Simple and Economical Method to Create Thoracolumbar Burst Fracture in a Calf Spine Model

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Study Design: Calf spine model study.

Purpose: To describe a technique of creating thoracolumbar burst fractures in calf spine model by low weight drop weight.

Overview of Literature: Burst fractures are one of the commonest types of thoracolumbar fractures and their treatment is controversial. Biomechanical studies aid in the decision of treatment of these fractures. A simple method of creation of burst fractures would help these biomechanical studies.

Methods: Ten specimens of thoracolumbar spines harvested from 6–8 week old calves were weakened at the target vertebra by standardized osteotomy cuts. Burst fractures were created by dropping a 5-kg weight from a height of 1.2 m using an in-house device. An accelerometer attached to the weight measured the acceleration at the point of impact.

Results: Average weight and bone mineral density of the specimens was 390 g and 0.67 g/cm², respectively. Computed tomography scan analysis of the fractures revealed McCormack grade 2 and grade 3 fractures in 5 and 3 specimens, respectively, Dennis type 2B in 4, type 2A burst fractures in 5 specimens and fracture dislocation in 1 specimen, AO type A3.1.1 in 4 specimens, type A3.2.2 in 4 and type A3.3.3 in 2 specimens. Vertical laminar split fracture was seen in 6 specimens. Average acceleration and energy at impact was 9.04 m/sec and 54.24 Nm, respectively.

Conclusions: We describe a technique to create thoracolumbar burst fractures in calf spine by a drop weight method using a device that is simple to operate and easy to construct. The method is consistent and produces fractures similar to those occurring naturally, and can be considered as an alternative method for creating burst fractures in biomechanical studies.

Keywords: Spine; Calf; Burst; Fracture

Introduction

Burst fractures are one of the most common types of fractures encountered in clinical practice, accounting for more than two-thirds of all types of thoracolumbar vertebral fractures [1]. Burst fractures were initially described by Holdsworth [2] and were later classified by Denis [3] as type II and by AO as type A3 fractures [1]. As described by Magerl et al. [1], these fractures are caused by axial compression with or without flexion, and are characterized by partial or complete comminution of the vertebral body with retropulsion of posterior wall fragments. The
posterior ligamentous complex remains intact and the posterior arch injury, if present, is always a vertical split of lamina, which does not contribute to stability [1]. The treatment of these fractures is controversial and varies from conservative to long posterior or combined anterior and posterior fixation [4]. Biomechanical studies can aid in decision making concerning the treatment of these fractures.

A number of methods have been described for creating burst fractures \textit{in vitro}, to perform biomechanical studies in both human cadavers and animal spine models. However, many of these methods involve complex devices, are not reproducible or do not mimic the fractures occurring by natural process. Even though the human cadaveric spine is ideal for these studies to produce comparable results with clinical trials, it may not be feasible in many centers because of their limited availability, risk of infection, and ethical and religious issues [5]. Calf spine has been shown to have mechanical and physical properties similar to that of human spine and so is a good substitute for biomechanical studies [6]. Vertebra from calves 6–8 weeks old have bone density and anatomical size similar to that of an adult human vertebra, and so can be ideal specimens for testing \textit{in vitro} [5].

However, there are subtle differences between the calf and human spine, which include the lower range of flexion and extension of calf spine compared to the human spine [5]. Furthermore, the properties of the end plate in immature calf spine in comparison to the adult spine have not been studied [7]. Because of these differences the technique described for creating burst fractures in human cadaveric spine cannot be directly applied to calf spine.

We describe a simple technique using an inexpensive and easily constructible device producing a burst fracture in an immature calf spine model that is easily reproducible and mimics the fracture occurring naturally.

1. Study design

Calf spine model study.

Materials and Methods

Ten specimens of thoracolumbar spine were acquired from 6–8 week old calves at a local slaughter house. Specimens were prepared so that each specimen consisted of five vertebrae from the second-last thoracic to third lumbar vertebra with disco-ligamentous structures. The specimens were dissected off the muscles and separated from the ribs to preserve the ligaments. They were stored by freezing at $-4^\circ$C. Plain radiographs and computed tomography (CT) scan of the specimens were taken to rule out any bony pathology and bone mineral density (BMD) of each specimen was measured using dual energy X-ray absorptiometry scanning (Fig. 1).

The device for creating the fracture was manufactured
at a workshop using locally available materials. It consisted of a rectangular base measuring 0.61×0.61 m with two parallel cylindrical rods of 3.8 cm diameter welded to the base. The rods were cross connected on the top using a bar with a cylindrical ring in the center that would allow another cylindrical rod 3.8 cm in diameter. Through the central ring on the top cross bar, another cylindrical rod of 3.8 cm diameter was passed through and an hemispherical impactor was attached to the end. This central rod acted as a guide for dropping the weight. A 5-kg weight was allowed to freely glide through this central post and was kept at a height of 1.2 m using a cross pin. An accelerometer was attached to the weight to calculate the pre-impact acceleration (Fig. 2).

The night before testing, the specimens were thawed in normal saline. Upper and lower vertebrae were mounted on dental cement and moulded into cup shapes. The index vertebra was weekend using a 1-cm wide osteotome. The cuts were standardized to all specimens. Three cuts were made: two were anterior posterior and one was medio-lateral through the upper end plate. The cuts divided the upper half of the body and upper end plate into six segments. The anterior posterior cuts extended into the posterior cortex, as confirmed by a sensation of giving way. Posterior elements remained undisturbed (Fig. 3).

The specimen was placed over the cylindrical support on the base of the device and fixed firmly by packing with non-compressible foam on the sides. The impactor was placed on the upper end of the mounted specimen. The specimen was positioned so that the point of contact of the impactor on the cement mould was anterior to the centre, thereby giving a flexion force when the weight was dropped. The 5-kg weight was dropped from a height of 1.2 m. The device attached to the weight measured the acceleration and the energy transmitted at the point of impact was calculated from the formula E=mah; where ‘m’ is the weight of the mass dropped (5 kg), ‘a’ is the pre-impact acceleration and ‘h’ is the height from which the mass was dropped (1.2 m).

**Results**

The weight of the specimens ranged from 350–460 g with an average weight of 390 g. The average BMD of the specimens was 0.67 g/cm². The 5 kg weight when dropped freely from a height of 1.2 m, produce an average acceleration of 9.1 m/sec as recorded by the accelerometer attached to the weight. The average energy at the point impact was calculated to be 54.24 Nm (range, 53.4–54.6 Nm) (Table 1).

CT scan analysis of the fractures revealed partial or complete comminution of the vertebral body in all the specimens with the fracture line extending to the posterior vertebral wall and retropulsion of the fragments with
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...confirming the burst type. Vertical split fractures of the lamina, a characteristic feature of burst fracture [1], was seen in 6 specimens. The facets and the posterior ligamentous complex remained intact in all the specimens, except in specimen 4. This specimen showed disruption of the posterior ligamentous complex with an anterior translation and subluxation of the facets along with comminution of the vertebral body (Figs. 4, 5).

The fractures created were classified by the McCormack, Dennis, and AO standard classification schemes. In McCormack load sharing classification, burst fractures are classified into three grades based on the comminution, opposition and angle of corrected kyphosis [8]. Our technique resulted in grade 2 fractures in 5 specimens and grade 3 in the remaining 5. Dennis classified thoracolumbar fractures into four types: wedge, burst, flexion distraction and fracture dislocation. Burst fractures are further subclassified into A, B, and C depending on whether the fracture involved both endplates or only the upper or the lower end plate [2]. In our series, burst fractures occurred in 9 specimens, while one specimen showed fracture dislocation (specimen 4). In 4 specimens fracture occurred in the vertebra below the level of the impact and in 3 specimens both vertebrae were involved.

Table 1. Description of the specimen details and fracture patterns

| Specimen | Weight (g) | BMD   | Acceleration | Energy at impact | Pedicles | Translation | McCormack grade | AO type | Dennis type | Vertical lamina fracture | Posterior elements | Facets | Posterior bodywall | Retropulsion |
|----------|------------|-------|---------------|------------------|----------|-------------|-----------------|---------|-------------|------------------------|-------------------|--------|------------------|-------------|
| 1        | 450        | 0.717 | 8.9           | 53.4             | Intact   | Absent      | Grade 2         | A 3.1.1 | Type 2B    | Absent                 | Intact            | Intact | Fractured        | Present     |
| 2        | 460        | 0.877 | 9             | 54               | Intact   | Absent      | Grade 2         | A 3.1.1 | Type 2B    | Absent                 | Intact            | Intact | Fractured        | Present     |
| 3        | 380        | 0.603 | 9.1           | 54.6             | Intact   | Absent      | Grade 2         | A 3.2.1 | Type 2A    | Absent                 | Intact            | Intact | Fractured        | Present     |
| 4        | 400        | 0.736 | 9             | 54               | Intact   | Present     | Grade 3         | B 2.1 + A 3.3.3 | Type 4A | Present     | Disrupted             | Subluxed         | Fractured | Present         | Present     |
| 5        | 390        | 0.666 | 9.1           | 54.6             | Intact   | Absent      | Grade 3         | A 3.2.1 | Type 2A    | Absent                 | Intact            | Intact | Fractured        | Present     |
| 6        | 380        | 0.646 | 9.1           | 54.6             | Intact   | Absent      | Grade 2         | A 3.1.1 | Type 2B    | Absent                 | Intact            | Intact | Fractured        | Present     |
| 7        | 360        | 0.606 | 9.1           | 54.6             | Intact   | Absent      | Grade 3         | A 3.2.1 | Type 2A    | Absent                 | Intact            | Intact | Fractured        | Present     |
| 8        | 350        | 0.537 | 9.1           | 54.6             | Intact   | Absent      | Grade 2         | A 3.2.1 | Type 2A    | Absent                 | Intact            | Intact | Fractured        | Present     |
| 9        | 360        | 0.636 | 9             | 54               | Intact   | Absent      | Grade 2         | A 3.1.1 | Type 2B    | Absent                 | Intact            | Intact | Fractured        | Present     |
| 10       | 370        | 0.639 | 9             | 54               | Intact   | Absent      | Grade 2         | A 3.1.1 | Type 2B    | Absent                 | Intact            | Intact | Fractured        | Present     |

BMD, bone mineral density.
limited to upper endplate causing type 2B fractures, while
the remaining 5 specimens showed fracture extending to
the lower end plate resulting in type 2A fractures. As per
the AO classification [1] 4 specimens showed incomplete
burst fractures involving superior endplate represent-
ing AO type A3.1.1. Another 4 specimens showed burst
fracture in the upper endplate with split in the lower half
representing type AO A3.2.1. In 2 specimens, the com-
mination involved entire vertebral body representing AO
type A3.3.3 fracture. One specimen showed complete
burst fracture anteriorly with disruption of posterior liga-
mentous complex and anterior translation representing
AO type B1.2.1+A3.3.3.

Discussion

Creating a burst fracture is the first step of in vitro biome-
chanical experiments studying thoracolumbar burst frac-
tures. A variety of methods have been described to create
thoracolumbar burst fractures in both human cadaveric
and animal spine models. These methods can be classified
basically into 3 types—axial compression either by drop
weight or by servohydraulic devices, surgical destabiliza-
tion or a combination of surgical destabilization with axial
compression.

Table 2 [7,9-13] summarizes the literature describing
the methods of creating thoracolumbar burst fractures
in human cadaveric vertebra. Every method has its own
advantages and disadvantages. Surgical destabilization
alone by fracturing the vertebral body with drill bits do
not mimic that occurring naturally because of absence of
retropulsion of the fragments of the vertebral body [9].
Moreover, most of these methods involve cutting pos-
terior ligamentous complex or the facet capsule, which
is not a feature of typical burst fracture [9,10]. Burst
fractures by axial compression can be produced by drop
weight through a specially designed apparatus or by ser-
vohydraulic compressive devices. Servohydraulic devices
can produce high compressive forces but these devices are
expensive and not accessible in many centers [7]. Creating
burst fractures by a single impact by drop weight alone
are ideal methods, mimicking naturally occurring mecha-
nism. However these methods generally involve large
weights and the apparatus for dropping them are bulky,
have complex designs and are difficult to reconstruct
[11,13]. Moreover, many of these studies did not have
a detailed description of the design of the apparatus or
the technique of dropping weight [11,12]. Some of these
methods protect the non-targeted vertebrae by weakening
them, making the specimen unsuitable for further studies
[7].

The methods described for creating burst fractures in
human cadaveric vertebrae cannot be directly applied to
calf spine because of the subtle differences between the
two. The calf spine is more rigid and has a lesser range of
flexion and extension movement [5]. Hence, flexing the
specimen to 10–15 degrees, which is essential for creat-
ing burst fractures by axial compression, is difficult to
achieve in calf spine. The characteristics of the endplates
and the disc of calf spine in comparison to adult human
spine have not been studied [7]. In our initial attempts,
we found the endplates of calf spine to be more elastic
and tough, and difficult to fracture even with larger
weights by methods described for human cadaveric
spine. Moreover using larger weights resulted in fracture
of the vertebral body with intact endplates. We failed to
produce burst fractures similar to naturally occurring
ones in calf spine by drop weight alone without surgical
weakening.

Table 3 [7,14-17] summarizes the literature describing the methods of creating a burst fractures in calf spine models. A method described by drop weight alone used a large weight (100 kg), yet produced burst fractures only in 13 of 24 specimens [14]. Most of the methods employed surgical pre-stressing or osteotomy cuts in the target vertebral prior to axial compression [7,15]. Surgical pre-stressing methods again employs larger weights with bulky apparatus. Different methods of osteotomy cuts have been described, but some of these do not produce naturally occurring patterns of the burst fracture [5]. Standardized osteotomy followed by axial compression by servohydraulic devices produced fractures in all the cadaveric specimens, but consistently failed to produce similar fractures in calf spine [7].

### Table 2. Analysis of methods of creating thoracolumbar burst fractures in human cadaveric spine described in the literature

| Study | Method | Technique in detail | Sample size | Analysis by CT scan | Consistency (%) | Positives | Negatives |
|-------|--------|---------------------|-------------|---------------------|-----------------|-----------|-----------|
| Lazaro et al. [9] | Surgical destabilisation | All, supra and interspinous ligaments cut and vertebral body fractured with thin cutting drill bit | - | No | Nil | Simple technique, no apparatus | Did not mimic naturally occurring fractures, 3 column injury with damage to posterior ligaments, did not produce burst fractures |
| Hartensuer et al. [7] | Surgical weakening with axial loading | Standardised osteotomy cuts and axial loading by servohydraulic device | 7 | Yes | 100 | Produce naturally occurring burst fractures, consistent | Used expensive complex hydraulic device, weakened other bones fixed by plate |
| Kallemeier et al. [10] | Surgical weakening and drop weight | Stress raisers by brr, 6–8 kg of weight dropped, repeated until burst fracture, interspinous ligaments and facet capsule cut | 9 | Yes | 100 | Simple apparatus, consistently produced type B2.1 with anterior burst | Not typical burst fracture, posterior ligaments damaged, repeated dropping of weight |
| Fredrickson et al. [11] | Drop weight | Height of 1 m, force of 260–300 nm | 6 | Yes | 100 | Simple apparatus | No detailed description of apparatus, technique or fracture pattern produced, large weight (approximately 30 kg) |
| Mermelstein et al. [12] | Surgical weakening with axial loading | 4.5 kg dropped from 1.25 m height with 10 degrees flexion after weakening of anterior cortex with osteotome | 6 | No | - | Low weight | Technique, design of apparatus and fracture pattern not described in details |
| Jones et al. [13] | Drop weight | 25 kg dropped from a height of 1 m with specimen at 15 degrees flexion using a specially designed apparatus | 5 | Yes | 100 | Consistent, no surgical weakening, details of apparatus and technique described | Large weight, complex bulky apparatus |

CT, computed tomography.
We describe a method of creating burst fracture in calf spine by standardized osteotomy cuts followed by drop weight. Osteotomy cuts extended to the posterior body wall and the fragments were retropulsed following drop weight, which mimicked naturally occurring burst fractures. The drop weight device had a simple design and was constructed at a local workshop from easily available materials. We employed a low weight and the impact at the anterior aspect of the specimen ensured that the force was transmitted to vertebral bodies preserving the facets and the posterior ligamentous complex. It also created vertical laminar split fractures in 6 specimens, which is characteristic of burst fractures. Disruption of the posterior ligamentous complex with facet subluxation and anterior translation occurred in one specimen, which was possibly due accidental posterior slipping of the point of impact, loading the facets.

**Conclusions**

We describe a simple technique of creating thoracolumbar burst fractures in a calf spine model. The technique involves low weight and the apparatus used for dropping weight can be easily constructed. The fractures produced...
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mimic those occurring naturally and can be reproduced consistently. This can be considered as an alternative technique for biomechanical experiments studying burst fractures.

Conflict of Interest

No potential conflict of interest relevant to this article was reported.

References

1. Magerl F, Aebi M, Gertzbein SD, Harms J, Nazarian S. A comprehensive classification of thoracic and lumbar injuries. Eur Spine J 1994;3:184-201.
2. Holdsworth F. Fractures, dislocations, and fracture-dislocations of the spine. J Bone Joint Surg Am 1970;52:1534-51.
3. Denis F. The three column spine and its significance in the classification of acute thoracolumbar spinal injuries. Spine (Phila Pa 1976) 1983;8:817-31.
4. Fakurnejad S, Scheer JK, Patwardhan AG, Havey RM, Voronov LI, Smith ZA. Biomechanics of thoracolumbar burst fractures: methods of induction and treatments. J Clin Neurosci 2014;21:2059-64.
5. Wilke HJ, Krischak ST, Wenger KH, Claes LE. Load-displacement properties of the thoracolumbar calf spine: experimental results and comparison to known human data. Eur Spine J 1997;6:129-37.
6. Swartz DE, Wittenberg RH, Shea M, White AA 3rd, Hayes WC. Physical and mechanical properties of calf lumbosacral trabecular bone. J Biomech 1991;24:1059-68.
7. Hartensuer R, Gasch A, Gehweiler D, et al. Experimentally induced incomplete burst fractures: a novel technique for calf and human specimens. BMC Musculoskelet Disord 2012;13:45.
8. McCormack T, Karaïkovic E, Gaines RW. The load sharing classification of spine fractures. Spine (Phila Pa 1976) 1994;19:1741-4.
9. Lazaro BC, Deniz FE, Brasiliense LB, et al. Biomechanics of thoracic short versus long fixation after 3-column injury. J Neurosurg Spine 2011;14:226-34.
10. Kallemeier PM, Beaubien BP, Buttermann GR, Polga DJ, Wood KB. In vitro analysis of anterior and posterior fixation in an experimental unstable burst fracture model. J Spinal Disord Tech 2008;21:216-24.
11. Fredrickson BE, Edwards WT, Rauschning W, Bayley JC, Yuan HA. Vertebral burst fractures: an experimental, morphologic, and radiographic study. Spine (Phila Pa 1976) 1992;17:1012-21.
12. Mermelstein LE, McLain RF, Yerby SA. Reinforcement of thoracolumbar burst fractures with calcium phosphate cement: a biomechanical study. Spine (Phila Pa 1976) 1998;23:664-70.
13. Jones HL, Crawley AL, Noble PC, Schoenfeld AJ, Weiner BK. A novel method for the reproducible production of thoracolumbar burst fractures in human cadaveric specimens. Spine J 2011;11:447-51.
14. Cain JE Jr, DeJong JT, Dinenberg AS, Stefko RM, Platenburg RC, Lauerman WC. Pathomechanical analysis of thoracolumbar burst fracture reduction: a calf spine model. Spine (Phila Pa 1976) 1993;18:1647-54.
15. Cotterill PC, Kostuik JP, Wilson JA, Fernie GR, Maki BE. Production of a reproducible spinal burst fracture for use in biomechanical testing. J Orthop Res 1987;5:462-5.
16. Wang H, Li C, Liu T, Zhao WD, Zhou Y. Biomechanical efficacy of monoaxial or polyaxial pedicle screw and additional screw insertion at the level of fracture, in lumbar burst fracture: an experimental study. Indian J Orthop 2012;46:395-401.
17. Turker M, Tezeren G, Tukenmez M, Percin S. Indirect spinal canal decompression of vertebral burst fracture in calf model. Arch Orthop Trauma Surg 2005;125:336-41.