Microbial electrosynthesis: Towards sustainable biorefineries for production of green chemicals from CO₂ emissions

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1. Introduction

Climate change has become one of the most challenging issues faced by humanity. After signing the Paris agreement in 2015, most countries worldwide committed to decreasing their greenhouse gas (GHG) emissions to contain global warming to 2°C (above pre-industrial levels), aiming to 1.5°C by 2050 (United Nations, 2015). Accordingly, the European Union (EU) set a target of 20% GHG reduction by 2020, 40% by 2030 and of achieving a net-zero carbon economy by 2050. The legislative pressure of EU on carbon emissions allowed to achieve the 2020 target already in 2017, when a total of 4483 Mt CO₂eq were produced, 22% lower than the emissions in 1990 (European Environment Agency, 2019). However, EU economy remains largely dependent on fossil fuels, which currently account for 65% of the energy supply and...
80% of the total GHG emissions (European Environment Agency, 2019). Significant efforts and innovative measures need to be developed to achieve the ambitious target of net-zero carbon emissions by 2050. Such efforts were translated into the European Green Deal, in which the EU will invest over one trillion euros to promote a low-carbon circular economy (European Commission, 2020).

CO₂ accounts for 65% of GHG emissions worldwide and the resulting environmental issues have contributed to change the paradigm towards its recycling (Aresta et al., 2013). CO₂ is indeed a resource that can be converted to carbon-neutral chemical commodities and fuels using carbon capture and utilization (CCU) technologies, with a future potential at the gigatonne scale (Bains, 2017). CCU technologies will mitigate GHG emissions both directly, by capturing CO₂ that would be otherwise released to the atmosphere, and indirectly, by displacing fossil fuel-based chemicals and fuels currently used by industries with green alternatives. It was estimated that every ton of heavy fuel displaced would avoid emissions of 300-500 g CO₂eq to the atmosphere (Masnadi et al., 2018), which is also valid for fossil fuel-derived chemicals.

Microbial electrosynthesis (MES) is a promising CCU technology for bio-electro CO₂ recycling into valuable chemical products, including organic acids (Batlle-Vilanova et al., 2017; Jourdin et al., 2015), alcohols (Arends et al., 2017; Gavilanes et al., 2019; Vassilev et al., 2019), and bioplastics (Pepè Sciarria et al., 2018). MES cells are essentially composed of two electrodes (cathode and anode), typically separated by a cation-exchange membrane (CEM), hosting a reductive (CO₂ bio-reduction) and an oxidative (e.g. oxidation of water or organic compounds) reaction, respectively (Fig. 1). CO₂ conversion into organic acids is catalysed by microorganisms that uptake electrons directly from the electrode or indirectly through intermediates such as (bio)electrochemically produced hydrogen (Nevin et al., 2010; Rabaey and Rozenval, 2020).

The use of microbial catalysts provides several advantages in comparison to conventional thermo-electrocatalytic CO₂ reduction. Microorganisms are cheap and self-regenerating catalysts that can achieve >80% electricity-to-product conversions under mild temperature (i.e. ambient or mesophilic conditions) (Bajracharya et al., 2017a). However, further efforts are required to optimise the conversion rate/yield and purity of products in MES reactors, and research on scaling-up CO₂ reduction processes is still scarce (Sánchez et al., 2019). The experience acquired in scaling-up related technologies such as commercially available electrolyses, as well as pilot-scale microbial fuel cells (Dong et al., 2015; Feng et al., 2014; Liang et al., 2018; Rossi et al., 2019; Vilajeliu-Pons et al., 2017), and microbial electrolysis cells (Gil-Carrera et al., 2015), can offer guidelines for deploying scalable MES configurations.

MES is currently a hot topic in biotechnology, and recent reviews gave an excellent summary of key aspects of the technology, from fundamental microbiology and electron transfer aspects (Karhikeyn et al., 2019; Logan et al., 2019) to the current state-of-art and future perspectives (Bian et al., 2020; Fruehauf et al., 2020; Jiang et al., 2019; Jiang and Jianxi Hong Zeng, 2018; Prévoteau et al., 2020), as well as techno-economic feasibility (Jourdin et al., 2020). Here we reviewed the main aspects hindering MES commercialisation, including the integration of MES reactors in industrial plants, reactor design, product synthesis and purification, and use of renewable electricity. Key issues were individuated, and future directions were suggested, based on previous experience on similar technologies, for putting forward resilient and sustainable CO₂ recycling MES biorefineries.

2. Integration of MES into industrial plants

2.1. CO₂ sources for MES

Energy supplies, together with industry and transportation, generate most greenhouse gas emissions in EU (1.27, 0.88 and 0.95 Gton CO₂eq/year, respectively). The energy sector accounts for 92.4% of the total CO₂ emissions, where energy generation (34.8%), transport (29.6%), and the manufacturing industry (15.4%) are the main contributors. The remaining non-energy related CO₂ emissions are mainly produced by the mineral, metal, and chemical industry (Fig. 2). MES is a bio-electrochemical recycling platform for CO₂ conversion to valuable products that can be directly applied for decarbonisation of flue gases from the energy supply and carbon-intensive industry sectors such as steel mills (20-30% CO₂), ceramic (15-20% CO₂), glass (10-15% CO₂), refineries (10-20% CO₂), cement industries (25-30% CO₂), and power plants (10-15% CO₂). Furthermore, MES can potentially recycle CO₂ produced from biological processes such as anaerobic digestion, fermentation and conventional wastewater treatment, which has been

![Fig. 1. Schematic representation of a typical MES configuration for biocommodities production from CO₂.](image-url)
estimated to produce around $4.4 \times 10^{-3}$ Gton CO$_2$/year worldwide (Rosso and Stenstrom, 2008).

### 2.2. CO$_2$ capture and utilisation in MES devices

Applying MES to industry requires infrastructures for gas transportation to the MES reactor, which inevitably lead to a higher footprint and costs. By performing a sensitivity analysis on the major costs associated to the adoption of carbon capture and storage (CCS) technologies in the iron and steel, cement and petroleum refining industries, Leeson et al. (2017) estimated that CO$_2$ capture and transportation can cost as high as 180 €/ton CO$_2$. Hence, integrated MES plants on industrial sites (i.e. close to the CO$_2$ emission sources) present a more economically viable solution than centralised plants. This highlights the need for designing flexible MES reactors, adaptable to the gas volumes and composition of the specific industry requiring gas treatment. Furthermore, when spent gasses are released during combustion, e.g. in boilers on combined heat-power (CHP) plants, reducing the temperature to 20-30$^\circ$C is required prior to feeding it to the MES cell. Such excess of heat can be recovered, using heat exchangers, and used for warming up the MES reactors, or recycled to other applications to further reduce operational costs. Another option is to operate MES reactors under therophilic conditions, thereby increasing the production kinetics and reducing the risk of microbial contamination, although the lower gas solubility at high temperature may limit the carbon and energy availability (Rovira-Alsina et al., 2020).

Depending on waste gas components, a pre-treatment may be required to remove impurities and toxic compounds for the MES microbial community (Fig. 3). This is the case, for example, of power plants powered by coal, peat or crude oil combustion, producing a gas containing CO, O$_2$, SO$_x$, NO$_x$, HCl and particulate ash besides CO$_2$ (Aouini et al., 2014; Pihu et al., 2017). In contrast, CO$_2$ constitutes 96-99% of flue gas produced in natural gas processing and alcohol fermentation. Complete natural gas combustion with air generates a clean flue gas stream of nitrogen (72% wt.), CO$_2$ (15-17%) and moisture (10-11%) (Sonibare and Akeredolu, 2004), which can be directly fed to MES reactors due to the absence of toxic compounds. Lab-scale MES reactors were indeed successfully operated on N$_2$:CO$_2$ 80:20% mixture gas feed (Deutzmann and Spormann, 2017; Nevin et al., 2010; Russell, 2013; Tahir et al., 2020; Zhang et al., 2013). In case of incomplete combustion, CO, NO$_x$ and residual O$_2$, detrimental for the microbial community, are also released, and on-line monitoring of the flue gas is thus required to prevent system breakdown. Nevertheless, regulations on CO, SO$_x$ and NO$_x$ emissions are, or will be, in place at the global level and thus, industries already have, or will require, a technology to remove these contaminants from flue gas. Oxygen concentration should also be minimised, since it can reduce MES efficiency by inhibiting the strictly anaerobic microorganisms, particularly in the absence of oxygen scavenging species (e.g. when oxygen-sensitive pure cultures are used as a microbial catalyst) (Giddings et al., 2015). Furthermore, O$_2$ exposure causes a decrease of the Coulombic efficiency (CE) by promoting the biological oxidation of MES organic products (Marshall et al., 2013), as well as diverging electrons towards O$_2$ electrochemical reduction into water.
The carbon capture cost is highly variable concerning the flue gas composition and increases with the level of CO₂ purity required (Bains, 2017; d’Amore et al., 2019; Leeson et al., 2017). In MES, the pre-treatment target is to reduce contaminants (e.g., NOₓ, SOₓ, and O₂) below the tolerance limit of the microorganisms, rather than generating a pure CO₂ stream, resulting in lower costs. Several SOₓ and NOₓ removal technologies are commercially available, being desulfurisation with lime or limestone, and catalytic NOₓ reduction, respectively, the most commonly applied worldwide (Sun et al., 2016). Furthermore, since CO₂ is a by-product of both processes when urea is used as reductant, it will contribute to the overall CO₂ feedstock for the MES cells. If the O₂ concentration in flue gas exceeds the tolerance of the MES community, a CO₂/O₂ separation step, such as adsorption or membrane separation (Wilberforce et al., 2019), is also required.

2.3. Reactor design for scale-up

Due to their simplicity, H-type MES cells have been commonly used for lab-scale experiments (Deutzmann and Spormann, 2017; Gavilanes et al., 2019; Mohanakrishna et al., 2020). Such design, however, is not an optimal solution for scale-up, due to (i) the large area requirements, (ii) the lack of modularity and versatility, and (iii) the high ohmic losses associated to low electrode surface/volume capability, low membrane surface, inefficient hydrodynamics, and a large distance between anode and cathode.

Since in bioelectrochemical systems the overpotential (i.e., the extra-voltage required for a reaction to occur in comparison to the theoretical) unavoidably increases with the reactor size (Rossi et al., 2019), a small, compact, and stackable reactor design is preferable for scaling-up rather than a single, large volume reactor (Greenman and Ieropoulos, 2017). Furthermore, stacks with several MES cells facilitate maintenance, since individual cells can be stopped without affecting the operation of the other cells. Multi-chamber reactors with flat (Bajracharya et al., 2016; Srikanth et al., 2018b) or tubular (Batlle-Vilanova et al., 2017; Blasco-Gómez et al., 2019; Pepe Sciarria et al., 2018) structures are examples of easily scalable and stackable configurations to increase the electrode surface/volume ratio and reduce area requirements. Projected surface/volume ratios above 1 cm²/mL are achievable with flat MES configurations (Srikanth et al., 2018b), and can be further optimised, although the limitations of the microbial catalysts will hamper to reach the extremely low electrolyte volumes of up-to-date electrochemical electrolyzers (Haas et al., 2018; Yin et al., 2019).

MES stacks can be operated with either series or parallel hydraulic and electric connections. Modules hydraulically connected in parallel receive the same feed rate, favouring replicability, whereas modules connected in series will receive a decreasing CO₂ load, thereby resulting in higher overall CO₂ removal efficiency (Fig. 4). However, the configuration in series is more exposed to the toxic effect of contaminants, if present in the flue gas to be treated, whereas the contaminant load is distributed when MES cells are connected in parallel. Therefore, a hybrid configuration, with parallel lines connected in series (Fig. 4), could be an advantageous solution. The number of parallel lines required can be dimensioned based on the waste flue gas production and reaction rates, whereas the length of the cell series is proportional to the required CO₂ removal efficiency. When comparing the electric configurations, superior performance of parallel than series connection was reported for bioelectrochemical systems stacks (Jafary et al., 2013; Liu et al., 2016). Connection in series could cause operation problems such as polarity reversal and substrate cross-conduction effect, and the resulting parasitic current flows (Gurung and Oh, 2012; Zhuang et al., 2012). Thus, connections in parallel appear preferable for MES, since a reliable cathode potential control (e.g., between -0.6 and -1.0 V vs. standard hydrogen electrode, SHE) is required, and because connections in parallel result in higher current densities than in series (Gurung and Oh, 2012). However, since MES cells are not identical, low resistance paths may occur in the MES stacks, requiring further potential control, as explained in Section 5.3.

Reporting on MES scaling-up is highly limited, and to date no pilot- or full-scale MES system is reported for CO₂ conversion. However, design of commercially available electrochemical cells, such as electrolyzers, can be potentially applied to scale-up the MES systems with minor modifications, and available pilot-scale studies on other bioelectrochemical systems, such as microbial fuel cells (MFCs), can provide useful guidelines. Configurations of scaled-up, stacked bioelectrochemical systems have been applied for the treatment of swine manure (Vilajeliu-Pons et al., 2017), brewery wastewater (Dong et al., 2015), and municipal wastewater (Feng et al., 2014; Liang et al., 2018; Rossi et al., 2019), as well as ammonia recovery (Zamora et al., 2017). So far, the largest scaled-up bioelectrochemical system is a 1000 L MFC (Liang et al., 2018), a device in which electric energy is produced by

![Fig. 4. Example of MES reactor stacks with hydraulic connections both in parallel and in series, and electric connections in parallel.](image-url)
biological oxidation of organic or inorganic contaminants and subsequent electron transfer to an electric circuit. It consisted of 50 squared modules (20 L each), electronically connected in parallel. A similar configuration, with the integration of CO$_2$ feeding lines, can be adapted to MES cells.

Flue gas can be delivered to MES reactors essentially in three ways: (i) CO$_2$ solubilisation and feeding as bicarbonate, (ii) direct gas feeding using gas spargers, or (iii) gas diffusion electrodes (Fig. 5). Dissolving CO$_2$ into a liquid bicarbonate-containing stream could simplify MES operation and improve the carbon conversion efficiency (Srikanth et al., 2018a). However, it requires an additional step for CO$_2$ solubilisation, leading to higher costs and area requirement. Direct gas utilisation requires more sophisticated design and control (e.g. gas composition and pressure monitoring) but is a more viable option in terms of costs and space utilisation. When gas spargers are used in MES, promoting contact between CO$_2$ and microorganisms is key to reach high production rates. This can be achieved by (i) maximising the active electrode surface by filling the cell with conductive granules (Vassilev et al., 2018), (ii) using electrodes with a high specific active surface such as multi-walled carbon nanotubes (Jourdin et al., 2016; Jourdin et al., 2015), (iii) forcing the CO$_2$ flow towards the electrode, e.g. using hollow fibre cathode electrodes (Katuri et al., 2018), or (iv) recirculating gas from the reactor headspace (Mateos et al., 2019).

Gas diffusion electrodes (GDEs) represent an effective alternative for decoupling the MES process from CO$_2$ solubilisation. GDEs, first applied to a MES reactor by Bajracharya et al. (2016), consist of a combination of hydrophobic polymeric gas diffusion and catalyst layers, enabling a three-phase (gas-liquid-solid) interphase that allows keeping high CO$_2$ concentrations in proximity of the (bio)catalyst. GDEs have been applied in lab-scale MES devices to produce both carboxylic acids and alcohols with production rates of 238 mg/(L·d) acetic acid (Bajracharya et al., 2016), 360 mg/(L·d) formate and 141 mg/(L·d) ethanol (Srikanth et al., 2018b). Multi-panel GDEs have also been applied as air diffusion cathodes in pilot-scale MFCs treating municipal wastewater with each panel having a surface of 324 cm$^2$ (Hiegemann et al., 2019; Rossi et al., 2019). Both studies reported a reduction of MFC performance over time due to fouling, which, nevertheless, is a minor issue in MES reactors owing to the low growth rate of autotrophic microorganisms and the relatively pure catholyte. Therefore, with such flexibility and efficiency, GDEs are promising electrodes for scaling-up MES.

Minimising the electrolyte volumes along with circulating the catholyte and anolyte towards and away from the respective electrodes is a scalable design solution discerning cell architecture, which is adopted in commercial-scale water electrolyser and fuel cells (Weekes et al., 2018). Such setup requires a separator to split apart the reduction and oxidation reactions occurring at the cathode and anode, respectively, promoting proton transfer while limiting O$_2$ flow from the anodic to the cathodic chamber. Proton exchange membranes (PEMs) such as Nafion, widely used in MES lab-scale devices (Kracke et al., 2019; Mohanakrishna et al., 2020; Srikanth et al., 2018b), are expensive. PEMs can cost as high as 2500 €/m$^2$ and represent up to 30-40% of the capital costs in both electrolyser and MFCs (Chakraborty et al., 2020; Mayyas et al., 2019). Cheaper options such as textile separators (Dong et al., 2015), as well as membrane-electrode assemblies (Salar-García et al., 2016) and membrane-less configurations (Feng et al., 2014; Hiegemann et al., 2019; Thung et al., 2019; Walter et al., 2020) have been generally preferred for scaling-up MFCs for wastewater treatment, and are potential solutions for MES as well. Low-cost ceramic separators were shown to achieve comparable, or even higher CE than Nafion membranes in MFCs (Khalili et al., 2017). Porous ceramic diaphragm separators are already available at commercial scale for alkaline electrolysis (Ursúa et al., 2012), and can replace expensive ion exchange membranes.
in MES.

Membrane-less MES systems can eliminate the costs and ohmic drops associated to separators, but oxygen diffusion towards the cathode needs to be prevented (Butler and Lovley, 2016). A membrane-less MES reactor, in which the CO$_2$-containing gas sparged from the bottom of the reactor was used to mitigate oxygen diffusion from the anode towards the cathode, was proposed by Giddings et al. (2015). However, the acetic acid production rate of 1.7-2.2 g/(m$^2$-d) achieved using Sporomusa ovata was substantially lower than that of 2.7-3.4 g/(m$^2$-d) obtained with the same strain using Nafion membranes (Russell, 2013; Zhang et al., 2013). A membraneless cell was also proposed for biomethane production from CO$_2$, achieving a production rate of 4.7 L/(m$^2$-d) (Giang et al., 2018). Microfluidic cells, with anode and cathode divided by a thin layer of electrolyte in which CO$_2$ diffuses, are an emerging technology for CO$_2$ electrolysis (Weekes et al., 2018), potentially applicable to designing membrane-less MES reactors with minimal distance between electrodes. However, scaling-up of such technology, hardly operable under pressure, is more problematic than traditional setups with membranes (Sánchez et al., 2019).

3. Carbon recycling in MES

3.1. Biocatalysts

Numerous microorganisms from all three domains of life have revealed ability to interact with solid electrodes for their metabolism (Logan et al., 2019). They are classified as exoelectrogens or electrotrohs, respectively, based on their ability of transferring electrons to, or accepting electrons from, an electrode. So far, four types of proteins have been identified to be responsible for electron transfer between electrode and cell surface: (i) porin-cytochrome complexes, (ii) cell-surface cytochromes, (iii) conductive nanowires and (iv) other redox proteins, including copper and iron-sulfur proteins (Costa et al., 2018). Electrotroths are the core of MES cells, acting as the catalyst for CO$_2$ conversion to a wide array of valuable products (Lee et al., 2019). They can reduce CO$_2$ by uptaking electrons either directly from the cathode electrode, or through mediators such as H$_2$ formate, ammonia, Fe$^{2+}$, or even more complex molecules such as self-produced flavins (Tremblay et al., 2017). Mixed microbial consortia and pure cultures of specific microorganisms, either natural or genetically modified, can act as biocatalyst in MES cells. Each inoculation strategy has its own advantages and disadvantages, as summarized in Table 1.

Mixed cultures from natural and anthropogenic environments have been widely used as biocatalyst in bench-scale MES cells for production of methan (Geppert et al., 2019; Jiang et al., 2013), acetate (Jourdin et al., 2015; Mateos et al., 2019), as well as mixtures of medium-chain carboxylic acids (Batlle-Vilanova et al., 2017; Vassilev et al., 2019, 2018) and alcohols (Arends et al., 2017; Blasco-Gómez et al., 2019; Gavilanes et al., 2019; Srikanth et al., 2018b) from CO$_2$. Mixed cultures represent the easiest and cheapest inoculation strategy for MES, but the low product selectivity (except for acetate) and the possible competition between acetogenic and methanogenic microbial communities are still unresolved challenges.

In comparison to mixed cultures, pure cultures offer higher product selectivity and eliminate competition issues. However, handling of pure cultures is laborious, requiring sterilization and a stable ecosystem. Nonetheless, avoiding contamination in CO$_2$-fed cells appears easier than in reactors treating solid or liquid waste, making the use of pure cultures suitable for industrial MES applications. Among pure cultures, acetogenic bacteria including Sporomusa ovata, S. phaeoïdes, Clostridium ljungdahlii and Moorella thermoacetica have been confirmed to reduce CO$_2$ to acetate by accepting electrons from a MES cathode (Nevin et al., 2011; Nevin et al., 2010), whereas other microorganisms such as Acetobacterium sp. exploit locally produced H$_2$ as the electron source (Marshall et al., 2017). Indirect (H$_2$-mediated) electromethanogenesis was reported by using a pure culture of Methanococcus maripaludis that converted CO$_2$ and on-site electrochemically produced H$_2$ to methane (Kracke et al., 2020). H$_2$-mediated electron transfer has been postulated to be less energy efficient than direct electron transfer (Karthikeyan et al., 2019), in which, nevertheless, the production yields can suffer of low electron exchange rates.

Genetic engineering approaches have been proposed to overcome the limitation of microorganisms in terms of electron transfer rates and cathode interaction, as well as to manipulate the metabolic pathways to target specific biocommodities (Shin et al., 2017). Metabolic engineering can provide a reliable method to go beyond the low-value chemicals naturally produced at the cathode (e.g. acetate), and achieve high-rate production of more valuable chemicals that are typically obtained in traces (e.g. multi-carbon chain biochemicals and biofuels (Kracke et al., 2018). However, an insufficient knowledge of the fundamental mechanisms is limiting the adoption of genetic engineering in MES, and research efforts are required to expand the toolset available for manipulating electricity-driven metabolic pathways. Furthermore, the high costs, as well as the legislative requirements, summarized in the review from Voiskova et al. (2020), make this approach complicated and economically dependent on the production capacity and value of the output products.

3.2. Production rates and product selectivity

Acetic acid is, to date, the major product obtained with MES. The highest specific production rate of 790 g/(m$^2$-d) was achieved using three-dimensional (3D) macroporous cathodes, far beyond the production rate obtained with unmodified carbon-based electrodes (Jourdin et al., 2018; Jourdin et al., 2016). Acetic acid can be produced from CO$_2$ in MES with high selectivity (>90%), and CE exceeding 85% (Nevin et al., 2010). Despite the developments in electrode design, the acetic acid production rate is limited by the low current densities, typically below 20 mA/cm$^2$, which is one order of magnitude lower than those achieved in electrolyzers (Prevotveau et al., 2020). In MES, besides the inherent limitations of the biological catalysts, the current density is limited by the kinetically unfavourable oxygen evolution reaction at the anode. This is particularly relevant when carbon electrodes are used, resulting in potential differences as high as 5 V, or even more, between cathode and anode (Bian et al., 2020). Furthermore, the anode has been individuated as the highest contributor to capital expenditure in MES.
cells (Jourdin et al., 2020). Using photoanodes, or exploiting less energy-demanding (bio)reactions at the anode, such as the oxidation of organic pollutants, are potential solutions currently under investigation (described in Section 5.2).

Methane can be produced at biocathodes in alternative to acetic acid. So far, the highest methane production rate of 12.5 L/(L·d) with 65% current-to-methane efficiency, was achieved using a mixed culture from a biogas plant in a galvanostatic flow-cell designed to maximise surface area (2 cm²/cm³) and optimise flow distribution (Geppert et al., 2019). In this study, the methane production rate was shown to increase linearly with the applied current (in the range 0.5-3.5 mA/cm²), although hydrogen was detected at currents above 2.5 mA/cm², suggesting metabolic limitations of the biocatalyst. Methane has often been reported as co-product in acetogenic MES (Marshall et al., 2013; Fatil et al., 2015). When mixed cultures are used as inoculum, and when MES cells are operated at neutral pH, methanogenic organisms can indeed compete with acetogens for H₂, or even convert carboxylic acid into methane. Methanogenic growth can be prevented by pre-treating the inoculum, e.g. by heat (Bajracharya et al., 2017c) or chemical treatment (Marshall et al., 2013), although these procedures do not ensure their permanent elimination.

The product spectrum of MES has expanded away from acetic acid towards more valuable compounds in the past few years, being butyrate and caproate two of the main products of interest (Table 2). Chemical commodities such as formate (Tashiro et al., 2018) and 3-hydroxybutyrate (Chen et al., 2018) have been obtained via MES from CO₂ as the sole carbon source using pure cultures and metabolic engineering tools. However, the scalability of this approach remains arguable and requires further investigation. Mixed cultures from different sources, nevertheless, have shown potential for the production of carboxylic acids and alcohols from CO₂ in MES, up-to six-carbon chains (Vassilev et al., 2018). Operation conditions, in particular pH, hydrogen partial pressure and inorganic carbon concentration, can be fine-tuned to steer the production of the target compound (Blasco-Gómez et al., 2019). In MES, pH can be controlled by CO₂ sparging, without the need for added chemicals (Bajracharya et al., 2017c; Ganiguet et al., 2015), which represents a key advantage for full-scale applications. Low pH (< 5.5) has been observed to promote solventogenesis, whereas pH close to neutrality is more favourable for butyric and caproic acid formation via chain elongation (Vassilev et al., 2018). Based on this observation, a dual biocathode arrangement was proposed to set an optimal pH of 6.9 for acetogenesis and chain elongation in one chamber, and a pH of 4.9 to promote solventogenesis in a second chamber (Vassilev et al., 2019). High hydrogen partial pressure was shown to promote acetic acid production rates, as well as solventogenesis, when combined with low pH (Blasco-Gómez et al., 2019), whereas low H₂ partial pressures turned out to favour biological H₂ evolution (Philips, 2020). Otherwise, a high concentration of dissolved CO₂ promotes acetic acid production, but results in lower product diversification (Arends et al., 2017).

Butyrate production from CO₂ in MES was achieved for the first time

| Product | Highest production rate (g/(L·d)) | Main carbon sources | pH | T (°C) | Potentiostatic control (V vs. SHE) | Galvanostatic control (mA/cm²) | Cathode | Reference |
|---------|-----------------------------------|---------------------|-----|--------|----------------------------------|-----------------------------|--------|----------|
| **Biochemicals** | | | | | | | | |
| Acetate | 77 | NaHCO₃ | 5.2 | 35 | -1.10 | n.a. | 3D-reticulated vitreous carbon | Jourdin et al. (2016) |
| | 66 | NaHCO₃ | 6.7 | 35 | -0.85 | n.a. | Multi-walled carbon nanotubes | Jourdin et al. (2015) |
| | 18.72 | CO₂ | 7.0 | 25 | n.a. | -83 | Reticulated vitreous carbon foam | LaBelle and May (2017) |
| | 9.85 | CO₂:N₂ 30:70% | 5.8 | 32 | -0.85 | n.a. | Carbon felt | Jourdin et al. (2018) |
| | 0.26 | Brewery flue gas (98% CO₂) | 7.0 | 28 | -0.80 | n.a. | Graphite plate | Roy et al. (2021) |
| Butyrate | 5.70 | CO₂:N₂ 30:70% | 5.8 | 32 | -0.85 | -5 to -12 | Carbon felt | Jourdin et al. (2019) |
| | 0.54 | Acetate, (NH₄)₂CO₃ and CO₂ | 5.5 | 30 | n.a. | -0.93 | Carbon felt | Rass et al. (2017) |
| | 0.16 | CO₂ | 6.3 | 38 | -0.80 | n.a. | Carbon cloth | Batlle-Vilanova et al. (2017) |
| | 0.04 | CO₂ | 6.4 | 35 | -0.80 | n.a. | Carbon cloth | Ganiguet et al. (2015) |
| Caproate | 2.41 | Ethanol, CO₂ and NaHCO₃ | 7.0 | 30 | n.a. | -1.0 | Carbon felt | Jiang et al. (2020) |
| | 2.00 | CO₂:N₂ 30:70% | 5.8 | 32 | -0.85 | -5 to -12 | Carbon felt | Jourdin et al. (2019) |
| Formate | 0.36 | CO₂ | 8.0 | 29 | -0.80 | n.a. | Gas diffusion electrode | Srikantan et al. (2018b) |
| **Biofuels** | | | | | | | | |
| Butanol | 0.06 | CO₂ | 8.0 | 29 | -0.80 | n.a. | Gas diffusion electrode | Srikantan et al. (2018b) |
| | 0.18 | CO₂ | 8.0 | 29 | -0.80 | n.a. | Gas diffusion electrode | Srikantan et al. (2018b) |
| | 0.05 | CO₂ | 5.4 | 25 | -0.80 | n.a. | Granular graphite | Blasco-Gómez et al. (2019) |
| Isopropanol | 0.06 | CO₂:N₂ 10:90% | 5.0 | 30 | n.a. | -0.5 | Carbon felt | Arends et al. (2017) |
| Methane | 12.5³ | NaHCO₃ | 7 | 30 | n.a. | -1.0 to -3.5 | Graphite felt | Geppert et al. (2019) |
| | 0.53³ | CO₂ | n. | 30 | -0.85 | n.a. | Carbon felt | Jiang et al. (2013) |

³ The cell was first operated in potentiostatic mode, and successively in galvanostatic mode; b Units in L/(L·d); n.a.: non-available.

Potentiostatic vs Cathode Reference
by Ganigué et al. (2015), with a production rate of 0.04 g/(L-d). Batlle-Vilanova et al. (2017b) triggered its selective production by operating the reactor at pH close to 5 and hydrogen partial pressure above 1 atm, reaching a maximum rate of 0.16 g/(L-d). Jourdin et al. (2019) reinforced butyrate and caproate production (maximum rates of 5.7 and 2.0 g/(L-d), respectively) by increasing the CO₂ loading rate up to 173.2 L/d. In this study, ethanol was first produced by acetate reduction and then acted as the electron donor for chain elongation. However, in another study (Jourdin et al., 2018), caproate was produced at a rate of 0.95 ± 0.05 g/(L-d), together with acetate (9.8 ± 0.65 g/(L-d)) and butyrate (3.2 ± 0.1 g/(L-d)), but without ethanol production, suggesting that the cathode was acting as the sole electron donor. At low pH, butyric and caproic acid were reduced to the corresponding alcohols (butanol and hexanol), opening possibilities of producing high-value biofuels in MES, although low titers of 0.8 and 0.2 g/L, respectively, were achieved (Vassilev et al., 2018). On the other hand, isopropanol production could be triggered in MES at pH 5 by maintaining low dissolved CO₂ concentrations in the catholyte. The production rate was stable at 5.85 ± 0.17 × 10⁻² g/(L-d) working under a hydraulic retention time of 5 days (Arends et al., 2017).

### 3.3. Production strategies

Development of cost-effective MES reactors for CO₂ recycling involves two diverging strategies: (i) maximise production rate of low-value products with high market request (i.e. acetic acid or methane), or (ii) steer production towards more valuable products, though at lower production rates (Fig. 6). The first strategy, in which the main target is the abatement of high CO₂ volumes, appears as the most feasible in the short term. Selective acetic acid production via MES, with both pure and mixed cultures, has been extensively demonstrated from different inorganic carbon sources, including bicarbonate (Jourdin et al., 2015), pure CO₂ gas (Song et al., 2017), and brewery flue gas (Roy et al., 2021). Versatile mixed cultures can achieve comparable, or even higher, acetic acid production rates than pure cultures, with similar specificity and CEs (Jiang et al., 2019). High product selectivity will make the product downstream processing easier and cheaper. Similarly, methane can be selectively produced in MES cells using widely available methanogenic cultures from biogas plants Geppert et al. (2019).

Despite the technological advances of the field, production rates far beyond the current record are required for MES commercialisation, due to the low value of acetic acid and methane (0.4–0.7 €/kg). When modelling for an industrial production of 1000 tons/year with an assumption of 69% CE, an unsustainable production cost of about 6.6 €/ton acetic acid was estimated, which could be reduced by 33% using renewable energy. Other products such as ethanol (1.0 €/kg) and formate (0.4 €/kg) are more cost-attractive (Christodoulou et al., 2017). Ethanol was also shown to have the most positive effect on GHG emissions, with a negative global warming potential of ~753 tons CO₂eq (Christodoulou et al., 2017).

Beyond acetic acid and ethanol, conversion of CO₂ to longer-chain carboxylic acids or alcohols, though with lower production rates, offers an interesting economic perspective. Such products are currently mainly manufactured via chemical synthesis from fossil-fuel based precursors. The expected dynamic growth in their market size, in combination with the fees (up to 99 €/ton, with an increasing trend) associated to CO₂ emission (Jackow et al., 2016), can foster the use of CO₂ as an alternative feedstock. Increasing demand for so-called cosmeceutical products is catalysing the global carboxylic acid market, in which compounds such as butyric and caproic acid are extensively used (Future Market Insights, 2020; Global Market Insights, 2020). Due to their high energy density and low hygroscopicity, higher alcohols such as butanol
and hexanol have been the focus of recent research initiatives (Vassilev et al., 2018). Butanol can be directly incorporated in the current fuel infrastructure, whereas hexanol, besides being an alternative to petro-derived gasoline, has multiple end-uses in the pharmaceutical, cosmetic, textile, food (both as pesticide and flavouring agent), and leather industry (Fernández-Naveira et al., 2017).

MES has the potential for meeting the future demand of the chemical industry, but further research is required to achieve production costs comparable to the currently applied chemical synthesis. Furthermore, despite the efforts aimed at understanding the metabolic pathways governing MES, and how they are affected by the operation conditions (Blasco-Gómez et al., 2019; Vassilev et al., 2018), a replicable, robust strategy for the selective production of carboxylic molecules other than acetic acid has not yet been developed.

4. Downstream processing

Downstream processing of MES products, including extraction, fractionation, concentration and purification, can account for more than 60% of the production cost (Prevoteau et al., 2020). Thus, development of a cost-effective extraction and separation method is crucial to achieve large-scale production of bio-based chemicals. Several extraction techniques have been proposed for extraction and separation of typical MES products, such as C2-C6 monocarboxylic acids (Table 3), described in the following sections.

4.1. Conventional separation processes

Conventional processes widely investigated for separation of organic acids are adsorption and liquid-liquid extraction (LLE). Adsorption is based on the ion exchange between carboxylate groups and functionalized solid sorbents, e.g. amine-based anion exchange resins (Rebecchi et al., 2016; Reyhanitash et al., 2017). In most cases, the performance of the sorbent depends on the pH of the solution. High adsorption capacities are achieved at intermediate pH values (~6.5), since an increasing pH causes an increasing concentration of acid in ionized form, but also a reduction of the amine concentration in protonated form (Rebecchi et al., 2016).

LLE is also a well-studied technology for separation of organic acids (Alkaya et al., 2009; Reyhanitash et al., 2016). Organophosphates such as tri-n-octylphosphine oxide (TOPO), tri-n-butyl phosphate and aliphatic amines have been identified as the most suitable extractants. Alkaya et al. (2009) used TOPO in kerosene to recover VFAs from a fermentation broth of sugar beet processing waste, reaching VFA recoveries of 61–98%, where the efficiency increases with increasing TOPO concentration (up to 20 wt%).

4.2. Concentration-driven and pressure-driven membrane processes

Pertraction is a membrane process where an organic solvent is immobilized (by capillary forces) inside the pores of a hydrophobic microfiltration membrane, thus separating the feed from the permeate (Dzygiel and Wieczorek, 2010). Organic compounds from the feed diffuse through the organic solvent in the membrane and can be continuously back-extracted on the permeate side. The membrane only acts as mechanical support, thus the extraction selectivity relies only on the extractant. Pertraction has been widely adopted for VFA extraction (Table 3), since it has several advantages compared to conventional LLE, such as (i) small amounts of organic solvent required, (ii) simultaneous extraction and solvent stripping, and (iii) lower operational costs. When

| Table 3 | Main investigated technologies for extraction and separation of organic acids from fermentation broths. |
| --- | --- |
| Technology | TRL | Advantages | Disadvantages | References |
| Adsorption in ion exchange resins | Industrial | Low CAPEX; no pretreatment needed | Ion-exchange influenced by pH | Bajracharya et al. (2017b); Recchetti et al. (2016); Reyhanitash et al. (2017); Saito et al. (2009) |
| Liquid-liquid extraction | Industrial | High extraction efficiency | High OPEX (compared to pertraction) and large use of extractant | Alkaya et al. (2009); Bekatorou et al. (2016); Reyhanitash et al. (2016); Saboie et al. (2018) |
| Pertraction (membrane liquid-liquid extraction) | Industrial | High extraction efficiency; low OPEX; selective extraction possible (based on hydrophobicity) | Selectivity depends on solvent | Agler et al. (2012); Aydin et al. (2018); Battle-Vilanova et al. (2017); Dessi et al. (2020); Nuchnoi et al. (1987); Outzam and Zhang (2018); Pârâide and Zhang (2018); Yesil et al. (2014) |
| Pervaporation | Lab | Simultaneous extraction and liquid-vapour phase change | Loss of extractant via evaporation; selectivity depends on permeate pressure (high vacuum needed) | Choudhari et al. (2015); Qin et al. (2003) |
| Nanofiltration | Industrial | Low CAPEX/OPEX; high rejection of high-molecular weight solutes | Separation strongly affected by pH and electrostatic interactions with membrane | Cho et al. (2012); Xiong et al. (2015); Zacharof et al. (2016) |
| Forward osmosis | Demo | High rejection of organics | Membrane fouling and VFA degradation; rejection rates dependent on availability and concentration of draw solution | Blandin et al. (2019); Cho et al. (2012) |
| Electro-membrane processes | | | | |
| Electrodialysis (ED) | Industrial | Low OPEX; easily scalable | Low selectivity among carboxylates and other anions | Cerullo et al. (2016); Jones et al. (2017, 2015); Gildemyn et al. (2015); Xu et al. (2015) |
| Membrane electrolysis | Industrial | Reduced chemical dosage thanks to in-situ production of H+ /OH- | Membrane fouling: less easily scalable than ED (because of non-modular unit) | Lopez and Hestekin (2015) |
| Electro-deionization (EDI) | Industrial | Possibility to treat very diluted streams; reduced energy consumption | Higher pressure drops and fouling tendency (compared to ED) | Scoma et al. (2016); Zhang and Angelidaki (2015) |
| Bipolar electrodialysis (BRMED) | Lab/ demo | Reduced chemical dosage thanks to in-situ production of H+ /OH- | No selectivity for a specific organic acid; higher membrane costs (compared to ED) | Arslan et al. (2017); Shi et al. (2018); Xue et al. (2017) |
| Reactive extraction processes | | | | |
| Reactive extraction with ionic liquids | Lab | Simultaneous extraction and esterification | High costs of ionic liquids with good extraction properties; ionic liquid losses | Andersen et al. (2016) |
| Reactive extraction in supercritical CO2 | Lab | Higher partition coefficient than physical extraction | Product losses due to formation of acid–amine complexes | Djas and Henczka (2018); Henczka and Djas (2016) |

* Technology readiness level; b Capital expenditures; c Operational expenditures.
using hollow fibre membranes, the organic phase is typically fed on the shell side and the aqueous feed on the tube side, although the opposite configuration could result in higher mass transfer rates (Pabby and Sastre, 2013). Recently, the use of silicone membranes has also been proposed, with water as extractant, showing good selectivity towards VFAs based on hydrophobicity (isovaleric > butyric > acetic) (Outram and Zhang, 2018). A silicone membrane was applied in-line to a cheese whey fermentation process by Dessì et al. (2020), achieving selective extraction of butyric acid over propionic and acetic acid. However, low pH (as close as possible to carboxylic acid pK_a) is required, since only undissociated acids can be extracted. The process was also shown suitable for alcohol extraction, whereas nutrients were retained, highlighting its potential for in-line product extraction from the MES catholyte.

In pervaporation, the target compounds are extracted via partial vaporization through a membrane, by maintaining the permeate side under vacuum. The extractant must have high boiling point, low viscosity, and low solubility in water, and the most used extractants are high-molecular-weight alkyl amines such as trioctylamine (TOA), tri-laurylamine (TLA), and tri-n-octylphosphine oxide (TOPO) (Nuchnoi et al., 1987; Qin et al., 2003).

Nanofiltration (NF) has been also widely investigated for VFA separation. Xiong et al. (2015) used commercial NF membranes to separate organic acids in lignocellulosic biomass digestion liquors, achieving 86% recovery (except for butyric acid, likely due to interactions with other components in the digestion liquor). In NF, the pH affects both the surface charge of the membrane and the degree of ionization of the acids. Acetic acid rejection increased from 0 to 62% with pH increase from 3 to 7 (Xiong et al., 2015), since at high pH the membrane (negatively charged) rejects carboxylate ions due to electrostatic effects. Therefore, low pH (in the range of 2.9-3.0) is advantageous for acetic acid separation via NF (Cho et al., 2012), which could preclude its in-line application to MES.

Forward osmosis (FO) exploits the osmotic pressure difference between the feed and a draw solution kept at the same hydrostatic pressure. The process efficiency, fouling and energy consumption are strongly influenced by the composition and concentration of the draw solution. Blandin et al. (2019) used FO to concentrate VFAs (mainly acetic acid) from domestic wastewater, achieving rejection rates >80% at pH 7.5. At pH 4, instead, the rejection drastically decreased, since the separation becomes mostly steric for undissociated acids (i.e., small molecules such as acetic acid can pass through the FO membrane, whereas larger molecules are rejected), thus showing the possibility to achieve selective separation. Rejection is also affected by molecule geometry (e.g., n-butyric acid shows higher rejection than iso-butyric acid), hydrophilicity, electrostatic and specific solute-membrane interactions. In general, anti-fouling strategies (e.g. backwashing) are crucial to limit VFA biodegradation on the membrane surface.

4.3. Electro-membrane processes

Electrodialysis (ED) is the most widely applied electro-membrane technology at industrial scale, and has also been widely investigated for organic acid recovery (Huang et al., 2007; Jones et al., 2017, 2015) achieved up to 99% VFA recovery from hydrogen fermentation broths, and also demonstrated the use of ED for in-line VFA extraction. However, ED suffers from low selectivity towards organic acids, and other anions (such as Cl-) are also inevitably extracted, especially if present at high concentration (Scorna et al., 2016).

Membrane electrolysis is an ED-based technology where anode and cathode play a crucial role in the process by producing H+ and OH (Xu et al., 2015). Membrane electrolysis has been applied (in combination to pervaporation) to selectively extract caproic acid from a fermentation broth, in which a pH gradient between the two chambers was electrochemically maintained, without chemicals addition (Xu et al., 2015).

Another alternative is bipolar membrane electrodialysis (BMED), i.e. an ED-like system that contains a bipolar membrane to promote water dissociation into H+ and OH via a catalysed protonation-deprotonation mechanism. The main advantage of BMED is the in-situ production of H+ and OH on the membrane surface, thus allowing pH change in the cell without dosing chemicals. BMED has been proposed for simultaneous electrochemical production and recovery of acetic acid (Zhang et al., 2011) and propionic acid (Boyaal et al., 1993).

A possible strategy to further enhance the separation efficiency is to use electrodéionisation (EDI), i.e., an ED-like system where the compartments are filled with ion exchange material (e.g. beads or wafers), to enhance ion transport in dilute stream conditions. Lopez and Hestekin (2015) used an ED cell with ion exchange wafer and ionic liquids to remove byurate and acetate from a synthetic fermentation broth, showing current efficiency up to 90% and energy consumptions of 1.25-2.80 kWh/kg acid recovered.

4.4. Reactive extraction processes

Ionic liquids (ILs) have been investigated for selective extraction of organic acids. Andersen et al. (2016) used ILs for the simultaneous concentration and esterification of MES-produced acetic acid (extracted via membrane electrolysis). Acetic acid was concentrated up to 80 mM using a bis(trifluoromethylsulfonyl)-imide IL, followed by esterification to ethyl acetate, upon ethanol addition, with a maximum conversion of 90%. This proof-of-concept study opens opportunities for widening the product spectrum of MES.

Another proposed strategy to recovery VFAs is the reactive extraction using organic solvents in supercritical CO2 (Dias and Henczka, 2018). Henczka and Dias (2016) investigated the reactive extraction of acetic and propionic acid (0.07–1.04 M) using TOA in supercritical CO2 (at 35–65°C and 80–160 bar), reaching a highest extraction efficiency of 94.7% for propionic acid, although part of the product was lost due to the formation of acid-amine complexes. Both pressure and temperature significantly influence the separation efficiency, due to the effect on the density and solvating power of supercritical CO2.

4.5. Perspectives for integrated MES-VFA extraction systems

Achieving selective separation of VFAs from dilute aqueous streams is still one of the biggest challenges for upscaling VFA biological production. The separation selectivity is influenced by several factors, such as pH, mobility, hydrophobicity, molecular weight, and ionization degree of the target product (Moon et al., 1998). This is especially challenging in MES, due to the low product concentration. For instance, MES reactors can only produce up to 7–10 g/L acetate, due to product inhibition (Bajracharya et al., 2017). These concentrations are not yet sufficient for economically upscaling if compared to industrial fermentation processes, where concentrations of 20–200 g/L of organic acids can be achieved (Lopez-Garzon and Straathof, 2014). In this regard, the maximisation of MES production rates is strictly linked to the development of an efficient in-situ extraction system, to minimise product degradation and alleviate the inhibition caused by the end-product accumulation (Batlle-Vilanova et al., 2017).

Since both extraction and concentration of VFAs are pH-dependent processes, an efficient pH control is of utmost importance to minimize the operational costs. In this respect, technologies that can provide in-situ production of H+ and OH+ (such as BMED, or membrane electrolysis) are advantageous to reduce the chemical dosage for pH control. For membrane-based extraction processes, one of the challenges in process integration with MES is preventing fouling. Pretreatment of the fermentation broths is required to remove suspended solids and colloids that can cause fouling, and tailored membrane with anti-fouling properties and increased selectivity toward organic anions should be designed. Since ED-based technologies suffer of low selectivity towards the target products, they can be deployed as final concentration step after extraction using membrane technologies with higher selective
extraction capabilities, such as pertraction, forward osmosis, or pervaporation (especially in the case of VFAs).

Very limited information is available in literature on capital and operation costs for VFA purification, which depend on the maturity and market of the separation technology, and on the economy of scale of the MES process. Jourdin et al. (2020) estimated a capital cost of 1000 €/ton, and an operation cost of 344 €/ton for the separation of caproic acid produced as the sole product in a MES cell. However, such rough estimation did not take into account the economy of scale factor, and costs will inevitably increase when separating specific products from mixtures of organic compounds, which appears as a more realistic scenario with the current state-of-art MES technology.

5. Development of sustainable MES biorefineries

5.1. Renewable energy sources to power MES

Electric energy is a major cost for (bio)electrochemical processes. When assuming an optimistic CE of 90% and an operational voltage of 3 V, it was estimated that about 12 kWhel are necessary for producing 1 kg of acetic acid, and such power consumption nearly doubles for producing caproic acid (Prevoteau et al., 2020). Considering the current average price of 69 €/MWh (Child et al., 2019), the electricity cost for producing 1 kg of acetic acid (0.83 €) is already higher than its commercial value, without taking into account operational, maintenance and downstream processing costs. Furthermore, if powered with fossil-fuel-based energy, MES could cause a net generation, rather than mitigation, of carbon emissions (Christodoulou et al., 2017). Thus, the use of renewable, low-cost energy is a crucial strategic factor for sustainable MES biorefineries. Renewable energy capacity in EU increased from 258 to 512 GWe over the period 2007–2017, with an exceptional growth of solar photovoltaics (+1966%), offshore wind (+1365%), onshore wind (+180%) and bioenergy (+94%). The adoption of renewable energy is forecasted to push down the electricity price by 20-30% at least, increasing competitiveness with fossil-fuel-based energy (Child et al., 2019).

Renewable energy sources can be integrated into MES either indirectly, by using renewable electric energy produced from solar, wind, geothermal, hydro or biomass to power MES, or directly, by solar-to-product conversion using photoactive electrodes producing the required power density (Fig. 7). The indirect approach appears particularly convenient for storing the low-cost excess power produced by the inherently fluctuating renewable sources as multi-carbon chemicals (Patil et al., 2015). However, fluctuating electric supply could temporarily decrease the production rates in MES, or even shift the metabolic pathway from carboxylic acid to methane production (Mateos et al., 2020). Such an issue can be avoided by using batteries and dedicated electronic circuits to deliver a constant current to the MES reactor (more details in Section 5.3).

The direct approach entails the key advantage of being independent of an electricity source (Bushuyev et al., 2018). However, photo-MES cells must be equipped with a power storage unit (see section 5.3) or light emitting diodes (LEDs) to ensure a continuous current delivery to the cathode. In the last decade, photoelectrochemical cells for water splitting have been technologically advanced, and are currently capable to deliver sufficient currents (up-to 5.8 mA/cm²) to drive electrochemical CO₂ reduction (Kirner and Finke, 2017). Hybrid systems, with biological cathodes coupled to photoelectrochemical anodes, have been thus demonstrated for self-sustained methane, isopropanol or acetic acid production from CO₂ (Table 4). An average solar conversion efficiency (SCE) of 0.62%, about three times higher than the global natural photosynthesis, was achieved for biological conversion of CO₂ to methane deploying the reducing current generated by a TiO₂ CdS photoanode (Xiao et al., 2020). Methane was generated at the cathode with a production rate of 15 L/(m²⋅d), which further increased to 20.8 L/(m²⋅d) (0.86% SCE) when a Cu₂ZnSnS₄ light adsorbing sensitizer was deployed.

Fig. 7. Indirect (1) and direct (2) power supply for microbial electrosynthesis (MES) cells. In the indirect approach, electric energy is generated from renewable sources and then used to drive water splitting (at the anode) and CO₂ bio-electrochemical reduction (at the cathode). In the direct approach, water oxidation is obtained from solar energy using a photoanode.
added to the photoanode. Liu et al. (2015) reported acetic acid concentrations as high as 6 g/L in a hybrid system with Fluorine-doped tin oxide; b Copper zinc tin sulphide.

| Inoculum | Cell design | Cathode | Anode | Current (mA/cm²) | Main product (yield/final concentration) | CE (%) | SCE (%) | Reference |
|-----------|-------------|---------|-------|------------------|------------------------------------------|--------|---------|-----------|
| Engineered Ralstonia eutropha | One-chamber | NiMoZn or stainless steel | CoP1 | 0.5-1.1 | Isopropanol (216 mg/L) | 3.9 | 0.7 | Torella et al. (2015) |
| Enriched methanogenic community | Two-chamber | Carbon cloth | TiO2 nanowire array | 0.07-0.09 | Methane (1.92 L/m²-d) | 95 | 0.1 | Fu et al. (2018) |
| Sporomusa ovata | Two-chamber | Si and TiO2 nanowires arrays | TiO2 nanowires | 0.3 | Acetic acid (6 g/L) | 86 | 0.38 | Liu et al. (2015) |
| Effluent from methanogenic MES | Two-chamber | Chitosan-modified carbon cloth | TiO2/CdS on FTO* (with CZTS® sensitiser) | 0.6 | Methane (15 L/m²-d), 20.8 L/m²-d with CZTS | 93 | 0.62 | Xiao et al. (2020) |

5.2. Integrated MES devices for CO2 recycling and wastewater treatment

When CO2 reduction at the cathode is coupled to water oxidation at the anode, high potentials or expensive catalysts are required to obtain the oxygen evolution reaction (Bian et al., 2020). Furthermore, a share of the oxygen produced at the anode can diffuse towards the cathode inhibiting the strictly anaerobic microorganisms. An integrated process combining CO2 reduction at the cathode and oxidation of pollutants at the anode not only will decrease the energy demand of MES, but will also simultaneously address two major challenges faced by industries (reduction of CO2 emissions and wastewater treatment). A maximum acetic acid production rate of 83 mg/(m²-d) was reported for a biocathode at a current density of 0.04 mA/cm² generated by a bioanode fed with synthetic wastewater containing 4 g/L sodium acetate. The COD removal rate reached 87% at a relatively low cell potential of 1.4 V (Xiang et al., 2017). Furthermore, acetic acid production from CO2 was demonstrated at potentials as low as 0.8 V though with a corresponding decrease in production rate. In addition, CO2 produced from wastewater treatment at the anode can be recycled to the cathodic chamber and act as a precursor for chemical production (Zhao et al., 2012). Photocatalytic oxidation can also be exploited for selective oxidation of target compounds such as alkenes (Farras et al., 2015). However, optimisation of both the cathodic and anodic reaction in integrated systems can be difficult, and further studies involving real wastewaters are required to assess the feasibility of this approach.

5.3. Energy storage and smart electronic design for MES

Although MES reactors demonstrated their resiliencies to current fluctuations, a constant electricity supply is required for a robust 24/7 operation. Thus, when fluctuating energy sources are used to power MES, additional investment is required for energy storage systems to recover excessive energy from the production peaks and deliver it to the MES reactors at a constant flow. The price of storage technologies, batteries in particular, decreased by 60% in the past five years, approaching the threshold of 100 €/kWh (Berekman et al., 2017). Power storage costs of 0.085 €/kWh have been estimated in Germany for 7 hours storage duration, low enough to incentivise the installation of batteries for harvesting solar power, and projected to further decrease to 0.065 €/kWh within four years (Comello and Reichelstein, 2019). As an alternative, MFCs treating wastewater can be used to produce electric energy for charging energy storage devices, which are subsequently discharged to power MES reactors (Hatzell et al., 2013).

In MES stacks, even if the cells are connected in parallel, the potential control is more challenging than in purely electrochemical electrolyzers. The inherently inhomogeneous microbial catalysts can indeed cause non-uniform charge distribution on the MES electrodes. This creates uneven potentials between the cells in the stack, that may cause a shift of the microbial communities (when mixed culture are used) or metabolic pathways underpinning CO2 recycling (Sánchez et al., 2020). Balancing charge distribution in MES stacks could find inspiration in power management systems (PMS) already available in battery stacks. PMS are capable of detecting overvoltage and overloading, switching off the connection to prolong the lifespan, and reducing stress on battery units (Stroe et al., 2018). Similarly, MES could use smart electronics to optimise voltage or current delivery (Fig. 8), allowing a stable chemical output. Such switching systems have already been implemented to improve the energy output in MFC grids (Kim et al., 2011). Potentiostatic cell control is costly, but enables a precise electrode potential control that allows to operate the cells under optimal conditions. Galvanostatic control is cheaper, but can result in fluctuations and divergence among the cells.

6. Outlook and future perspectives

The environmental incentives and increasing CO2 emission costs as carbon taxes are pushing industries towards the use of carbon conversion technologies. Although CCS technologies are already available at commercial scale, the emerging CCU technologies such as MES have the potential to gradually replace the existing chemical production facilities, producing a revenue stream that can offset the operation costs (Grim et al., 2020). When coupled to renewable energy, electrochemical CO2 conversion technologies can produce chemicals with a negative carbon footprint (De Luna et al., 2019), and their development is further incentivised by the decreasing electric energy cost. MES is a flexible technology with several market entry opportunities and potentially applicable to decarbonise industrial CO2-containing flue gas while producing fuels and chemicals that find application in the packaging, food, preservatives, rubber, metallurgy, pharmacy, polymers, chemical and renewable energy industry (ElMekawy et al., 2016).

Various platform chemicals and fuels can be produced in MES, raising argument about which products are the most viable from an economic perspective. Though a rough estimation on the techno-economic viability of different MES routes can be obtained with thermodynamic calculations, more in-depth techno-economic analyses are required. However, to date, no results on scaled-up MES reactors and operation under relevant conditions are available to support techno-economic analyses. Up to now, acetic acid is the only chemical that is produced in MES with selectivity >90%, and substantially higher rates than other chemicals (>100 g/(m²-d)), and has thus the highest decarbonisation potential (Jiang et al., 2019). Furthermore, acetic acid
has a huge market size of about 13 Mtons/year and can be used as a precursor for many valuable products. As such, it currently represents one of the most compelling targets. However, the economic viability of acetic acid production in MES is limited by its low market value (Christodoulou et al., 2017). Thus, research efforts are currently directed towards the selective production of more valuable compounds with reasonably high production rates. The main ongoing European research projects dealing with bio-electro CO₂ recycling, such as BioRECO2VER, SCALIBUR, BIOCON-CO₂, BAC-TO-FUEL, and Celbicon, are making a step beyond in demonstrating the technical feasibility for the production platform of valuable biochemicals and biocommodities (e.g. isobutene, lactic acid, biofuels, biopolymers, and surfactants). This is in line with the European strategy of seeking renewable fuels with high energy densities and low hygroscopicity, to be blended, or even to replace, fossil-based fuels for direct use in engines. Hybrid systems, in which enzymes or genetically modified organisms are applied to produce high-value compounds from electrochemically-produced building blocks, is another emerging field that is expected to play a key role in the future of CO₂ recycling (Bushuyev et al., 2018).

Besides commercial purposes, MES-derived chemicals can find application within the same industry they are produced. Such approach can decrease the costs of infrastructure required for product purification and transportation. For example, MES can be applied in existing power plants, as renewable energy storage during peak production, or in wastewater treatment plants, to convert CO₂ into organic substrates for processes such as denitrification (Osset-Alvarez et al., 2019). MES can also be seen as part of a biorefinery aiming at cleaning wastewater at the anode while upgrading biogas into biomethane at the cathode and recycling the resulting CO₂ to produce further methane, or for other purposes (Sadlukhan et al., 2016). Similarly, MES can provide reducing equivalents for syngas fermentation (Zhang and Tremblay, 2019). Biofuels produced from CO₂ can be used within the company as an alternative fuel for boilers, combined heat and power (CHP) plants and transportation. Integration of MES into bioethanol production plants would help increase the energetic efficiency of the whole process by recycling energy that is initially lost in the liquid waste, and increase the ethanol yield by recycling the CO₂ produced by solventogenic fermentation. Electrosynthesis products such as H₂, CH₄, CO and VFAs can be further upgraded to longer chain carboxylates, biofuels, bioplastics, polysaccharides and protein via multi-step bioconversions (Bian et al., 2020; Haas et al., 2018), or even in the same MES cell (Vassilev et al., 2019).

To date, most research interest in MES has been directed towards cathodic products, whereas anodic reactions have been overlooked. It was estimated that the anode, particularly when coated with expensive catalysts such as Pt, can generate as high as 59% of the capital costs (Jourdin et al., 2020). However, several value-added products can be obtained through oxidative reactions at the anode (Fig. 9), which could complement biocathodic products to increase the economic sustainability of MES. As an example, a relatively pure oxygen stream is generated by water oxidation at the anode, which can find a plethora of application in the chemical and manufacturing industry, as well as in waste and wastewater treatment facilities. Anodic reactions can be also exploited for producing disinfectants such as chlorine (Batlle-Vilanova et al., 2019), or ozone (Yan et al., 2020), although particular care should be given to prevent their cross-over to the biocathode. Oxidation reactions at the anode can also be applied for resource recovery. Hydrogen sulphide has been proposed as an electron donor in a MES for concomitant acetic acid production from CO₂ and sulphur/sulphate formation (Gong et al., 2013). Such process could be applied to sulphide-containing flue gas, allowing sulphur/sulphate recovery at the anode while reducing the power required for CO₂ reduction at the cathode in comparison to water oxidation. However, biological anodic processes, in particular when heterotrophic microorganisms are present, can result in a higher risk of membrane biofouling in comparison of MES cells where only the cathodic process is biological. Finally, the anodic process can be potentially applied to upgrade MES products (i.e. carboxylic acids), e.g. to octane via Kolbe electrolysis (Stang and Harzisch, 2016).

In summary, several challenges need to be overcome to push MES technology towards industrial adoption. Further research efforts are
required to decrease the capital costs associated to carbon capture and cell materials (in particular the anode electrode). Increasing the production rates, and developing strategies to selectively produce and extract high-value products, can boost the economic viability of the process. Powering the MES stack with renewable electricity is essential to ensure carbon-neutrality, and more attention is required to the anodic reaction to reduce current consumption, possibly generating a secondary revenue stream. MES technology is approaching the maturity level required to finally overstep the laboratory, and operation of pilot plants under relevant industrial conditions will corroborate its techno-economic feasibility.

7. Conclusions

MES has shown potential for replacing fossil-fuel based synthesis of platform chemicals or energy products, and significant opportunities for its establishment are yet to arise in response to the stringent legislation on carbon emissions and the decreasing cost of electric energy. The flexibility of MES, applicable to convert CO$_2$ containing gas from different sources to a plethora of different chemical products, can represent a key differentiator to enter the market. However, significant challenges need to be tackled before commercialisation. MES stacks need to be designed and operated under relevant condition (e.g. in pilot scale) to assess the technology from a techno-economic point of view. Efficient in-line product extraction and purification, as well as valorisation of the anodic reaction to obtain further commercial or commodity products, are key aspects in this regard. Since decarbonising the energy and the production sector is a priority, abatement of high CO$_2$ loads, even if producing low-value compounds such as acetic acid, appears as the most feasible approach for commercialising MES in the short term.

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