EUV Resists: Pushing to the Extreme

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Despite achieving 15-nm half pitch, the progress in extreme ultraviolet chemically amplified resist has arguably decelerated in recent years. We show that this deceleration is consistent with approaching stochastic limits both in photon counts and material parameters.

Contact hole printing is a crucial application for extreme ultraviolet lithography and is particularly challenged by resist sensitivity due to inherent inefficiencies in darkfield contact printing. Checkerboard strong phase shift masks have the potential to alleviate this problem through a 4× increase in optical efficiency. The feasibility of this method is demonstrated using the SEMATECH-Berkeley Microfield Exposure Tool pseudo phase shift mask configuration and preliminary results are provided on the fabrication of an etched multilayer checkerboard phase shift mask.

Keyword: photoresist, extreme ultraviolet, shot noise, phase-shift mask

1. Introduction

With extreme ultraviolet (EUV) lithography now at the pilot line phase, the focus of 0.3 numerical aperture (NA) microfield exposure tools is clearly on low-k\textsubscript{1} configurations studying 1× nm half pitch nodes. Moreover, to support research into the deep 1× nm half pitch regime, development is underway for new 0.5-NA tools [4,5].

Although significant progress has been made in chemically amplified resist performance over the past decade, it is evident that the rate of improvement has recently slowed down. Here we consider the improvement from the holistic perspective of resolution, line-edge roughness (LER), and sensitivity, known as the RLS tradeoff.

The analytical framework for the RLS tradeoff [6] comes directly from the photon-limited stochastic performance and thus approaching the RLS limit implies approaching photon limited performance. Here we present stochastic modeling of line-space features studying where the leading resolution EUV chemically amplified resists stand compared to expected stochastic limits.

Also of great importance for EUV lithography is contact hole printing and clearly the RLS tradeoff applies in this regime as well. In fact, the RLS tradeoff is even more onerous in this application due to the inherent inefficiencies in darkfield contact hole printing. A strong phase shift mask approach, however, has been proposed [7] to alleviate this challenge. Here we present the results of a proof of principle experiment on the SEMATECH-Berkeley Microfield Exposure Tool (MET) using its pseudo phase shift mode [8]. We also present preliminary results on the fabrication of an etched multilayer checkerboard phase shift mask.

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2. RLS status

A variety of commercial chemically amplified resists can now achieve 16-nm half pitch. In Table 1 we compare three such resists to the 2011 resolution champion which had a resolution limit of 22 nm. The results in the table are based on patterning performed using the SEMATECH-Berkeley MET in pseudo phase shift mode [8]. SEM images from these various resists are shown in Fig. 1. In addition to including the individual performance terms such as resolution, sensitivity and line-width roughness (LWR), Table 1 also shows the normalized Z-factor [9] (normalized to the 2011 resist performance). The Z-factor is a numerical representation of the RLS tradeoff as defined in Ref. [6]

$$Z \propto R^3L^2S,$$  \hspace{1cm} (1)

where $R$ represents the resolution, $L$ the LER (or LWR), and $S$ the sensitivity.

Table 1. Leading resolution EUV resist performance.

|                | 2011 Ref. | Resist A | Resist B | Resist C |
|----------------|-----------|----------|----------|----------|
| Resolution (nm) | 22        | 16       | 16       | 15       |
| LWR (nm) @ resolution | 4.4      | 3.1      | 4.8      | 3.8      |
| Sensitivity (mJ/cm²) | 15       | 30       | 20       | 22       |
| Normalized Z-factor | 1.00     | 0.38     | 0.62     | 0.35     |

The resist labels A, B, C represent the chronological order of the introduction of the resist, each being approximately 1 year apart. In addition to the strong resolution gain since 2011, we also see that the Z-factor has been improved in all three cases. However, not much gain in Z-factor is observed since the development of the first 16-nm resist.

The stagnation in Z-factor improvement raises the question of photon noise limits. To assess the status of the photon limit we use the stochastic Multivariate Poisson Propagation Model (MPPM) [10-12]. Starting with the known aerial image, resist absorptivity of approximately 0.004 nm⁻¹, 30 nm film thickness and an assumed acid blur as determined from the measured LWR correlation length, we determine the photon-noise limited line-width roughness (LWR) as shown in row two of Table 2. Figure 2 shows an example of the correlation length measurement determined from the LWR power spectral density (PSD) for Resist A [12].

Figure 2. Measured LWR power spectral density for 16-nm lines and spaces in Resist A.

Table 2. Predicted stochastic limited LWR performance compared to measured resist performance.

|                | Resist A | Resist B | Resist C |
|----------------|----------|----------|----------|
| Measured LWR @ 16 nm (nm) | 3.1      | 4.8      | 3.8      |
| Modeled Photon limited LWR (nm) | 2.1      | 2.7      | 2.5      |
| Estimated material limited LWR (nm) | 2.3      | 4.0      | 2.9      |
| Modeled material limited LWR (nm) | 2.4      | 2.4      | 2.4      |
The results show that even though we are not yet photon limited, we are getting close. Subtracting the theoretical photon limited LWR from the total measured LWR, provides an estimate of the material-limited LWR (row 3 of Table 2) which in all cases we find to be larger than the photon-limited contribution.

Although typically described in the context of photon noise, the concept of stochastic modeling is not limited to the photon noise problem. Rather, the Poisson model readily applies to counting experiments in general. Noting that resist material non-uniformity can also be viewed as a counting problem, the stochastic model above can be extended to materials effects. For example, we may be concerned with the number of photo acid generators (PAGs) or quencher in a given volume of resist, or in the number of acids generated per absorbed EUV photon. All these items can be treated as random variables and propagated through the resist model to generate the dependent random variables of final acid count and deprotection. This multivariate approach gives rise to the MPPM model and allows a variety of stochastic terms to be studied in combination as well as individually.

The fourth row of Table 2 shows the predicted material-limited LWR based on the inclusion of PAG, quencher, and acid generation random variables. The nominal values for PAG, quencher, and acid yield are based on average estimates provided by the resist suppliers and are assumed to be the same for all three resists, hence the same predicted stochastic material-limited LWR for all three.

In the case of Resist A, we find the predicted material limited LWR to be very close to the estimated experimental material limit shown in row 3. Note that the multivariate model as described above does not necessarily capture all stochastic effects nor does it capture molecular effects. In the cases where the model closely matches this measurement, the expectation is that the MPPM model does capture the dominant experimental terms.

3. Improved efficiency contact hole patterning

Contact hole patterning is expected to be one of the first high volume applications for EUV lithography and is a significant driver in shot noise requirements. The fact that conventional contact hole patterning typically requires at least $2 \times$ the dose compared to line-space patterning further exacerbates the concern over shot noise limits and resist sensitivity. The loss of efficiency relative to line-space patterning, however, is not a resist effect, but rather an optical effect.

As described in the literature, the contact efficiency problem can thus be mitigated by mask design [7] with a phase shift design being the most effective. In fact, for dense contacts, a chromeless checkerboard design can be employed to provide on the order of $4 \times$ efficiency gain compared to a conventional darkfield contact hole pattern.

As shown in Fig. 3, the printing of the checkerboard pure phase mask results in a square grid of contacts where the printed contact size is one half the size coded on the mask. For example, the 32-nm checkerboard in Fig. 1, prints a dense grid of 16-nm contacts.

For ease of fabrication, we first test this concept using the SEMATECH-Berkeley MET pseudo phase shift mode [8], allowing a conventional binary absorber mask to be used. In this case, the $180^\circ$ phase shift regions shown in Fig. 3 are simply replaced with absorber. Figure 4 shows a conventional (not pseudo phase shift mode) print of the mask where we see the actual checkerboard pattern. The patterns are coded to print as 27, 26, and 25 nm in pseudo phase shift mode, thus in this conventional print are actually twice that size.

![Figure 3. Phase only checkerboard design (left) which prints (right) a pitch split square grid of contacts.](image-url)
Figure 4 shows the pseudo phase shift mode print of the mask used to generate the print in Fig. 4. In this case we see the expected effect of pitch splitting and the contact grid becoming square. The printed contacts are 27, 26, and 25 nm. Figure 6, shows the results for the 20, 19 and 18 nm contacts.

4. Fabrication of a true phase shift mask

To achieve the efficiency gains of primary interest here, a true phase shift mask is needed instead of the pseudo phase shift. We are verifying the throughput gain through the fabrication of an etched multilayer phase mask. The process we use relies on an embedded etch stop at the proper location in the multilayer coating. The etch stop we use is Cr and its thickness must be carefully controlled to ensure that the multilayer above and below the etch stop remain in phase.

Figure 7 shows the fabrication process flow. In addition to the embedded Cr etch stop, Cr is also used on top of the multilayer as a hard mask for the etch process. KRS e-beam resist is used to define the pattern transferred to the Cr hard mask. The resist is stripped and the multilayer etched using reactive ion etching stopping on the embedded Cr. The final step is to remove the residual Cr hard mask and etch stop.

Figure 8 shows a cross-section scanning electron micrograph of a test grating fabricated using the process described above. In this case, however, we have not yet removed the Cr. The grating pitch is 200-nm which would correspond to 12.5-nm printed lines and spaces from the phase shift mask assuming a 4× reduction system. We test the effectiveness of the phase shift process by way of scatterometry (Fig. 9) on the Center for X-ray Optics Calibrations and Standards Beamline at the Advanced Light Source Synchrotron facility. As expected from a phase shift mask, strong suppression of the zero order is observed. Efficiencies of 20% are observed in both the ±1 diffraction orders. Ideally we would expect approximately 30% efficiency in each order and the difference is attributed to the residual Cr. The next step is to apply this process to checkerboard patterns and fabricate a mask compatible with the SEMATECH-Berkeley MET for print tests.
5. Conclusion

Stochastic modeling has been used to show that the recent slow down in RLS progress is consistent with approaching stochastic limits. The modeling suggests that further improvements require improvements in both photon and materials stochastics.

To mitigate the dose impact of stochastic limits in the printing of contacts, a chromeless phase shift mask design has been proposed. The viability of such a mask from the patterning perspective has been verified through the fabrication of a pseudo phase shift mask version of the mask and printing on the SEMATECH-Berkeley MET. The expected patterning performance was observed.

Fabrication of a true phase shift mask is underway and the fabrication process has been validated through the implementation of a phase shift grating and characterization in an EUV scatterometer.

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Figure 7. Fabrication process flow for etched multilayer phase shift mask.

Figure 8. Cross-section scanning electron micrograph of test grating fabricated using process described in Fig. 5. Grating pitch is 200-nm corresponding to 12.5-nm printed lines and spaces from assuming a 4× reduction system.

Figure 9. Scatterometry measurement of phase shift test grating shown in Fig. 6. As expected, strong suppression of the zero order is observed. Efficiencies of 20% are observed in both the ±1 diffraction orders.
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