Bipolar Electrode Arrays for Chemical Imaging and Multiplexed Sensing

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ABSTRACT: Bipolar electrodes (BPEs) with arrays of cathodic and anodic poles were developed for use in closed bipolar systems. To increase the number of BPEs in the array, the anodic and cathodic poles were connected with each other using thin leads. A further increase in the number of BPEs was achieved by connecting the anodic and cathodic poles of the BPEs and the leads in different layers. A device with 9 × 10 arrays of cathodes and anodes was thus realized. When using this device to sense hydrogen peroxide (H₂O₂), the sensitivity and linear range of calibration plots could be adjusted by changing the driving voltage and the area ratio between the cathodic and anodic poles. The devices were used to image H₂O₂ and obtain time-lapse images for the diffusion and dilution of H₂O₂. Furthermore, DNA detection was demonstrated using an electroactive intercalator. The sensitivity could be improved by making the anodic poles smaller with respect to the cathodic pole and concentrating the electrochemiluminescence (ECL) in a small area. The ECL intensity changed according to the target DNA concentration in the solution.

1. INTRODUCTION

There is an increasing demand for the imaging and multiplexed detection of molecules related to cellular functions. For this purpose, devices based on electrochemical principles have advantages with regard to miniaturization, integration, and batch fabrication as well as high sensitivity. A straightforward approach to miniaturizing and integrating a large number of sensing elements is to simply use more individual components such as three-electrode systems. However, this results in a larger number of contact pads to be connected to the external instrument. To solve this problem, electrodes with the same roles can be connected by common leads and arranged in the form of a matrix. Although this method significantly reduces the number of contact pads (from the product of rows and columns to their sum), it still has limitations. Eventually, a much larger number of sensing elements (e.g., hundreds, thousands, or more) and the signal processing circuits may be all integrated using the CMOS technology. However, when the system contains easily degraded parts (such as biomaterials) or when disposable devices are desired, the high fabrication cost of the CMOS technology is unfavorable.

Bipolar electrochemistry is an attractive solution to the aforementioned problems. Bipolar electrochemical systems contain one or more electrically isolated strips of electrodes called the bipolar electrodes (BPEs). In the initial development stage, open bipolar systems with the BPEs immersed in a single solution were mainly used. When a voltage is applied between two driving electrodes immersed in the solution, a potential gradient is generated. The potential differences generated at the interface between the solution and the BPE polarize the two ends of the BPE to work as the cathode and the anode. Because the BPEs are not connected to external instruments, the redox reaction on one pole related to detection is reported via electrochemiluminescence (ECL) on the other pole. Open bipolar systems are advantageous in integrating a large number of BPEs. However, electroactive materials that may react on the anodic and/or cathodic poles of the BPE coexist in the same solution, which could influence the output signal. To address this issue, closed bipolar systems with the cathodic and anodic poles immersed in different solutions are widely used now. Although the open and closed bipolar systems only differ structurally by a wall that separates the two solutions, they have quite dissimilar working principles. In a closed bipolar system, the relationship between the driving voltage, E, and the potentials of the driving electrodes and the poles of the BPE with respect to the solution they contact is expressed by Kirchhoff’s second law as follows, when the ohmic drop in the solutions can be neglected.

\[ E = \Delta \phi(D1) - \Delta \phi(C) + \Delta \phi(A) - \Delta \phi(D2) \]

here, \( \Delta \phi(D1) \), \( \Delta \phi(D2) \), \( \Delta \phi(C) \), and \( \Delta \phi(A) \) are the potentials of the driving electrodes 1 and 2, the cathodic pole, and the anodic pole with respect to the solution, respectively.

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Compared with the open bipolar system, there is a limitation in the number of integrated BPEs in the closed bipolar system because of the presence of the wall that separates two solutions. Indeed, previous closed bipolar systems for multiplexed detection integrated only a limited number of BPEs.

Nevertheless, to realize high-density BPE arrays, bundles of insulated fibers or pores in a membrane were used to form a large number of tiny BPEs, and the resultant device was used to demonstrate chemical imaging. However, this type of system has not been used in applications other than imaging, and batch fabrication and simplification of the entire measurement setup are also the remaining issues. A reason for the limitations in multiplexed detection using closed bipolar systems with a small number of BPEs lies in the use of simple strips of rectangular BPEs. The cathodic and anodic poles are the critical parts for redox reactions, while the part between them merely functions as a conductor to pass electrons. Therefore, as long as the connecting parts can pass electrons without any problems, their layout may be optimized to further increase the number of integrated BPEs.

In this study, we fabricated a closed bipolar system with BPE arrays consisting of a matrix of cathodic and anodic poles connected with leads for chemical imaging and multiplexed sensing. The system was successfully used for imaging hydrogen peroxide (H$_2$O$_2$) and multiplexed detection of DNA.

2. EXPERIMENTAL SECTION

2.1. Reagents and Materials. All reagents and materials used for fabricating and characterizing the devices were obtained from commercial sources: glass wafers (TEMPAX Float; diameter: 3 inch; thickness: 500 μm) from Schott Japan (Tokyo, Japan); positive photoresist (S1818G) from Dow Chemical (Midland, MI); polyimide precursor solution (SP-341) from Toray Industries (Tokyo, Japan); poly(dimethylsiloxane) (PDMS; KE-1300T) and curing agent (CAT1300) from Shin-Etsu Chemical (Tokyo, Japan); platinum wire (diameter: 0.5 mm) from Nilaco (Tokyo, Japan); tris (2,2′-bipyridyl) dichloro-ruthenium(II) hexahydrate (Ru(bpy)$_2$Cl$_2$·6H$_2$O), buffer of tris(hydroxyethyl) aminemethane (Tris), ethylenediaminetetraacetic acid (EDTA) (TE buffer, pH 7.4), 6-mercapto-1-hexanol (MCH), and methylene blue (MB) from Sigma-Aldrich Japan (Tokyo, Japan); tri-n-propylamine (TPA) and other reagents from Wako Pure Chemical Industries (Osaka, Japan). All chemicals were reagent grade. Deionized Milli-Q water (18.2 MΩ cm; Millipore, Billerica, MA) was used to prepare all solutions.

Single-stranded probe DNA (pDNA) and target DNA (tDNA) were obtained from Eurofins Genomics (Tokyo, Japan) with the following sequences:

- pDNA: 5′-SH-C6-GCA TCG TAA GTC GTC AGT CAG CTA-3′
- tDNA: 5′-TAG CTG ACT GAC GAC TTA CGA TGC-3′

Solutions containing pDNA, MCH, or tDNA were prepared with TE buffer (pH 7.4) containing 10 mM tris, 1 mM EDTA, and 100 mM NaCl. An MB solution (100 μM) was prepared with 50 mM phosphate buffer solution (PBS) at pH 7.4 containing 100 mM KNO$_3$.

2.2. Structure and Fabrication of Bipolar Electrode Array. Structures of the fabricated BPE arrays and the experimental setup are shown in Figure 2. The BPEs were fabricated using a thin-film process, and the details are described in the Supporting information. Platinum BPEs were used for basic characterization and imaging, whereas gold BPEs were used for immobilizing pDNA strands. Each BPE consisted of square areas for the cathodic and anodic poles and a lead that connects them. The width of the lead was 70 μm for all BPEs.

We fabricated two types of devices named types I and II. In the type I device (Figure 2A), the cathodic and anodic poles and leads were formed on the same glass plane. Areas other than the

![Figure 1](https://example.com/figure1.png)

**Figure 1.** Schematic diagram and working principles of (A) open and (B) closed bipolar electrochemical systems. The figure on the right side of panel A illustrates the relation between the potential gradient in the solution and the polarization in different parts of the BPE.

![Figure 2](https://example.com/figure2.png)

**Figure 2.** Devices with an array of BPEs. Electrode layouts of (A) type I device with arrays of 6 × 8 cathodic and anodic poles and (B) type II device with arrays of 9 × 10 cathodic and anodic poles. Cross section along the Y–Y’ line is shown on the bottom right of panel B. (C) Experimental setup with the BPEs on a glass substrate and PDMS chambers with driving electrodes placed atop the glass substrate.
anodic and cathodic poles were insulated with a polyimide layer. Platinum and gold BPEs were formed using arrays of 4 × 5 and 6 × 8 cathodic and anodic poles, respectively. Dimensions of the cathodic and anodic poles were generally 500 μm × 500 μm. BPEs with different cathode and anode areas were also fabricated (Figure S1), which will be discussed later. For the gold BPEs, dimensions of the cathodic and anodic poles were 1000 μm × 1000 μm and 100 μm × 100 μm, respectively.

In the type II device (Figure 2B), the arrays of the cathodic and anodic poles and the leads were formed in different layers. First, only the leads were formed on the glass substrate, and then the polyimide insulating layer was formed. The insulating layer was opened at the ends of the leads for the corresponding cathodic and anodic poles were formed to cover the exposed lead areas and establish electrical connections (Figure S2). Only platinum BPEs were used for type II devices, and the dimensions of the cathodic and anodic poles were 500 μm × 500 μm.

2.3. Fabrication of the Chamber and Construction of the Setup. A PDMS chamber (height: 10 mm) was formed by replica molding, and the details are described in the Supporting information. The chamber was placed on the glass substrate with BPEs and slightly pressed for fixing (Figure 2C). The arrays of anodic and cathodic poles were exposed in the chamber. Platinum wires (diameter: 0.5 mm) serving as the driving electrodes were fixed at the longitudinal ends of the chamber using a polyimide tape. The ECL chamber was then filled with 50 mM PBS (pH 7.4) containing 5 mM Ru(bpy)32+, 25 mM TPA, and 100 mM KNO3 as a supporting electrolyte. The sensing chamber was filled with 50 mM PBS (pH 7.4) containing the analyte to be detected and 100 mM KNO3.

2.4. Detection of ECL. The device with the BPEs and PDMS chamber was placed in the dark, and a constant voltage was applied between the two driving electrodes using a DC power supply (PMX110-0.6A, Kikusui Electronics, Kanagawa, Japan). ECL was captured with a CCD camera (VB-7010, Keyence, Osaka, Japan) attached to a fluorescence stereomicroscope (VB-G25, Keyence, Osaka, Japan). The sensitivity and exposure time of the camera were, respectively, set at ISO 200 and 60 s for multiplexed sensing and H2O2 imaging, while they were set at ISO 1600 and 30 s for DNA sensing. ECL intensity data were extracted with ImageJ (NIH) from a single pixel at the center of the related anodic poles in the captured photograph.

2.5. Modification of BPE Arrays for DNA Detection. A type I device with gold BPEs was used for DNA detection. To clean the surface of the BPEs, chips with BPEs were immersed for 10 min in a solution containing 50 mM KOH and 30% H2O2 (w/w). Then, the surface of the cathodic poles was cleaned by scanning 90 cycles at potentials between −1.0 and +1.2 V (vs Ag/AgCl) at a scan rate of 1.0 V/s in a solution containing 100 mM KNO3 and 10 mM K3[Fe(CN)6] until the shape of the voltammogram stabilized.

To modify the surface of BPEs, a piece of PDMS with five straight flow channels (height: 100 μm) was attached to the cathode side of the BPEs (Figure S3). The flow channels were used to accommodate solutions containing pDNA, MCH, or tDNA. The surface of cathodic poles was first kept in a 20 μM solution of thiolated single-stranded pDNA overnight and then in 1.0 mM MCH for 1 h, forming a self-assembled monolayer containing pDNA and MCH on the surface. MCH was used to block the surface of the gold electrode.27,28 After each step, the PDMS flow channels were removed, and the BPEs were rinsed with pure water and dried with nitrogen gas.

For the hybridization of pDNA and tDNA, the PDMS flow channels were again attached to the glass substrate with BPEs after pDNA modification. Then, standard solutions containing tDNA were injected into the flow channels and incubated for 2 h. Then, the flow channels were removed, and the BPEs were
rinsed with pure water to remove excess tDNA. Next, the BPEs were immersed in a 100 μM MB solution and incubated for 1 h. The BPEs were rinsed with pure water and then used in the experiments. The whole procedure was performed at room temperature.

2.6. Characterization Using the Three-Electrode System. Immobilization and hybridization of DNAs were first examined using one of the cathodic poles as the working electrode in a conventional three-electrode system (Figure S4). The PDMS chamber shown in Figure 2C was attached to the glass substrate with BPEs, and only the cathodic chamber was filled with 50 mM PBS containing 100 mM KNO₃ (pH 7.4). A commercial liquid-junction Ag/AgCl reference electrode (2060A-10T, Horiba; Kyoto, Japan) was inserted into the solution. The internal solution of the Ag/AgCl electrode was 3.0 M KCl. The platinum wire fixed at the end of the PDMS chamber was used as the auxiliary electrode.

2.7. Detection of tDNA. ECL from the BPEs with hybridized pDNA and tDNA on the cathodic poles was detected using the setup mentioned earlier in Figure 2C. The anodic chamber was filled with the ECL solution, whereas the cathodic chamber was filled with 50 mM PBS (pH 7.4) containing 100 mM KNO₃.

3. RESULTS AND DISCUSSION

3.1. Multiplexed Sensing and Imaging of H₂O₂. In the fabricated devices, the cathodic and anodic poles were connected with 70 μm wide lead patterns of different lengths. Table S1 summarizes the measured resistances of the shortest and longest leads used in type I and II devices. Even with the longest leads, the resistance was approximately 300 Ω. In contrast, the current flowing through a lead was anticipated to be on the order of a few μA, as per our previous results obtained using BPEs with cathodic and anodic poles of similar sizes.⁵⁹ Therefore, the ohmic drop at the leads was expected to be negligible. To confirm this, we filled the sensing chamber of a type I device with a 4 × 5 array with 50 mM PBS (pH 7.4) containing 100 mM KNO₃ and examined the ECL generated following the reduction of dissolved oxygen on the cathodic poles. The ECL images obtained at two different driving voltages are shown in Figure S5. Uniform ECL was observed from all anodic poles, although the length of leads in the device ranged from 5.7 to 22.5 mm. This result demonstrates that the conductivity of 70 μm wide leads is sufficient and that the lead length only has negligible influence.

Another type I device with the same cathodic and anodic areas (1000 μm × 1000 μm) was then used to detect H₂O₂ in standard solutions of different concentrations. Figure 3A shows ECL images obtained with 1, 2.5, 5, and 10 mM H₂O₂. Under a fixed driving voltage, the ECL became brighter with the increase in H₂O₂ concentration. Figure 3B shows the dependence of ECL intensity on the H₂O₂ concentration at various applied voltages. An enhanced sensitivity was clearly observed upon increasing the driving voltage, and the ECL intensity increased linearly at lower concentrations. The ECL intensity tends to become saturated because the ECL reaction on the anodic pole becomes rate-limiting at higher H₂O₂ concentrations.

The above experiments used an array of BPEs with cathodic and anodic poles having the same area. When the device is used to not only detect the target analyte but also measure its concentration, it is important to know which side of the poles is rate-limiting. To check this influence, BPEs with cathodic poles of different areas were used (Figure S1), while the area of the anodic poles was fixed (1000 μm × 1000 μm), and the results are
shown in Figure 3C. At an area ratio of $A_c/A_a = 1$ ($A_c$ and $A_a$ are the areas of cathodic and anodic poles, respectively), a linear relation between the ECL intensity and the H$_2$O$_2$ concentration was observed below 7.5 mM. Upon increasing the $A_c/A_a$ ratio, the sensitivity increased; however, the linear range of the calibration plot decreased at the same time. The opposite tendency was observed when decreasing $A_c/A_a$. As shown in Figure 3B,C, the sensitivity and the linear range of the calibration plot can be adjusted by changing both the applied driving voltage and the $A_c/A_a$ ratio. When the analyte concentration is very low (such as the case of DNA sensing, which will be discussed later), $A_c/A_a$ should be as large as possible subject to the limitation of observing ECL in small spots, and the driving voltage should be as small as possible to minimize the influence of redox-active interferents.

Figure 4A,B shows the diffusion and dilution of H$_2$O$_2$ after dropping 20 μL of 100 mM H$_2$O$_2$ solution at different locations in the sensing chamber of a type I device. The array of cathodic poles is shown on the right side of the figure, with the location of dropped H$_2$O$_2$ solution indicated by orange arrows. Note that the ECL image of the spreading H$_2$O$_2$ on the array of cathodic poles in the sensing chamber is a mirror image of that of the ECL image in the anodic chamber. In both cases shown in Figure 4, ECL was initially observed in a localized area near the dropped solution. As time elapsed, however, the area became larger and the ECL intensity decreased overall, suggesting that the H$_2$O$_2$ concentration decreased as a result of diffusion in the horizontal direction and a change in the diffusion layer due to the consumption of H$_2$O$_2$ by the cathodic poles. Imaging was also conducted using a type II device with an array of $9 \times 10$ cathodes and anodes (Figure 5). The same tendency was observed with higher spatial resolution.

Resolution of the images can be improved by simply decreasing the size of cathodic and anodic poles and the distance between neighboring poles, as well as increasing the density of cathodic and anodic poles. The current thin-film process is capable of fabricating the cathodic and anodic poles of submicrometer dimensions. Here, a trivial but challenging problem is where and how to place the lead patterns. In the type II device, the lead patterns were separated from the patterns of cathodic and anodic poles and formed in different layers. A straightforward method will be further separating the lead patterns into more layers and making them thinner while maintaining sufficient conductivity. As we stressed earlier, an advantage of our devices is using conventional thin-film technology to batch-fabricate arrays of BPEs, which will help lower the production cost of the devices.

3.2. Application to DNA Sensing. Figure 6 shows the principle of DNA detection. The electroactive MB works as an intercalator for insertion into double-stranded DNAs, and this can be used to detect hybridization between tDNA and pDNA on the cathodic poles of the gold BPEs. MB intercalated in the double strand is reduced by applying an appropriate potential to the electrode, and therefore the hybridization can be detected from the increase in current. First, we checked the modification of gold BPEs and detection using MB, using one of the cathodes of the BPEs as the working electrode in a conventional three-electrode system (Figure S4). Figure 7A shows changes in the cyclic voltammograms after each modification step of the electrode surface. With a bare gold
Figure 8. DNA sensing using a BPE array. (A) BPE array used for this purpose, with the area ratio of the cathodic to the anodic pole (A_c/A_a) of 100. Areas surrounded by the red lines correspond to the white dotted line in panel B. (B) ECL images obtained after incubating the BPEs with 0, 0.5, 1, 5, and 10 μM tDNA solutions and 100 μM MB solution in each flow channel. Driving voltage: 2.1 V. A magnified image of panel B is provided as Figure S6 in the Supporting information. (C) Dependence of ECL intensity on the concentration of tDNA obtained at driving voltages of 2.0 and 2.1 V. “BG” indicates the background intensity obtained from areas without ECL emission. (D) Dependence of ECL intensity normalized by the background intensity on tDNA concentration. Panels (C) and (D) display the average values and standard deviations of ECL intensities obtained from the four anodic poles at the same C_{tDNA} (n = 4).

used BPEs with A_c/A_a = 1. However, under the rate-limiting condition of the cathodic pole, the ECL was too weak to be detected. Therefore, the area of the anodic poles was decreased to 1/100 with respect to that of the cathodic poles (A_c/A_a = 100) to concentrate the emitted ECL within smaller areas (Figure 8A). At this area ratio, ECL could be detected, as shown in Figure 8B (and magnified images in Figure S6), and the ECL intensity increased with increasing tDNA concentration (Figure 8C,D).

In this experiment, we checked the response down to 500 nM. If the detection limit is defined as three times the standard deviation of the background, then it is around this concentration, which is relatively high compared with previous works using MB as an intercalator but based on different detection principles. The relatively high detection limit is not due to the detection chemistry but mainly to the method of measuring the ECL intensity using image analysis. Here, the ECL was captured by digital photography and its intensity was calculated from the images. The detection limit could be lowered by measuring the ECL intensity using photomultipliers or photodiodes instead. This approach is applicable in the case of a single sensor. However, it will be extremely difficult for a large number of ECL spots because the same number of photomultipliers or photodiodes will then have to be collected or integrated, and an additional structure is required to shield the ECL from neighboring sensing sites. Therefore, the application of these techniques will be unrealistic. In comparison, it is more realistic to extract ECL intensity information using the appropriate software from captured digital images. Recently, there is a
4. CONCLUSIONS

Unlike open bipolar systems in which all parts of the BPEs are immersed in a single solution, it was not straightforward to batch-fabricate devices with arrays of many cathodic and anodic poles for closed bipolar systems. Here, we increased the number of cathodic and anodic poles of BPEs by simply connecting them with thin leads and arranging the cathodic and anodic poles in the form of matrices. The number of integrated BPEs was further increased by separating the cathodic/anodic poles and the leads into different layers.

The fabricated device was used to image H₂O₂ as an electroactive analyte, as well as its diffusion and dilution. The sensitivity and linear range of calibration plots can be adjusted by changing the area ratio Aₐ/Aₙ between the cathodic and anodic poles. The devices were also used for multiplexed DNA detection. To facilitate measurement and improve detection sensitivity, it is effective to reduce the Aₐ/Aₙ ratio. The ECL intensity can be correlated with the concentration of DNA to be detected.

Although it is challenging to record many ECL signals and achieve high sensitivity, our devices fabricated using a simple method realized a large number of integrated sensing sites. These devices may be useful basic tools for clinical analysis and cell engineering.

ASSOCIATED CONTENT

Supporting Information
The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acsomega.2c02298.

Device fabrication; measurement of lead resistances; length and resistance of the shortest and longest leads in types I and II devices; BPEs with cathodic and anodic poles in different area ratios; magnified views of the type II device; device with gold BPEs and PDMS flow channels used for modifying the cathodic poles and detecting DNAs; setup of the three-electrode system; ECL from the array of platinum anodic poles at the driving voltages of 3.6 and 4.0 V; and magnified version of the ECL images in Figure 8B (PDF).

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Notes
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