Performance Analysis of 6063 Aluminium Alloy Semi-Circular Two Phase Closed Thermosyphon Tpct using Fe$_{3}O_{4}$ and Graphene Nano-Fluid

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Abstract - Nanofluids stability on rest is important to characterize the nanofluids thermophysical properties before being used on different thermal systems. However, this stability can be modified during devices operation because of different thermal loads, fluid movements and phase changes. Particularly, in Two Phase Closed-Thermosyphon (TPCT), Input response are heat input, flow rate and inclination angle. Graphene and Fe$_{3}$O$_{4}$ nanofluids used as working fluid in the fill ratio of 50%. An attempt is made to optimise the process parameters with Response Surface Methodology (RSM) using Box - Behnken design for 6063 aluminium alloy (AA) semi-circular two phase closed thermosyphon (TPCT). Experiments are conducted by varying the mass flow rates of water at condenser section and by varying the heat input at evaporator section and varying inclination angle. The effects of variables on the process parameters are studied. The study, predominantly, aims at assessing how the variables affect the process parameters.

I. INTRODUCTION

Development of new technologies is hampered by heat management, exchange and evacuation for numerous fields of application. Nanofluids are a relatively recent class of fluids that have the potential to drastically increase heat exchange in energy systems compared to conventional fluids. This is achieved through the dispersion of nano-sized particles with enhanced thermal properties and stably suspended in a liquid medium. Indeed, thermal conductivity of nanofluids prepared with various nanoparticles has been reported to be enhanced compared to base liquids (water, ethylene glycol, etc.) at very low concentration of nanoparticles. Carbon nanomaterials, such as carbon nanotubes (CNTs) or graphene, which combine lightness and high thermal conductivity are widely recognized as excellent candidates for the new generation of nanofluids [1]. Incorporation of Thermosyphon, generally, a device having passive nature, can dissipate the heat in engineering operations. The device has three parts, namely the evaporator, adiabatic and condenser; the adiabatic is found between evaporator and condenser; and the evaporator found below the condenser, allows the flow of condensate using the action of gravity. This is the chief mechanism employed in the functioning of thermosyphon. Different working fluids such as DI water, acetone, refrigerants etc., are used as working fluids. These fluids have lower thermal properties which lead to cause constraints in significant heat transfer. Therefore its necessary to increase the enhanced properties of the working fluid.

Most of the studies, conducted, focus attention on cylindrical shaped geometry [2,3,4-13]. But, in the case of thermal control in space craft, cooling process in electronic applications, besides commercial thermal applications, it has been an established fact that the capacity for removing heat and adopting geometric process in several applications, is found in the heat pipes having flat shape [14-17]. Asirvatham et.al., in their study of thermosyphon using graphene – acetone nano-fluid with a concentration of 0.05%, 0.07% and 0.09% by volume and between a heat load of 10 and 50 W observed a substantial reduction in thermal resistance of 70.3% for the maximum concentration of 0.09% by volume of graphene -acetone nano-fluid.[18] Not much work was found in the literature using semi-circular 6063 AA TPCTusing graphene nano-fluid and Fe$_{3}$O$_{4}$ nano-fluid. The literature review highlights the point that the types of cross-section, working fluid and the power input determine the TPCT functioning ability. This happens because the TPCT has a complex structure of boiling process which impacts on the thermal resistance and the overall performance of the TPCT. This experiment attempts to find the range of thermal enhancement of Fe$_{3}$O$_{4}$ and the Graphene nanofluid in semi-circular 6063 AA TPCT.

II. MATERIALS AND METHODS

In order to narrow down on the choice of material be used in this study, the chemical composition test is performed and it is presented in Table 1. The chemical composition identifies the container material as having alloyed with magnesium and silicon in a high quantity by weight percentage (wt%). Therefore the grade of the material chosen for the study is semi-circular 6063AA TPCT. Some of the important properties used for the study are listed in the Table 2.

| Material Properties | Value |
|---------------------|-------|
| Density             | 2.7 g/cm$^{3}$ |
| Thermal conductivity | 200 W/mK |
| Thermal expansion coefficient | 23 m/m°C |

Table 2. Key properties of 6063 AA

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III. EXPERIMENTAL SET UP

Using semi-circular 6063 AA TPCT and a set of working fluids having different nature, the two phase closed Thermosyphon (TPCT) analysis to determine the thermal performance is engaged as shown in figure 1. The setup consists of the following equipment and facilities.

Semi-circular 6063 AA TPCTs are used for this experimental study. The inclinometer (Bevel Protector) provision is made on the test rig to rotate the TPCT through 0° - 180° angle.

In order to provide heat input the evaporator section is wrapped with 200 watts capacity and the power supply is monitored with three phase variac which can regulate the power supply necessary for the experiment. The variac employed, here, is capable of holding 1800 watts with 230 volts and 20 amps. The power supply provided to the heater of the evaporator section is maintained by a wattmeter and the 3 phase variac holds a range of 0-250 watts and 230 volts. The load administered is found on the wattmeter digital display. The TPCT gets soldered, along its entire length, with the K-type thermocouples at eight different locations, which are connected with a logger system to obtain accurate results on temperature measurement. Water passing through the condenser jacket is the appropriate mode of measuring the power output of TPCT.

A design of 6063 AA TPCT and 6063 AA jacket having 30mm outer diameter and 250mm length with the provision of inlet and outlet and positioned, diagonally, opposite to each other, to facilitate swirl flow to proposed. Similarly, the semi-circular 6063 Al Alloy TPCT jacket is also fabricated with the same material and the rotometer is attached to monitor the flow rate of coolant water discharged from the water tank.

The evaporator section of the TPCT is connected with a heat source of plate type heater with a maximum power output of 200W at 220V. The condenser section is cooled by tap water. The mass flow rate of condenser section is controlled by rotometer. The adiabatic section is insulated by glass wool to avoid heat energy interaction with the ambience. Before charging the working fluid, the TPCT enclosure is evacuated and maintained at a vacuum of 99kPa to 100kPa. Then the required amount of the working fluid is charged.

The container material was tested with a filling ratio of 50 percent. The wall temperature on the TPCT container materials is measured by eight thermocouples of K-type. Two thermocouples were mounted on the evaporator section, two on the adiabatic section and four on the condenser section. The location of thermocouples is shown in Fig 1. All the thermocouples (K-Type) are connected and monitored using 8-channel data logger system. The flat plate type heater attached to the evaporator is connected to a variac having three phases with 20 amps capacity. The heat input is varied by using a variac. The heating power input can be observed from watt meter.

Preparation of nanofluids

In the present work, a two step method was employed to prepare the nanofluids. Graphene nano particles (30nm), purchased form USA, is well dispersed into DI water at a concentration of 0.09% by volume. The well dispersed sample is subjected to the sonication process in bath type ultrasonic homogenizer (Olee Pvt Ltd, 42KHz) up to 12 hours it is shown in fig 2. Similarly Fe₃O₄ nano fluid prepared in the concentration of 0.09% by volume and sonicated for 15 hours it is shown in fig 3.

Table 3. Indicates the process parameters with their levels

| Parameters              | Level |
|-------------------------|-------|
| Heat Input, W           | 60    |
| Angle of inclination, ° | 30    |
| Flow Rate, ml/min       | 60    |
**Table 4. Indicates the Design of Matrix**

| Std | Run | Factor 1 A: Heat Input | Factor 2 B: Angle of Inclination | Factor 3 C: Flow Rate |
|-----|-----|------------------------|----------------------------------|-----------------------|
| 2   | 1   | 80                     | 60                               | 90                    |
| 1   | 2   | 80                     | 90                               | 120                   |
| 7   | 3   | 60                     | 90                               | 90                    |
| 5   | 4   | 100                    | 60                               | 120                   |
| 16  | 5   | 100                    | 90                               | 90                    |
| 9   | 6   | 100                    | 30                               | 90                    |
| 10  | 7   | 80                     | 60                               | 90                    |
| 4   | 8   | 60                     | 60                               | 60                    |
| 14  | 9   | 80                     | 30                               | 60                    |
| 13  | 10  | 80                     | 30                               | 90                    |
| 8   | 11  | 80                     | 60                               | 90                    |
| 12  | 13  | 60                     | 30                               | 90                    |
| 17  | 14  | 80                     | 60                               | 90                    |
| 3   | 15  | 100                    | 60                               | 60                    |
| 15  | 16  | 80                     | 60                               | 90                    |
| 6   | 17  | 80                     | 90                               | 60                    |

Table 4 gives the results for BBD, based on the three factors, and the simulation arranged for 17 runs in their order. The 17 runs are conducted as per the resulting design matrix by varying, the mass flow rate of pure water flowing through the condenser section using rotometer, the inclination angle of TCPT and heat input. Approximately it took 15 minutes for graphene nano-fluid and 20 min for Fe₃O₄ nano-fluid to attain the steady state. The data logger system is used to record the temperature, during each trial, after arriving at the steady state.

**A. Data reduction**

Data reduction is a process which transforms the numerical and alphabetical information available in digital form, which have been evolved empirically and experimentally into a correct, orderly and simple pattern. The principle behind this reduction is condensation of large number of data into easily accessible and relevant segments.

The following formula is used to evaluate the thermosyphon’s thermal efficiency:

\[
\eta \% = \frac{Q_{out} - Q_{in}}{Q_{in}} \times 100
\]

where,

\[ Q_{out} = m_c \cdot c_p \cdot (T_{out} - T_{in}) \]

and

\[ m_c = \text{Mass flow rate of pure water in condenser section, kg/sec.} \]

\[ c_p = \text{Specific heat of water, J/kg°C} \]

\[
T_{out} \text{ = Temperature at outlet of the water condenser section, °C} \\
T_{in} \text{ = Temperature at inlet of the water condenser section °C} \\
Q_{in} \text{ = Heat input in watts} \\
\]

Uncertainty for \( \eta \% \) is evaluated by,

\[
e = \frac{1}{\eta} \left[ \sum_{i=1}^{N} \left( \frac{1}{\eta} \frac{\partial R}{\partial x_i} \right)^2 \right]^{1/2}
\]

\[
= \left[ \left( \frac{\partial m}{m} \right)^2 + \left( \frac{\partial Q_{out}}{Q_{out}} \right)^2 + \left( \frac{\partial Q_{in}}{Q_{in}} \right)^2 \right]^{1/2}
\]

By calculating \( \eta \) for the entire experimental range, the maximum uncertainty is associated with the resulting of \( \eta \% \) values that found to be around 1.42 percent.

**IV. RESULTS AND DISCUSSION**

Response 1 EFFICIENCY – Fe₃O₄ Nano-fluid ANOVA for Response Surface Quadratic Model Analysis of variance table [Partial sum of squares - Type III]

| Source | Sum of Squares | d.f. | Mean Square | F Value | p-value | Prob > F |
|--------|---------------|------|-------------|---------|---------|----------|
| Model  | 0.14          | 9    | 0.016       | 54.56   | < 0.0001 | significant |
| A-HEAT INPUT | 0.016 | 1   | 0.016       | 57.27   | 0.0001  |          |
| B-ANGLE | 6.037E-003   | 1    | 6.037E-003  | 21.02   | 0.0025  |          |
| C-FLOW RATE | 0.040 | 1   | 0.040       | 140.6   | < 0.0001 |          |
| AB     | 4.381E-004   | 1    | 4.381E-004  | 1.52    | 0.2567  |          |
| AC     | 1.947E-004   | 1    | 1.947E-004  | 0.68    | 0.4375  |          |
| BC     | 6.845E-004   | 1    | 6.845E-004  | 2.38    | 0.1666  |          |
| A²     | 0.014         | 1    | 0.014       | 47.83   | 0.0002  |          |
| B²     | 4.266E-003   | 1    | 4.266E-003  | 14.85   | 0.0063  |          |
| C²     | 0.053         | 1    | 0.053       | 184.0   | < 0.0001 |          |
| Residual | 2.011E-003  | 7    | 2.873E-004  |         |         |          |
| Lack of Fit | 2.011E-003 | 3    | 6.703E-004  |         |         |          |
| Pure Error | 0.000        | 4    | 0.000       |         |         |          |
| Cor Total | 0.14         | 1    | 0.14        |         |         |          |
|         | 6            |      |             |         |         |          |
The Model F-value of 54.56 indicates the model as important. The model F value of such a magnitude can occur rarely with 0.01% of chance because of noise. This large could occur due to noise.

The model term is considered significant when the “prob>F” value is found less than 0.0500. Here, the model terms A,B,C,A^2,B^2 and C^2 are considered significant. When the model terms values are found greater than 0.1000 they are considered not significant.

In case the number of insignificant model terms, excepting those which support the hierarchy, is large in number, the model reduction will improve the efficiency of the model.

The Pred R-Squared value of 0.7751 is in reasonable agreement with the Adj R-Squared value of 0.9679. “Adeq Precision” measures the signal to noise ratio. A ratio greater than 4 is desirable. Your ratio of 21.435 indicates an adequate signal. This model can be used to navigate the design space.

| Factor         | Coefficient Estimate | d.f. | Standard Error | 95% CI Low | 95% CI High | VIF |
|----------------|----------------------|------|----------------|------------|-------------|-----|
| Intercept      | 0.71                 | 1    | 7.580E-003     | 0.69       | 0.72        |     |
| A: HEAT INPUT  | 0.045                | 1    | 5.992E-003     | 0.03       | 0.060       | 1.0 |
| B: ANGLE       | 0.027                | 1    | 5.992E-003     | 0.01       | 0.042       | 1.0 |
| C: FLOW RATE   | 0.071                | 1    | 5.992E-003     | 0.05       | 0.085       | 1.0 |
| AB             | -0.010               | 1    | 8.474E-003     | -0.03      | 9.574       | 1.0 |
| AC             | 6.977E-003           | 1    | 8.474E-003     | 0.01       | 0.027       | 1.0 |
| BC             | -0.013               | 1    | 8.474E-003     | 0.03       | 6.958       | 1.0 |
| A^2            | -0.057               | 1    | 8.260E-003     | -0.07      | -0.038      | 1.0 |
| B^2            | -0.032               | 1    | 8.260E-003     | 0.05       | -0.012      | 1.0 |
| C^2            | -0.11                | 1    | 8.260E-003     | -0.13      | -0.093      | 1.0 |

Final Equation in Terms of Coded Factors:

\[
\text{EFFICIENCY} = +0.71 +0.045 \times A +0.027 \times B +0.071 \times C -0.010 \times A \times B +6.977 \times E-003 \times A \times C -0.013 \times B \times C -0.055 \times A^2 -0.032 \times B^2 -0.11 \times C^2
\]

Final Equation in Terms of Actual Factors:

\[
\text{EFFICIENCY} = 0.7751 
-1.87149 \times 21.435 
+0.025116 \times \text{HEAT INPUT} 
+7.86328E-003 \times \text{ANGLE} 
+0.024724 \times \text{FLOW RATE} 
-1.74417E-005 \times \text{HEAT INPUT} \times \text{ANGLE} 
+1.16278E-005 \times \text{HEAT INPUT} \times \text{FLOW RATE} 
-1.45347E-005 \times \text{ANGLE} \times \text{FLOW RATE} 
-1.42804E-004 \times \text{HEAT INPUT}^2 
-3.53678E-005 \times \text{ANGLE}^2 
-1.24514E-004 \times \text{FLOW RATE}^2
\]

The thermal efficiency is found to increase gradually with increase in heat input and angle. Integrated effect of inclination angle and flow rate maximum thermal efficiency is achieved. Whereas the combinatorial effect of heat input and flow rate shows the high value of thermal efficiency. On account of the heat flux increase, caused by the increase of temperature gradient occurring between evaporator and condenser, there is an increase in the thermal efficiency of heat pipe (Amit Faghri 2016). The heat input shows higher values as more heat is generated in the surface and the working fluid, found in state of vapour, enters rapidly into the condenser section.
The performance of the TPCT increases when the excess heat is absorbed by the circulating water in the condenser section. Hence, the influential input parameters among are the heat input at evaporator inclination angle Richter and Gottschlich, (1994) and flow rate. However, the semi-circular cross section carries the heat and transport in a proper way from evaporator section to condenser section with minimum heat loss. This occurs since the surface temperature, in the evaporation section, is found higher than the vapour temperature, the heat gets transferred to vapour core as the evaporator maintains direct contact with the electrical heater. The advantage of using semi-circular cross section helps in returning the working fluid quickly to the evaporator section from the condenser section after give up the heat. This phenomenon eventually maximizes the efficiency.

Response 1 EFFICIENCY – graphene nano-fluid
ANOVA for Response Surface Quadratic Model
Analysis of variance table [Partial sum of squares - Type III]

| Source         | Sum of Squares | d.f | Mean Square | F Value | P-value | Prob > F | F values | Significance |
|----------------|----------------|-----|-------------|---------|---------|----------|----------|-------------|
| Model          | 0.33           | 9   | 0.036       | 127.7   | < 0.0001| < 0.0001|          |             |
| A-HEAT INPUT   | 2.196E-003     | 1   | 2.196       | 7.75    | 0.027   |          |          |             |
| B-ANGL E       | 5.476E-005     | 1   | 5.476       | 0.19    | 0.673   |          |          |             |
| C- FLOW RATE   | 0.23           | 1   | 0.23        | 808.1   | < 0.0001|          |          |             |
| AB             | 0.013          | 1   | 0.013       | 46.77   | 0.0002  |          |          |             |
| AC             | 1.947E-004     | 1   | 1.947       | 0.69    | 0.434   |          |          |             |
| BC             | 0.011          | 1   | 0.011       | 38.65   | 0.004   |          |          |             |
| A²             | 0.011          | 1   | 0.011       | 39.34   | 0.004   |          |          |             |
| B²             | 0.027          | 1   | 0.027       | 93.59   | < 0.0001|          |          |             |
| C²             | 0.025          | 1   | 0.025       | 89.52   | 0.0001  |          |          |             |
| Residual       | 1.983E-003     | 7   | 2.834       |         |         |          |          |             |
| Lack of Fit    | 1.983E-003     | 3   | 6.612       |         |         |          |          |             |
| Pure Error     | 0.000          | 4   | 0.000       |         |         |          |          |             |
| Cor Total      | 0.33           | 6   | 0.000       |         |         |          |          |             |

The Model F is considered significant as it records the value of 127.73 and the model F value of this magnitude could occur with 0.01% chance.

When the model has the value of less than 0.0500 for “prob>F”, it is considered as significant. indicate model terms are significant.

Here the A, C, AB, BC, A², B² and C² are considered as they show the “prob>F” values as greater than 0.1000 to as certain that the model terms as non significant. In the event of more number of insigificant model terms occur, excepting those needed to maintain support hierarchy, the model reduction will improve the model.

The "Pred R-Squared" of 0.9032 is in reasonable agreement with the "Adj R-Squared" of 0.9862. "Adeq Precision" measures the signal to noise ratio. A ratio greater than 4 is desirable.

Your ratio of 3.4315 indicates an adequate signal. This model can be used to navigate the design space.

Analysis of variance table [Partial sum of squares - Type III]

| Factor       | Coefficient Estimate | d.f | Standard Error | 95% CI Low | 95% CI High | VI F |
|--------------|----------------------|-----|----------------|------------|-------------|------|
| Intercept    | 0.78                 | 1   | 7.528E-003     | 0.77       | 0.80        |
| A-HEAT INPUT | -0.017               | 1   | 5.951E-003     | -0.03      | 2.497       |
| B-ANGL E     | 2.616E-003           | 1   | 5.951E-003     | -0.01      | 0.017       |
| C-FLOW RATE  | 0.17                 | 1   | 5.951E-003     | 0.16       | 0.18        |
| AB           | 0.058                | 1   | 8.417E-003     | 0.03       | 0.077       |
| AC           | 6.977E-003           | 1   | 8.417E-003     | -0.01      | 0.027       |
| BC           | -0.052               | 1   | 8.417E-003     | -0.07      | -0.032      |
| A²           | -0.051               | 1   | 8.203E-003     | -0.07      | -0.032      |
| B²           | -0.079               | 1   | 8.203E-003     | -0.09      | -0.060      |
| C²           | -0.078               | 1   | 8.203E-003     | -0.09      | -0.058      |

Final Equation in Terms of Coded Factors:
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The circulating inclination angle and then decreases.

The fig 7. shows the effect of heat input and inclination angle on thermal efficiency. The figure shows how the effect of heat input causes gradual decrease in the thermal efficiency, initially, and increase when there is increase in flow rate causing a steep increase in the efficiency of the thermal state. The interactive effect of flow rate and angle increases the thermal efficiency. The heat flux being the cause for the increased thermal efficiency of the heat pipe, there is an increase in the temperature gradient lies between the evaporator and condenser section. For higher values of heat input in evaporator section, the heat generated in the surface is more and graphene nano-fluid which is in form of vapor moves vigorously in to the condenser section. The circulating water, in the condenser section, absorbs the excessive heat and so the efficiency of TPCT increases. Hence, the influential input parameters are the heat input at evaporator inclination and flow rate. The thermal efficiency is maximum up to 60$^0$ inclination angle and then decreases. Since the viscosity of graphene nano fluid is more so it shows a Newtonian behaviour when compared to Fe$_3$O$_4$ nano-fluid.

The fig 10. Shows the optimized value for semi – circular cross section TPCT along with Fe$_3$O$_4$ and graphene nano fluid . semi -circular TPCT with graphene nano-fluid the enhancement in thermal performance is 5% more when compare to Fe$_3$O$_4$ nano-fluid filled semi-circular tpt . this is because of higher wettability of graphene nano-fluid that enhances the efficiency .

V. CONCLUSIONS

- It is aimed to investigate the performance of semi -circular TPCT with Fe$_3$O$_4$ and graphene nano-fluids. Out of the present study the following conclusions have been made .
- The semi-circular 6063 AA TPCT increases the number of nucleation site and enhances the boiling characteristics as it introduces a large number of nucleation bubbles which are small in size.
- The presence of high nucleation bubble enhances high efficiency as high wetting of condenser occurs while using working fluid as graphene.
- Graphene nano-fluid the enhances the thermal performance by 5% more when compared to Fe$_3$O$_4$ nano-fluid filled semi-circular TPCT.
- In the magnetic fluid (Fe$_3$O$_4$ nano-fluid), the surface temperature is found higher than the vapour temperature in the evaporator section as the evaporator maintain direct contact with the electrical heater, hence the heat is transferred to the vapour core area. The advantage of using semi-circular cross section returning the working fluid quickly to the evaporator section from the condenser section after eliminating the heat. This phenomenon eventually increases efficiency.
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