen silicate hydrate, Sc sodium-calcium silicate and X xonotlite).](image)

| Phases                  | NaOH Conc. |
|-------------------------|-------------|
|             | 0M | 0.5M | 2M | 5M |
| \( \beta \)-C\(_2\)S  | 65 | 33  | 77 | 33 |
| Quartz                  | 16 | 9   | -  | -  |
| Lime                    | 4  | 14  | 10 | 4  |
| Portlandite             | 10 | 4   | -  | -  |
| CaO3                    | 5  | -   | -  | -  |
| Rankinite               | -  | 31  | -  | 15 |
| Combeite                | -  | 9   | 13 | -  |
| Sodium-calcium silicate | -  | -   | -  | 17 |
| Sodium-hydrogen silicate hydrates | - | - | - | 31 |

Table 2: The semi quantitative phase analysis.
Figure 5: DSC, TGA and DTG of 0M-5M hydrothermally treated.

Figure 6a: SEM-EDX of lime and sand.

Figure 5 illustrates DSC/TGA/DrTGA thermograms of the hydrothermally treated product. The thermograms illustrate the two thermal reactions that occur during the calcination of all the hydrothermally treated products at about 408 °C and 643 °C. A clear endothermic peak occurs at about 173 °C in case of sand/lime mixture that was hydrothermally treated in presence of 5M NaOH. Figure 6a illustrates the SEM-EDX analysis of raw materials as well as the hydrothermally treated and calcined products. SEM results of lime show the morphology of lime grains. SEM results of white sand show the existence of hexagonal platelets of kaolinite crystals [64] laying on the surface of quartz aggregates. The SEM results of hydrothermally treated products show the existence of calcium silicate hydrate (hillebrandite) gel. SEM results of calcined products show the existence of fine β-C₃S aggregates.
Discussion

FTIR results of raw materials (Figure 6b) illustrate that lime is partially carbonated as proved from the appearance of the absorption bands at 876 and 1468 cm\(^{-1}\) corresponding to the \(v_2\) and \(v_3\) vibration of carbonate. White sand contains residual kaolinite, which is found as an accessory mineral in white sand. During the hydrothermal treatment of white sand/lime mixture with the mole ratio of CaO/SiO\(_2\)=2 at 135 °C for 3 hours, the reaction between lime and silica was activated leading to the formation of calcium silicate hydrate, with the existence of residues of the starting materials (quartz and lime). The later under these conditions was hydrated (portlandite) as well as partially carbonated (calcite). The formation of other crystalline calcium silicate hydrates, i.e. afwillite and xonolite also was encouraged under the hydrothermal conditions. The hydrothermal treatment of white sand/lime mixture in the presence of increasing concentrations of NaOH favors the formation of more calcium silicate hydrate at the expense of afwillite and xonolite phases. The XRD results provided with the semi-quantitative phase analysis of the calcined products using the Bruker AXS configuration program give a relatively clear idea about the reactions and phase transformations which occur as a result of the hydrothermal treatment of lime/sand mixture (mole ratio CaO/SiO\(_2\)=2) in presence of NaOH solution (0.5-5M) at 135 °C and calcination of the products at 1000 °C.

Figure 6b: SEM-EDX of 0M-5M hydrothermally treated.

In the absence of NaOH, 64.73% β-C\(_2\)S formed in the calcined product leaving behind appreciable percent of silica and lime that was partially hydrated (portlandite) and carbonated (CaCO\(_3\)) Figure 6c. This means that the reaction between quartz and lime does not reach the state of completion in the absence of NaOH. In the presence of 0.5M NaOH, the hydrothermal reaction between lime and silica was deactivated (32.6% β-C\(_2\)S was formed). On the other hand, the formation of calcium silicate with mole ratio CaO/SiO\(_2\)=1.5 (rankinite, 30.9%) as well as sodium-calcium silicate (combeite, 8.6%) was activated. In the presence of 2M NaOH, the hydrothermal reaction between lime and silica was markedly activated leading to the formation of the highest percentage of β-C\(_2\)S (77.7%) and 12.4% combeite. In the presence of 5M NaOH, the hydrothermal reaction between lime and silica was effectively deactivated leading to the formation of the lowest percent of β-C\(_2\)S (32.9%). In contrast, the formation of sodium silicate (31%), rankinite (15.4%), and sodium-calcium silicate (16.7%) phases were encouraged. Regarding the DSC/TGA/DrTGA thermograms of the hydrothermally treated products, the first endothermic peak is attributed to the dehydration of Portlandite [65]. The second endothermic peak is attributed to the formation of β-C\(_2\)S as a result of the dehydration of calcium silicate hydrate [66]. The endothermic peak that occurs at about 173 °C in case of sand/lime mixture that was hydrothermally treated in presence of 5M NaOH, is attributed to the loss of water bound in different ways to the sodium silicate in the range of 50-200 °C [67]. The raw materials, as well as the hydrothermally treated and calcined products, were analyzed by SEM-EDX. The empirical formulae of different phases that were pointed out were calculated using the EDX data expressed in normalized atom%.
Taking into consideration that the calculated formulae are approximate due to the presence of variable contents of foreign ions depending on the proximity of the EDX point analysis to the underlying other phases [68]. SEM results of raw materials show the morphology of fine lime grains as well as that of large quartz grains with the existence of hexagonal platelets of kaolinite crystals [64] laying on its surface. The SEM images of the hydrothermally treated white sand/lime mixture in the absence of NaOH reveal an abrupt change in the microstructure of the starting materials. This proves that the reaction between lime and silica was activated dissolving much of quartz grains and the formation of calcium silicate hydrate gel with the existence of unreacted quartz grains. SEM results show that the amount of calcium silicate hydrate gel reaches the maximum percentage at 2M NaOH addition. Increasing the concentration of NaOH to 5M leads to the formation of sodium-calcium silicates. SEM results of calcined products show the presence of $\beta$-C$_2$S. Also, the formation of $\beta$-C$_2$S reaches its maximum at 2M NaOH addition. Increasing the concentration of NaOH to 5M leads to the formation of sodium-calcium silicates instead of $\beta$-C$_2$S.

**Conclusion**

This paper study the low-temperature synthesis of belite by the hydrothermal treatment of lime/sand mixture (mole ration CaO/SiO$_2$=2) in presence of (0.5-5M) NaOH solution at 135°C for 3 hours and calcination of the products at 1000 °C for 3 hours. The main conclusions of this investigation are:

A. The FTIR, TGA, SEM, and XRD results provided with the semi-quantitative phase analysis illustrate the different reactions and phase transformations that occur during the hydrothermal-calcination processes for the lime/sand mixture in presence of NaOH solution.

B. Without the addition of NaOH, the hydrothermal reaction between quartz and lime does not reach the state of completion. Hence, 64.73% $\beta$-C$_2$S formed in the calcined product leaving behind appreciable percent of unreacted silica and lime.

C. The addition of NaOH changed the composition of the hydrothermal and calcination products. Accordingly, different percent of $\beta$-C$_2$S and other calcium and sodium silicate phases were produced with raising the concentration of NaOH.

D. In presence of 0.5M NaOH, 32.6% $\beta$-C$_2$S was formed with the formation of calcium silicate with mole ratio CaO/SiO$_2$ =1.5 (rankinite, 30.9%) and sodium-calcium silicate (combeite, 8.6%).

E. In the presence of 2M NaOH, the higher percent of $\beta$-C$_2$S formed (77.7%) and 12.4% combeite.

F. In presence of 5M NaOH, the hydrothermal reaction between lime and silica was effectively deactivated leading to the formation of the lowest percent of $\beta$-C$_2$S (32.9%). Whereas, the formation of sodium silicate (31%), rankinite (15.4%), and sodium-calcium silicate (16.7%) phases were encouraged.
Accordingly, the optimum condition for preparation of low-temperature β-C₃S rich cement from lime and sand under these conditions can be achieved by the addition of 2M NaOH.

Further studies in the future must be conducted to investigate the reactivity and cementitious properties of belite prepared under the experimental procedure illustrated in this study.

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