Phase diagram of Fe-doped Ni-Mn-Ga ferromagnetic shape-memory alloys

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We have studied the effect of Fe addition on the structural and magnetic transitions in the magnetic shape memory alloy Ni-Mn-Ga by substituting systematically each atomic species by Fe. Calorimetric and AC susceptibility measurements have been carried out in order to study the magnetic and structural transformation properties. We find that the addition of Fe modifies the structural and magnetic transformation temperatures. Magnetic transition temperatures are displaced to higher values when Fe is substituted into Ni-Mn-Ga, while martensitic and premartensitic transformation temperatures shift to lower values. Moreover, it has been found that the electron per atom concentration essentially governs the phase stability in the quaternary system. However, the observed scaling of transition temperatures with $e/a$ differs from that reported in the related ternary system Ni-Mn-Ga.

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I. INTRODUCTION

Magnetic shape-memory alloys have drawn much attention in recent years owing to their unique magnetomechanical properties such as magnetic shape-memory [1] and the magnetic superelasticity [2]. These properties are a consequence of a strong coupling between magnetic and structural degrees of freedom. The prototypical and first discovered magnetic shape-memory material is the Heusler Ni$_2$MnGa [3]. This alloy undergoes a complex multi-stage transformation process from a high temperature paramagnetic cubic phase to a ferromagnetic martensitic phase. At intermediate temperatures it shows precursor tweed textures which may lock (via a first-order phase transition) into a modulated premartensitic structure due to the freezing of a specific phonon with a given wave vector. This behavior appears to be related to low resistance against distortions of the $\{110\}$ planes along the $\langle 110 \rangle$ directions and is evidenced by the features of the low energy TA$_2$ acoustic phonon branch $\Gamma \rightarrow R \rightarrow \Gamma$ and the low value of the elastic constant $C_{44}$ [4, 5, 6, 7]. While these features are essentially inherent to the high-temperature cubic structure, additional softening has been shown to arise from the coupling between structural and magnetic degrees of freedom [6, 7]. Thus, it has been suggested that the magnetostructural coupling is responsible for the phonon condensation yielding the intermediate modulated structure [11]. Nevertheless, the occurrence of a premartensitic phase is not yet a well understood phenomenon, as it only has been observed for a restricted number of magnetic shape memory alloys within limited composition ranges. Actually, the study of the structural (martensitic and premartensitic transformations) and magnetic properties of Ni-Mn-Ga alloys is a current topic of intense research [12, 13, 14, 15, 16, 17, 18].

The effect of doping elements on the martensitic and magnetic transformations in Ni-Mn-Ga alloys has received considerable attention [19, 20, 21, 22, 23, 24, 25]. However, the lack of a systematic study makes it difficult to compare directly the properties of different compounds. In the present paper, we investigate the dependence of transition temperatures (martensitic, intermediate and Curie) on the electron concentration by analyzing the effect of substituting Ni, Mn and Ga by Fe.

In all cases, the reference system is the stoichiometric Ni$_2$MnGa, which has a high temperature L2$_1$ structure ($Fm\bar{3}m$). This structure can be viewed as four interpenetrating fcc sublattices [in Wickoff notation, (4a)-1 is occupied by Mn-atoms, (4b)-2 by Ga-atoms, and (8c) by Ni-atoms]. The total magnetic moment is $\sim 4.1 \mu_B$ per formula unit and is largely confined to the Mn-sites contributing with $3.5 \mu_B$. 

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TABLE I: Compositions of the Ni-Mn-Ga-Fe samples determined by EDX. Different specimens are grouped into three distinct families, depending on the element that is substituted by Fe (elements within parenthesis, first column). The estimated error in the compositions is less than ±0.3%. Values of valence electron concentration per atom, $e/a$, are also given.

| Family   | Ni   | Mn   | Ga   | Fe   | $e/a$ |
|----------|------|------|------|------|-------|
| (Ni,Fe)  | 52.6 | 23.1 | 24.3 | 0 $^a$ | 7.606 |
|          | 51.3 | 22.8 | 24.5 | 1.4  | 7.573 |
|          | 50.1 | 23.1 | 24.6 | 2.2  | 7.541 |
|          | 49.3 | 23.1 | 24.5 | 3.1  | 7.530 |
|          | 48.1 | 23.0 | 24.5 | 4.4  | 7.507 |
|          | 47.0 | 23.1 | 24.6 | 5.3  | 7.479 |
| (Mn,Fe)  | 51.4 | 24.8 | 23.8 | 0 $^b$ | 7.589 |
|          | 51.5 | 24.2 | 23.5 | 0.8  | 7.613 |
|          | 51.1 | 24.6 | 23.4 | 0.9  | 7.606 |
|          | 51.7 | 23.1 | 23.4 | 1.8  | 7.633 |
| (Ga,Fe)  | 51.3 | 24.0 | 24.7 | 0 $^c$ | 7.551 |
|          | 51.2 | 24.2 | 23.8 | 0.8  | 7.592 |
|          | 51.8 | 24.8 | 21.7 | 1.7  | 7.703 |
|          | 51.3 | 24.5 | 22.2 | 2.0  | 7.671 |

$^a$Data extracted from reference 26. $^b$Data extracted from reference 25. Note that this composition slightly deviates (more than the experimental error, ±0.3%) from the fitted compositional line. $^c$Data extracted from reference 24. Note that this composition slightly deviates (more than the experimental error ±0.3%) from the fitted compositional line.

II. EXPERIMENTAL

Polycrystalline Ni-Mn-Ga-Fe ingots were prepared by arc melting pure metals under argon atmosphere in a water cooled Cu crucible. The ingots were melted several times for homogeneity and encapsulated under vacuum in quartz glass. They were then annealed at 1073 K for 72 hours to achieve a high degree of atomic order. Finally, the samples were quenched in ice-water. The compositions of the alloys were determined by energy dispersive x-ray photoluminescence analysis (EDX) with an estimated error less than ±0.3% (Table I). The alloys are grouped according to their compositions into the families $\text{Ni}_{52.5-x}\text{Mn}_{23}\text{Ga}_{24.5}\text{Fe}_x$ (1.2 $\leq x \leq 5.5$) for which Ni is replaced by Fe; $\text{Ni}_{51.4}\text{Mn}_{25.2-x}\text{Ga}_{23.4}\text{Fe}_x$ (0.8 $\leq x \leq 1.8$) for which Mn is replaced by Fe; and $\text{Ni}_{51.4}\text{Mn}_{24.5}\text{Ga}_{24.1-x}\text{Fe}_x$ (0.7 $\leq x \leq 2.0$) where Fe replaces Ga. The compositions are given in at%.

Specimens cut from the ingots using a low speed diamond saw (typical size $5 \times 1 \times 1 \text{ mm}^3$) were used as samples for susceptibility and calorimetric studies. Structural transition temperatures were obtained from AC susceptibility and calorimetric measurements. Magnetic susceptibility measurements were carried out in an AC susceptometer (LakeShore 7120A) in the temperature range 80 K $\leq T \leq 320$ K. The working parameters were 500 A m$^{-1}$ (6.28 Oe) applied field and 389 Hz frequency. For differential scanning calorimetry (DSC) measurements, one side of the samples was ground with SiC abrasive to ensure optimal thermal contact. Calorimetric measurements were carried out by means of a high sensitivity calorimeter in the temperature range 100 K $\leq T \leq 350$ K. Typical heating and cooling rates were 0.5 K min$^{-1}$. Magnetic transition temperatures were determined by means of a DSC calorimeter suitable for higher temperatures. All transition temperatures are affected by an error of ±1 K. The errors in entropy change are based on reproducibility and shown as errors bars in the figures.
FIG. 2: (a) Evolution of the transition temperatures of Ni$_{52.5-x}$Mn$_{23}$Ga$_{24.5}$Fe$_x$ as a function of Fe concentration. Open square and triangle symbols stand for data extracted from ref. [26]. (b) Entropy change at the martensitic transformation as a function of Fe concentration. Solid lines are linear fits to the experimental data.

FIG. 3: Ni$_{51.4}$Mn$_{25.2-x}$Ga$_{23.4}$Fe$_x$ family represented by the sample with $x = 1.8$. (a) Magnetic susceptibility versus temperature and (b) transformed fraction as a function of temperature, obtained by integration of the calorimetric curves (shown in the inset). Arrows in panel (b) and inset indicate direction of temperature change.

![Graph](image-url)

III. EXPERIMENTAL RESULTS

Eleven different alloys were studied in the present work. In this section, we present selected results of susceptibility and calorimetric measurements which are representative of each family. In the following the given Fe content is taken as the value corresponding to the fitted compositional line. From the complete set of data, we determine a phase diagram for each family and the transition entropy change at the martensitic transformation.

A. Substitution of Ni by Fe

Figure 1 shows the AC susceptibility and calorimetric curves for the sample with $x = 4.4$. The inset in figure 1(b) shows the calorimetric curves recorded on cooling and heating. The multiple peaks (noticeable in the thermograms corresponding to the forward transition on cooling) are a consequence of the well-known jerky character of martensitic transformations. On the other hand, the extra noise observed at the lowest temperatures in the thermograms on cooling is an artifact arising from the very low cooling rate in the low temperature regime (notice that $dQ/dT$ is obtained by dividing the calorimetric signal $\dot{Q}$ by $\dot{T}$). Figure 1(b) shows the austenitic transformed fraction, $y$ versus $T$, obtained from the calorimetric data shown in the inset. The austenitic transformed fraction is computed as $y = 1 - \Delta S(T)/\Delta S$ for the forward transition on cooling, and $y = \Delta S(T)/\Delta S$ for the reverse transition on heating, with $\Delta S(T) = \int_{T_i}^{T} (dQ/dT)/TdT$ ($T < T_i$ on cooling and $T > T_i$ on heating) and $\Delta S$, the entropy change at the martensitic transformation. This plot is illustrative for the typical results obtained for the Ni$_{52.5-x}$Mn$_{23}$Ga$_{24.5}$Fe$_x$ family. Both susceptibility and calorimetric measurements reveal the presence of a martensitic transformation. The corresponding transition temperatures are: martensite start temperature $M_s = 133$ K, martensite finish temperature $M_f = 119$ K, austenite start temperature $A_s = 132$ K and austenite finish temperature $A_f = 146$ K. The Curie point was determined from complementary DSC measurements as...
$T_C = 400$ K [shown in the inset of Fig. 1(a)]. Moreover, an additional feature is observed in the susceptibility curve at temperatures above the martensitic transition which is associated with the formation of the intermediate or premartensitic phase. The transition temperature is $T_f = 186$ K. No significant thermal hysteresis is detected at the premartensitic transition and no appreciable features are observed in the calorimetric curves at the premartensitic transition. This behaviour agrees with that observed in the related system Ni-Mn-Ga, where thermal anomalies are barely detected with differential scanning calorimetric techniques. By contrast, AC susceptibility measurements are very suited for the observation of the intermediate phase transition.

Figure 2(a) summarizes the results for the Ni$_{52.5-x}$Mn$_x$Ga$_{23.5}$Fe$_x$ family. To complete the picture, we have also included data for an $x = 0 \text{ sample}$ from reference 26. Transition temperatures are plotted as a function of the Fe concentration. All transition temperatures associated with the martensitic transformation ($M_s$, $M_f$, $A_s$ and $A_f$) follow the same $x$ dependence. Thus, for the sake of clarity, only $M_s$ temperatures are included. As can be seen from this figure, the martensitic transformation temperature decreases as the amount of Fe increases. In ternary Ni-Mn-X (X: Ga, Al, Sn, In and Sb) systems it is well established that martensitic transformation temperatures decrease as the valence electron concentration $e/a$ decreases. When replacing Ni by Fe, $e/a$ decreases and a drop in $M_s$ is expected. This behavior is seen in Fig. 2(a).

Premartensitic transformation temperatures also decrease as the Fe concentration increases, but at lower rate than $M_s$. In addition $T_C$ increases with increasing $x$.

Figure 2(b) shows the entropy change at the martensitic transformation as a function of Fe concentration. The concentration dependence of $\Delta S$ is similar to the behaviour of $M_s$, i.e., the entropy change decreases as the amount of Fe increases. Such a dependence reflects the stabilization of the cubic phase.

B. Substitution of Mn by Fe

Figure 3 illustrates typical results obtained when replacing Mn by Fe (Ni$_{51.4}$Mn$_{25.2-x}$Ga$_{23.4}$Fe$_x$ family). For the sample with $x = 1.8$ ($T_C = 374$ K) a martensitic transition is observed on cooling at $M_s = 275$ K and $M_f = 267$ K. On heating, the reverse transformation takes place at $A_s = 274$ K and $A_f = 281$ K. No signatures of a premartensitic transformation are observed.

The variation of transition temperatures with Fe concentration for this family is collected in Fig. 4. No significant changes in transition temperatures are observed over the compositional range studied. This is because $e/a$ varies little by replacing Mn with Fe in small amounts. Consistently, Fe addition does not substantially modifies the values of the entropy change at the martensitic tran-
C. Substitution of Ga by Fe

Figure 5 illustrates typical results obtained for the Ni$_{51.4}$Mn$_{24.5}$Ga$_{24.1-x}$Fe$_x$ family. Data for the sample with $x = 0.7$ ($T_C = 363$ K) are shown. The presence of a martensitic transformation near room temperature is evidenced from both susceptibility and calorimetric measurements. The corresponding transition temperatures are $M_s = 290$ K, $M_f = 281$ K, $A_s = 287$ K and $A_f = 297$ K. Again, no signature of the premartensitic transition is observed.

The phase diagram is shown in figure 6 where it is seen that $M_s$ increases with increasing Fe content. This is consistent with the rapid increase of $e/a$ when Fe is substituted for Ga. $T_C$ is essentially unaffected.

The entropy change at the martensitic transition as a function of Fe concentration is collected in the inset of figure 4. As can be seen from this figure, $\Delta S$ parallels the behaviour of the martensitic transformation temperatures and increases as the amount of Fe increases, pointing out the stabilization of the the low temperature phase due to Fe substitution.

IV. DISCUSSION

The complete set of results for the different transition temperatures is collected in Fig. 7. Here, the magnetic and structural transition temperatures of the quaternary Ni-Mn-Ga-Fe system is plotted as a function of $e/a$. As can be seen from this plot, data from different families scale with the electron concentration parameter. It was established for Ni-Mn-Ga that the phase stability is controlled by $e/a$ [31, 34]. In the case of the quaternary system, the reasonable scaling of the transition temperatures indicates that the phase stability is mostly governed by the electron concentration as well. However, the scatter in the data points is higher than that observed in the phase diagram as a function of composition (see Figs. 2 and 6), thus suggesting that additional parameters other than electron concentration could affect phase stability.

For comparison, figure 7(b) shows the phase diagram for the Ni-Mn-Ga system (data extracted from reference [35] and references therein). The behavior is similar for both alloy systems. $M_s$ and $T_I$ increase as $e/a$ increases, whereas $T_C$ decreases. At constant $e/a$, we find that the addition of Fe to Ni-Mn-Ga shifts $M_s$ and $T_I$ to lower values, whereas $T_C$ shifts to higher temperatures [as illustrated by dashed lines in Fig. 7(a)].

The relationship of $e/a$ and lattice instability in cubic
Heusler alloys has recently been investigated from first principles calculations [36]. It has been reported that $e/a$ plays a central role in the occurrence of anomalies in the phonon dispersion curves along [110] directions. These control the stability of the cubic structure. In particular, it has been found that adding and removing electrons has the same effect as replacing the $sp$ ($X$) element. In the present study, we have experimentally investigated the effect of different element substitution. The general trends in the phase stability are given by the change in $e/a$. This is consistent with a change in the position of the Fermi energy as in a rigid band model. Nevertheless, the larger scatter of the data when plotted as a function of $e/a$ compared to the one in the plots as a function of composition suggests that the effect of alloying is not just a change in the Fermi level, but the addition of Fe could also modify to some extent the orbital hybridization and bonding. Actually, changes in hybridization were reported for Ni$_2$MnGa with several substitutional elements [37]. This could be related to volume effects which have been reported for In-doped Ni-Mn-Ga alloys [38].

As can be seen in Fig. 7, the premartensitic phase exists when martensitic and magnetic transition are well separated. In the Ni-Mn-Ga system, it has been shown that magnetoelastic coupling between structural and magnetic degrees of freedom gives rise to the premartensitic transition $[11,39]$. The strength of such an interaction depends on the magnetization. Therefore, in order for the premartensitic phase to develop, the sample must remain in the cubic phase at temperatures well below the Curie point. This requires that the martensitic transition temperature is well below $T_C$. Moreover, the temperature that corresponds to the point where martensitic and premartensitic transformation temperatures meet is slightly displaced to higher $e/a$ values in the case of Ni-Mn-Ga-Fe system with respect to the ternary system. Such a shift is in agreement with the decrease of $M_s$ and the increase of $T_C$ due to Fe addition. As $M_s$ shifts to lower temperatures and $T_C$ to higher temperatures, the separation between both temperatures increases compared to the ternary system for equal $e/a$ values. Thus, the crossing point between $M_s$ and $T_I$ is displaced to higher electron concentration values.

The features in the [110] TA$_2$ phonon branch giving rise to the intermediate phase are associated with a nesting in the Fermi surface. It has been found that such a Fermi-surface nesting is strongly dependent on the magnetization of the cubic phase [40]. This scenario is consistent with the experimental finding that the premartensitic phase only develops for ferromagnetically ordered samples for which the martensitic instability is well below $T_C$.

Finally, figure 8 shows the entropy change at the martensitic transformation of Ni-Mn-Ga-Fe system as a function of electron per atom concentration $e/a$. Filled symbols stand for Ni$_{52.5-x}$Mn$_{23}Ga_{24.5}Fe_x$ family; half-filled symbols stand for Ni$_{31.4}Mn_{29.2}Ga_{24}Fe_x$ family; open symbols stand for Ni$_{51.4}Mn_{24.5}Ga_{24}Fe_x$ family. Red dashed line depicts the fitted entropy change of the related Ni-Mn-Ga ternary system. (b) Entropy change at the martensitic transformation of Ni-Mn-Ga system as a function of electron per atom concentration $e/a$ [data compiled from reference [41] (□) and [42] (■)]. Solid lines are linear fits to the experimental data.
V. CONCLUSION

We have studied the effect of Fe addition on the structural and magnetic transformation properties in the magnetic shape memory alloy Ni-Mn-Ga for compositions close to stoichiometry. We find that $M_s$ and $T_I$ shift to lower values when Fe is substituted into Ni-Mn-Ga, while $T_C$ shift to higher values. Despite of the similarities between ternary Ni-Mn-Ga and quaternary Ni-Mn-Ga-Fe systems, which indicate that phase stability is qualitatively governed by $e/a$, the shift in $M_s$ evidences that parameters other than $e/a$ affect phase stability (essentially volume effects associated with atom sizes as suggested in [38]). Hence, a simple choice of $e/a$ can only be considered to be a guideline for examining systematic changes within a single-alloy system. Actually, the lack of universal character of $e/a$ parameterization has been previously pointed out for the Heusler alloys Ni-Mn-X [33, 43] and has been recently confirmed by the manipulation of structural and magnetic transition temperatures in isoelectronic Ni-Mn-Ga and Ni-Mn-Ga-In compounds [38, 44].

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