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Sustainable Adsorption Method for the Remediation of Crystal Violet Dye Using Nutraceutical Industrial Fenugreek Seed Spent

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Abstract: Nutraceutical industrial fenugreek seed spent (NIFGS), a relatively low-cost material abundantly available with little toxicity is used in crystal violet (CV) dye remediation from aqueous media and reported in the present study. To access the adsorption capacity, the factors affecting it are kinetics and the equilibrium thermodynamics. All the experiments were designed at approximately pH 7. The adsorption isotherm model proposed by Langmuir fits better than the Freundlich isotherm model. Kinetic studies data confirm the pseudo-second order model. It is evident from thermodynamic parameter values that the process of adsorption is endothermic, physical and dynamic. The process optimization of independent variables that influence adsorption was carried out using response surface methodology (RSM) through bi-level fractional factorial experimental design (FEED). The analysis of variance (ANOVA) was implemented to investigate the combined effect of parameters influencing adsorption. The possibilities of using dye-adsorbed NIFGS (“sludge”) for the fabrication of the composites using plastic waste are suggested.
Keywords: nutraceutical industrial fenugreek seed spent; crystal violet; adsorption studies; fractional factorial experimental design; analysis of variance

1. Introduction

The Indian clothing and textile sector ranks second in the world. This sector has two divisions, manufacturing and agricultural related activities. The former employs over 35 million people and contributes 3% GDP; while the latter engages over 60 million workforces and adds 14% towards industrial production. These activities contribute to 3% GDP and about 14% towards industrial production [1]. The textile manufacturing sector is broadly classified into organized and unorganized sectors. The unorganized sector operates in small units and adopts traditional tools, techniques and outdated technologies which results in the release of large amounts of toxic and hazardous dyes into the environment [2]. Thus, the textile industries have a dubious distinction of being one amongst the top ten industries causing pollution [3].

An immediate challenge the textile industry faces is to attain sustainability by reducing carbon and water footprints [4], diminishing the colour and reducing ecological and public health problems [5]. The major causes of pollution from textile industries are low profit margins, the lack of cost-effective technologies, over-capacity, severe competition, and strict environmental regulations in the treatment of wastewater. The dyes designed for textile industries are environmentally stable which poses the additional challenge of removing the toxic compounds from TIE using conventional technologies. Thus, removal of dyes and allied materials with minimum overhead charges from TIE assumes paramount importance.

The methods, procedures and techniques used for the remediation of dyes in TIE are broadly classified as biological, biological cum chemical, electrochemical, electro-coagulation, physical methods using UV radiations, photo-catalytic degradation [6,7] and the use of nanomaterial and activated carbons. Various related studies have been carried out pertaining to thermal engineering [8–16], photocatalysis [17,18], supercapacitor [19] and sonocatalytic degradation [20]. All the methods and materials have serious limitations, such as the disposal of residual sludge, the high cost of plant establishment, increased operation cost, interference by wastewater ingredients, the problem of regeneration, secondary pollutants and sensitivity to changes in the wastewater input [21,22].

Currently, the adsorption technique with the characteristics of simplicity, efficiency, minimum discharge of toxic by-products and possibilities of scaling up to field-level is widely employed for the remediation of TIE. The pore structure, cost, abundant availability and ready-to-use adsorbent are the qualities required for enhancement of efficiency of the removal of toxic dyes from TIE. Most of the materials proposed as adsorbents do not qualify for the needs and demands of the textile industry. Scant literature available on the problem of sludge generated during the process poses an additional challenge. These limitations have created a surge amongst scientists to look for an alternative, which is economically feasible and environmentally acceptable.

Nutraceutical industries are growing rapidly with a possible profit and produces an unprecedented myriad of spent/waste. The nutraceutical industrial spent (NIS) produced as by-product has no feed, fuel or fertilizer value. Presently, NIS is disposed in landfills and as low-calorific value fuel which is attributed to the pore structure which traps moisture from the atmosphere. Incineration/burning of NIS results the formation of greenhouse gases which is environmental pollution and leaves a carbon footprint. Utilization of NIS as an adsorbent to amputate the toxic substances from TIE ecologically alleviates waste disposal problems and addresses the needs and demands of sustainability [23–25].

India ranks first by producing about $2.40 \times 10^5$ tons of fenugreek seed which is extensively used as nutraceutical [26]. Fenugreek (Trigonella foenum-graecum L.) is a nutraceutical belonging to the legume family. This is an annual crop native to the region stretching from Iran to northern India, but now it is widely cultivated in China, Ukraine,
Greece, and North and East Africa [27]. We reported the use of NIFGS as an adsorbent in the extraction of blue acid 113, a bisazo acidic dye from water and TIE [28].

Crystal violet (CV) dye belongs to the class of triarylmethane dyes. It is also called gentian violet, with the molecular formula C_{25}H_{30}N_{3}Cl. CV is extensively utilized for the dyeing of leather, cotton, paper, silk and nylon [29]. Dye with a high molar extinction coefficient, 88,000 moles$^{-1}$ L$^{-1}$ when released into the hydrosphere may cause significant pollution due to its resistant nature, reducing rays of sunlight and causing the unwanted colour present in the water bodies, fighting against photochemical and biological problems in aquatic life. Thus, removal of CV from industrial effluents assumes paramount importance. The current article exemplifies the incorporation of NIFGS for adsorption of CV from aqueous solution and TIE. The study also suggests the implementation of dye-adsorbed NIFGS as a filler ingredient in composite material fabrication from waste plastic. The novelty of the research work is there is a scant literature on the CV dye remediation and NIFGS use as adsorbent. This study endeavours to explore the use of nutraceutical industrial fenugreek seed spent adsorbent for bioremediation of CV. This poisonous dye used in textile industries is discharged as a pollutant.

2. Experiment Details

2.1. Materials

The dye used is crystal violet. It has a molecular weight of 407.98 g/mol, $\lambda_{\text{max}} = 590$ nm. The dye concentration is measured using an UV-vis spectrometer (Perkin-Elmer Lambda EZ-201, USA).

2.2. Parametric Effect Study

The experimental factors (pH grade, dye initial concentration, dosage and temperature) influence was studied using batch experiments. For preparing a stock solution of CV (1000 mg L$^{-1}$), double distilled water was used. Preparation of solution concentrations ranging from 25 mg L$^{-1}$ to 300 mg L$^{-1}$, was performed using the bulk stock solution. A 250 mL Erlenmeyer flask was combined with a dye solution dose of 50 mL. The calculated quantity of NIFGS was added to every flask. Parametrical evaluations were performed for various parameter ranges stated, pH (2, 4, 6, 7, 8, 10 and 12); initial concentration of CV dye solution (25–300 mg L$^{-1}$) and adsorbent quantity (0.025–0.200 g) in 50 mL (0.500–4.000 g L$^{-1}$). Thermal influence on adsorption was investigated for a dye concentration of 200 mg L$^{-1}$ at three selected temperatures. The data were fitted into Equations (1)–(3), observed in Table 1. Solution stirring at 165 rpm was carried out for 3 h in an orbital shaker under constant thermal conditions. Samples were withdrawn at predetermined equilibrium time. The unadsorbed CV dye in the solution phase was separated from NIFGS by centrifugation with 3000 rpm for five minutes. If the solution was unclear, the centrifugation was repeated for an additional 5 min. The CV dye concentration at an equilibrium pertaining to the supernatant centrifuged solution was determined using a spectrophotometer. To study the effect in a range of pH 2–12, batch experiments were performed. The pH regulation within a desired range was achieved by concentrating the solution with 0.01–1.00 M HCl or NaOH solution. For the adsorption kinetic studies of CV dye solution (200 mg L$^{-1}$), three temperatures (303, 313 and 323 K) were selected, and experiments carried out with time as independent variables. Experiments were replicated thrice, and the mean values were considered.

2.3. Characterization Methods

IR spectra were recorded using the FTIR spectrophotometer (Perkin Elmer 3 lambda). The JEOL model 3300 scanning electron microscope was used to record SEM images. A pH meter Model 802, Systronics, India, was used to measure pH.
| Eq. No. | Equation | Description | Parameter |
|---------|----------|-------------|-----------|
| (1) | \( q_e = \frac{(C_o - C_e)}{V} \) | Adsorption capacity at equilibrium | \( q_e \): equilibrium adsorption capacity (mg L\(^{-1}\)) \( C_o \): initial concentration of adsorbent (mg L\(^{-1}\)) \( C_e \): equilibrium adsorbent concentration (mg L\(^{-1}\)) |
| (2) | \( q_t = \frac{(C_o - C_t)}{W} \) | Adsorption capacity at time \( t \) | \( q_t \): time \( t \) adsorption capacity (mg L\(^{-1}\)) \( C_o \): initial concentration of adsorbent (mg L\(^{-1}\)) \( C_t \): time \( t \) adsorbent concentration |
| (3) | \( RE\% = \frac{[C_o - C_e]}{C_o} \times 100 \) | Percentage removal efficiency | \( RE\% \): adsorbent weight (g) |
| (4) | \( q_L = \frac{Q_m}{K_L \times C_o} \) | Langmuir isotherm [30] | \( Q_m \): monolayer adsorption capacity (mg g\(^{-1}\)) \( K_L \): adsorption constant of Langmuir isotherm (L mg\(^{-1}\)) |
| (5) | \( R_L = \frac{1}{1 + K_L C_o} \) | Separation factor of Langmuir isotherm | \( R_L \) factor implies whether the adsorption is when \( (R_L > 1) \): unfavourable \( (R_L = 1) \): linear \( (0 < R_L < 1) \): favourable and \( (R_L = 0) \): irreversible |
| (6) | \( q_e = K_F C_e^\frac{1}{n_F} \) | Freundlich isotherm [31] | \( K_F \): adsorption constant of Freundlich isotherm (mg/g) \( n_F \): heterogeneity factor indicates the nature of adsorption is \( (n_F < 1) \): chemisorption \( (n_F = 1) \): linear or \( (n_F > 1) \): physisorption |
| (7) | \( q_t = q_e \left(1 - e^{-k_1t}\right) \) | Pseudo-first order Equation [32] | \( q_t \): time \( t \) adsorption capacity (mg L\(^{-1}\)) \( q_e \): equilibrium adsorption capacity (mg L\(^{-1}\)) \( k_1 \): rate constant of pseudo-first order (s\(^{-1}\)) |
| (8) | \( q_t = \frac{q_e^2 k_2 t}{1 + q_e k_2 t} \) | Pseudo-second order Equation [33] | \( q_t \): time \( t \) adsorption capacity (mg L\(^{-1}\)) \( q_e \): equilibrium adsorption capacity (mg L\(^{-1}\)) \( k_2 \): rate constant of pseudo-second order (mol\(^{-1}\) L\(^{-1}\) s\(^{-1}\)) \( t \): adsorption duration (s) |
| (9) | \( \Delta G^o = \Delta H^o - \Delta S^o T \) | Standard Gibbs free energy | \( \Delta G^o \): standard free energy (J mol\(^{-1}\)) \( \Delta H^o \): enthalpy change (J mol\(^{-1}\)) \( \Delta S^o \): entropy change (J mol\(^{-1}\) K\(^{-1}\)) T: absolute temperature (K) |
| (10) | \( \Delta G^o = -RT \ln K_{eq} \) | Standard Gibbs free energy at chemical equilibrium | \( R \): ideal gas constant (J mol\(^{-1}\) K\(^{-1}\)) \( K_{eq} \): chemical equilibrium constant |
| (11) | \( K_{eq} = \frac{C_a}{C} \) | Thermodynamic equilibrium constant | \( C_a \): initial adsorbent concentration (mg L\(^{-1}\)) |
| (12) | \( \ln K_{eq} = \frac{\Delta S^o}{T} - \frac{\Delta H^o}{R} \) | Variant of standard Gibbs free energy | \( C_a \): adsorbent concentration at equilibrium (mg L\(^{-1}\)) |

2.4. Statistical Optimization of Process Parameters

An experimental design [34] for the optimization of five process parameters at two levels was prepared for the CV-NIFGS system to obtain a quadratic regression equation using the ANOVA model.

3. Experimental Outcomes

3.1. Analyses of SEM Images

Figure 1a,b, illustrates the pictorial presentation of SEM images. The dye adsorption onto the NIFGS surface can be depicted from these pictures. The NIFGS surface texture has a porous and fibrous structure which resembles a honeycomb shape, it enhances the
adsorption of the substrate (dye) on it. Figure 1a describes the structure of the pores which help to fasten the adsorption process, while Figure 1b shows the limited filling of pores by the dye.

![SEM images of (a) NIFGS and (b) CV-NIFGS.](image)

**Figure 1.** SEM images of (a) NIFGS and (b) CV-NIFGS.

3.2. The Influence of Variables on CV Adsorption on NIFGS

3.2.1. Solution pH

The adsorption capacity of NIFGS depends on solution pH. The pH plays dual roles: first, to instigate surface characteristics of adsorbent and second, the chemical nature of solution [35]. The pH as a parameter, and assumes importance to substantiate the efficiency of the adsorbent under study. The knowledge of this parameter is significant when the process is scaled to commercial levels [36]. The NIFGS exhibits good capacity of adsorption with increased pH. This characteristic is dedicated to the repulsion between cations and H⁺ ions with lower pH. Conversely, at higher pH the negatively charged OH⁻ attracts the cation of the dye and the negatively charged species (Figure 2a).

3.2.2. Dye Concentration Influence

The adsorption capacity of CV dye initial concentration has profound influence on NIFGS. The increase in the initial dye concentration from 25 to 300 mg L⁻¹ onto NIFGS increased from 10 to 78 mg g⁻¹. The adsorption of NIFGS related to the concentration gradient has a driving force on the dye adsorption (Figure 2b). The adsorption of CV was more with a higher concentration and reached almost constant after attaining equilibrium [37].

3.2.3. Adsorbent Dosage Influence

Adsorbent quantity has profound influence on the commercialization of the process because it decides the economic viability [38]. Adsorbent amount increment from 0.500 to 4.000 g L⁻¹ is associated with reduced CV dye removal from the solution (Figure 2c). This observation assumes importance in the commercialization process where the number of trials with minimum amounts of the adsorbent substantially increases the dye removal efficiency of the dye by NIFGS.
Figure 2. Cont.
3.2.4. Temperature Influence

Keeping in view our focus to scale to commercial applications, evaluation of the process of adsorption of dyes onto NIFGS in relevance to thermal influence was studied. Temperature influence on CV dye adsorption onto NIFGS is presented in Figure 2d. The data obtained for the classical thermodynamic parameters, namely, ΔG°, ΔH° and ΔS° indicate the nature and type of reaction. For example, the positive ΔH° (enthalpy) values obtained from 303 to 323 K of NIFGS indicate an endothermic process. The overall negative values of ΔG° (free energy) obtained for CV-NIFGS system confirm the spontaneity and viability of adsorption. For spontaneous adsorption at reduced temperature, the extent of ΔG° values indicates that the process of adsorption is rapid. Further, it is inferred that the positive ΔS° value suggests more randomness at a solid solution interface and good affinity of CV towards the adsorbent. Similar observations were reported elsewhere [39].

The uncertainty principle, also known as Heisenberg’s uncertainty principle, is a topic of quantum mechanics. Analytical chemists do not use this principle to determine the accuracy of the experiments carried out. Conversely, we report the accuracy in terms of the coefficient of variance which we incorporated in the text. The experiments which were carried out in our laboratory were performed in sets of three trials. The coefficients of variation in the results and uncertainty value for parametric influence such as pH grade of the solution, initial concentration of the dye, and the adsorbent quantity and temperature did not exceed ±2% error. The error bars are incorporated for the Figures 2 and 3 respectively.

3.3. Adsorption Isotherms—Modelling Analysis

A study on the analysis of adsorption data using isotherm models (Langmuir and Freundlich) was intended for an efficiency evaluation of NIFGS in the extraction of CV dye for commercial applications with an eye on the degree of economic advantages. The main criterion of the study of adsorption isotherms was to select a model, where qe (the experimental equilibrium) values were almost equal to Qm (the monolayer adsorption capacity) value with a coefficient of determination (R²) value ≥ 0.90. To refine the data and to make a distinction between the results obtained by two isotherm models, SSE and χ² as two additional error functions were incorporated in our study.
Langmuir [30] proposed a model on the assumption that the adsorbent has active sites possessing almost uniform energies. This was further established on the idea that no lateral interaction takes place between adsorbed molecules. A plateau in a two-dimensional graph with equilibrium concentration ($C_e$) as the independent variable and $q_e$ as the dependent variable characterizes that spontaneous surface sites of adsorbent are almost fully saturated. This implies that further adsorption cannot take place and the possibility of multilayer adsorption of the dye is ruled out. The equations of the Langmuir isotherm model are shown in Equations (4) and (5), Table 1. The Langmuir isotherm parameters, $q_{\text{max}}$ and $b$ tabulation involves the slope ($1/q_{\text{max}}$) and intercept ($1/bq_{\text{max}}$) of the graph $C_e/q_e$ versus $C_e$ as shown in Figure 3a.

In contrast to the Langmuir isotherm model, Freundlich proposed the heterogeneity of the surface sites with different energy of adsorption and demonstrated relevance to multilayer adsorption [31]. The mathematical expression is shown in Equation (6), Table 1.
A graph of $\ln(q_e)$ vs. $\ln(C_e)$ is utilized in calculation of the Freundlich constants $n_F$ (1.096) and $K_F$ (Figure 3b). The values suggest that the transfer of the dye from the bulk solution using NIFGS is physisorption and favours the Langmuir isotherm.

3.4. Adsorption Kinetics

The solute separation from solution adhering to adsorbent is known as adsorption which is dynamic in its nature. Kinetic models provide an insight on the performance of adsorption of CV dye on NIFGS with time as an independent variable. The studies will have a great impact on scaling for commercial applications. To provide the variation in adsorption rate, a concentration of 50, 100 and 200 g mL$^{-1}$ of CV dye was used to carry out kinetic studies at 303, 313 and 323 K. Results are presented in Table 2. Kinetic data of adsorption of CV on NIFGS was analysed using the pseudo-first order model Equation (7), Table 1 [32] and pseudo-second order model Equation (8), Table 1 [33]. For the CV-NIFGS system the latter fits more appropriately than the other.

Table 2. Adsorption kinetics model predicted parameters.

| Initial Concentration [µg mL$^{-1}$] | Pseudo-First Order | Pseudo-Second Order |
|--------------------------------------|--------------------|---------------------|
|                                      | $q_e$ (mg g$^{-1}$) | $K_1$ (min$^{-1}$)  | $R^2$ | $q_e$ (mg g$^{-1}$) | $K_1$ (min$^{-1}$) | $R^2$ |
| 50                                   | 3.22               | 0.054               | 0.99  | 19.12             | 48.77             | 0.97  |
| 100                                  | 4.52               | 0.045               | 0.98  | 44.24             | 237.25            | 0.98  |

3.5. Thermodynamics of the Adsorption Process

Entropy ($\Delta S^o$) and change in free energy ($\Delta G^o$) in the dye-adsorbent system are main features of the process design of adsorption thermodynamics. The relationship of $\Delta G^o$, $\Delta H^o$ and $\Delta S^o$ are presented in Equations (9)–(12) (Table 1). The thermodynamic parameters were presented in Table 3. The decrease in negative $\Delta G^o$ value with rise in temperature specifies the spontaneity of the adsorption process. The positive values of $\Delta S^o$ indicate the decrease in the randomness at the dye/NIFGS interface.

Table 3. CV-NIFGS thermodynamic factors.

| Dye Concentration [µg mL$^{-1}$] | Temperature [K] | Change in Free Energy $\Delta G^o$ [kJ/mol] | Change in Entropy $\Delta S^o$ [J/mol K] | Change in Enthalpy $\Delta H^o$ [kJ/mol] |
|----------------------------------|-----------------|---------------------------------------------|-------------------------------------------|------------------------------------------|
| 50                               | 303             | -2.52                                       |                                           |                                           |
|                                  | 313             | -2.65                                       | 23.28                                     | 9.91                                     |
|                                  | 323             | -2.77                                       |                                           |                                           |
| 100                              | 303             | -3.26                                       |                                           |                                           |
|                                  | 313             | -3.46                                       | 43.35                                     | 13.79                                    |
|                                  | 323             | -3.64                                       |                                           |                                           |
| 200                              | 303             | -4.07                                       |                                           |                                           |
|                                  | 313             | -4.29                                       | 63.28                                     | 17.82                                    |
|                                  | 323             | -4.53                                       |                                           |                                           |
3.6. Process Optimization

The quadratic model in the fraction factorial experimental design (FFED) is used to statistically optimize the adsorption capacity under response surface methodology (RSM) [40,41]. The general equation of model can be explained:

\[ Y = \beta_0 + \sum \beta_i X_i + \sum \beta_{ii} X_i^2 + \sum \beta_{ij} X_i X_j \]

where \( Y \) is the response variable, \( \beta_0 \) is the coefficient of regression, \( \beta_i \) is the linear influence, \( \beta_{ii} \) is the quadratic influence and \( \beta_{ij} \) is the variable \( X \) interaction influence. The Design expert (7.0.0), statistical software was used for the RSM study, and the graphical representation of 3D and contour plots can be achieved for the response obtained for independent variables with an effect. The quadratic regression equation derived from the analysis of variance (ANOVA) shows the possible individual and combined effect of the factors for the CV-NIFGS system (Table 4). The \( p \)-value < 0.05% was considered significant with a 95% confidence interval.

Table 4. CV-NIFGS ANOVA table.

| Sample | Summation of Squares | DoF | Square Mean | F-Value | \( p \)-Value |
|--------|----------------------|-----|-------------|---------|--------------|
| Model  | 13,547.2             | 1   | 13,547.2    | 103.2   | <0.0001      |
| A      | 113.6                | 1   | 113.6       | 0.9     | 0.3566       |
| B      | 717.6                | 1   | 717.6       | 5.5     | 0.0233       |
| C      | 1826.0               | 1   | 1826.0      | 13.9    | 0.0005       |
| D      | 10,862.6             | 1   | 10,862.6    | 82.7    | <0.0001      |
| E      | 878.9                | 1   | 878.9       | 6.7     | 0.0126       |
| AC     | 20.1                 | 1   | 20.1        | 0.2     | 0.6972       |
| BC     | 1323.5               | 1   | 1323.5      | 10.1    | 0.0025       |
| A\(^2\) | 736.5               | 1   | 736.5       | 4.8     | 0.0322       |
| B\(^2\) | 100.7               | 1   | 100.7       | 0.7     | 0.4218       |
| C\(^2\) | 223.0               | 1   | 223.0       | 1.4     | 0.2333       |
| D\(^2\) | 2437.6              | 1   | 2437.6      | 15.8    | 0.0002       |
| E\(^2\) | 494.3               | 1   | 494.3       | 3.2     | 0.0777       |
| Residual | 6695.6             | 51  | 131.3       |         |              |
| Lack of fit | 5782.9          | 49  | 118.0       | 0.3     | 0.9724       |
| Total  | 54,053.8            | 63  |             |         |              |

The regression equation obtained for CV-NIFGS system is shown below:

\[
\text{CV-NIFGS} = 36.14 + 28.10A - 3.52B + 19.15C - 21.21D62.29E + 11.92AC + 2.91BC + 12.54A2 + 12.54B2 - 35.16C2 + 10.77D2 + 20.80E2
\]

The values of the regression coefficient direct the parametric influence on the adsorption capacity. Surface and contour graphs illustrate the combined influence on adsorption by two factors. Graphical representation of the obtained results is in Figure 4. The fit of the second-order polynomial equation suggests A, C, D, AC and CE have maximum effects with the regression coefficient value of 0.978, which revealed the interaction of parameters studied and predicted adsorption capacity of 184 mg g\(^{-1}\) with the following optimum values based on a multiple regression analysis and the FFED model: pH 2, NIFGS dosage of 0.03 g L\(^{-1}\), 204 mg L\(^{-1}\) as initial dye concentration and 165 min as adsorption time. Based on these optimal values, the estimated adsorption capacity is 184 mg/g.
Figure 4. A 3D-surface plot and 2D-contour plot representing adsorption capacity variation relative to: (a) duration vs. temperature, (b) duration vs. concentration, (c) duration vs. adsorbent quantity and (d) duration vs. pH.
The effect of the interaction between two parameters and all other values are fixed and can be analysed by 3D response surface plots [42–47]. For example, the capacity increase in adsorption is noted at reduced pH grades and smaller NIFGS dosage. Significant effect on the dye adsorption was observed related to initial CV dye concentration. Similarly, adsorbent capacity to adsorb decreases with the increase in pH.

3.7. Mechanism of Adsorption

The adsorbate, NIFGS, is a cellulosic material. The processes of the adsorption of CV dye onto cellulosic NIFGS comprises cellulose, hemicellulose and lignin. All the three materials invariably contain –OH groups. The plausible mechanism of cationic CV dye adsorption is likely to take place as follows:

- The progression of adsorption is a multistep activity;
- The factors that have credible influence on the process of adsorption are the solution acidic level (pH), the concentration of dye, the amount of adsorbent used and variation in temperature;
- Monolayer is a formation initiated when the CV mass transfer occurs onto NIFGS;
- The process of diffusion is likely to be a slow process;
- The strong adherence of CV dye onto NIFGS is probably by bonds established between dye N\(^+\) anions and hydrogen of cellulosic –OH group;
- Weak interaction is due to Van der Waals forces of attraction and strong electrostatic forces of attraction is because the –N\(^+\) cationic group and the –OH\(^+\) group negative charge of NIFGS contribute substantially to the adherence of the dye onto NIFGS.

3.8. Optimized Condition

3.8.1. Studies on Composites

Preparation of CV Dye-Adsorbed NIFGS

At total of 100 g of commercial CV dye was transferred to a 100 L barrel. The dye was dissolved in 25 L of TIE. A total of 5 Kg of commercial NIFGS were transferred and the solution was stirred manually using a plastic rod. The solution was kept for about 24 h with occasional stirring. The dye-adsorbed NIFGS was separated using a cloth and the precipitate was washed thoroughly with distilled water until the filtrate was almost colourless. The blue colour dye-adsorbed NIFGS was air dried. The resultant powder containing lumps were grind and sieved through 177 \(\mu\)m mesh and dried in an oven at 60 °C for 24 h. The powder was cooled in a closed container with an airtight lid. CV dye-adsorbed NIFGS was referred to as dye-modified NIFGS powder (dmNIFGS).

Preparation of the Composites

The composites of high-density polyethylene/dye-modified nutraceutical industrial fenugreek seed spent (HDPE/dmNIFGS) were prepared in two stages; dry-blending of HDPE resin with different proportions of dmNIFGS in a tumble mixer and melt compounding of master batches. HDPE granules and/or recycled product and dmNIFGS master batch flakes were compounded using a twin-screw extruder. The specimens were prepared by cutting the extrudate strands into pellets and were tested for physico-mechanical and chemical properties. The results were encouraging. The details will be reported elsewhere.

4. Conclusions

The present research states the NIFGS implementation to amputate cations crystal violet dye from aqueous solution and textile industrial effluent. The observations made admit that NIFGS is an efficient, cost-effective and eco-friendly adsorbent. The experimental equilibrium \((q_e)\) values of 184.00 mg/g at pH value 2 and 82.00 mg/g at almost a neutral pH is quite encouraging to commercialize the process. Modelling analysis suggests the transfer of the dye from a bulk solution using NIFGS. The results categorise the process as physisorption compatible with the Langmuir isotherm. Adsorption followed the pseudo-second order model and reported as thermodynamically favourable. The process was
observed to be spontaneous and feasible which commemorates the endothermic nature. The value of $p < 0.001$ projects the significance of pH and the contact duration for efficient CV adsorption onto an adsorbent surface. The dye-modified NIFGS has potential as a reinforcing material for the fabrication of composites using plastic waste.

In brief, the study has relevance to three industrial sectors, namely: textile industries, nutraceutical industries and plastic industries. The industrial production has a linear model to create value in making the product and completes the life cycle with disposal after use. This model seriously affects the environment and ecology due to the unprecedented problem of resource depletion. To address the issue of resource depletion there is a need from the industries to shift from virgin inputs to recycled and/or reused products. This study is a step towards this goal.

**Author Contributions:** Conceptualization, S.N.T., M.E.M.S. and M.C.S.; Methodology, S.N.T., M.C.S. and B.A.K.; Investigation, S.N.T. and M.E.M.S.; Resources, S.N.T., M.C. and B.A.K.; Writing—original draft preparation, M.R.S. and M.S.G.; Writing—review and editing, I.B.K.; Review and editing, M.I.H.S., M.A.A. and Z.S.; Project Administration, M.R.S.; Supervision, M.R.S. and M.E.M.S.; Funding, M.A.E. and C.A.S.; Research Support, A.S.K.; Support, Review and Editing, A.E. All authors have read and agreed to the published version of the manuscript.

**Funding:** King Khalid University, Saudi Arabia, Research Group Program under grant no. RGP2/108/42. Taif University researchers supporting project number (TURSP-2020/123), Taif University, Taif, Saudi Arabia.

**Institutional Review Board Statement:** Not Applicable.

**Informed Consent Statement:** Not Applicable.

**Data Availability Statement:** Not Applicable.

**Acknowledgments:** The authors extend their appreciation to the Deanship of Scientific Research at King Khalid University, Saudi Arabia for funding this work through General Research Group Program under Grant No: RGP. 2/108/42. This work was supported by Taif University researchers supporting project number (TURSP-2020/123), Taif University, Taif, Saudi Arabia.

**Conflicts of Interest:** The authors declare no conflict of interest.

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