1. Introduction

Mg and its alloys have been considered as some of the most promising materials in recent years due to their advantageous mechanical properties and low density.\(^1\)\(^-\)\(^3\) To improve the corrosion resistance of Mg alloys, electrodeposition of chemically and mechanically protective Al coatings from ionic liquids has attracted both scientific and industrial curiosity.\(^4\)\(^-\)\(^8\) Most practices of electrodeposition of aluminum on Mg alloys are processed in an inert atmosphere, e.g., a glovebox owing to the high air and moisture sensitivity of common ionic liquids.\(^9\)\(^-\)\(^10\) This drawback has seriously limited the industrial production. Parallel to the exploration of air and water-stable ionic liquids in related fields,\(^11\)\(^-\)\(^12\) a way to protect working ionic liquids has been proposed. For example, using a non-water-absorbable layer of a particular hydrocarbon compound, such as decane, has helped realize electrodeposition in air. Nevertheless, the preparation of ionic liquid bath still needs to be conducted in an argon-filled glove box.\(^13\) Is it possible to develop a simple and practical method to allow the whole procedure of electrodeposition of Al coatings on Mg alloys to be carried out in air?

In the current communication, a solid water-absorbent material was introduced into the mixture of AlCl\(_3\) and 1-butyl-3-methylimidazolium chloride ([Bmim]Cl) to investigate the possibility of the preparation of ionic liquid in air. In addition, decane was used as the organic protective layer during electrodeposition. Under this dual protection, the electrodeposition of Al coatings on AZ91D Mg alloy was performed at the designated current and potential to investigate the effect and degree of the proposed treatment method.

2. Experimental

2.1 Chemicals

All employed chemicals were commercially available and used without further purification: 1-butyl-3-methylimidazolium chloride ([Bmim]Cl) with chemical formula \(C_{8}H_{15}ClN_{2}\) (Aldrich, 99%), aluminum chloride anhydrous (Aldrich, ≥99%), and undecane (Aldrich, ≥99%).

2.2 Procedure

AlCl\(_3\) and [Bmim]Cl were mixed in a molar ratio of 2 : 1 at room temperature,\(^14\)\(^-\)\(^15\) followed by the addition of the water-absorbent material (4A molecular sieve, around 10 wt% of ionic liquid). The mixture was then covered with undecane layer and stirred for 24 h to complete the reaction. Then, the resultant ionic liquid was transferred into an electrobath. The electrodeposition was carried out with a conventional three-electrode cell on electrochemical workstation (CS310, Wuhan CorrTest Instruments Corp., Ltd.) at ambient temperature. High-purity Al sheets (70 × 20 × 1 mm) were used as anode, and a die-cast AZ91D Mg alloy sheet (9.02 wt% Al and 0.49 wt% Zn) was used as cathode (70 × 20 × 2 mm). The area of working electrode was set as 6 cm\(^2\) as it was actually immersed in the electrolyte. The Al wire was connected as a reference electrode. Before electrodeposition, each metallic sample was ground with 1000-grit SiC papers, and the polished
Mg alloy sheet was further treated with 10% phosphoric acid to prevent oxidation and to increase the adhesion strength.

Constant potential (−0.67 V vs. the Al wire) and constant current (−30.08 mA) were applied to investigate the deposition of aluminum. A schematic diagram of the experiment is shown below (Fig. 1).

### 3. Results and discussion

The electrodeposition process was performed potentiostatically or galvanostatically for 7500 s in each case (Fig. 2). As shown in Fig. 2a, the current density under −0.67 V electrodeposition decreased rapidly at the beginning (0–300 s). In the first part of transition, a large cathodic current was observed due to sudden deposition of abundant Al ions to form nuclei on the surface of Mg alloy, and the subsequent decrease in current was caused by the formation of depletion layers of Al ions. The subsequent decrease in cathodic current was induced by nuclei growth, which enabled efficient collection of Al ions due to the steric effect. The continuously decreasing deposition current indicated continuous growth of diffusion layers due to the higher rate of Al ion consumption.

After that, the current density decreased steadily with electrodeposition time. This indicated that the Mg alloy was already covered with an Al coating, and the electrodeposition process changed to Al electroplating on the Al substrate.

When the cathode current was maintained at −30.08 mA (Fig. 2b), the potential shifted rapidly from −0.80 V to −0.87 V during the first 130 s. The large potential at the start of the transition might also be due to sudden deposition of Al to form nuclei; the subsequent increase in the cathodic potential was caused by nuclei growth. After the formation of a depletion layer of Al, the deposition potential continuously decreased for the growth of the diffusion layer with a higher rate of Al ion consumption. Hereinafter, the Al coatings were formed and the

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**Fig. 1** Scheme of the experimental process.
Electrodeposition potential started to decline as a function of time.\textsuperscript{5,16}

It can be found that the profiles of current density and potential change were different with constant potential and constant current density. The initial increasing potential obtained at constant current deposition was favorable for the formation of Al nuclei in the first part; the uniform nucleus arrangement at the starting determined the quality of the Al coating. As a comparison, the currents in constant potential deposition did not display a process of growth and then decline. This indicated that the formation of Al nuclei was insufficient.

The coatings obtained at a constant potential or constant current have similar appearance. One photograph of an Al-electroplated Mg alloy (AZ91D) strip from AlCl$_3$/[Bmim]Cl ionic liquid is shown in Fig. 3; it is obtained at a constant current of $30.08 \text{ mA}$ with 7500 s.

To conduct detailed investigation on the difference between the samples obtained at either constant potential or constant current density, XRD was used to characterize the crystallinity of coatings (Fig. 4). Characteristic diffraction peaks indicated that crystalline Al was deposited on both samples. Furthermore, the peaks of Al (111) of the two samples were explored to determine the grain size of the Al coatings. The full-width at half maximum (FWHM) values of the Al (111) peaks are displayed in Fig. 4. The grain sizes of Al coatings obtained with $-0.67 \text{ V}$ constant potential and $-30.08 \text{ mA}$ constant current were 42.5 and 41.0 nm, respectively, which were calculated with the Scherrer’s equation.\textsuperscript{17}

The Al coatings obtained from ionic liquid in the glove box reported by N. Koura\textsuperscript{18} showed similar crystal forms. However, the grain sizes of Al coatings obtained in the present study were slightly larger than that of the Al coating (32 nm) prepared from the ionic liquid in the glove box by S. Zein El Abedin.\textsuperscript{17}

The obtained Al coatings were also examined using a scanning electron microscope (SEM) (Philip XL-40FEG) and energy dispersive spectrometer (EDS) (Oxford instruments X-Max) (Fig. 5).

Fig. 5a and b demonstrate the SEM images of the coatings obtained with $-0.67 \text{ V}$ and $-30.08 \text{ mA}$, respectively. Fig. 5c shows a high resolution SEM micrograph of Al coatings on an Mg alloy substrate electrodeposited at a constant potential of $-0.67 \text{ V}$ for 7500 s at room temperature. It can be observed that there were fine cracks in the top coating, which may be due to internal or residual stress during electrodeposition, and this is
disadvantageous for corrosion resistance, resulting in serious oxidation.\textsuperscript{19} In contrast, the electrodeposition at \(-30.08\) mA for 7500 s afforded a continuous and compact Al coating, as shown in Fig. 5d.

EDS analysis indicated that Al and Mg atoms were mainly distributed on the outer coatings with mean compositions of 78\% Al and 22\% Mg for the potentiostatirical electrodeposition sample (Fig. 5e) and 84\% Al and 16\% Mg for the galvanostatirical one (Fig. 5d), respectively. It was suggested that the top coating formed at a constant current density had a slightly higher aluminum concentration than that obtained at a constant potential. Accordingly, it can be deduced that the constant current density is advantageous for the formation of uniform and coherent Al coatings.\textsuperscript{16} The Al contents (84.37\%, 78.32\%) in the present samples were comparable with that reported by H. Yang.\textsuperscript{19}

The corrosion resistances of the Mg alloy with Al coatings were adequately investigated by potentiodynamic polarization and electrochemical impedance spectroscopy (EIS). Fig. 6a displays the polarization curves of the three samples. The bare Mg alloy exhibits highly active dissolution performance, as displayed by curve 1. Also, the anodic current increased rapidly and reached the limit of 0.1 A cm\(^{-2}\) in a short time when the potential overcame \(E_{\text{corr}}\). However, the Al coatings could effectively slow down the corrosion of the Mg alloy, and passivation breakdown was observed in curves 2 and 3. The passive current densities of the coatings obtained with \(-0.67\) V and \(-30.08\) mA were close to \(10^{-4}\) and \(10^{-5}\) mA cm\(^{-2}\), respectively. This indicated that the dissolution rates were visibly suppressed as compared with that of the Mg alloy substrate. In addition, the coating obtained with \(-30.08\) mA manifested superior protective performance than that with \(-0.67\) V. Fig. 6b displays the Nyquist plots of the three samples. The single semicircle of these spectra demonstrates the one time constant equivalent circuit. The polarization resistances (\(R_p\)) of the Mg alloy, \(-0.67\) V Al sample and \(-30.08\) mA sample were 406, 758 and 1267 \(\Omega\), respectively. Clearly, the \(R_p\) values of the Al coatings were much higher than that of the bare Mg alloy, suggesting the effective protection of Al coatings. The better protective behavior of the Al coating obtained with \(-30.08\) mA was ascribed to its continuous and compact structure compared to the loose and cracked structure of the Al coating obtained with \(-0.67\) V (Fig. 5).

Clearly, the Al coating could be obtained by this method. Unlike the electrodeposition process in a glove box, which isolates water and air in the process, the ionic liquid
preparation and electroplating process was carried out in air in the present method.

4. Conclusion
A simple method using the water-absorbent material combined with an organic protective film was proposed to guarantee the electrodeposition of Al on an Mg alloy (AZ91D) substrate from a first-generation ionic liquid AlCl$_3$/[Bmim]Cl (2 : 1 mol%) in air. In the preparation of ionic liquid, a 4A molecular sieve was added to absorb the water infiltrated during the addition of chemicals. At the same time, undecane was added to form organic films on the liquid, which could prevent the infiltration of water and air efficiently. The electrodeposition experiment carried out with a constant current (–30.08 mA) led to the formation of a continuous and compact Al coating. The
proposed method has great potential to help realize the industrialization of Al electrodeposition on Mg alloys.

Conflicts of interest

There are no conflicts of interests.

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