I. INTRODUCTION

TEMPERATURE sensors play a fundamental role in countless technologies and industrial applications. The most common type of temperature sensors measure heat transported to the detector through conductive/convective transport. Examples of such sensors are thermocouples, resistance temperature detectors, thermistors and Si- and Ge- semiconductors embedded in integrated circuits [1], [2]. Most of these technologies rely on changes in resistance of some components/materials due to changes in temperature. Few instances of capacitive sensors also exist and display sensitivities that are about 1%/°C lower than those of more established sensing technologies [3]. Unlike contact temperature sensors, IR thermal sensors measure the temperature transported to the detector through infrared radiation. They are attractive because they are non-contact and have the potential to acquire information and detect events even in low-light and poor visual conditions. Among the different IR detectors, bolometers are extremely interesting for their commercial applications. In a bolometer, the incident IR radiation is absorbed by a black body, which heats up due to the absorbed energy. This change in temperature is then measured by a thermally-responsive layer as a change in resistivity or dielectric constant. Significant efforts have been dedicated to develop and optimize temperature resistive layers for microbolometers, as they represent the principal bottleneck for their sensitivity. Nowadays, the most employed microbolometers are VOx [4]–[6], Si [7] and Si-Ge alloys [8], [9], that display a temperature coefficient of resistance (TCR) between 2%/°C and 5%/°C.

Temperature sensors that rely on electromechanical principles – where the electrical response stems from engineered arrangements of materials that yield desired deformations and changes in resistance/capacitance/dielectric constant – are not common. Examples are capacitive sensors consisting of multi-layer cantilevers that bend in response to differential thermal expansion in each layer [10]–[12]. The bending deformations cause changes in the dielectric constant of one of the inner layers, leading to capacitance variations that can be detected by a readout circuit. However, these technologies are...
hampered by the fact that the strains achievable in a cantilever are limited, and the changes in dielectric constants with strains are small. Nonetheless, they find applications in MEMS, for example, due to their low energy consumption and low heat dissipation.

In recent years, considerable attention has been devoted to engineering structures with tailored response to environmental stimuli, such as temperature [13]–[18]. Through geometric arrangements of materials with contrasting coefficient of thermal expansion (CTE), it is possible to obtain composite structures with extreme values of effective CTE. This includes, for example, structures with zero or negative effective CTE [19]–[21], or structures that can achieve extreme shape changes in response to temperature variations [22]–[25]. In recent work, some of the authors of this letter demonstrated that joining a high-CTE frame with a low-CTE bar allows to produce large tangential displacements of the outer frame [26], owing to displacement-amplification mechanisms [27].

In this letter, we leverage similar displacement amplification mechanisms to create capacitive temperature sensors. We start from thin layers of materials, one conductive and one dielectric, with drastically-different thermal expansion. We show that, by engineering their spatial arrangement as to cause large relative displacements between conductive and dielectric layers, we produce large changes in capacitance per degree, of about 600% over 65°C. This amplified bulging can either be directed inwards or outwards. In our case, the fabrication process biases the outer layer to displace towards the inner one, and to close the air gaps. In turn, this causes an increase in capacitance.

II. UNIT CELL DESIGN

A sketch of a cross-section of the displacement-amplifying structure used to create our sensors is shown in Fig. 1(a). It features two outer metallic layers of high-CTE material (aluminum foil) and an inner low-CTE, dielectric layer (paper). The layers are bonded with cyanoacrylate glue at selected locations, that are chosen to create large air gaps for the metallic layers to expand. As we increase temperature, the high-CTE conductive layers tend to expand (axially) more than the dielectric one. However, this axial expansion is limited by the presence of the low-CTE dielectric and by the fact that the layers are partially glued together [26]. Thus, the conductive layers buckle and bulge tangentially (Fig. 1(c)). The tangential displacement, in particular, is much larger than any axial displacement in the layers – hence the displacement amplification term. This amplified bulging can either be directed inwards or outwards. In our case, the fabrication process biases the outer layers to displace towards the inner one, and to close the air gaps. In turn, this causes an increase in capacitance.

III. THEORETICAL ANALYSIS

Our first step is to perform numerical simulations on the two-dimensional version of our sensor shown in Fig. 1(a). To do so, we resort to the commercial finite element (FE) platform Abaqus/Standard. We select 8-node bi-quadratic plane strain quadrilateral elements to perform the analysis, and we consider geometric nonlinearities. The inner, low-CTE, dielectric layer is modeled as a beam of length $l_d = 20 \text{ mm}$ and thickness $t_d = 50 \mu\text{m}$, and is made of paper, with Young’s modulus $E_L = 3 \text{ GPa}$, Poisson’s ratio $\nu_L = 0.25$, coefficient of thermal expansion $\alpha_L = 4 \times 10^{-6}/\text{°C}$. The outer high-CTE layers are here represented by beams of length $l_c = 20 \text{ mm}$ and thickness $t_c = 12 \mu\text{m}$, and are made of Aluminum foil, with $E_H = 70 \text{ GPa}$, $\nu_H = 0.33$, and $\alpha_H = 23.1 \times 10^{-6}/\text{°C}$ [29].

Our model also includes layers of glue, represented as blocks of length $l_g = 2 \text{ mm}$; since we have little control over the glue thickness, we fit this parameter to match our experimental results. The most accurate fit yields $t_g = 71.56 \mu\text{m}$. Finally, we assume the coefficients of thermal expansion to be constant over large temperature ranges.

The simulation results for a single unit are given in Fig. 1(b). We choose $T_i = 10\text{°C}$ as the initial temperature, while the final one is $T_f = 75\text{°C}$. As the temperature rises, the metallic layer expands tangentially; its displacement is shown by the dashed curve. We can appreciate that these displacements are of the order of tens of $\mu\text{m}$ and are large in comparison to the individual layer thicknesses.

Obtaining an accurate measure of the change of capacitance as a function of temperature in our simulations is no simple task, as it requires us to understand the relationship between capacitance and deformation. There are two different cross-sections in our capacitive temperature sensors: one, region A, consists of glue, dielectric and metallic layers; the other one, region B, consists of dielectric, metal layers and the air gap. It is important to note that the paper absorbs some of the glue after it is applied, and this causes its dielectric constant to be higher than the nominal value for paper-only. The characterization of the dielectric constant of the glue-impregnated paper is provided in the Appendix.

In order to obtain the temperature-dependent capacitance of this sensor from our simulations, we need to calculate the
The capacitance of regions A and B (Fig. 1(a)), and add them up. The capacitance of Region A (made of glue, dielectric and metal layers) is assumed to be constant and is calculated as

\[ C_A = \frac{C_g C_{dA}}{C_g + C_{dA}}. \]  

(1)

where

\[ C_g = \frac{\kappa_g \varepsilon_0 A_A}{2t_g}, \quad C_{dA} = \frac{\kappa_d \varepsilon_0 A_A}{t_d}. \]  

(2)

The capacitance of the Region B is temperature dependent and it is calculated as

\[ C_B(T) = \frac{C_{\text{air}}(T) C_{dB}}{C_{\text{air}}(T) + C_{dB}}, \]  

(3)

where

\[ C_{\text{air}}(T) = \frac{\kappa_{\text{air}} \varepsilon_0 A_B}{2t_{\text{air}}(T)}, \quad C_{dB} = \frac{\kappa_d \varepsilon_0 A_B}{t_d} \]  

(4)

and

\[ t_{\text{air}}(T) = t_g - \frac{1}{n} \sum_{i=1}^{n} d_i(T). \]  

(5)

In Eqs. 1-5, \( C_A \) is the capacitance of Region A, \( C_B \) is the capacitance of Region B, \( A_A \) is the cross-sectional area of region A, \( A_B \) is the area of region B, \( \kappa_g \) is the relative permittivity of glue, \( \kappa_{\text{air}} \) is the relative permittivity of air, \( \kappa_d \) is the relative permittivity of the dielectric layer (glue-impregnated paper), \( \varepsilon_0 \) is the vacuum permittivity, \( t_g \) is the thickness of the glue layer, \( t_d \) is the thickness of the dielectric layer, \( n \) is the number of nodes corresponding to the lower surface of the metallic layer in the FEM model, and \( d_i \) is the displacement of each node. Finally, the total temperature-dependent capacitance of the sensor can be calculated as \( C_{\text{total}}(T) = C_A + C_B(T) \).

Using the numerical displacement results shown in Fig. 1(b) and this definition of total capacitance, we plot the variation of capacitance as a function of temperature in Fig. 1(b). We can see that the displacement of the conducting layers, as previously claimed, is accompanied by large changes in capacitance, of the order of 1000 pF over a range of 65°C. To validate our numerical predictions, we manufacture and test a set of paper-aluminum sensors, fabricated as described in Appendix A.

### IV. Experimental Validation

Capacitors are nowadays fabricated using different approaches (e.g., electrolytic, ceramic, tantalum, etc.). Manufacturers provide various figures of merit to compare the performances of different components. The most important are the frequency behavior, the operating voltage and the temperature dependence. The frequency dependence of a capacitor provides its effectiveness when used in decoupling supplies from the input noise. For this study, measuring the frequency behavior of our sensors is important for two reasons: (1) at the operating frequency, the sensors have to be away from their resonances to avoid unwanted oscillations; and (2) their parasitic resistance and inductance have to be negligible. Therefore, we measure the change of capacitance as a function of frequency in our sample, to select the most effective operating frequency for the readout system (Fig. 5(a) of the Appendix). The drop in the capacitance for increasing frequencies is likely caused by the decrease of the paper dielectric constant, as relaxation processes arise in the paper matrix [30]. In principle, since there is no resonance in the investigated frequency range, we could have chosen any frequency. However, in order to decrease the effect of parasitics on the measurement, we target the lower frequency spectrum (20 – 50 Hz) to electrically stimulate the sensor. Given the frequency dependence of the capacitance, we measure the dielectric constant through impedance spectroscopy (Fig. 5(b) of the Appendix) in order to fit the experimental results and the numerics. The static permittivity was measured to be 20. However, given the effect of frequency on the capacitance we used the value of 15.81 to fit the experimental data with the numerical simulation. After this study, we finalized the design of the capacitance meter based on the measurement of the phase lag of a first order RC circuit (Fig. 6 of the Appendix), which was then implemented on a printed circuit board.

The second figure of merit for the capacitive temperature sensor is the operating voltage. The magnitude of the applied field can break the dielectric, or lower the permittivity, by influencing the spontaneous polarization of the capacitor. When measuring the dependence of the capacitance to the applied voltage (100 mVpp, 250 mVpp and 500 mVpp) at different frequencies, we found no differences.

Lastly, we analyze the change of the capacitance as a function of temperature. Standard capacitors are built to have the least change of capacitance with temperature change. In this work, since the paper capacitors are used as temperature sensors, our objective is to obtain a change in capacitance as large as possible for a given \( \Delta T \). To assess the performance of the sensors, we cycle the temperature in their environment from 8°C to 45°C for over 5 hours (Fig. 2(a)). The capacitance is acquired by the capacitance meter at a sampling rate of 44 S/s. Over this temperature range, the capacitance is measured to vary between \( \sim 200 \text{pF} \) to \( \sim 450 \text{pF} \). As it can be seen in a zoomed-in section of the cycles (Fig. 2(b)) and in the capacitance versus temperature plot (Fig. 2(c)), the relation between temperature and capacitance is nonlinear. In this scenario, a linear temperature coefficient of resistance (TCR) cannot be defined. Therefore, we define the sensor’s temperature response as the ratio between the capacitance at the highest temperature (45°C) divided by the capacitance at the lowest temperature (8°C) of the temperature cycle. The response is shown in figure Fig. 2(d) as a function of the cycle number. The capacitance more than doubles over a 37°C interval and is stable over time. The stability over time is also confirmed by Fig. 2(e), where the capacitance at different temperatures (10°C to 45°C in 5°C increments) is plotted versus the cycle number. The capacitance values measured at different temperatures are constant over time.

As shown in Fig. 2(c), due to the thermal inertia of the system, the capacitance versus temperature shows hysteresis behavior, which makes it challenging to effectively compare the experimental and numerical results. Therefore,
we characterize the system with temperature steps instead of temperature cycles. By doing so, we allow the temperature on the samples to settle, to account for the thermal inertia of the system and the consequent time, achieving a quasi-static regime. The temperature is controlled via a PID controller and raised from $10^\circ C$ to $75^\circ C$ in steps of $5^\circ C$, and held constant for 10 minutes (Fig. 3(a)).

As in Fig. 2, the capacitance closely follows the temperature, going from $\sim200\,\text{pF}$ at $10^\circ C$ to $1200\,\text{pF}$ at $75^\circ C$, and shows that the sample is stable over time (Fig. 3(b)). The capacitance versus temperature curve measured following this procedure is then compared to the numerical results (Fig. 3(c)), finding excellent agreement.

To test the functionality of the capacitive sensor in a real-world scenario, we use the paper capacitors as IR absorbers. We fabricate a standard paper capacitor following the procedure described in Appendix A, sandwiching a thin piece of paper between two aluminum layers. We apply black paint on top of one of the two aluminum layers to create a surface that absorbs the incident IR radiation. As the radiation is absorbed by the black paint, the temperature of the absorbing layer increases, transferring the heat from the absorbing layer to the aluminum foil; this, in turn, alters the capacitance of the sensor. The sensor is kept on a thermoelectric cooler and a PID controller, in order to keep its temperature constant and to isolate the effects of the absorbed radiation. The radiation source is turned ON and OFF periodically for 10 ms, and the capacitance is measured using the readout systems described in the Appendix C (Fig. 4(a)).

From the time evolution of the measured capacitance (Fig. 4(b)), we can see that this is constant when the IR source is off, while an increase in capacitance is registered when turning on the IR source. we can also see that the sensor recovers after each ON/OFF cycle.

**V. CONCLUSION**

In this work, we have demonstrated that it is possible to create high-performing capacitive temperature sensors by leveraging mechanical displacement-amplification mechanisms. We have also shown that these sensors can be used for IR sensing applications. The proposed mechanism is suitable for micro-manufacturing and for the creation of low-cost IR sensors. For example, the fabrication of suspended Al membranes on top of a $\text{Si}$ base and a $\text{SiO}_2$ dielectric layer is a possible approach [31].
Micro-bolometers cover more than 95% of the uncooled IR detectors market [32]. The most common sensitive layer used in micro-bolometers is vanadium oxide, having a coefficient of resistance at room temperature of more than 4% per degree [33], [34]. Compared to uncooled micro-bolometers, the proposed micro-mechanism can achieve considerably higher sensitivity. Moreover, spatial arrays of our sensors could be used to create temperature sensing surfaces with finite pixellation, that could find use as low-cost temperature mapping devices in applications where monitoring the temperature is crucial, such as to monitor the health of batteries for electric vehicles.

**APPENDIX A**

**MATERIALS AND METHODS**

To validate our numerical and theoretical predictions, we manufacture and test a set of bi-material specimens. We use desktop cutting machine (Silhouette Cameo 3) on 50 um-thick sheets of copy paper and 12 um-thick aluminum foil, and we manually glue the Al foils to the paper. The samples were connected to the electronics read-out through copper wires attached via copper tape. The capacitance was measured with three independent systems an LCR meter (BK891, B&K Precision) to measure the capacitance frequency dependence, a lock-in amplifier to measure the static permittivity (MFIA 5 MHz, Zurich Instruments) (see Section B), and a custom-made capacitance-meter system to measure the temperature – capacitance dependence (see Appendix B). The temperature cycling was generated via a peltier element controlled by a specifically designed control PID circuit and measured via a platinum sensor, previously calibrated on a thermal camera (FLIR A655sc).

**APPENDIX B**

**CAPACITANCE CHARACTERIZATION**

To measure the electrical properties of the fabricated capacitors we measured the capacitance as a function of frequency. We swept the frequency from 20Hz to 10kHz, measuring 1000 different frequencies with the LCR Meter. For each frequency we acquired 50 points and calculated the average of these points. The static permittivity was calculated from the conductivity extracted though an impedance spectrum measured with the lock in amplifier. The real and imaginary part for the conductivity was measured between 100 mHz and 1 MHz at 1V. Then the real and imaginary part of the permittivity was respectively calculated by:

\[
\varepsilon' = \frac{1}{2\pi f \varepsilon_0 \sigma'} \quad (6)
\]

\[
\varepsilon'' = \frac{1}{2\pi f \varepsilon_0 \sigma} \quad (7)
\]

where \( f \) is the operational frequency, \( \varepsilon' \) is the real part of the permittivity, \( \varepsilon'' \) is the imaginary part of the permittivity, \( \varepsilon_0 \) is the vacuum permittivity and \( \sigma \) is the conductivity of the medium. The static permittivity corresponds to the low frequency plateau of the real permittivity.

**APPENDIX C**

**READOUT SYSTEM**

The custom-made electronics to measure the capacitance of the sensor is based on the measurement of the phase lag in a RC circuit. Generally speaking, a first order low pass RC filter shows a drop in the response of −20dB/dec after the cut-off frequency and a phase lag that reaches −45° at the cut-off, while it is 0° one decade before and −90° one decade after. At a constant frequency and resistance, a change in the capacitance will result in a change in the phase lag between the input and the output signals, according to the relation:

\[
\Delta \phi = \arctan \left( \frac{2\pi f R C}{1} \right) \quad (8)
\]

where \( f \) is the operational frequency, \( R \) is the resistance and \( \Delta \phi \) is the phase lag. By measuring the phase lag, the capacitance can be computed by:

\[
C = \frac{1}{2\pi f} \tan(\Delta \phi) \quad (9)
\]

In practice, the phase lag is measured by the time delay between the input sine and the resulting output. The time delay \( \Delta t \) can be converted to a phase lag according to the equation:

\[
\Delta \phi = 360^\circ f \Delta t \quad (10)
\]

The capacitance can be calculated from the measured time delay as:

\[
C = \frac{1}{2\pi f} \tan(360^\circ f \Delta t) \quad (11)
\]

The general structure of the circuit is presented in Fig. 6. The oscillator generates the input sine, the readout section converts the time delay between a reference resistor and the capacitor under test (CUT) into a square wave and the digital counter measures the ON period of the pulse generated by the readout section. The circuit was simulated using LTSpice and then implemented on a PCB manufactured by Eurocircuits. The oscillator to generate the input sine wave was implemented by a buffered quadrature oscillator, where each section provides a shift of −60° so that the three sections combined achieve the −180° necessary for the oscillation. A gain of 8.33 was necessary to sustain the oscillations. The targeted frequency was
Fig. 6. Capacitive measurement circuit designed to precisely measure temperature-capacitance relation. (a) Logic Diagram. (b) Oscillator. (c) Phase Detector. (d) Phase Counter.

20Hz, however, due to the mismatch between the components the circuit oscillates at 44Hz with an amplitude of 500mVpp. At the output of the oscillator a digital potentiometer, directly set by the microcontroller, was added to control the amplitude.
of the sine (Fig. 6). To avoid the use of a dual supply, which would have required extra components on the board powered via the USB single supply, the circuit was biased at 2.5V through a Zener diode, which was used as voltage reference for the analog part of the circuit. The generated sine wave is sent to the RC section of the circuit, where it is converted to a square wave by comparator U2. The delayed voltage across the capacitor is also converted to a square wave through comparator U3. The two resulting square waves are X-ored to generate a pulse that corresponds to the time delay between the two signals (Fig. 6). U2 and U3 are fast comparators, whose propagation delay (4.5ns) will only add an error of 0.02 fF. The pulse coming from the read-out section is used to gate a 12 MHz clock fed to a 64 bits counter. The count is then transferred to the microcontroller via a parallel to serial converter. The time delay is then calculated via the counter count as:

$$\Delta t = \frac{n_{\text{count}}}{12 \text{MHz}} \quad (12)$$

This approach provides a theoretical resolution of 3 × 10^{-16} F and a dynamic range of 125dB. To validate the circuit, we used different calibration ceramic capacitors (100, 300, 500, 1000 pF, 10%, 50V) that we previously calibrated with an impedance analyzer (MFIA Zurich Instruments, accuracy 0.05%) using the same frequency and output amplitude. The parasitic capacitance was measured by measuring the capacitance without any load (~150 pF) and then subtracted to the measured values. The results are summarized in the table below:

| Nominal Value (pF) | MFIA (pF) | Capacitance Meter (pF) |
|-------------------|-----------|------------------------|
| 100               | 105       | 103                    |
| 300               | 308       | 309                    |
| 500               | 481       | 493                    |
| 1000              | 977       | 974                    |

The calibration shows that the capacitances measured by the circuit are within the tolerance of the nominal values of the measured capacitors and good accordance with the capacitance measured with the impedance analyzer.

ACKNOWLEDGMENT

The authors would like to thank Luca Bonanomi for fruitful discussions during the initial stages of the project.

REFERENCES

[1] A. Feteira, “Negative temperature coefficient resistance (NTCR) ceramic thermistors: An industrial perspective,” J. Amer. Ceram. Soc., vol. 92, no. 5, pp. 967–983, 2009.
[2] J. Becker, C. Green, and G. Pearson, “Properties and uses of thermistors—Thermally sensitive resistors,” Elect. Eng., vol. 65, no. 11, pp. 711–725, Nov. 1946.
[3] B. Oertel, T. Hübner, D. Heinze, and U. Banach, “Capacitive sensor system for measurement of temperature and humidity,” Fresenius’ J. Anal. Chem., vol. 349, no. 5, pp. 391–393, 1994.
[4] Y.-H. Han, K.-T. Kim, H.-J. Shin, S. Moon, and I.-H. Choi, “Enhanced characteristics of an uncoiled microbolometer using vanadium-tungsten oxide as a thermometric material,” Appl. Phys. Lett., vol. 86, no. 25, 2005, Art. no. 254101.
[5] Y. Lv, M. Hu, M. Wu, and Z. Liu, “Preparation of vanadium oxide thin films with high temperature coefficient of resistance by facing targets D.C. reactive sputtering and annealing process,” Surf. Coatings Technol., vol. 201, nos. 9–11, pp. 4969–4972, Feb. 2007.
[6] R. T. R. Kumar et al., “Room temperature deposited vanadium oxide thin films for uncooled infrared detectors,” Mater. Res. Bull., vol. 38, no. 7, pp. 1235–1240, Jun. 2003. [Online]. Available: http://www.sciencedirect.com/science/article/pii/S0025541603001181
[7] A. Syllaïos, T. Schimert, R. Goog, W. McCardel, B. Ritchey, and J. Tregilgas, “Amorphous silicon microbolometer technology,” MRS Online Proc. Library, vol. 609, no. 1, pp. 1441–1446, 1999.
[8] T. Unold and J. David Cohen, “Electronic mobility gap structure and the nature of deep defects in amorphous silicon-germanium alloys grown by photo-CVD,” J. Non-Crystalline Solids, vols. 164–166, pp. 23–26, Dec. 1993.
[9] M. García, R. Ambrosio, A. Torres, and A. Kosarev, “IR bolometers based on amorphous silicon germanium alloys,” J. Non-Cryst. Solids, vols. 338–340, pp. 744–748, Jun. 2004.
[10] H.-Y. Ma, Q.-A. Huang, M. Qin, and T. Lu, “A micromachined silicon capacitive temperature sensor for radiosonde applications,” in Proc. IEEE Sensors, Oct. 2009, pp. 1693–1696.
[11] H.-Y. Ma, Q.-A. Huang, M. Qin, and T. Lu, “A micromachined silicon capacitive temperature sensor for wide temperature range applications,” J. Micromech. Microeng., vol. 20, no. 5, May 2010, Art. no. 055036.
[12] D. Peroulis, A. S. Kovacs, D. J. Koester, F. Sadeghi, S. M. Scott, and D. E. Adams, “Highly reliable micro-electromechanical system temperature sensor,” U.S. Patent 9039280, May 26, 2015.
[13] O. Sigmund and S. Torquato, “Composites with extremal thermal expansion coefficients,” Appl. Phys. Lett., vol. 69, no. 21, pp. 3203–3205, Nov. 1996.
[14] R. Lakes, “Cellular solids with tunable positive or negative thermal expansion of unbounded magnitude,” Appl. Phys. Lett., vol. 90, no. 22, May 2007, Art. no. 221905.
[15] G. Jefferson, T. A. Parthasarathy, and R. J. Kerans, “Tailorable thermal expansion hybrid structures,” Int. J. Solids Struct., vol. 46, nos. 11–12, pp. 2372–2387, Jun. 2009.
[16] K. Wei, H. Chen, Y. Pei, and D. Fang, “Planar lattices with tailorable coefficient of thermal expansion and high stiffness based on dual-material triangle unit,” J. Mech. Phys. Solids, vol. 86, pp. 173–191, Jan. 2016.
[17] K. Wei, Y. Peng, Z. Qu, Y. Pei, and D. Fang, “A cellular metastructure incorporating coupled negative thermal expansion and negative Poisson’s ratio,” Int. J. Solids Struct., vol. 150, pp. 255–267, Oct. 2018.
[18] Y. Li, Y. Chen, T. Li, S. Cao, and L. Wang, “Hoberman-sphere-inspired lattice metamaterials with tunable negative thermal expansion,” Compos. Struct., vol. 189, pp. 586–597, Apr. 2018.
[19] E. Gdoutos, A. A. Shapiro, and C. Daraio, “Thin and thermally stable periodic metastructures,” Experim. Mech., vol. 53, no. 9, pp. 1735–1742, Nov. 2013.
[20] N. Yamamoto, E. Gdoutos, R. Toda, V. White, H. Manohara, and C. Daraio, “Thin films with ultra-low thermal expansion,” Adv. Mater., vol. 26, no. 19, pp. 3076–3080, May 2014.
[21] Q. Wang, J. A. Jackson, Q. Ge, J. B. Hopkins, C. M. Spadaccini, and N. X. Fang, “Lightweight mechanical metamaterials with tunable negative thermal expansion,” Phys. Rev. Lett., vol. 117, no. 17, Oct. 2016, Art. no. 175901.
[22] E. Boatti, N. Vasios, and K. Bertoldi, “Origami metamaterials for tunable thermal expansion,” Adv. Mater., vol. 29, no. 26, Jul. 2017, Art. no. 1700360.
[23] Y. Tang, G. Lin, S. Yang, Y. K. Yi, R. D. Kamien, and J. Yin, “Programmable Kiri-Kirigami metamaterials,” Adv. Mater., vol. 29, no. 10, 2017, Art. no. 1604262.
[24] H. Xu, A. Farag, and D. Pasini, “Routes to program thermal expansion in three-dimensional lattice metamaterials built from tetrahedral building blocks,” J. Mech. Phys. Solids, vol. 117, pp. 54–87, Aug. 2018.
[25] L. Liu, C. Qiao, H. An, and D. Pasini, “Encoding Kirigami Bi-materials to morph on target in response to temperature,” Sci. Rep., vol. 9, no. 1, pp. 1–14, Dec. 2019.
[26] S. Taniker, P. Celli, D. Pasini, D. C. Hofmann, and C. Daraio, “Temperature-induced shape morphing of Bi-metallic structures,” Int. J. Solids Struct., vol. 190, pp. 22–32, May 2020.
[27] T. Idoigaki, T. Tominaga, K. Senda, N. Ohyta, and T. Hattori, “Bending and expanding motion actuators,” Sens. Actuators A, Phys., vol. 54, nos. 1–3, pp. 560–564, Mar. 1996.
[28] S. Iqbal and A. Malik, “A review on MEMS based micro-displacement amplification mechanisms,” Sens. Actuators A, Phys., vol. 300, Dec. 2019, Art. no. 111666.
[29] M. Ashby, *Materials Selection in Mechanical Design*, 5th ed. New York, NY, USA: Butterworth-Heinemann, 2016.

[30] S. Simula, S. Iikäinen, K. Niskanen, T. Varpula, H. Seppä, and A. Paukku, “Measurement of the dielectric properties of paper,” *J. Imag. Sci. Technol.*, vol. 43, no. 5, pp. 472–477, 1999.

[31] A. Guedes, S. Sheleton, R. Przybyla, I. Izyumin, B. Boser, and D. A. Horsley, “Aluminum nitride pMUT based on a flexurally-suspended membrane,” in *Proc. 16th Int. Solid-State Sensors, Actuat. Microsyst. Conf.* Jun. 2011, pp. 2062–2065.

[32] A. Rogalski, “History of infrared detectors,” *Opto-Electron. Rev.*, vol. 20, no. 3, pp. 279–308, Sep. 2012.

[33] B. Wang, J. Lai, H. Li, and S. Chen, “Nanostructured vanadium oxide thin film with high TCR at room temperature for microbolometer,” *Infr. Phys. Technol.*, vol. 57, pp. 8–13, Mar. 2013.

[34] M. F. Zia, M. Abdel-Rahman, M. Aldaraibi, B. Ilahi, and A. Alasaad, “Synthesis and electrical characterisation of vanadium oxide thin film thermometer for microbolometer applications,” *Electron. Lett.*, vol. 52, no. 10, pp. 827–828, 2016.

**Semih Taniker** received the B.S., M.S., and Ph.D. degrees in mechanical engineering from Bosphorus University, Turkey, in 2008, 2011, and 2015, respectively. From 2018 to 2020, he was a Postdoctoral Scholar at the Daraio Group. His research interests include design of novel mechanisms for aerospace applications, vibration isolation, and sensing.

**Vincenzo Costanza** received the B.S. degree in electrical engineering from the Universita di Palermo, Italy, in 2013, the first M.S. degree in micro and nanosystems from ETH Zürich, Switzerland, in 2016, and the second M.S. degree in mechanical engineering from the California Institute of Technology (Caltech), in 2018, where he is currently pursuing the Ph.D. degree in mechanical engineering. His research combines novel materials with sensing principles to develop wearable sensors for medical devices.

**Chiara Daraio** received the bachelor’s degree in mechanical engineering from the Universita’ Politecnica delle Marche, Italy, in 2001, and the M.S. and Ph.D. degrees in materials science and engineering from the University of California at San Diego, San Diego, CA, USA, in 2003 and 2006, respectively. She joined the Department of Aeronautics and the Department of Applied Physics, California Institute of Technology (Caltech), in Fall 2006, and was promoted to a Full Professor in 2010. From January 2013 to August 2016, she returned to Caltech as a Professor of Mechanical Engineering and Applied Physics. She is the G. Bradford Jones Professor of Mechanical Engineering and Applied Physics at Caltech. Her work is focused on developing new materials with advanced mechanical and sensing properties, for application in robotics, medical devices, and vibration absorption. She is a member of the ASME, APS, MRS, and SPIE societies. Prof. Daraio’s awards and honors include the Presidential Early Career Award from President Obama (PECASE), the Sloan Research Fellowship, the ONR Young Investigator Award, and the NSF CAREER Award. She also received the Richard Von Mises Prize and the Hetenyi Award from the Society for Experimental Mechanics. She serves as a Board Editor for *Science* (AAAS).

**Paolo Celli** received the B.S. degree in mechanical engineering from the Universita’ Politecnica delle Marche, Italy, in 2010, the M.S. degree in mechanical engineering from the Politecnico di Torino, Italy, in 2012, and the Ph.D. degree in civil engineering from the University of Minnesota in 2017. From 2017 to 2019, he was with the Daraio Group, Caltech, as a Postdoctoral Scholar. In 2012, he was a Visiting Research Scholar at the University of Minnesota. He is currently an Assistant Professor of Civil Engineering at Stony Brook University (State University of New York at Stony Brook). His research and teaching interests revolve around structural mechanics and structural dynamics, with particular emphasis on compliant and morphing structures.