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Predicting dynamic geotechnical parameters in near-surface coastal environment

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Abstract: Conduction of geotechnical survey prior construction is a non-negotiable requirement before the erection of any engineering structure so as to avoid building collapse which has been rampant in our country of late. An easier, faster and relatively cheaper approach to conducting a comprehensive geotechnical investigation for site characterization without compromise to standards was the focus of this study. Seismic refraction method; a quick, non-destructive and non-intrusive method of obtaining key subsoil geotechnical properties necessary for foundation design for proposed engineering facilities was suggested. This approach was used to generate some seismic parameters, which are very relevant to geotechnical investigation. The seismic wave velocities generated from near surface refraction method was used to determine the allowable bearing capacity, the ultimate bearing pressure, and the liquefaction potential so as to delineate the most competent layer. The seismic refraction method delineated two layers, with the result of the allowable bearing capacity ranging between 0.092 and 0.593 MPa, the ultimate bearing capacity varied from 0.369 to 2.298 MPa while the result of the liquefaction potential varied between 0.533 and 1.237. In all, it was observed that the second layer is more competent than the first layer. Furthermore, regression equations were derived for both geotechnical parameters in order to directly derive the geotechnical parameters from the compressional wave velocities. The results obtained correlated with the results of standard geotechnical investigations carried out, which

ABOUT THE AUTHOR
Adewoyin Olusegun Oladotun The authors are a group of young and dynamic researchers with common interest in conducting researches on subjects that directly affect man. They have published articles in different areas that are related to human safety and environment. The authors conducted this research in order to proffer solution to the untold hardship and risk people are exposed to as a result of building collapse in Nigeria. Other than geotechnical studies carried out in this article, the authors have also conducted researches in various areas of human concern such as, water contamination and remedy, heavy metal content in commonly consumed food items and the radionuclide contents in building tiles. The authors will always be committed to a safe environment and a quality life for all.

PUBLIC INTEREST STATEMENT
The recent cases of building collapse have become a concern to both the Government and the stakeholders in the building industry. This is because of the number of lives that are lost and the resources that are wastes in the process. One factor that often prevents building contractors from carrying out geotechnical surveys before embarking on building construction is the cost. This study has made effort to use seismic refraction method to characterize the area of study. The result obtained was correlated with borehole data, which presented the depth to the most competent layer in the study area to be at the depth between 7 and 15.4 m into the subsurface. This approach is much faster, cheaper, environment friendly and provided wider coverage of site investigation than the conventional geotechnical method. The results obtained was used to develop models that could relate p-wave velocities with some interested geotechnical parameters.
implies that the competence of any site having the same geological formation could be
determined using the same approach.

Subjects: Earth Sciences; Geology - Earth Sciences; Geophysics

Keywords: Site characterization; geotechnical; allowable bearing capacity; regression
equation; liquefaction potential

1. Introduction
The difficulty, delay and high expenses, involved in conducting a geotechnical investigation are few of
the factors that discourage many building developers from carrying out site characterization. These
have made many private developers carry out various construction projects without undertaking
proper site investigation (Abudeif, Raef, Abdel Maneim, Mohammed, & Farrag, 2017; Adewoyin,
Joshua, Akinwumi, Omeje, & Joel, 2017). One of the consequences of this is its significant contribution
to the incessant building collapse experienced in many developing countries. An attempt to simplify,
reduce the cost and reliably estimate the geotechnical parameters needed for proper foundation
design will be a major contribution to the field of geotechnical engineering. Using geophysical
techniques to predict the required geotechnical parameters has the potential to make this contribu-
tion. Typically, the results of geotechnical tests are for point measurements but geophysical investi-
gation techniques can give volumetric measurement and produce an image of the subsurface
without physically disturbing the subsoil (Mohd, Rosli, Fauziah, Devapriya, & Mohamed, 2012).

Geophysical technique such as seismic refraction method has the potential to provide a quick
test, to characterize and model a site and recommend regions recommended for detailed geo-
technical investigation when employed (Atat, Akpabio, & George, 2013; Lucas, Frankhauser, &
Springman, 2017). Many geo-mechanical parameters of the subsurface soils can be adequately
characterized by the propagation of elastic waves in soil deposits. Many soil properties may be
obtained by the use of seismic wave method; such properties include elastic properties and shear
strength (Bery & Saad, 2012; Fitzallen, 2012).

Studies have shown that both P- and S-waves are affected differently by changes in saturation,
porosity, or elastic moduli (Nastaran, 2012; Pegah & Liu, 2016; Sayeed, Adel, & Abd El-Aal, 2007;
Tezcan, Ozdemir, & Keceli, 2009). Salem (2000) deployed both P-wave and S-wave velocities to estimate
the Poisson's ratio of unsaturated natural soil deposits. Hunter et al. (2002) relied on seismic wave
velocities to understand the ground motion response of thick soil sites. Michael and Rucker (2006)
revealed that seismic wave methods could provide effective shallow subsurface characterization for
geotechnical engineering applications. Ozener (2012) estimated the residual shear strength of liquefied
soil deposits based on the shear wave velocities. Altindag (2012) studied the relationship between
p-wave velocity and mechanical properties of sedimentary rocks. He used an already acquired data
and simple regression analysis. All the data were later subjected to multi-regression analysis. He also
derived some empirical equations with high correlation coefficients which would be useful for rock
engineers (Sopios, Papazachos, Vargemezis, & Fikos, 2005). The compressional wave is the only wave
that is paramount in this study. In order to determine the zones of structural weakness in the basement
and analyze the stability of the subsurface and obtain the mechanical properties of rocks, there will be
need to evaluate seismic velocities, Vp and Vs obtained during the field survey (Uyanik, 2010). In this
study, near-surface seismic refraction method was used to generate mathematical equations that could
be used to determine the geotechnical parameters of a site prior construction.

1.1. Geology and location of the study area
The area under investigation lies within a part of the geologically termed alluvium deposits of
Southwestern Nigeria Basin, which is an integral part of the Dahomey embayment (Figure 1). The
superficial materials of the general area under investigation are silts, sands and clays with fibrous
peat at the surface in some places. The vegetation at the study area has given way to fens and
other water-loving shrubs and herbs (Adegbola & Badmus, 2014). The study area lies between latitude 06° 26’ N and 06° 32’ N and longitude 03° 35’ E and 03° 45’ E in Lagos Island area of Lagos State. The choice of Lagos Island as the study area is based on the fact that most part of this area is reclaimed from water using sand. The Nigeria coastal zone is within the tropical climate area which has two seasons: the rainy season and the dry season. The rainy season is between April and November, while the dry season is between December and March. The amount of annual rainfall varies between 2030 and 2540 mm (Obasi & Ikubuwaje, 2012).

2. Methodology
Seismic refraction method was carried out, using a 24-Channel ABEM Terraloc Mark 6 seismogram (ABEM Instrument, 1996). This method requires the following for its functionality; 12V-DC Battery, a roll of trigger cable, 2 seismic cable reels, a 15 kg sledge hammer, a metal base plate, 24 geophones of 14 Hertz frequency, a log book and measuring tapes. Four traverses were marked forming a square shape (Figure 2). The geophones were planted at 2 m interval to each other and then connected to the equipment. Along a single traverse that ranged between 100 and 150 m in length, due to accessibility, the geophones were planted on every 50 m length on each profile and later transferred to the remaining portion of the profile. This implies that measurements were taken in multiples of 50 m. The length of the traverses ranged between 100 m and 150 m. The geometry used for the data acquisition consisted of five shots taken at different positions between the geophones and at 2 m off each end of the spread. The first shot was taken at a position 2 m from the 1st geophone, between the 6th and the 7th geophones, also between the 12th and 13th geophones, similarly in the midst of the 18th and 19th geophones and finally 2 m after the 24th geophone. The same procedure was repeated across the length of the profile until the desired length is covered.

Plates 1: Image of the (a) array of geophones and (b) seismogram with a power source

The p-wave energy source was a 15 kg sledge hammer (Adewoyin et al., 2017). SeisImager software was used to produce the 2D seismic image of the data collected (Figure 3). Each traverse showed two geological layers with the topmost layer being characterized with low p-wave velocities which may be as a result of the loose and soft nature of the soil. The second layer, on the other hand, showed materials of relatively higher velocities which may be due to saturation and compression of the material in the subsurface. The significant change noticed in the elastic properties of the two layers may be due to change in the composition of the subsurface, uneven saturation and changes in the unit weight of the soil.

Figure 1. Geological map of Nigeria, showing the Nigerian part of the Dahomey basin (Aizebeokhai and Oyeyemi, 2014).
3. Results and discussion

The results obtained are presented as follows. Two geologic layers were delineated by the SeisImager software (Abudeif et al., 2017; SeisImager, 2009). The depth of investigation varied from the topsoil to a depth of about 15 m in the subsurface. The limitation in the depth of coverage could be as a result of the energy source that was used or the length of profile deployed. Some theoretical models were used to determine some of the geotechnical parameters, such as the bulk density, ultimate bearing and allowable bearing capacities, considered in this study (Tezcan et al., 2009; Fitzallen, 2012; Atat et al., 2013). The first geologic layer has the lower seismic wave velocity while the second geologic layer has the higher seismic wave velocity. The bulk density of the first layer ranged between 1708.8 kg/m³ and 1745.7 kg/m³ while the bulk density of the second layer varied between 1752.7 kg/m³ and 2043.3 kg/m³. This result showed that the second layer is more compressed than the first layer. This may be as a result of the geologic composition of the soil, it could also be as a result of the level of saturation and level of cementation of this geologic formation. It was also observed that the density of the subsurface increased in direct proportion with the seismic wave velocity and these two parameters were noted to increase with depth.
The ultimate bearing capacity and the allowable bearing pressure were estimated alongside the results provided by the elastic moduli. The ultimate bearing capacity for the study area was noted to vary between 0.3674 MPa and 0.5575 MPa while it ranged between 0.5941 MPa and 2.3699 MPa in the second layer. This showed that the second layer could have more bearing capacity than the first layer. Also, the allowable bearing pressure ranged between 0.0919 MPa and 0.1394 MPa in the first layer while it ranged between 0.1485 MPa and 0.5925 MPa in the second layer. The result also showed that the second layer is more competent than the first layer. Furthermore, the result of the liquefaction potentials of the study area was discovered to vary between 0.533 and 0.649 in the first layer while it ranged between 0.669 and 1.237 in the second layer. This result revealed that the first layer has higher liquefaction potential than the second layer, although, there are some parts of the second layer that are also prone to liquefaction, which could be as a result of the variation in the thickness/depth of the first layer as shown in Figure 3. The result of the seismic refraction method correlated with that of the borehole dug in the study area (Figure 4). From the two data, it could be inferred that the depth to the

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**Figure 4. Result of the Borehole log obtained in the area of study.**

| Depth (m) | Samples | Soil Description                     | Symbol | Not  |
|----------|---------|-------------------------------------|--------|------|
| 0        |         | Dark brownish silty fine SAND       |        |      |
| 0.75     |         |                                     |        |      |
| 1.5      |         |                                     |        |      |
| 1.75     |         |                                     |        |      |
| 3        |         | Soft light yellowish sandy CLAY     |        |      |
| 3.75     |         |                                     |        |      |
| 4.5      |         |                                     |        |      |
| 5.25     |         |                                     |        |      |
| 6        |         | Soft dark greyish organic silty CLAY|        |      |
| 7.5      |         |                                     |        |      |
| 9        |         | Loose becoming medium dense light greyish silty SAND | 13 |      |
| 10.5     |         |                                     |        |      |
| 12       |         | Firm dark greyish organic CLAY      |        |      |
| 13.5     |         |                                     |        |      |
| 14.25    |         | Light greyish coarse SAND           |        |      |
| 15       |         |                                     |        |      |
| 16.5     |         | Soft to firm dark greyish organic sandy CLAY |       |     |
| 18       |         |                                     |        |      |
| 21.5     |         |                                     |        |      |
| 22       |         | Firm to stiff dark greyish organic CLAY |      |     |
| 24.5     |         |                                     |        |      |
| 26.25    |         | Light greyish coarse SAND           |        |      |
| 28       |         |                                     |        |      |
| 30       |         |                                     |        |      |

**End of Borehole**

**KEYS:**
- DISTURBED SAMPLE
- UNDISTURBED SAMPLE
most competent layer ranged between 7 m and 15.7 m. This result is in agreement with the results obtained from the borehole log and the cone penetrometer tests earlier conducted in the study area.

This study went further to obtain model equations from the correlations of the primary wave velocities and the different geotechnical parameters studied (Atat et al., 2013; Tezcan et al., 2009). This is to obtain direct relationships between the p-wave velocity and the geotechnical parameters. These equations could be used for speedy evaluation and inexpensive estimation of the various geotechnical parameters. The graphs of the geotechnical parameters were plotted against the primary wave velocity. The regression equations and their coefficient of determinations were obtained. Also, the graph of ultimate bearing capacity was plotted against the primary wave velocity (Figure 5) and the correlation equation is given as

$$q_f = 0.0005V_p^{1.1042}$$ (1)

The correlation coefficient obtained for this relation is 0.9995.

The correlation equation derived from the graph of allowable bearing capacity versus the primary wave velocity (Figure 6) is, with a correlation coefficient of 0.9994.
In a similar vein, the graph of liquefaction potentiality was plotted against the primary wave velocity as presented in Figure 7. The correlation equation derived was found to be

\[ N = 0.0283V_p^{0.4968} \]  

(3)

The estimated correlation coefficient, in this case, was found to be 0.9993.

4. Conclusion

Geophysical survey was carried out using seismic refraction method, the results obtained were correlated with the results from other geotechnical methods. The results of the seismic refraction method revealed two geologic layers with the values of bulk density, ultimate bearing capacity and allowable bearing potential greater in the second layer than in the first layer making the second layer more competent. The results of the geotechnical method also confirmed the result obtained from the seismic refraction method. There was a correlation between the depths of competence delineated by the seismic refraction method and the borehole data obtained in the study area. Also, equation models that related both the p-wave velocities with other geotechnical parameters in the area of study were developed. This approach could ease the process of site characterization of the subsurface condition of the study area. Furthermore, the empirical equations obtained can be used to evaluate and predict the geotechnical parameters of a site, when information on the p-wave velocity is available. This study presents an approach that has the potential to reduce the cost of geotechnical investigations and also protect our environments from the destruction caused by the invasive nature of geotechnical equipment.

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