Dominance of Smartphone Exposure in 5G Mobile Networks

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Abstract—The deployment of 5G networks is sometimes questioned due to the impact of Electromagnetic Field (EMF) generated by Radio Base Station (RBS) on users. The goal of this work is to analyze such issue from a novel perspective, by comparing RBS EMF against exposure generated by 5G smartphones in commercial deployments. The measurement of exposure from 5G is hampered by several implementation aspects, such as dual connectivity between 4G and 5G, spectrum fragmentation, and carrier aggregation. To face such issues, we deploy a novel framework, called 5G-EA, tailored to the assessment of smartphone and RBS exposure through an innovative measurement algorithm, able to remotely control a programmable spectrum analyzer. Results, obtained in both outdoor and indoor locations, reveal that smartphone exposure (upon generation of uplink traffic) dominates over the RBS one. Moreover, Line-of-Sight locations experience a reduction of around one order of magnitude on the overall exposure compared to Non-Line-of-Sight ones. In addition, 5G exposure always represents a small share (up to 38%) compared to the total one radiated by the smartphone.

Index Terms—5G mobile communication, electromagnetic measurements, electromagnetic fields, performance analysis.

I. INTRODUCTION

According to recent reports [1], more than 80% of the world population own a smartphone. The diffusion of such equipment is so pervasive in the daily activities that it is almost impossible to imagine a future without a smartphone in our hands. One of the key drivers for the ever-increasing smartphone adoption is the ubiquitous Internet service, generally offered by mobile networks. To this purpose, 5G aims at delivering a true broadband connectivity service, especially in urban areas and densely populated zones. The sales of smartphone equipped with 5G interfaces are constantly rising, with more than 700 millions of units sold during 2022 [2], in parallel with the deployment of 5G networks across the world [3]. Therefore, 5G networks will (likely) become the main provider for smartphone connectivity in the near future.

In this scenario, the Electromagnetic Field (EMF) exposure from 5G networks is a hot topic in several communities (e.g., government, local committees, environmental protection agencies and academia), especially when considering the (possible, yet still not proven) implications of 5G exposure on the human health [4]. To this aim, EMF working groups of World Health Organization (WHO) [5], International Commission on Non-Ionizing Radiation Protection (ICNIRP) [6], Institute of Electrical and Electronics Engineers (IEEE) committees [7] and IEEE standards [8] periodically evaluate the scientific literature, including the assessment of biological effects from EMF exposure generated by telecommunication equipment. At present time, there is a consensus among such authoritative organizations that a clear causal correlation between exposure from mobile networks adhering to international exposure guidelines and emergence of long-term health diseases has not been observed so far. Consequently, 5G exposure does not pose any evident risk on the population health. Very frequently, however, the dispute about 5G exposure is dominated by the bias of non-scientific communities [9], who associate the exposure of 5G Radio Base Stations (RBSs) with severe health diseases - a connection that is not (presently) proven by science. As a result, the installation of new 5G RBSs over the territory is (sometimes) fiercely opposed by local communities and advocacy groups, who act against the (supposed) increase of exposure generated by the newly installed RBSs in their neighborhood.

Despite the exposure from 5G RBS is a matter of debate - at the extent that the presence of a 5G antenna over a real estate has an impact on the property value - little or no concerns are associated with 5G smartphones, which are another (and important) source of exposure [4]. Part of the population promptly reacts against the presence of 5G towers in proximity to their living and working spaces, while almost nobody cares about the exposure that is radiated by the own smartphone when uploading/downloading hundreds of Megabytes of data through a mobile network connection. Therefore, the total exposure levels, resulting from the combination of 5G smartphones and 5G RBSs, are almost overlooked.

The goal of this work is twofold. On one side, we assess in a scientific way the exposure generated by smartphones in a commercial 5G deployment. On the other one, we compare...
the observed smartphone exposure levels against the ones radiated by the serving RBS, showing that the increase of signal coverage from 5G RBS (and consequently the exposure) is highly beneficial in reducing the EMF from the smartphone. The measurement of smartphone versus RBS exposure has been preliminary investigated in the context of 4G (see e.g., the very interesting paper of Schilling et al. in [10]), but, to the best of our knowledge, none of the previous works have conducted an in-depth measurement analysis tailored to a 5G commercial deployment. We point out, however, that our purpose is not to spread worries or alarms - as both smartphone and RBS exposure naturally adhere to EMF regulations and are therefore legally safe - but rather to scientifically position the exposure from 5G RBSs in a wide picture that include the contribution of 5G smartphones, the effect of propagation conditions and the amount of traffic that is generated by User Equipment (UE).

More concretely, we target the following questions: What is the amount of exposure generated by a 5G smartphone and a 5G RBS in a commercial deployment? What is the impact of uplink (UL)/downlink (DL) traffic generated by the smartphone on the exposure levels? How do propagation conditions (like RBS proximity/remoteness, presence/absence of buildings on the radio link towards the RBS) influence 5G exposure levels? How does the dual connectivity between 4G and 5G affect the exposure? The answer to these intriguing questions is the technical goal of this paper. More specifically, our original contributions include: i) a ground-truth overview of 5G implementation features that are relevant for smartphone and RBS exposure assessments, with a focus on the Italian country; ii) the definition of the measurement requirements to achieve our goal, based on the technological features outlined in i); iii) the design of an innovative measurement framework, called 5G EXPOSURE ASSESSMENT (5G-EA), which strongly leverages networking features (e.g., traffic generation & monitoring, and remote programmability of spectrum analyzers) to satisfy the requirements in ii); iv) the application of 5G-EA in a real 5G deployment to collect an extensive campaign of exposure measurements.

Our results demonstrate that the smartphone exposure dominates over the RBS one upon generation of UL traffic, especially when the UE is in Non-Line-of-Sight (NLOS) with respect to the RBS. On the contrary, both smartphone exposure and total EMF are reduced up to one order of magnitude when the smartphone UL traffic traverses a radio link in Line-of-Sight (LOS) with respect to the serving RBS. Interestingly, the exploitation of dual connectivity feature between 4G and 5G reveals that only a small smartphone exposure share (at most equal to 38%) is due to 5G, while the largest exposure levels are derived from the carrier aggregation over 4G bands. Moreover, both total and smartphone exposure-per-bit metrics are inversely proportional to the maximum amount of UL traffic generated by the smartphone in the measurement location, thus suggesting that innovative exposure estimators, based on the reporting of maximum UL traffic from the smartphone, can be designed.

Last but not least, we demonstrate that the complexity of the measurement procedures (which need to track spatial/temporal variations of 4G carrier aggregation and dual connectivity between 4G and 5G) can be efficiently tackled by a framework encompassing a softwarized measurement algorithm, like the one developed in this work. The design of softwarized-based EMF measurement procedures, running on general purpose machines and able to remotely control spectrum analyzers, indicate the potentials of a new market, in which the EMF measurement algorithms are designed, shared and adopted by a community of experts, while the manufacturers “open” the interfaces of the measurement equipment to support the remote programmability from non-proprietary software.

The rest of the paper is organized as follows. Related works are analyzed in Section II. Section III includes a primer about the implementation aspects of 5G networks that are relevant to EMF monitoring, with a focus on the Italian country - useful for the layman in the field. Section IV defines the measurement requirements, taking into account our goals and the 5G implementation aspects of Section III. The design of the 5G-EA measurement framework is described in Section V. Results, retrieved from a real 5G deployment, are detailed in Section VI. Finally, Section VII concludes our work and reports possible future directions.

II. RELATED WORK

Fig. 1 sketches the main taxonomy of RBS and smartphone exposure measurements over an evaluation point. More in depth, we identify the following groups: G1) environmental exposure from 5G RBS, G2) environmental exposure from nearby 5G smartphones, G3) exposure generated by the 5G RBS when a 5G smartphone is used to inject active traffic in the evaluation point, G4) exposure generated by the 5G smartphone in the same condition of G3. Intuitively, groups G1-G2 identify measurements taken without injecting any traffic in the measurement positions, and resulting in general lower exposure levels than groups G3-G4.

In the following, we initially focus on the works tailored to the RBS side, i.e., covering groups G1 and/or G3. Then, we focus on the works investigating the active traffic exposure from 5G smartphone (group G4). Finally, we consider the works that integrate joint measurement of environmental/active traffic exposure from RBS and active traffic exposure from smartphone (groups G1 + G3 + G4) - although we did not find any previous work tailored to 5G. As a side comment, we intentionally leave
apart group $G_2$, as the exposure contributions from nearby terminals rapidly decrease to negligible levels when they are not in close proximity to the evaluation point.

A. Exposure Measurements From 5G RBS

We initially focus on the works targeting: i) measurement of environmental exposure from 5G RBS (group $G_1$) [11], [12], [13], [14], [15] and ii) measurement of active traffic exposure from 5G RBS (group $G_3$) [16], [17], [18], [19], [20], [21], [22], [23], [24], [25], [26].

Focusing on $G_1$ [11], [12], [13], [14], [15], Chiaraviglio et al. [11] perform a massive evaluation of a 5G RBS covering a town. Betta et al. [12], [13] and Elbasheir et al. [14] collect RBS exposure information through the measurement of the pilot signals. Hausl et al. [15] analyze the received power over the control channels in a 5G network by employing a code-selective measurement methodology.

Focusing on $G_3$ [16], [17], [18], [19], [20], [21], [22], [23], [24], [25], [26], Adda et al. [16], Aerts et al. [17], Migliore et al. [18], Bornkessel et al. [19], Schilling et al. [20], Chiaraviglio et al. [21], Liu et al. [22], Heliot et al. [23] share the idea of measuring the exposure from 5G RBSs by forcing traffic with a terminal in the DL direction from the RBS. The works of Aerts et al. [24], Chountala et al. [25] and Wali et al. [26] complement the previous ones by adding the evaluation of 5G RBS exposure when UL traffic is forced with a terminal. In general, such works demonstrate that the exposure from 5G RBSs depends on the amount of traffic that is injected towards the measurement location. Moreover, the active traffic contribution from the 5G RBS is generally higher than the environmental one.

Compared to [11], [12], [13], [14], [15], [16], [17], [18], [19], [20], [21], [22], [23], [24], [25], [26], we tackle the 5G EMF measurement from a novel perspective, by including the contribution of the smartphone in the EMF assessments (groups $G_1 + G_3 + G_4$). Although we exploit some findings/intuitions of the literature (like the idea of forcing DL/UL traffic towards the measurement location), our work presents an innovative measurement framework, called 5G-EA, tailored to the assessment of both smartphone and RBS EMF.

B. Exposure Measurement From 5G UE

We focus hereafter on the literature addressing active traffic exposure measurements from 5G UE (group $G_4$) [27], [28], [29], [30], [31], [32]. Xu et al. [27] perform measurements of 5G UE power density in a semi-anechoic chamber. Nedelcu et al. [28] analyze the UL contribution from 5G UE in terms of radiated power. Joshi et al. [29] and Lee et al. [30] analyze 5G UE output power levels that are collected from measurements in commercial networks. Deaconescu et al. [31] and Miclaus et al. [32] collect EMF measurement from a 5G UE in an indoor controlled environment, with and without generating UL/DL traffic. Overall, such works indicate that the exposure from 5G smartphones is non-negligible, and that a huge variation in the exposure levels can be observed. In contrast to [27], [28], [29], [30], [31], [32], in this work we go two steps further by: i) integrating the exposure from 5G RBS and ii) performing exposure assessments of groups $G_1 + G_3 + G_4$ both in indoor controlled environments and into the wild, i.e., several outdoor locations covered by a commercial 5G RBS.

C. Joint Measurement of Smartphone and RBS Exposure

The last category relevant to our study is focused on the joint assessment of smartphone and RBS exposure. In this case, we did not find any work covering groups $G_1 + G_3 + G_4$ in the 5G domain. Focusing instead on pre-5G technologies, the most relevant work to ours is the one of Schilling et al. [10], in which the authors propose a method based on EMF measurements to evaluate the combined exposure from both smartphone and RBS in 4G deployments. Interestingly, a strong reduction in the UL transmission power is observed when the link conditions are improved. Moreover, the total exposure in a macro cell scenario is dominated by the smartphone contribution. Eventually, the authors advocate the need for a balance between RBS and smartphone exposure.

In line with [10], our work is also focused on the joint assessment of smartphone and RBS exposure. However, differently from [10], we focus on a novel domain: the 5G exposure assessment of groups $G_1 + G_3 + G_4$, which requires a different exposure framework than the one used by [10] for the 4G evaluations. In addition, 5G smartphones currently employ a dual 4G/5G connectivity to support the data transfer. Therefore, our innovative framework evaluates the exposure over both 4G and 5G bands. This last aspects further complicates the exposure assessment compared to [10], since multiple 4G/5G carriers are dynamically used for the data transfer.

III. 5G IMPLEMENTATION ASPECTS RELEVANT TO EMF MONITORING

In this section, we provide a brief overview of the key 5G implementation aspects that have an influence on the design of our EMF assessments, with a focus on the Italian country.

Spectrum Fragmentation. 5G encompasses a wide set of spectrum portions, including frequencies lower than 1 GHz, frequencies between 1 and 6 GHz - a.k.a. the mid-band - and close-to-mm Wave frequencies at around 26-27 GHz. The most widespread option to provide 5G mobile service in Italy is the mid-band, thanks to the fact that the adopted frequencies can guarantee the mixture of coverage and capacity that is required during the current 5G early-adoption phase.

The mid-band spectrum, spanning over 3.4-3.8 GHz is rather a crowded space. Historically, the 3.4-3.6 GHz portion of the spectrum was allocated to Fixed Wireless Access (FWA) operators [33], which provided access to household customers over legacy technologies (pre-5G). The 3.6-3.8 GHz portion was instead allocated with the purpose of providing 5G service for mobile operators, with licensed spectrum blocks including both 80 MHz and 20 MHz portions [34]. Clearly, the operators that were licensed 20 MHz of 5G mid-band spectrum (like W3) could not support the same level of service as the one provided by providers operating on wider bandwidth, e.g., 80 MHz. To overcome this issue, W3 has recently signed an agreement with the FWA operator Fastweb to lease some portions of the 3.4-3.6
GHz spectrum for the 5G mobile service [35]. Despite the total allocation of licensed and leased bandwidth is non-negligible (typically equal to 60 MHz for W3), the spectrum blocks for delivering 5G in the mid-band are not contiguous. Up to this point, a natural question is: How do such spectrum allocations affect the considered measurements? The answer is that, for some operators (like W3), the 5G EMF monitoring (even focusing solely on the mid-band) has to be done over multiple not-contiguous spectrum portions. Such feature generally complicates the EMF measurement procedure, as it is necessarily (in principle) to iterate over the different 5G bands in use by the same operator to evaluate the total 5G exposure.

**Interviewing of 5G and 4G Networks.** At the time of preparing this work, the Non Stand Alone (NSA) option, in which the 5G radio access network is supported by a 4G core, is still the most widespread way to implement 5G networks in the country. Compared to a full Stand Alone (SA) deployment, NSA requires a strong dependability of the 5G service with respect to the 4G network. In particular, a 5G connection is always provided in parallel to a 4G one, which acts as the anchor for the dual 4G/5G connectivity [36]. Therefore, our EMF assessments have to include the monitoring of the 4G bands that are used in parallel to the 5G ones, as the injected traffic is (likely) flowing over both 4G and 5G channels. To further complicate such feature, Fig. 2 reports the band allocations of W3 over pre-5G and 5G technologies (valid for the city of Rome). Astonishingly, the number of possible bands that can be used by 4G is huge, as all the spectrum portions licensed to W3 over 800-2600 MHz frequencies can be potentially used for 4G services.

**Dynamics of Carrier Aggregation.** Another key implementation aspect that strongly affects the EMF monitoring is the (possible) carrier aggregation across multiple 4G bands, which are used in parallel to the 5G ones. As reported in relevant 3GPP standards [37], there are plenty of possible carrier aggregation combinations, ranging from sets composed of 1-2 bands up to ones including several pre-5G spectrum portions in use by the operator. The selected combination of aggregated carriers for a given connection is a local decision, which depends on many features (like the propagation conditions reported by the smartphone) that are monitored by the serving RBS. Consequently, the adopted set of carriers cannot be determined a priori and it depends on the measurement location. The dynamicity in the carrier aggregation has to be taken into account in our measurement procedures, in order to limit the exposure assessment only on those bands that are used for the transfer of the injected traffic.

**Time Division Duplexing.** Fig. 2 details the assignment of frequencies for the UL and DL directions. In different spectrum portions (B20, B8, B3, B1 and B7), the Frequency Division Duplexing (FDD) rigidly separates the UL frequencies with respect the DL ones. On the other hand, the B38 spectrum of 4G and all the 5G portions in use by W3 (covering the N78 band) are employing the Time Division Duplexing (TDD), which adopts multiplexing of both UL and DL over the same frequencies. Intuitively, TDD complicates the dissection of smartphone versus RBS exposure contributions, as both time-frequency domains have to be jointly analyzed to distinguish the DL from the RBS with respect to the UL from the smartphone.

**RBS Co-Location.** Fig. 3 shows a typical roof-top RBS installation, which includes multiple 5G and 4G sectors of W3 operator, as well as radio equipment of other operators that are co-located on the same site. Since our goal is to consider the impact of smartphone and RBS exposure for a given connection, we need to distinguish the EMF contribution of the considered operator with respect to the co-located ones that serve the same area (i.e., the sectors of other operators in the figure).

**IV. 5G EMF Measurement Requirements**

We analyze hereafter the measurement requirements that are instrumental for the definition of the EMF monitoring framework, starting from the goals of our work in Section I and the implementation features detailed in Section III. To this aim, Table I
TABLE I
5G FEATURES & GOALS versus EMF MEASUREMENT REQUIREMENTS

| Feature/Goal | Requirement | Operator and Technology Impact | Narrow-band frequency-selective measurements | R1 |
|-------------|-------------|-------------------------------|---------------------------------------------|----|
| FG1         |             |                               |                                             |    |
| FG2         | 5G (and 4G) TDD | Dissection of smartphone vs. RBS exposure | R2 |
| FG3         | 4G/5G Dual Connectivity | Multiple monitoring over 4G and 5G technologies | R3 |
| FG4         | Spectrum Fragmentation | Detection & iteration over the adopted set of carriers | R4 |
| FG5         | Dynamic carrier aggregation | Selecting representative measurement locations | R5 |
| FG6         | Impact of traffic | Forcing smartphone traffic in the UL/DL directions | R6 |
| FG7         | Impact of propagation |                                                             |    |

TABLE II
FREQUENCIES, WAVELENGTHS, FRAUNHOFER REGIONS AND FAR FIELD DISTANCES FOR THE W3 BANDS WITH SMARTPHONE ANTENNA LENGTH $L_A = 0.08$ [m]

| Frequency $f$ | Wavelength $\lambda_f$ | Fraunhofer Region $D_f^{FF}$ | Far-field distance $D_f^{FF}$ |
|--------------|------------------------|-----------------------------|-----------------------------|
| 800 [MHz]    | 0.37 [m]               | 0.03 [m]                    | >0.37 [m]                   |
| 900 [MHz]    | 0.33 [m]               | 0.04 [m]                    | >0.33 [m]                   |
| 1800 [MHz]   | 0.16 [m]               | 0.08 [m]                    | >0.16 [m]                   |
| 2100 [MHz]   | 0.14 [m]               | 0.09 [m]                    | >0.14 [m]                   |
| 2600 [MHz]   | 0.12 [m]               | 0.11 [m]                    | >0.12 [m]                   |
| 3447 [MHz]   | 0.09 [m]               | 0.15 [m]                    | >0.15 [m]                   |
| 3547 [MHz]   | 0.08 [m]               | 0.15 [m]                    | >0.15 [m]                   |
| 3610 [MHz]   | 0.08 [m]               | 0.15 [m]                    | >0.15 [m]                   |

A. Measured Exposure Metrics

In principle, any exposure assessment strongly depends on the target metrics that need to be measured. In particular, the classical taxonomy defines Specific Absorption Rate (SAR)/absorbed power density for UE assessments versus electric field/plane-wave power density for RBS evaluation [4]. The SAR and absorbed power density metrics are useful when the measurement target is the near-field assessment, in which the radiating source is (almost) attached to the body (e.g., an UE close to the ear during a phone call). Despite such metrics are still relevant for today equipment (and for UE SAR-based limits), we point out that the typical smartphone user makes phone calls with the equipment attached to the ear only to a limited extent. In fact, recent statistics [38] reveal that smartphones are mainly used for downloading/uploading data traffic, with the UE hold at a non negligible distance from the head/chest in order to read/produce content on the screen. Since our goal is to evaluate the exposure in such conditions - which represent a typical 5G scenario - in this work we always impose a minimum distance between the UE generating traffic and the evaluation point of our measurement.

Apart from better matching the actual smartphone usage, the introduction of a minimum distance between the UE and the measurement point may allow operating in the far-field region from the UE, which is formally defined as:

$$D_f^{FF} > \max \left( \lambda_f, \frac{2L_A^2}{\lambda_f} \right)$$ (1)

where $\lambda_f$ is the wavelength of frequency $f$, $L_A$ is the length of the radiating antenna, and the term $\frac{2L_A^2}{\lambda_f}$ represents the limit of the Fraunhofer region. To give an example, Table II reports the values of $\lambda_f$ and $D_f^{FF}$ for the bandwidth allocation of W3 and a smartphone antenna length $L_A$ equal to 0.08 [m]. As expected, the observed far-field distances $D_f^{FF}$ strongly depend on the considered frequencies, but, however, we can note that the minimum $D_f^{FF}$ is lower than 0.2 [m] for 4G frequencies above or equal 1800 [MHz] and for all 5G frequencies.

By imposing the distance $D_f^{FF}$ from the UE, we are able to operate in far-field, a condition that is also generally experienced when considering the RBS as the source of radiation. In this way, an homogeneous set of metrics (e.g., electric field and/or plane-wave power density) can be used to measure both UE and RBS exposure. This is in turn beneficial for adopting the same
B. Tools and HW Chains

We describe hereafter the equipment tools, which are also sketched in Fig. 4(a). Focusing on the exposure assessment chain, we employ the following HW ($E_1$-$E_5$):

$E_1$) Hand-held Spectrum ANalyzer (SAN) Anritsu MS2090A with maximum frequency range equal to 32 [GHz] with 110 [MHz] of maximum bandwidth analysis, equipped with one battery plus another one of backup;

$E_2$) Directive antenna Aaronia 6080, with frequency range 680 [MHz]-8 [GHz], maximum gain equal to 6 [dBi], nominal impedance of 50 [Ohm];

$E_3$) Coaxial cable Anritsu flexible RF 1 [m] Cable K(f)-K(m) DC-40 [GHz], connecting the SAN to the directive antenna;

$E_4$) Laptop MacBook Air with Intel Core i5 1.3 [GHz] CPU, 4 [GB] of RAM, 256 [GB] of memory, equipped with Matlab R2017b and RSVisa 5.12.1 driver;

$E_5$) Ethernet cable of 1 [m] length, Cat.5E, verified TIA-EIA-568-C.2, connecting the laptop to the SAN.

Focusing on $E_1$, the SAN allows implementing narrow-band measurements, and thus matching requirement $R_1$. Focusing then on $E_2$, the directionality of the adopted antenna allows spatially separating the contribution of the UE and the one of the RBS. As shown in Fig. 4(b), the antenna is oriented towards the considered source. In this way, the contribution of other sources, e.g., a UE placed behind the measurement antenna, is not sensed. By selectively pointing the directive antenna towards the UE or the RBS, we can isolate their respective contributions, and thus matching requirement $R_2$, even when the monitoring is performed over TDD bands. In addition, the short coaxial cable of $E_3$ guarantees almost negligible signal degradation between the directive antenna and the SAN - a feature that is instrumental for measuring the relatively low environmental exposure values of 5G. The SAN is then connected to the $E_4$ laptop via the dedicated $E_5$ cable. The core of our framework is a custom measurement algorithm written in Matlab and running on $E_4$. The algorithm allows remotely programming the SAN to perform multiple monitoring of 4G and 5G bands (requirement $R_3$), as well as to implement the automatic detection and iteration over the adopted set of carriers (requirement $R_4$).

Focusing then on the traffic generation chain, we adopt the following tools:

$T_1$) Samsung S20+ 5G smartphone, equipped with Android 11 (1st May 2021) and Magic Iperf v.1.0 App client.

$T_2$) Dell Poweredge R230 server, equipped with 4 cores Intel Xeon E3-1230, 64 GB of RAM, Ubuntu 18.04.1 OS and Iperf v.3.1.3.

More concretely, $T_2$ is installed at the University building, and made accessible through a public Internet Protocol (IP) address. In addition, the Iperf program is used to generate synthetic traffic between $T_1$ and $T_2$ (either in the DL or UL direction). In this way, we accomplish requirement $R_5$.

Fig. 4(a) shows the measurement setup in a given location. Both smartphone and SAN are placed on tripods above around 1 [m] from ground, in order to mimic exposure evaluations representative of users. The required setup does not involve any electricity plug. This fact, coupled also with the overall small size of $E_1$-$E_5$ and $T_1$ (as shown in Fig. 4(a)), as well as the availability of a second backup battery for the SAN, allows easily repeating the measurements in different locations of the territory, and thus matching requirement $R_6$.

C. Algorithm Description

Fig. 5 provides a high level description of the measurement algorithm implemented in the 5G-EA framework. In more detail, we apply a divide-et-impera approach to split the complex measurement procedure into the following sub-problems: i) evaluation of RBS environmental exposure (step $P_1$), ii) evaluation of active traffic exposure from the smartphone (step $P_2$), iii) evaluation of active traffic exposure from the RBS (step $P_3$). In addition, the algorithm is complemented by three manual orientations $M_1$-$M_3$ of the directive antenna, which are instrumental to correctly separate RBS versus smartphone
Algorithm 1: Pseudo-Code of the Adjust_Ref_Level_Scale_Div Routine of $P_1$

**Input:** set of SAN settings, current frequency start $\text{curr}_f\_\text{min}$, current frequency stop $\text{curr}_f\_\text{max}$, safety margin for the ref. level $\text{safety}\_\text{margin}$, maximum time (in s) for searching the maximum level $\text{max}\_\text{time}\_\text{search}$, pre-amplifier state $\text{pre}\_\text{amp}\_\text{state}$, minimum level matrix $\text{min}\_\text{l}$, number of y ticks on the screen $y\_\text{ticks}$

**Output:** $\text{ref}\_\text{level}$, $\text{scale}\_\text{div}$

1. set_SAN(SAN\_settings);
2. max_l=-200;
3. for $i=1$ to $\text{max}\_\text{time}\_\text{search}$ do
   4. $\text{max}\_\text{l}=$max_level_search($\text{max}\_\text{l}$,$\text{curr}_f\_\text{min}$,$\text{curr}_f\_\text{max}$);
   5. sleep(1);
6. end for
7. $\text{ref}\_\text{level}=\text{ceil}(\text{max}\_\text{l})+\text{safety}\_\text{margin}$;
8. set_SAN($\text{ref}\_\text{level}$);
9. $\text{scale}\_\text{div}=\text{abs}(\text{ref}\_\text{level}-\text{min}\_\text{l}($\text{curr}_f\_\text{min}$,$\text{pre}\_\text{amp}\_\text{state}$))$/y\_\text{ticks}$;
10. set_SAN(scale\_div);

contributions. More concretely, the directive antenna is pointed towards the RBS before starting $P_1$ ($M_1$ block of Fig. 5), then it is pointed towards the smartphone before running $P_2$ ($M_2$ block), and finally it is pointed again towards the RBS before executing $P_3$ ($M_3$ block).

Intuitively, all the considered bands in use by the operator (TDD and DL FDD) are swept during the environmental exposure assessment of $P_1$. Then, the goal of $P_2$ is to restrict the set of monitored bands only on those ones in use by the current active traffic connection - which is kept alive from $P_2$ to $P_3$. In this way, the monitoring during $P_3$ is done on the same traffic conditions that are experienced in $P_2$.

In the following, we describe in more details steps $P_1$-$P_3$.

1) $P_1$ - Environmental RBS EMF: Fig. 6 shows the high level flowchart of $P_1$. Initially, the set of bands to be monitored are selected, based on the operator that is under consideration. For example, in the case of W3 operator all TDD and DL FDD bands shown in Fig. 2 are considered for the environmental assessment of RBS exposure. The algorithm then iterates over the set of bands. For each considered band, an automatic procedure to adjust reference level and scale division of the observed signal is implemented. Intuitively, the reference level is the upper limit of the $y$ axis in a spectrum plot (where the $x$ axis is the set of monitored frequencies), while the scale division allows tuning the unit of the $y$ ticks and consequently the lower limit on the $y$ axis. By jointly optimizing the reference level and the scale division, we can achieve a double goal: i) the signal that is being monitored can be qualitatively checked on the screen of the SAN, ii) the measurement resolution is tuned to the actual signal that is observed, and thus the impact of (possible) measurement uncertainties is limited.

More specifically, the adjustment of the reference level and scale division reported in the flowchart of Fig. 6 is sketched in the adjust_ref_level_scale_div routine of Algorithm 1. This function requires as input a set of basic SAN settings (whose values are going to be presented in detail in Section VI-B2), the starting and ending frequency for the considered band ($\text{curr}_f\_\text{min}$ and $\text{curr}_f\_\text{max}$), the $\text{safety}\_\text{margin}$ parameter that is used when setting the reference level, the $\text{max}\_\text{time}\_\text{search}$ parameter to govern the maximum time for searching the maximum reference level, the $\text{pre}\_\text{amp}\_\text{state}$ boolean variable storing the state of the SAN pre-amplifier (active or inactive), the $\text{min}\_\text{l}$ matrix including the values of the minimum sensed levels (which depend on the adopted frequency and the pre-amplifier state) and the $y\_\text{ticks}$ parameter representing the number of $y$ ticks on the SAN screen.

![Flowchart of the measurement algorithm](image)

The routine then proceeds as follows. The basic SAN settings are implemented in line 1, which include e.g., the detector type, the measured unit, and the trace detector. The maximum signal level $\text{max}\_\text{l}$ is initialized to a very low value in line 2. Then, a live searching of $\text{max}\_\text{l}$ is iteratively performed in lines 3-6, up to the maximum time $\text{max}\_\text{time}\_\text{search}$. At the end of this step, the maximum recorded signal level is stored in $\text{max}\_\text{l}$. The reference level $\text{ref}\_\text{level}$ is then set by adding to $\text{max}\_\text{l}$ the safety margin in line 7. In line 8, the resulting reference level is applied. In addition, the exact scale division, in order to entirely show the dynamics of the signal between $\text{ref}\_\text{level}$ and $\text{min}\_\text{l}$, is computed in line 9 and then applied to the SAN in line 10.

The execution of Algorithm 1 is then iterated up to a maximum number (iterator index in the flowchart of Fig. 6), in order to improve the setting of reference level and scale division. In the following step, a check on the pre-amplification is performed. If the current reference level is lower than a pre-amplification threshold, the signal can be pre-amplified by the SAN (right part of Fig. 6).<ref>Such feature is particularly useful for the environmental assessment of 5G signals, which are normally very low and close to the equipment noise level, due to a relatively low usage of 5G on such early phase of adoption. After turning on the pre-amplifier, the adjust_ref_level_scale_div </ref>

1Reference levels higher than the pre-amplification threshold may result into an Analog-to-Digital Converter (ADC) over-range after activating the pre-amplification of the signal. Therefore, this feature should be activated only for those signals whose reference level and dynamics are within the ADC limits.
Algorithm 2: Pseudo-Code of the Nar_Band_Meas Routine of P1, P2 and P3.

Input: set of basic SAN_settings, current frequency start curr_f_min, current frequency stop curr_f_max, number of samples n_samples, inter sample time (in s) int_sample_time
Output: Array of exposure values curr_exp in dBm/m²

1: set_SAN(SAN_settings);
2: for i=1:n_samples do
3:  curr_exp(i)=get_SA(curr_f_min,curr_f_max);
4:  sleep(int_sample_time);
5: end for

routine is called again, in order to adjust the amplified signal levels. However, this procedure may increase the reference level again above the maximum one allowed by the pre-amplifier. Consequently, a check on the pre-amplification threshold is done again. In case pre-amplification can be kept turned on, a further adjustment of reference level and scale division is done - and a further check on the pre-amplification is performed. In case pre-amplification is not supported, the pre-amplification is turned off, the reference level and scale division are reverted back to the last values before pre-amplification, and (eventually) a further call of the adjust_ref_level_scale_div routine is run.

After setting reference level and scale division (and eventual activation of pre-amplification), the signal is ready to be measured. To this aim, a narrow band measurement, expanded in Algorithm 2, is invoked. The function takes as input a set of basic SAN settings, the current frequency start curr_f_min and frequency stop curr_f_max, the number of sampled channel power measurements n_samples, and the inter-sample time int_sample_time. The routine then produces as output an array of exposure values curr_exp. The logic of the procedure is very simple: after setting the SAN parameters, a channel power computation function is iteratively invoked on the SAN. When all the samples are recorded, the algorithm returns the array of exposure measurements curr_exp. At the end of P1, the RBS environmental exposure is measured for the set of bands in use by the operator.

2) P2 - Active Traffic Smartphone EMF: The goal of the second part of the algorithm is to perform the assessment of the exposure generated by the smartphone upon active traffic generation. To this aim, the dual 4G/5G connectivity and carrier aggregation features suggest that multiple bands (unknown a-priori) can be used in parallel for the data transfer. On the other hand, measuring the exposure on the entire set of bands in use by the operator may result in a waste of resources, in terms of: i) overly increase of time to perform the assessment, ii) waste of consumption of the SAN battery (which is a precious resource) and iii) excessive traffic consumption on the smartphone (which may be critical for limited data traffic plans). To face such issues altogether, P2 adopts the following intuition. First, the TDD and UL FDD bands in use by the data transfer are detected. Then, the exposure assessment is done only on the selected subset of spectrum portions currently in use.
The algorithm then produces as output the subset of bands \texttt{sel_band_array} that are detected for the current data transfer. The logic of the function is quite simple: for each considered frequency, the sample in \texttt{emf_array_2nd_span} is compared against the corresponding one \texttt{emf_array_1st_span}, by computing the percentage variation of EMF. If such variation is greater than the \texttt{thre_inc} parameter, the band is included in the list of spectrum portions that are monitored for the current data transfer. The intuition here is in fact to exploit the increase of EMF as a result of the usage of specific bands in the UL. In case the current selected band employs FDD, then the corresponding one in the DL is also included in the list of selected ones. For example, let us assume that the 1745-1765 [MHz] band of Fig. 2 is detected in the UL. This portion of the spectrum belongs to the B3 FDD band, which also includes the 1840-1860 [MHz] band for the DL. This second portion will be likely used when evaluating the active traffic from the RBS, and therefore it is included in the list of bands to be monitored - when considering RBS active traffic exposure. At the end of the algorithm the array \texttt{sel_band_array} stores the list of band indexes in use for the current data transfer.

Coming back to the flowchart of Fig. 7, the blocks on the right details the steps for the EMF assessment on the selected set of bands. In particular, the initial band is selected - the index in \texttt{sel_band_array} with lowest frequency and belonging to UL. Then, the narrow-band EMF measurement on the selected band is performed. The logic is in common with the exposure measurement of P1, and sketched in Algorithm 2. In particular, the main differences rely on a different set of basic SAN settings and on a different measurement metric (in terms of V/m). Once the measurement has been completed for the current band, P2 passes to the next one, until all the TDD and UL FDD bands in \texttt{sel_band_array} are considered (band index in Fig. 7). At the end of P2, a set of exposure arrays, one for each considered band, is available.

3) P3 - Active Traffic RBS EMF: The last part of our measurement technique involves the assessment of RBS exposure while keeping active the current data transfer. Fig. 8 highlights the main blocks that realize this functionality. The logic is very similar to the smartphone assessment, except for the following differences: i) the evaluation include TDD and FDD DL bands (with the directive antenna pointed towards the RBS), ii) the smartphone traffic is turned off after completing the scan over the considered band. Similarly to P2, a set of exposure arrays is available at the end of the procedure.

D. Implementation Details

We implement P1-P2-P3 parts of 5G-EA framework as a set of scripts written in Matlab - except from the traffic generation, which is governed by the \texttt{Iperf} program running on the smartphone and dedicated server. An unique aspect of our framework is the implementation of the measurement algorithm in software, on a general purpose machine that controls the SAN. This is another innovation brought by our work, which opens the way for possible future investigation in the softwarization of EMF assessments.

![Algorithm 3: Pseudo-Code of the Sel_Band_Use Routine of P2.](image-url)

To this aim, Fig. 7 sketches the main operations performed during P2. Initially, a wide span assessment is done, in order to detect the peak(s) of the sensed signals on a very large range of frequencies (including all the ones in use by the operator under investigation). The goal of this scan is not to measure exposure, but rather to get a quick indication on the frequencies that carry most of signal power before injecting any traffic. In the following step, the active traffic is generated towards the smartphone, by executing the \texttt{Iperf} program. Then, a second wide span assessment is done. The detection of the subset of 4G/5G bands in use for the data transfer is done by comparing the peaks recorded during the first scan versus the ones observed on the second one.

The detection of the 4G/5G bands is expanded in Algorithm 3. The routine takes as input the \texttt{emf_array_1st_span} array of EMF values (indexed by frequency) that were sensed during the first span, the \texttt{emf_array_2nd_span} array of EMF values that were sensed during the second span, and a threshold increase parameter \texttt{thre_inc} (in \%) to activate the detection.
More technically, the high level functionalities reported in \(P1-P2-P3\) are translated into a set of basic operations, coded as low-level Standard Commands for Programmable Instruments (SCPI) and transferred from/to the SAN through a Transmission Control Protocol (TCP) connection. The output of the SAN (e.g., the array including the exposure values) are then sent back over the same connection in SCPI format. In this way, the process is completely automated and the post-analysis of the obtained data can be done directly in Matlab - in the same script running the measurement algorithm.

VI. RESULTS

We present our outcomes through the following steps: i) description of evaluation scenarios, ii) parameter settings of 5G-EA framework, iii) exposure assessments.

A. Evaluation Scenarios

We consider a set of measurement points in the coverage area of the W3 roof-top installation shown in Fig. 3, with the frequency assignment reported in Fig. 2. The installation is located in the area close the University of Rome Tor Vergata in Rome (Italy). More concretely, we perform our experiments in both outdoor and indoor locations, due to the following reasons. First, we aim at massively performing measurements under different propagation conditions, which are obviously influenced by terrain parameters like the distance from the RBS, the level of urbanization around the measurement point and the presence of buildings/obstacles on the path towards the RBS. Second, we exploit the indoor locations to perform detailed and in-depth measurements, with the goal of corroborating the results from the outdoor locations with tests covering e.g., sensitivity analysis of the exposure versus variation key parameters, such as throughput, distance from the smartphone, and smartphone orientation.

Focusing on the outdoor tests, Fig. 9 reports a 3D map of the measurement locations. In total, 26 measurement locations are selected for the tests, based on the following criteria: i) spreading the tests over the territory around the W3 tower, and ii) finding locations that are suitable for placing the instruments (e.g., avoid private streets, locations in close proximity to each other, etc.). The 3D distance of each measurement location from the RBS varies between a minimum of 124 [m] up to a maximum of 1134 [m],\(^2\) in order to capture a wide set of exposure conditions. In addition, the measurement points are placed in the coverage area of each W3 sector shown in Fig. 3, in order to further strengthen our analysis. We refer the reader to Appendix A, which can be found on the Computer Society Digital Library at http://doi.ieeecomputersociety.org/10.1109/TMC.2023.3252662, which provides detailed information about: i) radio configuration of the W3 installation under consideration, ii) other RBSs in the surroundings of the considered area, iii) taxonomy of outdoor locations, iv) measurement time.

To give more insights, Fig. 10 reports two representative examples of outdoor measurement points. When considering LOS locations (Fig. 10(a)), the RBS is visible from the measurement point. On the contrary, the installation is not visible in NLOS locations (Fig. 10(b)). In both cases, the directive antenna is pointed towards the RBS location during operations \(M1\) and \(M3\).

\(^2\)The percentage difference between ground (2D) distance and 3D one is always smaller than 2%. Consequently, both distances almost overlap.
Focusing then on the indoor tests, we consider two locations at the Engineering building of the University, shown in Fig. 11(a). In particular, we consider a LOS location at the fourth floor and a NLOS one at the second one. The room hosting the LOS measurements is shown in Fig. 11(b). In addition, the environment hosting the NLOS tests is identical to the LOS one (not shown due to the lack of space). Interestingly, the walls are made of thin concrete pillars and big glasses that are mounted on small metallic frames. This structure provides in general good penetration of outdoor mobile signals inside the building. The window view from both locations is shown in Fig. 11(c) and (d).

Focusing on the LOS environment, the path towards the RBS is free from obstacles and the distance is within the RBS coverage area. Focusing instead on the NLOS location, the distance from the RBS is identical to the LOS one, but, obviously, the RBS sight is obstructed by a building, which forces the signal to follow a NLOS path.

B. Parameters Settings

We provide hereafter the settings of the main parameters of 5G-EA framework. In particular, we shed light on the measurement antenna positioning and the algorithm parameters in $P_1$, $P_2$, and $P_3$, respectively. We refer the reader to Appendix B, available in the online supplemental material for more insights about calibration and uncertainty aspects of the measurement chain.

1) MEASUREMENT ANTENNA PLACEMENT: 5G-EA requires a careful orientation and positioning of the measurement antenna, in order to properly dissect RBS versus smartphone exposure. Focusing on $M_1$ and $M_3$, the antenna is simply pointed towards the RBS location. Focusing on $M_2$, the antenna is pointed towards the smartphone. As already shown in Table II, the far-field distance $D_{FF}$ has to be enforced in our experiments, in order to avoid near-field effects. On the other hand, the distance should mimic the actual exposure conditions to the head/chest that is experienced by a typical user. Therefore, there is a trade-off between the (small) distance for a meaningful assessment and the (relatively large) distance that has to be enforced to preserve far-field conditions. In this work, we have found that a good compromise among such competing goals can be achieved by setting a distance from the smartphone equal to 0.25 [m]. Although this number may apparently violate the far-field conditions for the 800 [MHz] and 900 [MHz] bands (as shown in Table II), in practice we have found that such bands are not used for 4G data transfers.

To corroborate the previous outcome, Fig. 12 reports the occurrence of bands that are used for the data transfers in the outdoor locations of our experiments. Interestingly, most of transfers employ 4G bands at around 2600 [MHz], while the 1800 [MHz] band is seldom used. On the other hand, the 800 [MHz] and 900 [MHz] bands are not used by the data transfers. Eventually, all the three 5G bands at 3.4-3.6 [GHz] are almost equally adopted. In this way, the minimum frequency used for the exposure assessment can be assumed to be the 1800 [MHz], band. Therefore, the distance of 0.25 [m] is sufficiently large to provide far-field conditions.
2) P1 Parameters: Table III reports the parameters of the adjust_ref_level_scale_div function. In more detail, the upper part of the table expands the basic SAN parameters. In particular, we adopt a rolling max type detector, as our goal here is to first sense the maximum signal levels and then adjust accordingly reference level and scale division. Focusing on the other routine parameters (bottom part of the table), the values of curr_f_min and curr_f_max are taken from Fig. 2, by considering the W3 bands over FDD DL and TDD - since the exposure from RBS is the target of P1. In addition, the pre-amplifier state (on/off) is governed by the logic reported in Fig. 6. Obviously, the pre-amplifier is inactive when the first call of adjust_ref_level_scale_div is run (left part of Fig. 6). However, in case the pre-amplification management branch is followed (right part of Fig. 6), the pre_amp_state state that is passed to adjust_ref_level_scale_div may be active.

Focusing on the remaining parameters of adjust_ref_level_scale_div, the min_1 matrix is reported in Table IV. The values reported in the table are retrieved by visualizing the noise level on the SAN in each considered band. Clearly, when the pre-amplifier is turned on, the noise level can be notably reduced (right part of the table). Moreover, the pre_amp_thre threshold, which is used in the decision block of Fig. 6 to compare the reference level and activate/deactivate the pre-amplification, is set to -48.77 dBm/m² - an empirical value that was tested to correctly work on all the considered bands. Finally, the maximum time for searching the signal peak over the considered band is set to 5 [s], while the number of y ticks is set to y_ticks=10. In this way, the time required to run a single call of adjust_ref_level_scale_div is at least equal to 5 [s].

Table V reports the parameters for the nar_band_meas function. Focusing on the P1 settings (central column), the set of SAN_parameters this time includes a rolling average as type detector, as our primary goal during this step is to perform an exposure assessment over the considered signal. This setting is inline with relevant measurement standards in the field (see e.g., [39]). In addition, the number of samples for computing the average is set to 100, in order to consider a meaningful range. Clearly, the reference level and the scale division are updated by the logic implemented in Fig. 6. Focusing then on the remaining parameters, curr_f_min and curr_f_max are set in accordance to the set of W3 bands shown in Fig. 2 (restricted to FDD DL and TDD). Finally, the number of narrow band measurements n_samples is set to 12, while the time between consecutive queries of narrow band measurements is set to 0.5 [s]. In this way, the measurement time for each band is approximately equal to 12 × 0.5 [s] = 6 [s].

Finally, we shed light on the remaining parameters that appear in Fig. 6. Focusing on the maximum number of iterations for running the adjust_ref_level_scale_div function, we set it to 3 - a value that provides a good balance between overall duration of detection phase and precision in setting reference level and scale division values. Focusing on the number of bands to be monitored, we set it to 9, in accordance to the FDD DL and TDD bands of W3 shown in Fig. 2. With such settings, the required time to run P1 is at least equal to (5 [s] × 3 + 6 [s]) × 9 = 189 [s]. However, the actual total time for running P1 may be higher, due to the following reasons: i) the additional delay that is required when communicating with the SAN and ii) the eventual activation of the power amplifier, which requires further calls of the adjust_ref_level_scale_div routine.

3) P2 Parameters: We initially consider the parameters of the wide span measurement blocks reported in Fig. 7, detailed in Table VI. More in depth, most of SAN parameters are set to the default values (i.e., automatic setting). Focusing on the remaining parameters, the selected frequencies cover all the ones in use by W3 operator. In addition, the pre-amplifier is
powered off, as the exposure from the smartphone may be potentially higher than the maximum supported signal level with pre-amplification turned on - which we remind is a very effective feature to distinguish low signals w.r.t. noise level. Moreover, the reference level is set to a large value (6 [V/m]) in order to detect possible signal peaks. Focusing on the trace detector, a root mean square (RMS) setting is imposed (in line with $P_1$).

Eventually, the max detector is used, as we remind that the scope of the wide span measurement is to perform a quick scan over the entire frequency range and to detect the signal peaks.

The second block of $P_2$ is the activation of the smartphone traffic exposure. Unless otherwise specified, the $iperf$ client is run on the smartphone with the following parameters: i) IP address and port corresponding to the $iperf$ server installed at the University, ii) bandwidth report interval set to 1 [s], iii) number of simultaneous connections per data transfer set to 1, iv) maximum duration of $iperf$ transfer set to 120 [s] - an amount of time sufficiently large to complete the remaining steps in $P_2$ and $P_3$.

In the following, we focus on the parameters for selecting the 4G/5G bands in use by the data transfer (expanded in the $sel_band_use$ routine of Table 3). Obviously, the array of EMF measurements are set by the first and second wide span assessment. The array of frequency values $freq_array$ includes all the frequencies in use by W3 operator. Finally, the threshold increase parameter $thre_inc$ is set to 30% - a value that guarantees a good balance between (artificial) increase of EMF due to injection of traffic from the smartphone and (natural) variation of exposure due to other effects (e.g., nearby terminals, signal fading, etc.).

Eventually, the band index in Fig. 7 is initialized with the first UL bandwidth in which an increase of exposure was detected by the $sel_band_use$ routine. Finally, the narrow band EMF measurements is realized through the $nar_band_meas$ of Algorithm 2, whose parameters for $P_2$ are detailed in Table V on the right. The main difference w.r.t. $P_1$ case relies on a different measurement metric, expressed in terms of [V/m]. In addition, the reference level set to 6 [V/m], since the measured signal levels are expected to be non-negligible. It is interesting to note that, when the [V/m] metric is set, the scale div are automatically tuned to show a minimum level of 0 [V/m], i.e., the minimum one. Eventually, the minimum and maximum frequency are set

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**Fig. 13.** Characterization of exposure (top) and throughput (bottom) over the outdoor evaluation points. The points are ordered from left to right by increasing distance values with respect to the 5G W3 installation. The sight condition (L=Line-of-Sight, N=Non-Line-Of-Sight) is also reported.
in accordance to the considered bandwidth, whose set is saved in the sel_band_array by the sel_band_use routine.

4) P3 Parameters: Focusing on the P3 assessment shown in Fig. 8, the initial band index is set with the first DL bandwidth of W3 in use by the data transfer (detected by sel_band_use function). The narrow band assessment reported in the second block of P3 adopts the same parameters of P2 (detailed in Table V on the right). Finally, the iperf transfer is turned off on the smartphone when all the bands in use have been considered.

C. Exposure Assessments

We initially concentrate on the outcomes from outdoor measurements of Fig. 9 and then we shed light on the results obtained in the indoor locations of Fig. 11.

1) Outdoor Measurements: We run 5G-EA over the outdoor locations, by considering the generation of UL traffic from the smartphone to the iperf server. Fig. 13 reports the breakdown of exposure (top) and throughput (bottom). The exposure is expressed in terms of power density [W/m²], in order to display the different contributions (RBS versus smartphone, active versus environmental, pre-5G versus 5G) over a stacked bar. Each exposure component is expressed in terms of average value over the collected samples. Moreover, the error bars report the confidence intervals, which are computed by assuming a Gaussian distribution with a confidence level of 95%.

We initially focus on the collected exposure values, shown in Fig. 13(a). Several considerations hold by analyzing in detail the figure. First, the active traffic exposure from the smartphone (pre-5G and 5G) dominates over all the other ones, in all the considered locations. Second, the RBS environmental exposure can be identified for all locations in LOS w.r.t. the RBS, while the same metric is negligible for all locations in NLOS. Third, the contribution of active traffic exposure from the RBS is almost imperceptible in all locations (except from two). Fourth, the majority of active traffic exposure from the smartphone is due to pre-5G contributions (mostly 4G), while 5G always represents a small share (at most equal to 38%) compared to the total one that is radiated by the smartphone. Fifth, NLOS locations generally present higher level of 5G exposure than LOS ones. Sixth, the increase of distance generally results in an increase of exposure (left to right of the figure). However, the largest exposure variations are observed between LOS and NLOS evaluation points. In particular, the latters exhibit a strong increase of active traffic exposure from the smartphone compared to the formers. As a side comment, the measured exposure levels are always orders of magnitude lower than the whole body and localized maximum power density values of ICNIRP guidelines [6].

In the following step, we compare the exposure of Fig. 13(a) against the achieved throughput levels shown in Fig. 13(b). Interestingly, a strong variation in the throughput levels is observed. We argue that this phenomenon is due to the different propagation conditions that are experienced in the measurement locations. To substantiate such observation, Fig. 13(a) highlights the three locations exhibiting the lowest exposure and the other three ones providing the highest exposure levels. Interestingly, the formers are in LOS, while the latters experience NLOS. When considering the throughput metric for the same locations (Fig. 13(b)), we can note that locations with lowest exposure (LOS) achieve very large throughput levels, typically larger than 45 [Mbps] in the UL, while the opposite holds for locations experiencing the highest exposure levels (NLOS), being the observed throughput lower than 16 [Mbps]. Consequently, NLOS conditions are reflected into an increase of smartphone exposure and a degradation of throughput levels compared to LOS ones.\(^3\)

To provide more insights, Fig. 14(a) reports the percentage of active traffic exposure from the smartphone (w.r.t. the total one) versus the observed throughput level. Each point in the figure corresponds to a measurement location (distinguished between LOS and NLOS), while x-y error bars are computed by assuming again 95% of confidence levels. Interestingly, we can note that the percentage of smartphone exposure is huge (close to 100%) for all the NLOS measurement locations. On the contrary, the percentage of smartphone exposure tends to decrease to lower levels for the LOS measurement locations. Moreover, a decrease is also observed when the realized UL throughput increases. In all the cases, however, the active traffic exposure from the

\(^3\)We refer the interested reader to Appendix C, available in the online supplemental material for more speculations about the variations of exposure for smaller distances than the minimum one considered in this work.
Having understood that there may be a strong relationship between the realized UL throughput and the collected exposure levels, we compute a novel metric, called smartphone exposure-per-Mbps, which is obtained by dividing the total exposure measured in the location by the observed throughput. The metric expresses the efficiency in terms of exposure (in [V/m]) for delivering a given amount of information (in [Mbps]). When the exposure-per-Mbps is high, the system is largely inefficient, as a huge exposure is needed to transfer the information. On the contrary, when the exposure-per-Mbps is low, the efficiency of the system in delivering the same amount of information is improved.

Fig. 14(b) reports the smartphone exposure-per-Mbps versus the observed throughput levels. Interestingly, the exposure-per-Mbps is inversely proportional to the throughput levels. The higher is the throughput, the flatter and closer to zero is the observed smartphone exposure-per-Mbps. On the contrary, the lower is the throughput, the higher is the asymptotic behavior of the exposure-per-Mbps, with the highest values observed for the lowest throughput levels. To better capture the aforementioned effects, we have applied the following double exponential fitting model:

\[ C^{\text{EST}} = F_1 \cdot e^{E_1 \cdot T^{UL}} + F_2 \cdot e^{E_2 \cdot T^{UL}} \]  

(2)

where \( T^{UL} \) is the observed throughput level (in Mbps), \( F_1, E_1, F_2, E_2 \) are the fitting parameters (shown in Table VII) and \( C^{\text{EST}} \) is the estimated smartphone exposure-per-Mbps.

By observing in detail Fig. 14(b) we can note that the realized UL throughput with \texttt{iPerf} tool can be used as an estimator of the smartphone exposure. In a practical scenario, the user could measure \( T^{UL} \) by running an \texttt{iPerf} test in the UL direction and a given location. Then, the smartphone exposure could be retrieved by:  

\( i) \) applying the fitting model of (2) to compute
2) Indoor Measurements: In the following part of our work, we extend the results of the outdoor locations by investigating the exposure in the LOS/NLOS indoor locations. In particular, the availability of controlled environments allows performing extensive tests, in order to deeply analyze the impact of key parameters on the exposure levels. To this aim, we initially focus on the impact of UL versus DL traffic generation. For each location, we perform a wide range of UL and DL tests, including the variation of the generated traffic from very low values (set to 5 [Mbps]) up to the maximum one reachable on the wireless link (several dozens of Mbps). Moreover, three independent runs are executed for each parameter setting, in order to strengthen our outcomes.

Fig. 15 reports the breakdown of the exposure components for the considered tests. Four considerations hold by analyzing the figure. First, the exposure generated by the smartphone on pre-5G technologies dominates over the other components, both in the DL and in the UL. Second, the exposure in the DL is almost one order of magnitude lower than the one recorded in the UL tests. This is due to the fact that DL tests generate most of traffic flows from the Iperf server to the client, while a very low amount of information flows on the inverse direction (e.g., segment acknowledgements and/or control information). Third, the exposure tends to increase when the UL throughput is increased. Fourth, the exposure tends to be higher in the NLOS location than the LOS one, for a given level of generated traffic.

To better substantiate the previous findings, Fig. 16(a) details the total EMF versus throughput over the two indoor locations. Interestingly, a strong increase of exposure is recorded when the UL traffic is increased, easily reaching values greater than 1 [V/m] (top part of the figure). Moreover, the difference between NLOS and LOS exposure tends to increase with increasing UL throughput. At last, when Iperf is set to generate the maximum traffic, the UL throughput in the NLOS location is clearly lower than the LOS one - despite the fact that the exposure values are comparable in both locations. A similar behaviour is also observed for the maximum traffic in the DL direction (bottom part of the figure). However, the increase of exposure due to traffic rising is less evident than in UL tests.

Eventually, Fig. 16(b) reports the total exposure-per-Mbps versus throughput for the two locations and the UL/DL tests. Astonishingly, the inversely proportional law between exposure-per-Mbps and throughput clearly emerges in each location and in each direction. Given a location, the total exposure-per-Mbps is lower for the DL tests compared to the UL ones. Moreover, given a direction of traffic generation, the total exposure-per-Mbps in NLOS tends to be higher than the one recorded in the LOS condition.

In the final part of our work, we evaluate the impact of changing the orientation and relative positioning of the smartphone. Fig. 17(a) reports the exposure breakdown for each smartphone orientation setting reported on the bottom of the page.
figure, corresponding to a smartphone rotation of 0°, 90°, 270° in clockwise direction of the horizontal plane. For each angle, we perform three independent assessment with the maximum UL traffic. Interestingly, the dominance of smartphone exposure is evident in all the experiments. However, the 270° rotation generally results in an higher exposure from the smartphone than the other angles. We argue that this phenomenon is due to the positioning of the smartphone main antenna on bottom right part the smartphone - opposite to the RBS when an angle of 270° is set, which results in worse propagation conditions than the other settings.

Finally, we analyze the impact of increasing the distance of the exposure evaluation point w.r.t the smartphone, as shown in Fig. 17(b). Starting from the default value of 0.25 [m], we increase the distance up to 1 [m]. As expected, the exposure experiences a sharp decrease when the distance is increased. However, we point out that the smartphone exposure is still the dominant component even when the distance is set to the maximum value of 1 [m].

VII. CONCLUSIONS AND FUTURE WORK

We have investigated the problem of exposure assessment in a commercial 5G network, by evaluating the impact of user generated traffic on the exposure from the RBS and the smartphone. To solve the complex and innovative measurement requirements - which include several aspects related to 5G implementation and its inter-viewing with legacy 4G networks - we have designed an innovative framework, called 5G-EA. Our framework splits the complex problem into a set of procedures, which are tailored to a specific measurement goal (environmental versus active traffic assessment). In addition, 5G-EA relies on a completely softwareized approach, in which the measurement algorithm is run on a general purpose machine that controls the programmable spectrum analyzer.

We have then performed an extensive set of assessments in both outdoor and indoor locations. Interestingly, our results demonstrate that the smartphone contribution largely dominates over the other exposure components, particularly when UL traffic is injected. However, the largest contribution is due to pre-5G technologies, while 5G always constitute a small share (up to 38%) out of the total one that is radiated by the smartphone. In addition, the total exposure dramatically decreases when outdoor LOS conditions are experienced, and in general when the exposure from the RBS becomes detectable by the SAN. Moreover, we have designed and evaluated an exposure estimator based on the maximum UL traffic that is achieved by iPerf in the measurement location. Eventually, the exposure tends to increase in indoor locations when passing from LOS to NLOS condition, for a given level of UL traffic that is set towards the smartphone. Finally, we have demonstrated that the measured exposure levels are influenced by key parameters, like DL versus UL direction, smartphone orientation and relative distance of the smartphone w.r.t. the measurement antenna.

We believe that our work paves the way for future research in the field. First, the application of 5G-EA in other deployments (e.g., subject to different exposure regulations and/or different radio configurations) is an interesting step. Second, the evaluation of exposure should be extended by considering multiple UE models/types, locations in balconies/terraces in close proximity to the serving RBS, and additional sources like WiFi. Third, the assessment of exposure in 5G deployments including mmWave frequencies is another line of research. Fourth, we plan to perform extensive assessment by running commonly used smartphone applications (social media, video streaming, online conference, etc.). Fifth, the decrease of exposure observed in LOS locations suggest that deploying a dense 5G network, in which most of territory is in LOS w.r.t the serving RBS, is the best solution to reduce the exposure from the terminals. This goal could be alternatively achieved by installing intelligent surfaces (active or passive), to improve the signal coverage over the territory. The evaluation of exposure in such innovative deployments is therefore a future activity.

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