Does Load-Induced Shallow Subsidence Inhibit Delta Growth?

E. L. Chamberlain1,2, Z. Shen3, W. Kim4, S. McKinley3, S. Anderson3, and T. E. Törnqvist1

1Department of Earth and Environmental Sciences, Tulane University, New Orleans, LA, USA, 2Soil Geography and Landscape Group and Netherlands Centre for Luminescence dating of Wageningen University, Wageningen, The Netherlands, 3Department of Marine Science, Coastal Carolina University, Conway, SC, USA, 4Department of Earth System Sciences, Yonsei University, Seoul, Republic of Korea

Abstract. The ability of deltas to persist by building new land is critical to maintaining these vital ecologic environments that are often home to major economic and population centers. However, the deposition of land-building sediment triggers load-induced shallow subsidence which may undermine the effectiveness of natural and engineered emergent landforms. Here, we present a new method to quantify shallow subsidence in a 6,000–8,000 km² relict bayhead delta of the Mississippi Delta using the mouth bar to overbank stratigraphic boundary that formed near sea level, temporally constrained by optically stimulated luminescence dating. Vertical displacement rates at this boundary, averaged over 750–1,500 years, are on the order of a few mm/yr. Total subsidence scales to ~50% of the thickness of overlying deposits, significantly greater than the 28%–35% loss estimated for inland localities underlain by peat, indicating that bay muds in the study area are more compaction-prone than terrestrial organic-rich deposits. Modeling shows a modest reduction of ~13% in deltaic land-area gain under a realistic compaction scenario for 1,000 years of simulated delta progradation, compared to a no-compaction scenario. Our findings indicate that load-driven compaction does not majorly hinder land-area gain and may in fact promote long-term growth at engineered sediment diversions through channel maintenance driven by compaction, thereby adding further support to this restoration strategy.

Supporting Information: Supporting Information may be found in the online version of this article.

Correspondence to:
E. L. Chamberlain and W. Kim, liz.chamberlain@wur.nl; delta@yonsei.ac.kr

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1. Introduction

Despite a reduction in the sediment flux from continents to oceans on a global scale (Syvitski et al., 2005), many river deltas have continued to grow in recent decades (Nienhuis et al., 2020). However, it is unlikely that this growth can be sustained under future scenarios of relative sea-level rise (RSLR), in part due to the commonly high subsidence rates in deltas. RSLR is a major threat to the sustainability of these ecologically, economically, and culturally significant regions (e.g., Bijlsma et al., 1996; Ericson et al., 2006; Higgins, 2016; Milliman & Haq, 1996; Shirzaei et al., 2021). While it is well-documented that compaction of shallow Holocene deposits triggered by sediment loading is a major contributing process (e.g., Jelgersma, 1996; Mazzotti et al., 2009; Teatini et al., 2011; Törnqvist et al., 2008; Zoccarato et al., 2018), a lack of empirical evidence on the compressibility of various deltaic facies hinders our ability to predict future subsidence rates and their spatiotemporal variability. A better understanding of load-induced shallow subsidence is needed to assess whether deltas will maintain their sustainability by creating new land through progradation or whether short-term elevation and land-area gains may be lost to subsidence driven by the deposition of new sediment.

Although wetlands can aggrade to maintain delta-plain elevation, the net growth of deltaic land is fundamentally tied to clastic deposition in open water, including estuarine bays. Still, coastal subsidence research has historically emphasized the importance of organic-rich portions of deltas where the subsidence risk is regarded as high due to the propensity of peat to oxidize and compact (e.g., Kaye & Barghoorn, 1964; Van Asselen et al., 2009). In the Mississippi Delta, the target of our study, the majority of research into shallow subsidence has focused on organic-rich (paleo) wetlands (Cahoon et al., 1995; Jankowski et al., 2017; Morton et al., 2006; Törnqvist et al., 2008).
For example, the large network of rod surface-elevation tables (e.g., Webb et al., 2013) emplaced for wetland elevation-change monitoring (Steyer et al., 2003) enables instrumental-timescale evaluation of shallow subsidence, and peat beds preserved in the stratigraphic record are widely used sea-level or paleo-groundwater-table indicators that enable evaluating pre-instrumental rates of subsidence (Törnqvist et al., 2006). As such, there is a significant void of methodology as to how to determine subsidence in estuarine open-water environments where clastic sedimentation dominates.

Satisfying this knowledge gap is critical to determining the viability of coastal restoration initiatives, both for our study area and for coastal communities worldwide that are endangered by subsidence (Shirzaei et al., 2021). Over the past century, the Mississippi Delta has experienced net land loss at an average rate of 45 km²/yr (Couvillion et al., 2016). Harnessing the Mississippi River's natural ability to build land through sediment diversions is a key component of a 50 billion dollar coastal management strategy outlined in the Louisiana Coastal Master Plan that aims to offset historic land losses (CPRA, 2017). Lessons learned from this strategy may be applicable to coastal management initiatives worldwide. Little is known about how muddy substrates at diversion sites, which are planned mainly for open-water estuarine bays, may respond to loading with sediment and the degree to which load-driven shallow subsidence may inhibit land growth.

Here, we apply a new method to quantify subsidence of a bayhead delta that built into a large estuarine bay using the chronostratigraphic record of the Lafourche subdelta of the Mississippi Delta (Figure 1). The emergence of the 6,000–8,000 km² bayhead portion of the Lafourche subdelta from 1.6 to 0.6 ka was recorded as a ubiquitous succession of shell-rich bay floor, laminated delta front, sandy mouth bar, and mud-dominated overbank deposits (Chamberlain et al., 2018; Figure 2a). We obtain subsidence values using the present-day depths and previously determined optically stimulated luminescence (OSL) ages (Chamberlain et al., 2018) of a stratigraphic boundary within this succession that we introduce as a novel relative sea-level (RLS) indicator. We apply our findings by means of a modified delta growth model (Kim, Dai, et al., 2009) to evaluate the potential effects of load-induced subsidence on delta progradation and land building. Our findings also shed light on the predominant drivers of deltaic subsidence which has been a contentious topic in the Mississippi Delta (e.g., Allison et al., 2016; Dokka et al., 2006; Kolker et al., 2011; Morton et al., 2006; Törnqvist et al., 2008, 2006). Figure 3 gives an overview of potential drivers of deltaic RSLR, including the various processes contributing to subsidence, and whether our method captures them.

2. Methods and Study Area

2.1. A New Method for Measuring Subsidence

Mouth bars consist mainly of sand deposited at the river mouth that aggrades to fill the accommodation created by RSLR (Figure 2a; Edmonds & Slingerland, 2007; Wright, 1977). As the top of the mouth bar approaches sea level, currents become less able to transport sand to the bar top and colonization by vegetation enhances the trapping of fine-grained sediments (Olliver & Edmonds, 2017; Paola et al., 2011). This produces an abrupt lithofacies change from sand to mud, referred to herein as the mouth bar to overbank (M-O) boundary (Figure 4). A survey of the Wax Lake Delta (Figure 1), an actively prograding bayhead delta within the Mississippi Delta, suggests that the M-O boundary corresponds to a transition from mouth bar to intertidal flat which is related to coeval sea level with a mean lower quartile formation elevation of \(-0.4 ± 0.2\) m NAVD 88 (Olliver & Edmonds, 2017). We take this lower quartile as the elevation of the modern M-O boundary, assuming that higher intertidal flat elevations are due to sediment accretion above this boundary. Previous work has also related mouth-bar tops to the mean low water tidal datum (Wellner et al., 2005) and more broadly to sea level (Fisk et al., 1954; Roberts et al., 1997; Shen & Mauz, 2012), but without specific values for the elevation of this boundary. It is likely that the tidal range in this region has not changed significantly over the late Holocene (Hill et al., 2011).

Because the M-O boundary can be related to sea level and is a common stratigraphic boundary in river-dominated deltas, as well as in other coastal deposition systems such as tidal flat bars overlain by marsh deposits (Brivio et al., 2016), it provides a valuable and as of yet unexplored RSL indicator. A similar innovation was conceptualized by Fisk et al. (1954), however, the chronologic and RSL data needed to apply their insight were lacking in the 1950s. Here, we use stratigraphic data in combination with OSL ages (Chamberlain et al., 2018) that capture the timing of formation of the M-O boundary, and an established record of compaction-free RSLR in the Mississippi
Delta (González & Törnqvist, 2009; Törnqvist et al., 2006) to quantify cumulative subsidence. This is expressed as the net change in elevation of the M-O boundary ($\Delta E$), calculated as:

$$\Delta E = (E_i - E_0) + \Delta RSL$$

In Equation 1, $E_i$ is the present-day elevation of the M-O boundary from borehole data with 0.1 m uncertainty for land surface elevation determined by LiDAR (Cunningham et al., 2004; Gesch, 2018) and a unidirectional 2% uncertainty (that is, 2% potential shortening) for depth overestimation due to non-vertical drilling. $E_0$ is the elevation at which the M-O boundary formed with respect to coeval sea level (Olliver & Edmonds, 2017). $\Delta RSL$ is the change in RSL since the time of M-O boundary formation (Figure 2b) with 0.3 m uncertainty (Hijma et al., 2015). All elevations are relative to NAVD 88. We calculate the subsidence rate ($S$) as:

$$S = \frac{\Delta E}{\Delta T},$$

where $\Delta T$ is the difference between the time of formation of the M-O boundary ($T_i$, Figure 2c), obtained as the weighted mean of two mouth bar sand OSL ages for each site (Chamberlain et al., 2018) and 2010 CE ($T_f$, Figure 2c). We selected all Mississippi Delta sea-level index points (that is, datapoints with rigorously quantified
Figure 2. (a) The stratigraphic record of bayhead deltas can be generalized as bay floor clay overlain by delta front silt, then mouth bar sand, capped by mud-dominated overbank deposits that thin seaward (modified from Chamberlain et al., 2018). The mouth bar to overbank (M-O) boundary forms in relation to sea level (Fisk et al., 1954; Olliver & Edmonds, 2017; Roberts et al., 1997; Shen & Mauz, 2012; Wellner et al., 2005). Note that this cartoon does not consider compaction. (b) Compaction-free RSLR during the time of Lafourche subdelta progradation (after González & Törnqvist, 2009; Törnqvist et al., 2006). (c) Method for calculating subsidence uses the change in elevation of the M-O boundary (ΔE) from time of formation (E_0) to present (E_1), relative to NAVD 88 and corrected for RSLR (ΔRSL) since the time of M-O boundary formation (T_0) obtained from OSL dating of the mouth-bar deposits (Chamberlain et al., 2018).

Figure 3. Drivers of deltaic relative sea-level rise, and whether they are captured by our method. Key references are specific to the Mississippi Delta.
uncertainties that capture the position of paleo-sea level in space and time; e.g., Engelhart et al., 2011) that formed during the time of Lafourche activity within $2\sigma$ uncertainty (Figure 2) from studies by González and Törnqvist (2009, $n = 28$) and Törnqvist et al. (2006, $n = 2$) to determine $\Delta RSL$ and express calibrated radiocarbon ages relative to 2010 CE for consistency with the OSL ages. A schematic synthesis of the method is shown in Figure 2c. Because $\Delta RSL$ is obtained from Mississippi Delta basal peat records, this term includes any deep subsidence due to processes with comparatively long wavelength, including glacial isostatic adjustment (GIA; Love et al., 2016) and sedimentary isostatic adjustment (SIA; Wolstencroft et al., 2014; Yu et al., 2012), but does not capture more localized deep subsidence due to faulting. In other words, the subtraction of $\Delta RSL$ removes broad-scale deep subsidence due to GIA and SIA while preserving any subsidence contribution due to faulting near our sites (Figure 3). Uncertainties are summed in quadrature. Cumulative values and rates of subsidence associated with the downward displacement of the M-O boundary are expressed as negative values.

2.2. Study Area and Stratigraphic Characterizations

We apply our new method to assess subsidence at 10 sites in the Lafourche subdelta of the Mississippi Delta (Figure 1; Table 1). The Lafourche distributary channel network is characterized by a single trunk channel landward of a “polyfurcation point” or bayhead delta apex and several smaller distributaries seaward of the polyfurcation point (Figure 1). Beginning at $\sim 1.6$ ka, the Lafourche subdelta prograded in a radial fashion from its apex to construct a 6,000–8,000 km$^2$ bayhead delta (Chamberlain et al., 2018). After $\sim 1.2$ ka, discharge was shared between the Lafourche and Modern (Balize) subdeltas and complete avulsion to the modern Mississippi River occurred.
| Cross section       | St. Charles | Raceland | Bayou Cane | Larose | Chauvin | Dulac | Cocodrie | Galliano | Golden Meadow | Fourchon | Princourville |
|---------------------|-------------|----------|------------|--------|---------|-------|----------|----------|--------------|---------|---------------|
| Number of boreholes (total) | 7           | 6        | 5          | 7      | 6       | 7     | 3        | 12       | 8            | 3       | 103           |
| Number of boreholes (accepted) | 6           | 6        | 3          | 7      | 6       | 7     | 3        | 10       | 8            | 3       | 103           |
| Distance (river km) | 64          | 82       | 75         | 106    | 106     | 103   | 130      | 127      | 132          | 165     | 17            |
| Holocene succession thickness (m) | 43          | 46       | 38         | 37     | 58      | 58    | 61       | 40       | 40           | 49      | 44            |
| Overbank deposit thickness (m) | 6.73 ± 1.31 | 5.92 ± 0.85 | 3.99 ± 0.85 | 4.20 ± 0.70 | 3.18 ± 1.13 | 6.63 ± 1.16 | 4.22 ± 0.25 | 1.66 ± 0.76 | 2.07 ± 0.70 | 0.46 ± 0.16 | 5.37 ± 2.17 |
| $E_1$ (m, NAVD 88) | −4.32 ± 0.68 | −4.09 ± 0.61 | −3.10 ± 0.85 | −3.10 ± 0.35 | −3.23 ± 0.76 | −5.45 ± 0.59 | −3.53 ± 0.40 | −2.15 ± 0.43 | −2.48 ± 0.33 | −0.73 ± 0.26 | −2.33 ± 1.37 |
| $E_0$ (m, NAVD 88) | −0.40 ± 0.20 | −0.40 ± 0.20 | −0.40 ± 0.20 | −0.40 ± 0.20 | −0.40 ± 0.20 | −0.40 ± 0.20 | −0.40 ± 0.20 | −0.40 ± 0.20 | −0.40 ± 0.20 | −0.40 ± 0.20 | 0.45 ± 0.07  |
| $\Delta T$ (ka) | 1.49 ± 0.15 | 1.47 ± 0.11 | 1.46 ± 0.10 | 1.25 ± 0.08 | 1.10 ± 0.05 | 1.06 ± 0.05 | 0.94 ± 0.05 | 0.92 ± 0.07 | 0.92 ± 0.06 | 0.74 ± 0.06 | 1.42 ± 0.05  |
| $\Delta RSL$ (m) | 1.20 ± 0.30 | 1.18 ± 0.30 | 1.18 ± 0.30 | 1.05 ± 0.30 | 0.96 ± 0.30 | 0.94 ± 0.30 | 0.86 ± 0.30 | 0.85 ± 0.30 | 0.75 ± 0.30 | 0.75 ± 0.30 | 1.15 ± 0.30  |
| Reconstructed elevation of boundary at formation time (m, NAVD 88) | −1.60 ± 0.36 | −1.58 ± 0.36 | −1.58 ± 0.36 | −1.45 ± 0.36 | −1.36 ± 0.36 | −1.34 ± 0.36 | −1.26 ± 0.36 | −1.25 ± 0.36 | −1.15 ± 0.36 | −0.97 ± 0.31a |
| Cumulative subsidence, $\Delta E$ (m) | −2.73 ± 0.77 | −2.51 ± 0.71 | −1.53 ± 0.92 | −1.65 ± 0.50 | −1.88 ± 0.84 | −4.11 ± 0.69 | −2.27 ± 0.54 | −0.89 ± 0.56 | −1.22 ± 0.49 | 0.42 ± 0.44 | −1.63 ± 1.40 |
| Subsidence rate, $S$ (mm/yr) | −1.83 ± 0.53 | −1.71 ± 0.49 | −1.04 ± 0.63 | −1.31 ± 0.41 | −1.71 ± 0.77 | −3.88 ± 0.66 | −2.41 ± 0.58 | −0.97 ± 0.61 | −1.34 ± 0.54 | 0.56 ± 0.60 | −1.15 ± 0.99 |

*Note. Chronologic data are from Chamberlain et al. (2018). Relative sea-level rise ($\Delta RSL$) is determined using data from González and Törnqvist (2009) and Törnqvist et al. (2006). Holocene succession thickness data are from Heinrich et al. (2015). The other data presented here are novel to this study.

*aIncludes correction for groundwater table gradient.*
The study sites are located along the banks of the bayhead delta's distributaries and their associated along-river distances are measured relative to the Lafourche-Modern avulsion site (Figure 1). Each site hosts a transect of boreholes ($n = 64$) with depths ranging from 4.9 to 12.5 m that were hand-drilled and sampled between 2013 and 2015 CE (Chamberlain et al., 2018). We evaluated each borehole for suitability and rejected five boreholes where the M-O boundary was unclear or disturbed, often related to erosive paleochannels. We determined overbank deposit thickness between the land surface and the top of the mouth bar. We used the mean and standard deviation of all boreholes in a given transect to obtain average values for the depth of the M-O boundary and overbank deposit thickness at each site.

Three sites exhibit anthropogenic modification of the overbank deposits. The Dulac transect features an ~800 year old prehistoric earthen mound that appears to have enhanced subsidence of the underlying deposits (Chamberlain, Mehta, Reimann, & Wallinga, 2020), and the Cocodrie transect features ~20 cm of historic construction fill; no correction was made for this because the anthropogenic sediments were consolidated and have contributed to subsidence for decades to centuries. The Fourchon transect is in a region that has been actively elevated by dredge spoil pumping and features ~0.7–1.4 m of soft unconsolidated mud slurry overlying the overbank deposits at the time of coring; Google Earth imagery shows that the slurry was added within one year prior to our sampling. Here, we subtracted the unconsolidated anthropogenic mud from the overbank thickness because we deem it unlikely to have significantly contributed to subsidence.

Estimates of Holocene subsidence have been previously obtained for an inland site (Figure 1) within the Lafourche subdelta by measuring the displacement of a freshwater peat horizon formed at the coeval groundwater table (Törnqvist et al., 2008). We reanalyzed these data using a more recently published estimate of the local groundwater gradient (1 cm/km, González & Törnqvist, 2009), the tidal range obtained from NOAA tide gauges (tidesandcurrents.noaa.gov), and a ΔRSL reconstruction that matched our M-O boundary analysis. Törnqvist et al. (2008) identified a subset of their samples with low subsidence which they attributed to the presence of underlying sandy strata. We include this subset in our analysis; excluding it would not be justified because similar data are not available for the Lafourche bayhead delta deposits.

Prior numerical model simulations of Mississippi Delta growth suggested that land building by means of sediment diversions is feasible (Kim, Mohrig, et al., 2009), although that model treated compaction as an instantaneous elevation drop when a delta prograded over bay mud. Here, we apply a modification of the Kim, Dai, et al. (2009) model informed by our field results to approximate compaction by the behavior of pressure-driven viscous fluids. We use this model because it captures delta shoreline progradation with time and constructs the break in slope between the delta topset and foreset (i.e., analogous to the M-O boundary) in a computationally efficient manner that is appropriate to the centennial to millennial timescales we investigate. The overlying topset thickness dictates pressure, and the gradient in the pressure determines the rate of compaction associated with the expulsion of pore water due to overburden loading. While we retain a background RSLR component of 0.5 mm/yr that includes the contributions of GIA, SIA, and geocentric sea-level rise (Figure 3) during the period of Lafourche activity, a key difference between our approach and that of Kim, Dai, et al. (2009) is that we do not use an instantaneous and spatially uniform compaction input. Rather, compaction in our updated model is a function
of both time and space and happens in response to differential sediment loading. The model conserves mass yet allows the underlying mud substrate volume to change due to a simulated reduction in porosity. A compaction coefficient in the model is calibrated to match the observed relationship between overburden thickness (that is, the thickness of overbank deposits overlying the M-O boundary; see Supporting Information S1) and cumulative subsidence that we identify in the study area.

3. Results and Discussion

3.1. Subsidence Rates and Cumulative Values

We observe cumulative subsidence of up to −4.1 m (Table 1, Figure 5) and subsidence rates ranging from ~0 to −4 mm/yr (Table 1, Figure S3 in Supporting Information S1). Additional subsidence likely occurs within the overbank deposits, which is not captured by our method. We note that cumulative subsidence for the Fourchon transect yielded a positive mean value that approaches zero within its uncertainty. This is interpreted not as exhumation but rather as a reflection of high uncertainty in our elevation estimate at this site due to anthropogenic alteration of the land surface through impoundment and dredge-spoil pumping. This datapoint can be read as little to no subsidence of the M-O boundary.

Figure 5. Mean cumulative subsidence at each site and its relationship to (a) The total local thickness of the Holocene succession, (b) Distance along Bayou Lafourche from the Lafourche-Modern avulsion site seaward, and (c) Overburden thickness. The cumulative subsidence values shown here are the average of all accepted boreholes at each site with uncertainties expressed as one standard deviation (see Supporting Information S1).
The load-driven component of subsidence has been previously shown to be greatest at the onset of loading and to decrease exponentially with time (e.g., Holtz & Kovacs, 1981), and the majority of compaction may occur within the first ~20 year (Mazzotti et al., 2009). To investigate the time-dependent nature of the subsidence rates calculated here, we normalize rates by overburden thickness, yielding rates of subsidence (mm/yr) per meter of overbank sediment averaged over 750–1,500 years. These rates increase from older to younger sites (Figure 6). The age-wise trend in the normalized rates (i.e. higher normalized rates for younger deposits than for older deposits) indicates that load-induced subsidence is ongoing in the Lafourche subdelta, despite the passage of 750–1,500 years since loading began and about 600 years since loading ceased. Still, the present-day contributions of load-induced subsidence are likely very small compared to the average rate produced by our method.

Comparisons of such long-term rates can be valuable for assessing the processes active in delta-plain maintenance, especially if similar-timescale aggradation rates are also known (Chamberlain, Goodbred, Al Nahian, et al., 2020). In the Ganges-Brahmaputra Delta of Bangladesh, subsidence rates of about −2 to −4 mm/yr, also averaged over hundreds to thousands of years and obtained using the chronology of buried horizons, were determined by Grall et al. (2018) and attributed to buttressing of the delta by a thick succession of marine deposits. Our rates obtained for the Mississippi Delta are similar to those of Grall et al. (2018). However, we identify marine muds as a contributor to subsidence and interpret the relatively low (mm/yr) subsidence rates in both systems to simply be a function of averaging over a long timescale in relict portions of the deltas where load-induced compaction has slowed. Moreover, this comparison indicates that a similar sediment yield is needed to maintain the delta-plain area by offsetting RSLR in both deltas despite their vastly different tectonic settings. This has unfortunate implications for the sustainability of the Mississippi Delta, where sediment yield is about five times lower than in the Ganges-Brahmaputra Delta (Chamberlain, Goodbred, Hale, et al., 2020).

### 3.2. Stratigraphic, Tectonic, and Other Factors

The overbank unit is thickest at the bayhead delta apex and thins seaward (Figures 2a and 4) due to a shorter sedimentation time, that is, the time between the emergence of the mouth bar and the abandonment of the Lafourche subdelta at 0.6 ka (Chamberlain et al., 2018). Overbank deposits accumulated at an average rate of 0.7 cm/yr over the lifespan of the bayhead delta (Chamberlain, Mehta, Reimann, & Wallinga, 2020) and range in thickness from about 1–8 m at the sites studied herein (Table 1). These rates were determined from present-day (compacted) overbank-deposit thicknesses. Because the thickness of the mouth-bar and delta-front deposits is fairly uniform (Chamberlain et al., 2018), the thickness-trend of the overbank deposits yields a seaward-thinning, wedge-shaped geometry (Figure 2a). Cumulative subsidence is highest at the bayhead delta apex and lowest at the most seaward sites. Accommodation is therefore generated by subsidence near channels in proximal portions of the bayhead delta, a process that may inhibit superelevation and subsequent avulsion of the trunk channel (Liang et al., 2016). Our finding that spatial trends in subsidence may support trunk channel persistence is consistent with modeling of crevasse splays showing that the absence of subsidence results in channel choking (Nienhuis et al., 2018). This is consistent with the 1000-year growth history of the Lafourche bayhead delta which featured coactive distributary channels and no avulsions within the lobe (Chamberlain et al., 2018). The strong correlation of cumulative subsidence with overburden thickness (Figures 5c and 7) supports previous findings that compaction due to sediment loading is a primary driver of subsidence in actively aggrading deltas (e.g., Törnqvist et al., 2008) although rates of compaction-driven subsidence slow down and become less important after loading ceases.

We find no relationship between subsidence and the total thickness of the Holocene succession at our study sites ($r^2 = 0.15$, Figure 5a). Comparisons with other deltas also do not show a clear connection; our rates for the Mississippi Delta are similar to those documented in the Ganges-Brahmaputra Delta (Grall et al., 2018).
despite its significantly thicker Holocene sediment package (up to 90 m; Goodbred & Kuehl, 1999) yet lower than millennial-timescale estimates of about −17 mm/yr for the progradational portion of the Mekong Delta where Holocene sediment thicknesses are only ∼18–25 m (Zoccarato et al., 2018). Collectively, this evidence highlights the fact that a large proportion of sediment compaction occurs in the shallowest subsurface (e.g., <5 m; Keogh & Törnqvist, 2019).

We also see little impact from oil and gas extraction—the surface expression of which corresponds to the depth of wells such that deeper wells possess a greater footprint. The deepest wells and greatest extraction values are generally found at seaward locations in our study area (e.g., Golden Meadow and Fourchon sites; Figure 1; Figures S1 and S2 in Supporting Information S1) where subsidence values obtained with our method are the lowest. This can be attributed in part to our selection of study sites away from oil and gas fields. Over the spatial and temporal scales we studied, the total thickness of the entire Holocene succession also appears to be of little importance although it remains a significant factor in basin-wide subsidence trends acting over longer (i.e., >10^4 yr) timescales (Frederick et al., 2019) and measured at greater depths (Karegar et al., 2015). These seemingly contradictory observations can be reconciled by taking account of the fact that compaction rates increase both with reduced accumulation time of a given deposit thickness, but also with an increase in total deposit thickness for a given accumulation time (Meckel et al., 2006, 2007). In other words, compaction rates are governed by complex physical processes that can yield apparently disparate field results when measured over different depth and time scales.

Some studies have claimed that fault movement in the Mississippi Delta has driven a general trend of seaward increasing subsidence, associated with the submergence of large blocks of coastal land (Dokka et al., 2006; Gagliano et al., 2003). We find no evidence for such a trend (r² = 0.17, Figure 5b) in the shallow-subsidence data that we collected and no enhanced subsidence is observed seaward of previously mapped faults. For example, the rate of subsidence of the Golden Meadow transect (−1.34 ± 0.54 mm/yr) located seaward of the Golden Meadow Fault (Kuecher et al., 2001) is not significantly different from the rate of subsidence at the Galliano transect (−0.97 ± 0.61 mm/yr) located landward of this fault. Similarly, the subsidence rate of the Larose transect located seaward of the Lake Hatch Fault (−1.31 ± 0.41 mm/yr) is lower than that of the Raceland transect located landward of this fault (−1.71 ± 0.49 mm/yr). Despite uncertainty in the exact surface expression of faults in our study area, the lack of a seaward increase of subsidence suggests that faulting is producing at most only limited, local effects in the Mississippi Delta (e.g., Hopkins et al., 2021) and is not driving broad-scale subsidence in this part of the delta, consistent with the slow long-term rates of fault slip inferred by Frederick et al. (2019).

3.3. Paleoenvironmental Factors

The prevalence of subsurface peat is commonly linked to the highest rates of subsidence, indicating that organic-rich, terrestrial environments may be more compaction-prone than dominantly clastic estuarine bays. Törnqvist et al. (2008) estimated that 35% of elevation gained by overbank deposition is lost to shallow subsidence at an inland site in the Mississippi Delta underlain by peat (Figure 1); we obtain the value of 28% mainly due to the inclusion of the data excluded by Törnqvist et al. (2008). By reconstructing the original position of the M-O boundary at the time of its formation (Figure 4) and calculating the fraction of the overlying deposit occurring below this boundary at present-day, we estimate that ∼50% of elevation gained by the bayhead delta through overbank deposition is ultimately lost to subsidence (Figure 7). Our value is considerably higher than the 28%–35% value for load-induced subsidence at more inland localities underlain by peat (Törnqvist et al., 2008). This indicates that estuarine bays are especially prone to subsidence driven by load-induced compaction, consistent with observations of high subsidence rates associated with muddy Holocene strata elsewhere (e.g., Higgins et al., 2014; Zoccarato et al., 2018). The high vulnerability of muds to subsidence may be due to dewatering of deltaic sediments. The alternating layers of sand and clay typical of bayhead delta stratigraphy may generate optimal conditions for compaction because the high permeability of sand allows groundwater to escape, lowering the
porewater overpressure (Meckel et al., 2006). By contrast, peats confined by low-permeability clays—a condition typical of settings farther inland, upstream of the bayhead delta—are less likely to expel groundwater and may therefore be less prone to compaction.

3.4. Modeling Delta Growth Under a Data-Driven Compaction Scenario

Our findings imply that inactive portions of the delta plain may be fairly stable if they are not loaded. However, this is an unlikely condition in many deltas and especially in the Mississippi Delta where proposed delta restoration strategies may introduce large quantities of new sediment onto compaction-prone bay strata. To test whether load-driven subsidence by engineered diversions may significantly inhibit their land-building efficacy, we employed a modified version of the delta-growth model of Kim, Dai, et al. (2009) informed by our findings (Figure 8). We approximated sediment discharge based on the dimensions of Lafourche delta deposits along with an opening angle of 70° (Figure 1) and a basement with a slope of \(-4 \times 10^{-5}\) based on the field measurements (Figure 8d). We first ran the model with the initially sloped basement and a range of water discharges to match the Lafourche bayhead delta topset slope of \(4 \times 10^{-5}\) (a 4 m rise over a ~100 km run) observed in the field data (Figure 8d). The model organized a topset slope of \(4.01 \times 10^{-5}\) at a flood discharge of 10,240 m³/s. RSLR was set at 0.5 mm/yr and the deposit porosity was assumed at 0.6 (an average value of initial bar sand, bay mud, and prodelta deposits before compaction; Kuecher, 1994; Meckel et al., 2007). The model produced a shoreline advance of 108.8 km over 1,000 years under these conditions (Figure 8a), which is matched with ~100 km
progradation observed in the Lafourche bayhead delta. We then applied the same parameters to the tuned model to examine two scenarios: one with compaction scaled to 50% of the delta topset (i.e., overburden thickness), and one with no compaction, both over an initially flat basement at −4 m depth. These parameters approximate the growth conditions of the Lafourche bayhead delta. A detailed description of the model and its compaction component is provided in Supporting Information S1.

Under conditions with compaction, the delta prograded ∼110 km to build ∼7,800 km² of new deltaic land and the land-surface elevation at the delta apex gained up to ∼4.2 m of elevation (Figure 8b). With no compaction, the delta shoreline prograded ∼10 km farther to build an additional ∼1,100 km² of land and gained ∼0.7 m of additional elevation at the delta apex (Figure 8c) compared to the results from the compaction case. Both scenarios closely reproduce the Lafourche bayhead delta planform growth, suggesting the model is valid for our aims, although we note that modeled delta progradation rates slow with time whereas a constant, linear rate of progradation was documented for the Lafourche subdelta (Chamberlain et al., 2018). Chamberlain et al. (2018) hypothesized that other mechanisms such as enhanced mud retention in the interdistributary basins of maturing deltas may sustain progradation rates by filling the incrementally greater space between distributaries associated with the widening planform. Sand can generally be considered the limiting factor in Mississippi Delta growth; sand forms the mouth bar framework that facilitates progradation (Chamberlain et al., 2018) yet sand comprises <30% of the annual sediment load to the delta while mud comprises the majority (Allison et al., 2012). Mature deltas may serve as more efficient mud traps, thereby promoting increased rates of land-area gain coupled with sustained progradation rates. Alternatively, discrepancies between the model and the Lafourche bayhead delta may be due to temporal variation in sediment discharge which is presently unknown.

Delta progradation under the modeled compaction scenario is reduced by ∼6%, and the surface-area gain is reduced by ∼13% over the 1,000 year of simulation (Figure 9, Table S1 in Supporting Information S1). After the first 100 years of simulation (a typical engineering timescale), delta progradation under the compaction scenario is only reduced by ∼0.4% and the surface-area gain is reduced by ∼0.7% (Figure 9, Table S1 in Supporting Information S1). We caution against overinterpreting the results of the first hundred years of model simulation because our model is less suited for projecting delta growth over short timescales than other, more sophisticated morphodynamic models (e.g., Delft3D).

Both the Lafourche bayhead delta and the model deltas have a fan shape in planform. In the compaction model scenario, the greatest vertical displacement of the M-O boundary occurs near the delta apex, which results in a small overall loss of deposit volume due to compaction. Displacement of the simulated M-O boundary shallows seaward with decreasing overburden, similar to the stratigraphy identified in the Lafourche subdelta (Figure 8d). A greater volume of sediment is deposited over the much wider downstream portion of the fan-shaped delta. This downstream section is the relatively thin and newly prograded part of the delta, so the compaction effect is much smaller. Lateral migration of the apex channel can deposit a greater volume of sediment closer to the delta apex than the downstream portion and cause significant loss of elevation by compaction. On the other hand, the enhanced compaction at the delta apex promotes the maintenance of distributary channels that feed growth of the delta (Liang et al., 2016). In sum, our model results indicate that delta progradation and associated deltaic land-area gain can be sustained even under a realistic compaction scenario. Furthermore, load-driven compaction may in fact promote the viability of emergent coastal landforms including engineered diversions by sustaining the feeder channel. Similar to a recent model study that examined crevasse-splay formation in relation to shallow subsidence (Nienhuis et al., 2018), we find that sediment compaction is not necessarily a detrimental process with respect to land building in deltas.

Finally, the new findings presented here are also relevant to sequence-stratigraphic analyses of deltaic successions in deeper time, most notably trajectory analysis that is widely used in the rock record. Our case study from the
Mississippi Delta offers an exceptionally highly resolved example of an ascending regressive shoreline trajectory with an observed angle of about 0.0023°, which is at the low end of the range of such angles synthesized by Helland-Hansen and Hampson (2009). Nevertheless, we note that this angle would have been even eight times lower (0.0003°, i.e., essentially flat) in the absence of sediment compaction (i.e., Figures 8b vs. 8c). In other words, in mud-rich deltaic systems, sediment compaction can play a substantial role in affecting the shoreline trajectory and the associated thickness of facies belts, something that deserves consideration in the interpretation of the ancient rock record.

4. Conclusions

We present a new method for quantifying local RSLR in river-dominated deltas and use our findings to assess the role of subsidence in delta growth. Our method makes use of a stratigraphic boundary that is common to river-dominated deltas and other coastal systems. Combined with recent advancements in sediment dating (i.e., OSL), this offers a means to test centennial-to-millennial-timescale subsidence rates in deltas, a key element in assessing sustainability and management strategies for these vital landscapes. Applying this method to the Mississippi Delta, we arrive at the following conclusions:

1. Load-induced subsidence of shallow strata is a primary component of deltaic subsidence, while deeper processes such as faulting, oil and gas extraction, and compaction of the entire Holocene sediment package appear to have little impact over the space and time scales and at the locations we consider.

2. Mud-dominated bayfloor deposits may experience greater shallow subsidence than peat beds; up to 50% of elevation gained by overbank deposition in a growing delta may be lost to shallow subsidence.

3. Sediment loading and load-driven compaction are greatest at the delta apex, promoting the maintenance of a stable trunk channel and enabling continued sedimentation; these processes diminish radially downstream and have only a minor effect on progradation of the delta front.

4. Despite rapid shallow subsidence during bayhead delta progradation, sediment compaction has a limited effect on the rate and magnitude of land building.

In sum, this work provides new insights into how shallow subsidence operates in deltas and yields the surprising finding that bay-floor muds may be more compaction-prone than peats. Nevertheless, the high vulnerability to compaction of prograding deltas has a limited effect on the growth that can be accomplished through engineered sediment diversions.

Data Availability Statement

Data sets for this research are included in this article and its Supporting Information S1. Supporting stratigraphic details and subsidence calculations for each borehole are publicly accessible in the 4TU Research Data online repository at https://doi.org/10.4121/14170919.v2. Louisiana oil and gas production data are available online through the SONRIS database (http://www.sonris.com/) of the Louisiana Department of Natural Resources.

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