Abstract: Microbial fuel cell (MFC) technology has attracted a great amount of attention due to its potential for organic and inorganic waste treatment concomitant with power generation. It is thus seen as a clean energy alternative. Modifications and innovations have been conducted on standalone and hybrid/coupled MFC systems to improve the power output to meet the end goal, namely, commercialization and implementation into existing wastewater treatment plants. As the energy generated is inversely proportional to the size of the reactor, the stacking method has been proven to boost the power output from MFC. In recent years, stacked or scale-up MFCs have also been used as a power source to provide off-grid energy, as well as for in situ assessments. These scale-up studies, however, encountered various challenges, such as cell voltage reversal. This review paper explores recent scale-up studies, identifies trends and challenges, and provides a framework for current and future research.

Keywords: microbial fuel cell; clean energy; sustainability; wastewater; bioenergy; MFC; scale-up
inorganic matters and produce electrons and protons. The protons are transported to the cathode chamber via the proton exchange membrane (PEM), and the electrons are transferred through an external circuit to a terminal electron acceptor in the cathode chamber, thereby generating power (Figure 1).

Figure 1. Schematic of the basic components of a microbial fuel cell.

MFC technology has the potential to extract energy from various organic and inorganic substrates to generate a surplus of electricity for plant operation. The technology was used and tested mainly for municipal wastewaters [10] and various industrial effluents [11], such as protein-rich wastewater [12,13] and starch processing wastewater [14]. It was also used as a power source to provide off-grid energy for remote system charging [15–17]. The real applications would require the scale up of the MFC reactors. Various approaches were reported, for instance, modifications on the electrode design and materials [16,18,19], membrane design or use of a membrane-less system [20,21], and the use of the stacking method via series and/or parallel connections of multiple MFC units [22–26]. Allometric analysis conducted by Greenman and Ieropoulos [27] suggested that a stacked microbial fuel cell has the greatest potential for practical application, as increasing the size of a microbial fuel cell system by stacking individual units would result in a linear or slightly super-linear increase in power output (Figure 2a). Therefore, in order to achieve higher power output, the authors recommended to make MFCs as small as possible whilst maintaining a high supply of fuel (e.g., wastewater), and optimizing the number of MFC units for efficient stacks [27]. Gajda et al. [28] also identified that miniaturization and multiplicity via modularity is the future trend, in addition to system architecture and longevity studies and improvements.

Scale-up MFCs, however, are found to face several limitations and challenges, for instance, high capital and operational costs [29,30], low power densities [5], operational fouling of electrode and membrane [31] and voltage and current reversal problems in stacked MFCs [32]. With regard to the sustainable potentials of MFCs, this paper reviews the recent scale-up MFC systems and subsequently identifies trends and associated challenges, lastly proposing a framework for current and future research studies.
2. Scale up

The real voltage output is affected by two major factors—the overall potentials of the anode and cathode, and the ohmic loss. The former is attributed to three basic losses, which are activation, bacterial metabolism and mass transport [7,33]. Therefore, in scaling up, the size of an individual microbial fuel cell is inversely proportional to the power density produced [6,27]. As shown in Figure 2b, the increase in the current-limiting anodic area drastically reduced the power density generated, which could be explained by the increased biofilm deposits, causing an edge effect and an increase in internal resistance [5,34]. As internal resistance (ohmic overpotential) increases, the flow of electrons between the electrodes becomes restricted, as does the movement of ions between the chambers and in the electrolyte. Apart from internal resistance, mass transfer losses generally occur due to the low diffusivity within the chamber which causes reactant depletion or product accumulation. Table 1 shows the research conducted on the scale up of MFCs in the last five years. Scale-up approaches in recent years can generally be categorized into three major areas—MFC architecture, electrode modification, and application based.

2.1. MFC Architecture

From the summary of the literature in Table 1, for scale-up reactors, generally, there are two types—one-unit with single/multiple electrodes, and stacked MFCs. Despite differences in the design, type or number of electrodes used, both single-chamber and double-chamber MFCs (SCMFCs and DCMFCs, respectively) are the popular options for scale-up reactors. The largest MFC is the movable MFC system consisting of a primary clarifier, a DCMFC and a secondary clarifier, with a total size of 1.5 m$^3$ [21]. This movable system, consisting of 336 MFC units, was able to achieve up to 91% of chemical oxygen demand (COD) removal, 64% of total nitrogen removal and 91% of ammonium nitrogen removal when treating primary effluent, generating 0.4 W/m$^3$ of maximum power density with a hydraulic retention time (HRT) of 5 h. This system was designed to be easily stacked to an existing wastewater tank due to its plug-in architecture.
Table 1. Summary of MFC scale-up studies in the last five years (2016–2020).

| Reactor Type | Substrate | COD, Conductivity, pH | Anode (Number) | Cathode (Number), Catholyte | Membrane | Max P (W/m³, Unless Specified) | COD Removal (%) | CE (%) | Reference |
|--------------|-----------|-----------------------|----------------|-----------------------------|----------|--------------------------------|----------------|--------|-----------|
| Stacked or scale-up MFCs with volume > 10 L for wastewater treatment: | | | | | | | | | |
| 1 | Movable, 1.5 m³ (Primary clarifier-DCMFC-Secondary clarifier) | Primary effluent | 0.26 g/L | GFB (8) | Bio-GFB (7), Anode effluent | Dynamic (microbial) membrane | 0.4 | 91 | - | [21] |
| 2 | DCMFC, 64 units, 1000 L | Municipal ww | 0.2–0.45 g/L, pH 7.2 | RVC | RVC, Groundwater | VANA- Dion | 0.2 | 34–95 | 5–15 | [35] |
| 3 | DCMFC, 50 units, 1000 L | Municipal ww | 0.08–0.25 g/L | GAC | GAC, Artificial catholyte | CEM | 60 | 70–90 | 41–75 | [29] |
| 4 | SCMFC, 6 units, 720 L | Sanitary sewage | 1–8.2 g/L | C felt | CoZnFeO or SnCu/C felt | Clayware | 0.085 | 87 | - | [36] |
| 5 | Submergible MFC, 255 L | Municipal ww | 0.205 g/L, 540 mS/m, pH 7 | GFB (10) | SS-AC (16, VitoCORE®) | Glass fiber separator | 0.3 | 41 | 30 | [31] |
| 6 | DCMFC, 96 units, 200 L | Primary effluent | 0.16 g/L | CFB | C cloth/N-AC, Aerobic effluent | CEM | 1 | 75 | - | [30] |
| 7 | SCMFC, 12 units, 110 L | Swine ww | 1 g/L, pH 7.5 | GFB (20) | Gas diffusion cathode | None | 0.36 | 65 | - | [37] |
| 8 | SCMFC, 85 L | Domestic ww | 0.428 g/L | GFB (22) | SS-AC (15, VitoCORE®) | Glass fiber separator | 0.605 | 80 | 27 | [38] |
| 9 | DCMFC, 72 L | Synthetic ww | 0.2–1.2 g/L, pH 6.8–7.1 | GAC/Ti mesh | GAC/Ti mesh, Desalinization effluent | CEM | 51 | 97 | - | [39] |
| 10 | DCMFC, 6 units, 60 L | Swine manure | 2.47 g/L, 830 mS/m, pH 8.5 | GG | GR, Ammonium | AEM | 4 | 36 | 17 | [18] |
| 11 | SCMFC, 45 L | Primary effluent | 0.13 g/L, 300–420 mS/m | GFB (8) | Pt/C cloth/SS (2) | None | 0.875 | 14–67 | 10–25 | [40] |
| 12 | SCMFC, 40 units, 16 L | Municipal ww | 0.3 g/L | C felt | Pb/C cloth | CEM | 47 | 84 | - | [25] |
| 13 | DCMFC, 2 units, 20 L | Brewery ww | 3.2 g/L, 242 mS/m, pH 7 | Modified C cloth | Modified C cloth | Nano-filtration membrane | 0.44 | 95 | 14 | [41] |
Table 1. Cont.

| Reactor Type | Substrate | COD, Conductivity, pH | Anode (Number) | Cathode (Number), Catholyte | Membrane | Max P (W/m², Unless Specified) | COD Removal (%) | CE (%) | Reference |
|--------------|-----------|-----------------------|----------------|-----------------------------|----------|-------------------------------|----------------|--------|-----------|
| Hybrid/coupled MFC with volume > 10 L: | | | | | | | | | |
| 14 AD-SCMFC (1 m³) | Pre-treated pharmaceutical ww | 0.16–0.36 g/L | C felt/G-SS | C felt/G-SS | Isolation pad | 1.25 A/m² | 35 | - | [16] |
| 15 Hybrid AA/O- SCMFC, 1 m³ | Domestic ww | 0.45–0.65 g/L pH 7.5–8 | CFB-SS | CFB-SS | None | 0.0036 | 95 | - | [42] |
| 16 Septic tank-SCMFC (18 units, 700 L)-Disinfection | Domestic ww | 789 g/L pH 8 | SS-GAC | C cloth | Nafion 117 | 0.00043 | 87 | 22 | [23] |
| 17 CW-DCMFC, 30 L | Dewatered alum sludge | 0.5 g/L | SS-C felt (4) | SS-C felt, AS | None | 0.448 | 92 | 0.36 | [43] |
| Scale-up MFC as off-grid power source: | | | | | | | | | |
| 18 Sediment MFC, 350 L | Synthetic ww | - | C mesh | AC | None | 0.0064 | - | - | [44] |
| 19 Sediment MFC, 195 L | River sediment | 13.5 mS/m pH 6.8–7.4 | C mesh | AC/SS | None | 0.0415 | - | - | [45] |
| 20 Sediment MFC, 72 units, 72 L | River sediment water | 890 g/L 27.206 mS/m pH 8 | Copper | Zinc | None | 0.0019 | 23 | - | [46] |
| Sediment MFC, 35 units, 35 L | River sediment water | 890 g/L 27.206 mS/m pH 8 | Copper | Zinc | None | 0.0069 | - | - | [24] |
| 21 Self-stratifying SCMFC (38 units), 19.2–57.6 L | Urine | 5.6–6.5 g/L pH 8.5–9.2 | C veil fibers | micro-porous C | None | 7.3–9.9 | 48–88 | 1.6–3.8 | [47] |
| 22 DCMFC, 12 units, 12 L | Synthetic ww | - | RVC | Pt/RVC, PBS | Nafion 117 | 16.2 mW/m² | - | - | [26] |

(SCMFC: single-chamber MFC; DCMFC: double-chamber MFC; ww: wastewater; C: carbon; CB: carbon brush; CFB: carbon fiber brush; GG: granular graphite; GR: granular rod; SS: stainless steel; GFB: graphite fiber brush; RVC: reticulated vitreous carbon; GAC: granular activated carbon; N-AC: nitrogen-doped activated carbon; AS: activated sludge; CEM: Cationic exchange membrane; AEM: Anionic exchange membrane; AD: anaerobic digester; CW: constructed wetlands; AA/O: anaerobic-anoxic/oxic; Ti: titanium; Pb: lead; Pt: platinum; PBS: phosphate buffer solution.) Similarly, in an experimental scale-up study conducted by Liang et al. [29] where a 1000 L modularized DCMFC comprising 50 stacked modules connected parallel to each other (Figure 3b), a maximum power density of 60 W/m² was produced in treating municipal wastewater, with COD removal of 70–90% and CE of 41–75%. As shown in Table 1, the major differences of these studies [21,29,35] are the reactor design, type of electrodes and catholytes. In the movable DCMFC system [21], multiple electrodes made of graphite fiber brushes were used, with the effluent from anode chamber as the catholyte, whereas in the stretched DCMFC [35], reticulated vitreous carbon was used as the electrodes, with groundwater as the catholyte, and in the modularized DCMFC [29], granular activated carbon was used as the electrodes, with an artificial solution as the catholyte. In addition, these reactors also have different circuit architectures, hence the vast difference in the power densities.
Another recent large-scale MFC is the stretched DCMFC of 1000 L consisting of 64 units developed by Blatter et al. [35]. This MFC, which was installed in an underground gallery of a municipal wastewater treatment plant (WWTP) in Châteauneuf, Switzerland (Figure 3a), produced 0.2 W/m$^3$ of maximum power density in treating municipal wastewater while achieving COD removal of 34–95% and Coulombic efficiency (CE) of 5–15% during its one-year operation.

While cation exchange membranes (CEM), including Nafion$^\text{TM}$ 117, are commonly used, in recent years, more lower-cost membranes, such as dynamic microbial separators [21], glass fiber separators [31], and nano-filtration membranes [41] are rising in demand. It is also interesting to note that membrane-less single-chamber MFCs are becoming a popular topic for scale-up studies due to the high cost of membranes [37,42,47].

Unlike DCMFCs, which require use of aerated equipment for the catholyte, SCMFCs utilizing air cathodes have also shown comparable power densities (Table 1). Figure 3c shows the pilot-scale 110 L air-cathode MFC consisting of 12 stacked units used in Babanova et al. [37] for treating swine wastewater.

2.2. Electrode Modification

For higher energy recovery performance, the electrodes of a scale-up MFC system should have (1) high mechanical strength, (2) large surface area, (3) high biocompatibility and (4) acceptable electrical conductivity [48]. As shown in Table 1, for the recent scale-up reactors, carbon- and graphite-type electrodes are used in different forms—reticulated vitreous, granular, micro-porous, felt, brush, cloth and rod, with stainless-steel mesh as the common current collector.

Recently, He et al. [21] developed low-cost biocathodes consisting of graphite fiber brushes with microbial biofilm growth derived from the dynamic membrane and percolated anolyte. In addition, Bouwman et al. [49] patented a multi-panel air cathode, allowing the welding of several smaller cathodes into a single metal sheet (Figure 4). This multi-panel air cathode was tested in Rossi et al. [38] for treating domestic wastewater with a 85 L SCMFC. With a 22-graphite fiber brush as the anode and glass fiber as the separator, a maximum power density of 0.605 W/m$^3$ was achieved with COD removal of 80% and CE of 27%. The same electrode module was also tested in a 255 L MFC prototype [31].
The submergible MFC was able to produce a maximum power density of 0.3 W/m$^3$, COD removal of 41% and CE of 30% when treating municipal wastewater with COD of 0.205 g/L during its 98-day operation. The special feature about this multi-panel electrode module is that it was designed to be easily added/submerged to the pre-existing infrastructure at WWTP, such as sludge storage tanks or primary clarifier, and thus may not require the use of additional pumps. In addition to modifying the electrode, various studies also utilized multi-electrodes for scaling up [31,37,40].

![Figure 4. Pictures of the (a) air-facing and (b) solution-facing side of the patented multi-panel electrode module, reprinted from [38]. Copyright (2019), with permission from Elsevier; (c) sandwiched corrugated electrode [16].](image)

### 2.3. Application Based

In recent years, as shown in Table 1, MFC scale-up studies have mainly targeted two applications—wastewater treatment via a standalone MFC unit or a hybrid/coupled system, and as power sources to produce off-grid energy. The substrates used are mainly municipal/domestic wastewaters. As reviewed in the previous sections, MFCs can be scaled up for wastewater treatment via stacking and/or the use of a modified electrode module. When coupled with another wastewater treatment unit, for instance, an anaerobic digester (AD), with a total AD-MFC size of 45 m$^3$, a maximum current density of 1.25 A/m$^2$ and COD removal of 35% were achieved from pre-treated pharmaceutical wastewater [16]. An MFC was also integrated into an anaerobic-anoxic-oxic (AO/O) system, and thus known as a hybrid system combining the features of the two units, with a total volume of 1 m$^3$ (Figure 5a) for domestic wastewater treatment and power generation simultaneously [42]. Under an HRT of 18 h, temperature of 8–23 °C and recirculation ratio of 200%, a maximum current density of 3.6 mW/m$^3$ and COD removal of 95% were achieved during its one-year operation. In Tang et al. [43], an MFC was coupled with a constructed wetland (CW), yielding energy recovery of 0.448 W/m$^3$ and COD removal of 92% in treating dewatered alum sludge.

Notably, a recent study conducted by Valladares Linares et al. [23] demonstrated the feasibility and sustainability of a coupled septic tank-MFC-disinfection system for residential wastewater treatment. As shown in Figure 5b, the raw influent generated from a house of five inhabitants flowed to the 1300 L septic tank by gravity, then to the 700 L AQUOX® MFC consisting of two stacks of 9 MFC units, and finally to a disinfection system with sodium hypochlorite. An ultra-low energy consumption unit consisting of capacitors and microcontrollers harvested and stored energy from the MFC. The system was deemed sustainable and feasible as no external energy was required, and the treated effluent complied with the local discharge standard.

MFCs were also scaled up to be used as power sources. Following the publications on food-fueled robots, such as the Gastrobot [50] and Ecobot series [51], in recent years, single-chamber large-scale MFCs, such as sediment MFCs [24,44–46] and self-stratifying MFCs [47], were developed to provide off-grid energy. The self-stratifying stacked MFC known as PEE-POWER® was applied in a field test involving 250,000 people and demonstrated its ability to treat undiluted urine while generating power, which was then stored in a battery bank providing lighting at night [47]. An MFC was also developed for the purpose of cellphone and remote system charging [15], and lithium battery stack charging [26]. In addition to integrating MFCs into an existing WWTP via a standalone or hybrid...
system, serving as power sources to provide off-grid energy, MFCs are also evaluated widely as biosensors for in situ assessments (not shown in Table 1), for the detection of pollutants [52,53], metals [54,55], toxicity [56] and ship movements [57].

There is also a different family of the bioelectrochemical system—the microbial electrolysis cell (MEC, not listed in Table 1). In the MEC, external voltage (usually around 0.2–0.8 V) was supplied between the electrodes producing either electricity, hydrogen or methane [58]. MECs are also commonly tested for wastewater treatment and nutrient recovery to produce the clean hydrogen energy [59,60].

3. Challenges and Future Direction

A number of challenges have been identified from the scale-up studies. The top consideration would be the cost effectiveness of these MFCs. The capital costs of the scale-up system range from USD 735/m$^3$ to 36,000/m$^3$ [16,29]. The electrodes (especially the cathode) and membrane have been the primary culprits of the high cost of an MFC system [30,61].

Therefore, the recommended approach for scale up would be developing cost-effective reactor components and configuration. The focus of recent studies has been slowly shifted from membraned MFCs to membrane-less MFCs [46,47], or MFCs with low-cost membranes, e.g., dynamic membranes [21], glass fiber separators [31] and nano-filtration membranes [41]. Apart from the capital cost, operational costs such as pumping effluent and mixing are also detrimental to the energy usage and cost [62]. For this reason, among the MFC systems reviewed, submergible and stackable electrode modules, or sediment SCMFC types (Benthic MFCs), seem to stand out from the rest because these units are submergible, single-chambered and integrated directly into the existing treatment tanks; no additional pumps are required for feeding, discharging and aerating, which is more cost effective and sustainable.

The next challenge which is also of paramount importance is boosting the output yields. MFCs are generally known to produce much lower energy than other fuel cells or batteries. Owing to the highly non-linear inverse relationship between the power and size, the stacking of small MFC units via series and/or parallel connections has been proven to increase the current and voltage output. However, stacking presents new issues due to kinetics imbalance, i.e., the formation of shunt current, voltage reversal

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Figure 5. (a) Hybrid MFC-AA/O system for domestic wastewater treatment and power generation, reprinted from [42]. Copyright (2017), with permission from Elsevier; (b) hybrid septic tank-MFC-disinfection system for residential wastewater treatment and power generation [23].
and current reversal [32,39,63,64]. Different circuit connections also result in changes in microbial communities [25]. Wu et al. [39] suggested lowering the external resistances of the stacked MFC system to reduce current reversal problems, especially for parallel connections. Recently, Kim et al. [32] presented some realistic approaches to control and suppress the voltage reversal issue, such as using enriched electroactive microorganisms, altering and optimizing the circuitry mode. Careful design of the circuitry coupled with the use of a maximum power point tracker has been demonstrated to eliminate voltage reversal in series connections [35,65], achieving enhanced Coulombic efficiency and limiting the methanogenic activity of the bacteria [66,67].

In addition to the cost and output yield limitations, there are operational challenges, which require consideration of the substrate characteristics, operating conditions and long-term durability. Many studies have been conducted on investigating and optimizing the operating parameters, such as temperature [68], pH [69,70], organic loading rate [71], substrate salinity [72], conductivity [73], start-up [74] and hydraulic retention time [75]. However, parametric and optimization studies usually target certain substrate or substrate types. Therefore, there is still a need to conduct parametric and optimization studies on a case-by-case basis. High salt content in wastewater might cause severe inorganic fouling [31] due to blockage of the precipitates which are predominantly calcium (89%) and magnesium (7%) [76,77]. Therefore, long-term durability studies are required, especially regarding the possible biofouling, clogging and corrosion in the scale-up systems [20,30,78].

In view of the above challenges, a flow chart is presented in Figure 6 to provide a framework for ameliorating the current limitations faced in scaling up MFCs.

![Flow chart for MFC scale-up studies](image-url)
Depending upon the application purpose, and the type and characteristics of the substrate, small-scale MFCs (or electrode modules) can be designed by considering and justifying the types and designs of electrodes, membranes and the system architecture (type, shape, size, spacings, number of electrodes and materials). Hybrid or coupled systems are also a potential area to improve the degradable potential of the substrate [79]. The MFC design is then incorporated into the stacking circuitry design stage to obtain the optimized number of MFC units, stacks and circuit connections, and to incorporate a (super)capacitor/batteries, a converter/harvester and a maximum power point tracker. In order to achieve maximum possible energy recovery, substrate degradation and Coulombic efficiency, optimizations of the operational parameters are essential, as these parameters are closely related to the MFC and circuitry designs. These parameters include altering substrate characteristics (to improve the conductivity of the anolyte), inoculation methods (to improve the start-up time required), mode of operation, pH, temperature, hydraulic retention time and organic loading. Analyses and assessments, including cost, microbial, life cycle or energy sustainability, could greatly aid the feasibility study of the scale-up MFC, prior to the prototyping, field test and commissioning.

4. Conclusions

Microbial fuel cell systems have shown promising performances at a large scale, particularly in the areas of bioenergy generation from wastewater treatment and off-grid power sources. However, this is just the beginning of microbial fuel cell commercialization. There are various challenges involved in scaling up prior to commercialization. This paper reviewed the MFC scale-up research work in the last five years, and based on the trend observed, proposed a framework outlining the areas for current and future studies. Submergible and stackable MFCs or electrode modules are the potential area for further studies and development. Utilizing membrane-less systems or low-cost membranes further lowers the cost of MFCs.

There are vast future opportunities for the widespread application of MFC technology. The most profound application would be in wastewater treatment. Submergible and stackable MFCs can be integrated into any treatment tank of a wastewater treatment plant to further degrade the remaining organic matters and produce additional energy for plant operation. MFCs are also suitable to be coupled with an existing wastewater treatment unit, for instance, an anaerobic digester or primary clarifier, to reduce the effluent to well below the discharge standard while extracting additional power. MFCs can generate not only bioenergy, but also hydrogen when supplied with an external voltage. Another application of MFC technology which is rising in demand is the in situ bioremediation, utilizing sediment or Benthic MFCs. These MFCs can remediate sediments for organic matter removal or nutrient recovery while producing off-grid energy. Last but not least, MFCs are also widely studied as remote sensors for organic pollutants, metals, toxicity, etc.

For the realization of MFC technology, MFC unit/module design, stacking circuitry design, operational parameter optimization, cost analysis, microbial analysis, life cycle assessment and energy sustainability are the important research areas which require cross-disciplinary collaborations, from engineers/scientists (chemical, process, electrical, mechanical, environmental, civil and computer science), to microbiologists, technicians, governmental bodies and business investors.

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