Generation of real algebraic loci via complex detours

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Abstract
We discuss the locus generation algorithm used by the dynamic geometry software Cinderella, and how it uses complex detours to resolve singularities. We show that the algorithm is independent of the clockwise or anticlockwise orientation of its complex detours. We conjecture that the algorithm terminates if it takes small enough complex detours and small enough steps on every complex detour. Moreover, we introduce a variant of the algorithm that possibly generates entire real connected components of real algebraic loci. Several examples illustrate its use for organic generation of real algebraic loci. Another example shows how we can apply the algorithm to simulate mechanical linkages. Apparently, the use of complex detours produces physically reasonable motion of such linkages.

1 Introduction

A locus is a set of points in the plane with a common geometric property. For example, a circle is the set of points whose distance from the centre of the circle equals the radius of the circle. Here we focus on loci that are closed curves generated by dynamic geometric constructions.

The generation of loci has a very long history. We roughly follow the exposition of (Brieskorn and Knörrer, 1986, Chapter 1). Many ancient Greek mathematicians studied geometric constructions. Some classical problems, e.g. squaring the circle, duplication of the cube (Delian problem), and angle trisection, resisted any attempt of solution using only compass and straightedge. Unlike the ancient Greeks, we know that these problems cannot be solved by compass and straightedge constructions.[1]

1 Wantzel (1837) showed that using compass and straightedge, we can only construct points with coordinates in a field extension of \( \mathbb{Q} \) obtained by adjoining all roots of degree a power of two of rational numbers. He proved that duplication of the cube and angle trisection reduce to solving irreducible cubic equations, which is therefore impossible using only compass and straightedge.

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After many failed attempts using only compass and straightedge, the ancient Greeks sought other means of solving these problems. Menaechmus (c. 350 BC) found that duplication of the cube could be performed using compass, straightedge and conic sections. Other plane algebraic curves classically used as devices for duplication of the cube and angle trisection include the cissoid of Diocles (c. 180 BC) and the conchoid of Nicomedes (c. 180 BC). Diocles and Nicomedes solved duplication of the cube and angle trisection by intersecting these curves with other geometric elements. In order to find the intersections, it is essential that we can construct not only some points but whole arcs of these curves in a continuous manner.

To that end, we can use dynamic compass and straightedge constructions. We move one element of the construction, e.g. we rotate a line about a point or slide a point on a line/circle, and follow a point constructed from the moving element as it traces a curve. If the construction steps can be described algebraically, then the resulting curve is a real connected component of a plane algebraic curve. Such constructions for various curves were known to the ancient Greeks. Newton, who investigated this technique, called it ‘organic generation’.

We can use dynamic geometry software to carry out such constructions. Some applications allow us to select a line through a point or a point on a line/circle, which shall be the moving element (mover), and a dependent point, which shall be followed as it traces a curve (tracer). The software then attempts to automatically generate the real connected component of the real plane algebraic curve that is the locus of the tracer under movement of the mover.

Depending on the underlying model of geometry (and depending on the algorithm used), the software may fail to generate the entire real connected component of the real algebraic curve. [Kortenkamp (1999) Section 6.2, esp. Theorem 6.8] shows that dynamic geometry systems with geometric primitives like ‘intersection of a circle with a line’ or ‘angle bisector of two lines’ cannot be both determined and continuous: If we require that we can determine a unique instance of a construction for every possible position of its free elements (movable elements), then we cannot expect that its dependent elements always move continuously.

The reason behind this is that ‘intersection of a circle and a line’ or ‘angle bisector of two lines’ are ambiguous geometric operations. In general, a circle and a line have two (possibly complex) intersections. In general, two lines have two angle bisectors, which are perpendicular to each other. Consider an angle bisector of two (unoriented) lines $a$, $b$ through a common point $P$. If we rotate $a$ about $P$ and the angle bisector moves continuously, then the angle bisector rotates at half the angular velocity. When $a$ has rotated by an angle of $\pi$, it has reached its initial position. At the same time, the angle bisector has rotated by an angle of $\pi/2$ and has become perpendicular to its initial position. We have

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Squaring the circle reduces to constructing $\pi$. In the nineteenth century, it was known that $\pi$ is irrational. Mathematicians wondered whether it could be a solution of an equation of degree a power of two that was potentially solvable using only compass and straightedge by iterative construction of square roots. [Lindemann (1882)] settled the case, showing that $\pi$ is transcendental, i.e. not a root of any algebraic equation.
moved continuously from one possible instance of the construction to the other. Therefore the dynamic geometric system cannot be determined.

For that reason, we may sometimes observe dependent elements jump unexpectedly in most dynamic geometry software. If a tracer jumps during locus generation, the algorithm may miss part of its real algebraic locus.

As we have seen, if we want to avoid jumping elements, we need to take all possible output elements of ambiguous geometric operations into account. We parameterize the motion of the mover using a time parameter $t$. There may be some points in time when part of the construction degenerates or when two possible choices of a dependent element coincide and become indistinguishable. We call such points in time singularities. For example, the two intersections of a circle and a line coincide when we move the centre of the circle such that it merely touches the line. If we can somehow avoid singularities, then we can always distinguish all possible choices. Hence, we may be able to determine the instance that produces a continuous evolution of the construction.

In order to avoid jumping elements in their dynamic geometry software Cinderella (Kortenkamp and Richter-Gebert, 2006), Kortenkamp and Richter-Gebert introduced the paradigm of ‘complex detours’ (Kortenkamp, 1999 esp. Chapter 7; Kortenkamp and Richter-Gebert, 2001; 2002): We do not let the time parameter run along the real time axis where we often encounter singularities. Instead, we embed the real time axis as the real axis of the complex plane. Between two points on the real time axis, we let the time parameter take a detour through the complex plane to circumvent singularities. Thus we can avoid singularities with high probability.

The locus generation algorithm of Cinderella exploits this principle; it has been working very well in practice for many years, but from a theoretical perspective, the algorithm has not been examined in more detail yet (Richter-Gebert, 2014). In what follows, we analyze the algorithm and some assumptions on which it is based. Moreover, we introduce a variant of the algorithm that might always generate an entire real connected component of a real algebraic locus.

2 A locus generation algorithm

The locus generation algorithm addresses the following problem: Consider a geometric construction. Choose an element of the construction whose movement is constrained to one dimension, e.g. a line through a point, a point on a line, or a point on a circle. We call this element ‘mover’. Choose a point of the construction whose position depends on the position of the mover. We call this point ‘tracer’. Suppose the tracer can be constructed from the mover (and possibly further elements) using only geometric operations that have an algebraic representation. Then movement of the mover causes the tracer to move on a real plane algebraic curve. The goal of the locus generation algorithm is to automatically produce the locus of the tracer under movement of the mover.

The following locus generation algorithm has two variants. Variant A is
essentially equivalent to the locus generation algorithm implemented in Cinderella. Variant B possibly generates an entire real connected component of a real algebraic locus (see Conjecture 5.1).

Algorithm 2.1 (locus generation algorithm). We rationally parameterize the motion of the mover using a time parameter $t$. We assume that we start at a non-singular initial time $t_0 \in \mathbb{R}$ when the position of the tracer is real-valued.

1. Let $s := 1$, $t := t_0$.
2. Let $t' := t + s \cdot \varepsilon$ for some small step size $\varepsilon > 0$.

Consider the circle $c$ in the complex plane that has the segment between $t$ and $t'$ as its diameter. We let the time parameter take a complex detour on this circle.

3. Let $t$ take a small step on circle $c$ in anticlockwise direction.
4. Update the position of the mover according to its parameterization in $t$.
5. Update the rest of the construction. In doing so, for ambiguous elements, use proximity between old and new positions of the elements to determine the right instance of the construction.

6. **Variant A** If $t$ is real-valued and the tracer has real-valued coordinates, the tracer has reached a point of the real plane algebraic locus. It may happen that $t$ ends up in its initial position on circle $c$. In this case, we invert the direction of movement of the mover. To that end, we set $s := -s$. (Note that this affects only the choice of sampling points of time parameter $t$; the anticlockwise orientation of complex detours remains the same.) If $t = t_0$, $s = 1$, and the tracer has reached its initial position again, we stop. Otherwise, we go to step 2.

If $t$ is not real-valued or the tracer does not have real-valued coordinates, we go to step 3.

**Variant B** If the tracer has real-valued coordinates, it has reached a point of the real algebraic locus. It may happen that $t$ is not real-valued or that it ends up in its initial position on circle $c$. In any case, we update the direction of movement of the mover. To that end, we set

$$s = \frac{t - a}{|t - a|},$$

where $a$ denotes the centre of circle $c$. If $t = t_0$ and the tracer has reached its initial position again, in the initial direction of movement of the time parameter, we stop. Otherwise, we go to step 2.

If the tracer does not have real-valued coordinates, we go to step 3.

Remark 2.2. Algorithm 2.1 evaluates the geometric construction only at discrete points in time along a complex detour. At every sampling point, the algorithm should select the right instance of the construction, i.e. the instance that yields
a continuous evolution of the construction. More precisely, we want that the coordinates of the elements of the construction are locally analytic functions of time; the algorithm should select the instance that results from analytic continuation of the coordinate functions along the complex detours.

If the coordinates are analytic functions of time, then in particular they are continuous. Hence, if we take a small step in time along the complex detour, the coordinates change only little. If the step is small enough then we can select the right instance (in the above sense) by proximity, i.e. we choose every ambiguous element so that its coordinates change least.

Besides the assumption that we start at a non-singular initial time when the position of the tracer is real-valued, Algorithm 2.1 is based on the following assumptions. (This list of assumptions may not be complete; Algorithm 2.1 may be based on further implicit assumptions.)

Assumption 2.3. We assume that we always choose $\varepsilon$ small enough so that the complex detours wind around at most one ramification point of a coordinate of the tracer, and only around ramification points at which the position of the tracer is real-valued. Thus we preclude that the tracer jumps from one real arc of the real algebraic locus to another due to a complex detour around a ramification point of a coordinate at which the tracer has a complex position close to the real algebraic locus.

Assumption 2.4. We assume that the steps we take on the complex detour are small enough so that we can choose the right instance of the construction by proximity (see Remark 2.2).

Assumption 2.5. We assume that the steps we take on the complex detours are small enough so that we do not miss a real position of the tracer.

Remark 2.6. While we usually satisfy Assumption 2.4 in practice, it is very difficult to guarantee that it is satisfied in general. We cannot go into details here but refer to (Kortenkamp and Richter-Gebert, 2002).

Remark 2.7. While we usually satisfy Assumption 2.3 in practice, it is not clear how to guarantee that it is satisfied in general.

Remark 2.8. For Variant A of Algorithm 2.1 we can satisfy Assumption 2.5 if we ensure that time parameter $t$ always attains the real values on the complex detours. For Variant B of Algorithm 2.1 we must additionally determine complex points in time on the complex detours when the coordinates of the tracer are real-valued. We can try to approximate these points in time by bisection if the imaginary part of a coordinate of the tracer changes sign or has small absolute value; this may be really difficult in practice.

Remark 2.9. Since a real algebraic locus can contain points at infinity, it may sometimes be advantageous to describe the plane algebraic curve containing the real algebraic locus by a homogeneous equation $f(x, y, z) = 0$. Thus we can express points of the locus at infinity using finite coordinates $(x, y, z)\top$. We can homogenize an affine equation $f(x, y) = 0$ of total degree $n$ by plugging in
\[ x = x/z, \ y = y/z, \ \text{and multiplying by } z^n. \] If we set \( z = 1 \), we return to the affine equation.

**Remark 2.10.** If we use homogeneous coordinates \( (x, y, z)^\top \) to describe the position of the tracer, we require that none of \( x, y, \) and \( z \) become infinite; if necessary, we constantly normalize \( (x, y, z)^\top \) to avoid that one of the coordinates grows too much.

### 3 Orientation of complex detours

In Step 3 of **Algorithm 2.1**, we specify that time parameter \( t \) takes complex detours along circles in the complex plane in anticlockwise direction. In principle, \( t \) can also take complex detours in clockwise direction. Are there constructions where the generated locus changes depending on the clockwise or anticlockwise orientation of the complex detours?

In order to answer this question, we make some assumptions on the real algebraic loci to which we apply our locus generation algorithm, without loss of generality. Let

\[
C: f(x, y) = 0
\]
denote a plane algebraic curve containing such a locus.

**Assumption 3.1.** We assume that \( f(x, y) \) is irreducible. An analytic transition from one irreducible component of \( f(x, y) \) to another is impossible. Therefore, if \( f(x, y) \) is reducible, we can without loss of generality consider the irreducible component containing the starting point. (Note that the assumption that we start **Algorithm 2.1** at a non-singular initial time precludes that we start at an intersection of irreducible components.)

**Assumption 3.2.** We assume that \( C \) has a real connected component. Otherwise, the locus is not a real connected component of a real plane algebraic curve and the locus generation algorithm is not applicable.

**Lemma 3.3.** Under **Assumption 3.1** and **Assumption 3.2**, without loss of generality, \( f(x, y) \) has only real coefficients.

**Proof.** Conversely, suppose \( f(x, y) \) has complex coefficients. Then we can write \( f(x, y) \) in the form \( f(x, y) = f_R(x, y) + if_I(x, y) \) such that the real part polynomial \( f_R(x, y) \) and the imaginary part polynomial \( f_I(x, y) \) possess only real coefficients. By the assumption that \( f(x, y) \) has complex coefficients, \( f_I(x, y) \) does not vanish identically. If \( f_R(x, y) \) vanishes identically, then \( f(x, y) = if_I(x, y) \) and we can cancel the unit \( i \) from the equation \( f(x, y) = 0 \) to obtain an equation for \( C \) with only real coefficients. Hence, suppose that both real part polynomial and imaginary part polynomial do not vanish identically. By **Assumption 3.2**, \( C \) has a real connected component, i.e. over a real interval of \( x \)-values, \( f(x, y) \) vanishes for real \( y \)-values. This can only be the case if \( f_R(x, y) \) and \( f_I(x, y) \) vanish there, i.e. if \( f_R(x, y) \) and \( f_I(x, y) \) have infinitely many common zeros. If \( f_R(x, y) \) and \( f_I(x, y) \) have infinitely many common zeros, then they must have a common component
or \( f_3(x, y) \) must be a non-zero real multiple of \( f_R(x, y) \). By Assumption 3.1 \( f_R(x, y) \) and \( f_3(x, y) \) are irreducible; they cannot have a common component. Therefore, \( f_3(x, y) \) must be a non-zero real multiple of \( f_R(x, y) \). Hence, we can write \( f_3(x, y) = \lambda \cdot f_R(x, y) \) for some \( \lambda \in \mathbb{R} \). Therefore, \( f(x, y) = (1+i\lambda) f_R(x, y) \), i.e. \( f(x, y) \) has only real coefficients up to multiplication by a unit in \( \mathbb{C} \), which we can cancel from the equation \( f(x, y) = 0 \).

**Lemma 3.4.** Consider a plane algebraic curve \( K: p(x, y) = 0 \), where \( p(x, y) \) is a polynomial with only real-valued coefficients. The paths of the \( y \)-values on the complex plane algebraic curve \( K \) under complex conjugate movement of \( x \) are complex conjugate.

**Proof.** \( K \) is the zero set of a polynomial \( p(x, y) \) with only real coefficients. Real coefficients are invariant under complex conjugation. Hence, if we consider the complex conjugate of the defining equation of \( K \), we find that

\[
0 = \overline{0} = \overline{p(x, y)} = p(\overline{x}, \overline{y}),
\]

and \( p(\overline{x}, \overline{y}) \) vanishes if and only if \( p(x, y) \) vanishes.

Let \( x(t) \) be a parameterization of the movement of \( x \) through the complex plane. Let \( y(t) \) be a parameterization of the corresponding analytic motion of a \( y \)-value so that \( p(x(t), y(t)) = 0 \), for all \( t \). Then to complex conjugate movement of \( x \), parameterized by \( x(t) \), corresponds complex conjugate motion of the \( y \)-value, parameterized by \( y(t) \), since

\[
 p(x(t), y(t)) = 0 \Leftrightarrow p(\overline{x(t)}, \overline{y(t)}) = 0.
\]
(The \( y \)-values must be the same in both cases since they must agree at all real points of the complex plane algebraic curve \( K \), where complex conjugation has no effect.)

**Remark 3.5.** Suppose we can construct the tracer from the mover (and possibly further elements) using only geometric operations that have an algebraic representation. Moreover, suppose that the motion of the mover is rationally parameterized in time parameter \( t \). Then the \( x \)-coordinate and the \( y \)-coordinate of the tracer satisfy algebraic equations \( g(t, x) = 0 \) and \( h(t, y) = 0 \). In practice, it may often be too expensive to work these equations out symbolically. But in principle, we can determine an equation \( f(x, y) = 0 \) for the locus of the tracer by taking the \( t \)-resultant of \( g(t, x) \) and \( h(t, y) \) to eliminate \( t \) from these equations.

**Theorem 3.6.** The locus generation algorithm is independent of the clockwise or anticlockwise orientation of its complex detours.

**Proof.** By Remark 3.5 the \( x \)-coordinate of the tracer is determined by an algebraic equation \( g(t, x) = 0 \). Analogously to Assumption 3.1, Assumption 3.2, and Lemma 3.3, we may assume that \( g(t, x) \) has only real coefficients, without loss of generality. If we reverse the orientation of the complex detours, we obtain complex conjugate movement of time parameter \( t \). By Lemma 3.4 the motion

\[\]
of $x$ such that $g(t, x) = 0$ under complex conjugate movement of $t$ is complex conjugate. Particularly, the real values of $x$ resulting from either movement agree. The same argument applies to the algebraic equation $h(t, y) = 0$ that governs the motion of $y$ under movement of $t$. Consequently, Algorithm 2.1 produces the same real algebraic locus, independent of the clockwise or anticlockwise orientation of its complex detours.

4 Termination

Does the locus generation algorithm always terminate? Or can we get lost on algebraic Riemann surfaces?

Analogously to the previous section, we assume that $f(x, y)$ is an irreducible polynomial (cf. Assumption 3.1) with real coefficients (cf. Assumption 3.2 and Lemma 3.3).

Besides, recall the assumptions on which the locus generation algorithm (Algorithm 2.1) is based: Firstly, we assume that the complex detours of Algorithm 2.1 are small enough so that they wind around at most one ramification point of a coordinate of the tracer, and only around ramification points at which the position of the tracer is real-valued (Assumption 2.3). Thus we preclude that the tracer jumps from one real arc of the real algebraic locus to another due to a complex detour around a ramification point of a coordinate at which the tracer has a complex position close to the real algebraic locus. Secondly, we assume that the steps we take on the complex detours are small enough so that we can choose the right instance of the construction by proximity (Assumption 2.4) and so that we do not miss a real position of the tracer (Assumption 2.5).

A proof of termination of Algorithm 2.1 has remained elusive so far. However, the successful application of Variant A of Algorithm 2.1 in Cinderella supports the following conjecture:

Conjecture 4.1. The locus generation algorithm terminates if it takes small enough complex detours and small enough steps on every complex detour.

5 Generation of real connected components

Conjecture 5.1. Variant B of Algorithm 2.1 generates an entire real connected component of a real algebraic locus if it takes small enough complex detours and small enough steps on every complex detour.

Remark 5.2. Variant A of Algorithm 2.1 need not generate an entire real connected component of a real algebraic locus. It may miss real arcs of a locus that correspond to non-real complex values of time parameter $t$. For an example, see Section 6.2.

Remark 5.3. A real connected component of a real algebraic locus need not be an algebraic curve by itself. For example, consider a four-bar linkage with bars of lengths 4, 1, 4, and 2. (We discuss how we can express a mechanical linkage in
terms of dynamic geometry in Section 6.4.} We leave the first bar of the linkage fixed and trace the midpoint of the third bar under continuous movement of the linkage. Then the four-bar linkage generates one of the two real connected components of the plane algebraic sextic

\[ C: f(x, y) = (6 + 5x - 2x^3)^2 + 3(-45 + 4x(-2 + 2x + x^3))y^2 + 4(11 + 3x^2)y^4 + 4y^6 = 0. \]

The algebraic curve $C$ is irreducible (over the complex numbers). Thus, each of the two real connected components by itself cannot be an algebraic curve.

6 Examples

6.1 Conic through five points in general position

Consider Pascal’s theorem (also known as ‘hexagrammum mysticum’):

**Theorem 6.1** (Pascal’s theorem). If $A, B, C, D, E, F$ are six points on a conic, then opposite sides of the hexagon $ABCDEF$ (extended to lines, if necessary) meet in three collinear points.

For more details and proofs, see (Richter-Gebert, 2011, esp. Section 1.4 and Section 10.6).

The converse of the theorem is also true, which gives rise to organic generation of a conic through five points, by the following construction (see Figure 6.2).

![Figure 6.2: An instance of Construction 6.3. When line $c$ rotates about point $F$, point $K$ traces the conic through points $A, B, C, D, E$.](image)

**Construction 6.3.** Let $A, B, C, D, E$ be five points of the real projective plane, in general position.
1. Let $a$ be the line through $A$ and $B$.
2. Let $b$ be the line through $D$ and $E$.
3. Let $F$ be the intersection of $a$ and $b$.
4. Let $c$ be a line through $F$.
5. Let $d$ be the line through $B$ and $C$.
6. Let $G$ be the intersection of $c$ and $d$.
7. Let $e$ be the line through $C$ and $D$.
8. Let $H$ be the intersection of $c$ and $e$.
9. Let $f$ be the line through $A$ and $H$.
10. Let $g$ be the line through $E$ and $G$.
11. Let $K$ be the intersection of $f$ and $g$.

When line $c$ rotates about point $F$, point $K$ traces the conic through points $A, B, C, D, E$.

Remark 6.4. Construction 6.3 does not distinguish the orientation of line $c$. Point $K$ returns to its initial position after half a turn of line $c$ about point $F$. If line $c$ makes a full turn, point $K$ traces the conic through points $A, B, C, D, E$ twice.

6.2 Orthogonal projection of a circle onto a line

We consider the following (seemingly simple) construction (see Figure 6.5), because it highlights the difference between Variant A and Variant B of Algorithm 2.1.

![Figure 6.5: An instance of Construction 6.6. When point A moves around on circle $c_0$, point B traces a segment of line $b$.](image)
**Construction 6.6.** Let a line $b$, a circle $c_0$, and a point $A$ on circle $c_0$ be given.

1. Let $a$ be the line through $A$ perpendicular to $b$.
2. Let $B$ be the intersection of $a$ and $b$.

When point $A$ moves around on circle $c_0$, point $B$ traces a segment of line $b$.

**Remark 6.7.** For simplicity, we use the geometric primitive ‘perpendicular to a line through a point’. It can be easily constructed with compass and straightedge (see Book I, Proposition 12 of Euclid’s Elements).

**Remark 6.8.** Line $a$ intersects circle $c_0$ in two points (counted with multiplicity). Hence there are two positions of point $A$ (counted with multiplicity) for every position of point $B$ on the segment that point $B$ traces on line $b$. In other words, point $B$ covers the segment twice as point $A$ makes a full turn on circle $c_0$.

Let us work out the real algebraic locus of point $B$ under movement of point $A$ on circle $c_0$ algebraically. Without loss of generality, let $c_0$ be the unit circle and $b$ the line parallel to the $y$-axis intersecting the $x$-axis at $x = 2$. Let $O$ denote the origin. We need to parameterize the motion of point $A$ on circle $c_0$. To that end, we can use trigonometric functions, as follows:

$$A = (\cos \varphi, \sin \varphi)^	op, \quad -\pi \leq \varphi \leq \pi.$$

However, this parameterization is not rational. We use tangent half-angle substitution,

$$t = \tan \frac{\varphi}{2}, \quad \cos \varphi = \frac{1 - t^2}{1 + t^2}, \quad \sin \varphi = \frac{2t}{1 + t^2};$$

and homogeneous coordinates to derive the rational parameterization

$$A = (1 - t^2, 2t, 1 + t^2)^	op, \quad t \in \mathbb{R}.$$

Line $b$ has homogeneous coordinates

$$b = (1, 0, -2)^	op.$$

Line $a$ is perpendicular to line $b$ and therefore has homogeneous coordinates of the form

$$a = (0, 1, z(t))^	op,$$

where $z(t)$ has to be determined so that point $A$ lies on line $a$, i.e. so that

$$\langle a, A \rangle = 2t + z(t)(1 + t^2) = 0.$$

Hence, homogeneous coordinates of line $a$ are

$$a = (0, 1 + t^2, -2t)^	op.$$
We obtain homogeneous coordinates of point $B$ by taking the cross product of line $a$ and line $b$,

$$B = a \times b = (2(1 + t^2), 2t, 1 + t^2)\top \sim \left(2, \frac{2t}{1 + t^2}, 1\right)\top.$$

The real algebraic locus of point $B$ under movement of point $A$ on circle $c_0$ is described by the implicit equations

$$\begin{align*}
x - 2 &= 0 \\
t^2y - 2t + y &= 0.
\end{align*}$$

If we take the $t$-resultant of these equations, we arrive at a single equation for the real algebraic locus,

$$(x - 2)^2 = 0.$$

The construction has singularities at $t = \pm 1$, where the $y$-coordinate of point $B$ equals $\pm 1$. If we solve the equation between $t$ and the $y$-coordinate of point $B$,

$$t^2y - 2t + y = 0,$$

for $t$, we find that

$$t = \frac{1 \pm \sqrt{1 - y^2}}{y}.$$

For real $y$-values of absolute values greater than 1, $t$ becomes complex. Point $B$ moves higher or lower than the (real-valued) extreme positions of point $A$ on circle $c_0$ if and only if we allow point $A$ to become complex.

Variant A of [Algorithm 2.1] does not allow this to happen and skips the branch of the real algebraic locus where point $B$ has real-valued coordinates, but point $A$ (and thus $t$) is complex-valued. It generates that part of the real algebraic locus where both mover and tracer have real-valued coordinates.

Variant B of [Algorithm 2.1] does not skip the branch of the real algebraic locus where point $B$ has real-valued coordinates, but point $A$ (and thus $t$) is complex-valued. It generates the entire real algebraic locus.

Variant A seems more appropriate from the perspective of real projective geometry; Variant B seems more appropriate from the algebraic perspective.

### 6.3 Conchoid of Nicomedes

The conchoids of Nicomedes are a family of quartic plane algebraic curves

$$C: f(x, y) = (y + a)^2(x^2 + y^2) - b^2y^2 = 0, \quad a, b > 0.$$

For organic generation of a conchoid, we can use the following construction.

**Construction 6.10** (conchoid of Nicomedes). Let $A$ be a point on a line $g$. Let $B$ be a point at distance $a > 0$ from $g$. Let $c_0$ be a circle of radius $b$ centred at $A$. 
Figure 6.9: An instance of Construction 6.10. When point $A$ moves along line $g$, point $C$ traces the conchoid with pole $B$, base $g$ and distance $b$.

1. Let $h$ be the line through $A$ and $B$.

2. Let $C$ be an intersection of $c_0$ and $h$.

When point $A$ moves along line $g$, point $C$ traces the conchoid with pole $B$, base $g$, and distance $b$.

As mentioned in the introduction, part of the original motivation to study the conchoid of Nicomedes was that it can be used for angle trisection. The following construction is based on [Ferréol and Mandonnet, 2005, Conchoïde de Nicomède, http://www.mathcurve.com/courbes2d/conchoiddenicomede/conchoiddenicomede.shtml].

Figure 6.11: An instance of Construction 6.12. By construction, angle $\angle HEG$ trisects angle $\angle DEF$.

**Construction 6.12** (angle trisection). Let $\angle DEF$ be the angle to be trisected. We can trisect a right angle by constructing an equilateral triangle. Hence, without loss of generality, let angle $\angle DEF$ be acute.

1. Let $l$ be the line through $E$ and $F$. 
2. Use Construction 6.10 to generate the conchoid with pole $D$, base $l$, and distance $|DE|$.

3. Let $c_1$ be the circle centred at $E$, through $F$.

4. Let $G$ be the intersection of $c_1$ with the conchoid that lies on the same side of $l$ as $F$.

5. Let $m$ be the line through $D$ and $G$.

6. Let $H$ be the intersection of $l$ and $m$.

Then angle $\angle HEG$ trisects angle $\angle DEF$.

**Proof.** By construction of the conchoid, points $H$ and $E$ are equidistant to point $G$. Therefore, triangle $\triangle EGH$ is equilateral and

$$\angle HEG = \angle GHE.$$ 

We apply the exterior angle theorem to triangle $\triangle EGH$ and find that

$$\angle DGE = \angle GHE + \angle HEG = 2 \cdot \angle HEG.$$ 

Triangle $\triangle GED$ is equilateral by construction, and thus

$$\angle EDG = \angle DGE = 2 \cdot \angle HEG.$$ 

We apply the exterior angle theorem to triangle $\triangle HED$ and conclude

$$\angle DEF = \angle GHE + \angle EDH = \angle GHE + \angle EDG = \angle HEG + 2 \cdot \angle HEG = 3 \cdot \angle HEG.$$ 

\[\square\]

### 6.4 Watt curves

We can use Algorithm 2.1 to simulate mechanical linkages. For example, the following construction uses a four-bar linkage to generate a Watt curve, a plane algebraic sextic

$$C: f(x, y) = (x^2 + y^2)(x^2 + y^2 - a^2 - b^2 + c^2)^2 + 4a^2 y^2(x^2 + y^2 - b^2) = 0$$

with parameters $a, b, c > 0$.

**Construction 6.14.** Let $A$ and $B$ be two points in the plane at distance $2a$ from each other. Let $c_0$ be a circle with centre $A$ and radius $b$. Let $c_1$ be a circle with centre $B$ and radius $b$.

1. Let $C$ be a point on $c_0$.

2. Let $c_2$ be a circle with centre $C$ and radius $2c$.

3. Let $D$ be an intersection of $c_1$ and $c_2$. 

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4. Let $E$ be the midpoint of the segment between $C$ and $D$.

When point $C$ moves on circle $c_0$ according to Algorithm 2.1 point $E$ traces a Watt curve with parameters $a = |AB|/2$, $b = |AC| = |BD|$, and $c = |CD|/2$.

Remark 6.15. The first bar of the four-bar linkage, segment $AB$, has length $2a$. Circles $c_0$, $c_1$, and $c_2$ have fixed radii. Hence, they prescribe the lengths $|AC| = b$, $|CD| = 2c$, and $|DB| = b$ of the remaining bars of the four-bar linkage.

Remark 6.16. Depending on parameters $a, b, c$, Watt curves have a wide variety of different shapes.

Remark 6.17. In Figure 6.13 we choose parameters $a, b, c$ so that $a > c$. Therefore, the movement of point $C$ on circle $c_0$ is constrained. If point $C$ moved too far to the left, then circles $c_1$ and $c_2$ would move apart and would no longer have real-valued intersections. Such movement is not possible without breaking the linkage. Algorithm 2.1 resolves the singularities when circles $c_1$ and $c_2$ merely touch each other, by taking complex detours around them. At every such singularity, point $C$ reverses its direction of movement on circle $c_0$. Apparently, Algorithm 2.1 produces a physically reasonable motion of the four-bar linkage.
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