Passive observers for distributed port-Hamiltonian systems

Jesús Toledo ∗ Héctor Ramírez ∗∗ Yongxin Wu ∗
Yann Le Gorrec ∗

∗ FEMTO-ST, Univ. Bourgogne Franche-Comté, CNRS, Besançon, France, 24 rue Savary, F-25000 Besançon, France
** Department of Electronic Engineering, Universidad Técnica Federico Santa María, Avenida España 1680, Valparaíso, Chile

Abstract: The observer design for 1D boundary controlled infinite-dimensional systems is addressed using the port-Hamiltonian approach. The observer is defined by the same partial differential equations of the original system and the boundary conditions depend on the available information from sensors and actuators. The convergence of the observers is proved to be asymptotically or exponentially under some conditions. The vibrating string and the Timoshenko beam are used to illustrate the observer convergence in different scenarios.

Keywords: Observer design, port-Hamiltonian distributed parameter systems.

1. INTRODUCTION
An observer is a dynamical system which takes all the information available from sensors and actuators and uses the model to reconstruct the state of the system of interest (Luenberger, 1964). For systems governed by Ordinary Differential Equations (ODEs) (or Lumped Parameter Systems (LPSs)), the observer problem has been intensively investigated especially for linear systems. Nevertheless, for systems governed by Partial Differential Equations (PDEs) (or Distributed Parameter Systems (DPSs)), the observer design is more complex and it has drawn the attention of the researchers in recent years (Hidayat et al., 2011).

A natural observer is presented for LPSs and DPSs in (Demetriou, 2004), where for mechanical systems, the estimated velocity is the time derivative of the estimated position for all time. In (Deguenon et al., 2006) is introduced a simple observer for elastic systems, while in (Smyshlyaev and Krstic, 2005; Meurer, 2013) are given observers for a class of parabolic systems, where the backstepping strategy is used for the design. On the other hand, in (Castillo et al., 2013) it is presented an observer for hyperbolic systems with dynamic controllers for flow control applications. In this work, we try to group all these observer in the so-called class distributed boundary port-Hamiltonian (pH) systems.

In the last years, the pH approach has proven to be well-suited for modeling and control of DPSs, and more specifically for Boundary Control Systems (BCSs) (Fattorini, 1968). The well-posedness was developed using semigroup theory in (Le Gorrec et al., 2005), while the stability and control analysis was well developed in (Villegas, 2007; Augner and Jacob, 2014; Ramírez et al., 2014; Villegas et al., 2009; Macchelli, 2013). Nevertheless, pH observers have still not been developed for BCSs. In this note, taking the already results mentioned above and exponential stability, different observers are presented, depending on the available measurement. Several controllers for BCSs (Guo and Xu, 2007; Guo and Guo, 2009; Krstic et al., 2008) have been developed using infinite-dimensional observers (Deguenon et al., 2006; Demetriou, 2004). The main idea of this work is to cast all these observers into one general class under the pH framework.

The paper is organized as follows: a brief background on distributed pH systems is presented in Section 2, then in Section 3 is introduced the main problem of this paper. Section 4 shows the convergence conditions for the observer when the sensors are co-energy variables. Section 5 shows a more complex observer, where the sensors are not co-energy variables anymore. Section 6 shows the Timoshenko beam example, while along the paper the string equation is used to exemplify the observer design. Finally, Section 7 shows some conclusions of this work.

In this paper, $M_p(\mathbb{R})$ denotes the space of $n \times n$ square matrices whose entries lie in the space $\mathbb{R}$ and $I$ denotes the identity matrix of appropriate dimension. By $(\cdot, \cdot)$_2 or only $(\cdot, \cdot)$ we denote the standard inner product on $L_2([a,b]; \mathbb{R}^n)$ and the Sobolev space of order $p$ is denoted by $H^p([a,b], \mathbb{R}^n)$.

2. DISTRIBUTED PORT-HAMILTONIAN SYSTEMS
The class of BCSs that we consider in this paper has the form

$$\begin{align}
\frac{\partial x}{\partial t} & = P_1 \frac{\partial}{\partial \zeta} (Hx(\zeta,t)) + P_0 (Hy(\zeta,t)), \\
W_S(\tilde{z}_0(t)) & = u(t), \\
y(t) & = W_C(\tilde{z}_0(t)), \quad y_m(t) = C_y(t)
\end{align}$$

where $x(\zeta,t) \in \mathbb{R}^n$ is the state variable defined for all $t \geq 0$ and $\zeta \in [a,b]$ with initial condition $x(\zeta,0) = x_0(\zeta)$, $u(t) \in \mathbb{R}^n$ is the input, $y(t) \in \mathbb{R}^n$ is the output and $y_m(t) \in \mathbb{R}^p$ is the measured part of the output $y(t)$. $P_1 =$
$P_1^\top \in \mathbb{R}^{n \times n}$ is a non-singular matrix, $P_0 = -P_0^\top \in \mathbb{R}^{n \times n}$, $\mathcal{H}(\cdot) = M_0(L_2([a, b]))$ is a bounded and continuously differentiable matrix-valued function satisfying for all $\zeta \in [a, b]$, $\mathcal{H}(\zeta) = \mathcal{H}^\top(\zeta)$ and $mI < \mathcal{H}(\zeta) < MI$ with $M > m > 0$ both scalars independent on $\zeta \in \mathbb{R}^{p \times n}$ is a constant matrix of rank $p$ with $p \leq n$. The state space is $X = L_2([a, b]; \mathbb{R}^n)$ and let its inner product $(x_1, x_2)_{\mathcal{H}} = \langle x_1, x_2 \rangle_{\mathcal{H}}$, and norm $\|x\|_{\mathcal{H}} = \langle x, x \rangle_{\mathcal{H}}$ which is related with the Hamiltonian as $H(t) = \frac{1}{2} \|x(t)\|^2_{\mathcal{H}}$. Since $X$ is a Hilbert space and the norm $\| \cdot \|_{\mathcal{H}}$ is proportional to the stored energy of the system, hence $x(t)$ is called energy variable and $\mathcal{H}(\cdot)x(\cdot, t)$ is called co-energy variable. For simplicity, sometimes we write $x$ and $\mathcal{H}x$ instead of $x(\cdot, t)$ and $\mathcal{H}(\cdot)x(\cdot, t)$.

Then, for $W_c$ defined by

$$W_c(t) = \begin{pmatrix} f_\partial(x) \\ u_\partial \end{pmatrix}$$

and $u_\partial \in \mathbb{R}^n$, the system (1) with input (2) is a BCS system if and only if $\mathcal{H}(\cdot)x(\cdot, t)$ is a bounded and continuously differentiable function of $t$ in $\mathbb{R}$, and $W_c(t)$ is an $\mathbb{R}^n$-vector.

**Example 4.** The one-dimensional (1D) string, clamped at one side and controlled with a force actuator at the other side can be written in the force representation (1) with matrices

$$P_1 = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}, \quad P_0 = 0, \quad \mathcal{H}(\zeta) = \begin{bmatrix} E(\zeta) & 0 \\ 0 & \rho(\zeta)^{-1} \end{bmatrix},$$

where $E(\zeta)$ and $\rho(\zeta)$ are the Young's modulus and the mass density, respectively. The system variables are

$$x(\zeta, t) = \begin{bmatrix} q(\zeta, t) \\ p(\zeta, t) \end{bmatrix} := \begin{bmatrix} \frac{\partial q}{\partial \zeta}(\zeta, t) \\ \rho(\zeta)^{-1} \frac{\partial p}{\partial \zeta}(\zeta, t) \end{bmatrix},$$

where $w(\zeta, t)$ is the deformation of the string defined for $\zeta \in [a, b]$ and $t \geq 0$. The boundary port variables are

$$\left( f_\partial(t) \right) = \frac{1}{\sqrt{2}} \begin{bmatrix} \rho(a,b)(a(t) - \rho(a,b)(a(t)) \\ E(b)q(b, t) - E(a)q(a, t) \\ E(b)q(b, t) + E(a)q(a, t) \end{bmatrix},$$

The input and output matrices can be chosen as

$$W_c = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \quad W_c = \frac{1}{\sqrt{2}} \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}$$

which gives input and output variables

$$u(t) = \begin{bmatrix} \frac{\partial q}{\partial \zeta}(a, t) \\ \frac{\partial p}{\partial \zeta}(a, t) \end{bmatrix}, \quad y(t) = \begin{bmatrix} -T(a)q(a, t) \\ T(a)q(a, t) \end{bmatrix}.$$
Remark 5. Note that $\tilde{H}(t) \neq H(t) - H(t)$. Where $H(t)$ is the Hamiltonian of the plant and $\tilde{H}(t)$ is the estimated Hamiltonian.

4. PASSIVE OBSERVER DESIGN

Choosing the observer input $\hat{u}(t)$ as in the classical Luenberger observer formulation, i.e. the input of the plant $u(t)$ plus an error injection from the measurement, we obtain $\hat{u}(t) = u(t) + L(y_m(t) - \tilde{y}(t)) = u(t) + LC\tilde{y}(t)$ then,

$$\tilde{u}(t) = -LC\tilde{y}(t) \tag{5}$$

where $L \in \mathbb{R}^{n \times p}$ is a matrix to design. Note that this is exactly the classical damping injection ensuring that the error system (4) converges to zero asymptotically. Now, the error system is described by

$$\begin{aligned}
\dot{\tilde{x}}(\zeta, t) &= P_1 \frac{\partial}{\partial \zeta}(H\tilde{x}(\zeta, t)) + P_0(H\tilde{x}(\zeta, t)), \\
W_L(\tilde{y}_a(t), \tilde{e}_o(t)) &= 0,
\end{aligned} \tag{6}$$

where $W_L = WK_L$. \tag{7}

It is possible to prove that $W_L^TW_L = LC + (LC)^T$, which implies, by Theorem 2, that the error system (4) with $\tilde{u}(t) = L\tilde{y}(t)$ is a boundary control system since $LC$ is positive semi-definite, i.e. $LC \geq 0$. See (Villegas, 2007).

In the following we present two different scenarios: the first one is the ideal case, corresponding to full sensing of (1), i.e. $p = n$ and $C = I$ which implies $y_m(t) = y(t)$; the second one is that when not all the output $n$ is available, i.e. $p < n$ and $y_m(t) = Cy(t)$ with $C \in \mathbb{R}^{p \times n}$. In both scenarios, we give the conditions such that the asymptotic or exponential convergence of the observer is ensured.

4.1 Full sensing: $p = n$

In this case, $L$ is a square matrix of size $n$ and $C$ is the identity. The following theorem ensures the asymptotic convergence of the error system.

**Theorem 6.** Consider the BCS (6) from (4) and (5). The energy $\tilde{H}(t)$ is such that for all $t \geq 0$ it satisfies $\frac{d}{dt}||\tilde{x}(t)|| = -\langle L\tilde{y}(t), \tilde{y}(t) \rangle$ and $L \in \mathbb{R}^{n \times n}$. If the matrix $W_L$ defined in (7) satisfies $W_L^TW_L > 0$, or equivalently $L > 0$, the system converge to zero asymptotically.

**Proof.** The proof is a direct application of Theorem 5.1 of (Villegas, 2007, chapter 5).

**Example 7.** Following Example 4, now we design the observer for the string using Theorem 6. Note that in this scenario we have full sensing. Consider $L = \text{diag}([l_1, l_2])$, which gives

$$W_L = \frac{1}{\sqrt{2}} \begin{bmatrix} -1 & -1 \\ l_1 & 1 \\ l_2 & 1 \end{bmatrix}, \quad W_L^TW_L = \begin{bmatrix} 2l_1 & 0 \\ 0 & 2l_2 \end{bmatrix}.$$ 

Then, the error system converges asymptotically to zero for all $l_1 > 0$ and $l_2 > 0$, i.e., $\tilde{x}(\zeta, t) \to x(\zeta, t)$ as $t \to \infty$.

4.2 Partial sensing: $p < n$

In this case, the matrix $L$ is not anymore a square matrix and we can not apply anymore Theorem 6. Yet the follow Corollary 8 from (Villegas, 2007) can be rewritten in order to prove the convergence of the error system (6).

**Corollary 8.** (Villegas, 2007). Consider the BCS in (6) as described in Theorem 2 and assume that the energy of the system is such that for all $t \geq 0$ satisfy

$$\frac{1}{2} \frac{d}{dt}||\tilde{x}(t)||^2 = -\langle LC\tilde{y}(t), \tilde{y}(t) \rangle$$

where $LC$ is a positive semi-definite matrix, i.e. $LC \geq 0$. If either

$$||H\tilde{x}(b, t)||^2 \leq k_1 ||LC\tilde{y}(t), \tilde{y}(t)||$$

or

$$||H\tilde{x}(a, t)||^2 \leq k_1 ||LC\tilde{y}(t), \tilde{y}(t)||$$

for some positive constant $k_1$, then the system is exponentially stable.

**Proof.** The proof is a direct application of Corollary 5.19 of (Villegas, 2007, chapter 5).

Note that the result of the Corollary 8 is stronger than the one of Theorem 6 in terms of convergence even if we use more restrictive conditions/assumptions for the sensing (partial sensing). It is mainly due to the conservatism of the result state in Theorem 6. The conditions (8) are less conservative but may be more difficult to check.

**Example 9.** Following Examples 4 and 7, but now considering that we can only measure the strain at the left side of the string, i.e. $y_m = -T(a)q(a, t) \Rightarrow C = [1 \ 0]$ and $L = [l_1 \ l_2]^T$. We obtain the

$$W_L = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 & l_1 & -l_1 & 1 \\ 0 & l_2 & 1 - l_2 & 0 \end{bmatrix}, \quad W_L^TW_L = \begin{bmatrix} 2l_1 & l_2 \\ l_2 & 0 \end{bmatrix}.$$ 

where $W_L^TW_L \geq 0$ is equivalent to have $l_2 = 0$ and $l_1 \geq 0$ which is a sufficient condition to prove existence of solutions of the PDE. Now, we need to prove one of the conditions in (8). Considering $l_2 = 0$, we obtain $\langle LC\tilde{y}, \tilde{y} \rangle = l_1(T(a)\tilde{q}(a, t))^2$, $\langle Hq(a, t) \rangle^2 = (T(a)\tilde{q}(a, t))^2 + \left(\frac{1}{m}p(a, t)\right)^2 = (l_1 + 1)(T(a)\tilde{q}(a, t))^2$ in which, choosing $k_1 > l_1^2 + 1$, the conditions (8) $||H\tilde{x}(a, t)||^2 \leq k_1 ||LC\tilde{y}(t), \tilde{y}(t)||$ is satisfied.

5. PASSIVE OBSERVERS WITH DYNAMIC EXTENSION

We consider now the case where the sensors do not measure co-energy variables as in (1). This is the case for example of mechanical systems like waves or beams, where we can not measure the strain or velocity at the boundaries, but only displacement (laser sensor for example). In order to estimate the state of the system one has to add an integrator at the boundaries. Then, the global system is a mix between PDEs and ODEs which are interconnected through the spatial boundaries of the PDEs, where the ODEs are added to the observer to ensure the convergence of the observer. So, consider now that $u(t)$ from system (4) can be designed from a set of ODEs as Fig. 1 shows, where the block $C$ is given by

$$\begin{aligned}
C \begin{bmatrix} x_a(t) \\ y_a(t) \end{bmatrix} &= A_xx_a(t) + B_ux_u(t), \\
C \begin{bmatrix} x_e(t) \\ y_e(t) \end{bmatrix} &= C_xx_e(t) + D_xx_e(t),
\end{aligned} \tag{9}$$

where $x_c \in \mathbb{R}^{n-c}$ and $u_c \in \mathbb{R}^n$, $A_c \in \mathbb{R}^{n_c \times n_c}$, $B_c \in \mathbb{R}^{n_c \times n_u}$, $C_c \in \mathbb{R}^{n \times n_c}$ and $D_c \in \mathbb{R}^{n \times n_u}$ such that $A_c = (J_c - R_c)Q_c$, $B_c = G_c - P_c$, $C_c = (G_c + P_c)^TQ_c$ and $D_c = M_c + S_c$, where $J_c = -J_c^T$, $R_c = R_c^T$, $M_c = M_c^T$ and $S_c = S_c^T$, with these further condition satisfied:

$$\begin{bmatrix} R_c \\ P_c \end{bmatrix} \geq 0 \quad \text{and} \quad Q_c = Q_c^T > 0.$$
The closed-loop system can be characterized by the total Hamiltonian
\[ H_{cl}(\tilde{x}(t), x_c(t)) = \frac{1}{2} \| \tilde{x}(t) \|_H^2 + \frac{1}{2} x_c^T(t)Q_c x_c(t) \] (11)
and it can be compactly written as
\[ \begin{align*}
\dot{\tilde{x}} &= A_{cl} \tilde{x} \\
0 &= (B + D_c C_c) \tilde{x} := B_{cl} \tilde{x}
\end{align*} \] (12)
where
\[ \tilde{x} = (\tilde{x}^T \ x_c^T) \in Z := X \times \mathbb{R}^{n_c} \]
is the state variable of the new augmented system and \( A_{cl} : D(A_{cl}) \subset Z \rightarrow Z \) is the following linear operator
\[ A_{cl} \left( \begin{array}{c} \tilde{x} \\ x_c \end{array} \right) := \left( \begin{array}{cc} A & 0 \\ B_c C_c & A_c \end{array} \right) \left( \begin{array}{c} \tilde{x} \\ x_c \end{array} \right) \] (13)
with domain
\[ D(A_{cl}) = \left\{ \tilde{x} \in Z \mid \tilde{x} \in D(A), \ B_{cl} \tilde{x} = 0 \right\}. \] (14)

**Proposition 10.** Consider the infinite dimensional pH system (4) interconnected with the finite dimensional pH system (9) through the passive interconnection (10) as in Fig. 1. The augmented system (12) with \( A_{cl} \) defined in (13) with domain (14) is a BCS and the operator \( A_{cl} \) generates a contraction semigroup.

**Proof.** The proof is a direct application of Proposition 1 in (Macchelli, 2013).

In what follows we give two conditions that have to satisfy the observer in order to asymptotically or exponentially reconstruct the state of the system (1). Before that, we call these two technical Lemma and Corollary

**Lemma 11.** (Lefschetz-Kalman-Yakubovich) [More details in (Tao and Ioannou, 1988)]. Assume for the system (9) that \( A_c, B_c \) is controllable and \( A_c, C_c \) is observable. Then, the transfer matrix \( G_c(s) = C_c(sI - A_c)^{-1}B_c + D_c \) is Strictly Positive Real (SPR) if and only if there exist real matrices \( P = \begin{bmatrix} P & \hline \tilde{P} \end{bmatrix} < 0, \ L, W \) and a scalar \( \varepsilon > 0 \) such that
\[ PA_c + A_c^T P = -L^T L - \varepsilon P \] (15a)
\[ C_c - B_c^T P = W^T L \] (15b)
\[ D + D^T = W^T W \] (15c)

**Corollary 12.** The system (9) with \( A_c \equiv (J_c - R_c)Q_c, \ C_c = B_c^T Q_c \) and \( D_c = 0 \) is SPR if \( J_c = -J_c^T, \ R_c = R_c^T > 0 \) and \( Q_c = Q_c^T > 0 \).

**Proof.** From Lemma 11, choose \( P = Q_c \) and \( W = 0 \), then (15c) is trivial, (15b) is \( C_c = B_c^T Q_c \) and (15a) becomes \( L^T L = 2Q_c R_c Q_c - \varepsilon Q_c \), then for \( R_c > 0 \) there exists a constant \( \varepsilon > 0 \) such that the matrix \( 2Q_c R_c - \varepsilon Q_c \) is positive definite, giving a solution for \( L \), using for instance Cholesky factorization.

The following theorem ensures the asymptotic convergence of the observer

**Theorem 13.** Consider the system (4) with \( \tilde{u}(t) \) and \( \tilde{y}(t) \) defined according to Theorem 2 such that is an impedance energy preserving system (Definition 3). Consider also a finite dimensional system \( C \) (Fig. 1) such that its transfer matrix between \( y_c \) and \( u_c \) is SPR. Then, with the passive interconnection (10) the error system (4) is well-posed and converges asymptotically to zero.

**Proof.** The proof is a direct application of Theorems 5.8, 5.9 and 5.10 in (Villegas, 2007, chapter 5).
then the total energy (11) of the closed-loop system satisfies for $\tau$ large enough

$$\dot{H}_d \leq c(\tau) \int_0^\tau \|H(b)\dot{x}(b,t)\| \text{ and } $$

$$\dot{H}_d \leq c(\tau) \int_0^\tau \|H(b)\dot{a}(a,t)\|$$

where $c$ is a positive constant that depends on $\tau$.

**Proof.** The proof is a direct application of Proposition 3 in (Macchelli, 2013).

**Remark 16.** Condition (16) is not restrictive and it is natural in an scenario where we need to estimated the state, i.e. $\dot{x}(\zeta,t) \neq 0$, $x(\zeta,t) \neq \dot{x}(\zeta,t)$ or the error energy is different from zero.

**Proposition 17.** Under the hypothesis of Proposition 15 if

$$\dot{H}_d \leq -k_1\|H(b)\dot{x}(b,t)\|^2 \text{ or }$$

$$\dot{H}_d \leq -k_1\|H(a)\dot{a}(a,t)\|^2$$

for some $k_1 > 0$, then the error state $\dot{x}(\zeta,t)$ from system (4) converges exponentially to zero.

**Proof.** The proof is a direct application of Proposition 4 in (Macchelli, 2013).

**Example 18.** Consider now, the same as in Example 9, where we only can measure the strain at $a$, i.e. $y_m(t) = T_{1}^0q(a,t)$. The following observer estimates exponentially the state variables $q(\zeta,t)$ and $p(\zeta,t)$.

$$\begin{cases}
\frac{\partial}{\partial t} \left( \begin{array}{c} \dot{q} \\ \dot{p} \end{array} \right)(\zeta,t) = 
\left( \begin{array}{c} 0 \\ 1 \end{array} \right) \frac{\partial}{\partial \zeta} \left( \begin{array}{c} T \dot{q} \\ \frac{1}{\rho} \ddot{p} \end{array} \right)(\zeta,t) \\
T(a)\dot{q}(a,t) + \alpha \frac{1}{\rho(a)} \dot{p}(a,t) + \beta \dot{w}(a,t) + T(a)q(a,t) \\
T(b)\dot{q}(b,t) = u(t).
\end{cases}$$

Following Proposition 10 the error system is well-posed. Take as matrices $R_c = 0$, $R_0 = 0$, $Q_c = \beta$, $P_c = 0$, $G_c = 1$, $M_c = 0$ and $S_c = \alpha$. Take as variables $x_c(t) = -\dot{w}(a,t)$, $u_c(t) = -\frac{1}{\rho(a)} \dot{p}(a,t)$ and thus $y_c(t) = -\alpha \frac{1}{\rho(a)} \dot{p}(a,t) - \beta \dot{w}(a,t)$. Note that

$$\begin{pmatrix}
R_c & P_c \\
P_c^T & S_c
\end{pmatrix} = \begin{pmatrix}
0 & 0 \\
0 & \alpha
\end{pmatrix} \geq 0, \forall \alpha \geq 0.$$
through the boundaries with the system (9) using the interconnection (10) with \( J_e = 0, R_c = diag(l_{12}^{-1}, l_{12}^{-1}), Q_e = diag(l_{1}, l_{2}), B_c = (0_{2}, 2)\), \( C_c = B_l^T Q_l\) and \( D_c = 0\). Then, using the Corollary 12 the dynamic block is an SPR system for \( l_{1}, l_{2} > 0\). Now, using Theorem 13 the asymptotic convergence is ensured. Simulations are done for \( a = 0, b = 1\), \( T(\zeta) = \rho(\zeta) = EI(\zeta) = I_p(\zeta) = 1\) and \( u(t) = 0\) with initial conditions \( x_1(\zeta, 0) = 1, x_2(\zeta, 0) = 0,\) \( x_3(\zeta, 0) = b - \zeta\) and \( x_4(\zeta, 0) = 0\), while for the observer the initial conditions are all zero. The spatial discretization method used is the one given by (Trenchant et al., 2017), where an staggered grids finite difference allows to preserve the pH structure on the finite-dimensional system. On the other hand, the midpoint method is used for the time discretization using an step time \( dt = 0.1ms\). Fig. 2 shows the results of the simulation for an space discretization of 40 elements per state variable. Note that even for a smaller discretization (10 elements per state variable) the deformation curve of the observer (Fig. 2 (d)) converge to the real one (Fig. 2 (a)).

Fig. 2. (a): beam deformation, (b): observed beam deformation, (c): deformation error, (d): observed beam deformation for a low order observer.

7. CONCLUSIONS

Different observers have been addressed for infinite dimensional systems using the pH approach. Under some conditions the asymptotic or exponential convergence of the observer is ensured. The simplest case is when the sensor are co-energy variables like forces and velocities for mechanical systems. But, even in the case when this is not possible for example when the sensors are displacement variables, the convergence of the observer is guaranteed. A perspective of this work is the implementation of these observers in together with control action like damping injection, energy shaping, among others.

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