Wastewater Minimization in Indirect Electrochemical Synthesis of Phenylacetaldehyde

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Wastewater minimization in phenylacetaldehyde production by using indirect electrochemical oxidation of phenylethane instead of the seriously polluting traditional chemical process is described in this paper. Results show that high current efficiency of Mn(III) and high yield of phenylacetaldehyde can be obtained at the same sulfuric acid concentration (60%). The electrolytic mediator can be recycled and there will be no waste discharged.

KEY WORDS: indirect electrochemical synthesis, phenylacetaldehyde, wastewater minimization

DOMAINS: environmental management and policy, environmental monitoring

INTRODUCTION

Phenylacetaldehyde is an intermediate widely used in the syntheses of fine chemicals such as phenylacetaldehyde dimethyl acetal. The traditional chemical process for its production has the disadvantage of being lengthy, low yield, and discharging large amounts of acid and basic effluents (see Fig. 1).

While the electrochemical method for its production may not only improve the yield of phenylacetaldehyde, it may also reduce the source of wastewater because of the possibility of the mediator recycling. The basic chemical equations are:

\[
\text{Mn(II)} + \text{C}_6\text{H}_5\text{CH}_2\text{CH}_3 + \text{H}_2\text{O} \rightarrow 4\text{Mn(II)} + \text{C}_6\text{H}_5\text{CHO} + 4\text{H}^+ + \text{H}_2\text{SO}_4
\]

In recent years much work has been done to reduce the discharge of wastewater and improve the yield of benzaldehyde in electrochemical production processes[1,2,3,4,5]. Few reports have been shown about the production of phenylacetaldehyde by electrochemical synthesis with less pollution. In order to realize the mediator Mn(III)/Mn(II) used circularly without discharge in the
electrosynthesis of phenylacetaldehyde, electrolysis of Mn(II) to Mn(III), an oxidation of phenylethane to phenylacetaldehyde should be carried out in the same H₂SO₄ concentration. In this paper, the optimum condition of Mn(III) oxidizing phenylethane has been studied and the improvement of the current efficiency of electrolytic production of Mn(III) in the same H₂SO₄ concentration has also been discussed.

**EXPERIMENT**

**Materials and Instruments**

- MnSO₄·H₂O AR, concentrated H₂SO₄ (92%) AR, 0.2 mol/l standard ferrous ammonium sulfate solution, phenylethane AR, Na₂CO₃ (10%), NaOH AR, CTAB AR, self-made Pb-Sb-As electrode.
- Electric stirrer (D25-2F), voltage stabilizer (WYJ-50V, 3A), automatic electronic balance (Japan), Tachometer (Switzerland).

**Experimental Procedures**

100 ml 60% H₂SO₄ solution and 1 mol/l MnSO₄ are added into the electrolytic cell. Self-made Pb-Sb-As alloy is used as anode and cathode; the electrolysis is carried on under stirring. After electrolysis, the electrolyte is moved to a three-necked flask and oxidizes phenylethane to phenylacetaldehyde under strong stirring.

**Analyses of Mn(III) and Phenylacetaldehyde**

The concentration of Mn(III) is determined by titration with standard ferrous ammonium sulfate solution. The current efficiency \( \eta \) is:

\[
\eta\% = \frac{[Mn(III)] \cdot V \cdot F}{I \cdot t} \times 100\%
\]

where \( \eta \): current efficiency; [Mn(III)]: concentration of Mn(III), mol/l; V: volume of electrolyte, l; F: Faraday constant; I: current strength, A; t: time of electrolysis, h.

Phenylacetaldehyde is analyzed by the method of NaHSO₃ addition.

**RESULTS AND DISCUSSION**

**Optimization of the Conditions of Mn(III) Oxidizing Phenylethane to Phenylacetaldehyde in 60% H₂SO₄**

In order to obtain higher yield of phenylacetaldehyde, orthogonal tests of Mn(III) oxidizing phenylethane are carried out (see Table 1).
TABLE 1
Orthogonal Tests (L_{16}[^4]) of Mn(III) Oxidizing Phenylethane

| Number | H_2SO_4 Concentration (%) | Temperature (°C) | CTAB | Mn(III): Phenylethane (mole ratio) | Yield of Phenylacetaldehyde (%) |
|--------|--------------------------|------------------|------|----------------------------------|-------------------------------|
| 1      | (1) 40                   | (1) 40           | (1) 0.1 | (1) 1:2                          | 0 (15 h)                      |
| 2      | (1) 40                   | (2) 50           | (2) 0.0 | (2) 1:3                          | 27.8                          |
| 3      | (1) 40                   | (3) 60           | (3) 0.2 | (3) 1:4                          | 33.8                          |
| 4      | (1) 40                   | (4) 70           | (4) 0.3 | (4) 1:5                          | 10.0                          |
| 5      | (2) 50                   | (1) 40           | (2) 0.0 | (3) 1:4                          | 43.4                          |
| 6      | (2) 50                   | (2) 50           | (1) 0.1 | (4) 1:5                          | 54.1                          |
| 7      | (2) 50                   | (3) 60           | (4) 0.3 | (1) 1:2                          | 31.2                          |
| 8      | (2) 50                   | (4) 70           | (3) 0.2 | (2) 1:3                          | 32.0                          |
| 9      | (3) 60                   | (1) 40           | (3) 0.2 | (4) 1:5                          | 38.2                          |
| 10     | (3) 60                   | (2) 50           | (4) 0.3 | (3) 1:4                          | 33.0                          |
| 11     | (3) 60                   | (3) 60           | (1) 0.1 | (2) 1:3                          | 55.2                          |
| 12     | (3) 60                   | (4) 70           | (2) 0.0 | (1) 1:2                          | 52.0                          |
| 13     | (4) 70                   | (1) 40           | (4) 0.3 | (2) 1:3                          | 22.0                          |
| 14     | (4) 70                   | (2) 50           | (3) 0.2 | (1) 1:2                          | 21.4                          |
| 15     | (4) 70                   | (3) 60           | (2) 0.0 | (4) 1:5                          | 45.8                          |
| 16     | (4) 70                   | (4) 70           | (1) 0.1 | (3) 1:4                          | 32.5                          |
| r_1j   | 17.9                     | 25.9             | 35.5  | 26.2                             |
| r_2j   | 40.2                     | 34.1             | 42.3  | 34.3                             |
| r_3j   | 44.6                     | 41.5             | 31.4  | 35.7                             |
| r_4j   | 30.4                     | 32.6             | 24.1  | 37.0                             |
| R_j    | 26.7                     | 15.6             | 18.2  | 10.8                             |

CTAB: a kind of phase transfer catalyst.

Table 1 shows that H_2SO_4 concentration and CTAB have great effects on yield of phenylacetaldehyde. The optimum condition of Mn(III) oxidizing phenylethane to phenylacetaldehyde is: H_2SO_4 concentration, 60%; temperature, 60ºC; mole ratio of Mn(III) to phenylethane, 1:3–1:5; strong stirring; and the yield of phenylacetaldehyde will be 58% under this condition.

The optimum H_2SO_4 concentration for Mn(III) oxidizing phenylethane to phenylacetaldehyde has been obtained as 60%, so the optimum electrolytic condition is studied in the same H_2SO_4 concentration.

Optimization of the Conditions of Electrolyzing MnSO_4 to Mn(III)

Current efficiency of heterogeneous electrochemical oxidation of Mn(II) to Mn(III) is closely related to the electrolytic conditions. The effects of MnSO_4 concentration, electrolytic temperature, current density, electrolytic time, and stirring speed on the current efficiency are discussed in this paper. Experimental results show that the optimum parameters for heterogeneous electrolysis of MnSO_4 in 60% H_2SO_4 using both Pb-Sb-As alloy as anode and cathode are: MnSO_4 concentration, 1.0 mol/l; current density, 60 mA/cm²; temperature, 60ºC; electrolytic time, 2 h; stirring speed, 1000 r/min. Under the above conditions, a current efficiency up to 76% can be obtained, which is a little less than that of 80% obtained in the 40% H_2SO_4 electrolytic solution.

Recycling of the Mediator and Sulfuric Acid Solution

In order to exert the characteristics of the technology of phenylethane to phenylacetaldehyde without waste, MnSO_4 and sulfuric acid solution should be used circularly. But experimental
results have shown that if the sulfuric acid solution and solid MnSO₄ are recycled, and used as they are obtained from oil/water separation without any purification, current efficiency will fall greatly. This is probably due to the small amounts of organic impurities produced in the oxidation of phenylethane by Mn(III) and remaining in the sulfuric acid solution and solid MnSO₄. These impurities either will react on the anode or cathode or will further react with Mn(III) causing the fall in current efficiency.

Experimental results show that after the sulfuric acid solution is treated with activated carbon A, solid MnSO₄ is washed with anhydroethanol; the current efficiency during recycling processes can remain in a constant level, approximately above 70% (see Fig. 2). The yield of phenylacetaldehyde can remain about 57% (see Fig. 3). So the recycling of mediator in indirect electroproduction of phenylacetaldehyde is realized and there is no waste to be discharged (see Fig. 4).

**CONCLUSION**

Electrosynthesis of phenylacetaldehyde with less pollution is studied in this paper. Both processes of heterogeneous electrolysis of MnSO₄ and synthesis of phenylacetaldehyde by oxidation of Mn(III) can be carried out separately in the same concentration of sulfuric acid (60% H₂SO₄) with high current efficiency and high yield of phenylacetaldehyde. The organic impurities in sulfuric acid solution and solid MnSO₄ causing the fall in current efficiency are removed effectively by
activated carbon A and anhydroethanol, respectively. So the cleaner technology of the mediator recycling of electrosynthesis of phenylacetaldehyde can be realized and it may be used in production in the future.

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