Particle Mass Spectrometer (PMS) and its Application to Nano-Particle Sizing in Various Systems†

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Abstract

Particle mass spectrometry has been shown to be an effective diagnostic technique to determine particle size and size distribution of charged nano-particles originating from different reactive sources. In the present paper, the principle of the PMS is described in detail and examples of application to various particle formation systems are presented. A spark generator, a microwave reactor, and a low-pressure premixed flame burner were used to produce particles of different materials in different size ranges between 1 and 10 nm. The resolution and sensitivity of the PMS has been improved by the adaptation of a preamplifier consisting of a secondary electron multiplier coupled to an external conversion dynode. The particle mass – being the main parameter of the measurements – is not influenced by the additional acceleration due to the conversion current. The use of a secondary electron multiplier leads to a signal gain of $10^4$ compared with measurements without the preamplifier.

Introduction

A large number of commercial powders, e.g. for the semiconductor industry, pigments, carbon blacks, and high-purity materials for optical fibers and thin films, are produced via aerosol routes, see for example [1]–[4]. The control of the process is necessary in order to determine the powder characteristics and to specifically influence the properties of the product particles, [5]. Consequently, in-situ analysis is desired to follow the formation process and to control the characteristics of the particles. Available techniques for sizing and detecting aerosol particles are often limited to operation near atmospheric pressure (e.g. differential mobility analyser, condensation nuclei counter, diffusion batteries, etc.). Furthermore, most of the methods require sampling and dilution prior to analysis [6], which may change the powder characteristics. It is thus necessary to realize a continuous sampling method which has no effect on the particle characteristics which is effective in size determination.

Molecular beam sampling, which is widely known from conventional time-of-flight mass spectrometry, can fulfill the requirements of almost undisturbed, continuous sampling, thus giving a clear image of the reactive environment in the probe. Disturbances are avoided by an expansion into the free-molecular regime with coinciding rapid freezing of the sample. The particle mass spectrometer described here [7] allows the determination of the particle size and size distribution by combining measured particle kinetic energy and particle velocity. In contrast to the particle beam mass spectrometer used by Ziemann et al. [8], the PMS does not require any calibration and is applicable for particles down to 1 nm and large molecules.

Measurement Principles

The basic principle of the particle beam mass spectrometer is the behavior of charged particles in an electric field. The situation is shown schematically in Fig. 1. The particle beam enters a uniform electric field in a capacitor of length $l_c$ and width $b_c$ supplied with a voltage $U_c$. The lines of force of the electric field are assumed to exist only inside the capacitor and to be perpendicular to the electrode surfaces. The field strength therefore is $E = U_c / b_c$. An individual charged particle entering the capacitor is deflected by a force $F_y = zeU_c / b_c$. It causes an acceleration in the y-direction in relation to its mass $m_p$.

The trajectories of the particles inside the capacitor can be described as follows:

$$y_p = \frac{1}{2} \frac{z\cdot e\cdot U_c}{m_p b_c} \cdot t^2$$

$$x_p = v_p \cdot t$$

(1)

$$\dot{y}_p = \frac{z\cdot e\cdot U_c}{m_p b_c} \cdot t$$

$$\dot{x}_p = v_p$$
After leaving the capacitor, the particles move along straight lines as indicated on the left side of Fig. 1. Assuming constant velocity components \( y_p \) and \( x_p \), the trajectory of an individual particle is therefore given by:

\[
y_p = \frac{z \cdot e \cdot U_e}{m_p \cdot v_p^2} \cdot \frac{l_c}{b_c} \left( x_p - \frac{l_c}{2} \right) \quad \text{for} \quad x_p \geq l_c. (2)
\]

Since every particle of mass \( m_p \) and charge \( z \) has its individual trajectory, the originally uniform and well-focused particle beam is split up into a fan-shaped beam. The mass classification is now realized by introducing a "monochromator" slit which selects particles of one distinct mass whereas the others are blocked. The slit is located at a distance of \( x=l \) downstream of the capacitor, has a slit width \( \Delta d \), and a position \( y=d \) from the beam axis. By rearranging Eq. (2) and introducing \( y_p=d \) and \( x_p=l \), the kinetic energy selecting operation of the whole arrangement is:

\[
E_{kin} = \frac{m_p}{2} \cdot \frac{v_p^2}{z \cdot e} = U_c \frac{l_c}{b_c} \left( \frac{2 \cdot l_c}{d} - \frac{l_c}{d} \right). (3)
\]

The equation above indicates that for known values of \( l_c, b_c, d, \) and \( l \), the voltage \( U_c \) selects particles of kinetic energies \( m_p \cdot v_p^2/2 \) carrying \( z \) elementary charges. By varying the deflection voltage \( U_c \), particles of various kinetic energies can be made to pass the "monochromator" slit. Thus:

\[
U_c = \text{const.} \cdot \frac{m_p}{z \cdot e} \cdot \frac{v_p^2}{2}. (4)
\]

The particle mass \( m_p \) can be determined from the deflection voltage \( U_c \), if the velocity of the particles is known. The set-up shown on the right side of Fig. 1 is used to measure the required velocity of the particles. The selected beam of charged particles passes two grids supplied with a synchronously pulsed repelling potential. The upper grid forms packages of length \( l_p \) which depend on the frequency \( f \) of the grid voltage and the particle velocity \( v_p \). Only very few or no particles can pass the second grid if the particle package length \( l_p \) is an odd-numbered multiple of the distance \( l_c \) between the grids. By changing the frequency of the deflection voltage \( U_c \), a fluctuating particle current with maxima and minima is obtained. These minima and maxima of the particle current \( I_p \) obey the following conditions:

\[
v_p = 2 \cdot f_{\text{min},i} \cdot l_p, i = l_c, l_c/3, l_c/5, \text{etc.} (5)
\]

Combination of Eqs. (4) and (5) leads to

\[
U_c = \text{const.} \cdot \frac{m_p}{z \cdot e}. (6)
\]

The resultant signals are current/voltage spectra of the kinetic energy of the particles. From the principle of the particle mass spectrometer (PMS), it is also clear that the current/voltage spectra are not the probability density function (PDF) of the particle mass or the kinetic energy, because the sensitivity of the PMS depends on the deflection voltage. Roth and Hospital [9] have shown the following relation between the measured particle current, the deflection voltage \( U_c \), and the PDF to be valid:

\[
\text{PDF}(m_p) = \text{const.} \cdot \frac{I(U_c)}{U_c}. (7)
\]

The realization of the particle mass spectrometer is schematically shown in Fig. 2. It consists of a molecular beam sampling system by which a small sample taken from the respective aerosol generator is supersonically expanded through a silver-plated and electrically grounded glass nozzle \( a \) into a vacuum chamber where the pressure is kept at about \( 10^{-3} \) mbar. The supersonic free jet formed by the nozzle expansion flow contains both particles and gas molecules. The flow conditions are such that the gas temperature decreases very rapidly, freezing any physical and chemical reactions inside the expanding sample almost completely. The center of the free jet is extracted by a sharp-edged skimmer \( b \) and moves as a "particle-loaded" molecular beam into the second vacuum chamber. The molecular beam is directed through a
deflection capacitor $c$, where charged particles are deflected from the beam axis and analysed due to their kinetic energy, as described above. The particles deliver their charge to a Faraday-Cup $e$, which is connected to an ultra-sensitive amplifier $f$.

In order to improve the sensitivity of the PMS, a third vacuum chamber $d$ is added to the PMS. The pressure in this chamber was maintained at about $10^{-4}$ mbar by a turbomolecular pump in order to obtain a further signal amplification compared with the Faraday-Cup. It consists of a conversion dynode $h$ and a secondary electron multiplier $i$. The dynode is supplied with a high positive voltage of 15 to 20 kV. This high electric field accelerates negatively charged particles from an initial kinetic energy of some hundred eV to some keV. The energy of the particles is then high enough to produce secondary electrons or ions when impacting on the surface of the dynode. The secondary charge carriers are further accelerated towards the cathode of the secondary electron multiplier which consists of 17 dynodes, causing an exponential electron increase by a factor of about $10^8$ to $10^9$. The generated current can be further amplified by an ultra-sensitive amplifier $k$.

**Experimental Study and Results**

In this study, four different types of particle sources have been connected to the PMS, and the respective mass evolutions of the nano-sized particles have been studied in:

- premixed low-pressure $\text{H}_2/\text{O}_2/\text{Ar}$ flames doped with $\text{SiH}_4$ to produce SiO$_2$ particles,
- a spark generator to produce charged particles at different spark frequencies $10 \text{ Hz} \leq f \leq 1000 \text{ Hz}$ from different materials,
- a microwave plasma burning in $\text{C}_2\text{H}_2/\text{Ar}$ mixtures to generate nano-sized soot particles,
- premixed low-pressure $\text{C}_2\text{H}_2/\text{O}_2/\text{Ar}$ flames to produce soot particles.

In the case of soot particle formation in low-pressure hydrocarbon flames, Faraday-Cup measurements were compared with results obtained from secondary-electron multiplier measurements.

In the first series of experiments, the PMS was connected to a low-pressure flame reactor. Mixtures of hydrogen, oxygen, and argon were doped with small amounts of $\text{SiH}_4$ to produce ultrafine silica particles [10]. The pressure was held between 25 and 30 mbar providing an extended reaction and particle formation zone, thus ensuring a higher spatial resolution. The gases were premixed and supplied to the burner head by mass-flow controllers. The low-pressure burner was movable in the horizontal direction to vary the distance between the burner head and the probing nozzle, i.e., the flow coordinate $\xi$. Examples of simultaneously measured current/voltage spectra and current/frequency spectra of positively charged particles, from which the particle mass can be determined, are shown in Fig. 3. Samples containing silica particles were taken from the low-pressure burner at a flow coordinate of $\xi=60$ mm. The flame conditions are given in the figure caption. The upper part of Fig. 3 shows the particle current measured with the Faraday-Cup as a function of the deflection voltage. The curve shows one distinct maximum at $U_c=11$ V. According to Eq. (6), the deflection voltage can be directly related to the particle kinetic energy. For a singly charged particle, a voltage of $U_c=11$ V results in a kinetic energy of $E_{\text{kin}}=4.7 \cdot 10^{-17}$ J. The measurement for the
determination of the particle velocity shown in the lower part of Fig. 3 was performed for particles deflected at $U_c=11$ V. The measured currents plotted as a function of the frequency of the repelling grid's voltage exhibit minima at $f_{\text{min1}}=1.3$ kHz, $f_{\text{min2}}=3.9$ kHz, and $f_{\text{min3}}=6.5$ kHz. Applying Eq. (5) leads to a particle velocity of about 650 m s$^{-1}$. Combination of Eq. (4) and (5) results in a mean particle mass of $22 \times 10^{-20}$ g, from which in turn a mean particle diameter of $d_p=5.4$ nm can be determined, assuming a density for the silica particles of $\rho=2.65$ g cm$^{-3}$.

Fig. 4 summarizes the measured mean particle mass as a function of the flow coordinate (upper part) and as a function of the precursor concentration (lower part) for the SiH$_4$-doped flames. The pressure was kept constant at $p=30$ mbar, the velocity of the unburnt gases was $v_u=1.32$ m s$^{-1}$, $H_2/O_2=1.69$, and the ratio of the inert gas to the fuel gases Ar/(H$_2$+$O_2$) =1.36 and 1.04, respectively. As can be seen in the upper part of Fig. 4, particles formed in the hotter flame (open triangles) show an evolution of the mean particle mass from about $m_p=10 \times 10^{-20}$ g at $\xi=20$ mm to about $m_p=22 \times 10^{-20}$ g at $\xi=70$ mm, whereas the particles generated in the cooler flame (closed symbols) are smaller by a factor of about 1.7. The mean particle mass was measured at three different positions in the flame as a function of initial precursor concentration, see lower part of Fig. 4. The dependence of mean particle mass on the sampling position is not very distinct in the range $20 \text{ mm} \leq \xi \leq 40$ mm, whereas it is obvious that the mean mass increases with increasing initial concentration of the dopant.

In the next series of experiments, the PMS was applied to particles generated by a spark generator using three different types of electrode materials. Conventional spark plug material was operated at atmospheric pressure, a silver electrode was used at 400 mbar, and for glassy carbon (Sigradur-G), the pressure was held between 20 and 30 mbar. Fig. 5 shows results of the measured probability density of the particle diameter obtained from the three materials at a spark frequency of $f=1000$ Hz. All particles show a very narrow size distribution with mean particle sizes between 2 and 4 nm. Fig. 6 shows the dependence of particle size on both the spark frequency and the ignition voltage. The mean particle diameter...
increases slightly from 2.2 nm to 2.6 nm with spark frequency for normal spark material (open circles), and decreases from 4.5 nm to 4.2 nm for Sigradur-G, see upper part of Fig. 6. For silver electrodes, the frequency has almost no influence on the particle size. On the other hand, the ignition voltage and thus the spark energy is the main parameter determining the mean size of the silver particles, see lower part of Fig. 6. The mean size shows linear behavior, increasing from 3.1 to 3.4 nm.

Next, soot particles formed during pyrolysis of a C2H2/Ar mixture in a microwave reactor were investigated. Fig. 7 shows the measured probability density function of the particle diameter for negatively and positively charged particles. According to Fig. 7, the mean diameter for both polarities is almost the same, but the standard deviation is slightly different. An increase in the flow velocity of the C2H2/Ar mixture through the microwave reactor causes a decrease in the residence time of the particles in the reaction zone. Fig. 8 shows the expected trends of decreasing particle diameter with increasing mixture volume flow.

The last series of experiments was conducted on particles generated in sooting C2H2/O2/Ar flames. The aim was to compare Faraday-Cup measurements with those performed with an external dynode and the secondary electron multiplier. The main parameter for signal amplification is the voltage applied to
the external dynode, which is proportional to the strength of the electric field between the dynode and the multiplier. The acceleration of the particles in the electric field must be high enough to produce secondary electrons by impaction on the surface of the dynode. Initially, the influence of the dynode voltage on the mean properties of soot particles was investigated. A flame burning with a C/O ratio of 1.2 was employed, and particles were extracted from a flow coordinate of $\xi=30$ mm above the burner head. As shown in Fig. 9, the apparent mean particle mass first increases with increasing voltage and then remains constant at over $13 \text{kV}$. The voltage-independent size of $d_p=6.41 \text{ nm}$ is in agreement with the Faraday-Cup measurement of $d_p=6.36 \text{ nm}$. From these experiments, the minimum external dynode voltage was determined, which yields a particle mass that is independent of the acceleration voltage. Fig. 10 shows the mean mass and diameter of negatively charged soot particles, generated in $\text{C}_2\text{H}_2/\text{O}_2/\text{Ar}$ flames with C/O ratios of $0.85 \leq \text{C/O} \leq 1.2$. The flames were burned at 30 mbar and the samples were taken at a fixed flow coordinate of $\xi=30$ mm. The secondary electron multiplier (closed symbols) and the Faraday-Cup (open symbols) measurements show no significant differences in size for C/O $>0.95$, indicating the correctness of the multiplier transfer function. Due to the much larger signal of the multiplier compared with the Faraday-Cup measurements, it was also possible to detect soot particles for extremely mild soot conditions. Furthermore, an additional particle fraction of $d_p=3.6 \text{ nm}$ was identified, which could not be resolved by the Faraday-Cup device. The size of this particle class seems to be independent of the burning conditions of the sooting flames. The overall gain in the particle current obtained by the multiplier technique is summarized in Fig. 11. The particle flux measured with the SEM is related to the particle flux measured with the Faraday-Cup as a function of the flow coordinate $\xi$. The signal gain for positively charged particles is about $10^4$, whereas negatively charged particles lead to a multiplier current which is always larger than $10^4$.

**Conclusion**

The particle mass spectrometer (PMS) has been successfully applied to four different aerosols generated under different conditions in various pressure ranges. Soot as well as ceramic or metallic particles were generated in low-pressure flames, microwave plasma, and electric sparks, yielding particles in the size range of 1 to 10 nm. The only conditions of operation are that the process is stationary over a sample time of about two minutes and that the process results...
in charged particles. The use of a secondary electron multiplier with an external dynode as a preamplifier leads to a clear increase in the sensitivity of the PMS. As expected, the particle diameter, being the most important parameter, is not affected by the multiplier. The signal could be increased by a factor of 10^4. It would be possible to additionally improve the sensitivity by further lowering the pressure in the detection chamber, which has a twofold influence. On the one hand, the signal-to-noise-ratio will increase due to the reduced gas in the vacuum chamber, and on the other hand, the reduced pressure will allow the use of a higher voltage applied to the conversion dynode which would lead to a higher degree of conversion, and hence an additional signal gain.

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Nomenclature

\( b_c \) : deflection capacitor width \([\text{cm}]\)

\( d_p \) : particle diameter \([\text{nm}]\)

\( e \) : elementary charge \([\text{C}]\)

\( E \) : kinetic energy \([\text{J}]\)

\( I_p \) : particle current \([\text{fA}]\)

\( l_c \) : deflection capacitor length \([\text{cm}]\)

\( l_G \) : distance between repelling grids \([\text{m}]\)

\( l_p \) : length of particle package \([\text{m}]\)

\( m_p \) : particle mass \([\text{g}]\)

\( t \) : time \([\text{s}]\)

\( U_C \) : deflection voltage \([\text{V}]\)

\( v_p \) : particle velocity \([\text{m s}^{-1}]\)

\( x_p \) : x coordinate of a particle \([\text{m}]\)

\( x_p \) : particle velocity in x-direction \([\text{m s}^{-1}]\)

\( y_p \) : particle velocity in y-direction \([\text{m s}^{-1}]\)

\( z \) : number of elementary charges on a particle \([-]\)

\( \xi \) : flow coordinate \([\text{mm}]\)

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