Organic Pollutants in Shale Gas Flowback and Produced Waters: Identification, Potential Ecological Impact, and Implications for Treatment Strategies

Andrii Butkovskyi,*‡ Harry Bruning,† Stefan A.E. Kools,‡ Huub H.M. Rijnaarts,† and Annemarie P. Van Wezel§

1Department of Environmental Technology, Wageningen University, P.O. Box 17, 6700 AA Wageningen, The Netherlands
2KWR Watercycle Research Institute, P.O. Box 1072, 3430 BB Nieuwegein, The Netherlands
3Copernicus Institute of Sustainable Development, Utrecht University, P.O. Box 80.115, 3508 TC Utrecht, The Netherlands

ABSTRACT: Organic contaminants in shale gas flowback and produced water (FPW) are traditionally expressed as total organic carbon (TOC) or chemical oxygen demand (COD), though these parameters do not provide information on the toxicity and environmental fate of individual components. This review addresses identification of individual organic contaminants in FPW, and stresses the gaps in the knowledge on FPW composition that exist so far. Furthermore, the risk quotient approach was applied to predict the toxicity of the quantified organic compounds for fresh water organisms in recipient surface waters. This resulted in an identification of a number of FPW related organic compounds that are potentially harmful namely those compounds originating from shale formations (e.g., polycyclic aromatic hydrocarbons, phthalates), fracturing fluids (e.g., quaternary ammonium biocides, 2-butoxyethanol) and downhole transformations of organic compounds (e.g., carbon disulfide, halogenated organic compounds). Removal of these compounds by FPW treatment processes is reviewed and potential and efficient abatement strategies are defined.

1. INTRODUCTION

The worldwide depletion of conventional oil and gas reserves inspired growing attention to alternative energy sources. However, the current gap between nonrenewable (81.6%) and renewable (13.4%) energy sources in the global total primary energy supply remains too wide to be closed in the coming decennia, as stated by market analysts.¹ Shale gas is here considered as an additional nonrenewable energy source for the transition period.² It can partly substitute the depleting conventional gas resources and thus decrease the dependency of many countries on these traditional supplies.³ At the same time, shale gas development has become a source of controversies among researchers, policy makers and the general public with respect to largely unknown environmental impacts.⁴ The suspected deterioration of quality and quantity of water resources, air pollution, increased traffic, noise, and light pollution, induced seismic activity and adverse health impacts are the subjects of concern.⁵

The water-related issues deserve special attention. Hydraulic fracturing, which is a basic technology for gas production from shale gas reservoirs, involves pumping of the fracturing fluid into the well under high pressure in order to increase permeability of the shale.⁶ The fracturing fluid contains chemicals added to facilitate shale gas recovery, including gelling agents, surfactants, friction reducers, corrosion and scale inhibitors, biocides, acids and pH adjusting agents.⁷—¹⁰ A mixture of the fracturing fluid and formation water, generally known as flowback water, returns to the surface within several days after fracturing with the daily flows sometimes exceeding 1000 m³.¹¹ Flowback water is less saline than formation water and contains chemicals from fracturing fluid as well as their transformation products.¹² Formative and connate water, generally known as produced water, continues flowing from the well for months to years after fracturing, though its daily flow constitutes only a few cubic meters. Produced water is generally more saline than flowback water and contains released methane and constituents of the shale, such as organic hydrocarbons and naturally occurring radioactive material (NORM).¹³

Options for flowback and produced water (FPW) management include disposal in the subsurface through deep injection wells, reuse for the next fracturing activity and/or treatment with subsequent discharge to injection wells or surface waters.¹⁴ Whereas disposal in the deep injection wells was the main technology for FPW management in the initial years of the shale gas boom in the U.S., reuse of flowback and discharge of

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Table 1. Overview of Original Literature Data on Analysis of Individual Organic Compounds in Shale Gas FPW

| Source                  | Shale Basins                  | Water             | Analyzed Compounds                                                                 | Extraction Method                                                                 | Analytical Method       | Detection |
|-------------------------|-------------------------------|-------------------|-------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------|------------------------|-----------|
| Hayes, 2009; Hayes and Severin, 2012 | Marcellus shale (19 wells); Barnett shale (5 wells) | Flowback and produced (Marcellus shale); Flowback (Barnett shale) | 70 VOC; 116 sVOC; 22 pesticides; 7 PCBs; ethylene glycol | purge-and-trap          | GC-MS^a     | quantitative |
| Maguire-Boylee and Barron, 2014 | Marcellus shale; Eagle Ford shale; Barnett shale | produced | Identification of organic compounds using NIST library | Liquid/liquid extraction with chloroform (acidified and nonacidified conditions) | GC-MS^a                | qualitative |
| Orem et al., 2014       | Marcellus shale; New Albany shale | Flowback and produced | Identification of organic compounds using NIST library and standard compounds | Ethoxylated surfactants | GC-MS^a                | semiquantitative |
| Thurman et al., 2014    | Denver-Julesburg basin; Barnett shale; Marcellus shale; Haynesville basin | Flowback and produced | Ethoxylated surfactants | Direct injection | HPLC/Q-TOF-MS^b | qualitative |
| Ferrer and Thurman, 2015 | Denver-Julesburg basin | Flowback and produced | Biocides (ADBAC, glutaraldehyde); surfactant (cocomidopropyl dimethylamine); thickener (guar gum) | Direct injection | HPLC/Q-TOF-MS^b | qualitative |
| Lester et al., 2015     | Denver-Julesburg basin | Flowback | VOC; sVOC; surfactants | Purge and trap (VOC, sVOC); Direct injection (trace organics) | GC-MS^a; HPLC/Q-TOF-MS^b | quantitative |
| Thacker et al., 2015    | Barnett shale | Not specified | VOC; sVOC; nonvolatile organics | Purge and trap (VOC, sVOC); Direct injection (trace organics) | GC-MS^a; HPLC-Q-TOF-MS^b | qualitative |
| Regnery et al., 2016    | Denver-Julesburg basin | Produced | Linear aliphatic hydrocarbons (n-C_{10} to n-C_{32}); PAH-16 | Solid-phase extraction | GC-MS^a              | quantitative |

^aGas chromatography coupled with mass spectrometry. ^bHigh pressure liquid chromatography coupled with quadrupole time-of-flight mass spectrometry. ^cHigh performance liquid chromatography coupled to high resolution mass spectrometry.
produced water after appropriate treatment has become more often utilized recently. The development of the Marcellus shale in the U.S. lacking deep injection wells in proximity of the shale gas play was the main driver for searching for reuse alternatives.

The choice of the FPW management strategy in favor of treatment followed by reuse or discharge is also expected in Europe due to the lack of deep injection wells and legislative constraints. European legislative instruments, including among others the EU Water Framework Directive, the associated Groundwater Directive and the Convention for the Protection of the Marine Environment of the North-East Atlantic (OSPAR convention) aim at zero environmental harmful discharge of oil and gas wastewater. To date only general water quality parameters and inorganic constituents of shale gas FPW are extensively characterized, whereas knowledge on presence and effects of individual organic compounds is rather scarce.

Characteristics, potential toxicity and treatability of compounds, which are present in fracturing fluids are evaluated in recent reviews. However, these compounds may and are partly known to undergo structural changes downhole under high pressure, temperature and salinity. Whereas fracturing fluids will reach the environment only as a result of accidental events, such as surface spills, fracturing of the well casing or interconnection with neighboring wells, at least part of shale gas FPW will be inevitably discharged to open water bodies after certain level of treatment. FPW treatment strategies focus on removal of oil, grease and salts, whereas specific contaminants originating from fracturing fluids remain largely unaddressed and may negatively influence and surface water ecosystems and drinking water sources. The aim of this paper is to identify organic contaminants in FPW potentially hazardous to environment using a risk quotient approach. The paper presents the case of the Dommel river in The Netherlands as an example calculation of the FPW impact on the ecosystems of small rivers and streams, thus giving a wider applicable framework for further calculations of such impacts for other watersheds. Furthermore, the efficiency of the FPW treatment methods toward removal of the identified potentially hazardous compounds is reviewed and the strategies for their elimination are proposed. Because the existing literature on the composition of flowback and produced water currently does not provide sufficient data on the concentrations of a vast number of compounds with proven human toxicity, which are regulated by U.S. National Primary Drinking Water Regulations, WHO guidelines and EU regulations (e.g., many chlorinated organic compounds), impact of FPW on drinking water sources deserves additional research and is not covered by this review.

2. IDENTIFICATION OF INDIVIDUAL ORGANIC COMPOUNDS IN FLOWBACK AND PRODUCED WATERS

The organic contaminants of shale gas FPW include compounds injected in the fracturing fluid, compounds of the formation which are mobilized when being brought in contact with fracturing fluid, and products of physicochemical and biological transformation of organic fracturing chemicals. It is anticipated that fracturing chemicals dominate in early flowback, whereas chemicals of formation dominate in late flowback and produced water. In this paper, ultimately the organic chemicals of both flowback and produced water are assessed.

Chemical characterization of FPW addresses mostly inorganic chemicals including salts, scalants and heavy metals. With respect to organic components, FPW is usually characterized using general parameters, such as total and dissolved organic carbon (TOC and DOC), oil and grease and the sum of concentrations of benzene, toluene, ethylbenzene, and xylenes (BTEX). For example, the U.S. Geological Survey National Produced Water Database contains data on TOC, DOC, biological oxygen demand (BOD), chemical oxygen demand (COD) and several individual organic compounds (methane, acetone, acetate, BTEX, phenols, ethylene glycol) but only for limited number of shale gas producing wells. At the same time reporting exact composition of fracturing fluids is done by many shale gas production companies and the vast amount of data are available online in a FracFocus database. The presence of potentially hazardous organic compounds in the fracturing fluids became one of the main reasons for negative public and policy attitude in many countries toward shale gas production. Much uncertainty about the fate of these chemicals in the well under high pressure and high temperature conditions exists. Data on the exact FPW composition with respect to organic compounds are still scarce, mostly because the complex nature of these liquids remains a challenge for analytical chemistry. The overview of original data on analytical detection of individual organic compounds in shale gas FPW available in the open literature sources is given in Table 1.

2.1. Detection of Volatile and Semivolatile Organic Compounds Using Gas Chromatography. To date, the largest sources of information on quantitative determination of particular organic compounds in shale gas FPW are the reports of Hayes (2009) and Hayes and Severin (2012). The reports cover sampling of 19 wells of Marcellus shale (Pennsylvania and West Virginia, USA) and 5 wells of the Barnett Shale (Texas, U.S.) (Table 1). Fifteen volatile organic compounds (VOCs) and 17 semivolatile organic compounds (sVOCs) were detected by the authors in more than one FPW sample. The detected VOCs included BTEX and their alkyl derivatives, carbon disulfide, acetone and halogenated compounds, including trichlorobenzene and bromofluorene. Polycyclic aromatic hydrocarbons (PAHs), phthalates, phenols, and pyridine were present among analyzed sVOCs. Most of the compounds were found in µg/L levels, whereas BTEX, carbon disulfide and pyridine were determined in low mg/L in the FPW from several wells. Pesticides, polychlorinated biphenyls (PCBs) and a number of VOCs and sVOCs were occasionally detected in single samples. The authors concluded that their detection is attributed rather to the sampling and analytical errors then to the actual presence of these compounds in the FPW.

Lester et al. (2014) showed similar composition of flowback water from Denver-Julesburg basin with respect to sVOCs. Acetone was the dominating VOC in flowback water with a concentration of 16 mg/L, thus 2 orders of magnitude higher than concentration reported by Hayes (2009). Other VOCs, present in the FPW analyzed by Hayes (2009), were not reported by Lester et al. (2014), except for xylenes and 2-butane. This difference can be explained by the less sensitive sampling and analytical methods used in the latter study.
Several recent peer-reviewed publications were aiming at qualitative or semiquantitative detection of organic pollutants in shale gas FPW by nontarget analysis.\textsuperscript{32,29} The authors identified a variety of saturated aliphatic and aromatic hydrocarbons present in the FPW. Maguire-Boyle and Barron (2014) applying acidified conditions for polar compound extraction from FPW detected large number of alkanes, resins, asphaltenes, heterocyclic and halogenated compounds, which were not reported by Orem et al. (2014).\textsuperscript{29,32} Also Maguire-Boyle and Barron (2014) analyzed produced rather than flowback water, where compounds of formation typical for oil and gas produced waters are present in higher variety and concentrations.\textsuperscript{29} In contrast, Orem et al. (2014) reported presence of compounds originating from fracturing fluids (solvent 2,2,4-trimethyl-1,3-pentanediol, biocide hexahydro-1,3,5-trimethyl-1,3,5-triazine-2-thione, friction reducer ethylene glycol), which were not detected by Maguire-Boyle and Barron (2014).\textsuperscript{32} Whereas some compounds were present in early flowback samples in concentrations reaching low mg/L levels, the rapid decrease of concentrations in samples taken during first 20 days after fracturing operation was observed.

2.2. Detection of Nonvolatile Organic Compounds Using Liquid Chromatography. Several authors used HPLC/Q-TOF-MS for qualitative detection of nonvolatile organic compounds in shale gas FPW.\textsuperscript{39−42} A number of constituents of fracturing fluids were detected by these authors. Thus, presence of ethoxylated surfactants in flowback waters from different shale gas basins in the U.S. was proven in two studies.\textsuperscript{39,44} Representative compounds of the cocamidopropyl family of surfactants were detected in FPW samples by several authors.\textsuperscript{40,42} Biocide alkyldimethyl benzyl ammonium chloride (ADBAC) was found in 54% of analyzed FPW samples by Ferrer and Thurman (2015), whereas another biocide, glutaraldehyde, was found in none of the samples.\textsuperscript{40} Thacker et al. (2015) reported presence of alkyl amines (acid dispersants/surfactants) and 2-butoxyethanol (solvent/acid dispersant/surfactant) in shale gas wastewater without specifying the water type.\textsuperscript{45}

2.3. Knowledge Gaps in Detection of Organic Compounds in FPW. Both quantitative and qualitative data on the presence of organic pollutants in shale gas FPW are scarce, especially concerning the compounds used in fracturing fluids for shale gas production. Thus, no research on the presence of corrosion inhibitors and clay stabilizers, including toxic compounds such as propargyl alcohol, thiourea and tetramethylammonium chloride, in FPW has been conducted yet. The knowledge on biocides presence and concentrations in FPW is limited to few compounds (ADBAC, hexahydro-1,3,5-trimethyl-1,3,5-triazine-2-thione and glutaraldehyde).\textsuperscript{32,40} Little is known on the transformation products of fracturing fluid additives that are formed downhole under high temperature and high pressure and return to the surface with FPW. The low molecular weight organics such as acetone, acetate and pyridine, which is not attributed to the compounds commonly present in fracturing fluids and formation waters, were found in the FPW in high concentrations as possible transformation products of more complex organic molecules.\textsuperscript{17,39} Formation of halogenated organic compounds in FPW is predicted by several authors, given high chloride and bromide content of FPW and possible decomposition of fracturing fluid additives that contain Cl and Br atoms in their molecular structure.\textsuperscript{29} However, knowledge on halogenated organics in FPW is still limited to identification of few aliphatic structures.\textsuperscript{17,29}

3. RISK SCREENING OF INDIVIDUAL ORGANIC COMPOUNDS

The available literature data on concentrations of individual organic compounds in the shale gas FPW were used for their environmental risk screening via Predicted Effect Concentration/Predicted No Effect Concentration (PEC/PNEC) approach.\textsuperscript{53} Briefly, the environmental concentrations in the receiving surface water (PECs) were predicted for the worst
| compound | CAS no. | C_{MAX} | Predicted | PNEC, μg/L | RQ | end point |
|-----------|---------|---------|-----------|-------------|----|----------|
|           |         | C_{MAX} | C_{MAX} river |             |    |          |
| Volatile Organic Compounds, μg/L | | | | | | |
| 1,2,4-trimethylbenzene | 95–63–6 | 4000 | 9.2 | 45 | 100 | 2.3 | reproduction of Daphnia magna, NOEC (21 d) |
| 1,3,5-Trimethylbenzene | 108–67–8 | 1900 | 4.4 | 45 | 100 | 1.1 | reproduction of Daphnia magna, NOEC (21 d) |
| 2-butane | 79–93–3 | 240 | 0.6 | 55 800 | 1 (SSD) | 0.00001 | growth of Microcystis aeruginosa, NOEC (8 d) |
| acetone | 67–64–1 | 16000 | 36.7 | 10 600 | 50 | 0.003 |
| benzene | 71–43–2 | 5300 | 12.2 | 1900 | 1 (SSD) | 0.006 |
| benzothiazole | 95–16–9 | 25 | <0.1 | 15 | 100 | <0.007 |
| bromoform | 75–25–2 | 9.3 | 0.0 | 29 | 1000 | 0.001 | Lepomis macrochirus, LC_{50} |
| carbon disulfide | 75–15–0 | 7300 | 16.8 | 10 | 100 | 1.7 | number of hatched eggs of Danio rerio, NOEC (8 d) |
| chloromethane (methyl chloride) | 74–87–3 | 150 | 0.3 | 200 | 1000 | 0.002 | mobility of Daphnia magna, EC_{50} (48h) |
| di-n-octyl phthalate | 100–41–4 | 670 | 1.5 | 100 | 10 | 0.02 | reproduction of Ceriodaphnia dubia, NOEC (7 d) |
| di-n-octyl phthalate | 98–82–8 | 160 | 0.4 | 35 | 10 | 0.01 | reproduction of Daphnia magna, NOEC (21 d) |

| Nonvolatile Organic Compounds, μg/L | | | | | | |
| Methylene Chloride | | | | | | |
| (dichloromethane) | 75–09–2 | 5.5 | 0.0 | 310 | 10 | 20 (QSAR) | 0.00004 | QSR case study: prediction of long-term NOEC for Daphnia magna (21 d) |
| n-isopropyltoluene | 99–87–6 | 54 | 0.1 | 6.5 | 1000 | 0.02 | Daphnia magna, LC_{50} (48h) |
| toluene | 108–88–3 | 8100 | 18.6 | 680 | 1 (SSD) | 0.03 |
| xylene | 1330–20–7 | 6500 | 14.9 | 327 | 1 (SSD) | 0.05 |
| 1,4-dioxane | 123–91–1 | 60 | 0.1 | 10 000 | 10 | 0.00001 | mortality of Pimephales promelas, NOEC (32 d) |
| 2-butoxyethanol (EGBE) | 111–76–2 | 66000 | 151.5 | 880 | 100 | 0.2 | growth of Pseudokirchneriella subcapitata, NOEC (72 h) |
| 2,4-dimethylphenol | 105–67–9 | 790 | 1.8 | 2.12 | 1000 | 0.9 | Daphnia magna, LC_{50} (48 h) |
| 2-methylphenol | 91–57–6 | 20000 | 45.9 | 2.3 | 100 | 20 | reproduction of Daphnia magna, NOEC (21 d) |
| ethylbenzene | 95–48–7 | 150 | 0.3 | 100 | 10 | 0.003 | mortality of Daphnia magna, NOEC (21 d) |
| isopropylbenzene | 80–82–8 | 160 | 0.4 | 35 | 10 | 0.01 | reproduction of Daphnia magna, NOEC (21 d) |
| benzyl alcohol | 100–51–6 | 750 | 1.7 | 1000 | 50 | 0.002 | reproduction of Daphnia magna, NOEC (21 d) |
| bis(2-ethylhexyl) phthalate (DEHP) | 117–81–7 | 870 | 2.0 | 0.2 | 49 | 1 (SSD) | 10 |
| butyl benzyl phthalate | 85–68–7 | 110 | 0.3 | 6.5 | 10 | 0.04 | Pimephales promelas, NOEC (42 d) |
| dimethyl phthalate | 131–11–3 | 15 | 0.03 | 220 | 50 | 0.0002 | mortality of Oncorhynchus mykiss, NOEC (102 d) |
| di-n-butyl phthalate | 84–74–2 | 130 | 0.3 | 10 | 10 | 0.03 | length of Oncorhynchus mykiss, NOEC (99 d) |
| di-n-octyl phthalate | 117–84–0 | 5600 | 12.9 | 6.4 | 50 | 19 | Daphnia magna, LC_{50} (48 h) |
| ethylene glycol | 107–21–1 | 58 | 0.1 | 1000 | 10 | 0.00001 | growth of Pseudokirchneriella subcapitata, NOEC (72 h) |
| fluorene | 86–73–3 | 407 | 0.1 | 0.25 | 100 | 0.22 | Ictalurus punctatus, LC_{50} (48 h) |
| naphthalene | 91–20–3 | 1400 | 3.2 | 2.4 | 50 | 1.3 | growth of Oncorhynchus gorbuscha NOEC (40 d) |
| phenanthrene | 85–01–8 | 1400 | 3.2 | 2.57 | 100 | 65.6 | changes in general physiology of Lepomis macrochirus, EC_{50} (96 h) |
| phenol | 108–95–2 | 830 | 1.9 | 8 | 10 | 0.2 | growth of Ceriichia mrigala, NOEC (60 d) |
| propylene glycol | 57–55–6 | 160 | 0.4 | 260 | 50 | 0.000001 | growth of Ceriodaphnia dubia, NOEC (7 d) |
| pyrene | 129–00–0 | 13 | 0.03 | 0.626 | 100 | 0.41 | mobility of Daphnia magna, EC_{50} (24 h) |
| pyridine | 110–86–1 | 2600 | 6.0 | 300 | 1000 | 0.02 | reproduction of Daphnia magna, NOEC (21 d) |
| alkyl dimethyl benzyl ammonium chloride (ADBAC) | 68424–85–1 | >10 | >0.02 | 0.415 | 10 | >0.05 | immobilization of Daphnia magna, EC_{50} (48 h) |
| hexahydro-1,3,5-Trimethyl-1,3,5-triazinane-2-thione | 59887–80–8 | 1500 | 3.4 | 0.114 | 1000 | 11.1 | |

**Table 2. Risk Screening of Organic Compounds Detected in FPW**
case scenario of FPW discharge with no removal of individual organic compounds because of inadequate treatment. They were compared with PNECs for fresh water organisms derived from literature or calculated from toxicity data using assessment factors. A resulting risk quotient (RQ) above the value of 1 indicates potential risk of an organic compound to the surface water ecosystems and implies the necessity of its removal prior to wastewater discharge.

### 3.1. Determination of PEC for Surface Fresh Waters

Small streams can be heavily impacted by the discharge of shale gas FPW, even after FPW treatment. The river Dommel located in the province of Noord Brabant (The Netherlands) was used as a model stream for calculation of the impact of FPW chemicals on aquatic environment (Figure 1). The Dommel has a total length of 120 km, with 85 km of downstream flow located within The Netherlands. The average flow at the river mouth is 14 m$^3$/s, dropping to 3 m$^3$/s in the dry periods. The water is not directly abstracted for drinking water production, nor intensively used for recreational purposes, therefore, direct discharge of FPW to Dommel is assumed to wastewater discharge. The river Dommel mouth is 14 m$^3$/s, dropping to 3 m$^3$/s in the dry periods.

**Average FPW volume of 2900 m$^3$ is collected during 90 days of well operation.** However, on-site storage capacities for flowback water allows for equalization of the FPW discharge. Therefore, an average daily flow of 32 m$^3$/well was calculated assuming complete equalization of the FPW flow during initial 90 days of well operation.

The time-evolution of the shale gas production includes the rapid development of the field during first 10–15 years followed by the decrease of the number of wells. Nicot et al. (2012) estimated the total water use in the peak year of the shale development equal to 3.6% of the total water use for Haynesville Shale, 3.1% for Eagle Ford Shale and 5.7% for Barnett Shale. The average peak year water use for the three shales is equal to 4.1% of the total water demand for shale gas production. This figure can be also extrapolated into the number of wells within a shale, hence Nicot et al. (2012) assumed the equal water use throughout a shale. With an estimate number of 1510 wells within the Dommel catchment basin fracturing of 62 wells during a peak year is expected. A total daily generation of 1980 m$^3$ of FPW is estimated for these 62 wells based on the average daily flow of 32 m$^3$/well. Possible refracturing of the wells was not accounted for. The water reuse ratio of 70% similar to that reported for Marcellus Shale was assumed, therefore, decreasing predicted discharge of treated FPW to Dommel to 600 m$^3$/d. This value was compared with the lowest average river flow of 3 m$^3$/s (2.6 · 10$^3$ m$^3$/d), resulting in a dilution factor of 435 for discharged FPW.

The maximal concentrations of organic compounds in FPW reported in the literature (see Section 2) were divided by dilution factor to obtain their mean PECs. In total, PEC of 22 VOCs, 37 sVOCs and 3 nonvolatile organic compounds were calculated (Table 2).

### 3.2. PNEC Assessment and RQ Calculation

PNEC of a chemical compound in aquatic environment is an indication parameter calculated by extrapolation of toxicological laboratory data for the most sensitive species to possible field impact of the compound, using the assessment factors. The PNECs for individual organic compounds in FPW were either obtained from online databases or from peer-reviewed literature sources. Most of the PNECs in these databases were calculated from chronic and acute toxicity data with assessment factors of 10–1000. PNECs of benzene, toluene, xylene, and 2-butanol were calculated using the fifth percentile of a species sensitivity distribution (SSD).

Risk quotients of three VOCs (1,2,4-trimethylbenzene, 1,3,5-trimethylbenzene, and carbon disulfide), three PAHs (naphthalene, 2-methylphenanthrene and phenanthrene), two phthalates (DEHP and di-n-octyl phthalate (DnOP)), and the transformation product of biocide azomet (hexahydro-1,3,5-trimethyl-1,3,5-triazinane-2-thione) exceeded 1. These compounds will be further referred to as "prioritized shale gas-related organic compounds". PAHs and phthalates may originate from the connate water of formation, as well as the fracturing fluid. Methylation of benzene rings which leads to the formation of 1,2,4-trimethylbenzene and 1,3,5-trimethylbenzene possibly takes place downhole under high temperature and high pressure conditions. Carbon disulfide is not used in fracturing fluid, but is a degradation product of some components of fracturing fluid, such as friction reducers and biocides.

Removal of 2-butoxyethanol is reviewed in this paper despite its comparatively low RQ (0.2) because of its abundant
Critical Review

4. TREATMENT STRATEGIES FOR REMOVAL OF PRIORITIZED SHALE GAS-RELATED ORGANIC COMPOUNDS

The treatment methods used for shale gas FPW include basic separation technologies designed for removal of TSS, oil and grease, and advanced treatment technologies designed for removal of dissolved organic compounds, inorganic ions, and radioactive materials.18,58,55 Phase separation underlies basic separation technologies, which include centrifugation, hydrocyclones, flotation, media filtration, coagulation/floculation, and evaporation. Centrifugation and hydrocyclones provide separation of suspended solids from water by gravity, but are less effective toward oil and grease removal.55 Flotation and coagulation can efficiently remove dispersed oil and grease, therefore, they are often utilized for produced water treatment.

The most common advanced treatment technologies utilized for oil and gas produced water treatment include membrane filtration, thermal distillation, adsorption, ion exchange and advanced oxidation. Nanofiltration and reverse osmosis (RO) units are utilized for removal of inorganic ions from produced water with TDS below 40 g/L.36 However, TDS of shale gas produced water can reach 200 g/L, therefore other technologies such as thermal distillation are used instead of RO.58 Mechanical vapor recompression is particularly suitable for demineralized water recovery from shale gas produced water with high TDS.37 Sorption to activated carbon, advanced oxidation and biological treatment are used for removal of dissolved organic compounds, often preceding reverse osmosis in order to remove potential foulants from feedwater.58

The detailed description of treatment technologies, their advantages and drawbacks, energy consumption and cost efficiency can be found in a number of reviews on produced water treatment.26,54,55,59–62 This review is focused instead on the ability of produced water treatment technologies to remove prioritized shale gas-related organic compounds as defined in Section 3. Influence of operational parameters and matrix effects, especially high salt content, on organic compounds removal is also discussed.

4.1. Basic Separation Technologies. Basic separation technologies are not designed for removal of individual organic contaminants. However, some of the compounds are removed through volatilization or sorption to suspended particles. Stripping of VOCs and, to lesser extent, sVOCs, occurs in dissolved air flotation (DAF) units63 (Table 3). In contrast, low (10%) removal of volatile and semivolatile chlorinated organic compounds, such as halomethanes and chloroethylenes in a DAF unit was observed.64 Removal of VOCs decreases when oil and grease content of refinery wastewater increases from 100 to 500 mg/L, possibly because oil and grease accumulation on the water surface reduces surface volatilization of these compounds.64 With oil and grease content being on average 100 to 500 mg/L,17 significant fraction of VOCs is expected to be removed from shale gas FPW in DAF units.

Partial removal of hydrophobic semivolatile and nonvolatile compounds, such as high molecular weight PAHs, can be accomplished by their distribution to dispersed oil droplets with subsequent skimming of the droplets from water surface.55 However, removal of PAHs via this mechanism is quite low, for example, YOUNKER and WALSH (2014) reported naphthalene removal of <15% in the DAF unit with initial naphthalene concentration of 1 mg/L.65 Phenol removal was not observed in the same study, therefore, removal of water-soluble organic compounds, including 2-butoxyethanol, is not expected, if absorption to dispersed oil with subsequent skimming is the major mechanism of their removal.66

Removal of PAH reached 20% (initial concentration: 19.1 μg/L) in the pilot-scale coagulation-floculation unit treating oil plant produced water with comparatively low salinity (5 g/L of NaCl) with aluminum sulfate used as a coagulant.67 YOUNKER and WALSH (2014) observed increase of naphthalene removal from 20% to 50% after addition of FeCl3 to DAF unit as a coagulant.68 Removal of phthalates (DEHP, dibutyl-phthalate, diethyl-phthalate) in the full-scale installation treating landfill leachate by coagulation with FeCl3 was below 50%.68 Correlation between removal of phthalates and removal of DOC exists, with higher phthalate removal observed when higher fraction of DOC is removed.69 Higher phthalate removal is achieved with aluminum ions used as coagulant instead of iron.70 Gopal (2007) reported low removal of halogenated disinfection byproducts in coagulation processes used in utilization in fracturing fluids and numerous cases of ground-water and surface water contaminations reported in the USA.12,53 ADBAC was detected in FPW only semiquantitatively with RQ > 0.05. Giving the low acute toxicity of ADBAC and uncertainty over the maximal concentrations of this biocide in FPW it is reviewed as prioritized shale gas-related organic compound. Removal of halogenated organics is also considered in this study. Despite 1,2,3-trichlorobenzene was the only organohalogen in FPW with RQ above 1, a number of authors confirmed the presence of halogenated aliphatic and aromatic organics and predicted their formation from high concentrations of Cl and Br in FPW.26,55 Removal of hexahydro-1,3,5-trimethyl-1,3,5-triazinane-2-thione is not further reviewed in order to remove potential foulants from feedwater.58

| technology | VOCs | PAHs | phthalates | ADBAC | 2-BE | organohalogen |
|------------|------|------|------------|-------|------|---------------|
| flotation  | + to + 61 | + to + 64 | ND | ND | ND | +62 |
| coagulation/floculation | +65 | +66 | +66 | ND | ND | ND |
| electrocoagulation | ND | +67 | +68 | ND | ND | ND |
| membrane separation (nanofiltration & reverse osmosis) | + to + 69 | +70 | +++71 | ND | ND | ND |
| thermal distillation (VCD, MSF, desalination) | +65 | +72 | ND | ND | ND | 73 |
| MPPE | +++74 | ND | ND | ND | ND | ND |
| aerobic biodegradation | +++75 | ND | ND | ND | ND | ND |
| anaerobic biodegradation | + to + 76,77 | + to + 78 | ND | ND | ND | ND |
| MBR | + to + 79 | + to + 80 | ND | ND | ND | ND |
| & | | | | | | ND |

Use of alternatives to reverse osmosis (RO).26 Mechanical vapor recompression is particularly suitable for removal of inorganic ions from produced water treatment.26,54,55,59

Table 3. Removal of Prioritized Shale Gas-Related Organic Compounds via Selected FPW Treatment Processes

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drinking water treatment. Combination of charge neutralization, adsorption, entrapment, and complexation with coagulant ions are responsible for removal of organic compounds in coagulation unit. Therefore, removal efficiencies depend on physicochemical characteristics of compounds but also on operational parameters of the process.

Electrocoagulation is the variation of coagulation process, where coagulant is generated in situ by oxidation of electrode material. Besides generation of coagulant, the process promotes degradation of organic matter by generation of oxidative species, such as hydroxyl ions, hypochlorite and hypochlorous acid. Kabdasli et al. (2009) reported complete mineralization of aqueous DEHP (50−100 mg/L) in NaCl solution. Nassef (2014) achieved complete removal of PAHs (β-naphthols) from NaCl solution of 1−7 g/L by electrocoagulation, with higher removal efficiencies at higher NaCl concentrations. However, the author did not study the mechanisms of β-naphthols removal and formation of halogenated transformation products. At the same time, halogenation of organic compounds in highly saline produced water can be expected during electrocoagulation.

4.2. Advanced Treatment Technologies. 4.2.1. Membrane Separation. Membrane separation is often employed for produced water treatment in oil and gas industry, either as a combination of membranes with different retention properties (microfiltration and ultrafiltration for removal of suspended matter followed by nanofiltration and reverse osmosis for desalination) or as a desalination technology (reverse osmosis). The membranes in oil and gas wastewater are preceded by different pretreatment technologies (media filtration, dissolved air flotation or biological treatment), because they are not resistant to oil constituents, such as BTEX. Microfiltration and ultrafiltration membranes are designed for removal of suspended and colloidal matter, bacteria, viruses and high molecular weight hydrocarbons and have low to moderate efficiency toward removal of low molecular weight organic contaminants.

Removal of VOCs, chlorinated organics and phthalates by nanofiltration and reverse osmosis (RO) is reviewed by Agenson et al. (2003) and Rodriguez et al. (2012). Rejection of these organic compounds is more effective with high desalting membranes with molecular weight cutoff (MWCO) ≤ 100 Da, then low desalting membranes with MWCO = 200 Da. Consistently low removal of dichloroethylenes (<40%), halogenated methane (<50%) and benzene (<55%) was observed with different types of high desalting RO membranes. Removal of molecules with higher molecular weight, such as toluene (>65%) and xylenes (>90%) was considerably higher. The authors concluded that membrane material, as well as size, dimensions and logKow of organic molecules appeared to be important parameters governing removal of organic compounds via RO with low rejection of volatile nonbranched low molecular weight compounds.

Removal of high molecular weight phthalates, including DEHP, exceeded 90% with RO, but also nanofiltration (MWCO = 300 Da) and ultrafiltration (MWCO = 8000 Da) membranes independent of the concentrations of phthalates. Sorption to membrane surface is possible mechanism for phthalate removal by ultrafiltration. Removal of eight PAHs, including naphthalene and phenanthrene exceeded 95% in a pilot-scale RO system applied to shale gas produced water. DBNPA, a biocide, often used in hydraulic fracturing operations, is also efficiently removed by RO membranes (reaction of 98.5−99.5%). DBNPA is even recommended for usage as an antifouling agent in drinking water treatment. At the same time, low molecular weight semivolatile 2-butoxyethanol was not rejected with ASF-99 RO membrane characterized by high NaCl rejection.

In summary, reverse osmosis can remove most of the organic compounds of concern from FPW, except of low molecular weight chlorinated hydrocarbons and 2-butoxyethanol, which are not rejected even by high-desalting RO membranes (Table 3).

4.2.2. Thermal Distillation. The operational costs of thermal distillation technologies are several times higher than that of reverse osmosis because of the high energy consumption. At the same time, thermal distillation is often utilized for FPW treatment in the full-scale installations, though it is justified rather by the need to handle produced water with high salinity (TDS > 40 g/L) then by cost efficiency. Multistage flash (MSF), multieffect distillation (MSD), mechanical vapor recompression (MVR) and dew-vaporation are four most common thermal distillation technologies, with MVR being most often used for shale gas FPW treatment.

High removal of VOCs in thermal distillation units is achieved mainly due to volatilization with vapor being removed from the system during degassing events (Table 3). Thus, Hayes et al. (2014) observed 94% removal of VOCs in full scale MVTR plant treating shale gas FPW through degassing and pressure-relief valves throughout the separator tank. The rest of VOCs (6% of the initial concentration) was found in distillate, being condensed from vapor together with distilled water, while brine did not contain VOCs. Removal of chlorinated disinfection byproducts (trihalomethanes and haloacetic acids) from seawater with high bromide content reached 99% in a MSF unit. Whereas trihalomethanes were completely vented to the air, 82% of less volatile haloacetic acids were found in brine. PAH removal by distillation is less effective, with 8% of naphthalene and >50% of methyl naphthalene recovered in the distillate of the circulation evaporator treating oil field produced water. No data on removal of phthalates, 2-butoxyethanol and quaternary ammonium compounds were found in the literature, though high solubility and moderate volatility of 2-butoxyethanol indicate that this compound can be partly condensed from vapor.

The available literature implies that thermal distillation technologies do not abate VOCs and sVOCs, but rather transform them from liquid to gas phase, followed by partial condensation in treated distillate (Table 3). The vapor thus needs to be treated before being released to the atmosphere in order to prevent environmental and human health risks related to VOCs.

4.2.3. Adsorption to Activated Carbon. Adsorption to activated carbon is usually utilized as a polishing step in wastewater treatment, because carbon can be easily overloaded with organics, especially with oil and grease. Granular activated carbon (GAC) is preferred to powdered activated carbon (PAC) for oil and gas industry applications because of the lower carbon usage rate and associated operational costs. Adsorption to activated carbon is efficient toward wide variety of organic compounds, but strongly depends on many factors, including dose and contact time, intrinsic properties of activated carbon, size, chemical structure and polarity of the adsorbates and solution properties, such as presence of competing organic matter, pH, and salinity.
Efficient removal of PAHs, including naphthalene and phenanthrene, quaternary ammonium compounds, 2-butoxyethanol, and chlorinated organic compounds via sorption to activated carbon was reported in the literature. However, removal of phthalates by activated carbon is inefficient, especially at basic pH, because of the increased electrostatic resistance between negatively charged activated carbon surface and phthalate anions, produced under basic conditions. Low affinity of phthalates to activated carbon will ultimately result in low performance of full scale installation, as shown by Asakura and Matsuto (2009), who predicted 50–70% removal of DEHP from leachate, based on carbon utilization rate of 1 kg/m³·d and initial DEHP concentration of 50 μg/L.

It should be noted, that most of the experiments on sorption of organic contaminants were performed in distilled water or distilled water with artificial addition of organic matter or NaCl, therefore, knowledge on sorption of individual organic contaminants in real FPW is missing. Moreover, different conditions of the experiments, reported in the literature, did not allow comparison of the adsorption capacity of activated carbon for all prioritized shale gas-related compounds from shale gas FPW.

High water salinity has several opposite effects on the adsorption of organic compounds. It is widely accepted that increased salinity improves sorption of organic compounds to activated carbon decreasing their solubility in the solution (so-called “salting out effect”) and suppressing electrostatic repulsions between organic compounds and activated carbon. Thus, adsorption of benzyldiethylammonium chloride in the presence of NaCl (Freundlich adsorption constant \( K_f = 235 \) mg/g) is higher than its adsorption in fresh water solution (\( K_f = 235 \) mg/g). Increased adsorption of PAH to different adsorbents with increased salt concentration was reported by several authors. At the same time, high salinity does not influence or may even enhance the adsorption of strongly hydrophobic compounds with low solubility, such as naphthalene or di-n-butyl phthalate, at low concentrations. Negative effect of increased salinity was also observed by some authors. Thus, adsorption of phenanthrene at low concentrations (3–10 μg/L) is lower in salt water, than in fresh water, whereas at high concentration (50–200 μg/L) the effect is opposite. High salinity may induce formation of water clusters on surface hydrophilic oxygen and carbonyl group, thus, directly competing with sorption of organics and hindering access to the graphic basal planes of activated carbon. Thus, sorption of toluene in controlled pH solution decreased from 750 to 350 mg/g with increase of KCl concentration from 0.05 to 0.7 M.

Other parameters, influencing sorption of organic compounds from FPW to activated carbon include dispersed oil content, temperature and pH. Dispersed oil decreases sorption of low molecular weight organic matter by competing with sorption sites on the surface of activated carbon and blocking access of low molecular weight organics to the inner micropores. Thus, addition of 100 mg/L emulsified crude oil decreased BET surface area of powdered activated carbon from 907.7 m²/g to 3.8 m²/g. Consequently, adsorption to GAC in oil and gas produced water treatment always follows pretreatment step designed for oil and grease removal, for example, DAF or coagulation.

4.2.4. Macro Porous Polymer Extraction (MPPE). MPPE is a liquid–liquid extraction technique developed for hydrocarbon removal from oil and gas produced water with extraction liquid immobilized in porous polymer particles. The particles are immobilized in columns and periodically regenerated in situ by stripping with low pressure steam followed by condensation of recovered hydrocarbons in a concentrated solution. The pilot field tests and results obtained from full scale installations proved that 95–99% removal of BTEX, PAHs, CS<sub>v</sub>, aliphatic and aromatic chlorinated hydrocarbons, including volatile chlorinated hydrocarbons with low molecular weight, is achieved with this technology (Table 3). MPPE performance toward removal of fracturing fluid chemicals has not been studied so far.

4.2.5. Advanced Oxidation. Advanced oxidation processes are used in oil and gas produced water treatment for removal of organic and some inorganic compounds, disinfection and removal of odor and color. Commonly used oxidants include ozone, hydrogen peroxide, chlorine and Fenton’s reagent (combination of hydrogen peroxide with ferrous iron). Flowback water treatment technology based on the combination of hydrodynamic cavitation, ozonation, acoustic cavitation and electrochemical oxidation is used for removal of organic matter, bacteria and scalants either for flowback reuse or as a pretreatment for reverse osmosis aiming at water discharge.

Advanced oxidation processes remove vast majority of organic compounds present in FPW (Table 3). PAHs, including naphthalene and phenanthrene are efficiently removed by ozonation with reaction rate being higher at acidic and neutral conditions. Combination of ozonation with hydrogen peroxide, ultraviolet (UV) or both does not enhance PAH removal. Photocatalytic oxidation of PAH in produced water is much slower than ozonation, probably, because of the light scavenging effect by turbidity. Contrary to PAH removal, only moderate removal of phthalates (30%) is achieved with ozone. Combination of ozone with catalysts (Co<sup>3+</sup>, GAC) or alkalination of solution increases removal efficiency of phthalates to 65–80% due to the higher decomposition of ozone into hydroxyl radicals.

Ozonation is efficient toward removal of quaternary ammonium compounds, as shown by Hernandez Leal et al. (2011), who achieved >98% removal of benzalkonium chloride (initial concentration 1 mg/L) in aerobically treated gray water after application of 1.22 mg/L of ozone. Removal of 2-butoxyethanol by ozonation is not reported in the literature. However, its removal by Fenton oxidation (combination of H<sub>2</sub>O<sub>2</sub> and Fe(II)) from water-based food paint wastewater (COD = 18 g/L, Cl<sup>−</sup> = 3.9 g/L) was above 95%.

Halogenated aliphatic compounds (e.g., trichloromethane, trichloroethylene tetrachloroethylene), as well as halogenated aromatic compounds and phthalates do not react readily with ozone, therefore, combination with other oxidation processes, such as O<sub>3</sub>–UV and O<sub>3</sub>–H<sub>2</sub>O<sub>2</sub> systems generating OH and other strong oxidants, are required for their destruction. Additionally, ozonation of FPW with high chloride and bromide concentration will promote formation of chlorinated and brominated organic compounds that can be more toxic than parent compounds since ozone enhances formation of Cl<sup>−</sup> and Br<sup>−</sup> radicals.

The rate constant of OH reaction with chloride (\( k_{OH} = 7.5 \times 10^3 M^{-1} s^{-1} \)) is significantly lower than the rate constants of OH reaction with organic compounds (\( k_{OH} > 1 \times 10^7 M^{-1} s^{-1} \)). Therefore, increase of Cl<sup>−</sup> concentrations from 0 to 50 g/L only slightly decreases ozonation efficiency catalyzing ozone destruction by high salinity. The presence of chloride also slightly enhances ozone decomposition and radical
formation, thus, decreasing ozone selectivity.\textsuperscript{110,111} In contrast, significant negative influence of salinity on Fenton’s oxidation process was found with Fenton’s reaction being inhibited by complexation of Fe\textsuperscript{3+} with Cl\textsuperscript{−} and scavenging of OH radicals by chloride.\textsuperscript{112}

Contrary to chloride, bromide with $k_{\text{OH}}$ of $8.5 \cdot 10^4 \text{ M}^{-1} \text{s}^{-1}$ may compete with organic compounds significantly decreasing efficiency of ozonation in FPW by high concentrations of bromide.\textsuperscript{58} Whereas organic compounds with $k_{\text{OH}} > 1 \times 10^6 \text{ M}^{-1} \text{s}^{-1}$ including BTEX, PAHs, and chloroethylenes will be targeted by hydroxyl radicals, oxidation of common low molecular weight degradation products, such as acetate ($k_{\text{OH}} = 1.9 \times 10^4 \text{ M}^{-1} \text{s}^{-1}$), methanol ($k_{\text{OH}} = 4.6 \times 10^3 \text{ M}^{-1} \text{s}^{-1}$) and trichloroacetate ($k_{\text{OH}} = 6 \times 10^2 \text{ M}^{-1} \text{s}^{-1}$) will be scavenged by bromides.\textsuperscript{39,108} Application of ozonation for partial destruction of high molecular weight organic compounds with high $k_{\text{OH}}$ followed by biological treatment or adsorption to activated carbon can be implemented for removal of intermediates from FPW with high bromide content.\textsuperscript{113}

4.3. Biological Treatment. Biological aerobic and anaerobic treatment of FPW was successfully implemented both in the lab and industrial scale.\textsuperscript{39,58,114} Aerobic biological treatment in sequencing batch reactor is suitable for shale gas FPW with moderate salinity (TDS = 22.5 g/L) and high acetic acid content (16 mg/L).\textsuperscript{58} Combination of anaerobic and aerobic treatment and a membrane bioreactor is used as pretreatment for organic matter removal prior to a membrane unit at the Pinedale Antcline FPW treatment facility.\textsuperscript{58,114}

Low to moderate removal of VOCs, PAHs and phthalates during aerobic and anaerobic treatment of industrial wastewaters is reported by several authors.\textsuperscript{67,115−117} Thus, 40% of the sum of PAHs present at initial concentrations of 15.2 μg/L were degraded in pilot-scale aerobic SBR treating petrochemical wastewater at long hydraulic retention time (HRT = 22 d.).\textsuperscript{67}

Two to three ring PAHs are more amenable to biodegradation under both aerobic and anaerobic conditions when compared to PAH with >3 rings.\textsuperscript{117} Thus, naphthalene removal reached 61% in the aeration tank of the municipal sewage treatment plant (HRT = 3 h), whereas removal of phenanthrene was <40% and removal of benzo(a)pyrene did not exceed 15%.\textsuperscript{118} Selection of bacteria responsible for degradation of PAH might occur with increased SRT after long-term reactor operation.\textsuperscript{15,119}

Biodegradation of phthalates depends on their molecular weight, with high removal observed for low molecular weight phthalates, such as dimethyl phthalate and diethyl phthalate, under both aerobic and anaerobic conditions.\textsuperscript{120,121} Aerobic biological removal of high molecular weight phthalates, such as DEHP, is negligible at different HRT and SRT.\textsuperscript{120,121} DEHP and DnOP are not degraded under anaerobic conditions either.\textsuperscript{121}

Aerobic conditions are more favorable for biodegradation of quaternary ammonium compounds, including ADBAC, when compared to anaerobic conditions.\textsuperscript{123−125} Apart from biodegradation, sorption to sludge contributes significantly to removal of QAC.\textsuperscript{126} Decrease of benzalkonium chloride concentrations in sludge of USB reactor, operated on a mixture of black water and kitchen waste for more than 2 years without sludge removal, was observed over one year period, indicating that adaptation of anaerobic bacterial consortium with subsequent increase of QAC biodegradation might occur.\textsuperscript{126} 2-butoxyethanol was readily biodegradable both under aerobic and anaerobic conditions in batch experiments with saline water and marine sediments.\textsuperscript{127} Similar results were obtained in an aeration tank of sewage treatment plant, with 2-butoxyethanol concentrations decreasing from 140.6 μg/L to <0.1 μg/L.\textsuperscript{128}

Biological removal of halogenated organic compounds under aerobic conditions is generally low.\textsuperscript{129} Co-metabolic removal by several groups of aerobic bacteria, including methane-oxidizing methanotrophs, toluene oxidizers and phenol oxidizers is achieved, therefore, high concentrations of methane, toluene and phenols observed in FPW will promote aerobic degradation of halogenated organic compounds.\textsuperscript{130} Combination of subsequent anaerobic treatment for dehalogenation and aerobic treatment for ring cleavage of aromatic structures and complete mineralization is the most efficient strategy for mineralization of haloorganic compounds.\textsuperscript{129−131}

Removal of organic pollutants is generally higher in membrane bioreactors (MBR) than in conventional activated sludge treatment systems.\textsuperscript{132} Membrane bioreactors (MBR) are effective toward polar organic compounds that are removed by combination of sorption and biodegradation, whereas removal of hydrophilic compounds is variable and depends on their structure.\textsuperscript{133} Removal of six PAHs, including naphthalene and phenanthrene, from synthetic petrochemical wastewater in two aerobic MBR with sidestream filtration based on cross-flow and semi dead-end filtration systems respectively, exceeded 90%.\textsuperscript{134} Biological degradation was the main removal mechanisms, responsible for at least 50% removal of each investigated compound. Volatilization was responsible for removal of <15% of low molecular weight PAH, whereas >20% of high molecular weight PAH were removed by adsorption.\textsuperscript{133} Aerobic submerged MBR is also suitable for removal of aliphatic hydrocarbons, monoaromatic hydrocarbons, aliphatic acids, aromatic acids, and PAH from oil produced water with high salinity.\textsuperscript{135} However, phthalates are poorly removed in membrane bioreactor, as shown by Llop et al. (2009), who observed negligible removal of DEHP in the submerged-filter MBR treating wastewater from chemical industry.\textsuperscript{132} The data on QAC and 2-butoxyethanol removal in MBR were not found, though high removal of these compounds is expected based on the results achieved in conventional aerobic activated sludge reactors.

Removal of halogenated organic compounds in MBR depends not only on biodegradation and/or volatilization, but also on sorption. Compounds with high log $D$ (>3.2) and high halogen content (>0.3), as well as compounds with low log $D$ (<3.2) and low halogen content (<0.1) are well removed (>85%) when compared to other organohalogenes.\textsuperscript{136} Combination of anaerobic and aerobic MBR promote biodegradation of halogenated compounds, as mentioned earlier.\textsuperscript{129,130}

High salinity of produced water is the main challenge for application of biological processes for FPW treatment, because TDS concentrations above 10 g/L can negatively influence biological activity by plasmolysis and loss of cell activity.\textsuperscript{132} However, removal of organic compounds in anaerobic and aerobic treatment systems are observed even at much higher salinity. Thus, Belkin et al. (1993) reported DOC removal of 70% at TDS of 32 g/L and 40% at TDS of 100 g/L in the combination of anaerobic and aerobic SBRs with HRTs of 20 days and 6 days respectively treating wastewater from chemical industry.\textsuperscript{131} TOC removal decreased from 90% to 40% and COD removal—from 90% to 17% in the MBR treating real
Critical Review

The impact of FPW salinity on biological removal of PAH, phthalates and QAC in activated sludge systems and MBR requires further investigation, since available literature mainly reports biological removal of these compounds from municipal and industrial wastewaters with low salinity.

5. PROSPECTS FOR REMOVAL OF PRIORITIZED SHALE GAS-RELATED ORGANIC COMPOUNDS WITH SELECTED TECHNOLOGIES

The main objectives for FPW treatment aimed at discharge to surface water include removal of suspended matter, oil and grease, dissolved organic compounds and salts. Removal of NORM is also required for the FPW with enhanced NORM content. The review of technologies supports the choice in favor of DAF with coagulation followed by MBR, ultrafiltration and reverse osmosis for FPW with low salinity and ozonation, GAC filtration and thermal distillation for FPW with high salinity.

DAF assisted with coagulant addition achieves the best performance among the basic separation technologies removing particles down to 0.3 μm, though removing only a minor fraction of prioritized shale gas-related organic compounds mostly by stripping. Collection and treatment of the generated off-gases is required to minimize negative impacts on the environment and human health.

Removal of organic compounds should precede the salt removal, because main methods utilized for desalination are either negatively influenced by organic matter (reverse osmosis) or cannot provide adequate removal of organic compounds with low molecular weight (thermal distillation). Application of subsequent anaerobic and aerobic biological treatment, where aerobic treatment stage can be designed as a submerged-filter MBR, is desired for removal of organohalogens, naturally present in the produced water. MBR is more efficient in removal of PAHs then conventional activated sludge, whereas its submerged-filter configuration is characterized by lower volatilization of organic compounds, when compared to the sidestream filtration. MBR can be followed by ultrafiltration and RO for removal of TDS and, eventually, radioactive materials, such as radium-226.

Fraction of low molecular weight hydrophilic organic compounds is often dominating DOM of FPW making biological treatment feasible. However, presence of refractory organic compounds, such as phthalates and certain transformation products of fracturing chemicals may require application of alternative treatment strategies, such as adsorption to activated carbon or ozonation instead of in combination with biological treatment or as a stand-alone processes.

Treatment of FPW with high salinity (TDS > 40 g/L) requires another strategy, as both biological treatment and RO are not applicable at such salt concentrations. Thermal distillation is normally used for treatment of FPW with high salinity. Apart from high energy costs and significant amount of solid waste created, thermal distillation processes have several disadvantages with respect to removal of prioritized shale gas-related organic compounds. They transfer the VOCs and sVOCs mostly to the gas phase, concentrate organic compounds with high molecular weight in brine, which can constitute up to 30% of initial water volume, whereas low-molecular weight VOCs and sVOCs end up in the distillate. Preozoneation of high-molecular weight organics coupled to adsorption to activated carbon or adsorption to activated carbon alone can be used as a pretreatment step before thermal distillation.

Source control measures, such as substitution of prioritized shale gas-related organic compounds in fract fluids by less hazardous alternatives should be considered. Thus, QAC biocides should be substituted by easily biodegradable and less hazardous compounds, such as glutaraldehyde. The separation and multiple reuse of early low flowback may be an effective measure for prevention of environmental contamination, because prioritized shale gas-related organic compounds originating from fract fluid will remain within the shale gas production cycle, with only minor portion entering the environment.

Finally, the impact of organic compounds from shale gas FPW on drinking water sources deserves special attention. The existing uncertainties include the human toxicity thresholds, the fate of organic contaminants in surface waters, their dilution before water intake for drinking water production and capacity of various drinking water treatment technologies for removal of these specific compounds. More elaborated studies on human toxicity assessment of FPW chemicals, including analysis of organic compounds with proven human toxicity in FPW and potential formation of disinfection byproducts from FPW-originated precursors in drinking water sources are needed.

AUTHOR INFORMATION

Corresponding Author *Phone: +31 317 483997; e-mail: andrii.butkovskyi@wur.nl.

ORCID

Andrii Butkovskyi: 0000-0003-4649-0271

Notes

The authors declare no competing financial interest.

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