Phase Diagram and Snap-Off Transition for Twisted Party Balloons

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All children enjoy inflating balloons and twisting them into different shapes and animals. Snapping the balloon into two separate compartments is a necessary step that bears resemblance to the pinch-off phenomenon for water droplet detached from the faucet. In addition to testing whether balloons exhibit the properties of self-similarity and memory effect that are often associated with the latter event, we determine their phase diagram by experiments. It turns out that a common party balloon does not just snap. They in fact can assume five more shapes, i.e., straight, necking, wrinkled, helix, and supercoil, depending on the twist angle and ratio of its length and diameter. Moreover, history also matters due to their prominent hysteresis. One may shift the phase boundary or/and reshuffle the phases by untwisting or lengthening the balloon at different twist angle and initial length. Heuristic models are provided to obtain analytic expressions for the phase boundaries.

Twisting and bending elastic filaments or ribbons [1] has fascinated scientists for centuries, such as a coil formed by twisting a rope [2] and tendril of the climbing plant [3][4]. In recent years, due to the progress in biology, researches on DNA and protein structures and functions make this topic popular again [5][7]. For a long rod or wire, a one-dimensional description suffices since the thickness is much smaller than the length. In this Letter, we investigate the twisting of an inflated party balloon, as in Fig. 1(a), for which the rubber thickness \( t \) is replaced by radius \( R \) that is comparable to length \( L \). As a result, the balloon geometry can be viewed as being intermediate between a 1-D rod [8][10] and a 2-D ribbon [11].

Balloon is an example of soft material that is easily accessible and fun to play with. When inflated with air or fluid, it exhibits many interesting phenomena, such as a longitudinal phase separation during inflating [12], deformation and bursting when it impacts a rigid wall [13], fragmentation due to bursting [14], and air transfer between two balloons [15]. Our initial goal is more mundane, i.e., we want to know how many configurations a twisted balloon can adopt besides the familiar snapping phase. It turns out that the phase diagram is not a state function of the twist angle \( \theta \) and ratio of length and diameter, but also depends on history. For instance, do you crank up \( \theta \) or allow it to relax while fixing \( L/2R \)? Alternatively, one may choose to increase \( L/2R \) while fixing \( \theta \), in which case the initial value of \( L/2R \) and \( \theta \) may also affect the phase boundaries \( \alpha \)/and possible configurations. Although similar hysteretic behavior has been reported for a stretched loop ribbon [1], the rearrangements of soap films in a triangular prism frame [16], and when the frequency of an applied force to zip or unzip DNA is varied [17], one cannot help but being mesmerized by clowns who take advantage of this property to transfigure the balloon in a magical way. Finally, we notice and spend time studying the similarity between the snap-off transition and pinch-off phenomena for water dripping from a faucet [18][19], bubble formation [20][21], elephant trunks of interstellar gas and dust in the Eagle Nebula [22], and the sticky “capture blob” used by Bolas spider [23].

Produced by Sempertex, our balloon samples come in three diameters, 1, 2 and 3 inches. They can be blown up to 60 inches long - about five times their original length. When inflated, their material characteristics are:
FIG. 2: Conserved quantity in Eq. (1) is checked in (a) and (b) for phase-2 and -3 with $L/2R = 1.5$. Circle and triangle represent torque and minimum radius $r_0$, with solid and open symbols denoting twist and untwist, in the double-$y$ plot vs $\theta$ for $L/2R = 1.4$ in (c), 2.0 in (d), and 14 in (e).

Young’s modulus $Y = 0.75$ GPa, thickness $t = 0.07$ mm, and shear modulus $S = 0.0002$ GPa. The experimental setup in Fig. 1(b) consists mainly of two parts, a frictionless rail and a force sensor. The rail is composed of two hollow coaxial cylinders, A and B, through which the balloon is inserted. Cylinder A is the active side via which we twist the balloon around a bearing fixed on a desk. As the stepping motor rotates at a steady angular velocity, a tension meter measures the twist force.

Why should the balloon voluntarily concave in phase 2 against the penalty of surface energy? By use of the elasticity relation for shearing, we can rewrite the constant torque in static equilibrium as

$$S \frac{r^3 t}{\sqrt{1 + (dr/dz)^2}} \frac{d\theta}{dz} = \text{const.} \quad (1)$$

This conserved quantity is verified in Fig. 2 (a,b) for the concave and smooth region. The dip in $4 < z < 8$ cm in Fig. 2(b) is presumably due to the weakening of $S$ by wrinkles. The $r^3$ factor in Eq. (1) informs us that lowering $r$ can redirect most shear angle into the concave segment.

In the following, we refer short and medium balloons to $L/2R \leq 2.5$ and $2.5 < L/2R \leq 8$. As shown in Fig. 1(d~f), their configuration evolves continuously from being (1) straight and smooth to (2) concave and smooth and (3) concave and wrinkled. Upon reaching the snapping phase 4 in Fig. 1(g), the balloon suddenly loses its resistance. In contrast to being continuous in Fig. 2(c), the transition in Fig. 2(d) is abrupt for a medium balloon. For short balloons, the torque in Fig. 2(c) increases linearly with $\theta$ during phases 1 and 2, but bends over in phase 3 before dropping to zero at phase 4. This mechanical response is reminiscent of that for a twisted cylindrical paper or metal shell [24], except for the absence of phases 2 and 4 and only a partial region about $2R$ is initially concave.

For a long balloon, the configurations associated with phases (2~4) are now replaced by (5) helix and (6) supercoil, as shown in Fig. 1(h, i). The torque plummets discontinuously with an extent that decreases with each appearance of a new supercoil. A larger slope in its buildup follows this to the next drop. Why? By examining the marker line on the balloon, we know that shear stress hardly affects the bended region, i.e., the supercoil. Thus, according to Eq. (2) to be shown later, the torque will be inversely proportion to a shortened $L$ that measures only the straight region.

Hysteresis is observed when the balloon is allowed to untwist. The torque in Fig. 2(c, d) changes continuously from phase 4 to 3 to the best resolution of our force meter, and the neck radius does not pop up to full $R$ until $\theta$ is much smaller than the critical angle when phase 1 transits to 2 in the forward twist process. This relaxation line is reversible until it meets the forward twisting line that will take over the evolution. Relaxation for long balloons in Fig. 2(e) is special in that the discontinuous change in torque remains when phase 6 is reverted to 5. Considering that helix and supercoil phases are shared by twisted filaments, it comes as no surprise that their torque vs. $\theta$ relation is similar [2]. Since the marker line always reverts to horizontal after $\theta$ relaxes to zero, we believe hysteresis is intrinsic and not due to plasticity.

In order to determine the phase boundaries in Fig. 3(a), we need to write down the potential energy characteristic to all phases. Shear energy for phase 1 is the
When the shear angle reaches $E_1$ by optimizing two remaining free parameters can then be determined. In other words, the transition angle $\theta_{3,4}$ can be estimated by equating Eqs. (2) and (5):

$$\theta_{3,4} \sim \sqrt{\frac{T L}{St R}}. \tag{6}$$

Phase 5 for long balloons is trickier in that it relieves part of the shear energy by angle $\eta$ by distorting or bending itself into a helix. Furthermore, a second bending term is needed because our experimental setup in Fig. 1(b) requires both ends of the balloon aligned. By twisting with real balloons, it is easy to realize that this extra energy (1) is redundant for $\eta = 0$ and $2\pi$ when the alignment is automatic, and (2) can be diminished by lengthening the balloon which justifies an additional factor of $R/L$. Overall, we expect

$$E_5 \sim \frac{SR^3t}{L} (\theta - \eta)^2 + K_b \frac{\eta}{L}^2 R L + K_b \frac{\eta (2\pi - \eta)}{L^2} R^2 \tag{7}$$

where $K_b \sim Y R^2 t$ from elasticity with $\eta/L$ in the second term coming from the curvature $1/\rho$ that can be derived from the Pythagorean theorem in Fig. 1(h), $\rho^2 = (\rho - \xi)^2 + L^2$, that requires $\rho \sim L^2/\xi$. The fact that $\xi$ is linked to $\eta$ by $\xi \sim \eta L$ immediately leads to $\rho \sim L/\eta$.

Minimizing Eq. (7) with respect to $\eta$ gives

$$\eta \sim \frac{S \theta - Y \pi \frac{R}{L}}{S + Y (1 - 2\pi)}. \tag{8}$$

In order for phase 1 to enter phase 5 and $\eta$ to increase from zero, Eq. (8) sets a lower bound on $\theta$ that can be duly identified as the boundary

$$\theta_{1,5} \sim \frac{Y R}{S L}. \tag{9}$$

As the twisting continues, we come to the next boundary by setting $\eta = 2\pi$ in Eq. (7). This renders

$$\theta_{5,6} \sim 2\pi + \frac{Y}{S}, \tag{10}$$

independent of $L, R$. The same conclusion has been derived \[25\] for a twisted filament.

Having established in Fig. 2(c-e) that the value of torque and $r_0$ can be different at the same $\theta$, depending on the sign of $d\theta/dt$, we thus expect a different phase diagram for relaxation. As plotted in Fig. 3(b), it turns out that the phase boundary of $\theta_{3,4}$ indeed changes. Instead of following Eq. (6), its value decreases and is roughly independent of $L/2R$ for short and medium balloons. For long balloons, $\theta_{5,6}$ now increases rather than decreases with $L/2R$ as Eq. (10). In the mean time, $\theta_{1,2}$ and $\theta_{1,5}$ becomes negligibly small for all lengths, in contrast to Eqs. (4) and (9). It is surprising that a system as simple as the party balloon should exhibit a third or even fourth phase diagram when we lengthen $L$. Experimentally this is achieved by shifting the moving end B in Fig. 1(a) while holding the balloon to keep the twist angle fixed.
If we start from phase 4, it remains so without entering phase 6, as shown in Fig. 3(c). But if we start from phase 5, it will transit to phase 1 in Fig. 3(d).

Like the collapse of a over-stretched bubble film, we expect the configuration of a medium balloon to transit from reversible to irreversible beyond $\theta_{3,4}$. A high-speed camera with 8000 fps captures the dynamical process that leads up to the singular neck. Photos in Fig. 4(a) and (b) are reversible and correspond to phase 2 and 3. Being taken at successive time at the same twist angle, Fig. 4(c) and (d), categorized as phase 3 and 4, thus reveals their irreversibility. In the following, we define

$$\tilde{\tau} = (\tau_0 - \tau)(\sqrt{\frac{2 \sigma}{\beta}} L^2)/R^3$$

where $\sigma$ is the surface density, $\tau_0$ is the time of pinch-off and $\tau$ is real time. Their profile mapped out by photo detection in Fig. 4(e) can be divided into three regimes. Regime I is reversible in which the shrink speed $v$ is determined by the twist velocity. After a brief acceleration, $v$ is roughly a constant in most of regime II, as demonstrated in Fig. 4(f) that shows $r_0/R$ vs. $\tilde{\tau}$. This can be understood by comparing the energy scales $\sigma v^2 \sim St$ from inertia and shear stress. Deceleration finally halts the shrinkage in regime III.

To test whether there exists the property of self-similarity that is characteristic of the pinch-off phenomenon, we rescale the profiles in regime II by $r/(R\tilde{\tau}^\alpha)$ and $(z - z_0)/(R\tilde{\tau}^\beta)$ where $\alpha = 1$ and $\beta = 2$. As shown in Fig. 4(g), they can indeed be made to collapse to a master curve. The scaling exponent $\alpha = 1$ is expected from the constant $v$. Why is our observation $\alpha < \beta$ different from $0 < \beta \leq \alpha \leq 1$ for most pinch-off systems? For starters, rubber does not obey the Rayleigh-Plateau instability that predicts the breakup of water column occurs when $r \leq z - z_0$. Therefore, $\beta - \alpha < 0$ is required to revert the relative size in at small $\tilde{\tau}$. Figure 4(h) shows that $v \propto (L/2R)^2$, as expected from Eq. (6) since longer balloons pump more twist angle and shear energy into the concave segment at the snapping transition. It is worth noting that this dependence on the initial length violates the lack of memory effect which property is often flaunted for pinch-off systems where $v$ only depends on the flow of inner liquid. There has been a debate whether this oblivion of initial condition is a natural consequence of the scaling property. Had our snap-off transition shared the same physics as pinch-off phenomenon, the fact that Fig. 4(e-h) bleaches this correlation would have supported the negative view held by Ref.

In summary, we show that party balloons do not always snap when twisted. It in fact exhibits five other configurations, depending on the twist angle and aspect ratio between length and diameter. Physical arguments, including the finding of a conserved quantity that links radius and the gradient of strain, are provided to derive and verify boundaries in the phase diagram obtained empirically. Hysteresis is surprisingly pronounced in this simple system. The allowed phases and location of phase boundaries are subject to change not only when the balloon is untwisted, but when lengthened at different twist angles. Special attention is paid to clarify the analogy between snapping and the well-studied pinch-off phenomenon in fluid dynamics. Unlike the latter, the shrinking speed of balloon is sensitive to the initial length and radius.

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