Reduction of vibration and noise pollution from agricultural tractor engine using novel pine oil and soapnut oil methyl ester as fuel

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Received: 31 December 2021 / Accepted: 2 December 2022 / Published online: 22 December 2022
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Abstract
The exhaust emissions from automotive diesel engines are successfully controlled over the years by adopting different combustion strategies and after treatment devices, whereas the combustion induced vibration and noise are the major pollutant in off-road vehicle engines and yet to be optimized. In the present study, a twin cylinder, Simpson’s S-217 tractor diesel engine was used to evaluate the performance, combustion, vibration, and noise characteristics, using biofuel blends. For this study, the blends of pine oil — soapnut oil biodiesel (P75SNB25), diesel — soapnut oil biodiesel (SNB20) and diesel were used as fuel. The pine oil used in this research was purchased and used in its neat form. The soapnut oil was extracted from the soapnut seeds by cold pressing method and trans-esterified in two stages by using methanol and catalysts. The experimental results revealed that the performance and combustion characteristics of the blend P75SNB25 was superior to diesel and the blend SNB20 was slightly inferior to diesel. For the blend P75SNB25, the amplitude of acceleration with respect to time was reduced by 19.48% and 11.58% at no load and full load conditions respectively, whereas for the blend SNB20, the amplitude of acceleration showed a reduction of 14.27% and 9.46% at no load and full load conditions respectively in comparison with diesel operation. But both the blends P75SNB25 and SNB20 showed a maximum reduction of noise by 2.34% at different engine loads compared to diesel operation.

Keywords Environmental pollution · Noise reduction · Pine oil · Soapnut oil biodiesel · Tractor engines · Vibration

Introduction
Diesel engines also called as self-ignition engines are the most preferred engine type for powering transport, agricultural, construction, and mining vehicles because of its greater thermal efficiency. Due to the exhaustion of conventional fuel resources and increasing greenhouse gas emission to the environment, the efforts are taken place worldwide towards the development of new, renewable, and green fuels as alternative to diesel and new power-trains alternative to internal combustion engines. The refinement of noise, vibration, and harshness are the key targets for the diesel engine powered vehicles in the future as it might have direct impact on the users. Most of the engine researchers investigated the feasibility of using biofuels in the compression ignition engines from the perspective of its performance, combustion and emission, but the long-term negative effects such as engine life and durability of their components while using biofuels are yet to be investigated (Calik 2018). The operating parameters of the engine and the quality of fuel used may lead either erratic or smooth combustion. The erratic combustion inside the combustion chamber results in knocking which leads to vibration (Uludamar et al. 2017). Unwarranted engine vibrations will shrink the lifespan of the engine components and increases the maintenance. However, it is inevitable for the diesel engines to operate without vibration and noise. Noise is caused by the rapid pressure rise in the combustion chamber during combustion and by moving parts.
Hence, the comprehensive analysis is necessary to understand the causes of vibration and noise in the engine in order to avert their generation. Also the effect of using biofuels on engine vibration is essential so as to decide their sustainability. Various factors which causes engine vibration and noise, the impact of fuel characteristics and problems associated with excessive noise and vibration are reported by many researchers.

The effect of injection pressure and the quantity of fuel injected on engine vibration were studied by using Classical Fourier transforms analysis and time–frequency analysis. It was reported that there is a degree of correlation between injection parameters, in-cylinder pressure and vibration signals (Carlucci et al. 2005). The effect of using lemon peel oil biodiesel blends on vibration and noise characteristics at different injection timing, injection pressure, and engine speed are proved to be an excellent damper for the combustion vibration (Ashok et al. 2020).

The effect of higher biodiesel blends with hydrogen addition was investigated in a four stroke, single cylinder diesel engine runs at a constant speed of 1500 rpm. The blends of 50%, 75%, and 100% by volume of Pongamia Pinnata and Tung oil with diesel were used as fuel. The results revealed that the reduction in vibration acceleration by 8.15%, 9.02%, 5.84%, and 8.70% for the blends PP50, PP75, T50, and T75 respectively was achieved with the addition of hydrogen into the intake manifold (Celebi et al. 2017). The engine vibration and acoustic signals were used as a diagnostic tool for monitoring the working of diesel engine and its combustion quality and found a viable correlation to predict indicated mean effective pressure inside the cylinders (Barelli et al. 2009). From the experiments, the greater vibration signal peaks were recorded with an increase in load.

Investigations were carried out to study the influence of waste cooking oil biodiesel blend on the vibration and noise of a twin cylinder diesel engine. Accelerometer and microphone were used to record vibration and noise signals from the engine running on three different blends namely B10, B20, and B40 at the speeds of 2400 rpm to 3600 rpm. For all the blends, the amplitude of vibration and noise increases with the increase of engine speed. The blend B40 is characterized by highest values of accelerometer root mean square (RMS) and lowest noise index at higher load and speed (Chiatti et al. 2016). The effects of using mustard oil biodiesel (MOB) and hydrogen gas mixture on vibration, noise, and emission were studied in a Mitsubishi Canter, 4 cylinder direct injection diesel engine. The use of neat biodiesel resulted significant reduction in engine vibration and noise level due to the better combustion of oxygenated fuel. With the addition of a constant flow rate of 5 lit/min hydrogen into the intake manifold reduced the vibration and noise level further compared to diesel. This is due to the finer operational stability of the engine achieved with easier ignition of fuel (Tuccar 2021). An investigation was carried out in a single cylinder direct injection diesel engine using Jatropha Methyl Ester (JME) biodiesel with 100 ppm concentration of Zinc Oxide (ZnO) Nano particles of 20 and 40 nm sizes along with hydrogen as secondary fuel to study the vibration level. Using Artificial Neural Network, a model was developed to predict RMS velocity. It was concluded that the blends B30JME40 (JME 30%: diesel 70%: ZnO 40) and B20JME40 (JME 20%: diesel 80%: ZnO 40) are best fuel blend with least vibration at all loads (Javed et al. 2016). Similarly lowest level of vibration was observed while testing a single cylinder diesel engine using cottonseed oil methyl ester blend B20 (Saridemir and Agbulut 2022). Another study using cotton seed oil biodiesel blend B20 recorded a maximum drop in amplitude of vibration of about 58.1% at full load condition compared to other loads (Sakharkar et al. 2021). Experimental investigations were carried out on a four cylinder, turbocharged, common rail direct injection diesel engine to study the vibration characteristics using coconut biodiesel- diesel blends at different loads. It was observed that the blend B50 shows a significant reduction in RMS of accelerations than diesel at all loading conditions. A maximum reduction in RMS acceleration was observed as 13.7% with the use of B50 at full load condition compared to diesel (How et al. 2014). The comprehensive literature review concludes that there is still a research scope to study the vibration and noise characteristics of off-road vehicle engines running on biodiesel fuels. In this research work, the effects of biofuel on the engine performance, combustion, vibration, and noise were investigated in an agricultural tractor engine. The blends of pine oil-soapnut oil biodiesel and diesel-soapnut oil biodiesel were tested in the unmodified diesel engine used in agricultural tractors and the results were compared with the standard diesel operation.

Materials and methods

Soapnut oil biodiesel preparation

Soapnut trees are commonly grown at higher altitudes ranging from 200 to 1500 m in tropical and sub-tropical atmosphere territories of India, China, Hawaii, and Florida. There are different varieties of soapnuts or washing nuts grow in several parts of India, from the southern state of Tamil nadu to the northern regions of Rajasthan, and the eastern planes of the Himalayas. Figure 1 shows
the photographic view of Soapnuts, shell, and oil containing kernels.

The pericarp of the soapnut is used as natural detergents to wash fabrics, bathing, and to produce traditional medicines and the seeds remains unutilized. The soapnut seeds which are thrown away by laundry detergent industries after consuming the fruit shells have been identified as promising non-edible oil source for the production of biodiesel. The oil containing seeds were collected for free of cost and the kernels were crushed in cold press to extract soapnut oil. The oil yield of 44.2% by weight of soapnut kernel was achieved, which is competitive to some other nonedible seeds such as soybean, rubber seed, corn etc... (Silva and Chandel 2014). Earlier works on the characterization of soapnut oil reported that their acid value is about 13.4 mg KOH/g in which the conversion of soapnut oil into soapnut oil biodiesel was done by acid catalyst transesterification followed by base catalyst transesterification (Chen et al. 2012). The transesterification was carried out using methanol and soapnut oil at 6: 1 volumetric ratio. The mixture is heated up to 55 °C and 1% weight of anhydrous sulfuric acid is added to the mixture drop-wise. During the reaction time of 60 min, the mixture is stirred using a motorized stirrer at 600 rpm. The product is then moved to a separating funnel to separate unreacted methanol and free fatty acid. The same procedure is repeated for the base catalyzed transesterification for another one hour using methanol and esterified soapnut oil in a molar ratio of 6:1. The reaction temperature of 60 °C which is closer to the boiling point of methanol is selected and KOH concentration of 1% weight of oil was used. After the reaction is completed, the solution was allowed to settle for 24 h. The glycerin settles at the bottom, whereas the biodiesel was separated at the top and washed with warm water. Figure 2 shows the two-stage transesterification of soapnut oil into soapnut oil biodiesel.

**Blend preparation**

In the present work, low viscous pine oil was procured from the market, which is derived from the fresh needles, cones, resins, and twigs of pine tree by steam distillation process. 75% vol. of neat pine oil was blended with 25% vol. of soapnut oil biodiesel to obtain the hybrid biofuel blend P75SNB25. A 20% vol. of soapnut oil biodiesel was blended with 80% vol. of diesel to obtain the blend SNB20. In the present investigation, the optimum blends P75SNB25 (pine oil 75%: biodiesel 25%) and SNB20 (biodiesel 20%: diesel 80%) were used in a twin cylinder
tractor diesel engine to study its vibration and noise characteristics at different loads and the results were compared with diesel fuel operation.

Fuel properties

The physical and chemical properties of test fuels such as density (ASTM D1298), viscosity (ASTM D445), flash point (ASTM D93), calorific value (ASTM D240), and cetane number were experimentally found as per standard. The fuel properties are listed in Table 1, and the nomenclature of test fuels are presented in Table 2. All the measuring instruments were calibrated before taking measurements for its accuracy.

Based on the research, carried out by the authors using pine oil-soapnut oil biodiesel blends and diesel-soapnut oil biodiesel blends, the two optimum blends P75SNB25 and SNB20 were derived. From Table 2, it was noted that the heating value of P75SNB25 and the cetane number of SNB20 were highly competitive to diesel which enhances better performance and combustion (Venkatesan and Nal-lusamy 2020; Venkatesan et al. 2020).

Experimental setup and measurements

A Simpson’s S217 twin-cylinder, water cooled direct injection diesel engine was used for the investigation. The rated power of the test engine is 15 kW at 1500 rpm. An eddy current dynamometer of (Make & model: Accurate test equipments—E50) is coupled with the engine for loading. The specifications of research engine, testing equipment, and measuring instruments are tabulated (Table 3).

The engine is instrumented with a tri-axial accelerometer transducer to measure the vibration signals. The accelerometer transducer (Make: Dytran 3053B) is mounted over the engine block using adhesive materials to measure the vibration acceleration along the axis of crank shaft (X), the transverse axis (Y) and along the cylinder axis (Z). The transducer incorporates quartz sensing elements and packaged in light-weight titanium housing. Voltage signals were modulated by charge amplifier (DEWE-43A).

The experimental setup for the test engine is shown in Fig. 3. An USB data acquisition system which uses the system software (DEWE soft) processes the input signals and generates time domain signals. Vibrations of time domains signals were converted in to frequency domain by Fast Fourier Transform (FFT). A microphone is kept at a distance of one meter from the engine to obtain more accurate noise levels with the help of Dewe software.

Experimental procedure

In this study, the performance, combustion, vibration, and acoustic characteristics were investigated in order to explore the effect of diesel (D100), P75SNB25, and SNB20. In order to bring the steady state in engine, the test engine was allowed to run for 20 min. Experiments were conducted at a rated speed of 1500 rpm under 0%, 25%, 50%, 75%, and 100% loading conditions to obtain engine performance, combustion, vibration, and noise data. From the observed values of engine load, speed, and fuel consumption, the performance parameters like brake thermal efficiency (BTE) and brake specific fuel consumption (BSFC) were calculated. The combustion characteristics like cylinder pressure

| Table 1 Properties of test fuels |
|----------------------------------|
| Test fuels | Density at 15 ºC (kg/m³) | Viscosity at 40 ºC (mm²/s) | Flash point (ºC) | Calorific value (kJ/kg) | Cetane number |
|----------------|-----------------------------|----------------------------|-----------------|------------------------|--------------|
| Standard diesel (D100) | 832                         | 3.42                       | 52              | 40,290                 | 53           |
| P100           | 847                         | 1.2                        | 36              | 41,848                 | 22           |
| SNB100         | 868                         | 3.60                       | 158             | 37,723                 | 56           |
| P75SNB25       | 851                         | 1.8                        | 67              | 40,816                 | 30           |
| SNB20          | 839                         | 3.46                       | 73              | 39,776                 | 53           |
| ASTM standard  | ASTM D1298                  | ASTM D445                  | ASTM D93        | ASTM D240              | -            |

| Table 2 Nomenclature of test fuels |
|-------------------------------------|
| Fuel                               | Diesel (Vol %) | SNB (Vol %) | Pine oil (Vol %) | Resulting fuel |
|-------------------------------------|----------------|-------------|-----------------|----------------|
| Standard diesel (D100)             | 100            | -           | -               | Base fuel       |
| P100                                | -              | -           | 100             | Neat pine oil   |
| SNB100                              | -              | 100         | -               | Neat biodiesel  |
| P75SNB25                            | -              | 25          | 75              | Hybrid biofuel  |
| SNB20                               | 80             | 20          | -               | Biodiesel blend |
and heat release rate were obtained by using the data acquisition system and Engine Performance Analyzer EPA 1.0.1.

Vibration data was obtained by using a tri-axial, 8 channel accelerometer transducer and the collected data was analyzed by the data acquisition system which provides time domain signals and frequency domain signals using FFT. The engine noise was measured by Dewesoft sound level meter (SLM) which consists of a microphone, a preamplifier, signal processor, and a display. The microphone converts the sound signal to an equivalent electrical signal. This low level electrical signal is amplified to stronger signals and processed by the signal processor. The Dewesoft SLM supports ISO 9614–2 sound intensity scanning method. The sound pressure generated in the engine relative to a reference value is measured in decibels (dB). Error analysis was carried out to find out the uncertainty of

![Diagram of the test engine setup](image-url)

**Table 3** Specifications of the testing equipment/instruments

| Test engine | Make & Model | Simpson’s S217 tractor engine |
|-------------|--------------|-------------------------------|
| Type        | Water cooled, DI diesel engine |
| No of cylinders | 2          |
| Bore X stroke | 91.44 X 127 mm |
| Con. rod length | 232 mm      |
| Compression ratio | 18.5: 1    |
| Cubic capacity | 1670 C.C    |
| Rated power | 15 kW at 1500 rpm |
| Fuel pump   | Mico-Bosch Inline pump |
| Spray hole diameter | 0.263 mm |
| Start of injection | 23° bTDC   |
| Injection pressure | 200 bar   |
| Mass emission | TREM III A |

| Eddy current dynamometer | Make | Accurate test equipments and engineers |
|--------------------------|------|--------------------------------------|
| Model                    | E 50 |
| Maximum Power            | 75 kW @ 3000 to 6000 rpm |
| Maximum Torque           | 234 N-m @ 1500 to 3000 rpm |
| Accuracy                 | +0.25% of Max. Dyno. torque |

| Accelerometer transducer (Dytran 3053B) | Sensitivity | 1.02 mV/m/s² |
|----------------------------------------|------------|-------------|
| Range                                  | 4905 m/s² |
| Connector                              | 4 pin, ¼-28 radial |
| Weight                                 | 7.5 gms |
| Operating temp                         | 51 to 121 °C |

| Data acquisition system (DEWE 43A) | Make | KISTLER, Switzerland |
|-----------------------------------|------|-----------------------|
| No of channels                    | 8    |
| ADC type                          | 24 bit sigma-delta |
| Sampling rate                     | Simultaneous 200 kS/s |
| Input type                        | Differential |

**Fig. 3** Experimental setup of the test engine
various parameters like specific fuel consumption, brake power, brake thermal efficiency, cylinder pressure, exhaust gas temperature, vibration, and noise. Table 4 gives the instruments used in the present study and their uncertainties. The total uncertainty of the present experiment was calculated using the formula derived by Holman (2012) and found to be 1.47%.

### Results and discussion

The results of different fuel combinations of diesel-soapnut oil methyl esters SNB10 (biodiesel 10%: diesel 90%), SNB20 (biodiesel 20%: diesel 80%), SNB30 (biodiesel 30%: diesel 70%), the hybrid biofuel blends with different proportions of pine oil and soapnut oil methyl ester namely P25SNB75 (pine oil 25%: biodiesel 75%), P50SNB50 (pine oil 50%: biodiesel 50%) and P75SNB25 (pine oil 75%: biodiesel 25%) were presented and the percentage variations in performance and emission parameters with respect to diesel at different loads are shown in Fig. 4 (Venkatesan and Nal-lusamy 2020; Venkatesan et al. 2020).

It is observed that the diesel- biodiesel blend SNB20 and pine oil-soapnut oil biodiesel blend P75SNB25 were proved to be the optimum blend combinations which offered improved performance and reduced exhaust emission except NOx. Hence in this research, the optimum blends SNB20 and P75SNB25 were selected and their combustion, performance, vibration, and noise characteristics were tested and the results are discussed.

### Performance analysis

Brake thermal efficiency (BTE) and brake specific fuel consumption (BSFC) for the blends D100, P75SNB25, and SNB20 for various loads are shown in Fig. 5. The combustion characteristics of soapnut oil biodiesel were enhanced by blending it with low viscous pine oil. Due to high volatility and low viscosity of pine oil and the resulting blend, atomization and vaporization are improved (Balasubramanian et al. 2022). The magnitude of BTE for D100, P75SNB25, and SNB20 at full load was recorded as 30.48%, 31.52%, and 29.22% respectively. From Fig. 5, it is observed that, for the blend P75SNB25, there is an enhancement in brake thermal efficiency at all loads and particularly 3.50% enhancement at full load compared to diesel. The use of blend P75SNB25 resulted with the increase in brake thermal efficiency at all loads and especially. The heating value of P75SNB25 is found as 40,816 kJ/kg and is higher than that of diesel (40,290 kJ/kg). This results in lower specific fuel consumption and higher brake thermal efficiency for the blend at all loads (Venkatesan et al. 2021).

The reduction in BTE by 3.3% and increase in BSFC by 1.35% was noted for the blend SNB20 at full load compared to diesel. The increase in BSFC of biodiesel- diesel blend is due to its lower energy content compared with that of the diesel fuel.

### Combustion analysis

The cetane number, viscosity, and oxygen content of the fuels have huge impact on ignition delay, combustion duration, cylinder peak pressure, and heat release rate [Emiroglu and Sen 2018]. These are the most important parameters which affect the engine performance, emission and acoustic characteristics. Generally, the cylinder peak pressure increases with engine load. The variation of cylinder pressure for the test fuels at full load condition at constant engine speed of 1500 rpm is depicted in Fig. 6. From the pressure-crank angle diagram, a highest peak cylinder pressure of 88.6 bar was observed for diesel. The peak cylinder pressure of SNB20 was found to be 84.9 bar which is lower than that of diesel due to the lower heat energy released. For the blend P75SNB25, the peak cylinder pressure was observed as 87.96 bar which is almost closer to diesel due to its lower cetane number, slightly higher heating value, and lower viscosity compared to diesel and SNB20. The heat release rate is an important combustion parameter used to predict the emission.

### Table 4 Uncertainty of the measuring instruments/equipment

| Sl. No | Instrument       | Make          | Type                        | Accuracy | % Uncertainty |
|-------|------------------|---------------|-----------------------------|----------|---------------|
| 1     | Pressure sensor  | Kistler       | Piezo electric sensor       | ±0.5 bar | ±1            |
| 2     | Crank angle encoder | AVL          | Magnetic pickup type        | ±1°      | ±0.2          |
| 3     | Load indicator   | Epoch         | Strain gauge type load cell | ±0.1 kg  | ±0.2          |
| 4     | CO               | AVL 444 digas | NDIR principle             | ±0.02%   | ±0.2          |
| 5     | HC               | AVL 444 digas | NDIR principle             | ±20 ppm  | ±0.2          |
| 6     | CO2              | AVL 444 digas | NDIR principle             | ±0.03%   | ±0.15         |
| 7     | NOx              | AVL 444 digas | NDIR principle             | ±10 ppm  | ±1            |
| 8     | Smoke meter      | AVL           | Hatridge smoke meter       | ±1%      | ±1            |
| 9     | Burette          | Sigma-aldrich | Volumetric measurement of fuel | ±0.1 cm³ | ±1            |
| 10    | Orifice meter    | Malhar        | U tube manometer           | ±1 mm    | ±1            |
Fig. 4  Variations in performance and emission parameters in comparison with diesel at (a) no load, (b) 50% load, and (c) full load
behavior of a fuel. Figure 7 illustrates the variation of heat release rate in relation with crank angle at full load for different test fuels. The maximum heat release rate values are 62.5 J/ºCA, 65.02 J/ºCA, and 58.7 J/ºCA for D100, P75SNB25, and SNB20 respectively. The higher heat release rate was observed for the pine oil blend because of its higher heating value and lower viscosity compared to diesel. The heat release pattern for the biofuel blends is similar to the heat release rate pattern for diesel at full load. The heat release rate was marginally negative during the ignition delay period due to the cooling effect of freshly injected fuel.

Figure 8 shows the variation of exhaust gas temperature (EGT) for D100, P75SNB25, and SNB20 at different loads. For all the test fuels, the EGT increases with increase in engine load. EGT of the biofuel blends is greater than diesel at all loads. The exhaust gas temperature for D100, P75SNB25, and SNB20 was found to be 512 ºC, 514 ºC, and 516 ºC respectively at full load. This increase in EGT is due to the oxygenated nature of the biofuel blends and improved combustion.

Vibration and noise analysis

Combustion induced vibration is considered as one of the major drawback associated with the diesel engine and this can be reduced by use of biofuels. The addition of isobutyl alcohol up to 1% with the biofuel blends has the
ability to control the combustion induced vibration and noise [Jaikumar et al. 2020]. The vibration acceleration is measured in m/s². Engine vibration is an undesirable thing which increased stress on engine parts resulting in wear and noise. The vibration and noise level mainly depends upon the engine operating conditions such as load and
Fig. 10  Frequency vs. acceleration at no load

Fig. 11  Frequency vs. acceleration at full load
speed as a result of moving parts inside the engine (Bharath et al. 2021). Vibration frequency data of up to 10 kHz can be obtained using the present accelerometer. Considering the engine speed of 1500 rpm, one cycle of operation is completed in 0.08 s to produce one power stroke and an acceleration peak. Hence, vibration was obtained (in time domain mode) at the determined sampling frequency of 0.10 s. The number of data within the time period was 1280. Figure 9 shows the total vibration acceleration with respect to time for diesel, P75SNB25, and SNB20 at no load and full load. Figure 10 and Fig. 11 show the total vibration acceleration with respect to frequency for diesel, P75SNB25, and SNB20 at no load and full load condition respectively. The maximum amplitude of acceleration was observed as 19.97 m/s² for diesel at no load (Fig. 9a) and 48.07 m/s² at full load condition (Fig. 9b). Experimental results showed that the biofuel blends generated least vibrations compared to diesel at both no load and full load. For the blend P75SNB25, the amplitude of acceleration was recorded as 16.08 m/s² which is 19.48% lower than diesel at no load condition (Fig. 9c).

Whereas, the amplitude of acceleration for the blend SNB20 was observed as 17.12 m/s² at no load (Fig. 9e) and 43.52 m/s² at full load condition (Fig. 9f) respectively. The reduction in 14.27% and 9.46% was recorded for the blend at no load and full load compared to diesel operation. This reduction is the indication of improved combustion and is due to the higher cetane number of SNB20 which results less tendency of knock. Some other factors responsible for the reduced vibration are advanced injection timing and viscosity pertaining to the biodiesel blends (Taghizadeh et al. 2012; Lakshmi et al. 2022).

At the engine speed of 1500 rpm, one peak value of vibration acceleration occurs for every 25 Hz as the engine combustion frequency is 25 Hz. The total amplitude of acceleration is the sum of combustion shock and valve seating vibrations (Yang et al. 2018). Hence, the vibration acceleration was recorded for a sampling frequency of 500 Hz (20 times of the combustion frequency) by which about 20 combustion peaks can be recorded. Figure 10 and Fig. 11 show the vibration acceleration for the test fuels as a function of frequency at no load and full load condition respectively. For D100, the vibration peak was observed as 0.434 g and 0.651 g at no load and full load condition respectively at the engine combustion frequency of 87.50 Hz. For the blend P75SNB25, the vibration peak was observed as 0.383 g at the combustion frequency of 81.25 Hz in no load condition and 0.727 g at the frequency of 87.50 Hz in full load condition. For the blend SNB20, the vibration peak was observed as 0.446 g and 0.502 g at no load and full load condition respectively at the engine combustion frequency of 87.50 Hz. The blend P75SNB25 offered the lowest vibration peak at no load and the blend SNB20 offered lowest vibration peak at full load compared to diesel. From the results, it was concluded that the shortened ignition delay and decrease in the rate of cylinder pressure rise which resulted in knock free operation are the reasons for this reduction [Siavash et al. 2021].

Among the various sources, combustion noise and piston slap noise account for 80% of total internal combustion engine noise (Ahmadian et al. 2021). These noises most often occur near the top dead center and identified largely in the time–frequency domain. Noise level in the internal combustion engines depends upon the cylinder peak pressure and heat release rate (Ghaderi et al. 2019). In-cylinder pressure generated inside the combustion chamber causes vibrations in the engine block which results in noise to the environment. Figure 12 shows the variation in engine noise level at different loads for the test fuel. The noise level was recorded as 102.41 dB, 101.05 dB and 101.23 dB for D100, P75SNB25, and SNB20 respectively at no load. The noise produced by the engine is proportional to the engine’s vibration and it increases as the engine load increases. The magnitude of noise value for D100, P75SNB25, and SNB20 was recorded as 104.47 dB, 103.18 dB, and 103.90 dB respectively at full load condition. The results revealed that the noise level for the biofuel blends shown a reduction because of the smoother combustion and lower cylinder peak pressure as a result of changes in fuel properties [Zikri et al. 2022].
Conclusions

In this study, the effects of novel hybrid biofuel blend (P75SNB25) and conventional diesel-biodiesel blend (SNB20) on engine performance, combustion, vibration, and noise in a tractor diesel engine were investigated. From the experimental results, it was observed that an increase in BTE by 3.50% for the blend P75SNB25 at full load compared to diesel due to its higher energy content. A decrease in BTE for the blend SNB20 by 3.3% was also observed at full load operation compared to diesel fuel. The exhaust gas temperature for the blends was higher than diesel at all the engine loads as a result of better combustion of oxygenated biofuels. For the blend P75SNB25, the amplitude of acceleration with respect to time was reduced by 19.48% and 11.58% at no load and full load respectively. For the blend SNB20, the amplitude of acceleration showed a reduction by 14.27% and 9.46% at no load and full load respectively compared to diesel. The noise emission of the biofuel blends was decreased up to a maximum of 1.87% at the entire load range compared to baseline diesel. The reduction in vibration and noise is due to the smooth combustion of low viscous, higher energy content pine oil, and improved cetane number of soapnut oil methyl ester. From the experimental investigations, it was concluded that the blends P75SNB25 and SNB20 had shown better results in terms of vibration and noise with the blend P75SNB25 has a slight edge over SNB20 in terms of engine performance and combustion. The hybrid biofuel blend P75SNB25 could eventually replace the use of diesel and serve as a potential alternative fuel for off-road vehicle engines, which contribute a substantial amount of pollution.

Author contribution V. Venkatesan: Initial idea, Sampling, Laboratory activity, Conceptualization, Methodology, Investigation, Interpretation, Writing, Review and Editing. N. Nallusamy: Conceptualization, Interpretation, Review and Editing. P. Nagapandiselvi: Laboratory activity, Investigation, Review and Editing.

Data availability All data generated or analyzed during this study are included in this published article.

Declarations

Ethics approval Not applicable.

Consent to participate All the authors consented to participate in the drafting of this manuscript.

Consent for publication All the authors consented to publish this manuscript.

Competing interests The authors declare no competing interests.

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