Effects of micronized-roasted coffee concentration and temperature process on technological properties of rice-based extruded

Efeitos da concentração do café torrado micronizado e temperatura de processo nas propriedades tecnológicas de extrusados à base de arroz

Efectos de la concentración de café tostado micronizado y de la temperatura del proceso sobre las propiedades tecnológicas de los extruidos a base de arroz

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Abstract

New ingredients have been used in extruded products to increase the healthiness and regionalization of these products. However, the process variables that can interfere with the technological quality of the product should be studied, aimed at good acceptance by consumers. This study aimed to evaluate the effects of the concentration of micronized roasted coffee (MRC) and the barrel temperature on the technological properties of rice-based extrudates. The extrudates were made with 3 and 8% MRC to replace rice flour and processed in a mono-extruder at 140 and 180 °C. They were characterized for color, expansion index, hardness, bowl-life, porosity, water absorption index, and solubility index, and paste properties. To assess the effects of the process variables, analysis of variance, and Scott-Knott test (p <0.05) were applied to compare the means. The increase in MRC concentration reduced the color parameters and hardness, while the increase in temperature affected the expansion index. A joint effect of the variables concentration and temperature was observed for the other properties evaluated. The study showed that MRC is a potential source of fibers and natural pigments, with a direct effect on the main technological properties of the final product.

Keywords: Coffee; Extrusion cooking; Physical process; Technological properties.

Resumo

Novos ingredientes em produtos extrusados estão sendo inseridos para aumentar a saudabilidade e a regionalidade destes produtos. Entretanto, para se obter um produto com boa aceitação por parte dos consumidores, é necessário compreender primeiro quais variáveis de processo podem interferir na qualidade tecnológica do mesmo. Este trabalho teve como objetivo avaliar os efeitos da concentração de café torrado e micronizado (MRC) e da temperatura nas propriedades tecnológicas de extrusados à base de arroz. Os extrusados foram elaborados com 3 e 8% MRC em substituição à farinha de arroz e processados em extrusora monorrosca a 140 e 180 °C. Estes foram avaliados quanto à cor, índice de expansão, dureza, bowl-life, porosidade, índices de absorção e solubilidade em água e propriedades de pasta. Para avaliar os efeitos das variáveis de processo foi aplicada análise de variância e teste Scott-Knott (p<0.05) para comparação das médias. O aumento da concentração de café reduziu os valores dos parâmetros de cor e a dureza, já o aumento da temperatura influenciou na expansão. Para as demais propriedades avaliadas, as duas variáveis influenciaram em conjunto. O estudo mostrou que MRC é fonte potencial de fibras e de pigmentos naturais, apresentando uma influência direta nas principais propriedades tecnológicas do produto final.

Palavras-chave: Café; Extrusão termoplástica; Processo físico; Propriedades tecnológicas.
Resumen
Nuevos ingredientes vienen siendo adicionados en productos extruidos a fin de aumentar su salubridad y regionalidad. Sin embargo, para obtener un producto con una buena aceptación de parte de los consumidores, primero es necesario evaluar los efectos de la concentración de café tostado y micronizado (MRC) y de la temperatura en las propiedades tecnológicas de los extruidos a base de arroz. Los extrusados fueron elaborados con 3 y 8% de MCR como sustituto de la harina de arroz, y después fueron procesados en extrusora mono-tornillo a 140 y 180°C. Se evaluaron sus características como el color, índice de expansión, dureza, bowl-life, porosidad, índices de absorción y solubilidad en agua, y propiedades de pasta. Para evaluar los efectos de las variables de proceso fue aplicado el análisis de varianza y test de Scott-Knott (p<0.05) de comparaciones múltiples. El aumento de la concentración de café redujo los valores de los parámetros de color y dureza, mientras que el aumento de la temperatura influyó en la expansión. En las demás propiedades evaluadas, las dos variables influyeron en conjunto. El estudio mostró que MRC es una fuente potencial de fibras y pigmentos naturales, que tiene una influencia directa en las principales propiedades tecnológicas del producto final.

Palabras clave: Café; Extrusión termoplástica; Proceso físico, Propiedades tecnológicas.

1. Introduction

Coffee is one of the main raw materials produced in Brazil, which is the world’s largest producer and exporter (ICO, 2020). Due to its unique sensory characteristics, coffee is present in the daily lives of millions of people around the world. The popularity of coffee is also based on its health benefits. Coffee has been extensively studied for its chemical composition and functional properties, being a natural source of fibers and antioxidant compounds (Pereira et al., 2020). Although coffee is mostly consumed as a beverage, it can also be a potential ingredient for extruded cereal products.

There is a growing concern for healthier eating, which has become more evident with the Covid-19 pandemic (Euromonitor, 2020). Ready-to-eat extruded products, such as extrudates and snacks, can be a practical alternative to meet everyday life demands. The insertion of coffee into these products can provide a combination of flavour and healthiness, which are, in that order, the first two factors that consumers understand by “eating well”, as reported by The Food Market Institute (2019).

However, the incorporation of new ingredients into cereal-based extruded products is still a challenge. New ingredients can negatively alter the technological characteristics of the final product, influencing the consumers’ acceptance (Shah et al., 2019). Therefore, the effects of the parameters involved in the extrusion process should be studied to provide a quality product from the physicochemical and sensory point of view (Obradović et al., 2014).

Response surface methodology has been used as a statistical tool to study the introduction of new ingredients. However, regression models are effective only within the experimental range of the variables, without extrapolation (Dean et al., 2017). Therefore, preliminary experiments are necessary to find the most important variables and the appropriate intervals to determine the experimental design and optimization (Eerikainen & Linko, 1989).

The intervals of these factors must be wide and proportional enough to determine the actual effects of each variable to obtain the best responses for the dependent variables. In this way, this study aimed to evaluate the effect of micronized-roasted coffee concentration and barrel temperature on the technological properties of rice-based extruded products.

2. Materials and Methods

2.1 Raw materials and micronized-roasted coffee (MRC) preparation

Rice flour (RF) was provided by SL Alimentos (Mauá da Serra, Brazil), and green coffee (Coffea arabica) by Ipanema Coffees (Alfenas, Brazil). Green coffee beans were subjected to a medium roasting process for 180 °C at 15 min. After the treatment, the coffee was ground until reaching a particle size of 150 µm and subsequently stored in vacuum plastic bags at -18 °C.
The RF and the micronized-roasted coffee (MRC) presented, respectively, the following average composition (g/100 g sample) on a dry basis: 0.69±0.02 and 4.40±0.01 ash, 1.11±0.01 and 13.28±0.28 crude fat, 10.28±0.18 and 14.63±0.15 protein, 0.00±0.00 g and 56.53±0.77 total dietary fibers, and 87.93±0.18 and 11.17±0.77 digestible carbohydrates.

2.2 Extrusion cooking

The extrusion was conducted using a single screw extruder (Brabender, Duisburg, GNF), keeping constant the compression ratio (3:1), die diameter (3 mm), screw speed (120 rpm), blend moisture (16%), and temperatures of the first zone (70 °C) and the second zone (120 °C). Different MRC concentrations (3 and 8% w/w) and different barrel temperature of the third zone (140 and 180 °C) was varied (Table 1), based on the fiber content of blends and process temperature used to produce directly expanded products. After the thermal process, the extrudates were immediately transferred to an oven at 50 °C until the moisture reached below 6%. The products were then stored in plastic bags for further analysis.

Table 1. Experimental design of rice flour-micronized-roasted coffee extruded.

| Assays | RF:MRC (%) | Temperature (°C) |
|--------|------------|------------------|
| C3-140 | 97:3       | 140              |
| C3-180 | 97:3       | 180              |
| C8-140 | 92:8       | 140              |
| C8-180 | 92:8       | 180              |

Source: Authors.

2.3 Technological properties of extruded products

2.3.1 Expansion index (EI)

Ten random extrudate samples from each treatment were subjected to diameter measurements using a Craftsman caliper. The EI was determined by the ratio between the diameter of the extrudate and the diameter of the die (Faubion & Hoseney, 1986).

2.3.2 Hardness

The hardness was determined using a TA-XT2i texture analyzer (Stable Micro Systems Ltd., Godalming, Surrey, U.K.) with a Warner-Bratzler shear blade with a ‘‘V’’ shape probe (Paula & Conti-Silva, 2014). The extrudates were cut to 5 cm in length, and the test conditions were probe distance of 20 mm, pre-test speed of 2 mm/s, test speed of 1 mm/s, and post-test speed of 1 mm/s. The hardness was defined as the peak force (N) required to rupture the sample, and the results were represented by an average of ten measurements.

2.3.3 Bowl-life

The bowl-life was determined according to Oliveira et al. (2017). The extrudates were immersed in 100 mL of whole milk at 10 °C for 3 minutes and then drained for 10 seconds. After that, the analysis was conducted in the same conditions described in item 2.3.2.
2.3.4 Cross-section images analysis

The images of extrudates were evaluated according to Oliveira et al. (2015). The extrudates were cut (n=10) in half using a Stanley knife. The images of cross-sections of the extrudates were captured using a scanner equipped with the HP PrecisoScan software version Pro 3.1 (HP Scanjet 4400C, Hewlett-Packard, USA), using a black background paper. Diameter (mm), perimeter (mm), area (mm²), the circularity of the particles (0-1), and porosity (%) were determined, and the mean values were subjected to statistical analysis.

2.3.5 Instrumental color

The color of raw materials and extrudates was determined using a MiniScan HUNTERLAB CR-400 spectrophotometer (Konica Minolta Sensing Americas), according to the CIELab system. L* represents the lightness of the sample, with values between 0 (black) and 100 (white), a* and b* representing the color ranging from red (+a*) to green (-a*) and from yellow (+b*) to blue (-b*), respectively. The illuminant D65 was used, and the readings were performed in triplicate at three different points, and the values were expressed as averages.

2.3.6 Water absorption index (WAI) and water solubility index (WSI)

The water absorption and solubility indices were determined according to (Anderson, 1982). Initially, the extrudates were ground until reaching a particle size of 60 mesh. Then, 2.5 g was suspended in 30 mL of distilled water in a centrifuge tube. The suspension was stirred for 30 minutes intermittently and centrifuged for 10 min at 3000 x g. The supernatant was transferred to an aluminum plate and dried in an air circulation oven at 105 °C for 4 hours. The WAI corresponded to the ratio of the weight of the centrifuged residue to the initial weight of the sample. The WSI corresponded to the ratio of the weight of the evaporated residue to the initial weight of the sample, in percentage. All determinations were carried out in triplicate, and the results were expressed on a dry basis.

2.3.7 Pasting properties

The pasting viscosity was determined using the Rapid Visco Analyzer (RVA 4500, Perten Instruments, Australia) and the software Thermocline for Windows, according to the following procedures (AACCI, 2010): the suspension was heated from 25 to 95 °C at 14 °C/min (after equilibrium for 2 min at 25 °C), held at 95 °C for 5 min, and cooled at 14 °C/min to 25 °C, totaling 20 min of analysis. The parameters evaluated were: cold peak viscosity, raw peak viscosity, hold peak viscosity, breakdown viscosity, final viscosity, and setback viscosity. All determinations were performed in triplicate.

2.4. Data analysis

The technological characterization of the extrudates was evaluated by analysis of variance (ANOVA) at a 5% level of significance, using the Scott-Knott test to compare means through software SISVAR (version 5.6).

3. Results and Discussion

3.1 Expansion index (EI)

The expansion index is one of the most important physical characteristics of extruded products and is related to the formation of air bubbles that generate a porous, expanded, and sponge-like structure (Bouvier & Campanella, 2014). Significant differences (p <0.05) were observed between the treatments, with EI ranging between 2.65 and 3.05 (Table 2). The graphs (Figure 1) and the ANOVA table for main effects (Table 3) showed a significant effect (p<0.05) of the temperature and the interaction concentration X temperature.
Concerning the barrel temperature, a greater difference was observed at 140 °C for both MRC concentrations, with a greater EI for the concentration of 8% (Figure 1). However, this behavior changed with increasing the temperature to 180 °C, and the EI values were statistically equal, regardless of the MRC concentration. The expansion index of the extrudates can be improved by increasing the temperature to an ideal point followed by a decrease, and the peak temperature depends on the chemical composition of the blends (Bouvier & Campanella, 2014).

Table 2. Technological properties of rice-micronized-roasted coffee extrudates.

| Properties                  | Assays       |
|-----------------------------|--------------|
|                             | C3-140       | C3-180       | C8-140       | C8-180       |
| Expansion index             | 2.70 ± 0.24b | 2.77 ± 0.27b | 3.05 ± 0.18c | 2.65 ± 0.24b |
| Hardness (N)                | 30.43 ± 3.96a| 27.06 ± 3.62a| 22.76 ± 3.87b| 22.77 ± 3.23b|
| Bowl-life (N)               | 22.18 ± 2.10ns| 22.95 ± 2.77ns| 21.11 ± 2.09ns| 22.94 ± 3.47ns|
| Cross-section               |              |              |              |              |
| Diameter (mm)              | 7.80 ± 0.22a | 8.00 ± 0.23a | 6.79 ± 0.30c | 7.36 ± 0.12b |
| Perimeter (mm)             | 26.17 ± 0.62a| 26.32 ± 0.75a| 23.13 ± 0.80c| 24.02 ± 0.52b|
| Area (mm²)                 | 49.23 ± 2.37a| 50.22 ± 2.82a| 38.52 ± 2.94c| 41.92 ± 1.75b|
| Extruded circularity       | 0.90 ± 0.01n.s.| 0.90 ± 0.02n.s.| 0.91 ± 0.01n.s.| 0.91 ± 0.02n.s.|
| Cell circularity           | 0.36 ± 0.08a | 0.30 ± 0.07b | 0.26 ± 0.07b | 0.30 ± 0.09b |
| Porosity (%)               | 44.48 ± 3.19n.s.| 47.39 ± 7.03n.s.| 52.68 ± 6.50n.s.| 50.92 ± 11.81n.s.|
| Color                      |              |              |              |              |
| L*                         | 68.16 ± 0.22a| 67.04 ± 0.71a| 64.82 ± 0.66b| 61.90 ± 0.52c|
| a*                         | 6.32 ± 0.09d | 6.65 ± 0.17c | 7.09 ± 0.20b | 7.72 ± 0.09a |
| b*                         | 19.67 ± 0.07n.s.| 19.57 ± 0.20n.s.| 19.34 ± 0.25n.s.| 19.03 ± 0.22n.s.|
| WAI                        | 7.57 ± 0.09a | 6.19 ± 0.03b | 6.40 ± 0.56b | 5.83 ± 0.03b |
| WSI (%)                    | 4.36 ± 0.41b | 5.51 ± 0.02a | 5.64 ± 0.31a | 5.61 ± 0.01a |

1 Values are means ± standard deviations of triplicate trials. Means with different letters within the same line are significantly different by Scott-Knott test (p<0.05). ns–not significant.
Source: Authors.
Figure 1. Effects of MRC concentration and process temperature on technological properties of rice-based extrudates.

Robin et al. (2012) reported that fibers can form a matrix with starch and water, leading to the starch dilution or breakage of the bubble wall. In the present study, the bubbles did not reach their maximum growth and suffered a premature collapse, resulting in a product with less expansion index due to the presence of MRC. This trend was also observed in rice and roasted coffee blends (Silva et al., 2013) and sorghum and roasted coffee blends (Chávez et al., 2017).

However, a higher EI was observed for C8-140, probably due to the interaction concentration X temperature; once roasted coffee, in addition to insoluble fibers, also has a significant concentration of soluble fibers that favors expansion (Robin et al. 2012). As reported by Silván et al. (2010), soluble fibers content in coffee can present a mean value of 64.9 mg/100g. The micronization processing of coffee may also have favored the formation of soluble fibers through the physical disruption of the molecular structure of insoluble fibers, as was also reported by Zhu et al. (2014) in the micronization of buckwheat hulls.

3.2 Hardness

The hardness of the expanded extrudates is a noticeable and striking attribute for consumers, with an essential role in this type of product. It is correlated with the expansion and the cellular structure of the product (Dalbhagat et al., 2019) once the porosity and uniformity of the air bubbles formed in the extrusion can increase or reduce hardness (Ding et al., 2005). In addition to the process parameters, the chemical composition of the ingredients also interferes with this property, as also observed for EI (Bouvier & Campanella, 2014).

A significant difference in the texture parameters was observed between treatments (p <0.05) (Table 2), with a significant effect of the MRC concentration, as shown in the results of ANOVA (Table 3). In spite of the known negative impact of insoluble fiber on extrudate hardness, Figure 1 shows that the increase in MRC concentration reduced the hardness values. According to Riaz & Rockey (2012), the smaller particle size of the raw material containing fiber can reduce the negative impacts on this property. Also, Robin et al. (2012) reported that increasing the contact surface between fiber and starch can improve the physicochemical compatibility between them, directly affecting the expansion index and texture of the final product.
### Table 3. Analysis of variance (ANOVA) of the technological properties of rice-micronized-roasted coffee extrudates.

| Parameters         | Source    | SS       | df | MS       | F-value  | P       |
|--------------------|-----------|----------|----|----------|----------|---------|
| Expansion index    | Intercept | 311.92   | 1  | 311.92   | 5703.64  | <0.0000*|
|                    | C         | 0.13     | 1  | 0.13     | 2.42     | 0.1287  |
|                    | T         | 0.27     | 1  | 0.27     | 4.98     | 0.0319* |
|                    | C*T       | 0.55     | 1  | 0.55     | 10.10    | 0.0030* |
|                    | Error     | 1.97     | 36 | 0.06     |          |         |
| Hardness           | Intercept | 39684.93 | 1  | 39684.93 | 818.756  | <0.0000*|
|                    | C         | 1032.02  | 1  | 1032.02  | 21.29    | <0.0000*|
|                    | T         | 38.02    | 1  | 38.02    | 0.78     | 0.3796  |
|                    | C*T       | 10.22    | 1  | 10.22    | 0.21     | 0.6479  |
|                    | Error     | 2714.30  | 56 | 48.47    |          |         |
| Bowl-life          | Intercept | 13941.07 | 1  | 13941.07 | 3812.57  | <0.0000*|
|                    | C         | 0.42     | 1  | 0.42     | 0.12     | 0.7368  |
|                    | T         | 12.28    | 1  | 12.28    | 3.36     | 0.0794  |
|                    | C*T       | 13.61    | 1  | 13.61    | 3.72     | 0.0656  |
|                    | Error     | 87.76    | 24 | 3.66     |          |         |
| Diameter           | Intercept | 2241.68  | 1  | 2241.68  | 4297.04  | <0.0000*|
|                    | C         | 6.75     | 1  | 6.75     | 129.45   | <0.0000*|
|                    | T         | 1.47     | 1  | 1.47     | 28.08    | <0.0000*|
|                    | C*T       | 0.33     | 1  | 0.33     | 6.40     | 0.0159* |
|                    | Error     | 1.88     | 36 | 0.05     |          |         |
| Perimeter          | Intercept | 24823.21 | 1  | 24823.21 | 5312.23  | <0.0000*|
|                    | C         | 71.26    | 1  | 71.26    | 152.49   | <0.0000*|
|                    | T         | 2.70     | 1  | 2.70     | 5.77     | 0.0216* |
|                    | C*T       | 1.39     | 1  | 1.39     | 2.97     | 0.0933  |
|                    | Error     | 16.82    | 36 | 0.47     |          |         |
| Area               | Intercept | 80892.22 | 1  | 80892.22 | 17288.51 | <0.0000*|
|                    | C         | 903.74   | 1  | 903.74   | 142.87   | <0.0000*|
|                    | T         | 48.13    | 1  | 48.13    | 7.61     | 0.0091* |
|                    | C*T       | 14.60    | 1  | 14.60    | 2.31     | 0.1374  |
|                    | Error     | 227.71   | 36 | 6.33     |          |         |
| Extrudate circularity | Intercept   | 32.91  | 1  | 32.91  | 117619.55 | <0.0000*|
|                    | C         | 0.00     | 1  | 0.00    | 0.13     | 0.7216  |
|                    | T         | 0.00     | 1  | 0.00    | 2.83     | 0.1011  |
|                    | C*T       | 0.00     | 1  | 0.00    | 0.01     | 0.9401  |
|                    | Error     | 0.01     | 36 | 0.00     |          |         |
| Cell circularity   | Intercept | 3.69     | 1  | 3.69    | 571.21   | <0.0000*|
|                    | C         | 0.03     | 1  | 0.03    | 4.03     | 0.0523  |
|                    | T         | 0.00     | 1  | 0.00    | 0.42     | 0.5194  |
|                    | C*T       | 0.03     | 1  | 0.03    | 4.20     | 0.0476* |
|                    | Error     | 0.23     | 36 | 0.01     |          |         |
| Porosity           | Intercept | 95512.12 | 1  | 95512.12 | 1583.46  | <0.0000*|
|                    | C         | 343.95   | 1  | 343.95  | 5.70     | 0.0223* |
|                    | T         | 3.33     | 1  | 3.33    | 0.06     | 0.8155  |
|                    | C*T       | 54.45    | 1  | 54.45   | 0.90     | 0.3484  |
|                    | Error     | 2171.48  | 36 | 60.32    |          |         |
L*  Intercept  51452.87  1  51452.87  110260.10  <0.0000*  
  C  53.98  1  53.98  115.67  <0.0000*  
  T  2.46  1  2.46  5.27  0.0509  
  C*T  12.26  1  12.26  26.28  0.0009*  
  Error  3.73  8  0.47  

a*  Intercept  578.94  1  578.94  18511.12  <0.0000*  
  C  2.55  1  2.55  81.48  <0.0000*  
  T  0.06  1  0.06  2.02  0.1933  
  C*T  0.70  1  0.70  22.25  0.0015*  
  Error  0.25  8  0.03  

b*  Intercept  4518.65  1  4518.65  76749.86  <0.0000*  
  C  0.56  1  0.56  9.57  0.0148*  
  T  0.13  1  0.13  2.18  0.1784  
  C*T  0.03  1  0.03  0.54  0.4818  
  Error  0.47  8  0.06  

WAI  Intercept  698.16  1  698.16  4174.24  <0.0000*  
  C  1.77  1  1.77  10.60  0.0069*  
  T  5.11  1  5.11  30.53  0.0001*  
  C*T  0.39  1  0.39  2.31  0.1542  
  Error  2.0071  12  0.17  

WSI  Intercept  448.43  1  448.43  2986.69  <0.0000*  
  C  0.91  1  0.91  6.04  0.0302*  
  T  1.22  1  1.22  8.09  0.0147*  
  C*T  0.63  1  0.63  4.16  0.0639  
  Error  1.80  12  0.15  

*Significant at p<0.05; SS: sum of square; df: Degrees of freedom; MS: mean of square. Source: Authors.

3.3 Bowl-life

Extrudates, when immersed in milk, change texture due to the sudden water absorption, losing its brittle texture, and becoming soaked. The ability of the extrudate to hydrate is correlated with the heat treatment used in the process, as different temperatures provide different degrees of starch gelatinization, resulting in different water absorption rates and softening of the product (Sacchetti et al., 2005).

The bowl-life values ranged between 21.11–22.94 N, with no significant differences (p<0.05) between the formulations (Table 2), and with no effects of the process variables and their interactions (Table 3). For extruded foods, the initial texture and the texture after immersion in milk should remain similar, with minimal loss of structure during the immersion period, to ensure good crispness characteristics while chewing the product. When comparing the initial hardness and hardness after immersion in milk, the treatments with 8% of MRC showed close values, with a reduction of 6.5%, demonstrating that at this MRC concentration, it is possible to achieve a stable product with low hydration. For the other treatments, C3-140 and C3-180, a reduction in hardness of 26.9 and 15.0% were observed, respectively, probably due to the higher starch content of these formulations.

3.4 Cross-section images analysis

The image analysis of the cross-section of the extrudates showed a significant effect (p <0.05) of the concentration and temperature for most of the parameters analyzed, except for the circularity of the extrudate.
The diameter varied between 6.79 and 8.00 mm, with a significant difference between the averages (Table 2), and significant effects of temperature, MRC concentration, and the interaction between these factors. The treatments C8-140 and C8-180 had the smallest diameters. It is known that starch has better expansion properties during extrusion, with a tendency to reduce the diameter of the extrudates when fibers replace starch. This behavior was also observed by Oliveira et al. (2015) when incorporating whole grain wheat flour in corn extrudates with jabuticaba powder.

At a process temperature of 180 °C, the extrudates had significantly larger diameters when compared to those subjected to 140 °C (Table 2, Figure 2). The increase in temperature favored rapid water evaporation, increasing the internal pressure in the extrudates, leading to expansion. Similar behavior was observed for the perimeter and area of the extrudates. Although no significant differences were observed between the porosity of the extrudates, the MRC concentration had a marked effect on this property (Table 3). A tendency towards greater porosity was observed in the treatments with the addition of 8% MRC. Robin et al. (2012) reported that fibers can change the size of the air cells, leading to an increase in cell wall thickness, which can explain the changes in the circularity of air bubbles (Table 2).

**Figure 2.** Effects of MRC concentration and process temperature on cross section parameters of rice-based extrudates.

### 3.5 Instrumental color

The color of the extruded product plays an important role in consumers’ acceptance and is largely affected by the composition of the food matrix and the process conditions (Dalbhagat et al., 2019). RF presented white color ($L^* = 96.2 \pm 0.14$;...
a* = -0.37 ± 0.02; b* = 5.5 ± 0.06) corroborating with the literature due to the polishing process of rice grains (Becker et al., 2014), while MRC presented luminosity below 50 (L* = 43.3 ± 0.39; a* = 10.99 ± 0.07; b* = 15.42 ± 0.12). The low luminosity of roasted coffee is due to the roasting process, with the occurrence of the Maillard reaction, and formation of melanoidins, loss of dry matter, and water evaporation from the grains (Spiller, 1998).

The color results of the extrudates are shown in Table 2, with no significant differences observed only for the coordinate b*. Significant differences were observed for the parameters L* (concentration and interaction), a* (concentration and interaction), and b* (concentration) (Table 3). A significant effect of the MRC concentration was expected due to its characteristic color, which affected the color parameters of the extrudates (Figure 3).

![Figure 3. Color of the final products obtained with rice flour and micronized-roasted coffee.](source)

For luminosity, the highest values were obtained for the extrudates with 3%, as expected. An increase in process temperature decreased L* of the treatment made with 8% MRC (Figure 4). This reduction may be due to the synergistic effect between high temperature and MRC concentration, degrading the bioactive compounds in the extrudate and producing other compounds with a darker color. Borah et al. (2016) also reported that the Maillard reaction may have favored the reduction of color parameters in rice-seeded banana and carambola pomace blends.

![Figure 4. Effects of MRC concentration and process temperature on color parameters of extrudates.](source)

3.6 Water absorption index (WAI) and water solubility index (WSI)

The WAI indicates the degree of integrity of the starch granule, reflecting the severity of the heat treatment. The loss of the starch structure during the extrusion process leads to the formation of hydrophilic groups available to bind to water molecules, resulting in a reduction in the water absorption capacity (Bouvier & Campanella, 2014). In the present study, WAI ranged from 5.86 to 7.66, with significant differences (p < 0.05) between the extrudates and a significant effect (p < 0.05) of the temperature and MRC concentration (Table 3). Figure 1 shows a reduction of WAI with increasing the temperature and the MRC concentration.
Altan et al. (2008) also observed a reduction in WAI of barley-tomato pomace blends with the increase in temperature. During the extrusion, the high temperature can degrade starch molecules, reducing their ability to absorb water, which is improved with a high degree of starch dextrinization (Bouvier & Campanella, 2014).

The increase in the MRC concentration also reduced the water absorption, probably due to the presence of fibers, less starch availability, and competition of the fibers with the starch for the water available in the system, thus preventing the swelling of the granules. This behavior has already been reported by Robin et al. (2012), and Chávez et al. (2017) in extruded snacks made with sorghum flour and roasted coffee powder.

WSI is used as an indicator of molecular degradation as it measures the amount of soluble compounds released from starch after the extrusion. A high WSI can indicate a good starch digestibility, as it implies the extension of gelatinization and dextrinization (Bouvier & Campanella, 2014). In the present study, WSI varied from 4.58 to 5.61%, with a significant difference (p <0.05) between the treatments (Table 2). Also, WSI had a significant effect (p <0.05) for temperature and MRC concentration (Table 3). Although an increase in WSI was observed with the increase in temperature and MRC concentration, the effect of temperature was more evident for the samples containing higher MRC concentration.

Mesquita et al. (2013) and Taverna et al. (2012) reported that high temperatures led to an increase in WSI of cassava extrudates with flaxseed, and cassava extrudates with quinoa, respectively. The authors pointed out that in addition to starch gelatinization, which results in the release of amylose and amylopectin, dextrinization and other reactions that lead to the formation of low molecular weight compounds can also occur, affecting WSI. Pardhi et al. (2019) observed an increase in WSI in brown rice extrudates with the increase in extrusion temperature.

3.7 Pasting properties

The results of the pasting properties allow evaluating the impact of the thermoplastic extrusion on the formulations, which are dependent on the degree of gelatinization and rupture of the starch granule. Figure 5 and Table 4 presents the viscosity profile and the results of this parameter, with significant differences between them (p<0.05).

**Figure 5.** Viscosity profile of extrudates containing RC and MRC at different concentrations and process temperature.
Table 4. Pasting properties of rice-micronized-roasted coffee extrudates.

| Parameters (cP) | Assays       |       |       |       |
|----------------|--------------|-------|-------|-------|
|                | C3-140       | C3-180| C8-140| C8-180|
| Cold peak      | 936.00 ± 57.24<sup>a</sup> | 811.67 ± 70.71<sup>b</sup> | 824.33 ± 44.24<sup>b</sup> | 629.67 ± 25.11<sup>c</sup> |
| Raw peak       | 886.00 ± 11.79<sup>a</sup> | 721.33 ± 7.37<sup>d</sup> | 797.67 ± 2.31<sup>c</sup> | 852.00 ± 12.17<sup>b</sup> |
| Hold peak      | 614.33 ± 4.04<sup>a</sup> | 465.67 ± 4.73<sup>d</sup> | 525.67 ± 2.89<sup>c</sup> | 536.00 ± 5.57<sup>b</sup> |
| Breakdown      | 271.67 ± 7.77<sup>b</sup> | 255.67 ± 4.51<sup>c</sup> | 272.00 ± 2.65<sup>b</sup> | 316.00 ± 8.19<sup>a</sup> |
| Final viscosity| 1094.67 ± 4.93<sup>a</sup> | 864.67 ± 5.51<sup>c</sup> | 946.00 ± 2.65<sup>b</sup> | 944.33 ± 13.20<sup>b</sup> |
| Setback        | 480.33 ± 1.53<sup>b</sup> | 399.00 ± 8.54<sup>c</sup> | 420.33 ± 4.51<sup>b</sup> | 408.33 ± 8.14<sup>c</sup> |

<sup>1</sup>Values are means ± standard deviations of triplicate trials. Means with different letters within the same line are significantly different by Scott-Knott test (p<0.05). ns–not significant.

Source: Authors.

Significant effects (p <0.05) were observed for concentration, temperature, and the interaction between them for all pasting properties studied, except for the cold peak viscosity (concentration and temperature) (Table 5). The cold peak viscosity indicates the ability of the extruded flour to absorb water at room temperature (25 °C), allowing to evaluate the degree of cooking through starch gelatinization and dextrinization caused by the friction between the dough and the screw (Clerici et al., 2019). Despite the higher WSI discussed earlier, severe process conditions and the presence of fibers can lead to a reduction in cold peak viscosity once they do not provide enough viscous material, limiting the starch gelatinization (Robin et al., 2012).
Table 5. Analysis of variance (ANOVA) of the pasting properties of rice-micronized-roasted coffee extrudates.

| Parameters      | Source    | SS            | df | MS       | F-value | P      |
|-----------------|-----------|---------------|----|----------|---------|--------|
| Cold peak       | Intercept | 7688002.08    | 1  | 7688002.08 | 2830.63 | <0.0000* |
|                 | C         | 64680.08      | 1  | 64680.08  | 23.81   | 0.0012* |
|                 | T         | 76320.75      | 1  | 76320.75  | 28.10   | 0.0007* |
|                 | C*T       | 3710.08       | 1  | 3710.08   | 1.37    | 0.2761 |
|                 | Error     | 21728.00      | 8  | 2716.00   |         |        |
| Raw peak        | Intercept | 7956036.75    | 1  | 7956036.75 | 91800.42 | <0.0000* |
|                 | C         | 1344.08       | 1  | 1344.08   | 15.51   | 0.0043* |
|                 | T         | 9130.08       | 1  | 9130.08   | 105.35  | <0.0000* |
|                 | C*T       | 35970.75      | 1  | 35970.75  | 415.05  | <0.0000* |
|                 | Error     | 693.33        | 8  | 86.67     |         |        |
| Hold peak       | Intercept | 3440052.08    | 1  | 3440052.08 | 176412.93 | <0.0000* |
|                 | C         | 252.08        | 1  | 252.08    | 12.93   | 0.0070* |
|                 | T         | 14352.08      | 1  | 14352.08  | 736.00  | <0.0000* |
|                 | C*T       | 18960.75      | 1  | 18960.75  | 972.35  | <0.0000* |
|                 | Error     | 155.99        | 8  | 19.49     |         |        |
| Breakdown       | Intercept | 932976.33     | 1  | 932976.33 | 24128.70 | <0.0000* |
|                 | C         | 2760.33       | 1  | 2760.33   | 71.39   | <0.0000* |
|                 | T         | 588.00        | 1  | 588.00    | 15.21   | 0.0045* |
|                 | C*T       | 2700.00       | 1  | 2700.00   | 69.83   | <0.0000* |
|                 | Error     | 309.33        | 8  | 38.67     |         |        |
| Final viscosity | Intercept | 11114950.08   | 1  | 11114950.08 | 188388.98 | <0.0000* |
|                 | C         | 3570.75       | 1  | 3570.75   | 60.52   | 0.0001* |
|                 | T         | 40252.08      | 1  | 40252.08  | 682.24  | <0.0000* |
|                 | C*T       | 39102.08      | 1  | 39102.08  | 662.75  | <0.0000* |
|                 | Error     | 471.99        | 8  | 59        |         |        |
| Setback         | Intercept | 2187948.00    | 1  | 2187948.00 | 54023.41 | <0.0000* |
|                 | C         | 1925.33       | 1  | 1925.33   | 47.54   | 0.0001* |
|                 | T         | 6533.33       | 1  | 6533.33   | 161.32  | <0.0000* |
|                 | C*T       | 3605.33       | 1  | 3605.33   | 89.02   | <0.0000* |
|                 | Error     | 324.00        | 8  | 40.50     |         |        |

*Significant at p<0.05; SS: sum of square; df: Degrees of freedom; MS: mean of square. Source: Authors.

The loss of the starch granule structure reduces the swelling capacity during heating, presenting low viscosity at 95 °C. However, a raw peak viscosity higher or similar to cold peak viscosity indicates the existence of intact starch granules or partially preserved starchy structure (Bouvier & Campanella, 2014). This result can be seen in the viscosity profile of the samples (Figure 5) and in the findings of Chávez et al. (2017). The existence of intact granules may be associated with a significant plasticizer concentration, such as the lipids in raw materials, which prevent starch degradation or provide a low shear rate (Bouvier & Campanella, 2014).

When the maximum rupture of the available starch granules is reached by stirring the medium at a constant temperature, there is a decrease in viscosity. However, the increase in the MRC concentration increased both raw peak and hold peak viscosities (Figure 6) for the treatments at 180 °C, probably due to the contribution of fibers in the preserved starchy structure that still present the swelling capacity.
Figure 6. Effects of MRC concentration and process temperature on pasting properties of extrudates.

Breakdown refers to the stability of starch paste to heating and mechanical shear while setback viscosity, refers to the behavior of starch during cooling by the recrystallization of the amylose and amyllopectin chains through hydrogen bonds, leading to the formation of precipitates and syneresis, with an increase in final viscosity (Clerici et al., 2019). An increase in breakdown and reduction of setback viscosity values was observed for the formulations made with 8% of MRC (Figure 5). This behavior is a consequence of the variation in the starch and fiber ratio of the formulations, with the effect of the concentration being more noticeable for breakdown viscosity of C8-140 and C8-180, while the temperature more significantly affected the setback viscosity of C3-140 and C3-180.

Although the final viscosity ($V_{\text{final}}$) is related to the moisture and the temperatures used in the extrusion process, the screw speed, the particle size, and the proximate composition of the raw material can also affect this parameter (Clerici et al., 2019). WAI is also associated with $V_{\text{final}}$, as a high absorption rate leads to a higher $V_{\text{final}}$ (Bouvier & Campanella, 2014). Due to the estimated WAI values for the treatments (Table 2), a reduction in the final viscosity between C3-140 and C3-180 was expected, as well as the maintenance of the final viscosity between C8-140 and C8-140.

4. Conclusion

The partial replacement of micronized-roasted coffee by rice flour affected the technological properties of the extrudates, especially the color, expansion index, and texture parameters, due to the presence of fibers and color compounds from the raw material, as a result of coffee roasting and the Maillard reaction during thermoplastic extrusion. The effect of
temperature was more significant for water absorption and solubility indexes, while the other parameters were affected by the combination of temperature and MRC concentration, such as expansion index.

The results showed that the C8-140 and C8-180 assays presented technological characteristics suitable for an expanded extruded product. They showed similar expansion to the assays with 3% MRC, with lower hardness and stability in water absorption and bowl-life. At this concentration, there may be a greater sensory acceptance for the probable contribution to the flavour. I any case, sensory attributes should be investigated. As for the process temperatures, the next step would be to study the retention of bioactive compounds.

Therefore, understanding the factors that interfere in producing ready-to-eat extruded products with MRC makes it possible to perform a better process optimization, resulting in a product with technological and sensory characteristics more accepted by consumers looking for a healthier and more pleasurable diet.

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