Optimizing the Choice of Limestone Deposits for the Production of Portland Cement in Cameroon

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Abstract: Despite the presence of raw materials (limestone and clay) deposits for Portland cement production, the major part of cement sold in Cameroon is from crushed imported clinker. This contributes to high cost of this material and reduction of local employment. In this study and based on existing data, a multi-criteria analysis tool was developed and applied to guide decision in the choice of limestone deposits in Cameroon for the production of Portland cement. The criteria evaluated were: calcium carbonate (CaCO₃) content of limestone, proximity of the limestone deposit to a qualified clay source, estimate of its capacity, area covered by the limestone deposit, extraction of limestone easiness, accessibility to the limestone deposit and the proximity of the limestone deposit to a source of energy. The study is conducted on twelve limestone deposits identified by previous studies around the country. The PROMETHEE II methodology used made it possible to highlight the best deposits with respect to the criteria set. The results showed in terms of preference that, the Bidzar and Mintom deposits respectively in the North and South Regions are the two best deposits to be considered for the local production of Portland cement. Their exploitation will more promote purely local cement industry in Cameroon.

Keywords: Cameroon, Limestone Deposits, Portland Cement Production, Multi-criteria Analysis, Promethee II

1. Introduction

Cameroon, like all other developing countries, is experiencing considerable growth in terms of infrastructure development in recent years [1]. This is leading to a growing demand for building materials, of which Portland cement is a major component. This cement is the main binder used in construction for the manufacture of concrete, mortars and plaster. It is obtained after firing at about 1450°C a mixture of 80% limestone and 20% clay to obtain Portland clinker which is then crushed with other admixtures such as gypsum and pozzolans to obtain the final cement. Four over five Portland cement plants located in Cameroon are crushing imported clinker with negative consequences on the cost of finished products and local jobs. Physicochemical characteristics of the raw materials for Portland clinker production have been presented by several authors [2, 3]. For clinker composition, limestone is the source of calcium carbonate (CaCO₃) and clay that of silica (SiO₂), alumina (Al₂O₃) and iron oxide (Fe₂O₃). Deposits of limestone and clay are scattered throughout the whole territory of Cameroon. Only on the basis of their physicochemical characteristics and the capacity of deposits, previous work has stated that Cameroonien limestone could be suitable for the production of Portland clinker [4]. However, these two criteria are not the only ones to be considered in order to actually set up a cement industry. To manufacture a ton of clinker, 1.55 to 1.60 tons of raw materials, mainly consisted
of limestone is required. This justifies the proximity of the cement plant to the limestone source, to avoid long distance transportation of this raw material [2]. Since the mixture is heated to about 1450°C, a source of energy is necessary around the production area [2]. Other criteria such as the proximity of the limestone deposit to a qualified clay deposit, the extraction easiness of the resource and the accessibility to the deposit are also to be taken in consideration.

The objective of the present study is to provide optimized guiding data for the sustainable production of Portland cement in Cameroon, using the multi-criteria approach.

2. Method

In recent years, several multi-criteria decision making techniques (MCDA) have been suggested to select the best materials for a particular application [5-8]. The selection of the most appropriate MCDA method is performed by comparing the property framework characterizing each MCDA method with the qualifications that the method must possess (the expected properties), depending on the decision problem to be solved and taking into account both the exogenous and endogenous variables. The weighting of the variables (optional action): A set of variables (representing the criteria) and their potential qualifications. In the present study, the Preference Ranking Organization Method for Enrichment Evaluations (PROMETHEE) II multi-criteria synthesis improvement method was chosen [9].

2.1. Materials

Table 1 indicates the main limestone deposits in Cameroon. They are located in South-west, South, Littoral and North Regions.

| Region       | Deposit       | Code | Geographic location | Area (S) | Depth (H) | % of CaCO₃ | Estimated capacity (tons) | Ref.   |
|--------------|---------------|------|---------------------|----------|-----------|-------------|----------------------------|--------|
| North        | Figuïl        | D1   | 9°45'32" X 13°57'32" Y | -        | -         | 90          | 600000                    | [10-13]|
|              | Bidzarr       | D2   | 14°7" X 9°53'45"      | -        | -         | 95          | 2 500000                  |        |
|              | Leb-Ngô        | D3   | 10°1'38" X 3°55'27"    | -        | -         | -           | -                         |        |
|              | Koa-nalép     | D4   | 10°01'41" X 3°56'00"   | -        | -         | 35 m        | 66                        |        |
|              | Logbadjéck    | D5   | 10°01'15" X 3°55'55"   | -        | 42 m      | -           | -                         |        |
|              | Ngol           | D6   | 9°45'52" X 4°51'00"    | -        | -         | 98          | 10 000000                 |        |
|              | Mungo Balangui| D7   | 4°7' X 4°31'50"        | -        | -         | 93,5        | 7-9000000                 |        |
|              | Kompina        | D8   | 9°35'22" X 4°21'25"    | -        | 5 m       | 84 à 92     |                            | [10]   |
| South        | Mintom         | D9   | 13°40'30" X 2°1000" and 2°40'01" | 700 ha   | -         | 98          | 1458 000000               | [14]   |
|              | Bogonkó        | D10  | 9°07' X 4°37"          | -        | -         | 76,32       | -                         | [15]   |
| South-West   | Lobé           | D11  | 9°0525" X 4°34'25"     | 50 ha    | 7-8 m     | 92,5        | -                         | [4, 10]|
|              | Moko           | D12  | 8°54' and 8°55' X 4°50' and 4°52' | -        | 0,2-9 m   | 51           | -                         | [4]    |

2.2. PROMETHEE II Multi-criteria Method

In this study, the Preference Ranking Organization Method for Enrichment Evaluations (PROMETHEE) II multi-criteria synthesis improvement method [9] have been chosen because it relies on the elementary mechanism which is the two-to-two comparison of actions according to each criterion. It is based on the weighting of threshold criteria and produces a ranking of actions, [16]. PROMETHEE II makes a judicious comparison of two alternatives in each criterion in order to determine the partial binary relations presenting the preferences of the alternatives «a» on the alternative «b» [9, 17]. After considering a set of actions A= {a₁,a₂,a₃,...,aₙ}, it classifies these actions by comparing them in pairs. Each action is compared to others on the basis of the criteria considered. The evaluation of the actions is carried out by a real function. For each criterion, the set G = {g₁,g₂,...,gₙ} containing the evaluation of the action on all the criteria is defined. The importance of the criteria in decision-making is evaluated by a set of weights W = {w₁,w₂,...,wₙ}. For this method, the difference, preference and veto thresholds depend on the evaluation of the action for each criterion.

For an action a, evaluated by gᵢ(a) for the criterion j, in this case the difference threshold is noted qᵢ(gᵢ(a)), the preference threshold pᵢ(gᵢ(a)) and the standard deviation σᵢ(gᵢ(a)). These thresholds depend on the evaluations of the actions according to each criterion; they can vary in an interval from 10 to 20% around their initial value in order to take account of uncertainty relating to the data [18]. Taking into account an uncertainty of 10%, the following proposal can be made:

\[
pᵢ = 2 \times 10% \times \max_{i,k}(g_i(a_i) - g_i(a_k));
\]
\[
qᵢ = 10% \times \max_{i,k}(g_i(a_i) - g_i(a_k));
\]
\[
σᵢ = 3 \times 10% \times \max_{i,k}(g_i(a_i) - g_i(a_k))
\]

The value of the preference function is either 0 or 1 and it is defined separately for each criterion [16]. These evaluations mainly involve quantitative data and require two types of additive information, namely: relative import information which is the weight of the criterion considered and information of the preference function used when comparing the contributions of the alternatives of each criterion.
2.3. Weight Coefficient

The weight measures the relative importance of the criteria as seen by the decision maker. This measure is not always easily determined by the decision maker in many situations. Methods for evaluating the weights of the criteria [19] are developed to overcome this difficulty. The weighing of the criteria therefore corresponds to the attribution of a weight to each chosen criterion which can be determined by several methods among which: the weighted analysis, the weighted vote, the entropy method and the hierarchization criteria [20]. In this study, the entropy method is retained because the weight reflects the experience of the decision-makers and their insights.

2.4. Preference Function

The PROMETHEE methods are based on an extension of the notion of criterion by the introduction of a function expressing the Preference $F_j(a,b)$ the decision-maker have for an action $a_i$ with respect to another action $a$. For each criterion, the decision-maker is called to choose one of the six curve shapes represented in table 2. The parameters relating to each curve represent indifference and / or preference thresholds.

| Function | Expressions | Shape |
|----------|-------------|-------|
| Usual    | $F_j(a,b) = \begin{cases} 1 & \text{if } g_j(a) > g_j(b) \\ 0 & \text{if } g_j(a) \leq g_j(b) \end{cases}$ | $F(a,b)$ |
| U-shape  | $F_j(a,b) = \begin{cases} 1 & \text{if } g_j(a) - g_j(b) > q_j \\ 0 & \text{if } g_j(a) - g_j(b) \leq q_j \end{cases}$ | $F(a,b)$ |
| V-shape  | $F_j(a,b) = \begin{cases} 1 & \text{if } g_j(a) - g_j(b) > p_j \\ 0 & \text{if } g_j(a) - g_j(b) \leq 0 \end{cases}$ | $F(a,b)$ |
| Level    | $F_j(a,b) = \begin{cases} 1 & \text{if } g_j(a) - g_j(b) > p_j \\ 0 & \text{if } g_j(a) - g_j(b) \leq q_j \end{cases}$ | $F(a,b)$ |
| Linear   | $F_j(a,b) = \begin{cases} 1 & \text{if } g_j(a) - g_j(b) > p_j \\ 0 & \text{if } g_j(a) - g_j(b) \leq q_j \end{cases}$ | $F(a,b)$ |
| Gaussian | $F_j(a,b) = 1 - \exp\left(-\frac{(g_j(a) - g_j(b))^2}{2\sigma^2}\right)$ (with $\sigma = \text{standard deviation}$) | $F(a,b)$ |

2.5. Implementation of the PROMETHEE II Method

The PROMETHEE II method is implemented as follows:

Step 1:
For each criterion, one of the six forms of curves proposed above, and the parameters associated with it are chosen.

Step 2:
For each pair of shares $(a_i, a_k)$, the preferably global matrix (degree of over classing) is calculated as follows:

$$P(a_j, a_k) = \frac{\sum_{i=1}^{n} w_i \times F_j(a_i, a_k)}{\sum_{i=1}^{n} w_i}$$  (1)

Step 3:
The outgoing ($\Phi^+(a_i)$) and the incoming $\Phi^-(a_i)$ flows for
each action \( a_i \) are calculated as follows:

\[
\Phi^+(a_i) = \sum_{a_k \in A \land a_k \neq a_i} P(a_i, a_k)
\]

(2)

Positive flow that expresses the strength of \( a_i \) outgoing flow;

\[
\Phi^-(a_i) = \sum_{a_k \in A \land a_k \neq a_i} P(a_k, a_i)
\]

(3)

Negative flow which expresses the weakness of \( a_i \) incoming flow.

Step 4 : Arranging shares in descending order of net flows \( \Phi(a_3) \) defined as follows:

\[
\Phi(a_i) = \Phi^+(a_i) - \Phi^-(a_i)
\]

(4)

At the end, PROMETHEE II provides a total pre-order.

2.6. Evaluation of Criteria

Seven criteria (\( C_i \)) used in the present study are detailed below. Each criterion is split in three levels or sub-criterion

(1)(C1): Calcium carbonate content (\( \text{CaCO}_3 \)) generally called "carbonate titration" [3], which varies from one deposit to another. When \( \text{CaCO}_3 \) content \( \geq 80\% \), the source is said to be prior; for \( 75\% < \text{CaCO}_3 \) content \( < 80\% \), the source is acceptable and \( \text{CaCO}_3 \) content \( < 75\% \), the source is unqualified [22, 23].

(2)(C2): Proximity of the limestone deposit to a qualified clay source. According to Spencer [2], the capacity of the clay source must be one-fifth of that of the limestone deposit. Its proximity to the limestone deposit reduces the costs of transporting this material. Based on previous studies, six major clay deposits have been identified for the production of Portland clinker (Table 3). The minimum distances between the limestone deposits and those of clays were estimated using the map of roads in Cameroon. Thus deposits located within 50 km of the limestone deposit are prior, those between 50 and 100 km are acceptable and those at more than 100 km, the transportation cost will be high.

| Region         | Locality     | Geographic location | Oxides | Ref. |
|---------------|--------------|---------------------|--------|------|
| North         | Figuil       | 13°57′46″N   9°45′31″E | X: 46.40, Y: 16.27, Al₂O₃: 8.77, Fe₂O₃: 6.35, CaO: 1.53, MgO: 0.86, K₂O: 0.34 | [24] |
| Centre        | Etoa         | 11°27′21″N 3°45′04″E | X: 50.11, Y: 24.80, Al₂O₃: 5.42, Fe₂O₃: 0.48, CaO: 0.46, MgO: 0.67, K₂O: 0.04 | [25] |
| Littoral      | Bonkoul      | 9°48′04″N 4°06′07″E | X: 48.01, Y: 27.41, Al₂O₃: 7.34, Fe₂O₃: 0.06, CaO: 0.31, MgO: 0.31, K₂O: 0.02 | [26] |
| West          | Mayoum       | 10°22′53″N 5°50′88″E | X: 63.02, Y: 25.79, Al₂O₃: 1.06, Fe₂O₃: < id, CaO: < id, MgO: 0.87, K₂O: < id | [27] |
| North-West    | Lembo (Mont Bana) | 10°20′02″N 5°57′00″E | X: 68.10, Y: 21.60, Al₂O₃: 1.04, Fe₂O₃: 0.03, CaO: 0.062, MgO: 2.57, K₂O: 0.093 | [28] |
|               | Sabga        | 10°18′02″N 6°02′00″E | X: 68.23, Y: 13.57, Al₂O₃: 6.60, Fe₂O₃: 0.68, CaO: 0.44, MgO: 0.44, K₂O: 0.21 | [29] |

|     | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|-----|-----|-----|-----|-----|-----|-----|-----|
| (C1)| (C2)| (C3)| (C4)| (C5)| (C6)| (C7)|     |
|     |     |     |     |     |     |     |     |
| (C1)| Calcium carbonate content (\( \text{CaCO}_3 \)) generally called "carbonate titration" [3], which varies from one deposit to another. When \( \text{CaCO}_3 \) content \( \geq 80\% \), the source is said to be prior; for \( 75\% < \text{CaCO}_3 \) content \( < 80\% \), the source is acceptable and \( \text{CaCO}_3 \) content \( < 75\% \), the source is unqualified [22, 23].
|     |     |     |     |     |     |     |     |
| (C2)| Proximity of the limestone deposit to a qualified clay source. According to Spencer [2], the capacity of the clay source must be one-fifth of that of the limestone deposit. Its proximity to the limestone deposit reduces the costs of transporting this material. Based on previous studies, six major clay deposits have been identified for the production of Portland clinker (Table 3). The minimum distances between the limestone deposits and those of clays were estimated using the map of roads in Cameroon. Thus deposits located within 50 km of the limestone deposit are prior, those between 50 and 100 km are acceptable and those at more than 100 km, the transportation cost will be high.
|     |     |     |     |     |     |     |     |
| (C3)| Estimated capacity of the deposit: the potential must be exploitable for at least 30 years [30]. The qualification of the limestone deposit must be made according to the demand for cement [2]. In the case of Cameroon, the demand for cement is estimated at 3 million tons / year. Considering that, the production of Portland clinker requires 80% of limestone, a deposit capacity equal or more than 72 millions tons of limestone will be preferable. Otherwise between 48 millions and 17 millions tons would be acceptable but, less than 48 millions would not allow a return in investment.
|     |     |     |     |     |     |     |     |
| (C4)| The area of the limestone deposit: that area is also a major criterion in the choice of limestone deposits. It must be greater than 300 ha [2]. Between 200 and 300 ha, the deposit can be acceptable in function of the depth of the layer of the ore. An area of less than 200 ha is negligible.
|     |     |     |     |     |     |     |     |
| (C5)| Limestone extraction easiness: it depends if the deposit is open, deep or under water. This situation may affect the extraction of the material and the position or the activation of explosives. In this case, surfaced limestone is preferable, followed by deposits with material at negligible depth. Deposits underwater are less preferable.
|     |     |     |     |     |     |     |     |
| (C6)| Accessibility to the limestone deposit: the paved road and the presence of the bridges on the watercourse facilitate access to the site to allow the exploitation and transportation of the material. The ideal would be that, the limestone deposit is close to a paved road for less than 50 km, between 50 and 100 km would be acceptable but more than 100 km, accessibility would be very difficult.
|     |     |     |     |     |     |     |     |
| (C7)| Proximity of the limestone deposit to a source of energy production: energy cannot be neglected because the production of cement is energy intensive. The electricity consumption is between 70 and 160 kWh/ton of cement and this energy represents between 30 to 40% of the production cost of the cement. The main fuels used for firing clinker are: petroleum, coke, coal and lignin, some wastes, heavy fuel oil and gas [31]. In the context of Cameroon, the sources of energy selected are: hydroelectric and thermal power plants. Table 4 shows the energy sources and their minimum distances from the limestone deposits. Distance of 50 km from the energy source would be ideal, between 50 and 100 km would be acceptable and at more than this distance, energy availability would be considered difficult.
An important step in a decision analysis is the stage where the decision maker structures the hierarchy of criteria in the decomposition of groups into sub-criteria. In the framework of this study, 7 different evaluation criteria are defined and the values of the scores are given on the basis of quantitative and qualitative measures. The scale of 1 to 10 is used for the calibration of the criteria described analytically [32]. Then their characteristics are shown in Table 5. The ranking of deposit as a function of one criterion is done by scoring. The first alternative obtains high scores on particular criteria, the second half and the last obtain the low scores.

### Table 5. Calibration of the 7 criteria in the (1-10) scale.

| Criteria | Description | Score |
|----------|-------------|-------|
| C₁       | 80%<CaCO₃ content ≤ 100% | 10    |
| C₁       | 75% ≤ CaCO₃ content <80% | 5     |
| C₁       | A clay deposit located less than 50 km | 1     |
| C₂       | A clay deposit located between 50 and 100 km | 10    |
| C₂       | A clay deposit located further than 100 km | 1     |
| C₃       | Deposit capacity ≥ 72 000 000 tons | 10    |
| C₃       | Deposit capacity < 72 000 000 tons | 5     |
| C₄       | Deposit Area ≥ 300 ha | 10    |
| C₄       | Deposit Area < 300 ha | 5     |
| C₅       | Deposit Area < 200 ha | 1     |
| C₅       | Deposit at the surface | 10    |
| C₆       | Deposit at negligible depth | 5     |
| C₆       | Underwater deposit | 1     |
| C₇       | Bituminous road within 50 km | 10    |
| C₇       | Bituminous road between 50 and 100 km | 5     |
| C₇       | Bituminous road located further than 100 km | 1     |
| C₇       | Deposit within 50 km of an energy production unit | 10    |
| C₇       | Deposit between 50 and 100 km from an energy production unit | 5     |
| C₇       | Deposit located more than 100 km from an energy production unit | 1     |

#### 2.7. Criteria Weight Coefficients

In this work, all the criteria are weighted according to their degree of importance, by the weight coefficient by criterion and sub criterion. The determination of the weight of a criterion (table 6) was based on:

i. The experience observed in the application of this decision support tool;

ii. The specific data of each deposit obtained by the documentary analysis of the work carried out in this field, observations and existing infrastructures in the country;

iii. Opinions and suggestions of some actors in the field of industry, research and decision-making in the field of Portland cement [33].

The weights were distributed in such a way that: the chemical composition of the raw materials and the estimated capacity was attributed 20%, the proximity to a qualified clay source, the area of the deposit and the limestone extraction easiness 15%, the accessibility 5% and proximity of an energy source 10%. The sum of the weight is 100% and the final coefficient retained is that obtained after multiplication of the weight of the criterion by the weight of the group [35] which is presented in Table 6. PROMETHEE II fully classifies alternatives from best to worst using the net flow. The analysis of the sensitivity of the results can be done according to the change of "weight" and "thresholds".

### Table 6. Estimation of criteria final weights.

| Criteria description | Weight |
|----------------------|--------|
| Chemical composition(C₁) | 20    |
| Proximity to a qualified clay source(C₂) | 15    |
| Estimated capacity(C₃) | 20    |
| Area of the deposit(C₄) | 15    |
| Limestone extraction easiness(C₅) | 15    |
| Accessibility to the deposit(C₆) | 5     |
| Proximity with an energy source(C₇) | 10    |

#### 2.8. Application of the Method and Presentation of Results

Table 7 served as a content template in the "performances.xls" file and summarized the indiffERENCE and preference criteria. It presented the 1.8 preference threshold, the 0.9 indiffERENCE threshold and the 2.7 veto threshold, as well as the performance of the scores for each deposit in each criterion.

The first application consisted of the Usual, U-shape, V-shape, Level and Linear functions individually and by calculating each time the flows to classify the deposits in table 8. This presented a complete ranking of alternatives,
from best to worst based on their net flow. The second application consisted of varying only the Gaussian function and the results are shown in Table 9. The last application combined all the six functions of the PROMETHEE II method, calculated the flows and gave the ranking presented in Table 10. From the algorithm obtained, a Matlab program was realized which imported the performances edited in the Excel file. It collected for each resource, the evaluations of each criterion. The preference scales of criteria must be either increasing (value to be maximized) or decreasing (value to be minimized). At the end, it calculated the matrixes of global preference, the flow vectors entering, leaving and finally the net flow.

The preference threshold is set at 20% of the difference between the highest score and the lowest one, while, the indifference threshold is set at 10% of the same difference. The preference threshold indicated that the strict preference (F_p(a,b) = 1) of the alternatives a on b is only observed if the difference in performance is greater than this threshold. At the indifference threshold, if the difference in the performance is greater than this threshold.

### Table 7. Performances for the classification of limestone deposits.

| Criteria | C1 | C2 | C3 | C4 | C5 | C6 | C7 |
|----------|----|----|----|----|----|----|----|
| Weight   | 20 | 15 | 20 | 15 | 15 | 5  | 10 |
| Preferred Threshold | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 |
| Threshold of indifference | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 |
| Threshold of veto | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |
| Alternatives (Limestone deposits) |
| D1 | 10 | 10 | 1 | 10 | 10 | 1 |
| D2 | 10 | 10 | 10 | 10 | 10 | 1 |
| D3 | 1 | 5 | 1 | 10 | 1 | 1 |
| D4 | 1 | 5 | 1 | 1 | 5 | 1 |
| D5 | 1 | 10 | 1 | 1 | 5 | 10 |
| D6 | 10 | 1 | 1 | 10 | 10 | 1 |
| D7 | 10 | 1 | 1 | 1 | 10 | 1 |
| D8 | 10 | 10 | 1 | 5 | 5 | 10 |
| D9 | 1 | 10 | 10 | 10 | 1 | 10 |
| D10 | 1 | 1 | 1 | 10 | 10 | 1 |
| D11 | 10 | 1 | 1 | 5 | 1 |
| D12 | 1 | 1 | 1 | 5 | 1 |

### Table 8. Flow matrix and classification of limestone deposits with variation of Usual, U-shape, V-shape, Level, and Linear functions.

| Alternatives | D1 | D2 | D3 | D4 | D5 | D6 | D7 | D8 | D9 | D10 | D11 | D12 |
|--------------|----|----|----|----|----|----|----|----|----|-----|-----|-----|
| Φ+           | 3.4 | 4.9 | 2.5 | 1.75 | 2.25 | 2.2 | 2.2 | 3.25 | 5.7 | 1.2 | 1.15 | 0.15 |
| Φ-           | 1.07 | 2.9 | 3.8 | 3.1 | 1.9 | 1.9 | 1.7 | 2.55 | 3.3 | 3.2 | 4.6 |
| Φ            | 2.4 | 4.2 | -0.4 | -2.05 | -0.85 | 0.3 | 0.3 | 1.55 | 3.15 | -2.1 | -2.06 | -4.45 |
| Rank         | 3   | 1  | 10 | 8  | 5  | 5  | 4  | 2  | 11 | 9   | 12  |

### Table 9. Flow matrix and classification of limestone deposits with Gaussian function.

| Alternatives | D1 | D2 | D3 | D4 | D5 | D6 | D7 | D8 | D9 | D10 | D11 | D12 |
|--------------|----|----|----|----|----|----|----|----|----|-----|-----|-----|
| Φ+           | 1.37 | 2.06 | 0.82 | 0.57 | 0.9 | 0.87 | 0.87 | 1.36 | 2.6 | 0.41 | 0.49 | 0.03 |
| Φ-           | 0.46 | 0.32 | 1.21 | 1.47 | 1.22 | 0.8 | 0.8 | 0.57 | 0.94 | 1.45 | 1.23 | 1.87 |
| Φ            | 0.9 | 1.73 | -0.38 | -0.89 | -0.31 | 0.07 | 0.07 | 0.78 | 1.66 | -1.04 | -0.73 | -1.84 |
| Rank         | 3   | 1  | 8  | 10 | 7  | 5  | 5  | 4  | 2  | 11  | 9   | 12  |

The results presented in Table 9 show that the Bidzar deposit is at the top of the rankings with an outflow of 2.06, an inflow of 0.32 and a net flow of 1.73 followed by the Mintom deposit with an outflow of 2.6, a flow of entering 0.94 and a net flow of 1.66. Ranked third was the Figuil deposit with an outflow of 1.37, an inflow of 0.46 and a net flow of 0.9. From the 7th position, the net flows also become negative, which shows that from this rank the deposits become

### 3. Results

#### 3.1. Performances and Flow Matrix

The results presented in Table 8 show that the Bidzar deposit is at the top of the rankings with an outflow of 4.9, an inflow of 0.7 and a net flow of 4.2 followed by the Mintom deposit with an outflow of 5.7, an inflow of 2.55 and a net flow of 3.15. The third rank was for the Figuil deposit with an outflow of 3.4, an inflow of 1 and a net flow of 2.4. The deposit of Komppina is at the 4th rank. In the 5th rank are the Ngol and Mungo Balangui deposits with the same flows that are 2.2 as outflow, 1.9 as inflow and 0.3 as net flow. At the 7th rank, the net flow becomes negative, which shows that from this rank the deposits become unusable because the inflow is greater than the outflow. The unfavorable criteria are superior to the favorable operating criteria. The end of the ranking was occupied by the Bogongo deposit (11th position) deposit with an outflow of 1.2, an inflow of 3.3 and a negative net flow of 2.1 and finally the Moko deposit (12th position) with an outflow of 0.15, an inflow 4.6 and a negative net flow of 4.45.
The results presented in Table 10 show once more that the Bidzar deposit comes at the top of the rankings with an outflow of 4.36, an inflow of 0.43 and a net flow of 3.93 followed by the Mintom deposit with an outflow of 4.78, an inflow of 2.55 and a net flow of 2.23. In the third rank is the Figuil deposit with an outflow of 2.86, an inflow of 0.73 and a net flow of 2.13. The 5th position is occupied by the Ngol and Mungo Balangui deposits with the same outflow of 1.66, an inflow of 1.63 and net flow of 0.03. From the 7th position, the net flow also becomes negative. The end of classification is occupied this time by the Lobé deposit in 11th position with an outflow of 0.61, an inflow of 2.93 and a negative net flow of 2.32 and finally the Moko deposit with an outflow of 0.15, an inflow of 3.57 and a negative net flow of 3.42.

From the Excel spreadsheet, the flow histogram showing the outflow, inflow and net flow from each deposit according the application from tables 8-10 was plotted (Figure 1-3).

Figure 1. Histogram of Flows of limestone deposits with Usual, U-shape, V-shape, Level and Linear functions.

The results presented in Figure 1 show the high outflow for the Mintom deposit followed by Bidzar and the high inflow for the Moko deposit with a very low outflow justifying the fact that deposits with negative net flows do not fulfill the operating conditions.

Figure 2. Histogram of flows of limestone deposits with Gaussian function.

Table 10. Flow matrix and classification of limestone deposits with combination of the 6 functions.

| Alternatives | D1  | D2  | D3  | D4  | D5  | D6  | D7  | D8  | D9  | D10 | D11 | D12 |
|--------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Φ+           | 2.86| 4.36| 2.12| 1.37| 1.87| 1.66| 1.66| 2.33| 4.78| 1.2 | 0.61| 0.15|
| Φ-           | 0.73| 0.43| 2.14| 3.04| 2.34| 1.63| 1.63| 1.7  | 2.55| 2.27| 2.93| 3.57|
| Φ            | 2.13| 3.93| -0.02| -1.67| -0.47| 0.03| 0.03| 0.63| 2.23| -1.07| -2.32| -3.42|
| Rank         | 3   | 1   | 7   | 10  | 8   | 5   | 5   | 4   | 2   | 9   | 11  | 12  |
The results presented in Figure 2 show the outflow almost half high from the value of Figure 1 for the Mintom deposit followed by Bidzar with a low inflow. The high inflow for the Moko deposit and an outflow almost equal to the net flow justify the fact that deposits with inflows greater than outflows do not fulfill the conditions of exploitation.

![Figure 3. Histogram of Flows of limestone deposits with combination of the 6 functions.](image)

The results presented in Figure 3 show that the flow values of this figure are comparable to those of the Figure 1. Some deposits such as Kouamalep and Lobe have increased their inflow and are losing their positions.

### 3.2. Final Arrangement

The final arrangement consisted of ordering the actions in descending order of the scores $\Phi(a_i)$ was defined as follows:

$$\Phi(a_i) = \Phi^+(a_i) - \Phi^-(a_i).$$

Using Tables 8-10, the upgrade charts below from best to worst deposit was build.

![Figure 4. Classification of limestone deposits with the Usual, U-shape, V-shape, Level and Linear functions.](image)

The upgraded chart in Figure 4 shows the ranking of the best to worst deposits as follows: the first is the Bidzar deposit, then Mintom, Figuil, Kompina, Mungo Balangui and Ngol at the same rank, Leb-Ngog, Logbadjeck, Lobe, Kouamalep, Bogongo, and finally the Moko deposit.

The over-classification graph of Figure 5 has the same classification as that of the graph of Figure 4, but with generally low net flow values.
Figure 5. Classification of limestone deposits with Gaussian function.

Figure 6. Classification of limestone deposits with variation of the 6 PROMETHEE II functions.

The upgraded chart in Figure 6 shows the ranking of the best to worst deposits as follows: the first is the Bidzar deposit, then Mintom, Figuil, Kompina, Mungo Balangui and Ngol at the same rank, Leb-Ngog, Logbadjeck, Bogongo, Kouamalep, Lobe and finally the Moko deposit.

4. Discussion of Results

The results show that:

(1) The criteria with quantitative evaluation are prior the easiest to use for an aggregation. However, they present the problem of unit uniformity and require standardization at the level of the sub-criteria;

(2) Qualitative criteria are tricky to manage and require the decision-maker's subjective intervention to score the actions on a discrete scale large enough to account for all the possible sensitivity aspects of the decision maker (for example, a scale from 0 to 10);

(3) The PROMETHEE II method is easy and comprehensible for the user. It makes it possible to establish a net classification. Compared to the other methods of outclassing of synthesis, each solution has a
(4) The results obtained after having varied each type of criterion individually and simultaneously are satisfactory. The order was identical from the first to the sixth place. It proved that the PROMETHEE II method is adapted to the analysis with a good stability of results.

(5) The present method has established that each deposit has a rank of its own. The values presented in figures 4 to 6 quantify the degree to which each field outperforms (positive value) or is outperformed (negative value) by others:

ii From the over-classification graphs (Fig. 4-5), it can be seen that the applications with the first 5 functions of the PROMETHEE II method and the Gaussian function give the net ranking of the limestone deposits in Cameroon compared to the combination of 6 functions that maintain the same ranking of the first 6 deposits in which the deposits of Bogongo and Kouamalep have outperformed the Lobé deposit with a slight increase in flows as shown in Fig. 6. The Moko deposit occupied the last rank. The classification retained being the following:

ii The best deposit is that of Bidzar. This deposit is already being exploited by the first pure local cement company producing 180 000 tons of clinker per year [35]. This fact validated the precision of the method;

iii The Mintom deposit, which is estimated at 1458,000,000 tons of raw materials with about 98% CaCO₃, ranked second. This position of the deposit is mostly due to the fact that the deposit is under the river Dja [10] making it difficult to exploit despite its important volume;

iv The third is the Figuil deposit, which is not far from Bidzar and could be exploited for cement production by the local cement company in addition to the Bidzar deposit;

v The Kompina deposit is fourth and it is not yet exploited like that of Mungo, Balangui and Ngol at the same rank. Limestone deposits of Leb-Ngog, Logbadjeck, Lobe, Kouamalep, Bogongo and Moko obtained low ranks because of their low percentage in CaCO₃ varies between 35 and 51%. The deposits of Mungo Balangui and Ngol were ex-aequo in all the various classifications showing similar evaluation performance in the decision of investment in cement production with these deposits;

vi With only the matrix of evaluations, it could have not be easy to have the idea about the best alternative showing that the PROMETHE II method formalizes well the desired aggregation;

vii The PROMETHEE II method with the Gaussian function allowed a complete classification of alternatives from the best to the worst according to the net flows [34]. The change in the weight of the criteria makes it possible to highlight the results of the comparisons of the deposits. It showed that the deposits of Bidzar and Mintom achieved the best compromise between the criteria for the industrial production of Portland clinker in Cameroon and they are therefore the two best choices for that investment.

5. Conclusion

This study was devoted to the application of the multi-criteria selection tool for the optimization of the choice of limestone deposits for the production of Portland clinker in Cameroon. Data mining on about 12 limestone deposits and 6 important clay deposits in Cameroun were done. The classification of limestone deposits was made on the basis of comparisons of alternatives taking into account the chemical characteristics of the raw material and the conditions of the deposit which allowed the definition of a set of selection criteria that was applied to each limestone deposit. These criteria were: calcium carbonate (CaCO₃) content of limestones, proximity of the limestone deposit to a qualified clay source, estimate of its capacity, area covered by the limestone deposit, extraction of limestone easiness, accessibility to the limestone deposit and the proximity of the limestone deposit to a source of energy. The multi-criteria decision approach used was based on the PROMETHE II method. The application consisted firstly to vary individually the functions: Usual, U-shape, V-shape, Level and Linear function. Secondly, to fix only the Gaussian function and finally to combine the 6 functions of PROMETHE II method. The calculation of the flows and the complete ranking of the alternatives from best to worst according to their net flow were done for each application. A program created in Matlab software imported the performances edited in the Microsoft Excel file, calculated the global preference matrixes, the flow vectors entering or leaving and the net flow. The ranking of potential actions on 12 deposits of limestone in decreasing order has been made. At the end of the investigation, it can be concluded that the Bidzar deposit is at the forefront of the deposits making it possible to achieve the best compromise between the criteria for the production of Portland clinker in Cameroon followed of by the Mintom deposit, despite the fact that it is the largest deposit in term of raw materials volume when data on deposits are considered individually. The tool was subjected to a sensibility analysis (by varying the weights) to test its consistency, stability and reliability. The optimized data obtained in the present study could help investors and decision makers in the choice of limestone deposits necessary for the sustainable production of Portland clinker in Cameroon.

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