Research Article

Analysis of Heating Effects and Different Wave Forms on Peristaltic Flow of Carreau Fluid in Rectangular Duct

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1. Introduction

The applications of peristaltic flows in medical and engineering sciences have attracted the attention of a number of researchers. Applications of peristalsis occur in swallowing food through the esophagus, urine transport from the kidney to the bladder through the ureter, transport of the spermatozoa in the efferent ducts of the male reproductive tract, movement of the ovum in the fallopian tube, movement of the chyme in the gastrointestinal tract, the transport of lymph in the lymphatic vessels, and vasomotion in the small blood vessels such as the arterioles, veins, and capillaries. The peristaltic phenomenon was first discussed by Latham [1]. Based on his experimental theory, numerous researchers have inspected the phenomenon of peristaltic transport under many conjectures [2–10].

Another fascinating area in connection with peristaltic motion is the heat transfer which has industrial applications like sanitary fluid transport, blood pumps in the heart-lungs machine and transport of corrosive fluids where the contact of fluid with the machinery parts are prohibited. Only a limited attention has been focused to the study of peristaltic flows with heat transfer [11–15].

An immense amount of literature is presented on two-dimensional peristaltic flow problems. The study of peristaltic phenomenon in a rectangular channel was first examined by [16]. Based on the theory of [16], several researchers have studied the phenomenon of peristaltic transport in a rectangular duct under various approximations [17–23]. In the papers cited above, the phenomena of heat transfer are not taken into account. Keeping in mind the present information, the heat transfer phenomena on the peristaltic flow of non-Newtonian fluid have not been discussed in a three-dimensional channel. So, the aim of the present problem is to discuss the effects of heat transfer on peristaltic flow of a non-Newtonian fluid in a rectangular duct with different wave forms. The governing equations for the three-dimensional rectangular channel are first modeled for Carreau fluid and then simplified under the long wavelength and low Reynolds number approximation. Homotopy perturbation technique is carried out to calculate the analytical solution of the highly nonlinear partial differential equations. The expressions for
velocity, pressure rise, pressure gradient, and temperature have been computed and discussed through graphs. Three-
dimensional graphical representations for the velocity field
are also discussed through graphs. In the end, different wave
forms are also used.

2. Mathematical Formulation of the Problem

Let us consider the peristaltic flow of an incompressible
Carreau fluid in a duct of rectangular cross section having
the channel width 2d and height 2a. We are considering the
Cartesian coordinates system in such a way that the X-axis
is taken along the axial direction, Y-axis is taken along the
lateral direction, and Z-axis is along the vertical direction of
a rectangular duct.

The peristaltic waves on the walls are represented as

\[ Z = H(X, t) = \pm a \pm b \cos \left( \frac{2\pi}{\lambda} (X - ct) \right), \]

(1)

where \( a \) and \( b \) are the amplitudes of the waves, \( \lambda \) is the wave
length, \( c \) is the velocity of propagation, \( t \) is the time, and \( X \) is
the direction of wave propagation. The walls parallel to the
\( XZ \) plane remain undisturbed and are not subjected to any
peristaltic wave motion. We assume that the lateral velocity
is zero as there is no change in the lateral direction of the duct
cross section. Let \( (U, 0, W) \) be the velocity for a rectangular
duct. The governing equations for the flow problem are

\[ \frac{\partial U}{\partial X} + \frac{\partial W}{\partial Z} = 0, \]

(2)

\[ \rho \left( \frac{\partial U}{\partial t} + U \frac{\partial U}{\partial X} + W \frac{\partial U}{\partial Z} \right) \]

\[ = - \frac{\partial P}{\partial X} + \frac{\partial}{\partial X} S_{XX} + \frac{\partial}{\partial Y} S_{XY} + \frac{\partial}{\partial Z} S_{XZ}, \]

(3)

\[ 0 = - \frac{\partial P}{\partial Y} + \frac{\partial}{\partial X} S_{YX} + \frac{\partial}{\partial Y} S_{YY} + \frac{\partial}{\partial Z} S_{YZ}, \]

(4)

\[ \rho \left( \frac{\partial W}{\partial t} + U \frac{\partial W}{\partial X} + W \frac{\partial W}{\partial Z} \right) \]

\[ = - \frac{\partial P}{\partial Z} + \frac{\partial}{\partial X} S_{ZX} + \frac{\partial}{\partial Y} S_{ZY} + \frac{\partial}{\partial Z} S_{ZZ}, \]

(5)

\[ \rho C' (\frac{\partial T}{\partial t} + U \frac{\partial T}{\partial X} + W \frac{\partial T}{\partial Z}) \]

\[ = K' \left( \frac{\partial^2 T}{\partial X^2} + \frac{\partial^2 T}{\partial Y^2} + \frac{\partial^2 T}{\partial Z^2} \right) + S_{XX} \frac{\partial U}{\partial X} + S_{XY} \frac{\partial U}{\partial Y} + S_{XZ} \frac{\partial U}{\partial Z}, \]

(6)

in which \( \rho \) is the density, \( P \) is the pressure, \( t \) is the time,
and \( S \)'s is the stress tensor for the Carreau fluid; \( C' \) is the
specific heat; and \( T \) is the temperature. The stress tensor for
the Carreau fluid is defined by [17].
Using the above nondimensional quantities in Equations (2), (3), (4), (5) and (7), the resulting equations after dropping the bars can be written as

\[
\frac{\partial u}{\partial x} + \frac{\partial \omega}{\partial z} = 0, \tag{10}
\]

\[
\text{Re} \left( \frac{\partial u}{\partial x} + u \frac{\partial u}{\partial z} \right) = -\frac{\partial p}{\partial x} + \delta \frac{\partial}{\partial x} S_{xx} + \beta^2 \frac{\partial}{\partial y} S_{xy} + \frac{\partial}{\partial z} S_{xz},
\]

\[
0 = -\frac{\partial p}{\partial y} + \delta \frac{\partial}{\partial x} S_{xy} + \delta^2 \frac{\partial}{\partial y} S_{yy} + \delta \frac{\partial}{\partial z} S_{yz}, \tag{11}
\]

\[
\text{Re} \delta \left( \frac{\partial \omega}{\partial x} + u \frac{\partial \omega}{\partial z} \right) = -\frac{\partial p}{\partial x} + \delta^2 \frac{\partial}{\partial x} S_{xx} + \delta \beta^2 \frac{\partial}{\partial y} S_{xy} + \delta^2 \frac{\partial}{\partial z} S_{xz}, \tag{12}
\]

\[
\text{Re} \delta \left( \frac{\partial \theta}{\partial x} + u \frac{\partial \theta}{\partial z} \right) = \frac{1}{Pr} \left( \delta \frac{\partial^2 \theta}{\partial x^2} + \beta^2 \frac{\partial^2 \theta}{\partial y^2} + \frac{\partial^2 \theta}{\partial z^2} \right)
+ Ec \delta S_{xx} \frac{\partial u}{\partial x} + \beta^2 S_{xy} \frac{\partial u}{\partial y} + \beta \delta S_{yz} \frac{\partial \omega}{\partial y}
+ \delta S_{zz} \frac{\partial \omega}{\partial z} + S_{zz} \left( \delta \frac{\partial \omega}{\partial x} + \frac{\partial u}{\partial z} \right), \tag{13}
\]

where

\[
S_{xx} = -2\delta \left( 1 + \frac{(n-1)}{2} We^2 \gamma \right) \frac{\partial u}{\partial x}, \tag{15}
\]

\[
S_{xy} = -\left( 1 + \frac{(n-1)}{2} We^2 \gamma \right) \frac{\partial u}{\partial y}, \tag{16}
\]

\[
S_{xz} = -\left( 1 + \frac{(n-1)}{2} We^2 \gamma \right) \left( \frac{\partial u}{\partial z} + \delta^2 \frac{\partial \omega}{\partial x} \right), \tag{17}
\]

\[
S_{yy} = 0, \tag{18}
\]

\[
S_{yz} = -\delta \left( 1 + \frac{(n-1)}{2} We^2 \gamma \right) \frac{\partial \omega}{\partial y}, \tag{19}
\]

\[
S_{zz} = -2 \left( 1 + \frac{(n-1)}{2} We^2 \gamma \right) \frac{\partial \omega}{\partial z}, \tag{20}
\]

\[
\gamma^2 = 2\delta^2 \left( \frac{\partial u}{\partial x} \right)^2 + \beta^2 \left( \frac{\partial u}{\partial y} \right)^2 + \delta^2 \beta^2 \left( \frac{\partial \omega}{\partial y} \right)^2 + \delta^2 \left( \frac{\partial \omega}{\partial z} + \frac{\partial u}{\partial x} \right)^2, \tag{21}
\]

Under the assumption of long wavelength \( \delta \leq 1 \) and low Reynolds number \( \text{Re} \rightarrow 0 \), Equations (10), (11), (12), (13), (14) and (21) take the form

\[
\frac{d}{dx} + \beta^2 \frac{\partial^2 u}{\partial y^2} + \frac{n-1}{2} We^2 \beta \frac{\partial}{\partial z} \left( \frac{\partial u}{\partial y} \right)^3
+ \frac{n-1}{2} We^2 \beta^2 \frac{\partial}{\partial y} \left( \frac{\partial u}{\partial y} \right)^2
+ \frac{n-1}{2} We^2 \beta \frac{\partial}{\partial z} \left( \frac{\partial u}{\partial y} \right)^2
+ \frac{n-1}{2} We^2 \beta^2 \frac{\partial}{\partial y} \left( \frac{\partial u}{\partial y} \right)^2
- \frac{dp}{dx} = 0, \tag{22}
\]

\[
\frac{\partial^2 \theta}{\partial x^2} + \beta^2 \frac{\partial^2 \theta}{\partial y^2} + Ec Pr \left( \beta^2 \left( \frac{\partial u}{\partial y} \right)^2 + \frac{n-1}{2} \beta^4 We^2 \left( \frac{\partial u}{\partial y} \right)^4
+ \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial u}{\partial y} \right)^2 + \left( \frac{\partial u}{\partial y} \right)^2
+ \frac{n-1}{2} We^2 \left( \frac{\partial u}{\partial y} \right)^4 + \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial u}{\partial y} \right)^2 \left( \frac{\partial u}{\partial y} \right)^2 \right) = 0. \tag{23}
\]

The corresponding boundary conditions are

\[
\begin{align*}
u &= -1 \text{ at } y = \pm 1, \\
u &= -1 \text{ at } z = h(x) = \pm 1 + \varphi \cos 2\pi x, \\
\theta &= 0 \text{ at } y = 1, \\
\theta &= 0 \text{ at } z = h(x), \\
\theta &= 1 \text{ at } y = -1, \\
\theta &= 1 \text{ at } z = -h(x).
\end{align*} \tag{24}
\]

where 0 ≤ \( \varphi \leq 1 \), \( \varphi = 0 \) for straight duct and \( \varphi = 1 \) corresponds to total occlusion.

### 3. Solution of the Problem

#### 3.1. Homotopy Perturbation Method

The solution of the nonlinear partial differential Equations (22) and (23) has been calculated using homotopy perturbation technique. The homotopy perturbation method for Equations (22) and (23) can be defined as [24–30].

\[
H(v, q) = (1 - q) (E(v) - E(u_0)) + q \left( E(v) + \beta^2 \frac{\partial^2 u}{\partial y^2} + \frac{n-1}{2} We^2 \beta \frac{\partial}{\partial z} \left( \frac{\partial u}{\partial y} \right)^3 + \frac{n-1}{2} We^2 \beta \frac{\partial}{\partial z} \left( \frac{\partial u}{\partial y} \right)^2
+ \frac{n-1}{2} We^2 \beta^2 \frac{\partial}{\partial y} \left( \frac{\partial u}{\partial y} \right)^2
- \frac{dp}{dx} = 0,
\]
\[ H(\Theta, q) = (1 - q) \left( \mathcal{E}(\Theta) - \mathcal{E}(\Theta_0) \right) + q \left( \mathcal{E}(\Theta) + \beta^2 \frac{\partial^2 \Theta}{\partial y^2} \right) + Ec Pr \left( \beta^2 \left( \frac{\partial \nu}{\partial y} \right)^2 + \frac{n-1}{2} \beta^4 We^2 \left( \frac{\partial \nu}{\partial y} \right)^4 \right. \]
\[ + \left. \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial \nu}{\partial y} \right)^2 \left( \frac{\partial \nu}{\partial z} \right)^2 + \left( \frac{\partial \nu}{\partial z} \right)^2 + \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial \nu}{\partial y} \right)^2 \left( \frac{\partial \nu}{\partial z} \right)^2 \right) = 0, \]
\[ (25) \]

or

\[ H(v, q) = \mathcal{E}(v) - \mathcal{E}(u_0) + q \mathcal{E}(u_0) + q \left( \beta^2 \frac{\partial^2 u}{\partial y^2} \right) \]
\[ + \frac{n-1}{2} We^2 \beta^3 \frac{\partial}{\partial y} \left( \frac{\partial \nu}{\partial y} \right)^3 + \frac{n-1}{2} We^2 \beta \frac{\partial}{\partial y} \left( \frac{\partial \nu}{\partial z} \right)^2 \]
\[ + \frac{n-1}{2} We^2 \beta \frac{\partial}{\partial z} \left( \frac{\partial \nu}{\partial y} \right)^2 - \frac{dp}{dx} \right) = 0, \]
\[ (26) \]

\[ H(\Theta, q) = \mathcal{E}(\Theta) - \mathcal{E}(\Theta_0) + q \mathcal{E}(\Theta_0) + q \left( \beta^2 \frac{\partial^2 \Theta}{\partial y^2} \right) + Ec Pr \left( \beta^2 \left( \frac{\partial \nu}{\partial y} \right)^2 + \frac{n-1}{2} \beta^4 We^2 \left( \frac{\partial \nu}{\partial y} \right)^4 \right) \]
\[ + \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial \nu}{\partial y} \right)^2 \left( \frac{\partial \nu}{\partial z} \right)^2 + \left( \frac{\partial \nu}{\partial z} \right)^2 + \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial \nu}{\partial y} \right)^2 \left( \frac{\partial \nu}{\partial z} \right)^2 \right) = 0. \]
\[ (27) \]

Here, \( q \) is an embedding parameter which has the range \( 0 \leq q \leq 1 \), under the condition that for \( q = 0 \), we get the initial solution, and for \( q = 1 \), we seek the final solution. Here, \( \mathcal{E} \) is the linear operator which is taken here as \( \mathcal{E} = \beta^2 \frac{\partial^2}{\partial z^2} \). We define the initial guess as

\[ u_0 = -1 + (h^2 - z^2) + \frac{(1 - y)}{2} - \frac{(h - z)}{2h}, \]
\[ \tilde{\Theta}_0 = (z^2 - h^2) + \frac{(h - z)}{2h} + \frac{1}{\beta^2} (1 - y^2). \]
\[ (28) \]
We = 0.0
We = 0.2
We = 0.4
We = 0.6

Figure 4: Variation of pressure rise with volume flow rate $Q$ for different values of $\text{We}$ for fixed values of $\phi = 0.7$, $n = 0.3$, and $\beta = 6$.

We = 0.0
We = 0.2
We = 0.4
We = 0.6

Figure 7: Variation of pressure gradient with $x$ for different values of $\phi$ for fixed values of $n = 0.5$, $\beta = 4$, $\text{We} = 0.6$, and $Q = -1$.

$\beta = 1.0$
$\beta = 3.0$
$\beta = 5.0$
$\beta = 0.7$

Figure 5: Variation of pressure gradient with $x$ for different values of $\beta$ for fixed values of $\phi = 0.5$, $n = 0.5$, $\text{We} = 0.4$, and $Q = -2$.

$\phi = 0.4$
$\phi = 0.5$
$\phi = 0.6$
$\phi = 0.7$

Figure 8: Variation of pressure gradient with $x$ for different values of $\phi$ for fixed values of $n = 0.5$, $\beta = 4$, $\text{We} = 0.6$, and $Q = -2$.

$n = -1.0$
$n = 0.0$
$n = 1.0$

Figure 6: Variation of pressure gradient with $x$ for different values of $n$ for fixed values of $\phi = 0.5$, $\beta = 4$, $\text{We} = 0.6$, and $Q = -2$.

$n = -1.0$
$n = 0.0$
$n = 1.0$

Figure 9: Variation of pressure gradient with $x$ for different values of $n$ for fixed values of $\phi = 0.5$, $\beta = 4$, $\text{We} = 0.6$, and $Q = -2$. 

Multisinusoidal wave
Let us define
\[ v(x, y, z, q) = v_0 + q v_1 + q^2 v_2 + \cdots, \]  
(29)
\[ \Theta(x, y, z, q) = \Theta_0 + q \Theta_1 + q^2 \Theta_2 + \cdots, \]  
(30)
substituting Equation (30) into Equations (26) and (27), and then comparing the like powers of \( q \), one obtains the following problems with the corresponding boundary conditions.

3.2. Zeroth Order System.
\[ \mathcal{L}(v_0) - \mathcal{L}(u_0) = 0, \]
\[ \mathcal{L}(\Theta_0) - \mathcal{L}(\theta_0) = 0, \]
\[ v_0 = -1 \text{ at } y = \pm 1, \]
\[ v_0 = -1 \text{ at } z = \pm h(x), \]
\[ \Theta_0 = 0 \text{ at } y = 1, \]
\[ \Theta_0 = 0 \text{ at } z = h(x), \]
\[ \Theta_0 = 1 \text{ at } y = -1, \]
\[ \Theta_0 = 1 \text{ at } z = -h(x). \]
(31)

3.3. First-Order System.
\[ \mathcal{L}(v_1) + \mathcal{L}(u_0) + \left( \beta^2 \frac{\partial^2 v_0}{\partial y^2} + \frac{n-1}{2} We^2 \beta^2 \frac{\partial}{\partial y} \left( \frac{\partial v_0}{\partial y} \right)^2 \right)
\]
\[ + \frac{n-1}{2} We^2 \beta^2 \frac{\partial}{\partial z} \left( \frac{\partial v_0}{\partial y} \right)^2 + \frac{n-1}{2} We^2 \beta^2 \frac{\partial}{\partial z} \left( \frac{\partial v_0}{\partial y} \right)^2 \]
\[ + \frac{n-1}{2} We^2 \beta^2 \frac{\partial}{\partial z} \left( \frac{\partial v_0}{\partial y} \right)^2 - \frac{dp}{dx} = 0, \]
\[ \mathcal{L}(\Theta_1) + \mathcal{L}(\theta_0) + \left( \beta^2 \frac{\partial^2 \Theta_0}{\partial y^2} + Ec Pr \left( \beta^2 \left( \frac{\partial v_0}{\partial y} \right)^2 \right) \right)
\]
\[ + \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial v_0}{\partial y} \right)^4 + \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial v_0}{\partial y} \right)^4 \]
\[ \left( \frac{\partial v_0}{\partial z} \right)^2 + \left( \frac{\partial v_0}{\partial z} \right)^2 + \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial v_0}{\partial y} \right)^4 \]
\[ + \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial v_0}{\partial y} \right)^2 \left( \frac{\partial v_0}{\partial z} \right)^2 \right) = 0, \]
\[ v_1 = 0 \text{ at } y = \pm 1, \]
\[ v_1 = 0 \text{ at } z = \pm h(x), \]
\[ \Theta_1 = 0 \text{ at } y = 1, \]
\[ \Theta_1 = 0 \text{ at } z = h(x), \]
\[ \Theta_1 = 0 \text{ at } y = -1, \]
\[ \Theta_1 = 0 \text{ at } z = -h(x). \]
(32)

3.4. Second-Order System.
\[ \mathcal{L}(v_2) + \beta^2 \frac{\partial^2 v_1}{\partial y^2} + \frac{n-1}{2} We^2 \beta^2 \frac{\partial}{\partial y} \left( \frac{\partial v_0}{\partial y} \right)^2 \]
\[ + \frac{n-1}{2} We^2 \beta^2 \frac{\partial}{\partial z} \left( \frac{\partial v_0}{\partial y} \right)^2 + \frac{n-1}{2} We^2 \beta^2 \frac{\partial}{\partial z} \left( \frac{\partial v_0}{\partial y} \right)^2 \]
\[ + \left( \frac{\partial v_1}{\partial y} \right)^2 \left( \frac{\partial v_0}{\partial y} \right)^2 + \frac{n-1}{2} We^2 \beta^2 \frac{\partial}{\partial z} \left( \frac{\partial v_0}{\partial y} \right)^2 \]
\[ + \left( \frac{\partial v_1}{\partial y} \right)^2 \left( \frac{\partial v_0}{\partial y} \right)^2 + \frac{n-1}{2} We^2 \beta^2 \frac{\partial}{\partial z} \left( \frac{\partial v_0}{\partial y} \right)^2 \right) = 0, \]
\[ \mathcal{L}(\Theta_2) + \left( \beta^2 \frac{\partial^2 \Theta_1}{\partial y^2} + Ec Pr \left( \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial v_0}{\partial y} \right)^4 \right) \right)
\]
\[ + \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial v_0}{\partial y} \right)^4 + \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial v_0}{\partial y} \right)^4 \]
\[ \left( \frac{\partial v_0}{\partial z} \right)^2 + \left( \frac{\partial v_0}{\partial z} \right)^2 + \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial v_0}{\partial y} \right)^4 \]
\[ + \frac{n-1}{2} \beta^2 We^2 \left( \frac{\partial v_0}{\partial y} \right)^2 \left( \frac{\partial v_0}{\partial z} \right)^2 \right) = 0, \]
\[ v_2 = 0 \text{ at } y = \pm 1, \]
\[ v_2 = 0 \text{ at } z = \pm h(x), \]
\[ \Theta_2 = 0 \text{ at } y = 1, \]
\[ \Theta_2 = 0 \text{ at } z = h(x), \]
\[ \Theta_2 = 0 \text{ at } y = -1, \]
\[ \Theta_2 = 0 \text{ at } z = -h(x). \]
(33)
Figure 11: Variation of pressure gradient with $x$ for different values of $n$ for fixed values of $\phi = 0.5$, $\beta = 6$, $We = 0.6$, and $Q = -3.5$.

Figure 12: Variation of pressure gradient with $x$ for different values of $n$ for fixed values of $\phi = 0.5$, $\beta = 4$, $We = 0.6$, and $Q = -2$.

Figure 13: Temperature profile for different values of $We$ for fixed values of $\phi = 0.6$, $x = 0$, $\beta = 0.5$, $n = 2$, $Q = -1$, $y = 1$, $Pr = 0.5$, and $Ec = 0.2$.

The resulting series solutions after three iterations are determined using Equation (30) as (when $q \rightarrow 1$) and are evaluated as

\[
u(x, y, z) = -1 + (h^2 - z^2) + \frac{1 - y}{2h} - \frac{h - z}{2h} + \frac{1}{12} \cdot (-12h^4(n - 1) We^2 + 12(n - 1) We^2 z^4) - 6h^2 \left(2 + \frac{dp}{dx} + \frac{1}{4} (n - 1) We^2 \beta^2\right) + 6z^2 \cdot \left(2 + \frac{dp}{dx} + \frac{1}{4} (n - 1) We^2 \beta^2\right) + \frac{1}{96} (n - 1) We^2 \cdot (h - z) (h + z) \left(384(n - 1) We^2 (h^4 + h^2 z^2 + z^4) + 12(n - 1) \beta^2 We^2 (h^2 + z^2) + (n - 1) We^2 (h^2 + z^2) + \beta^2\right) \left(2 + \frac{dp}{dx} + \frac{1}{4} (n - 1) We^2 \beta^2\right),
\]

\[
\theta(x, y, z) = -h^2 + \frac{h - z}{2h} + z^2 + \frac{1 - y^2}{\beta^2} + \frac{1}{60} \left(Pr Ec 16(n - 1) We^2 (h^6 - z^6) + 5 Pr Ec (h^4 - z^4) (4 + (n - 1) We^2 \beta^2) + \frac{15}{16} Pr Ec (h - z) (h + z) \beta^2 (8 + (n - 1) We^2 \beta^2) - \frac{1}{1260} Pr Ec \left(21 \left(2 + \frac{dp}{dx} + \frac{1}{4} (n - 1) We^2 \beta^2\right) (32h^6(n - 1) We^2 + 5h^4 (4 + (n - 1) We^2 \beta^2) + z^4 (-20 - (n - 1) We^2 (32z^2 + 5\beta^2)) + 24(n - 1) We^2 (60h^6(n - 1) We^2 + 7h^6 (4 + (n - 1) We^2 \beta^2) + z^6 (-28 - (n - 1) We^2 (60z^2 + 7\beta^2)) \right)\right) \right).}
\]

(34)

The volumetric flow rate is given by

\[
q = \int_{-h(x)}^{h(x)} h(x, y, z) dy dz = -h(x) + \frac{8}{5} h^3(n - 1) We^2 + \frac{24}{7} h^7(n - 1)^2 We^4 + \frac{5}{2} h^5(n - 1)^2 \beta^2 We^4 + \frac{1}{96} h^3(n - 1)^2 We^4 \beta^4 + \frac{6}{5} h^3(n - 1) We^2
\]

(35)
Figure 14: Temperature profile for different values of $\beta$ for fixed values of $\varphi = 0.6$, $x = 0$, $We = 0.03$, $n = 2$, $Q = -1$, $y = 1$, $Pr = 0.5$, and $Ec = 0.2$.

Figure 15: Temperature profile for different values of $Pr$ for fixed values of $\varphi = 0.6$, $x = 0$, $We = 0.03$, $n = 2$, $Q = -1$, $y = 1$, $\beta = 0.2$, and $Ec = 0.5$.

Figure 16: Temperature profile for different values of $Ec$ for fixed values of $\varphi = 0.6$, $x = 0$, $We = 0.03$, $n = 2$, $Q = -1$, $y = 1$, $\beta = 0.2$, and $Pr = 0.5$.

Figure 17: Velocity profile for different values of $\beta$. The other parameters are $\varphi = 0.6$, $x = 0$, $Q = -0.5$, $We = 0.3$, and $n = 2$. 
The instantaneous flux is defined as

\[
Q = \int_0^1 (u + 1) \, dy \, dz = q + h(x).
\] (36)

The average volume flow rate over one period \((T = \lambda/c)\) of the peristaltic wave is defined as

\[
Q = \frac{1}{T} \int_0^T Q \, dt = q + h(x).
\] (37)

The pressure gradient is obtained from Equations (35) and (37) as

\[
\frac{dp}{dx} = \frac{Q - 1 + h(x) - (8/5)h^2(n - 1)We^2 - (24/7)h^2(n - 1)^2We^4 - (2/5)h^2(n - 1)^2 \beta^2 We^4 - (1/96)h^2(n - 1)^2 \beta^4 We^4}{\left((6/5)h^2(n - 1)We^2 + (1/24)h^2(-8 + (n - 1)We^2\beta^2)\right)},
\] (38)

Integration of Equation (38) over one wavelength yields

\[
\Delta p = \int_0^1 \frac{dp}{dx} \, dx.
\] (39)

It is noticed here that the limit \(\beta \rightarrow 0\) (keeping it fixed and \(d \rightarrow \infty\)), the rectangular duct reduces to a two-dimensional channel. It is also noticed that when \(\beta = 1\) the rectangular duct becomes a square duct.

### 4. Expressions for Different Wave Shapes

The nondimensional expressions for five considered wave forms are given by [11]. The expression for the triangular, square, and trapezoidal waves are derived from the Fourier series.

1. **Sinusoidal wave**
   \[ h(x) = \pm 1 \pm \phi \sin 2\pi x \] (40)

2. **Multisinusoidal wave**
   \[ h(x) = \pm 1 \pm \phi \sin 2m\pi x \] (41)

3. **Triangular wave**
   \[ h(x) = \pm 1 \pm \phi \left[ \frac{8}{\pi^2} \sum_{m=1}^{\infty} \frac{(-1)^{m+1}}{(2m-1)^2} \sin \left( \frac{2\pi (2m-1)x}{2} \right) \right] \] (42)

4. **Trapezoidal wave**
   \[ h(x) = \pm 1 \pm \phi \left[ \frac{32}{\pi^2} \sum_{m=1}^{\infty} \frac{\sin \left( \frac{\pi}{8} (2m-1) \right)}{(2m-1)^2} \sin \left( \frac{2\pi (2m-1)x}{2} \right) \right] \] (43)

5. **Square wave**
   \[ h(x) = \pm 1 \pm \phi \left[ \frac{4}{\pi} \sum_{m=1}^{\infty} \frac{(-1)^{m+1}}{(2m-1)} \cos \left( \frac{2\pi (2m-1)x}{2} \right) \right] \] (44)

### 5. Numerical Results and Discussion

In this segment, the graphical representation of the proposed problem is discussed. With the help of mathematics software
Mathematica, the expression for pressure rise and pressure gradient is calculated. In order to see the behavior of pressure rise with volume flow rate $Q$ for different values of aspect ratio $\beta$, power law index $n$, amplitude ratio $\phi$, and Weissenberg number $\text{We}$. It is observed from Figure 1 that in the peristaltic pumping ($\Delta p > 0$, $Q > 0$) and retrograde pumping ($\Delta p > 0$, $Q < 0$) regions, the pumping rate decreases with an increase in aspect ratio $\beta$, while in the copumping region ($\Delta p < 0$, $Q > 0$), the behavior is quite opposite; here, the pumping rate increases with an increase in aspect ratio $\beta$.

Figures 2 and 3 show the variation of pressure rise with volume flow rate $Q$ for different values of $n$ and $\phi$. It is observed from Figure 2 that in the retrograde pumping ($\Delta p > 0$, $Q > 0$) and peristaltic pumping ($\Delta p > 0$, $Q < 0$) regions, the pumping rate increases with an increase in $n$ and $\phi$, while in the copumping region ($\Delta p < 0$, $Q > 0$), the pressure rise decreases with an increase in values of $n$ and $\phi$. In order to see the behavior of pressure rise with volume flow rate $Q$ for different values of $\text{We}$, Figure 4 is plotted. It is depicted from Figure 4 that in the peristaltic pumping ($\Delta p > 0$, $Q > 0$) and retrograde pumping ($\Delta p > 0$, $Q < 0$) regions, the pumping rate decreases with an increase in $\text{We}$, while in the copumping region ($\Delta p < 0$, $Q > 0$), the behavior is quite opposite; here, the pumping rate increases with an increase in $\text{We}$.

The pressure gradient for different values of aspect ratio $\beta$, $n$, amplitude ratio $\phi$, and $\text{We}$ against space variable $x$ is plotted in Figures 5–8. It is depicted from Figures 5–8 that for $x \in [0, 0.2]$ and $x \in [0.8, 1]$, the pressure gradient is small, i.e., the flow can easily pass without the imposition of a large pressure gradient, while in the region $x \in [0.2, 0.8]$ that the pressure gradient decreases with an increase in aspect ratio $\beta$ and $\text{We}$ and increases with an increase in amplitude ratio $\phi$. 

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**Figure 20:** Stream lines for different values of $\beta$. The other parameters are $\phi = 0.7$, $\text{We} = 0.51$, $y = 1$, $n = -0.8$, and $Q = 2.0$.

**Figure 21:** Stream lines for different values of $n$. The other parameters are $\phi = 0.7$, $\beta = 4$, $\text{We} = 0.51$, $y = 1$, and $Q = 2.0$. 

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and \(n\), so much pressure gradient is required to maintain the flux to pass. Figures 9–12 show the stream lines for different wave forms. It is observed from Figures 9–12 that the pressure gradient retains the same shape of the waves as we consider.

Figures 13–16 show the temperature profile for different values of \(\text{We}, \beta, \text{Pr},\) and \(\text{Ec}\). It is depicted from Figure 13 that the magnitude value of the temperature profile increases with an increase in \(\text{We}\). It is observed from Figure 14 that the magnitude value of the temperature profile decreases with an increase in \(\beta\). Figures 15 and 16 show the temperature profile for different values of \(\text{Pr}\) and \(\text{Ec}\). It is observed from Figures 15 and 16 that temperature profile increases with an increase in \(\text{Pr}\) and \(\text{Ec}\). Velocity profile for different values of \(\beta, Q,\) and \(\text{We}\) is plotted in Figures 17–19. It is observed from Figures 17 and 18 that the magnitude value of the velocity profile decreases with an increase in \(\beta\) volume flow rate \(Q\). It is depicted from Figure 19 that the magnitude value of the velocity profile increases with an increase in \(\text{We}\). Stream lines for different values of aspect ratio \(\beta\) amplitude ratio \(\phi\), power law index \(n\), and Weissenberg number \(\text{We}\) is plotted in Figures 20–23. It is observed from Figure 20 that the number of the trapping bolus decreases with an increase in aspect ratio \(\beta\). It is observed from Figures 21 and 22 that the size of the trapping bolus increases with an increase in power law index \(n\) and amplitude ratio \(\phi\). Figure 23 shows the stream lines for different values of the Weissenberg number \(\text{We}\). It is depicted from Figure 23 that the number of the trapping bolus increases in the lower half of the channel with an increase in \(\text{We}\), while in the upper half of the channel the size
Figure 24: Stream lines for different wave forms (a) for the sinusoidal wave, (b) for the multisinsoidal wave, (c) for the square wave, (d) for the trapezoidal wave, and (e) for the triangular wave. The other parameters are $n = -0.8$, $\beta = 6$, $\varphi = 0.7$, $y = 1$, $We = 0.53$, and $Q = 3.3$. 
of the trapping bolus increases. Figure 24 shows the stream lines for different wave forms.

6. Conclusion

We have discussed the impact of heat transfer on peristaltic flow of a Carreau fluid in a rectangular duct with different wave forms. The governing equations for a three-dimensional rectangular channel are the first model for Carreau fluid and then simplified under long wave length and low Reynolds number approximation. The analytical solutions of highly nonlinear equations are calculated. The results are discussed through graphs. It is observed that pumping rate decreases with an increase in aspect ratio $\beta$ and We in the peristaltic ($\Delta p > 0$, $Q > 0$) and retrograde pumping ($\Delta p > 0$, $Q < 0$) regions, while in the copumping region ($\Delta p < 0$, $Q > 0$), the behavior is quite opposite. It is also noted that in the retrograde pumping ($\Delta p > 0$, $Q < 0$) and peristaltic pumping ($\Delta p > 0$, $Q > 0$) regions, the pumping rate increases with an increase in $n$ and $\varphi$. It is observed that the profile of temperature increases with an increase in We, Pr, and Ec, while temperature profile shows the opposite behavior in the case of $\beta$. It is also observed that number of trapping bolus increases in the lower half of the channel with an increase in We, while in the upper half of the channel, size of the trapping bolus increases.

Nomenclature

$a,b$: Amplitudes of waves
$c$: Velocity of propagation
$X$: Direction of wave propagation
$C'$: Specific heat
$T$: Temperature
$\delta$: Dimensionless wave number
$\beta$: Aspect ratio
$We$: Weissenberg number
$n$: Power law index
$\theta$: Temperature of fluid in dimensionless form
$\lambda$: Wavelength
$t$: Time
$\rho$: Density
$P$: Pressure
$Re$: Reynolds number
$Q$: Volume flow rate
$Pr$: Prandtl number
$\varphi$: Amplitude ratio
$Ec$: Eckert number
$S$: Stress tensor for Carreau fluid.

Data Availability

Data used to support the findings of this work are included in the article.

Conflicts of Interest

The authors declare no conflict of interest.

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