Influence of Building Heights and Nature of Rooftop Views on Propagation Loss Prediction for Tropical Environment in Ondo State, Nigeria

P. Akinyemi  
Department of Physics  
Adeyemi College of Education  
Ondo State, Nigeria

O. O. Adeoye-Oladapo  
Department of Physics  
Adeyemi College of Education  
Ondo State, Nigeria

O. T. Kolebaje  
Department of Physics  
Adeyemi College of Education  
Ondo State, Nigeria

ABSTRACT
In one of the underlying difficulties with the application of a predicting path loss model for any environment is that no two areas have the same building composition. It is therefore intractable to formulate the exact path loss model for all location. In order to overcome some of the problem stated above, parameters of certain propagation models must be fine-tuned with reference to target environment. In this study, the ITU-R 526 adopted Walfisch-Bertoni (W/B) path loss model is modified base on the experimental campaign over some selected locations in Western part of Nigeria. Afterwards, the multiple diffraction loss component of the W/B model was modified to incorporate effects of building height variation $\Delta H_b$. In addition to variations in buildings height, the effect of top view of buildings on the diffraction of roof top fields down to street level were estimated between 1.61 dB and 5.32. The optimized model will be useful for the new breed technologies especially the advanced long term evolution in Nigeria.

Keywords
Pathloss, Walfisch-Bertoni model, Western Nigeria and optimized model.

1. INTRODUCTION
The introduction of cellular networks has imposed the need to predict radio path loss in all environments between elevated antenna and mobile street level [2]. Response to this need has been the development of models to describe the propagation in space [1, 3, 7]. In literature, series of propagation models were published because descriptions of terrain and land-use information can vary widely from location to location [6,3]. To account for the variations in building heights in the studied locations, parameters of certain propagation models must be optimized with reference to target environment [7, 4]. Outdoor radio wireless communication is ruled by reflection, diffraction, multipath from natural and man-made objects obstructing the propagation channels [8, 5]. The arrival of the same signal from different paths and times and its combination at the receiver causes the signal to fade. This phenomenon is referred to as multipath fading and is a direct result of multipath propagation. Specifically, it has been reported in academic literature that the propagation models applied to microcells mobile systems have built-in-error generally of the order of 7-10 dB standard deviation [9].

This study present a theoretical model which account for the effect of building heights variation to make a site-specific prediction of the path loss averaged over sectors live signals transmission on macro-cellular service provider in an outdoor propagation in the western part of Nigeria.

2. MEASUREMENT CAMPAIGN
A site verification exercise was done using testing tool (Ericsson k800i mobile station) running on the software mode, calls were initiated at each test point until it established and the signal strength information sent over the air interface between the base station and the mobile station. The field tests were conducted in Ondo State, Nigeria, with two different operators namely A and B respectively. Site where one of the measurements are taken in Ondo State are depicted in Figure 1. Eight BS cell sites were randomly selected in the locations of study and calls were initiated at each test point until it is established and the signal strength information sent over the air interface between the base and the mobile station. These sites consist of building with varying heights. For every site, received signal strength were measured at a reference distance of 100m from the base station and at subsequent interval of 100m. The environmental parameters of the studied locations are presented in Table 1. All measurements were taken in the mobile active mode and in three sectors of each base station. This was to ensure that the mobile phone was in constant touch with the base station. The obtained values from field measurements are then compared with those calculated using the existing models. The essence of this is to investigate the degree of consistence of these existing models with field measurements. Map showing one of the Investigated Urban Environments is depicted in Figure 2.

Figure 1: Site where one of the measurements are taken in Ondo State.
Table 1: Base Station Parameter

| Parameters                              | Values for Operator A | Values for Operator B |
|-----------------------------------------|-----------------------|-----------------------|
| Base station transmitter power          | 40 dB                 | 40 Db                 |
| Base station antenna height             | 40 m                  | 42 m                  |
| Mobile antenna height                   | 1.2 m                 | 1.5 m                 |
| Transmitter antenna gain                | 17.5 dB               | 17.5 dB               |
| Frequency                               | 900 MHz               | 1800 MHz              |
| Feeder loss                             | 2.52 dB               | 2.58 dB               |
| Duplexer loss                           | 4.5 dB                | 4.75 dB               |

3. THE WALFISCH-BERTONI MODEL

Walfisch-Bertoni (W/B) modeled path loss to three elements: Free space loss, $P_{GO}$; reduction in the field at the rooftop just before the mobile due to propagation past previous buildings, $P_{G1}$ and diffraction of the rooftop field down to the mobile (add ray power to get the small area average), $P_{G2}$.

![Figure 3: propagation geometry for Walfisch-Bertoni model](image)

**Total Path Loss**, $P_G = (P_{GO})(P_{G1})(P_{G2})$

(1) Free space path loss is given as [8, 10]

$$P_{GO} = \left(\frac{\lambda}{4\pi r}\right)^2$$  \hspace{1cm} (2)

Path loss as a result of multi-screen loss $(P_{G1})$ is given as [7,8]

$$P_{G1} = PL_{rooftops} = 0.01\left(\frac{h_T-H_B}{0.03R}\right)^{1.8}\left(\frac{d}{\lambda}\right)^{0.9}$$  \hspace{1cm} (3)

Path loss as result of Diffraction and Reflection of propagated Signal form Rooftop down to the Street $(P_{G2})$ is given as [7,8]

$$\rho_{G2} = \frac{1}{2\pi K \rho_1} \left[\frac{1}{|\theta_2|} - \frac{1}{2\pi |\theta_1|}\right]^2 \approx \frac{1}{K \pi \rho_1 \theta_1^2}$$  \hspace{1cm} (4)

Substituting Equations (2), (3) and (4) into Equation (1)

$$P_G = \left(\frac{\lambda}{4\pi r}\right)^2 0.01\left(\frac{h_T-H_B}{0.03R}\right)^{1.8}\left(\frac{d}{\lambda}\right)^{0.9} \frac{\lambda \rho_1}{2\pi^2(H_B-h_m)}$$  \hspace{1cm} (5)
Equation (5) can be expressed in decibels as:

\[
PG = 89.5 - 10 \log \left( \frac{\rho 1d^{0.9}}{(H_B - h_m)^2} \right) + \\
21 \log f_M - 18 \log(h_T - (H_B \pm \Delta H_B)) + \\
38 \log R_k
\]  

(6)

where,

\( f_M \) = Frequency in MHz ; \( h_T \) = Antenna height in meters;

\( H_B \) = Building height in meters

\( h_m \) : Mobile height in meters.

4. MODEL COMPARISON

Among lots of propagation models: Hata, S U I, COST-231, Free Space and W/B models were suggested as good solutions for macro cellular signal in the studied locations because they are the most used propagation model in literature [7, 8]. From the results presented in Table 2 and 3, the data obtained from the measurement are closer to the Walfisch-Bertoni model with RMSE value between 9.29-13.16 and far from FSPL with RMSE value between 32.67-47.44 for operator A and B. Based on the closest agreement with measurement data, the Walfisch-Bertoni is selected as the best model for signals prediction in Ondo State, Nigeria.

4.1 W-B Model Optimization

The influence of variations in building height from row to row is investigated by simulating random height variations and computing the resulting signal at the mobile for many such variations. In the studied locations, the buildings were assigned different heights that were uniformly distributed between \( (H_B) \pm \Delta H_B \) where \( (H_B) \) is the height of building and \( \Delta H_B \) is the maximum height deviation. Therefore, the multiple diffraction loss components of the W/B model will be modified to include in building height, \( \Delta H_B \) as thus:

\[
P_{G_{1(\text{New})}} = P_{LT(\text{New})} = 0.01 \left( \frac{h_T - (H_B \pm \Delta H_B)}{0.83R} \right) \left( \frac{\lambda}{\lambda_0} \right)^{1.8} \left( \frac{\rho}{\rho_0} \right)^{0.9}
\]

(7)

Combining equation (2), (4) and (7), the optimized W/B pathloss model becomes:

\[
P_L T(\text{New}) = 89.5 - 10 \log \left( \frac{\rho 1d^{0.9}}{(H_B - h_m)^2} \right) + \\
21 \log f_M - 18 \log(h_T - (H_B \pm \Delta H_B)) + \\
38 \log R_k
\]

(8)

In order to obtain an accurate estimate of building heights, for each configuration, building height variations, \( \Delta H_B \) between 1.61 dB and 5.32, were simulated. The simulations were performed on 350 buildings of various heights measured with aid of clinometers in the studied locations. Also, the RMSE of the optimized W/B path loss model of the studied locations were calculated using equation (8) and summarized in Table 2-3.

| BS site | FSPL model | HATA model | COS T 231 model | SUI model | W/B model | Optimize d W/B model |
|---------|------------|------------|-----------------|-----------|------------|---------------------|
| BS 1    | 42.64      | 14.36      | 13.81           | 31.45     | 13.16      | 4.69                |
| BS 2    | 43.21      | 17.62      | 16.46           | 27.51     | 12.27      | 6.93                |
| BS 3    | 41.19      | 13.28      | 13.62           | 24.60     | 9.29       | 5.59                |
| BS 4    | 47.44      | 15.31      | 14.62           | 27.88     | 11.70      | 7.71                |

| BS site | FSPL model | HATA model | COS T 231 model | SUI model | W/B model | Optimize d W/B model |
|---------|------------|------------|-----------------|-----------|------------|---------------------|
| BS 1    | 34.54      | 13.29      | 14.76           | 21.69     | 11.43      | 6.17                |
| BS 2    | 32.67      | 12.88      | 16.30           | 27.46     | 9.49       | 5.49                |
| BS 3    | 38.31      | 11.70      | 14.45           | 24.11     | 8.82       | 4.71                |
| BS 4    | 41.28      | 16.31      | 13.14           | 27.66     | 9.68       | 6.88                |
Fig. 4: Plots of the original W/B, optimized model W/B and measured path loss for operator A and B operating at 900 and 1800 MHz

5. VARIABILITY DUE TO TOP VIEW

In addition to variations in building height, another source of variability considered was the effect of top view of buildings on the diffraction of roof top fields down to street level.

Several cases of building construction are depicted in top view as shown in Figure 5. For cases (A) and (C) in Figure 5, diffraction were considered as if it had occurred on an absorbing half screen using the diffraction factor in Equation (9) with d/2 replaced by the horizontal distance x from the equivalent half screen to the mobile. For building with a absorbing insulation, the diffraction factor is given as:

$$\theta = \tan^{-1} \left( m \frac{h_B - h_m}{x} \right) - \alpha$$

For building with aluminized insulator or aluminized siding as shown in cases (B) and (D) in Figure 5, the diffraction factor is given as:

$$F_c = \frac{\sqrt{\lambda}}{4 \pi \left( x^2 + (h_B - h_m)^2 \right)^{\frac{1}{2}}} \left[ \cos \left( \frac{\pi + \theta}{2} \right) - \sec \left( \frac{\pi + \theta}{2} \right) \right]$$

For average path loss model, diffraction down to street level is gives an intensity proportional to $2 \left[ F(d/2) \right]^2$

The individual ray intensities relative to that used in the average path loss are given by

$$1/2 \left[ F(x)/F(d/2) \right]^2$$

or by

$$1/2 \left[ F_c(x)/F(d/2) \right]^2$$

For these calculations $\lambda = 1/4$ m and $\alpha = 0.9$ rad is assumed.
6. CONCLUSION
This paper presented a comparative study between measurement survey on live signal transmission of macro-cellular service providers situated in Ondo, Nigeria. The result revealed that the optimized W/B model have better predicting accuracy when compared to the original W/B in the studied locations. It could be observed from Figure 4 and Table 2-3 that the optimized W/B model have better predicting accuracy when compared to the original W/B in the studied locations. Difference in RMSE values between the proposed and Walfisch-Bertoni model are ranged from 0 dB up to 3 dB. Therefore, for all the studied macro cells, the introduction of building heights variation in the multiple diffraction loss components of the W/B model improved the model’s prediction accuracy. Thus, the proposed optimized path loss models indicate better prediction accuracy in term of root mean square error when compared to the original Walfisch Bertoni model. It was also observed that the nature of the rooftop (view of buildings) and its effect on diffraction of roof top fields down to street level will result in deviations sector averaged signals that range between 1.6 dB and 5.32 dB.

7. ACKNOWLEDGEMENT
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