An alternative method to determine the diffusion coefficient for the shrinking core model

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A new method to determine the effective diffusion coefficient of sorbate in sorbent granule based on the analytical solution of the shrinking core model (SCM) has been proposed. The experimental data presented by Lewandowski and Roe concerning the sorption of copper ions by alginate granules have been applied to compare the analytical and numerical methods. The results obtained by both methods are very close.

Keywords: Shrinking core model, Sorption, Alginate gel, Diffusion coefficient.

INTRODUCTION

In the last several years, the studies on possibility of the wider application of shrinking core model developed by Levenspiel have been carried out. Works among others, confirmed usability of the above mentioned model for more complex situations than that described by Levenspiel. Lazaridis and Charalamous evaluated the effective diffusion coefficients by employing the SCM model for tri-valent chromium ions, which were removed from binary aqueous solutions by composite alginate-goethite beads in a batch mode. Ko et al investigated the sorption of copper and cadmium ions onto bone char in single component systems using fixed-bed column adsorbers. A film-pore diffusion model (based on the unreacted core model) was successfully used to predict the fixed-bed breakthrough curves for the two metal ions. In Pritzker work shrinking-core equation for pore diffusion control has been extended to the case of a facile heterogeneous reaction coupled to a facile homogeneous reaction occurring within the pores of the product layer and in the bulk solution. A model based on the shrinking-core principle was presented for three cases of oxidative metal leaching from non-porous mineral particles. Several limitations inherent in the assumptions of the traditional SCM model, such as those of oxidation agent in excess and first-order irreversible kinetics, are overcome. Crundwell and Godorr presented a mathematical model (based on the SCM model) of the leaching of gold in cyanide solutions. In this work the authors proposed that a layer of passivating material forms on the surface of the gold particle as it dissolves.

After modification, the model can be applied to determine the effective diffusion coefficient in the processes which tend to eliminate the heavy metals from aqueous solutions in the cases when the sorption process occurs besides diffusion. Moreover, the SCM model can be applied in hydrometallurgy for the liquid-solid system.

Alginic acid is a biopolymer carrying carboxyl groups capable of forming complexes with metal ion. Many studies have been carried out on the application of alginic acid to the aqueous-phase separation of heavy metals. Deans and Dixon studied the efficiency of alginic acid for removing lead (II) and copper (II) ions from water. Carboxylated alginic acid prepared through oxidation reaction with potassium permanganate had a high uptake capacity of 3.1 mmol/g dry mass at pH 4 and showed higher affinity to heavy metals compared to alkaline metals (Ca²⁺, Mg²⁺) in the mixed metal system. Removal of Co, Cu and Zn was achieved by producing Cu/Co-alginate gels or Cu-Zn-H-alginate gels in situ. A viscous Na-alginate solution was directly dispensed dropwise into the acidic aqueous media containing the dissolved copper and zinc or copper and cobalt to form spherical alginate gels which subsequently absorbed these ions until the final equilibrium was reached.

CONVENTIONAL METHOD TO DETERMINE THE EFFECTIVE DIFFUSION COEFFICIENT

According to the SCM model, effective diffusion coefficient of copper in porous granules is determined from the relationship (1) by Rao and Gupta

\[ \frac{1}{C^0} \int_0^t C_i \, dt = \frac{6D}{C^0 R^2} \left( 1 - 3(1 - X_t) \right)^{2/3} \]  

(1)

where:

\[ X_t = \frac{C_i - C_t}{C_i - C_u} \]  

(2)

For the closed system and sorption limited by internal diffusion, assuming a quasi-steady state:

\[ C^0 = \frac{(C_i - C_u) V}{N \cdot \frac{4}{3} \pi R^3} \]  

(3)

The values of \( \int_0^t C_i \, dt \) are usually determined numerically by the trapezoidal method.

Then, the dependence between the left side of equation (1) and the calculated integral values are plotted. The value of the effective diffusion coefficient is calculated from the slope of the above plot as equation (4):

\[ D = \frac{\text{slope} \cdot C^0 \cdot R^2}{6} \]  

(4)

The described method is very often applied to study the sorption and desorption of such elements as: copper, cobalt, chromium, nickel, lead, gold and silver. Alginic gel and their application in hydrometallurgy for the mixed metal system of cobalt, copper, and lead have been also investigated. In Pritzker work the sorption of copper and chromium ions by alginate granules has been studied for different pH values. Also, by using the SCM model the effective diffusion coefficients by employing the SCM model for tri-valent chromium ions, which were removed from binary aqueous solutions by composite alginate-goethite beads in a batch mode. Ko et al investigated the sorption of copper and cadmium ions onto bone char in single component systems using fixed-bed column adsorbers. A film-pore diffusion model (based on the unreacted core model) was successfully used to predict the fixed-bed breakthrough curves for the two metal ions. In Pritzker work shrinking-core equation for pore diffusion control has been extended to the case of a facile heterogeneous reaction coupled to a facile homogeneous reaction occurring within the pores of the product layer and in the bulk solution. A model based on the shrinking-core principle was presented for three cases of oxidative metal leaching from non-porous mineral particles. Several limitations inherent in the assumptions of the traditional SCM model, such as those of oxidation agent in excess and first-order irreversible kinetics, are overcome. Crundwell and Godorr presented a mathematical model (based on the SCM model) of the leaching of gold in cyanide solutions. In this work the authors proposed that a layer of passivating material forms on the surface of the gold particle as it dissolves.

After modification, the model can be applied to determine the effective diffusion coefficient in the processes which tend to eliminate the heavy metals from aqueous solutions in the cases when the sorption process occurs besides diffusion. Moreover, the SCM model can be applied in hydrometallurgy for the liquid-solid system.

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ALTERNATIVE METHOD

Alternative to the conventional method for the calculation of the effective diffusion coefficient (let us name it numerical method) is the analytical method. The difference between the analytical and numerical methods consists in the manner of the solution of the equation (1) describing the process of metal sorption in granule. In the numerical method, the integral is calculated by applying the numerical trapezoidal method however, the analytical method consists in analytical integration. The starting point in both methods was the differential equation\(^{16}\) describing radius \(r_c\) (unreacted core) change of the unreacted part in granule progressing in time:

\[
-C^0 r_c^2 \frac{dr_c}{dt} \left( \frac{1}{r_c} - \frac{1}{R} \right) = DC_i
\]

(5)

By applying a suitable substitution, Rao and Gupta\(^{16}\) obtained the following equation:

\[
-C^0 r_c^2 \left( \frac{1}{r_c} - \frac{1}{R} \right)^2 dr_c = \int_0^t C_i dt
\]

(6)

After the integration of the left side of equation (6) and rearrangement, equation (1) is obtained.

Otherwise, after rearrangement of equation (5), we obtain:

\[
\frac{dr_c}{dt} = -\frac{RDC_i}{C^0 r_c (R-r_c)}
\]

(7)

Radius \(r_c\) to granule radius \(R\) ratio is described by relationship:

\[
1 - \left( \frac{r_c}{R} \right)^3 = X
\]

Simultaneously:

\[
X = \frac{C_i - C_i}{C_i - C_u}
\]

therefore:

\[
C_i = C_i - \left( 1 - \left( \frac{r_c}{R} \right)^3 \right) (C_i - C_u)
\]

(8)

After substituting Eq. (8) to Eq. (7), integration and rearrangement, we obtain:

\[
t = \frac{C^0 r_i^2}{DC_i - C_u} \int \frac{R-r_c}{C_i - C_u} \frac{dr_c}{R-r_c^3 + r_c^3} (C_i - C_u)
\]

(9)

By integration of the integral occurring in Eq. (9), the following relationship is obtained:

\[
t = \frac{C^0 r_i^2}{DC_i - C_u} \left[ \frac{1}{3} \left( \frac{X^3 + \omega^3}{X^3 + 1} \right) + \frac{1}{6X} \ln \left( \frac{(X^2 + 1)(X + \omega)^2}{(X + 1)^2(X - \omega^2)} \right) \right] +
\]

\[
+ \frac{1}{X \sqrt{3}} \left\{ \arctan \left( \frac{2 - X}{X \sqrt{3}} \right) - \arctan \left( \frac{2X - \omega}{X \sqrt{3}} \right) \right\}
\]

(10)

where:

\[
\chi = \left( \frac{C_u}{C_i - C_u} \right)^{1/3}
\]

(11)

and:

\[
\omega = \left( \frac{C_i - C_u}{C_i - C_u} \right)^{1/3} \frac{r_c}{R}
\]

(12)

In order to calculate the effective diffusion coefficient, first of all, for the given values of time \(t\) and for the known \(C_i\) and \(C_u\) values, \(P(\omega)\) is calculated as follows:

\[
P(\omega) = \left\{ \frac{1}{3} \ln \left( \frac{X^3 + \omega^3}{X^3 + 1} \right) + \frac{1}{6X} \ln \left( \frac{(X^2 + 1)(X + \omega)^2}{(X + 1)^2(X - \omega^2)} \right) \right\} +
\]

\[
+ \frac{1}{X \sqrt{3}} \left\{ \arctan \left( \frac{2 - X}{X \sqrt{3}} \right) - \arctan \left( \frac{2X - \omega}{X \sqrt{3}} \right) \right\}
\]

(13)

Then, a graph of relationship: \(P(\omega)=f(t)\) is plotted. Effective diffusion coefficient \(D\) is calculated from the slope of the above plot as equation (14):

\[
D = \frac{[\text{slope}] \cdot C^0 \cdot R^3}{(C_i - C_u)}
\]

(14)

RESULTS AND DISCUSSION

For the determination of the diffusion coefficient of copper ions in alginate granules by analytical method, we made use of the data presented by Lewandowski and Roe\(^{1}\).

The dependence between \(P(\omega)\) values and time, taking into account the content of alginate in granules determined for the diffusion of Cu (II) ions is presented in Fig.1. Biopolymer content in the beads was varied between 2\% and 5\% w/w. It can be clearly seen that the points lay along the straight lines, and all correlation coefficients are greater than 0.99.

![Figure 1. Dependence between \(P(\omega)\) values and time for various contents of alginate in granules determined for the diffusion of Cu (II) ions](image)

The obtained results were compared with the results determined by the numerical method by Lewandowski and Roe\(^{4}\) (Table 1).

| Table 1. Effective diffusion coefficient of Cu(II) ions in calcium alginate granules with various content of biosorbent |
|-----------------------------------|-----------------|-----------------|
| Content of alginate | \(D \times 10^9\) \(\text{cm}^2/\text{s}\) | numerical method | analytical method |
| [% wt] | \(\times 10^9\) | \(\times 10^9\) | \(\times 10^9\) |
| 2 | 0.89 | 0.82 |
| 3 | 0.98 | 0.98 |
| 4 | 1.47 | 1.47 |
| 5 | 1.84 | 1.84 |
CONCLUSIONS

It was shown that the analytical method can be effectively applied instead of the numerical method in order to calculate the effective diffusion coefficient. The results obtained by both methods are very similar.

NOMENCLATURE

- $C_t$: Concentration of sorbate ions in the solution in moment $t$.
- $C_i$: Initial concentration of sorbate ions in the solution.
- $C_\infty$: Equilibrium concentration of sorbate ions in the solution.
- $C_0$: Mean density of sites bonding sorbate ions in the sorbent granule.
- $D$: Effective diffusion coefficient of sorbate in the sorbent granule.
- $N$: Number of the sorbent granules.
- $r_c$: Radius of the unreacted sorbent core.
- $R$: Radius of the sorbent granules.
- $t$: Time.
- $V$: Volume of the solution containing the sorbate.

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