Establishment of a finite element model and stress analysis of intra-articular impacted fragments in posterior malleolar fractures

Wenyong Xie†, Hao Lu†, Sizheng Zhan†, Yijun Liu, Yuan Quan, Hailin Xu*, Zhongguo Fu and Dianying Zhang

Abstract

Background: Intra-articular impacted fragments (IAIFs) are considered articular surface fragments resulting from impact and compressive forces. The malreduction of IAIFs in posterior malleolar fractures has been associated with talar subluxation and long-term post-traumatic arthritis. In this study, we establish IAIF defect finite element models of different sizes in posterior malleolar fractures and explored how IAIF defects predict the onset of post-traumatic arthritis.

Methods: A reliable three-dimensional finite element model of the normal ankle was established. Finite element models with different sizes of IAIF defects were created to calculate ankle joint contact stress. The finite element data were recorded and analyzed.

Results: There was a linear relationship between the size of the IAIF defect and MCS with IAIF defects in the posterolateral region. The result of Pearson linear correlation analysis was $r = 0.963, P = 0.009$. The regression equation was $MCS = 0.087 \times AI + 2.951$ (AI, area of IAIF) by simple linear regression analysis. When the IAIF defect was in the posteromedial region, there was also a linear relationship between the size of the IAIF defect and MCS. The result of Pearson linear correlation analysis was $r = 0.908, P = 0.033$. The regression equation was $MCS = 0.065 \times AI + 1.841$. The MCS was increased mainly in the border of the IAIF defect.

Conclusions: A small IAIF defect in the posterior malleolus will result in a high MCS, and the MCS in the posterolateral region is larger than the MCS in the posteromedial region when the size of the IAIF defect is the same. We obtain the regression equation of MCS and area of IAIF defect. This indicates that patients are more prone to post-trauma arthritis when the size of IAIF defects is more than 17.8 mm² in the posterolateral region and more than 40.9 mm² in the posteromedial region.

Trial registration Retrospectively registered.

Keywords: Finite element analysis, Ankle fractures, Posterior malleolus, Intra-articular fragment, Post-traumatic arthritis

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Background

The incidence of ankle fractures has been reported to be 10% among all fractures [1]. A system review reported that about 95% ankle fracture were acute fractures [2]. Posterior malleolar fractures can have a high incidence among ankle fractures [3]. It was unstable fractures...
when ankle fractures involved posterior malleolar fractures and common on supination-external rotation ankle fractures, which were also associated with negative outcome and development of radiographic osteoarthritis [4]. At present, due to the use of CT scans, intra-articular impacted fragments (IAIFs) in ankle fractures are commonly found, and the morphology of IAIFs varies [5–7]. Scheck et al. [8] first described the die-punch fragment, the intra-articular fragment, in distal radius fractures, and subsequently, the intra-articular fracture of the distal tibia was studied [9]. However, only three studies have reported the relevant description of IAIF [5–7].

IAIFs are articular surface fragments that are impacted by the talus. Talus subluxation can be found in ankle fractures with IAIF [5]. Long-term post-traumatic arthritis is related to malreduction of IAIFs [7, 10, 11] and is more likely to occur [12, 13]. Important pathomechanical determinants of post-traumatic arthritis may exist as peak instantaneous contact stresses [14]. Anderson et al. [15] proposed that elevated contact stress exposure would predict the onset of post-traumatic arthritis based on FEA modeling and clinical follow-up. It is considered to be critically important to reduce displaced articular fractures anatomically, which could minimize the risk of developing post-traumatic arthritis [16].

The finite element analysis (FEA) technology had become a common form of biomechanical simulation, which was based on modern computational method and structural mechanics analysis and had many advantages compared to cadaver specimens. In some studies, the technology of FEA was also used in tumor bone and thermal necrosis with many advantages [17, 18]. It was difficult to study the thermal necrosis from drilling bone though cadaver specimens, while the FEA could be well applied [17]. We have already established an IAIF defect finite element model in posterior malleolar fractures and discussed the relation between IAIF defects and post-traumatic arthritis [19].

However, the size of IAIF defects and post-traumatic arthritis, which is of great importance for clinical treatment, has not been studied. Due to equipment issues, costs and ethical issues, FEA technology, which is based on modern computational methods and structural mechanics analysis, is a better choice to study the relationship of different sizes of IAIF defects and post-traumatic arthritis. This would enable the result of FEA to be as realistic in terms of ontology as possible [20].

The aim of this study was to establish IAIF defect finite element models of different sizes in posterior malleolar fractures and explore the IAIF defects and how to predict the onset of post-traumatic arthritis.

**Materials and methods**

First, DICOM data from a normal ankle joint CT in our institution were obtained. Then, a finite element model of the ankle joint was established through relevant software. After verifying the stability and reliability of the finite element model, IAIF defects were established in the finite element model. The detailed methods of the above have been published in the journal of Injury [19].

The bottom view of the distal tibial articular surface is shown in Fig. 1. The AB line was the midpoint of the lateral malleolus to the midpoint of the medial malleolus, and the CD line was the midpoint of the posterior edge of the tibia to the midpoint of the anterior edge of the tibia. The O point was the intersection point of the AB and CD lines. It was difficult to study the thermal necrosis from drilling bone though cadaver specimens, while the FEA could be well applied [17]. We have already established an IAIF defect finite element model in posterior malleolar fractures and discussed the relation between IAIF defects and post-traumatic arthritis [19].

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malleolus [5–7]. We established IAIF defects in the cartilage and subchondral bone in the center of the posterolateral region (fragment I) and posteromedial region (fragment M). There was no description of the relevant IAIF defect in the existing literature. From the description of IAIF in some studies [5–7], we started a defect IAIF depth with cartilage and subchondral bone missing at 2 mm, area with a size of $1 \times 2$, $3 \times 4$, $4 \times 5.5$, $5 \times 6.4$ and $6 \times 7$ mm$^2$ (Fig. 1).

Statistical analysis was done using SPSS 23.0. A $P$ value $<0.05$ was considered significant. The relation between the size of the IAIF defect and maximum contact stress was analyzed with Pearson correlation analysis. Simple linear regression analysis was carried out to obtain a regression equation when there was a linear correlation between the size of the IAIF defect and the maximum contact stress.

**Results**

Finite element analysis of different sizes of IAIF defects:

We recorded the maximum contact stress in different sizes of IAIF defects in the posterolateral region or posteromedial region. We also recorded the maximum contact stress in four quadrants of regions AOC, BOC, AOD and BOD (Fig. 2, Table 1).

The data of the size of the IAIF defect and maximum contact stress (MCS) were input into SPSS 23.0 to analyze their correlation. The $X$ axis is taken as the size of the IAIF defect, and the $Y$ axis is taken as the MCS. When the IAIF defect was in the posterolateral region,

![Fig. 2](contact_stress_distribution.png)

**Table 1** Maximum contact stress on the distal tibial articular surface in the different size of intra-articular impacted fragment (IAIF) defect

| Size of defect (mm$^3$) | Maximum contact stress (IAIF Defect in BOC, MPa) Intact | BOC | AOC | BOD | AOD | Maximum contact stress (IAIF Defect in AOC, MPa) Intact | BOC | AOC | BOD | AOD |
|------------------------|-----------------------------|-----|-----|-----|-----|-----------------------------|-----|-----|-----|-----|
| $1 \times 2 \times 2$  | 3.3465                      | 3.3465 | 1.1558 | 1.4459 | 1.1432 | 1.4425                     | 1.2966 | 1.4137 | 1.4425 | 1.1432 |
| $3 \times 4 \times 2$  | 3.9653                      | 3.9653 | 1.1757 | 1.4588 | 1.148 | 3.2958                     | 1.303 | 3.2958 | 1.4473 | 1.1612 |
| $4 \times 5.5 \times 2$ | 4.7455                      | 4.7455 | 1.1639 | 1.4732 | 1.15 | 5.1854                     | 1.3022 | 1.4496 | 1.1974 | 1.2457 |
| $5 \times 6.4 \times 2$ | 5.1854                      | 5.1854 | 1.1843 | 1.4935 | 1.1679 | 7.089                      | 1.3185 | 4.5605 | 1.5378 | 1.2806 |
| $6 \times 7 \times 2$  | 7.089                       | 7.089 | 1.2162 | 6.5087 | 5.4433 | 4.5605                     | 1.3185 | 4.5605 | 1.5378 | 1.2806 |

IAIF intra-articular impacted fragment
there was a linear relationship between the size of the IAIF defect and MCS. The results of Pearson linear correlation analysis were \( r = 0.963, P = 0.009 \). The MCS was positively correlated with the size of the IAIF defect. The regression equation was \( \text{MCS} = 0.087^*\text{AI} + 2.951 \) (AI, area of IAIF) by simple linear regression analysis. When the IAIF defect was in the posteromedial region, there was also a linear relationship between the size of the IAIF defect and MCS. The results of Pearson linear correlation analysis were \( r = 0.908, P < 0.033 \). It was positively correlated between the size of the IAIF defect and MCS. The regression equation was \( \text{MCS} = 0.065^*\text{AI} + 1.841 \), although simple linear regression analysis was performed (Fig. 3).

**Discussion**

Through finite element analysis, it is found that a small IAIF defect in the posterior malleolus will result in a high MCS, and the MCS in the posterolateral region is larger than the MCS in the posteromedial region when the size of the IAIF defect is the same. There is an obvious linear correlation between the size of the IAIF defect and the MCS. Therefore, the MCS of any IAIF can be calculated and then further discuss the relation between IAIF defects and traumatic arthritis. We established IAIF defect finite element models with sizes of 1 \( \times \) 2, 3 \( \times \) 4, 4 \( \times \) 5.5, 5 \( \times \) 6.4 and 6 \( \times \) 7 mm\(^2\) in the posterolateral region and posteromedial region. The relation between IAIF defects and MCS has not been studied before. The characteristics of IAIF make it easy to ignore in surgery, which can be vulnerable to malreduction or loss.

The intact anatomical structure plays an important role in the stability and function of the ankle joint. Chronically elevated contact stresses resulting from articular incongruity overload the cartilage and may be important pathomechanical determinants of post-traumatic arthritis [14, 21]. A high occurrence of IAIF in posterior malleolar fractures is considered the major driver of articular incongruity leading to post-traumatic arthritis. Sultan et al. [7] reported that IAIF was found in 43% of posterior malleolar fractures, and the position of IAIF was posterolateral in 64%, midposterior in 19% and posteromedial in 17% of cases. IAIF has not received enough attention during the operation, and it was reported that more than 40% of cases of posterior malleolar fractures with IAIF were considered poor reduction [7].

Our research results showed that when the IAIF defect was in the posterolateral region, a small defect of 2 mm\(^2\) made the maximum contact stress more than double that of the normal ankle joint. When the IAIF defect increased, the maximum contact stress increased gradually. There was a sharp increase in defect of 32–42 mm\(^2\). We obtained a regression equation of \( \text{MCS} = 0.087^*\text{AI} + 2.951 \). Therefore, we could know the relative MCS of different sizes of IAIF defects. There were insignificant changes when the IAIF defect was in the posteromedial region with a defect of 2 mm\(^2\). The greatest increase in MCS occurred in a defect of 2–12 mm\(^2\), while the defect of 12–22 mm\(^2\) increased slowly and then had a sharp increase in defects of 32–42 mm\(^2\). The regression equation was \( \text{MCS} = 0.065^*\text{AI} + 1.841 \). From our results, we found that there was a greater influence on MCS with a defect of 32–42 mm\(^2\) in both the posterolateral and posteromedial regions. Hence, more importance should be placed on this aspect.

Anderson et al. [15] indicated that patients were more prone to post-trauma arthritis when MCS exceeded 4.5 MPa in long-term follow-up. We obtained an associated IAIF defect size of 17.8 mm\(^2\) in the posterolateral region and 40.9 mm\(^2\) in the posteromedial region when

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**Fig. 3** Relation and simple linear regression between MCS (maximum contact stress) and AI (area of IAIF) through GraphPad Prism: a \( \text{MCS} = 0.087^*\text{AI} + 2.951, P = 0.009 \), b \( \text{MCS} = 0.065^*\text{AI} + 1.841, P = 0.033 \)
the MCS exceeded 4.5 MPa. Therefore, IAIF defects greater than 17.8 mm² in the posterolateral region and more than 40.9 mm² in the posteromedial region should be reduced anatomically to reduce the occurrence of long-term post-trauma arthritis. The results are consistent with our other study showing that patients will suffer a poor prognosis and post-traumatic osteoarthritis if AIAIF is over 40 mm² based on a large patient cohort [22]. Otherwise, the ankle joint will bear a maximum stress of 5 times the body weight when we run or jump in some activities. Therefore, for any size of defect, the impact on joint stress and stability should be considered in the treatment of ankle fractures to reduce damage caused by the IAIF defect.

McKinley et al. [14] found that contact stress peaks did not occur at the stepoff edge but rather occurred 2–3 mm away from the edge of the stepoff. Huber-Betzer et al. [23] attributed the phenomenon to the absence of buttressing at the lip of the step. In our study, the MCS was increased mainly in the border of the defect. We considered that there is a buttress around our IAIF defect. We divided the distal tibial articular surface into four quadrants: AOC, BOC, AOD and BOD. We recorded the MCS for each region and found that the MCS increases slowly with the increase in the size of the IAIF defect in the residual three regions, except for the region of the IAIF defect. The increased contact stress area also continuously increases with increasing IAIF defect size. There was a substantial impact on the distribution of MCS when the defect area was 42 mm² in the posterolateral region. The MCS has a rapid increase in the BOD and AOD regions. For IAIF defects of the same size, the MCS in the posterolateral region is larger than that in the posteromedial region. This indicates a higher impact of the contact stress of the ankle joint when the IAIF defect is in the posterolateral region. The posterolateral IAIF defect in ankle fracture should be taken more seriously.

There were several limitations in this study. The mechanical properties of the ankle joint are quite complicated. Although our model can simulate the anatomy of the ankle joint and surrounding structures more realistically and accurately, it still results in little difference between finite element analysis results and actual situations. However, there is no influence on the size of the IAIF defect. The next step in our research is to further verify the results of this experiment in cadaver samples or clinical patients.

Conclusion
In summary, a small IAIF defect in the posterior malleolus will result in a high MCS, and the MCS in the posterolateral region is larger than the MCS in the posteromedial region when the size of the IAIF defect is the same. We obtain the regression equation of MCS and area of IAIF defect. It has been indicated that patients are more prone to post-trauma arthritis when the size of IAIF defect is about more than 17.8 mm² in posterolateral region and about more than 40.9 mm² in posteromedial region. The MCS is increased mainly in the border of the IAIF defect. The increased contact stress area is also continuously increased with the increase in the size of the IAIF defect. These findings suggest that doctors should pay attention to IAIF defects in posterior malleolar fractures, and it is also helpful to develop optimal treatment protocols.

Abbreviations
IAIF: Intra-articular impacted fragment; MCS: Maximum contact stress; FEA: Finite element analysis; PTOA: Post-traumatic osteoarthritis.

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Authors’ contributions
WX, HL and SZZ performed data analysis, as well as writing the manuscript. YJL and QY contributed to the collection of data and manuscript editing. ZGF and DYZ revised the manuscript. HLX edited the manuscript and were the guarantor of this article. All authors read and approved the final manuscript.

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Availability of data and materials
The datasets and materials are available from corresponding authors on reasonable request.

Declarations
Ethics approval and consent to participate
This study was approved by the institutional review board of our institution (Peking University People’s Hospital Ethics Review Committee, 2021PHB134-001). This is a cohort study. The volunteer gave his written consent to have all his clinical data.

Consent for publication
The volunteer gave his explicit written consent to have all his clinical data included in this review write-up and for publication.

Competing interests
The authors declare that there are no competing interests.

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References
1. Tenenbaum S, Shazar N, Bruck N, Banteau J. Posterior malleolus fractures. Orthop Clin North Am. 2017;48(1):81–9.
2. Del Buono A, Smith R, Coco M, Woolley L, Denaro V, Maffulli N. Return to sports after ankle fractures: a systematic review. Br Med Bull. 2012;106(1):79–91.
3. Jaskulka RA, Ittner C, Schedi R. Fractures of the posterior tibial margin: their role in the prognosis of malleolar fractures. J Trauma. 1989;29(11):1565–70.
4. Gougoulias N, Khanna A, Sakellariou A, Maffulli N. Supination-external rotation ankle fractures: stability a key issue. Clin Orthop Relat Res. 2010;468(1):243–51.
5. Bartoníček J, Rammelt S, Kostivý J, Vaněček V, Klika D, Tesl I. Anatomy and classification of the posterior tibial fragment in ankle fractures. Arch Orthop Trauma Surg. 2015;135(4):505–16.
6. Weber M. Trimalleolar fractures with impaction of the posteromedial tibial plafond: implications for talar stability. Foot Ankle Int. 2004;25(10):716–27.
7. Sultan F, Zheng X, Pan Z, Zheng Q, Li H, Wang J. Characteristics of intercalary fragment in posterior malleolar fractures. Foot Ankle Surg Off J Eur Soc Foot Ankle Surg. 2020;26(3):289–94.
8. Scheck M. Long-term follow-up of treatment of comminuted fractures of the distal end of the radius by transfixation with Kirschner wires and cast. J Bone Joint Surg Am. 1962;44-a:337–51.
9. Maller BN, Krebs B. Intra-articular fractures of the distal tibia. Acta Orthop Scand. 1982;53(6):991–6.
10. Rammelt S, Bartoníček J. Posterior malleolar fractures: a critical analysis review. JBJS Rev. 2020;8(8):e1900207.
11. Blom RP, Hayat B, Al-Dirini RMA, Sierevelt I, Kerkhoffs GMMJ, Goslings JC, Jaarsma RL, Doornberg JN. Posterior malleolar ankle fractures. Bone Joint J. 2020;102-B(9):1229–41.
12. Matta JM. Fractures of the acetabulum: accuracy of reduction and clinical results in patients managed operatively within three weeks after the injury. J Bone Joint Surg Am. 1996;78(11):1632–45.
13. Ovadia DN, Beals RK. Fractures of the tibial plafond. J Bone Joint Surg Am. 1986;68(4):543–51.
14. McKinley TO, Rudert MJ, Koos DC, Pedersen DR, Baer TE, Tochigi Y, Brown TD. Contact stress transients during functional loading of ankle stepoff incongruencies. J Biomech. 2006;39(4):617–26.
15. Anderson DC, Van Hofwegen C, Marsh JA, Brown TD. Is elevated contact stress predictive of post-traumatic osteoarthritis for imprecisely reduced tibial plafond fractures? J Orthop Res Off Publ Orthop Res Soc. 2011;29(1):33–9.
16. Buckwalter JA, Brown TD. Joint injury, repair, and remodeling: roles in post-traumatic osteoarthritis. Clin Orthop Relat Res. 2004;423:7–16.
17. Mediouni M, Schlatterer DR, Khoury A, Von Bergen T, Shetty SH, Arora M, Dhond A, Vaughan N, Volosnikov A. Optimal parameters to avoid thermal necrosis during bone drilling: a finite element analysis. J Orthop Res Off Publ Orthop Res Soc. 2017;35(11):2386–91.
18. Mediouni M, Schlatterer DR. Orthopaedic tumors: What problems are we solving, and are universities and major medical centers doing enough? J Orthop. 2017;14(2):319–21.
19. Xie W, Lu H, Yuan Y, Xu H. A new finite element model of intra-articular impacted fragment in posterior malleolar fractures: a technical note. Injury. 2022;53(2):784–8.
20. Ramlee MH, Kadir MR, Murali MR, Kamarul T. Finite element analysis of three commonly used external fixation devices for treating Type III pilon fractures. Med Eng Phys. 2014;36(10):1322–30.
21. Linas A, McKellop HA, Marshall GJ, Sharpe F, Kirchen M, Sarmiento A. Healing and remodeling of articular incongruities in a rabbit fracture model. J Bone Joint Surg Am. 1993;75(10):1508–23.
22. Xie W, Lu H, Zhan S, Liu Y, Xu H, Fu Z, Zhang D, Jiang B. Outcomes of posterior malleolar fractures with intra-articular impacted fragment. Arch Orthop Trauma Surg 2021.
23. Huber-Betz H, Brown TD, Mattheck C. Some effects of global joint morphology on local stress aberrations near impacently reduced intra-articular fractures. J Biomech. 1990;23(8):811–22.

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