Perspectives of reactive ion etching of silicate glasses for optical microsystems

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Abstract. We provide a review of the latest research findings as well as the future potential of plasma-based etching technology for the fabrication of micro-optical components and systems. Reactive ion etching (RIE) in combination with lithographic patterning is a well-established technology in the field of micro- and nanofabrication. Nevertheless, practical implementation, especially for plasma-based patterning of complex optical materials such as alumino-silicate glasses or glass-ceramics, is still largely based on technological experience rather than established models. Such models require an in-depth understanding of the underlying chemical and physical processes within the plasma and at the glass–plasma/mask–plasma interfaces. We therefore present results that should pave the way for a better understanding of processes and thus for the extension of RIE processes toward innovative three-dimensional (3D) patterning as well as for the processing of chemically and structurally inhomogeneous silicate-based substrates. To this end, we present and discuss the results of a variety of microstructuring strategies for different application areas with a focus on micro-optics. We consider the requirements for refractive and diffractive micro-optical systems and highlight potentials for 3D dry chemical etching by selective tailoring of the material structure. The results thus provide first steps toward a knowledge-based approach to RIE processing of universal dielectric glass materials for optical microsystems, which also has a significant impact on other microscale applications. © The Authors. Published by SPIE under a Creative Commons Attribution 4.0 International License. Distribution or reproduction of this work in whole or in part requires full attribution of the original publication, including its DOI. [DOI: 10.1117/1.JOM.1.4.040901]

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1 Introduction

Micro-optical elements and complex optical microsystems require ultraprecise manufacturing processes. The maximum tolerable roughness is defined by fractions of the used wavelength λ, e.g., λ/100 or better, whereas the overall size and shape of the elements can easily reach the millimeter or centimeter range. Next to the industrially established ion beam polishing approaches for optical surfaces with ultra low surface roughness, reactive ion etching (RIE) has been demonstrated for the efficient realization of highly precise microstructured optical surfaces for beam-shaping and beam-splitting, as well as for imaging and illumination applications. During RIE, material transport is achieved by a combination of physical and chemical (reactive) interaction of ions and reactive gases with the surface in a plasma reactor. The chemical fraction of the process is naturally highly dependent on the substrate/precursor gas composition.

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Thus, the process has been developed for the semiconductor industry and is well-established and successfully applied for microstructuring of pure materials (e.g., semiconducting alloys such as GaAs, GaN, and others or Si)\(^7\) as well as pure fused silica (FS) substrates for optical purposes.\(^8\) Also polymers can be etched in a reactive plasma based on oxygen and in combination with other gases (if required).\(^9\) Significant advantages are provided as plasma etching does not necessarily require high process temperatures, while the energy of the individual etching species can be very high. This decoupling of temperature and energy is a significant advantage of plasma enhanced etching processes against purely chemical etching in which the activation energy is applied by temperature only. On the other hand, numerous effects influence the local material removal rate, so defined etching profiles require a detailed knowledge of the etching process.

Silicates are inorganic nonmetallic materials with a common basic unit, \(\text{SiO}_2\), and a large variety of structures built by different ways of connecting \(\text{SiO}_4\) tetrahedra via corners, edges, or faces. Therefore, silicates are available and utilized in the form of crystalline minerals, ceramics, glass ceramics, and glasses. Crystalline minerals are the raw materials for the production of the other forms. The versatility of structures from neso- to ino- to phyllosilicates [connected via secondary bonds, in covalent chains, layers, or three-dimensional (3D) frameworks] with and without long-range order and the variety of other elements that can be hosted as part of the connected structure or in the free volume is essential for their huge technical relevance. The main difference from organic polymers is the high thermal and chemical stability. In contrast to metals, silicates are isolators. In general, no free electrons occur in the untreated initial state. Mixed covalent and ionic bonds result in large bandgaps, in conductivity increasing with temperature, and in high optical transmission within a large window of wavelengths. The hardness of silicates is higher than that of organic polymers and metals in many cases. They are brittle with subcritical crack growth accompanied by a strong scattering of the practical strength. A high melting point above 1000°C is typical for crystalline compounds. Transformation temperatures for vitreous silicates are usually above 400°C. In vitreous silicates, nucleation and crystal growth can be controlled to produce glass ceramics with fine-tuned combinations of properties of glass matrix and crystal phases that would not be feasible with homogeneous materials. Figure 1 shows an overview regarding the range of adjustable properties of silicates in context with optical applications based on selected examples.

In this paper, we present results that pave the way for the extension of RIE processes for innovative 3D patterning as well as for the processing of chemically and structurally

| State | Vitreous | Semi-crystalline | Crystalline |
|-------|----------|------------------|------------|
| Type  | Single-component glasses | Multi-component glasses | In total | In subareas | Mono-crystals | Poly-crystals |
|       | Homogeneous | Phase separated |          |             | (one phase or multi-phase) |
| Examples | Fused silica | Soda-lime silicate | 
|         | | Alkaline-alumino-silicate | 
|         | | Optical glass | 
|         | | Borosilicate (bimodal) | 
|         | | Vycor® type (monomodal) | 
|         | | Zirconia | 
|         | | Macor® | 
|         | | Photosensitive glasses | 
|         | | 
| Characteristic and selected properties | High connectivity | Strong chemical bonds | High thermal and chemical durability | High mechanical strength | High transmission range | Low density and refractive index | 
|         | | Cheap production | Easy to handle | Different chemical compositions lead to tunable property profiles | 
|         | | Thermal expansion adapted to Si | Chemical durability | High mechanical strength | 
|         | | Zero thermal expansion between 90°C and 100°C | Good transparency for inspection | Malleable | 
|         | | Crystalisation in radiolysis exposed areas | 3D structurable | 
|         | | Anisotropic property profiles | 
|         | | 
| Application fields | Lenses | Mask blends | Layer anti-reflection, diffusion barrier, adhesion control | Waveguides | Solar modules | 
|         | | Ultraviolet protective glasses | 
|         | | 
| Potential for future optical applications | Doping for free-tuned properties | Durability adapted to etch process | Increased anisotropy in dry etching processes | Smooth surfaces | Porous glass with high specific surface | Diffuser | Microfluidic | 3D shaping of mechanically stable reorientations | 3D shaping of optical volume apertures | 

Fig. 1 Overview of silicate material types, properties, application fields, and their potential for optical applications.
inhomogeneous silicate-based substrates. This is of specific interest for optical applications since the optical and thermal properties of the microstructured substrate are controlled by the chemical material composition and have a significant impact on the overall elements or systems performance. To tune the functionality of the resulting optical microsystems, it is necessary to gain control over the complete hierarchy of 3D feature sizes, from the element shape at a mm to 100-μm scale to microstructures at the scale of the wavelength to nanostructures in the subwavelength range to surface roughnesses in the lower nm range and below. With respect to optical properties such as the intrinsic refractive indices, the chemical material composition (in the bulk material as well as at the surface) gains considerable significance (see Table 1). For precise microstructuring of optical glasses in general, e.g. it is crucial to understand the details of the chemical reactions and products generated during the RIE process.

The challenges related to the fabrication of micro-optical elements and optical microsystems are illustrated by the example of multilevel diffractive optical elements (DOEs) in Sec. 2. In Sec. 3, we introduce the fundamental RIE process providing the required control for the generation of unique micro-optical structures. High aspect ratio microstructures in FS and deep 2.5D optical microstructures for micro-optical systems integration are presented in Sec. 4. The (deep) etching and microstructuring of complex silicate-based materials enables the further expansion of the accessible element functionality. Microstructures with optical quality can be fabricated, e.g., in ultra low expansion glasses, using a tailored plasma etching process introduced in Sec. 5. An enhancement toward 3D micro-optical systems can be achieved by gradient index (GRIN) materials. The deposition of multilayer stacks with variable refractive index and the following tailored deep plasma structuring enables 3D in-plane micro-optics such as lenses for beam shaping as demonstrated in Sec. 5.2. In Sec. 5.3, the influence of the material structure on the etching behavior is investigated. The different levels durability of the material phases in the plasma process allows for the simultaneous generation of surface shapes with strongly varying optical properties. Finally, the combination of sophisticated etching processes in silicon with oxidation steps for the generation of 3D microresonators is presented in Sec. 6. High Q-factors of the resulting resonators with ultrasmooth sidewalls are possible due to the annealing effect during the oxidation of the 3D resonator profiles. The basic manufacturing processes from the selection of the functional material to the micro-optical functional structure are shown in Fig. 2.

2 Micro-Optics and Multilevel Diffractive Optical Elements

Optical microsystems are composed of surfaces and elements modulating an incoming light field in amplitude and phase. Depending on the surface profiles and the minimum feature sizes present in the elements, the effects of refraction or diffraction become dominant and determine design

Table 1 Optical properties of different optical materials used in the following sections.

| Material                        | Refractive index $n_d$ | Abbe number $v_d$ | Reference |
|---------------------------------|------------------------|-------------------|-----------|
| SiO$_2$ (thermal)               | 1.464                  | 67.2$^a$          | cf.$^{10}$ |
| Quartz crystal (uniaxial)       | 1.544                  | 69.7$^a$          | cf.$^{11}$ |
| FS (synthetic)                  | 1.458                  | 67.9              | 12        |
| Silicon oxynitride              | 1.47 to 2.3            | n. a.             | 13        |
|                                 | 1.45 to 2.05           |                   | 14        |
| ULE glass                       | 1.483                  | 53.1              | 15        |
| Zerodur                         | 1.542                  | 56.1$^a$          | cf.$^{16}$ |
| Foturan II (glass state)        | 1.512                  | 64.0$^a$          | cf.$^{17}$ |
| Foturan II (crystallized)$^b$   | 1.513                  | 64.1$^a$          | cf.$^{17}$ |

$a$Computed based on the given refractive indices.
$b$Crystallized at 560°C (lithium metasilicate glass ceramic).
approaches and fabrication concepts. The accurate transfer of steep analog profiles by etching needed for the fabrication of especially aspheric refractive microlenses is challenging and requires precise control of the etching performance. Alternatively, DOE may be used to approximate the refractive surface by exploiting the periodic nature of light and quantizing the desired phase profile in steps of $2\pi$. The continuous phase values can be further reduced to an integer number of discrete phase steps that are normally distributed uniformly. These quantized phase profiles may be used to illustrate the requirements of optical microstructures and their fabrication technologies.

Figure 3(a) shows the phase profile of a spherical (micro-)lens and the quantized approximations with four and two phase levels. While DOE are light in weight and compact while...
allowing for almost arbitrary phase functions, the main drawback is their limited efficiency as the light is diffracted into several orders. Theoretically, a binary phase element, such as a simple diffraction grating or Fresnel zone plate, can have a maximum efficiency of only 40% in the first order if the thin element approximation can be assumed. To achieve higher efficiencies, multilevel versions of DOEs are necessary, e.g., with 4, 8, or 16 phase levels.

The precise control of the etch rates as well as the quasi perfect perpendicular sidewalls enable the fabrication of such multilevel DOEs through a series of etching steps. The number of etched steps per $2\pi$ and the optical path difference corresponding to the introduced phase retardation between the etched and unetched levels determine the diffraction efficiency $\eta_m$ (i.e., the optical performance) of the element. A fabrication process with $N$ masks potentially produces $2^N$ phase levels.

Despite these conceptually straightforward relations between the individual features in the DOE and its performance, it is surprisingly easy to run into significant challenges when fabricating DOEs. In real fabricated structures, there is always some degree of deviation from the ideal shape resulting from deviation in the height of the phase steps, nonvertical sidewalls, rounding of corners, increased surface roughness, and mask alignment errors, to name a few. These errors directly influence the power distribution between the various diffraction orders generated by the DOE. In any optical application, the quantitative measure for the required precision is related to the wavelength $\lambda$. Thus, as a rule of thumb, any surface (or sidewall) of the microstructured optical element needs to be fabricated with a precision of better than $\lambda/10$, i.e., with deviations of less than a few tens of nanometers. Depending on the number of phase steps, these requirements for the DOE implementation may even be significantly higher. For analog refractive micro-optical elements, the shape of the profile decides the elements performance. In this context, the stability of the etching process during etching periods of potentially several hours is absolutely crucial.

The overall effect of fabrication deviations strongly depends on the specific DOE design. Beam fanout elements suffer from changes in the locations of phase transitions leading to non-uniformity in the intensity distribution. Dammann grating-based beam fanouts show a strong dependence on transition point errors. A differing etch depth results mainly in a zero-order change, while the other orders remain uniform. Surface roughness leads to increased background light. In general, the larger the number of phase steps is, the bigger the fabrication challenges are due to the necessary etching precision and lithographic resolution. Consequently, the fabrication of quasicontinuous phase profiles, e.g., through gray scale lithography, poses the most extreme challenges to the fabrication processes. Additional requirements arise for efficiently achromatized or polarization-sensitive diffractive elements as well as for integrated 3D optical microsystems. They often require the fabrication of extremely high aspect ratios and possibly the processing of more complex optical glasses with adapted refractive indices. These requirements on the optical microstructures define the challenges on the etching technology applied during the fabrication process. The plasma-based RIE process potentially provides the necessary control over the etching profile in a wide range of materials relevant for optical applications.

### 3 Reactive Ion Etching Process

RIE is cross-scale patterning method developed for microelectronic materials, such as silicon, silica, silicon nitride, and other semiconducting materials, which combine physical and chemical etching mechanisms. Whereas RIE etching with a large chemical contribution provides high etch rates, e.g., in silicon, the etch rate for SiO$_2$, is very low (with fluorine radicals: $1/40^\text{th}$ of silicon). Physical etching with ions (sputter etching, e.g., Ar) exhibits low selectivity against resists and other mask materials as well as a low etch rate. The combination of physical and chemical effects in the RIE process allows for a reasonable etch rate as well as a sufficient selectivity against mask materials through a combination of ion bombardment and chemical reactions adapted to the substrate material. The process is adaptable to a wide variety of materials and has thus become a standard technology in microelectronics and microsystems technology.

In a cold nonthermal plasma, inelastic collisions with high-energy electrons lead to excitation, dissociation, and ionization of gas molecules, resulting in a number of different chemically...
active radicals, inert as well as reactive ions and electrons. The plasma is typically based on an
abnormal glow discharge with a distinct cathode fall in front of the substrate. For nonconductive
glasses, RF-driven electrodes are mandatory to avoid a self-charging layer that would protect the
surface from ion bombardment.

The ions provide additional kinetic energy for chemical surface reactions. Chemical etching
takes place with reactive ions as well as radicals as long as the product exhibits a sufficiently
high vapor pressure. Non-volatile by-products can stop the etching process. On the other hand,
accelerated ions (inert or reactive) are able to knock out atoms from the surface (sputter etching),
even non-volatile by-products.38,39

The evolution of an anisotropic profile (here almost vertical trenches in place of isotropic
spherical grooves) is defined by directed energetic ions and inhibitor-induced anisotropy.
In low-pressure plasmas, the directionality of ion bombardment causes a preferred removal at
vertical incidence (bottom), whereas a sidewall polymer layer inhibits the lateral etching of
the material.40 Thus, surfaces oriented perpendicular to the ion incidence usually show a higher
etch rate than the sidewalls of the structures.41

The overall etching is defined by the amount of chemically active species in the plasma, their
diffusion onto the substrate surface and the flux, the angular distribution, and the kinetic energy
of the positive ions accelerated to the substrate surface.

The interaction between the plasma and the material is controlled by the process parameters.
The selected gases influence the spectrum of the (reactive) neutrals, the (reactive) ions as well as
a potential surface polymerization and the reaction products and thus their volatility. The amount
of chemically reactive neutrals is influenced by the source power, the process pressure, and the
gas flow that influence the residence time in the plasma. The ion density is determined by the
source power and the kinetic energy by the bias (self-bias or bias power). The angular distribu-
tion is affected by the process pressure, which is a measure of the mean-free path length.
Variation of the plasma–material interaction enables a wide range of etching profiles from almost
isotropic etching to directed anisotropic etching.42–44

Compared with chemically simple and homogeneous materials such as silicon, plasma etch-
ing of complex silicate glasses is significantly more challenging. Due to the high binding energy
and the heterogeneous material character of glasses, effective etching demands sufficient acti-
vation energy by ion bombardment. The low thermal conductivity of glasses (about 100 times
lower than for silicon) and the energy introduced by ion bombardment require sufficiently tem-
perature-stable mask materials. In complex optical glasses, various reaction products are formed.
Many of them are non-volatile and accumulate at the surface. In particular, (earth-)alkali metals
result in halides with low vapor pressure. Their removal requires sputtering by ion bombardment.
This reduces surface roughness but also keeps the etch rate high.45–49 A schematic overview of the
etching process in an inductively coupled plasma RIE (ICP-RIE) tool for etching complex
glass compositions is shown in Fig. 4.

Continuous plasma processes with fluorocarbon gases are often used for the etching of
quartz, vitreous silica, and other glasses.35,50–59 In this case, the sidewall is protected by an intrin-
sic passivation layer while the bottom is ablated simultaneously. At the bottom, ideally, a thin
steady-state polymer is formed, which does not significantly reduce the ion energy but contrib-
utes to chemical reactions at the surface. During etching of dielectric materials, it is observed that
charging effects influence the direction of the ions and thus cause etch stops in high aspect ratio
features.1,50 The surface polymer can no longer be removed at a sufficient rate and inhibits the
etching.60 SF6 is also used for glass etching,46,48,51,52,61,62 partly in combination with fluorocar-
bons or Ar.47,49,63–66 SF6 does not support the formation of polymer layers and thus enables a
physical ion impact on the substrate material, e.g., for more efficient removal of non-volatile
reaction products.42,49

Currently, ICP-RIE machines are mainly used for high etch rates and the generation of large
etch depths. Compared with capacitively coupled plasma, the plasma density of inductively
coupled plasma (ICP) is significantly higher, and the ion energy can be controlled by the bias
power separately from the plasma generation. The possibility of generating the plasma at lower
pressures facilitates the formation of volatile reaction products and improves the removal of non-
volatile reaction products by directed ion bombardment.7,49,67 This allows for etch rates of about
1 μm/min\(^{56,61,62}\) with vertical sidewalls and high aspect ratios\(^{47,51,55,56}\) in FS and borosilicate glasses (BSGs) with fluorocarbon gases, SF\(_6\), or a mixture of both (Table 2).

Classical masking layers made of organic resists result in low selectivities (relative etch rates) when structuring glasses and are therefore interesting for lower etch depths and low thermomechanical stresses.\(^{46,54,57,71}\) For deep etching with high etch rates, on the other hand, thin-film hard masks (e.g., AlN, Al, Cr) or electrodeposited Ni layers\(^{47,51,57,63}\) are used.\(^{52,58,62}\) They provide high selectivity because they are stable chemically as well as against high temperatures and ion bombardment. Optimized mask materials and properties are also the focus of current research. For example, mask materials such as ruthenium provide selectivities of over 300 in fluorine plasma when patterning thermal SiO\(_2\) thin films.\(^{72}\) A targeted discharge of conductive metal masks also shows an influence on the patterning process in current studies.\(^{61}\)

4 Deep RIE for Integrated Optical Microsystems

For free-space micro-optical systems, the alignment of individual components is a challenging task and usually accounts for a significant portion of the total manufacturing effort. Monolithic integration concepts can help to overcome this issue; however especially for in-plane optical elements for the visible wavelength range, optical surfaces have to fulfill critical demands. Deep-etched vertical structure profiles with low surface roughness \(Ra\) of the sidewalls (below...
10 nm in the visible range) are needed for high quality integrated optical modules. Their fabrication from bulk substrates through surface micromachining requires a highly controlled deep etching process with stable etching masks, high selectivity, and high-quality edges. An exemplary process flow to fulfill the requirements is shown by Weigel et al. The etching was performed by ICP-RIE in a fluorine-based plasma at a pressure of 0.35 Pa using CHF₃ and SF₆. The best process conditions were found at a gas ratio of CHF₃/SF₆ with an overall gas flow of 30 sccm. Etching rates of up to 300 nm/min have been demonstrated. The selectivity between the utilized nickel mask and the FS substrate was found to be as large as 20. Thus, quasivertical sidewalls of about 100 μm in etch depth and a sidewall angle of 88° were achieved. By increasing the amount of CHF₃/SF₆ to a ratio of 1:1, the arithmetic mean roughness (Ra) is decreased to about 7.2 nm [Fig. 5(c)]. The etching face exhibits Ra values between 8 and 30 nm. Both values have been demonstrated to be suitable for decent micro-optical applications.

Mirrors can be realized using reflective coatings on the smooth sidewalls. To define these structures, a lift-off technique can be used. A negative resist (AZ nLof 2070) is spray-coated in a four-layer-process and structured by UV-lithography [Fig. 5(b)]. Suitable reflective coatings are based on aluminum that exhibits a strong adhesion on glasses.

### Table 2 Selection of published results on deep etching of FS, BSG, and crystalline quartz.

| Reference | Material | Etch tool | Process gases | Mask material | Etch rate (nm/min) | Aspect ratio | Selectivity | Etch depth (μm) | Sidewall angle (°) |
|-----------|----------|-----------|---------------|---------------|-------------------|--------------|-------------|----------------|-----------------|
| 52        | FS       | ICP-RIE   | C₄F₈/O₂       | Al            | 520               | 2            | 20          | 10             | 83              |
| 52        | FS       | ICP-RIE   | SF₆           | AlN           | 320               | 2            | 49          | n.a.           | n.a.            |
| 51        | FS       | ICP-RIE   | C₄F₈/He/O₂    | Si            | 600               | 3.5          | 3.5         | 300            | 86              |
| 51        | FS       | ICP-RIE   | C₄F₈/O₂       | Ni            | 700               | 2.5          | 35          | 80             | 78              |
| 55        | FS       | ICP-RIE   | C₃F₈/O₂       | Ni            | 500               | 10           | 10          | 100            | 89              |
| 58        | FS       | ICP-RIE   | C₄F₈/Ar       | Al            | 487               | n.a.         | n.a.        | 48.7           | 90              |
| 58        | FS       | ICP-RIE   | C₄F₈/Ar       | Al            | 758               | n.a.         | n.a.        | 75.8           | 82              |
| 61        | FS       | ICP-RIE   | SF₆/NF₃/H₂O   | Ni            | 1000              | 10           | n.a.        | n.a.           | n.a.            |
| 63        | FS       | ICP-RIE   | SF₆/CHF₃      | Ni            | 300               | 10           | 20          | 100            | 88              |
| 54        | FS       | NLD       | C₃F₈/CHF₃/Ar  | Resist        | 420               | n.a.         | n.a.        | 35             | 89              |
| 64        | FS       | RIE       | CF₄/CHF₃/Ar   | Resist        | 55.4              | 1.13         | 20          | 85             | n.a.            |
| 64        | FS       | RIE       | SF₆/CHF₃      | Resist        | 93.3              | 0.26         | 20          | 85             | n.a.            |
| 56        | Pyrex    | ICP-RIE   | C₄F₈/O₂       | Ni            | 1000              | 20           | 18          | 200            | 88              |
| 47        | Pyrex    | ICP-RIE   | SF₆           | Ni            | 600               | n.a.         | 20          | 200            | 88              |
| 62        | Pyrex    | ICP-RIE   | SF₆           | Cr            | 1200              | n.a.         | 24          | n.a.           | n.a.            |
| 62        | Pyrex    | ICP-RIE   | SF₆/Ar        | Cr            | 1000              | n.a.         | 34          | n.a.           | n.a.            |
| 61        | BSG      | ICP-RIE   | SF₆/NF₃/H₂O   | Ni            | 720               | 10           | 27          | 103            | 87              |
| 57        | BSG      | NLD       | C₃F₈/Ar       | Ni            | 350               | 8            | 70          | 100            | 84              |
| 56        | Quartz   | ICP-RIE   | C₄F₈/O₂       | Ni            | 735               | n.a.         | 100         | 12.5           | 85              |
| 68        | Quartz   | µW-RIE    | CF₄/Ar        | Ni            | 100               | n.a.         | n.a.        | n.a.           | n.a.            |
| 69        | Quartz   | DRIE      | C₄F₈/O₂       | Resist        | 450               | n.a.         | 1.25        | 30             | 75              |
| 70        | Quartz   | RIE       | CHF₃/CF₄     | Resist        | 68                | n.a.         | n.a.        | n.a.           | n.a.            |
The described process flow can be used for realizing free-space monolithic optical microsystems such as interferometer structures as shown in Fig. 5(a). This new kind of in-plane monolithic, free-space interferometer reached a resolution of 20 nm in the first demonstration experiments. The high achievable aspect ratios of 10:1 enable a spatially tight arrangement of multiple depth-etched structures with lithographic accuracy without further alignment effort. This is a significant advantage when multiple micro-optical structures need to be combined.

5 Microstructuring of Special Silicate Substrates

The possibility of deep etching high-quality mirror surfaces with quasivertical sidewalls, presented in Sec. 4, represents an important step toward the fabrication of integrated optical microsystems. The use of optical glass with customizable properties can further enhance the optical performance. The potential to adapt RIE etching processes to the ultraprecise microstructuring of a large variety of silicate-based dielectric substrates marks a tremendous step that offers increased design flexibility for optical microsystems. Although up to date predominately FS substrates have been accessible for microstructuring, in the following, we demonstrate the increased design flexibility available with innovative new RIE processes for optimized multi-component silicate materials, enabling a large variety of optical properties. This is also due to the high requirements of optical systems, such as low roughness, accurate step height at low resolution, and the generation of vertical sidewalls as previously discussed for diffractive and refractive structures. We show in Sec. 5.1 that an adapted RIE process allows for the implementation of depth-etched structures in optical quality even in multicomponent materials such as ultra low expansion (ULE) glass.

However, to achieve more general optical functionality, such as focusing or beam shaping, the implementation of real 3D shaping is required, e.g., to fabricate curved vertical optical surfaces. Since precisely controlled etching techniques for 3D shaping are still missing, the potential of light deflection in GRIN media can be exploited in the vertical coordinate. In this case, the challenge again is put on the etching techniques since processes and recipes for the etching of complex material compositions with high precision are needed.

5.1 Microstructuring of Ultra Low Expansion Glasses

Materials with very low thermal expansion, such as ULE glass or Zerodur glass-ceramics, are particularly interesting for applications in which the geometric variables of a system must be temperature-independent, for example, for masks for blanks in EUV lithography, for substrates in projection optics, and in precision metrology.\textsuperscript{74–79}

Ultra low expansion glass-ceramics are complex in composition and structure (e.g. Zerodur), whereas ULE glass is a single-phase vitreous material consisting of SiO\textsubscript{2} and TiO\textsubscript{2}.\textsuperscript{80–82} As described earlier, material complexity has a strong effect on the patterning process. During the etching of glass ceramics and other complex glasses, a large amount of non-volatile reaction...
products is generated, which makes structuring more difficult in a fluorine-based plasma. In particular, the metal fluorides (e.g., AlF$_3$, NaF$_2$, and more) do not reach a sufficiently high vapor pressure at the surface conditions and thus accumulate on the substrate surface. An overview of selected reaction products in fluorine plasma and their volatility classification at commonly used process conditions is shown in Fig. 6.

By contrast, and with the use of optimized process conditions, the etching of ULE glass generates only volatile reaction products. Thus, the special glass can be patterned comparable to FS with high etch rates, high selectivity, high verticality of the sidewalls, and low surface roughness. A direct comparison of etching results in FS, ULE glass, and Zerodur has been presented elsewhere and is summarized in Fig. 7.

This is the first detailed investigation and demonstration of micropatterning of low expansion materials using RIE. With the introduced processes, it is thus possible to close the gap between conventional patterning and microstructuring for the integration in micro-optical, -mechanical,

| Material / Etch gases | SEM images of different deep etched structures with nickel hard mask | Process results |
|-----------------------|---------------------------------------------------------------|-----------------|
| Zerodur SF$_6$/Ar     | ![SEM images](image1)                                          | Etch rate [nm/min]: 240  |
|                       |                                                                | Selectivity: 8    |
|                       |                                                                | Sidewall angle [deg]: 71 |
|                       |                                                                | Roughness Ra [nm]: 27 |
| ULE glass SF$_6$/CHF$_3$ | ![SEM images](image2)                                       | Etch rate [nm/min]: 380  |
|                       |                                                                | Selectivity: 26   |
|                       |                                                                | Sidewall angle [deg]: 86 |
|                       |                                                                | Roughness Ra [nm]: 30 |
| Fused silica SF$_6$/CHF$_3$ | ![SEM images](image3)                                 | Etch rate [nm/min]: 300  |
|                       |                                                                | Selectivity: 20   |
|                       |                                                                | Sidewall angle [deg]: 88 |
|                       |                                                                | Roughness Ra [nm]: 50 |

Fig. 7 Comparative SEM images of depth-etched structures with different sizes (trench widths between 10 and 100 μm) in materials with low thermal expansion and determined process parameters for etch rate, selectivity, sidewall angle, and roughness of the etched bottom (adapted from Ref. 66).
and fluidic systems. Applications such as released spiral springs have successfully been demonstrated in a glass ceramic with ultra low thermal expansion. Due to its higher refractive index \((n_d = 1.4828)\) and lower Abbe number \((v_d = 53.1)\) as compared with FS, ULE glass offers further design options for micro-optical applications (e.g., refractive functional structures such as dispersion prisms). The high aspect ratios in ULE glass allow for deep etching of multiple micro-optical elements tightly together comparable to the above-mentioned results in FS. The optimization of the sidewall roughness as an important parameter for integrated optical structures with lateral beam injection is the focus of the current work.

### 5.2 Integrated 3D Microstructured GRIN Lenses

Planar lithographic fabrication techniques offer ultraprecise alignment for micro-optical applications, but in general 3D beam shaping is required for flexible optical systems design. This cannot be achieved with 2.5D (deep) structuring only and requires variable optical properties in the vertical dimension, which can be realized by GRIN systems. Hybrid GRIN lenses using different mechanisms for light deflection in vertical and horizontal directions are feasible with optimized RIE structuring and are suited, e.g., to wafer-level coupling of optical and optoelectronic components. To this end, a sequential approach for the well-defined deposition of thin layers with slightly varying material composition has been demonstrated and combined with the planar RIE approach. This planar stack of materials effectively forms a one-dimensional GRIN material in which the light propagation perpendicular to the substrate is determined through the refractive index variation.

3D optical functionality can thus be reached with 2.5D structuring methods. The variation of the refractive index during the layer deposition process is used to enable the control of the light propagation in the vertical direction, whereas deep 3D etching determines the optical functionality via the shape of the surface in the orientation of the substrate surface. In the vertical direction, a properly designed stepwise variation of the refractive index during the layer deposition produces GRIN elements leading to a focusing effect perpendicular to this direction. In the second direction, parallel to the substrate, the geometrical profile achieved by vertical etching of the optical layer stack determines a beam shaping property. The combination of these technological approaches leads to an optical element that can influence light propagation in directions both parallel and perpendicular to the substrate surface.

GRIN materials include optical glasses, plastics, germanium, zinc selenide, and sodium chloride. The techniques for the generation of different refractive indexes involve thereby neutron irradiation, polymerization, ion exchange, and CVD processes. The latter process can be seamlessly integrated into microtechnological fabrication, and various optical properties can be reached by varying the chemical composition of the silicon oxynitride layer.

For the demonstration of this concept, the GRIN layer was fabricated as a stack of 115 layers of silicon oxynitride of varying material composition. We used plasma-enhanced chemical vapor deposition (PECVD) with different \(\text{SiH}_4: \text{N}_2: \text{N}_2\text{O}\) gas ratios to produce layers with refractive indices between those of almost pure silica and almost pure silicon nitride. Thus, the refractive index could be varied from 1.47 to 1.85 in the stack with an overall thickness of 20 \(\mu\)m. The microlenses were then etched perpendicular to the substrate by an optimized fluoro-based ICP-RIE. For the etching process, we reverted to the previously shown patterning process using a nickel hard mask in a \(\text{SF}_6/\text{CHF}_3\) plasma. Figures 8(b) and 8(c) show that the sidewall angle and roughness could be controlled precisely despite the inhomogeneous substrate materials.

### 5.3 Plasma-Supported Etching of Photosensitive Glasses

By considering photosensitive silicate materials, we present in this section an additional degree of freedom for the 3D design of micro-optical elements. The combination of photoinitiation with plasma-based etching techniques opens up new possibilities for the technological realization of 3D profiles for optical microsystems and extends the understanding of plasma-based etching processes.
5.3.1 Photoform process for micro-optical components

Photosensitive lithium alumino silicate glasses doped with minute amounts of oxides of cerium, silver, antimony, and tin/zinc can be microstructured via a three-step photoform process. The original glasses themselves, e.g., Foturan or FS21, conceptually behave like a photoresist. Therefore, it is possible to apply the following standard processing sequence (see Fig. 9):

1. masking of the glass substrate and exposure to UV light,
2. thermal treatment for lithiummetasilicate (LMS) crystal growth initialization in the exposed areas (glass ceramic phase), and

![Diagram](image-url)

**Fig. 8** (a) Principle of 3D beam shaping by a GRIN lens; (b) and (c) SEM pictures of fabricated GRIN lenses using PECVD deposition and subsequently plasma structuring on a silicon substrate.

**Fig. 9** 2.5D photoform process by parallel UV light (above); simultaneous patterning process by wet and dry chemical etching processes (different etch selectivity between crystallized and vitreous material phases leads to the formation of a surface pattern depending on the used process).
3. formation of geometrically defined microstructures by means of wet chemical etching using diluted hydrofluoric acid with a phase selective etch rate.

Direct laser writing enables the local introduction of defined amounts of optical energy into the volume and, thus, the generation of buried 3D geometries, e.g., for optically transparent, fluidic systems.\textsuperscript{87–90} (see Fig. 10). Surface topography and surface energy enable control to produce smooth surfaces with optical quality for imaging systems.\textsuperscript{91–95} Roughness can be adopted specifically for the attachment of living cells in tissue engineering.\textsuperscript{90} Other processing operations typical for glass, such as ion exchange or glass crystallization, enable the optimization of properties such as refractive index profile, spectral absorption, or mechanical strength. The applications are manifold, e.g., micromechanical and microfluidic functional elements can be functionalized with additional beam shaping and a filtering micro-optical component based on one material.\textsuperscript{96,97}

5.3.2 Fluorine-Based Plasma Etching Process Versus Wet Chemical Etching

In the described process, wet and dry chemical etching processes are suitable for etching either the glass or the crystalline phase, with significant differences in the achievable etch rate selectivity. The clarification of basic reactions providing selectivity is part of current research. So far, wet chemical etching has been the dominant shaping method in the photoform process. In general, the etching attack of hydrofluoric acid on a silicate network is described by the overall chemical reaction scheme:

\[ \text{SiO}_2(\text{s}) + 6\text{HF}(\text{l}) \rightarrow 2\text{H}_2\text{O}(\text{l}) + \text{H}_2\text{SiF}_6(\text{aq}) \].

The underlying mechanism is not yet clearly understood, and several reaction steps are discussed in this context.\textsuperscript{98–102} However, their detailed understanding is necessary for precise control of the variables influencing the etching process. Several investigations suggest that water species play an important role in the attack of silicon–oxygen (siloxane) bonds.\textsuperscript{100,103} According to Ernsberger,\textsuperscript{98} the incorporation of water species locally changes the degree of cross-linking of the silicate network, so F\textsuperscript{−} ions primarily replace OH\textsuperscript{−} groups, whereby the network is progressively dissolved. Kline and Fogler\textsuperscript{99,104} described three models of interaction of HF with silicate surfaces and point out that water presence is a prerequisite. Spierings\textsuperscript{102} considered the presence of HF and HF\textsubscript{2}\textsuperscript{−} rather than F\textsuperscript{−} to be crucial. Adsorption and chemisorption of the reactive species and the effect of adsorption at the siloxane bonds dominate the dissolution process. Achievable etch rates depend on the connectivity of the glass and glass ceramic phases and are subject to parameters such as etchant concentration, temperature, time, and transport processes in the boundary layer between the etchant and substrate surface. Wet chemical etching is characterized by a high selectivity between glassy and crystallized areas, where the crystallized phase exhibits a much higher solubility in the etchant with typical etch rate ratios around 1:30.\textsuperscript{90}

RIE of photosensitive glasses appears to be significantly different from wet chemical etching. This is evident from the observation of an inversion of the etch selectivity between glassy and crystalline phases; see Fig. 9.

A fluorine-based plasma etching was performed using a CF\textsubscript{4}/H\textsubscript{2} mixture. The samples were examined with SEM after the plasma etching. The result is shown in Fig. 9 in comparison with a
wet chemically etched sample. The etch rate at the crystallized areas is lower than the glass etch rate. This result is in contrast to wet etching and points to the complexity of network or lattice dissolving mechanisms accompanied with the mechanical attack of ions during the dry etching process. First investigations indicate that the availability of water species in the glass and glass ceramic structure has a decisive influence on fluorine activity. The impact on photosensitive glass treatment has hardly been investigated so far. One study reporting on H relevance to dry etching by Anthony et al. investigated a Ga$^+$ focused ion beam process for Foturan glass. They reported for the first time an experimental sputter yield of 0.23 $\mu$m$^3$ nC$^{-1}$ for 30 keV Ga$^+$ irradiation of Foturan. They assume a mechanism based on the deep implantation of protons in combination with the generation of secondary electrons that massively damages the bonds of the glass structure.

The characteristic values of micro-optical components made of photosensitive glass are controlled by the chemical composition and the microstructure of glassy and crystalline areas. The refractive index and optical transmission are determined by the material, i.e., components, density, and internal interfaces. The surface roughness, the topography of spheroidal etch patterns, and the geometry of volume diaphragms are largely determined by the microforming process. According to Lambert–Beers law, the absorption is dependent on the concentration of absorbing species and on the thickness of the absorbing layer. The use of dry etching techniques allows thin transparent glass areas to be placed next to thicker nontransparent glass ceramic areas in one monolithic component. Another characteristic is the surface roughness, which is the result of the etch selectivity between the individual LMS crystals and the glass environment around each individual crystal. Dry-etched glass ceramic surfaces differ significantly from wet-chemically prepared glass surfaces. In both cases, the roughness depends on the size and distribution of the LMS crystals. The high solubility of the LMS crystals in a wet chemical etching process leads to cavities in the glass matrix, which develop into a typical pattern of spherical depressions by overetching. According to current knowledge, dry etching processes are significantly influenced by the formation of passivation layers on the silicate glass substrate surface. Self-masking effects dominate the surface topography. Using photosensitive glasses, the influence of structural heterogeneities in the glass and glass ceramic phase on etch selectivity is currently being investigated. Future investigations will focus on optimizing the etch selectivity with the aim of smooth surfaces. Realizing dynamic conditions in dry etching regarding gas mixtures, pressures, and temperatures offers a particularly high potential for future microforming processes of optical components, i.e., for nonplanar 3D volume diaphragms (Fig. 10). The plasma-based dry etching process for the microstructuring of photosensitive glasses is an innovative approach and therefore the subject of current research. In the context presented, the requirement for an etching process is to achieve precision across scales, from the mm to nm range. The main questions include the following: (i) What potential do photosensitive glasses offer in connection with a dry etching process for the production of micro-optical components, i.e., with high aspect ratios? (ii) What mechanisms underlie the etching attacks in glass and glass-ceramic phases? (iii) How can these be controlled to produce surfaces with a defined optical quality?

6 Fabrication of 3D Microresonators

In this section, we introduce an additional degree of freedom available during the fabrication process of 3D profiles for optical microsystems. The integration of an oxidation step for material conversion turns out to be highly beneficial for the fabrication of well-defined 3D optical microstructures such as optical microresonators with high $Q$-factors. Our concept is to use the well-established 2.5D micromachining of silicon for determining the overall shape of the resonator. A suitably integrated oxidation step then allows the resonator layer to be converted into the dielectric $\text{SiO}_2$ layer. The annealing process coming along with the oxidation guarantees extremely smooth sidewalls of the resonator layer, which is reflected in the high $Q$-factors that could be demonstrated for the optical elements.

The fabrication of whispering gallery mode resonators using state-of-the-art plasma etching is a challenging endeavor. High $Q$ factors and, therefore, low loss can be achieved by confining the light at the cavity boundary due to total internal reflection. Therefore, a low surface roughness at the cavity boundary is vital to avoid scattering losses and thus lower $Q$-factors.
The established fabrication process applied for whispering gallery resonators thus includes a postprocessing step that heats the resonator until it starts to melt and forms a donut-like shape since the silicon pad underneath acts as a heat sink. Due to these postprocessing steps, which effectively represent an individual treatment of each resonator separately, it is not easy to scale this process. However, it has been shown that a wafer scale fabrication process is feasible by integration of a thermal annealing process.

We realized a fabrication technique that allows for the fabrication of several thousands of high $Q$ factor ($>10^5$) whispering gallery resonators using state-of-the-art i-line lithography and fluorocarbon etching tools. Furthermore, we developed a particular fabrication workflow with a self-limiting postprocessing step conducted at the wafer level. For this, we create a 2.5D resonator profile out of a silicon substrate using a combination of passivation, passivation etch, and anisotropic and isotropic etch steps using $SF_6$ and $C_4F_8$ or cryogenic $SF_6$ and $O_2$ as feed gases as shown in Fig. 11. Since the etching of 2.5D in silicon profiles is well understood, we have more flexibility for structuring as compared with silicon dioxide etching. After the etching, we use a thermal oxidation furnace to create an amorphous silicon dioxide shell with a thickness from a few hundred nanometers up to $5 \, \mu m$. The necessary thickness of the amorphous $SiO_2$ shell is determined by the amount of surface damage caused during the etching steps. We remove the shell by a wet chemical HF dip. After this step, we obtain a very smooth silicone resonator with a surface roughness of $R_q \leq 0.8 \, nm$. Then, we use an additional oxidation step to produce the shell, which is used to guide light into the resonator. A critical point is the thickness of the silica shell in comparison with the wavelength. A thickness that is smaller than two wavelengths leads to mode migration into the silicon core. Simulations show that a thickness of several $\mu m$ (i.e., three to five times the wavelengths) should be sufficient to avoid mode migration.

7 Conclusion and Outlook

We demonstrated a broad variety of technological processes for the fabrication of 3D micro- and nanostructures for optical microsystems. In all cases, extraordinarily well-defined etching is a crucial part of the fabrication process. The presented results show that plasma-based etching processes allow for a broad range of 3D shapes and surface properties in different kinds of silicate-based optical glasses ranging from pure silica to low expansion materials, photosensitive glasses, and thin amorphous silica layers. These encouraging results show the potential of this structuring technology for various optical applications. Figure 12 shows a summary of the various fields of application, the structuring requirements, and the relevant process parameters.

Nevertheless, numerous challenges and potential for future research activities remain, specifically for knowledge-based etching of complex silicate materials (glasses, glass ceramics), which are of special interest for optical microsystems. Although many of the results achieved so far are still gained through experience-based optimization of the suitable processing parameters, in many cases the understanding of the underlying chemical and physical processes during the interaction of the plasma and the silicate substrates is still fragmentary. Due to the huge potential of 3D micro- and nanostructures fabricated in this class of materials with flexibly tunable...
material properties (cf. the numerous types of optical glasses), it is easy to foresee tremendous interdisciplinary scientific potential for this area.

Future research activities need to deepen the understanding and technical control of glass etching for optical microsystems. This includes, first, the in-situ observation of chemical and physical processes within the plasma and at the glass–plasma/mask–plasma interface. Based on an improved understanding of this interaction, the processes will be adapted with respect to the different optimization goals that are required within a complex optical microsystem with 3D microprofiles and specific localized surface properties. The interaction between process, material, and mask and their specific influence plays an important role. Interdisciplinary research activities need to cover the whole range from the physical understanding and technical control of the plasma generation and formation, the in-situ observation and characterization of the reactions in the plasma and at the substrate surfaces all the way to the chemical interaction between the reactive gases and the glass surfaces. This will be accompanied by research on the huge range of applications for the resulting 3D microstructures in optical microsystems.

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**Fig. 12** Overview of micro-optical systems generated in glass, the requirements from the application side as well as the used processes and masking technologies.

| Applications | Requirements | Processes |
|--------------|--------------|-----------|
| 2.5D diffractive | | |
| 2.5D refractive | - Defined etch depth  
- Low sidewall roughness of etch bottom  
Ra < λ / 20  
- Aligned step profile | Etch tool: ICP-RIE  
Etch gases: CHF₃  
Process pressure: 0.25 - 0.3 Pa  
Process temperature: 30°C  
Mask material: Resist |
| 3D beam shaping | - Vertical sidewalls  
- Low sidewall roughness  
Ra < λ / 20  
- High etch depth  
- Defined GRIN layer thickness | Etch tool: ICP-RIE  
Etch gases: SF₆/CHF₃  
Process pressure: 0.35 Pa  
Process temperature: 20°C  
Mask material: Ni (plated) |
| 3D optical resonators | - Low sidewall roughness at cavity boundary  
- 3D shape profile  
- Oxide layer thickness (3-5 times wavelength) | Etch tool: ICP-RIE  
Process steps:  
1. Cryogenic anisotropic etch  
(SF₆/O₂, 1 Pa, -120°C)  
2. Passivation  
(C₄F₈, 4 Pa, 0°C)  
3. Passivation etch  
(SF₆/C₄F₈, 2.6 Pa, 0°C)  
4. Isotropic etch  
(SF₆, 5.3 Pa, 0°C)  
5. Thermal oxidation of Si structures  
Mask material: Resist or hard mask |
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