Heat Management System in A Vehicle When Parked

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Abstract:- This study aims to formulate competencies in automobile air conditioning system, using TEC for its effectiveness, efficiency, environment friendliness, comfort and convenience. The heating up of the vehicle cabin on being parked under direct sunlight due to green house effect causes immense discomfort to the passengers when they enter the cabin. The proposed design analyses the heating methodology of a passenger car parked under sunlight by experimental methods taking into consideration, the solar irradiance, temperature at various data points in the cabin, on the basis of which, design an air conditioning system by the usage of thermo-electric device and optimizing it to perform more efficiently with the least power consumption suited for imminent technologies in automotive industry.

Keywords: TEM (Thermo Electric Module), TEC(Thermo Electric cooling), Cooling Chamber , HVAC (Heating, Ventilation and Air Conditioning) and fins

1. INTRODUCTION

The overall idea of the system is to use the roof of a car equipped with solar cells to collect the energy of sunlight in the hot summer. It is stored in the car battery to drive the automobile blower and the TEC. The blower to ventilate the cabin, and the TEC cools the blower duct’s air, the air conditioning condensate collected during the driving process is used to cool the hot end of the TEC to improve the cooling effect.

The TEC is a refrigerating device based on the Peltier effect, which has the advantages of small volume and no noise, but the cooling effect is limited because the TEC’s refrigeration power is affected by the hot end temperature. The higher the hot end temperature, the lower the cooling power when the input power is constant. Here we are using 4 modules of Peltier device in which we are using 2 heat sinks, one for cold side and other is hot end side.

The design should achieve the primary goal of maintaining ambient temperature in the cabin and also maintain minimum space requirements. The secondary goal is to maintain the interior parts and to protect the goods and products kept at the cabin from aging and damage respectively. Other than the damaging or aging taking place, the other major problem is that the dangerous gases like Benzene, Volatile Organic Chemicals, etc, being released which causes increase in the risk of heart diseases, asthma, emphysema, causes skin cancer, lung cancer and damages to nervous system.

In this study we focus on developing a model that works on non renewable source of energy to maintain ambient atmospheric conditions inside the cabin and by minimal cost. Where the conventional HVAC system consumes about 8 h.p with a unit capacity of 3 tones of engine power, the use of peltier embedded system can overcome this engine power loss making it more efficient.

2. METHODOLOGY

The main objective of this project is to design a cooling system installed on a conventional blower of car AC. The idea of cooling is based on Peltier effect, as when a dc current flows through TE modules it generates a heat transfer and temperature difference across the ceramic substrates causing one side of the module to be cold and the other side to be hot. The purpose of the project is to make use of the cold side to cool the ambient air to a lower temperature, so that it can be used as a personal cooler. Testing and measurements are also performed on car (Hyundai i20). A simple temperature controller to interface with the cooling system has also been incorporated. Based on an analysis of sizing and design of the TEC air cooling for car, it can be deduced that the cooling system is indeed feasible. Readings taken during testing also testify to the fact that the TE cooling for car can lower the ambient temperature by 7 degree Celsius.

3. EXPERIMENTAL SET UP AND SURVEY

The temperature range inside the cabin due to radiations incident on glass and heating up of cabin space are recorded for over a period of five months from January to May 2020 where temperature survey is conducted.
4. DESIGN AND CALCULATIONS

4.1 VOLUME OF CAR CABIN

Volume of car cabin = 2300 Litre

4.2 HEAT LOAD CALCULATION

4.2.1 WINDSHIELD

The heat generated is \( Q_1 = A_\omega Z_d I_d + A_\omega Z_d I_d \Delta T \)

\[ Q_1 = 0.9942 \times 0.79 \times (100.29 + 80.54) \]

\[ Q_1 = 142.027 \text{ Watts} \]

4.2.2 SIDE GLASS

The heat generated is \( Q_2 = A_\omega Z_d I_d + A_\omega Z_d I_d \Delta T \)

\[ Q_2 = 1.14895 \times 0.79 \times (393.088 + 104.839) \]

\[ Q_2 = 467.762 \text{ Watts} \]

4.2.3 REAR WINDSHIELD

The heat generated is \( Q_3 = A_\omega Z_d I_d + A_\omega Z_d I_d \Delta T \)

\[ Q_3 = 0.3346 \times 0.79 \times (237.063 + 92.85) \]

\[ Q_3 = 87.207 \text{ Watts} \]

Total Heat Generated, \( Q_T = Q_1 + Q_2 + Q_3 \)

\[ Q_T = 142.027 + 467.762 + 87.207 \]

\[ Q_T = 696.996 \text{ W} \]

Therefore, the total maximum heat generated in the cabin space is 700 W.
4.3 SELECTION OF PELTIER

Heat Transmitted = 30W
Hot Side Temperature = 50°C
Cold Temperature = 8°C
Voltage = 12V
Current = 6.2A
Power = 74.4 W

Therefore based on the study and analysis we selected the Peltier module of
Peltier = CP85438

4.4 COOLING LOAD CALCULATION

4.4.1 ADIABATIC MIXING

Temperature of air at cabin, \( T_h = 33°C \)
\( = 306 K \)

Temperature of air from cooling chamber, \( T_c = 20°C \)
\( = 293 K \)

Mass of air at 2300 L volume,
\( m_h = \text{Density} \times \text{volume} \)
\( = 2.67 \text{ kg} \)

Equation of Adiabatic Mixing:
\[ m_h C_p (T_h - T_f) = m_c C_p (T_f - T_c) \]
Here we are finding the mass of cooling air, \( m_c = (\lambda - \lambda) \lambda \)
\( = 2.67 \times (306 - 305.9) \times 305.9 - 293 \)
\( m_c = 0.020697 \text{ kg} \)

4.4.2 DESIGN OF COOLING CYLINDER

\[ \text{Volume of Cylinder} = \frac{\pi}{6} \times d_c \]
\[ d_c = 0.2 \text{ m} \]

Effective Chamber volume
\[ = \frac{\pi}{6} \times 0.2 \times 0.2 \]
\[ = 6.283185 \times 10^{-3} \text{ m}^3 \]

4.4.3 DESIGN OF FAN AND CALCULATION OF EXIT VELOCITY

Fan diameter, \( d_{fan} = 18 \text{ cm} = 0.18 \text{ m} \)

Required volume flow rate
\[ \text{Exit velocity} = \frac{d_{fan}}{3} \times \frac{m}{\text{air}} \]
\( = 0.6749714111 \text{ m/s} \)

4.4.4 DESIGN OF INLET

\[ D = 0.025 \text{ m} \]
\[ L = 0.175 \text{ m} \]
Equivalent diameter of circle for inlet slot, \( D_{eq} = \)

\[ = 78.710 \text{ mm} \]

Velocity of air at inlet, \( U_i = 3.6862508 \text{ m} / \text{s} \)

4.5 CONVECTIVE HEAT TRANSFER COEFFICIENT OF AIR (\( h \))

4.5.3 CALCULATING THE REYNOLDS NUMBER OF AIR AT INLET

\[ R_e = \]

\[ = 17811.1455 \]

\( R_e > 2300 \) turbulent

As the air entering the chamber is turbulent

4.5.4 CALCULATING THE REYNOLDS NUMBER OF AIR AT FIN

\[ R_e = \]

\[ = 36375.0819 \]

As the air at the fin surface is laminar flow

\( Pr = 21.5 \) = 0.7027

To find \( h \)

\[ N_u = 0.332 \times R_e^{0.5} \times Pr^{0.333} \]

\[ = 0.332 \times 36375.0819^{0.5} \times 0.7027^{0.333} \]

\[ = 56.30078 \]

Nusselt number, \( Nu = \)

\[ h = 9.77869 \text{ W} / \text{m}^2 \text{ K} \]

4.6 DESIGN OF COLD FIN

4.6.3 CONVECTION OF FIN

\[ P = 2 (1 \times 10^{-3} + 15 \times 10^{-3}) = 0.032 \text{ m} \]

\[ A = 1 \times 10^{-3} + 15 \times 10^{-3} = 1.5 \times 10^{-5} \text{ m}^2 \]

\( k = 200 \text{ W} / \text{m K} \) for aluminium

\( T_b = 10^\circ \text{ C} \)

\( T = 33^\circ \text{ C} \)

\[ Q_{cv} = 0.6418108226 \]

\[ Q_d = 16.8025 \text{ W} \]

No: of fin (n) = ---

\[ = 27 \]

4.6.4 CONDUCTION OF FIN

\[ Q_{cd} = k A = \]

\[ = 0.27074 \text{ J} / \text{s} \]

Total heat transferred through ‘n’ Fin,

\[ Q_{TF} = Q_{fin} \times n \]

\[ = 7.30998 \text{ W} \text{ or } J / \text{s} \]

Total Peltier Power = \( Q_{pelt} = Q_{TF} + Q_d \)

\[ = 24.11248 \text{ W} \text{ or } J / \text{s} \]

4.7 DESIGN OF HOT FIN

\[ Q = \sqrt{(T_b - T_\infty) \tan h (mL)} \]

\[ = 4.2814 \text{ W} \]

Efficiency of the fin with accessories

\[ = \]

\[ = 76\% \]
5 ARRANGEMENT OF COOLING CHAMBER

6.3 VELOCITY FLOW TRAJECTORIES OF COLD SIDE

6 THERMAL ANALYSIS OF HEAT ABSORPTION FIN

6.4 MATERIAL PROPERTIES

Name: 1060 Alloy
Model type: Linear Elastic Isotropic
Default failure criterion: Max von Mises Stress
Thermal conductivity: 200 W/(m.K)
Specific heat: 900 J/(kg.K)
Mass density: 2700 kg/m³

6.2 TEMPERATURE DISTRIBUTION

7 THERMAL ANALYSIS OF HEAT REJECTION FIN

7.1 MATERIAL PROPERTIES

Name: 1060 Alloy
Model type: Linear Elastic Isotropic
Default failure criterion: Max von Mises Stress
Thermal conductivity: 200 W/(m.K)
Specific heat: 900 J/(kg.K)
Mass density: 2700 kg/m³

7.2 TEMPERATURE DISTRIBUTION

Fig 5.3 Peltier position in cooling chamber
Fig 5.1 Orthogonal view of the cooling chamber
Fig 5.2 Cold fin position in cooling chamber
Fig 6.2 Velocity flow of Trajectories of Cold side
Fig 6.1 Thermal analysis of the heat absorption fin
Fig 7.1 Thermal analysis of the heat rejection fin
7.2 VELOCITY TRAJECTORIES

Fig 7.2 Velocity flow of trajectories of Hot side

8. CIRCUIT BLOCK DIAGRAM

9. RESULTS AND DISCUSSIONS

As per the aim the system will be able to maintain the ambient temperature in the cabin. On the basis of calculations, the proposed design tends to confirm with the expected standards set forward as the base criteria. The system is considered power efficient and reliable for commercial implementation in passenger cars and is assumed to meet the expectations of the consumer base (as depicted from survey). The system is designed in such a way that it eases its integration to the existing vehicle design and implementation in the forthcoming vehicles as modified design.

10. CONCLUSION

It seems to provide acceptable results concerning to the primary aim to maintain the ambient temperature by implementation of the proposed system into a passenger vehicle.

By the methodology of air recirculation (by suction, cooling and delivery) of cabin air at a specified temperature such that, the rate of cooling tends to match with the rate of solar heating with considerations to compensate for all major thermal loses by taking sufficient design factors. A specific mass flow rate is decided to achieve the same, the air is passed through a chamber with fins to absorb the heat and deliver it back to the cabin using an axial flow fan. Air is hotter near the windshield, by taking into consideration, necessary heat distribution; air is sucked from this portion into the chamber and delivered back into the cabin through dashboard A/C vents. The system uses two thermo-electric cooler units working in parallel to achieve the goal. It has an efficiency of 60-65 percent with accessories included. This works on a solar powered control circuit.

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