Space-time discontinuous Galerkin method for the numerical simulation of the compressible turbulent gas flow through the porous media

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Abstract. The article is concerned with the numerical simulation of the compressible turbulent gas flow through the porous media using space-time discontinuous Galerkin method. The mathematical model of flow is represented by the system of non-stationary Reynolds-Averaged Navier-Stokes (RANS) equations. The flow through the porous media is characterized by the loss of momentum. This RANS system is equipped with two-equation k-omega turbulence model. The discretization of these two systems is carried out separately by the space-time discontinuous Galerkin method. This method is based on the piecewise polynomial discontinuous approximation of the sought solution in space and in time. We present some numerical experiments to demonstrate the applicability of the method using own-developed code.

1 Introduction

During the last decade the space-time discontinuous Galerkin finite element method (ST-DG), which is based on piecewise polynomial discontinuous approximations of the sought solution, became very popular in the field of numerical simulation of the fluid flow. This method of numerical simulation of the fluid flow can be written in the form

\[
\begin{align*}
\frac{\partial w}{\partial t} + \sum_{s=1}^{2} \frac{\partial f_s(w)}{\partial x_i} + \sum_{s=1}^{2} \frac{\partial f^T_s(w)}{\partial x_i} & = \sum_{s=1}^{2} \frac{\partial k_s(w)}{\partial x_i} + \sum_{s=1}^{2} \frac{\partial R_s(w, \nabla w)}{\partial x_i} + S(w),
\end{align*}
\]

where for \( s = 1, 2 \) we have

\[
\begin{align*}
w & = (w_1, ..., w_4)^T = (\rho, \rho v_1, \rho v_2, E) \in \mathbb{R}^4, \\
f_s(w) & = (f_{s,1}, ..., f_{s,4})^T \\
& = (\rho v_s, \rho v_1 v_s + \delta_{s,1} \rho, \\
& \quad \rho v_2 v_s + \delta_{s,2} \rho, \quad (E + p) v_s)^T, \\
f^T_s(w) & = (f_{s,1}^T, ..., f_{s,4}^T)^T \\
& = (0, \frac{2}{3} \rho k \delta_{s,1}, \frac{2}{3} \rho k \delta_{s,2}, \frac{2}{3} \rho k v_s)^T, \\
R_s(w, \nabla w) & = (R_{s,1}, ..., R_{s,4})^T \\
& = (0, \tau_{s,1}^T, \tau_{s,2}^T, \\
& \quad \sum_{r=1}^{2} \tau_{r,s}^T v_r + \left( \frac{c_p H}{\Pr} + \frac{c_p \mu T}{Pr} \right) \frac{\partial \theta}{\partial x_j})^T, \\
k_s(w) & = (k_{s,1}, ..., k_{s,4})^T \\
& = \left( 0, ..., 0, \mu_k + \frac{\sigma_k \rho k}{\rho}, \frac{\partial k}{\partial x_j} \right)^T, \\
S(w) & = \left( 0, -C_0 \frac{\rho^2}{2} |v|^2 - C_0 \frac{\rho}{2} |v|^2 - C_0 \frac{\rho}{2} |v|^2 \right)
\end{align*}
\]

2 Formulation of the \( k - \omega \) turbulence model

We consider compressible turbulent flow in a bounded domain \( \Omega \subset \mathbb{R}^2 \). We assume that the boundary \( \Gamma \) consists of three disjoint parts \( \partial \Omega = \Gamma_i \cup \Gamma_o \cup \Gamma_w \), where \( \Gamma_i \) is the inlet, \( \Gamma_o \) is the outlet, and \( \Gamma_w \) is impermeable wall.

The system of the RANS equations describing the viscous compressible turbulent flow can be written in the form

\[
\begin{align*}
\frac{\partial w}{\partial t} + \sum_{s=1}^{2} \frac{\partial f_s(w)}{\partial x_i} + \sum_{s=1}^{2} \frac{\partial f^T_s(w)}{\partial x_i} & = \sum_{s=1}^{2} \frac{\partial k_s(w)}{\partial x_i} + \sum_{s=1}^{2} \frac{\partial R_s(w, \nabla w)}{\partial x_i} + S(w),
\end{align*}
\]

where for \( s = 1, 2 \) we have

\[
\begin{align*}
w & = (w_1, ..., w_4)^T = (\rho, \rho v_1, \rho v_2, E) \in \mathbb{R}^4, \\
f_s(w) & = (f_{s,1}, ..., f_{s,4})^T \\
& = (\rho v_s, \rho v_1 v_s + \delta_{s,1} \rho, \\
& \quad \rho v_2 v_s + \delta_{s,2} \rho, \quad (E + p) v_s)^T, \\
f^T_s(w) & = (f_{s,1}^T, ..., f_{s,4}^T)^T \\
& = (0, \frac{2}{3} \rho k \delta_{s,1}, \frac{2}{3} \rho k \delta_{s,2}, \frac{2}{3} \rho k v_s)^T, \\
R_s(w, \nabla w) & = (R_{s,1}, ..., R_{s,4})^T \\
& = (0, \tau_{s,1}^T, \tau_{s,2}^T, \\
& \quad \sum_{r=1}^{2} \tau_{r,s}^T v_r + \left( \frac{c_p H}{\Pr} + \frac{c_p \mu T}{Pr} \right) \frac{\partial \theta}{\partial x_j})^T, \\
k_s(w) & = (k_{s,1}, ..., k_{s,4})^T \\
& = \left( 0, ..., 0, \mu_k + \frac{\sigma_k \rho k}{\rho}, \frac{\partial k}{\partial x_j} \right)^T, \\
S(w) & = \left( 0, -C_0 \frac{\rho^2}{2} |v|^2 - C_0 \frac{\rho}{2} |v|^2 - C_0 \frac{\rho}{2} |v|^2 \right)
\end{align*}
\]
\[ \tau_{sv}^V = -\frac{2}{3}(\mu_L + \mu_T) \text{div} \delta_{sv} + 2(\mu_L + \mu_T) d_{sv}(\mathbf{v}), \]
\[ d_{sv}(\mathbf{v}) = \frac{1}{2} \left( \frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right). \]

We use the following notation: \( \mathbf{v} = (v_1, v_2) \) - velocity, \( \rho \) - density, \( p \) - pressure, \( \theta \) - absolute temperature, \( E \) - total energy, \( \gamma \) - Poisson adiabatic constant, \( \kappa \) - heat conduction coefficient, \( c_v \) - specific heat at constant volume, \( c_p \) - specific heat at constant pressure, where \( c_p = \gamma c_v \). \( Pr \) is the Prandtl number, which can be express in the form \( Pr = \frac{\nu_{\text{eddy}}}{\nu_{\text{laminar}}} \), \( Pr_T \) is the turbulent Prandtl constant number, \( \mu_T \) is the eddy-viscosity coefficient, \( \mu_L \) is the dynamic viscosity coefficient dependent on temperature via Sutherland’s formula, \( C_0 \) is the parameter of the porous media.

The above system is completed by the thermodynamical relations
\[ p = (\gamma - 1) \left( E - \frac{1}{2} \rho |\mathbf{v}|^2 - \rho k \right), \]
\[ \theta = \frac{1}{C_v} \left( E - \frac{1}{2} \rho |\mathbf{v}|^2 - k \right) \]
and is equipped with the initial condition
\[ \mathbf{w}(x, 0) = \mathbf{w}_0(x), \quad x \in \Omega \]
and the following boundary conditions

1. \( \rho_0 |v_1| = \rho_D \),
2. \( \mathbf{v}_0|_{\Gamma_D} = \mathbf{v}_D = (u_{D1}, u_{D2})^T \),
3. \( \sum_{s=1}^{2} \left( \tau_{sv}^V n_j + \left( \frac{c_p \mu_L}{Pr} + \frac{c_p \mu_T}{Pr_T} \right) \frac{\partial \theta}{\partial n} \right) |_{\Gamma_D} = 0 \),
4. \( \mathbf{v}_0|_{\Gamma_N} = \mathbf{0} \),
5. \( \sum_{s=1}^{2} \tau_{sv}^V n_s = 0, \quad r = 1, 2 \quad \text{on} \ \Gamma_D, \)
6. \( \sum_{s=1}^{2} \tau_{sv}^V n_s = 0, \quad r = 1, 2 \quad \text{on} \ \Gamma_D, \)

with given data \( \mathbf{w}_0, \rho_D, \mathbf{v}_D \). It is possible to show that \( \mathbf{f}_r(\alpha \mathbf{w}) = \alpha \mathbf{f}_r(\mathbf{w}) \) for \( \alpha > 0 \). This property implies that
\[ \mathbf{f}_r(\mathbf{w}) = A_r(\mathbf{w}) \mathbf{w}, \quad s = 1, 2, \]
where
\[ A_r(\mathbf{w}) = \frac{D \mathbf{f}_r(\mathbf{w})}{D \mathbf{w}}, \quad s = 1, 2, \]
are the Jacobi matrices of the mappings \( \mathbf{f}_r \). Similary we can express
\[ \mathbf{f}_r(\mathbf{w}) = A_r^\prime(\mathbf{w}) \mathbf{w}, \quad s = 1, 2. \]
The viscous terms \( \mathbf{R}_s(\mathbf{w}, \nabla \mathbf{w}) \) can be expressed in the form
\[ \mathbf{R}_s(\mathbf{w}, \nabla \mathbf{w}) = \sum_{k=1}^{2} \mathbf{K}_{s,k}(\mathbf{w}) \frac{\partial \mathbf{w}}{\partial x_k}, \quad s = 1, 2, \]
where \( \mathbf{K}_{s,k}(\mathbf{w}) \in \mathbb{R}^{4 \times 4} \) are matrices depending on \( \mathbf{w} \).

The aforesaid system of the RANS equations is completed by the Wilcox’s turbulence model (see [11]) for \( \mu_T \).

For the sake of the stability we introduce new variable \( \tilde{\omega} = ln \omega \). (For details see [7]). Then the turbulence model reads
\[ \frac{\partial \rho \tilde{\mathbf{w}}}{\partial t} + \sum_{s=1}^{2} \frac{\partial \mathbf{R}_s(\tilde{\mathbf{w}}, \nabla \tilde{\mathbf{w}})}{\partial x_s} = \frac{2}{3} \frac{\partial \mathbf{R}_s(\mathbf{w}, \nabla \mathbf{w})}{\partial x_s} + \tilde{s}(\tilde{\mathbf{w}}), \quad (4) \]
where for \( s = 1, 2 \) we have
\[ \tilde{\mathbf{w}} = (\tilde{u}_1, \tilde{u}_2)^T = (\tilde{\omega}, k)^T \in \mathbb{R}^2, \]
\[ \tilde{\mathbf{f}}_r(\tilde{\mathbf{w}}) = (\tilde{f}_{r1}^1, \tilde{f}_{r2}^2)^T = (\rho \tilde{\omega} v_3, \rho k v_3)^T, \]
\[ \tilde{\mathbf{R}}_r(\tilde{\mathbf{w}}, \nabla \tilde{\mathbf{w}}) = (\tilde{\mathbf{R}}_{r1,1}^1, \tilde{\mathbf{R}}_{r2,2}^2)^T = \left( \left( \mu_L + \sigma_{u \mu_T} \right) \frac{\partial \tilde{\omega}}{\partial x_k}, \left( \mu_L + \sigma_{u \mu_T} \right) \frac{\partial k}{\partial x_k} \right)^T, \]
\[ \tilde{s}(\tilde{\mathbf{w}}) = \left( \alpha_1 \frac{P_k}{\omega_{\text{lim}}} - \beta \frac{p \rho \epsilon \omega}{\omega_{\text{lim}}} \right) + \frac{2}{3} \sum_{s=1}^{2} \left( \mu_L + \sigma_{u \mu_T} \right) \frac{\partial \tilde{\omega}}{\partial x_s} \frac{\partial \tilde{\omega}}{\partial x_s} \frac{\partial \tilde{k}}{\partial x_s} \frac{\partial \tilde{k}}{\partial x_s}, \]
\[ \tilde{C}_D + P_k - \tilde{\beta} \frac{p \rho \epsilon \omega}{\omega_{\text{lim}}} \frac{\partial \tilde{\omega}}{\partial x_s} \frac{\partial \tilde{k}}{\partial x_s} \frac{\partial \tilde{k}}{\partial x_s}. \]

Here \( \omega \) is the turbulence dissipation, \( k \) is the turbulence kinetic energy and \( \mu_T \) is the eddy viscosity. We can write the production term as
\[ P_k = \sum_{s=1}^{2} \sum_{r=1}^{2} \tau_{sr} \frac{\partial v_s}{\partial x_r}, \]
where
\[ \tau_{sr} = -\frac{2}{3} \mu_T \text{div} \delta_{sr} - \frac{2}{3} \rho k \delta_{sr} + 2 \mu_T d_{sr}(\mathbf{v}), \]
\[ d_{sr}(\mathbf{v}) = \frac{1}{2} \left( \frac{\partial v_s}{\partial x_r} + \frac{\partial v_r}{\partial x_s} \right), \]
\[ \mu_T = \frac{\rho k}{\omega_{\text{lim}}}. \]

Limited eddy viscosity \( \omega_{\text{lim}} \) is given by the term
\[ \omega_{\text{lim}} = \max \left\{ \tilde{\omega}, C_{\text{lim}} \left[ \frac{1}{2 \beta} \frac{2}{3} \sum_{r=1}^{2} \tilde{r}_{rs} \tilde{r}_{rs} \right] \right\}, \]
\[ \tilde{r}_{rs} = -\frac{2}{3} \text{div} \delta_{rs} + 2 d_{rs}(\mathbf{v}). \]

The cross-diffusion term \( C_D \) is defined as
\[ C_D = \sigma_D \frac{\rho}{\omega_{\text{lim}}} \max \left\{ \sum_{k=1}^{4} \frac{\partial k}{\partial x_k}, 0 \right\}. \]

The coefficients \( \tilde{\beta}, \tilde{\beta}, \sigma_1, \sigma_2, \sigma_3, C_\text{lim}, \text{Pr}_T \) are chosen by [11]:
\[ \sigma_1 = \frac{13}{25}, \quad \beta = 0.0708, \quad \beta = 0.09, \quad \sigma_2 = 0.6, \]
\[ \sigma_1 = 0.5, \quad C_\text{lim} = \frac{7}{8}, \quad \sigma_3 = \frac{1}{8}, \quad \text{Pr}_T = \frac{8}{9}. \]
This system is also equipped with the initial condition
\[ \mathbf{w}(x,0) = \mathbf{w}^0(x), \quad x \in \Omega \]
and the following boundary conditions
\[ \begin{align*}
& a) \quad \partial_t \mathbf{w} = \partial_t \mathbf{w}, \quad b) \quad k_1 \mathbf{w} = k_2 \mathbf{w}, \\
& a) \quad \partial_{\mathbf{w}} \mathbf{w} = \partial_{\mathbf{w}} \mathbf{w}, \quad b) \quad k_1 \mathbf{w} = 0, \\
& a) \quad \frac{\partial \mathbf{w}}{\partial n} \bigg|_{\Gamma_o} = 0, \quad b) \quad \frac{\partial k}{\partial n} \bigg|_{\Gamma_o} = 0,
\end{align*} \]
with given data \( \mathbf{w}^0, \partial_{\mathbf{w}} \mathbf{w}, k_D, \partial_{\mathbf{w}} \mathbf{w} \). Similary like in the RANS case we can express convect terms
\[ \tilde{\mathbf{f}}_s^i(\mathbf{w}) = \tilde{\mathbf{A}}_s^i(\mathbf{w}) \tilde{\mathbf{w}}, \quad s = 1, 2 \]
and diffusion terms
\[ \tilde{\mathbf{R}}_s(\tilde{\mathbf{w}}, \nabla \tilde{\mathbf{w}}) = \tilde{\mathbf{K}}_s(\tilde{\mathbf{w}}) \frac{\partial \tilde{\mathbf{w}}}{\partial x_s}, \quad s = 1, 2, \]
where \( \tilde{\mathbf{K}}_s(\tilde{\mathbf{w}}) \in \mathbb{R}^{2s \times 2} \) are matrices depending on \( \tilde{\mathbf{w}} \).

### 3 Discretization

#### 3.1 Space discretization of the problem

By \( \Omega_h \) we denote polygonal approximation of the domain \( \Omega \). Let \( \mathcal{T}_h \) be a partition of the domain \( \Omega_h \) into finite number of closed elements with mutually disjoint interiors such that \( \Omega_h = \bigcup_{K \in \mathcal{T}_h} K \). In 2D problems, we usually choose \( K \in \mathcal{T}_h \) as triangles or quadrilaterals. By \( \mathcal{T}_h \) we denote the system of all faces of all elements \( K \in \mathcal{T}_h \). Further, we introduce the set of boundary faces \( \mathcal{F}_h^b = \{ \Gamma \in \mathcal{F}_h^b : \Gamma \in \partial \Omega_h \} \) and the set of inner faces \( \mathcal{F}_h^i = \mathcal{F}_h \setminus \mathcal{F}_h^b \). Each \( \Gamma \in \mathcal{F}_h^i \) is associated with a unit normal vector \( n_\Gamma \). For \( \Gamma \in \mathcal{F}_h^b \) the normal \( n_\Gamma \) has the same orientation as the outer normal to \( \partial \Omega_h \). For each \( \Gamma \in \mathcal{F}_h^i \) there exist two neighbouring elements \( K_1^\Gamma, K_2^\Gamma \in \mathcal{T}_h \) such that \( \Gamma \subset \partial K_1^\Gamma \cap \partial K_2^\Gamma \). We use the convention that \( K_1^\Gamma \) lies in the direction of \( n_\Gamma \) and \( K_2^\Gamma \) lies in the opposite direction to \( n_\Gamma \). If \( \Gamma \in \mathcal{F}_h^b \), then the element adjacent to \( \Gamma \) will be denoted by \( K_1^\Gamma \).

We shall look for an approximate solution of the problem in the space of piecewise polynomial functions
\[ S^p_h = (S^p_h)^4, \quad S^p = \{ v; \partial_v \in P^p(K), \forall K \in \mathcal{T}_h \}, \]
where \( p > 0 \) is an integer and \( P^p(K) \) denotes the space of all polynomials on \( K \) of degree \( \leq p \). A function \( \Phi \in S^p_h \) is, in general, discontinuous on interfaces \( \Gamma \in \mathcal{F}_h^i \). By \( \Phi^{k}_h \) and \( \Phi^{k}_h \) we denote the values of \( \Phi \) on \( \Gamma \) considered from the interior and the exterior of \( K^{\Gamma}_1 \), respectively, and set
\[ \langle \Phi \rangle_{\Gamma} = \frac{1}{2} (\Phi^{k}_h + \Phi^{k}_h), \quad [\Phi]_{\Gamma} = \Phi^{k}_h - \Phi^{k}_h, \]
which denotes the average and jump of \( \Phi \) on \( \Gamma \).

The discrete problem is derived in the following way: For arbitrary \( t \in [0, T] \) we can multiply the system by a test function \( S^p_h \), integrate over \( K \in \mathcal{T}_h \), apply Green’s theorem, sum over all elements \( K \in \mathcal{T}_h \), use the concept of the numerical flux and introduce suitable terms mutually vanishing for a regular exact solution. Moreover, we carry out a suitable partial linearization of nonlinear terms and then we can define the following forms.

In order to evaluate the integrals over \( \Gamma \in \mathcal{F}_h \) in inviscid term we use the approximation
\[ \mathbf{H}(w_L^r, w_R^r, n_\Gamma) \approx \sum_{s=1}^{2} f_s(w(n_\Gamma))_s, \]
where \( \mathbf{H} \) is a numerical flux. For the construction of the numerical flux we use the properties (2) of \( f_s \). Let us define the matrix
\[ P(w, n) := \sum_{s=1}^{2} A_s(w) n_s, \]
where \( n = (n_1, n_2) \), \( n_1^2 + n_2^2 = 1 \). Then we have
\[ P(w, n)w := \sum_{s=1}^{2} f_s(w) n_s. \]
It is possible to show that the matrix \( P \) is diagonalizable. It means that there exists a nonsingular matrix \( T = T(w, n) \) and a diagonal matrix \( \Lambda = \Lambda(w, n) \) such that
\[ P = T \Lambda T^{-1}, \quad \Lambda = \text{diag}(\lambda_1, ..., \lambda_4), \]
where \( \lambda_i = \lambda_i(w, n) \) are eigenvalues of the matrix \( P \). Then we can define the "positive" and "negative" parts of the matrix \( P \) by
\[ P^+ = T \Lambda^+ T^{-1}, \quad \Lambda^+ = \text{diag}(\lambda^+_1, ..., \lambda^+_4), \]
where \( \lambda^+_i = \max(\lambda, 0), \lambda^- = \min(\lambda, 0) \). Using this concept, we introduce the so-called Vijayasundaram numerical flux
\[ \mathbf{H}(w^+, w^-, n) = P^+ \left( \frac{w_L + w_R}{2} \cdot n \right) w^L + P^- \left( \frac{w_L + w_R}{2} \cdot n \right) w^R. \]
This numerical flux has suitable form for a linearization. Now we can define inviscid form in the following way
\[ b_h(\bar{w}_h, w_h, \Phi_h) := \]
\[ + \sum_{\Gamma \in \mathcal{F}_h^i} \int_{\Gamma} \left( P^+ (\langle \bar{w}_h \rangle, n_\Gamma) w_h^L + P^- (\langle \bar{w}_h \rangle, n_\Gamma) w_h^R \right) \cdot [\Phi_h]_{\Gamma} dS, \]
where the boundary state \( w_h^R \) is evaluated with the aid of the local linearized Riemann problem described in [5]. For the discretization of the viscous terms we use the property
We set $\Theta = 1$ or $\Theta = 0$ or $\Theta = -1$ and get the so-called symmetric version (SIPG) or incomplete version (IIPG) or nonsymmetric version (NIPG), respectively, of the discretization of the viscous terms.

Further, we define the turbulent forms $p_h, k_h$, the interior and boundary penalty form $J^*_h$ and the right-hand side form $l_h$ in the following way:

$$p_h(\tilde{w}_h, w_h, \Phi_h) := \sum_{\kappa \in \mathcal{T}_h} \int_{\kappa} \sum_{s=1}^{2} \sum_{k=1}^{2} A_{\kappa,s}^h (\tilde{w}_h^k) \cdot \Phi^s_h (m^s) \, dS + \sum_{\kappa \in \mathcal{T}_h} \int_{\kappa} \sum_{s=1}^{2} \sum_{k=1}^{2} A_{\kappa,s}^h (\tilde{w}_h^k) \cdot \Phi^s_h (m^s) \, dS$$

$$- \sum_{\kappa \in \mathcal{T}_h} \int_{\kappa} \sum_{s=1}^{2} \sum_{k=1}^{2} k_{\kappa,s} (\tilde{w}_h^k) \cdot \Phi^s_h (m^s) \, dS + \sum_{\kappa \in \mathcal{T}_h} \int_{\kappa} \sum_{s=1}^{2} \sum_{k=1}^{2} k_{\kappa,s} (\tilde{w}_h^k) \cdot \Phi^s_h (m^s) \, dS$$

$$- \sum_{\kappa \in \mathcal{T}_h} \int_{\kappa} \sum_{s=1}^{2} \sum_{k=1}^{2} k_{\kappa,s} (\tilde{w}_h^k) \cdot \Phi^s_h (m^s) \, dS + \sum_{\kappa \in \mathcal{T}_h} \int_{\kappa} \sum_{s=1}^{2} \sum_{k=1}^{2} k_{\kappa,s} (\tilde{w}_h^k) \cdot \Phi^s_h (m^s) \, dS$$

$$J^*_h (w_h, \Phi_h) := \sum_{\kappa \in \mathcal{T}_h} \int_{\kappa} \sigma [w_h] \cdot [\Phi_h] \, dS + \sum_{\kappa \in \mathcal{T}_h} \int_{\kappa} \sigma [w_h] \cdot [\Phi_h] \, dS$$

$$+ \sum_{\kappa \in \mathcal{T}_h} \int_{\kappa} \sigma [w_h] \cdot [\Phi_h] \, dS + \sum_{\kappa \in \mathcal{T}_h} \int_{\kappa} \sigma [w_h] \cdot [\Phi_h] \, dS$$

where $\sigma$ is a parameter of the method and boundary state $w_B$ is defined on the basis of the Dirichlet boundary conditions and extrapolation.

In the vicinity of discontinuities or steep gradients non-physical oscillations can appear in the approximate solution. In order to overcome this difficulty we employ artificial viscosity forms, see [6]. They are based on the discontinuity indicator

$$g(K) := \frac{1}{d(K) [K]^{\frac{1}{2}}} \int_{\partial K} [\tilde{\rho}_h]^2 \, dS, \quad K \in \mathcal{T}_h,$$

where $[\tilde{\rho}_h]$ is the jump of the function $\tilde{\rho}_h (= \text{the first component of the vector function} \tilde{w}_h)$ on the boundary $\partial K$, $d(K)$ denotes the diameter of $K$ and $|K|$ denotes the area of the element $K$. Then we define the discrete discontinuity indicator

$$G(K) := 0 \quad \text{if} \quad g(K) < 1,$$

$$G(K) := 1 \quad \text{if} \quad g(K) \geq 1, \quad K \in \mathcal{T}_h,$$

and the artificial viscosity forms

$$\tilde{\rho}_h (\tilde{w}_h, w_h, \Phi_h) := \sum_{k \in \mathcal{F}_h} \bar{\nu}_1 \sum_{k \in \mathcal{F}_h} d(K) G(K) \int_K \nabla \Phi_h \cdot \nabla \Phi_h \, dx,$$

$$J_h (w_h, \Phi_h) := \sum_{k \in \mathcal{F}_h} \nu_2 \frac{1}{2} \left( G(K^\phi_h) + G(K^\psi_h) \right) \int_K [w_h] \cdot [\Phi_h] \, dS,$$

with constants $\bar{\nu}_1$ and $\nu_2$.

All these forms are linear with respect to $w_h$ and nonlinear with respect to $\tilde{w}_h$.

Finally, we set

$$(\varphi, \psi) = \int_{\Omega_h} \varphi \psi \, dx.$$
with integers \( p, q \geq 1 \). \( P^n(I_m) \) denotes the space of all polynomials in \( t \) on \( I_m \) of degree \( \leq q \). Moreover for \( \Phi \in S^{p,q}_{h,t} \) we introduce the following notation:

\[
\Phi^n_m = \Phi(t^n_m) = \lim_{t \to t^n_m} \Phi(t), \quad \{\Phi\}_m = \Phi^n_m - \Phi^m_0.
\]

Approximate solution \( w_{hr} \) of the problem will be sought in the space \( S^{p,q}_{h,t} \). Since the functions of this space are in general discontinuous in time, we ensure the connection between \( I_{m-1} \) and \( I_m \) by the penalty term in time

\[
\langle [w_{hr}]_{m-1} , \Phi_{hr}(t_{m-1}^-) \rangle.
\]

The initial state \( w_{hr} \) is included by the \( L^2(\Omega_h(t_0)) \)-projection of \( w^0 \) on \( S^{p,q}_{h,t} \):

\[
\langle [w_{hr}(t_0^-), \Phi_{hr}(t_0^-) \rangle = \langle w^0, \Phi_{hr}(t_0^-) \rangle \quad \forall \Phi_{hr} \in S^{p,q}_{h,t}.
\]

Now we introduce a suitable linearization. We can use two possibilities.

1) We put \( w_{hr}(t) = w_h(t_{m-1}) \) for \( t \in I_m \).

2) We prolong the solution from the time interval \( I_{m-1} \) to the time interval \( I_m \).

We say that a function \( w_{hr} \in S^{p,q}_{h,t} \) is the approximate solution of the problem (1) obtained by the ST-DG method, if it satisfies the following conditions

\[
\sum_{m=1}^M \int_{I_m} \left( \frac{\partial w_{hr}}{\partial t} , \Phi_{hr} \right) dt + \sum_{m=1}^M \int_{I_m} \left( a_h(w_{hr}, w_{hr}, \Phi_{hr}) + b_h(w_{hr}, w_{hr}, \Phi_{hr}) \right) dt + \sum_{m=1}^M \int_{I_m} \left( \partial_h(w_{hr}, w_{hr}, \Phi_{hr}) + J_h(w_{hr}, w_{hr}, \Phi_{hr}) \right) dt + \sum_{m=1}^M \left( J_h^*(w_{hr}, w_{hr}, \Phi_{hr}) + p_h(w_{hr}, w_{hr}, \Phi_{hr}) \right) dt + \sum_{m=1}^M \left( [w_{hr}]_{m-1} , \Phi_{hr}(t_{m-1}) \right) + \left( w^0 , \Phi_{hr}(t_0^-) \right) \}
\]

\[
= \sum_{m=1}^M \int_{I_m} l_h(w_{hr}, \Phi_{hr}) dt + \left( w^0 , \Phi_{hr}(t_0^-) \right) \quad \forall \Phi_{hr} \in S^{p,q}_{h,t}.
\]

### 4 Discretization of the \( k - \omega \) turbulence model

#### 4.1 Space discretization of the problem

We apply discontinuous Galerkin method in the similar way as in the previous section. Discretization is carried out on the same mesh for simplicity. An approximate solution of the problem is looked for in the space \( S^p_h = (S^p_{h,t})^2 \) and a function \( \Phi \in S^p_h \) is, in general, discontinuous on interfaces \( \Gamma \in F^I_h \).

If we define \( \mathbf{P}^* = (\langle \rho(\mathbf{v}) \cdot \mathbf{n} \rangle_1 + \mathbf{I} \), where \( \mathbf{I} = \text{diag}(1, 1) \), and use the property (5) then we can define convect form

\[
\tilde{b}_h(w_h, \Phi_h) := - \sum_{k \in E_h} \int_{T} \sum_{s=1}^2 \tilde{A}_s \cdot \partial \Phi_h^s \cdot \frac{\partial \Phi_h}{\partial x_s} dx + \sum_{\Gamma \in F^I_h} \int_{\Gamma} \left( \tilde{P}^* \tilde{w}_h^I + \tilde{P}^{-} \tilde{w}_h^I \right) \cdot [\tilde{\Phi}_h] dS + \sum_{\Gamma \in F^I_h} \int_{\Gamma} \left( \tilde{P}^* \tilde{w}_h^I + \tilde{P}^{-} \tilde{w}_h^I \right) \cdot \Phi_h dS,
\]

where the state \( \tilde{w}_h^I \) is based on the boundary conditions.

For the discretization of the diffusion term we use the property (6) and then we have

\[
\tilde{a}_h(w_h, \tilde{w}_h, \tilde{\Phi}_h) := + \sum_{k \in E_h} \int_{T} \sum_{s=1}^2 \tilde{K}_s \cdot \partial \tilde{w}_h^s \cdot \frac{\partial \tilde{\Phi}_h}{\partial x_s} dx - \sum_{\Gamma \in F^I_h} \int_{\Gamma} \sum_{s=1}^2 \left( \tilde{K}_s \cdot \tilde{w}_h^s \right) \cdot [\tilde{\Phi}_h] dS - \sum_{\Gamma \in F^I_h} \int_{\Gamma} \sum_{s=1}^2 \left( \tilde{K}_s \cdot \tilde{w}_h^s \right) \cdot \tilde{\Phi}_h dS - \Theta \sum_{\Gamma \in F^I_h} \int_{\Gamma} \sum_{s=1}^2 \left( \tilde{K}_s \cdot \tilde{w}_h^s \right) \cdot \tilde{\Phi}_h dS.
\]

Further we define the turbulent form \( \tilde{\phi}_h \), the interior and boundary penalty form \( \tilde{\phi}_h^p \) and the right-hand side form \( \tilde{\phi}_h \) in the following way:

\[
\tilde{\phi}_h^p(w_h, \tilde{\Phi}_h) := \sum_{\Gamma \in F^I_h} \int_{\Gamma} \tilde{\sigma} [\tilde{w}_h] \cdot [\tilde{\Phi}_h] dS + \sum_{\Gamma \in F^I_h} \int_{\Gamma} \tilde{\sigma} \tilde{w}_h \cdot \tilde{\Phi}_h dS, \tilde{\phi}_h(w_h, \tilde{\Phi}_h) := \sum_{\Gamma \in F^I_h} \int_{\Gamma} \tilde{\sigma} \tilde{w}_h \cdot \tilde{\Phi}_h dS - \Theta \sum_{\Gamma \in F^I_h} \int_{\Gamma} \sum_{s=1}^2 \tilde{K}_s \cdot \tilde{w}_h^s \cdot \tilde{\Phi}_h dS.
\]

Boundary state \( \tilde{w}_h \) is defined on the basis of the Dirichlet boundary conditions and extrapolation.

#### 4.2 Full space-time DG discretization

For the full space-time discontinuous Galerkin discretization we use the same partition of the interval \([0, T]\) as in the previous section. We say that a function \( w_{hr} \in S^{p,q}_{h,t} \) is
the approximate solution of the problem (4) obtained by the ST-DG method, if it satisfies the following conditions

\[ \sum_{m=0}^{M-1} \int_{I_m} \left( \frac{\partial \rho}{\partial t} \tilde{w}_{hr}, \tilde{\Phi}_{hr} \right) \, dt 
+ \sum_{m=0}^{M-1} \int_{I_m} \left( \tilde{a}_h(\tilde{w}_{hr}, \tilde{w}_{hr}, \tilde{\Phi}_{hr}) + \tilde{b}_h(\tilde{w}_{hr}, \tilde{w}_{hr}, \tilde{\Phi}_{hr}) \right) \, dt 
+ \sum_{m=0}^{M-1} \int_{I_m} \tilde{J}_h(\tilde{w}_{hr}, \tilde{\Phi}_{hr}) \, dt 
+ \sum_{m=1}^{M-1} \left( [\tilde{w}_{hr}]_{m}, \tilde{\Phi}_{hr}(t_m^r) \right) + \left( \tilde{w}_{hr}(t_0^r), \tilde{\Phi}_{hr}(t_0^r) \right) 
= \sum_{m=0}^{M-1} \int_{I_m} \left( \tilde{\delta}_h(\tilde{w}_{hr}, \tilde{\Phi}_{hr}) + \tilde{s}_h(\tilde{w}_{hr}, \tilde{\Phi}_{hr}) \right) \, dt 
+ \left( \tilde{w}_0, \tilde{\Phi}_{hr}(t_0^r) \right) \quad \forall \tilde{\Phi}_{hr} \in S_{k,hr}. \]

5 Numerical experiments

In this section we will demonstrate the applicability of the developed method and present numerical simulations of the compressible turbulent gas flow through the porous media. Such approach can be used for the simulation of various permeable obstacles. In our case it will be the dense fence (figure 1). We will simulate the fence 0.1m high which will be placed in the free stream. We consider input flow with the total temperature \( \theta_0 = 293 \text{K} \), the total pressure \( p_0 = 101325 \text{Pa} \) and the velocity \( 20 \text{ms}^{-1} \) and \( 30 \text{ms}^{-1} \). The area of the porous media is situated in the same place as is occupied by the fence and we set the parameter \( C_0 = 5000 \). The following figures show the results of the numerical experiments and we can compare porous media with the fence. Figures 3-4 and 7-8 show the velocity distribution and Figures 5-6 and 9-10 show the pressure distribution for the fence and porous media. Figure 2 shows detail of the mesh which consist of 346034 elements in total. From the proposed simulation we can guess that porous media is good approximation of the dense fence. The main advantage of this approach is that we do not have to use so much fine mesh around the real fence.

6 Conclusion

In this paper we dealt with the space-time discontinuous Galerkin method for the numerical simulation of the compressible turbulent gas flow through the porous media. The applicability of the proposed method was demonstrated on the examples which show that the presented method is an efficient numerical scheme for the solution of these types of problems.

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**Fig. 4.** The distribution of the velocity for the fence for $20\text{ms}^{-1}$.

**Fig. 5.** The distribution of the pressure for the porous media for $20\text{ms}^{-1}$.

**Fig. 6.** The distribution of the pressure for the fence for $20\text{ms}^{-1}$.

**Fig. 7.** The distribution of the velocity for the porous media for $30\text{ms}^{-1}$. 
Fig. 8. The distribution of the velocity for the fence for 30\text{ms}^{-1}.

Fig. 9. The distribution of the pressure for the porous media for 30\text{ms}^{-1}.

Fig. 10. The distribution of the pressure for the fence for 30\text{ms}^{-1}.

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