Ultrasonic Piezoelectric Nebulization of Propoxur for the Determination by Corona Discharge Ionization Ion Mobility Spectrometry

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Abstract

Propoxur insecticide as a thermally unstable compound (decomposed at its boiling point) could not be analyzed by traditional sample introduction systems based on the thermal desorption. In this study, an ultrasonic piezoelectric nebulizing injection port was applied for the evaporation of this compound prior to its determination by corona discharge ionization ion mobility spectrometry (CD-IMS). The target analyte was extracted from different water samples by using the extraction method of dispersive liquid-liquid microextraction. Methanol and trichloromethane were utilized as the disperser and extraction solvents, respectively. The effective variables included the volume of disperser and extraction solvents, pH, and the centrifugation time were studied by a Fractional Factorial Design to identify the important parameter(s) and their interaction. To that end, a Central Composite Design was performed to achieve optimum levels of each effective parameter. The results showed that the optimum conditions were 78 µL of the extraction solvent, 1.2 mL for disperser solvent, centrifugation time; 1 minute at 1010 g, and finally pH 7. The detection limit of 2.1 µg L⁻¹, the linear range of 2.5-80 µg L⁻¹, and the relative standard deviation of 7 % were obtained. Different water samples were analyzed by the proposed technique, and the propoxur amounts were successfully determined. The obtained results revealed satisfactory relative recovery values between 91% and 105%.

Keywords: Propoxur; Thermally Unstable Compounds; Dispersive Liquid-Liquid Microextraction; Ultrasonic Piezoelectric Nebulization; Ion Mobility Spectrometry
Introduction

Propoxur is an N-methylcarbamate insecticide with IUPAC name of 2-isopropoxyphenyl methylcarbamate. Carbamate insecticides are very effective for pests’ eradication and cause irreversible inhibition of acetylcholinesterase enzyme (AChE) that leads to interruption the nervous system \(^1\). Propoxur is suitable for killing the most insect pests like fleas, household pests, and flies and used for both agriculture and public health properties \(^2\). This compound is soluble in water (1860 mg L\(^{-1}\) at 30 °C), and polar organic solvents but has a little solubility in non-polar organic solvents \(^3\). Propoxur has medium or low stability and also low affinity in the soil matrix \(^4\), and so, it can cause groundwater pollution, seriously\(^5\). As reported by the World Health Organization, the maximum residue limit of propoxur is estimated 3 mg kg\(^{-1}\) for vegetables, and lower than 0.05 mg kg\(^{-1}\) for other foods \(^6\).

On the other hand, most N-carbamates are thermally unstable and are usually analyzed by spectrophotometric methods \(^7\)–\(^9\) and high-performance liquid chromatography (HPLC) \(^10\)–\(^12\). Gas chromatography (GC) as one of the popular analytical instruments may also be used for analyzing these compounds; however, with some modification in sample preparation or instrumentation. In fact, using a common GC with hot injectors leads to the destruction of chemical structures of these compounds. In many cases, carbamate compounds have been determined by GC after derivatization of analyte \(^13\)–\(^14\). Some other methods included programmed temperature vaporizer devices \(^15\), short column GC \(^16\) and low pressure GC \(^17\) have been developed to make the possibility of GC usage; with the minimum decomposition of N-carbamate. For example, Song and McNair reported a method for analyzing carbamates by using a fast GC with cold on-column injection \(^18\). However, according to their results, in the
heating rate more than 50 °C min⁻¹, thermal decomposition of propoxur would be significant. Therefore with considering this problem, many researchers have been encouraged to use LC or HPLC, for the determination of propoxur; however, this method also suffers from expensive and harmful chemical solvents, in addition to a long run-time required for analysis ¹⁹.

Ion mobility spectrometry (IMS), introduced by Karasek in 1970 ²⁰, has been used as an analytical technique to separate and identify chemical compounds in the gaseous environment and atmospheric pressure. The operation principle of the technique is based on the ionic mobility of species in an electric field, depended on the mass, charge, and shape of ions. The sample molecules need to be ionized, usually through the techniques of radioactive sources ²¹, corona discharge ²², and electrospray ionization source ²³,²⁴. The originated ions are separated under the influence of electric field and drift gas flow, in the opposite direction of ions migration. When ions arrive to the collector, positioned at the end of the drift tube, the corresponding ion peak(s) appear in the ion mobility spectrum ²⁵. IMS has a wide range of application in the analysis of explosives, medical drugs, pesticides, and air pollutants, due to its high speed, ruggedness, sensitivity, and ease of maintenances ²⁶,²⁷.

The thermal desorption injection port is commonly used to make a gas phase sample, prior to analysis by IMS equipped with corona discharge or ⁶³Ni ionization sources. However, this sample introduction system cannot be used for thermally unstable materials due to the decomposition of their molecules. Very recently, an ultra-sonic piezoelectric injection port has been introduced for analyzing the thermally unstable compounds by a stand-alone IMS equipped to corona discharge ionization source (CD-IMS) ²⁸. This injection port can evaporate the sample based on an ultrasonic piezoelectric device, oscillating with RF frequency to transfer the energy to liquid and
form fine droplets.

In this work, the propoxur insecticide was successfully identified and measured with corona discharge ion mobility spectrometry equipped with an ultrasonic injection port (US-CD-IMS). In order to pre-concentrate and extract the propoxur from aqueous solution, the dispersive liquid-liquid microextraction (DLLME) method was used with extraction solvent heavier than water. Some parameters affected the extraction were optimized using Design–of–Experiment (DOE) method. Some real samples of agricultural wastewater, underground water, and wastewater of aviculture were analyzed for the applicability survey.

**Experimental**

**Reagents and chemicals**

Acetone, dichloromethane, acetonitrile, trichloromethane, and tetrachloromethane obtained from Merck (Darmstadt, Germany) and methanol (HPLC grade) were purchased from Dae-Jung (Shiheung, Korea). The propoxur pesticide was prepared from Samgol Company (Tehran, Iran) and its stock solution was prepared in methanol with a concentration of 1000 mg L\(^{-1}\). Working solutions were prepared, daily, by diluting the stock solution. All the solutions were stored at 4 °C in a refrigerator.

**Apparatus**

The instrument, ion mobility spectrometer, with corona discharge ionization source was designed and constructed by Teif Azmon Espadana Company (Isfahan, Iran). The instrument was equipped with an ultrasonic piezoelectric nebulizer as sample introduction system, described previously \(^{28-30}\). Briefly, the IMS instrument comprises
the IMS cell counting the corona discharge ionization system, a pulse generator, two high voltage power supplies, an analog to digital converter, and a computer. The sample introduction system contained a piezoelectric element in a cylindrical glass which was closed by a piece of PTFE. Samples were injected through a septum by a 25µL syringe. By applying an electric voltage (40V and 2.5MHz) to the piezoelectric element, the sample solution was nebulized and carried into the reaction region, by the nitrogen gas flow. Working conditions of CD-IMS are shown in Table S1, in the Supporting Information. The ion mobility spectrum obtained after injecting the standard propoxur compared to the background of the instrument is shown in the Supporting Information. Fig. S1. This figure shows only one ion peak (drift time 9.92 ms) was originated from the analyte.

Procedure

Dispersive liquid-liquid microextraction

For the pre-concentration process, 4 mL aqueous solution of propoxur was placed in a 10 mL-conic bottom test tube. The volumes of 78 µL extraction solvent (trichloromethane) and 1.2 mL disperser solvent (methanol) were firstly mixed and then injected into the sample solution, rapidly, to appear a cloudy mixture. After centrifugation for 1 minute at 1010 g, the extraction solvent, enriched with the analyte, was separated from the aqueous solution. Afterward, 5 µL sediment phase was injected into the sample introduction system for determining the analyte.

To evaluate the DLLME method for pre-concentration of propoxur in the real sample, some samples including agricultural wastewater, underground water (obtained from Vandadeh village, Isfahan-Iran) and wastewater of aviculture. Except in the wastewater of aviculture, no propoxur was detected in the studies of real samples. The
samples were spiked with standard solutions of propoxur, for calculating the relative recovery of the method.

Results and Discussion

Selection of disperser and extraction solvents

Before using Response Surface Method (RSM) methodology, the types of disperser and extraction solvents must be indicated. In this work, the DLLME method base on the extraction solvents with a higher density than water was used. Initially, to obtain the comparable results, the ratio of disperser and extraction solvents was examined for different solvents for reaching out to the same volume of the sediment phase. In this regard, different disperser solvents included acetone, acetonitrile, and methanol, and three extraction solvents of trichloromethane, dichloromethane, and tetrachloromethane were selected for DLLME method. The volumes of disperser and extraction solvents needed to obtain 10 µL sediment phase were shown in Table S2 (in the Supporting Information). The obtained results are shown in Fig. 1, showing that the maximum extraction was achieved for the pair of methanol and trichloromethane.

Optimization of parameters using RSM

For optimizing the experimental parameters in the DLLME process, the RSM based on Central Composite Design (CCD) was used. To that end, type and volume of extraction and disperser solvents, pH, and time of centrifuging were studied and optimized. Firstly to screen the main variables affecting the extraction procedures, a Fractional Factorial Design (FFD) was carried out. The optimum experimental conditions were obtained by using the trial version of Design-Expert 7.1.3 (Stat-Ease Inc., Minneapolis, USA) software.
**Fractional Factorial Design**

For optimization of the experiment parameters, it is necessary to determine the most important factors that affect the result. This reduces the number of experiments in a multivariable system. After the screening experiments, the relationship between the effective factors and the final response were explored for obtaining the optimized experimental parameters.\textsuperscript{31,32} In this regard, the peak area in the ion mobility spectrum was calculated and considered as the response of the instrument. The main factors examined are presented in Table S3, in the Supporting Information. It is notable that degradation of propoxur may occur in alkaline condition;\textsuperscript{33,34} so, the pH range 3-8 was selected for studying this parameter. According to the number of variables, eight experiments were designed for FFD, which are shown in Table 1. The method of ANOVA was used to examine the precision and accuracy of the design. The results are presented in Table 2. According to the results, the significance of the model can be concluded from the $F$-value of 20.22, with only 0.70% chance of noise generation. General, $p$-values < 0.05 indicate that the model terms are significant, and the terms with $p$-values more than 0.1000 are not significant. So, based on the results, only the terms of extraction solvent (A) and disperser solvent (B) have a significant effect on the experiment response. Therefore, these parameters should be used in CCD optimization. Other parameters including pH and the time of centrifugation showed a $p$-value higher than 0.05, and so, their effect on the extraction can be disregarded. The optimum pH and centrifugation duration were considered 7 and one min.

**Central Composites Design**

After screening and determining the effective factors, the CCD method was used to determine the exact values for optimum conditions of the DLLME. Table S4 (in the Supporting Information) shows the effective factors and their symbols and levels in the CCD method. The designed matrix and the corresponding responses are also presented in Table S5 (in the
Supporting Information). Moreover, the results of the ANOVA obtained for CCD are shown in Table 3. According to these results, the significance of the model is concluded from F-value (14.87). This indicates that there is only 0.13% chance for occurring of "Model F-Value" due to the noise. According to the P value, A, B, A^2, and B^2 are significant terms of the model. The model equation is shown in Eq. (1) and Fig. 2 shows three-dimensional and the counter plot of CCD model.

\[
y = 2473.80 - 406.09 \times A + 148.94 \times B - 201.5AB + 268.00 \times A^2 + 104.03 \times B^2
\]  

(1)

Considering the pure error and the “Lack of Fit (LOF) F-value” of 0.04, the model is not significant. The model quality was evaluated using the coefficient of determination (R^2, adjusted-R^2, and adequate precision). The R^2 was obtained 0.9139, indicating the accuracy of the model in the prediction of measured responses. The value of adjusted-R^2 was equal to 0.8525, calculated from the significant variables of the model. The signal-to-noise ratio is characterized by adequate precision and used to compare the predicted values relative to the average error. In this work, the signal-to-noise ratio was obtained 10.4950, indicating adequate model discrimination.

**Instrumental Parameters affecting the analyte signal**

Before analyzing the propoxur by ion mobility spectrometer with the ultrasonic nebulizer, the effects of IMS cell temperature and carrier gas flow rate on the signal intensity were investigated.

**Cell temperature**

As mentioned in the Introduction section, propoxur is known as a thermally unstable compound, so the temperature of the IMS cell can affect the analyte signal, significantly. For investigating this parameter, the standard solution of propoxur in methanol (10 mg L⁻¹) was
injected into the ultrasonic nebulizer system. The signal (area of the originated analyte peak) was calculated and considered as the IMS response. As be shown in Fig. 3, with increasing the IMS cell temperature, the analyte signal was firstly increased up to 140 °C, might be due to raising the ionization efficiency. The response was then decreased at higher temperatures because of the thermal degradation of propoxur, inside the reaction region.

**Carrier gas flow rate**

The produced droplets of the sample were entered into the ionization source, by passing the carrier gas (nitrogen) through the ultrasonic nebulizer chamber. The flow rate of this carrier gas should be optimized to achieve the maximum response. To that end, 5 µL of propoxur solution in methanol (10 mg L\(^{-1}\)) was injected and the corresponding response was explored, by varying the carrier gas flow rate. Based on the results depicted in Fig. 4, the maximum IMS response was obtained at the carrier gas flow rate of 0.3 L min\(^{-1}\). In fact, the flow rates lower than 0.3 L min\(^{-1}\) cannot carry the sample into the ionization source, sufficiently, and otherwise, the nebulization efficiency might be affected by increasing the gas pressure inside the chamber, at very high gas flows. So, the flow rate of 0.3 L min\(^{-1}\) was selected for carrier gas, in all the subsequent experiments.

**Validation of the method**

To evaluate the method, propoxur was extracted from different synthesized sample solutions, and the analyte was determined by IMS. Under the optimum conditions of the method, some figures of merit including the limits of quantification (LOQ) and detection (LOD), the linear dynamic range (LDR), and the relative standard deviation (RSD%) were calculated for propoxur. The calibration plot of the analyte was provided and the results showed a linear range from 2.5 to 80 µg L\(^{-1}\) with determination coefficients of 0.9977. The values of LOQ (S/N = 10)
and LOD (S/N = 3) were calculated to be 5.0 and 2.1 µg L\(^{-1}\), respectively. The RDS values were calculated 9% and 7% for standard solutions of propoxur, 10 and 60 µg L\(^{-1}\), respectively. The enrichment factor of 48 was calculated by analysis of propoxur in 40 µg mL\(^{-1}\) solution. This value of enrichment factor is well comparable with some other methods such as graphene-based solid-phase extraction (34.2-51.7) \(^{35}\), single-drop microextraction (38) \(^{36}\), micro-solid-phase extraction (50) \(^{37}\), which have been used for propoxur extraction, previously.

**Analysis of field sample**

To further investigate the capability of the DLLME-US-CD-IMS, the applicability of the method was examined for determination of propoxur in different water samples including agriculture wastewater, wastewater of aviculture, and underground water. The extraction and instrumental analysis were done under the optimum condition obtained as extraction solvent volume, 78 µL; disperser solvent volume, 1.2 mL; centrifugation time, one minute, and the pH value of 7. Fig. 5 shows the ion mobility spectra obtained after injecting the samples extracted from different water solutions compared with their corresponding backgrounds. According to these results, propoxur peak was not detected in agriculture wastewater and underground water, while a peak with considerable intensity was detected for aviculture wastewater. To overcome the matrix interference, the amount of propoxur in the samples was determined by the multiple standard addition technique. The recovery values were calculated based on the Eq. (2) for spiked samples, and the results are presented in Table 4.

\[
\text{ery(}RR\%) = \frac{\text{found}}{\text{real}}
\]

(2)

Herein, \(C_{\text{found}}\), \(C_{\text{real}}\), and \(C_{\text{added}}\) are related to the analyte concentration, obtained after adding a certain amount of analyte to sample, the real analyte concentration in the sample, and the analyte concentration which is spiked to sample, respectively. According to the results, the relative recovery values were in the range of 91%-102%, and the calculated RSD values were
lower than 9% for real samples. Consequently, this method can successfully be used for the determination of propoxur in real samples.

Comparison with other methods

Table 5 shows the comparison of some analytical parameters obtained by DLLME-US-CD-IMS with those reported previously by other techniques, for the determination of propoxur in different samples. As shown in this Table, the proposed method has acceptable and comparable LOD and recovery values with other listed methods. Generally, the method of HPLC is used for separation and detection of thermally unstable compounds. Unlike HPLC, IMS instrument has very short time of analysis (<1 min) and needs very low volume of solvents; so, applying the ultrasonic nebulizer as sample introduction system was suggested to be provided the possibility of IMS utilizing in the determination of thermally unstable compound of propoxur. On the other hand, the IMS instrument has high portability potential, which is helpful in the field analysis of samples.

Conclusions

In this work, propoxur, as a thermally unstable pesticide, was determined successfully by using CD-IMS assisted with an ultrasonic nebulizer injection port. Pre-concentration of analyte was accomplished based on dispersive liquid-liquid microextraction from the different water samples. Using ultrasonic nebulizer as an injection port provide a method to transfer the liquid sample to the gaseous phase in ambient temperature and avoided the thermal decomposition of the analyte. This feature makes the possibility of the analysis of thermally unstable compounds. Based on the satisfactory results as well as the advantages of CD-IMS such as the high speed of analysis, ease of maintenance
and relatively high sensitivity, DLLME-US-CD-IMS method can be suggested as a proper alternative method for determination of propoxur comparable to the commonly used methods such as HPLC or GC/MS.

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Table 1  Design matrix and the responses for a fractional factorial ($2^{4-1}$) design. (Variables are coded)

| Run No. | A  | B  | C  | D  | Response |
|---------|----|----|----|----|----------|
| 1       | 85 | 0.6| 3  | 1  | 2702     |
| 2       | 120| 1.2| 3  | 1  | 2676     |
| 3       | 120| 0.6| 8  | 1  | 2542     |
| 4       | 120| 0.6| 3  | 4  | 2193     |
| 5       | 85 | 1.2| 3  | 4  | 3443     |
| 6       | 85 | 0.6| 8  | 4  | 3023     |
| 7       | 120| 1.2| 8  | 4  | 2442     |
| 8       | 85 | 1.2| 8  | 2  | 3406     |

a. Volume of extraction solvent (µL)

b. Volume of disperser solvent (mL)

c. pH value

d. Centrifugation time (min)
Table 2  Analysis of variance (ANOVA) for fractional factorial design.

| Source      | Sum of Squares | DF\textsuperscript{a} | Mean Square | F-value\textsuperscript{b} | P-value\textsuperscript{c} |
|-------------|----------------|------------------------|-------------|-----------------------------|------------------------------|
| Model       | 1.612E+06      | 3                      | 5.373E+05   | 20.22                       | 0.0070                       |
| A-Extractor | 1.097E+06      | 1                      | 1.097E+06   | 41.30                       | 0.0030                       |
| B-Disperser | 3.634E+05      | 1                      | 3.634E+05   | 13.67                       | 0.0209                       |
| AB          | 1.510E+05      | 1                      | 1.510E+05   | 5.68                        | 0.0757                       |
| Residual    | 1.063E+05      | 4                      | 26573.62    |                             |                              |
| Cor. Total\textsuperscript{d} | 1.718E+06 | 7                      |             |                             |                              |

\textsuperscript{a} Degrees of freedom.

\textsuperscript{b} Test for comparing model variance with residual (error) variance.

\textsuperscript{c} Probability of seeing the observed “F value” if the null hypothesis is true.

\textsuperscript{d} Totals of all information corrected for the mean
Table 3  Analysis of variance (ANOVA) for central composite design.

| Source | Sum of Squares | Df\(^a\) | Mean Square | F-value\(^b\) | p-value\(^c\) |
|--------|----------------|----------|-------------|---------------|---------------|
| Model  | 2.159E+06      | 5        | 4.318E+05   | 14.87         | 0.0013        |
| A-Extractor | 1.306E+06 | 1        | 1.306E+06   | 44.96         | 0.0003        |
| B-Disperser | 1.676E+05 | 1        | 1.676E+05   | 5.77          | 0.0473        |
| AB     | 1.624E+05      | 1        | 1.624E+05   | 5.59          | 0.0500        |
| A\(^2\) | 4.882E+05      | 1        | 4.882E+05   | 16.81         | 0.0046        |
| B\(^2\) | 63602.93      | 1        | 63602.93    | 2.19          | 0.1825        |
| Residual| 2.033E+05      | 7        | 29047.35    |               |               |
| Lack of Fit | 1.684E+05    | 3        | 56148.75    | 6.44          | 0.0519        |
| Pure Error | 34885.20      | 4        | 8721.30     |               |               |
| Cor.\(^d\) Total | 2.363E+06    | 12       |              |               |               |

\(^a\) Degrees of freedom.

\(^b\) Test for comparing model variance with residual (error) variance.

\(^c\) Probability of seeing the observed “F value” if the null hypothesis is true.

\(^d\) Totals of all information corrected for the mean
Table 4  Analysis of propoxur in real samples by DLLME-US-CD-IMS.

| Sample                        | Added$^a$ | Found$^a$ | Relative Recovery (%) |
|-------------------------------|-----------|-----------|-----------------------|
| Agricultural wastewater      | -         | ND$^b$    |                       |
|                               | 10        | 10.10 (5)$^c$ | 101                   |
| Underground water             | -         | ND        |                       |
|                               | 10        | 9.90 (3)  | 99                    |
| Wastewater of aviculture      | -         | 5.3 (4)   |                       |
|                               | 5         | 10.10 (9) | 96                    |

a. Propoxur concentration (µg L$^{-1}$)
b. Not detected
c. The value of Relative Standard Deviation (%)
Table 5  Comparison of the DLLME-US-CD-IMS method with other reported method for the extraction and determination of the propoxur.

| Analytical method | Real sample            | LOD\(^a\) (µg g\(^{-1}\)) | LDR\(^b\) (µg L\(^{-1}\)) | RSD\(^c\) (%) | Recovery (%) | Ref |
|-------------------|------------------------|-----------------------------|-----------------------------|---------------|--------------|-----|
| MSPE\(^e\)-HPLC/UV-vis | Apple                  | 0.2                         | 1.0-100.0 (ng g\(^{-1}\)) | 5.7           | 89.3 – 109.7 | [38]|
|                   | Water and zucchini     | 0.03                        | 0.1-100                     | 4.2           | 86.1-99.4    | [10]|
| USAEME\(^e\)-HPLC/UV-vis | Beverage              | 1                           | 10-10\(^4\)                | 6.2           | 93–106       | [39]|
| QuEChERS\(^f\)-LC-MS/MS | Dates                 | 0.95 (µg kg\(^{-1}\))      | 1-200 (µg kg\(^{-1}\))    | 7.7           | 90-115       | [40]|
| MIP\(^g\)-IPP/GC\(^h\) | Pig liver              | 18.8                        | 18.8-9416.8                 | 8.67          | 101.7        | [41]|
| VSLLME\(^i\)-MEKC\(^j\)-MS/MS | Juices                | 2.3                         | 2.3-250 (µg kg\(^{-1}\))  | 15            | 81-104       | [42]|
|                   | Tap water              |                             |                             |               |              |     |
| MIP\(^g\)-IMS\(^h\) | Agricultural wastewater | 0.3                         | 1-250                      | 5-7           | 94-102       | [43]|
|                   | Agricultural wastewater, Underground water | 2.1                         | 5-80                       | 6-9           | 96-101       | This work |
| DLLME-US-CD-IMS   | Wastewater of aviculture |                             |                             |               |              |     |
a. Limit of detection
b. linear dynamic range
c. Relative standard deviation
d. Magnetic solid-phase extraction
e. Ultrasound-assisted emulsification-microextraction
f. The quick, easy, cheap, effective, rugged and safe method
g. Molecularly imprinted polymer
h. 2-isopropoxyphenol Glassy carbon electrode
i. Vortex-assisted liquid-liquid microextraction
j. Micellar electrokinetic chromatography
k. Ion mobility spectrometry
Figure Captions

Fig. 1 The effect of extraction and disperser solvents type on the extraction efficiency of DLLME. (Propoxur concentration, 1 mg L\(^{-1}\)).

Fig. 2 Three-dimensional (3D) plot (A) and contour plots (B) of the instrument responses for extracted propoxur related to disperser and extraction solvents volume.

Fig. 3 The effect of IMS cell temperature on the propoxur signal by using the ultrasonic nebulizer injection port. (propoxur concentration, 10 mg L\(^{-1}\)).

Fig. 4 The effect of carrier gas flow rate on the propoxur signal of IMS. (propoxur concentration, 10 mg L\(^{-1}\)).

Fig. 5 The CD-IMS spectra of propoxur extracted before (blank) and after spiked samples of A) agricultural wastewater, B) underground water, C) wastewater of aviculture. (The propoxur concentration spiked in A, B real samples are 40 µg L\(^{-1}\), and in C real sample is 10 µg L\(^{-1}\)).
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