Subcritical Water Technology for Enhanced Extraction of Biochemical Compounds from *Chlorella vulgaris*

S. A. Awaluddin,¹ Selvakumar Thiruvenkadamb,¹ Shamsul Izhar,¹ Yoshida Hiroyuki,¹ Michael K. Danquah,² and Razif Harun¹

¹Department of Chemical and Environmental Engineering, Universiti Putra Malaysia, 43400 Serdang, Malaysia
²Department of Chemical Engineering, Curtin University, 98009 Sarawak, Malaysia

Correspondence should be addressed to Razif Harun; mh_razif@upm.edu.my

Received 12 January 2016; Revised 25 March 2016; Accepted 24 April 2016

1. Introduction

Global energy demands continue to increase at a current annual consumption rate of about 500 Quadrillion Btu (QBtu). Approximately 92% of this consumption demand is met by nonrenewable fossil energy sources which have significant negative impacts on the environment and the economy [1]. Biofuels represent a class of renewable energy with the potential to contribute significantly to the sustainable energy mix required to meet future energy demands. Microalgal biomass is heavily researched as feedstock for the production of different types of biofuels as a result of its fast growth rate, nonedibility, and the capacity to accumulate high concentrations of biochemical compounds such as lipids and carbohydrates for biofuel synthesis [2].

Microalgal primary metabolites, such as proteins, fatty acids, and carbohydrates, are produced intracellularly and entrapped within the cells; thus an effective extraction technology is required to release these biochemical products [3]. The primary metabolites are source of bioactive metabolites, such as vitamins and enzymes, which are commercially beneficial due to their antioxidant, anti-inflammatory, antiangiogenic, antiobesity, and anticancer properties [3]. Commonly used extraction technologies via chemical and mechanical methods include expellers, liquid-liquid extraction (solvent extraction), super-critical fluid extraction (SFE), and ultrasound techniques [4–7].

Expellers are commonly used to extract oil from nuts and seeds [4]. However, they could find applications in the extraction of lipids from dry microalgal biomass. The expeller uses pressure to compress and expel oil from the feedstock biomass. Although this method produces high yields of oil, it is disadvantaged with high energy consumption and prolonged extraction time [4]. Solvent extraction (SE)
has demonstrated to be efficient for lipid extraction from microalgal biomass [5]. In this approach, an organic solvent or a mixture of solvents including benzene, cyclohexane, hexane, acetone, and chloroform react with the microalgal biomass [8]. The solvent ruptures and/or penetrates the microalgal cell wall and extracts lipid from the intracellular aqueous medium since lipids have higher solubilities in organic solvents than water. Solvent extract is then subjected to distillation to separate the lipid from the solvent. The solvent can be recycled for further use. Supercritical fluid extraction (SFE) makes use of high pressures to rupture the biomass cells. This method of extraction has proven to be extremely time efficient and has been employed for a wide range of biomass materials [6]. It has been reported that the operating temperature and pressure of SFE do not significantly affect product yield but rather the extraction rate [9, 10]. Andrich et al. [11] compared the polyunsaturated fatty acids (PUFA) extraction yields of SFE and SE using *Spirulina platensis* and reported that SFE demonstrated a higher PUFA yield and fatty acid composition compared to SE. Another promising technology for lipid extraction from microalgal biomass is via ultrasound. This method exposes the microalgae biomass to high intensity ultrasonic waves to create tiny cavitation bubbles around the cells. The collapse of the bubbles emits shockwaves which shatter the cell wall to enable the release of intracellular materials. Wiltshire et al. [7] reported ultrasound extraction yields of 90% for fatty acids and pigments from *Scenedesmus obliquus*. Although ultrasound extraction yields of lipids from microalgae is quite effective at small scale, numerous technoeconomic challenges arise with large scale applications. This has dwindled interests in the use of ultrasound extraction technology for microalgae biomass extraction outside laboratory environment. One of the recent advancements in the extraction of intracellularly entrapped compounds from biomass materials is the use of subcritical water extraction (SWE) technology. The technology has been demonstrated to offer lower production costs, mild operating conditions, and shorter production duration compared to the aforementioned conventional methods [12–14]. In this technology water reacted as a solvent and catalyst to convert biomass into value added products [15]. Water ionization and dielectric potential are the two characteristics of water which are of unique importance during SWE. As the temperature of water increases, its hydrogen bonding cleaves with decreasing dielectric constant and polarity [16]. This results in an increase in the concentration of hydrogen ion [17]. Extensive studies led by Yoshida and coworkers found that valuable and useful substances such as organic acids, amino acids, proteins, fatty acids, and oils are recoverable through the use of SWE, and the technology can be applied in wastewater treatment. For example, fish waste was liquefied by hydrolysis using subcritical water technology to enable the recovery of organic acids and amino acids and the extraction of fatty acids [18]. Similar results were also obtained with squid waste where free fatty acids containing EPA and DHA were produced during hydrolysis with subcritical water technology [19].

With increasing research interests in microalgal biotechnology through the development of value added products, along with the limited application of SWE on microalgal biomass, this work seeks to investigate the application of SWE for optimal extraction of biochemical compounds from *Chlorella vulgaris*.

### 2. Materials and Methodology

#### 2.1. Microalgal Species and Biomass Development. *C. vulgaris* (green microalga) biomass was used for the extraction process. The microalgal species was obtained from Pure Bulk Inc. (USA) and delivered in a green powdered form with an average particulate size of 100 µm. The powdered microalgal cells were stored in a desiccator until further use.

#### 2.2. Characterization of Microalgal Biomass

##### 2.2.1. Proximate Analysis. The moisture, volatile matter, fixed carbon, and ash contents of *C. vulgaris* biomass were determined using a thermogravimetric analyzer (TGA) (TGA/SDTA851, Mettler Toledo, USA). 20 mg of fine biomass powder was placed in an alumina crucible and heated inside a furnace. The sample was continuously heated under different conditions of temperature (0–1000 °C) and heating rate (5, 10, and 20 °C min⁻¹) and at a constant gaseous nitrogen (N₂)/air atmosphere flowing at 25 mL/min.

##### 2.2.2. Ultimate Analysis. The elemental composition of *C. vulgaris* biomass was determined using CHNS analyzer (LECO True Spec CHNS628, USA). Approximately 1.0 mg of dry biomass sample was weighed into a tin capsule and transferred to the autosampler. The temperature was set at 1000 °C, and oxygen, nitrogen, and helium were used as the carrier gases.

##### 2.2.3. Scanning Electron Microscopy (SEM). Scanning Electron Microscopy (SEM) analysis of both intact and extracted biomass fractions was performed using a Hitachi S-3400N Tabletop Microscope configured with an energy dispersive system (EDS) and operated at a voltage of 20 kV. The samples were sputter coated with gold at 5 mA for 45 s prior to SEM analysis. The images were examined under different resolutions ranging from 300 SE to 6.00 kSE.

#### 2.3. Subcritical Water Extraction (SWE). *C. vulgaris* used for SWE was first pulverized into different particle sizes ranging from 38 µm to 250 µm. The different particle size fractions were separated by passing the pulverized sample through a series of cascaded stainless steel sieves. Four process parameters were investigated at five different levels to understand the impacts on microalgal SWE. The four process parameters are temperature (180–374 °C), extraction time (1–20 min), particle size (38–250 µm), and biomass loading (5–40 wt.%). The schematic diagram of the SWE system is shown in Figure 1. The dried microalgal biomass at a specific loading concentration was mixed with 6 mL of Milli-Q water and loaded into a stainless steel reaction tube (SUS316) having an inner diameter of 7.5 × 10⁻³ m and 1.5 × 10⁻¹ m length. Argon gas was used to purge the reactor for 5 min to release trapped air from the reactor. The reactor tube was then closed tightly
Table 1: CCD for *C. vulgaris* SWE experimental conditions.

| Sample | Temperature (°C) | Extraction time (min) | Particlesize (µm) | Concentration microalgae (%) |
|--------|------------------|-----------------------|-------------------|----------------------------|
| 1      | 229 (−1)         | 3 (−1)                | 75 (−1)           | 10 (−1)                    |
| 2      | 229 (−1)         | 3 (−1)                | 75 (−1)           | 30 (+1)                    |
| 3      | 229 (−1)         | 3 (−1)                | 180 (+1)          | 10 (−1)                    |
| 4      | 229 (−1)         | 3 (−1)                | 180 (+1)          | 30 (+1)                    |
| 5      | 229 (−1)         | 10 (+1)               | 75 (−1)           | 10 (−1)                    |
| 6      | 229 (−1)         | 10 (+1)               | 75 (−1)           | 30 (+1)                    |
| 7      | 229 (−1)         | 10 (+1)               | 180 (+1)          | 10 (−1)                    |
| 8      | 229 (−1)         | 10 (+1)               | 180 (+1)          | 30 (+1)                    |
| 9      | 326 (+1)         | 3 (−1)                | 75 (−1)           | 10 (−1)                    |
| 10     | 326 (+1)         | 3 (−1)                | 75 (−1)           | 30 (+1)                    |
| 11     | 326 (+1)         | 3 (−1)                | 180 (+1)          | 10 (−1)                    |
| 12     | 326 (+1)         | 3 (−1)                | 180 (+1)          | 30 (+1)                    |
| 13     | 326 (+1)         | 10 (+1)               | 75 (−1)           | 10 (−1)                    |
| 14     | 326 (+1)         | 10 (+1)               | 75 (−1)           | 30 (+1)                    |
| 15     | 326 (+1)         | 10 (+1)               | 180 (+1)          | 10 (−1)                    |
| 16     | 326 (+1)         | 10 (+1)               | 180 (+1)          | 30 (+1)                    |
| 17     | 180 (−2)         | 5 (0)                 | 90 (0)            | 20 (0)                     |
| 18     | 374 (+2)         | 5 (0)                 | 90 (0)            | 20 (0)                     |
| 19     | 277 (0)          | 1 (−2)                | 90 (0)            | 20 (0)                     |
| 20     | 277 (0)          | 20 (+2)               | 90 (0)            | 20 (0)                     |
| 21     | 277 (0)          | 5 (0)                 | 38 (−2)           | 20 (0)                     |
| 22     | 277 (0)          | 5 (0)                 | 250 (+2)          | 20 (0)                     |
| 23     | 277 (0)          | 5 (0)                 | 90 (0)            | 5 (−2)                     |
| 24     | 277 (0)          | 5 (0)                 | 90 (0)            | 40 (+2)                    |
| 25     | 277 (0)          | 5 (0)                 | 90 (0)            | 20 (0)                     |

with Swagelok caps. The sample filled tube was immersed in a salt bath at a specific temperature for a specific time. After the reaction process, the reactor tube was quenched in a cooling water basin to terminate the reaction. Table 1 summarizes the process conditions.

2.4. SWE Product Analysis

2.4.1. Product Separation. Product extracts from the SWE process were centrifuged (KUBOTA 2420, Japan) at 4000 rpm for 10 min. The centrifuged samples formed three different layers of oil, water, and solid residue as shown in Figure 2. Afterwards, 1.5 mL of hexane was added to the extracted samples for oil separation. The mixture was left for 10 min before recovery by decantation. The process was repeated 8 times for complete oil separation. The residual mixtures were further centrifuged at 4000 rpm for 10 min. The supernatant and solid residue were separated by filtration and stored at −20°C until further analysis [23].

2.4.2. Protein Analysis. Protein concentration was determined using the Lowry method [21]. A serial dilution of Bovine Serum Albumin (BSA) solution was prepared from its stock solution (1 mg/mL). 0.2 mL of BSA solutions with concentrations ranging from 0.05 mg/mL to 1 mg/mL was pipetted into multiple test tubes. 2 mL of alkaline copper sulphate reagent was added to each aliquot and incubated for 10 min.
The alkaline copper sulphate reagent consists of Na$_2$CO$_3$, NaOH, CuSO$_4$·5H$_2$O, and C$_4$H$_4$KNaO$_6$·4H$_2$O. Also, 0.2 mL of Folin Ciocalteu reagent was added to the solution, and the optical density was measured at 660 nm using UV spectrophotometer (UV-160A, SHIMADZU, Japan). Water phase sample was pipetted into test tube to determine protein concentration using this method.

2.4.3. Total Carbohydrate Content. Phenol-sulphuric acid method was used to determine total carbohydrate content [22]. A serial dilution of sugar standard (20–100 mg/L) was prepared from glucose. UV spectrophotometer was used to determine the optical density at 490 nm. 1mL of sample was mixed with 1mL of 5% phenol and 5mL of H$_2$SO$_4$. The sample was left at ambient conditions for 10 min, and the glass lid covered for 25 min incubation before UV spectrophotometric analysis.

2.4.4. Total Organic Carbon (TOC) Analysis. The TOC of the liquid phase extract sample was analyzed using total organic carbon analyzer (TOC-V CPH, Shimadzu, Japan) [23], where 25 μL of aqueous sample was injected. Hydrogen phthalate of 250 ppm was used as a standard solution for this analysis. 250 ppm of sodium bicarbonate and 250 ppm of sodium carbonate were mixed with the sample aqueous phase and injected into the analyzer. The TOC of the sample was obtained by subtracting the measured inorganic carbon (IC) from the measured total carbon (TC).

2.5. Statistical Analysis. Central Composite Design (CCD) was employed to optimize process parameters during SWE in order to maximize product yield. The parameters optimized in this study are temperature, extraction time, particle size of microalgae, and microalgae loading concentration. The results from the experimental work were statistically analyzed using the Statistical Software (Statsoft, v.5.0). The dependent variable for the statistical analysis is the yield of extracted product, whilst the independent variables are the process parameters. The effect of each parameter was analyzed in order to evaluate the synergistic effects of multiple process parameters on maximizing the yield of bioactive compounds.

### 3. Results and Discussion

#### 3.1. Biomass Characterization

#### 3.1.1. Proximate and Ultimate Analysis

Proximate analysis gives a quantitative estimation of the microalgal biomass material composition. The composition of *C. vulgaris* biomass used in this study is divided into four main groups as shown in Table 2. The high volatile matter percentage of microalgal biomass is advantageous for biofuel production [24].

Ultimate analysis generates biomass compositions such as carbon, hydrogen, oxygen, nitrogen, sulphur, and ash through combustion and can be used to investigate the effect of reaction temperature on CHNS ratio (number of atoms to carbon) of the solid residual. During the process, carbon is converted to carbon dioxide; hydrogen to water; nitrogen to nitrogen gas; and sulphur to sulphur dioxide [24]. Table 2 shows the CHNS percentage of SWE treated and raw samples of the biomass. The SWE treated samples were exposed to SWE under the conditions of 277°C temperature, 5 min extraction time, 90 μm biomass particle size, and 5% biomass loading concentration. The carbon content increased by 25% with SWE treatment compared to the intact cells, indicating that the extraction process resulted in some degree of biomass disruption and this enabled a higher amount of carbon to be available for combustion. The results of ultimate compositions of *C. vulgaris* are also compared with other biomass (Table 3). The *C. vulgaris* biomass provides higher carbon percentage, hence indicating that it contains substantial amounts of lipid, cellulose, and hemicellulose which are good for biodiesel and bioethanol production [25].

#### 3.1.2. Scanning Electron Microscopy (SEM)

Figure 3 shows the surface morphology of SWE treated and nontreated
Table 3: Ultimate composition of biomass samples.

| Biomass       | C        | H        | N        | S        | O        | Reference |
|---------------|----------|----------|----------|----------|----------|-----------|
| C. vulgaris   | 47.11±0.5| 7.47±0.3 | 8.26±0.4 | —        | 37.16±0.3| This study|
| Rice bran     | 44.40    | 7.11     | 2.16     | —        | 46.30    | [20]      |
| Jatropha shell| 42.45    | 5.12     | 1.60     | —        | 50.83    | [21]      |
| Sargassum sp. | 26.70    | 4.23     | 1.35     | 0.19     | 67.53    | [22]      |

Figure 3: SEM images of nontreated (a and b) and SWE treated (c and d) C. vulgaris biomass samples. The images were captured at the same voltage of 20 kV and multiple resolutions of 7.2 mm × 1.00 kSE (a), 7.2 mm × 3.00 kSE (b), 7.3 mm × 1.00 kSE (c), and 7.3 mm × 3.00 kSE (d). SWE treatment occurred at 215°C for 6 min using 28 wt.% microalgal biomass with particulate size of 180 µm.

3.2. SWE Product Analysis

3.2.1. Protein. The highest protein concentration of 31.16 g/100 g was obtained when 5 wt.% microalgal biomass with 90 µm particulate size was treated under 277°C temperature condition for 5 min. The statistical analysis indicated that the optimum conditions to maximize protein yield from SWE of C. vulgaris are temperature (281°C), extraction time (17 min), particle size (75 µm), and microalgae loading (45 wt.%). Table 4 shows the protein yield characteristic equation generated for SWE of the microalgal biomass as a function of the process parameters. It was determined that the most significant process parameters affecting protein extraction from the biomass were microalgal loading concentration. The microalgal loading concentration demonstrated a positive effect whilst the other process parameters demonstrated a negative effect as shown in Figure 4(a). Increasing the microalgal biomass concentration resulted in an increase in protein yield.
Table 4: Generated characteristic equations for optimum product yields from SWE treatment of C. vulgaris biomass.

| Extraction product | Formula of optimum product* |
|--------------------|-----------------------------|
| Protein            | $5.707608d - 1.87442a^2 - 1.35416b - 1.89065a - 0.196542c + 0.8136935b^2 + 1.22666ab - 1.05ad - 1.04515ac - 0.623285cd + 0.4767914c^2 + 0.9863567d^2 - 0.335209bd - 0.302402bc$ |
| Total carbohydrates | $3.822194ab - 2.4369ad - 2.35744a - 1.63113b + 1.57958d - 1.1742d^2 + 1.153092c - 0.908555bd + 0.174052c^2 + 0.4734103bc + 0.4169475cd + 0.3989977ac + 0.2869922c^2 - 0.280178a^2 + 0.2793208b^2$ |
| TOC                | $7.607638d - 1.92788b + 1.635715b^2 - 1.09245a + 0.672907d^2 - 0.53976a^2 + 0.528741d - 0.5033bd - 0.471897ad - 0.45396bc + 0.1342441c + 0.1244762c + 0.071781ab - 0.056626c^2$ |

* a: extraction temperature; b: extraction time; c: particle size; d: microalgal biomass loading.

Figure 4: Standard Pareto chart of the process parameter for bioactive compound extraction from C. vulgaris, (a) protein, (b) total carbohydrate content, and (c) TOC. +ve and −ve sign describe the effect of the selected parameter that gives a positive and negative impact on the bioactive compounds extraction.

loading concentration in SWE increases protein yield as high biomass loading concentrations present an increased amount of available proteins for extractions. Proteins denature at high temperatures, and this explains the negative effect of decreasing protein yield under high SWE temperature conditions. Protein denaturation happens when the supplied heat increases the molecular kinetic energy of the protein, causing it to vibrate rapidly and destroying the protein tertiary structure through the cleavage of its hydrogen bonds and nonpolar hydrophobic interaction [28]. Figure 6(a) shows the relationship between the independent process variables and the protein yield. The yield of protein increases with
### Table 5: Analysis of variance (ANOVA) for the different components.

| Response variables | Protein (%) | Total carbohydrate (%) | TOC (%) |
|--------------------|-------------|------------------------|---------|
|                    | SS          | DF                     | P       | SS          | DF | P      | SS       | DF         | P      |
| Linear             |             |                        |         |             |        |        |          |            |        |
| a                  | 1.22908     | 1                      | 0.0879  | 527185      | 1     | 0.0401 | 73767    | 1          | 0.3003 |
| b                  | 0.63051     | 1                      | 0.2055  | 252382      | 1     | 0.1340 | 229731   | 1          | 0.0827 |
| c                  | 1.32821     | 1                      | 0.0777  | 126127      | 1     | 0.2757 | 1114     | 1          | 0.8959 |
| d                  | 11.2011     | 1                      | 0.0002  | 236669      | 1     | 0.1453 | 3577326  | 1          | 0.00002 |
| Square             |             |                        |         |             |        |        |          |            |        |
| a^2                | 1.20806     | 1                      | 0.0903  | 7446        | 1     | 0.7851 | 18008    | 1          | 0.6012 |
| b^2                | 0.22765     | 1                      | 0.4348  | 7401        | 1     | 0.7857 | 165268   | 1          | 0.1331 |
| c^2                | 0.07816     | 1                      | 0.6438  | 7813        | 1     | 0.7800 | 198      | 1          | 0.9560 |
| d^2                | 0.33452     | 1                      | 0.3472  | 130787      | 1     | 0.2675 | 27970    | 1          | 0.5164 |
| 2-way interaction  |             |                        |         |             |        |        |          |            |        |
| a*b                | 0.51737     | 1                      | 0.2480  | 1385817     | 1     | 0.0034 | 340      | 1          | 0.9423 |
| a*c                | 0.37559     | 1                      | 0.3205  | 15102       | 1     | 0.6982 | 958      | 1          | 0.9034 |
| a*d                | 0.37908     | 1                      | 0.3184  | 557228      | 1     | 0.0358 | 13764    | 1          | 0.6471 |
| b*c                | 0.0344       | 1                      | 0.7685  | 21259       | 1     | 0.6461 | 12706    | 1          | 0.6600 |
| b*d                | 0.03864     | 1                      | 0.7444  | 78304       | 1     | 0.3845 | 15659    | 1          | 0.6256 |
| c*d                | 0.13358     | 1                      | 0.5470  | 16491       | 1     | 0.6855 | 17280    | 1          | 0.6085 |
| Lack of fit        | 3.4338      | 10                     |         | 948594      | 10    |         | 618000   | 10         |        |
| Total              | 26.3276     | 24                     |          | 5074315     | 24    |          | 5320338  | 24         |        |
| R^2                | 0.8694      |                        |          | 0.81306     |       |          | 0.8838   |            |        |
| Adj.-R^2           | 0.68656     |                        |          | 0.55134     |       |          | 0.72118  |            |        |

*a: extraction temperature; b: extraction time; c: particle size; d: microalgal biomass loading; SS: sum of squares; DF: degrees of freedom; P: probability.

### Figure 5: Total carbohydrate, protein, and TOC yields from different SWE treatment conditions of C. vulgaris biomass.

Increasing microalgal loading concentration. Increasing the extraction temperature to the optimum point (280–300°C) results in increasing protein yield. However, a further increase in temperature results in decreasing protein yields, and this is due to thermal denaturation as explained earlier.

**3.2.2. Carbohydrate.** Figure 5 shows a summary of the total carbohydrate yields obtained from the experimental design. The maximum carbohydrate yield of 14.18 g/100 g was achieved under SWE conditions of 277°C for 5 min with 5 wt.% microalgal biomass having 90 μm particulate size. The lowest carbohydrate yield of 0.255 mg/mL was obtained at 326°C for 3 min with 30 wt.% microalgal biomass with particulate size 75 μm. The microalgae biomass carbohydrate has previously been reported to have different types of polysaccharides, including cellulose, xylose, galactose, and arabinose, entrapped in the cell walls [29]. Based on the statistical analysis in Figure 4(b), the carbohydrate yield was influenced by extraction temperature, time, and microalgal biomass loading. The extraction temperature and microalgal biomass loading demonstrated a negative effect on carbohydrate yield whilst the extraction time demonstrated a positive effect. In brief, low temperature, longer extraction time, and low biomass loading during SWE support high carbohydrate yields. Extraction of carbohydrate gives negative effects because carbohydrate rapidly decomposed when exposed to higher temperatures [30,31]. Also, biomass loading has an effect on carbohydrate extraction as the yield decreases when the sample is concentrated. The sample was not extracted well when the amount of sample inside the reactor is too concentrated. Microalgae have rigid cell walls which are hard to break; in order to increase the efficiency of carbohydrate extraction, longer extraction time is needed [32,33]. According to the statistical analysis, the optimum SWE conditions for maximum carbohydrate extraction yield were 302°C temperature, 8 min extraction time, 38 μm particulate size, and 16 wt.% microalgal biomass loading. The equation for the optimum conditions of carbohydrate extraction yield is shown in Table 5. The relationship between the microalgal biomass loading and the extraction temperature is shown in Figure 6(b). Based on the surface plot, it can
Figure 6: Fitted response surface curves for (a) protein, (b) total carbohydrate, and (c) TOC.
be seen that the maximum carbohydrate yield was achieved when the concentration of biomass loading and extraction temperature were higher. The highest carbohydrate concentration of ~2000 mg/L at 40–45% microalgal biomass loading was obtained under the temperature range of 100 to 200°C.

3.2.3. Total Organic Carbon (TOC). Total organic carbon (TOC) analysis determines the concentration of total organic carbon covalently bonded in the microalgal biomass. Amongst all the process parameters investigated, TOC of the biomass was only influenced by the loading concentration of the microalgal biomass as shown in Figure 4(c). With increasing concentration of microalgal biomass loading, the quantity of organic carbon under covalent bonding within the biomass increases. This can be seen from the surface plot in Figure 6(c). From the experimental results, the highest concentration of TOC of 8.01 g/100 g was obtained for the sample exposed to SWE treatment 229°C for 3 min with 10 wt.% microalgal biomass having 75 μm particle size. Figure 5 presents a summary of TOC yield. The characteristic equation relating the optimum conditions of TOC yield is presented in Table 5.

3.3. ANOVA. Analysis of variance (ANOVA) for the responses is presented in Table 5. \( R^2 \) values for the selected responses were 0.87, 0.81, and 0.88 for protein, total carbohydrate content, and TOC, respectively. The observed \( R^2 \) values, which were above 0.75, indicated the aptness of the model. The quadratic models presented in Table 4 are, therefore, considered as a satisfactory interpretation to the experimental data.

4. Conclusion

This work investigated the optimum conditions to extract biochemical compounds, mainly protein and total carbohydrate, from C. vulgaris biomass using SWE. From the results obtained, microalgal loading concentration was the most significant parameter affecting protein yield, whereas extraction temperature, biomass loading, and extraction time affected carbohydrate yield. The results obtained demonstrate the potential of SWE of microalgae biomass for large scale production of biochemical compounds, such as proteins and carbohydrates, that have wide applications in production of algae-based biofuels and other useful materials. From economic and environmental perspectives, SWE has proven attractive in recovering valuable biochemical materials from a wide range of biomass feedstocks. The use of SWE for the generation of bioproducts from microalgal biomass is expected to herald future sustainable bioextraction technologies, and this work contributes significantly to the validation of SWE technology for optimal biochemical products extraction.

Competing Interests

The authors declare that they have no competing interests.

Acknowledgments

This work has been supported by the Ministry of Higher Education (MOHE) Fundamental Research Grant Scheme (Project Code: 03-02-13-1297FR) and the Department of Chemical and Environmental Engineering, Universiti Putra Malaysia.

References

[1] R. Harun, M. Davidson, M. Doyle, R. Gopiraj, M. Danquah, and G. Forde, “Technoeconomic analysis of an integrated microalgae photobioreactor, biodiesel and biogas production facility,” Biomass and Bioenergy, vol. 35, no. 1, pp. 741–747, 2011.
[2] C.-Y. Chen, X.-Q. Zhao, H.-W. Yen et al., “Microalgae-based carbohydrates for biofuel production,” Biochemical Engineering Journal, vol. 78, pp. 1–10, 2013.
[3] M. G. De Morais, B. D. S. Vaz, E. G. De Morais, and J. A. V. Costa, “Biologically active metabolites synthesized by microalgae,” BioMed Research International, vol. 2015, Article ID 835761, 15 pages, 2015.
[4] T. O. S. Popoola and O. D. Yangomodou, “Extraction, properties and utilization potentials of cassava seed oil,” Biotechnology, vol. 5, no. 1, pp. 38–41, 2006.
[5] M. Plaza, S. Santoyo, L. Jaime et al., “Screening for bioactive compounds from algae,” Journal of Pharmaceutical and Biomedical Analysis, vol. 51, no. 2, pp. 450–455, 2010.
[6] M. D. Macías-Sánchez, C. Mantell, M. Rodriguez, E. Martínez De La Ossa, L. M. Lubión, and O. Montero, “Supercritical fluid extraction of carotenoids and chlorophyll a from Nannochloropsis gaditana,” Journal of Food Engineering, vol. 66, no. 2, pp. 245–251, 2005.
[7] K. H. Wiltshire, M. Boersma, A. Möller, and H. Buhtz, “Extraction of pigments and fatty acids from the green alga Scenedesmus obliquus (Chlorophyceae),” Aquatic Ecology, vol. 34, no. 2, pp. 119–126, 2000.
[8] Raghvendra, V. Tomar, A. Chaudhary, M. Kumar, U. Kumar, and B. Singh, “Synthesis of biodiesel from microbial algae,” International Journal of Pharmaceutical, Chemical and Biological Sciences, vol. 5, no. 1, pp. 189–195, 2015.
[9] A. P. R. F. Canelo, L. V. Rosa, M. O. M. Marques, and M. A. A. Meireles, “Supercritical fluid extraction of fatty acids and carotenoids from the microalgae Spirulina maxima,” Industrial and Engineering Chemistry Research, vol. 41, no. 12, pp. 3012–3018, 2002.
[10] G. Andrich, U. Nesti, F. Venturi, A. Zinnai, and R. Fiorentini, “Supercritical fluid extraction of bioactive lipids from the microalga Nannochloropsis sp.,” European Journal of Lipid Science and Technology, vol. 107, no. 6, pp. 381–386, 2005.
[11] G. Andrich, A. Zinnai, U. Nesti, F. Venturi, and R. Fiorentini, “Supercritical fluid extraction of oil from microalga Spirulina (Arthrospira) platensis,” Acta Alimentaria, vol. 35, no. 2, pp. 195–203, 2006.
[12] S. M. Zakaria and S. M. M. Kamal, “Subcritical water extraction of bioactive compounds from plants and algae: applications in pharmaceutical and food ingredients,” Food Engineering Reviews, vol. 8, no. 1, pp. 23–34, 2016.
[13] S. B. Hawthorne, C. B. Grabanski, E. Martin, and D. J. Miller, “Comparisons of Soxhlet extraction, pressurized liquid extraction, supercritical fluid extraction and subcritical water extraction for environmental solids: recovery, selectivity and
[14] X. Liang and Q. Fan, “Application of sub-critical water extraction in pharmaceutical industry,” Journal of Materials Science and Chemical Engineering, vol. 5, no. 1, pp. 1–6, 2013.

[15] W. Abdelmoez, T. Nakahasi, and H. Yoshida, “Amino acid transformation and decomposition in saturated subcritical water conditions,” Industrial and Engineering Chemistry Research, vol. 46, no. 16, pp. 5286–5294, 2007.

[16] H. Mazaheri, K. T. Lee, S. Bhatia, and A. R. Mohamed, “Subcritical water liquefaction of oil palm fruit press fiber in the presence of sodium hydroxide: an optimisation study using response surface methodology,” Bioresource Technology, vol. 101, no. 23, pp. 9335–9341, 2010.

[17] O. Pourali, F. S. Asghari, and H. Yoshida, “Sub-critical water treatment of rice bran to produce valuable materials,” Food Science and Technology Research, vol. 18, no. 3, pp. 333–340, 2012.

[18] Z. Bi and B. B. He, “Characterization of microalgae for the purpose of biofuel production,” Transactions of the ASABE, vol. 56, no. 4, pp. 1529–1539, 2013.

[19] Y. C. Sharma, B. Singh, and J. Korstad, “A critical review on recent methods used for economically viable and eco-friendly development of microalgae as a potential feedstock for synthesis of biodiesel,” Green Chemistry, vol. 13, no. 11, pp. 2993–3006, 2011.

[20] I. Rodríguez-Meizoso, L. Jaime, S. Santoyo, F. J. Señorans, A. Cifuentes, and E. Ibáñez, “Subcritical water extraction and characterization of bioactive compounds from Haematococcus pluvialis microalg,” Journal of Pharmaceutical and Biomedical Analysis, vol. 51, no. 2, pp. 456–463, 2010.

[21] I. Marcet, C. Alvarez, B. Paredes, and M. Diaz, “The use of sub-critical water hydrolysis for the recovery of peptides and free amino acids from food processing wastes. Review of sources and main parameters,” Waste Management, vol. 49, pp. 364–371, 2016.

[22] Z. Bi and B. B. He, “Characterization of microalgae for the purpose of biofuel production,” Transactions of the ASABE, vol. 56, no. 4, pp. 1529–1539, 2013.

[23] Y. C. Sharma, B. Singh, and J. Korstad, “A critical review on recent methods used for economically viable and eco-friendly development of microalgae as a potential feedstock for synthesis of biodiesel,” Green Chemistry, vol. 13, no. 11, pp. 2993–3006, 2011.

[24] I. Rodríguez-Meizoso, L. Jaime, S. Santoyo, F. J. Señorans, A. Cifuentes, and E. Ibáñez, “Subcritical water extraction and characterization of bioactive compounds from Haematococcus pluvialis microalg,” Journal of Pharmaceutical and Biomedical Analysis, vol. 51, no. 2, pp. 456–463, 2010.

[25] I. Marcet, C. Alvarez, B. Paredes, and M. Diaz, “The use of sub-critical water hydrolysis for the recovery of peptides and free amino acids from food processing wastes. Review of sources and main parameters,” Waste Management, vol. 49, pp. 364–371, 2016.

[26] Z. Bi and B. B. He, “Characterization of microalgae for the purpose of biofuel production,” Transactions of the ASABE, vol. 56, no. 4, pp. 1529–1539, 2013.

[27] Y. C. Sharma, B. Singh, and J. Korstad, “A critical review on recent methods used for economically viable and eco-friendly development of microalgae as a potential feedstock for synthesis of biodiesel,” Green Chemistry, vol. 13, no. 11, pp. 2993–3006, 2011.

[28] I. Rodríguez-Meizoso, L. Jaime, S. Santoyo, F. J. Señorans, A. Cifuentes, and E. Ibáñez, “Subcritical water extraction and characterization of bioactive compounds from Haematococcus pluvialis microalg,” Journal of Pharmaceutical and Biomedical Analysis, vol. 51, no. 2, pp. 456–463, 2010.

[29] I. Marcet, C. Alvarez, B. Paredes, and M. Diaz, “The use of sub-critical water hydrolysis for the recovery of peptides and free amino acids from food processing wastes. Review of sources and main parameters,” Waste Management, vol. 49, pp. 364–371, 2016.