The biomechanical role of periodontal ligament in bonded and replanted vertically fractured teeth under cyclic biting forces

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After teeth are replanted, there are two possible healing responses: periodontal ligament healing or ankylosis with subsequent replacement resorption. The purpose of this study was to compare the fatigue resistance of vertically fractured teeth after bonding the fragments under conditions simulating both healing modes. Thirty-two human premolars were vertically fractured and the fragments were bonded together with Super-Bond C&B. They were then randomly distributed into four groups (BP, CP, CA, BA). The BP and CP groups were used to investigate the periodontal ligament healing mode whilst the BA and CA groups simulated ankylosis. All teeth had root canal treatment performed. Metal crowns were constructed for the CP and CA groups. The BP and BA groups only had composite resin restorations in the access cavities. All specimens were subjected to a 260 N load at 4 Hz until failure of the bond or until $2 \times 10^6$ cycles had been reached if no fracture occurred. Cracks were detected by stereomicroscope imaging and also assessed via dye penetration tests. Finally, interfaces of the resin luting agent were examined by scanning electron microscope. The results confirmed that the fatigue resistance was higher in the groups with simulated periodontal ligament healing. Periodontal reattachment showed important biomechanical role in bonded and replanted vertically fractured teeth.

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INTRODUCTION

Vertical crown-root fracture of molar and premolar teeth is a common non-caries problem especially following endodontic treatment or when there are cracks in the tooth.¹⁻⁶ Several approaches have been adopted to try and retain vertically fractured posterior teeth, including attempts to splint the fractured segments together using wire.⁷⁻⁸ However, this approach has a poor prognosis and no data to support it. No reliable method has been reported for retaining vertically fractured posterior teeth and these teeth are usually extracted.

A multidisciplinary approach combining tooth extraction, bonding of the segments with adhesive material followed by intentional replantation may be an alternative method of managing vertically fractured posterior teeth. Trope & Rosenberg successfully repaired a vertically fractured upper left second molar using this approach.⁹ After one year, the tooth still functioned normally and had no clinical or radiographic signs of disease.

With the improvement of adhesive dentistry and the availability of materials such as 4-methyl-acryloyl-ethyl-trimmellitic anhydride (4-META)/(methyl methacrylate-tributylborane MMA-TBB) resin cement, this treatment approach has been applied to vertically fractured anterior teeth and crown-root fractures in posterior teeth.¹⁻²,⁶⁻¹² The short-term prognosis following this procedure appears to be reasonable, but it has a poor long-term prognosis.¹³

Replantation is one of the most important steps in this treatment approach. The periodontal ligament (PDL) is injured during extraction of the tooth and, according to Andreasen,¹⁴⁻¹⁵ this may result in ankylosis and replacement resorption following replantation. There may also be varying reactions of the PDL to the layer of adhesive dental material in the fracture line of the tooth.¹⁶ The effect of the occlusion is also unknown as there have been no reports in the literature.

The purpose of this study was to explore the biomechanical role of periodontal reattachment in bonded and replanted vertically fractured tooth under cyclic biting force.

MATERIALS AND METHODS

Fractured teeth specimen preparation

Forty human maxillary upper first premolars with two roots, extracted for orthodontic reasons, without cracks or cavities were used in this
study. The teeth were stored in water with 0.5% chloramine at 4 °C, and used within 1 month following extraction. The teeth were chosen from a collection of more than 80 premolar teeth so they were all of similar size and dimensions. The length of the teeth, the length from the central fossa to the root furcation, and the angle of the root furcation were measured. Teeth with measurements within 90% of the medians were chosen. The length of the teeth was (17.50±0.70) mm. The length from central fossa to root furcation was (11.00±0.75) mm, and the angle of the root furcation was 16.5±2.5°. The study was independently reviewed and approved by the ethical board of the hospital.

In order to simulate a vertical fracture, the teeth were separated into two halves with a low-speed cutting saw and a blade of 0.2 mm thickness (Isomet 11-1280-250; Buehler, Lake Bluff, IL, USA) mesiodistally along the vertical axis (Figure 1a). In order to further standardize the specimens, the surface areas of each section were calculated using Adobe Photoshop CS2. Sections with surface areas within 90% of the median area were chosen.

The two halves were then bonded together with 4-META/MMA-TBB resin agent (Super-Bond C&B; Sun Medical, Tokyo, Japan). Endodontic access cavities were cut and root canal treatment was performed (Figure 1b). The access cavities were then restored with an adhesive bond (Adper Prompt; 3M ESPE, Seefeld, Germany) and composite resin restoration (Filtek Z350; 3M ESPE Dental Products, St. Paul, MN, USA). The teeth were randomly divided into four groups, labelled BP, BA, CP and CA, with each group managed as follows:

- Group BP: bonding, no crown restoration and with periodontal ligament (n=10);
- Group BA: bonding, no crown restoration and ankylosis (n=10);
- Group CP: bonding, Ni–Cr metal full crown restoration and with periodontal ligament (n=10);
- Group CA: bonding, Ni–Cr metal full crown restoration and ankylosis (n=10).

The teeth were embedded in epoxy resin (Phoenix; Blue-star Manufacturing, Wuxi, China) to a level 2 mm apical to the cemento-enamel junction. Two groups (BP and CP) had an additional intermediate elastic layer of silicone rubber (Honigum-Mixstar MonoDMG; Dental-Material Gesellschaft, Elbgaustr, Germany) to simulate the periodontal ligament while the groups without this layer (BA and CA) simulated dento-alveolar ankylosis. All specimens formed cylinders 30 mm high and 20 mm in diameter (Figure 2). The epoxy resin simulated the alveolar bone. 18–19

In order to create an even thickness (0.2–0.3 mm) of silicone rubber simulating the PDL, the roots were immersed in fluid wax and then removed. A layer of 0.2–0.3 mm wax remained on the root surface. The tooth with the wax was then encased in the epoxy resin block (Figure 1c and 1d). After the resin had cured, the teeth and wax were removed from the block. The wax was removed from the tooth and the tooth was then replaced in the resin block with silicone rubber.

Compression testing

As part of Standardizations GB/T2569-1995 and GB/T7757-1993, the elastic modulus in compression of rubber and epoxy resin were measured with a Universal Testing Instrument (Instron 4466; Instron, Hensgrand, MA, USA). Rectangular parallel specimens 10 mm×10 mm×20 mm were prepared. Those specimens with smooth surface, no cracks, no obvious defects such as impurities and processing damage were considered

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![Figure 1](image1.png) Photos of tooth specimen and cyclic-load device. (a) An example of a tooth showing the direction and location of the vertical cutting. (b) The tooth after bonding the fragments together with Super-Bond C&B. (c) A tooth specimen without crown restoration. (d) A tooth specimen with the crown restoration. (e) The conical loading instrument with an 80° angle tip specifically manufactured to imitate the cusp of a premolar. (f) The loading point on the central fossa of the tooth.

![Figure 2](image2.png) Conceptual diagram of the model used. (a) The model used for the ankylosis healing group; (b) the model used for the periodontal ligament healing group.
suitable for testing. The specimens were stored for 24 h under standard ambient conditions at (23±2) °C and 50%±5% humidity. The elastic modulus of the rubber and epoxy resin were based on this compression test. The load, displacement, stress, strain rate and the modulus were recorded.

Cyclic-load testing

Cyclic-load testing was performed with a cyclic-loading device (K655; Tokyo Giken, Tokyo, Japan) simulating clinical biting conditions. The conical loading instrument, as shown in Figure 1e, was manufactured specifically for this experiment. The angle of the apex is 80° to imitate the typical cusp of premolar teeth. An instant force of 260 N was applied to each specimen at 4 Hz.17 Figure 1f shows the loading point that was situated in the central fossa of the teeth. There is a viewing computer screen attached to the testing machine and the values of load, frequency, amplitude and rate were displayed on the screen in real time. At the end of loading, three results were possible and were recorded as ‘broken’, ‘cracked’ and ‘no failure’. In Groups BP and BA, a clearly ‘broken’ specimen that was visible to the naked eye is shown in Figure 3a and 3b. The number of load cycles was recorded when the bonding layer broke completely. Data were presented as means±standard deviation and were compared using Mann–Whitney U test at a 95% level of confidence.

No complete breakages occurred in Groups CP and CA after 2×10^6 repetitions.20 The loading test was stopped and the teeth were examined under a stereomicroscope (×50; Wild Heerbrugg Type 308700; Euromex, Heerbrugg, Switzerland) in order to assess them for a ‘crack’ (Figure 3c) or ‘no failure’ (Figure 3d).

All statistical analyses were carried out using the statistical software (SPSS, Chicago, IL, USA). Comparisons between Groups CP and CA were performed using Fisher exact probabilities in 2×2 table. P<0.05 was considered to be statistically significant.

Fluid penetration test

Specimens recorded as ‘no failure’ after cyclic-loading testing were subsequently tested for fluid penetration. There were 13 samples tested in this manner—nine from Group BP and four from Group BA. Another set of 13 specimens, prepared in the same manner but not subjected to fatigue loading were used as a control group for this test. The apical foramen of each sample was sealed with wax and the root surface, except the bonded layer, was coated with nail polish to seal the cementum, dentine tubules and any lateral canals. The specimens were stored in artificial saliva (Bioxtra Healthcare, Weesp, Belgium) at 37 °C for 1 week. They were then immersed in a 1% solution of methylene blue dye at 37 °C for 48 h.21 After being rinsed in tap water, each tooth was separated into two parts transversally 3 mm above the root furcation (Figure 4b and 4c). The crown was also sectioned, again transversally (Figure 4d). The root was sectioned vertically through its long axis in the buccolingual plane using a diamond blade (Isomet 11-1280-250; Buehler, Lake Bluff, IL, USA) (Figure 4d). The depth of dye penetration beneath the enamel or dentine margins in the two locations was measured under a stereomicroscope at ×50 magnification. Two independent-samples test was used to determine the variance of the depths of two groups and two locations.

Figure 3 Three results after cyclic loading. (a and b) ‘Broke’: an example of a specimen without a metal crown that broke completely after fatigue loading. (c) ‘Crack’: typical appearances of the bonding layer crack under stereomicroscope (×50). (d) ‘No failure’: the image of the bonding layer without cracks under stereomicroscope (×50).

Figure 4 Conceptual diagram of the section direction in the fluid penetrating testing. (a) The specimens were stored in artificial saliva at 37 °C for a period of 1 week and were then immersed in a 1% solution of methylene blue dye at 37 °C for 48 h. (b and c) The teeth were separated into two parts transversally 3 mm above the root furcation. (d) The crown was also sectioned, again transversally and the root was sectioned through its long axis in the buccolingual plane using a diamond blade.
Scanning electron microscopy
Those specimens with or without cracks in Group CP and CA were also examined under scanning electron microscopy (SEM) (JSM 6300; Zeisse, Oberkocher, Germany). First the teeth were transected, and then all specimens were mounted on aluminum stubs and sputter-coated with gold. The bonding layers and the dentin/resin interfaces were observed under SEM.

RESULTS
Compression testing
The values of the compression test including the load, displacement, stress, strain rate and the elastic modulus are shown in Table 1. The elastic modulus of the rubber was (13.9±0.7) MPa, and the epoxy resin was (1.43±0.17) GPa. The values were similar to those of periodontal ligament (10 MPa) and alveolar bone (1.370 GPa), respectively.22

Cyclic-load testing
Completely different results were evident in the specimens with or without metal crown restorations. In the BP and BA groups without crowns, all fractures occurred in the bonding layer (Figure 5). The load cycles of the BP group (150 580±21 570) were significantly larger than the BA group (29 268±9 473) (P<0.001). However, in the other two groups with crown restoration, no fractures were observed in the bonding layer (Table 2). One specimen in the CP group and six in the CA group had cracks when examined under stereomicroscope. The others remained intact for the 2×106 repetitions. Fisher exact probabilities in 2×2 table revealed a significant difference between Groups CP and CA (P<0.05).

Table 1 Results of the compression testing

| Materials physical quantities | Rubber       | Epoxy resin |
|------------------------------|--------------|-------------|
| Load at maximum/kN           | 0.501±0.001  | 6.999±0.294 |
| Displacement at maximum/mm   | 2.568±0.306  | 1.414±0.132 |
| Stress at maximum/MPa        | 4.838±0.430  | 66.620±4.488|
| Strain at maximum/%          | 34.535±2.750 | 5.713±0.303 |
| Modulus/MPa                  | 13.944±0.699 | 1428.668±170.090|

Result showed as mean±standard deviation.

Table 2 Results of cyclic-load testing in Groups CP and CA

| Group | No failure | Crack | Total |
|-------|------------|-------|-------|
| CP    | 9 (90%)    | 1 (10%)| 10    |
| CA    | 4 (40%)    | 6 (60%)| 10    |
| Total | 13         | 7     | 20    |

*P=0.029

Fluid penetration
Dye penetration depths observed in the loaded and control groups are presented in Figure 6. Statistical analysis showed no significant difference in depth of dye penetration at the transverse section of the crown between the loaded and the control group (P>0.05). However, for the root furcation vertical sections, the loaded group experienced significantly more dye penetration than the control group (P<0.001). On the other hand, there was no significant difference in depth of dye penetration between the transverse section and the vertical section in the control group (P>0.05). In the loaded group the depth of dye penetration at the vertical section was significantly deeper than the transverse section of the crown (P=0.001).

SEM observation
SEM indicated that the dentin/resin interfaces broke between the smear layer and the bonding agent. Microscopic cracks were found inside the bonding agent even in those specimens that looked intact under a stereomicroscope. Figure 7 presents scanning electron microscope images of cross-sections of the dentin/bonding agent interface. Images a (×300), b (×800) and c (×2 000) zoom in on an apparently undamaged specimen after submitting it to the cyclic-loading test. The fracture is between the smear layer and the bonding agent. Image d shows the bonding layer without cracks (×1 500). Image e shows a smear layer without cracks (×2 000). Image f shows a series of microscopic cracks found inside the bonding agent of another specimen (×2 000).

Figure 5 Results of load cycles of Groups BP and BA. There is significant difference in fatigue cycles between Groups BP and BA (P<0.05). Group BP experienced significantly more fatigue cycles than group BA.

Figure 6 The result of fluid penetration. At the vertical section of root furcation, the loaded group experienced significantly more dye penetration than the control group (*P<0.001). In the loaded group, the depth of dye penetration at the vertical section experienced significantly deeper than the transverse section of crown (*P=0.001).
Cyclic-load testing of vertically fractured tooth

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DISCUSSION

The multidisciplinary treatment of vertically fractured teeth requires several procedures including extraction, bonding and replantation. Predictably, success involves disinfection of the fractured segments, bonding them to an acceptable clinical strength with a biocompatible material, and maintaining the health of the tooth with periodontal reattachment at the bonded fracture site. Two kinds of PDL response can occur—either normal PDL or ankylosis state—after replantation according Andreasen et al.14,23–24 This may be one of the most important factors for cyclic-loading resistance of the bonding layer and the long-term prognosis of vertically fractured teeth.

This in vitro study examined the cyclic-loading resistance of bonded, vertically fractured premolars with and without crown restoration, in a setting simulating two different PDL states.

The oral cavity is a complicated biomechanical environment and tooth fracture is caused by an equally complicated mechanical process. Complete vertical fractures occur most frequently in molars, followed by premolars. The position, direction and depth of the fracture may vary considerably. In order to make the tests reproducible, this study focused on a very similar set of upper first premolars of adolescent humans aged 14–20 years old with two roots. These teeth were chosen because of their ready availability. According to the literature, vertical fractures occur frequently in the middle-aged population but intact premolars are not easy to obtain from middle-aged people. Although different ages may mean differences in organic matter and different reactions to bonding agents, the standardisation of teeth from one age group implies that they are likely to they perform consistently. No effect was shown in the relationship of the cyclic-loading resistance and the PDL state. The 4-META/MMA-TBB resin is not affected by blood contamination, has a high tensile strength and is biocompatible25–27—hence, it was selected to bond the vertical fractures in this study. Its high bonding strength is due to the active component, 4-META. This compound has both hydrophilic and hydrophobic properties. Acid anhydride groups are strongly polarized by these molecules, which increases the wettability of the resin.

This research aimed to simulate the clinical station, so the methodology, especially the model was critical. Firstly, in order to simulate the vertical fracture as seen clinically, several approaches were tested in preliminary experiments. Although it is impossible to exactly reproduce clinical fractures, the method outlined was chosen because it was repeatable, and convenient. It also ensured that there was no difference between the samples regarding the direction of fracture and the areas available for bonding.

The two types of PDL conditions were difficult to mimic. A layer of silicone rubber surrounding the tooth was used to simulate a fully healed periodontal ligament. The surrounding epoxy resin played the role of alveolar bone. Since their elastic modulus are similar, the artificial materials and the natural tissues function similarly in transmitting stress.22 The epoxy resin used in this experiment was very closely adapted to the teeth and no mobility was detected—hence, the model was used to mimic ankylosis.

The results of cyclic-loading testing showed that crown restoration and functional healing of the periodontal tissues are both of critical importance for long-term retention of vertically fractured teeth. The health of the periodontal tissues decreases the effect of repeated stresses on the bonding agent, in addition to being desirable for its own sake. Three-dimensional finite element analysis of premolars in normal occlusion has shown that vertical stress on the tooth always occurs around the root apex and in the wall of the root furcation.21 The repaired periodontal ligament acts as a buffer between the hard dental tissues and the alveolar bone. It absorbs shocks, dispersing the stress on the dentin. This is of great significance to the cyclic-loading resistance of the bonding layer.

Cyclic-loading testing changed the microscopic structure of the bond to some extent in most specimens and the SEM evaluation supported this finding. If the resin broke, the fracture always occurred...
between the hybrid layer and the luting agent. This region is thought to be the main weakness of the bonding layer.\textsuperscript{79–30} Under SEM examination, microscopic cracks were found inside the bonding resin, but these defects did not appear to greatly influence the cyclic-loading resistance and stability of the bonding agent. Thus, the prognosis for vertically fractured teeth with crowns and functional healing of the periodontal tissues may be favourable.

As previously mentioned, taking into account the limitations of this \textit{in vitro} model and the cyclic-loading test procedure, a better model duplicating the true clinical situation should be explored and future research should be carried out to support these findings. However, the results of this study support the conclusion that periodontal reattachment can benefit the prognosis of bonded fractured teeth from the point of view of biomechanics.

With advances in dental science, such as better storage media for maintaining the periodontal health of avulsed teeth, high-strength and relatively biocompatible bonding agents, and barrier techniques aiding the establishment of reattachment on denuded root surfaces, the long term restoration and retention of vertically fractured posterior teeth may be as possible.

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