Static behaviour of natural gas and its flow in pipes

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Abstract

A general differential equation that governs static and flow behavior of a compressible fluid in horizontal, uphill and downhill inclined pipes is developed. The equation is developed by the combination of Euler equation for the steady flow of any fluid, the Darcy–Weisbach formula for lost head during fluid flow in pipes, the equation of continuity and the Colebrook friction factor equation. The classical fourth order Runge-Kutta numerical algorithm is used to solve to the new differential equation. The numerical algorithm is first programmed and applied to a problem of uphill gas flow in a vertical well. The program calculates the flowing bottom hole pressure as 2544.8 psia while the Cullender and Smith method obtains 2544 psia for the 5700 ft (above perforations) deep well. Next, the Runge-Kutta solution is transformed to a formula that is suitable for hand calculation of the static or flowing bottom hole pressure of a gas well. The new formula gives close result to that from the computer program, in the case of a flowing gas well. In the static case, the new formula predicts a bottom hole pressure of 2640 psia for the 5790 ft (including perforations) deep well. Ikoku average temperature and deviation factor method obtains 2639 psia while the Cullender and Smith method obtains 2641 psia for the same well. The Runge-Kutta algorithm is also used to provide a formula for the direct calculation of the pressure drop during downhill gas flow in a pipe. Comparison of results from the formula with values from a fluid mechanics text book confirmed its accuracy. The direct computation formulas of this work are faster and less tedious than the current methods. They also permit large temperature gradients just as the Cullender and Smith method. Finally, the direct pressure transverse formulas developed in this work are combined with the Reynolds number and the Colebrook friction factor equation to provide formulas for the direct calculation of the gas volumetric rate.

Introduction

The main tasks that face Engineers and Scientists that deal with fluid behavior in pipes can be divided into two broad categories – the computation of flow rate and prediction of pressure at some section of the pipe. Whether in computation of flow rate, or in pressure transverse, the method employed is to solve the energy equation (Bernoulli equation for...
liquid and Euler equation for compressible fluid), simultaneously with the equation of lost head during fluid flow, the Colebrook (1938) friction factor equation for fluid flow in pipes and the equation of continuity (conservation of mass / weight). For the case of a gas the equation of state for gases is also included to account for the variation of gas volume with pressure and temperature.

In the first part of this work, the Euler equation for the steady flow of any fluid in a pipe/conduit is combined with the Darcy – Weisbach equation for the lost head during fluid flow in pipes and the Colebrook friction factor equation. The combination yields a general differential equation applicable to any compressible fluid; in a static column, or flowing through a pipe. The pipe may be horizontal, inclined uphill or down hill.

The accuracy of the differential equation was ascertained by applying it to a problem of uphill gas flow in a vertical well. The problem came from the book of Ikoku (1984), “Natural Gas Production Engineering”. The classical fourth order Runge-Kutta method was first of all programmed in FORTRAN to solve the differential equation. By use of the average temperature and gas deviation factor method, Ikoku obtained the flowing bottom hole pressure (P_w_f) as 2543 psia for the 5700 ft well. The Cullender and Smith (1956) method that allows wide variation of temperature gave a P_w_f of 2544 psia. The computer program obtaines the flowing bottom hole pressure (P_w_f) as 2544.8 psia. Ouyang and Aziz (1996) developed another average temperature and deviation method for the calculation of flow rate and pressure transverse in gas wells. The average temperature and gas deviation formulas cannot be used directly to obtain pressure transverse in gas wells. The Cullender and Smith method involves numerical integration and is long and tedious to use.

The next thing in this work was to use the Runge-Kutta method to generate formulas suitable for the direct calculation of the pressure transverse in a static gas column, and in uphill and downhill dipping pipes. The accuracy of the formula is tested by application to two problems from the book of Ikoku. The first problem was prediction of static bottom hole pressure (P_w_s). The new formula gives a P_w_s of 2640 psia for the 5790ft deep gas well. Ikoku average pressure and gas deviation factor method gives the P_w_s as 2639 psia, while the Cullender and Smith method gives the P_w_s as 2641 psia. The second problem involves the calculation of flowing bottom hole pressure (P_w_f). The new formula gives the P_w_f as 2545 psia while the average temperature and gas deviation factor of Ikoku gives the P_w_f as 2543 psia. The Cullender and Smith method obtains a P_w_f of 2544 psia. The downhill formula was first tested by its application to a slight modification of a problem from the book of Giles et al.(2009). There was a close agreement between exit pressure calculated by the formula and that from the text book. The formula is also used to calculate bottom hole pressure in a gas injection well.

The direct pressure transverse formulas developed in this work are also combined with the Reynolds number and the Colebrook friction factor equation to provide formulas for the direct calculation of the gas volumetric rate in uphill and down hill dipping pipes.
A differential equation for static behaviour of a compressible fluid and its flow in pipes

The Euler equation is generally accepted for the flow of a compressible fluid in a pipe. The equation from Giles et al. (2009) is:

\[ \frac{dp}{\gamma} + \frac{vdv}{g} \pm d\ell \sin \theta + dh_l = 0 \] \hspace{1cm} (1)

In equation (1), the plus sign (+) before \( d\ell \sin \theta \) corresponds to the upward direction of the positive \( z \) coordinate and the minus sign (-) to the downward direction of the positive \( z \) coordinate.

The generally accepted equation for the loss of head in a pipe transporting a fluid is that of Darcy-Weisbach. The equation is:

\[ H_L = \frac{fL v^2}{2gd} \] \hspace{1cm} (2)

The equation of continuity for compressible flow in a pipe is:

\[ W = A \gamma v \] \hspace{1cm} (3)

Taking the first derivation of equation (3) and solving simultaneously with equation (1) and (2) we have after some simplifications,

\[ \frac{dp}{d\ell} = - \left[ \frac{f W^2}{2\gamma A^2 d\gamma} \mp \gamma \sin \theta \right] \] \hspace{1cm} (4)

All equations used to derive equation (4) are generally accepted equations. No limiting assumptions were made during the combination of these equations. Thus, equation (4) is a general differential equation that governs static behavior compressible fluid flow in a pipe. The compressible fluid can be a liquid of constant compressibility, gas or combination of gas and liquid (multiphase flow).

By noting that the compressibility of a fluid \((C_f)\) is:

\[ C_f = \frac{1}{\gamma} \frac{d\gamma}{dp} \] \hspace{1cm} (5)

Equation (4) can be written as:
Equation (6) can be simplified further for a gas. Multiply through equation (6) by \( \gamma \), then

\[
\gamma \frac{dp}{d\ell} = -\left[ \frac{fW^2}{2A^2dg} - \gamma^2 \sin \theta \gamma \sin \theta \right] \left[ 1 - \frac{W^2C_f}{\gamma A^2g} \right]
\]  
(7)

The equation of state for a non-ideal gas can be written as

\[
\gamma = \frac{pm}{zRT}
\]  
(8)

Substitution of equation (8) into equation (7) and using the fact that

\[
\frac{dp}{d\ell} = \frac{1}{2} \frac{dp}{d\ell}^2, \text{ gives}
\]

\[
\frac{dp}{d\ell}^2 = -\left[ \frac{fW^2zRT}{A^2Mg} - \frac{2p^2M \sin \theta}{zRT} \right] \left[ 1 - \frac{W^2zR \gamma C_f}{MA^2g \gamma p} \right]
\]  
(9)

The cross-sectional area (A) of a pipe is

\[
A^2 = \left( \frac{\pi d^2}{4} \right)^2 = \frac{\pi^2 d^4}{16}
\]  
(10)

Then equation (9) becomes:
\[
\frac{dp^2}{d\ell} = -\left[ \frac{1.621139fW^2 zRT}{d^5 M g} \frac{2 M \sin \theta P^2}{zRT} \right] - \left[ 1 - \frac{1.621139W^2 zRTC_f}{M g d^4 p} \right].
\]  

(11)

The denominator of equation (11) accounts for the effect of the change in kinetic energy during fluid flow in pipes. The kinetic effect is small and can be neglected as pointed out by previous researchers such as Ikoku (1984) and Uoyang and Aziz(1996). Where the kinetic effect is to be evaluated, the compressibility of the gas (C_f) can be calculated as follows:

For an ideal gas such as air,
\[ C_f = \frac{1}{p}. \]

For a non ideal gas, \( C_f = \frac{1}{p} - \frac{1}{z} \frac{\partial z}{\partial p} \).

Matter et al. (1975) and Ohirhian (2008) have proposed equations for the calculation of the compressibility of hydrocarbon gases. For a sweet natural gas (natural gas that contains CO_2 as major contaminant), Ohirhian (2008) has expressed the compressibility of the real gas (C_i) as:

\[ C_i = \frac{K}{p} \]

For Nigerian (sweet) natural gas K = 1.0328 when p is in psia

The denominator of equation (11) can then be written as

\[ 1 - \frac{KW^2 zRT}{M g d^4 P^2} \], where K = constant.

Then equation (11) can be written as

\[
\frac{dy}{d\ell} = \frac{(A \pm By)}{(1 - \frac{G}{y})}
\]

(12)

where

\[ y = p^2, \quad A = \frac{1.621139fW^2 zRT}{gd^5 M}, \quad B = \frac{2M \sin \theta}{zRT}, \quad G = \frac{KW^2 zRT}{gMd^4}. \]

The plus (+) sign in numerator of equation (12) is used for compressible uphill flow and the negative sign (-) is used for the compressible downhill flow. In both cases the z coordinate is taken positive upward. In equation (12) the pressure drop is \( \sqrt{y_1 - y_2} \), with \( y_1 > y_2 \) and incremental length is \( l_2 - l_1 \). Flow occurs from point (1) to point (2). Uphill flow of gas occurs in gas transmission lines and flow from the foot of a gas well to the surface. The pressure at
the surface is usually known. Downhill flow of gas occurs in gas injection wells and gas transmission lines. We shall illustrate the solution to the compressible flow equation by taking a problem involving an uphill flow of gas in a vertical gas well.

**Computation of the variables in the gas differential equation**

We need to discuss the computation of the variables that occur in the differential equation for gas before finding a suitable solution to it. The gas deviation factor \( z \) can be obtained from the chart of Standing and Katz (1942). The Standing and Katz chart has been curve fitted by many researchers. The version that was used in this section of the work that of Gopal (1977). The dimensionless friction factor in the compressible flow equation is a function of relative roughness \( \frac{\varepsilon}{d} \) and the Reynolds number \( R_N \). The Reynolds number is defined as:

\[
R_N = \frac{\rho v_d}{\mu} = \frac{W_d}{A_g \mu} \quad (13)
\]

The Reynolds number can also be written in terms of the gas volumetric flow rate. Then

\[
W = \gamma_b Q_b
\]

Since the specific weight at base condition is:

\[
\gamma_b = \frac{p_b M}{z_b T_b R} = \frac{28.97 G_g p_b}{z_b T_b R} \quad (14)
\]

The Reynolds number can be written as:

\[
R_N = \frac{36.88575 G_g p_b Q_b}{R g d \mu_g z_b T_b} \quad (15)
\]

By use of a base pressure \( (p_b) = 14.7 \text{psia} \), base temperature \( (T_b) = 520^\circ R \) and \( R = 1545 \)

\[
R_N = \frac{20071 Q_b G_g}{\mu_g d} \quad (16)
\]

Where \( d \) is expressed in inches, \( Q_b = \text{MMSCF} / \text{Day} \) and \( \mu_g \) is in centipoises.

Ohirhian and Abu (2008) have presented a formula for the calculation of the viscosity of natural gas. The natural gas can contain impurities of \( \text{CO}_2 \) and \( \text{H}_2\text{S} \). The formula is:
The generally accepted equation for the calculation of the dimensionless friction factor \( f \) is that of Colebrook (1938). The equation is:

\[
\frac{1}{\sqrt{f}} = -2 \log \left( \frac{\epsilon}{3.7d} + \frac{2.51}{R_N \sqrt{f}} \right)
\]

The equation is non-linear and requires iterative solution. Several researchers have proposed equations for the direct calculation of \( f \). The equation used in this work is that proposed by Ohirhian (2005). The equation is

\[
f = \left[ -2 \log \left( a - 2b \log \left( a + bx_1 \right) \right) \right]^{-2}
\]

Where

\[
a = \frac{\epsilon}{3.7d}, \quad b = \frac{2.51}{R_N},
\]

\[
x_1 = -1.14 \log \left( \frac{\epsilon}{d} + 0.30558 \right) + 0.57 \log R_N \left( 0.01772 \log R_N + 1.0693 \right)
\]

After evaluating the variables in the gas differential equation, a suitable numerical scheme can be used to it.

**Solution to the gas differential equation for direct calculation of pressure transverse in static and uphill gas flow in pipes.**

The classical fourth order Range Kutta method that allows large increment in the independent variable when used to solve a differential equation is used in this work. The solution by use of the Runge-Kutta method allows direct calculation of pressure transverse. The Runge-Kutta approximate solution to the differential equation
\[
\frac{dy}{dx} = f(x, y) \quad \text{at} \quad x = x_n
\]  
(20)

given that \( y = y_o \) when \( x = x_o \) is

\[
y = y_o + \frac{1}{6}(k_1 + 2(k_2 + k_3) + k_4)
\]  
(21)

where

\[
k_1 = Hf(x_o, y_o)
\]

\[
k_2 = Hf(x + \frac{1}{2}H, y_o + \frac{1}{2}k_1)
\]

\[
k_3 = Hf(x_o + \frac{1}{2}H, y_o + \frac{1}{2}k_1)
\]

\[
k_4 = Hf(x_o + H, y + k_3)
\]

\[
H = \frac{x_n - x_o}{n}
\]

\( n \) = number of applications

The Runge-Kutta algorithm can obtain an accurate solution with a large value of \( H \). The Runge-Kutta Algorithm can solve equation (6) or (12). The test problem used in this work is from the book of Ikoku (1984), “Natural Gas Production Engineering”. Ikoku has solved this problem with some of the available methods in the literature.

**Example 1**

Calculate the sand face pressure (\( p_{wf} \)) of a flowing gas well from the following surface measurements.

Flow rate (\( Q \)) = 5.153 MMSCF / Day
Tubing internal diameter (\( d \)) = 1.9956in
Gas gravity (\( G_g \)) = 0.6
Depth = 5790ft (bottom of casing)

Temperature at foot of tubing (\( T_{wf} \)) = 160 °F
Surface temperature (\( T_{sf} \)) = 83 °F

Tubing head pressure (\( p_{tf} \)) = 2122 psia
Absolute roughness of tubing (\( \varepsilon \)) = 0.0006 in
Length of tubing (\( l \)) = 5700ft (well is vertical)

**Solution**

When length (\( l \)) is zero, \( p = 2122 \) psia
That is \( (x_o, y_o) = (0, 2122) \)
By use of 1 step Runge-Kutta.

\[
H = \frac{5700 - 0}{1} = 5700ft.
\]
The Runge-Kutta algorithm is programmed in Fortran 77 and used to solve this problem. The program is also used to study the size of depth(length) increment needed to obtain an accurate solution by use of the Runge-Kutta method. The first output shows result for one-step Runge-Kutta (Depth increment = 5700ft). The program obtains 2544.823 psia as the flowing bottom hole pressure \( P_{wf} \).

\[
\begin{align*}
\text{TUBING HEAD PRESSURE} & = 2122.0000000 \text{ PSIA} \\
\text{SURFACE TEMPERATURE} & = 543.0000000 \text{ DEGREE RANKINE} \\
\text{TEMPERATURE AT TOTAL DEPTH} & = 620.0000000 \text{ DEGREE RANKINE} \\
\text{GAS GRAVITY} & = 6.000000E-001 \\
\text{GAS FLOW RATE} & = 5.1530000 \text{ MMSCFD} \\
\text{DEPTH AT SURFACE} & = .0000000 \text{ FT} \\
\text{TOTAL DEPTH} & = 5700.0000000 \text{ FT} \\
\text{INTERNAL TUBING DIAMETER} & = 1.9956000 \text{ INCHES} \\
\text{ROUGHNESS OF TUBING} & = 6.000000E-004 \text{ INCHES} \\
\text{INCREMENTAL DEPTH} & = 5700.0000000 \text{ FT} \\
\text{PRESSURE PSIA} & \quad \text{DEPTH FT} \\
2122.000 & \quad 0.000 \\
2544.823 & \quad 5700.000
\end{align*}
\]

To check the accuracy of the Runge-Kutta algorithm for the depth increment of 5700 ft another run is made with a smaller length increment of 1000 ft. The output gives a \( P_{wf} \) of 2544.823 psia as it is with a depth increment of 5700 ft. This confirmes that the Runge-Kutta solution can be accurate for a length increment of 5700 ft.

\[
\begin{align*}
\text{TUBING HEAD PRESSURE} & = 2122.0000000 \text{ PSIA} \\
\text{SURFACE TEMPERATURE} & = 543.0000000 \text{ DEGREE RANKINE} \\
\text{TEMPERATURE AT TOTAL DEPTH} & = 620.0000000 \text{ DEGREE RANKINE} \\
\text{GAS GRAVITY} & = 6.000000E-001 \\
\text{GAS FLOW RATE} & = 5.1530000 \text{ MMSCFD} \\
\text{DEPTH AT SURFACE} & = .0000000 \text{ FT} \\
\text{TOTAL DEPTH} & = 5700.0000000 \text{ FT} \\
\text{INTERNAL TUBING DIAMETER} & = 1.9956000 \text{ INCHES} \\
\text{ROUGHNESS OF TUBING} & = 6.000000E-004 \text{ INCHES} \\
\text{INCREMENTAL DEPTH} & = 1000.0000000 \text{ FT} \\
\text{PRESSURE PSIA} & \quad \text{DEPTH FT} \\
2122.000 & \quad 0.000 \\
2206.614 & \quad 1140.000 \\
2291.203 & \quad 2280.000 \\
2375.767 & \quad 3420.000 \\
2460.306 & \quad 4560.000 \\
2544.823 & \quad 5700.000
\end{align*}
\]
In order to determine the maximum length of pipe (depth) for which the computed $P_w$ can be considered as accurate, the depth of the test well is arbitrarily increased to 10,000ft and the program run with one step (length increment = 10,000ft). The program produces the $P_w$ as 2861.060 psia.

Next the total depth of 10000ft is subdivided into ten steps (length increment = 1,000ft). The program gives the $P_w$ as 2861.057 psia for the length increment of 1000ft.

The computed values of $P_w$ for the depth increment of 10,000ft and 1000ft differ only in the third decimal place. This suggests that the depth increment for the Range-Kutta solution to the differential equation generated in this work could be a large as 10,000ft. By neglecting the denominator of equation (6) that accounts for the kinetic effect, the result can be compared with Ikoku's average temperature and gas deviation method that uses an average value of the gas deviation factor ($z$) and negligible kinetic effects. In the program $z$ is allowed to vary with pressure and temperature. The temperature in the program also varies with depth (length of tubing) as

$$T = GTG \times \text{current length} + T_{swf},$$

where,

$swf(T T)GTG \text{Total Depth} =

The program obtains the $P_w$ as 2544.737 psia when the kinetic effect is ignored. The output is as follows:

| PRESSURE PSIA | DEPTH FT |
|---------------|----------|
| 2122.000      | .000     |
| 2861.060      | 10000.000|

Comparing the $P_w$ of 2544.737 psia with the $P_w$ of 2544.823 psia when the kinetic effect is considered, the kinetic contribution to the pressure drop is $2544.823 \text{ psia} - 2544.737 \text{ psia} = 0.086 \text{ psia}$. The kinetic effect during calculation of pressure transverse in uphill dipping pipes is small and can be neglected as pointed out by previous researchers such as Ikoku (1984) and Uoyang and Aziz (1996). Ikoku obtained 2543 psia by use of the the average temperature and gas deviation method. The average temperature and gas deviation method goes through trial and error calculations in order to obtain an accurate solution. Ikoku also used the Cullendar and Smith method to solve the problem under consideration. The Cullendar and Smith method does not consider the kinetic effect but allows a wide variation of the temperature. The Cullendar and Smith method involves the use of Simpson rule to carry out an integration of a cumbersome function. The solution to the given problem by the Cullendar and Smith method is $P_w = 2544$ psia.

If we neglect the denominator of equation (12), then the differential equation for pressure transverse in a flowing gas well becomes

$$\frac{dP}{dz} = \frac{z}{T^2} \left( \frac{\alpha}{\beta} \right)$$

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The computed values of $P_{wf}$ for the depth increment of 10,000ft and 1000ft differ only in the third decimal place. This suggests that the depth increment for the Range-Kutta solution to the differential equation generated in this work could be as large as 10,000ft. By neglecting the denominator of equation (6) that accounts for the kinetic effect, the result can be compared with Ikoku’s average temperature and gas deviation method that uses an average value of the gas deviation factor ($z$) and negligible kinetic effects. In the program $z$ is allowed to vary with pressure and temperature. The temperature in the program also varies with depth (length of tubing) as

$$T = GTG \times \text{current length} + T_s f,$$

where, $GTG = \frac{(T_{wf} - T_{sf})}{\text{Total Depth}}$

The program obtains the $P_{wf}$ as 2544.737 psia when the kinetic effect is ignored. The output is as follows:

| TUBING HEAD PRESSURE | 2122.0000000 PSIA |
| SURFACE TEMPERATURE  | 543.0000000 DEGREE RANKINE |
| TEMPERATURE AT TOTAL DEPTH | 620.0000000 DEGREE RANKINE |
| GAS GRAVITY          | 6.000000E-001 |
| GAS FLOW RATE         | 5.1530000 MMSCFD |
| DEPTH AT SURFACE      | .0000000 FT |
| TOTALDEPTH            | 5700.0000000 FT |
| INTERNAL TUBING DIAMETER | 1.9956000 INCHES |
| ROUGHNESS OF TUBING   | 6.000000E-004 INCHES |
| INCREMENTALDEPTH      | 5700.0000000 FT |
| PRESSURE PSIA         | DEPTH FT |
| 2122.000             | .000 |
| 2544.737             | 5700.000 |

Comparing the $P_{wf}$ of 2544.737 psia with the $P_{wf}$ of 2544.823 psia when the kinetic effect is considered, the kinetic contribution to the pressure drop is 2544.823 psia - 2544.737 psia = 0.086 psia. The kinetic effect during calculation of pressure transverse in uphill dipping pipes is small and can be neglected as pointed out by previous researchers such as Ikoku (1984) and Uoyang and Aziz (1996)

Ikoku obtained 2543 psia by use of the the average temperature and gas deviation method. The average temperature and gas deviation method goes through trial and error calculations in order to obtain an accurate solution. Ikoku also used the Cullendar and Smith method to solve the problem under consideration. The Cullendar and Smith method does not consider the kinetic effect but allows a wide variation of the temperature. The Cullendar and Smith method involves the use of Simpson rule to carry out an integration of a cumbersome function. The solution to the given problem by the Cullendar and Smith method is $P_{wf} = 2544$ psia.

If we neglect the denominator of equation (12), then the differential equation for pressure transverse in a flowing gas well becomes
\[
\frac{dy}{dl} = A + By
\]

where

\[
A = \frac{1.621139fW^2zRT}{gd^5M}
\]

\[
B = \frac{2M \sin \theta}{zRT} = \frac{2 \times 28.79G_g \sin \theta}{RTz}
\]

The equation is valid in any consistent set of units. If we assume that the pressure and temperature in the tubing are held constant from the mid section of the pipe to the foot of the tubing, the Runge-Kutta method can be used to obtain the pressure transverse in the tubing as follows.

\[
\frac{dy}{d\ell} = \frac{46.9643686G_gQ_b^2fzRT + 59.940G_g \sin \theta y}{gd^5} + \frac{zRT}{1 - \frac{46.9643686KzG_gQ_b^2}{gRd^4} \left( \frac{p_b}{T_b} \right)^2 \left( \frac{T}{y} \right)}
\]

The weight flow rate \( W \) in equation (12) is related to \( Q_b \) (the volumetric rate measurement at a base pressure \( P_b \) and a base temperature \( T_b \)) in equation (25) by:

\[
W = \gamma_b Q_b
\]

Equation (25) is a general differential equation that governs pressure transverse in a gas pipe that conveys gas uphill. When the angle of inclination \( \theta \) is zero, \( \sin \theta \) is zero and the differential equation reduces to that of a static gas column. The differential equation (25) is valid in any consistent set of units. The constant \( K = 1.0328 \) for Nigerian Natural Gas when the unit of pressure is psia.

The classical 4th order Runge Kutta algorithm can be used to provide a formula that serves as a general solution to the differential equation (25). To achieve this, the temperature and gas deviation factors are held constant at some average value, starting from the mid section of the pipe to the inlet end of the pipe. The solution to equation (25) by the Runge Kutta algorithm can be written as:

\[
P_1 = \sqrt{P_2^2 + y}
\]

Where
\[ y = \frac{aa}{6} \left( 1 + x + 0.5x^2 + 0.36x^3 \right) + \frac{P_2^2}{6} \left( 4.96x + 1.48x^2 + 0.72x^3 \right) + \frac{u}{6} \left( 4.96 + 1.96x + 0.72x^2 \right) \]

\[ aa = \left( \frac{46.9643686G_gQ_b^2f_2z_2RT_2}{gd^5} + \frac{57.94G_g\sin\theta P_2^2}{z_2T_zR} \right) L \]

\[ u = \frac{46.9643686G_gQ_b^2f_2z_{av}T_{av}L}{gd^5} \]

\[ x = \frac{57.94G_g\sin\theta L}{z_{av}T_{av}R} \]

When \( Q_b = 0 \), equation (27) reduces to the formula for pressure transverse in a static gas column.

In equation (27), the component \( k_4 \) in the Runge Kutta method given by \( k_4 = H f(x_o + \Delta y, y + k_3) \) was given some weighting to compensate for the fact that the temperature and gas deviation factor vary between the mid section and the inlet end of the pipe.

Equation (27) can be converted to oil field units. In oil field units in which \( L \) is in feet, \( R = 1545 \), temperature is in °R, \( g = 32.2 \text{ ft/sec}^2 \), diameter (\( d \)) is in inches, pressure (\( p \)) is in pound per square inch (psia), flow rate (\( Q_b \)) is in MMSCF / Day, \( P_b = 14.7 \text{ psia} \) and \( T_b = 520 \text{ oR} \), the variables \( a, u \) and \( x \) that occur in equation (25) can be written as:

\[ u = \frac{25.130920G_gQ_b^2f_2z_{av}T_{av}L}{d^5} \]

\[ x = 0.03749 \times \frac{G_gL\sin\theta}{z_{av}T_{av}} \]

The following steps are taken in order to use equation (27) to solve a problem.

1. Evaluate the gas deviation factor at a given pressure and temperature. When equation (27) is used to calculate pressure transverse in a gas well, the given pressure and temperature are the surface temperature and gas exit pressure (tubing head pressure).
2. Evaluate the viscosity of the gas at surface condition. This step is only necessary when calculating pressure transverse in a flowing gas well. It is omitted when static pressure transverse is calculated.
3. Evaluate the Reynolds number and dimensionless friction factor by use of surface properties. This step is also omitted when considering a static gas column.
4. Evaluate the coefficient \( a \) in the formula. This coefficient depends only on surface properties.
5. Evaluate the average pressure \( (p_{av}) \) and average temperature \( (T_{av}) \).

6. Evaluate the average gas deviation factor \( (z_{av}) \).

7. Evaluate the coefficients \( x \) and \( u \) in the formula. Note that \( u = 0 \) when \( Q_b = 0 \).

8. Evaluate \( y \) in the formula.

9. Evaluate the pressure \( p_1 \). In a flowing gas well, \( p_1 \) is the flowing bottom hole pressure. In a static column, it is the static bottom hole pressure.

Equation (27) is tested by using it to solve two problems from the book of Ikoku (1984), “Natural Gas Production Engineering”. The first problem involves calculation of the static bottom hole in a gas well. The second involves the calculation of the flowing bottom hole pressure of a gas well.

**Example 2**

Calculate the static bottom hole pressure of a gas well having a depth of 5790 ft. The gas gravity is 0.6 and the pressure at the well head is 2300 psia. The surface temperature is 83°F and the average flowing temperature is 117°F.

**Solution**

Following the steps that were listed for the solution to a problem by use of equation (27) we have:

1. Evaluation of \( z \) – factor.
   
   The standing equation for \( P_c \) and \( T_c \) are:
   
   \[
   P_c \text{(psia)} = 677.0 + 15.0 \, G_g - 37.5 \, G_g^2
   \]
   
   \[
   T_c \text{(°R)} = 168.0 + 325.0 \, G_g - 12.5 \, G_g^2
   \]

   Substitution of \( G_g = 0.6 \) gives, \( P_c = 672.5 \) psia and \( T_c = 358.5 \)°R. Then \( P_r = 2300/672.5 = 3.42 \) and \( T_r = 543/358.5 = 1.52 \).

   The Standing and Katz chart gives \( z_2 = 0.78 \).

   Steps 2 and 3 omitted in the static case.

4. \[
aa = \left( \frac{25.13092 \, G_g \, Q_b^2 \, f \, z_2 \, T_2}{d^5} + \frac{0.037417 \, G_g \, P_2^2 \, \sin \theta}{z_2 \, T_2} \right) \, L
\]

   Here, \( G_g = 0.6, Q_b = 0.0, \, z_2 = 0.78, \, d = 1.9956 \) inches, \( P_2 = 2300 \) psia,

   \[
   T_2 = 543 \circ \text{R and L} = 5700 \text{ ft. Well is vertical, } \theta = 90 \circ, \, \sin \theta = 1. \text{ Substitution of the given values gives:}
   \]
   
   \[
   aa = 0.0374917 \times 0.6 \times 2300^2 \times 5790 / (0.78 \times 543) = 1626696
   \]

5. \[
   p_{av} = \sqrt{2300^2 + 0.5 \times 1626696} = 2470.5 \text{ psia}
   \]

   Reduced \( p_{av} = 2470.5 / 672.5 = 3.68 \)

   \[
   T_{av} = 117 \circ \text{F} = 577 \circ \text{R}
   \]
5. Evaluate the average pressure \( p_{av} \) and average temperature \( T_{av} \).

6. Evaluate the average gas deviation factor \( z_{av} \).

7. Evaluate the coefficients \( x \) and \( u \) in the formula. Note that \( u = 0 \) when \( Q_b = 0 \).

8. Evaluate \( y \) in the formula.

9. Evaluate the pressure \( p_1 \). In a flowing gas well, \( p_1 \) is the flowing bottom hole pressure. In a static column, it is the static bottom hole pressure.

Equation (27) is tested by using it to solve two problems from the book of Ikoku (1984), “Natural Gas Production Engineering”. The first problem involves calculation of the static bottom hole in a gas well. The second involves the calculation of the flowing bottom hole pressure of a gas well.

Example 2
Calculate the static bottom hole pressure of a gas well having a depth of 5790 ft. The gas gravity is 0.6 and the pressure at the well head is 2300 psia. The surface temperature is 83°F and the average flowing temperature is 117°F.

Solution
Following the steps that were listed for the solution to a problem by use of equation (27) we have:

1. Evaluation of \( z \) – factor.

   The standing equation for \( P_c \) and \( T_c \) are:
   \[
   P_c (\text{psia}) = 677.0 + 15.0 G_g - 37.5 G_g^2
   \]
   \[
   T_c (\text{oR}) = 168.0 + 325.0 G_g - 12.5 G_g^2
   \]

   Substitution of \( G_g = 0.6 \) gives, \( P_c = 672.5 \text{ psia} \) and \( T_c = 358.5 \text{ oR} \). Then \( P_r = 2300 / 672.5 = 3.42 \) and \( T_r = 543 / 358.5 = 1.52 \).

   The Standing and Katz chart gives \( z_{2} = 0.78 \).

   Steps 2 and 3 omitted in the static case.

2. Evaluation of \( y \) in the formula.

   Here, \( G_g = 0.6, Q_b = 0, z_{2} = 0.78, d = 1.9956 \text{ inches}, p_2 = 2300 \text{ psia}, T_2 = 543 \text{ oR} \) and \( L = 5700 \text{ ft} \). Well is vertical, \( \theta = 90^\circ \), \( \sin \theta = 1 \). Substitution of the given values gives:

   \[
   a = 0.0374917 \times 0.6 \times 2300 \times 5790 / (0.78 \times 543) = 1626696
   \]

   \[
   p_{av} = 2300 \times 0.5 \times 1626696 = 2470.5 \text{ psia}
   \]

   Reduced \( p_{av} = 2470.5 / 672.5 = 3.68 \)

   \[
   T_{av} = 117 \text{ oF} = 577 \text{ oR}
   \]

   Reduced \( T_{av} = 577 / 358.5 = 1.61 \)

   From the standing and Katz chart, \( z_{av} = 0.816 \).

   In the static case \( u = 0 \), so we only evaluate \( x \)

   \[
   x = \frac{0.0374917 \times 0.6 \times 5790 \times \sin 90^\circ}{0.816 \times 577} = 0.2766
   \]

8. \[
\bar{y} = \frac{aa}{6} \left( 1 + x + 0.5x^2 + 0.36x^3 \right) + \frac{P_2^2}{6} \left( 4.96x + 1.48x^2 + 0.72x^3 \right)
\]

   Substitution of \( a = 1626696, x = 0.2766 \) and \( P_2 = 2300 \) gives

   \[
   \bar{y} = 358543 + 1322856 = 1681399
   \]

9. \[
p_1 = \sqrt{p_2^2 + \bar{y}} = \left( 2300^2 + 1681399 \right)^{0.5} = 2640.34 \text{ psia} = 2640 \text{ psia}
\]

Ikoku used 3 methods to work this problem. His answers of the static bottom hole pressure are:

- Average temperature and deviation factor = 2639 psia
- Sukkar and Cornell method = 2634 psia
- Cullender and Smith method = 2641 psia

The direct calculation formula of this work is faster.

Example 3
Use equation (27) to solve the problem of example 1 that was previously solved by computer programming.

Solution
1. Obtain the gas deviation factor at the surface. From example 2, the pseudocritical properties for a 0.6 gravity gas are, \( P_c = 672.5 \text{ psia} \) and \( T_c = 358.5 \text{ oR} \), then

   \[
P_r = 2122 / 672.5 = 3.16
   \]

   \[
T_r = 543 / 358.5 = 1.52
   \]

   From the Standing and Katz chart, \( z_2 = 0.78 \).

2. Obtain, the viscosity of the gas at surface condition. By use of Ohirhian and Abu equation,

   \[
\mu_g = \frac{0.0059723 p}{z \left( 16.393443 - \frac{T}{p} \right)}
   \]

   Then

   \[
\mu_g = \frac{0.0109388 - 0.008823 (0.9985) - 0.0075720 (0.9985)^2}{1.0 - 1.3633077 (0.9985) - 0.0461989 (0.9985)^2} = 0.0133 \text{ cp}
   \]

3. Evaluation of the Reynolds number and dimensionless friction factor

   \[
R_N \frac{20071 Q_b G_g}{\mu g d} = \frac{20071 \times 5.153 \times 0.6}{0.0133 \times 1.9956} = 2.34 \times 10^6
   \]
The dimensionless friction factor by Ohirhian formula is

\[ f = \left[ -2 \log \left( a - 2b \log (a + bx_1) \right) \right]^{-2} \]

Where

\[ a = \varepsilon / 3.7d, \quad b = 2.51 / R_N, \]

\[ x_1 = -1.14 \log \left( \frac{\varepsilon}{d} + 0.30558 \right) + 0.57 \log R_N \left( 0.01772 \log R_N + 1.0693 \right) \]

Substitute of \( \varepsilon = 0.0006, \quad d = 1.9956, \quad R_N = 2.34 \times 10^6 \) gives \( f = 0.01527 \)

4. Evaluate the coefficient \( a_a \) in the formula. This coefficient depends only on surface properties.

\[ a_a = \left( \frac{25.13092 G \_g Q \_b^2 f z_2 T_2 + 0.037417 G \_g z_2 T_2 \sin \theta}{d^3} \right) L \]

Here, \( G \_g = 0.6, \quad Q \_b = 5.153 \text{ MMSCF/Day}, \quad f = 0.01527, \quad z_2 = 0.78, \quad d = 1.9956 \text{ inches}, \quad p_2 = 2122 \text{ psia}, \quad T_2 = 543 \text{o R}, \quad z = 5700 \text{ ft} \)

Substitution of the given values gives;

\[ a_a = (81.817446 + 239.14594) \times 5700 = 1829491 \]

5. Evaluate \( p \_a \_v \)

\[ p \_a \_v = \sqrt{p_2^2 + 0.5a_a} = \sqrt{2122^2 + 0.5 \times 1829491} = 2327.6 \text{ psia} \]

6. Evaluation of average gas deviation factor.

Reduced average pressure = \( p \_a \_v / p \_c = 2327.6 / 672.5 = 3.46 \)

\( T \_a \_v = T_2 + \alpha L / 2 \)

Where \( \alpha \) is the geothermal gradient.

\[ \alpha = (T_1 - T_2) / L = (620 - 543) / 5700 = 0.01351 \]

T \_a \_v at the mid section of the pipe is 2850 ft. Then, T \_a \_v = 543 + 0.01351 \times 2850 = 581.5 \text{o R} \)

Reduced T \_a \_v = 581.5 / 358.5 = 1.62

Standing and Katz chart gives \( z \_a \_v = 0.822 \)

7. Evaluation of the coefficients x and u

\[ x = \frac{0.0374917 G \_g L}{z \_a \_v T \_a \_v} = \frac{0.0374919 \times 0.6 \times 5700}{0.822 \times 581.5} = 0.26824 \]

\[ u = \frac{25.13092 G \_g Q \_b^2 f z \_a \_v T \_a \_v L}{d^3} = \frac{25.13092 \times 0.6 \times 5.153^2 \times 0.01527 \times 0.822 \times 581.5 \times 5700}{1.9956^3} = 526662 \]
8. Evaluate \( \overline{y} \)

\[
\overline{y} = \frac{aa}{6} \left( 1 + x + 0.5x^2 + 0.36x^3 \right) + \frac{p_2^2}{6} \left( 4.96x + 1.48x^2 + 0.72x^3 \right) + \frac{u}{6} \left( 4.96 + 1.96 + 0.72x^2 \right)
\]

Where \( u = 526662, x = 0.26824, p_2 = 2122 \) psia and \( aa = 1829491 \). Then,

\[
\overline{y} = 399794 + 1088840 + 485752 = 1974386 \text{ psia}^2
\]

9. Evaluate \( p_1 \) (the flowing bottom hole pressure)

\[
p_1 = \sqrt{p_2 + \overline{y}}
= \sqrt{2122^2 + 1974386} = 2545.05 \text{ psia}
\approx 2545 \text{ psia}
\]

The computer program obtains, the flowing bottom hole pressure as 2544.823 psia. For comparison with other methods of solution, the flowing bottom hole pressure by:

- Average Temperature and Deviation Factor, \( P_1 = 2543 \) psia
- Cullender and Smith, \( P_1 = 2544 \)

The direct calculating formula of this work is faster. The Cullendar and Smith method is even more cumbersome than that of Ikoku. It involves the use of special tables and charts (Ikoku, 1984) page 338 - 344.

The differential equation for static gas behaviour and its downhill flow in pipes

The problem of calculating pressure transverse during downhill gas flow in pipes is encountered in the transportation of gas to the market and in gas injection operations. In the literature, models for pressure prediction during downhill gas flow are rare and in many instances the same equations for uphill flow are used for downhill flow.

In this section, we present the use of the Runge-Kutta solution to the downhill gas flow differential equation.

During downhill gas flow in pipes, the negative sign in the numerator of differential equation (12) is used. The differential equation also breaks down to a simple differential equation for pressure transverse in static columns when the flow rate is zero. The equation to be solved is:

\[
\frac{dy}{d\ell} = \frac{(A-By)}{(1-\frac{G}{y})} \tag{28}
\]

Where \( y = p^2 \),

\[
A = \frac{1.621139 f W^2 zRT}{gd^3 M}, \quad B = \frac{2M \sin \theta}{zRT}, \quad G = \frac{KW^2 zRT}{gMd^4}
\]

Also, the molecular weight (M) of a gas, can be expressed as \( M = 28.97Gg \).
Then, the differential equation (28) can be written as:

\[
\frac{dp}{dt} = \left[ \frac{0.0559592 \, f \, z \, R \, W \, q^2}{g \, d \, ^5 \, G \, g} - \frac{59.940 \, G \, g \, \sin \, \theta \, p^2}{z \, R \, T} \right] \left[ 1 - \frac{0.0559592 \, z \, R \, T \, W \, q^2}{g \, d \, ^5 \, G \, g \, p^2} \right]
\]  

(29)

The differential equation (29) is valid in any consistent set of units. The relationship between weight flow rate (W) and the volumetric flow rate measured at a base condition of pressure and temperature (Q_b) is;

\[ W = \gamma_b \, Q_b \]  

(30)

The specific weight at base condition is:

\[ \gamma_b = \frac{p_b \, M}{z_b \, T_b \, R} = \frac{28.97 \, G \, g \, p_b}{z_b \, T_b \, R} \]  

(31)

Substitution of equations (30) and (31) into differential equation (29) gives:

\[
\frac{dp}{dl} = \left[ \frac{46.9583259 \, f \, z \, T \, G \, g \, p_b^2 \, Q_b^2}{g \, d \, ^5 \, Z_b \, T_b \, R} - \frac{59.940 \, G \, g \, \sin \, \theta \, p^2}{z \, R \, T} \right] \left[ 1 - \frac{46.95832593 \, G \, g \, Q_b^2 \, K}{g \, R \, d \, ^4} \left( \frac{p_b^2}{T_b} \right) \left( \frac{T}{p^2} \right) \right]
\]  

(32)

The differential equation (32) is also valid in any consistent set of units.

**Solution to the differential equation for downhill flow**

In order to find a solution to the differential equation for downhill flow (as presented in equation (29) and (32)) we need equations or charts that can provide values of the variables z and f. The widely accepted chart for the values of the gas deviation factor (z) is that of Standing and Katz (1942). The chart has been curve fitted by some researchers. The version used in this section is that of Ohirhian (1993). The Ohirhian set of equations are able to read the chart within ± 0.777% error. The Standing and Katz charts require reduced pressure (Pr) and reduced temperature (T r). The Pr is defined as \( Pr = P_c / P_c \) and the T r is defined as \( T_r = T / T_c \); where P_c and T_c are pseudo critical pressure and pseudo critical temperature, respectively.

Standing (1977) has presented equations for P_c and T_c as functions of gas gravity (G g). The equations are:

\[ P_c = 677 + 15.0 \, G \, g - 37.5 \, G \, g^2 \]  

(33)

\[ T_c = 168 + 325 \, G \, g - 12.5 \, G \, g^2 \]  

(34)
The differential equation for the downhill gas flow can also be solved by the classical fourth order Runge-Kutta method.

The downhill flow differential equation was tested by reversing the direction of flow in the problem solved in example 3.

**Example 4**

Calculate the sand face pressure ($p_{wf}$) of an injection gas well from the following surface measurements.

- Flow rate ($Q$) = 5.153 MMSCF / Day
- Tubing internal diameter ($d$) = 1.9956 in
- Gas gravity ($G_g$) = 0.6
- Depth = 5790ft (bottom of casing)
- Temperature at foot of tubing ($T_{wf}$) = 160°F
- Surface temperature ($T_{sf}$) = 83°F
- Tubing head pressure ($P_{sf}'$) = 2545 psia
- Absolute roughness of tubing ($\varepsilon$) = 0.0006in
- Length of tubing ($L$) = 5700ft (well is vertical)

**Solution**

Here, $(x_0, y_0) = (0, 2545)$

By use of 1 step Runge-Kutta.

$$H = \frac{(5700 - 0)}{1} = 5700$$

The Runge-Kutta algorithm is programmed in Fortran 77 to solve this problem. The output is as follows.

- **Tubing Head Pressure** = 2545.0000000 PSIA
- **Surface Temperature** = 543.0000000 DEGREE RANKINE
- **Temperature at Total Depth** = 620.0000000 DEGREE RANKINE
- **GAS GRAVITY** = 6.000000E-001
- **GAS FLOW RATE** = 5.1530000 MMSCFD
- **Depth at Surface** = 0.0000000 FT
- **Total Depth** = 5700.0000000 FT
- **Internal Tubing Diameter** = 1.9956000 INCHES
- **Roughness of Tubing** = 6.0000000E-004 INCHES
- **Incremental Depth** = 5700.0000000 FT

| PRESSURE PSIA | DEPTH FT |
|--------------|----------|
| 2545.000     | .000     |
| 2327.930     | 5700.000 |

The other outputs from the program (not shown here) indicates that the contribution of kinetic effect to pressure transverse during downhill flow is also negligible. The program also shows that an incremental length as large as 5700 ft can yield accurate result in pressure transverse calculations.
Neglecting the kinetic effect, the Runge-Kutta algorithm can be used to provide a solution to the differential equation (32) as follows

\[ p_1 = \sqrt{p_2^2 - \overline{y}} \]  

(35)

Here

\[ \overline{y} = \frac{aa}{6} \left( 1 - x + 0.5x^2 + 0.3x^3 \right) + \frac{P_1^2}{6} \left( -5.2x + 2.2x^2 - 0.6x^3 \right) + \frac{u}{6} \left( 5.2 - 2.2x + 0.6x^2 \right) \]

\[ aa = \left( \frac{46.958326 f_1 z_1 T_1 G_g P_b^2 Q_b^2}{gd^5 z_b^2 T_b^2 R} - \frac{57.940 G_g \sin \theta p_1^2}{z_1 T_1 R} \right) L \]

\[ u = \frac{46.958326 f_1 z_{av} T_{av} G_g P_b^2 Q_b^2 L}{gd^5 z_b^2 T_b^2 R}, \quad x = \frac{57.940 G_g \sin \theta L}{z_{av} T_{av} R} \]

\[ f_1 = \text{Moody friction factor evaluated at inlet end pipe} \]
\[ T_1 = \text{Temperature at inlet end of pipe} \]
\[ p_1 = \text{Pressure at inlet end of pipe} \]
\[ z_1 = \text{Gas deviation factor evaluated with } p_1 \text{ and } T_1 \]
\[ z_{av} = \text{Gas deviation factor calculated with temperature at mid section (} T_{av} \text{) and pressure at the mid section of pipe (} p_{av} \text{) given by } p_{av} = \sqrt{p_1^2 - 0.5|aa|} \]
\[ p_2 = \text{Pressure at exit end of pipe, psia} \]
\[ p_1 = \text{Pressure at inlet end of pipe} \]
\[ \text{Note that } p_1 > p_2 \text{ and flows occurs from point (1) to point (2)} \]

Equation (35) is valid in any consistent set of units.

Equation (35) can be converted to oil field units. In oil field units in which L is in feet, R = 1545, temperature(T) is in °R, g = 32.2 ft/sec\(^2\), diameter (d) is in inches, pressure (p) is in pound per square inch (psia), flow rate (Q_b) is in MMSCF / Day and P_b = 14.7 psia, T_b = 520° R. The variables aa, u and x that occur in equation (35) can be written as:

\[ aa = \left( \frac{25.1472069 G_g f_1 z_1 T_1 Q_b^2}{d^5} - \frac{0.0375016 G_g \sin \theta p_1^2}{z_1 T_1} \right) L \]

\[ u = \frac{25.1472069 G_g f_1 z_{av} T_{av} Q_b^2 L}{d^5}, \quad x = \frac{0.0375016 G_g \sin \theta L}{z_{av} T_{av}} \]
Example 5
Use equation (35) to solve the problem of example 4

Solution
Step 1: obtain the gas deviation factor at the inlet end

\[ T_1 = 83^\circ F = 543^\circ R \]
\[ P_1 = 2545 \text{ psia} \]
\[ G_g = 0.6 \]

By use of equation (33) and (34)

\[ P_c (\text{psia}) = 677 + 15 \times 0.6 - 37.5 \times 0.6^2 = 672.5 \text{ psia} \]
\[ T_c (^\circ R) = 168 + 325 \times 0.6 - 12.5 \times 0.6^2 = 358.5 ^\circ R \]

Then, \[ P_{1r} = 2545/672.5 = 3.784, T_{1r} = 543/358.5 = 1.515 \]
The required Ohirhian equation is

\[ z = \left( z_1 + (1.39022 + Pr(0.06202 - 0.02113 \times Pr)) \times \log Tr \right) F_c \]

Where

\[ z_1 = 0.60163 + Pr(-0.06533 + 0.0133Pr) \]
\[ F_c = 20.208372 + Tr(-44.0548 + Tr(37.55915 + Tr(-14.105177 + 1.9688Tr))) \]

Substitution of values of \( Pr = 3.784 \) and \( Tr = 1.515 \) gives \( z = 0.780588 \)

Step 2
Evaluate the viscosity of the gas at inlet condition. By use of Ohirhian and Abu formula (equation 17)

\[ \mu_g = \frac{0.0059723 \times 2545}{0.780588(16.393443 - 543/2545)} = 0.015045 \text{ cp} \]

Step 3
Evaluation of Reynolds number \( (R_N) \) and dimensionless friction factor \((f)\). From eqn. (26)

\[ R_N = \frac{20071 \times 5.153 \times 0.6}{0.015045 \times 1.9956} = 2066877 \]

The dimensionless friction factor can be explicitly evaluated by use of Ohirhian formula (equation 19)

\[ \epsilon / d = 0.0006 / 1.9956 = 3.066146E - 4 \]
\[ a = 3.066146E - 4 / 3.7 = 8.125985E - 5 \]
\[ b = 2.51/2066877 = 1.21393E - 6 \]
\[ x_1 = -1.14 \log(3.066146E - 4 + 0.30558) + 0.57 \times \log 2066877 (0.01772 \log 2066877 + 1.0693) \]
\[ = 4.838498 \]

Substitution of values of \( a, b \) and \( x_1 \) into \( f = \left[ -2 \log(a - 2b \log(a + bh)) \right]^{-2} \) gives

\( f = 0.01765 \)
Step 4
Evaluate the coefficient $aa$ in the formula. This coefficient depends only on surface (inlet) properties. Note that the pipe is vertical $\theta = 90^\circ$ and $\sin 90^\circ = 1$

$$aa = \left(25.147207 \times 0.6 \times 0.017650 \times 0.780588 \times 543 \times 5.153^2 \times 5700\right)/1.9956^5$$

$$= -\left(0.037502 \times 0.6 \times 1 \times 2545 \times 5700\right)/(0.780588 \times 543)$$

$$= 539803 - 1959902 = -1420099$$

Step 5
Evaluate the average pressure ($p_{av}$) at the mid section of the pipe given by

$$p_{av} = \sqrt{p_1^2 - 0.5|aa|} = \sqrt{2545^2 - 0.5 \times 1420099} = 2401.5$$

Step 6:
Evaluate the average gas deviation factor ($z_{av}$). Reduced average pressure ($p_{avr}$) = 2401.5/672.5 = 3.571. $T_{av} = T_1 + \alpha L/2$ where $\alpha =$ geothermal gradient given by:

$$\alpha = (T_2 - T_1)/L = (620 - 543)/5700 = 0.013509$$

$T_{av}$ at mid section of pipe (2850 ft) then, is:

$$T_{av} = 543 + 0.013509 \times 2850 = 581.5^\circ R$$

Reduced $T_{av} = 581.5/358.5 = 1.622$

Substitution into the Ohirhian equation used in step 1, gives $z = 0.821102$

Step 7:
Evaluate the coefficients $x$ and $u$

$$x = \frac{0.0375016 \times 0.6 \times 1 \times 5700}{0.821102 \times 581.5} = 0.268614$$

$$u = \left(25.147207 \times 0.6 \times 0.017650 \times 0.821102 \times 581.5 \times 5.153^2 \times 5700\right)/1.9956^5 = 608079$$

Step 8: Evaluate $\bar{y}$

$$\bar{y} = \frac{u}{6} \left(5.2 - 2.2x + 0.6x^2\right) + \frac{p_1^2}{6} \left(-5.2x + 2.2x^2 - 0.6x^3\right) + \frac{aa}{6} \left(1 - x + 0.5x^2 - 0.3x^3\right)$$

Substitution of $u = 608079, p_1 = 2545$ psia, $aa = -1420099$ and $x = 0.268614$ gives

$$\bar{y} = 471499 - 1349039 - 180269 = -1057809$$

Step 9: Evaluate $p_2$, the pressure at the exit end of the pipe

$$p_2 = \sqrt{2545^2 - 1057809} = 2327.92 \text{ psia} \approx 2328 \text{ psia}$$

Pressure drop across 5700 ft of tubing is 2545 psia – 2328 psia = 217 psia
This pressure drop may be compared with the pressure drop across the 5700 ft of tubing when gas flows uphill against the force of gravity. From example 3, tubing pressure at the surface = 2122 psia when the bottom hole pressure (inlet pressure) = 2545 psia. Then pressure drop = 2545 psia - 2122 psia = 423 psia. The pressure drop during down hill flow is less than that during up hill flow.

The general solution (valid in any system of units) to the differential equation for downhill flow was tested with slight modification of a problem from the book of Giles et al (2009). In the original problem the pipe was horizontal. In the modification used in this work, the pipe
was made to incline at 10 degrees from the horizontal in the downhill direction. Other data remained as they were in the book of Giles et al. The data are as follows:

**Example 6**

Given the following data,

Length of pipe (L) = 1800ft

\[ Z_2 = Z_1 = Z_{av} = 1 \] (air is flowing fluid)

\[ p_1 = 49.5 \text{ psia} = 49.5 \times 144 \text{ psf} = 7128 \text{ psf} \]

\[ W = 0.75 \text{ lb/sec} \]

\[ Q_b = 9.81937 \text{ ft}^3/\text{sec} \]

\[ P_b = 14.7 \text{ psia} = 2116.8 \text{ psf} \]

\[ T_b = 60 \degree F = 520 \degree R \]

\[ T_1 = T_{av} = 90 \degree F = 550 \degree R \]

\[ G = 1.0 \text{ (air)} \]

\[ R = 1544 \]

\[ \mu = 390 \times 10^{-9} \text{ lb sec/ft}^2 \]

\[ d = 4 \text{ inch} = 0.33333 \text{ ft} \]

Absolute Roughness (\( \varepsilon \)) = 0.0003 ft

calculate the exit pressure \( (p_2) \) at 1800 ft of pipe.

**Solution**

Step 1: Obtain the gas elevation factor at inlet end, \( z_1 = 1.0 \), air in flowing fluid

Step 2: Obtain the viscosity of the gas at inlet condition. Viscosity of gas is \( 390 \times 10^{-9} \text{ lb sec/ft}^2 \) (given)

Step 3: Evaluate the Reynolds number and friction factor.

\[
R_N = \frac{36.88575 G_g P_b Q_b b}{g R d \mu z_b T_b} 
\]

Here,

\[ G_g = 1.0 \text{ (air)} \], \[ P_b = 2116.8 \text{ psf}, \] \[ Q_b = 9.81937 \text{ ft}^3/\text{sec}, \]

\[ g = 32.2 \text{ ft/sec}^2, \] \[ d = 0.33333 \text{ ft}, \]

\[ R = 1544, \mu = 390 \times 10^{-9}, \] \[ z_b = 1.0 \text{ (air)}, T_b = 520 \degree R \]

Then

\[
R_N = \frac{36.88575 \times 1 \times 2116.8 \times 9.81937 \times 10^9}{32.2 \times 1544 \times 0.33333 \times 390 \times 1 \times 520} = 2281249
\]

\[
\varepsilon = \frac{0.0003}{0.33333} = 0.0009
\]

From Moody chart, \( f_1 = 0.0205 \)

Step 4: Evaluate the coefficient \( a_a \) in the formula

\[
a_a = \left( \frac{46.958326 f_1 z_1 T_1 G_g P_b^2 Q_b^2}{g d^5 z_b^2 T_b^2 R} - \frac{57.940 G_g \sin \theta_1 P_b^2}{z_1 T_1 R} \right) L
\]

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\[
\frac{46.958326 \times 0.0205 \times 1 \times 550 \times 1 \times 2116.8^2 \times 9.81937^2}{32.2 \times 0.33333^5 \times 520^2 \times 1544} = 4134.70
\]

\[
\frac{57.94 \times 1 \times 0.173648 \times 7128^2}{1 \times 550 \times 1544} = \frac{511191540.9}{849200} = 601.97
\]

Then \( aa = (4134.70 - 601.97) \times 1800 = 6358914 \)

Step 5
Evaluate the average pressure \( (p_{av}) \) at the mid section of the pipe
\[
p_{av} = \sqrt{p_1^2 - 0.5 \times 6358914} = 6901.4 \text{ psf}
\]

Step 6: Evaluate average gas derivation factor \( (z_{av}) \) for air, \( z_{av} = 1.0 \)

Step 7: Evaluate the coefficients \( x \) and \( u \)
\[
x = \frac{57.94 G_g \sin \theta L}{z_{av} T_{av} R} = \frac{57.94 \times 1 \times 0.173648 \times 1800}{1 \times 550 \times 1544} = 0.021326
\]
\[
u = \frac{46.958326 f_z \lambda_{av} G_g \rho_b^2 Q_b^2 L}{gd^5 z_{av} T_{av} R}
\]
\[
= \frac{46.958326 \times 0.0205 \times 1 \times 550 \times 1 \times 2116.8^2 \times 9.81937^2 \times 1800}{32.2 \times 0.33333^5 \times 1 \times 520^2 \times 1544} = 7442642.4
\]

Step 8: Evaluate \( y \)
\[
- \frac{y}{6} = \left( \frac{5.2 - 2.2x + 0.6x^2}{6} \right) + \frac{p_1^2}{6} \left( -5.2x + 2.2x^2 - 0.6x^3 \right) + \frac{aa}{6} \left( 1 - x + 0.5x^2 - 0.3x^3 \right)
\]

Where \( x = 0.021326, (5.2 - 2.2x + 0.6x^2) = 5.153356, (-5.2x + 2.2x^2 - 0.6x^3) = -0.10990 \)
\( (1 - x + 0.5x^2 - 0.3x^3) = 0.9789 \).

Then, \[
- \frac{y}{6} = \frac{7442642.4}{6} \times \frac{5.153356}{6} + \frac{7128^2}{8} (-0.1099) + \frac{6358914}{6} (0.9789)
\]
\[
= \frac{6392431}{6} - \frac{930644}{6} + \frac{1037457}{6} = 6499244
\]

Step 9: Evaluate \( p_2 \), the pressure at the exit end of the pipe
\[
p_2 = \sqrt{7128^2 - 6499244} = 6656.5 \text{ psf} = \frac{6656.5 \text{ psia}}{144} = 46.2 \text{ psia}
\]

Pressure drop = 49.5 psia - 46.2 psia = 3.3 psia

When the pipe is horizontal, \( p_2 \) (from Fluid Mechanics and Hydraulics) is 45.7 psia. Then, pressure drop = 49.5 psia - 45.7 psia = 3.8 psia
Direct calculation of the gas volumetric rate

The rate of gas flow through a pipe can be calculated if the pipe properties, the gas properties, the inlet and outlet pressures are known. The gas volumetric rate is obtained by solving an equation of pressure transverse simultaneously with the Reynolds number and the Colebrook friction factor equation.

Direct calculation of the gas rate in uphill pipes

Ohirhian (2002) combined the Weymouth equation with the Reynolds number and the Colebrook friction factor equation to arrive at an equation for the direct calculation of the gas volumetric rate during uphill gas flow. In this section, the formula type solution to the differential equation for horizontal and uphill gas flow is combined with the Reynolds number and the Colebrook equation to arrive at another equation for calculating the gas volumetric rate during uphill gas flow.

Combination of the pressure transverse formula for uphill gas flow (equation (27) in oil field units, with the Reynolds number, equation (16) and equation (18) which is the Colebrook friction factor equation, leads to:

\[
\frac{1}{\sqrt{f}} = -2 \log \left( \frac{\varepsilon}{3.7 d} + \frac{2.51}{\alpha} \right) \quad \ldots (36)
\]

\[
R_N = -2 \alpha \log \left( \frac{\varepsilon}{3.7 d} + \frac{2.51}{\alpha} \right) \quad (37)
\]

\[
Q_B = \frac{-\mu_2 d R_N}{20071 G_g} = \frac{-2 \mu_2 d \alpha}{20071 G_g} \log \left( \frac{\varepsilon}{3.7 d} + \frac{2.51}{\alpha} \right) \quad (38)
\]

\[
\frac{20071 G_g}{\alpha} \left[ \frac{p_1^2}{2} - \frac{p_2^2}{2} \left( 1 + \frac{x b}{6} \right) - \frac{1}{6} \left( S L x_a \right) \right]^{0.5}
\]

\[
\frac{\mu_2 d \sqrt{B \left[ z_{av} T_2 x_a + z_{av} T_{av} x_c \right]}}{0.5}
\]

Where,

\[
x = \frac{0.0375016 G g \sin \theta L}{z_{av} T_{av}}
\]

\[
B = \frac{4.191201 G g L}{d^5}
\]

\[
S = \frac{0.03075016 G g \sin \theta p^2}{z_2 T_2}
\]

\[z_{av} \text{ is computed with } T_{av} = 0.5(T_1 + T_2) \text{ and } p_{av}^2 = 0.5(p_1^2 + p_2^2).\]

\[\mu_2 \text{ is viscosity of gas at } p_2 \text{ and } T_2. \text{ The subscript } 2 \text{ refers to surface condition.}\]
\[ x_a = 1 + x + 0.5x^2 + 0.36x^3 \]
\[ x_b = 4.96x + 1.48x^2 + 0.72x^3 \]
\[ x_c = 4.96 + 1.96x + 0.72x^2 \]

The above equations are in oil field units in which \( d \) is expressed in inches, \( L \) in feet, \( \mu \) in centipoises, \( T \) in degrees rankine and pressure in pounds per square inches. In this system of units, \( p_b = 14.7 \) psia, \( T_b = 520^\circ R \), \( z_b = 1.0 \). The subscript 2 refers to surface condition in the gas well.

**Example 7**

A gas well has the following data:
\( L = 5700 \) ft, \( G_g = 0.6 \), \( \theta = 90^\circ \), \( Z_2 = 0.78 \), \( Z_{av} = 0.821 \), \( f = 0.0176 \), \( T_2 = 543^\circ R \), \( T_{av} = 581.5^\circ R \), \( d = 1.9956 \) in, absolute roughness of pipe = 0.0006 in., \( p_1 = 2545 \) psia, \( p_2 = 2122 \) psia, \( \mu_2 \), viscosity of gas at \( p_2 \) and \( T_2 = 0.0133 \) cp. Calculate the flow rate of the well (\( Q_b \)) in MM SCF / Day.

**Solution**

Substituting given values,
\[ x = 0.0375016 \times \frac{0.6 \times 1 \times 5700}{0.822 \times 581.5} = 0.268250 \]
\[ B = 4.191201 \times \frac{0.6 \times 5700}{1.9956^5} = 452.6012689 \]
\[ S = 0.0375016 \times \frac{0.6 \times 1 \times 2122^2}{0.78 \times 543} = 238.680281 \]
\[ x_a = 1 + x + 0.5x^2 + 0.36x^3 = 1 + 0.268250 + 0.5 \times 0.268250^2 + 0.36 \times 0.268250^3 \]
\[ = 1.311178 \]
\[ x_b = 4.96x + 1.48x^2 + 0.72x^3 = 4.96 \times 0.268250 + 1.48 \times 0.268250^2 + 0.72 \times 0.268250^3 \]
\[ = 1.45096 \]
\[ x_c = 4.96 + 1.96x + 0.72x^2 = 4.96 + 1.96 \times 0.268250 + 0.72 \times 0.268250^2 = 5.53758 \]
\[ \alpha = \frac{20071 \times 0.6 \left[ 2545^2 - 2122^2 \left( 1 + \frac{1.45096}{6} \right) - \frac{1}{6} \left( 238.680281 \times 5700 \times 1.311178 \right) \right]^{0.5}}{0.0133 \times 1.9956 \sqrt{452.6012689 \left[ 1.45096 \times 0.78 \times 543 + 0.822 \times 581.5 \times 5.53758 \right]^{0.5}}} \]
\[ = 288996.2 \]
From example 3, actual Reynolds number is 2.34E06 and \( f = 0.01527 \). Then,

\[
\alpha = R_N \sqrt{f} = 234000 \times \sqrt{0.01527} = 289158.1
\]

\[
Q_b = -\frac{2 \mu}{20071 \frac{G}{g}} \frac{d \alpha}{\alpha_1} \log \left( \frac{\epsilon}{3.7 \frac{d}{G}} + \frac{2.51}{\alpha_1} \right) \ldots \quad \ldots (39)
\]

\[
R_N = -2 \alpha_1 \log \left( \frac{\epsilon}{3.7 \frac{d}{G}} + \frac{2.51}{\alpha_1} \right) \ldots \quad \ldots (40)
\]

\[
Q_b = -\frac{\mu_{av}}{20071 \frac{G}{g}} \frac{d \alpha}{\alpha_1} \log \left( \frac{\epsilon}{3.7 \frac{d}{G}} + \frac{2.51}{\alpha_1} \right) \quad \ldots (40)
\]

\[
\alpha_1 = \frac{20071 \frac{G}{g}}{\mu_1 \frac{d}{B} \sqrt{z_i T_i x_d + z_{av} T_{av} x_f}}^{0.5}
\]

\[
J = p_2^2 - p_1^2 \left( 1 - \frac{x_e}{6} \right), \quad \text{if } B \geq S \quad (42a)
\]

\[
J = p_1^2 \left( 1 - \frac{x_e}{6} \right) - p_2^2, \quad \text{if } B < S \quad (42b)
\]

\[
x_d = 1 - x + 0.5x^2 + 0.3x^3
\]

\[
x_e = -5.2x + 2.2x^2 - 0.6x^3
\]

\[
x_f = 5.2 - 2.2x + 0.6x^2
\]

\[
B = \frac{4.191201 \frac{G}{g} L}{d^5}
\]
\[ S = \frac{0.03075016 G g \sin \theta \cdot p_1^2}{z_1 T_1} \]
\[ x = \frac{0.0375016 G g \sin \theta \cdot L}{z_{av} T_{av}} \]

\[ z_{av} \] and \[ \mu_{av} \] are evaluated with \( T_{av} = 0.5(T_1 + T_2) \) and \( p_{av} = \frac{2p_1 p_2}{p_1 + p_2} \)

The subscript 1 refers to surface condition and 2 to exit condition in the gas injection well. The above equations are in oil field units in which \( d \) is expressed in inches, \( L \) in feet, \( \mu \) in centipoises, \( T \) in degrees Rankine and pressure in pounds per square inches. In this system of units, \( p_b = 14.7 \) psia, \( T_b = 520 \) R, \( z_b = 1.0 \). The subscript 2 refers to surface condition in the gas well.

**Example 8**

A gas injection well has the following data:

- \( L = 5700 \) ft
- \( G_g = 0.6 \)
- \( \theta = 90^\circ \)
- \( \sin 90^\circ = 1 \)
- \( z_1 = 0.78059 \)
- \( z_{av} = 0.821 \)
- \( T_1 = 543^\circ \) R
- \( \frac{T_{av}}{T_{av}} = 543^\circ \) R
- \( d = 1.9956 \) in
- \( p_1 = 2545 \) psia
- \( p_2 = 2327.92 \) psia
- Absolute roughness of tubing \( (\epsilon) = 0.0006 \) in.

Calculate the gas injection rate in MMSCF / Day. Take the viscosity of the at surface condition \( (\mu_1) \) as 0.015045 cp and the average viscosity of the gas \( (\mu_{av}) \) as 0.0142 cp.

**Solution**

\[ x = 0.0375016 \times \frac{0.6 \times 1 \times 5700}{0.821 \times 581.5} = 0.26865 \]
\[ B = 4.191201 \times \frac{0.6 \times 5700}{1.9956} = 452.89458 \]
\[ S = 0.0375016 \times \frac{0.6 \times 2545^2}{0.78059 \times 543} = 343.83795 \]
\[ x_d = 1 - x + 0.5x^2 + 0.3x^3 = 1 - 0.26865 + 0.5 \times 0.26865^2 + 0.36 \times 0.26865^3 \]
\[ = 0.76162 \]
\[ x_e = -5.2x + 2.2x^2 - 0.6x^3 \]
\[ = -5.2 \times 0.26865 + 2.2 \times 0.26865^2 - 0.6 \times 0.26865^3 \]
\[ = -1.24982 \]
\[ x_f = 5.2 - 2.2x + 0.6x^2 = 5.2 - 2.2 \times 0.26865 + 0.6 \times 0.26865^2 = 4.65228 \]
Static behaviour of natural gas and its flow in pipes

\[ J = 2327.92^2 - 2545^2 \left( 1 - \frac{1.24982}{6} \right) = 291372.42 \]

\[ \frac{1}{6} (S Lx_d) = \frac{1}{6} (343.83795 \times 5700 \times 0.76162) = 248780.17 \]

\[ \left[ z_1 T_1 \ x_d + z_\text{av} \ T_\text{av} \ x_f \right]^{0.5} = (0.78 \times 543 \times 0.76162 + 0.821 \times 581.5 \times 4.65228)^{0.5} = 50.43440 \]

\[ \alpha = \frac{20071 \ G_g \left[ J + \frac{1}{6} (S Lx_d) \right]^{0.5}}{\mu_1 \ d \ \sqrt{B} \left[ z_1 T_1 \ x_d + z_\text{av} \ T_\text{av} \ x_f \right]^{0.5}} = \frac{20071 \times 0.6 \ [291372.42 + 248780.17]^{0.5}}{0.015045 \times 1.9956 \times \sqrt{452.89458 \times 50.43440}} = 274641.7 \]

From example 5, actual Reynolds number is 2066877 and \( f = 0.01765 \). Then,

\[ \alpha = \frac{R_N \sqrt{f}}{20071 \ G_g} = \frac{2066877 \times \sqrt{0.01765}}{274591.4} = 5.227 \text{ MMSCF / Day} \]

By use of an average viscosity of 0.0140 cp, the calculated \( Q_b = 5.153 \text{ MMSCF / Day} \). Taking 0.014 cp as the accurate value of the average gas viscosity, the absolute error in estimated average viscosity is \((0.0002 / 0.014 = 1.43 \%) \). The equation for the gas volumetric rate is very sensitive to values of the average gas viscosity. Accurate values of the average gas viscosity should be used in the direct calculation of the gas volumetric rate.

Conclusions

1. A general differential equation that governs static behavior of any fluid and its flow in horizontal, uphill and downhill pipes has been developed.
2. Classical fourth order Runge-Kutta numerical method is programmed in Fortran 77, to test the equation and results are accurate. The program shows that a length increment as large as 10,000 ft can be used in the Runge-Kutta method of solution to differential equation during uphill gas flow and up to 5700 ft for downhill gas flow.
3. The Runge-Kutta method was used to generate a formulas suitable to the direct calculation of pressure transverse in static gas pipes and pipes that transport gas uphill or downhill. The formulas yield very close results to other tedious methods available in the literature.
4. The direct pressure transverse formulas developed are suitable for wells and pipelines with large temperature gradients.
5. Contribution of kinetic effect to pressure transverse in pipes that transport gas is small and can be neglected.
6. The pressure transverse formulas developed in this work are combined with the Reynolds number and Colebrook friction factor equation to provide accurate formulas for the direct calculation of the gas volumetric rate. The direct calculating formulas are applicable to gas flow in uphill and downhill pipes.

Nomenclature

\( p \) = Pressure
\( \gamma \) = Specific weight of flowing fluid
\( v \) = Average fluid velocity
\( g \) = Acceleration due to gravity in a consistent set of units.
\( d \) = Change in length of pipe
\( \theta \) = Angle of pipe inclination with the horizontal, degrees
\( dh_1 \) = Incremental pressure head loss
\( f \) = Dimensionless friction factor
\( L \) = Length of pipe
\( d \) = Internal diameter of pipe
\( W \) = Weight flow rate of fluid
\( C_f \) = Compressibility of a fluid
\( C_g \) = Compressibility of a gas
\( K \) = Constant for expressing the compressibility of a gas
\( M \) = Molecular weight of gas
\( T \) = Temperature
\( R_N \) = Reynolds number
\( \rho \) = Mass density of a fluid
\( \mu \) = Absolute viscosity of a fluid
\( z \) = Gas deviation factor
\( \gamma_{b} \) = Specific weight of the gas at \( p_b \) and \( T_b \)
\( p_b \) = Base pressure, absolute unit
\( T_b \) = Base temperature, absolute unit
\( z_b \) = Gas deviation at \( p_b \) and \( T_b \) usually taken as 1
\( G_g \) = Specific gravity of gas (air = 1) at standard condition
\( \mu_g \) = Absolute viscosity of a gas
\( \varepsilon \) = Absolute roughness of tubing
\( \text{GTG} \) = Geothermal gradient
\( f_2 \) = Moody friction factor evaluated at outlet end of pipe.
4. The direct pressure transverse formulas developed are suitable for wells and pipelines with large temperature gradients.

5. Contribution of kinetic effect to pressure transverse in pipes that transport gas is small and can be neglected.

6. The pressure transverse formulas developed in this work are combined with the Reynolds number and Colebrook friction factor equation to provide accurate formulas for the direct calculation of the gas volumetric rate. The direct calculating formulas are applicable to gas flow in uphill and downhill pipes.

Nomenclature

- $p_2$ = Pressure at exit end of pipe.
- $p_1$ = Pressure at inlet end of pipe $p_1 > p_2$
- $T_2$ = Temperature at exit end of pipe
- $T_1$ = Temperature at inlet end of pipe
- $T_{av} = 0.5(T_1 + T_2)$
- $z_{av} = \text{Gas deviation factor evaluated with } T_{av} \text{ and average pressure } (p_{av}) \text{ given by}$
- $p_{av} = \sqrt{p_1^2 - 0.5|a_a|}$ in downhill flow

SI Metric Conversion Factors

\[
\begin{align*}
(\degree F - 32) / 18 & = \degree C \\
ft \times 3.048000 \times 10^{-1} & = m \\
m \times 2.540 \times 10^0 & = cm \\
lbf \times 4.448222 \times 10^0 & = N \\
lbm \times 4.535924 \times 10^{-1} & = kg \\
psi \times 6.894757 \times 10^0 & = Pa \\
\text{lb sec / ft}^2 \times 4.788026 \times 10^0 & = Pa.s \\
\text{cp} \times 1.0 \times 10^{-3} & = Pas \\
\text{foot}^3 / \text{second (ft}^3 / \text{sec}) \times 2.831685 \times 10^{-2} & = \text{metre}^3 / \text{sec (m}^3 / \text{s}) \\
\text{foot}^3 / \text{second x 8.64 \times 10^{-2}} & = \text{MMSCF / Day} \\
\text{MMSCF / Day x 1.157407 \times 10^1} & = \text{foot}^3 / \text{second (ft}^3 / \text{sec}) \\
\text{MMSCF / Day x 3.2774132E + 01} & = \text{metre}^3 / \text{sec (m}^3 / \text{s}) \\
\text{MMSCF / Day} = 4.166667E + 04 \text{ ft}^3 / \text{hr} \\
\text{ft}^3 / \text{hr} = 7.865792E - 06 \text{m}^3 / \text{s} \\
\end{align*}
\]

* Conversion factor is exact.

References

1. Colebrook, C.F.J. (1938), Inst. Civil Engineers, 11, p 133
2. Cullender, M.H. and R.V. Smith (1956). “Practical solution of gas flow equations for wells and pipelines with large temperature gradients”. Transactions, AIME 207, pp 281-89.
3. Giles, R.V., Cheng, L. and Evert, J (2009). Schaum’s Outline Series of Fluid Mechanics and Hydraulics, McGraw Hill Book Company, New York.
4. Gopal, V.N. (1977), “Gas Z-factor Equations Developed for Computer”, Oil and Gas Journal, pp 58 - 60.
5. Ikoku, C.U. (1984), Natural Gas Production Engineering, John Wiley & Sons, New York, pp. 317 - 346
6. Matter, L.G.S. Brar, and K. Aziz (1975), Compressibility of Natural Gases”, Journal of Canadian Petroleum Technology”, pp. 77-80.
7. Ohirhian, P.U.(1993), “A set of Equations for Calculating the Gas Compressibility Factor” Paper SPE 27411, Richardson, Texas, U.S.A.
8. Ohirhian, P.U.: “Direct Calculation of the Gas Volumetric Rates”, PetEng. Calculators, Chemical Engineering Dept. Stanford University, California, U.S.A, 2002
9. Ohirhian, P.U. and I.N. Abu (2008), “A new Correlation for the Viscosity of Natural Gas” Paper SPE 106391 USMS, Richardson, Texas, U.S.A.
10. Ohirhian, P.U. (2005) “Explicit Presentation of Colebrook’s friction factor equation”. Journal of the Nigerian Association of Mathematical physics, Vol. 9, pp 325 – 330.
11. Ohirhian, P.U. (2008). “Equations for the z-factor and compressibility of Nigerian Natural gas”, Advances in Materials and Systems Technologies, Trans Tech Publications Ltd, Laubisrtistr. 24, Stafa – Zurich, Switzerland.
12. Ouyang, I and K. Aziz (1996) “Steady state Gas flow in Pipes”, Journal of Petroleum Science and Engineering, No. 14, pp. 137 – 158.
13. Standing, M.B., and D.L. Katz (1942) “Density of Natural Gases”, Trans AIME 146, pp. 140–9.
14. Standing, M.B. (1970), Volumetric and Phase Behavior of Oil Field Hydrocarbon Systems, La Habra, California.
The contributions in this book present an overview of cutting edge research on natural gas which is a vital component of the world’s supply of energy. Natural gas is a combustible mixture of hydrocarbon gases, primarily methane but also heavier gaseous hydrocarbons such as ethane, propane and butane. Unlike other fossil fuels, natural gas is clean burning and emits lower levels of potentially harmful by-products into the air. Therefore, it is considered as one of the cleanest, safest, and most useful of all energy sources applied in a variety of residential, commercial and industrial fields. The book is organized in 25 chapters that cover various aspects of natural gas research: technology, applications, forecasting, numerical simulations, transport and risk assessment.

How to reference
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Peter Ohirhian (2010). Static Behaviour of Natural Gas and its Flow in Pipes, Natural Gas, Primož Potočnik (Ed.), ISBN: 978-953-307-112-1, InTech, Available from: http://www.intechopen.com/books/natural-gas/static-behaviour-of-natural-gas-and-its-flow-in-pipes
