Posteriorsi analysis of technical resource of complex electrotechnical systems

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Abstract. In this paper, we consider a probabilistic mathematical model for estimating the state of the traction motor of a trolleybus. The operation of electric motors in transport is inevitably associated with a gradual wear and tear and the need for periodic repairs. For the effective construction of systems of preventive measures, control, testing, current and major repairs, the importance of the causes of the failure of electric motors is necessary.

1. Introduction
The operation of electric motors in transport is inevitably associated with a gradual wear and tear and the need for periodic repairs. For the effective construction of systems of preventive measures, control, testing, current and major repairs, the importance of the causes of the failure of electric motors is necessary.

The growing share of electric motors that have exhausted their regulatory life of work contributes to the growth of failures. The need to predict the destruction of elements, assessing the risk of exploitation in conditions of incomplete information about the quality and condition of the equipment is a constant factor [1].

In the process, operation of the trolleybus under the influence arising in the course of maintenance of traction electric motor (TEM) continuously deteriorates, its reliability decreases and the number of failures increases.

The required level of reliability of the TEM can be maintained only if it is systematically monitored and diagnosed for its technical condition and timely technical service (TS).

The reliability of mechanical and electrical equipment of vehicles was widespread in the automotive industry, aviation, railway transport, agricultural machinery. However, it follows from the patent information search that the reliability of the TEM of the trolleybus has been studied little and it is necessary to continue work in this direction.

At the same time, experience in operating trolleybuses shows that the costs of maintaining (restoring) reliability are 3 to 6 times higher than the costs of their creation. One of the significant factors affecting the technical condition of the trolleybus is the imperfection of the TS system currently in use.

For technical inspection and repair (maintenance and repair) of the trolleybus, up to 75% of all depot facilities are spent, and the costs for TS and R of the traction motor of the trolleybus are about
60% of the total cost of maintenance. Considering the fact that the actual rolling stock is worn out by more than 70%, the problems of ensuring the reliability of the EE in the process of operation and determining the actual technical condition and its prediction are top priorities.

2. Formulation of the problem

There are known mathematical methods for modeling the state of objects: graphical (using probabilistic papers and nomograms) and analytical (the maximum likelihood method, the method of moments, quantiles, tabular, Boolean algebras, probabilistic-statistical, modeling by the Markov process) [3, 4]. Modeling by the Markov process is one of the fundamental methods, which has drawbacks. The most important disadvantages are the rigid exponentially of the distribution laws of a random variable and the fact that the elements of the system can only be in two states (workable and inoperative). There are known mathematical methods for modeling the state of objects: graphical (using probabilistic papers and nomograms) and analytical (the maximum likelihood method, the method of moments, quantiles, tabular, Boolean algebras, probabilistic-statistical, modeling by the Markov process) [3, 4, 6]. Modeling by the Markov process is one of the fundamental methods, which has drawbacks - the rigid exponentiality of the distribution laws of a random variable and the fact that the elements of the system can only be in two states (workable and inoperative).

For the simulation of the TEM state, the most probable statistical method is the one used as the basis for the model of the technical state of the trolleybus traction motor [2].

The determination of the numerical characteristics of the statistical series is shown below.

For each case of failure, electric rolling stock (ERS) runs were recorded since the last repair. The obtained data on the failures of the trolleybus engine are reduced to ordered statistical series. Such series for TEM faults are given in Tab. 1. The grouping step was taken $\Delta L = 5 \cdot 10^3$ km.

For all statistical series, the following numerical characteristics characterizing a sample of a random variable were determined.

3. Theory

1. Mathematical expectation of mileages:

$$L_o = \frac{\sum_{i=1}^{k} L_i \cdot m_i}{\sum_{i=1}^{k} m_i},$$

where $L_i$ - mileage $i$-th discharge, km; $m_i$ number of failures in $i$-th discharge; $k$ - number of discharges.

| Denomination of the failed node | The mileage intervals of the mobile unit $\Delta L$, thous. km |
|---------------------------------|----------------------------------------------------------|
|                                 | 0-15 | 15-30 | 30-45 | 45-60 |
| Collector, armature of the TEM  | 3    | 5     | 2     | 1     |
| Windings of the TEM             | 1    | 2     | 2     | 1     |
| Brush assembly of the TEM       | 1    | 2     | 2     | 1     |
| Insulation Resistance           | 1    | 2     | 2     | 1     |
2. Dispersion of the scattering of ranges:

\[ D = \sigma^2 = \frac{\sum_{i=1}^{k} (L_i - L_o)^2 \cdot m_i}{\sum_{i=1}^{k} m_i}. \]  

(2)

3. Mean square deviation of ranges or scattering:

\[ \sigma = \sqrt{D} = \sqrt{\frac{\sum_{i=1}^{k} (L_i - L_o)^2 \cdot m_i}{\sum_{i=1}^{k} m_i}}. \]  

(3)

4. The coefficient of variation:

\[ V = \frac{\sigma}{L_o}. \]  

(4)

**Table 2.** Results of calculations of numerical characteristics of the problems for the investigated of ‘ZIU’ trolleybuses

| Denomination of the failed node                  | Numeric characteristics |
|-----------------------------------------------|-------------------------|
| Collector, armature of the TEM                 | \( L_o \)   | \( D \) | \( \sigma \) | \( V \) |
| Collector, armature of the TEM                 | 31.875        | 221.484 | 14.882        | 0.467 |
| Windings of the TEM                            | 22.354        | 92.332  | 9.601         | 0.429 |
| Brush assembly of the TEM                      | 18.358        | 66.292  | 8.142         | 0.522 |
| Insulation Resistance                          | 19.813        | 80.335  | 8.963         | 0.471 |

For a justified solution of theoretical and practical problems of reliability, its current monitoring and forecasting for the TEM of a trolleybus, it is necessary to know the distribution laws of the initial random variables. However, almost exact knowledge of these laws is possible only if there is a sufficiently large statistical material on equipment failures [10].

Obtaining as a result of the experiment a statistical material about a random variable in the form of a sufficiently large number of experiments, it is necessary to process it. Thus, from \( n \) of values of independent quantities \( x_i \) of the studied quantity \( x \), called a statistical sample or a statistical series of the volume \( n \), can determine the analytical form of the unknown probability density and the distribution function.

It is necessary to solve the problem of mathematical statistics [7, 8, 11], which consists in smoothing (aligning) statistical data by choosing comparatively simple analytic functions \( \varphi(x) \) for estimation \( f(x) \):

\[ \varphi(x) \approx f(x). \]  

(5)

For assess the likelihood of this approximate probability equality, the criteria for the agreement of the hypotheses under test with respect to the type of functions \( \varphi(x) \) and \( f(x) \).

As the basic criterions, we adopted criterion \( \chi^2 \) of Pirson and criterion of Kolmogorov [8].

The criterion of consent of N.A. Kolmogorov distinguished by simplicity and determined by the relation:
\[ \gamma_1 = P\left\{ \Delta = D_n \cdot \sqrt{n} \geq \lambda \right\}. \] (6)

**Figure 1.** Probability \( a \) – failure \( W(L) \); \( b \) – troubleproof operation \( P(L) \) of the collector traction motor of ‘ziu’ trolleybus.
Figure 2. Probability trouble proof operation \( P(L) \): brushes of TEM.

The application of the Kolmogorov criterion is limited to the requirement of preliminary (a priori) knowledge of the parameters for \( F(x) \), meanwhile, in practice the problem of statistical estimation of unknown parameters is most often posed.

This criterion \( \chi^2 \) of Pearson's consent is free from this shortcoming. As a measure of the discrepancy for this criterion, the value of:

\[
\Delta = \chi^2 = \sum_{i=1}^{k} \frac{(\Delta n_i^* - \Delta n_i)^2}{\Delta n_i} 
\]

where \( \Delta n_i^* \) – the experimental number of realizations of the statistical series, grouping \( i \)-th interval; \( \Delta n_i \) – the theoretical (expected) number of realizations under the assumption that the unknown probability density is described by the chosen function \( f(x) \).

As a result of the implementation of the above interpolation methods using programs developed by the author and analyzing the convergence of functions, a universal analytic function was chosen with the help of which it was possible to smooth out the experimental data and obtain the characteristics of failures \( W(L) \) and troubleproof operation \( P(L) \) for each type of electrical equipment of the trolleybus. In detail, the method of selecting a smoothing function for one node is shown in Fig. 1. The universal analytic function has a form:

\[
\psi(L) = \frac{\xi_1 - \xi_2}{(L-L_0)} + \xi_2. 
\]

4. Experimental results

The results of calculations of the numerical characteristics of the ranges for the samples studied are presented in Table. II, from which it is possible to determine an important characteristic of the failure of the electrical equipment of the trolleybus, when the maximum number of its failures will be
observed.

The mathematical expectation of the run \( L_0 \) characterizes the mileage of a unit of ERS when the number of equipment failures is maximized. Scattering \( \sigma \) and the coefficient of variation indicate a possible range of ranges from their expectation.

Proposed to estimate the relative reliability characteristic of the traction motor as the main term of its reliability and to determine it through the indicator that characterizes the number of failures of the engine equipment per unit of run, that is, through the failure flow \( W' \).

For determination the relative characteristics of the reliability of the TEM trolleybus, the following numerical characteristics were determined characterizing the sampling of a random amount of equipment failures:

1. Mathematical expectation of failures:
   \[
   W_o = \frac{\sum_{i=1}^{k} L_i \cdot m_i}{\sum_{i=1}^{k} L_i},
   \]
   where \( L_i \) – mileage in \( i \)-th interval, km; \( m_i \) – number of failures in \( i \)-th interval; \( k \) – number of interval.

2. Dispersion failure scattering:
   \[
   D = \sigma^2 = \frac{\sum_{i=1}^{k} (m_i - W_o)^2 \cdot L_i}{\sum_{i=1}^{k} L_i}.
   \]

**Table 3.** Results of calculation of the numerical fault characteristics for investigated selections TEM of ‘ziu’ trolleybuses

| Denomination of the failed node | Numeric characteristics | \( W_o \) | \( W'_o \) | \( D \) | \( \sigma \) | \( V \) |
|---------------------------------|-------------------------|----------|---------|-----|-----|-----|
| Collector, armature of the TEM  |                        | 2.242    | 0.0344  | 1.656 | 1.287 | 0.574 |
| Windings of the TEM             |                        | 1.931    | 0.0292  | 1.321 | 1.149 | 0.595 |
| Brush assembly of the TEM       |                        | 1.626    | 0.0251  | 1.047 | 1.023 | 0.629 |
| Insulation Resistance           |                        | 1.626    | 0.0251  | 1.047 | 1.023 | 0.629 |

**Table 4.** Coefficients and numerical characteristics of smoothing functions TEM of ‘ziu’ trolleybuses

| Denomination of the failed node | Coefficient and numeric characteristics | \( \Delta L \) | \( \pm \sigma \) | \( k \) | \( \chi^2 \) |
|---------------------------------|-----------------------------------------|------|--------|------|------|

\( \xi_1, \xi_2, L_o, \Delta L \)
Collector and anchor of the TEM  
-0.05189, 0.01983, 0.988  
1.07877, 0.02601, 0.0016  
36.7195, 0.60945, 0.00197  
11.78097, 0.71925, 0.0019

Windings of the TEM  
-0.21321, 0.09377, 0.923  
1.32577, 0.03989, 0.0019

Brush assembly of the TEM  
-0.20721, 0.04562, 0.991  
1.39359, 0.08456, 0.0011

Insulation Resistance  
-1099.6672, 40.835642, 0.988  
0.6535002, 0.0711454, 0.0026

3. Mean square deviation of failures or scattering of failures:

\[
\sigma = \sqrt{D} = \sqrt{\frac{\sum_{i=1}^{k} (m_i - W_0)^2 \cdot L_i}{\sum_{i=1}^{k} L_i}}.
\]

4. The coefficient of variation:

\[
V = \frac{\sigma}{L_0}.
\]

5. The discussion of the results

From Table III, it is possible to determine the expected maximum number of failures of the trolleybus TEM equipment by the grouping interval. Knowing the magnitude of the run, it is not difficult to calculate the maximum number of failures per 1000 km of mileage. The mathematical expectation of failures \( W_0 \) determines the maximum number of failures per 1000 km. Scattering \( \sigma \) and the coefficient of variation \( V \) indicate a possible spread of the failure parameter from their expectation.

6. Conclusions

As a result of the statistical analysis, the degree of damage to the elements of the electric motor is determined, which is an important parameter for assessing the reliability of the TEM of a trolleybus.

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