Experimental Study of Diesel Engine Power Test Based on the No-Load Power Measuring

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Abstract: In view of the fact that the traditional dynamometer can not test diesel engine power in the production site, based on the principle of No-Load Power Measuring, a mathematical model between the maximum power of diesel engine and crankshaft speed, equivalent moment of inertia and acceleration time was established. And a set of diesel power test system was set up in which the NET2801 data acquisition card is the core. The time-speed curve of the diesel engine acceleration and deceleration process is obtained by MATLAB software programming. The equivalent moment of inertia and the maximum power of the diesel engine are deduced. The reliability of the test method is verified and the cause of the error is analyzed, which provides a research idea to improve the field test accuracy of diesel engine power.

Keywords: diesel engine power; No-Load Power Measuring; equivalent moment of inertia; Instantaneous speed

1. Introduction

As an important power equipment for drilling wells, the maximum power value of the diesel engine will decrease with the increase of the use time¹. The best way to master the overall technical condition of a diesel engine is to measure its existing maximum power². The traditional power test instrument³ is generally a dedicated test bench that is fixed in the room. It need to carry the diesel engine from the production site after the demolition back to the test center when testing, which is time consuming and costly. The No-Load Power Measuring⁴ is a convenient and quick power test method, which do not need a dedicated test bench and can be applied to diesel engine in the production site. The research of No-Load Power Measuring rose in the automotive industry⁵. When the engine is idling, the throttle is suddenly added to the maximum position. At the same time, the instrument is used to continuously acquire the amount of change in crankshaft speed and the effective power is expressed by the acceleration power. According to the principle of No-Load Power Measuring in this paper, the maximum power calculation model was established, and the corresponding power test system was developed. The power test system was used to test the maximum power of the diesel engine in production site, and the power test results were analyzed, which provides a research direction for further improving the stability and calculation accuracy of power test.

2. Principle of No-Load Power Measuring of diesel engine

2.1 Test principle of equivalent moment of inertia of diesel engine

The equivalent moment of inertia is a necessary parameter for No-Load Power Measuring⁶, which represents the sum of the moment of inertia of all rotary motion parts centered on the crankshaft. At present, there are several main measurement methods, namely, Calculation Method⁶, Instantaneous Speed Method⁷, No-Load Deceleration Method⁸ and Additional Mass Method⁹. It is necessary to know the parts size and material of diesel engine when using the Calculation Method, and the calculation process is cumbersome and difficult. When using the Instantaneous Speed Method and No-Load Deceleration Method, the diesel cylinder pressure needs to be measured, but there is no way to install a pressure sensor because there is generally no pressure test hole on the diesel engines in production site.

In this paper, the practical Additional Mass Method is used to test the equivalent moment of inertia of diesel engine. Its principle is as follows.

\[
J' = \frac{\frac{dn}{dt} - \frac{dn}{dt}}{\frac{dn}{dt} - \frac{dn}{dt}}
\]

Where, \( J' \) is the equivalent moment of inertia of diesel engine, kg·m²; \( \frac{dn}{dt} \) is the speed acceleration of diesel engine, t/min · s. \( J' \) is the moment of inertia of the additional mass, kg · m²; \( \frac{dn}{dt} \) is the speed acceleration of diesel engine with the additional mass, t/min · s.

According to the Equation (1), the equivalent moment of inertia of the diesel engine can be obtained by measuring the
speed acceleration of the diesel engine during the free
deceleration process and the speed acceleration of the diesel
engine with the additional mass.

1.2 Power test principle

There are two power calculation models in the principle of
No-Load Power Measuring, one of which is to calculate the
instantaneous power, the other is to calculate the average
power. The instantaneous power calculation model is shown in Equation (2).

\[ P_e = K_1 \cdot \frac{\pi L}{9550 \times 30} \cdot n \cdot \frac{dn}{dt} \]  

(2)

Where, \( P_e \) is the instantaneous power at the speed \( n \) of
the diesel engine during acceleration, kW. \( n \) is the
instantaneous speed of diesel engine, \( r/min \). \( K_1 \) is the
Power correction factor.

According to the Equation (2), in order to obtain the
maximum effective power, it is necessary to know the
acceleration at the rated speed during the crankshaft
acceleration process. However, when diesel engine is
accelerated to near the maximum speed, the acceleration at
the rated speed is difficult to obtain as the speed
acceleration value has been reduced. Therefore, this
calculation model is not used in this paper.

The average power calculation model is shown in Equation
(3).

\[ P_{\text{max}} = K_2 \cdot \frac{j \pi^2 (n_2^2 - n_1^2)}{1800000 \Delta T} \]  

(3)

Where, \( P_{\text{max}} \) is the maximum power of diesel engine after
the correction, kW. \( n_1 \) is the starting speed in the
measuring range, \( r/min \). \( n_2 \) is the ending speed in the
measuring range, \( r/min \). \( \Delta T \) is the acceleration time from
speed \( n_1 \) to speed \( n_2 \), s. \( K_2 \) is the Power correction
factor.

Under the condition of already knowing the equivalent
moment of inertia \( J \), we can calculate the average power
of the diesel engine as long as we know starting speed \( n_1 \)
and ending speed \( n_2 \) and its corresponding time
increments \( \Delta T \). And the maximum power is the value of
the average power calibrated by the power correction factor
\( K_2 \). Therefore, the average power calculation model is the
theoretical basis of this paper.

3. Design of the power test system

According to the principle of No-Load Power Measuring,
the acceleration and deceleration test only need to be carried
out after installing an additional mass with known moment
of inertia, the diesel engine power can be measured. And the
acceleration and deceleration test is to test the instantaneous
speed signal during the acceleration and deceleration process\(^{[11]}\).

The design of the additional mass is to be followed by
principles such as ease of manufacture, ease of calculation,
small air friction and better balance. According to this, the
ring-shaped additional mass as shown in Figure 1 was
designed in this paper, which is installed in the diesel
flywheel end.

![Figure 1: Shape of the additional mass](Image)

![Figure 2: Block diagram of the power test system](Image)
A data acquisition instrument is NET2801 data acquisition system. The magnetoelectric speed sensor is installed in the diesel engine test hole, and its distance from the flywheel tooth tip is kept at 2~4mm. When diesel engine is running, the sensor output signal is periodically changed. The output signal is filtered and shaped by signal conditioning board to obtain the pulse signal as shown in Figure 3. Each pulse signal corresponds to the teeth of the flywheel. The time between each two pulse signals is calculated from the clock frequency and count value between the two pulses, so that the instantaneous speed of the crankshaft is obtained. 

4. Analysis of test results

Three different types of diesel engines in the drilling site were selected to perform the maximum power test. The test process is divided into two parts: test of equivalent moment of inertia and power test. The specific parameters of three diesel engines are shown in Table 1. After the test experiment is completed, the digital pulse signal is converted to the diesel engine speed curve for subsequent processing by MATLAB software.

![Image of measurement principle of magnetoelectric sensor](image)

**Figure 3: Measurement principle of magnetoelectric sensor**

**Figure 4: Non-load deceleration curve of diesel engine**

**Figure 5: Deceleration curve after installing the additional mass on diesel engine**

3.1 Analysis of test results of equivalent moment of inertia

When calculating the speed acceleration value, a speed curve with good linearity was selected in MATLAB software firstly. And then, as shown in Figure 4 and Figure 5, the acceleration value can be obtained by simple calculation \( \frac{\Delta n}{\Delta T} \) according to the speed difference \( \Delta n \) between starting speed and ending speed and corresponding time interval \( \Delta T \).

![Image of data acquisition instrument](image)

3.1.1 Technical parameters of diesel engines

| Model number | Rated power(kW) | Rated speed(r/min) | Number of cylinders | Years of service |
|---------------|-----------------|--------------------|---------------------|-----------------|
| BG12V190PZLG3| 810             | 1300               | 12                  | 1               |
| CAT 3406      | 269             | 1800               | 6                   | 4               |
| CAT 3408      | 354             | 2100               | 6                   | 12              |

![Table 1: Technical parameters of diesel engines](image)

3.1.2 Test results of equivalent moment of inertia of diesel engine

The speed curves with good linearity from 530r/min to 580r/min were selected to calculate the acceleration value for three kinds of diesel engines in Table 1. The calculation results of acceleration value and equivalent moment of inertia are shown in Table 2.

| Model number | Number of test times | No-load deceleration value (r/min - s) | Deceleration value with additional mass(r/min - s) | Equivalent moment of inertia (kg - m²) | Average value (kg - m²) | Coefficient of Variation |
|---------------|---------------------|----------------------------------------|-----------------------------------------------|---------------------------------------|------------------------|--------------------------|
| BG12V190PZLG3| 1                   | -182.235                               | -152.863                                      | 31.220                                 | 30.321                 | 1.74%                    |
|               | 2                   | -180.870                               | -150.612                                      | 29.866                                 | 30.142                 | 9.02%                    |
|               | 3                   | -181.121                               | -151.053                                      | 30.142                                 | 30.057                 | 1.74%                    |
|               | 4                   | -180.981                               | -150.865                                      | 30.057                                 | 30.057                 | 1.74%                    |
| CAT 3406      | 1                   | -218.554                               | -184.270                                      | 10.750                                 | 12.268                 | 9.02%                    |
|               | 2                   | -220.036                               | -188.430                                      | 11.924                                 | 12.268                 | 9.02%                    |

![Table 2: Test results of equivalent moment of inertia of diesel engine](image)
According to the calculation results in Table 2, it can be seen that the acceleration values of BG12V190PZLG-3 diesel engine in four tests are less discrete during the same speed range, and the calculated equivalent moments of inertia of diesel engine are relatively stable. The coefficient of variation is only 1.74% and test results are good. The acceleration values of CAT3406 diesel engine in four tests fluctuate slightly during the same speed range, and the calculated equivalent moments of inertia of the diesel engine are between 10.750 kg·m² and 13.808 kg·m². However, the minimum calculated result of equivalent moment of inertia of CAT3408 diesel engine is 10.906 kg·m² and the maximum value is 26.137 kg·m², which indicates that the discretization of results is very serious. By comparing the speed curves of four tests, it can be seen that the curve coincidence degree is low and the randomness is large. Therefore, the equivalent moment of inertia of this diesel engine can not be determined accurately.

After analysis, the factors that affect the test accuracy of equivalent moment of inertia are as follows.

(1) Years of service
When testing, the BG12V190PZLG-3 diesel engine was only used for one year, and the technical condition was good. There is a high degree of coincidence for speed curves during many tests. And thus the calculated moment of inertia is stable and reliable. However, CAT3408 diesel engine has been serving for 12 years in the drilling site, which means a long period of continuous work and many different levels of maintenance. Due to a variety of factors such as mechanical wear and poor lubrication, the stability of speed curve is poor. The calculated speed acceleration value fluctuates greatly and a uniform moment of inertia value can not be obtained under this test method.

(2) System error of time interval $\Delta T$
In the actual measurement, the speed $n$ is the average speed after a certain angle, rather than the instantaneous speed of a moment. There may not be exactly the speed of 530r/min and 580r/min during the sampling process, then starting time and ending time of the time interval $\Delta T$ will appear random error, which has an impact on the calculation of speed acceleration.

(3) Test error caused by operation
When diesel engine is running, there is a large vibration on engine body. If the speed sensor can not be installed firmly, it can not collect a complete and accurate signal, which will have a direct impact on the measurement of speed. If the warm-up time of diesel engine is insufficient before the test, the lubricant temperature does not reach normal operating temperature and the deceleration process speed curve can not be measured accurately. In order to eliminate the error caused by the test operation, we can solve it by repeated measurements.

3.2 Analysis of diesel power test results

The no-load acceleration curve of diesel engine is shown in Figure 6. A speed curve with good linearity was selected to calculate the average power and the maximum power can be obtained by calibrating the average power. According to the Equation (3), it is important to measure the stability of the acceleration values.
calculation results \( \frac{n_2^2 - n_1^2}{\Delta T} \) in the acceleration process. The test data processing results are shown in Table 3 after substituting the corresponding moment of inertia in Table 2.

### Table 3: Data processing results of no-load acceleration

| Model number | Serial number | Starting and ending time(s) | Starting and ending speed(r/min) | \( \frac{n_2^2 - n_1^2}{\Delta T} \) (r\(^2\)/s\(^3\)) | Average power(kW) |
|--------------|---------------|-----------------------------|----------------------------------|---------------------------------------------|-------------------|
| BG12V190     | 1             | 0.542                       | 807.749                          | 424.793                                     | 689.775           |
|              | 1             | 1.212                       | 1295.013                         |                                             |                   |
|              | 2             | 0.281                       | 811.605                          | 424.736                                     |                   |
|              | 2             | 0.953                       | 1298.547                         |                                             |                   |
|              | 3             | 0.328                       | 818.567                          | 426.371                                     |                   |
|              | 3             | 0.998                       | 1303.249                         |                                             |                   |
| PZLG-3       | 1             | 6.017                       | 1063.022                         | 897.041                                     | 211.146           |
|              | 1             | 6.848                       | 1952.580                         |                                             |                   |
|              | 2             | 6.064                       | 1138.211                         | 888.691                                     |                   |
|              | 2             | 6.658                       | 1787.995                         |                                             |                   |
|              | 3             | 6.027                       | 1082.753                         | 897.676                                     |                   |
|              | 3             | 6.661                       | 1794.872                         |                                             |                   |
| CAT 3406     | 1             | 0.927                       | 964.187                          | 636.734                                     | 203.026           |
|              | 1             | 1.769                       | 1690.821                         |                                             |                   |
|              | 2             | 0.945                       | 984.529                          | 649.780                                     |                   |
|              | 2             | 1.762                       | 1696.970                         |                                             |                   |
|              | 3             | 0.869                       | 913.242                          | 618.699                                     |                   |
|              | 3             | 1.550                       | 1515.152                         |                                             |                   |
| CAT 3408     | 1             | 1657.849                    | 1894.872                         | 636.734                                     | 203.026           |
|              | 1             | 1690.821                    | 1794.872                         |                                             |                   |
|              | 2             | 1696.970                    | 1787.995                         |                                             |                   |
|              | 2             | 1690.821                    | 1787.995                         |                                             |                   |
|              | 3             | 1696.970                    | 1787.995                         |                                             |                   |

It can be seen from the calculation results of \( \frac{n_2^2 - n_1^2}{\Delta T} \) in Table 3 that the average power calculation has a small range of fluctuations, and there is still a systematic error effect of the time interval \( \Delta T \).

But the degree of dispersion of calculation results is small. It is feasible to test the maximum power of diesel engine at production site, which indicates that the average power calculation model is feasible both in theory and practice.

### Conclusion

According to the principle of No-Load Power Measuring, a practical power test system has been developed for the diesel engine at production site. It has been proved through many field tests that the No-Load Power Measuring technology can achieve the measurement of the maximum power in the case of non-demolition for diesel engine, but there is also a need for further optimization. In order to improve the accuracy and stability of diesel engine power test, the following two optimization must be carried out on the basis of the existing technology.

1. It is necessary to find a way to easily and accurately determine the equivalent moment of inertia of old diesel engine.
2. It is necessary to perform appropriate data smoothing and data fitting on the instantaneous speed signal to eliminate the systematic error of the time interval \( \Delta T \).

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