The Caltech-NRAO Stripe 82 Survey (CNSS). II. On-the-fly Mosaicking Methodology

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Abstract

Telescope slew and settle time markedly reduce the efficiency of wide-field multi-epoch surveys for sensitive interferometers with small fields of view. The overheads can be mitigated through the use of on-the-fly mosaicking (OTFM), where the antennas are driven at a non-sidereal rate and visibilities are recorded continuously. Here we introduce the OTFM technique for the Very Large Array (VLA), and describe its implementation for the Caltech-NRAO Stripe 82 Survey (CNSS), a dedicated five-epoch survey for slow transients at the S band (2–4 GHz). We also describe the OTFSim tool for planning dynamically scheduled OTFM observations on the VLA, the latest imaging capabilities for OTFM in CASA, and present a comparison of OTFM observations with pointed observations. Using the subset of our observations from the CNSS pilot and final surveys, we demonstrate that the wide-band and wide-field OTFM observations with the VLA can be imaged accurately, and that this technique offers a more efficient alternative to standard mosaicking for multi-epoch shallow surveys such as the CNSS and the VLA Sky Survey. We envisage that the new OTFM mode will facilitate new synoptic surveys and high-frequency mapping experiments on the VLA.

Key words: methods: observational – surveys – techniques: interferometric

1. Introduction

Survey science, both line and continuum, has become a major driver for next generation radio facilities. A fast imaging capability with large étendue is a necessary requirement for all of these experiments (Cordes 2008). At centimeter wavelengths, the Australian Square Kilometre Array Pathfinder (ASKAP) and the Apertif instrument on the Westerbork Synthesis Radio Telescope (WSRT) will be using phased array technology to image large instantaneous fields of view (FOV) on the sky (Johnston et al. 2008; Oosterloo et al. 2010). The MeerKAT array undergoing commissioning in South Africa will achieve a high survey speed by building a large numbers of small dishes (Booth & Jonas 2012). Traditionally, single dish telescopes have a narrow FOV but come equipped with sensitive, state-of-the-art backend receivers. In order to achieve fast survey speeds in these cases it is necessary to rapidly slew the telescope across the sky in what is called “on-the-fly” (OTF) imaging, continually collecting data, utilizing the large instantaneous sensitivity of the telescope (Mangum et al. 2007). The need for OTF is most acute in mm/sub-mm astronomy where it has been heavily used; for example, at the Nobeyama Radio Observatory 45 m and the Atacama Submillimeter Telescope Experiment 10 m (Sawada et al. 2008), and when implementing the Legacy science programs at the James Clark Maxwell Telescope (Sandell 2000). Interferometers have developed an analogous technique called mosaicking to be used when the primary beam is smaller than the size of the source being imaged (e.g., Sault et al. 1996).

In this paper we describe a new mode for the Karl G. Jansky Very Large Array (VLA: Perley et al. 2011) that takes advantage of receiver upgrades that have enabled an order-of-magnitude increase in continuum sensitivity and we use it to implement a fast survey mode called on-the-fly mosaicking (OTFM4). OTFM eliminates the slew and setup overheads and is thus ideal for either continuum or spectral line projects that require shallow, very large-area mosaics. In Section 1.1 we give the basic interferometric theory for OTFM. In Section 2 we describe the technical aspects relevant for the OTFM implemented for the VLA. Informed by the contents in the preceding sections, Section 3 gives the survey and OTFM parameters chosen for the Caltech-NRAO Stripe 82 Survey (CNSS). In Section 4 we describe a series of tests that were carried out for verification of the OTFM mode. The CNSS was designed to be a pathfinder for later wide-field surveys such as the VLA Sky Survey (VLASS5; M. Lacy et al. 2018, in preparation). The scope of OTFM for a wide range of experiments on the VLA, including the CNSS and the VLASS, is given in Section 5.

1.1. OTFM Theory

The measurement equation of interest for an interferometric imaging problem (neglecting the W term; Taylor et al. 1999) is,

\[ V_\nu(u) = \int B_\nu(s - s_p) I_\nu(s) e^{-i2\pi u(s - s_p)} ds \]  

where \( V_\nu \) is the k’th visibility, \( u = (u, v) \) is the 2D spatial frequency with respect to the phase center \( s_p \), \( s_p \) is the pointing center, \( s = (l, m) \) is the sky coordinate, \( I \) is the sky brightness (in this paper we neglect the time dependence in \( I \)), \( B \) the primary beam pattern, and the subscript \( \nu \) implies a dependence on the observing frequency. The slew of the antennas during OTFM requires the pointing center to change with respect to the phase center with time, and the phase center is also usually updated at regular intervals. Hence, we generally have \( s_p = s_p(t), s_0 = s_0(t) \). Within a certain integration time \( \Delta t \) in which the phase center is constant while the pointing center

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4 https://science.nrao.edu/facilities/vla/docs/manuals/obsguide/modes/mosaicking

5 https://science.nrao.edu/science/surveys/vlass
changes, the equation should be rewritten as
\[ V_i(\hat{u}_k) = \int \left[ \frac{1}{\Delta t} \int_{t_0 - \Delta t/2}^{t_0 + \Delta t/2} B_s(s - s_p) \, dt \right] \times I_s(s) e^{-\lambda_0^2 \hat{u}_k^T(s-s_0)} \, ds, \]  
where \( t_0 \) is the time of measurement (typically taken to be the time when the pointing center coincides with the phase center) and \( s_{x,0} = s_x(t_0) \). The time-averaged quantity \( \hat{s}_p \) is defined here for completeness, and will be used below. The “smearing” described by Equation (2), which occurs over time, does not introduce any phase errors (it is purely an amplitude error) as long as the time interval is sufficiently small (see below). Furthermore, unless there are variations in the scanning (which are equivalent to pointing errors) from one antenna to another, this is purely an overall amplitude error and not antenna or baseline based. The motion of the primary beam across a finite region on the sky during the integration time therefore necessitates the introduction of an “effective primary beam” \( (B_{\text{eff}}) \). We can rewrite Equation (2) in the following manner using \( B_{\text{eff}} \):
\[ B_{\text{eff}}(s - \hat{s}_p; \Delta t) = \frac{1}{\Delta t} \int_{t_0 - \Delta t/2}^{t_0 + \Delta t/2} B_s(s - s_p(t)) \, dt. \]  
The accuracy of the flux densities in the image is affected by the use of the antenna primary beam instead of the effective primary beam for primary beam correction. The associated fractional error is \( B_{\text{eff}}/B_{\text{a}} \) and is a function of the position within the image. For example, moving a fifth of the primary beam (assumed to be Gaussian) within the data dump time gives a <2% loss in accuracy, as shown below.

2. VLA Implementation of OTFM

The VLA implementation of OTFM scanning employs uniform slew rates in right ascension (R.A., \( \alpha \)) and declination (decl., \( \delta \)), with the coordinates of the start and endpoints and effective duration determining the rates in R.A. and decl. A single OTFM scan (“stripes”) must be either in constant R.A. or constant decl. to enforce uniform dwell time on a given point in the sky. Furthermore, uniform sensitivity requires the same separation between adjacent stripes (“rows”), \( \theta_{\text{row}} \), which in turn means that scanning should be in R.A. at constant decl.\(^6\) For scan in R.A. with rows separated by \( \theta_{\text{row}} \) in decl. at a fixed on-the-sky scan rate \( \dot{\theta} \), the effective R.A. rate will be given by \( \dot{\theta}_e = \dot{\theta} / \cos(\delta) \). In the VLA Observation Preparation Tool (OPT\(^10\)), this is effected by specifying the number of phase center steps \( (n_{\text{step}}) \) and integrations per step \( (n_i) \) such that the scanning time is\(^\dagger\) \[ t_{\text{step}} = \theta_e N, \]  
and \( \theta_e \) is the span of the stripe in R.A. The VLA data corresponding to a unique phase center, and having a duration of \( t_{\text{step}} \), is referred to as a “subscan,” and each phase center step produces a new subscan. In this section we describe the technical issues and formulae relevant for OTFM implemented for the VLA.

2.1. OTFM Uniformity and Row Separation

The row separation \( \theta_{\text{row}} \) is set by some allowed limit to the non-uniformity of the effective noise level in the resulting mosaic. Reconstructing a mosaic at a sky position of interest is carried out by a linear weighted sum of the radio data either in the image or \( uv \) plane. This is equivalent to the sum,
\[ S_\nu = \frac{1}{Z_\nu} \sum_i S_{\nu,i} w_{\nu,i}, \]  
where \( Z_\nu = \sum_i w_{\nu,i} \) is the sum of weights (the subscript \( \nu \) denotes frequency dependence), \( S_\nu \) is the flux density values from the mosaic image (or gridded \( uv \) data) and \( b_i = B_{\text{eff}} (x_i, y_i; t_0) \) denotes the primary beam correction at offset \( (x_i, y_i) \) from the sky position of interest. For optimal weighting, \( w_i = (b_i/\sigma_i)^2 \), and using standard propagation of uncertainty, the rms in the weighted average \( S_\nu \) is
\[ \sigma_{S,\nu}^2 = \frac{1}{Z_\nu} \sum_i b_i^2 / \sigma_i^2 = \frac{1}{Z_\nu} \]  
The mosaic rms noise is therefore simply the inverse of the sum of mosaic weights, \( Z \). The normalized maximum deviation is defined as
\[ \frac{\Delta \sigma}{\sigma} = \sqrt{\frac{\sigma_{\text{max}} - \sigma_{\text{min}}}{\sigma_{\text{max}} + \sigma_{\text{min}}}}, \]  
where \( \sigma_{\text{max}} \) and \( \sigma_{\text{min}} \) are the maximum and minimum rms noise in the reconstructed mosaic assuming uniform intrinsic noise per scan. We simulated a grid of pointings with uniform rms noise and varied the row separation. For each value of row separation, we numerically calculated the effective mosaic rms noise given by Equation (6) and then the normalized maximum deviation as per Equation (7). The resulting curve is shown as the solid black curve in Figure 1. We repeated this exercise restricting each pointing to within the 20% power point (0.8\( \theta_{\text{ph}} \)). The curve obtained using this constraint is shown as the dashed cyan curve in Figure 1. While the unrestricted curve gives a perfectly uniform rms noise below \( \theta_{\text{row}} = 0.8\theta_{\text{ph}} \), the restricted curve plateaus with a non-uniformity of around 2%.

\(^6\) There is another source of smearing, the baseline-based time smearing, that occurs due to \( u \) changing over the integration time, but the degree of smearing in this case is the same as that in any standard pointed observing mode.
\(^7\) For the purposes of the CNSS survey (specifically, the accuracy of source flux densities needed for the variability and transient search), we will show later that the use of antenna primary beam, which is predefined in standard radio astronomy software such as CASA, for primary beam correction is sufficient.
\(^8\) In this work, we have used a simplification, that the primary beam is Gaussian, for analytical derivations (Equation (10)). The FWHM from Perley (2016) is used. In reality, however, the azimuthally averaged beam within the first null differs from Gaussian by a maximum of 7% (see Perley 2016, this will change the smeared beam estimates by 1% or less), and additionally the beam is not azimuthally symmetric (see Jagannathan et al. 2017). Further amplitude errors may also arise from the leakage of Stokes \( I \) flux into Stokes \( Q \) and \( U \), as detailed in Jagannathan et al. (2017).

\(^9\) OTFM on the VLA is not restricted to constant decl. stripes, however.\(^10\) http://science.nrao.edu/facilities/vla/docs/manuals/opt/otf
\(^\dagger\) In reality, the VLA employs a “running start” in order to reach the required constant OTFM slew speed, \( \dot{\theta}_e \), at the starting coordinates of the OTFM stripe. Hence, there is an additional time \( t_{\text{run}} \) required at the beginning of each stripe.
which is in practice the best achievable using standard imaging procedures.

2.2. OTFM Smearing

We now derive an expression for the fractional change in the flux density of sources if the motion of the primary beam within a subscan (duration in which the phase center is constant) or data dump time is neglected. Describing the primary beam with a 2D Gaussian function we have

$$B_p(x, y) = e^{-(x^2 + y^2)/2\rho_v^2},$$

(8)

where \(x\) and \(y\) are Cartesian coordinates in the image plane defined with respect to the pointing center. We assume for simplicity that the motion of the antennas is along the \(x\)-direction. For data taken over the interval from \(t_0 - \Delta t/2\) to \(t_0 + \Delta t/2\) at OTFM scanning rate \(\dot{\theta}\) in the \(x\)-direction, a visibility centered at an offset point \((x_0, y_0)\) in the primary beam will see an effective beam value of:

$$B_{p,\text{eff}}(x_0, y_0; \Delta x) = \frac{1}{\Delta x} \int_{x_0-\Delta x/2}^{x_0+\Delta x/2} B_p(x, y_0) \, dx,$$

(9)

$$= e^{-x_0^2/2\rho_v^2} \int_{x_0-\Delta x/2}^{x_0+\Delta x/2} e^{-x^2/2\rho_v^2} \, dx$$

$$= \frac{\rho_v}{\Delta x} \left[ \frac{\pi}{2} e^{-x_0^2/2\rho_v^2} \right] \left[ \operatorname{erf} \left( \frac{x_0 + \Delta x/2}{\sqrt{2} \rho_v} \right) - \operatorname{erf} \left( \frac{x_0 - \Delta x/2}{\sqrt{2} \rho_v} \right) \right],$$

$$\approx \frac{\rho_v}{\Delta x} B_p(x_0, y_0) \left[ \frac{\pi}{2} e^{-x_0^2/2\rho_v^2} \right] \left[ \operatorname{erf} \left( \frac{x_0 + \Delta x/2}{\sqrt{2} \rho_v} \right) - \operatorname{erf} \left( \frac{x_0 - \Delta x/2}{\sqrt{2} \rho_v} \right) \right],$$

(10)

where \(\rho_v = \theta_{pb,v}/2.355\) is the standard deviation of the primary beam at frequency \(v\), \(\theta_{pb,v}\) is the FWHM of the primary beam, and \(\Delta x = \dot{\theta} \Delta t\) is the slew of the antennas within time interval \(\Delta t\). The net effect of the smearing is an overall change in the flux densities, and the fractional error, \(B_{p,\text{eff}}/B_p\), is shown in Figure 2. We see from this figure that, for \(\Delta x < 0.3\theta_{pb}\), the fractional error is \(<2\%\). Also, according to this expression, the fractional error is independent of the \(y\)-coordinate (orthogonal direction to the motion of antennas).

As noted above, the OTFM smeared beam, and therefore the error introduced in the flux densities, is a function of frequency. Since the beam gets smaller with frequency, the error is larger at the top of the band (i.e., at higher frequencies) than the bottom of the band. Figure 3 shows the frequency dependence of the smeared beam relevant for the CNSS (\(\Delta x/\theta_{pb,v} = 0.36(v/3\,\text{GHz})\) per subscan; see Section 3.1).

2.3. Data Dump Time and OTFM Scan Rate

To avoid phase errors\(^\text{12}\) within the data dump time \(t_d\), it is necessary to have \(s_p(t)\) varying by a magnitude less than the distance associated with the tolerable aliasing (\(d_{\text{alias}}\); see Pety et al. 2001; Pety \& Rodriguez-Fernandez 2010) within this time interval. It requires the following condition to be met (Pety \& Rodriguez-Fernandez 2010):

$$t_d \ll \frac{d_{\text{alias}}}{d_{\text{max}} \omega_{\text{earth}}} \equiv t_d \ll \frac{6900 \, \text{s}}{\theta_{\text{alias}}/\theta_{\text{syn}}}$$

(11)

where \(d_{\text{max}}\) is the maximum baseline length and \(\omega_{\text{earth}}\) is the angular velocity of a spatial frequency due to the Earth rotation (7.3 \times 10^{-5} \, \text{rad s}^{-1}). \(\theta_{\text{alias}}\) and \(\theta_{\text{syn}}\) are the angular values corresponding to the FOV giving a tolerable aliasing, and the synthesized beam respectively.

Conversely, the lower limit to the dump time (and equivalently an upper limit on the OTFM scan rate) is set by the data rate, \(R\). For the VLA, \(R = 45 \times n_{\text{spw}} n_{\text{chan}} n_{\text{pol}}/16,384 \times t_d\). For the

\(^{12}\) See D’Addario \& Emerson (2010) for an analogous approach for estimating the coherence loss for a linear scan with a fixed phase center.
regular $S$ band setup, the number of spectral windows (SPWs) is $n_{\text{spw}} = 16$, channels is $n_{\text{chan}} = 64$ (2 MHz wide, over a 2 GHz bandwidth), and polarizations is $n_{\text{pol}} = 4$. This sets the lower limit of $t_d = 0.45$ s, assuming standard data rates (maximum rate of 25 MB s$^{-1}$).

2.4. Image Mosaic Construction

Standard imaging techniques are applicable to OTF data, and the dirty image is the Fourier transform of visibilities described in Equation (2). The image mosaic for OTF observations can be constructed through joint mosaicking or linear mosaicking of all scans within a region of interest. In joint mosaicking, the $uv$ data of all the scans of interest are gridded together using the aperture function and then deconvolved. In linear mosaicking, each scan is imaged separately and later combined using primary beam weights.

Either the smeared beam ($B_{\text{eff}}$) or the actual beam ($B_{\nu}$) can be used for primary beam correction. Some amplitude error will be expected$^{13}$ by the use of either of these beams, as described in Section 2.2, unless the data within each dump time is corrected with the appropriate smeared beam. Note that there are additional sources of amplitude error, resulting from antenna pointing error and error in the absolute flux scale calibration, amounting to $\sim 5\%$ (e.g., Thyagarajan et al. 2011; Mooley et al. 2013). Taken in quadrature together with the OTF smearing error, the amplitude errors should be $\sim 5\%$--$15\%$ for OTF observations (the maximum error occurring due to the use of the actual beam rather than the smeared beam; assuming $\Delta x/x_{\text{ph},\nu} < 0.5$), with the most severe errors seen in sources that are well beyond the half power point of the primary beam throughout the OTF scans.

$^{13}$ The thermal rms noise continues to follow the radiometer equation, of course.

Figure 3. OTF smeared beam plotted as a function of frequency within the $S$ band. The plot shows the fractional change in the flux density with respect to the true flux density (colorbar at the right) when only a single, time invariant, primary beam correction (at the corresponding frequency shown on the $y$-axis) is applied to each scan. The $x$-axis is the same as in Figure 2. Parameters relevant for the CNSS ($\Delta x/x_{\text{ph},\nu} = 4'/(42^2/\nu_{\text{GHz}}) = 0.36(\nu/3$ GHz) per subscan) are used. See Sections 2.2 and 3.1 for details.

Unless the motion of the primary beam within the pointing (or scan) is taken into account, the flux densities are added linearly without any weighting, which might limit the dynamic range. Faster scanning rates are thus expected to be more limiting in dynamic range.

Currently, the pointing direction of the antennas is recorded at regular intervals and stored as a pointing table in the Science Data Model (SDM) format of the VLA observations. The motion of the antennas (i.e., the smeared beam) can be corrected in the imaging step with the CASA task $t$-clean using the pointing table, as briefly described in the following subsection. However, the pointing table feature was implemented in the VLA OTF observations starting in 2016, and for the CNSS there are no such tables in the SDM data files. The $\sim 5\%$--$15\%$ error is, however, acceptable for the primary science goal of the CNSS, which is finding highly variable and transient sources.

2.5. Joint Deconvolution and A-projection

Image-plane mosaicking does not account for the frequency dependence of the primary beam, thus introducing spectral (and therefore amplitude) errors. Mosaicking in the $uv$ domain (or joint deconvolution incorporating A-projection; e.g., Bhatnagar et al. 2008, 2013), where the Fourier transform of the beam of each antenna at different frequencies can be taken into account during the convolution step, is therefore preferred for wide-bandwidth OTF data. This method is currently available in $\text{clean}$ (using $\text{fmachine} =$ “mosaic”) and $t$-clean (gridded = “mosaic$^{\text{ft}}$”) tasks within CASA (version 5.3.0). In CASA, joint deconvolution is done on the dirty mosaic image (or residual) using an approximate point-spread function (PSF; using one for the OTF scans near the center of the image). Due to the approximate PSF used for all the scans, many Cotton–Schwab major cycles are carried out to correct for the errors from the minor cycle deconvolution stage. Currently, the primary beam correction (using the actual beam, not the smeared beam) is done for at every dump time for each baseline. Some amplitude errors will therefore be introduced if the beam is moving a large fraction within the dump time. A detailed description of imaging with the new CASA task, $t$-clean, and its application to OTF data will be given elsewhere (U. Rau et al. 2018, in preparation).

2.6. Effective Survey Speed

For a large OTF region covered, the raw survey speed is given by $SS = \Omega_{\text{ph}}/\tau$, where $\Omega_{\text{ph}} = 0.566\theta_{\text{ph}}$ is the area under the primary beam and $\tau$ is the on-source time required for reaching the desired point-source sensitivity, $\sigma$. Since CNSS is a broadband mosacikd survey, the effective (weighted arithmetic mean) frequency of the images, $\nu \simeq 2.8$ GHz, is different from the nominal observing (arithmetic mean) frequency, $\nu_{\text{obs}} \simeq 3.0$ GHz (Condon 2015). Here we have ignored the fact that some SPWs at the bottom of the band are lost due to satellite-induced radio frequency interference (RFI; see Section 3.3). The effective area under the beam therefore becomes $\Omega_{\text{eff}} = \Omega_{\text{ph}}(\nu) = 0.566\theta_{\text{ph}}$. The VLA primary beam (FWHM) as a function of frequency is approximately $\theta_{\text{ph},\nu} \simeq (42'/\nu)$ (Perley 2016). Thus, $\Omega_{\text{eff}} = 0.035$ deg$^2$. Now, the effective weighted system equivalent flux density (SEFD) over the VLA $S$ band is 350.7 Jy (E. Momjian 2018, private
communication). Therefore,
\[ \tau = \frac{(\text{SEFD})^2}{n_p \sigma^2 \eta^2 N(N-1)} = 7.45 \left( \frac{\sigma}{100 \text{ mJy}} \right)^2 \]

where \( N = 26 \) is the number of antennas, \( n_p = 2 \) is the number of polarization angles, \( \eta = 0.92 \) is the correlator efficiency. For the \( S \) band we therefore get,
\[ SS = 16.9 \text{ deg}^2 \text{ hr}^{-1}(\sigma/100 \text{ mJy})^{-2}. \]

3. CNSS Survey Design

3.1. Design of the OTFM Observations

The CNSS (project codes VLA/13B-370, VLA/15A-421, PI: G. Hallinan; see Mooley et al. 2016, for the pilot survey) is designed to survey the entire 270 deg² of the SDSS Stripe 82 region over five epochs. With the aim of characterizing the sub-nJy transient population, the required rms noise is 80 \( \mu \text{Jy} \) beam\(^{-1} \) (with natural weighting) per epoch. From Equation (13) we can calculate the survey speed as 10.8 deg² hr\(^{-1} \). For ease of dynamic scheduling, we designed individual scheduling blocks (SBs) to be of 3 hr duration. Each block was equipped with its own flux calibrator and polarization angle calibrator (C348), polarization leakage calibrator (C348), and nearby phase calibrators (see below).

In each hour we are able to survey 22.5 deg² (9º in R.A. and 2º5 in decl.) in 3 hr, including overheads. The on-target time per SB was 2.25 hr, and overhead was therefore 33%. Our coverage of Stripe 82 with OTFM was in the region \( \alpha \in [-50, 58] \) and \( \delta \in [-1.25, 1.25] \), divided into 12 SBs.\(^{14} \)

The desired rms noise requires an OTFM scan rate of \( \theta_\text{ant} \simeq \theta / \cos(0º) = 1' / s \). In order to get a fairly uniform sensitivity across the survey region, we chose a row separation of \( \theta_\text{obs} = \theta_{\text{ant}, 2.8 \text{GHz}} / \sqrt{2} = 10.6' \). This gives a normalized maximum deviation (see Equation (7)) of 0.05. We used 15 stripes to cover the decl. range of Stripe 82. At the scan rate chosen, each stripe took 0.25 minutes to get 9 minutes on-source integration (3% scan overhead\(^{15} \)). Groups of two stripes were interspersed with phase calibrator scans (with a single stripe left over in the block; typically 1 minute of overhead for every 20 minutes of OTFM).

There were extra observations of calibrators from adjacent blocks included to help link the blocks. This was a fairly conservative strategy, but control of calibration errors was important for the CNSS observing program, given the proximity to the Clarke Belt (see also Section 3.3).

In order to choose the data dump time, we refer to Equation (11). For a dynamic range of a few thousand, \( \theta_\text{dumps} / \theta_\text{ph} \simeq 5 \) (Table 4 of Pety & Rodríguez-Fernández 2010). Hence, and further using the parameters associated with the CNSS observations at a frequency of 3 GHz (\( \theta_{\text{ph}} \approx 1.3' \), \( \theta_{\text{syn}} \approx 20.5' \)) we arrive at, \( \Delta t \ll 1400 \text{s} / (\theta_{\text{ph}} / \theta_{\text{syn}}) \approx 4.2 \text{s} \). For the CNSS survey we have used a data dump time of 0.5 s for the first three epochs and 1 s for the final two epochs (due to data rate constraints; Section 2.3). This implies 30 dumps per primary beam (at 3 GHz; 0.5 s dumps). The fractional amplitude error in source flux densities introduced due to the motion of the primary beam within the dump time is <1%.

The correlator phase center was stepped every 4 s (i.e., every 4' or \( \Delta x / \theta_{\text{ph, p}} = 0.36 \) at 3 GHz). Each subscan was thus 4 s long and had the phase center same as the pointing center at the center of the subscan. This corresponds to a \( \lesssim 5% \) error in the flux densities of sources (within the 20% attenuation radius of the primary beam) due to the use of the antenna primary beam instead of the effective primary beam (see Figure 3). Note that, for the gain calibration observations, standard pointed mode observations are used.

3.2. Construction of the Observing Blocks via OTFSim

The CNSS is designed to be a pathfinder for future wide-field surveys with the VLA, and was therefore executed with completely dynamic scheduling. With the VLA dynamic scheduling, constraints can only be placed on the local sidereal time (LST); the exact date and start time of the observations cannot be predicted beforehand. This necessitated the design of observing blocks such that each block is self-contained, with the standard calibrator observations. Additionally,Stripe 82 being close to the Clarke belt, some azimuth (AZ) ranges need to be avoided to mitigate strong RFI due to satellite downlink signals. In order to determine the desirable LST ranges for our observations, we therefore wrote a Python-based program, OTFSim\(^{16} \) to simulate the position of the antennas in AZ and elevation (EL). Given a simple user input, OTFSim computes the entire sequence of an observing block, and allows the visualization of the antenna positions and optimization of block. It outputs the source list and schedules files that can be uploaded to the OPT of the VLA.

Figure 4 shows the plot of the AZ and EL simulated for one of our SBs executed on 2013 December 21. The assumed

\(^{14} \) Regions R1–R12, with each region spanning 9º in R.A. and 2º5 in decl.

\(^{15} \) For the CNSS, an OTFM scan required a “start-up” time of \( \sim 15–20 \) s at the beginning of a stripe and a “running-stop” overhead of 4 s.

\(^{16} \) Available via GitHub.
starting location of the antennas is R.A. and decl. of $0^\circ$, corresponding to AZ $\approx 100^\circ$ and el $\approx 10^\circ$ at the specified start LST of 18 hr. The blue line denotes the motion of the antennas during the observation. At the beginning of the observation, the antennas slew to a tertiary calibrator (denoted by magenta circles), J2101+0341, which is observed once at the beginning and once toward the end of the observation. A secondary calibrator (denoted by green circles), J2136+0041, is then observed, followed by the gain calibrator (red circles), J2212+0152. The survey region is then observed with OTFM interleaved with phase calibrator observations. At the end of the SB, the flux calibrator, 3C48, and the polarization calibrator, 3C84 are observed (black circles).

### 3.3. RFI Monitoring

Since Stripe 82 is close to the Clarke belt, radio observations are prone to severe RFI from satellites in geostationary and geosynchronous (GSO) orbits. Two SPWs, between 2.125 and 2.375 GHz are severely and irreparably affected by RFI from the Satellite Digital Audio Radio Service and satellite downlink. The RFI in the frequency range 3.62–4.00 GHz, which is also due to satellite downlink, is low level in amplitude, but it distorts the phase information quite significantly. GSO satellites seen by the VLA have not been individually characterized in terms of downlink frequencies and polarizations, but the locations of some of these satellites are known (Figure 4). The RFI in the gain calibrator (J2212+0152) observations from the region R3 epoch E1 of the CNSS (observed on 2013 December 21) is shown in Figure 5.

An anomalous effect of RFI on the amplitude gain values, called “gain compression,” was seen in the gain calibrator observations by Mooley et al. (2016). This anomaly, where the gain response is nonlinear and causes the amplitude gain values to decrease (by up to 30%) with respect to their true values, affects pointings that are very close to the Clarke belt (mostly declinations are between $-3^\circ$ and $-10^\circ$, but can also affect declinations up to $+8^\circ$). For the CNSS survey, we used gain calibrators far from the Clarke belt in order to avoid this gain compression issue.

To investigate RFI at different hour angles (HAs), we observed 10 hr in an HA at a decl. of $-4^\circ.5$ (near the satellite belt) with OTFM. Figure 6 shows the corresponding dynamic spectrum. Although there are some regions that seem relatively quiet for most of the HA range, more than half of the $S$ band is affected by severe RFI for a wide range of HAs. Most, but not all, of the resulting gain compression can be corrected using the switched power, since during gain compression the inverse gain amplitude is proportional to the switched power (see also Mooley et al. 2016).

### 4. OTFM Testing Results

In 2013, the VLA OTFM observing mode was offered in the Resident Shared Risk Observing (RSRO) program. For the CNSS we ran some tests in this mode as part of the RSRO program and subsequently, in 2016, some additional test data were taken for the VLASS. In the context of the primary science case for the CNSS, radio transient phenomena, here we give a brief description of the technical problems that were uncovered with OTFM observations. Some of these were solved and some still exist in the data.

The test observations were undertaken as part of VLA programs TRSR0015 and TSKY0001. We observed a bright phase calibrator source, J1229+0203 (3C273), with several back-and-forth OTFM scans. For most of the tests, we used dump time of 0.5 s at $S$ band and correlator phase center change every 6 arcmin (i.e., 15 dumps per primary beam, for scan rate of $1'\ s^{-1}$, and 12 dumps per phase center step).

#### 4.1. Data-recording and Source-tracking Issues

After calibrating the phases in the test data, we took the visibility data for each antenna, vector averaged all baselines, and inspected for amplitude versus time and phase versus time plots for RR and LL correlations (in CASA plotms). We recovered several issues in the data. (1) There were systematic phase errors on a fraction of the dumps on all antennas, such that the calibrated phases deviated from zero ($\pm 0.3^\circ$ and $10^\circ$), but can also affect pointings that are very close to the Clarke belt mostly declinations are between $-3^\circ$ and $-10^\circ$, but can also affect declinations up to $+8^\circ$). For the CNSS survey, we used gain calibrators far from the Clarke belt in order to avoid this gain compression issue.

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scan/stripe, the antennas were not yet up to tracking speed in spite of the backup scan used. As a consequence, the first few integrations in a row are likely to be flagged on most antennas. (7) In the VLASS test observations, ghost images of real sources were found in the image plane. This occurred due to correlator phase centers being incorrectly written into the dataset. This problem was fixed only in 2016. Although there may have been some extreme cases in the CNSS where this problem occurred, we expect only a few (or less) of the CNSS observations to be affected.

4.2. Flux Density and Source Position Issues Recovered by Comparing OTFM Mode Data with Standard Pointing Mode Data (Image Plane)

We compared the image mosaics and source catalogs from the CNSS survey, observed in OTFM mode, and the 50 deg² CNSS Pilot survey (Mooley et al. 2016), observed in standard pointing (PTG) mode. The necessary details of the observations, data processing, imaging, and source cataloging for both of these surveys are given in Mooley et al. (2016).

The ratios of flux densities of point-like sources¹⁷ between the CNSS (center frequency 3.0 GHz) and the CNSS Pilot survey (center frequency 2.8 GHz) are plotted as a function of R.A. and decl. in Figure 8. The ratio has a sinusoidal pattern, varying with decl., having an amplitude of ≤12% (i.e., ≤10⁰.⁰⁵). The decl. values of the crests and troughs of the pattern are consistent approximately with the half power points of the primary beam and the pointing centers, respectively, of the pointing locations of the CNSS Pilot survey (see Figure 1 of Mooley et al. 2016). This suggests that the pattern is arising largely (if not entirely) from the primary beam corrections applied to the OTFM, where we have used the VLA primary beam instead of the OTFM smeared beam, and PTG, where the old VLA primary beam was used instead of the narrower primary beam of the upgraded VLA (see Perley 2016). Once the sinusoidal pattern is corrected using the moving average (solid red curve in the top panel of Figure 8), the ratios of flux densities show a slight systematic effect (≤6%, i.e., 10⁰.⁰²⁵) as a function of R.A. This is shown in the bottom panel of Figure 8. We are currently investigating in more detail the cause of these offsets.

The positional offsets¹⁸ between the OTFM mode and PTG mode observations are shown in Figure 9. While no significant discrepancy is seen in decl., there appears to be systematic uncertainties in the R.A. by 0″2–0″6. The histogram of the

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¹⁷ We selected sources having a detection signal-to-noise ratio (S/N) > 7 and a ratio of integrated-to-peak flux density smaller than 1.5; see Mooley et al. (2016).

¹⁸ We note that, since we have used sources having an S/N > 7, the ~3″ synthesized beam implies an uncertainty in R.A. and decl. of ~0″2 or better.
R.A. offset is bimodal, with peaks at $-0.25^\circ$ and $0.55^\circ$, and this suggests that the R.A. offset may be a function of R.A. and/or decl. In Figure 10 we show the positional offsets of sources plotted as functions of R.A. and decl. The plots indicate that there are discrepant offsets, between $0^\circ$ and $0.5^\circ$, in the different regions as well as in decl. R5 is the most severely affected region. After the positional offsets were corrected for the discrepancies as a function R.A. (left panels of Figure 10; using the moving average shown as red curves in the figure), a sinusoidal pattern in the offset plotted as a function of decl. can be seen (right panels of Figure 10), similar to but less distinct than in the case of the ratio of flux densities (see above). The R.A. offset in region R3 (shown as black points in the top right panel of Figure 10) also shows a monotonic increase as a function of the decl. The CNSS Pilot survey covered only $50^\circ$ of Stripe 82, so in order to investigate the positional offsets over the entire Stripe 82 region we cross-matched our CNSS catalog of point-like sources with the FIRST survey catalog (version 12feb16; White et al. 1997). The corresponding positional offsets are shown in Figure 11. A similar trend as recovered with the OTFM versus PTG comparison is seen in this figure. R5 remains the most severely affected region, with offsets of $-0.5^\circ$. We explore the possible causes of the positional offsets in the next subsection.
the image cutouts for (a) a bright point source, (b) a double-lobe source, (c) an extended source and (d) faint point-like sources from the CNSS Pilot (2.8 GHz; Mooley et al. 2016), the CNSS (3.0 GHz; coaddition of epochs E1, E2, and E3), and the VLA Stripe 82 (1.4 GHz; Hodge et al. 2011) surveys.

4.3. Comparing OTFM Mode Data between Different Epochs

We also compared the single-epoch source catalogs from the CNSS survey with each other to investigate how the OTFM data compare between the different epochs. The necessary details of the observations, data processing, imaging, and source cataloging are given in Mooley et al. (2016).

The ratios of flux densities of point-like sources between the epochs E1 and E2 of the CNSS are plotted as a function R.A. and decl. in Figure 13. The ratios of flux densities show significant systematic offset from unity (0%–26%, i.e., ≤10⁻²⁶) as a function of R.A. and decl. in Figure 13. The ratios for the different regions are generally within 12% (i.e., ≤10⁻¹²), but for region R9 there is a large discrepancy, ∼25%, at decl. ≈ 0°6 (black points in the bottom panel of Figure 13). Manual inspection of the decl. ≈ 0°6 region reveals that epoch E2 image is noisy and has an slightly elongated beam. The flux density offset may be due to RFI-induced gain compression. This issue will be investigated further in CNSS Paper III.

The positional offsets between the OTFM epochs E1 and E2 are shown in Figure 14, where the different regions are color-coded. Although there are systematic offsets for most of the regions, the median offsets in R.A. and decl. are ≲0°25. Region R5 is an exception, where the offsets in R.A. and decl. are −0°4 and −0°7, respectively. It is likely that the positional offsets are caused by incorrect positions for some of the phase calibrator sources. For example, in the observing for region R5, the VLA calibrator J2323−0317 was used in epoch E1, while a bright source (quasar) from the VLA Stripe 82 survey (Hodge et al. 2011), J224730+000006, was used in epoch E2 (since J2323−0317 showed some indication for gain compression in E1). While J2323−0317 has an accurate source position, we have found that in the image plane J224730+000006 is offset by ∼0.8 arcsec with respect to its position reported by (Hodge et al. 2011). This is consistent with the offset seen in Figure 9. The epoch-to-epoch positional offsets in R5 also explains the severe offsets seen in the OTFM versus PTG comparisons (Section 4.2, Figures 10–11).

5. Summary and Discussion

We have developed and tested a new imaging capability for the VLA in which the antennas are driven at a non-sidereal rate and visibilities are recorded continuously. We find that OTFM observations significantly reduce the slew-and-settle overheads as compared with pointed observations requiring on-source time of less than ∼30 s per pointing. Through the use of newly developed imaging techniques in the CASA package, we have also demonstrated that the flux densities of sources can be reliably and accurately reproduced not only between two epochs observed using OTFM, but also between pointed observations and those observed with the OTFM technique.

The implementation of OTFM substantially improves the efficiency of conducting wide-field shallow surveys with the VLA. The VLA’s survey capabilities can be compared with Square Kilometre Array Pathfinders that are undergoing commissioning and will soon start science operations. As noted in Section 1, this includes the ASKAP (Johnston et al. 2008), the Apertif instrument on the WSRT (Röttgering et al. 2011; Adams et al. 2018), and MeerKAT (Brederode et al. 2016; Santos et al. 2016). The proper figure of merit for comparing different imaging interferometers is the survey speed (SS; Section 2.6), expressed as: SS ∝ BW × Ω (A_c / T_{sys})^{2} where BW is the bandwidth, Ω is the FOV, A_c is the total collecting area times the aperture efficiency, and T_{sys} is the antenna system temperature (Cordes 2008). For the VLA L band and S band we estimate19 the survey speeds to be about 15.3 deg² hr⁻¹ and 13.4 deg² hr⁻¹, respectively. It is OTFM that makes the VLA a competitive survey instrument, while ASKAP and Apertif achieve high SS values using phased array feeds, and MeerKAT employs large numbers of small diameter antennas having high A_c / T_{sys}.

OTFM opens up several new applications. In this work we have used OTFM for the CNSS, which was carried out primarily to search for long-duration transients.20 The large FOV that are required are driven primarily by the rarity of radio transients (e.g.,

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19 For details, see https://science.nrao.edu/facilities/vla/docs/manuals/obsguide/modes/mosaicking and Mooley et al. (2013).

20 We define slow or long-duration transients in accordance with literature as those having timescales >1 s. See http://www.tauceti.caltech.edu/kunal/radio-transient-surveys/ for an up-to-date list of radio surveys aimed at exploring slow transient phenomena.
surveys, which bring the observable transient population closer in optical counterparts. This tends to favor multi-epoch shallow surveys. This emphasizes the unique advantage of associating radio sources with galaxy searches therefore call for wide-field shallow surveys.

Figure 11. Same as Figure 10, but comparing the source positions in the full CNSS survey (OTFM mode) with those in the FIRST survey. See Section 4.2 for details.

Figure 12. Image cutouts from the OTFM (middle panels) and the PTG (left and right panels) mode observations agree very well. From left to right, the panels show cutouts from the CNSS Pilot (2.8 GHz; Mooley et al. 2016), the CNSS (3.0 GHz; coaddition of epochs E1, E2, and E3), and the VLA Stripe 82 (1.4 GHz; Hodge et al. 2011) surveys. This figure shows (from top to bottom) the comparisons for (a) a bright source CNSS J221947.2−005132 (300 mJy peak flux density, slightly resolved), (b) a double-lobe source CNSS J221155.6+000447 (15–20 mJy peak flux density, resolved), (c) an extended source CNSS J221830.3+001219, and (d) faint point-like sources (sub-mJy, cutouts centered on coordinates 22 16 27 −00 54 00). The color palette used is hot metal (white represents maximum flux density, orange is intermediate, and black is minimum), and in of the above cases the colorbar spans −1 to +4 mJy (white–black), −0.35 to +1.50 mJy, −0.7 to +3.0 mJy, and −50 to +500 μJy. Each cutout is 2′ × 2′ except for those in the bottom panels, which are 6′ × 6′. See Section 4.2 for details.

Mooley et al. 2016; Murphy et al. 2017). Likewise, recent near-real-time surveys (Ofek et al. 2011; Mooley et al. 2016) have stressed the unique advantage of associating radio sources with optical counterparts. This tends to favor multi-epoch shallow surveys, which bring the observable transient population closer in distance, improving the ability to find optical/infrared counterparts and to characterize host galaxies and/or progenitors. Radio transient searches therefore call for wide-field shallow surveys.

OTFM has also been applied in an all-sky continuum survey and in the search for the electromagnetic counterparts of gravitational waves (GW). The VLASS is using OTFM to efficiently survey the entire sky in the continuum band between 2 and 4 GHz above a decl. of −40° with a resolution of 2′/5 (Myers et al. 2017). In the recent binary neutron star merger event GW170817, radio observations played a key role in the study of the afterglow component (Hallinan et al. 2017; Margutti et al. 2018; Mooley et al. 2018b). However, looking ahead to the near future, while the sensitivity of existing GW detectors will be improved, the median sky localizations will remain ~150 deg² (Abbott et al. 2016). These large, elongated error regions lend themselves well to OTFM. In Mooley et al. (2018a), we carried out a successful proof-of-concept demonstration toward the binary black hole merger event GW151226, using OTFM to image a 100 deg² region over three epochs separated by 1.5 and 6 months post-merger. OTFM of the entire error region will not likely be as efficient as optical/UV searches for the thermal kilonova component, nor will they be as optimal as using volume-limited galaxy searches (e.g., Singer et al. 2016) but it occupies a valuable
Figure 14. Scatter plot of the positional offsets of point-like sources in R.A. and decl. between CNSS epoch 1 and epoch 2 (observed in OTFM mode). The different regions (R1–R12) of CNSS, observed in different scheduling blocks with the VLA, are color-coded (see legend below). The panel to the top and panel to the right are histograms of the R.A. offset and decl. offset, respectively. There are systematic offsets of ≲0'075 in R.A. and decl. for most of the regions. For region R5 the offsets are severe, −0'04 and −0'07 in R.A. and decl., respectively. The positional offsets are likely due to inaccurate coordinates used for the phase calibrator pointings. See Section 4.3 for details.

niches. As noted in Mooley et al. (2018a), there will be GW events with solar/lunar constraints, events that occur in obscured environments, incomplete galaxy catalogs, and faint or non-existent kilonova signals (e.g., double neutron star mergers with large binary mass; Metzger 2017). In these cases blind radio searches of the GW localization, aided by valuable “before” images from the VLASS (or OTFM observations immediately after the merger), may be our best hope at detecting the afterglow signature of a GW event.

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Appendix

OTFSim is similar to SCHED used for VLBA, in some respects. The algorithm for the simulator script is relatively straightforward:

1. Start the antennas at an arbitrary AZ and EL. Count the time and for each time increment check the user-specified order of scans for the following.
2. If a calibrator is to be observed next, then slew to the current AZ and EL of that calibrator source and track the source for the user-specified duration.
3. If OTFM observations to be carried out next, then slew to the required part of the survey region, then slew the antennas across a single stripe in R.A. along constant decl. with a user-specified slew speed. Repeat the slew in adjacent stripes until the user-specified duration is complete.

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