A Programmable Proton Exchange Membrane Fuel Cell Emulator Based on a DC-DC Synchronous Buck Converter

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Abstract: In the development of fuel cell (FC) systems and related control technologies, it is convenient to employ FC emulators instead of using real FC systems for the testing of various FC characteristic parameters and operating conditions. This paper proposes a low-cost, fast-response, and programmable proton exchange membrane FC (PEMFC) hardware emulator based on a two-switch DC-DC synchronous buck converter and a digital signal processor (DSP) acting as a kernel controller. The V-I characteristics and control signals of the emulated PEMFC are determined through system analysis, modeling, and digitalization of the PEMFC model. The developed PEMFC model is then used to construct a programmable user-interface module through C programming. The programmable digital module can be directly embedded into the DSP for simulation studies and experimental tests on various hardware integrated implementations of FCs. Results obtained from simulations and hardware tests are in good consistent with each other and both prove the correctness and effectiveness of the developed converter based PEMFC emulator.

Keywords: proton exchange membrane fuel cell (PEMFC) emulator, digital signal processor (DSP), DC-DC synchronous buck converter.

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1. Introduction

In recent years, people are paying more and more attention to the issue of greenhouse gas emissions. Therefore, there is little room left for further development of fossil fuel-based power generation. However, the energy demand for various industrial sectors continues to grow. Among the reported low-carbon power generation technologies, fuel cell (FC) is one of the fairly attractive options. A FC is a device that converts the chemical energy of hydrogen directly into electrical energy, and the resulting emissions are only heat and clean water. The main advantages of FCs include portability, high reliability, low pollutant emissions, and low maintenance requirements; it is recognized as a clean energy resource with high application flexibility. At present, there are a lot of research and
publications related to FCs [1-8]. Although FC is a clean energy resource, the system’s output is usually an unregulated low DC voltage. It is a basic processing stage to adjust the output voltage with a suitable power converter interface before the connection to a grid or a load.

When designing a FC power converter, typical considerations include the FC’s nonlinear dynamics and steady state characteristics, which are strongly depending on the control technology used and the design parameters of each FC. Programmable FC emulator provides several advantages through digital formulation of FC types, environmental parameters, operating ranges, etc. Some mathematical models and simulation verification of proton exchange membrane FCs (PEMFCs) have been proposed in [9-13]. A Matlab/Simulink model was proposed in [9], and the effect of double-layer capacitor on the performance was also explored. The polarization equation of a humidified low-temperature PEMFC was proposed for all possible current densities and experimentally validated using a novel methodology in [10]. C. Restrepo et al. [11] proposed an improved diffusive model based on a finite-dimensional linear parameter-varying model and data of current inputs and voltage outputs. A 1.2-kW, Ballard Nexa FC was used to validate the advantages of the proposed model. D. Zhou et al. proposed two two-dimensional real-time models using tridiagonal matrix algorithm (Thomas algorithm) [12], validated using Ballard Nexa 1.2-kW FC, and a proposed secant algorithm [13] was validated using a computational COMSOL FC model. Hardware implementation of FC emulators can be found in [14-19]. In [14], a new software-hardware-integrated emulator was proposed based on electromotive force and internal impedance obtained through (1) constant current load characteristics and (2) step response characteristics + frequency characteristics, respectively. This model was later modified in [15] for a wider application frequency range. To match the power supply and the power requirement of an FC emulator, F. Flores-Bahamonde et al. [16] used a DC-DC non-inverting buck-boost converter-based DC transformer with a DC power supply. Ballard NEXA 1.2 kW diffusive FC model was used to validate the proposed method. In [17], a real-time FC emulator for Horizon H-500 was built based on a scaled-down electrical equivalent circuit. The mathematical and electrical models were simulated in MATLAB/Simulink environment, and then the implementation validated the design. A DC-DC buck converter was used in [18] as the FC emulator in MATLAB/Simulink environment with PI controller for voltage mode control. Relative humidity was considered in this design. P. A. Lindahl et al. [19] proposed a universal FC emulator that allowed simultaneous investigation of single cell and the entire hardware by employing a voltage amplifier whose input signal is the voltage output of a single cell. A single planar solid oxide FC (SOFC) was used to demonstrate the design. All of the abovementioned schemes, designed for a specific FC, are lacking application flexibility.

To eliminate the above disadvantage, this paper proposes a power converter based low-cost, fast-response and programmable PEMFC emulator. The proposed emulator adopts a two-switch DC-DC synchronous buck power converter as the main circuit and a DSP as the control core for achieving programmability and digital control mechanism. Following this introduction section, the basic principle of FC, FC’s simple equivalent model, and a detailed equivalent model are introduced in the next section. In section three, the derivation of PEMFC models is explained, and an actual PEMFC characteristic curve is modeled and verified to obtain its output voltage-current (V-I) equation to be embedded into the DSP’s interface module. In the fourth section, the accuracy and effectiveness of the proposed emulator are proven through typical simulation and experimental results. Finally, this paper is concluded in the last section.

2. Materials and Methods
2.1. PEMFC System.

The schematic of a FC system is shown in Fig. 1. In response to the need in addressing the systematic design procedure of a programmable FC emulator, this paper explores two PEMFC models, i.e. simplified model and detailed model [20].
2.1.1. Simplified PEMFC model.

The simplified model of a PEMFC is shown in Fig. 2, including a controlled voltage source and a fixed resistance in series. The internal voltage of FC (Equation (1)), Tafel slope (Equation (2)), and voltage output of FC (Equation (3)) can be expressed as in (1)-(3).

\[
E = E_\text{oc} - N \Delta \ln(i_\text{f}/i_\text{b}) \times 11 \left[ (sT_\text{r}/3) + 1 \right]; \quad (1)
\]

\[
A = R \times T \left[ (z \times \alpha \times F) \right]; \quad (2)
\]

\[
V_{\text{fc}} = E - R_{\text{int}} \times i_{\text{f}}; \quad (3)
\]

where \( R_{\text{int}} \) represents internal resistance (Ω), \( V_{\text{fc}} \) represents FC voltage (V), \( R = 8.3145 \text{ J/(mol·K)} \), \( T_{\text{r}} \) represents response time (for 95% of final value) (s), \( F = 96485 \text{ A·s/mol} \), and \( z \) represents number of moving electrons (which equals 2).

\[
E_{\text{oc}} = K_i \times E_n; \quad (4)
\]

\[
i_{\text{f}} = \left[ \left( z \times F \times k \times (P_{\text{H}_2} + P_{\text{O}_2}) \right) / \text{Rh} \right] \exp(-\Delta G / RT); \quad (5)
\]

where \( P_{\text{O}_2} \) represents partial pressure of oxygen (atm), \( k = 1.38 \times 10^{-23} \text{ J/K} \), \( b = 6.626 \times 10^{-34} \text{ J·s} \), \( K_i \) is a constant under normal operation condition, \( E_n \) represents Nernst voltage (V), \( \Delta G \) represents activation barrier (J), \( \alpha \) represents charge transfer coefficient, \( T \) represents operating temperature (K), and \( P_{\text{H}_2} \) represents partial pressure of hydrogen (atm). As shown in Fig. 3, blocks A, B, and C calculate the new values of \( E_{\text{oc}}, i_{\text{f}}, \) and \( A \). First, block A determines the utilization rate of hydrogen and oxygen (Equation (6) and (7)) as follows:

\[
U_{\text{H}_2} = (6000 \times R \times T \times i_\text{f}) / (z \times F \times P_{\text{H}_2} \times V_{\text{fuel}} \times x \times P_{\text{fuel}}); \quad (6)
\]

\[
U_{\text{O}_2} = (6000 \times R \times T \times i_\text{f}) / (z \times F \times P_{\text{O}_2} \times V_{\text{air}} \times y \times P_{\text{air}}); \quad (7)
\]

where \( P_{\text{fuel}} \) represents absolute supply pressure of fuel (atm), \( V_{\text{fuel}} \) represents air flow rate (l/min), \( P_{\text{air}} \) represents absolute supply pressure of air (atm), \( x \) represents composition percentage of hydrogen in the fuel (%), \( V_{\text{fuel}} \) represents fuel flow rate (l/min), and \( y \) represents composition percentage of oxygen in the oxidant (%).

2.1.2 Detailed PEMFC Model.

The detailed model of PEMFC is shown in Fig. 3. To construct a detailed model, pressures, temperatures, compositions, and flow rates of air and fuel are all considered in the calculation. These parameter changes will directly affect Tafel slope, exchange current, and the open circuit voltage. The equivalent circuit of this model is roughly the same as the simplified model, with the difference being that pressures and flow rate as needed to update FC related parameters. The difference is that the user can input real-time pressures and flow rates to update related parameters. The detailed calculation for open-circuit voltage and exchange current is shown in (4) and (5), respectively.

\[
E_{\text{oc}} = K_i \times E_n; \quad (4)
\]

\[
i_{\text{f}} = \left[ \left( z \times F \times k \times (P_{\text{H}_2} + P_{\text{O}_2}) \right) / \text{Rh} \right] \exp(-\Delta G / RT); \quad (5)
\]

Partial pressures and Nernst voltage and be determined in block B as follows:
The relationship between the input and output voltages is as follows:

\[ V_{fc} = D \times V_{in} \]

where the duty cycle \( D \) is as follows:

\[ D = \frac{t_{on}}{T_s} \]

When \( S1 \) is on, the voltage across the inductor \( L \) is

\[ V_L(t) = L \frac{di_L}{dt} = V_{in} - V_{fc} \]

During on period, inductor current increases from \( i_{L_{min}} \) to \( i_{L_{max}} \), where

\[ i_{L_{min}} = i_L(0) = \frac{V_{fc}}{R_f} - \frac{\Delta I}{2} \]

and

\[ i_{L_{max}} = i_L(DT) = \frac{V_{fc}}{R_f} + \frac{\Delta I}{2} \]

where \( R_f \) represents FC resistance. Capacitor current \( i_c \) is as follows:

\[ i_c = i_L(T) - i_k(T) = i_L(T) - \frac{V_{fc}}{R} \]

\[ i_c(0) = -\frac{\Delta I}{2} \]

\[ i_c(DT) = \frac{\Delta I}{2} \]

Because of the linear change of \( i_c \), the average inductance current is half of the peak value of the triangle wave. The peak value of the triangular wave is \( \Delta I/2 \) and thus equal \( \Delta I/4 \). According to average current in half of the period, the output voltage change \( \Delta V' \) can be expressed as follows:

\[ \Delta V = \left( I_c \times \frac{T}{2} \right) / C = \Delta I \times T / 8C = \Delta I / 8fC \]
In order to improve output current ripple, a low pass filter (LPF) can be used to help suppress the variations. In addition, using a switch S2 in parallel with the filter solves the efficiency issue related to filter inductance discharge, giving it a low-resistance path to discharge while S1 is off. As shown in Fig. 5, while S1 is on, and S2 is off, the body diode of S2 is off because of the reverse bias, and thus the energy is sent to the inductor, the capacitor, and the load; while S1 is off, and S2 is on, the current is able to freewheel, sending the energy stored in the inductor to the output terminal.

2.3. FC Model Verification.

The model parameters in [20] are first adopted to verify the correctness of the proposed FC mathematical model. For steady state fixed-point verification, the nominal operation parameters are as follows: FC voltages at 0 A and 1 A \([E_0, V]\) = [65,63], nominal operation point \([I_{nom}, V_{nom}] = [133,3,45]\), maximum operation point \([I_{max}, V_{max}] = [225,37]\), nominal FC stack efficiency = 55\%, number of FCs in series \(N = 65\), operation temperature = 65 °C, nominal air flow rate \(V_{air(nom)} = 297 \text{l/min}\), nominal compositions of fuel and air \([x_{nom}, y_{nom}] = [99.999\%, 21.1\%]\), and nominal supply pressures \([P_{H2}, P_{air}] = [1.5,1]\). The verification results are shown in Fig. 6. The proposed model is capable of accurately calculating the FC V-I curve, proving the correctness of this module.

3. Results and Discussion

3.1. Simulation and Hardware Implementation Results.

This section verifies the characteristics of the proposed 110W PEMFC mathematical model and the hardware emulator at different temperatures through simulation and implementation measurements. The specifications of experimental circuit and measuring devices for the proposed PEMFC emulator are as follows: voltage input \(V_{in} = 200 \text{V}\), buck inductance \(L = 500 \mu\text{H}\), output capacitance \(C = 47 \mu\text{F}\), maximum short circuit current \(I_{sh,max} = 5.5 \text{ & 7.5 (A)}\), and maximum open circuit voltage \(V_{oc,max} = 42 \text{ & 45.67 (V)}\).

Figure 7 shows the experimental setup and measuring devices, and Fig. 8 shows the simulation results of V-I and P-I curves using Matlab at the different operating temperatures. The hardware implementation test is performed at two operating temperatures: 45°C and 85 °C. Figs. 9 & 10 show the comparison between simulated and implemented V-I and P-I curves of the proposed PEMFC emulator at 45°C operating temperature, respectively (I_{fc}: 2A/div; V_{in}: 2V/div; P_{fc}: 2W/div; T: 1s/div).
4. Conclusions

This paper has successfully developed an 110W, low-cost, programmable PEMFC emulator. The proposed PEMFC hardware emulator employs a DC-DC synchronous buck converter as the main circuit and a DSP as the digital controller to achieve fast tracking of the dynamic V-I characteristics of a real PEMFC and to achieve the feature of programmable emulation mechanisms. In the processes of emulation, the real-time voltage commands, the corresponding output voltage values of a given PEMFC operating conditions, were calculated using a derived mathematical model that considers the pressure, temperature, composition percentage, and flow rate of both fuel and air. A programmable digital user interface was then constructed through a C programming module. The correctness and effectiveness of the proposed PEMFC emulator have been tested through simulation at different operating temperatures and verified with hardware implementation at two operating temperatures.

Figs. 11 & 12 show the comparison between simulated and implemented V-I and P-I curves of the proposed PEMFC emulator at 85°C operating temperature, respectively ($I_f$: 2A/div; $V_{in}$: 2V/div; $P_{fc}$: 2W/div; $T$: 1s/div).
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Conflicts of Interest

The authors declare no conflict of interest.

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