Interference Exploitation Precoding Made Practical: Closed-Form Solutions with Optimal Performance
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Abstract—In this paper, we propose closed-form precoding schemes with optimal performance for constructive interference (CI) exploitation in the multiuser multiple-input single-output (MU-MISO) downlink. We first consider an optimization where we maximize the distance between the constructive region and the detection thresholds. The cases of both strict and non-strict phase rotation are considered and can further be formulated as convex optimization problems. For optimization with strict phase rotation, we mathematically derive the optimal beamforming structure with Lagrangian and Karush-Kuhn-Tucker (KKT) conditions. By formulating its dual problem, the optimization problem is further shown to be equivalent to a quadratic programming (QP) over a simplex, which can be solved more efficiently. We then extend our analysis to the case of non-strict phase rotation, where it is mathematically shown that a K-dimensional optimization for non-strict phase rotation is equivalent to a 2K-dimensional optimization for strict phase rotation in terms of the problem formulation. The connection with the conventional zero-forcing (ZF) precoding is also discussed. Based on the above analysis, we further propose an iterative closed-form scheme to obtain the optimal beamforming matrix, where within each iteration a closed-form solution can be obtained. Numerical results validate our analysis and the optimality of the proposed iterative scheme, and further show that the proposed closed-form scheme is more efficient than the conventional QP algorithms with interior-point methods, which motivates the use of CI beamforming in practical wireless systems.

Index Terms—MIMO, transmit beamforming, constructive interference, optimization, Lagrangian, closed-form solutions.

I. INTRODUCTION

MULTIPLE-input multiple-output (MIMO) systems have been widely acknowledged as a promising technology in the field of wireless communications, due to the significant gains over single-antenna systems [1]. When the channel knowledge is known at the base station (BS), the capacity-achieving dirty-paper coding (DPC) scheme is proposed in [2] by pre-subtracting the interference prior to transmission. However, DPC is difficult to implement in practical systems due to the impractical assumption of infinite length of codewords and its high computational cost. To achieve a compromise between performance and complexity, its non-linear counterparts in the form of Tomlinson-Harashima precoding (THP) [3] and vector perturbation (VP) [4] have been proposed, which however are still too complicated for practice due to the inclusion of the sophisticated sphere-search algorithms. Therefore, low-complexity linear precoding schemes based on zero-forcing (ZF) have received increasing research attention [5], and a regularized ZF (RZF) scheme is proposed in [6] to further improve the performance of ZF. On the other hand, transmit beamforming schemes based on optimization have also been a popular research topic [7]–[13]. Among the optimization-based schemes, one form of the optimization known as signal-to-interference-plus-noise ratio (SINR) balancing is to maximize the minimum SINR subject to a total power constraint [7], [8] or a per-antenna power constraint [9]. An alternative downlink beamforming targets at minimizing the total transmit power at the BS subject to a minimum SINR requirement [10], [11]. It has been shown that the power minimization problems can be formulated either as a virtual uplink problem with power control or as a semi-definite programming (SDP) and solved via semi-definite relaxation (SDR) [11]. As for the SINR balancing problem, it is proven to be an inverse problem to the power minimization optimization, based on which schemes via bisection search [7] and iterative algorithms [10] have been proposed.

Nevertheless, both the above precoding schemes and the optimization-based transmit beamforming designs mentioned above have ignored the fact that interference can be beneficial and further exploited on an instantaneous basis [14], [15]. The concept of constructive interference (CI) was firstly introduced in [16], where it is shown that the instantaneous interference can be categorized into constructive and destructive. A modified ZF precoding scheme is then proposed in [17], where the constructive interference is exploited while the destructive interference is cancelled. A correlation rotation scheme has been further proposed in [18], where it is shown that the destructive interference can be manipulated and rotated such that all the interference becomes constructive. Symbol-level transmit beamforming schemes based on convex optimization for CI has been proposed in [19], [20], where the concept of constructive interference is introduced to relax the strict phase rotation constraint in [18] and achieve an improved performance. Further studies on the optimization-based CI beamforming schemes can be found in [20]–[23]. Due to the performance benefits over conventional schemes, the concept of CI has been extended to many wireless application scenarios, including cognitive radio [24], [25], constant envelope precoding [26], wireless information and power transfer [27] and mutual coupling exploitation [28].

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a convex optimization problem, which can be computationally inefficient, especially when executed on a symbol-by-symbol basis.

In this paper, we design low-complexity optimal and suboptimal solutions for CI precoding, culminating in closed-form iterative precoders. We consider an optimization problem where we maximize the distance between the constructive region and the detection thresholds such that the effect of CI is maximized. We firstly consider the optimization for strict phase rotation, where the phases of the interfering signals are rotated such that they are strictly aligned to the symbol of interest. By analyzing the formulated second-order cone programming (SOCP) optimization with Lagrangian and KKT conditions, we derive the structure of the optimal beamforming matrix, which leads to an equivalent optimization and further simplifies the beamforming design. By formulating the dual problem of the equivalent optimization problem, it is mathematically shown that the optimization for CI beamforming is equivalent to a quadratic programming (QP) optimization over a simplex, which finally leads to a closed-form expression. We extend our analysis to the case of non-strict phase rotation, where the phases of the interfering signals are rotated such that the resulting interfered signal is located within the constructive region. By following a similar approach for the case of strict phase rotation, we analytically show that the optimal beamforming matrix for these two scenarios shares a similar closed-form expression, and a \( K \)-dimensional optimization for non-strict phase rotation is equivalent to a \( 2K \)-dimensional optimization for strict phase rotation in terms of the problem formulation. Our above analysis also provides some insights on the connection between the CI beamforming and the generic ZF precoding.

Moreover, our efforts to facilitate the symbol-level CI beamforming in practice culminate in an iterative closed-form scheme to efficiently obtain the optimal beamforming matrix, where a closed-form solution is obtained within each iteration. We show that only in a few iterations, the closed-form approach obtains optimal performance. Numerical results validate our above analysis and the optimality of the proposed iterative closed-form method for both strict and non-strict phase rotation. Moreover, it is numerically shown that the proposed iterative approach is more time-efficient compared to the conventional QP algorithms based on interior-point methods, especially when the number of users is small. By constraining the maximum number of iterations, we further obtain a flexible performance-complexity tradeoff for the proposed iterative method, based on its connection with conventional ZF precoding. Both of the above motivate the use of CI-based beamforming in practical wireless systems.

For reasons of clarity, we summarize the contributions of this paper as:

1) We formulate the optimization problem for CI-based beamforming, where we maximize the distance between the constructive region and the detection thresholds. We derive the optimal beamforming matrix for strict phase rotation and further formulate an equivalent and simplified optimization problem.

2) The optimization for strict phase rotation is transformed and further shown to be equivalent to a QP problem over a simplex, which can be more efficiently solved than the originally formulated problem.

3) We extend our analysis to the case of non-strict phase rotation, where the closed-form expression is similar to the case of strict phase rotation. It is further shown that a \( K \)-dimensional optimization for non-strict phase rotation is equivalent to a \( 2K \)-dimensional optimization for strict phase rotation in terms of the problem formulation.

4) We analytically study the connection between the CI beamforming and the ZF precoding, where it is shown that ZF precoding can be regarded as a special case of CI-based beamforming with all the dual variables being zero.

5) We further propose an iterative closed-form scheme to obtain the optimal beamforming matrix for both the strict and non-strict phase rotation cases, where within each iteration a closed-form solution can be derived. We show that the closed-form precoder obtains an optimal performance in only a few iterations.

The remainder of this paper is organized as follows. Section II introduces the system model and briefly reviews CI. Section III includes the analysis for the optimization problems with both strict and non-strict phase rotation constraints. The connection between the CI beamforming and conventional ZF precoding is discussed in Section IV. The proposed iterative closed-form scheme is introduced in Section V. The numerical results are shown in Section VI, and Section VII concludes the paper.

Notations: \( a \), \( A \), and \( \mathbf{A} \) denote scalar, vector and matrix, respectively. \( (\cdot)^T \), \( (\cdot)^H \) and \( tr \{ \cdot \} \) denote transposition, conjugate transposition and trace of a matrix, respectively. \( j \) denotes the imaginary unit, and \( vec(\cdot) \) denotes the vectorization operation. \( \mathbf{A}(k, i) \) denotes the entry in the \( k \)-row and \( i \)-th column of \( \mathbf{A} \). \( || \cdot || \) denotes the absolute value of a real number or the modulus of a complex number, and \( \| \cdot \|_F \) denotes the Frobenius norm. \( C^{n \times n} \) represents an \( n \times n \) matrix in the complex set, and \( \mathbf{I} \) denotes the identity matrix. \( \Re(\cdot) \) and \( \Im(\cdot) \) denote the real and imaginary part of a complex number, respectively. \( \text{card}(\cdot) \) denotes the cardinality of a set.

II. SYSTEM MODEL AND CONSTRUCTIVE INTERFERENCE

In this section, the system model that we consider is firstly introduced, followed by a brief review of CI and the constructive region.

A. System Model

We consider a multiuser MISO system in the downlink, where the BS structure with a symbol-level precoding is depicted in Fig. 1, where the iterative closed-form algorithm will be introduced in Section V. The BS with \( N_t \) transmit antennas is simultaneously communicating with \( K \) single-antenna users in the same time-frequency resource, where \( K \leq N_t \). We focus on the transmit beamforming designs and perfect CSI is assumed throughout the paper. The data symbol vector is assumed to be from a normalized PSK modulation.
Fig. 1: A block diagram for the proposed symbol level precoding based on constructive interference.

constellation \( C_K \), denoted as \( s \in C^K \times 1 \). Then, the received signal at the \( k \)-th user can be expressed as

\[
r_k = h_k W s + n_k,
\]

where \( h_k \in C^{1 \times N_t} \) denotes the flat-fading Rayleigh channel vector from user \( k \) to the BS, and each entry in \( h_k \) follows a standard complex Gaussian distribution. \( W \in C^{N_t \times K} \) is the beamforming matrix and \( n_k \) is the additive Gaussian noise with zero mean and variance \( \sigma^2 \) at the receiver.

**B. Constructive Interference**

CI is defined as the interference that pushes the received signals away from the detection thresholds [14]–[18]. CI for strict phase rotation refers to the cases where the phases of the interfering signals are controlled and rotated, such that they are strictly aligned to those of the data symbols of interest [18]. The constructive region has been further introduced in [19], where it is shown that the phases of the interfering signals may not be necessarily strictly aligned to that of the data symbols of interest, known as the non-strict phase rotation. It is demonstrated that, as long as the resulting interfered signals are located in the constructive region, this increases the distance to the detection thresholds and returns an improved performance. To show this intuitively, in Fig. 2 and Fig. 3 we depict the case for strict phase rotation and non-strict phase rotation respectively, where the constellation point \( \left( \frac{1}{\sqrt{2}} + \frac{1}{\sqrt{2}} \cdot j \right) \) from a normalized QPSK constellation is employed as the example to illustrate these two cases. We can observe that for both strict phase rotation and non-strict phase rotation, the distance of the received signals to the detection thresholds is increased, which will improve the

Fig. 2: Constructive interference, QPSK, strict phase rotation.
Fig. 3: Constructive region, QPSK, non-strict phase rotation
detection performance.

III. CONSTRUCTIVE INTERFERENCE BEAMFORMING

In this section, we firstly focus on the CI beamforming for
strict phase rotation, and we further extend our analysis to the
case of non-strict phase rotation.

A. Strict Phase Rotation

Before formulating the optimization problem, based on the
geometry of the modulation constellation we firstly construct
the conditions that the beamformer should satisfy to achieve
the strict phase rotation. In Fig. 2, without loss of generality
we denote \( \overrightarrow{OA} = t \cdot s_k \) and \( t = |\overrightarrow{OA}| \) is the
object to be maximized. We further assume that the node ‘B’
denotes the noiseless received signal for user \( k \) that is co-linear to \( \overrightarrow{OA} \) for
strict phase rotation, which leads to
\[
\overrightarrow{OB} = h_k W s.
\]

Then, by introducing a real-valued scaling factor \( \lambda_k \),
we further express \( \overrightarrow{OB} \) as
\[
\overrightarrow{OB} = h_k W s = \lambda_k s_k,
\]
where based on the geometry we can obtain that \( \lambda_k \) is a real
number, and the condition on \( \lambda_k \) to achieve CI for strict phase
rotation is given by
\[
\lambda_k \geq t, \quad \forall k \in K,
\]
where \( K = \{1, 2, \cdots, K\} \). With the above formulation, we
can construct the optimization problem for strict phase rotation as
\[
P_1 : \max_{w, t} t
\]
s.t. \( h_k W s = \lambda_k s_k, \quad \forall k \in K \)
\( \lambda_k \geq t, \quad \forall k \in K \)
\( \| W s \|^2_F \leq p_0 \)
where \( p_0 \) denotes the total available transmit power. A symbol-
level power constraint is employed, as the exploitation of CI is
related to the transmit symbol vector, which will also be shown
mathematically in the following. \( P_1 \) belongs to the SOCP and
can be solved with convex optimization tools such as CVX [19]. We decompose the beamforming matrix into vectors
\[
W = [w_1, w_2, \cdots, w_K],
\]
and based on the virtual multicast formulation in [19] we
obtain that each \( w_i s_i \) is identical. This leads to the equivalent
transformation of the power constraint, given by
\[
\| W s \|^2_F \leq p_0 \Rightarrow \sum_{i=1}^{K} s_i^H W_i^H W_i s_i \leq \frac{p_0}{K}.
\]

We further transform \( P_1 \) in (5) into a standard minimization
problem, expressed as
\[
P_2 : \min_{w_i, t} \quad -t
\]
s.t. \( h_k \sum_{i=1}^{K} w_i s_i - \lambda_k s_k = 0, \quad \forall k \in K \)
\( t - \lambda_k \leq 0, \quad \forall k \in K \)
\( \sum_{i=1}^{K} s_i^H W_i^H W_i s_i - \frac{p_0}{K} \leq 0 \)
In the following we analyze \( P_2 \) with Lagrangian and KKT
conditions. The Lagrangian of \( P_2 \) is expressed as [29]
\[
\mathcal{L}(w_i, t, \delta_k, \mu_k, \mu_0) = -t + \sum_{k=1}^{K} \delta_k \left( h_k \sum_{i=1}^{K} w_i s_i - \lambda_k s_k \right) + \sum_{k=1}^{K} \mu_k \left( t - \lambda_k \right) + \mu_0 \left( \sum_{i=1}^{K} s_i^H W_i^H W_i s_i - \frac{p_0}{K} \right),
\]
where \( \delta_k, \mu_k \) and \( \mu_0 \) are the dual variables, and we have \( \mu_0 \geq 0 \) and \( \mu_k \geq 0, \quad \forall k \in K \). Based on the Lagrangian in [9], the
KKT conditions for optimality can be obtained as
\[
\frac{\partial \mathcal{L}}{\partial \delta_k} = 0, \quad \forall k \in K
\]
\[
\frac{\partial \mathcal{L}}{\partial w_i} = \left( \sum_{k=1}^{K} \delta_k \cdot h_k \right) s_i + \mu_0 \cdot w_i^H = 0, \quad \forall i \in K
\]
\[
\delta_k \left( h_k \sum_{i=1}^{K} w_i s_i - \lambda_k s_k \right) = 0, \quad \forall k \in K
\]
\[
\mu_k \left( t - \lambda_k \right) = 0, \quad \forall k \in K
\]
\[
\mu_0 \left( \sum_{i=1}^{K} s_i^H W_i^H W_i s_i - \frac{p_0}{K} \right) = 0
\]
Based on (10b), it is firstly obtained that \( \mu_0 \neq 0 \), and with the
fact that \( \mu_0 \geq 0 \) we can further obtain \( \mu_0 > 0 \). Then, \( w_i^H \) in
(10b) can be expressed as
\[
w_i^H = -\frac{1}{\mu_0} \left( \sum_{k=1}^{K} \delta_k \cdot h_k \right) s_i, \quad \forall i \in K.
\]
By denoting
\[ v_k = -\frac{\delta_k^H}{\mu_0}, \forall k \in \mathcal{K}, \]  
(12)
where we note that \( \delta_k \) can be complex, the expression of \( w_i \) is obtained as
\[ w_i = \left( \sum_{k=1}^{K} v_k \cdot h_k^H \right) s_i^H, \forall k \in \mathcal{K}. \]
(13)
Based on (13), we further obtain that
\[ w_i s_i = \left( \sum_{k=1}^{K} v_k \cdot h_k^H \right) s_i^H, \forall i \in \mathcal{K}, \]
(14)
which is a constant for any \( i \). This mathematically verifies that the beamforming vector for one symbol is a phase-rotated version of the beamforming vector for another symbol. Then, with each \( w_i \) obtained, the beamforming matrix \( W \) can be obtained and further expressed in a matrix form as
\[ W = [w_1, w_2, \ldots, w_K] \]
\[ = \left( \sum_{k=1}^{K} v_k \cdot h_k^H \right) \cdot [s_1^H, s_2^H, \ldots, s_K^H] \]
\[ = [h_1^H, h_2^H, \ldots, h_K^H] [v_1, v_2, \ldots, v_K]^T \cdot [s_1^H, s_2^H, \ldots, s_K^H] \]
\[ = H^H \Psi s^H. \]
(15)
We further express (3) in a compact form as
\[ HWs = diag (\Lambda) s, \]
(16)
where \( H = [h_1^T, h_2^T, \ldots, h_K^T]^T \) is the channel matrix and \( \Lambda = [\lambda_1, \lambda_2, \ldots, \lambda_K]^T \). By substituting (15) into (16), we can further obtain
\[ HH^H \Psi s^H s = diag (\Lambda) s \]
\[ \Rightarrow \Psi = \frac{1}{K} (HH^H)^{-1} diag (\Lambda) s. \]
(17)
With (17), we can obtain the structure of the optimal beamforming matrix as a function of scaling vector \( \Lambda \) as
\[ W = \frac{1}{K} \cdot H^H (HH^H)^{-1} diag (\Lambda) ss^H. \]
(18)
It is easy to observe from (18) that the CI beamforming is a symbol-level beamforming scheme since the beamforming matrix includes the expression of the symbol vector \( s \). Moreover, with (18) the original optimization problem on \( W \) is transformed into an optimization on the real-valued scaling vector \( \Lambda \). With the fact that \( \mu_0 > 0 \), based on (10c) we can obtain that the power constraint is strictly active, which leads to
\[ \| Ws \|^2_F = p_0 \]
\[ \Rightarrow tr \{WW^H s^H W \} = p_0 \]
\[ \Rightarrow s^H W^H WS = p_0 \]
\[ \Rightarrow \frac{1}{K^2} \cdot s^H s^H diag (\Lambda) (HH^H)^{-1} diag (\Lambda) s = p_0 \]
\[ \Rightarrow s^H diag (\Lambda) (HH^H)^{-1} diag (\Lambda) s = p_0 \]
\[ \Rightarrow H^T diag (s^H) (HH^H)^{-1} diag (s) \Lambda = p_0 \]
\[ \Rightarrow \Lambda^T TA = p_0, \]
(19)
where we note that \( \lambda_k^H = \lambda_k \) as each \( \lambda_k \) is real, and \( T \) is defined as
\[ T = diag (s^H) (HH^H)^{-1} diag (s). \]
(20)
It is easy to obtain that \( T \) is Hermitian and positive semi-definite, which further leads to
\[ \Lambda^T TA = \Lambda^T \Re (T) \Lambda = \Lambda^T VA = p_0, \]
(21)
where \( V = \Re (T) \) is a symmetric and positive semi-definite matrix. With (21) obtained, we can formulate a new convex optimization problem on \( \Lambda \) that is equivalent to the original optimization \( P_1 \), expressed as
\[ P_3: \min_{\Lambda, t} -t \]
\[ s.t. \quad \Lambda^T VA - p_0 = 0 \]
\[ t - \lambda_k \leq 0, \forall k \in \mathcal{K} \]
(22)
The optimal beamforming matrix for the original problem \( P_1 \) in (5) can be obtained with (18) based on the obtained \( \Lambda \) by solving \( P_3 \). In the following, we analyze the convex optimization \( P_3 \) with the Lagrangian approach, where the Lagrangian of \( P_3 \) is formulated as
\[ L (\Lambda, t, \alpha_0, \mu_k) = -t + \alpha_0 (\Lambda^T VA - p_0) + \sum_{k=1}^{K} \mu_k (t - \lambda_k) \]
\[ = (1^T u - 1) t + \alpha_0 \Lambda^T VA - u^T \Lambda - \alpha_0 p_0, \]
(23)
where \( \alpha_0 \) and \( \mu_k \) are the dual variables and \( \mu_k \geq 0, \forall k \in \mathcal{K} \). \( u = [\mu_1, \mu_2, \ldots, \mu_K]^T \) is a dual vector that consists of the dual variables and the vector \( 1 = [1, 1, \ldots, 1]^T \). Based on (23), the KKT conditions of \( P_3 \) for optimality are expressed as
\[ \frac{\partial L}{\partial \Lambda} = 0 \]
\[ \frac{\partial L}{\partial \alpha_0} = 0 \]
\[ \frac{\partial L}{\partial \mu_k} = 0, \forall k \in \mathcal{K} \]
(24)
Based on (24b), firstly we have \( \alpha_0 \neq 0 \), and we can further obtain the expression of \( \Lambda \), given by
\[ \Lambda = \frac{1}{2\alpha_0} V^{-1} u, \]
(25)
where we note that \( V \) is symmetric. With \( \alpha_0 \neq 0 \), based on (24a) it is obtained that the power constraint is strictly active, and by substituting (25) into (24c), we can express \( \alpha_0 \) as a function of the dual vector \( u \), given by
\[ \left( \frac{1}{2\alpha_0} V^{-1} u \right)^T V \left( \frac{1}{2\alpha_0} V^{-1} u \right) = p_0 \]
\[ \Rightarrow \frac{1}{4\alpha_0^2} u^T V^{-1} V V^{-1} u = p_0 \]
\[ \Rightarrow \alpha_0 = \sqrt{\frac{u^T V^{-1} u}{4p_0}}. \]
(26)
For the convex optimization \( P_3 \) in (22), it is easy to verify that the Slater’s condition is satisfied [29], which means that
the dual gap is zero. Therefore, we can solve $\mathcal{P}_3$ by solving its corresponding dual problem, which is given by

$$\mathcal{U} = \max_{u, \alpha} \min_{\Lambda, t} \mathcal{L}(\Lambda, t, \alpha, u).$$  (27)

For the dual problem $\mathcal{U}$, the inner minimization is achieved with (24a) and the obtained $\Lambda$ in (25), and therefore the dual problem can be further transformed into

$$\mathcal{U} = \max_{u, \alpha} \alpha \left( \frac{1}{2\alpha} V^{-1} u \right)^T V \left( \frac{1}{2\alpha} V^{-1} u \right) - u^T \left( \frac{1}{2\alpha} V^{-1} u \right) - \alpha_0 p_0$$

$$= \max_{u, \alpha} \frac{1}{4\alpha} u^T V^{-1} V^{-1} u - \frac{1}{2\alpha} u^T V^{-1} u - \alpha_0 p_0$$

$$= \max_{u, \alpha} - \frac{1}{4\alpha} u^T V^{-1} u - \frac{1}{4\alpha} \cdot p_0$$

$$= \max_{u} \sqrt{p_0 \cdot u^T V^{-1} u}. \quad (28)$$

Due to the fact that $y = \sqrt{x}$ is a monotonic function, therefore the dual problem $\mathcal{U}$ is equivalent to the following optimization problem

$$\mathcal{P}_4 : \min_{u} \frac{1}{4} \| u^T V \|_F^2$$

s.t. $1^T u = 1$

$$\mu_k \geq 0, \forall k \in \mathcal{K}$$

where the first constraint comes from (24a).

Based on our analysis and transformations above, we have transformed and simplified the original problem, and shown that the original optimization can be solved by solving $\mathcal{P}_4$. To be more specific, through (26), (25) and (18), we arrive at a final closed-form expression of the optimal beamforming matrix as a function of $u$, given by

$$\mathbf{W} = \frac{1}{K} H^H (HH^H)^{-1} \text{diag} \left\{ \sqrt{\frac{p_0}{4\alpha}} \cdot u^T V^{-1} u \right\} \mathbf{s} s^H. \quad (30)$$

Moreover, it is observed that $\mathcal{P}_4$ is a typical QP optimization problem over a simplex, which can be more efficiently solved with the simplex method [30] or interior-point methods [31], compared to the original CI beamforming formulation $\mathcal{P}_1$ which is a SOCP optimization.

B. Non-Strict Phase Rotation

We extend our analysis to the case of non-strict phase rotation. Similarly, before formulating the optimization problem, we firstly construct the condition that the beamforming designs should satisfy such that the received signals are located in the constructive region. Based on Fig. 3, for consistency we denote $\overrightarrow{OA} = t \cdot s_k$ and $t = |\overrightarrow{OA}|$ is the objective to be maximized. Following (2), we denote the received signal for user $k$ as $\overrightarrow{OB}$, which is expressed as

$$\overrightarrow{OB} = \mathbf{h}_k \mathbf{W} \mathbf{s} = \lambda_k s_k. \quad (31)$$

In the case of non-strict phase rotation, each $\lambda_k$ can be a complex value, which mathematically represents that a phase rotation is included for the received signal $\overrightarrow{OB}$ compared to the data symbol $s_k$, as shown in Fig. 3. This is different from the case of strict phase rotation where each $\lambda_k$ is strictly real. Then, based on the fact that $\overrightarrow{OC}$ and $\overrightarrow{CB}$ are perpendicular, we can obtain the expression of $\overrightarrow{OC}$ and $\overrightarrow{CB}$, given by

$$\overrightarrow{OC} = \Re (\lambda_k) s_k = \lambda_k^R s_k, \quad \overrightarrow{CB} = j \cdot \Im (\lambda_k) s_k = j \cdot \lambda_k^\Im s_k. \quad (32)$$

where based on Fig. 3 the imaginary unit ‘$j$’ denotes a phase rotation of $90^\circ$ geometrically. For simplicity of denotation, we denote $\lambda_k^R = \Re (\lambda_k)$ and $\lambda_k^\Im = \Im (\lambda_k)$, respectively. Due to the fact that the nodes ‘O’, ‘A’ and ‘C’ are co-linear, we can further obtain the expression of $\overrightarrow{AC}$ as

$$\overrightarrow{AC} = (\lambda_k^R - t) s_k. \quad (33)$$

In Fig. 3, we can observe that to have the received signal $\overrightarrow{OB}$ located in the constructive region is equivalent to the following condition:

$$\theta_{AB} \leq \theta_t \Rightarrow \tan \theta_{AB} \leq \tan \theta_t \Rightarrow \frac{\overrightarrow{CB}}{\overrightarrow{AC}} = \frac{|\lambda_k^\Im s_k|}{|\lambda_k^R - t s_k|} \leq \tan \theta_t \Rightarrow (\lambda_k^R - t) \tan \theta_t \geq |\lambda_k^\Im|. \quad (34)$$

In the case of $\lambda_k^\Im = 0$, $\forall k \in \mathcal{K}$, (34) is identical to (4), and the non-strict phase rotation reduces to the strict phase rotation. For $M$-PSK modulation, it is observed from the modulation constellation that the threshold angle $\theta_t$ can be expressed as

$$\theta_t = \frac{\pi}{M}. \quad (35)$$

With the above formulation, we can construct the optimization problem of CI for non-strict phase rotation as

$$\mathcal{P}_5 : \max_{\mathbf{W}, t} t$$

s.t. $\mathbf{h}_k \mathbf{W} \mathbf{s} = \lambda_k s_k, \forall k \in \mathcal{K}$

$$|\lambda_k^R - t) \tan \theta_t \geq |\lambda_k^\Im|, \forall k \in \mathcal{K}$$

$$\|\mathbf{W} s\|_F^2 \leq p_0 \quad (36)$$

To further analyze the optimization problem for non-strict phase rotation, we first transform $\mathcal{P}_5$ in (36) into a standard minimization form, given by

$$\mathcal{P}_6 : \min_{\mathbf{W}, t} -t$$

s.t. $\mathbf{h}_k \mathbf{W} \mathbf{s} - \lambda_k s_k = 0, \forall k \in \mathcal{K}$

$$|\lambda_k^R - (\lambda_k^R - t) \tan \theta_t| \leq 0, \forall k \in \mathcal{K} \quad (37)$$

$$\sum_{i=1}^{K} s_i^H \mathbf{w}_i^H \mathbf{w}_i s_i - \frac{p_0}{K} \leq 0$$

Then, by following a similar step in (9)-(17) with the Lagrangian approach, we can obtain that the optimal beamforming structure for non-strict phase rotation is the same as that
for strict phase rotation, which is given in \(13\). With the power constraint strictly active, we can further obtain that
\[
\|Ws\|_P^2 = p_0
\Rightarrow s^H W^H W s = p_0
\Rightarrow s^H \text{diag}(\Lambda^H)(HH^H)^{-1} \text{diag}(\Lambda)s = p_0
\Rightarrow \Lambda^H T \Lambda = p_0,
\]
where \(T\) is given by \(20\). However, we note that, different from the case of strict phase rotation, for the case of non-strict phase rotation \(13\) is not in a quadratic form since each \(\lambda_k\) can be complex. By decomposing
\[
\Lambda = \left[\Re(\Lambda^T), \Im(\Lambda^T)\right]^T,
\]
we can expand \(13\) with its real and imaginary components and further transform the power constraint into a quadratic form, given by
\[
\|Ws\|_P^2 = p_0
\Rightarrow \Lambda^T T \Lambda - p_0 = 0.
\]
(40)

Similar to the optimization \(P_3\) in \(22\) for strict phase rotation, we can formulate an optimization problem on \(\Lambda\) for non-strict phase rotation, expressed as
\[
P_7: \min_{\Lambda, t} - t
\text{s.t. } \Lambda^T T \Lambda - p_0 = 0
\frac{\lambda_k^3}{\tan \theta_t} + t - \lambda_k^R \leq 0, \forall k \in K
\frac{\lambda_k^3}{\tan \theta_t} + t - \lambda_k^R \leq 0, \forall k \in K
\]
(41)

where we have transformed the CI constraint with the absolute value on \(\lambda_k^3\) into two separate constraints. We then analyze \(P_7\) with Lagrangian and KKT conditions, where the Lagrangian of \(P_7\) is constructed as
\[
\mathcal{L}(\Lambda, t, \alpha_0, \hat{\mu}_k, \hat{\nu}_k) = -t + \alpha_0(\Lambda^T T \Lambda - p_0)
+ \sum_{k=1}^K \hat{\mu}_k \left(\frac{\lambda_k^3}{\tan \theta_t} + t - \lambda_k^R\right) + \sum_{k=1}^K \hat{\nu}_k \left(-\frac{\lambda_k^3}{\tan \theta_t} + t - \lambda_k^R\right)
= \sum_{k=1}^K (\hat{\mu}_k + \hat{\nu}_k - 1) t - \alpha_0 T \Lambda - \alpha_0 p_0
- \sum_{k=1}^K (\hat{\mu}_k + \hat{\nu}_k) \lambda_k^R + \sum_{k=1}^K (\hat{\mu}_k - \hat{\nu}_k) \frac{\lambda_k^3}{\tan \theta_t},
\]
(42)

where \(\alpha_0, \hat{\mu}_k\) and \(\hat{\nu}_k\) are the dual variables, and \(\hat{\mu}_k \geq 0, \hat{\nu}_k \geq 0, \forall k\). By introducing
\[
\hat{u}_k \equiv \sqrt{p_0} \cdot \hat{u}_k,
\]
where \(\hat{u}_k \in \mathbb{C}^{2K \times 1}\) and \(S \in \mathbb{C}^{2K \times 2K}\), the Lagrangian for \(P_7\) can be further simplified into
\[
\mathcal{L}(\Lambda, t, \alpha_0, \hat{u}) = (1^T \hat{u} - 1) t + \alpha_0 \hat{u}^T \hat{\Lambda} - \hat{u}^T S \hat{\Lambda} - \alpha_0 p_0.
\]
(44)

Based on \(44\), we express the KKT conditions for optimality of \(P_7\) in the following:
\[
\frac{\partial \mathcal{L}}{\partial \hat{u}} = 1^T \hat{u} - 1 = 0
\frac{\partial \mathcal{L}}{\partial \hat{\Lambda}} = 2\alpha_0 \hat{\Lambda} - S^T \hat{u} = 0
\alpha_0 (\hat{\Lambda}^T T \hat{\Lambda} - p_0) = 0
\hat{\mu}_k \left(\frac{\lambda_k^3}{\tan \theta_t} + t - \lambda_k^R\right) = 0, \forall k \in K
\hat{\nu}_k \left(-\frac{\lambda_k^3}{\tan \theta_t} + t - \lambda_k^R\right) = 0, \forall k \in K
\]
(45)

Based on \(45\), we can obtain \(\alpha_0 = 0\) and the expression of \(\hat{\Lambda}\), given by
\[
\hat{\Lambda} = \frac{1}{2\alpha_0} \hat{T}^{-1} S^T \hat{u},
\]
(46)

where we note that \(\hat{T}\) is symmetric. Moreover, from \(45\), we obtain that the power constraint is strictly active with \(\alpha_0 = 0\), and we can further obtain the expression of \(\alpha_0\) as
\[
\frac{\hat{u}^T S \hat{T}^{-1} S^T \hat{u}}{4p_0} = \left(\hat{u}^T \hat{V}^{-1} \hat{u}\right)_{4p_0}
\]
(47)

where for simplicity and consistency we introduce
\[
\hat{V}^{-1} = S \hat{T}^{-1} S^T.
\]
(48)

Similar to the case for strict phase rotation, it is easy to observe that the Slater’s condition is satisfied for \(P_7\), and therefore by following a similar approach in \(27\) and \(28\), the dual problem for \(P_7\) can be formulated into
\[
\hat{U} = \max_{\hat{u}} - \sqrt{p_0} \cdot \hat{u}^T \hat{V}^{-1} \hat{u},
\]
(49)

which further leads to the following equivalent optimization for non-strict phase rotation
\[
P_8: \min_{\hat{u}} \hat{u}^T \hat{V}^{-1} \hat{u}
\text{s.t. } 1^T \hat{u} = 1
\hat{u}_k \geq 0, \forall k \in \{1, 2, \cdots, 2K\}
\]
(50)

where we denote \(\hat{u}_k\) as the \(k\)-th entry in \(\hat{u}\), and we obtain \(\hat{V}^{-1} \in \mathbb{C}^{2K \times 2K}\) based on \(13\). \(P_8\) is also a QP optimization over a simplex, which can be efficiently solved. The final optimal beamforming matrix for non-strict phase rotation can be similarly obtained in a closed form as a function of \(\hat{u}\), given by
\[
W = \frac{1}{K} (H^H (HH^H)^{-1} \text{diag}\left(\sqrt{p_0} \cdot \hat{u}^T \hat{V}^{-1} \hat{u}\right)) S^H,
\]
(51)
where $\mathbf{U} = \begin{bmatrix} \mathbf{I} & \mathbf{I} \cdot \mathbf{I} \end{bmatrix}$ is a transformation matrix that transform the real-valued vector $\mathbf{A}$ into its complex equivalence.

Based on the formulated equivalent optimization problems $\mathcal{P}_4$ in (59) and $\mathcal{P}_8$ in (50), we note the similarity of the optimization problem for strict phase rotation and non-strict phase rotation. We observe that the objective function of $\mathcal{P}_4$ for strict phase rotation and $\mathcal{P}_8$ for non-strict phase rotation is identical, and both optimization problems share the same constraints. It is further observed that the only difference between $\mathcal{P}_4$ and $\mathcal{P}_8$ is the problem size. It is then concluded that a $K$-dimensional optimization problem for non-strict phase rotation and a $2K$-dimensional optimization for strict phase rotation share the same problem formulation, and therefore they can be solved in a similar way.

IV. CI AS A GENERALIZATION OF ZF PRECODING

In this section, we discuss the connection between the CI beamforming for strict phase rotation and the conventional ZF precoding. For the CI beamforming with non-strict phase rotation, the connection can be obtained in a similar way. To compare the CI beamforming and the conventional ZF precoding, as a reference we first present the precoded signal vector of ZF, given by

$$ x_{ZF} = \mathbf{W}_{ZF} s = \frac{1}{f} \cdot \mathbf{H}^H (\mathbf{H} \mathbf{H}^H)^{-1} s, \quad (52) $$

where $f$ is the scaling factor to meet the transmit power constraint. For fairness of comparison, we employ a symbol-level normalization for $\mathbf{W}_{ZF}$ such that $\|\mathbf{W}_{ZF} s\|^2_F = p_0$ as for the considered CI beamforming, which leads to the expression of $f$ as

$$ f = \sqrt{\frac{\|\mathbf{W}_{ZF} s\|^2_F}{p_0}} = \sqrt{\frac{s^H (\mathbf{H} \mathbf{H}^H)^{-1} s}{p_0}}. \quad (53) $$

By denoting $\mathbf{C} = (\mathbf{H} \mathbf{H}^H)^{-1}$, the expression of $f$ can be further transformed into

$$ f = \sqrt{\sum_{m=1}^{K} \sum_{n=1}^{K} \mathbf{C}(m,n) s_m^H s_n} \quad \Rightarrow \sum_{m=1}^{K} \sum_{n=1}^{K} \mathbf{C}(m,n) s_m^H s_n = f^2 p_0. \quad (54) $$

Subsequently, we perform the mathematical analysis on the optimization problem $\mathcal{P}_4$ on $u$ for strict phase rotation. By applying the Lagrangian approach, we can obtain the Lagrangian of $\mathcal{P}_4$, given by

$$ \mathcal{L}(u, q_0, q) = u^T \mathbf{V}^{-1} u + q_0 (1^T u - 1) - \sum_{k=1}^{K} q_k \mu_k = u^T \mathbf{V}^{-1} u + q_0 \cdot 1^T u - q^T u - q_0, \quad (55) $$

where the vector $q = [q_1, q_2, \cdots, q_K]^T$ consists of each non-negative dual variable $q_k$ of $\mathcal{P}_4$. Based on (55), we express the KKT conditions of $\mathcal{P}_4$ as

$$ \frac{\partial \mathcal{L}}{\partial u} = 2 \mathbf{V}^{-1} u + q_0 \cdot 1 - q = 0 \quad (56a) $$

$$ q_0 (1^T u - 1) = 0 \quad (56b) $$

$$ q_k \mu_k = 0, \quad \forall k \in \mathcal{K} \quad (56c) $$

Based on (56a) we can obtain the expression of $u$ as a function of the dual variables, given by

$$ u = \frac{1}{2} \mathbf{V} (q - q_0 \cdot 1), \quad (57) $$

and each $\mu_k$ as

$$ \mu_k = \frac{1}{2} (v_k q_k - q_0 a_k), \forall k \in \mathcal{K}, \quad (58) $$

where we have decomposed $\mathbf{V}$ into $\mathbf{V} = [v_1^T, v_2^T, \cdots, v_K^T]^T$. $a = [a_1, a_2, \cdots, a_K]^T$ denotes the column vector obtained from the sum of $\mathbf{V}$ by column, with each entry given by

$$ a_k = \sum_{i=1}^{K} \mathbf{V}(k,i). \quad (59) $$

By substituting the expression of $u$ into (53b), we further obtain that

$$ 1^T u - 1 = 0 \Rightarrow \frac{1}{2} \sum_{k=1}^{K} \left\{ q_0 \sum_{i=1}^{K} \mathbf{V}(k,i) q_i - q_0 a_k \right\} - 1 = 0 \Rightarrow \frac{1}{2} \sum_{i=1}^{K} \sum_{k=1}^{K} \mathbf{V}(k,i) q_i - \frac{1}{2} q_0 c - 1 = 0 \Rightarrow \frac{1}{2} \sum_{i=1}^{K} b_i q_i - \frac{1}{2} q_0 c - 1 = 0 \Rightarrow q_0 = \frac{b q - 2}{c}, $$

where $b$ is a row vector obtained from the sum of $\mathbf{V}$ by row and $c$ denotes the sum of all the entries in $\mathbf{V}$. $b$ and $c$ are given by

$$ b = \sum_{k=1}^{K} v_k = a^T, \quad (61) $$

$$ c = \sum_{k=1}^{K} \sum_{i=1}^{K} \mathbf{V}(k,i) = a^T 1, $$

where $b = a^T$ is based on the fact that $\mathbf{V}$ is symmetric. By substituting the expression of $q_0$ in (60) into (58), the expression of each $\mu_k$ can be further transformed into

$$ \mu_k = \frac{1}{2} v_k q_k - \frac{a_k a^T q - 2}{c} \Rightarrow \frac{1}{2} \left( v_k - \frac{a_k a^T}{c} \right) q + \frac{a_k}{c}, $$

which further leads to the expression of $u$ as

$$ u = \frac{1}{2} (\mathbf{V} - \Phi) q + \frac{a}{c}, \quad (63) $$
where $\Phi = \frac{aa^H}{c}$. By substituting the expression of $u$ into the expression of $\Lambda$ in (25), we can further obtain that

$$
\Lambda = \frac{1}{2\alpha_0} V^{-1} \left[ \frac{1}{2} (V - \Phi) q + \frac{a}{c} \right] = \frac{1}{2\alpha_0} V^{-1} a + \frac{1}{4\alpha_0} (I - V^{-1}\Phi) q
$$

(64)

where we have defined

$$
m = V^{-1} a.
$$

(65)

In (65), $m \in C^{K \times 1}$ and $m = [m_1, m_2, \cdots, m_K]^T$. Based on the expression of $a$, each $m_k$ is obtained as

$$
m_k = \sum_{n=1}^{K} V^{-1}(k, n) a_n = \sum_{n=1}^{K} V^{-1}(k, n) \sum_{i=1}^{K} V(n, i)
$$

(66)

$$
= \sum_{n=1}^{K} V^{-1}(k, n) V(n, k) + \sum_{i \neq k}^{K} \sum_{n=1}^{K} V^{-1}(k, n) V(n, i)
$$

$$
= 1 + \sum_{i \neq k}^{K} 0 = 1,
$$

which also means that $m = V^{-1} a = 1$. With this fact, the expression of $\Lambda$ is further transformed into

$$
\Lambda = \frac{1}{2\alpha_0} V^{-1} a + \frac{1}{4\alpha_0} (I - V^{-1}\Phi) q,
$$

(67)

based on which we shall discuss the connection between the CI beamforming and the conventional ZF scheme. In (67), if we set

$$
q_k = 0, \forall k \in K,
$$

(68)

based on (63) we can obtain that

$$
u = \frac{a}{c}
$$

(69)

and based on (26) we further obtain that

$$
\alpha_0 = \sqrt{\frac{\mathbf{a}^T V^{-1} \mathbf{a}}{4c^2 p_0}} = \sqrt{\frac{\mathbf{a}^T \mathbf{1}}{4c^2 p_0}} = \sqrt{\frac{c}{4c^2 p_0}} = \frac{1}{2c \sqrt{p_0}}
$$

(70)

Then, the expression of $\Lambda$ is simplified into

$$
\Lambda = \frac{1}{2\alpha_0} V^{-1} a + \frac{2}{2c \sqrt{p_0}} = \frac{\sqrt{p_0}}{c}
$$

(71)

Based on the expression of $T$ in (20), we can obtain the expression of $T(m, n)$ as

$$
T(m, n) = C(m, n) s_m^H s_n,
$$

(72)

and with the fact that $T$ is Hermitian, we further obtain that

$$
c = \sum_{m=1}^{K} \sum_{n=1}^{K} V(m, n) = \sum_{m=1}^{K} \sum_{n=1}^{K} T(m, n)
$$

$$
= \sum_{m=1}^{K} \sum_{n=1}^{K} C(m, n) s_m^H s_n
$$

(73)

$$
= f^T p_0.
$$

By substituting (73) into (71), we obtain

$$
\Lambda = \frac{f p_0}{f^2 p_0} = \frac{1}{f}
$$

(74)

In this case, with all dual variables equal to zero, each $\lambda_k$ is real and identical, which further leads to the expression of the precoded signal vector for CI as

$$
x_{CI} = W s = \frac{1}{K} H^H (H H^H)^{-1} s
$$

(75)

$$
= \frac{1}{f} H^H (H H^H)^{-1} s = x_{ZF},
$$

which is identical to the precoded signal vector based on ZF, where we denote $x_{CI}$ as the transmit signal vector for the CI beamforming.

The above results show that the conventional ZF precoding can be regarded as a special case of the CI beamforming with all the dual variables being zero, as demonstrated in (68). The performance of ZF method is therefore the lower-bound of the CI beamforming. We shall discuss under what conditions the CI beamforming is equivalent to the ZF approach in the following section. It can be further observed that the performance of the CI beamforming will be superior to the ZF scheme if not all the dual variables are zero, as shown in (67) where the existence of non-zero dual variables will increase the minimum value in $\Lambda$. We further note that when the optimality is achieved, the minimum value in $\Lambda$ is guaranteed to be not smaller than (74), for otherwise the ZF beamforming will generate a larger minimum value in $\Lambda$, which means that ZF should be the optimal and this causes contradiction.

**V. PROPOSED ITERATIVE CLOSED-FORM SCHEME**

In this section, our proposed iterative close-form scheme is introduced. Throughout this section, we consider the case of strict phase rotation, while the extension to the non-strict phase rotation is trivial and briefly included, as both optimization problems share the same problem formulation, discussed in Section IV. To introduce the proposed scheme, we first transform the expression of $u$ in (63) into

$$
u = \frac{1}{2} \mathbf{G} q + \frac{a}{c},
$$

(76)

where $\mathbf{G}$ is defined as

$$
\mathbf{G} = V - \Phi.
$$

(77)

Then, based on the optimality conditions in (55), as long as we find $u$ and the corresponding dual vector $q$ that satisfy (55), the obtained $u$ is the optimal solution for $P_4$. This further leads to the following optimization problem

$$
P_9: \quad \text{find } q_k \quad \text{s.t. } u = \frac{1}{2} \mathbf{G} q + \frac{a}{c}
$$

(78)

$$
1^T u - 1 = 0
$$

$$
\mu_k q_k = 0, \mu_k \geq 0, q_k \geq 0, \forall k \in K
$$
For clarity of description, we define a set $S$ as
\[ S = \{ k \mid a_k < 0, \forall k \in K \}. \]  
(79)

In the following based on $S$ we discuss the solution of $P_9$ and propose the iterative closed-form scheme.

A. $S = \emptyset$

When $S = \emptyset$, this means $a_k \geq 0, \forall k \in K$. Then, based on the fact that $1^T a = c$ in (61), it is obvious that
\[ u = \frac{a}{c}, \quad q_k = 0, \quad \forall k \in K \]  
(80)

satisfies all the conditions in (78). Therefore, when $S = \emptyset$, the optimal $u^*$ and $q^*$ can be obtained as
\[ u^* = \frac{a}{c}, \quad q^* = 0. \]  
(81)

In this case, based on our analysis in Section IV the CI beam-forming is identical to the ZF approach, where no performance gains can be obtained.

B. $\text{card}(S) \neq \emptyset$

When $\text{card}(S) \neq \emptyset$, this means that there is at least one entry in $a$ that is smaller than zero. It is then obvious that the optimal $u^* \neq \frac{a}{c}$ due to the requirement that $\mu_k \geq 0$. In this case, we can obtain that not all the dual variables are zero, and we need to introduce at least one positive $q_i$ such that each $\mu_k \geq 0$. We firstly set
\[ u = \frac{a}{c}, \quad q = 0. \]  
(82)

Subsequently, we sort the entries in $u$ following an ascending order, expressed as
\[ d = \text{sort}\left( u \right), \]  
(83)

where $d$ is the sorted vector and $d = [d_1, d_2, \cdots, d_K]^T$. sort(·) denotes the sort function, and without loss of generality we denote $k$ as the minimum value in $u$, which leads to
\[ \mu_k = \min(\mathbf{u}) = d_1. \]  
(84)

With (83) we can also obtain $a_k < 0$ and $d_1 < 0$. Let us firstly introduce only one positive dual variable $q_k$ that corresponds to $\mu_k$ while keeping other dual variables zero. Based on the complementarity slackness condition, when $q_k \neq 0$, we obtain $\mu_k = 0$, and this further leads to
\[ \mu_k = \frac{1}{2} \sum_{i=1}^{K} \mathbf{G}(k, i) q_i + \frac{a_k}{c} = 0 \]  
\[ \Rightarrow \frac{1}{2} \mathbf{G}(k, k) q_k + \frac{a_k}{c} = 0 \]  
(85)

\[ \Rightarrow q_k = -\frac{2a_k}{\mathbf{G}(k, k) c}. \]

where based on the definition of $\mathbf{G}$ we can verify that $\mathbf{G}(k, k) > 0$. Based on the fact that $a_k < 0$ it is then obtained that $q_k > 0$. We further define a vector $i$
\[ i = [k], \quad \forall q_k \neq 0, \]  
(86)

and a set $I$ that consists of all the entries in $i$, where we denote $i = [i_1, i_2, \cdots, i_M]$ and $\text{card}(I) = M$. By updating $q$ with the updated $q_k$ based on (85), the updated $u$ can be expressed as
\[ u = \frac{1}{2} \sum_{k \in I} \mathbf{g}_k q_k + \frac{a}{c}, \]  
(87)

where we have decomposed $\mathbf{G} = [\mathbf{g}_1, \mathbf{g}_2, \cdots, \mathbf{g}_K]$, and (87) satisfies $\mu_k = 0$. We verify whether the minimum value in the updated $u$ satisfies the non-negative condition, and the updated $u$ is the optimal solution of $P_9$ if $\min(u) = 0$. If this condition is not satisfied, this means that one dual variable is not enough and we need to introduce an additional dual variable. In this case, we first sort the updated $u$ based on (83) and then find the minimum value in the updated $d$, where without loss of generality we denote
\[ \mu_l = d_1, \quad q_l \neq 0, \]  
(88)

where we note that $d_1$ in (83) is different from $d_1$ in (84) as $u$ has been updated. With the existence of two non-zero dual variables, we obtain $i = [k, l]$ and $I = \{k, l\}$. We can then formulate a matrix $\mathbf{Z} \in \mathbb{C}^{\text{card}(S) \times \text{card}(S)}$ as
\[ \mathbf{Z} = \begin{bmatrix} \mathbf{G}(k, k) & \mathbf{G}(k, l) \\ \mathbf{G}(l, k) & \mathbf{G}(l, l) \end{bmatrix}. \]  
(89)

By defining
\[ \tilde{q} = [q_k, q_l]^T, \tilde{a} = [a_k, a_l]^T, \tilde{u} = [\mu_k, \mu_l]^T \]  
(90)

that consists of the entries that correspond to the numbers of non-zero dual variables, we obtain
\[ \tilde{u} = 0, \]  
(91)

which is due to the complementary slackness condition. With (87) and (91), we can further obtain $\tilde{q}$ as
\[ \tilde{u} = \frac{1}{2} \left( \begin{bmatrix} \mathbf{G}(k, k) & \mathbf{G}(k, l) \\ \mathbf{G}(l, k) & \mathbf{G}(l, l) \end{bmatrix} q_k + \begin{bmatrix} \mathbf{G}(k, k) \\ \mathbf{G}(l, k) \end{bmatrix} q_l \right) + \frac{\tilde{a}}{c} = 0 \]  
\[ \Rightarrow \frac{1}{2} \mathbf{Z} \tilde{q} + \frac{\tilde{a}}{c} = 0 \]  
\[ \Rightarrow \tilde{q} = -\frac{1}{2} \mathbf{Z}^{-1} \tilde{a}. \]  
(92)

If each entry in the obtained $\tilde{q}$ satisfies the non-negative condition, we update $u$ based on (87) with the updated $\mathbf{Z}$, and further check whether the minimum value in the updated $u$ satisfies the non-negative condition.

Nevertheless, when $\text{card}(S) > 1$, it cannot be guaranteed that each entry in the obtained $\tilde{q}$ in (92) satisfies the non-negative condition. In this case, a retraction approach is required. To be more specific, if there is one entry in the obtained $\tilde{q}$ that is negative, we firstly find the corresponding number of the negative dual variable, given by
\[ k = \text{find}(q_k < 0), \]  
(93)

where the ‘find’ function returns the index of the negative entry in $q$. We further obtain the corresponding column index of $k$ in $i$, expressed as
\[ i_m = k. \]  
(94)
We then reset
\[ i = [i_1, i_2, \cdots, i_{m-1}], \tag{95} \]
which means that there are currently \((m - 1)\) positive dual variables and we set all the obtained dual variables obtained after \((m-1)\) to 0. With \(95\), we reformulate the corresponding \(I\) and \(u\). Then, for the \(m\)-th dual variable, instead of selecting the number that corresponds to the minimum value in \(d\) as in \(84\), we select \(\mu_m\) that corresponds to the second minimum value in \(d\). Based on \(83\) we obtain
\[ \mu_m = d_2, \tag{96} \]
and we update \(i\) and \(I\). With the updated \(I\), we calculate \(\tilde{q}\) based on \(92\), and we repeat the above process \(83\) to \(96\) by increasing the number of non-zero dual variables one at a time until all the entries in the updated \(u\) are non-negative, on the condition that in each step the entries in the obtained \(\tilde{q}\) are non-negative.

Algorithm 1 Proposed Iterative Closed-form Scheme for Strict Phase Rotation

\begin{verbatim}
input : s, H
output : W*
Initialize \(i = [], I = \emptyset, N = [1], t = 1, n = 0;\)
Calculate \(T\) based on \(20\); Obtain \(V = \Re(T)\);
Calculate \(a\) based on \(69\) and \(c\) based on \(61\);
Calculate \(G = V * \frac{a}{c}\); Calculate \(u = \frac{\hat{G}}{c}\);
Obtain \(S\) based on \(79\);
if \(card(S) = 0\) then
    Obtain \(u^* = u;\)
else
    while \(\min (u) < 0\) and \(n < n_{\text{max}}\) do
        \(d = \text{sort}(u)\);
        find \(k\) such that \(\mu_k = d_t\);
        Stack \(N = [N 1]\);
        Update \(i\) and \(I\); Formulate \(Z\) based on \(I\) and \(G\);
        Calculate \(\tilde{q}\) based on \(I\) and \(Z\) with \(92\);
        if \(\min (\tilde{q}) \geq 0\) then
            Update \(u\) based on \(87\);
            \(t = 1;\)
        else
            find \(k\) such that \(q_k = \min (\tilde{q})\);
            find \(m\) such that \(i_m = k;\)
            Set \(i\) based on \(95\); Update \(I\);
            Formulate \(Z\) based on \(I\) and \(G\);
            Update \(\tilde{q}\) with \(92\); Update \(u\) with \(86\);
            Reformulate \(N = N(1:m)\);
            Update \(N(m) \leftarrow N(m) + 1;\)
            Update \(t = N(m);\)
        end if
        \(n \leftarrow n + 1;\)
    end while
    Obtain \(u^* = u;\)
end if
Calculate \(W^*\) based on the obtained \(u^*\) with \(29\).
\end{verbatim}

C. The Iterative Algorithm

Based on the above description, we summarize the proposed scheme for strict phase rotation in Algorithm 1. Since the algorithm will find the \(u\) and \(q\) that satisfy the KKT conditions for optimality, the obtained \(u^*\) is therefore the optimal solution to the optimization problem \(P_4\) for strict phase rotation, and the optimal beamforming matrix can be obtained with \(29\) accordingly. While the algorithm is for the case of the strict phase rotation, it is trivial to extend to the case of non-strict phase rotation by substituting \(V\) with \(\hat{V}\) in \(48\) to obtain the optimal \(\hat{u}^*\). Subsequently, the optimal beamforming matrix for non-strict phase rotation is obtained with \(50\).

We note that, while the above algorithm includes an iterative design, within each iteration a closed-form solution is indeed obtained and the algorithm only includes linear matrix manipulations, which is computationally efficient. Moreover, it will be shown that the number of iterations required is small, especially when the number of users is small. We further note that, while the KKT optimality conditions are not satisfied before the final iteration, the solution obtained within each iteration is indeed a feasible solution that satisfies the power constraint for the beamforming and achieves an improved performance over ZF but a sub-optimal performance compared to the optimal CI beamforming. Indeed, the obtained beamformer in each iteration approaches the optimal beamforming strategy with the increasing iteration number. Therefore, the proposed iterative scheme can also achieve a flexible performance-complexity tradeoff by limiting the maximum number of iterations \(n_{\text{max}}\) in Algorithm 1. The complexity gain of the proposed scheme and the performance-complexity tradeoff will both be numerically studied in the following section.

VI. Numerical Results

In this section, the numerical results of the proposed schemes are presented and compared with the traditional CI beamforming based on the Monte Carlo simulations. In each plot, we assume the total transmit power available as \(p_0 = 1\), and the transmit SNR per antenna as \(\rho = 1/\sigma^2\). We compare our proposed iterative schemes with the traditional closed-form ZF-based methods, optimization-based SINR balancing approaches \([7][10]\), and CI beamforming approaches \(P_1\) and \(P_5\) for both strict and non-strict phase rotation.

For clarity the following abbreviations are used throughout this section:
1) ‘ZF’: traditional ZF scheme with symbol-level power normalization in \(52\) and \(53\);
2) ‘RZF’: traditional RZF scheme with symbol-level power normalization, where the precoded signal vector is given by
\[ x_{RZF} = W_{RZF}s = \frac{1}{f} H^H \left( HH^H + \frac{K}{\rho} I \right)^{-1} s \tag{97} \]
with the symbol-level scaling factor \(f\) given by
\[ f = \frac{\|W_{RZF}s\|_F}{\sqrt{p_0}}; \tag{98} \]
3) ‘SINR Balancing’: the SINR balancing approach based on bisection search method [11];
4) ‘CI-opt, Strict/Non-Strict’: traditional CI beamforming, $P_1$ for strict phase rotation and $P_5$ for non-strict phase rotation;
5) ‘CI-CF, Strict/Non-Strict’: the proposed iterative closed-form scheme for strict/non-strict phase rotation based on Algorithm 1.

In Fig. 4, we compare the bit error rate (BER) performance of different schemes with QPSK modulation, and $N_t = K = 8$. As can be observed, the CI beamforming approaches for both strict phase rotation and non-strict phase rotation achieve an improved performance over the ZF approach, and the gain for non-strict phase rotation is more significant. For the CI beamforming for non-strict phase rotation at high SNR regime, we observe a SNR gain of more than 10dB over ZF and 8dB SNR gain over RZF.

In Fig. 5, we show the BER performance with respect to the increasing transmit SNR when 8PSK modulation is employed, where $N_t = K = 8$. Similarly, both transmit beamforming approaches based on the CI achieve an improved performance over the ZF method, and the proposed iterative closed-form schemes achieve the same performance as the optimization-based schemes. At high SNR ($\rho > 20$ dB), both CI-based approaches outperform the ZF-based schemes. For CI with non-strict phase rotation, we observe a SNR gain of over 7dB compared to ZF, and a SNR gain of 5dB compared to RZF precoding.

In Fig. 6 shows the BER performance of different schemes for QPSK with $N_t = K = 12$, where a similar BER trend can be observed. Particularly, comparing Fig. 4 and Fig. 6, we observe that the performance gains of the CI-based approaches over the conventional ZF precoding are more significant with the increasing number of antennas and users.

In Fig. 7, the average number of iterations required for
the proposed iterative scheme is numerically studied with the increasing number of users, where we include two cases of $N_i = K$ and $N_i = 16$. We observe that the average number of iterations increases with the increase in the number of users, as a larger number of users means a high possibility that more entries in $\mathbf{a}$ can be negative. The non-strict phase rotation requires more iterations than the strict phase rotation because the problem size is doubled. We also observe that when the number of users $K$ is small, the average number of iterations can be smaller than 1 because the number of iterations is zero when $S = \emptyset$.

To show the flexible performance-complexity tradeoff for the proposed algorithm, in Fig. 8 we depict the BER performance of the proposed iterative approach with respect to the maximum iteration number $n_{\max}$, where $N_i = K = 4$. As expected, we observe that the performance of the iterative approach is identical to the conventional ZF approach when $n_{\max} = 0$. With $n_{\max}$ increases, the performance of the iterative method approaches the optimal CI-based beamforming, which validates our statement in Section V-C.

In Fig. 9, we compare the execution time required for each scheme to show the complexity benefits of the proposed iterative closed-form scheme over 5000 channel realizations, where ‘CI-QP, Strict/Non-Strict’ refers to the QP optimizations $P_4$ and $P_5$, and ‘CI-SOCP, Strict/Non-Strict’ refers to the SOCP optimizations $P_1$ and $P_5$. It is observed that the optimization for non-strict phase rotation requires more time to obtain the optimal solution that the strict-phase rotation because of the larger problem size. It is also observed that solving the equivalent QP optimization is much faster than solving the original SOCP optimization. More importantly, our proposed iterative scheme is more time-efficient than the QP algorithms, which motivates the use of the symbol-level CI beamforming in practice.

VII. CONCLUSION

In this paper, we study the symbol-level downlink beamforming schemes based on CI, where both the strict and non-strict phase rotation cases are considered. By analyzing the optimization problems with Lagrangian and KKT conditions, we firstly obtain the optimal structure of the beamforming matrix, and further transform the optimization into a QP over a simplex by formulating the dual problem. We show that the optimizations for strict and non-strict phase rotation are equivalent in terms of the problem formulation. We further illustrate that ZF precoding is a special case and lower-bound of the CI beamforming. The proposed iterative closed-form scheme is shown to achieve an identical performance to the optimization-based schemes with a reduced computational cost, which enables the use of symbol-level CI beamforming in practical wireless systems.

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