Characterization of black slags obtained during smelting in the electric arc furnace from SIDERPERU following reduction

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Accepted: 2 January 2022
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Abstract
The primary process in an electrical arc furnace (EAF) during industrial steelmaking results in tons of black slags which cause pollution to the environment. In this work, the iron oxides of black slags generated in the EAF from the SIDERPERU plant, Peru was reduced via the carbothermal reaction. The reduction of the black slag to α-Fe is demonstrated by X-ray diffraction, Mössbauer spectroscopy and magnetometry. However, phases with calcium and silicon persist in the sample after the carbothermal process. The thermodynamic calculations of the most probable reactions sequence were performed to understand the reduction process. The magnetometry measurements confirm the presence of ferromagnetic domains, supporting the success of the reduction of the black slag to α-Fe. The reduced black slags were recycled into a HRB335 steel rod by consolidation and extrusion processes and inspected by X-ray fluorescence.

Keywords Black slag · iron oxides · electric arc furnace · carbothermal reduction · Mössbauer spectroscopy, HRB335 steel

1 Introduction

Steel production is one of the most important economic activities for industrial development worldwide [1, 2]. However, the industry faces great challenges mainly related to the environmental impact caused by pollution due to millions of tons of slags generated every year [3–5]. One of the ways to reduce pollution is the recycling of scrap from an electric...
arc furnace (EAF) into new steel which is known as ‘Secondary production’. The use of steel scrap implies a great reduction in energy consumption and CO₂ emissions. However, the first steelmaking process in an EAF also generates black slags rich in iron oxides, such as hematite (α-Fe₂O₃), magnetite (Fe₃O₄) and wüstite (FeO) [6]. It is not possible to directly recycle black slags into new steel ingots since the containing oxides would make the resulting pieces brittle. In order to recycle black slags, the reduction of iron oxides is prior needed. Thus, the metal iron could be used as a raw material for steel production.

Although the reduction of iron oxides has been widely investigated, there is not much information about the reduction of the black slags as such. Even more, there is still a lack of comprehension about the chemical mechanisms governing the reduction processes of the iron oxide components [7]. Nevertheless, some progress is reported in the literature. For example, the reduction process of hematite in a blast furnace is well known [8]. During this process, iron-bearings (pellet, sinter, and lump) and coke are placed inside the blast furnace at high temperatures and after a sequence of solid and gaseous reactions, the iron is obtained, which is separated from the other materials by density [9]. Furthermore, recently the recovery of pure iron through carbothermal reduction of discarded iron ore slimes produced in the mining extraction of iron was reported [10]. And this technique was also used to reduce copper slag from the pyrometallurgical treatment of metalliferous minerals and obtained iron [11]. Besides, the iron ore reduction process is quite complex and can be carried out through various reaction paths depending on the thermodynamic conditions of the process [12].

In this work, we report the reduction of black slag produced after scrap smelting in the EAF from the SIDERPERU steel plant, Chimbote city, Perú. The sample was carbothermal reduced and characterized using X-Ray diffraction (XRD) and Mössbauer spectroscopy (MS). The XRD identified the mineralogical composition, whereas the use of MS was fundamental to identify the iron oxides in the sample. Thermodynamic calculations were used to clarify the reactions occurring during the reduction process and magnetometry measurements were performed to analyse the magnetic properties of the sample. The reduced black slags were recycled into HRB335 steel by consolidation and extrusion and analysed by X-ray fluorescence (XRF).

2 Experimental

The sample analysed in this article was collected from the first smelting process in the EAF belonging to the company SIDERPERU located in Chimbote city, Peru. In the EAF, the waste can be separated from the liquid steel due to differences in densities. The waste was collected from this remnant material, and it is named black slags because of its characteristic colour. After being collected, the samples went through a crushing process until the grain size ranged in the interval 53 - 600 μm and were sieved in a 72 μm mesh. The X-ray diffraction measurements were performed in a Shimadzu brand diffractometer (model XRD-6000) using cobalt (Co Kα) radiation. The 2θ data collection ranged from 20° to 80° with a step of 0.02° and a velocity of 4 s/step.

The reduction process was carried out through a carbothermal reaction in a tubular furnace in an argon atmosphere. Previously, the sample was mixed with graphite in the ratio sample: graphite 5:1. The thermal treatment was performed in three steps. First, the sample was heated at 10°C/min until reaching a temperature of 1000°C, keeping it at this temperature for one hour, then the temperature was increased to 1150°C for one hour and finally, the temperature was increased up to 1200 °C for 2 h.
The Mössbauer spectroscopy was performed using a 57Co (Rh) radioactive source of 50 mCi of nominal activity, linear velocity and at room temperature (RT). The spectrometer was calibrated at room temperature using α-Fe as an absorber and was adjusted using the WinNormos program applying Lorentzian functions. The magnetic measurements of the sample were performed in a DC- MPMS-SQUID magnetometer from Quantum Desing Inc. The magnetization response with temperature M(T) was collected in zero-field cooling (ZFC) and field cooling (FC) modes under 500 Oe and 5 kOe. The magnetization response with the applied field was collected in the range ±10 kOe at 10 and 300 K.

The reduced black slags were recycled into a HRB335 steel rod by following consolidation and extrusion at 400 °C. The rod was filled by a Wire Electrical Discharge Machine (WEDM) and the chips were inspected through an optical Olympus CX23 microscope at 40×. The XRF analysis for elemental composition was performed in EDX-720 Shimadzu equipment.

3 Results and discussions

Figures 1(a) and (b), respectively, show the XRD of the sample before and after the reduction process. The black slag sample (Fig. 1(a)) presents calcium silicon (CaSi, ICSD card No. 01-074-0147), magnetite (Fe₃O₄, ICSD card No. 01-076-1849), srebrodolskite (Ca₂Fe₂O₅, ICSD card No. 00-047-1744), larnite (Ca₂SiO₄, ICSD card No. 00-033-0303),

![XRD plots](image)

Fig. 1 XRD obtained by Co-radiation of a black slag collected from the electrical arc furnace from SIDER-PERU: a) Before and b) after carbothermal reduction process

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and wüstite (FeO, ICSD card No.01-073-2143). These components are in good agreement with the composition of EAF slags reported in the surveys performed by Teo et al. and Menad et al. [13, 14]. Fig. 1(b) shows the XRD of the black slag sample after carbothermic reduction. The reduction is demonstrated by the lack of iron oxides components and the presence of ferrite (α-Fe, ICSD card No. 01-087-0721) and austenite (γ-Fe, ICSD card No.01-901-4056). The calcium silicon remains after the reduction process. Besides, other phases such as CaO (ICSD card No. 01-074-1226) and SiO₂ (ICSD card No. 01-085-0335) might come from the partial decomposition of Ca₂SiO₄. It means that the conditions were enough to reduce the iron oxide contents, but it was not sufficient to completely decompose Ca₂SiO₄, persisting in the XRD. A little amount of unreacted carbon (C, ICSD card No. 00-041-1487) is also detected in the XRD suggesting that lower amounts of C could be also used to achieve the reduction of the iron oxide components. Note that there are some other peaks not identified in the diffractogram coming from impurity phases in the sample. 

Figures 2(a) and (b) show the Mössbauer spectra of the black slags before and after the carbothermal reduction process, respectively. The hyperfine parameters and relative areas are listed in Table 1. The spectra fitting for the black slag sample before reduction (Fig. 2(a)) shows two doublets corresponding to nonstoichiometric wüstite (Fe₁₋ₓO). The electronic exchange between Fe²⁺ and Fe³⁺ in octahedral sites is presented as one doublet with IS=1.01 mm/s and QS=0.97 mm/s. The other doublet, with IS=0.35 mm/s and QS=0.72 mm/s, is attributed to the electronic exchange between tetrahedral Fe³⁺ and octahedral Fe²⁺ in wüstite [15, 16]. In addition, two sextets of hyperfine fields Bhf=48.8 and 45.7 T, typical for magnetite are observed for tetrahedral Fe³⁺ and octahedral Fe²⁺/Fe³⁺ sites [17, 18]. The ratio of the area between octahedral and tetrahedral sites is around 1.8 and this value is related to the lower Mössbauer fraction in Fe²⁺/Fe³⁺ (Site B) than in Fe³⁺ (Site A) [19]. The last two sextets correspond to Ca₂Fe₂O₅ with octahedral and tetrahedral Fe³⁺ sites with Bhf=50.6 a 41.9 T [20, 21].

After the carbothermal reduction process, the fitting of the spectrum (see Fig. 2(b)) shows one paramagnetic singlet with IS=-0.12 mm/s related to austenite (γ-Fe) [22, 23], and one paramagnetic doublet with IS=0.17 mm/s and QS=0.41 mm/s associated to Fe³⁺ in a tetrahedral site. The plot shown in Fig. 2(c) provides the hyperfine magnetic field distribution P(Bhf) using 40 magnetic sub-spectra with the linear correlation between Bhf and isomer shift. Four peaks (G01-G04) corresponding to 33.5, 31.0, 29.3 and 26.0 T were calculated using four Gaussian functions. The value of the highest peak (33.5 T) is very close to that for ferrite [24, 25]. The other peaks could be related to the superparamagnetic relaxation due to the presence of nanoparticles, with large distribution size, formed during the carbothermal reduction process at high temperatures [26]. Note that the presence of ferrite and austenite here is in well agreement with the XRD analysis above and confirms the reduction of the black slags.

Figure 3 shows the magnetic measurements of the reduced sample. Fig.3(a) shows the temperature dependence of the magnetization M(T) obtained under 500 Oe and 5 kOe applied fields. Note that the magnetization values decrease when the temperature increases indicating a strong paramagnetic alignment which might be generated by CaSi, C, Ca₂SiO₄, CaO, SiO₂ and other impurities. However, the presence of a ferromagnetic contribution (assumed to come from the α-Fe, detected by the other techniques
### Before reduction

| Sample          | Fit     | Doublet | $\gamma$-Fe | $\alpha$-Fe |
|-----------------|---------|---------|-------------|-------------|
| Fe$_{1-x}$O (Site A) | Fit     | Doublet | $\gamma$-Fe | $\alpha$-Fe |
| Fe$_{1-x}$O (Site B) | Fit     | Doublet | $\gamma$-Fe | $\alpha$-Fe |
| Fe$_3$O$_4$ (Site A) | Fit     | Doublet | $\gamma$-Fe | $\alpha$-Fe |
| Fe$_3$O$_4$ (Site B) | Fit     | Doublet | $\gamma$-Fe | $\alpha$-Fe |
| Ca$_2$Fe$_2$O$_5$ (Site A) | Fit     | Doublet | $\gamma$-Fe | $\alpha$-Fe |
| Ca$_2$Fe$_2$O$_5$ (Site B) | Fit     | Doublet | $\gamma$-Fe | $\alpha$-Fe |

### After reduction

| Isomer shift | G01    | G02    | G03    | G04    | SUM     |
|--------------|--------|--------|--------|--------|---------|
|              | 26.0(5)| 29.3(7)| 31.0(1)| 33.5(5)| SUM     |

### Isomer shift vs. $B_{hf}$ (T)

- $P(B_{hf})$
- $\text{Isomer shift (mm/s)}$

![Graph showing isomer shift vs. $B_{hf}$ (T)](image)
above) prevents a fast exponential decay of the ZFC and FC loops with increasing temperature. The ZFC and FC branches obtained under 500 Oe present irreversibility in all the ranges of temperature. However, under an external field of 5 kOe, they turn reversible together with the increase in magnetization values since this applied field is strong enough to align most of the magnetic domains. Remarkably, the M(T) loops do not present any of the following transitions: Verwey at ~124 K, Neel at ~197 K, nor Morin at ~275 K, corresponding to magnetite, wüstite and hematite, respectively, confirming the correct reduction of the iron oxides of the black slags.

Figure 3(b) shows the applied field dependence of the magnetization at 10 and 300 K. In the plots, the paramagnetic contribution of the non-iron impurities is demonstrated by the increase of the magnetization values when decreasing the temperature under high applied fields. Under low applied fields the loops present hysteresis (see inset plot), confirming the ferromagnetic domains mainly caused by α-Fe. The law values of the remanence and coercive fields indicate that the reduced sample is a soft ferromagnetic. These results corroborate the XRD and Mössbauer analysis above.

Following the analysis above, the reduction process of the iron oxide components contained in the black slags is next discussed. As mentioned in the experimental section, the reduction was carried out in an argon atmosphere at high temperatures using graphite as a reducer agent. As the temperature increased in the furnace, a series of chemical reactions occurred that lead to the reduction of the iron contents in the black slag sample. This should have followed a similar three-stage reduction mechanism suggested in the literature ($\text{Fe}_2\text{O}_3 \rightarrow \text{Fe}_3\text{O}_4 \rightarrow \text{FeO} \rightarrow \text{Fe}$) [27]. Although there is also the possibility that some of the stages do not occur or they occur simultaneously [28, 29]. In order to elucidate the sequence of the reactions occurring in the process, the Gibbs free energies and enthalpy changes of the reactions were calculated using the Shomate equation provided by the National Institute of Standards and Technology (NIST) [30]. The relationship of both thermodynamic quantities with temperature is shown in Fig. 4 which considers the conditions during the experimental procedure described above.

| Table 1 | Mössbauer parameters of the black slag samples before and after the carbothermal reduction process. |
|---------|--------------------------------------------------------------------------------------------------|
| Site    | IS (mm/s) | QS (mm/s) | $B_{\text{ef}}$ (T) | W (mm/s) | RAA* (%) |
|---------|-----------|-----------|---------------------|----------|-----------|
| Before carbothermal reduction | | | | | |
| $\text{Fe}_{1-x}\text{O}$ | $\text{Fe}^{2+}$ | 1.01(1) | 0.97(9) | - | 0.66(3) | 57.2(2) |
| | $\text{Fe}^{3+}$ | 0.35(6) | 0.72(8) | - | 0.29(2) | 5.8(5) |
| $\text{Fe}_3\text{O}_4$ | $\text{Fe}^{3+}$ | 0.27(6) | 0.01(6) | 48.8(8) | 0.41(6) | 10.5(7) |
| | $\text{Fe}^{2+}/\text{Fe}^{3+}$ | 0.66(5) | - | 45.7(3) | 0.76(6) | 19.1(7) |
| $\text{Ca}_2\text{Fe}_2\text{O}_5$ | $\text{Fe}^{3+}$ | 0.35(2) | -0.51(1) | 50.6(7) | 0.44(7) | 3.3(8) |
| | $\text{Fe}^{3+}$ | 0.22(1) | 0.71(2) | 41.9(1) | 0.74(7) | 4.1(1) |
| After carbothermal reduction | | | | | |
| $\gamma$-Fe | $\text{Fe}^0$ | -0.12(5) | - | - | 0.38(5) | 34.1(8) |
| Doublet | $\text{Fe}^{3+}$ | 0.17(8) | 0.41(6) | - | 0.35(7) | 37.7(1) |
| Distribution | $\langle\text{IS}\rangle$ (mm/s) | $2\varepsilon$ (mm/s) | $\langle B_{\text{ef}}\rangle$ (T) | W (mm/s) | RAA* (%) |
| | | | | | |
| $\alpha$-Fe | $\text{Fe}^0$ | 0.00(5) | - | 32.6(6) | 0.30(0) | 28.2(1) |

*RAA: Relative Absorption Area
Fig. 3 Magnetization vs temperature (a) and magnetization vs magnetic applied field (b) responses of the black slag powder after the carbothermal reduction
Since the initial black slag does not contain hematite, the carbothermal process would start with the reduction of the magnetite content by graphite given by the equations

\[
2\text{Fe}_3\text{O}_4 + \text{C} \rightarrow 6\text{FeO} + \text{CO}_2 \tag{1}
\]

\[
\text{Fe}_3\text{O}_4 + \text{C} \rightarrow 3\text{FeO} + \text{CO} \tag{2}
\]

the equations (1) and (2) are exergonic at temperatures above 500 °C (see Fig. 4a). Then, carbon dioxide should have interacted easily with the solid graphite because it is in a gaseous state. This would facilitate the disproportionation of carbon dioxide through the reaction

\[
\text{CO}_2 + \text{C} \rightarrow 2\text{CO} \tag{3}
\]

which was performed at 1000°C in the present work (the last reaction is only possible at temperatures above 700 °C as seen in Fig. 4a). Eventually, the reduction of wüstite content in the black slag due to the interaction with graphite follows as

\[
\text{FeO} + \text{C} \rightarrow \text{Fe} + \text{CO} \tag{4}
\]
and thus, the iron is recovered from the black slags. The reactions described in equations (4) and (5) were achieved by setting the temperature to 1200 °C in the present work (see experimental section) since the spontaneity of the reactions occurs at temperatures above 900 °C and 1000 °C, respectively (see Fig. 4a) and are expected to occur at higher temperatures than reactions (1), (2) and (3).

On the other hand, it is important to note that all five reactions above are endothermic as is observed in Fig. 4b. However, the entropic increase at high temperatures makes them viable. That is, the reason why reduction through gaseous interaction with carbon monoxide is not being considered. In this way, the reactions

$$2\text{FeO} + \text{C} \rightarrow 2\text{Fe} + \text{CO}_2$$ (5)

$$2\text{Fe}_3\text{O}_4 + 4\text{CO} \rightarrow 6\text{Fe} + 4\text{CO}_2$$ (6)

$$\text{FeO} + \text{CO} \rightarrow \text{Fe} + \text{CO}_2$$ (7)

are discarded even though they are exergonic at high temperatures and would require an increase in the concentration of carbon monoxide relative to that of carbon dioxide to force the reduction [8, 31, 32]. Otherwise, the direction of the reactions (6) and (7) would be in the backward direction i.e., the iron would oxidize, which according to our results above, it did not happen. Moreover, the reaction

![Fig. 5 HRB335 steel rod elaborated from the reduced powder obtained after the carbothermal reduction of the black slag (a), Photography of the recycled HRB335 steel chips and a microscope image taken at 40× magnification (b), XRF spectrum of the HRB335 steel chips (c)](image)

| Elements | Fe   | Ca  | Mn   | Cr   |
|----------|------|-----|------|------|
| XRF (%)  | 96.41| 1.70| 1.67 | 0.22 |
is also discarded even though it is exergonic. Note that this equation implies the previous formation of carbon monoxide which at the reported temperatures, it is not sufficient enough to reduce magnetite to wüstite. Thus equations (1) and (2) are most probable.

The reduced black slags were recycled into a HRB335 steel ingot by the following consolidation at 400°C. Fig. 5(a) shows the HRB335 steel piece where a compact of 5.8 cm diameter and 3 cm thickness remains after the extrusion process leading to a rod of 30 cm length and 19 mm diameter. The rod has a smooth surface and is bent due to contraction during cooling in response to the thermal dilatation during the hot extrusion process. The rod was filled and Figure 5(b) shows the chips. They are metal in colour, curled in shape and of different sizes. Also, the surface of the chips is rough, have many small cracks and their borders are not uniform due to micro-vibrations during cutting by the WEDM. Fig. 5(c) shows the XRF spectrum of the chips. The detected elements are listed in Table 2. The results indicate the presence of Fe (96.41%) as the major component and Ca (1.70%), Mn (1.67%) and Cr (0.22%) in less proportion. The role of manganese is to improve the hardness, whereas chromium increases the resistance to corrosion and oxidation [33].

4 Conclusions

A black slag sample was collected from the electrical arc furnace from the SIDERPERU steel plant and reduced through a carbothermal reaction. The XRD analysis shows that the black slag contains calcium silicates and iron oxides such as CaSi, Ca$_2$SiO$_4$, Ca$_2$Fe$_2$O$_5$, Fe$_3$O$_4$, and FeO. After the carbothermal reduction, α-Fe and γ-Fe are achieved, as expected. Moreover, some other components such as Ca$_2$SiO$_4$ and Ca$_2$Fe$_2$O$_5$ partially reduced to SiO$_2$ and CaO. However, some CaSi and Ca$_2$SiO$_4$ remain. The MS of the sample before the reduction process indicate that wüstite is nonstoichiometric and confirm the presence of Ca$_2$Fe$_2$O$_5$ and Fe$_3$O$_4$. After the reduction process, a hyperfine field distribution related to α-Fe and one singlet of γ-Fe are observed. The paramagnetic doublet detected is associated with the tetrahedral Fe$^{3+}$ site. Additionally, another sextet is found but not identified with some phase related to the carbothermal reduction. The magnetic measurements show a ferromagnetic behaviour that should correspond to α-Fe and without the evidence of remaining iron oxides. The thermodynamic analysis and the characteristics of our procedure suggest a two-stage reduction process (Fe$_3$O$_4$ → FeO → Fe), releasing significant amounts of carbon monoxide and dioxide during the process. Therefore, the iron oxides contained in the black slag can be successfully reduced to α-Fe. The black slags were successfully recycled to HRB335 steel.
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