Phosphorus immobilisation in Al-drinking water treatment sludge (Al-DWTS) and soil under laboratory conditions

W.C. LI AND Y.Q. ZHAO*

Centre for Water Resources Research, School of Architecture, Landscape and Civil Engineering, University College Dublin, Newstead, Belfield, Dublin 4, Ireland

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This study assessed the potential reuse of an aluminium coagulated drinking water treatment sludge (Al-DWTS) as a main substrate in constructed wetland to replace soil for the treatment of P-enriched wastewater. The adsorption isotherm and kinetics of phosphorus (P) removal from high-P solution by Al-DWTS and a local soil from Bailieborough, Ireland, were studied and compared. The P adsorption process was examined as a function of contact time, initial P concentration, pH and temperature. Data of P adsorption were well fitted to the Langmuir and the Freundlich isotherms but the Freundlich isotherm had a higher correlation coefficient. The P adsorption capacity on the Al-DWTS and the soil tended to increase with an increase in temperature. The maximum P adsorption capacity of the Al-DWTS and the soil was 39.4 mg P mg⁻¹ and 9.5 mg P mg⁻¹, respectively, at conditions of pH of 4.0 and temperature of 23°C. Kinetics studies show that adsorption in both cases followed pseudo-second-order kinetics. The fact that the Al-DWTS exhibited a significantly higher P adsorption capacity at high P solution compared with the soil suggests that Al-DWTS can be a ‘novel-waste’ biosorbent with promising application in wastewater treatment engineering, such as constructed wetland systems.

Keywords: Adsorption; Aluminium-drinking water treatment sludge; Phosphorus; Soil; Wastewater treatment

1. Introduction

In recent years, much attention has been paid to phosphorus (P) pollution, its causes, ecological effects and the costs of clean up. Phosphorus enters the natural waters from various industries, domestic sewage, laundries, running water over phosphate rocks and extensive application of manure and fertilisers in agriculture. Typically, domestic wastewater has a total P concentration of approximately 10 mg P L⁻¹. The principal forms of phosphate are orthophosphate (5 mg P L⁻¹), pyrophosphate (1 mg P L⁻¹), and tripolyphosphate (3 mg P L⁻¹), together with smaller amounts of organic phosphate [1]. It is now necessary to adopt effective methods for the removal of P from wastewater before discharge, in order to meet

*Corresponding author. Email: yaqian.zhao@ucd.ie
Reducing P levels in wastewater may be achieved by various techniques, such as enhanced biological P removal; traditional chemical precipitation with aluminium, calcium and iron salts and various physicochemical methods including reverse osmosis, electrodialysis, contact filtration and adsorption, etc. In recent decades, many researchers have investigated removal of phosphate from wastewater using adsorption techniques with various adsorbents and biosorbents such as activated aluminium oxide, half-burnt dolomite, soil, tamarind nut shell activated carbon, fly ash, iron oxide tailings, blast furnace slag, recycled Fe(III)/Cr(III) hydroxide.

Drinking water treatment sludge (DWTS), is a resultant byproduct generated in the process of using aluminium- or iron-based salts as coagulants during the production of drinking water. DWTS mainly consists of suspended solids (in terms of turbidity), silt particles, organic matter (in terms of colour) and microorganisms from source water, together with residual chemicals (coagulants, polyelectrolytes and conditioning agents) that are added during the treatment processes. DWTS is classified as high plasticity organic clay. In most cases worldwide, DWTS is disposed of as waste to landfill. Nevertheless, the application of DWTS in P immobilisation has been increasingly studied to convert it from a ‘waste’ into low cost biosorbents for beneficial reuse. It is now clear that DWTS can be used as a soil amendment to increase considerably the P sorption capacity of soil for reducing offsite P transport. Research has demonstrated that a P-binding capacity of approximately 12.5 g P kg\(^{-1}\) DWTS can be achieved. A higher capacity up to 37.0 g P kg\(^{-1}\) DWTS was reported by Dayton and Basta in examining 18 DWTSs in the US.

Recent study by our group in University College Dublin, Ireland focused on exploiting and developing novel reuses of DWTS as raw material in civil and environmental engineering. Results have shown some remarkable potential in DWTS for immobilising a wide range of P species from simulated P-enriched wastewater. Considerable amounts of P can be adsorbed onto a relatively low mass of DWTS. Furthermore, the DWTS has been tested as the first of its kind as main substrate in a constructed wetland system for treating animal farm wastewater with high P levels. Since the main substrate in constructed wetland is normally soil, sand or gravel, the use of easily and locally available DWTS provides not only a low cost technological solution of improving P removal, but also an effective DWTS management option for its beneficial reuse.

The objective of our research was to evaluate the P sorption capacity of an aluminium-coagulated DWTS (termed as Al-DWTS) under the condition of using a high-P solution. Emphasis was placed on the comparative study of P-adsorption behaviour and capacity between the Al-DWTS and a local soil obtained from Bailieborough, Ireland. The soil has previously been employed as the main substrate in a full-scale constructed wetland system for an agricultural-industry wastewater treatment. We investigated the equilibrium and kinetics of adsorption of P onto the Al-DWTS and the soil. We used the Langmuir and Freundlich models to fit the equilibrium isotherms at different temperatures. We analysed the kinetics of adsorption using pseudo-first-order, pseudo-second-order and intra-particle diffusion models.

2. Materials and methods

2.1. Al-DWTS, soil and P solution preparation

The Al-DWTS was the brownish-green residual produced at the Ballymore–Eustace Water Treatment Plant located in South Dublin, Co. Kildare, Ireland from the treatment of a...
medium colour, medium turbidity, raw water that had been sourced from the Dublin and Wicklow mountains (upland catchments of peat over granite bedrock), and stored in Poulaphouca reservoir, County Wicklow. Dewatered Al-DWTS samples were collected from the dewatering unit of the plant, which uses aluminium sulphate as main coagulant with a dose of 42–60 mg L\(^{-1}\) for flocculation. The soil samples were obtained from the top 10 cm soil of the agricultural land at Lakeland Dairies, Bailieborough, County Cavan, Ireland, where the same soil has been used for constructing a full-scale constructed wetland system treating a cheese industry effluent. The Al-DWTS and soil were air-dried, ground and sieved through a 150 µm sieve size. The major element components of the Al-DWTS and soil were determined mainly by ICP analysis and listed in table 1. This shows that the Al-DWTS contains an abundant amount of Al (42,880 mg kg\(^{-1}\) DM (dry mass)) with significant level of organics indicated by the loss of ignition, which ranged 49–57%. This may be attributed to humic substances contained in the treated source water. Relatively, the soil contains much less Al (5409 mg kg\(^{-1}\) DM) and high P (2400 mg kg\(^{-1}\) DM), S (4759 mg kg\(^{-1}\) DM) and Mg (3696 mg kg\(^{-1}\) DM). This may be due to the Irish peat land nature. The stock solution of P was prepared in distilled water using potassium dihydrogen phosphate (KH\(_2\)PO\(_4\)). All working solutions were prepared by diluting the stock solution with distilled water.

### Table 1. Principal chemical compositions of Al-DWTS and soil

| Chemical composition | Unit       | Al-DWTS   | Soil    |
|----------------------|------------|-----------|---------|
| Aluminium (Al)       | mg kg-DM\(^{-1}\) | 42,880.0  | 5409.0  |
| Iron (Fe)            | mg kg-DM\(^{-1}\) | 2465.0    | 2231.0  |
| Calcium (Ca)         | mg kg-DM\(^{-1}\) | 1964.0    | 3400.0  |
| Magnesium (Mg)       | mg kg-DM\(^{-1}\) | 227.4     | 3696.0  |
| Lead (Pb)            | mg kg-DM\(^{-1}\) | 4.8       | 5.3     |
| Arsenic (As)         | mg kg-DM\(^{-1}\) | 23.6      | 1.4     |
| Mercury (Hg)         | mg kg-DM\(^{-1}\) | N/A       | < 0.4   |
| Sulphur (S)          | mg kg-DM\(^{-1}\) | 18.9      | 4759.0  |
| Chlorine (Cl)        | mg kg-DM\(^{-1}\) | 16.0      | 11.7    |
| Phosphorus (P)       | mg kg-DM\(^{-1}\) | 154       | 2400.0  |
| Moisture content     | %          | 25.5      | 15.5    |
| Loss in dry mass on ignition | %     | 49–57          | N/A     |

\(a\)DM denotes dry mass.

P-sorption experiments were conducted by equilibrating 3 g each of Al-DWTS and soil with 30 mL of varying P concentration in 150 mL plastic bottles. The bottles were then placed on a Stuart Orbital Shaker (SSL 1, Bibby Sterilin Ltd) and the mixture was agitated at 200 rpm for 6 h to ensure equilibrium. The pH values of the suspensions were adjusted to 3.0, 4.0, 5.5, 7.0, and 9.0 using either HNO\(_3\) or NaOH. After equilibration, samples were filtered using a 0.45 Millipore membrane filter to separate the solids from the liquid and the residual P concentration was measured according to method 8114 (HACH) using a HACH DR/2400 spectrophotometer [16]. For the isotherm studies, six levels of initial phosphate concentrations (69; 343; 856; 1142; 1712; 3425 mg P L\(^{-1}\)) were used while the pH was maintained at
an adjusted value of 4.0. Kinetic studies were also carried out at pH 4.0 using 3 g of the adsorbent and six different initial concentrations. The effect of temperature on adsorption equilibrium was investigated by conducting the shaking experiment in an oven with temperature varying from 23 to 37°C.

3. Results

3.1. Effect of contact time and concentration

In order to establish equilibrium time for maximum adsorption and also investigate the kinetics of the adsorption process, the adsorption of P on the Al-DWTS and the soil at various initial concentrations was studied as a function of contact time. Figures 1 and 2 show the results. Figure 1 shows that the equilibrium time for the adsorption of phosphate by Al-DWTS was 2 h when the P concentration \( C_0 \) ranged from 69 to 1712 mg P L\(^{-1}\), while for an initial concentration of 3425 mg P L\(^{-1}\), the equilibration time was 6 h. Figure 2 indicates that the equilibrium adsorption by soil can be attained in 2 h when the initial P concentrations are below 1142 mg P L\(^{-1}\). Accordingly, 4 h is required to reach the equilibrium adsorption when the initial P concentrations are 1712 mg P L\(^{-1}\) and 3425 mg P L\(^{-1}\), as shown in figure 2. Both the figures exhibit a rapid adsorption trend at the instant of contact. For instance, 50% adsorption on Al-DWTS was completed within 0.5 h for 3,425 mg P L\(^{-1}\) and within less than 0.25 h for the soil. Table 2 shows the effect of different initial concentrations on P adsorption ability by Al-DWTS and soil. The amount of P absorbed per unit mass \( q_t \) of Al-DWTS and soil seems to increase with an increased \( C_0 \), whereas an exception was observed at P initial concentration of 3425 mg L\(^{-1}\) for soil adsorption.

![Figure 1. Time variation of P-adsorption at various initial P concentrations for Al-DWTS (T = 23°C, pH = 4.0).](image)
3.2. Effect of pH

Figure 3 presents the effect of pH on the P adsorption by Al-DWTS and soil. Figure 3 shows that the optimum pH for both Al-DWTS and soil is 4.0. This corresponds to adsorption capacities of 31.6 mg P g\(^{-1}\) and 8.2 mg P g\(^{-1}\) for Al-DWTS and soil, respectively. Adsorption at pH 9.0 was the least, with a corresponding adsorption capacity of 14.7 mg P g\(^{-1}\) and 2.9 mg P g\(^{-1}\) for Al-DWTS and soil, respectively. The results indicate that the P adsorption onto Al-DWTS and soil is a physicochemical process and the adsorption ability is strongly dependent upon solution pH. The adsorptions are favoured in the acidic range with adsorption maxima obtained at pH 4.0 for both Al-DWTS and soil.

### Table 2.

| Initial concentration (mg P L\(^{-1}\)) | Adsorption capacity, \(q_e\) (mg P g\(^{-1}\)) |
|----------------------------------------|-----------------------------------------------|
|                                        | Al-DWTS                                      | Soil                                         |
| 69                                     | 0.67                                         | 0.52                                         |
| 343                                    | 3.32                                         | 2.28                                         |
| 856                                    | 8.37                                         | 3.67                                         |
| 1142                                   | 11.08                                        | 4.56                                         |
| 1712                                   | 16.60                                        | 8.35                                         |
| 3425                                   | 31.64                                        | 8.15                                         |

3.3. Kinetics study

The kinetics of P adsorption onto Al-DWTS and soil were studied using two models: pseudo-first- and second-order kinetics.
3.3.1. Pseudo-first-order model. The pseudo-first-order equation is given as:

$$\frac{dq_t}{dt} = k_1(q_e - q_t)$$  \hspace{1cm} (1)

where $q_t$ is the amount of adsorbate adsorbed at time $t$ (mg g$^{-1}$), $q_e$ the adsorption capacity at equilibrium (mg g$^{-1}$), $k_1$ the pseudo-first-order rate constant (h$^{-1}$) and $t$ the contact time (h).

The integration of equation (1) with the initial condition, $q_t = 0$ at $t = 0$ leads to:

$$\log(q_e - q_t) = \log q_e - \frac{k_1}{2.303}t.$$  \hspace{1cm} (2)

The values of the adsorption rate constant ($k_1$) for P were determined from the plot of $\log(q_e - q_t)$ against $t$.

3.3.2. Pseudo-second-order model. The pseudo-second-order model is described as below [20]:

$$\frac{dq_t}{dt} = k_s(q_e - q_t)^2.$$  \hspace{1cm} (3)

After integration by applying the boundary conditions, equation (3) becomes:

$$q_t = \frac{tk_eq_e^2}{1 + tk_eq_e}.$$  \hspace{1cm} (4)

The initial sorption rate, $r$ (mg/g h), at $t \to 0$ is defined as:
Equation (4) can then be rearranged to obtain:

\[ q_t = \frac{t}{1/r + (1/q_e)t} \]  
\[ (6) \]

Thus \( q_e \) can be obtained from the slope of \( t/q_t \) versus \( t \) and \( r \) is obtained from the intercept. Therefore, \( k_s \) can be calculated from equation (5). Figures 4 and 5 show the plot of equation (6) for adsorption of P onto Al-DWTS and soil, respectively. The results demonstrate a linear relationship between adsorbed phosphate and \( t \), with high correlation coefficients. The kinetic parameters for the pseudo-first- and second-order equations and correlation coefficients are tabulated in table 3 (for Al-DWTS) and table 4 (for soil). By inspecting \( R^2 \) in tables 3 and 4, it is clear that the pseudo-second-order model is better than the pseudo-first-order model to describe the P adsorption for both Al-DWTS and soil. Several authors have also reported the validity of the pseudo-second-order model in description of P adsorption onto ZnCl₂ activated coir pith carbon [3], recycled Fe(III)/Cr(III) hydroxide [9] and alunite [21].

Plots of \( q_e \) and \( r \) against \( C_0 \) were regressed to obtain the values in terms of \( C_0 \) with a high regression coefficient for Al-DWTS (\( R^2 = 0.999, 0.996 \), respectively). Regressions were gained to the best fitting of \( q_e \) and \( r \) against \( C_0 \) for soil with a slightly lower regression coefficient (\( R^2 = 0.960, 0.976 \), respectively). Nevertheless, \( q_e \) and \( r \) can be expressed as a function of \( C_0 \), as shown in equations (7) and (8) for Al-DWTS, and equations (9) and (10) for soil, respectively.

\[ q_e = 0.0092 \times C_0 + 0.3784. \]  
\[ (7) \]
Figure 5. Plot of the pseudo-second-order adsorption kinetics of P on soil at different initial concentrations (T = 23°C, pH = 4.0).

Table 3. Kinetic parameters for the removal of P by Al-DWTS (T = 23°C, pH = 4.0)

| $C_0$ (mg P L$^{-1}$) | First-order model | Second-order model |
|-----------------------|-------------------|-------------------|
|                       | $k_1$ (h$^{-1}$)  | $R^2$             | $r$ (mg g$^{-1}$ h$^{-1}$) | $k_s$ (g mg$^{-1}$ h$^{-1}$) | $R^2$ |
| 69                    | 1.58              | 0.970             | 6                           | 13.37                        | 0.995 |
| 343                   | 1.38              | 0.967             | 30                          | 2.72                         | 0.999 |
| 856                   | 1.14              | 0.985             | 75                          | 1.07                         | 0.998 |
| 1142                  | 0.90              | 0.946             | 96                          | 0.78                         | 0.998 |
| 1712                  | 0.87              | 0.967             | 112                         | 0.41                         | 0.999 |
| 3425                  | 0.72              | 0.943             | 86.9                        | 0.09                         | 0.999 |

Table 4. Kinetic parameters for the removal of P by soil (T = 23°C, pH = 4.0)

| $C_0$ (mg P L$^{-1}$) | First-order model | Second-order model |
|-----------------------|-------------------|-------------------|
|                       | $k_1$ (h$^{-1}$)  | $R^2$             | $r$ (mg g$^{-1}$ h$^{-1}$) | $k_s$ (g mg$^{-1}$ h$^{-1}$) | $R^2$ |
| 69                    | 2.23              | 0.990             | 3.86                        | 14.3                         | 0.995 |
| 343                   | 1.59              | 0.990             | 7.85                        | 1.51                         | 0.998 |
| 856                   | 3.15              | 0.997             | 17.8                        | 1.32                         | 0.998 |
| 1142                  | 1.95              | 0.973             | 21.7                        | 1.04                         | 0.999 |
| 1712                  | 1.17              | 0.977             | 35.6                        | 0.51                         | 0.999 |
| 3425                  | 0.70              | 0.874             | 54.4                        | 0.82                         | 0.999 |
Substituting the values of $q_e$ and $r$ into equation (6), the relationship of $q_t$, $C_0$ and $t$ can be represented for Al-DWTS (equation (11)) and soil (equation (12)) as follows:

$$q_t = \frac{t}{1/(-2 \times 10^{-5} \times C_0^2 + 0.1112 \times C_0 - 2.4243) + (1/(0.0092 \times C_0 + 0.3784)) \times t}$$  (11)

$$q_t = \frac{t}{1/(-1 \times 10^{-6} \times C_0^2 + 0.0188 \times C_0 + 1.9256) + (1/(0.0273 \times C_0^{0.7264})) \times t}$$  (12)

These equations can then be used to derive the amount of P adsorbed on Al-DWTS and soil at any given $C_0$ (from 69 to 3,425 mg P L$^{-1}$) and $t$.

### 3.4. Adsorption isotherm

To assess the adsorption potential of Al-DWTS and soil for high–P solution, Langmuir and Freundlich isotherms were used for fitting sorption equilibrium data. Equations (13) and (14) respectively give the linear forms of the Langmuir isotherm and the Freundlich isotherm.

$$\frac{C_e}{q_e} = \frac{1}{Q_0b} + \frac{C_e}{Q_0}$$  (13)

$$\log q_e = \log k_d + (1/n) \log C_e$$  (14)

where $q_e$ is defined as before (mg P g$^{-1}$), $b$ (L mg$^{-1}$) a sorption constant related to P binding energy, $Q_0$ the maximum adsorption capacity (mg P g$^{-1}$ sludge) and $C_e$ is the equilibrium P concentration (mg P L$^{-1}$). The slope and the intercept of the plot of $(C_e/q_e)$ versus $C_e$ gives the values of $Q_0$ and $b$. $k_d$ is the distribution coefficient, and $n$ is a parameter of the Freundlich model.

By fitting the equilibrium data at 23, 30 and 37°C with equation (13) and equation (14), respectively, the isotherms for Al-DWTS and soil are generated. Figures 6 and 7 illustrate this. Table 5 lists the theoretical parameters of isotherms along with correlation coefficients. It is seen that the experimental data of P adsorption onto the Al-DWTS and the soil could be well fitted by the two models. The Freundlich isotherm exhibited a better fitting than Langmuir isotherm, and this is in agreement with that reported recently by Mortula and Gagnon [22] in a similar study. In addition, table 5 also shows that the adsorption capacity increased from 39.4 to 42.9 mg P g$^{-1}$ for Al-DWTS and from 9.49 to 11.03 mg P g$^{-1}$ for soil when the temperature was increased from 23 to 37°C.
Figure 6. Langmuir (upper) and Freundlich (lower) adsorption isotherms of P adsorption onto Al-DWTS at different temperatures (pH = 4.0).

4. Discussion

The aim of this study was to provide comparative data on P adsorption by Al-DWTS and a local soil. A series of adsorption experiments were designed and in particular, from the results, the Al-DWTS was found to be capable of removing P even at a very high P level. Table 5 shows that the P adsorption capacity of Al-DWTS (39.4 mg P g$^{-1}$) is more than four times greater than that of soil (9.5 mg P g$^{-1}$). Although various factors can contribute to P retention mechanisms in the Al-DWTS and soil, it is believed that aluminium oxide is the major cause because it is particularly strong in binding P through ligand exchange and precipitation reactions, which have been investigated previously [23,24]. Table 1 shows that Al in Al-DWTS is eight-fold greater than that in soil. Although the properties of Al-DWTS
Figure 7. Langmuir (upper) and Freundlich (lower) adsorption isotherms of P adsorption onto soil at different temperatures (pH = 4.0).

Table 5. Langmuir and Freundlich isotherms constants obtained at obtained pH = 4.0

| Adsorbent | $T$ (°C) | $Q_0$ (mg P g$^{-1}$) | $b$   | $R^2$ | $k_d$ | $1/n$ | $R^2$ |
|-----------|----------|------------------------|-------|-------|-------|-------|-------|
| Al-DWTS   | 23       | 39.4                   | 0.0156| 0.973 | 0.994 | 0.668 | 0.986 |
|           | 30       | 40.7                   | 0.0167| 0.962 | 1.137 | 0.661 | 0.989 |
|           | 37       | 42.9                   | 0.0190| 0.969 | 1.316 | 0.655 | 0.985 |
| Soil      | 23       | 9.5                    | 0.00220| 0.931 | 0.125 | 0.563 | 0.938 |
|           | 30       | 10.1                   | 0.00256| 0.942 | 0.163 | 0.541 | 0.945 |
|           | 37       | 11.0                   | 0.00293| 0.962 | 0.210 | 0.514 | 0.945 |
are variable and dependent upon the characteristics of the raw waters and the coagulant used, which is believed to result in different P adsorption capacities, it is reasonable to conclude that the alum based DWTS has a very high P adsorption capacity over soil due to the feature of significantly high Al content. As such, the feasibility of augmenting soil’s P sorption capacity by mixing DWTS into soils as a new chemical-based P immobilisation method has already been investigated and confirmed by different researchers [10–12,25]. In addition, the specific surface area (SSA) of the Al-DWTS tested was in the range of 49.0–62.3 m² g⁻¹ [26]. Although the SSA of the soil was not monitored, in comparison to the range of SSA of other materials reported in literature such as 2.6–3.9 m² g⁻¹ [27] and 6.8–31.4 m² g⁻¹ [28], the Al-DWTS used herein can be seen to have a comparatively higher SSA. This is believed to be relevant to the high P adsorption capacity.

With regard to the factors that affect the P adsorption behaviour on Al-DWTS and soil, initial concentrations, contact time, pH and temperature have all shown pronounced effects on the adsorption capacity of both adsorbents (see figures 1–3, tables 2, 5). In particular, computed models (equations (11) and (12)) derived from the data of this study have provided a quantitative description of the integrated effect of some major factors especially the initial P concentration on adsorption behaviour. Although P adsorption is a complicated process, ligand exchange may be the dominating mechanism [23]; more Al content in Al-DWTS may provide more activated exchange sites than soil. From figures 1 and 2, it seems that when P adsorptions on Al-DWTS and soil occur at lower concentration, the time required to achieve a definite fraction of equilibrium is independent of initial concentration. It is reasonable to expect that at lower concentration, the ratio of the initial number of P molecules to the available exchange sites is low and subsequently the fractional adsorption becomes independent of initial concentration. But, at a higher concentration, fewer exchange sites are available to occupy, so the amount of P adsorbed is dependent upon the initial concentration. In a previous study [15], P adsorption capacity of 10.2 mg PO₄³⁻ g⁻¹ Al-DWTS was obtained at a low P concentration which simulated the typical P level in municipal wastewater. This reflects the effect of initial P concentration on adsorption capacity.

The amount of P absorbed onto Al-DWTS and soil increased with an increase of agitation time before equilibrium was reached (figures 1 and 2). P was initially adsorbed by the activated exchange sites in the exterior surface. When the adsorption at the exterior surface reached the saturation level, P begins to diffuse into the pores within the particles. The determination of pore size distribution of the Al-DWTS indicated that pores with sizes less than 5.98 nm contributed 50% of the surface area while pores of size less than 9.67 nm contributed 90% of the surface area. The pore size larger than 20 nm only contributed an insignificant amount to the surface area [26]. Through the intra-particle diffusion study [29,30], an intra-particle diffusion coefficient $k_{id}$ is given by the equation:

$$q_t = k_{id}t^{1/2}. \quad (15)$$

Figures 8 and 9 show the plots of $q_t$ versus $t^{1/2}$ for Al-DWTS and soil, respectively. Table 6 lists the calculated intra-particle diffusion coefficient $k_{id}$ values. Figures 8 and 9 reveal two separate regions active in the P adsorption process on Al-DWTS and soil at high initial concentration. The initial portion is attributed to the mass transfer of P molecules from bulk solution to absorbent surface; the second portion is the intra-particle diffusion on the absorbent. It is believed that the intra-particle diffusion might be the rate-controlling step in the P adsorption process. As mentioned previously, the pH of the aqueous solution is an important variable that influences the P adsorption on Al-DWTS and soil. As figure 3 shows, the
amount of P adsorbed onto Al-DWTS and soil tends to decrease when pH increases from 4.0 to 9.0. In an early study [23], the increase of OH\(^-\) in solution could affect the electrostatic properties of the sludge, which makes the surface charge of the Al-DWTS change from positive to negative. This is confirmed by measuring the zeta potential, which ranged from +75.8 to −33.7 mV corresponding to a pH change from 4.3 to 9.0. The more negatively charged
surface would repulse the negatively charged species (such as \( \text{PO}_4^{3-} \)) in solution to break the P-binding process.

Although chemical precipitation of the various forms of calcium phosphates is favoured at a pH above 7.5 [31], this is not the case for the Al-DWTS and soil studied in spite of the reasonably high contents of calcium in Al-DWTS and soil (see table 1). It is noted in figure 3 that when pH < 4.0, such as pH = 3.0, the P adsorption capacity of Al-DWTS and soil decreases. This may be caused by a higher solubility of aluminium oxide as it occurs below a pH value of about 4.0–4.5 [8,32]. The effect of temperature on the P adsorption capacity of Al-DWTS and Bailieborough soil shows (in table 5) that the sorption of phosphate is an endothermic process. Yet, although the P adsorption on Al-DWTS tends to increase with increased temperature from 23°C to 37°C, there is a relatively slight increase on soil. The sorption constant \( b \), which relates to the P binding energy, increased from 0.0156 to 0.0190 L mg\(^{-1}\) for Al-DWTS and increased from 0.0022 to 0.0029 L mg\(^{-1}\) for soil at adsorption conducted at temperatures from 23°C to 37°C. This suggests that increasing temperature favours the P sorption.

5. Conclusions

An aluminium coagulated drinking water treatment sludge (Al-DWTS) and a constructed wetland soil were assessed for their P removing ability. The same trends of P adsorption were obtained in both cases. However, the Al-DWTS exhibited a significant P immobilisation ability at high-P concentration in contrast to the soil. P adsorption capacity on Al-DWTS in high-P solution is 39.4 mg P g\(^{-1}\), which is more than four times greater than the value (9.14 mg P g\(^{-1}\)) on soil. Analysis of kinetic data showed that uptake of P onto Al-DWTS and soil followed pseudo-second-order kinetics. Equilibrium adsorption data of Al-DWTS and soil obey both Langmuir and Freundlich isotherms with the Freundlich isotherm being better than the Langmuir. Maximum P removal occurred at pH = 4.0 for both adsorbents tested. The sorption capacity of both Al-DWTS and soil increases at a temperature range from 23 to 37°C. Overall, this result provides the technical support for using Al-DWTS to benefit soil as an absorbent for removal of P in a wider range of concentration from P-rich wastewaters.

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