Bio-Adsorbent Derived from Sewage Sludge Blended with Waste Coal for Nitrate and Methyl Red Removal: Synthesis, Oxidation, Performance and Environmental Consideration

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Research Article

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Bio-adsorbent derived from sewage sludge blended with waste coal for nitrate and methyl red removal: synthesis, oxidation, performance and environmental consideration.

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Abstract
Low-cost bio-adsorbents were synthesized using two types of sewage sludge: D, which was obtained during the dissolved air flotation stage, and S, which was a mixture of primary and secondary sludge from the digestion and dewatering stages. The sewage sludge was mixed with waste coal before being activated with Potassium Hydroxide (KOH) and oxidized with ammonium persulfate (APS). The nitrate and methyl red removal capacities of the synthesized bio-adsorbents were evaluated and compared to those of industrial activated charcoal. The oxidation surface area of bio-adsorbents derived from sludge S shrunk by six fold after modification, while those derived from D only varied narrowly from 312.72 m²/g to 282.22 m²/g, but surface modification had no effect on inorganic composition in either case. The adsorption of nitrate and methyl red (MR) was performed in batch mode, and the removal processes followed the pseudo second order kinetic model and the Langmuir isotherm fairly well. The adsorption capacities of nitrate and MR were higher at pH=2 and pH=4, respectively. The total nitrate Langmuir adsorption potential was DC-5-750 (26.735 mg/g) > commercial activated carbon (Com-AC) (20.61 mg/g) > DC-55-750M1 (17.06 mg/g), and for MR, Com-AC (196.07 mg/g) > DC-5-750M2 (175 mg/g).

Statement of Novelty: This paper examines how the chemical structure of activated carbon derived from sewage sludge and blended with waste coal is altered during the chemical activation process to provide the optimal porous surface for nitrate and methyl red adsorptive remediation. The formation of carboxylic sites or the transformation of oxygen sites to carboxylic sites is the aim of the oxidation process of activated carbon in general. Ammonium peroxydisulfate was chosen because of its ability to oxidize the
surface without significantly altering the porous structure and increase surface acidity by increasing carboxylic group presence. There are no studies that we are aware of that use ammonium peroxydisulfate to oxidize activated carbon from sewage sludge blended with waste coal.

**Keywords:** Sewage sludge, waste coal, activated carbon, oxidation, APS, adsorption, nitrate, MR.

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1. Introduction

Sewage sludge is an unavoidable by-product of wastewater treatment plants, with treatment costs accounting for 25% to 65% of the overall operating costs [1]. South Africa's population has gradually increased over the last two decades, rising from 48.8 million in 2005 to 51.58 million in 2010 to 57.7 million in 2018, with more than half of the country's population now residing in densely populated urban areas [2]. Rapid population growth, combined with rapid urbanization, has put additional pressure on existing wastewater treatment plant (WWTP) facilities, resulting in increased sewage sludge production. Several lines of evidence demonstrate that dumping waste sludge in landfills is not a long-term sewage sludge management solution. Despite the risk of soil and subsoil contamination, nearly 80% of wastewater treatment plants continue to discharge sewage sludge at designated sites [3].

The South African Department of Water Affairs and Forestry has identified five potential applications for sewage sludge: agriculture (fertilizer), on-site and off-site land application (within and outside WWTP boundaries), thermal management activities (e.g., full or partial combustion of organic solids by incineration), and benign land application [3]. The use of sewage sludge fertilizers is restricted due to the difficulties in meeting quality requirements (faecal coliform cap of 10000 CFU/g dry, Helminth Ova maximum of one viable ova/g dry, pollution) [3]. As a result of these
restrictions, large quantities of untreated sludge have accumulated on open fields. South Africa produces 673,360 metric tons of sewage sludge annually, of which only about 19% is recycled and the rest is landfilled, necessitating the development of innovative approaches to reduce sewage sludge emissions [2]. Landfilling as a wastewater treatment residue management alternative poses significant environmental concerns about bacteria, heavy metals, and trace organic pollutants; the same conclusion applies to traditional sea dumping and forestry, both of which are deemed unsustainable [4].

Due to the high cost of industrial activated carbons, research on activated carbon materials extracted from bio-waste, such as olive stones, lemon grass, wall nutsheels and pine cones has taken center stage [5, 6, 7, 8] and among these, activated carbon extracted from sewage sludge (SBAC) has shown promise in the adsorption of inorganic elements such as Ni, Cu, Pb, Cd and Hg [1,9,10,11,12,13].

However, due to the inorganic composition of raw sewage sludge, SBAC has a low surface area, and increasing porosity by adding richer carbonaceous such as coal, bagasse, and coconut shell may be preferable [7,9,11,14,15]. On the other hand, The use of HCl and NaOH, HNO₃ and N,N-Dimethylformamide for the oxidation of SBAC in liquid phase has been reported to increase their adsorption potential by adding surface functionalities groups as shown in Table 1 [9,16,17,18]. An in-depth analysis of the existing body of works, on the other hand, exposes knowledge gaps, such as the fact that very few studies take into account the specific chemical composition of the source materials used. The synthesis of activated carbon from sewage sludge has traditionally been oriented toward particular applications and thus has been more focused on results than on understanding the intrinsic structure within the materials (Table 1). In particular, understanding the adsorption of certain inorganic compounds in aqueous solution by activated carbon requires knowledge of the chemical structure of the activated carbon surface, i.e. determining how the chemical structure of the activated carbon surface is oxidized during the chemical activation process in order to achieve the optimal porous surface. When the source material has been chemically treated, the surface of the activated carbons is normally filled with oxygenated sites and probably amine sites which result in three types of oxides on the surface: acidic, basic, and neutral. Acidic sites increase the hydrophilicity of activated carbon, lower the pH in aqueous suspension, and increase the negative charge density at the surface, while
simple sites are primarily of the Lewis form and are associated with -rich regions located at the basal planes [19]. Additional benefits can be obtained by oxidizing activated carbon after the activation phase to induce the formation of oxygen complexes. The oxidation process raises the oxygen content by lowering the electronic density of the basal planes, which lowers the basicity at the surface [19,20,21]. The oxidation of activated carbon extracted from sewage sludge blended with coal using ammonium peroxydisulfate [(NH₄)₂S₂O₈] is investigated in this paper. In general, the oxidation process is intended to result in the formation of carboxylic sites or the transformation of oxygen sites to carboxylic sites. The choice of ammonium peroxydisulfate is based on its ability to oxidizes the surface without modifying drastically the porous structure and enhance surface acidity by increasing carboxylic group presence [22, 23,24]. To our knowledge, there are no reports on the oxidation of activated carbon from sewage sludge blended with waste coal using ammonium peroxydisulfate. Finally, the oxidized activated carbons are tested for nitrate and MR adsorptive remediation.

Table 1 Literature oxidized activated carbon extracted from sewage sludge (SBAC) and adsorption capacity

| References | SBAC State | Modification Conditions | Oxidant Concentration | Soaking time | Temperature | S_BET (m²/g) | pH_PZC | Adsorption |
|------------|------------|-------------------------|-----------------------|--------------|-------------|-------------|--------|-----------|
| [18]       | Unoxidized | -                       | -                     | -            | -           | 1003,8      | 4,02   | Malachite Green: 269,54 mg/g |
|            | Oxidized   | 1: 2M HNO₃ 1: 3h 1: 60 °C | 838,3                 | 3,78         | Malachite Green: 303,03 mg/g |
| Oxidized   | (2 stages: 1 and 2) | 2:- 3h 2: 300 °C | 2:- 3h 2: 300 °C | 960 | 3,66 | Malachite Green: 284,90 mg/g |
2. Experimental

2.1 Materials

All reagents, including NaOH, NaNO₃, KOH, HCl (32%), (NH₄)₂S₂O₈ (APS), H₂SO₄, and NaCl, were obtained from Associate Chemical Enterprise (ACE) and were analytical grade. Sigma-Aldrich (SA) supplied activated charcoal (C3014-500G), which was designated Com-AC.

Two forms of sewage sludge namely D and S were collected at the East Rand Water Care Company (ERWAT) wastewater treatment plant facilities. D was collected during...
the dissolved air flotation stage, while S was a combination of the primary and secondary sludge from the digestion and dewatering stages, respectively.

2.2 Methods

Raw sewage sludges were sun dried for 24 hours before being oven-dried. The dried sludge was crushed to 100 % passing through 125 µm sieves, and pyrolyzed at different temperatures (DC-5-750, DC-7-900, SC-3-600, and SC-5-900). The products from the pyrolysis were mixed with discard coal in a proportion of 1:1 and activated with KOH under N\textsubscript{2} atmosphere at a flow rate of 5 l/min. To achieve surface modification via oxidation, 1 g of pyrolyzed sewage sludge was incubated in 25 ml of 1M or 2M APS dissolved in 1M H\textsubscript{2}SO\textsubscript{4} at 60°C for 240 minutes before being washed with distilled water until the pH neutral value was reached. Batch adsorption experiments were carried out with an adsorbent dose of 0.5% (5 mg of adsorbent in 10 ml of solution) and the performance of bio-adsorbents was compared to commercial activated carbon. The best oxidized and/or unoxidized SBACs were chosen based on preliminary evaluation test results conducted at 303 K in an incubator shaker. The initial concentration of nitrate was 50 mg/l, with contact times of 180 and 360 minutes, respectively, while the initial concentration of MR was 75 ppm, with contact times of 90 and 180 minutes, and initial pH of 2 and 4 for nitrate and methyl red, respectively. The initial pH value of 2 in the case of nitrate was chosen because adsorbent surfaces are prone to being positively charged as pH decreases, and nitrate ions cannot compete with hydroxyl anions [25] and pH 4 was chosen in the case of MR to prevent competition with H\textsuperscript{+} cations while attempting to preserve the adsorbent surface deprotonated [26].

2.3 Chemical analysis

SEM and EDS analysis were done using a ZEISS SIGMA FESEM 03-39 apparatus on coated samples on a carbon tape support using Gold-Palladium techniques. TGA was performed with the Pioneer (SDT-Q500) equipment. Proximate analysis of sewage was performed using a Perkin-Elmer STA 6000 simultaneous thermal analyser. FT-IR
analyses were done using the Perkin-Elmer FT-IR Spectrometer Spectrum 2. Ultimate
analysis was conducted with the thermoscientific flash 2000. XRD study was done
using a Bruker 2D phaser instrument with CuKα1 radiation at a wavelength of 1,54060
\( \text{cm}^{-1} \) and a 20 angle. The NH\(_4\)OAC method [27] was used to determine cations exchange
capacity. The Boehm titration method was used to determine the acidity of SBAC [28].
The pH point of zero charge was determined using the procedure described by Leng et
al. [29]. Surface functionalities and graphitization or carbon disorder structure of the
adsorbent were assessed using FT-IR analysis and Raman spectroscopy, respectively.
For the pH point of zero charge, 50 mg of adsorbent were placed in vials with 40ml of
0,01 M NaCl solution and shaken for 48 hours, the solution pH ranged from 2 to 12
with an incremental of 2. The concentrations of nitrate and MR were calculated using
an IC dionex-120 and a U-vis Shimadzu 1800, the latter at a wavelength of 480 nm, as
per Ding et al. [30].

3. Results and discussion

3.1 Pretreatment and characterisation of precursors

The precursors were sun dried, and the moisture content of the sample was
determined by mass losses after oven drying at 105 °C for 24 hours as shown in Table 2.

| Types of sludge | Non-dried sample Moisture (%) | Moisture content After sun drying (%) |
|-----------------|-----------------------------|-------------------------------------|
| D               | 96,28                       | 6,285                               |
| S               | 85,33                       | 7,037                               |

The elemental analysis (Table 3) reveals that there is only a minor difference
between the two samples, indicating that digestion has no effect on the organic content
of sewage sludge, despite the volatile solid content being slightly different. However,
although the surface area of sludge from D was approximately 1.5 m$^2$/g, the surface area of sludge S could not be determined, possibly due to a lack of porosity in the precursor materials.

### Table 3 Precursors properties

| Precursors | D | S | Discard coal |
|------------|---|---|--------------|
| Elemental analysis | | | |
| C (%) | 36.511 | 36.640 | 43.133 |
| H (%) | 5.526 | 5.215 | 2.424 |
| N (%) | 5.020 | 2.681 | 0 |
| S (%) | 2.002 | 2.225 | 2.429 |
| H/C | 0.151 | 0.142 | 0.056 |
| N/C | 0.137 | 0.073 | 0 |
| Proximate analysis | | | |
| Fixed carbon (%) | 4.15 | 4.86 | 15.76 |
| Ash (%) | 29.15 | 35.98 | 67.96 |
| Volatile (%) | 66.7 | 59.16 | 16.28 |
| Volatile solid | 2.161 | 1.216 | 1.474 |
| Surface properties | | | |
| $S_{BET}$ (m$^2$/g) | 1.411 | - | 3.848 |
| Pore volume | 0.011 | - | 0.014 |
| Pore size (nm) | 30.72 | - | 15.11 |

In Figure 1, the TGA curve of dried sludge shows that between 30 °C and 190 °C, there is a slight mass loss, and the mass of both sludge was roughly 5%, possibly due to adsorbed water. The most mass loss occurred between 200 and 600 degrees Celsius, with mass loss of D and S increasing from about 5% at 200 degrees Celsius to about two-thirds (64%) and half (46%) at 600 degrees Celsius, respectively. The mass loss from 600 °C to 1000 °C is less pronounced for both sludge with 17 and 13 % for D and S respectively. As a result, 600 °C was chosen as the minimum temperature for pyrolysis. S appears to be slightly more stable than D based on the TGA curves.
Both samples D and S show heterogeneous morphology and composition as revealed by microscopic examination by SEM analysis in Figures 2 (a, b), (c, d), and EDS analysis in Figures 3 (a, b) and Figures 4 (a, b), respectively. The sponge-like morphology shown in Figure 2.b may be attributed to an organic water-repellent compound that adhered to the bubbles during the dissolved air flotation process. Both Figures 3 (a, b) and Figures 4 (a, b) reveal that the main elements in the sewage sludge samples were carbon and oxygen, with silica and aluminium at trace concentrations. In contrast to D sludge, energy dispersive X-Ray (EDX) examination of sample S revealed an advanced inorganic content, probably generated from domestic wastewater particles collected during decantation or solid-liquid separation.
Fig. 2 microscopic observation of raw sewage sludge D: (a) and (b), S: (c) and (d).

Fig. 3 Elemental analysis of raw sewage sludge D: (a) and (b)
Figure 5 shows the FT-IR spectra of the raw sewage sludge with wavenumbers ranging from 450 cm\(^{-1}\) to 4000 cm\(^{-1}\). Reading the peaks spectra wavelengths from left to right, the peak observed at 3688-3619 cm\(^{-1}\) is attributed to OH-kaolinite and gibbsite lattice stretching \([31,32]\), 2988-2901 cm\(^{-1}\) to \(-\text{C-H group vibration} [7,33]\), 1631 cm\(^{-1}\) and 1538 cm\(^{-1}\) to sulphur and nitrogen functional groups, respectively \([33]\). The shape of the shoulder peaks at 1050-1090 cm\(^{-1}\) was attributed to Si-C or Si-O-Si bands \((\text{Liang et al., 2020})\), C-O-C vibration \([33]\), and finally, under 1000 cm\(^{-1}\), the peaks at 749 cm\(^{-1}\), 535 cm\(^{-1}\), and 467 cm\(^{-1}\) were attributed to silica or calcium carbonate stretching \([32,34]\). Discard coal has a lower transmittance from 1498 cm\(^{-1}\) peaks than FT-IR spectra sludge.1007 cm\(^{-1}\), 1030 cm\(^{-1}\), implying that waste coal contains more mineral elements whereas sludge S has lower transmittance than D, implying that the former contains more functional classes.
3.2 Characterisation of activated samples

Table 4 Nomenclature and conditions of the activation experiments

| Name   | Sludge | discard coal | Concentration KOH: mol/l | Temperature (°C) |
|--------|--------|--------------|--------------------------|-----------------|
| D-3-600| D      | No           | 3                        | 600             |
| D-3-750| D      | No           | 3                        | 750             |
| D-5-600| D      | No           | 5                        | 600             |
| D-5-900| D      | No           | 5                        | 900             |
| D-7-600| D      | No           | 7                        | 600             |
| DC-3-900| D    | Yes          | 3                        | 900             |
| DC-5-600| D    | Yes          | 5                        | 600             |
| DC-5-750| D    | Yes          | 5                        | 750             |
| DC-7-900| D    | Yes          | 7                        | 900             |
| S-3-600| S      | No           | 3                        | 600             |
Figure 6.a shows the microscopic examination of the sorbent SC-3-600 after activation. Pyrolysis and washing stages may have facilitated cavity formation of highly formed cavities due to the remarkable depletion of inorganic and organic components [35]. Furthermore, some particles (Figure 6a and 6b) lack or have insignificant cavities, which may be attributable to a lack of volatile and decomposed matter escaping to facilitate porosity [9]. The EDS qualitative analysis (Figure 6.c) of the local particle (6.b) revealed inorganic characteristics as well as the presence of K and Cl from activation and washing, respectively.
Fig. 6 SEM microscopic analysis of SBAC SC-3-600, (a) multiple particle (b) focus on particle without cavity after activation and (c) qualitative analysis of the targeted particle

The FT-IR spectrum of the various SBAC (as per Table 4) exhibited almost identical shape and peaks with different intensities regardless of the parameter involved in the synthesis process, as shown in Figures 7 and 8. The spectra have six main peaks, which are 3676 cm$^{-1}$, 2901-2998 cm$^{-1}$, 1394 cm$^{-1}$, 1225 cm$^{-1}$, and 892 cm$^{-1}$ in all SBAC samples.

In comparison to feedstock spectra, the disappearance of the wavelength peak at 470 cm$^{-1}$ and 500 cm$^{-1}$ in SBAC could be due to inorganic matter solubilisation during the acid washing phase [36,37,38], while 798 cm$^{-1}$ could be due to dehydrogenation reactions [24], 1631 cm$^{-1}$ and 1538 cm$^{-1}$ could be due to thermal degradation of protein for nitrogen related compound or sulphur [33].
Fig. 7 FT-IR spectra of SBAC obtained from raw sewage sludge D as precursor
The peaks associated with C-H group stretching not only shifted slightly from 2859-2922 cm\(^{-1}\) in feedstock to a higher value (2901-2988 cm\(^{-1}\)) in SBAC, which can be related to the presence of saturated group [11] but also transmittance increased after activation for all samples, which is in contrast to some literature [7,33,39] in which it was argued that the disappearance of the peaks was due to the decomposition of fatty organic matter and dehydration [7]. Organometallic formation may be a possible explanation for the increased transmittance of SBAC pyrolyzed at lower temperatures followed by depletion as temperature rises; for example, the abundance of functional groups (hydroxyl, carboxyl) on the biochar surface synthesized from sewage sludge pyrolyzed at 300 °C reduced extractable cations due to the formation of organometallic compounds [40,41]. The functional groups present in SBAC can be summarized as O-H, C=C, C=O, aliphatic C-H, Si-C, Si-O-Si, phosphate, and carbonate, based on the observations.

Com-AC has broad peaks (2 = 25.3° and 2 = 44.6°) linked to its amorphous phases, while the XRD pattern (Figure 9a and b) demonstrated mineral phases transformation from broad peak in the precursors to sharp in the manufactured absorbent, which clarified transition from amorphous to crystalline phase due to pyrolysis. XRD verified the existence of minerals such as wustite, quarts, illite, and feldspars in SBAC. It is
worth noting that the presence of alkaline earth elements in the minerals (feldspars and illite) led to magnesium, calcium, and iron being classified as exchangeable cations.

Fig. 9 XRD graph of feedstock (a), SBAC and Com-AC (b)

Ca: calcite, F: feldspar, G: graphite, Gi: gismondine, Gy: gypsum, Illite, K: kaolinite, Mo: moderrnite, Q: quartz, W: whittle,
3.3 Surface modification via oxidation

The oxidation of SBAC resulted in surface functionalities modifications with formation of peaks in the oxidized adsorbent around 1550-1575 cm\(^{-1}\) (Fig. 10), which can be linked to symmetric COO\(^-\) and nanoaromatic C=O stretching entailed in formation of carboxylic functional groups (Teng et al., 2015) or C=C bond of the aromatic skeleton ring of adsorbent [13]. On further notice the reduction in -CH (2901-2988 cm\(^{-1}\)) and -OH (3640 cm\(^{-1}\)) stretching substances which may be ascribed to their solubility/affinity with H\(_2\)SO\(_4\). On the other side, Com-AC did not have functional group.

![Fig. 10 FT-IR spectra of Com-AC, DC-5-750 and its two derived oxidized sorbents](image)

Raman spectra pattern is shown in Figure 11. The peak located at 1587 cm\(^{-1}\) (G band) and 1357 cm\(^{-1}\) (D band) are associated to sp\(^2\)-bonded carbon and disorder of carbon structure respectively and their intensity I\(_G\) and I\(_D\) reveal the adsorbent degree of
graphitization and carbon disorder structure from which $I_D/I_G$ ratio enunciates prevalence of carbon disorder structure over graphitization and vice-versa [13].

As shown in Table 5, graphitic structure is more predominant than carbon disorder structure and augmented with oxidation, partial graphitization of activated carbon was reported with acidic oxidation treatment with HNO$_3$ [42].

| Adsorbents  | $I_D$ (1387 cm$^{-1}$) | $I_G$ (1587 cm$^{-1}$) | $I_D/I_G$ |
|-------------|------------------------|------------------------|-----------|
| Com-AC      | 1028,126               | 1397,75                | 0,735     |
| DC-5-750    | 385,270                | 398,887                | 0,965     |
| DC-5-750M1  | 2476,854               | 2921,75                | 0,847     |
| DC-5-750M2  | 5262,40                | 6284,252               | 0,837     |

The surface of oxidized adsorbent (Figure 12.b) exhibited less irregularities and soften surfaces than the unoxidized adsorbent (Figure 12.a) and Com-AC (Figure 12.c) probably as results of corrosive H$_2$SO$_4$-adsorbent surface interaction [18] and also disintegration of pore structure situated at the carbon edge [17]. XRD spectra of adsorbent are represented in Figure 13 after oxidation treatment the unoxidized sorbent exhibited a broader peak ($\theta = 25,3^\circ$) associated to amorphous or graphite structure as
endorsed by Raman spectra analysis, on the other hand augmentation in peak (2θ = 30°) ascribed to peak might be corollaries of other mineral (feldspar and illite) solubilisation/decline.

Fig. 12 morphology of (a) DC-5-750, (b) DC-5-750 M1 and (c) Com-AC
The oxidation with APS did not impact significantly carbon composition as per ultimate analysis results since the biggest difference was 6.771 % (from DC-5-750: 23.612 % to DC-5-750M2:30.383%) while with other sorbents (SC-3-600,SC-5-900,DC-7-900) variation was less than 2%, alike tendency was reported by Ang et al. [22]

Furthermore, textural properties in Table 6 receded severely after modification, in case of bio-adsorbent derived from sludge S, for instance prior oxidation SC-3-600 had surface area of 281.72 m²/g that shrunk to 68.22 m²/g and 46.673 m²/g when treated with a solution of 1M and 2M APS respectively, probably due to thinness of walls pores, which are prone to collapse [43] and/or micropore occlusion [44]. In the case of DC-5-750, surface area varied slightly (7.28-30.57 m²/g: variation) and micropore areas changed from 124.14 m²/g to about 157.36 m²/g and 176.11 m²/g after modification with 1M APS and 2M APS respectively. After modifications DC-7-900 surface area (247.57 m²/g) increased probably as results of micropore and mesopore collapse emerging from activated carbon surface etching by reagents, it was 285.59 m²/g for DC-7-900M1 and 295.31 m²/g for DC-7-900M2.
### Table 6 Structural properties and ultimate analysis results of SBAC after and before oxidation

| Adsorbent Modification conditions | \( \text{S}_{\text{BET}} \) (m\(^2\)/g) | \( \text{S}_{\text{meso}} \) (m\(^2\)/g) | \( \text{S}_{\text{micro}} \) (m\(^2\)/g) | \( \text{V}_{\text{tot}} \) (cm\(^3\)/g) | \( \text{V}_{\text{micro}} \) (cm\(^3\)/g) | Pore size (nm) | C (%) | H (%) |
|----------------------------------|----------------------------------------|----------------------------------------|----------------------------------------|----------------------------------------|----------------------------------------|----------------|-------|-------|
| Com-AC -                          | 609.209                                | 195.74                                | 336.236                                | 0.469                                  | 0.165                                  | 3.14           | 78.411| 0.000 |
| SC-3-600 Unoxidized              | 281.72                                 | 90.942                                | 123.49                                 | 0.342                                  | 0.075                                  | 4.857          | 45.227| 0.7411|
| 1M APS                           | 68.227                                 | 24.098                                | 35.241                                 | 0.0953                                 | 0.0175                                 | 5.58           | 47.411| 1.007 |
| 2M APS                           | 46.573                                 | 19.631                                | 14.807                                 | 0.085                                  | 0.0073                                 | 9.02           | 46.394| 1.017 |
| SC-5-900 Unoxidized              | 422.09                                 | 222.394                               | 111.15                                 | 0.453                                  | 0.0495                                 | 4.296          | 2.014 | 0.000 |
| 2M APS                           | 313.05                                 | 61.156                                | 223.75                                 | 0.291                                  | 0.117                                  | 3.604          | 1.891 | 0.000 |
| DC-5-750 Unoxidized              | 312.79                                 | 100.212                               | 124.14                                 | 0.366                                  | 0.0898                                 | 4.681          | 23.612| 0.454 |
| 1M APS                           | 305.51                                 | 115.232                               | 157.36                                 | 0.421                                  | 0.0741                                 | 4.51           | 20.901| 1.087 |
| 2M APS                           | 282.22                                 | 77.816                                | 176.113                                | 0.299                                  | 0.083                                  | 4.244          | 30.383| 1.019 |
| DC-7-900 Unoxidized              | 247.57                                 | 129.83                                | 175.60                                 | 0.265                                  | 0.0320                                 | 4.28           | 15.460| 0.000 |
| 1M APS                           | 285.59                                 | 117.275                               | 133.148                                | 0.302                                  | 0.0666                                 | 4.099          | 14.831| 0.0075|
| 2M APS                           | 295.31                                 | 103.47                                | 121.553                                | 0.289                                  | 0.061                                  | 3.923          | 15.111| 0.0079|

### 3.4 Adsorption experiments

To better understand kinetics order and intra particle diffusion, the effect of time was investigated using the following relationships:

\[
Q_e = \frac{(C_0 - C_e) \cdot V}{m} \quad (1)
\]

\[
Rp = \frac{(C_0 - C_e)}{C_0} \cdot 100 \quad (2)
\]

Where \( Q_e \) (mg/g), \( C_0 \) (mg/l), \( C_e \) (mg/l), \( m \) (mg) and \( V \) (ml) represent the adsorption capacity, initial concentration, equilibrium concentration, adsorbent mass and volume of liquid in contact with adsorbent respectively. The removal %age is calculated via equation (2).

The first and second order kinetics models, as well as interparticle diffusion, are commonly used to understand the adsorption mechanism of pollutants with activated carbon [45].

Adsorption kinetics can be expressed in terms of the hypothesis that adsorbate removals obey a first-order kinetics:

\[
\frac{dq}{dt} = k_1(q_e - q) \quad (3)
\]
where \( q_t \) and \( q_e \) are the amount of pollutants adsorbed per mass of adsorbent (mg/g) at the targeted time and equilibrium, respectively, and \( k_1 \) is the constant rate (min\(^{-1}\)).

After integration with conditions that \( q_e = 0 \) if \( t = 0 \), equation (3) can be written:

\[
\ln \left( \frac{q_e - q_t}{q_e} \right) = -K_1 t \quad (4)
\]

Or alternatively

\[
ln \left( 1 - \frac{n_t}{q_e} \right) = ln q_e - K_1 t \quad (5)
\]

The adsorption capacity at equilibrium (\( q_e \)) and the first-order sorption rate constant (\( k_1 \)) can be evaluated from the slope and the intercept respectively from plot of \( \ln (1 - n_t/q_e) \) vs \( t \).

The second pseudo order kinetics is defined by equation:

\[
\frac{dq}{dt} = K_2 (q_e - q_t)^2 \quad (6)
\]

where \( K_2 \) is the second order rate constant, integration of equation (6) with initial conditions when \( t = 0 \) and \( q_e = 0 \), lead to:

\[
\frac{t}{q_t} = \frac{1}{K_2 q_e^2} + \frac{t}{q_e} \quad (7)
\]

\( K_2 \) and \( q_e \) can deducted from the slope and the intercept of the plot \( t/q_t \) vs \( t \), where \( q_t \) is the adsorption capacity at a specific time.

The intraparticle diffusion model is a convenient means to depict diffusion mechanism and examine whether intraparticle diffusion is the rate-limiting step in the adsorption process. The intraparticle model diffusion is represented by:

\[
q_t = K_{int} t^{1/2} + C \quad (8)
\]

\( K_{int} \) and \( C \) are determined from the slope and intercept of \( q_t \) vs \( t^{1/2} \).

Where \( K_{int} \) is the intraparticle diffusion rate constant (mg. g\(^{-1}\) min\(^{-1/2}\)) and \( C \) is the boundary layer effect intercept; the larger \( C \), the greater the contribution of surface sorption to the rate-controlling step.

The “preferred” oxidized and unoxidized SBAC were chosen based on removal evaluation tests performed at a constant temperature of 303 K for 180 and 360 min with an initial concentration of 50 mg/l of nitrate, 90 min and 180 min for MR with 75 ppm as an initial concentration and an initial pH of 2 for nitrate and 4 for methyl red. The initial pH of 2 in the case of nitrate was chosen based on the hypothesis that adsorbent surfaces become positively charged as pH decreases, preventing competition with
hydroxyl anions and pH 4 in the case of methyl red to avoid competition with H⁺ cations while attempting to keep the surface deprotonated (below the pHpzc for the oxidized adsorbent) as MR pKa = 5.1. Initially, unoxidized SBAC outperformed oxidized SBAC as shown in Figure 14, probably due to the former's proclivity for having a highly deprotonated surface at lower pH. The adsorption capacity decreased as time progressed, with the exception of Com-AC, where it changed slightly from 16.32 mg/g to 13.2 mg/g for contact times of 180 and 360 minutes, respectively. Furthermore, SBAC (DC-5-750M1 and SC-5-900M2) released a significant amount of nitrate ion in solution after 360 minutes of agitation, while this amount was lower when the process was carried out with other adsorbents. This situation may be related to the release of compound contained in the adsorbent ash in the liquid phase and/or the adsorption equilibrium phenomenon, in which optimum equilibrium contact was reached. DC-5-750 and SC-3-600, as well as the oxidized sorbents DC-5-750M2 and SC-3-600M2, were chosen for further nitrate adsorption experiments. The bio-adsorbent had mesopores, making it ideal for removing medium-sized substances from liquid process [1]. Despite having a larger surface area, SC-5-900 (422.09 m²/g) and SC-5-900M2 (313.05 m²/g) had a lower adsorption capacity than other SBAC. This may be attributed to lower carbon content (Table 1) or the disappearance of acidic functional groups as temperatures rose [36], and this result confirmed the significance of functional group presence. Based on the test results in Figure 6, DC-5-750 M1 and DC-7-900 M1, with adsorption capacities of 127,634 mg/g and 124,376 mg/g, respectively, were chosen for additional experiments in relation to Com-AC (121,10 mg/g) performances, as well as unoxidized SBAC (DC-5-750 and DC-7-900). Figure 7a depicts the nitrate removal pattern over time. Prior to 30 minutes of contact time, all adsorbents had negligible adsorption power, most likely due to film diffusion resistance (external diffusion) [46], but it increased significantly up to 120 minutes for Com-AC, DC-5-750, and DC-5-750M1 at 15,132 mg/g, 17,46 mg/g, and 10,72 mg/g, respectively.
As illustrated in Figure 15, adsorption rises with time except for Com-AC, where the change was insignificant (from 123.8 mg/g at 90 min to 121.2 mg/g at 180 min), owing to the fact that equilibrium had already been established. Despite having the highest surface area, SC-5-900 and SC-5-900M2 had a lower qe than other sorbents, most likely due to a lower carbon content (Table 6) or a lack of acidic functional groups due to their depletion during temperature augmentation [14]. This finding emphasizes the critical nature of functional group presence.

As depicted in Figure 15, the synthesised sorbents with the highest adsorption potential were DC-5-750 M1 (127.6 mg/g) and DC-7-900 M1 (124.4 mg/g), and they were therefore chosen for future experiments, along with the unmodified sorbents (DC-5-750 and DC-7-900). The upward tendency may be associated to pore diffusion and
surface reaction which are deemed to present less component resistance than external
diffusion [46], while stagnant trend after 120 min may be ascribed to occupation of
available adsorption site by nitrate ions as the process progress [25,47,48], which
weaken the interaction between sorbate and adsorbent surface [48].

Preliminary tests shown in Figure 6 revealed that the adsorption capacity increased
significantly with time with a little fluctuation in Com-AC from 123, 8 mg/g at 90
minutes to 121, 172 mg/g at 180 minutes, implying that equilibrium had already been
reached.

Although having a higher surface area, the adsorption capacity of SC-5-900 (422,1
m²/g) and SC-5-900M2 (313,1 m²/g) was lower than other SBAC. This could be due
to lower carbon content (Table 5) and/or depletion of acidic functional groups as they
vanished with temperature rise (28). This observation further corroborated the
importance of functional group presence.

Based on results in Figure 6, DC-5-750 M1 and DC-7-900 M1 with adsorption
capacities of 127, 6 mg/g and 124, 4 mg/g, respectively, were chosen for additional
investigations in comparison to Com-Ac (121,1 mg/g) performances.

![Fig. 15 preliminary adsorption capacity results for MR](image-url)
Fig. 16 effect of time on nitrate (a) and MR (b) adsorption capacity

Figure 16a depicts the nitrate removal trend as a function of time. Initially, all adsorbent adsorption capacities were negligible prior to 30 minutes of contact time possibly due to film diffusion resistance (external diffusion), and thereafter rose significantly for Com-AC (15.1 mg/g), DC-5-750 (17.5 mg/g), and DC-5-750M1 (10.72 mg/g).

Figure 16.b depicts the changes in dye adsorption capacity with contact time. Com-Ac adsorption capacities increased slightly from 109.63 mg/g at 30 min to 123.868 mg/g at 90 min and 121.107 mg/g at 180 min, while DC-5-750 and DC-5-750M1 adsorption capacities increased from 83.08 mg/g and 113 mg/g at 30 min to 113.126 mg/g and 123.8 mg/g at 90 min and 114.36 mg/g and 127mg/g at 180 min.

The rapid increase in adsorption capability at the start of the process could be attributed to the abundance of adsorption sites [26,49].

Nitrate pseudo first order (PFO) and Pseudo second order (PSO) plots are recorded in Figure 17a-b and the corresponding parameters are recorded in Table 6. From the results in Figure 17a-b, Com-AC fitted better the PFO ($R^2=0.9693$) than PSO ($R^2=0.8569$) kinetic model, while other sorbents fitted better PSO kinetic model albeit lower coefficient correlation ($R^2$) 0.7859 and 0.793 for SC-3-600 and SC-3-600 M1 respectively.
Figure 18 depicts intraparticle diffusion model line plots for nitrate adsorption that did not pass through the axis origin, indicating that the nitrate removal mechanism was not solely controlled by the intraparticle diffusion model. Observations of similar nitrate removal were recorded by others [25,50].
Table 7 parameters of PFO, PSO kinetics and intraparticle diffusion nitrate model

|                      | Com-AC | DC-5-750 | DC-5-750M1 | SC-3-600 | SC-3-600M1 |
|----------------------|--------|----------|------------|----------|------------|
| Pseudo first-order   |        |          |            |          |            |
| Qe (mg/g)            | 3.49   | N/A      | N/A        | N/A      | N/A        |
| $K_1$(min$^{-1}$)    | 0.0344 | N/A      | N/A        | N/A      | N/A        |
| $R^2$                | 0.9683 | 0.108    | 0.1128     | 0.1543   | 0.1186     |
| Pseudo second order  |        |          |            |          |            |
| Qe (mg/g)            | 15.748 | 19.342   | 11.764     | 15.797   | 10.277     |
| $K_2$ (g. mg$^{-1}$.min$^{-1}$) | 0.016  | 0.016    | 0.037      | 0.0072   | 0.0091     |
| $R^2$                | 0.8569 | 0.8698   | 0.8663     | 0.7859   | 0.793      |
| Interparticle diffusion |    |          |            |          |            |
| $K_d$ (g.mg$^{-1}$. min$^{-0.5}$) | 2.327  | 2.367    | 1.451      | 1.937    | 1.2479     |
| C                    | -14.032 | -8.966  | -5.475     | -7.8526  | -5.159     |
| $R^2$                | 0.8953 | 0.8525   | 0.8287     | 0.8446   | 0.8827     |

Nitrate PFO and PSO parameters are shown in Table 7. It was noticed that Com-AC fitted better PFO ($R^2$=0.9693) than PSO ($R^2$=0.8569) kinetic model, whereas other sorbents fit better PSO kinetic model, albeit with lower coefficient correlation ($R^2$) 0.7859 and 0.793 for SC-3-600 and SC-3-600 M1, respectively. The plot of MR PFO and PSO kinetic models are depicted in Figures 19a and 19b. The MR adsorption
process could not be depicted using the PFO kinetics model due to insufficient linearity fitting induced by the inherent equation formula where $q_e$ (adsorption capacity) is concomitantly fitting data and determining value. The parameters for parameters value of MR PFO and PSO kinetic and intraparticle model are presented in Table 8.

Fig. 19 MR PFO (a) and PSO (b) kinetic model
Table 8 parameters value of MR PFO and PSO kinetic and intraparticle model

|                     | Com-AC 750 | DC-5-750M1 | DC-7-900 | DC-7-900M1 |
|---------------------|------------|------------|----------|------------|
| **Pseudo first-order** |            |            |          |            |
| Qe (mg/g)           | NA         | NA         | NA       | NA         |
| K (min⁻¹)           | 0.3935     | 0.7036     | 0.2932   | 0.619      | 0.5439     |
| **Pseudo second order** |           |            |          |            |
| Qe (mg/g)           | 123,456    | 136,986    | 140,84   | 131,578    | 136,98     |
| K (g*mg⁻¹*min⁻¹)   | 2.84 10⁻³  | 2.441 10⁻⁴| 3.552 10⁻⁴| 1.824 10⁻⁴| 2.169 10⁻⁴|
| **Interparticle diffusion** |       |            |          |            |
| K_d                 | 1.4188     | 6.1545     | 5.045    | 6.165      | 5.802      |
| C                   | 105.07     | 40.275     | 63.086   | 27.736     | 40.181     |
| R²                  | 0.9815     | 0.9815     | 0.9966   | 0.9831     | 0.9779     |

The effect of pH was measured by varying the pH solution from 2 to 10, as shown in Figure 20. The process was pH dependable, as evidenced by adsorption decrease with pH increasing, in the case of DC-5-750 (pHpzc=6.6) from 20.56 mg/g at pH 2, to 6.24 mg/g at pH 6 and 4.2 mg/g at pH 10, Com-AC (pHpzc=10.3) and DC-5-750M2 (pHpzc=3.1). At pH 2, adsorption potential was 16.32 mg/g and 12.24 mg/g, respectively, at pH 6, 11.12 mg/g and 9.6 mg/g, respectively, and at pH 10, 6mg/g and 1.8mg/g. This pattern was more likely caused by: (i) favorable conditions of nitrate removal accentuated by electrostatic attraction as adsorbent surface bears positive charge at lower pH. (ii) the presence of rivalry between nitrate ions and hydroxyl ions in basic solution, as also stated in other works using carbon-based activated carbon content [47,48,51]. In addition to the above-mentioned justifications, it may be further hypothesized that the underperformance of oxidized SBAC is due to the introduction of an acidic surface functional group; in the case of deprotonation, if pH> pHpzc, more binding sites for cationic sorbate are created on the surface than if it was an unoxidized adsorbent [44,52].

Taking into account that MR is negative if pH>pKa and positive if pH>pKa (Khan et al., 2018), the introduction of acidic functional groups caused a shift in pHpzc, from neutral 6.6 (DC-5-750) to acidic after oxidation 3.1 (DC-5-750-M1) and Com-AC was basic.
10.2, surface functional group deprotonated when pHpzc < pH and adsorbsent surface becomes negatively charged [53]. In contrast to SBAC, Com-AC (pHpzc=10.2) has a wider range where the surface’s net charge is positive. Adsorption of MR with changed SBAC, which had a lower pHpzc than unoxidized, was more pH dependable due to electrostatic attraction between the adsorbent negatively charge and positive MR below pH4 [26]; at pH4, the adsorption potential of DC5-750M1 and DC-7-900M1 was 127.634mg/g and 117.176 mg/g, respectively. from pH 6, pH 8, and pH 10. Adsorption capacity decreased at pH6 from 97.488mg/g for DC-5-750M1 and 109.278 for DC-7-900M1 to 81.854 mg/g for DC-5-750M1 and 71.028 mg/g for DC-7-900M1, the results show that for the oxidized adsorbent at pH4 the adsorption mechanism was related to electrostatic attraction and hydrophobic associated to/or hydrogen bond [54]. Similarly, the adsorption potential of unoxidized SBAC (DC-5-750 and DC-7-900) decreased from 123,868 mg/g and 111,76 mg/g at pH 2 to 81,854 mg/g and 90,32 mg/g at pH 10.

Fig. 20 Effect of pH solution on nitrate (a) and MR (b) adsorption
The outperformance in basic solution could be attributed to adsorption site rivalry between hydroxyl ion and MR negatively charged ions [49]. Similarly, in an acidic solution with a pH of 2, the rivalry may have been between H\(^+\) and positive MR [55] or/and repulsion force between protonated adsorbent surface and MR [26].

However, pH solution variation affected slightly the Com-AC adsorption capacity of MR, from 101.894 mg/g at pH 2 to 113.04 mg/g at pH 10, possibly because the electrostatic attraction mechanism was not very pronounced in the process because below pH 5.1 dye was charged positively and the protonated adsorbent had positive net charge, similar results were recorded on adsorption of cationic dye (Methyl blue) [56]. The adsorption capacity increased as initial concentration increased because driving force of concentration gradient prevailed and had propensity to subjugate mass transfer resistance barrier between solid and liquid interface. Conversely, the proportion of nitrate extracted decreased due to adsorbent site saturation, so a fraction of sorbate remained in solution [14]. As the initial pollutant concentration increased, the adsorbent's dye adsorption capacity increased, but the proportion of dye removed decreased due to a stronger driving force to overcome mass transfer resistance in terms of adsorption capacity and less available adsorption [55,57]. For example, the adsorption capacity of Com-AC, DC-5-750, DC-5-750M2, and SC-3-600 at the lowest initial concentration (10 mg/l) was 5.78 mg/g, 8.50 mg/g, 6.28 mg/g, and 8.51 mg/g, respectively; at 50 mg/l it was 16.32 mg/g, 20.56 mg/g, 12.24 mg/g, and 18.32 mg/g, respectively; and at the highest initial concentration (90 mg/l) 13 mg/g, 23.98 mg/g, 14.65 mg/g, and 18.77 mg/g, while the proportion of nitrate extracted displayed the opposite pattern. At the lowest initial concentration (10 mg/l), it was 27.78 %, 40.87 %, 30.19 %, and 40.91 %, and then decreased at the initial concentration of 50 mg/l to 16.32 %, 20.56 %, 12.4 %, and 18.32 %.

Figures 21 a-b and 22 a-b display Langmuir and Freundlich isotherms fitted to elucidate the nitrate and MR removal processes, respectively. Tables 9 and 10 provide data on the fitting parameters. For all adsorbents, the Langmuir isotherm suit the process better with a higher \(R^2\) than the Freundlich model. The presence of \(R_L\) values between 0 and 1 suggested that nitrate and MR adsorption were favorable on all sorbent surfaces (Tan and Hameed, 2017). It is worth noting, however, that as the \(R_L\) value reached zero, MR adsorption became more irreversible with increasing concentration [12, 35].
Fig. 21 Langmuir (a) and Freundlich (b) isotherm plot of MR adsorption
Fig. 22 Langmuir (a) and Freundlich (b) isotherm plot of nitrate adsorption

|                        | Com-AC | DC-5-750 | DC-5-750M1 | DC-7-900 | DC-7-900M1 |
|------------------------|--------|----------|------------|----------|------------|
| **Langmuir**           |        |          |            |          |            |
| $Q_m$ (mg/g)           | 196.07 | 147.058  | 175.438    | 136.986  | 156.25     |
| $K_L$ (L/mg)           | 0.2082 | 0.1645   | 0.1919     | 0.1648   | 0.2229     |
| $R_L$                  | 0.1617-0.037 | 0.194-0.046 | 0.1724-0.04 | 0.1953-0.046 | 0.1521-0.0346 |
| $R^2$                  | 0.9515 | 0.9955   | 0.9707     | 0.9992   | 0.9967     |
| **Freundlich**         |        |          |            |          |            |
| $K_F$ (mg/g) $(1/L/mg)^{1/n}$ | 51.997 | 37.765   | 48.443     | 33.794   | 45.141     |
| $l/n$ (l/mg)           | 0.035  | 0.3306   | 0.324      | 0.345    | 0.3199     |
| $R^2$                  | 0.9492 | 0.957    | 0.9463     | 0.9242   | 0.9578     |
Table 10 comparison of MR adsorption capacity with literature values

| Adsorbent type       | Surface area (m²/g) | Solution pH | Concentration range | qₘ (mg/g) | Reference |
|----------------------|---------------------|-------------|---------------------|-----------|-----------|
| NaOH lemongrass leaves AC* | 834.04              | 2           | 25-500              | 76.923    | [6]       |
| KOH durian seed AC   | 980.62              | -           | 25-500              | 384.62    | [49]      |
| Iron oxidized AC     | 153.32              | -           | -                   | 526       | [26,58]   |
| K₂CO₃ custard apple AC | 431.05               | 5           | 80-120              | 171.23    |           |
| H₃PO₄ custard apple AC | 1065                | 4           | 80-120              | 435.25    |           |
| Woody biochar        | 4.96                | -           | -                   | 156.25    | [30]      |
| COM-AC DC-5-750      | 630.209             | 4           | 25-125              | 196.07    | This work |
| DC-5-750M1           | 312.79              | 4           | 25-125              | 147.058   | work      |
| DC-5-750             | 305.51              | 4           | 25-125              | 175.438   |           |

AC=Activated carbon

Table 11 value of isotherms parameters of nitrate removal

|                     | Com-AC | DC-5-750 | DC-5-750M1 | DC-7-900 | DC-7-900M1 |
|---------------------|--------|----------|------------|----------|------------|
| **Langmuir**        |        |          |            |          |            |
| Qₘ (mg/g)           | 20.618 | 26.737   | 17.064     | 21.276   | 17.513     |
| Kₗ (L/mg)           | 0.8165 | 0.5165   | 0.8561     | 0.5437   | 1.2918     |
| Rₗ                  | 0.109-0.0134 | 0.1622-0.021 | 0.1045-0.0128 | 0.1553-0.02 | 0.0718-0.0085 |
| R²                  | 0.9759 | 0.9772   | 0.9959     | 0.9813   | 0.9967     |
| **Freundlich**      |        |          |            |          |            |
| Kₚ (mg/g) (l/mg)¹/ₙ | 2.454  | 4.4942   | 3.2072     | 4.744    | 1.8323     |
| 1/ₙ (l/mg)          | 0.4648 | 0.3873   | 0.3552     | 0.322    | 0.4724     |
| R²                  | 0.9264 | 0.9455   | 0.9901     | 0.9317   | 0.9583     |

¹/ₙ = Specific surface area
Nitrate Langmuir and Freundlich isotherms were used to investigate the nitrate removal process. The findings are presented in Table 11.

As predicted, the Langmuir isotherm described the process better than the Freundlich model, with a greater R² for all adsorbents involved on a monolayer surface. The value of RL between 0 and 1 indicated that both sorbate adsorption was favourable on all sorbent surfaces of the Langmuir isotherm model, it is regarded as unfavourable if RL>1 [36], for Freundlich model adsorption intensity (1/n) value was less than 0,5 in all cases, indicating that sorbate was easily adsorbed, it is hardly adsorbed if 1/n>2 [42].

| Adsorbent type | Surface area (m²/g) | Solution pH | Concentration range (mg/l) | qₘ (mg/g) | Reference |
|----------------|---------------------|-------------|----------------------------|-----------|-----------|
| Sawdust AC* with KOH | 768                | 2           | 8.5-510                    | 25,499    | [51]      |
| Commercial AC | 1424                | 2           | 8.5-510                    | 19,549    |           |
| Urea treated AC | 192                 | 2           | 8.5-680                    | 38,824    | [8]       |
| Thermally post-treat AC | 772             | 2           | 8.5-680                    | 25,499    |           |
| AC oxidized with CETAB* | 901               | 7           | 40-200                     | 21,51     | [25]      |
| Metal oxidized biochar | 155.08          | -           | 50-1500                    | 32.23     | [59]      |
| ZnCl₂ olive stone AC | 1480               | 4           | 100-300                    | 5,525     | [5]       |
| Municipal sewage sludge biochar | 2.82             | 2           | 20-100                     | 2,1127    | [60]      |
| Commercial AC | 603.209             | 2           | 10-90                      | 20,618    | This work |
| DC-5-750 | 312.79              | 2           | 10-90                      | 26,737    |           |
| DC-5-750M2 | 282.22              | 2           | 10-90                      | 17,064    |           |

AC* = Activated carbon  
CETAB = cetyl trimethyl ammonium bromide
It is worth noting that MR adsorption became more irreversible with increasing concentration since the RL value approached zero at higher concentration [25, 26]. The published data are also compared to the present study’s nitrate adsorption capacities in Table 12. To assess the effect of ionic strength, MR was diluted in NaCl solution with a concentration of 0.01 M and 0.05M and the pH was adjusted at 4. As shown in Figure 23, presumably Na\(^+\) cations competition and screening effect of Cl\(^-\) anions at the external surface of adsorbent [54] caused adsorption capacity of oxidized SABC to dwindle narrowly with NaCl concentration change from 127.63 mg/g (without NaCl) to 117.08 mg/g (0.05M NaCl) for DC-5-750M1 and 122.29 mg/g (without NaCl) to 119.61 mg/g (0.05M NaCl) for DC-7-900M1, contrariwise Com-AC and unoxidized adsorbents (DC-5-750 and DC-7-900) increased with NaCl concentration augmentation from 121.08 mg/g to 129.42 mg/g, 114.43 mg/g without NaCl to 125.31 mg/g and 110.29 mg/g to 122.85 mg/g in presence of 0.05M NaCl respectively, adsorption capacity upward trend could have been imputed arguably to dye aggregation drove by salt ions force [61].

Figure 23 effect of ionic strength on MR uptake
3.5 Environmental consideration: toxicity characteristic leaching procedure

The toxicity contaminant leaching procedure was carried out as described elsewhere [39,62], and the element concentrations were determined using a Perkin-Elmer AA spectrometer. Table 13 shows the results of the TCLP test; in general, the concentration of leachable heavy metal in the pyrolyzed adsorbent was lower than the precursor due to the higher thermal stability of heavy metal acquired through pyrolysis [62].

However, after pyrolysis, SC-5-900 released more heavy metals (Fe, Cr, Co, and Ni) than its precursors. This may be due to the disintegration of some stable inorganic minerals (primarily silicate and carbonate) from sludge during pyrolysis with temperature augmentation, which caused the liberation of the fixed metals from the lattice [17].

| Elements (mg/l) | Cu    | Zn    | Pb    | Ni    | Co    | Cr    | Fe    | Mn   |
|----------------|-------|-------|-------|-------|-------|-------|-------|------|
| D              | 3.534 | 0.0498| 18.99 | 0.329 | 0.0061| 0.000 | 0.670 | 0.000|
| S              | 3.228 | 0.0970| 25.11 | 0.000 | 0.332 | 0.000 | 0.145 | 0.006|
| Discard Coal   | 3.520 | 0.2773| 27.46 | 0.000 | 0.336 | 0.000 | 0.000 | 0.005|
| Com-AC         | 0.897 | 0.1238| 0.58  | 0.073 | 0.713 | 0.575 | 0.000 | 0.068|
| SC-3-600       | 3.154 | 0.1247| 24.93 | 4.064 | 0.326 | 0.000 | 0.000 | 0.007|
| SC-5-900       | 1.922 | 0.2474| 20.09 | 4.236 | 0.752 | 1.555 | 17.092| 2.798|
| DC-5-750       | 3.191 | 0.0379| 24.99 | 0.000 | 0.279 | 0.000 | 0.000 | 0.003|
| DC-7-900       | 3.306 | 0.0294| 24.81 | 0.000 | 0.489 | 0.000 | 0.000 | 0.000|
4. Conclusion

In this paper, two types of sewage sludge were used to make low-cost bio-adsorbents: D, which was collected during the dissolved air flotation stage, and S, which was a mixture of primary and secondary sludge from the digestion and dewatering stages. The sewage sludge was mixed with waste coal before being activated with KOH and oxidized with APS. The ability of the synthesized bio-adsorbents to remove nitrate and MR was assessed and compared to that of industrial activated charcoal. The oxidation with APS influenced (i) the textural properties of bio-adsorbent derived from sludge S more negatively than those derived from D, (ii) influenced organic composition only marginally as revealed by ultimate analysis, and (iii) induced the introduction of acidic functional groups as revealed by FT-IR and Raman spectroscopy analysis, respectively. Adsorbents' adsorption capability increased with time and initial concentrations of contaminants. The removal processes of nitrate and MR followed the pseudo second order kinetic model and the Langmuir isotherm reasonably well. At pH=2 and pH=4, nitrate and MR adsorption capacities were higher, respectively.

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