Maximum velocity of a fluxon in a stack of coupled Josephson junctions

E. Goldobin
Institute of Thin Film and Ion Technology, Research Center Jülich GmbH (FZJ), D-52425, Jülich, Germany
B. A. Malomed
Department of Interdisciplinary Studies, Faculty of Engineering, Tel Aviv University, Tel Aviv 69978, Israel
A. V. Ustinov
Physikalisches Institut III, Universität Erlangen-Nürnberg, D-91058, Erlangen, Germany

I. INTRODUCTION

Experimental and theoretical studies of magnetic flux quanta (fluxons) in stacks of inductively coupled long Josephson junctions (LJJ’s) have recently attracted a great deal of attention. The interest to the stacks is stimulated both by the fact that the high-$T_c$ superconductors, on the atomic level, have a naturally layered structure that is tantamount to an intrinsic Josephson stack and by the development of the (Nb-Al-AlO$_x$)$_N$-Nb low-$T_c$ technology which is demonstrated fabrication of artificial stacks of up to 28 LJJ’s, with a parameter spread between them < 10%. A fundamental characteristic of a single LJJ is its Swihart velocity $c_0$, i.e., a minimum phase velocity of the electromagnetic (Josephson plasma) waves propagating in the superconducting micro-strip structure. Simultaneously, $c_0$ is the maximum velocity for fluxons that correspond to topological solitons of the sine-Gordon model describing LJJ. In a system of $N$ linearly coupled junctions, the dispersion curve has $N$ branches corresponding to different modes of the linear electromagnetic waves propagating in the system. Accordingly, there are $N$ split (different) Swihart velocities $c_n^{(N)}$, $n = 1, 2, \ldots, N$ (see, Refs. [13]), such that $c_n^{(N)} < c_{n+1}^{(N)}$. For example, in the simplest case of two coupled junctions, there are two Swihart velocities $c_1^{(2)}$ and $c_2^{(2)}$ which correspond, respectively, to the system’s in-phase and out-of-phase Josephson plasma wave eigenmodes. In the $N$-fold stack, we also use notation $\bar{c}_- \equiv c_1^{(N)}$ and $\bar{c}_+ \equiv c_N^{(N)}$, which are the smallest and largest Swihart velocities.

An important issue is to study the conditions for the existence and stability of a single-fluxon state in the stacked system. It is implied that the fluxon is trapped in one junction and its screening currents spread over neighboring junctions. The fluxon induces, through the magnetic coupling, “images” in adjacent layers, so that a full solution for the single fluxon state in the stack includes both the core topological soliton in the central layer and its non-topological junctions. The exact value of $u_{\text{max}}$ has not been found until now.

We will discuss three cases which differ by the number $N$ of the coupled LJJ’s. These cases are $N = 2$, $N = 3$, and $\infty$. For $N = 2$ and $N = 3$ we will consider a system of asymmetric LJJ’s with different critical currents $j_e$, in which...
the maximum velocity is different depending on where the fluxon is trapped. In the case $N = 3$ and $N = \infty$ we will assume that the core topological soliton is placed in the central junction which will be labeled by 0, while LJJ’s above and below the central one will be labeled by 1, 2, . . . , $\infty$ and $−1, −2, . . . , −\infty$, respectively.

In section II we formulate the model, section III displays results of full PDE numerical simulations of the asymmetric model for the cases $N = 2$ and $N = 3$. To choose an analytical form for the fitting function which predicts the dependence $u_{\text{max}}$ on junction parameters, in section IV we use the variational approximation (VA). Although VA does not produce very accurate quantitative results, it predicts reasonable functional dependence for $u_{\text{max}}$. Section V concludes the work and summarizes the obtained results for different $N$.

II. THE MODEL

A model for $N$-fold stack of long Josephson junctions is well known.\[1\]

$$(\phi_n)_{xx} = (\phi_n)_{tt} + \sin \phi_n + \gamma + \alpha(\phi_n)_t$$

$$−S[(\phi_{n-1})_{tt} + \sin \phi_{n-1} + \alpha(\phi_{n-1})_t + (\phi_{n+1})_{tt} + \sin \phi_{n+1} + \alpha(\phi_{n+1})_t + 2\gamma]$$,

(1)

where $\phi_n$ is the Josephson phase across the $n$-th LJJ, $n = −N/2 \ldots N/2$, the coordinate $x$ and time $t$ are measured in units of the Josephson length $\lambda_J$ and inverse plasma frequency $\omega_p^{-1}$ of single-layer LJJ, $S < 0$ is a dimensionless coupling parameter, $\alpha$ is a dissipative constant, and $\gamma$ is the density of the bias current flowing through the stack. We consider the most natural case when the bias current is the same in all layers.

The model pertains to a stack consisting of an infinite number of junctions, or to an exotic configuration, in which the stack is closed in a loop in $z$ direction ($\phi_{N+1} \equiv \phi_1$). In practice, the equations for the edge (top and bottom) junctions include only a half of the coupling terms corresponding to the neighboring LJJ’s. Note also that the model implies that all the junctions are identical. In particular, the Swihart velocity of each uncoupled LJJ, is $c_0 \equiv 1$ in the notation adopted hereafter.

In the case of $N = 2$, a relevant version of the model, which takes into account the difference in the critical currents of the LJJ’s, writes as\[1]

$$(\phi_0)_{xx} - (\phi_0)_{tt} - \sin \phi_0 - S(\phi_0)_{xx} = \alpha(\phi_0)_t + \gamma;$$

(2)

$$(\phi_1)_{xx} - (\phi_1)_{tt} - \sin \phi_1 - S(\phi_0)_{xx} = \alpha(\phi_1)_t + \gamma,$$

(3)

where $J = j_{0}/j_{1}$ is the ratio of the critical currents of the two junctions. When considering the model and below, we will place the fluxon into the LJJ whose phase is denoted as $\phi_0$.

Discussing the case of $N = 3$, we impose the symmetry condition $\phi_1 \equiv \phi_{−1}$, which is natural when the fluxon moves in the middle layer. Thus, we can write Eqs. \[1\] in the form

$$\frac{1}{1−S^2}(\phi_1)_{xx} - (\phi_1)_{tt} - \sin \phi_1 - S(\phi_0)_{xx} = \gamma - \alpha(\phi_1)_t;$$

(4)

$$\frac{1}{1−S^2}(\phi_0)_{xx} - (\phi_0)_{tt} - \sin \phi_0 - \frac{2S}{1−S^2}(\phi_1)_{xx} = \gamma − \alpha(\phi_0)_t.$$  

(5)

Note the factor of 2 in the last term of the left-hand side of Eq. \[1\].

For further theoretical treatment of the case $N = \infty$, we will assume that the coupling parameter $S$ is small. This assumption will allow us to write a Lagrangian corresponding to the dynamical equations \[1\], which is a key ingredient of VA. In the case of small $S$, neglecting terms $\sim S^2$ and smaller, one can easily transform Eqs. \[1\] into a simplified form:

$$(\phi_n)_{xx} - (\phi_n)_{tt} - \sin \phi_n - S[(\phi_{n-1})_{xx} + (\phi_{n+1})_{xx}] = \alpha(\phi_n)_t - \gamma,$$

(6)

which we will use for further analysis of the $N = \infty$ case.

A fluxon steadily moving at a constant velocity $u$ can be described by a solution to the above equations (without the $\alpha$ and $\gamma$ terms) which depends on the single variable $\xi = C(x − ut)$. The constant $C$ is introduced for renormalization purposes and will be different in the cases $N = 2, 3,$ and $\infty$. Substituting

$$\xi \equiv x − ut$$

(7)
into Eqs. (3) and (4) and neglecting the $\alpha$ and $\gamma$ terms (which must be kept if one aims to find an equilibrium velocity determined by the balance between the losses and bias current, that is not our objective in this work), we get:

$$\sigma^{(2)} \phi''_0 + \phi''_1 - \sin \phi_0 = 0, \quad (8)$$
$$\sigma^{(2)} \phi''_1 + \phi''_0 - \frac{\sin \phi_1}{f} = 0. \quad (9)$$

The parameter $\sigma^{(2)}$ (the subscript 2 implies that the definition is adjusted to the case $N = 2$), that will be used instead of the velocity, is defined as:

$$\sigma^{(2)} \equiv 1 - \frac{(1 - S^2) u^2}{-S} \quad (10).$$

For the 3-fold stack, introduction of the traveling coordinate

$$\xi \equiv \sqrt{\frac{1 - 2 S^2}{-S}} (x - ut) \quad (11)$$
transforms Eqs. (3) and (4) into

$$\sigma^{(3)} \phi''_1 + \phi''_0 - \frac{\sin \phi_1}{f} = 0, \quad (12)$$
$$\sigma^{(3)} \phi''_0 + 2 \phi''_1 - \sin \phi_0 = 0, \quad (13)$$

where

$$\sigma^{(3)} \equiv 1 - \frac{(1 - 2 S^2) u^2}{-S} \quad (14).$$

And, finally, for the case $N = \infty$ the substitution of

$$\xi \equiv (x - ut)/\sqrt{-S} \quad (15)$$
into Eqs. (5) yields

$$\sigma^{(\infty)} \phi''_n + \phi''_{n-1} + \phi''_{n+1} - \sin \phi_n = 0, \quad (16)$$

where

$$\sigma^{(\infty)} \equiv 1 - \frac{u^2}{-S}. \quad (17)$$

Thus, from the mathematical viewpoint, the issue is to look for solutions of Eqs. (5) and (6), or (12) and (13), or of Eqs. (16) that describe the stationary fluxon. The eventual objective is finding the maximum velocity $u_{\text{max}}$, or the minimum value of the parameter $\sigma$, beyond which the fluxon solution does not exist. The fluxon solution is defined by the following boundary conditions: $\phi_0(-\infty) = 0$, $\phi_0(+\infty) = 2\pi$, and $\phi_n \neq 0 (\pm \infty) = 0$.

To conclude this section, we recall that the set of the split Swihart velocities can be found in an exact form from the linearized version of Eqs. (1), setting there $\gamma = \alpha = 0$. These velocities are given by the following expression:

$$c_n^{(N)} = \frac{1}{\sqrt{1 - 2 S \cos \left( \frac{\pi n}{N + 1} \right)}}, \quad n = 1, 2, \ldots, N. \quad (18)$$

It is also useful to find the values of the parameter $\sigma$ corresponding to the minimum velocity $\bar{c}_-$ and the maximum velocity among all the velocities given by Eq. (18). From Eqs. (10), (14) and (17), using Eq. (18), we find

$$\sigma^{(2)}(\bar{c}_\pm) = \mp 1, \quad (19)$$
$$\sigma^{(3)}(\bar{c}_\pm) = \mp \sqrt{2}, \quad (20)$$
$$\sigma^{(\infty)}(\bar{c}_\pm) = \mp 2. \quad (21)$$
while zero velocity corresponds to \( \sigma^{(2,3,\infty)} = -1/S \).

We can immediately find the values of \( \sigma_{\text{min}} \) for some specially selected values of \( J \). Let us set \( \sigma^{(2)} = 1 \) in Eqs. (8) and (9). This reduces Eqs. (8) and (9) to a simple algebraic equation:

\[
\sin \phi_0 = \frac{\sin \phi_1}{J}.
\]

The state with a fluxon only in the first junction (\( \phi_1 \)) can be realized only for \( J < 1 \). This means that

\[
\sigma_{\text{min}}^{(2)} (J = 1) = 1.
\]

In the same fashion, setting \( \sigma^{(3)} = \sqrt{2} \) in Eqs. (12) and (13), we get

\[
\sin \phi_0 = \frac{\sqrt{2}}{J} \sin \phi_1.
\]

This means that

\[
\sigma_{\text{min}}^{(3)} (J = \sqrt{2}) = \sqrt{2}.
\]

A similar relation can be obtained for any \( N \)-fold stack. Using Eqs. (14), we get the following result. The value \( \sigma_{\text{min}}^{(2N-1)} \) in the stack consisting of \( 2N-1 \) LJJ’s is given by the maximum eigenvalue of the \( N \times N \) matrix,

\[
\begin{pmatrix}
0 & -1 & & & \\
-1 & 0 & -1 & & \\
& \ddots & \ddots & \ddots & \\
& & -1 & 0 & -1 \\
& & & -2 & 0
\end{pmatrix}.
\]

This matrix has the size \( N \times N \) due to the symmetry which, as we suppose, is present when the fluxon moves in the middle layer. In this case \( 2N-1 \) coupled equations can be reduced to \( N \) equations in the same way as we reduced 3 equations for \( N = 3 \) to only 2 independent equations. As a result of this reduction, the \( N \)-th equation, which describes the junction containing the fluxon and corresponds to the last row of matrix (24), contains the factor of 2.

The values of \( \sigma_{\text{min}} \) calculated for some \( N \) are summarized in Table I. One can see that as \( N \to \infty \), \( \sigma_{\text{min}} \to 2 \). Similar to the above considerations, the single-fluxon state exists only if \( J < \sigma_{\text{min}} \). Note that this is, actually, quite a noteworthy result, which means that, for any \( N > 2 \), the steady motion of the fluxon accompanied by the emission of the Cherenkov radiation is possible at \( J = 1 \), i.e., in the uniform stack of identical LJJ’s.

Another simple case is obtained by setting \( J = 0 \). In this case Eq. (1) or Eq. (12) yield \( \phi_1 = 0 \), hence, the remaining equation (6) or (13), respectively is nothing else but the single sine-Gordon equation, which has proper solitonic solution (giving the \( |1 \rangle \) state) only for positive \( \sigma \). Therefore

\[
\sigma_{\text{min}}(0) = 0, \text{ for any } N.
\]

Physically this means that at large disbalance of critical currents the maximum velocity of fluxon is approaching \( 1 \equiv \bar{c}_0 \).

### III. NUMERICAL RESULTS

In the region \( u > \bar{c}_- \), i.e. at fluxon velocities larger than the lowest phase velocity of plasma waves, the phase dynamics in a stack is quite complex. Analytically, it can not be reduced just to looking for solutions of unperturbed equation in the form \( \phi = \phi(x - ut) \). Therefore, direct numerical simulations are necessary to get an insight into the problem.

The PDE’s (2) and (3) for \( N = 2 \) or (5) and (6) for \( N = 3 \) were solved numerically using an explicit method [expressing \( \phi^{A,B}(t + \Delta t) \) as a function of \( \phi^{A,B}(t) \) and \( \phi^{A,B}(t - \Delta t) \)], and treating \( \phi_{xx} \) with a five-point, \( \phi_t \) with a three-point and \( \phi_1 \) with a two-point symmetric finite-difference scheme. Equations were supplemented by the periodic boundary conditions, \( \phi_0(x + \ell) \equiv \phi_0(x) + 2\pi \), and \( \phi_1(x + \ell) \equiv \phi_1(x) \), with the period \( \ell = 200 \), so that the fluxon moves in the quasi-infinite system. Numerical stability was checked by doubling the spatial and temporal discretization steps \( \Delta x \) and \( \Delta t \) and checking its influence on the fluxon profiles and current-voltage curves (IVC).
values used for the simulations were \( \Delta x = 0.025 \) and \( \Delta t = 0.00625 \). To calculate the voltage in each point of the IVC, the instant voltage was averaged over the progressively increasing time intervals and also averaged over the length of the system. The following convergence criterion was adopted: the difference between the voltages obtained by averaging over two successive time intervals must not exceed \( \delta V = 5 \cdot 10^{-4} \). When the average voltage corresponding to the current \( \gamma \) is found, the current is increased by a small amount \( \delta \gamma = 0.001 \) to calculate the voltages at the next point of the IVC. We use the phases (and their derivatives) attained in the previous point of the IVC as the initial conditions for the next point. By gradually increasing \( \gamma \) and, thus, \( u \), we encountered a maximum value \( u_{\text{max}} \) of \( u \) above which the single-fluxon mode becomes unstable, and the system switches into a resistive state.

The simulations of IVC’s were carried out for the damping values \( \alpha = 0.02, 0.04, 0.1 \), in order to understand the effect of the dissipation on \( u_{\text{max}} \). In experiment, at low temperatures, \( \alpha \) can be about 0.01 and less. It turns that the simulations of the system with \( \alpha < 0.02 \) incurs unaffordable computational expenses. Therefore, we focus on higher values of \( \alpha \) and then will try to extrapolate \( u_{\text{max}} \) (if possible) to the ideal case \( \alpha = 0 \), which is of fundamental theoretical importance.

Here, we will only display the numerical results obtained for the cases \( N = 2 \) and \( N = 3 \). Examples of IVC’s for \( N = 2 \) and 3 different values of \( J \) are shown in Fig. 1 and Fig. 2. Strong effect of the ratio \( J \) between the critical currents of the junctions on \( u_{\text{max}} \) can be learned from Fig. 1. In the case \( J = 2 \), i.e., when the fluxon is located in the junction with the \( \delta \) critical current, the fluxon’s maximum velocity is smaller than the lowest Swihart velocity \( \bar{c} \). In addition, one can observe a back bended of the IVC close to its tip. The last point on back bent IVC marked as \([1, 1, -1]\) corresponds to the state when fluxon-antifluxon pair stretched out in the idle junction with lower \( J_c \). In the case \( J = 0.5 \), i.e., when the fluxon moves in the junction with the smaller critical current, the fluxon’s maximum velocity is larger than \( \bar{c} \). We note that the latter case is nontrivial and of the particular interest since, as it was already mentioned above, the fluxon can propagate stably, emitting the Cherenkov radiation.

Fig. 2 shows IVC’s of the \([0, 1, 0] \) state for \( J = 1 \) and different values of \( \alpha \). As long as we consider 3-fold stack with \( J < \sqrt{2} \), the IVC bends to the right into the Cherenkov region. The fluxon motion in such a case is very similar to the case \( J < 1, N = 2 \). Fig. 3 demonstrates that the damping not only changes the slope of the IVC at low velocity, but also affects \( u_{\text{max}} \).

The numerically found values \( u_{\text{max}} \) for different values of \( J \) are transformed into the corresponding values of the parameter \( \sigma_{\min} \) according to Eqs. (11) and (14). The values of \( \sigma_{\min} \) for \( N = 2 \) and \( N = 3 \) are plotted in Fig. 3 and Fig. 4, respectively. Note, that the numerically obtained dependence \( \sigma_{\min}(J) \) is in agreement with our analytical predictions given by Eqs. (23), (25) and (27). These three conditions work better for small \( \alpha \) which is quite natural since they were derived from the unperturbed \( (\alpha = \gamma = 0) \) equations. We remind that predictions (23), (25) and (27) are strict results and must be considered exact in the framework of inductive-coupling model. We found it interesting that the dependence of the maximum current \( \gamma_{\max} = \gamma(u_{\max}) \) on \( J \) is almost linear with \( \gamma_{\max}/J = 0.476, 0.531, 0.623 \) for \( \alpha = 0.02, 0.04, 0.10 \), respectively.

In the following section we suggest a functional dependence for \( \sigma_{\min}(u) \) and will compare this dependence with numerical results presented in Fig. 3 and Fig. 4.

### IV. THE VARIATIONAL APPROXIMATION

The purpose of this section is to find an analytical dependence which describes the simulation data obtained in the previous section. We will present an analysis using VA only for \( N = 2 \), but other cases can be considered similarly.

VA is based on the fundamental fact that Eqs. (1) and (4) admit the variational representation with the Lagrangian \( L = \int_{-\infty}^{+\infty} \mathcal{L}_2 \, d\xi \), where the Lagrangian density corresponding to Eqs. (5) and (8) is

\[
\mathcal{L}_2 = \frac{1}{2} \sigma (\phi_0')^2 + \frac{1}{2} \sigma (\phi_1')^2 + \phi_0' \phi_1' + (1 - \cos \phi_0) + \frac{1}{J} (1 - \cos \phi_1) \quad .
\]

A crucial step in the application of VA is to adopt an ansatz, i.e., a trial form of the solution. The ansatz is then to be inserted into the corresponding Lagrangian, and the integration over \( \xi \) given by Eq. (6) must be performed explicitly. This will produce an effective Lagrangian as a function of free parameters that the ansatz contains. Finally, the values of this parameters will be found from the condition that they must realize an extremum of the effective Lagrangian.

Thus, it is necessary to select a tractable ansatz (that admits an analytical calculation of the integrals in the expression for the Lagrangian), which satisfies the above boundary conditions for the fluxon. Here, both when selecting the ansatz and considering the boundary conditions, we ignore the above-mentioned nonvanishing Cherenkov oscillatory tails (note that the tail is formally infinitely long in the ideal model with \( \alpha = \gamma = 0 \), while in the damped system the tail decays exponentially far from the fluxon’s “body”). The simplest and, in fact, the only practical ansatz is
\[ \phi_0(\xi) = 4 \arctan \exp(\lambda \xi) , \]  
\[ \phi_n \neq 0 = B \frac{\sinh(\lambda \xi)}{\cosh^2(\lambda \xi)} . \]

Here, \( \lambda \) and \( B \) are free real parameters. Note that \( \lambda \) can always be defined positive, while \( B \) may be positive as well as negative. The expression was chosen in such a way that it describes the “image” profile qualitatively well in comparison with simulation and analytical results.

Still, the effective Lagrangian cannot be immediately calculated with the above ansatz. A further necessary simplification is to assume that the amplitude \( B \) of the fluxon’s images in the noncore layers is sufficiently small, so that the nonlinear term \( \sin \phi_1 \) in Eq. (11) may be linearized. In other words, the term \( (1 - \cos \phi_1) \) in the Lagrangian density is to be replaced by \( \frac{1}{2} \phi_1^2 \).

The final expression for the effective Lagrangian is

\[ L = 4 \sigma \lambda + \frac{4}{\lambda} + \frac{7}{15} \sigma B^2 \lambda + \frac{1}{3} \frac{B^2}{J \lambda} + \frac{4}{3} B \lambda . \]  

The variation of (31) in \( B \) leads to an equation that allows us to eliminate \( B \), i.e.,

\[ B = -\frac{10 J \lambda^2}{(5 + 7 J \sigma \lambda^2)} . \]

The remaining algebraic equation for the fluxon’s inverse width \( \lambda \) is

\[ 7 J^2 \sigma (21 \sigma^2 - 5) \lambda^6 - 3 J \left[ 25 - 7 \sigma^2 (10 - 7 J) \right] \lambda^4 - 15 \sigma (14 J - 5) \lambda^2 - 75 = 0 . \]

This equation has one or three positive roots for \( \lambda^2 \). The first two solutions exist and disappear simultaneously at some value of \( \sigma \). The third solution disappears diverging at \( \sigma_{\min} = \sqrt{5}/21 \). This can be seen from the form of the coefficient in front of the term \( \sim \lambda^6 \). We drop the third solution from the consideration since it gives a constant \( \sigma_{\min} \) which is unphysical due to Eqs. (23) and (24).

To find the minimum value of \( \sigma \) at which two smallest positive roots disappear, we write two conditions: the function \( f(\lambda) \) touches \( \lambda \)-axis and its derivative \( f'(\lambda) \) vanishes. These two equations determine \( \sigma_{\min} \) and \( \lambda(\sigma_{\min}) \) for given value of \( J \). Eliminating, consecutively, the terms \( \sim \lambda_6 \), \( \lambda_4 \) and \( \lambda^2 \) yields an equation which determines the dependence of \( \sigma_{\min} \) on \( J \):

\[ 56 (7 J + 5)^3 \sigma_{\min}^4 - (3675 J^2 + 36750 J + 1875) \sigma_{\min}^2 + 7500 J = 0 , \]

A solution to this equation is

\[ \sigma_{\min}^2 = \frac{3675 J + 1875 + 3675 J^2 + 125 \sqrt{15} \sqrt{(15 + 7 J) (1 - 7 J)^3}}{112 (5 + 7 J)^3} . \]

One can see that this solution exists only for \( J < 1/7 \). For \( J > 1/7 \), Eqs. (33) has only one (third) root, which is unphysical.

To relax the latter limitation, we can make use of the fact that, as it was said above, the asymmetry parameter \( J \) always takes values \( J < 1 \). We will make use of this, treating \( J \) as a small parameter, which is also justified by the fact that the stack with a sufficiently strong asymmetry might be of special physical interest. With regard to this, \( V \) leads to a simple expression for \( \sigma_{\min} \) (we just expand Eq. (35) in a Taylor series around \( J = 0\)):

\[ \sigma_{\min} \approx 2 \sqrt{J} . \]

The essential feature in Eq. (36) is a square root dependence. To comply with the strict analytical result for the unperturbed case, see Eqs. (23) and (24), we adopt

\[ \sigma_{(2)}_{\min} \approx \sqrt{J} , \]

For \( N = 3 \), a similar dependence is found to be

\[ \sigma_{(3)}_{\min} \approx \sqrt{2 J}.

as an approximation. The bold solid lines corresponding to these approximations are shown in Fig. 3 and Fig. 4.

Apparently, the smaller the dissipation, the better the approximations \((37)\) and \((38)\) work. In the presence of the dissipation, the fluxons can exist at velocities somewhat larger than in the idealized model. The latter circumstance is quite natural, as in the single Josephson junction the onset of the fluxon’s instability past the Swihart velocity is also delayed by the dissipation \(15\).

We can also obtain an analytical approximation for \(N \to \infty\). In this case,

\[
\sigma_{\text{min}} \approx \sqrt{2J}.
\]

The stack with the uniform critical current distribution, therefore, has \(\sigma_{\text{min}} = \sqrt{2}\). The Cherenkov radiation will appear in the range \(\sqrt{2} < \sigma_{\text{min}} < 2\).

It is convenient to present the results of our calculations as the plot \(u_{\text{max}}(|S|)\). Such a plot for \(N = 3\) and \(\sigma^{(3)} = 2^{1/4}\) (uniform stack) is shown in Fig. 5. The region where the fluxon moves faster than \(\bar{c}_-\) is shaded. It is the domain of existence of the Cherenkov radiation. The range of \(S\) in Fig. 5 corresponds to the maximum value of the coupling parameter \(|S|_{\text{max}}\) in 3-fold stack which is equal to \(1/\sqrt{2}\).

V. CONCLUSION

We have demonstrated that a single fluxon moving in the stack of Josephson junctions has the maximum velocity which does not necessarily coincide with one of the Swihart velocities of the system. The dependence \(u_{\text{max}}(J)\) was studied numerically for \(N = 2\) and 3. An analytical approximation for this dependence was put forward on the basis of the variational approximation in the limit of small dissipation and is given by Eqs. \((37)\) and \((38)\). Our results show that \(u_{\text{max}} > \bar{c}_-\) for \(J < 1\), in the case \(N = 2\), and for \(J < \sqrt{2}\), in the case \(N = 3\). This leads to Cherenkov radiation of plasma waves by a fluxon in the velocity range \(\bar{c}_- < u < u_{\text{max}}\). Simulations also show that the damping stabilizes the fluxon motion at higher velocities, i.e., \(u_{\text{max}}(\alpha > 0) > u_{\text{max}}(\alpha = 0)\). In uniform stack with large \(N\) (e.g., intrinsic Josephson stacks in crystals of high-\(T_c\) superconductors), \(u_{\text{max}}\) exceeds \(\bar{c}_-\) and, therefore, a single fluxon always generates Cherenkov radiation. Experiments with high-\(T_c\) stacks \(16\) show that flux-flow branches do not have vanishing differential resistance \(R_d\) close to the top of the flux-flow step as in the single LJJ but bend towards higher voltages, in agreement with our results. From the theoretical point of view, the absence of the “relativistic” singularity at \(u = \bar{c}_-\) is a result of the lack of the Lorentz invariance in the coupled sine-Gordon equations.

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* e-mail: e.goldobin@fz-juelich.de, homepage: http://www.geocities.com/e_goldobin
† e-mail: malomed@ayalon.eng.tau.ac.il
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FIGURE CAPTIONS

FIG. 1. The IVC’s $u(\gamma)$ of a 2-fold stack with a single fluxon trapped in one LJJ (the state $|10\rangle$) for three different values of $J = 0.5, 1,$ and $2$. The branches for $J = 0.5$ and $J = 1$ terminate at a value $u_{\text{max}}$ at which the fluxon becomes unstable and the system switches to high voltages. The inset is a blowup of the rectangular area on the main diagram. The simulations were performed for $\alpha = 0.1$ and demonstrate the dependence of $u_{\text{max}}$ on $J$.

FIG. 2. The IVC’s of the 3-fold stack with a fluxon in the central layer for three different values of $\alpha = 0.02, 0.04,$ and $0.1$. The simulations performed for $J = 1$ demonstrate the dependence of $u_{\text{max}}$ on $\alpha$.

FIG. 3. The dependence of $\sigma_{\text{min}}^{(2)}$ on $J$ for three different values of $\alpha = 0.02$ (circles), $0.04$ (squares), and $0.10$ (diamonds). The bold solid line shows the analytical dependence $\sigma_{\text{min}}^{(2)}$ produced by the variational approximation.

FIG. 4. The dependence of $\sigma_{\text{min}}^{(3)}$ on $J$ for three different values of $\alpha = 0.02$ (circles), $0.04$ (squares), and $0.10$ (diamonds). The bold solid line shows the analytical prediction $\sigma_{\text{min}}^{(3)}$ based on the variational approximation.

FIG. 5. The dependence of maximum velocity $u_{\text{max}}$ and Swihart velocities $\bar{c}_{\pm}$ on the coupling strength $|S|$ for three coupled junctions at $J = 1$. The shaded area shows the domain of the Cherenkov radiation.

| $N$ | 3 | 5 | 7 | 9 | 13 | 19 | 39 | 99 |
|-----|---|---|---|---|----|----|----|----|
| $\sigma_{\text{min}}$ | 1.414 | 1.732 | 1.848 | 1.902 | 1.950 | 1.975 | 1.994 | 1.999 |

TABLE I. The values of $\sigma_{\text{min}}$ for different numbers $N$ of junctions in the stack. As $N \to \infty$, $\sigma_{\text{min}} \to 2$. 

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