Study on Load Parameters Estimation during AMT Startup

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The identification problem of the load parameters is the basis of researching the clutch control strategy and the shift schedule for heavy-duty AMT (Automated Mechanical Transmission). AMT is proposed as the soft starter for the belt conveyor which expands AMT application areas. In order to accomplish the goal of AMT as the soft starter, the load parameters estimation methods including the load resistance torque and the load inertia are firstly studied to accommodate the actual control for AMT startup as the soft starter for belt conveyor. In the paper, the estimation models of the load resistance torque and the load inertia are established during AMT startup for belt conveyor. On the basis of the recursion least squares method, the on-line estimations for the load parameters are recognized according to the test data during AMT startup. The estimation results of these two parameters prove that the load parameters estimation models and the estimation methods during AMT startup are valid.

1. Introduction

Heavy-duty AMT is a type of transmission with complicated working condition and wider load range. The load parameters identification has significant influences on control method and control law for AMT. The researchers have studied the transmitting torque estimation of the clutch during the shifting process in terms of smaller vehicles for decades. Zhao et al. studied the transmitting torque estimation of the clutch during the shifting process on dry double-clutch transmission [1–3]. Pettersson et al. studied the output torque of the vehicle drive shaft during the shifting process based on the transmission model with elastic drive shaft [4, 5]. Baumann et al. designed a Luenberger observer to estimate the actual output torque of the drive shaft [6]. Yi et al. designed a self-adapt slid mode observer to estimate the transmitting torque of the automatic transmission [7]. The identification accuracies of these studies should be verified on real vehicles to demonstrate the theoretical validity. The recursive least squares method is widely used to identify the load parameters. The researchers have studied the least squares parameter estimation methods to for nonlinear system. Wang et al. studied highly efficient identification methods for dual-rate Hammerstein systems [8]. Zhang et al. studied separate block-based parameter estimation method for Hammerstein systems [9].

Belt faults such as breakage and slipping are often caused on account of excessive belt acceleration during the starting process of belt conveyors [10, 11]. Generally, the belt acceleration value is under 0.3 meter per square seconds in order to accelerate the belt conveyor slowly [12–15]. Li et al. studied the starting process and the shifting process for AMT softly starting the belt conveyor based on known load parameters [16, 17]. In application of AMT as the soft starter for belt conveyors, the unknown load parameters should be identified so that the starting process and the shifting process can be better controlled.

The half engagement point of the clutch is a critical point during the starting process which is related to the driving resistance torque on the transmission input shaft. As is known, the half engagement point of the clutch is related to the load resistance torque and the gear position. As a result, it is different if the load resistance torque or the gear position is different. In consequence, the identification for the half engagement of the clutch is the premise to recognize the load parameters. In this paper, the characteristics of the half engagement of the clutch will be used to establish the estimation model of the load resistance torque. Then the estimation model of the load inertia is proposed on the basis of the information about the output shaft speed and the clutch location. The recursion least squares method is applied to the load inertia estimation during AMT startup.
As is shown in Figure 1, the drive line of AMT softly starting the belt conveyor mainly composes of the three-phase induction motor, AMT, the reducer, and the driving pulley of the belt conveyor. The symbolic meanings are as follows: $T_m$ is the output torque of the three-phase induction motor, $T_c$ is the transmitting torque of the clutch, $T_{conveyor}$ is the resistance torque at the driving pulley of the belt conveyor, $M_g$ is the friction loss of the transmission, $M_r$ is the friction loss of the reducer, $n_m$ is the motor speed, $n_i$ is the input speed of the transmission, $n_o$ and $n_c$ are the output speed of the transmission and the driving pulley speed separately.

2. Structure of AMT Test Bed

AMT test bed consisting of the three-phase induction motor with 55 kilowatts, the efficiency instrument, HW19710 type pneumatic AMT manufactured by China Sinotruk, the inertia plate which is used to simulate the load inertia, the loading device which is used to simulate the load resistance torque, the hydraulic station which is used to provide the hydraulic pressure for the loading device to change the resistance torque conveniently, the air compressor which is used to provide the compressed air for AMT actuator, the AMT measurement and control system which is used to provide the command controls, and the sensors signal collections for communicates between AMT and the computer. The reduce gearbox is omitted for the limited space in the laboratory. The test bed system is shown in Figure 2.

3. Identification Models of the Load Parameters

3.1. Clutch Torque Characteristics. As is known, the torque characteristics of the dry clutch are related to the wear loss. Based on the clutch displacement sensor and the input shaft speed sensor, the estimation of the clutch wear loss can be measured which the diagram of the wear testing program is shown in Figure 3.

The dry clutch torque characteristics can be expressed by the displacement of the clutch actuator with a cubic displacement polynomial in

$$T_c (x_c) = \mu' \left[ K_1 (x_c - x_{ce} - \Delta x_{ce}) + K_2 (x_c - x_{ce} - \Delta x_{ce})^2 + K_3 (x_c - x_{ce} - \Delta x_{ce})^3 \right]$$

where $K_1, K_2, K_3$ are first-order coefficient, second-order coefficient, and third-order coefficient respectively, $\mu'$ is the dynamic friction coefficient between the driving disc and the friction disc, $x_c$ is the displacement of the clutch actuator, $x_{ce}$ is the corresponding displacement of the clutch actuator related to the critical point of the new clutch empty running, and $\Delta x_{ce}$ is the increase of the clutch actuator empty running displacement caused by the clutch wear.

3.2. Estimation Model of the Load Resistance Torque. The load resistance torque can be estimated on the basis of the relationship between the half engagement joint and the clutch.
transmitted torque. The signal of the transmission output shaft speed sensor can be collected after the signal gear turns the first tooth. The speed of the transmission output shaft can be measured as long as the output shaft turns. The load resistance torque can be calculated until the transmission output shaft speed data updates m-1 times (m is less than or equal to n) is defined as \( t_k \) and the time of the output shaft speed update m times is considered as \( t_i \). The parameter of \( \Delta n_m \) is ordered as \( n_d \) minus \( n_d \). The load angular momentum on the transmission output shaft can be calculated in (3) during the period of the time of \( t_k \) to that of \( t_i \).

\[
M_{loadm} = \left[ \left( \frac{T_{ek} + T_{el}}{2} + \sum_{x=k+1}^{i-1} T_{ex} \right) \eta_g i_g - \hat{T}_{load}(I-k) \right] \Delta t_s \tag{3}
\]

Consequently, the observation equation between the load angular momentum on the transmission output shaft and the unknown load inertia during the period of the time of \( t_k \) to that of \( t_i \) can be expressed in

\[
M_{loadm} = \frac{\pi \Delta n_m}{30} I_{load} + \nu_m \tag{4}
\]

where \( I_{load} \) is the load equivalent inertia on the transmission output shaft.

The observation matrix of the load equivalent inertia on the transmission output shaft can be described in (5) if the load angular momentum on the transmission output shaft can be taken as the observation matrix and the output shaft speed variation can be treated as the gain matrix.

\[
M_{loadi} = H_i I_{load} + V_i \tag{5}
\]

where \( i \) is equal to 1, 2, \ldots, m, \( M_{loadi} \) is the observation matrix which is equal to the transpose of \([M_{load1} M_{load2} \cdots M_{loadm}]\), \( H_i \) is the gain matrix which is equal to the transpose of \([\Delta n_1 \Delta n_2 \cdots \Delta n_m]\), and \( V_i \) is the measurement error matrix which is equal to the transpose of \([v_1 v_2 \cdots v_m]\).

### 3.4. Recursion Least Squares Estimation Method of the Load Inertia

The estimation model for the load inertia can be shown in

\[
J_W (\hat{I}_{load}) = (M_{loadm} - H_m \hat{I}_{load})^T W_m (M_{loadm} - H_m \hat{I}_{load}) \tag{6}
\]

where \((M_{loadm} - H_m \hat{I}_{load})^T\) is the transposed matrix of \((M_{loadm} - H_m \hat{I}_{load})\) and \(W_m\) is a positive weighting matrix.

If the mean value of the observation errors is zero and the variance matrix is \(Q_m\) which is equal to the mathematical expectation of the product between \(V_m\) and its transpose, the optimal weighting least squares estimation for the load inertia

**Figure 3:** The diagram of the clutch wear testing program.
with m sets of observation data can be expressed in (7) under the condition that the weighting matrix in $W_m$ is equal to the inverse of the variance matrix in $Q_m$.

$$\tilde{J}_{loadLSW}(m) = \left[ H_m^T Q_m^{-1} H_m \right]^{-1} H_m^T Q_m^{-1} M_{loadm}$$

where $Q_m^{-1}$ is the inverse matrix of $Q_m$, $H_m^T$ is the transpose matrix of $H_m$, and $[H_m^T Q_m^{-1} H_m]^{-1}$ is the inverse matrix of $[H_m^T Q_m^{-1} H_m]$.

In the same way, the optimal weighting least squares estimation for the load inertia can be expressed in

$$\tilde{J}_{loadLSW} (m + 1) = [H_{m+1}^T Q_{m+1}^{-1} H_{m+1}]^{-1} H_{m+1}^T Q_{m+1}^{-1} M_{load(m+1)}$$

where $Q_{m+1}$ is equal to $[Q_m 0; 0, q_{m+1}]$ and $q_{m+1}$ is the measurement error variance of number $m+1$ times.

If $P_m$ and $P_{m+1}$ are $H_m^T Q_m^{-1} H_m$ and $H_m^T Q_{m+1}^{-1} H_{m+1}$ separately, the recursive least squares estimation for the load inertia can be expressed in (9) when the number $m+1$ set of test data is observed.

$$\tilde{J}_{loadLSW} (m + 1) = \tilde{J}_{loadLSW} (m) + K_{m+1} [M_{load(m+1)} - h_{m+1}\tilde{J}_{LSW} (m)]$$

$$K_{m+1} = P_{m+1}^{-1} h_{m+1}^T q_{m+1}^{-1}$$

$$P_{m+1}^{-1} = P_m^{-1} - P_m^{-1} h_{m+1}^T \left( q_{m+1} + h_{m+1} P_m^{-1} h_{m+1}^T \right)^{-1} h_{m+1} P_m^{-1}$$

The recursive least squares estimation for the load inertia is finished until the number of estimation is equal to that of observational data. The recursive least squares estimation algorithm for the load inertia can be shown in Figure 4.

4. Real-Time Estimation of the Load Parameters Based on the Recursive Least-Square Algorithm

4.1. Estimation of the Load Parameters. The torque-displacement characteristics of the new clutch can be received which the input torque of the clutch and the output torque of the transmission can be tested using the mechanical efficiency instrument. The experiment methods are described as follows. Firstly, the critical point of the clutch empty stroke is tested on the condition of no load. Secondly, the different half engagement point and the transmitting torque of the clutch can be tested and recorded under the first gear position with the help of the mechanical efficiency instrument and the loading device of which the different resistance torque can be simulated by changing the hydraulic pressure of the hydraulic station. Then, the clutch torque-displacement characteristics in (1) can be expressed with the test data using the method of least squares fit.

On the basis of above methods, the new clutch torque-displacement characteristics in this paper can be expressed approximately in (10) if the friction coefficient $\mu$ is 0.25.

$$T_c (x_c) = 17.2431 (x_c - x_{ce}) + 21.0131 (x_c - x_{ce})^2$$
$$+ 0.2839 (x_c - x_{ce})^3$$

The starting process under the first gear is shown in Figure 5 on the condition of unknown load inertia and unknown load resistance torque. Based on (2) and (10), the clutch transmitting torque is 100 N·m. The mechanical efficiency under the first gear is 90 percent by using the efficiency instrument. For this reason, the load resistance torque is 1285.20 N·m.

The zero time of the parameter estimation is determined when the half engagement point is tested. The eighteen sets of observation data with the clutch transmitting torque and the output shaft speed are used to estimate the load inertia. The Gaussian random white noise N(0,1) is added on the basis of

![Figure 4: The flow block diagram of the recursive least squares estimation algorithm.](image-url)
the observation data. The recursive least squares method is applied in (5) of which the initial value of the load equivalent recursive least squares estimation (RLSE) derived from the top four sets of test data is 261.88 kg·m². The estimation accuracy is defined as the former estimation divided by the difference value of the current estimation value and the former estimation value. The estimation results containing the load momentum observation on the transmission output shaft, the load equivalent inertia estimation (the recursive least squares estimation of the load equivalent inertia on the transmission output shaft), and the estimation accuracy are shown in Figures 6, 7, and 8 respectively.

On the same working condition above, the starting process under the third gear is shown in Figure 9. Forty-one sets of observation data with the clutch transmitting torque and the output shaft speed during the starting process under the third gear are used to estimate the load inertia using the recursive least squares method. The zero time of the parameter estimation is still determined when the half engagement point is tested. The Gaussian random white noise N(0,1) is added on the basis of the observation data. The recursive least squares method is applied in (5) of which the starting value of RLSE derived from the top four sets of test data is 69.76 kg·m². The estimation results of the load momentum observation, the recursive least squares estimation of the load equivalent inertia on the transmission output shaft, and the estimation accuracy are betrayed in Figures 10, 11, and 12 separately.

4.2. Analyzation of Estimation Results. The value of the actual test bed inertia plate is 130 kg·m². As a result, the actual load equivalent inertia on the transmission output shaft under the
The load parameters estimation methods are studied during AMT startup as the soft starter for belt conveyor in the paper. The main conclusions are as follows. Firstly, the mathematical models of the load parameters estimation are established according to the mechanical characteristics during AMT startup. Secondly, the recursion least squares method of the load inertia is analyzed. Thirdly, based on the clutch torque-displacement characteristics and the test data during AMT startup, the load resistance torque and the load equivalent inertia are identified. The on-line estimation results show that the load parameters can be effectively recognized by the use of the above identification methods of the load parameters which provides the theoretical and experimental evidences to further study the clutch control strategy and the shift schedule for heavy-duty AMT.

5. Conclusion

The load parameters estimation methods are studied during AMT startup as the soft starter for belt conveyor in the paper. The main conclusions are as follows. Firstly, the mathematical models of the load parameters estimation are established according to the mechanical characteristics during AMT startup. Secondly, the recursion least squares method of the load inertia is analyzed. Thirdly, based on the clutch torque-displacement characteristics and the test data during AMT startup, the load resistance torque and the load equivalent inertia are identified. The on-line estimation results show that the load parameters can be effectively recognized by the use of the above identification methods of the load parameters which provides the theoretical and experimental evidences to further study the clutch control strategy and the shift schedule for heavy-duty AMT.

Data Availability

The data used to support the findings of this study are available from the corresponding author upon request.

Conflicts of Interest

The authors declare that they have no conflicts of interest.
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References

[1] Z. Zhao, J. Gu, and L. He, "Estimation of torques transited by twin-clutch during shifting process for dry dual clutch transmission," Journal of Mechanical Engineering, vol. 53, no. 14, pp. 77–87, 2017.

[2] Z. Zhao, L. He, Y. Yang, C. Wu, X. Li, and I. Karl Hedrick, "Estimation of torque transmitted by clutch during shifting process for dry dual clutch transmission," Mechanical Systems and Signal Processing, vol. 75, pp. 413–433, 2016.

[3] Z. Zhao, C. Wu, Y. Yang, and H. Chen, "Optimal robust control of shifting process for hybrid electric car with dry dual clutch transmission," Journal of Mechanical Engineering, vol. 52, no. 18, pp. 105–117, 2016.

[4] M. Pettersson and L. Nielsen, "Gear shifting by engine control," IEEE Transactions on Control Systems Technology, vol. 8, no. 3, pp. 495–507, 2000.

[5] M. Pettersson and L. Nielsen, "Diesel engine speed control with handling of driveline resonances," Control Engineering Practice, vol. 11, no. 3, pp. 319–328, 2003.

[6] J. Baumann, D. D. Torkzadeh, A. Ramstein, U. Kiencke, and T. Schlegl, "Model-based predictive anti-jerk control," Control Engineering Practice, vol. 14, no. 3, pp. 259–266, 2006.

[7] K. Yi, B. Shin, and K. Lee, "Estimation of turbine torque of automatic transmissions using nonlinear observers," Journal of Dynamic Systems, Measurement, and Control, vol. 122, no. 2, pp. 276–283, 2000.

[8] D.-Q. Wang, H.-B. Liu, and F. Ding, "Highly efficient identification methods for dual-rate hammerstein systems," IEEE Transactions on Control Systems Technology, vol. 23, no. 5, pp. 1952–1960, 2015.

[9] S. Zhang, D. Wang, and F. Liu, “Separate block-based parameter estimation method for Hammerstein systems,” Royal Society Open Science, vol. 5, no. 6, Article ID 172194, 2018.

[10] M. Qing-Rui and H. You-Fu, "Effect of oil film squeezing on hydro-viscous drive speed regulating start," Tribology International, vol. 43, no. 11, pp. 2134–2138, 2010.

[11] M. H. Ghayesh, "Nonlinear transversal vibration and stability of an axially moving viscoelastic string supported by a partial viscoelastic guide," Journal of Sound and Vibration, vol. 314, no. 3-5, pp. 757–774, 2008.

[12] G. Lodewijks, "Two decades dynamics of belt conveyor systems," Bulk Solids Handling, vol. 22, no. 2, pp. 124–173, 2002.

[13] L. K. Nordell, "Zisco installs world's longest troughed belt 15.6 km horizontally curved overland conveyor," in Proceedings of the International Materials Handling Conference, Belcon, pp. 1–11, 1997.

[14] L. K. Nordell and Z. P. Ciozda, "Transient belt stresses during starting and stopping: elastic response simulated by finite element methods," Bulk Solids Handling, vol. 4, no. 1, pp. 93–98, 1984.

[15] M. P. Singh, "Role of drive system technology in maximizing the performance and economics of long belt conveyors," Bulk Solids Handling, vol. 14, no. 4, pp. 695–702, 1994.

[16] Y. Li, Z. Wang, and X. Cong, "Constant acceleration control for AMT’s application in belt conveyor’s soft starting," International Journal of Control and Automation, vol. 6, no. 6, pp. 315–326, 2013.

[17] Y. Li, Z. Wang, W. Peng, and Z. Zheng, “Experimental study on synchronous shifting for AMT without synchronizer based on three-phase induction motor,” International Journal of Smart Home, vol. 10, no. 2, pp. 197–212, 2016.
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