Abstract: The results of testing a prototype of a separator for detecting diamonds in kimberlite ore using tagged neutron method are discussed. Kimberlite ore was irradiated with fast tagged neutrons with an energy of 14.1 MeV. The elemental content of the tray with kimberlite ore was determined. The criterion for detecting diamond was the presence of excess carbon concentration in a certain region of a kimberlite sample.

Keywords: tagged neutron method; diamonds; kimberlite

1. Introduction

The present technology of finding diamonds in the kimberlite ore consists in exposing a diamond from the kimberlite. Open diamonds are detected either by X-rays irradiation or by floatation. To extract diamond from kimberlite, the ore is subjected to few iterative processes of crushing in grinding rolls or wet mills down to a size of 0.2 mm. This procedure of repetitive crushing destroys not only kimberlite ore but also damages diamonds and the most valuable large diamonds suffer the most. Its breaking drastically decreases the price of the diamond.

We have proposed [1] a new technology for detecting diamond inside the kimberlite stones without breaking the stone. It is based on tagged neutron method (also called Associated Particle Imaging (API) method) [2–6]. The scheme of the method is shown in Figure 1. The kimberlite ore is irradiated by fast 14.1 MeV neutron produced in a neutron generator where the following reaction takes place:

\[
d + ^3\text{H} \rightarrow ^4\text{He} + n.
\]

In this binary reaction \(\gamma\)-particle and neutron are flying practically back-to-back. Detecting the \(\alpha\)-particle gives possibility to know momentum of the neutron. In this regard, a neutron generator with built-in special matrix \(\gamma\)-detector is used. Tagging neutron by detecting the \(\gamma\)-particle gives possibility to analyse \(\gamma\)-rays from reactions of inelastic scattering

\[
n + A \rightarrow n' + A^*, A^* \rightarrow \gamma + A.
\]
In the neutron module, ore is irradiated with beams of fast tagged neutrons. Using a system of gamma detectors located above the tray conveyor, the characteristic gamma radiation is recorded in coincidence with the signal from the $\gamma$-detector located inside the neutron generator. Information from $\alpha$- and $\gamma$-detectors is analysed by decision-making software. According to the results of the analysis, the tray with the rock is separated either to the concentrate bunker, or to the tailings.
the γ-quantum. Knowing the velocity of monoenergetic 14.1 MeV neutron of 5 cm/ns one could determine all 3D coordinates of the region from which the γ-quantum is radiated. Using time-of-flight information allows selecting events only from the inspection region. It drastically reduces the background, the signal-to-background ratio increases by factor of 200.

Figure 1. Scheme of tagged neutron method.

High penetrability of fast neutrons makes it possible to examine appreciably large samples of kimberlite. Thus, kimberlite stones containing diamonds can be identified before the crushing stage. The results of proof-of-principle laboratory experiments are discussed in [1]. Now we have developed a prototype of a separator with 2 tons hopper for detecting diamonds in kimberlite using the tagged neutron method. The results of the testing the prototype are discussed.

2. Materials and Methods

The prototype of a separator consists of an ore supply system and a neutron module, which are located in a 20-foot transport container. The schematic setup is shown in Figure 2.

Figure 2. Schematic setup.

The neutron module consists of a portable neutron generator ING-27M produced by Dukhov Institute of Automatics (Moscow, Russia), block of γ detectors and a data acquisition system. For diamonds detection the granularity of α-detector should be as high as possible. It determines minimal size of diamonds which could be detected. For this task a special modification of the ING-27, which produced 256 tagged beams of neutrons, is developed.

2.1. Neutron Generator

The neutron generator is a sealed tube portable neutron generator with an inbuilt alpha-detector. The generator provides a continuous neutron flux with an intensity of $1 \times 10^8$ s$^{-1}$. It operates in DC mode and accelerates deuterium up to 100 KeV towards the tritium target. Power consumption of neutron generator is 40 W. The lifetime of the generator is 800 h.

The inbuilt alpha-detector consists of a gallium arsenide plate, which is a semiconductor position-sensitive detector having 16 vertical and 16 horizontal strips, which formed 256 square pixels of 4 mm size. The dead zone between the strips is 0.1 mm. In Table 1 the comparison of this alpha-detector with existing ones is given.

Table 1. Characteristics of different alpha detectors.

| Type Of Neutron Generator | Number Of Tagged Beams | Size of the Pixel, mm | Spacing between Pixels, mm |
|---------------------------|------------------------|----------------------|---------------------------|
| ING-27 [7]                | 9                      | 10                   | 1                         |
| Sodern, Euritrack [8]     | 64                     | 5.8                  | 0.2                       |
| API-120 [9]               | 256                    | 3                    | -                         |
| ING-27-256                | 256                    | 4                    | 0.1                       |

The spatial sizes of the tagged beams are important because they determined the size of diamonds which could be detected. To measure the spatial dimensions of the tagged beams a scintillation stripped profilometer is used. It consists of 16 strips of plastic scintillator each 7.5 mm wide. The profilometer is placed at the distance of 570 mm from the target of neutron generator. The spatial distribution of 16 tagged beams produced by the coincidences of the pulses from 16 vertical strips with a single horizontal strip of α-detector is measured. The measured values have been approximated by the gaussians which are shown in Figure 3.
The averaged width of each tagged beam is $\Gamma_X = (37.1 \pm 0.9)$ mm and $\Gamma_Y = (36.6 \pm 1.1)$ mm. This is consistent with the value of 38 mm expected at the distance of 570 mm from the tritium target assuming a point-like deuteron beam. It is important for all further estimations to note that the deuteron beam of this neutron generator could be indeed considered point-like.

2.2. Gamma Detectors

Characteristic $\gamma$-rays produced by irradiated ore are detected by 22 bismuth germanate oxide (BGO) detectors with a thickness of 65 mm and a diameter of 76 mm. These detectors have an energy resolution of 8 to 2.5% within the energy range of 1 to 12 MeV and have high efficiency of gamma rays energy detection within the specified energy range and low sensitivity for detection of background neutrons.

2.3. Data Acquisition System

The data acquisition system for $\alpha$ and $\gamma$ detectors is designed as two boards of 32 inputs each. The board has the size of a standard peripheral component interconnect (PCI) card and can be installed in PCI-E slot of a personal computer (PC). The hardware data acquisition board utilizes high speed analog to digital converter (ADC) for sampling input signals. The system of registration processing signals from the alpha and gamma detectors is based on the principle of waveform digitalizing with subsequent calculation of their time and amplitude characteristics. It means that an average pulse waveform for each channel is measured, filtered and stored as a number of parameters. The detector signal timing is done using its filtered shape taken as Gaussian. As data is being taken signals from each detector are filtered with stored filter parameters, and signal timing is done via transformed signal shape analysis. Amplitude (i.e., energy) of the signal is calculated as an integral over predefined range of the original signal with subtraction of premeasured offset value.

Channels of digitalizing signals from the detectors are built on the same scheme which includes an amplifier of 0–20 MHz band pass filter and analog to digital converter measurements interval of 10ns (100 MHz). The digital code corresponding to each of measurements is fed to analog to digital converter logic circuit in which there is a definition of moments of $\alpha$-$\gamma$ coincidence in digital form.

2.4. Geometry of the Setup and Minimal Registered Diamond Size

Since diamonds entirely consist of carbon, the signal of diamond is local excess of carbon in some area of a tray with kimberlite. The tagged neutron technique allows dividing the tray with kimberlite
into 256 regions (voxels), determining carbon concentration in each voxel and comparing it with average carbon concentration of the tray. The size of the voxel $D$ in the direction perpendicular to the neutron momentum is determined by the size of the alpha detector pixel $d$, the distance between alpha detector and tritium target $l$ and distance from the tritium target to the kimberlite tray $L$. These parameters are shown in Table 2. The size of the voxel is an important parameter which determines minimal size of diamonds which could be detected by the setup. In this prototype it is possible to detect large diamonds of 9 mm and larger.

**Table 2.** General parameters of the prototype.

| Parameter                              | Value       |
|----------------------------------------|-------------|
| $L$, distance to the tray, mm          | 134         |
| $l$, distance to the $\alpha$-detector, mm | 60         |
| $d$, size of $\alpha$-detector pixel, mm | 4          |
| Matrix of $\alpha$-detector           | $16 \times 16$ |
| Dimension of $\alpha$-detector, mm    | $64 \times 64$ |
| Dimension of the inspected area, mm    | $143 \times 143$ |
| Dimension of voxel, $D$, mm            | 8.93        |
| Mass of the ore in tray, kg            | 2.5         |
| Inspection time, s                     | 6           |
| Throughput, t/h                        | 1.5         |

3. Results

3.1. Time and Energy Resolutions

The characteristic energy spectrum of gamma rays from a carbon sample is given in Figure 4.

![Energy spectrum of carbon.](image)

The spectrum is dominated by single line with energy 4.44 MeV and its first escape. That facilitates the search of local excess of carbon concentration. The energy resolution is $\Gamma_E = (4.51 \pm 0.25)\%$ at the 4.44 MeV line. The time resolution of ($\alpha$-$\gamma$)-coincidences, averaged over all $\gamma$-detectors is $\Gamma_1 = 3.86 \pm 0.39$ ns.
In Figure 5 the distribution of the time between signals from gamma-detector №3 and alpha-pixel №120 is shown for γ-quanta with energy around carbon line of 4.44 MeV. The blue line shows the approximation by Gaussian and the red line shows the linear background.

![Time Distribution](image)

**Figure 5.** Time distribution between signals from γ-detector №3 and α-pixel №120 (X-strip №8, Y-strip №8) for γ-quanta with energy around the 4.44 MeV carbon line.

One could see the main peak from the γ-quanta of the kimberlite ore on the flat background of random coincidences. The ratio peak/background is about 7:1, that is characteristic of the γ-detectors shielding. For the further analysis, events with time signals within ±2 ns from the maximum of the peak were selected. In Figure 5 one can see that the main peak is not a perfect Gaussian. Some excess of the events with large times is seen on the right side of the Gaussian. These are signals from neutrons backscattered on the ore. The distance between γ-detectors and the tray is quite small and the time signals from the γ-quanta and from backscattered neutrons are not completely separated.

### 3.2. Energy Spectra of γ-Quanta from the Kimberlite Ore

In Figure 6 the energy spectrum of γ-quanta from kimberlite ore of Karpinski mine (Archangelsk, Russia) is shown. The arrow shows the carbon 4.44 MeV line position. One could see that this peak is not large in the kimberlite due to small percentage of the carbon. To decrease the data flow, high energy threshold of 2.5 MeV was established. That is why there are no low energy lines of magnum, silicon and other elements. Actually, at this high energy threshold the spectrum is dominated by oxygen lines only. Around 3.8 MeV contamination of calcium line is also appeared.
3.3. Energy Spectra of $\gamma$-Quanta from the Kimberlite Ore with Diamond Imitators

To study the signal from a diamond inside the kimberlite stones we prepared a set of diamond imitators. They are made from synthetic diamond powder and are cylinders with diameter equal to its height. The size of imitator varied from 8 to 20 mm. In a stone a hole is made where the diamond imitator is placed.

Typical spectrum of $\gamma$-quanta from kimberlite ore of 90 mm with 12 mm diamond imitator is shown in Figure 7. The histogram corresponds to the spectrum averaged on all voxels of the tray, whereas the points with errors are the spectrum from some voxel. In this voxel, one could see a clear excess of events in the region of carbon line of 4.44 MeV.

3.4. Probability of False Alarms

The probability to find even open diamond in the kimberlite ore is quite small. The separator will mainly work with empty ore. Therefore, it is important to choose selection criteria in such a way that the probability of positive false alarms should be as low as possible. Positive false alarms mean appearance of the diamond signal from empty kimberlite ore.

Figure 6. Energy spectrum of $\gamma$-quanta from kimberlite ore of the Karpinski mine.

Figure 7. The energy spectrum of $\gamma$-quanta from 90 mm kimberlite ore with 12 mm diamond imitator. The histogram shows the spectrum averaged over all voxels of the tray. The points with errors are the spectrum from some voxel where the excess over background is 3.03 $\sigma$. 
Another example is shown in Figure 8. It shows the spectrum of the voxel where diamond imitator of 20 mm is situated in the stone of 90 mm. The stones have irregular shapes so we assigned the size of a stone according to its largest dimension. One could see that the value of carbon signal is much larger.

![Figure 8](image.png)

**Figure 8.** The energy spectrum of γ-quanta from 90 mm kimberlite ore with 20 mm diamond imitator. The histogram shows the spectrum averaged over all voxels of the tray. The points with errors are the spectrum from the voxel where the diamond imitator was situated.

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Main selection criterion is excess of the local concentration of carbon in spectrum of certain voxel in comparison with carbon concentration averaged over whole sample. The value of the excess is expressed in terms of $\sigma$, where $\sigma$ is calculated as follows:

$$\sigma = \frac{(c - \bar{C})}{(\varepsilon_c^2 + \varepsilon_C^2)}.$$  (3)

Here $c$ is the number of events in carbon line region in a certain voxel, $\bar{C}$ is the average number of events in carbon line region in measured sample, $\varepsilon_c$ and $\varepsilon_C$ are corresponding statistical errors.

The tests are carried out on kimberlite ore with size of 90 mm. This ore in a tray is irradiated for 10 s with average neutron intensity of $3.1 \times 10^7$ s$^{-1}$. In total, 100 different trays with the ore are tested. The results of tests for different values of $\sigma$ are shown in Table 3.
Table 3. Probability of false positive alarms.

| Criterium of Diamond Signal in Terms of $\sigma$ | Probability of Positive False Alarms |
|----------------------------------------|--------------------------------------|
| 2.38                                    | 0.59                                 |
| 2.50                                    | 0.47                                 |
| 2.63                                    | 0.36                                 |
| 2.75                                    | 0.21                                 |
| 2.88                                    | 0.14                                 |
| 3.00                                    | 0.07                                 |
| 3.13                                    | 0.03                                 |

Table 3 shows that probability of positive false alarms decreases with increasing $\sigma$ detection parameter and is equal to 3% when $\sigma = 3.13$. The false alarms rate is expected to be the same for all grades provided the chemical composition of the ore is the same.

3.5. Probability to Detect Diamonds

The objective is to obtain probability of detecting diamond no less than 95%. The tests are carried out with the kimberlite ore of different size: $-30$, $-75$, $-90$ and $-150$ mm. The notation $(−A + B)$ mm for ore size means that the largest dimension of the stone is smaller than A mm and the smallest dimension is larger than B mm. The kimberlite stones are arranged as a single layer in a tray. In one stone a hole was made where the diamond imitators of different sizes are placed. The intensity of neutron beam is $3.2 \times 10^7$ s$^{-1}$. The results of tests for decision making parameter $\sigma = 3.0$ are shown in Table 4.

Table 4. Probability to detect diamond in kimberlite stones of different size.

| Size of Diamond Imitator, mm | Size of Kimberlite Stones, mm | Detection Probability, % | Number of Measurements |
|------------------------------|--------------------------------|--------------------------|------------------------|
| 8                            | $-30 + 6$                      | 0.95                     | 23                     |
| 12                           | $-75 + 40$                     | 0.96                     | 18                     |
| 16                           | $-75 + 40$                     | 0.99                     | 20                     |
| 16                           | $-90 + 50$                     | 0.97                     | 19                     |
| 20                           | $-150 + 100$                   | 0.95                     | 20                     |

From the results in Table 4 one could conclude that the minimal detectable diamond size is 8 mm in ore of $-30 + 6$ mm. In Figure 9 the operator interface is shown for irradiation of 20 mm imitator inserted inside the kimberlite stone of $-90$ mm.

![Figure 9. The operator interface for irradiation of 20 mm imitator inserted inside the $-90$ mm kimberlite stone. In grey colored cells there is no enough statistics to calculate the carbon concentration, the green colored cells depict carbon excess less than $3\sigma$, the red ones show carbon excess larger than $3\sigma$.](image)
The interface shows color-coded excess of local concentration of carbon in each of 256 voxels. For large imitator its signal could be detected in several voxels and may appear in different configuration as it is shown in Figure 9. In that case the excess over background was as large as $7\sigma$.

4. Conclusions

A prototype of neutron separator based on tagged neutron method is constructed. The neutron module of the separator consists from 22 $\gamma$-detectors and a neutron generator with 256 $\alpha$-channels. The detection of diamonds is carried out by local carbon excess. Main advantage of the tagged neutron method is possibility to detect diamond inside the kimberlite stone without crushing. The tests of the prototype is carried out at Lomonosov mine of LLC “Severalmaz” (Archangelsk, Russia). It shows that:

- throughput of the prototype is 1060 kg/h
- minimal size of diamond imitator is 8 mm (5 carats)
- probability of false alarms is 3%
- probability to detect diamonds hidden in the stone is 95%
- in the stones $-90 + 50$ mm it is possible to find diamonds larger than 12 mm, in the stones $-150 + 100$ mm it is possible to find diamonds larger than 20 mm
- electricity consumption is 0.6 kW/ton of ore.

Therefore it is proved that the method works in the field conditions of a mine. However, the throughput is too small in comparison with 30–50 ton/hour needed for practical applications. To increase the throughput one needs large inspecting volume. As a first step in this direction the project of the separator on 5 ton/hour is prepared.

5. Patents

This work is resulted in the patent PCT/RU2017/000069 “Separator and method for the dry beneficiation of diamond ore”.

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References

1. Alexakhin, V.Y.; Bystritsky, V.M.; Zamyatin, N.I.; Zubarev, E.V.; Krasnoperov, A.V.; Rapatsky, V.L.; Rogov, Y.N.; Sadovsky, A.B.; Salamatin, A.V.; Salmin, R.A.; et al. Detection of Diamonds in Kimberlite by the Tagged Neutron Method. Nucl. Instrum. Methods 2015, 785, 9–13. [CrossRef]
2. Valkovic, V. 14 MeV Neutrons: Physics and Applications; CRC Press: Boca Raton, FL, USA, 2015; ISBN 13: 978-1482238006.
3. Hawkins, P.O.; Sutton, R.W. Compact pulsed generator of fast neutrons. Rev. Sci. Instrum. 1960, 31, 241–248. [CrossRef]
4. Rhodes, E.A.; Dickerman, C.E.; Peters, C.W. Associated-particle sealed-tube neutron probe for characterization of materials. In Proceedings of the Substance Detection Systems, Innsbruck, Austria, 28 March 1994; Volume 2092, pp. 288–300.
5. Rhodes, E.; Dickerman, C.E.; DeVolpi, A.; Peters, C.W. APSTNG: Radiation interrogation for verification of chemical and nuclear weapons. *IEEE Trans. Nucl. Sci.* 1992, 39, 1041–1045. [CrossRef]

6. Beyerle, A.; Hurley, J.P.; Tunnell, L. Design of an associated particle imaging system. Nuclear Instruments and Methods in Physics Research Section A: Accelerators, Spectrometers, Detectors and Associated Equipment. *Nucl. Instrum. Methods* 1990, A299, 458. [CrossRef]

7. Bystritsky, V.M.; Gerasimov, V.V.; Kadychevskiy, V.G.; Kobzev, A.P.; Nozdrin, A.A.; Rogov, Y.N.; Rapatsky, V.L.; Sadovsky, A.B.; Salamatin, A.V.; Sapozhnikov, M.G.; et al. DViN—Stationary setup for identification of explosives. *Phys. Part. Nucl. Lett.* 2008, 5, 441–446. [CrossRef]

8. Pesente, S.; Nebbia, G.; Viesti, G.; Daniele, F.; Fabris, D.; Lunardon, M.; Moretto, S.; Nad, K.; Sudac, D.; Valkovic, V. Progress in tagged neutron beams for cargo inspections. Nuclear Instruments and Methods in Physics Research Section B: Beam Interactions with Materials and Atoms. *Nucl. Instrum. Methods* 2007, 261, 268–271. [CrossRef]

9. Mihalczo, J.T.; Bingham, P.R.; Blackston, M.A.; Crye, J.M.; Grogan, B.R.; Hausladen, P.A.; McConchie, S.M.; Mullens, J.A. Fast Neutron Imaging with API DT Neutron Generators. In Proceedings of the International Technical and Scientific Conference—Portable Neutron Generators and Technologies on their Bases, The All Russian Institute of Automatics (VNIIA), Moscow, Russia, 28 September 2012; pp. 198–212.

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