Effects of Shoal Margin Collapses on the Morphodynamics of a Sandy Estuary

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Abstract. Shoal margin collapses of several million cubic meters have occurred in the Western Scheldt estuary, the Netherlands, on average five times a year over the last decades. While these collapses involve significant volumes of material, their effect on the channel-shoal morphology is unknown. We hypothesize that collapses dynamicize the channel-shoal interactions, which could impact the ecological functioning, flood safety, and navigation in the estuary. The objective is to investigate how locations, probability, type, and volume of shoal margin collapse affect the channel-shoal dynamics. We implemented an empirically validated parameterization for shoal margin collapses and tested its effect on simulated estuary morphological development in a Delft3D schematization of the Western Scheldt. Three sets of scenarios were analyzed for near-field and far-field effects on flow pattern and channel-shoal morphology: (1) an observed shoal margin collapse of 2014, (2) initial large collapses on 10 locations, and (3) continuous collapses predicted by our novel probabilistic model over a time span of decades. Results show that a single shoal margin collapse only affects the local dynamics in the longitudinal flow direction and damps out within a year for typical volumes, whereas larger disturbances that reach the seaward or landward sill at tidal channel junctions grow. The direction of the strongest tidally averaged flow determined the redistribution of the collapsed sediment. We conclude that adding the process of shoal margin collapses increases the channel-shoal interactions and that in intensively dredged estuaries shoal margins oversteepen, amplifying the number of collapses, but because of dredging the natural morphological response is interrupted.

1. Introduction

The process of channel bank failure and collapses of shoal margins has been recognized in estuaries and rivers around the world (Beinssen et al., 2014; Coleman, 1969; Dunbar et al., 1999; Laury, 1971; Silvis & De Groot, 1995; Torrey, 1995; Van den Berg et al., 2002), but their effect on long-term morphological development remains unknown. The implementation of channel bank failure in numerical morphodynamic models has been studied more recently (Kleinhans, 2010; Nicholas, 2013a; Schuurman et al., 2013) but focused on outer cut bank erosion in rivers. Though, channel banks can also collapse at the inner bank of rivers (Nieuwboer, 2012), collapses of shoal margins are more often observed at the inner side of a bend in estuaries (Mastbergen & Van den Berg, 2003; Van Dijk, Mastbergen, et al., 2018; Wilderom, 1972). Because of the relatively large volume of up to several million cubic meters that is involved, the associated displaced sediment in the channel perturbs the sediment transport, affecting channel geometry, for example, the width-depth ratio and channel dynamics. We hypothesize that such morphological perturbations within the system may amplify the sediment transport in estuaries as much as extreme events imposed in the boundary conditions, indirectly affecting the morphological changes. This is important because morphological models of estuaries invariably evolve toward bar-scale equilibrium (Dam, 2017; Van der Wegen & Roelvink, 2012). This means that the channel-shoal dynamics are presently underpredicted because of internal dynamics and disturbances, such as collapses, are not captured in the model.

Effects of disturbances and perturbations on morphology in rivers and estuaries have been studied in the past century. The damping and lag associated with environmental disturbances propagating through a system are determined by the magnitude and timescale of the event (Paola et al., 1992; Whipple &
Shoal margin collapses often occur suddenly, which makes them difficult to predict in current numerical morphodynamic models, such as Delft3D. Shoal margin collapses occur at sufficiently high and steep slopes, but there is a difference in the sediment properties between the two types of flow slides, known as liquefaction and breaching (Van den Ham et al., 2014). Liquefaction requires loosely packed, nonlithified, and water-saturated sand or silt, whereas breaching requires the presence of a sufficiently large body of densely packed fine sand or silt (Van den Ham et al., 2014). These short-term processes have been represented by various models but not implemented in a numerical morphodynamic model. Van den Ham et al. (2014) argued that these theoretical liquefaction and breaching models quantify the relative influences of channel geometry and soil parameters, but the reliability of the estimated probability remains limited. Thus, Van den Ham et al. (2014) proposed a semiempirical model that predicts the probability of shoal margin collapses on profiles, which was modified and extended for application on spatial bathymetry data by Van Dijk, Mastbergen, et al. (2018). This predictor includes an empirical factor based on the frequency of historical flow slides in the Eastern Scheldt and Western Scheldt estuaries (Van Dijk, Mastbergen, et al., 2018; Wilderom, 1979), which is applied in this study instead of the full process-based modeling of flow slides.

Our objective is to increase understanding of the interactions between shoal margin collapses and the channel dynamics of a sandy estuary, the relevant timescales, and the large-scale morphological effects. The posed research questions are the following: (i) What are the local (near-field) effects of individual shoal margin collapses, such as the observed 2014 shoal margin collapse? (ii) How do multiple shoal margin collapses affect the channel dynamics of the estuary (far-field effect)? Our method was to use the numerical morphodynamic model Delft3D and implement an effective parametrization for the process of shoal margin collapses in a calibrated model. We then tested how disturbances, such as multiple collapses, propagate and change the channel-shoal interactions of the Western Scheldt, a sandy estuary. In this paper, we first give a detailed description of the study area, the method for implementation of the shoal margin collapses in Delft3D and the tested scenarios. Then, we present the near-field and far-field effects of shoal margin collapses.
collapses on the short-term as well as the long-term morphodynamics of the Western Scheldt. Finally, we discuss the model performance and the implications of persistent perturbations on a sandy estuary.

2. Study Area

This study focuses on shoal margin collapses in the Western Scheldt. The Western Scheldt is located in the southwestern part of the Netherlands (51°41’51”N, 5°40’35”E) and is the seaward section (60 km) of the 200-km tide-dominated Scheldt estuary. The Scheldt is a well-studied and monitored estuary (e.g., Bolle et al., 2010; Van der Wegen & Roelvink, 2012; Wang et al., 1999; Winterwerp et al., 2000) that provides access to various harbors, of which the port of Antwerp (Belgium) is the largest. The Western Scheldt is characterized by a convergent geometry and has a well-developed system of channels and shoals (Figure 1a).

Channel bank failures have been recorded systematically in the Western Scheldt for the past 200 years (Wilderom, 1961, 1979). Over the years, bank protection measures have been implemented to protect the channel banks and dikes of the Western Scheldt against new failures and collapses. Yet these measures did not prevent the occurrence of shoal margin collapses (Wilderom, 1972). A recent study identified 300 shoal margin collapses between 1959 and 2015 (Figure 1a; Van Dijk, Mastbergen, et al., 2018), ranging from very small collapsed volumes of 20,000 m³ up to volumes of 3,000,000 m³. The majority of the collapses occur at unprotected areas. The estuary consists of relatively fine sediment, which affects the occurrence of shoal margin collapses (Van den Ham et al., 2014). In general, the $D_{50}$ of the channel bed varies between about 200 and 300 $\mu$m, whereas at the higher elevation areas of the shoals, the sediment size is generally finer than 200 $\mu$m (Cancino & Neves, 1999; De Vriend et al., 2011). Additionally, a significant percentage of mud, up to 25%, is found in the intertidal areas but increases above 25% on the flanks of the estuary (Braat et al., 2017; Van de Lageweg et al., 2018).

The natural development of the morphology, as well as the effect of perturbations, is the result of interactions between water flow, sediment transport, and bed elevation. An important factor causing bidirectional flow and mean sediment transport is the tidal forcing in the Western Scheldt (Wang et al., 1999). From the mouth of the estuary to the Dutch/Belgian border, the tidal range increases from 3.5 to 5 m (Jeuken, 2000). The tidal prism at the mouth is about two billion cubic meters (Wang et al., 1999), whereas the yearly averaged river discharge of the Scheldt into the Western Scheldt is a negligible 120 m³/s (Cancino & Neves, 1999; De Vriend et al., 2011), but peak discharges are observed up to 600 m³/s (Baeyens et al., 1997). The Western Scheldt has several recirculation zones of sediment through the ebb and flood channels, which enclose the intertidal flats (Figure 1b; Wang et al., 1995; Winterwerp et al., 2000). The tidal flow is asymmetric, that is, slower but longer ebb flows compared to flood flows (Figures 1c and 1d). The difference between the maximum flow velocity for ebb and flood illustrated that the flood is generally stronger (Figure 1e) even in the ebb-dominated channels as illustrated by the tidally averaged flow (Figure 1b).

3. Model Description and Methods

3.1. Model Setup and Boundary Conditions

In this study, we used two Delft3D schematizations that are both based on the NeVla-Delft3D model of the Scheldt estuary, which includes the upstream Flemish branches of the estuary, the Western Scheldt, and part of the North Sea. The NeVla model is a state-of-the-art numerical model that has been optimized for hydrodynamics (Maximova, Ides, Vanlede, et al., 2009; Maximova et al., 2009a, 2009b; Vroom et al., 2015) and morphology (Grasmeijer et al., 2013; Schrijvershof & Vroom, 2016). To study the effect of shoal margin collapses, we focused on the Western Scheldt part of the NeVla model. Two nested models were produced from the NeVla-Delft3D model for reducing the computational time.

The first nested model boundaries (model 1) were located around the tidal flat of Walsroorden (see boundaries in Figure 1a), which was used to study the morphodynamic response of the 2014 shoal margin collapses and the sensitivity to collapse sizes, grain-size of the collapsed material, and location of the collapsed deposits. Van Schaick (2015) validated the water level and discharge from the nested model with the NeVla-Delft3D model as well as the response of the 2014 collapse and concluded that the errors were small enough to be neglected for the area of interest.

The second nested model boundaries (model 2) include the Western Scheldt from the mouth at Vlissingen to the Dutch/Belgian border (see seaward boundaries in Figure 1a), which was used for testing the effect of shoal margin collapse locations as well as the effect of multiple shoal margin collapses in the Western Scheldt.
Figure 1. Overview of hydromorphodynamics in the Western Scheldt Estuary. (a) Shoal margin collapse locations plotted on a digital elevation model of January 2014 (Van Dijk, Mastbergen, et al., 2018). Seaward boundaries indicated for the two morphological model schematizations in this study. A–J show locations susceptible to shoal margin collapses that are applied in the model scenario with 10 initial collapses and refer to the locations for Figures 5 and 6. (b) Streamlines of the tidally averaged flow of the original NeVla-Delft3D flow model showing circulation cells that correspond to the macrocells indicated in white defined by Winterwerp et al. (2000) and Bolle et al. (2010). (c) Maximum flow velocity in the ebb direction from the NeVla-Delft3D model. (d) Maximum flow velocity in the flood direction from the NeVla-Delft3D model. (e) Difference (in m/s) between the maximum ebb and maximum flood velocity showing flood dominance in the main channels.

over time. The downstream boundary was chosen at the smallest but deepest part of the Western Scheldt to limit boundary effects. Still, we excluded the seaward effects for further interpretation and conclusions as it was difficult to distinguish the boundary effects from an effect associated to the actual collapses. A single spring-neap-spring cycle shows that the tidally averaged flow of this model (supporting information Figure S4b) is comparable with the outcome of the full NeVla-Delft3D model (Figure 1b), except for a small variation at the seaward end.
The nested model consists of a curvilinear grid with various grid sizes. The boundary conditions include a water level fluctuation due to tides at the seaward boundary and current at the landward boundary. Sediment fraction was uniform, with a median grain size of 200 $\mu$m. For simplification, the boundary conditions were selected from a single spring-neap-spring tide cycle of January 2013 (about 14 days) and repeated for a 2-year period. Furthermore, we excluded the wind direction and magnitude from the NeVla model to reduce computational time because the effect of wind is negligible within the Western Scheldt. The roughness field in the model is defined in Manning $n$ and is variable over the model domain (Maximova, Ides, Vanlede, et al., 2009; Maximova et al., 2009a, 2009b; Vroom et al., 2015), which was $0.022 \, s/m^{1/3}$ for the eastern part, $0.027 \, s/m^{1/3}$ for the western part, and $0.028 \, s/m^{1/3}$ for the Verdronken Land van Saeftinghe. The bed consisted of erodible and nonerodible layers (Gruijters et al., 2004), the nonerodible layers formed due to previous deposits that are hardly erodible (Dam, 2013), and so the sediment thickness varies within the Western Scheldt model (Figure S1). Because sediment transport was calculated by Van Rijn, (2007a, 2007b), the bedload and suspended load transport could be separated.

### 3.2. Transverse Bed Slope and Morphological Factor

The Delft3D model (version FLOW 6.01.07.3574, 2 April 2014) has been applied in many scientific projects to compute hydrodynamics, sediment transport, and morphological changes (Crosato & Saleh, 2011; Deltares, 2009; Roelvink, 2006; Schuurman et al., 2013; Schuurman, Kleinhans, et al., 2016; Van der Wegen & Roelvink, 2012; Van Dijk et al., 2014). In this study, we applied a 2-D depth-averaged flow field, which meant that the effect of helical flow driven by flow curvature on bed shear-stress direction was parametrized (Baar, Albernaz, et al., 2018; Baar, De Smit, et al., 2018; Schuurman et al., 2013). The parametrization affected the transverse bed slopes at the shoal margins, which influenced the moment that shoal margin collapses were predicted. We performed a sensitivity analysis to determine how the sediment transport direction affects the slopes for $\alpha_{bn}$ between 1.5 and 100 (see Text S1; Bagnold, 1966; Ikeda, 1982a, 1982b; Van Rijn, 1993). To reduce computational time, Delft3D includes a morphological acceleration factor $M$. Based on a sensitivity analyses (see Text S1), we set $\alpha_{bn}$ to 30 and $M$ to 20 as a default, so that the realistic dimensions of the slopes for long-term simulations were maintained (Figure S2).

### 3.3. Model Scenarios and Sensitivity

We assessed the effect of shoal margin collapses on the morphodynamics of a sandy estuary in three scenarios (see Table 1). We compare each scenario with a control run without collapses, so that natural variation of the morphodynamics by the model could be excluded and check if collapses dynamicize the model.

The first scenario focused on understanding the near-field effect of a single shoal margin collapse, such as the observed 2014 shoal margin collapse at the tidal flat of Walsoorden. The sensitivity of the shoal margin collapse size, location of the collapsed deposits, and grain size of the deposits were studied (see Text S3). The sensitivity scenarios of the size and the location are based on the evaluation of historical collapses by Van Dijk, Mastbergen, et al. (2018). The grain size of the deposited material was varied as the grain-size distribution in the field showed minor variation between 100 $\mu$m on the shoals and 300 $\mu$m in the channel (Mastbergen et al., 2016). The first scenario and sensitivity tests were conducted on only the eastern part of the Western Scheldt (see the seaward boundary of model 1 in Figure 1a).

The second scenario included a model run with initially 10 shoal margin collapses of 1,000,000 m$^3$ located at various locations within the Western Scheldt. Here we tested the far-field effect on the sediment transport.
and channel-shoal dynamics over the long term (40 years). The locations corresponded to observed shoal margin collapse locations as described in Van Dijk, Mastbergen, et al. (2018; Figure 1a).

The third scenario tested the role of multiple shoal margin collapses over a period of 40 years, where multiple collapses occurred within 1 year, hereafter referred to multiple yearly collapses. These collapses were controlled by the implementation of our novel shoal margin collapse rules in a Matlab environment as described in the next section. These last two scenarios were applied on a different nested model (see Table 1), which includes the Western Scheldt from Vlissingen to the Dutch/Belgian border (see the seaward boundary of model 2 in Figure 1a).

3.4. Shoal Margin Collapses

Including the process of shoal margin collapses into a morphodynamic model might be necessary to increase dynamics within the model domain, such as the channel-shoal interactions. Currently, bank erosion is implemented by coupling horizontal bank retreat to bed degradation in Delft3D. Bank erosion occurs between an inundated grid cell and a dry grid cell and thus is not restricted to the outer banks. Incision of the inundated grid cell could be equally divided over both grid cells or solely on the dry cell, so that the dry cell was lowered and the bank eroded (Mastbergen & Schrijvershof, 2016; Schuurman, Shimizu, et al., 2016). This process continues until the grid cell becomes inundated, but shoal margin collapses may occur suddenly at growing shoals that become less inundated.

In this study, shoal margin collapses are enforced based on the historical evaluation of collapses in the Western Scheldt and the adapted forecasting method by Van Dijk, Mastbergen, et al. (2018). The first step toward implementation is by determining the intertidal shoals and their margins using the method of Leuven, De Haas, et al. (2018) by fitting a linear regression for the median bed elevation along the estuary channel. Elevation above the regression line was interpreted as a shoal and below as a channel. The boundary of the shoal was then extracted to determine the shoal margin. Subsequently, shoal margin collapse frequencies, $F_{SC}$, were calculated (adapted from Van Dijk, Mastbergen, et al., 2018) as follows

$$F_{SC} = \left[ \left( \frac{H}{11} \right)^{2.5} \left( \frac{9.5}{3 \cot \alpha} \right) \right] \frac{SC_{avg}}{L_{sm}},$$

where $H$ is the elevation of the local maximum between the center and the deepest part within a window size of 300 by 300 m on a 20 by 20 m interpolated grid of the bed elevation, $\alpha$ is the corresponding angle to $H$, $SC_{avg}$ is an empirical value based on the average number of collapses observed per year (5.3 for the Western Scheldt; Van Dijk, Mastbergen, et al., 2018), and $L_{sm}$ is the measured total length of shoal margins (300 km for the Western Scheldt; Van Dijk, Mastbergen, et al., 2018). The form of equation (1) allowed the frequency of collapse to be greater than 1, which was prevented by a transformation, namely, a Poisson process, of the frequency into a probability ($P_{SC}$):

$$P_{SC} = 1 - e^{-F_{SC}}.$$ 

Van Dijk, Mastbergen, et al. (2018) found that at a probability threshold ($P_{SC}$) value of $10^{-4}$, the true positive rate, defined as the number of cells that had shoal margin collapses in both the predictive probability and observed collapses divided by the number of observed locations of collapses, was almost 0.5. At this probability threshold, the remaining predicted shoal margin collapse locations show a low false positive rate, which is defined as the number of cells that had shoal margin collapses in the predictive probability but no observations of collapses divided by the number of cells with no shoal margin collapse observations. Because multiple locations at the shoal margin could have a probability value greater than the given threshold of $10^{-4}$, we capped the number of collapses to a maximum of 1 per tidal flat (shoal margin) per time interval. This means that per time interval, only a maximum of eight collapses can occur along the Western Scheldt. The time interval was set to one morphological year. Eroding shoal margins were excluded, because these were already eroding by continuous channel migration, and collapses mostly occurred suddenly at vertical aggradational margins. The highest probability above the critical probability of $10^{-4}$ was used to select the location of the shoal margin collapse per tidal flat. These slopes collapsed to a postevent slope while conserving mass, in which the size and geometric shape of the collapses followed a one-third ellipsoid according to the analysis of Van Dijk, Mastbergen, et al. (2018) of the geometric shape of the erosion scar (see Text S2).
3.5. Data Analyses
The Delft3D model outcomes were analyzed for near-field and far-field effects, that is, local and estuary scale. The analysis of the near-field effects on a short term was conducted on the first scenario, whereas for the Western Scheldt model (second and third scenarios), the far-field effect on the long-term morphology was analyzed. For the near-field effect, we analyzed the distribution of the collapsed sediment by labeling the collapsed deposit as a second sediment fraction with the same grain size in the model. The model outcomes were also analyzed by looking at the Digital Elevation Model (DEM) of Difference (DoD) between a run with the collapse and the control run. The distribution of the collapsed sediment was plotted in a time-space diagram for the cross flow direction as well as longitudinal flow direction. Furthermore, the width-averaged bed elevation was calculated on the channel centerline-normal transects and compared between the runs with and without collapses.

For analyzing the shoal margin collapse effects, the tidally averaged flow and mean sediment transport were calculated over a spring-neap-spring tidal cycle, starting and stopping at the same water level point. The tidally averaged flow and mean sediment transport were summarized by plotting the vectors for determining the net direction of the flow and of the sediment transport. For the second scenario, the sediment transport direction was determined for the spring-neap-spring tidal cycle at the 10 locations of the collapsed scar and associated deposit and plotted in a rose diagram. Smoothing of the bed elevation after the collapse was determined by calculating the average bed elevation within the scar and the associated deposit locations.

We were specifically interested in the role of shoal margin collapses on the channel-shoal interactions. Thus, we used an existing network extraction tool to characterize the channel dynamics. This tool has been applied to braided rivers to determine the drainage network, so it includes channel bifurcations and confluences (Kleinhans et al., 2017). The tool uses the local lows of the channel bed to determine its lowest path. Specifically, the tool determines minimums, maximums, and saddle points and connects the minimums through a saddle point, according to a descending quasi Morse-Smale complex (Kleinhans et al., 2017). Besides the lowest path, the algorithm computes a complete set of paths that form the entire channel network. To achieve this, an ordered set of noncrossing paths, known as striation, is computed (Figure 2a). To do this, the DEM is split around the lowest path $\pi$ into two parts. Then the lowest paths in those two parts of the DEM are found, and the DEM is split around these paths, and so on. This continues until a threshold, referred to as a sand function ($\delta$), is reached. The sand function is defined as the summation of the volume of sediment that has to be removed before two channels become one in the network. The volume of sediment is calculated from the elevation above the saddle point (Kleinhans et al., 2017). This made it possible to compute graphs representing the channel network, consisting of the lowest paths for “sufficiently different” scales (Figures 2a and 2b).

Three threshold values for $\delta$ were chosen, representing three different network scales. The networks scales are similar to the names used in the Western Scheldt (Jeuken, 2000). But there is a mismatch between extracted channels from the network tool and field observations. The largest scale is the main channel, the next scale is the secondary channel, and the third scale is the connecting channel. In nature, the connecting channel connects the secondary channel to the main channel. We used the channel network to analyze the channel depths for the three network scales and between model outcomes.

4. Results
4.1. The 2014 Shoal Margin Collapse
4.1.1. Hydrodynamics
Changes in bed elevation and associated bed friction due to a shoal margin collapse affected the water level around the collapse as well as the associated deposit. Over time, the water level fluctuates within 1 cm between scenario 1 and the control run under the same boundary conditions (Figures 3a and 3b). The main water level difference is noted in the transverse direction of the collapse (Figures 3c, 3d, & 3g). In the longitudinal direction, there is less water level difference between scenario 1 and the control run (Figures 3e and 3f). The largest difference in the water level change is observed at the scar of the shoal margin collapse (Figure 3d). Here the inundated time is longer because of the lower elevation. The two runs do not dominantly show lower or higher water levels. The skewness in the distribution of the water level changes indicates that water level increases for the shoal margin collapse deposit locations (Figures 3c and 3g), while the other locations show a decrease in the water level. The distribution of the water level changes varies between ebb and flood conditions for locations landward and seaward of the shoal.
Figure 2. Illustration of the network extraction approach. (a) First, from the DEM, the striation is computed (top). Then, different paths are found (represented by three sand function values, $\delta$, which form the final network including the main, secondary, and connecting scale. (b) Example network for the initial bathymetry of the Western Scheldt.

DEm = Digital Elevation Model

margin collapse (Figures 3e and 3f), indicating that water level increases for flood conditions seaward and decreases for flood conditions landward.

The small changes in the water levels affected the tidally averaged flow direction along the shoal margin. The control run shows that the tidally averaged flow direction (Figure 4a) is comparable with the original NeVla-Delft3D model (Figure 1b) around the tidal flat of Walsoorden. The tidally averaged flow remains similar for both simulations. The direction and magnitude of the tidally averaged flow are affected around the location of the collapse. For example, flow velocity increases along the shoal margin with 0.1 m/s because of the collapse (Figure 4b).

4.1.2. Sediment Transport

Sediment transport is calculated with the Van Rijn, (2007a, 2007b) equation, which separates the bedload from suspended load transport. The mean total transport follows the direction of the tidally average flow. On the north side of the channel, the total transport is toward the center (Figure 4c). In the center of the channel, sediment transport is ebb dominated. On the south side of the channel, sediment transport is flood dominated. The mean bedload transport follows the direction of the tidally averaged flow (Figure S5a), which indicates a clear distinction in ebb- and flood-directed transport. The mean suspended sediment transport does not follow the tidally averaged flow direction at all locations, especially in the main channel south of the tidal flat of Walsoorden (Figure S5b). Here the direction is in the opposite direction of the bedload transport. Suspended sediment transport is flood directed at the north side of the channel and ebb directed at the south side. We suspect that this is the result of the transverse bed slope predictor, which has no effect on the suspended sediment transport. The transverse bed slope of $\alpha_{bn}$ of 30 showed a strong transverse direction of the sediment transport (Figure 4c). Analysis of model runs with the default $\alpha_{bn}$ of 1.5 (Figure S5d) showed that the magnitude in the longitudinal direction is comparable.

Changes in the tidally averaged flow due to the shoal margin collapse affected the sediment transport direction and magnitude. The run with the shoal margin collapse of 2014 showed an 80% reduction against the control run for the mean total transport, that is, the effective sediment, at the deposition location of the collapsed shoal margin (Figure 4d). The mean total transport along the shoal margin increases by 15% and even more within the shoal margin collapse. The decrease in sediment transport means that erosion of the
Figure 3. Changes in the water elevation relative to the control run at the five surrounding grid cells of the shoal margin collapse of 2014 (locations in Figure 4b). (a) Water level at the location of the collapsed sediment deposit (location I) for a simulation without (thick black line) and with the 2014 shoal margin collapse (thin white line on top). (b) The difference in water surface elevation at the deposited collapsed sediment is within 1 cm. Positive values show water level rise following the collapse. (c) Distribution of water level change shows a slight increase in the water level. Here $s_k$ indicates if the distribution is skewed to the left (negative) or right (positive) from the mean of the distribution, where the mean is 0 m for all distributions. The two different colors show differences between ebb and flood conditions but no systematic lower or higher water levels. (d) The water level generally decreases. (e) Seaward there is a slight difference in the water level, whereas (f) landward there is more difference as in generally the water level lowers. (g) Water level increases on the shoal margin
deposited sediment from the collapse will take longer. The increase of sediment transport along the margin increases erosion potential.

4.1.3. Morphodynamics
By comparing scenario 1 to the control run, changes in the morphology between the runs can be ascribed to the shoal margin collapse. The DoD shows that the bed elevation in the channel landward as well as seaward of the collapsed deposit is raised after about 1 year of morphological time, whereas the location of the deposit is lowered from the start of the simulation (Figure 4e). This suggests smoothing of the profile after the collapse. The shoal margin collapse scar is still visible in the landscape. The process of sedimentation in the scar is slower than the erosion of the deposited sediment in the channel.

The difference in bed elevation shows the changes between the two runs but does not show the distribution of the sediment from the collapse. Figure 4f shows the distribution of the labeled sediment from the 2014 collapse around the tidal flat of Walsoorden. Large portions deposited at the sides of the original location, which corresponds with the DoD. The distribution of the collapsed sediments spread over a large area in the landward as well as seaward direction. This was less visible from the DoD because of the modest changes in bed elevation. Suspended sediment transport traveled a longer distance, whereas bedload transport affected bed elevation. Despite the transport in both directions, the dominant distribution of the tracer sediment was in the ebb direction (Figure 4f).

4.2. Shoal Margin Collapse Scenarios to Determine Sensitivity
In Supporting Information S1, we elaborate in more detail on the sensitivity of various scenarios, such as the size of the collapse, the location of the collapsed sediment, and the role of grain size. The analysis shows that the migration rate of the disturbance is hardly affected by the collapsed volume and that only large collapses, > 100,000 m$^3$, affect the far-field channel-shoal interactions (Figure S7). This is because the volume of collapsed material is relatively small compared to the characteristic shoal volume of 34 million cubic meters. The tidally averaged flow direction at the location of the collapsed deposits determines the dominant direction of the disturbance. Collapses that occurred more landward are less reworked, and the transport direction is dominantly in the seaward direction (Figure S7). Model outcomes for different $\alpha_{bn}$ values do not change the longitudinal displacement of the disturbance but do affect the distribution of the sediments in the transverse direction (Figures S5c and S5d). Alongside the location of the collapsed deposit, the grain-size distribution of the deposited sediment also determines the direction of the disturbance. A sand fraction
Figure 4. Hydromorphodynamics at a single shoal margin collapse after 1 year compared with a run without the collapse. (a) The modeled tidally averaged flow for the control run shows ebb-dominated flow along the shoal margin collapse of 2014 (yellow), while at the deposit (white), it is around zero. The contour lines were plotted at 1-m elevation intervals. (b) Tidally averaged flow increases along the shoal margin seaward of the collapse and slows down at the collapse. Crosses numbered I–V are the locations for water elevation shown in Figure 3. (c) The mean total transport is ebb-dominated at the shoal margin (note vectors) but, as $a_{bn} = 30$, as a large transverse component into the channel along the Tidal flat of Walsoorden. (d) The total transport reduces around the shoal margin collapse. (e) The deposited sediment is spread only directly landward and seaward of the collapse, whereas the eroded collapse location remains unfilled. (f) Sediment is spread dominantly in the seaward direction in the channel along the vectors of the mean total sediment transport (see Figure 4c). DEM = Digital Elevation Model

smaller than 200 $\mu$m (100 $\mu$m) follows the same longitudinal direction as the median sand fraction of 200 $\mu$m but more sediment deposited at the sides of the channel. Sand fraction coarser than 200 $\mu$m (300 $\mu$m) is, however, transported in the strongest flow direction rather than that of the tidally averaged flow, so that only the sediment in the deepest part of the channel is entrained (Figure S6).

To summarize, shoal margin collapse scars and associated sediment deposits in the channel affect the local dynamics of the Western Scheldt, such as the sediment transport direction and morphology within the first year after the occurrence. Additionally, the size and location of the collapse have direct effects on the magnitude and direction of these dynamics.

4.3. Shoal Margin Collapses in the Western Scheldt

The 2014 shoal margin collapse is one of the larger collapses that occurred, but its effect on the estuary morphodynamics is modest. Here we first assess how much effect each individual location susceptible to collapse (see specific collapsed locations in Figure S4a) has on the morphodynamics. Then, we apply our novel
4.3.1. Multiple Initial Collapses

We used the Western Scheldt schematization (model 2) to test the long-term effect of multiple shoal margin collapses on the morphodynamics of the system. In the first scenario, 10 shoal margin collapses of a volume of 1,000,000 m$^3$ are added to the initial bed elevation of the Western Scheldt. Sediment transport is dominantly in two directions for most locations, corresponding with the ebb and flood current. The dominant direction differs between the source (scar) and the associated sediment deposit (Figure 5). Generally, the sediment transport is less for the location of the scar compared to the location of the associated sediment deposit. This is particularly true for more landward scars, which becomes dry during low tide. There are some exceptions to this, where the collapse occurs underwater, for example, the Spijkerplaat (location A), and the scar remains underwater during the tidal cycle. Perpendicular to the ebb and flood flow sediment is transported on the transverse bed slope. A strong perpendicular vector is observed for the collapse at the Molenplaat and Plaat van Walsoorden (locations F and I). This is probably the result of the relatively high value of $\alpha_{bn}$ of 30.

Sediment transport determines the rate at which the shoal margin collapse is filled and the associated collapsed sediment is eroded. The net sediment transport varies between ebb and flood flow as well as between spring and neap tidal cycles. The net sediment transport for a neap tidal cycle is about $5 \times 10^5$ m$^3$ and for a spring tidal cycle about $5 \times 10^6$ m$^3$. The net sediment transport is higher during rising tide than for falling tide. Locations (location A and H) with the highest sediment transport rates show faster infilling of the scar (Figure 6a). The collapse at the tidal flat Walsoorden (location I) is less filled. This is also observed from the first scenario model outcome and corresponds with lower sediment transport rates. Yet the rate of filling and erosion deviates from the observations of the 2014 collapse. In general, the filling of the scar is less (Figure 6a). Sediment transport rate also determines the rate of erosion of the collapsed sediment. In general, the erosion is faster than the infilling. There are some exceptions where collapsed deposits are slowly eroded. This applies for the collapses that occurred along the shallower secondary channels (Figure 6b), for example, the Brouwersplaat (location E) and Molenplaat (location F).

The initial collapses affect the long-term changes of the morphology in the estuary. The sediment transport direction and magnitude at the collapsed locations (Figure 5) determine the distribution of the collapsed sediment and the bed elevation difference (Figure 7a). The bed elevation changed majorly around the shoal margin collapse locations (Figure 7a). Sediment is locally distributed in the landward and seaward directions.
Figure 6. Development of shoal margin collapse scar and deposit volumes normalized by its initial volume at various locations for the Delft3D simulation in the first year (see locations in Figure 1a). The observed shoal margin collapse of 2014, close to the modeled location I, is shown for comparison (see Van Schaick, 2015). (a) Filling of the scar varies with location but is never completed within a single morphological year. (b) Deposit removal is faster than scar filling. In particular, shoal margin collapses in secondary channels develop slowly, for example, tidal flats of Brouwerplaat (E) and Molenplaat (F), and the less dynamic landward part of the estuary, Verdonken Land van Saeftinghe (J). Wiggles indicate effects of neap-spring tidal cycles from its original location. Interesting long-term effects are observed when the disturbances enter areas that accommodate less sediment transport but are morphodynamically active and control sediment division, that is, the junctions seaward or landward of the channel. Here the bed elevation is not only affected in the longitudinal direction but also in the transverse direction into connected channels (Figure 7a), that is, effectively following the sediment vectors. For example, the collapse at location B changes the bed morphology of both landward channels compared to the control run, which also appears at the landward direction of location H (Figure 7a).

On a longer timescale, the shoal margin collapses affect the dynamics of the system. A total volume change of $4.53 \times 10^8$ m$^3$ was observed compared to the control run, in which less than 10% of the volume comes from the initial collapses. The width-averaged mean bed level difference between scenario 2 and the control run shows that changes excite, that is, grow, over time (Figure 7b). In the beginning, there is a slight difference between the runs, which was also demonstrated with the 2014 collapse. But on the long term, the mean bed elevation between scenario 2 and the control run varies more than a meter (Figure 7b). This is primarily the result of migration of the junction around location C and landward of location H (Figure 7a). Following the tracer sediment along the estuary gives more insights into the dominant migrating direction of the disturbance (Figure 7c). The dominant direction depends on location but is generally landward for the seaward collapses and seaward for the more landward collapses. This corresponds with the dominant sediment transport direction shown in Figure 5. Bed elevation changes even occur in the locations where no sediment originated from the shoal margin collapse is located, for example, at 25 km (Figures 7b and 7c). This location corresponds to one of the channel junctions.

4.3.2. Multiple Yearly Collapses
In the third scenario, shoal margin collapses occurred after each morphological year. The shoal margin collapses vary in size and location according to the given rules (see section 3). These rules led to 227 collapses, that is, 5.7 per year, at 58 independent locations of distinct tidal flats over 40 morphological years (illustrated by contour lines in Figure 8a). A total volume of 40 million cubic meters, that is, 1 million cubic meters per year, is eroded, which is more than the historical field observations. Previous scenarios show that the distribution of the disturbance varies with location depending on flow conditions (see direction in Figures 1b–1e). Again, changes in the bed elevation occur mainly in the longitudinal direction, that is, landward and seaward of the collapse (Figure 8a). Collapses near the junctions lead to changes in the bed elevation across the channel because the channel is wider and shallower. This occurred at the same locations (B and H) as for the initial collapses, where the bed elevation differs up to 10 m compared to the control run. The total bed
Figure 7. Effect of multiple initial collapses in the Western Scheldt. (a) Elevation difference after 40 years between a simulation with and without 10 shoal margin collapses shows that for several locations the perturbation has migrated landward as well as seaward, whereas other collapses hardly migrated over 40 years, for example, locations E and F (see Figure 1a). The colored contour lines show the spatial distribution of the collapsed material. (b) The width-averaged bed elevation difference between the run with and without initial collapses shows some migration of the perturbations but mainly shows cumulative excitation effects after two decades. (c) Spatiotemporal distribution of the collapsed sediment, showing spreading in both seaward and landward directions. DoD = Digital Elevation Model of Difference volume difference at the end of the model run is $4.63 \times 10^8$ m$^3$ compared to the control run. Twenty percent of the volume comes from the 227 collapses.

The width-averaged bed level difference between scenario 3 and the control run (Figure 8b) illustrates the migration of the disturbance in both directions, excitation of the disturbance over time and also dampening of the disturbance. The bed elevation difference is dampened for the collapses that occurred at 13 km from the seaward end (Figure 8b), whereas migration is detected at 28 km from the seaward end (Figure 8b). Furthermore, there are some unexplained responses that are not associated with the collapses themselves, such as observed between 25 and 37 km from the Western Scheldt mouth, which probably is due to excitation of earlier collapses (Figure 8b). Because of the number of collapses and the yearly adding of new collapses, the effect of a single disturbance is difficult to follow. Most changes occur at the locations with several collapses. The total eroded and deposited volume is $2.31 \times 10^9$ m$^3$ for scenario 3 and $2.26 \times 10^9$ m$^3$ for the control run. This suggests that the simulations are equally dynamic as the difference of 50 million cubic meters is explained by the collapsed volume of 40 million cubic meters.

4.4. Reorganization of the Channel-Shoal Network by Collapses

The addition of yearly collapses in the model leads to detected changes in the channel network structure and scale compared to the control run (Figures 9a and 9b). While the main channel location and scale are generally the same between the three runs over time (Figure S8), many of the smaller scale channels are identified differently for the model run with yearly collapses. In the control run, fewer smaller-scale channels, that is, secondary and connecting, are observed compared to the run with yearly collapses (Figures 9a and 9b). This means there is better connectivity among the channels for the model with yearly collapses.
Figure 8. (a) Bed elevation difference between a control run and a run with yearly shoal margin collapses (indicated by the contour lines) shows that the entire system is modified, especially at junctions forming ebb-flood channels (landward of location B and at location H). (b) The width-averaged bed elevation difference between both runs shows that the location of incision and deposition migrates, excites, or dampens depending on the location of the collapse. DoD = Digital Elevation Model of Difference.

The scale, or sand function volume, at which channels are detected changes between the runs as well. The shifting of the channel network is associated with the differences in the morphological development of the system. In the case of the collapses, the secondary channel network shifts in space (Figure 9b). Sediment deposition in the channel decreases the volume of sediment between adjacent channels and so the volume for $\delta$. So that identified secondary channels in the control run are identified as connecting channels in the run with collapses. Over time, the location of the main channel, associated to channel migration, covers 2% less, whereas the secondary channel covers 4% more of the Western Scheldt in the situation with yearly collapses (Figure S8).

The various channel networks are used to determine the depth distribution of the channels. The initial network shows a deep main channel (Table 2 and Figure 9c). This deep channel is because of dredging activities for maintaining a specific depth of the shipping fairway in the Western Scheldt. After 40 years of morphological development, the main channel becomes deeper, but the variation increases (Table 2), showing deeper but also shallower channels. There is an increase in the number of smaller-scale channels (Figure 9d), especially for the run with yearly collapses (Figure 9f). We observed some changes in bed elevation between the control run and the model run with yearly collapses, which has a wider distribution (Figures 9d and 9f). The main channel depth for the model run with 10 initial collapses is more comparable to the control run (Figures 9d and 9e). Major changes are observed between the secondary and connecting scale channels, the number of connecting scale channels increases for the run with initial collapses, while the depth generally decreases. The depth of the secondary channel, however, increases for the run with initial collapses. The system with yearly collapses develops to a system with shallower channels because collapses occur primarily in

| Table 2: Statistics of the Mean $\mu$ and Standard Deviation $\sigma$ of the Depth for the Various Runs for All Network Scales |
| --- |
| $\mu$ (m) | $\sigma$ (m) |
| Scale | Scenario | | | | Scenario | | | |
| | Initial | Control | 2 | 3 | Initial | Control | 2 | 3 |
| Main | $-23.91$ | $-26.16$ | $-25.79$ | $-25.73$ | 8.16 | 10.95 | 11.13 | 11.02 |
| Secondary | $-15.65$ | $-17.41$ | $-17.88$ | $-19.15$ | 7.19 | 10.87 | 10.11 | 11.93 |
| Connecting | $-10.60$ | $-12.23$ | $-10.62$ | $-12.35$ | 6.60 | 8.00 | 5.95 | 7.09 |

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Figure 9. Networks in (a) the control run without collapses and (b) the scenario with yearly collapses, showing that 
spatial channel shifts and changes in the scale of channels after 40 years of morphological development. (c–f) Depth 
distributions of the channel networks show a deep initial main channel (c), which becomes shallower when modeled 
(d). The depth distribution for the run with initial collapses develops toward the control run (e), whereas continuous 
yearly collapses lead to further shallowing of the main channel in the estuary (f).

5. Discussion

We introduced an effective parametrization for the process of shoal margin collapse, based on the local bed 
elevation and slope gradient. Here we discuss how the response of the modeled collapses affects the morpho-
dynamics and how this differs from observations. We also consider the implication of shoal margin collapses 
on perturbing the channel-shoal interactions and hypothesize these are comparable to larger perturbations 
caused by dredging and disposal activities.

5.1. Modeled Collapses Versus Observations

The 2014 shoal margin collapse shows the near-field effects of a single collapse. This collapse is well stud-
eyed by Van Schaick (2015) by analyzing field measurements and Delft3D simulations. Van Schaick (2015) 
concluded that some morphodynamics of the model differs from the observations (Mastbergen et al., 2016). 
According to field measurements, sediment deposited from the shoal margin collapse migrated in the flood 
direction, that is, flood-directed net bedload, while the model outcome suggests ebb-directed net bedload. 
The discrepancy in the net bedload direction could be explained by the inaccuracy in the modeled hydro-
dynamics. The deposit from the 2014 shoal margin collapse is located in that part of the channel where
the tidally averaged flow is ebb dominated but almost zero, whereas south from the deposit, the tidally averaged flow and mean sediment transport suggest transport in the flood direction. Yet the flood current is generally stronger in the channel, which might have led to the distribution of the deposit in the flood direction instead of the modeled ebb direction. The rate of infilling of erosion scars was less in the model compared to field observations (Figure 6a), whereas the field observation of erosion of the associated deposit compares more closely to the modeled results. The difference indicates that the model has difficulties with the simulation of the shallower regions, maybe because no extreme water level conditions are included (only one repeated month of real time series) nor combined astronomical and meteorological forces (De Vet et al., 2018). Additionally, filling of the scars increases when a mud fraction is added to the model (Van Schaick, 2015).

The shoal margin collapse parametrization leads to several collapses along the Western Scheldt Estuary. The location is based on the bed elevation, such that steep slopes collapse, whereas the collapsed size and volume is randomly drawn from a log-normal distribution. Locations for shoal margin collapses (Figure 8a) do vary from the observed locations (Figure 1a). We expect that for the chosen probability threshold value, the number of false positives is at least equal to the number of true positives. This means that steep high slopes that are not susceptible to collapses are included as well (Van Dijk, Mastbergen, et al., 2018). Nonetheless, the collapses are widely distributed on tidal flats that do have collapses over time. Locations with rapid infilling of the scar relate to locations with multiple collapses, for example, at Spijkerplaat (location A) and Ossenisse (location H; Van Dijk, Mastbergen, et al., 2018).

Our parametrization differs from earlier attempts to prevent steep slopes of bars in rivers with Delft3D (Nieuwboer, 2012). Nieuwboer (2012) applies two strategies to reduce steep slopes in Delft3D; (1) slope avalanching and (2) slope slumping, in which avalanching stopped deposition of sediment on steep slopes and slumping leads to changing steep slopes to equilibrium. The slope slumping, however, leads to numerically unstable simulations because of large changes in the water levels. Here no numerical instabilities were observed, because the collapses mainly occurred underwater and water depths are higher in the estuary setting compared to shallow rivers. Furthermore, sediment was not deposited in adjacent cells but spread in the deeper parts of the channel following the slope of the collapsed shoal.

Our parametrization is limited in the correct prediction of the collapses as the original probability prediction of Van den Ham et al. (2014) includes also variables for sediment properties, such as grain size, relative density, and the number of mud layers (Mastbergen & Van den Berg, 2003). We calculated the probability for a uniform sediment size. Variations in sediment properties form when the channels migrate, forming new shoals on the inner banks while collapsing outer banks retreat into the layer cake of sand and mud of past shoals and marshes (Dalrymple & Rhodes, 1995; Fagherazzi et al., 2004; Van den Berg et al., 1996). Spatial information of the stratigraphy is lacking for most systems, because of the limited field data availability. Even for the well-studied Western Scheldt, a model is used to predict clay availability within the tidal flats (Dam, 2017). It will be of interest for future studies to use multiple fractions, especially to construct a subsurface including variations in sediment properties, such as observed in mud drapes (Braat et al., 2017).

5.2. Implications of Shoal Margin Collapse Perturbations on the Morphodynamics

The rate of sediment removal and the volume of a single collapse determine the channel dynamics around the collapse. In the less dynamic secondary channels, the sediment is less spread, so that the collapse has less impact on the channel-shoal interactions. Small collapses can be seen as noise to the system, while larger collapses can be seen as a perturbation of the system (Kleinhans et al., 2015). The shoal margin collapse first affects the local bed elevation by depositing sediments into the main channel. Over time, the disturbance propagates through the channel network affecting other parts. Our findings correspond partly with the conceptual model described by Schuurman, Kleinhans, et al. (2016) for disturbances in braided rivers. In the estuary, however, a perturbation in the channel leads to adjustments in the downstream and upstream directions. The dominant direction depends on whether the channel is ebb- or flood-dominant. The migration rate is low for the disturbance but larger than the spatial change rates of the shoals (tidal flats) themselves. Shoals are more or less fixed at their locations (Hoitink et al., 2017; Leuven, Braat, et al., 2018).

The initial 10 collapses show that the perturbations lead to excitation of the difference in bed elevation on the long term (Figure 7). Specifically, the bed elevation difference between the runs increases rapidly after 20 years. After 40 years of morphological development, the modeled bed elevation difference is only explained by less than 10% of the initial collapsed volume. In the case of the scenario with yearly collapses, the modeled...
Figure 10. Depth over time for the three model runs illustrating an increasing variation in depth for the various network scales. (a) Median depth for the main channel network over time shows minor differences with the control run. (b) Secondary channel network deviates after 10 years for the run with yearly collapses. (c) Connecting channel network shows a faster response time to collapses. Shading indicates quartiles. Considerable deviations are observed for the yearly collapses at 9, 18, and 30 years and for the initial collapses at 13, 27, and 36 years. (d) Time and volume of shoal margin collapses for the scenario with yearly collapses.

The bed elevation difference (Figure 8) is explained by 20% of the collapsed volume. We expect this percentage is less because the effects from the disturbances are still growing. Also, the perturbations are less effective because of the smaller collapses or small perturbations are overprinted by larger ones. In the case of the initial collapses, the perturbation grows over time, but besides some deepening of the secondary channel, the channel network remains the same. On the other hand, the yearly collapses change the course of the secondary and main channel at a few locations (Animation S1).

In general, the shoal margin collapses change the channel-shoal network by shallowing of the major channels and forming new smaller channels on the tidal flats. The extracted channel network from the final time step (Figure 9) illustrates the changes between the control run and the yearly collapse; however, these cannot be linked to the collapses themselves. Analysis of the channel depth for the various scales in time shows that the variation in channel depth increases in time, except for the secondary channels (Figure 10). The channel network changes part of the main channel into the secondary channel within the first 5 years for all runs. So the secondary channel deepens, and the main channel becomes shallower (Figures 10a and 10b). The collapses in the scenario with yearly collapses deepens the secondary, whereas connecting scale channels become generally shallower (Figures 10b and 10c). A few collapse events can be linked to changes in the channel network depth. For example, the collapses in year 22 result in shallowing of the secondary scale channel (Figure 10b). But changes in the depth of the main and secondary channel network scales are generally not linked to individual collapses. We suggest that the changes in the larger channel scales are the result of multiple collapses that first affected the connecting channel scale. For example, the shallower secondary scale channels after 10 years follow a deepening of the connecting scale channel network that occurred a year before (Figures 10b and 10c).

The shoal margin collapses do not dynamicize the model as we hypothesized but do affect the estuary channel-shoal interaction. The most interesting effect is observed near junctions (sills; Figures 7 and 8), corresponding to the overlapping sediment circulation cells (Wang et al., 1995). Here there is less gross sediment transport, but the channels shift more often than other parts of the Western Scheldt (Van Dijk, Mastbergen, et al., 2018). This is observed from the DEM of differences for the last decades (Grasmeijer et al., 2013). Analysis of the development of channel-shoals in the Western Scheldt shows a more dynamic system for the period 1860–1955 (Dam, 2017). These field observations suggest that dynamics of the shoals have decreased in the last decades and that perturbations, such as shoal margin collapses, are efficiently removed in the main and secondary channels and therefore only affect the development at the shallower sills and channel...
junctions. The role of the junction is significant as this leads to excitation of the disturbance. Disturbances at the junction change the flow direction toward the successive shoal, like the successive bifurcation in a braided river (Schuurman, Kleinhans, et al., 2016), but also the flow direction toward the shoal itself as the tidally averaged flow circulates, that is, forming a macrocell, around the shoal (Figure 1b). This means that disturbances near a junction would have a larger effect on the channel-shoal interactions. In the field, however, these junctions (sills) are well managed as this is part of the shipping fairway, and therefore, its depth is maintained by dredging activities (Verbeek et al., 1998), which means that the role of collapses is interrupted in the field.

The role of the shoal margin collapses might affect the estuary differently compared to dredging and disposal activities, associated with maintaining/deepening the main channel for navigation. In this study, we have not included dredging and disposal, which would affect our findings. Dredging activities at the toe of the Platen van Ossenisse (Drempel van Hansweert; Groenewoud, 1997) might lead to deepening and increase the number of shoal margin collapses in the field. This is not included in our simulations. Analysis from disposal strategies also showed that disposal of sediment in the secondary channels takes longer to spread, because of lower sediment transport, and forms a threat for the existence of the multichannel network (Meerschaut et al., 2004). Dredged volumes are 10 times larger compared to the volume of shoal margin collapses in the Western Scheldt, and we would argue, therefore, that the role of shoal margin collapses on the morphodynamics in the Western Scheldt is hardly observable. But this study shows that collapses do play a role in the more local, mesoscale morphology, for example, additional channel-shoal interaction leading to more dynamics. It will be of interest to test what the effect of dredging and disposal is on the stability of the multichannel network (Wang, 2015).

6. Conclusions

Detailed analysis of the large 2014 shoal margin collapse shows that the hydrological and morphological processes around the collapse affect both water levels and the sediment transport direction. Model results show that single shoal margin collapses only affect the local dynamics in the longitudinal direction and dampen out within a year when volumes are small. The extent of far-field effects is sensitive to the grain size of the deposit, where finer sediments are transported further away and settle on the sides of the channel while larger grains are hardly entrained and only eroded during the stronger flood flow. The distribution of the collapsed sediment deposit across the channel disturbs the region around the collapse, where sediment transport is dominantly following the tidally averaged flow but coarser sediment follows the stronger flood flow. The perturbation by the shoal margin collapses increases channel migration rate, as the deposited sediment pushes the flow against the banks. These results imply that disturbances caused by dredging and dumping may likewise affect the dynamics of channel junctions as well because dredging volumes are at least 10 times larger than the collapsed volumes.

We presented a parametrization for shoal margin collapses and coupled this to the Delft3D model, so that effects of multiple yearly collapses of various sizes on the morphodynamics could be tested. We found that near-field morphodynamics in the channel is slightly affected at a timescale of a year due to increasing bed elevation and changing water levels, but far-field effects controlled by the tidally averaged flow vectors are negligibly affected by the collapses. When larger disturbances reach the seaward or landward junction at tidal channel junctions over a longer time span, the bed elevation at the junction increases on average and decrease the cross-section geometry of the channel junctions. Here the perturbation affects the morphology in the longitudinal as well as transverse direction and affects the channel network on a longer term when the flow and sediment distributions into the multiple channels are shifted. The initial collapses have no effect on the long-term channel-shoal morphodynamics, although only 10% of bed elevation difference is explained by the collapsed volume. The yearly collapses resulted in a shallowing of the main channel as they mostly occur along the main channel and change the channel networks at the various scales. Furthermore, the secondary channels become deeper and the number of connecting channels increases. We conclude that multiple yearly collapses are changing the channel-shoal morphodynamics in estuaries, but that the role of the collapses is limited for heavily dredged systems such as the Western Scheldt. On the other hand, estuaries that are not intensively dredged may not develop oversteepened bar margins with frequent shoal margin collapses.
References

Akhbar, M. P., Sharma, N., & Ozja, C. S. P. (2011). Braiding process and bank erosion in the Brahmaputra River. International Journal of Sedimentary Research, 26, 431–444. https://doi.org/10.1016/S0167-6232(12)60031-1

Ashwath, P. J., & Levin, J. (2012). How do big rivers come to be different? Earth-Science Reviews, 114, 84–107. https://doi.org/10.1016/j.earscirev.2012.05.003

Baar, A., Albernan, M. B., Van Dijk, W., & Kleinmans, M. (2018). The influence of transverse slope effects on large scale morphology in model Hjelmodynamic models. in Riverflow 2018, vol. 40. https://doi.org/10.1051/e3sconf/20184004021

Baar, A. W., De Smitt, J., Uijttewaal, W. S. J., & Kleinmans, M. G. (2018). Sediment transport of fine sand to fine gravel on transverse bed slopes in rotating annular flume experiments. Water Resources Research, 54(1), 19–45. https://doi.org/10.1002/2017WR020604

Baeyens, W., Van Eck, R., Lambert, C., Wollast, R., & Goeyens, L. (1997). General description of the Scheldt Estuary. Hydrobiologia, 366(1), 1–14. https://doi.org/10.1007/BF0031640903

Bagnold, R. (1966). An approach to the sediment transport problem from general physics. General Geology, 36, 55–64.

Bolle, A., Wang, Z. B., Amos, C., & De Ronde, J. (2010). The influence of changes in tidal asymmetry on residual sediment transport in the Western Scheldt. Continental Shelf Research, 30, 871–882. https://doi.org/10.1016/j.csr.2010.03.001

Braat, L., Van Kessel, T., Leuven, J. R. F. W., & Kleinhans, M. G. (2017). Effects of mud supply on large-scale estuary morphology and development over centuries to millennia. Earth Surface Dynamics Discussion, 5, 617–652. https://doi.org/10.1519/efsd-5-617-2017

Cancino, L., & Neves, R. (1999). Hydrodynamic and sediment suspension modelling in estuarine systems. Journal of Marine Systems, 22, 117–131. https://doi.org/10.1016/S0924-7963(99)00036-6

Cannestri, A., Spruyt, A., Jaggers, B., Slingerland, R., & Borsboom, M. (2016). A mass-conservative staggered immersed boundary model for solving the shallow water equations on complex geometries. International Journal for Numerical Methods in Fluids, 81, 151–177. https://doi.org/10.1002/fld.4180

Coleman, J. M. (1969). Brahmaputra River: Channel processes and sedimentation. Sedimentary Geology, 3, 129–239. https://doi.org/10.1016/0037-0738(69)90010-4

Crosato, A., & Saleh, M. S. (2011). Numerical study on the effects of floodplain vegetation on river planform style. Earth Surface Processes and Landforms, 36, 711–720.

Dalrymple, R., & Rhodes, R. (1995). Estuarine dunes and bars, Developments in sedimentology (pp. 359–422). New York: Elsevier. https://doi.org/10.1016/S0070-4571(05)80033-0

Dam, G. (2013). Harde lagen Westerschelde (in Dutch) (Tech. Rep.). International Marine & Dredging Consultants.

Dam, G. (2017). Lange-tijmigendemolhals Westerschelde (in Dutch) (Tech. Rep.). SVASEK hydraulics.

Darby, S. E., Alabyan, A. M., & Van de Wiel, M. J. (2002). Numerical simulation of bank erosion and channel migration in meandering rivers. Water Resources Research, 38(9), 1163. https://doi.org/10.1029/2001WR000602

De Vet, P. L. M., Van Prooijen, B. C., Schrijvershof, R. A., Van der Werf, J. J., Ysebaert, T., Schrijver, M. C., & Wang, Z. B. (2018). The influence of combined tidal and meteorological forces for the flow and sediment transport on intertidal shoals. Journal of Geophysical Research: Earth, 123, 2464–2480. https://doi.org/10.1029/2018JF004605

De Vriend, H. J., Wang, Z. B., Ysebaert, T., Herman, P. M. J., & Ding, P. (2011). Ecomorphological problems in the Yangtze Estuary and the Western Scheldt. Wetlands, 31, 1033–1042. https://doi.org/10.1139/wet-2011-0239-7

Deltas (2009). Delta3D-FLOW user manual, simulation of multi-dimensional hydrodynamic flows and transport phenomena, including sediments. Deltares, Delft, The Netherlands.

Dunbar, J. B., Torrey, V. H., & Wakeley, L. D. (1999). A case history of embankment failure: Geological and geotechnical aspects of the Celotex levee failure, New Orleans, Louisiana (Technical report). Mississippi, USA: US Army Corps of Engineers, Vicksburg.

Fagherazzi, S., Gabet, E. J., & Furbish, D. J. (2004). The effect of bidirectional flow on tidal channel planforms. Earth Surface Processes and Landforms, 29, 295–309. https://doi.org/10.1002/esp.1016

Graasmeijer, B., Dam, G., & Taal, M. (2013). Actualisatierapport Delta3D Schelde-estuarium (in Dutch) (Tech. Rep.). International Marine & Dredging Consultants.

Groenevoud, M. D. (1997). Modelling morphodynamisch gedrag van de Drempel van Hansweert (in Dutch) (Master's thesis). Delft University of Technology.

Gruijters, S. H. L. S., Schokker, J., & Veldkamp, J. G. (2004). Kartering moeilijk erodeerbare lagen in het Schelde estuarium (in Dutch). rapport NTG 200318213, 208, TNO.

Hoitink, A. J., Wang, Z. B., Vermeulen, B., Huismans, Y., & Kästner, K. (2017). Tidal controls on river delta morphology. Nature Geoscience, 10, 637–645. https://doi.org/10.1038/ngeo3000

Ikeda, S. (1982a). Incipient motion of sand particles on side slopes. Journal of Hydraulics Division, 108(1), 95–114.

Ikeda, S. (1982b). Lateral bed load transport on side slopes. Journal of Hydraulics Division, 108(11), 1369–1373.

Jørgensen, D. J., & Paola, C. (2010). Shredding of environmental signals by sediment transport. Geophysical Research Letters, 37, 119401. https://doi.org/10.1029/2010GL044638

Jeucken, M. C. J. L. (2000). On the morphological behaviour of the tidal channnels in the Westerschelde estuary (PhD thesis), Universiteit Utrecht.

Khan, N. I., & Islam, A. (2003). Quantification of erosion patterns in the Brahmaputra-Jamuna River using geographical information system and remote sensing techniques. Hydrological Processes, 17, 959–966. https://doi.org/10.1002/hyp.1173

Kleinmans, M. G. (2010). Sorting out river channel patterns. Progress in Physical Geography, 34, 287–326. https://doi.org/10.1177/0309133310365300

Kleinmans, M. G., Braudrick, C., Van Dijk, W. M., Van de Lageweg, W. I., Teske, R., & Van Oorschot, M. (2015). Swiftness of biomorphodynamics in Lilliput- to giant-sized rivers and deltas. Geomorphology, 244, 56–73. https://doi.org/10.1016/j.geomorph.2015.04.022

Kleinmans, M. G., Kreveld, M., Ophelders, T., Sonke, W., Speckmann, B., & Verbeek, K. (2017). Computing representative networks for braided rivers. In B. Aronov & M. J. Katz (Eds.), 33rd International Symposium on Computational Geometry (SoCG 2017). Leibniz International Proceedings in Informatics (LIPIcs) (Vol. 77, pp. 48:1–48:16). Dagstuhl, Germany: Schloss Dagstuhl–Leibniz-Zentrum fuer Informatik. https://doi.org/10.4230/LIPIcs.SoCG.2017.48

Laury, R. L. (1971). Stream bank failure and rotational slump: Preservation and significance in the geologic record. Geological Society of America Bulletin, 82, 1251–1266.
Leuven, J. R. F. W., Braat, L., Van Dijk, W. M., De Haas, T., Cleveringa, J., & Kleinhans, M. G. (2018). Growing forced bars determine non-ideal estuary planform. *Journal of Geophysical Research: Earth Surface*, 123, 2971–2992. doi:10.1029/2018JF004718

Leuven, J. R. F. W., De Haas, T., Braat, L., & Kleinhans, M. G. (2018). Topographic forcing of tidal sand bar patterns for irregular estuary planforms. *Earth Surface Processes and Landforms*, 43(1), 172–186. doi:10.1002/esp.4166

Mastbergen, D. R., & Schrijvershof, R. (2016). Sedimentatiepatronen Plaat van Walsoorden na plaatval 22 juli 2014 (in Dutch) (Tech. Rep.). Deltares.

Mastbergen, D. R., & Van den Berg, J. H. (2003). Breaching in fine sands and the generation of sustained turbidity currents in submarine canyons. *Sedimentology*, 50(4), 625–637. doi:10.1046/j.1365-3091.2003.00554.x

Mastbergen, D. R., Van den Ham, G. A., Cartigny, M., Koelewijn, A., De Kleine, M., Hizett, J., Azpiroz, M., & Vellinga, A. (2016). Multiple flow slide experiment in the Westerschelde Estuary, The Netherlands. In G. Lamarche, et al. (Eds.), *Submarine mass movements and their consequences, 7th Int. Symp. Advances in Natural and Technological Hazards Research* (Vol. 41, pp. 241–249). New Zealand: Springer International Publishing, Wellington. doi:10.1007/978-3-319-20979-1

Maximova, T., Ides, S., De Mulder, T., & Mostaert, F. (2009a). LTV O & M thema Veiligheid - Deelproject 1: Verbetering hydrodynamisch NeVa model ten behoeve van scenario-analyse (in Dutch) (WL rapporten 756_05). Antwerp, Belgium: Flanders Hydraulics Research & Deltares.

Maximova, T., Ides, S., De Mulder, T., & Mostaert, F. (2009b). Verbetering randvoorwaardenmodel. Deelrapport 4: Extra aanpassingen Zeeschelde (in Dutch) (WL rapporten 753_09). Antwerp, Belgium: Flanders Hydraulics Research.

Maximova, T., Ides, S., Vanlede, J., De Mulder, T., & Mostaert, F. (2009). Verbetering 2D randvoorwaardenmodel. Deelrapport 3: kalibratie bovenlopen (in Dutch) (WL rapporten 753_09). Antwerp, Belgium: Flanders Hydraulics Research.

Meerschaut, Y. M. A., Parker, W. R., Peters, J. J., & Plancke, Y. M. G. (2004). A dredging and disposal strategy for managing the Western Scheldt’s morphology and ecology. In: WODCON XVII: Dredging in a Sensitive Environment.

Nicholas, A. P. (2013a). Morphodynamic diversity of the world’s largest rivers. *Geology*, 41(4), 475–478. doi:10.1130/G34016.1

Nicholas, A. P. (2013b). Modelling the continuum of river channel patterns. *Earth Surface Processes and Landforms*, 38, 1187–1196. doi:10.1002/esp.20100F001774

Nieuwboer, B. (2012). Numerical modelling of Colorado sandbar growth (Master’s thesis), TU Delft.

Olsen, N. R. (2003). Three-dimensional CFD modelling of self-forming meandering channel. *Journal of Hydraulic Engineering*, 129, 366–372. https://doi.org/10.1061/(ASCE)0733-9429(2003)129:5(366)

Paola, C., Keller, F., & Angeline, C. (1992). The large-scale dynamics of grain-size variation in alluvial basins I: Theory. *Basin Reserve*, 4, 73–90.

Roelvink, J. A. (2006). Coastal morphodynamic evolution techniques. *Coastal Engineering*, 53(2–3), 277–287. doi:10.1016/j.coastaleng.2005.10.015

Schrijvershof, R., & Vroom, J. (2016). Effecten van realistische (extreme) stortstrategieën in de Westerschelde (in Dutch) (Tech. Rep.). Deltares.

Schuurman, F., Kleinhans, M. G., & Marra, W. A. (2013). Physics-based modeling of large braided sand-bed rivers: Bar pattern formation, dynamics, and sensitivity. *Journal of Geophysical Research: Earth Surface*, 118, 2509–2527. doi:10.1002/jgrf.20086

Schuurman, F., Kleinhans, M. G., & Middelkoop, H. (2016). Network response to disturbances in large sand-bed braided rivers. *Earth Surface Dynamics*, 4, 25–45. doi:10.5194/esurf-4-25-2016

Schuurman, F., Shimizu, Y., Iwasaki, T., & Kleinhans, M. G. (2016). Dynamic meandering in response to upstream perturbations and floodplain formation. *Geomorphology*, 253, 94–109. doi:10.1016/j.geomorph.2015.05.039

Silvis, F., & De Groot, M. B. (1995). Flow slide in the Netherlands: Experience and engineering practice. In: WODCON XVII: Dredging in a Sensitive Environment.

Simon, A., & Collinson, A. J. C. (2002). Quantifying the mechanical and hydrologic effects of riparian vegetation on streambank stability. *Earth Surface Processes and Landforms*, 27(5), 527–546. doi:10.1002/esp.325

Torrey, V. H. (1995). Flow slides in Mississippi Riverbanks. In C. R. Thorne, et al. (Eds.), *River, coastal and shoreline protection-erosion control. Using riprap and armourstone* (pp. 361–377). Chichester: Wiley.

Van Dijk, W. M., Hiatt, M. R., Van der Werf, J. J., & Kleinhans, M. G. (2018). Shoal margin collapses in Delft3D. GitHub.

Van Dijk, W. M., De Haas, T., Braat, L., & Kleinhans, M. G. (2018). Topographic forcing of tidal sand bar patterns for irregular estuary planforms. *Earth Surface Processes and Landforms*, 43, 2342–2357. https://doi.org/10.1002/esp.4395

Van Dijk, W. M., Schuurman, F., Van de Lageweg, M. I., & Kleinhans, M. G. (2014). Bifurcation instability determines chute cutoff development in meandering gravel-bed rivers. *Geomorphology*, 213, 277–291. https://doi.org/10.1016/j.geomorph.2014.01.018

Van Rijn, L. C. (2007a). Unified view of sediment transport by currents and waves: i. Initiation of motion, bed roughness, and bed-load transport. *Journal of Hydraulic Engineering*, 133(6), 649–667.

Van Rijn, L. C. (2007b). Unified view of sediment transport by currents and waves, ii: Suspended transport. *Journal of Hydraulic Engineering*, 133(6), 668–689.

Van Schaick, S. (2015). Morphological development after the July 2014, flow slide on the tidal flat of Walsoorden in the Western Scheldt (Master’s thesis), Delft University of Technology.

Van de Lageweg, W. I., Braat, L., Parsons, D. R., & Kleinhans, M. G. (2018). Controls on mud distribution and architecture along the fluvial-to-marine transition. *Geology*, 46, 911–914. doi:10.1130/G45504.1

Van de Lageweg, W. I., Van Dijk, W. M., Baar, A. W., Rutten, J., & Kleinhans, M. G. (2014). Bank pull or bar push: What drives scroll-bar development in meandering gravel-bed rivers, *Geomorphology*, 239, 133–136. doi:10.1016/j.geomorph.2015.05.039

Van Rijn, L. C. (2006). Coastal morphodynamic evolution techniques. *Coastal Engineering*, 53(2–3), 277–287. doi:10.1016/j.coastaleng.2005.10.015

Werkman, J. R. F. W., De Haas, T., Cleveringa, J., & Kleinhans, M. G. (2018). Growing forced bars determine non-ideal estuary planform. *Journal of Geophysical Research: Earth Surface*, 123, 2971–2992. doi:10.1029/2018JF004718
Van der Wegen, M., & Roelvink, J. A. (2012). Reproduction of estuarine bathymetry by means of a process-based model: Western Scheldt case study, the Netherlands. Geomorphology, 179, 152–167. https://doi.org/10.1016/j.geomorph.2012.08.007

Verbeek, H., Tank, F. T. G., & Groenewoud, M. D. (1998). Drempels in de Westerschelde (in Dutch) (Tech. Rep.). Rijksinstituut voor kust en zee/RIKZ.

Vroom, J., De Vet, P. L. M., & Van der Werf, J. J. (2015). Validatie waterbeweging Delft3D NeVla model Westerschelde monding (in Dutch) (Tech. Rep.). Deltares.

Wang, Z. B. (2015). Sustainability of the multi-channel system in the Westerschelde under influence of dredging and disposal. In Scheldt Estuary, physics and integrated management (pp. 65–70). The Hague, Netherlands. International Association for Hydro-Environment Engineering and Research.

Wang, Z., Fokkink, R., de Vries, M., & Langerak, A. (1995). Stability of river bifurcations in 1D morphodynamic models. Journal of Hydraulic Research, 33(6), 739–750.

Winterwerp, J. C., Jeuken, M. C. J. L., Stive, M. J. F., & De Vriend, H. J. (2000). Lange termijnvisie Westerschelde - Cluster Morfologie (in Dutch) (Tech. Rep.). WL Delft Hydraulics.

Xu, J. (1997). Evolution of mid-channel bars in a braided river and complex response to reservoir construction: An example from the middle Hanjiang River, China. Earth Surface Processes and Landforms, 22, 953–965. https://doi.org/10.1002/(SICI)1096-9837(199710)22:10<953::AIDESP789>3.0.CO;2-N