Combined Effects of Annealing and Cyclic Loading on Structural Rejuvenation and Mechanical Properties of CuZr Metallic Glass: A Molecular Dynamics Study

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Structural rejuvenation is one of the key topics in the field of metallic glasses (MGs). In this work, we evaluated the combined effects of annealing treatment and elastic cyclic loading to discover pathways for promoting structural rejuvenation and improving the mechanical properties in the MGs. Using molecular dynamics (MD) simulations, it was revealed that the sole cyclic loading led to the increase of rejuvenation degree; however, a saturated state was observed upon the 40th cycle. On the other side, the sample exposed to the combined treatment exhibited a slight relaxation at the first step of cycling process and then a sharp rejuvenation degree was detected in the material. The thorough analyses indicated that the change in the fraction of coordination polyhedrons at the relaxation stage was the main reason for the extra rejuvenation in the sample exposed to the combined treatments. The results also suggest that the combination of rejuvenation treatments improves the magnitude of rejuvenation in the amorphous alloys. It should be noted that the increase of rejuvenation in the alloying systems accompanied with a reduction in the tensile strength and an enhancement in the homogenous plastic deformation.

Keywords: Metallic glass, molecular dynamics, rejuvenation, heterogeneity.

1. Introduction

Owing to the absence of conventional structural defects, bulk metallic glasses (BMGs) show outstanding properties such as excellent compressive strength, extensive elastic limit and high corrosion resistance[1-4]. However, their embrittlement at the room temperature restricts their potential applications in the industries[5-7]. To tackle this problem, it was suggested to excite the atomic structure of glassy alloys, namely rejuvenation, leading to the higher energy state with the better plasticity[8,9]. Several rejuvenating methods have been proposed by researchers to improve the energy state and the ductility of amorphous alloys[10-14]. Among them, external elastic loading without any macroscopic alteration of bulk sample is one of the favored techniques, tuning the mechanical properties and plasticity[15-18]. To provide some examples, Samavatian et al.[19-21] indicated that the tensile elastostatic loading leads to the significant disordering of short- and medium- atomic arrangements and induces the structural rejuvenation in the Zr-based BMGs. Their comprehensive study revealed that the interaction of stress domains under elastostatic loading is the main reason for the sharp variations of internal stresses at the atomic level, inducing the nanoscale heterogeneity in the amorphous alloy. Zhang et al.[22] reported that the elastostatic rejuvenation leads to the bimodal patterns of serration flows and shear bands. Using molecular dynamics (MD) simulation, it was unveiled that the prolonged elastostatic compression below the yield stress is manifested by the irreversible rearrangements of atoms and the increase in the typical size of atomic clusters with large non-affine displacements[23,24]. In another work, it was indicated that a mechanical relaxation-to-rejuvenation transition happens in the elastostatic compression[25]. It was suggested that the de-mixing tendency of the constituent

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atoms is dominated in the rejuvenation stage. Utariarman et al. determined that the pre-elastostatic loading before the cryogenic cycling treatment significantly improves the degree of rejuvenation increment in a Ce-based BMG. Using MD simulation, Chen et al. evaluated the structural features of MGs under the localized complex stress fields (LCSF). They found that the ultimate strength and elastic limits were increased in the LCSFed samples, which was due to the elimination of stress concentrations in the amorphous structure. Moreover, the investigations showed that a gradient rejuvenated amorphous structure increased the homogenous plasticity in the structure under the tensile loading. This event was highlighted when the volume fraction and degree of structural disordering exceeded from a certain value.

The MD simulation of cyclic loading in a CuZr system indicated that the structural rejuvenation is associated with the nucleation and development of shear events in the bulk of Mg. Louzguine-Luzgin et al. demonstrated that the room-temperature cyclic loading up to 0.4% of elastic strain may induce the nanocrystallization in the amorphous material. Employing a kind of cyclic loading, i.e. the ultrasonic vibration, Lou et al. found that the high frequency strain energy is converted into internal energy owing to heterogeneous atomic packing configuration of MGs. The MD simulation also shows that the structural rejuvenation increases effectively with the rise in the cyclic loading number and ultimately reached a saturated regime. Moreover, other works with different treating techniques reported the saturation of structural rejuvenation in the amorphous alloys. Consequently, finding solutions for the enhancement of rejuvenation degree plays a crucial role in the improvement of structural features and plasticity. For this purpose, in this work, we employed the cyclic loading and annealing treatment simultaneously to promote the rejuvenation degree of an Mg alloy and study the atomic structural evolution under the combined effects of treating methods. Using the MD simulation, the details of atomic rearrangement, potential energy landscape and structural heterogeneity are comprehensively discussed.

### 2. Computational Method

The Large-scale Atomic/Molecular Massively Parallel Simulator (LAMMPS) with the embedded atom method potential for CuZr alloys was applied to perform the MD simulations. The favored alloying composition (Cu$_{52}$Zr$_{48}$) for modelling the binary MG was obtained through randomly substitution of copper atoms in a Zr-based crystalline atomic structure. The model respectively has sizes of 6 × 6.5 × 12 nm in the x, y and z directions, while the system includes 17840 atoms. To create the model, the copper atoms were added into the alloying system by replacing the zirconium atoms (52 at. %) were added into the alloying system by replacing the copper atoms. After the initial preparations, the atomic structure of CuZr MG. For the high temperature treatment, the sample was heated to 600 K and kept in this temperature for 1 ns. Afterwards, the cycling loading was carried out and then the sample cooled down to the room temperature and a latter relaxation stage was considered to eliminate any effects of cooling rate. The heating and cooling rates were 10$^{10}$ K/s. Moreover, the high temperature state (600 K) is below the glass transition temperature to avoid any possible crystallization. During the MD simulation of treatments, the pressure and temperature were controlled by the NPT ensemble. The uniaxial tensile loading of the CuZr glassy alloy simulated along the z direction with a constant strain and plasticity in the structure under the tensile loading. It should be noted that the cyclic loading was conducted below the elastic limit and the lateral directions were adjusted to zero bar for observing any possible dimensional changes during the cyclic treatment. As illustrated in Figure 1, the cyclic loading was carried out at the temperature values of 300 K (room temperature) and 600 K to identify the role of temperature, i.e. annealing treatment, on the atomic structure of CuZr MG. For the high temperature treatment, the sample was heated to 600 K and kept in this temperature for 1 ns. Afterwards, the cycling loading was carried out and then the sample cooled down to the room temperature and a latter relaxation stage was considered to eliminate any effects of cooling rate. The heating and cooling rates were 10$^{10}$ K/s. Moreover, the high temperature state (600 K) is below the glass transition temperature to avoid any possible crystallization. During the MD simulation of treatments, the pressure and temperature were controlled by the NPT ensemble. The uniaxial tensile loading of the CuZr glassy alloy simulated along the z direction with a constant strain.

\[
\epsilon_t = \epsilon_0 \sin \left(\frac{2\pi t}{t_w}\right)
\]

Where the values of $t_w$ and $\epsilon_0$ are 0.2 ns and 3%, respectively.

Figure 1. Schematic of stress-strain curves (inset shows the trend of cyclic loading process, conducted at the elastic limit).
rate of $8 \times 10^6$ s$^{-1}$ at 300 K to assess the effects of structural rejuvenation on the mechanical properties. In the simulation, the periodic boundary conditions in the different directions were considered, and the temperature and pressure were controlled by the NPT ensemble.

3. Results and Discussion

At the first step, it is critical to investigate the energy alterations and volume changes, which are indicators of rejuvenation in the amorphous alloys$^{25,40}$. In general, the change in the potential energy of material indicates the stored energy in its atomic configuration. With the increase in potential energy, the nanoscale defects enhance in the system and the disordering event is intensified in the atomic arrangement of MGs$^{41}$. As illustrated in Figure 2, the cyclic loading at 300 K leads to the positive change of potential energy ($\Delta E$) for more than 260 eV, which means that the cyclic treatment induces structural disordering, i.e. rejuvenation, in the CuZr alloy. However, one can see that the $\Delta E$ remained stable above the N=40 and just fluctuated between 245-265 eV. Hence, it is concluded that a saturated energy state happens in the structure.

The degree of volume changes under the cyclic loading was also presented in Figure 2. The trends of bulk volume and potential energy are similar to each other, which indicates that the increase in energy state is accompanied with the generation of free volumes and loosely packed structures in the material$^{25,43}$. Figure 2 also indicates the effects of simultaneous cyclic and annealing (600 K) treatments on the structural rejuvenation of CuZr glassy alloy. Under the 10 cycling number, some volume contraction and $\Delta E$ decrement (~70 eV) were observed, showing the dominant role of high temperature process. On the other side, a sharp increment is detected in both of volume and $\Delta E$ up to the 45 cycling number and then a saturation happens in the structure. The results also demonstrated that the degree of $\Delta E$ increment in the annealing/cyclic treatment is considerably higher than the MG alloy induced by the sole cyclic loading. This event confirmed that the high temperature treatment facilitated the nanoscale structural rearrangement under the cyclic loading.

The induced strain distribution of treated samples gives important information regarding the structural heterogeneity in the atomic configurations. Figure 3 illustrates the snapshots of Von-Mises after the certain number of cyclic loadings.

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**Figure 2.** a) Potential energy variations and b) Volume variations as a function cycle numbers for the samples.

**Figure 3.** The Von Mises strain distribution of sample exposed to a) the sole cyclic loading and b) the annealing-cycling treatment.
As observed, the cyclic loading leads to the introduction of strain into the system. However, one can see that the strain distribution changes when the annealing process comes into play. Under the combined treatment, no significant induced strain was detected at the first number of cycles, which was consistent with the negative variations of potential energy at the first stage. Thereafter, the induced increased in the system with rise in number of cycles. With the detailed observation of snapshots, it was indicated that there existed no accumulated strain regions in the atomic configuration of sample treated by annealing-cycling process. On the other side, some accumulated strains were detected in the sample treated by the sole cycling. In several works, it was unveiled that the increase in the intensification of strained regions in the atomic configuration goes along with the creation of potential sites for the initiation of nanoscale shear events. In the other words, the structural heterogeneity was intensified in the sample treated by the annealing-cycling process, which may lead to the improvement of homogeneous plasticity under an external loading. In the following, the mechanical response and the plasticity behavior of samples under the tensile loading will be discussed.

To better understand the atomic reconfiguration under the cyclic loading, the partial pair distribution function (PDF) analysis was conducted. As presented in Figure 4, the PDF analysis provides information regarding the atomic density distribution as a function of atomic distances. The results showed that the sole cyclic loading leads to the slight shift of Zr-Zr first peak to the lower values, while there is no significant change in the peak height. On the other side, the height of Cu-Cu and Cu-Zr first peaks show the increasing and decreasing trends under the sole cyclic loading, respectively. Hence, it is concluded that the number of Cu-Cu pairs rises under the treatment, while the Cu-Zr pairs tend to be annihilated. Moreover, one can see that the average interatomic distance of Zr-Zr pairs gets constricted; however, their population in the atomic structure remains stable. On the other side, the combination of annealing and cyclic loading treatments leads to the different atomic rearrangement in the amorphous structure. As observed in Figure 4, there is no considerable shift in the Zr-Zr peak; however, the peak intensity shows a slight increment. Moreover, the degree of Cu-Zr annihilation is significantly higher than the sample treated under the sole cyclic loading. One can also see that the population of Cu-Cu exhibited a slight decrement under the combined treatment. This result clearly indicated that the mechanism of rejuvenation in the samples is almost different, so that the sole cyclic loading tends to replace the Cu-Zr pairs with Cu-Cu ones in the first nearest-neighbor shell. On the other side, the sample under the combined treatment induces more Zr-Zr pairs with longer bonding length through the sharp annihilation of Cu-Zr pairs with shorter bonding length. Accordingly, it is suggested that the high temperature treatment significantly alters the type of atomic reconfiguration during the cyclic loading.

Figure 5a illustrates the stress-strain curves of rejuvenated samples under the tensile loading process. As clear in the figure, the tensile plasticity under the evolution of cyclic number is different in the samples, suggesting that the cycle number along with the applied temperature (annealing treatment) play a significant role in the deformation behavior of amorphous alloys. At the low number of cycles, the samples experienced a stress peak accompanied with a sharp decrement, which is a sign of strain localization under the tensile loading (See Figure 5b). This prompt strain localization is the main reason for the lower plasticity of untreated and low-cycled samples in comparison with the samples rejuvenated with the high number of cycles. Hence, the results showed that the increase in the number of cyclic numbers improves the plasticity and postpones the nanoscale shear localization in the amorphous structure. However, one should notice that the aspect ratio and the sample size in the MD simulation act as the crucial roles in the plasticity behavior of MGs. As depicted by Sopu et al., the decrease of specimen size to the nanoscale regime, the strain softening is extended in the structure and the failure is deferred in the system. Moreover, it was found that the low aspect ratio inhibits the catastrophic failure under the tension mode, especially in the rejuvenated structures with high potential sites for the formation of nanoscale shear events. Hence, it is concluded that the significant homogeneous plastic deformation in the high-cycled samples may be related to the features of MD simulation.

Figure 5b demonstrated the strain snapshots of selected regions in the stress-strain curves of samples. As can be seen, the cyclic loading significantly affects the strain distribution in the loaded samples. To provide some examples, the strain snapshots are presented for the samples exposed to the 10, 20 and 30 cycles at the same stress values. According to the marked points in the stress-strain curves, the total induced strain in these samples are ~ 11%, 14% and 18%, respectively. However, the snapshots show that the strain distribution is different. In the sample loaded with 10 cycles, a shear localization along with a necking event occurred in the
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system, which is manifested in the sharp stress decrement in the stress-strain curve. On the other side, the strain distribution is less localized in the samples loaded by 20 and 30 cycles, suggesting the evolution of structural rejuvenation under the sole cyclic loading. The stress-strain curves also showed that the combination of annealing treatment and cyclic loading significantly improves the plasticity in the material, so that for the samples exposed to the 40 and 50 loading cycles, there is no sign of stress drop in the curves. This means that the plasticity mechanism in the samples can transform from a localized shear event to a homogenous plastic deformation. The stress-strain curves also confirmed that the induced strain was homogenously distributed in the structure, inhibiting any immediate localized event during the tensile deformation. This phenomenon is due to the increase of structural heterogeneity under the rejuvenation process. In general, the structural rejuvenation induces more defects such as free volumes in the structure leading to a pronounced nanoscale heterogeneity with numerous potential sites for the shear events. Consequently, the catastrophic failure by the localized deformation is replaced with the stable plastic flow in the rejuvenated sample.

To better understand the rejuvenation mechanism, it is necessary to interpret the energy state based on the potential energy landscape (PEL). Figure 6 illustrates the evolution of energy state under the sole cyclic loading and its combination with the annealing process. As can be seen, it is possible to describe the evolution of atomic rearrangement based on the local barrier energies. In general, the local atomic movement under an external excitation comprises two main energy stages, called the activation step ($E_{\text{act}}$) and relaxation step ($E_{\text{rel}}$). With this definition, when the total energy of activation becomes bigger than the relaxation energy, the structural rejuvenation happens in the material. Consequently, the catastrophic failure by the localized deformation is replaced with the stable plastic flow in the rejuvenated sample.

occurs, which means that the fluctuation of activation and relaxation stages remained stable after a certain number of cycle numbers. On the other side, in the sample treated by the annealing and cycling processes, a relaxation trend in the energy state was detected at the first cycling numbers and then the sharp activation events come into play from 10 to 40–45 cycle numbers. Agreeing with Figure 2, one can conclude that the annealing event provides conditions for facilitating the atomic rearrangement in the structure. Under the first relaxation event at low cycling numbers, the potential sites were produced to induce the Zr-Zr pairs under the rejuvenation and significantly annihilate the Cu-Zr pairs, as shown in Figure 4. Consequently, it is suggested that the creation of more Zr-Zr atomic pairs under the combined treatment is the main reason for the sharp activation events in the rejuvenation of CuZr alloy.

For detailed characterization of atomic structure under the rejuvenation process, the coordination polyhedron study...
was conducted in accordance with the Voronoi tessellation. Totally, the Voronoi index is indicative of characteristics in a coordinated component, in which the number of n-edged faces of a Voronoi polyhedron, \(<i_1, i_2, i_3, i_4, i_5>\), is introduced\(^9\). As given in Figure 7a, the fraction of Voronoi polyhedron strongly depends on the evolution of rejuvenation/relaxation in the amorphous structure. The Cu-centered clusters are favored in the CuZr MGs\(^1\), which means that the sum of coordination polyhedron comprises the backbone and main ordered structure of amorphous alloy. According to the results, the fraction of ordered structure gradually decreases in the sample exposed to the sole cyclic process and then a steady state upon the 40\(^{th}\) cycle number. On the other side, the sample exposed to the combined treatment shows a slight increment at the first stage of cyclic loading and then experiences a moderate decline of ordered structure, which is correlated to the structural rejuvenation. Figure 7b reveals the normalized fraction of main coordination polyhedrons versus the cycle numbers for both samples.

As plotted in Figure 7b, the backbone of samples is dominated by the polyhedrons with indices of \(<0, 2, 8, 1>\) and \(<0, 0, 12, 0>\). However, the fraction of polyhedrons is significantly affected under the evolution of treatment. As reported in Figure 2a, the potential energy decreases at the first stage (5-10 cycles) of annealing-cycling treatment in the sample, which shows a slight relaxation in the system. The Voronoi analysis indicated that the relaxation stage goes along with the sharp rise of polyhedron \(<0, 0, 12, 0>\) in the structure, leading to the decrease of potential energy of amorphous structure. After this stage, the rejuvenation proceeds with the sharp rise of \(<0, 3, 6, 3>\) and the moderate decrement of \(<0, 2, 8, 1>\) and \(<0, 0, 12, 0>\) in the material. This event is far different from what happened in the sample exposed to the sole cycling process, in which a gradual increment in fractions of \(<0, 2, 8, 2>\) and \(<0, 3, 6, 3>\) occurs under the rejuvenation. Consequently, it is suggested that the primary increase of \(<0, 0, 12, 0>\) icosahedral coordination structure in the system would be the main reason for the sharp rejuvenation of CuZr MGs under the combined effects of annealing and cycling processes.

4. Conclusions

This work aims to show the role of combined treatments on the magnitude of rejuvenation in the MGs. For this purpose, MD simulation was used to model the CuZr MG under the sole and simultaneous application of annealing and cyclic loading. The results indicated the evolution of rejuvenation in the amorphous structure strongly depends on the type of treatment. Under the sole cyclic treatment, the rejuvenation degree gradually increases and reaches a saturated state after the 40\(^{th}\) cycle. On the other side, for the sample exposed to the combined treatment, a relaxation event was observed at the first steps and then a sharp increment of rejuvenation occurs with the advance of cycling loading. The results demonstrated that the alterations in the population of polyhedrons at the relaxation stage is the main reason for the change in the rejuvenation degree in the CuZr MG.

5. References

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