Giant bubble pinch–off

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Self-similarity has been the paradigmatic picture for the pinch-off of a drop. Here we will show through high-speed imaging and boundary integral simulations that the inverse problem, the pinch-off of an air bubble in water, is not self-similar in a strict sense: A disk is quickly pulled through a water surface, leading to a giant, cylindrical void which after collapse creates an upward and a downward jet. Only in the limiting case of large Froude number the neck radius scales as $h(-\log h)^{1/4} \propto \tau^{1/2}$, the purely inertial scaling. For any finite Froude number the collapse is slower, and a second length-scale, the curvature of the void, comes into play. Both length-scales are found to exhibit power-law scaling in time, but with different exponents depending on the Froude number, signaling the non-universality of the bubble pinch-off.

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The pinch–off of a liquid drop is a prime example of a hydrodynamic singularity and has been studied extensively in recent years. It has become paradigmatic for self–similar behavior in fluid dynamics: After appropriate rescaling, the shapes of the pinching neck at different times can be superimposed onto a single shape. With the exception of some pioneering work, the inverse problem of the collapse of a gas–filled neck surrounded by a liquid has not attracted much attention until very recently, with the analysis of the pinch–off of a bubble arising from a needle and the break–up of a gas bubble in a straining flow. The time–evolution of these collapsing gas–filled necks is found to follow a power law. If the dynamics near the singularity are solely governed by liquid inertia, then the radius of the neck $h$ expressed in the time $\tau$ remaining until collapse scales as $h \propto \tau^{1/2}$ or, with a logarithmic correction, as $h(-\log h)^{1/4} \propto \tau^{1/2}$. Deviations from this exponent of $1/2$ are reported to occur only due to the inclusion of other effects. The collapse may be slowed down by viscosity ($h \propto \tau^{2/3}$) or surface tension ($h \propto \tau^{2/3}$), or accelerated by the inertia of the gas flowing inside the neck, leading to $h \propto \tau^{1/3}$.

In this paper we focus on another example of this “inverse pinch-off”, namely the violent collapse of the void created at a fluid surface by the impact of an object. Here we find exponents which deviate substantially from $1/2$, even though the dynamics are shown to be purely governed by liquid inertia, without significant contributions from the effects mentioned above. The self-similar behavior $h(-\log h)^{1/4} \propto \tau^{1/2}$ appears to hold only in the asymptotic regime of very high impact velocities.

In our experiment, a linear motor is used to drag metal disks with radii $h_{disk}$ between 10 and 40 mm through an air/water interface with a well-controlled, constant velocity $V$ between 0.5 and 3 m/s (see Fig. 11). A rod running through a seal in the bottom of a large water tank connects the disk with the linear motor. This arrangement generates giant voids in a very controlled fashion. The advantage of this setup is that the velocity is a control parameter and not the response of the object to the fluid forces upon impact. Secondly, due to the large scale of the experiment, viscosity and surface tension play a negligible role. Therefore the only important dimensionless parameter is the Froude number $Fr = V^2/(h_{disk} g)$, the ratio of kinetic to gravitational energy, which ranges from 0.6 to 90. The large scale of the experiment is also advantageous for the observation of details during the impact and collapse process, which is imaged with digital high-speed cameras with frame rates up to 100,000 frames per second.

A typical series of events is seen in Fig. 11–d. The impact of the disk creates an axisymmetric void which first expands until the hydrostatic pressure drives the walls inward. The inward moving walls collide and cause a pinch-off at some depth below the undisturbed free surface. The energy focusing of this violent collapse creates a strong pressure spike on the axis of symmetry which releases itself in a downward and an upward jet. The latter reaches heights exceeding 1.5 m for the higher impact speeds in this experiment. It is this dominating role of inertia that makes our system different from other pinch-off processes in the literature. At higher recording speeds the pinch-off can be investigated in more detail as in Fig. 11–h. There is a clear loss of both azimuthal and axial symmetry in Figs. 11 and 12, which can be attributed to a combination of the same convergence effect that causes an instability in a collapsing bubble, and a Kelvin-Helmholtz instability due to the rapid air flow in the neck. The latter increases with increasing Froude number and limits the range of our experiments. Another factor which limits the Froude number range is the so-called surface seal, in which the void closes at the water surface as the crown-like splash is entrained by the air flowing into the expanding void.
FIG. 1: Snapshots of the formation and collapse of a surface void for the plunger experiment: A linear motor pulls down a disk of radius $h_{disk} = 30$ mm through the water surface at a constant velocity $V = 1.0$ m/s ($Fr = 3.4$). (a-d) The collapse of the void imaged at a 1000 frames per second. The white lines (overlay) are the void profiles obtained from boundary integral simulations with the same initial condition, and without the use of any free parameter. (e-f) Details of the collapse imaged at 12800 frames per second. (g-h) Details of the collapse imaged at 48000 frames per second. Note that the field of view decreases with increasing frame rate. In the very last stages of the collapse (f-g) there is a Kelvin-Helmholtz instability that complicates the determination of the time of collapse. Immediately after the collapse air is entrapped, both in the form of a large bubble above disk (d) and as a cloud of microbubbles at the collapse point (h).

20, 21. This process, which occurs at large Froude numbers, changes the pinch-off considerably since in this case the gas pressure inside the void differs appreciably from that of the ambient air.

In view of these experimental limitations, we performed numerical simulations using a boundary integral method based on potential theory without ambient gas. There is an excellent agreement between the numerical calculations and the experiments, as seen in Fig. 1b-c. Here, the numerical void profiles (the solid white lines) coincide very well with the experimental profiles in the pinch-off region without the use of any adjustable parameter, either in space or in time.

To further quantify the pinch-off process, we now turn to the time evolution of the neck radius $h(\tau)$, measured at the depth at which the void eventually closes. Because both length and time scales become very small close to collapse, it is not feasible to experimentally observe the collapse with only one high-speed camera recording. 22. Due to the reproducibility of the experiment, we overcame this difficulty by matching several data sets imaged at different frame rates, increasingly magnifying the region around the pinch-off. Figure 2a contains a doubly logarithmic plot of $h(\tau)$ (compensated with $\tau^{1/2}$) for both the high-speed imaged experiments and the numerical calculations, again showing excellent agreement for different Froude numbers. In this graph, a straight line corresponds to the power law behavior $h = h_0 \tau^{\alpha_h}$. The exponent $\alpha_h$ is plotted as a function of $Fr$ in Fig. 2b. Clearly, there are large deviations from the suggested behavior $\alpha_h = 1/2$. Can these be explained by a logarithmic correction as proposed in 14?

Let us first establish the origin of this logarithmic correction in our system. Near the neck, the flow induced by the collapsing void looks very much like that of a collapsing cylinder, while it must look like that of a sink, plus its image in the free surface (i.e., a dipole) in the far region. In the language of singular perturbations, the former would be the inner region and the latter the outer region; a complete description would require the matching of these two regions. If we disregard the outer region, we can use a two-dimensional version of the Rayleigh-equation, which describes the collapse of an infinite cylindrical cavity under uniform pressure 4, 10, 22.

$$
\left[ \frac{d(h^2)}{d\tau} \right] \log \frac{h}{h_\infty} + \frac{1}{2} \hbar^2 = gZ .
$$

The pressure difference driving the collapse has been equated to $\rho gZ$, where $Z$ denotes the depth below the fluid surface, which implies that the system is composed
of non-interacting horizontal layers of fluid, with a negligible vertical velocity component \[26\]. Although the quantity \( h_\infty \) must in principle be determined by the matching process alluded to before, it is expected to be of the order of a typical length scale of the process, such as the cavity depth. Thus, strictly speaking, \( h_\infty \) is a function of time and of the Froude number. However, near pinch-off, the time scale for the neck motion is much faster than that for the evolution of the other parts of the cavity so that \( h_\infty \) may be considered only a function of \( Fr \).

After an initial expansion of the void, the collapse starts from rest at a maximal radius \( h_{\text{max}} \) (of the order of \( h_{\text{disk}} \)). Using this as an initial condition, and treating \( h_\infty \) as a constant, the energy integral of Eq. \( 1 \) can be readily found:

\[
\left( \frac{dh}{d\tau} \right)^2 = \frac{1}{\log(h/h_\infty)} \left[ 1 - (1/h)^2 \right],
\]

where we have introduced the non-dimensional variables \( \tilde{h} \equiv h/h_{\text{max}}, \ h_\infty \equiv h_\infty/h_{\text{max}}, \) and \( \tilde{\tau} \equiv \tau \sqrt{gZ/h_{\text{max}}^2}. \) Close to pinch-off, \( \tilde{h}^2 \ll 1, \) such that \( \tilde{h}^{-2} - 1 \approx \tilde{h}^{-2}. \) With this approximation, we can integrate Eq. \( 2 \) once more to arrive at

\[
2 \tilde{\tau} = \tilde{h}^2 \sqrt{\log(h_\infty/h)} + \sqrt{\frac{\pi}{2}} \tilde{h}_\infty^2 \text{erfc} \left( \sqrt{2\log(h_\infty/h)} \right).
\]

For small \( \tilde{h} \) the term with the complementary error function is always small compared to the first one and their ratio vanishes for \( h \downarrow 0. \) Neglecting this term we find two asymptotic regimes

\[
\tilde{h} \left( \log(h_\infty) \right)^{1/4} = \sqrt{2} \tilde{\tau}^{1/2} \quad \text{for} \quad \tilde{h} \gg 1/h_\infty, \quad \text{and} \quad (4)
\]

\[
\tilde{h} \left( -\log(h) \right)^{1/4} = \sqrt{2} \tilde{\tau}^{1/2} \quad \text{for} \quad \tilde{h} \ll 1/h_\infty. \quad (5)
\]

From Eqs. \( 1 \) and \( 5 \) we conclude that the scaling depends crucially on the value of \( h_\infty: \) Initially, for the intermediate regime \( h \gg h_{\text{max}}^2/h_\infty, \) we expect to find a strict power law \( h \propto \tilde{\tau}^{1/2}, \) since \( \log(h_\infty) \) is constant. For times closer to the pinch-off, when \( h \ll h_{\text{max}}^2/h_\infty, \) the logarithmic corrections play a role, and the power law should be modified into Eq. \( 5. \)

As \( h_\infty \approx h_{\text{max}} \) in our experiments, the latter inequality can be read as \( h \ll h_{\text{max}}, \) which is satisfied in most of the region where \( h(\tau) \) asymptotically behaves as a power law (cf. Fig. \( 2a \)). We conclude that in our system the logarithmic correction cannot be neglected. If we plot the quantity \( y = h(-\log h)^{1/4} \) vs. \( \tau, \) we again observe a power law \( y \propto \tau^{\alpha_y} \), but with a slightly different exponent \( \alpha_y \) than the one found for \( h. \) In Fig. \( 2a \) we compare \( \alpha_h \) and \( \alpha_y \) as functions of the Froude number. As discussed before, \( \alpha_h \) is substantially larger than \( 1/2, \) but even if the logarithmic term is included we continue to find a slower collapse for low Froude numbers. Although the logarithmic correction does bring the result closer to the suggested value \( 1/2, \) it cannot account for all of the observed deviations.

Clearly, the observed anomalous power law behavior of the neck radius must reflect itself in the time-evolution of the free-surface profiles of the collapsing void. If the process were self-similar, the free-surface profiles at different times \( \tau \) would superpose when scaled by any characteristic length, e.g., the neck radius \( h. \) Actually, it is found
that the depth of minimum radius increases somewhat as the collapse progresses and it is therefore necessary to translate the profiles in the vertical direction so as to match the position of the minimum radius point before attempting this operation. Even if this is done, however, the results fail to collapse onto a single shape. The rescaled profiles become more and more elongated as the pinch-off is approached which proves that the collapsing void is not self-similar in a strict sense.

The free-surface shapes near the minimum point should thus not only be characterized by \( h(\tau) \), but also by a second length-scale, the radius of curvature \( R(\tau) \) in the vertical plane (see Fig. 2b). The spatial resolution of the high-speed camera images limits the accuracy with which \( R \) can be extracted from the experimental observations, but this quantity is easily determined from the numerical calculations (see Fig. 2b). When the radial dimensions \( (H, \text{ cf. Fig. 1b}) \) are scaled by \( h \) and vertical ones \( (Z) \) by \( \sqrt{\tau R} \), the profiles do collapse, which may only signal that their shape is very close to parabolic [27]. The time-evolution of this radius of curvature is also found to follow a power law, \( R = R_0 \tau^{\alpha_R} \), the exponent \( \alpha_R \) of which increases with the Froude number as can be seen in Fig. 2b [25].

The essence of the time-evolution of the void profile and the departure from self-similarity in the strict sense is captured in the aspect ratio \( h/R \) of the collapsing void, \( h(\tau)/R(\tau) = (h_0/R_0) \tau^{(\alpha_h-\alpha_R)} \), in which the prefactor \( h_0/R_0 \) and the exponent \( (\alpha_h-\alpha_R) \) both are found to depend on the Froude number. It is seen in Fig. 2a that \( \alpha_h - \alpha_R > 0 \) for any finite Froude number, causing the ratio \( h(\tau)/R(\tau) \) to vanish in the limit \( \tau \to 0 \). This means that in this limit \( R(\tau) \) becomes large with respect to the neck radius, elongating the profiles more and more towards the cylindrical shape close to the pinch-off, thereby justifying the assumptions made in the derivation of Eq. (1) in the limit \( \tau \to 0 \). A numerical fit gives \( (\alpha_h-\alpha_R) \propto Fr^{-0.14} \), which indicates that \( h \) and \( R \) have the same time dependence as \( Fr \to \infty \) and, therefore, that self-similarity is recovered in this limit.

A second numerical fit shows that \( h_0/R_0 \propto Fr^{-0.60} \), which tends to zero as \( Fr \to \infty \). This feature expresses the experimental observation that the initial elongation of the neck is larger for large Froude number, which effectively increases the time-interval for which the assumption of pure radial flow is valid [cf. Eq. (1)].

In conclusion, our experiments on the collapse of a giant surface void are in excellent agreement with boundary integral calculations without the use of any adjustable parameter. Even when we exclude the effects of air, viscosity, and surface tension, the collapse is found to be not self-similar in a strict sense, but governed by power laws with non-universal, Froude-dependent exponents. Self-similarity is recovered only in the limit of infinite Froude number, where the influence of gravity becomes negligible and the collapse is truly inertially driven.

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hole sequence should then be imaged at a frame rate corresponding to the smallest timescale (10 µs), i.e., 100 kHz requiring at least 10 GB of fast storage capacity, greatly exceeding the physical capabilities of our cameras.

[26] A similar equation is used in [14], without the term \( h_\infty \) and also without the hydrostatic driving pressure \( gZ \).

[27] At the minimum \( 1/R(\tau) = \frac{d^2 H}{dZ^2}|_{Z=Z_{\text{min}}} \) and the shape of the interface can be taken to be locally parabolic, which implies \( H = (\delta Z)^2/R(\tau) + h(\tau) \) with \( \delta Z = Z - Z_{\text{min}} \). The scaling of the radial direction \( H \) with \( h(\tau) \) then leads to the scaling \( \sqrt{h(\tau)R(\tau)} \) for the axial direction \( Z \). The aspect ratio of the void is then given by \( H/Z = (h(\tau)/R(\tau))^{1/2} \).

[28] The fact that both \( h \) and \( R \) are described by power laws suggests that we may be dealing with self-similarity of the second kind, in which the radial and axial coordinates are rescaled by different power laws of time [23]. At present there is however insufficient experimental and theoretical ground to substantiate such a claim.