Investigation of engineering properties of blast furnace slag additive mortars

Hüseyin Boran,¹,* Osman Gunaydın,¹ Kadir Gucluer²

¹ Adiyaman University, Faculty of Engineering., Department of Civil Engineering, Adiyaman, Turkey, huseyinboran044@gmail.com, gunaydin@adiyaman.edu.tr, ORCID: 0000-0001-5007-1788, ORCID: 0000-0001-7559-5684
² Adiyaman University, Vocational School of Technical Sciences, Department of Construction, Adiyaman, Turkey, kgucluer@adiyaman.edu.tr, ORCID: 0000-0001-7617-198X

ABSTRACT

Cement, water and fine aggregate mixture is called mortar. Mortar samples suitable for the desired purpose can be obtained by adding various additives to the mortar samples. In this study, instead of standard sand, blast furnace slag (BFS) was used at 10%, 20% and 30% by weight in mortar samples. In order to determine the mechanical properties of the samples, compressive and flexural strength tests were applied. For the electrical resistivity values, a device with constant 30V voltage was prepared and the electrical resistivity values were measured. To determine the freeze-thaw resisting properties, it was applied sodium sulfate experiment. As a result, it was seen that the best values were obtained from 30% BFS additive samples in all series. The highest resistivity values are in the sample with 30% BFS doped with 0.1856 ohm.m and 0.268 ohm.m values. The highest freeze-thaw resisting value was seen in the sample with 30% BFS with 1.35%.

1. Introduction

A mixture of water and cement is called cement paste. The new mixture obtained as a result of adding a fine aggregate to this mixture is called mortar. Mortars are special concretes that do not contain coarse aggregate. Currently, it is possible to gain main features according to the desired purpose by used mineral and chemical additives in production of mortar [1].

The cost of natural sand used as fine aggregate in recently developed concrete has increased the cost of construction. In this case, research has turned to studies for alternative materials that are cheap and easily accessible for natural sand [2]. To meet the global demand for concrete in the future, finding suitable alternatives to natural aggregates for preparing concrete can become a more difficult task. Therefore, the use of alternative sources for natural aggregates is becoming increasingly important. The use of granulated blast furnace slag (GBFS) aggregates in concrete by replacing natural aggregates is a promising concept because its impact strength is higher than natural aggregate. Steel slag aggregates are already used as aggregates in asphalt paved road mixes due to their mechanical strength, hardness, porosity, abrasion resistance and water absorption capacity [3].

Blast furnace slag (BFS) is a material produced by the melting of iron ore to produce iron metal [4]. The wastes as a result of the burning of limestone, coke and iron ore gangue generate BFS. The formation temperature of BFS is between 1400-1600 °C [5]. The fact that BFS has a crystal structure occurs when it is slowly cooled. In this case, it can be preferred as concrete aggregate and has mechanical properties similar to basalt. On the other hand, rapid cooling is required for the formation of glassy slag [5].

It is known that blast furnace slag improves the workability of fresh concrete, extends the setting time of cement paste, affects hydration rate and perspiration reduction, and strengthens durability values in hardened concrete. Looking at the literature; It has been said that it causes a decrease in the strength gaining speed especially in the first days and an extension of the concrete setting in cold weather conditions [6].

Studies up to now show that slag additive improves concrete characteristics such as durability, permeability, corrosion resistance, workability and strength [7]. The highest electrical resistivity can be achieved with cement mortars containing high levels of BFS. With C-S-H gels reducing the water content in the cement paste as a result of the hydration of free
Ca(OH)\(_2\) and pozzolanic mineral mixtures (containing Al\(_2\)O, Fe\(_2\)O\(_3\), SiO\(_2\) etc.) and accelerates the formation of ettringite-monosulfate [8,9]. As a result of the reaction of BFS particles during hydration, Ca(OH)\(_2\) content decreases and C-S-H gels increase. Thus, it is thought that BFS grains contribute to the formation of C-S-H gels [10].

When the use of BFS as aggregate in the literature and the sulphate strengths of using BFS and pumice instead of a certain amount of aggregate in concrete pipe production; It was observed that the weight loss was the lowest in BFS and pumice added samples. While samples kept in sulphate solution for 180 days showed the best resistance of samples with 15% BFS, while the most unstable sample was the witness sample [11]. Nataraja et al. [12] investigated the use of fine aggregate GBFS in cement mortar. In this study, they changed cement mortar 1:3 and GBFS at 0, 25, 50, 75 and 100 ratios to natural sand for a fixed w/c ratio of 0%. In the study, they looked at 100% of natural sand change with GBFS for 0.4 and 0.6 w/c ratios. Flow properties of various mixtures and their compressive strength at various ages were investigated. From this study, they observed that the GBFS could be partially used as an alternative building material for natural sand in mortar applications. They found that the reduction in flowability can be compensated for by adding an appropriate percentage of super plasticizer. Babu and Mahendran [13] investigate the physical and mechanical properties of concrete by replacing fine aggregate with BFS and GBFS. Conclusions have been drawn based on the experimental results. Based on their results, it encourages the use of BFS up to 25% in concrete as a substitute for fine aggregate. The maximum compressive strength of 40.39 MPa was obtained by replacing 25% of the fine aggregate with BFS. The use of BFS will reduce the cost of concrete by 8 to 10%. Autade [14] investigated the use of steel slag in concrete instead of fine aggregate. He examined the change in the range of 0, 20, 40, 60, 80, 100%. He observed that the workability of concrete decreases as the percentage of substitution increases. There is a significant increase in compressive strength for 20% and 40% change; It has been stated that there is an increase of more than 20% in flexural strength and tensile strength. With regard to the strength parameters obtained at 80% and 100% substitution, it was stated as expected. 10% - 20% difference in compressive strength has been observed. Seker [15] GBFS is a by-product and its use as aggregate in concrete can be an economical and environmentally friendly solution in the local area. Thus, it will become more important to find suitable alternatives for future aggregates. When the results are examined, it has shown that it has properties similar to natural aggregates and will not cause any harm if it is included in concrete.

The purpose of this study is to use these wastes in the construction sector due to the difficulties of storing by-products that occur as a result of the use of industrial materials and damage to the environment. The selection of blast furnace slag, which is one of these by-products, as aggregate is to protect the nature, reduce the need for natural aggregate raw materials and to obtain impermeable and high quality mortar samples in terms of durability properties by using thinner materials. For this purpose, BFS additive samples were produced, compressive and flexural strength tests were made, electrical resistivity measurements were carried out and sodium sulfate test was applied.

### 2. Material and method

In this study, Portland composite cement of CEM II 42.5 type consistent with TS EN 197-1 [16] was used as a binder. Chemical components of cement and BFS used in the study are given in Table 1. BFC’s blaine fineness 2685 cm\(^2\)/gr.

#### Table 1. Chemical component of cement and BFS

| Oxide | SiO\(_2\) | Al\(_2\)O\(_3\) | Fe\(_2\)O\(_3\) | CaO | MgO | K\(_2\)O | Na\(_2\)O | (%) |
|-------|----------|----------------|----------------|-----|-----|--------|--------|-----|
| Cement | 19.2     | 3.88           | 4.25           | 62.8| 3.42| 0.34   | 2.1    |     |
| BFS   | 40.1     | 12.8           | 0.9            | 39.6| 4.2 | 1.2    | 0.05   |     |

CEN standard sand in accordance with TS EN 196-1 [17] was used in the prepared mortar mixtures. The samples have been prepared with reference to 225 gr water, 450 gr cement and 1350 gr standard sand given in TS EN 196-1 [17]. Samples were prepared by replacing 10%, 20% and 30% by weight BFS with standard sand. Mortar samples were prepared in a mixer and placed in molds of 40 × 40 × 160 mm using a shaking table. After the samples were kept in the mold in the laboratory for 24 hours, they were kept in the cure pool at 20±2 °C for 7, 28 and 90 days experiments. The samples produced 3 pieces for each series were first subjected to the flexural strength test and the average values of the results calculated with the help of formula (1) were taken and the flexural strength values were accepted. Compressive strength test was performed on the samples obtained after flexural strength and the average of the results calculated with the help of formula (2) was accepted as the value of compressive strength.

\[
R_f = \frac{1.5 \times F_f \times 1}{b^3} \quad (1)
\]

Here; \(R_f\): Flexural strength, (Newton / mm2), \(b\): Side length of the square section of the prism (mm), \(F_f\): The force applied to the middle of the prism when it breaks (Newton), \(l\): The distance between the support cylinders (mm)

\[
f_b = \frac{P_k}{A_0} \quad (2)
\]

Here; \(f_b\): Compressive strength (MPa), \(A_0\): Surface area (mm2), \(P_k\): Load at break (N)
For electrical resistivity measurements, the resistivity values of the samples were calculated with the help of formulas (3) and (4) by giving a constant 30 V voltage to the samples.

\[ \rho = R \times \frac{S}{L} \quad (3) \]

\[ R = \frac{U}{I} \quad (4) \]

Here; \( \rho \) = electrical resistivity (Ω.m); \( R \) is the measured resistance (Ω); \( L \), distance between copper electrodes (m); \( S \), electrode conductor area (m²); \( U \) Voltage value (volts) on U Electrodes; \( I \) The current intensity (amperes) passing through the sample.

For the sodium sulphate test, the solution was prepared by adding 350 g of sodium sulphate to 1 liter of water in accordance with ASTM C88-05 [18]. The samples were weighed as it is the state of driving oven before the experiment. The samples placed in the solution were kept between 16-18 hours. The samples removed from the solution were placed in the oven and kept in the oven at 105 °C for about 4-6 hours until they reached their constant weight. This cycle was repeated 5 times, and as a result, the oven-dried samples were weighed. With the help of formula (5), freezing loss values were calculated. Finally, samples were subjected to compressive strength test. Compressive strength values of the samples were calculated with the help of formula (2).

\[ \left( \frac{G_1 - G_2}{G_1} \right) \times 100 \quad (5) \]

\( G_1 \): The oven-dry weight of the samples before sodium sulphate the test,

\( G_2 \): The oven-dry weight of the samples after sodium sulphate the test

3. Findings

3.1. Compressive and Flexural Strength Findings

The compressive and flexural strength findings of the mortars used in 10%, 20% and 30% rates from BFS are given in Fig. 1 (a) and (b).
was seen that the lowest values were at 3.48 MPa and 3.75 MPa in the sample with 10% BFS and the highest values were in the sample with 4.48 MPa and 5.9 MPa with 30% BFS. When the comparison is made from the literature, Quasrawi et al. [20], in their study, as a result of the replacement of fine aggregate and BFS, samples with BFS additives at 30-50% have obtained the best results for flexural strength. The findings obtained support this view. Slag concretes with tensile strength have slightly higher tensile strength than Portland cement concrete for a given compressive strength [23]. It can be said that by using BFS as a mineral additive in certain proportions, its use as fine aggregate yields better flexural strength results compared to witness samples.

3.2. The Electrical Resistivity Findings

The electrical resistivity findings of the mortars used at 10%, 20% and 30% rates from BFS are given in Fig. 2.

![Figure 2 The electrical resistivity findings](image)

When the electrical resistivity findings were examined, it was seen that the lowest values were in the witness sample with 0.0517 ohm.m and 0.0691 ohm.m values. The resistivity value increased with the increase in the amount of BFS. The highest values are in the sample with 30% BFS doped with 0.1856 ohm.m and 0.268 ohm.m values. Topçu et al. [10] in their study, they think that adding BFS to cement paste increases the electrical resistivity of the mixtures. Considering the values obtained above and the values obtained from this study, it can be said that preferring BFS as both mineral additive and fine aggregate gives better results than witness samples. Increasing electrical resistivity decreases electrical conductivity. As a result, it is seen that the most conductive sample is the witness sample and the least conductive one is the sample with 30% BFS doping.

3.3. Sodium Sulphate Findings

Findings of sodium sulphate belonging to the mortars used in 10%, 20% and 30% rates from BFS are given in Figure 3.

![Figure 3 Sodium sulphate findings](image)

Considering the sodium sulphate test findings, the lowest compressive strength is in the witness sample with 41 MPa. The increase in BFS positively affected the compressive strength. The highest compressive strength is 57.93 MPa with 30% BFS added sample. The increase in the amount of BFS caused a decrease in freezing loss. As a result of, the lowest freezing loss value was seen in the sample with 30% BFS with 1.35%. Binici et al. [20] obtained the lowest mass loss among the samples with high contribution from blast furnace slag. They also stated that blast furnace slag additive contributes positively to durability and strength. These studies confirm the results obtained above.

4. Results

Considering the findings obtained by adding BFS to the mortar samples instead of fine aggregate at the rates of 10%, 20% and 30%,

- It has been observed that increasing the amount of BFS has a positive effect on compressive strength. The fact that the witness sample has the highest value in 7-day early strength is thought to be due to the fact that mineral additives have an effect on reducing the cement setting speed.

- When looking at 7, 28 and 90 days values, it was seen that the highest flexural strength values were 3.54 MPa at 7 days, 4.48 MPa at 28 days and 5.9 MPa at 90 days in the sample with 30% BFS.

- The increase in the amount of BFS has also increased the electrical resistivity value. It was observed that the highest value was at 0.268 ohm.m with 30% BFS additive sample. Parallel values were obtained with the compressive strength values. Since it is known that increasing the electrical resistivity decreases the electrical conductivity, the best
 conductive witness sample is considered to be the least conductive 30% BFS additive sample.

- The increase in the amount of BFS, an increase in compressive strength has been observed under the presence of sodium sulphate. The lowest freezing loss with a value of 1.5% is in the sample with 30% BFS. In addition, it has been observed that the increase in the amount of BFS reduces the freezing loss.

- It is recommended to use the 30% BFS additive sample in mortar concrete since it is seen that the best values are obtained in terms of durability and strength.

- It can be said that the use of BFS, which is an industrial waste, in concrete or mortars at certain rates for recycling and environmental protection is not considered harmful in terms of its mechanical and durability properties.

References

[1]. Baradan B., Yazıcı H. ve Aydın S., Beton. Dokuz Eylül Üniversitesi Mühendislik Fakültesi Yayınları, İzmir: 2015.

[2]. Jadhav, P.A. ve Kulkarni, D.K., “Effect of Replacement of Natural Sand By Manufactured Sand on the Properties of Cement Mortar,” International Journal of Advanced Engineering Technology, Vol. 3, No 3, (2013).

[3]. Hiraskar, K.G. ve Patil, C. “Use of Blast Furnace Slag Aggregate in Concrete,” International Journal Of Scientific & Engineering Research, Volume 4, Issue 5, (2013), s 95.

[4]. Thomas D., Concrete Durability. CRC Press, 2014.

[5]. Babu K. D. and Kumar V. S. R., “Efficiency of GGBS in Concrete”, Cement and Concrete Research, 30, (2000), 1031- 1036.

[6]. Erdoğan T. Y., Beton. Metu Press, 5. Baskı, 2015.

[7]. Babu K. D. and Kumar V. S. R., “Efficiency of GGBS in Concrete”, Cement and Concrete Research, 30, (2000), 1031- 1036.

[8]. Salem T.M., “Electrical conductivity and rheological properties of ordinary portland cement–silica fume and calcium hydroxide–silica fume pastes”, Cem Concr Res, 32, (2002), 1473-1481.

[9]. McCarter W.J., Starrs G. and Chrisp T.M., Electrical conductivity, diffusion, and permeability of portland cement-based mortars, Cem Concr Res, 30, (2000), 1395-1400.

[10]. Topçu İ. B., Uygunoğlu T. ve Hocaoğlu İ., “Yüksek fırın cüruf katkılı çimento pastalarının elektriksel özüresicilerinin araştırılması”, Politeknik Dergisi, 21(2), (2018), 257-264.

[11]. Binici H. et al, “Kum Boyutunda Yüksek Fırın Cürufü ve Pomza Katkılı Beton Borularının Durabilite Özelliklerinin Araştırılması”, Kahramanmaraş Sütçü İmam Üniversitesi Mühendislik Bilimleri Dergisi, 14.3, (2012), 33-44.

[12]. Nataraja, M.C., Kumar, D.P.G., Manu, A.S. ve Sanjay, M.C., “Use Of Granulated Blast Furnace Slag As Fine Aggregate In Cement Mortar,” International Journal of Structural and Civil Engineering Research. No.2, May, (2013).

[13]. Babu, J.S. ve Mahendran, N., “Experimental Studies on Concrete Replacing Fine Aggregate with Blast Furnace Slags,” International Journal of Engineering Trends and Technology (IJETT). Volume 10, Number 8, Apr, (2014).

[14]. Autade, P. B., & Saluja, H. S. J. S. Effect of Steel Slag as a Replacement of Fine Aggregate in M40 Grade of Concrete, 2016.

[15]. Şeker, O., “Granüle Yüksek fırın cürufunun Kendiliğinden Yerleşen Beton Özelliklerine Etkisi,” Master's thesis, Bartın Üniversitesi, Fen Bilimleri Enstitüsü, 2019.

[16]. Çimento-Genel Çimentolar-Bileşim, Özellikler ve Uygunluk Kriterleri, TS EN 197-1, 2002.

[17]. Çimento Deney Metotları-Dayanım Tayini, EN 196-1, 2002.

[18]. Standard Test Method for Soundness of Aggregates by Use of Sodium Sulfate or Magnesium Sulfate, ASTM C88-05, 2005.

[19]. Yazıcı H., “Yüksek fırın cürufu katkılı harçların sülfat dayanıklılığının incelenmesi”, DEÜ Mühendislik Fakültesi Fen ve Mühendislik Dergisi, 8, 1, (Ocak 2006), 51.

[20]. Qasrawi, H., Shalabi, F., & Asi, I., “Use of low CaO unprocessed steel slag in concrete as fine aggregate,” Construction and Building Materials, 23(2), (2009), 1118-1125.
[21]. Soroka I., “Concrete in Hot Environments”, National
Building Research Institute, Faculty of Civil
Engineering, Technion-Israel Institute of Technology,
Haifa, Israel, 1993.

[22]. Yeau K. Y. and Kim E. K., “An Experimental Study on
Corrosion Resistance of Concrete with Ground
Granulated Blast-Furnace Slag”, Cement and Concrete
Research, 35, (2005), 1391-1399.

[23]. Newman J., and Choo B.S., “Advanced Concrete
Technology”, Elsevier Publishing, Great Britain, 2003.

[24]. Binici H., Eken M. ve Dinçer A., “Silis Dumanı,
Uçucu Kül ve Yüksek Fırın Cürüfu Katkılı Betonların
Bazı Durabilite Özellikleri”, Çukurova Üniversitesi
Mühendislik-Mimarlık Fakültesi Dergisi, 28(1), (2013),
11-21.