Mitigation of Torsional Vibrations in Drilling Systems using Adaptive Nonlinear Control System

S. Suba, M. Dineshkumar D. Eee.

Abstract: The reason for this work is to plan a robust yield feedback control way to deal with dispense with torque stick-slip vibrations in boring frameworks. Current industry controllers generally neglect to dispose of stick-slip vibrations, particularly when different torque flex modes assume a job in maniacal assault. In terms of build controller production, a real training-string system performs a multi-level model work such as torque mechanics. The proposed controller design is artfully distorted at optimizing the stability with respect to the uncertainty of the nonlinear bit-rock interaction. Based on heroes and intentions. Besides, a closed loop strength examination of the nonlinear preparing string model is displayed. This controller structure system offers a few points of interest contrasted with existing controllers. To begin with, just surface estimations are utilized, barring the requirement for entire estimations underneath it. Second, multi-level training-string dynamics are effectively handled in ways to access state-training controllers. Third, stability is explicitly provided with respect to bit-rock contact uncertainty and closed-loop performance specifications include controller design. The results of the study report confirm that stick-slip vibrations are actually eliminated in realistic drilling scenarios using a controller designed to achieve this state-of-control control.

Key words: stick-slip vibrations, bit-rock, drilling, torsional, adaptive nonlinear system

I. INTRODUCTION

The problem of vibration corrosion is seen in many branches of modern engineering. Vibrations under moving vehicles, as well as neighboring objects, which can damage the system of bridges and railway tracks. The robot has to operate at high speeds to enter and the accuracy of the videos intensifies. Machines such as lathe engines and grinders can cause vibrations induced by machine tools, reduce the shape of the product, and may damage the engine.

In the present paper, we demonstrate a novel adaptive optimal control scheme for time-varying mechanical vibrating systems. Akak model of the state concerned. The vibration degradation of a drilling system works by undergoing a change in the ground friction properties of the proposed project. A common resistance of land is considered by drilling friction drilling. It can be both a time and a gradual variable in softness and a sudden jump in properties. When it goes to a layer of training soil or rock or encounters solid contents it creates a barrier force that can suddenly change.

The voltage control function provided by the electric motor and when applied later, dominates the dynamic response in a nonlinear way. An example of such a system is a training string used for gas and oil drilling. The string has a low diameter-to-length ratio. Sticky phase and friction coefficient to reduce the instability of the system and the stick-slip flicker. Training may also impair self-induced resonance drilling. The result of friction measurements depends on the formation of the friction drilling depth, which depends on the rock formation.

II. RESEARCH BACKGROUND

Methods in many studies have been used to target torque stick-slip vibrations in excavation systems. Only torque mechanics [1-4] [5] [6] complement the experimental analysis. Many of these models of torque dynamics have been used to design control for the removal of stick-slip vibrations [7]. In such works, a (locally) kinetic-weakening effect that is usually caused by the bit-rock interaction on the opposing torque [8] is generally assumed by modeling a frictional interaction on stick-slip vibrations (digging system). In other words, this rate effect is considered an intrinsic property of the bit-rock interface. However, single cutters do not report any mechanism-weakening effect [9]; Tests using Bit-Rock Communication Law is aimed at identification. This discrepancy prompted a different approach, initiated in [10] where, in addition to the torque mechanics, axial dynamics include training-string modeling. The axial and torsional dynamics are coupled using a rate-independent bit-rock correlation law, developed in [11]. Analysis of this type of model with the demonstration that axial mechanics exhibits a stick-slip boundary rotation [12-15]. This axial boundary rotation creates torque on-bit and inherently an apparent kinetic-weakening effect leading to torsional vibrations. As a result, the ratio effect in the direction of torque is the result of the interaction between the axial and the property inherent in the structure of the bit-rock contact law instead of the torque dynamics.

Where infinite dimensional models, such as partial or delay microstructures, can be formalized, [18], - a different modeling approach is taken from [16] and [17]. Individualization comes with infinite-dimensional models [19-21]. A whole-parameter model based on finite-element representations of training-string dynamics, as a result; this approach is taken from this paper. In summary, we use a fast-rate-weakening bit-rock interaction law for training-string dynamics model involving a (multi-level) fem only torque dynamics to support the design art of a model-based controller.

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III. PROPOSED MITIGATION OF TORSIONAL VIBRATIONS

Questions have also been raised about the rapid wear of gears and bearings engines, such as nuts and bolts, and the ease of attachment such as reducing the dimensionality of an object and surface coating during metal cutting. Product engines can transmit vibration, noise problems and, through the support structures, transmit other functions, thereby reducing their performance. Vibratory transmission to humans can cause disorders and loss of performance. Vibrations can be transmitted through the support structures, thereby reducing their performance. Vibratory transmission to humans can cause disorders and loss of performance. Inaccuracies in power transmission lines and communication cables (e.g., telephone lines) can cause service interruptions and sometimes major structural damage. Vibrations thus are an important purpose. In engineering, mounting of the correct machinery should reduce the vibration with a well-balanced design. Proper design and control are critical to maintaining high performance and productivity and increasing the effective life expectancy of machinery, structures and business processes. The Block Diagram of proposed system is shown in Figure 1.

Figure 1. Block Diagram of Proposed System

3.1 Adaptive Neuro Sliding Mode Control algorithm (ANSMC)

The reverse deep learning technique has become the most well-known strategy for rail systems to shut down. It has used recognition training from virtual and organizing training at issue locations, including a few others. An organization of similar centers that appeared to have the proposed ANSMC architecture sorted out in layers

Figure 2. ANSMC structure

At least three layers of centers have a common ANSMC arrangement: an input layer that has external data sources, at least one hidden layer and a yield layer that produces grouping results. When the system rule information is displayed in the input layer, the system centers run the calculations in consecutive layers until a yield value can be acquired for each of the yield centers. This yielding input information can be proved by the appropriate class.

3.2 Training

The training process requires quantitative ordering of the correct organizational behavior facts that incorporate direct evidence of input and objective yield. In the midst of training, weights and prospects of the organization are balanced to improve organizational execution work and vice versa. Average Square Error Between Organization Yield and Actual Yield - Performance work per tool is the mean square error (MSE). There are five stages of the training process

Step 1: Provide more efficient training on preprocess data, preprocess information is useful before it grows. This way the data sources and the learning goals are proportional to ensure they are covered in a prior work.

Step 2: Launch weight values. Before planning a system, weights and options should be introduced. As a result, strategic distance is maintained in an established position region, with arbitrary weight qualities being chosen.

Step 3: Predict the hidden layer output and the layer (in backward spreading) errors.

Step 4: Adjust the weight values such that the error is indicated by the job until the error is executed. Weights settled on the path of preparation and can be used for practical calculation.

This parameter yields 0 and 1. The mean square error ($\delta_{\text{max}}$) is near. Setup Mistake is the setting where a particular error is underneath the edge. The range of squared errors of 0.001 is drawn. The ANSMC is ready for the relationship between massively inferred values and classifications regardless. Structural learning factors are regulated by the determination of some hidden layers and resulting in better organization of hidden layer neurons.

3.3 Evaluation Metrics

An ANSMC-based solution for creating PWM signs for angles is being developed. For this purpose, the optimization of the objective function is determined by fitting the multiple modulation code to the angles of the multiple modulation code and changing the angles of the optimal 11 transform angles. Root mean square error (RMSE), determination ($R^2$) and mean absolute error (MAE) coefficient have been used to evaluate ANSMC performance. The rules are:

$$RMSE = \sqrt{\frac{\sum_{i=1}^{n}(y_{\text{pre},i} - y_i)^2}{n}}$$

$$R^2 = 1 - \frac{\sum_{i=1}^{n}(y_{\text{pre},i} - y_i)^2}{\sum_{i=1}^{n}(y_{\text{mea},i})^2}$$

$$MAE = \frac{\sum_{i=1}^{n}(y_{\text{pre},i} - y_i)}{n}$$
The flowchart of proposed system is shown in Figure 3. Acceptability of the ANSMC structure is proportional to a smaller RMSE and MAE values and with an amount of $R^2$ closer to 1.

IV. SIMULATION RESULTS AND DISCUSSION

In this section discuss the simulation results and performance analysis of proposed mitigation of torsional vibrations in drilling systems using adaptive nonlinear control system

The simulation result and functional response of inner ring input signal is shown in Figure 4. The function of the ring is controlled using Adaptive Neuro Sliding Mode Control Method

The simulation result and functional response of frequency in inner ring is shown in Figure 5. The function of the ring is controlled using Adaptive Neuro Sliding Mode Control Method

The simulation result and functional response of noise in inner ring is shown in Figure 6. The function of the ring is controlled using Adaptive Neuro Sliding Mode Control Method

The simulation result and functional response of filtered signal in inner ring is shown in Figure 7. The function of the ring is controlled using Adaptive Neuro Sliding Mode Control Method.
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From a practical point of view, many aspects of stability have been explored. It has been proven that the operating envelope of the training string system increases in terms of angular velocity and the length of the training string. Another aspect to investigate is the stability of the uncertainty relative to the bit rock contact. Studies show that changing the bit rock contrast while simulating results can be effectively resolved by this controller. In summary, it asserts that the proposed effective address drilling conditions for the controller, and that it currently exceeds its use, based on the industrial controller, the stick-slip imbalance of its operating envelope is eliminated.

REFERENCES
1. A. Cunha, Jr., C. Soize, and R. Sampaio, “Exploring the nonlinear dynamics of horizontal drillstrings subjected to friction and shocks effects,” in Proc. 21st Congr. Numer. Methods Appl., McCom (ENIEF), Bariloche, Argentina, Sep. 2014, pp. 1–11.
2. Besselink, T. Vromen, N. Kremers, and N. van de Wouw, “Analysis and control of stick-slip oscillations in drilling systems,” IEEE Trans. Control Syst. Technol., vol. 24, no. 5, pp. 1582–1593, Sep. 2016.
3. Bresch-Pietri D, Krstic M. Adaptive output-feedback for wave PDE with anti-damping - application to surface-based control of oil drilling stick–slip instability. Proceedings of the 53rd IEEE Conference on Decision and Control, Los Angeles, California, U.S.A., 2014; 1295–1300.
4. D. J. Runia, S. Dwars, and I. P. J. M. Stulmeijer, “A brief history of the shell “soft torque rotary system” and some recent case studies,” in Proc. 2nd Int. Colloq. Nonlinear Dyn. Control Deep Drilling Syst., Eindhoven, The Netherlands, May 2012, pp. 69–76.
5. E. Fridman, S. Mondié, and B. Saídvar, “Bounds on the response of a drilling pipe model,” IMA J. Math. Control Inf., vol. 27, no. 4, pp. 513–526, 2010.
6. F. A. Serrarens, J. M. G. van de Molengraft, J. J. Kok, and L. van den Steen, “H∞ control for suppressing stick-slip in oil well drillstrings,” IEEE Control Syst., vol. 18, no. 2, pp. 19–30, Apr. 1998.
7. Germay, V. Denoël, and E. Drotournay, “Multiple mode analysis of the self-excited vibrations of rotary drilling systems,” J. Sound Vibrat., vol. 325, nos. 1–2, pp. 362–381, 2009.
8. J. C. A. de Bruin, A. Doris, N. van de Wouw, W. P. M. H. Heemels, and H. Nijmeijer, “Control of mechanical motion systems with noncollocation of actuation and friction: A Popov criterion approach for input-to-state stability and set-valued nonlinearities,” Automatica, vol. 45, no. 2, pp. 405–415, 2009.
9. J. D. Hansen and L. van den Steen, “Active damping of self-excited torsional vibrations in oil well drillstrings,” J. Sound Vibrat., vol. 179, no. 4, pp. 647–668, 1995.
10. J. D. Hansen, “Nonlinear dynamics of oilwell drillstrings,”Ph.D. dissertation, Dept. Mech. Maritime Mater. Eng., Delft Univ. Technol., Delft, The Netherlands, 1993.
11. K. Nandakumar and M. Wiercigroch, “Stability analysis of a state dependent delayed, coupled two DOF model of drill-string vibration,” J. Sound Vibrat., vol. 332, no. 10, pp. 2575–2592, 2013.
12. K. Vromen, N. Kremers, and N. van de Wouw, “Analysis and control of stick-slip oscillations in drilling systems,” Proc. 3rd Int. Colloq. Nonlinear Dyn. Control Deep Drilling Syst., Eindhoven, The Netherlands, May 2012, pp. 69–76.
13. Kreuzer E, Steidl M. Controlling torsional vibrations of drill strings via decomposition of traveling waves. Archive of Applied Mechanics 2012; 82(4):515–531. 25. Vromen TGM. Control of stick–slip vibrations in drilling systems. Ph.D. Thesis, 2015.

V. CONCLUSION

In this study, a novel synthesis strategy for targeted control is developed to minimize tensional stick-slip imbalances in excavation systems. Controller Design Distorted - μ DK Many gains of heroes and privileges are based on pre-existing control. First, the guarantee of the desired operating point (local) stability is designed to fit a multi-level training-string model. Secondly, the controller is optimized to have stability with respect to bit-rock contact uncertainty. Third, performance indicators for measuring noise sensitivity and driving range are integrated into the design of the controller. Fourth, measuring only the use of ground controllers is an important requirement from a practical standpoint. The industrial controller program has persisted to the point where the controller creates results with stick-slip imbalances-where the model of the 18-degree-of-freedom drill string with vibrations in actual drilling conditions shows eliminated slip.
structure,” J. Sound Vibrat., vol. 233, no. 2, pp. 235–254, 2000.
15. P. Christoforou and A. S. Yigit, “Fully coupled vibrations of activelycontrolled drillstrings,” J. Sound Vibrat., vol. 267, no. 5, pp. 1029–1045, 2003.
16. P. J. Nessjøen, A. Kyllingstad, P. D’Ambrosio, I. S. Fornea, A. Garcia, and B. Levy, “Field experience with an active stick-slip prevention system,” in Proc. SPE/IADC Drilling Conf. Exhib., Amsterdam, The Netherlands, Mar. 2011, pp. 139956-1–139956-10.
17. Perneder L, Detournay E. Steady-state solutions of a propagating borehole. International Journal of Solids and Structures 2013; 50:1226 –1240. 27. Tucker RW, Wang C. Torsional vibration control and cosserat dynamics of a drill-rig assembly. Meccanica 2003; 38(1):143–159.
18. Saldivar B, Mondié S, Loiseau J-J, Rasvan V. Suppressing axial-torsional coupled vibrations in drillstrings. Journal of Control Engineering and Applied Informatics 2013; 15(1):3–10.
19. T. Richard, C. Germay, and E. Detournay, “A simplified model to explore the root cause of stick–slip vibrations in drilling systems with drag bits,” J. Sound Vibrat., vol. 305, no. 3, pp. 432–456, 2007.
20. T. Ritto, “Numerical analysis of the nonlinear dynamics of a drillstring with uncertainty modeling,” Ph.D. dissertation, Univ. Paris-Est, Champs-sur-Marne, France, 2010.
21. Y. A. Khulief, F. A. Al-Sulaiman, and S. Bashmal, “Vibration analysis of drillstrings with self-excited stick–slip oscillations,” J. Sound Vibrat., vol. 299, no. 3, pp. 540–558, 2007.

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