The Effects of Slicing Parameters on Surface Quality of European Beech Wood

Utjecaj parametara rezanja na kvalitetu površine bukovine

ABSTRACT • The main objective of this work was to evaluate the effects of flat slicing processes on wood surface characteristics of the European beech (Fagus sylvatica L.). The relation between wettability, roughness and machining methods were studied. Two different wood thickness (3.4 and 4.0 mm) and three levels of compression during slicing (67.5 %, 57.5 % and 47.5 % of desired veneer thickness) were used to prepare surfaces prior to testing. The smaller variation of the thickness of thinner veneers was observed. No significant impact of compression on variation of the thickness was found. The contact angle was lower when roughness measured parallel to the grain was higher. The influence of selected compression on roughness of European beech veneers measured perpendicular to the grain was confirmed. This indicated that the influence of the set of machining processes, such as pressure bar setting during slicing, is significant for wooden veneers surface properties.

Keywords: contact angles; wood wettability; European beech; slicing; pressure bar set

SAŽETAK • Glavni cilj rada bio je procijeniti učinke plošnog rezanja furnira na svojstva površine bukovine (Fagus sylvatica L.). Proučavan je odnos između kvašenja i hrapavosti bukovine i metoda rezanja furnira. Za pripremu površine za ispitivanja upotrijebljene su dvije različite debljine furnira (3,4 i 4,0 mm) i tri razine kompresije tijekom rezanja furnira (67,5 %, 57,5 % i 47,5 % željene debljine furnira). Opoziv je manja plošna varijacija debljine tanjih furnira. Nije utvrden značajni utjecaj kompresije na varijacije debljine furnira. Kontaktni kut bio je manji kada je hrapavost paralelno s vlakancima drva bila veća. Potvrđen je utjecaj odabranog pritiska na hrapavost bukova furnira okomit na vlakancima drva. To je pokazalo da postavke procesa obrade, primjerice odabir pritiska tijekom rezanja, znatno utječu na svojstva površine furnira.

Ključne riječi: kontaktni kut; kvašenje drva; bukovina; rezanje; postavke pritiska

1 INTRODUCTION

According to the European Federation of the Parquet Industry, Poland is the leader in the production of flooring materials in Europe, reaching almost 17 % of the European production, which gives approx. 29.5 million m² of flooring produced each year. Most of manufactured floor materials are layered floorboards (EPLF/GFA, 2020). The significance of proper management of raw materials leads to savings and reducing of production costs and forced modification of current-
...ly used machining methods and development of new solutions, such as replacing flat-sawing by more efficient (chipless) technology like slicing. A well-planned production process can provide more proficient production by reducing the amount of waste. It is already known that slicing (or peeling) conditions clearly affect the process energy and forces as well as the quality of wood surface (Aguilera and Zamora, 2009; Aguilera and Muñoz, 2011; Thoma et al., 2015). Thus, the effects of different machining methods are of great interest in order to improve the preparation of materials. In every industrial production process, the occurrence of faults in processing is unavoidable. However, in the context of technological requirements, if the quality deviations are within certain limit values, then the detail is considered to have been properly processed. However, it occurs that the dimensions of the detail are within the limit values, and the problem lies in the quality of the machined surface. This is partly due to the fact that mechanical treatments change the chemical and morphological characteristics of wood surfaces (Liptákova and Kúdela, 1994), with the types of machining along with the characteristics of the raw material, or a combination of both these parameters, determining the surface quality and influencing the cost (Kilic et al., 2006; Mitchell and Lemaster, 2002).

In addition to the physical, mechanical, as well as the anatomical properties of wood, the surface quality of finished products is influenced by numerous factors such as: the direction of slicing, geometry of the blade and its sharpness, thickness of the cut part, any sharpening faults, as well as the technological parameters (speed of slicing, speed of movement, pressure bar settings, etc.) (Richter et al., 1995; Hernández and Cool, 2008; Hauouzali et al., 2019). Surface properties are usually monitored in order to assess the quality of machining processes (Hernández and Cool, 2008). The surface roughness affects the wetting characteristics of materials, and the increase of surface roughness is associated with an increase of surface wettability. Surface roughness of veneer plays an important role in plywood manufacturing. Because of its effect on gluing and bonding characteristics, veneer surface roughness is an important factor in the production of glued timber products such as LVL (Dündar et al., 2008). Moreover, desired surface roughness is strongly and directly linked to or influenced by the future use condition, making it crucial in flooring production, especially in case of glue laminated floorboards. An effective control of surface roughness is important in production processes related to the adhesive bonding of wood elements and the final processing of finished products (Lemaster et al., 1982; Keturakis, 2007; Arnold, 2010; Thoma et al., 2015). Relatively little research has been made concerning the effects of machining on the wetting characteristics of wood surfaces. Wood of deciduous porous structure has been tested more often (Gindl et al., 2001; Qin et al., 2014; Ugulino and Hernandez, 2015).

Beech, next to birch and oak, is the most abundant deciduous species in Europe (Boratyński and Boratyński 1990). The total area of beech dominated forest in Europe is estimated to cover ca 14–15 Mha (excluding the Caucasian mountains) with the largest areas in France, central and southern Germany, and the southeast European mountains (Carpathians, Dinaric and Balkan mountains) (Hahn and Fanta, 2001; Stand-ovár and Kenderes, 2003). In Poland only, the stock of thick beech wood is about 90 million m$^3$. It is estimated that the market share of beech wood will systematically increase due to the observed expansion of this species (Tarasiuk, 1999; Dobrowska, 2011). European beech is an expansive, fast-growing tree species gradually expanding its area of occurrence, whose wood can be an alternative to the dominant European oak in flooring.

The main objective of this work was to evaluate the effects of slicing processes on wood surface characteristics of the European beech (Fagus sylvatica L.). The relations between wettability, roughness and slicing parameters were studied. Two different wood thicknesses and three levels of compression were used during slicing to prepare surfaces prior to testing of selected characteristics.

2 MATERIALS AND METHODS
2. MATERIJALI I METODE

Typical European beech (Fagus sylvatica L.) was selected as a test species, because of its wide application in the European wood industry for the production of floors, both from solid wood and glue laminated wood. Sawn wood of diameters of 20.5 cm $\times$ 12.0 cm $\times$ 100.0 cm (tangential $\times$ radial $\times$ longitude) was used. Material derived from Polish forest managed by the State Forests National Forest Holding. Beams were graded into two groups for flat slicing thickness of about 3.4 and 4.0 mm.

The beech wood beams were hydrothermally treated before slicing. The treatment process included: 5 h of heating up to the temperature of 60 °C, 42 h of thermo-hydro treatment at a temperature of 90 °C and 1 h of cooling down to a temperature of 60 °C. The flat slicing process was carried out on a FEZER Lumber Slicer FM 30 adapted for this purpose. The wood was sliced flat with variable compression of 67.5 %, 57.5 % and 47.5 % of desired veneer thickness. Slicing speed was set at 100 m/min. Drying was carried out in a Van-iek 25 dryer. After drying, moisture content of wood was approx. 8.0 %.

The thickness variation of the obtained European beech veneers was determined using an optical microscope (SMZ 1500, Nikon) with image analysing software. The same microscope was used to prepare images of analysed veneer surfaces.

The contact angles of expanding droplets, i.e. advancing angles, were determined using a contact angle measuring device and using the Owens–Wendt methods (Owens and Wendt, 1969) with Petrić and Oven recommendations (Petrić and Oven, 2015) on a Goniometer Haas Phoenix 300 contact angle analyser connected to imaging software. The image analysis system calculated the contour of the drop from an image cap-
The coefficient of variation (defined as the ratio of the standard deviation to the mean) was 1.8 % (mean value) for 3.4 mm thick veneers and 2.3 % (mean value) for 4.0 mm thick veneers. These values were in 5 % industrial range recommendation (Feihl, 1986) and so the slicing quality was good. A slight variation of the thickness of thinner veneers was most probably caused by lower tensions in material as slicing thin veneer generates lower cutting forces (Haouzali et al., 2019).

Previous experiments (Rahayu, 2016) indicated that it is more difficult to maintain thickness regularity for thinner veneers. On the other hand, a study conducted on Fagus sylvatica L. wood (Daoui, 2011) confirmed our conclusion. Probably, an observation of the inverse relation resulted from the use of relatively high material compression during cutting. It allowed to reduce tensions and made dimensions more stable. The regression analysis made for each veneer thicknesses did not confirm the significance of compression values.

3.2 Wettability and roughness of European beach veneers

3.2. Kvašenje i hrapavost bukova furnira

The results of measurements of contact angles as well as the results of measurements of roughness parallel and perpendicular to the grain are shown in Table 2. The wood surfaces in case of each veneer thickness obtained with different compression, contact angle was in the range of 79.7° to 99.8° for tight side and 85.8° to 93.7° for loose side. There was no significant difference in contact angle measurements on those sides.

A statistical analysis of the test results was carried out using Statistica v. 10 software (StatSoft Inc.). The data were analysed and provided as the mean ± standard deviation. To determine the relations between the tested wood properties, simple regressions were used. Analysis of variance (ANOVA) was also made at the 0.05 level of significance. The test factors and their variability levels are given in Table 1.

### Table 1: Levels of tested factors in relation to European beech veneer wettability and roughness

| Veneer thickness, mm | Veneer side | Compression, % of the thickness | Measurement direction |
|----------------------|-------------|---------------------------------|-----------------------|
| Debljina furnira, mm | Strana furnira | Kompressija, postotak debljine | Smjer mjerenja |
| 3.4                  | tight / zatvorena | 67.5                            | perpendicular to the grain (L) |
| 4.0                  | loose / otvorena  | 57.5, 47.5                       | okomito na vlaknca drva (L) |

The obtained veneers were characterised by a relatively small variation in the thickness (Figure 1). The coefficient of variation (defined as the ratio of the standard deviation to the mean) was 1.8 % (mean value) for 3.4 mm thick veneers and 2.3 % (mean value) for 4.0 mm thick veneers. These values were in 5 % industrial range recommendation (Feihl, 1986) and so the slicing quality was good. A slight variation of the thickness of thinner veneers was most probably caused by lower tensions in material as slicing thin veneer generates lower cutting forces (Haouzali et al., 2019).

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The different machining process did not affect surface wettability, as determined by contact measurements. The ANOVA did not confirm significant dependence between veneer thickness, veneer side or use of different compression values (Table 3). It was ob-

![Figure 1 Variation in European beech veneer with a nominal thickness of 3.4 mm and 4.0 mm](image1.png)

**Figure 1** Variation in European beech veneer with a nominal thickness of 3.4 mm and 4.0 mm

**Slika 1.** Varijacije bukova furnira nominalne debljine 3,4 i 4 mm
Table 2: Contact angles, roughness parallel to the grain and perpendicular to the grain of tested European beech veneers (in parentheses standard deviations are given)

| Side          | Thickness, mm Debljina, mm | Compression, % of thickness Kompresija, postotak debljine | Roughness ⊥ μm Hrapavost ⊥, μm | Roughness || μm Hrapavost ||, μm | Wettability, ° Kvašenje, ° |
|---------------|----------------------------|-----------------------------------------------------------|---------------------------------|---------------------------------|----------------------------|
| Tight zatvorena | 3.4                        | 67.5                                                      | 7.85 (1.37)                     | 4.68 (1.45)                     | 99.8 (2.6)                 |
|               | 57.5                        | 8.98 (1.12)                                               | 4.81 (2.81)                     | 95.5 (5.7)                      |                            |
|               | 47.5                        | 9.60 (2.05)                                               | 4.95 (2.41)                     | 82.4 (3.8)                      |                            |
|               | 67.5                        | 8.19 (1.96)                                               | 4.84 (2.24)                     | 88.5 (8.5)                      |                            |
|               | 57.5                        | 8.82 (1.15)                                               | 4.73 (1.04)                     | 87.8 (5.4)                      |                            |
|               | 47.5                        | 9.16 (1.67)                                               | 5.10 (1.23)                     | 79.9 (6.1)                      |                            |
| Loose otvorena | 3.4                        | 67.5                                                      | 13.29 (3.01)                    | 6.45 (0.90)                     | 87.7 (5.8)                 |
|               | 57.5                        | 12.47 (2.65)                                              | 7.78 (1.77)                     | 93.7 (4.0)                      |                            |
|               | 47.5                        | 11.58 (2.62)                                              | 7.47 (2.06)                     | 90.8 (1.1)                      |                            |
|               | 67.5                        | 13.45 (3.33)                                              | 7.00 (1.16)                     | 85.8 (9.0)                      |                            |
|               | 57.5                        | 11.19 (1.44)                                              | 7.59 (2.94)                     | 87.2 (5.6)                      |                            |
|               | 47.5                        | 11.66 (1.79)                                              | 5.76 (1.51)                     | 89.3 (4.3)                      |                            |

Table 3: Results of ANOVA for wettability, roughness parallel to the grain and perpendicular to the grain

| Feature Svojstvo | Factor Čimbenik | Sum of squares Zbroj kvadrata | Degrees of freedom Stupnjevi slobode | Mean sum of squares Srednji zbroj kvadrata | Fisher’s F-test Fisherov F-test | Significance level Razina značajnosti |
|------------------|----------------|-----------------------------|---------------------------------------|-------------------------------------------|---------------------------------|--------------------------------------|
| Wettability kvašenje | Side / strana | 0.000                       | 1                                     | 0.000                                    | 0.000                           | 0.989304 NS                          |
|                   | Thickness / debljina | 80.701                     | 1                                     | 80.701                                   | 3.245                           | 0.114673 NS                          |
|                   | Compression / kompresija | 72.771                     | 2                                     | 36.392                                   | 1.463                           | 0.294580 NS                          |
| Roughness ⊥ hrapavost ⊥ | Side / strana | 36.867                       | 1                                     | 36.867                                   | 39.478                           | 0.000351*                            |
|                   | Thickness / debljina | 0.144                       | 1                                     | 0.144                                    | 0.163                           | 0.698875 NS                          |
|                   | Compression / kompresija | 0.219                      | 2                                     | 0.109                                    | 0.123                           | 0.885925 NS                          |
| Roughness || hrapavost || | Side / strana | 13.944                      | 1                                     | 13.944                                 | 39.478                           | 0.000411*                            |
|                   | Thickness / debljina | 0.102                      | 1                                     | 0.102                                   | 0.290                           | 0.606905 NS                          |
|                   | Compression / kompresija | 0.545                      | 2                                     | 0.273                                    | 0.772                           | 0.497982 NS                          |

NS – not significant, * – significant at the 0.05 level / NS – nije značajno, * – značajno na razini 0,05

Table 4: Results of simple regression analysis for wettability, roughness parallel to the grain and perpendicular to the grain depending on compression

| Side Strana | Feature Svojstvo | Coefficient of correlation Koeficijent korelacije | Sum of squares Zbroj kvadrata | Mean sum of squares Srednji zbroj kvadrata | Degrees of freedom Stupnjevi slobode | Fisher’s F-test Fisherov F-test | Significance level Razina značajnosti |
|-------------|------------------|-----------------------------------------------|-------------------------------|---------------------------------------------|--------------------------------------|---------------------------------|--------------------------------------|
| Tight zatvorena | Wettability kvašenje | 0.776                                         | 173.054                       | 173.054                                     | 4                                    | 6.075                           | 0.069340 NS                          |
|             | Roughness ⊥ hrapavost ⊥ | 0.945                                         | 1.856                         | 1.856                                       | 4                                    | 33.630                          | 0.004397*                            |
|             | Roughness || hrapavost || | 0.781                                         | 0.072                         | 0.072                                       | 4                                    | 6.255                           | 0.066696 NS                          |
| Loose otvorena | Wettability kvašenje | 0.517                                         | 10.857                        | 10.857                                      | 4                                    | 1.461                           | 0.293387 NS                          |
|             | Roughness ⊥ hrapavost ⊥ | 0.826                                         | 3.062                         | 3.062                                       | 4                                    | 8.542                           | 0.043125*                            |
|             | Roughness || hrapavost || | 0.061                                         | 0.011                         | 0.011                                       | 4                                    | 0.015                           | 0.908011 NS                          |

NS – not significant, * – significant at the 0.05 level / NS – nije značajno, * – značajno na razini 0,05
served that the higher compression during slicing, the higher is the contact angle with water. Simple regression analysis confirmed the influence of selected compression values on roughness of European beech veneers in both parallel and perpendicular to the grain directions (Table 4). Wood roughness was higher when the compression was lower. This indicates that the influence of the set of machining parameters, such as slicing, is visible in the surface quality. The same conclusion was made by de Moura and Hernández (2007), who tested sugar maple wood surfaces machined with the fixed-oblique knife pressure-bar cutting system.

The wood surface roughness is an important characteristic in terms of surface quality and properties, particularly in the case of finishing treatments (Buyuksari et al., 2011). Veneer with a rough surface can also cause excessive resin use and may result in resin bleeding through the face veneer (Dündar et al., 2008). The roughness of tested veneers varied significantly depending on the measurement direction (parallel and perpendicular to the grain) and veneer side. The roughness values measured perpendicular to the grain were twice as high as those measured parallel to the grain. ANOVA confirmed significance of veneer side on roughness values (Table 3). The loose side was characterised by a greater roughness because more irregularities and cracks appeared on that side due to tensile stresses. Such stresses are an effect of veneer bending during the peeling process. According to previous studies (Candan et al., 2010; Bekhta et al., 2012), the improvement of surface quality of veneers is very important for bonding quality in bonded wood panels. Reducing the roughness, mainly on the loose side, reduces stress points between the wood surface and the adhesive, increasing the shear strength of the glue line (Rahayu, 2016).

Wood is not a homogeneous material, and its properties vary in different directions as a result of its anatomical structure (Li et al., 2018). The measurement perpendicular to the grain contains irregularities that are mainly caused by the size of the structural wood elements. In the case of deciduous wood species, these ele-

![Figure 2](image1.png)

*Figure 2* Macrographs of tight side (a) and loose side (b) of tested veneers - magnification 4x

![Figure 3](image2.png)

*Figure 3* Micrographs of tight side (a) and loose side (b) of tested veneers - magnification 20x
ments are primarily fibres and vessels. The observed differences were due to the difference in texture in perpendicular and longitudinal direction of European beech wood. Moreover, wood quality depends on surface morphology (Jankowska et al., 2019). In case of tight side of veneers, only a few cell wall fibrillations roughed the surface. Microscopic images revealed that on loose side the wood fibres and other cellular elements were torn out, mechanically destroyed and even crushed. In addition, loose side of veneers exhibited some cracks and some delamination (Figure 2 and 3).

Simple regression analysis was carried out to verify the existence of a relation between surface roughness measured perpendicular and parallel to the grain and wood wettability. According to results, the correlation between these properties was poor in case of roughness measured parallel to the grain (coefficient of correlation $R_p=0.719$ was not significant) and in case of roughness measured parallel to the grain $R_w=0.851$ was significant. On the other hand, based on our results, it can be concluded that the contact angle is lower when roughness (value of $R_p$ parameter) is higher and that, consequently, wood wettability is also higher. The same inference was made by Arnold (2010), who tested differently machined solid wood surfaces regarding surface properties and coating performance.

4 CONCLUSIONS

4. ZAKLJUČAK

Based on the results of the research conducted, it can be concluded that compression is significant for the surfaces of wood such as European beech slicing. Using pressure bar set (relatively high material compression) during wood slicing allowed to reduce internal stresses providing dimensions to be more stable. The smaller variation of the thickness was observed in thinner veneers. The contact angle was lower when roughness was higher, thus wood wettability was higher. The influence of selected compression factors on roughness of European beech veneers perpendicular to the grain was confirmed. This indicates that the influence of the machining parameters of processes such as slicing is significant for the surface properties of wooden veneers. This type of innovation has the potential to be used, among others, in the furniture industry and the production of wooden layered floors.

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