Ballistic Bunching of Photo-Injected Electron Bunches with Dielectric-Lined Waveguides

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We describe a simple technique to passively bunch non-ultrarelativistics (\(\lesssim 10\) MeV) electron bunches produced in conventional photoinjectors. The scheme employs a dielectric-lined waveguide located downstream of the electron source to impress an energy modulation on a picosecond bunch. The energy modulation is then converted into a density modulation via ballistic bunching. The method is shown to support the generation of sub-picosecond bunch train with multi-kA peak currents. The relatively simple technique is expected to find applications in compact, accelerator-based, light sources and advanced beam-driven accelerator methods.

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I. INTRODUCTION

Low-energy (\(\lesssim 10\) MeV) electron beams are conventionally produced in photoemission electron sources based on radio frequency (RF) guns or “photoinjectors”. The final bunch length downstream of a photoinjector is dictated by the initial parameters including the photocathode-laser duration, transverse spot size and the electric-field amplitude in the gun cavity and its phase relative to the laser. Typically, bunch lengths on the order of picoseconds are commonly produced in L- and S-bands RF guns. Shortening these bunches or producing trains of sub-ps microbunches is appealing to a variety of applications including ultra-fast electron diffraction [1, 2], coherent accelerator-based, e.g., THz light sources [3, 4], and injectors for short-wavelength advanced-accelerator concepts [5, 6].

To date, bunch compression to produce kA peak current is often realized after acceleration to \(\gtrsim 100\) MeV by employing dispersive sections arranged as, e.g., magnetic chicanes [7]. Alternative methods to shorten a relativistic bunch also include velocity bunching [8–11], and ballistic bunching using an accelerating cavity operating at zero crossing. The latter method demonstrated bunching at the sub-100-fs time scale [12] and could possibly produce shorter temporal structures [13]. Similar methods have been extended to the mm-wave regime, e.g., by coupling laser-produced THz pulses to the beam using undulators [14] or dielectric waveguides [15].

In addition, several techniques have demonstrated narrow-band THz radiation generation with photoinjector beams by coupling a density-modulated bunch with electromagnetic-radiation mechanisms [16–20]. Among these techniques, two of them are based on impressing a density modulation using a temporally-modulated photocathode-laser pulse [19–21]. The use of such a modulated laser was also experimentally shown to support the formation of short-current spikes via wave breaking seeded by non-linear longitudinal space-charge effects [22].

Most recently, a technique to produce train of microbunches based on a dielectric-lined waveguide (DLW) was realized in a \(\sim 70\)-MeV accelerator [23]. In the latter experiment a density modulation was produced using a small chicane to provide the longitudinal dispersion necessary to convert the energy modulation imparted by the beam self-interaction with its short-range wakefield in the DLW structure.

In this paper, we propose a simple method extending the mechanism proposed in Ref. [23] to low-energy beams. In our configuration a \(\sim 5\text{-}10\) MeV ps-duration beam is energy-modulated as it passes through a DLW structure and ballistically bunched in a subsequent drift. Our approach is similar to the bunching technique commonly used in klystrons [24, 25]. Owing to the low intrinsic energy spread typically achieved in photoinjectors, final beam currents in excess of kA’s can be produced.

II. BALLISTIC COMPRESSION FROM WAVEFIELD-INDUCED ENERGY MODULATIONS

A feature critical to the production of density modulated beams is the capability to produce the required large local longitudinal-phase-space (LPS) chirps via the self-wakefield in the considered DLW structure. We investigate this point with a cylindrically-symmetric DLW consisting of a hollow dielectric cylinder with inner and outer radii \(a\) and \(b\) [26], and relative electric permittivity \(\varepsilon_r\). The outer surface of the dielectric is metalized. We consider the axial longitudinal wakefunction modes supported by such a structure to be of the form [27, 28]

\[ w_{z,m}(\zeta) = \kappa_m \cos(k_m \zeta), \]

where \(\zeta\) is the position of the observer charge referenced with respect to the source electron and \(\kappa_m\) (with units
of $V/m/C$ and $k_m$ are respectively the loss factor and wave vector associated to the $m$ mode supported by the DLW structure. The mode parameters $\kappa_m$ and $k_m$ are obtained following the methodology described in Ref. [26] by numerically solving the dispersion equation.

An example of computed Green’s function for a structure with parameter $a = 400 \mu m$, $b = 450 \mu m$, and $\varepsilon_r = 5.7$ (corresponding to diamond) appears in Fig. 1. The Green’s function converges after inclusion of 4 modes (the 50-\mu m thickness of the structure supports multiple modes with significant axial fields).

Note that the field in Eq. 1 and the wake function have no dependence on the transverse coordinates. The expected change in longitudinal momentum for a particle within and behind a bunch with line-charge distribution $\Lambda(z)$ is obtained from the convolution integral

$$\Delta E(z) \simeq \sum_{m=1}^{\infty} E \{\sin[k_m(z + a)] - k_m a \cos[k_m(z + a)] + k_m z\},$$

where $L_{dlw}$ is the length of the DLW structure and $z$ the longitudinal coordinate within the bunch.

In contrast with an energy modulation imparted by external fields (e.g. from lasers or RF cavities), the modulation imparted via wakefield depends on the bunch shape. In particular, given the selected parameters for the DLW structure, one should ideally select an electron-bunch distribution with spectral contents capable of exciting the mode(s) supported by the structure; see Fig. 2. Reference [23] utilizes a relativistic bunch shape with linearly-ramped current profile as the associated energy modulation was shown to exhibit a uniform-amplitude modulation throughout the bunch.

In order to illustrate the proposed concept we elaborate a simple model based on the ideal case of a line-charge electron bunch with a parabolic charge-density profile $\Lambda(z) = [3Q/(a^2)](a^2 - z^2)$ where $Q$ is the total bunch charge and $a$ the half width of the distribution; see Fig. 3(a). The corresponding change in energy along the bunch is given by

$$\Delta E(z) \simeq \frac{Q}{k_1 L_{dlw} \sin(k_1 a)},$$

where $E_i$ is the bunch’s initial mean energy, $z_f = z_1$, and $\sin(x) \equiv \sin(x)/x$ is the usual “sampling function”.

After a section with longitudinal dispersion $R_{06}$, the energy modulation induces a density modulation and the final longitudinal coordinate of an electron is mapped as $z_d = z_f + R_{06} \delta_f$ under a linear single-particle dynamics approximation.

We first consider the case when the root-mean-square (rms) bunch length satisfies $\sigma_{z,i} \equiv \langle z_i^2 \rangle^{1/2} = a/\sqrt{5} \gtrsim \lambda_1 \equiv 2\pi/k_1$ so that an energy modulation along the bunch can be impressed; Fig. 3(b, red trace). In such
The microbunches’ separation is \( \Delta \) rms fractional momentum spread. is approximately given by \( \sigma \)

The characteristic length of the microbunches formed the local LPS correlation is given by \( z \)

The denominator is negligible. The maximum bunching where we have further assumed that the sinc(\( k_1a \)) in the denominator is negligible. The maximum bunching occurs at these zero-crossing points when the following beamline provides a longitudinal dispersion \( R_{56} \equiv -\frac{1}{\gamma} \). The characteristic length of the microbunches formed is approximately given by \( \sigma_z \simeq R_{56} \delta \) where \( \delta \) is the uncorrelated (or slice) rms fractional momentum spread. The microbunches’ separation is \( \Delta z \equiv z_{f,n}-z_{f,n-1} \approx \lambda_1 \) for an incoming beam with vanishing correlated energy spread upstream of the DLW structure.

At relativistic energies, the longitudinal dispersion \( R_{56} \) necessary to form the microbunches is often provided by a dispersive section, e.g., a bunch-compressor chicane [7] as accomplished in Ref. [23]. Here we note that at energies below \( \sim 10 \text{ MeV} \) (non-ultra-relativistic regime), the large LPS slope resulting from the large axial fields supported in a DLW requires a relatively small \( R_{56} \) that can be readily produced by a drift space. A drift with length \( D \) has a longitudinal dispersion

\[
R_{56} \simeq -\frac{D}{\gamma^2},
\]

where \( \gamma \) is the bunch’s Lorentz factor and we take \( \beta = (1 - 1/\gamma^2)^{1/2} \approx 1 \) for simplicity.

![FIG. 3. Charge distributions (a) and corresponding wake potential (b) for two cases of ratio between the rms bunch length \( \sigma_z \) and fundamental-mode wavelength \( \lambda_1 \). The DLW structure parameters are identical to one used in Fig. 1. The head of the bunch corresponds to \( z \leq 0 \). The wake potential associated to the \( \sigma_z = 0.5\lambda_1 \) case is scaled by a factor 50 for clarity.](image-url)

Practically, for a \( \sim 5\text{-MeV} \) electron bunch passing through a 10-cm long DLW structure capable of supporting \( \sim 0.5 \text{ MV/m} \) peak field a “local” chirp \( C \approx 10^5 \text{ m}^{-1} \) can be obtained for a 0.5-mm modulation wavelength. The corresponding local density spike could form via ballistic bunching after a drift of length below \( D \leq 1 \text{ m} \). The expected modulation amplitude \( \sim 0.5 \text{ MeV} \) is much larger than the typical uncorrelated energy spread of a few keV routinely achieved in RF guns [33, 34]. Additionally, the relatively low \( R_{56} \) and small uncorrelated energy spread are also beneficial to the production of very short (< 100-fs) density spikes. This simple estimate motivates further investigation of the scheme using a bunch generated by a conventional photoemission electron gun.

In addition, furthering our point about the dependence of the energy modulation on bunch parameters we now examine the case when the rms bunch length fulfills \( \sigma_z \simeq \lambda_1/2 \); see Fig. 3(b, blue trace). In this regime, the induced energy change along the bunch produced an energy depression between the head and tail of the bunch. The produced correlation between the depleted energy location and tail has the proper sign to be compressed via ballistic bunching. Although the introduced chirp is nonlinear, it eventually can lead to the production of high-peak-current spikes. This approach however only bunches a fraction of the bunch and actually debunch the beam within the front of the bunch. Despite this drawback, this scheme is appealing given its simplicity and absence of need for a precisely synchronized external field as used in ballistic bunching using a buncher cavity [12]. This passive bunching method is therefore inherently self synchronized and in principle not subject to time jitter (the main source of jitter is associated to charge fluctuations that impact the imparted energy modulation and could consequently result in shot-to-shot fluctuation of the peak-current value).

Finally, it should be pointed out that higher-order, e.g., dipole, modes can also affect the bunch transverse dynamics but are neglected in the present treatment as we assume the bunch is cylindrical-symmetric and is centered on the DLW axis. Given the short length of the DLW considered in the remainder of the paper, possible detrimental effects on the transverse beam dynamics can be practically corrected, e.g., by mounting the DLW structure on translational stages.
III. NUMERICAL MODELING AND ANALYSIS

To explore the possibilities discussed in the previous section we perform beam-dynamics simulations. The numerical simulations are carried with the beam-dynamics program Astra [35] which takes into account space-charge effects using a cylindrical-symmetric quasi-static space charge algorithm. The beam-DLW interaction is modeled via the Green’s function approach briefly outlined above and detailed in Ref. [36]. In the simulations the electron bunch is modeled as an ensemble of 100,000 macroparticles.

To characterize the temporal structure of the bunch, we represent the macroparticles’ temporal distribution as

\[
\Lambda(z) = \frac{1}{N} \sum_{i=1}^{N} \delta(z - z_i)
\]

and compute the bunch factor factor (BFF) \( \overline{F}(\omega) = |1/(2\pi) \int_{-\infty}^{+\infty} \Lambda(z/c) e^{-i\omega t} |^2 \) as

\[
\overline{F}(\omega) = \frac{1}{N^2} \left( \sum_{i=1}^{N} \cos \frac{\omega z_i}{c} \right)^2 + \left( \sum_{i=1}^{N} \sin \frac{\omega z_i}{c} \right)^2,
\]

where \( N \) is the number of macroparticles used in the simulation. The BFF is commonly used to characterize the performance of accelerator-based radiation source [37]. We note that in some cases, e.g., for the production of coherent radiation, transverse suppression effects might be prominent and should be properly accounted for by utilizing a three-dimensional expression for the BFF; see, e.g., Ref. [38].

A. Sub-picosecond bunch train formation

We first investigate the practical realization of the scheme described in section II to produce trains of sub-picosecond bunches and to demonstrate the versatility of the method, we consider two examples of implementation. The generic setup consists of an RF-gun electron source followed by a DLW as diagrammed in Fig. 4. Downstream of the DLW the beam is focussed with a second solenoid, e.g., to produce a waist at the location a transition-radiation target. The RF gun is taken to be an S-band (2.856 GHz) 1/2-cell cavity similar to the one currently in use at the linac coherent light source (LCLS) [39]. Similar results are then confirmed using a 1/2-cell L-Band (1.3 GHz) gun similar to the one used at the FLASH facility in DESY [40].

Table I. Beamline settings and DLW-structure parameters used in the astra simulations. The beamline configuration with some of the associated parameters is depicted in Fig. 4.

| parameter                  | S-Band | L-Band |
|----------------------------|--------|--------|
| Laser pulse RMS duration   | 3      | 7      |
| Laser pulse rise time      | 100    | 100    |
| Laser RMS spot size        | 0.72   | 1.1    |
| Initial charge             | 1      | 1      |
| Peak field on cathode      | 120    | 34     |
| Solenoid 1 position        | 0.20   | 0.0    |
| Solenoid 1 strength        | 0.26   | 0.17   |
| Solenoid 2 position        | 1.35   | 1.0    |
| Solenoid 2 strength        | 0.45   | 0.15   |
| DLW position               | 0.9    | 0.34   |
| DLW inner radius (a)       | 350    | 500    |
| DLW outer radius (b)       | 363    | 550    |
| DLW length                 | 11     | 4      |
| DLW fund. frequency \( f_1 \) | 1000   | 400    |
| Transmission through DLW   | 85     | 98     |
| Average kinetic energy     | 6.1    | 3.8    |

The photocathode-laser distribution was chosen to follow a plateau temporal distribution and its transverse size along with the location of the DLW, and solenoid strength were optimized using a multi-objective optimizer [41] to maximize beam transmission through the structure and minimize the transverse beam size at the DLW center. The list of optimized operating parameters are displayed Tab. I (“S-band” column). We note that the choice of the DLW parameters is a compromise between modulation wavelength \( \lambda_1 \), energy modulation amplitude – which affects the bunching parameter – and beam transmission. For example, a shorter DLW structure relaxes the requirements on beam sizes and emittances at the structure, but necessitates a longer drift to bunch the beam (as the imparted energy amplitude modulation is smaller than for a longer structure). Additionally, the number of potential microbunches depends on the incoming bunch length and \( \lambda_1 \). For example, a Gaussian bunch with rms length \( \sigma_z \) will eventually result in the generation of \( N_b \sim 4\sigma_z/\lambda_1 \) microbunches; varying \( \sigma_z \) for a given bunch charge and \( \lambda_1 \) affects the initial peak current and amplitude of the imparted energy modulation as inferred from Eq. 4.

We present, for the “S-band” case of Tab. I, the evolution of the BFF over a frequency range \( f \equiv \frac{\omega}{2\pi} \in [0.5,3.5] \) THz as a function of drift distance from the DLW exit \( z_{\text{drift}} \) in Fig. 5(a). The corresponding longitudinal-density evolution appears in Fig. 5(b). For this set of parameters, 10 microbunches are produced and a maximum bunching of \( \overline{F}(\omega_1) \simeq 0.20 \) is obtained at the
FIG. 5. Bunch form factor (BFF) (a) and bunch longitudinal density (b) evolution as a function of the drift length referenced with respect to the DLW exit. The simulations correspond to the parameters listed under the “S-band” column in Tab. I.

DLW fundamental mode’s wavelength $\lambda_1 \simeq 382 \, \mu$m. In addition, harmonics of the fundamental mode $f_{1,n} = nf_1$ are observed. For the selected DLW parameters and the corresponding thin dielectric layer, only the fundamental mode significantly influences the bunch dynamics.

The current and LPS distributions at the DLW entrance and at the location of maximum bunching (at $s \simeq 1.30 \, m$ from the photocathode) appear in Fig. 6. Peak current on the order of 1 kA are achieved for a beam with mean momentum of $\langle p_z \rangle \simeq 6.12 \, \text{MeV}/c$. The shortest current spike generated has an full-width half-max (fwhm) duration of $\sim 30 \, \text{fs}$. These results are comparable to the one experimentally obtained through wave-breaking in Ref. [22] albeit with a much higher contrast ratio [42]. The origin of the non-uniform bunching across the beam with peak-to-peak variation in the microbunch current is twofold. First, the slice-energy-spread positional variation along the bunch affects the shortest structure achievable at a given location. Second, the LPS prior to the DLW has initial correlations [as seen on the blue density plotted in Fig. 6(b)] which affect the bunching uniformity across the microbunches. This latter initial correlation is also responsible for the apparent “walk-off” feature (the microbunches spread apart from each others as they drift) of the microbunches visible in Fig. 5(b). Figure 6(c) indicates strong harmonic content at the second and third harmonic frequencies of $f_1$ is also observed at the location of maximum bunching.

Moreover, the higher harmonics are limited by the precision of the micro-bunch spacing within the bunch; a higher frequency DLW will lead to more micro bunches which will be more limited by the initial correlated LPS. We can investigate this feature by using a lower frequency structure of 500 GHz in the same context of the 1 THz example illustrated above. The current and LPS is shown in Fig. 7(a,b) and associated BFF over the frequency range (0.25 THz, 10 THz), is shown in Fig. 7(c) for maximum compression (red trace). The very strong higher harmonic content is notably due to the precise spacing of the microbunches. Additionally, we may want to suppress higher harmonics or amplify the fundamental; this can easily be done by selecting a bunch which is under or over-compressed such that the micro-bunches span a larger spatial extent; see Fig. 7(a,b,c) blue trace.

Finally, the evolution of the transverse beam sizes and emittance is respectively shown in Fig. 8(a) and (b) for the case presented in Fig. 6. The addition of a second solenoid at $s \simeq 1.2 \, m$ can transversely focus the beam down to $\sigma_x = \sigma_y \simeq 45 \, \mu$m at an axial location close to the maximum bunching; see Fig. 8(c). The simulated small rms beam size confirms that the one-dimensional BFF approach adopted earlier can accurately be used to estimate the properties of radiation emitted at wavelengths $\lambda \gg \gamma^{-1}\sigma_{x,y} \sim 5 \, \mu$m. It is therefore applicable to the THz regime. The small transverse size could also permit the use of a second DLW as a narrowband THz radiator.
as explored in Ref. [43].

The location of maximum bunching depends primarily on the wakefield amplitude compared to the average bunch energy. Applying higher peak fields in the RF-gun leads to larger ballistic bunching lengths downstream of the DLW structure and vice versa. Alternatively, shorter bunching lengths can be achieved by decreasing the bunch length at the cost of more microbunches. To confirm the applicability of our concept to other configurations we carried a similar study as the one presented above for the case of an L-band RF gun.

For this case we consider the setup available at the Fermilab’s A0 photoinjector [44] which incorporates a first-generation L-band gun used at the decommissioned Tesla-test facility at DESY [45]. The gun is nested in three solenoidal lenses. An optimization similar to the one carried for the S-band case was conducted and the resulting operating parameters are displayed in Tab. I ("L-band" column). For completeness the BFF and longitudinal density evolution downstream of the DLW are shown in Fig. 9. As in the S-band case we observe strong bunching at the DLW fundamental mode’s frequency (in this case $\lambda_1 \approx 750 \, \mu$m as the DLW parameters are different). But in contrast with the S-band case the higher-harmonic content of the BFF are significantly suppressed. The change in the fundamental frequency as the bunch drift downstream of the DLW appear stronger than for the S-band case and is due to a more prominent "walk-
off" effect due to the lower beam energy.

### B. Passive Bunching and Shaping

We now turn to another potential application of the scheme detailed in Section II to bunch or shape an electron beam produced via photoemission from an RF gun (this corresponds to the case when $\sigma_z \lesssim \lambda_1$).

To illustrate our point, we consider the case of the L-band gun just discussed in the previous section and instead of using the DLW parameters of Tab. I, we consider a structure with inner radius $a = 650 \, \mu$m to produce a global correlated energy spread as the fundamental-mode wavelength of the DLW becomes comparable to the bunch length. We use a 10-cm long DLW structure and note that due to the relatively large wavelengths required, the aperture becomes larger and the beam size requirement are significantly relaxed. As mentioned earlier, the inherent nonlinear LPS distortion exhibits a correlation between the depleted energy location and tail that has the proper sign for compression via ballistic bunching.

We exemplify this possibility by exploring the change in peak current downstream of a DLW structure with fixed inner radius $a = 650 \, \mu$m as a function of the fundamental-mode wavelength. The mode's wavelength is varied with different dielectric thicknesses due to the relatively small impact on the bunching length compared to changing $a$ directly. The results appear in Fig. 10 and indicate that a peak current of $\sim 12$ kA are attained when the fundamental-mode wavelength is $\sim 2.06$ mm (corresponding to $\lambda_1 = 0.49 \sigma_z$). The latter wavelength illustrates the role of the initial longitudinal emittance of the bunch before the DLW (i.e. the maximum peak current is achieved for an initial axial slice with the smallest slice energy spread.) In Fig. 11 only 7.1% of the population resides within the current spike while the rest contributes to the formation of longitudinal tails. This low-current population of the bunch could in principle be reduced via dispersive scraping or by exploring some energy-transverse correlations in conjunction with transverse collimators. Also, due to the relatively large inner radii needed to support wavelengths comparable to the bunch length, this technique can in principle easily be scaled to higher bunch charges. Finally, we note that the current profiles shown in Fig. 11 can actually find applications, e.g. to investigate wakefield effects in accelerating structures [46] and in compact beam-driven acceleration schemes utilizing low-energy drive bunches.

![FIG. 10. Maximum peak current as function of the fundamental-mode wavelength $\lambda_1$. The observed noise comes from numerical errors in precisely determining the value of the the axial position where the peak current is maximized. These simulations are carried with the beam parameters summarized in Tab. I “L-band” column but for a DLW structure with inner radius $a = 650 \, \mu$m. The fundamental-mode wavelength is varied by changing the structure outer radius $b$.](image)

As a final application we investigate the possibility to produce low-energy bunches with linearly-ramped current profiles. This type of distribution is sought after to improve the transformer ratio – the maximum accelerating wakefield over the decelerating field experienced by the driving bunch – in collinear beam-driven acceleration schemes [47]. We demonstrate that a standard distribution typically produced downstream of an RF gun can be transformed into a ramped bunch with quasi-linear dependency on $z$. We take the example of the S-band gun considered in Sec. III A and set $L/\lambda_1 \approx 1/2$ where $L$ is the full longitudinal size of the bunch upstream of the DLW structure. For these simulations, the axial-field amplitude at the cathode is set to $E_0 = 140$ MV/m. Such an increase (compared to the set of parameters displayed in Tab. I) was required to mitigate bunch lengthening. Figure 12 depicts the LPS evolution and associ-
ated current profiles associate to the bunch as it enters (red trace), exits (blue trace) the DLW and after a drift of 0.2 m (green traces). The interplay of the DLW field and longitudinal-space charge force results in the appearance of nonlinear correlations in the LPS. These nonlinearities provide some control over the current profile.

FIG. 12. Current profiles (a) and longitudinal phase spaces (b) at the entrance (red traces) and exit (red traces) of the DLW structure and 0.2-m downstream of the structure (s ≃ 0.54 m from the photocathode surface) where a quasi-linear current profile is achieved (green traces).

To quantify the performance of the current profiles simulated in Fig. 12(b, green trace), we compute the expected wakefield that such a bunch would produce in a DLW structure optimized to sustain a large axial field. The structure’s inner and outer radii are respectively a = 165 µm, b = 197 µm and εr = 5.7.

To quantify the performance of the current profiles simulated in Fig. 12(b, green trace), we compute the expected wakefield that such a bunch would produce in a DLW structure optimized to sustain a large axial field. The structure’s inner and outer radii are respectively a = 165 µm, b = 197 µm and the relative dielectric permittivity is kept to εr = 5.7. The resulting wakefield behind the bunch has a peak accelerating field amplitude of E+ ≃ 60 MV/m; see Fig. 13. The transformer ratio is numerically inferred as $R ≡ |E_+/E_-|$ where $E_- ≃ 8.2$ MV/m is the maximum amplitude of the decelerating electric field within the electron bunch. The achieved transformer ratio of $R ≃ 7.3$ is comparable to the ideal ratio of $R = n_p π ≃ 9.4$ predicted for an ideal linearly-ramped current profile (here $n_p ≃ 3$ is the number of mode wavelength comprised within the total bunch length) [47]. Depending on the desired application, the photoinjector settings and DLW parameters could be adjusted to produce a ramped current profile after further acceleration in a subsequent linac.

Finally, a finer control over the bunch shape could possibly be implemented using several DLW structures with properly selected fundamental-mode wavelengths. Such a multifrequency DLW approach would be an extension of the scheme described in Ref. [48] to higher frequencies.

IV. SUMMARY

In summary, we presented a relatively simple technique to bunch non-ultrarelativistic beams commonly produced by photoinjectors. The method was shown to support the generation of bunch train consisting of sub-picosecond microbunches. Alternatively, we demonstrated that a DLW with a lower-frequency fundamental mode could act as a passive buncher and produce multi-kA bunches. In addition, we discuss the application of the technique to form bunches with linearly-ramped current profiles as needed to improve the transformer ratio in beam-driven advanced-acceleration techniques. One of the main advantages of the method is that it relies on the bunch interaction with its self-induced fields which are inherently synchronized: the technique is therefore not prone to temporal jitter.

We expect the proposed method to find useful applications that span accelerator-based compact THz-radiation sources, ultra-fast electron diffraction and in photoinjectors for short-wavelength linacs.

It is also worth noting that the scheme could in principle be combined with other electron-emission processes (e.g. thermionic- or field-emission) but a detailed exploration is beyond the scope of the present study.

Finally, other wakefield mechanisms, e.g., the use of a corrugated pipe [49, 50] could provide an alternative to DLW and lead to similar results [51]. Our selection of a DLW structure was mainly motivated by its manufacturing simplicity and wide use in advanced accelerator R&D.

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