Statistics of tumbling of a single polymer molecule in shear flow.

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We present experimental results on statistics of polymer orientation angles relatively to shear plane and tumbling times in shear flow with thermal noise. Strong deviation of probability distribution functions (PDF) of these parameters from Gaussian was observed and a good accord with theory was found. The scaling relations of PDF widths for both angles as a function of the control parameter Wi are verified and compared with numerics. An universal exponential PDF tail for the tumbling times and its predicted scaling with Wi are also tested experimentally against numerics.

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Dynamics and statistics of a single polymer molecule in stationary as well as in random flows have recently attracted attention of both experimentalists [1–4] and theorists [5–10]. Stretching dynamics and statistics and coil-stretch transition in these flows were investigated in detail. Besides, another remarkable effect was first observed in a shear flow [2], namely large fluctuations in a polymer elongation due to end-to-end aperiodic tumbling (see Fig.1D).

Recently rather extensive theoretical [11,12] and numerical [13,14] efforts were conducted with the goal to understand the statistics of the angular orientation of a polymer molecule and of the tumbling time in a random velocity field with a mean shear. Shear flow with a thermal noise was considered there as a particular case. A role of thermal noise on a solid rod tumbling in a shear flow was first considered in Ref. [15]. Then the role of the Brownian fluctuations in the polymer dynamics and statistics was studied in numerical simulations [7], where, however, only the power spectral density and the statistics of polymer extension in a shear flow were investigated. An average polymer extension and angular orientation were theoretically considered also in Ref. [8], where the results of calculations were compared with light scattering measurements [16,17].

In this Letter we concentrate on statistics of angular orientation and tumbling and scaling relations of their characteristics for a single DNA molecule in a shear flow, when thermal fluctuations are the main cause for tumbling.

It is well known that a probability distribution function (PDF) of the end-to-end vector $\vec{R}$ for a polymer described by a dumbbell model with a linear relaxation in a simple shear is Gaussian [7]. Nevertheless, PDFs of the polymer extension, $|\vec{R}| \equiv R$, as well as polymer angular orientation are strongly non-Gaussian due to anisotropy introduced by the shear. A functional form of the PDF of the polymer extension in a shear flow was first identified experimentally [2] and then explained theoretically and numerically [7].

The main result of the recent theory [11,12] is the prediction of the intermittent (non-Gaussian) statistics of polymer angular orientation in a shear flow. Moreover, it was also shown that intermediate asymptotic of the angular polymer statistics bears some universal features independent of the nature of polymer random excitation [11,13,14].

The universal features of the orientation statistics are related to a deterministic nature of the angle evolution at large angles, where a random pumping can be neglected. Then the theory [11,12] predicts the following results on the angular distributions and tumbling time statistics: (i) at $|\phi| \gg \Delta \phi \sim W^{-1}$ one gets $P(\phi) \propto (\sin \phi)^{-2}$, where $\Delta \phi$ is the width of $P(\phi)$; (ii) at $1 \gg |\theta| \gg \Delta \phi$ the PDF tail for $\theta$ is determined as $P(\theta) \propto |\theta|^{-2}$; both scalings follow from the deterministic process; (iii) the tail of PDF of tumbling time between two consequent flips, $\tau_\phi$, is exponential at $\tau_\phi \gg \tau_\mathrm{rel}$, where $\tau_\phi$ is the characteristic tumbling time that is proportional to $\tau_\mathrm{rel}$. Thus, the major theoretical finding is the intermittency phenomenon in the statistics of a single polymer tumbling that results in either algebraic or exponential tails of the distribution of polymer angular orientations and tumbling times, respectively.

Another theoretical result verified by extensive numerical simulations based on linear dumbbell as well as FENE models describes the scaling relations for the width of the angular distributions and the characteristic tumbling time with $W_i$ [11–14]. The scaling can be derived by simple physical arguments used by the theory [11,14]. The dynamic equation for one of the molecule orientation angles (see Fig.1A), namely $\phi$, in the region of $\phi \ll 1$ can be written as $d\phi = -s \sin^2 \phi + R_g^2 (\tau_\mathrm{rel})^{-1/2} \eta_\phi$ [11–14], where $R_g$ is the polymer gyration radius, and $\eta_\phi$ is the white thermal noise. In a stationary state one gets from a balance of shear and noise terms the following estimates for the rms of the angular fluctuations (or the PDF width), $\Delta \phi$, and the characteristic tumbling time, $\tau_\phi$:

$$\Delta \phi \propto W^{-1} \left( \frac{R_g}{R} \right)^{3/2}, \quad \tau_\phi \propto \tau_\mathrm{rel} W^{-1} \left( \frac{R_g}{R} \right)^{-3/2}. \quad (1)$$

Then one can consider two limits at $W \gg 1$ (or small
\(\Delta \phi \) and \(\Delta \theta\). In the linear extension limit, \( R \ll R_{\text{max}}\), where \( R_{\text{max}}\) is the maximum polymer extension, a typical polymer elongation, \( R \), can be estimated as \( R_g \cdot W_i \) that is realized at sufficiently small extensions (up to 20\% of \( R_{\text{max}}\) [1,4]). It leads to [11–14]

\[
\Delta \phi \propto W_i^{-1}, \quad \tau_i \propto \tau_{\text{rel}}. \tag{2}
\]

In the opposite limit of a non-linear regime, where typically \( W_i \geq R_{\text{max}}/R_g \), a stretched polymer can be treated as a rigid rod with \( R \sim R_{\text{max}} \) subjected to the Brownian motion [15]. Then the resulting scaling appears to be strikingly different [11–14]:

\[
\Delta \phi \propto W_i^{-1/3}, \quad \tau_i \propto \tau_{\text{rel}} W_i^{-2/3}. \tag{3}
\]

Similar scalings can be also expected for \(\Delta \theta\).

The experiments were carried out in a shear flow in two flow configurations. To measure \( \theta \) we used a shear flow in a gap between the flat bottom of the uniformly rotating glass rod of radius \( r_1 = 1.5 \) mm and a cover slip (see for details of the set-up [4]). The measurements were made at the fixed height of \( \sim 30 \) \( \mu \)m above the cover glass in the region located at radius \( r \approx 700 \) \( \mu \)m, where the main shear occurs in the vertical plane. Then only \( \theta \) can be measured in this configuration (see Fig.1B).

To measure \( \phi \) a shear boundary layer of a Poiseuille flow in a micro-channel was used. The micro-channel of \( \sim 500 \)\( \mu \)m wide and \( \sim 100 \)\( \mu \)m deep was produced from a single cast of a silicon elastomer Polydimethyl-siloxane (PDMS) using the soft lithography method [18]. The measurements were carried out at about the middle height of the channel in a small region at a distance of \( \sim 30 \)\( \mu \)m from the channel wall, where only \( \phi \) was detected via the cover glass (see Fig.1C).

Particle image velocimetry (PIV) measurements were conducted with 0.2\( \mu \)m fluorescent beads in both flow configurations. In the swirling flow the shear rate in the vertical plane is rather constant at the location of measurements of \( \sim 30 \)\( \mu \)m (Fig.2A), while the azimuthal velocity in the horizontal plane almost independent of radius in the region of measurements (inset in Fig.2A). In the channel flow the longitudinal velocity measured in the horizontal plane changes rather linear in the observation region of \( \sim 30 \)\( \mu \)m from the wall, while looks fairly constant in the vertical plane at the middle height of the channel within the focus depth (0.4 \( \mu \)m) (see Fig.2B). In both cases the measured velocity profiles are compared with numerical calculations, and good quantitative agreement is found (solid lines, Fig.2A,B). A limitation to conduct PIV measurements in a vertical plane deeper than \( \sim 50 \)\( \mu \)m in both geometries is due to the objective working distance that is about 200\( \mu \)m.

As a working fluid a buffer solvent [19] with sucrose concentration varied in the range between 47\% (w/w) and 67\% (w/w) to tune viscosity in the range between \( \eta_s = 0.012 \) Pa-s and \( \eta_s = 0.24 \) Pa-s at the working temperature of 22.5\(^\circ\)C was used.

To study the tumbling dynamics and statistics of polymer molecules in a flow 10\(^{-3}\) ppm of \( \lambda \)-DNA molecules, fluorescently labelled with YOYO-1 (Molecular Probes) at a dye/base ratio of 1:4 for \( \sim 1 \) hour, were added into the solvent. At equilibrium the coiled \( \lambda \)-DNA has \( R_g = 0.73 \)\( \mu \)m, while the entire contour length is \( R_{\text{max}} \approx 21 \)\( \mu \)m. So it may be considered as a "flexible" polymer with roughly 300 persistence lengths [1]. The maximum relaxation time relevant for further analysis, \( \tau_{\text{rel}} = 11 \pm 0.1 \) sec for a solvent with 62\% (w/w) sucrose was found. \( \tau_{\text{rel}} \) for solvents with different sucrose concentrations was taken proportional to its concentration variation [1,2]. Fluorescently labelled DNA molecules were monitored via \( \times 63, 1.4 \)NA oil immersion objective (Zeiss) with 0.4 \( \mu \)m depth of focus with a homemade inverted epi-fluorescent microscope [4]. Images of the molecules were digitized, and their \( \theta \) and \( \phi \) angles were automatically measured by approximation of a molecule outline with an ellipse, which main axis was used as the end-to-end vector, \( \vec{R} \), to define an inclination angle, either \( \theta \) or \( \phi \) depending on the flow configuration (see Fig.1A,B,C). This approximation works well for sufficiently stretched molecules down to \( \sim 3 \)\( \mu \)m for the main axis. Two time series of different scenarios of tumbling that occur in a shear flow are presented in Fig.1D. One mentions that tumbling can take a place via coiled as well as folded states.

In the lower inset in Fig.3 we present PDFs of \( \theta \) for two values of \( W_i \). Each plot is based on up to 30,000 points. It is clear seen that at low \( W_i = 1.6 \) PDF can be fitted by Gaussian almost entirely, while at high \( W_i = 17.6 \) the PDF tails strongly deviate from the Gaussian. In Fig.3 PDFs for three values of \( W_i \) are presented in the logarithmic coordinates. The PDF tails for all values of \( W_i \) decay algebraically with the exponent rather close to the theoretical, \( | \theta |^{-2} \), indicated by a solid line on the plot. The larger \( W_i \), the wider the scaling region at the tail as predicted by the theory [11]. Variations in \( W_i \) values were achieved by viscosity tuning as well as variation in \( \dot{\gamma} \) by changing rotation speed \( \Omega \) between 0 and 0.7 sec\(^{-1}\). The half-height width of PDFs, \( \Delta \theta \), decreases as \( \propto W_i^{-0.38 \pm 0.03} \) (see the upper inset in Fig.3) in a rather good agreement with the recent numerical simulations based on the FENE model [14].

In the same set-up with the rotating rod we measured PDFs of the tumbling time \( P(\tau) \), determined in the experiment as time between two following consequent conformations: two coiled, two folded, or coiled and folded ones (see Fig.1D). This tumbling time, \( \tau \), is elongation based time defined by a certain length threshold \( R_{th} > R_g \), and it is different from \( \tau_0 \) that is angular based. The lower the threshold, the higher \( \tau_0 \) [14]. We present in Fig.4 \( P(\tau) \) for three values of \( W_i \) together with the exponential fits. Each plot is based on up to 600
points. The same data presented in the log-linear coordinates together with the fits demonstrate the fit quality (inset in Fig.4). Figure 5 shows the characteristic tumbling time, $\tau_t$, obtained from the slopes of the PDF tails, versus $Wi$. The value $\tau_t$ depends on the threshold value $R_{th}/R_g$. $Wi$ was varied in two ways: full squares present the data, where $Wi$ was tuned just by viscosity variation (it means the variation of $\tau_{rel}$), and open squares were obtained at different $Wi$ by adjusting $s$. By presenting the same data as the ratio $\tau_{rel}/\tau_t$ versus $Wi$ in the inset in Fig.5 we show, first, that $\tau_t$ is proportional to $\tau_{rel}$ at lower $Wi$, and second, $\tau_{rel}/\tau_t$ grows as $\propto W_i^{0.54\pm0.04}$ at higher $Wi$ in a rather close agreement with Eqs.(3,4). We would like also to point out the fact that the cross-over region for scaling in $\tau_t$ takes place at $Wi \approx 10$ in amazing agreement between the experiment and the recent numerical simulations [14]. An obvious shift upwards of the data relative to the simulations (inset in Fig.5) is explained by about twice smaller value of $R_{th}/R_g$ for determination of $\tau_t$ in the simulations [14].

In Fig.6 PDF of $\phi$ measured in a micro-channel flow at $Wi = 25$ together with the fit by $(\sin \phi)^{-2}$ is shown. It is clear that the PDF maximum is located at $\phi_t \neq 0$ but limited angular resolution does not allow us to study its dependence on $Wi$. Similar data on $P(\phi)$, based on 2000-3000 points for each plot, were obtained for several values of $Wi$. The half-height width of PDFs, $\Delta \phi$, as a function of $Wi$ is shown in the inset in Fig.6 together with the fit and the results of the numerical simulations based on the FENE model [14]. The observed scaling $\propto W_i^{-0.51\pm0.04}$ manifests the cross-over region between $\propto W_i^{-1/3}$ expected at high $Wi$ and $W_i^{-1}$ at lower $Wi$ values (see Eq.(3,4)).

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FIG. 1. A) Polymer orientation angles in a shear flow; B) Schematic diagram of rotating rod set-up; C) Schematic diagram of micro-channel set-up; D) Images of various polymer conformations consequent in time during tumbling. White bar is 3.5µm.

FIG. 2. A) Azimuthal velocity vs vertical coordinate; inset: the same vs radius. Region of measurements is around $R = 700\mu m$ and at height of $\sim 30 \mu m$. B) Squares are longitudinal velocity in horizontal plane, circles- the same in vertical plane. Region of measurements at $30 \pm 10 \mu m$ from the channel wall and at height of $\sim 50 \mu m$ (dash line). Solid lines on all plots are theoretical.

FIG. 3. PDFs of $|\theta|$ in logarithmic coordinates: $Wi = 1.6-$pluses, $Wi = 8.5-$circles, $Wi = 17.6-$squares. A solid line is theoretically predicted asymptotic scaling for PDF tails. Lower inset: PDFs of $\theta$ for $Wi = 1.6-$pluses, and $Wi = 17.6-$squares presented in log-linear coordinates; the solid curves are Gaussian fits. Upper inset: $\Delta \theta$ vs $Wi$; squares-data, triangles-numerics. A solid line is the fit.

FIG. 4. PDFs of $\tau$ at several values of $Wi$. The solid lines are exponential fits. Inset: PDFs of $\tau$ in log-linear coordinates with fits to the data at $Wi = 4.7-$triangles, $Wi = 8.5-$circles, $Wi = 17.6-$squares.
FIG. 5. $\tau_i$ vs $Wi$: full squares-data taken at constant $s$ and varying viscosity; open squares-data taken at constant viscosity and varying $s$. The dash lines are guides to eye. Inset: $\tau_{ext}/\tau_i$ vs $Wi$; triangles-numerics. Solid lines are the fits.

FIG. 6. PDFs of $\phi$ in log-linear coordinates at $Wi = 25$. A solid curve is the fit by $\alpha (\sin \phi)^{-2}$. Upper inset: $\Delta \phi$ vs $Wi$; squares-data, triangles-numerics. A solid line is the fit.
