Trajectory Tracking Control Optimization with Neural Network for Autonomous Vehicles

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1. Introduction

There have been growing demands for autonomous vehicles with excellent maneuvering capabilities both for commercial and military applications [1, 2]. Significant amount of work is ongoing to realize the commercial operation of autonomous cars [3, 4], and Wheeled Mobile Robots (WMRs) are finding increasing use in industrial and service applications [5]. Autonomous Surface Vehicles (ASV) have been utilized to improve port safety and for ecological as well as meteorological purposes [6], whereas Autonomous Underwater Vehicles (AUVs) are useful tools for underwater search and inspection [7].

Safe navigation will require both excellent path planning and path tracking strategies. Path planning involves the determination of an appropriate trajectory for the vehicle whereas path tracking, which is the focus of this study, is the following of a desired trajectory. Several schemes have been reported in the literature for path planning, including in [8], where a framework was proposed to synthesize sequences of maneuvers that are tracked using nonlinear controllers, and other strategies are presented in [9, 10]. To execute the maneuvers generated by path planners, control strategies have been proposed as well.

In [11], Fuzzy Logic Controller (FLC) was proposed for robot tracking and Proportional-Integral-Derivative (PID) controller was utilized to control the speed of WMRs in [12]. The authors of [13] presented an observer-based approach, whereas backstepping control strategy was presented in [14, 15]. Sliding-mode control for WMR trajectory tracking with initial error was reported in [16], and modular-based method was proposed in [17]. The authors of [18] proposed a Model Predictive Control (MPC) approach and Kalman filter-based strategy was presented in [19]. Lyapunov-based scheme was reported in [20] and controller design by approximate linearization utilizing Taylor expansion was proposed in [21]. In order to enhance the performance of traditional control methods, Least Square Policy Iteration (LSPI) and Dynamic Heuristic Programming (DHP) algorithms were utilized in [22] for optimizing a Proportional-Derivative (PD) controller. Also, the authors of [23] utilized neural network (NN) to describe the inverse dynamics of a biped robot with respect to output errors for the control of level walking. However, application examples were limited to scenarios where the robot is initialized at the desired starting coordinate.

In order to execute maneuvers for unmanned Air Vehicles (UAVs), feedback linearization [24, 25] and sliding mode control [26] have been proposed, but they have failed for certain models due to the nonlinear dynamics of the vehicle [27]. For helicopter control, backstepping control strategy [28] and Linear Quadratic Regulator (LQR)-based control [29] have been proposed.
In this study, a novel learning-based adaptive scheme utilizing the neural network is developed for autonomous vehicle trajectory tracking. Whereas, plant models predict the vehicular motion for a given control command, accuracy is limited by modelling errors and approximations. Also, for certain models with complex nonlinear dynamics, it is difficult to obtain a suitable controller. Since machine learning models provide a more powerful tool to describe nonlinear dynamics of a plant given example data of plant operation, this article presents a parameterized control law designed to achieve trajectory tracking of autonomous vehicles adaptively. Rather than using a single controller, a family of controllers is obtained utilizing the NN model to estimate the time varying controller parameters. The scheme was applied to optimize a Lyapunov-based nonlinear controller parameters used to execute an eight-shaped maneuver for a mobile robot. Furthermore, LQR-based controller parameters for 2-Degree-Of-Freedom (DOF) helicopter position control were optimized using the proposed scheme. Simulation results show that the scheme outperforms the traditional control strategies, not only the error varying controller parameters, but also the states and control input as the output. Hence,

\[ K(t) = f(x(t), x(t + k)) \]  

The NN model is made up of processing units called neurons with weighted interconnections among them [30], and the neurons with nonlinear activation functions are arranged into layers as shown in Figure 1.

![Feed forward neural network structure](image)

Figure 1: Feed forward neural network structure

The input layer is the vector of input variables, which are system states in the study. For a single hidden layer system, the hidden layer is a nonlinear combination of the input signals, and for multiple hidden layer system, subsequent layers are nonlinear combination of the previous layers. Knowledge is extracted from the output layer after model training. In supervised learning employed in this study, an error function based on the difference between the actual outputs called labels and the predicted outputs from the NN is minimized to adjust the interconnection weights among the neurons. After several iterations, the model is said to be trained. Whereas only a portion of the dataset is used for training, the remainder is used for testing the performance of the trained model. The mathematical description of the NN model as utilized in this study is,

\[ K^{l+1}_n = \theta(s^{l+1}_n) \]  
\[ s^{l+1}_n = w^{l+1}_n K^l + b^{l+1}_n \]

where the output vector of a layer \( l \) is denoted by \( K^l \). Hence, the input layer vector \( K^0 \) is equivalent to the state input \( \{x(t), x(t + k)\} \). The activation function is denoted by \( \theta \) and \( s^l \) represents the input vector to layer \( l \). The interconnecting weights and biases from layer \( l - 1 \) to unit \( n \) of layer \( l \) are represented by \( w^l_n \) and \( b^l_n \) respectively.

Following offline training as described above, the trained NN model is integrated as a control gain estimator in the traditional control system as shown in Figure 2.
For online control gain estimation, the NN input due to the next state \( x(t + k) \) is replaced with the reference signal \( r(t) \). Hence,

\[
K(t) = f(x(t), r(t))
\]

(6)

Then, \( (2) \) is transformed to,

\[
u(t) = f(x(t), r(t)) \ast e(t)
\]

(7)

### 3. Illustrative Examples

In order to prove the effectiveness of the proposed scheme, two application case studies are presented. One is the tracking of an eight-shaped trajectory by a mobile robot, and the other is the position tracking of a 2-DOF helicopter.

#### 3.1. Mobile Robot Trajectory Tracking

The nonlinear kinetic model [31] of a non-holonomic wheeled mobile robot is described as,

\[
\begin{bmatrix}
\dot{x} \\
y \\
\dot{\theta}
\end{bmatrix} =
\begin{bmatrix}
\cos \theta & \sin \theta & 0 \\
-\sin \theta & \cos \theta & 0 \\
0 & 0 & 1
\end{bmatrix}
\begin{bmatrix}
v \\
w
\end{bmatrix}
\]

(8)

The robot’s states \( x, y, \theta \) are the cartesian \( x, y \), and angular displacements respectively. Whereas \( \dot{x}, \dot{y}, \) and \( \dot{\theta} \) are the state derivatives, \( v \) corresponds to the linear velocity and \( w \) represents the angular velocity around the vertical axis.

#### 3.1.1. Traditional Control Design

Motion control of the mobile robot is achieved by computing appropriate linear and angular velocities to drive the robot in the desired trajectory. According to the procedure in [32], the state tracking error is generalized by defining it through a rotation matrix to obtain,

\[
\begin{bmatrix}
e_x \\
e_y \\
e_{\theta}
\end{bmatrix} =
\begin{bmatrix}
\cos \theta & \sin \theta & 0 \\
-\sin \theta & \cos \theta & 0 \\
0 & 0 & 1
\end{bmatrix}
\begin{bmatrix}
x_d - x \\
y_d - y \\
\theta_d - \theta
\end{bmatrix}
\]

(9)

where \( x_d, y_d, \) and \( \theta_d \) are the target coordinates for the robot. Then the error dynamics in generalized coordinates is obtained by taking the derivative of \( (9) \) as,

\[
\begin{bmatrix}
\dot{e}_x \\
\dot{e}_y \\
\dot{e}_{\theta}
\end{bmatrix} =
\begin{bmatrix}
0 & w_d & 0 \\
-w_d & 0 & 0 \\
0 & 0 & 0
\end{bmatrix}
\begin{bmatrix}
e_x \\
e_y \\
e_{\theta}
\end{bmatrix} +
\begin{bmatrix}
v \cos e_{\theta} - v \\
v \sin e_{\theta} \\
w_d - w
\end{bmatrix}
\]

(10)

Making the following substitutions,

\[
u_1 = v \cos e_{\theta} - v
\]

(11)

\[
u_2 = w_d - w
\]

(12)

The error dynamics is transformed to the subsequent form,

\[
\begin{bmatrix}
\dot{e}_x \\
\dot{e}_y \\
\dot{e}_{\theta}
\end{bmatrix} =
\begin{bmatrix}
0 & w_d & 0 \\
-w_d & 0 & 0 \\
0 & 0 & 0
\end{bmatrix}
\begin{bmatrix}
e_x \\
e_y \\
e_{\theta}
\end{bmatrix} +
\begin{bmatrix}
0 & e_x \\
0 & e_y \\
0 & e_{\theta}
\end{bmatrix} +
\begin{bmatrix}
0 & 1 & 0 \\
0 & 0 & 1
\end{bmatrix}
\begin{bmatrix}
u_1 \\
u_2
\end{bmatrix}
\]

(13)

To ensure global stability for the nonlinear dynamics, the following Lyapunov function is selected,

\[
V = \frac{K_2}{2} (e_x^2 + e_y^2) + \frac{e_{\theta}^2}{2}
\]

(14)

Taking the derivative of \( (14) \) gives

\[
\dot{V} = K_2 (e_x \dot{e}_x + e_y \dot{e}_y) + e_{\theta} \dot{e}_{\theta}
\]

(15)

By substituting for \( \dot{e}_x, \dot{e}_y, \) and \( \dot{e}_{\theta} \) from \( (13) \),

\[
\dot{V} = K_2 (e_x u_1 + e_y v_d \sin e_{\theta}) + e_{\theta} u_2
\]

(16)

Hence, the Lyapunov-based control law such that \( \dot{V} < 0 \) is guaranteed is obtained as,

\[
u_1 = -K_1 e_x
\]

(17)

\[
u_2 = -K_2 v_d \sin e_{\theta} e_y - K_3 e_{\theta}
\]

(18)

The controller gains are defined as,

\[
K_1(t) = K_3(t) = 2 \zeta \sqrt{w_d^2(t) + c v_d^2(t)}
\]

(19)

where \( K_2 = c > 0 \) is a constant, and \( \zeta \) is the damping ratio.

The control law defined by \( (17) \) and \( (18) \) are composed of both the feedback and feedforward signals. The feedforward commands are determined from \( (8) \) as,

\[
v_d(t) = \pm \sqrt{x_d^2(t) + y_d^2(t)}
\]

(20)

\[
w_d(t) = \frac{v_d(0)x_d(t) - x_d(t)v_d(t)}{x_d^2(t) + y_d^2(t)}
\]

(21)

\[
\theta_d(t) = atan2(y_d(t), x_d(t)) + \pi i
\]

(22)

where \( i \) is 0 or 1 for forward or backward motion respectively. The feedback commands are adaptively computed based on NN estimation as described next.

#### 3.1.2. Controller Parameter Estimation using the Neural Network

In order to optimize the controller for fast convergence to the desired trajectory and improved steady-state performance, the NN is utilized to adaptively estimate the feedback control parameters. Sample runs of the traditional closed-loop system are performed for 15 sequences of 1258 state transitions to make a total of 18870 data samples. The input features are the current state \([x(t) \ y(t) \ \theta(t)]\), the nominal velocities \([v_d(t) \ w_d(t)]\), and
the next state \([x(t+k) y(t+k) \theta(t+k)]\). The output labels are the control gains \([K_x(t) K_\varphi(t) K_\theta(t)]\) responsible for the state transition. Data was normalized and the training was implemented using the MATLAB NN tool box using 70% of the dataset. The remaining dataset was divided into 15% validation and 15% testing. The Levenberg-Marquardt algorithm [33, 34, 35] was used for training using two hidden neurons. The performance of the NN estimator was evaluated using the Mean Square Error (MSE) plot shown in Figure 3. The figure shows good generalization performance as the test error is approximately equal to that of the training.

![Figure 3: MSE of the NN estimator for robot control](image)

The trained NN estimator is integrated in the second loop of Figure 2, where a normalizer and denormalizer are embedded for better control performance. Simulation results of the adaptive closed loop control system is presented in Section 4.

### 3.2. 2-DOF Helicopter Position Control

A Two-Input-Two-Output (TITO) Quanser 2D Helicopter model [35] is considered. The linearized model is obtained in [36] as follows.

\[
\begin{bmatrix}
\dot{\theta} \\
\dot{\varphi} \\
\dot{\psi}
\end{bmatrix} =
\begin{bmatrix}
0 & 0 & 1.0000 & 0 \\
0 & 0 & 0 & 1.0000 \\
0 & 0 & -0.0315 & 0
\end{bmatrix}
\begin{bmatrix}
\theta \\
\varphi \\
\psi
\end{bmatrix}
+ \\
\begin{bmatrix}
0 & 0 \\
0 & 0 \\
0.5293 & 0.0404
\end{bmatrix}
\begin{bmatrix}
V_{mp} \\
V_{my}
\end{bmatrix}
\]

(23)

where \(\theta\) and \(\varphi\) are the pitch and yaw angles respectively. The first and second derivatives of the pitch and yaw angles are \(\dot{\theta}, \ddot{\theta}\) and \(\dot{\varphi}, \ddot{\varphi}\) respectively. The pitch and yaw propeller voltages \(V_{mp}\) and \(V_{my}\) are applied to the corresponding motors driving the propellers.

#### 3.2.1. Traditional Control Design

The pitch and yaw angles of the 2-DOF helicopter were regulated using the optimal LQR-based control design presented in [29]. And the control law was obtained as,

\[
u = K_x \dot{x}(t) - K_e e(t)
\]

(24)

The realized state feedback gains are,

\[
K_x = \begin{bmatrix}
547.8 & -2.8 & 45.7 & -4.8 \\
2.8 & 547.9 & -4.1 & 91
\end{bmatrix}
\]

(25)

and the error feedback gains were obtained as,

\[
K_e = \begin{bmatrix}
-1.000 & 0.0051 \\
-0.0051 & -1.000
\end{bmatrix}
\]

(26)

The system states are represented by \(x(t)\) whereas \(e(t)\) is the error feedback signal. The adaptive computation of the error feedback gains using the NN is subsequently described.

#### 3.2.2. Controller Parameter Estimation using the Neural Network

In order to achieve better accuracy and faster tracking convergence, the NN is employed to optimize the error feedback control gains. In this case, six sequences of 700 state transitions totaling 4195 data samples were sufficient, since the plant has been linearized. The input features are the current angular orientation \([\theta(t) \varphi(t)]\) along with the next angular orientation \([\theta(t+k) \varphi(t+k)]\) of the 2-DOF helicopter. The output labels are the error feedback gains \([K_{\theta11}(t) K_{\theta12}(t) K_{\phi11}(t) K_{\phi12}(t)]\) responsible for the angular orientation change. Similar procedures as proposed in Subsession 3.1.2 of this paper are followed, and the MSE plot is as shown in Figure 4. The figure shows good generalization of the estimator similar to observation in the previous section since the test error approximates the training error. The trained NN estimator is integrated in the second loop of Figure 2 to obtain optimized performance as presented next in Section 4.

![Figure 4: MSE of the NN estimator for helicopter control](image)

### 4. Simulation Results

Closed-loop simulation was conducted in Matlab Simulink for both the traditional and the NN-optimized control system. The results for different initial state shifts were compared to prove the effectiveness of the proposed scheme. The desired eight-shaped trajectory for the mobile robot was defined as,

\[
x(t) = \sin \frac{t}{10}
\]

(25)

\[
y(t) = \sin \frac{t}{20}
\]

(26)
The feed-forward driving and steering velocities as described by (20) and (21) are shown in Figures 5 and 6 respectively.

\[
\theta_d(t) = \text{atan2}(y_d(t), x_d(t))
\]  

(27)

Figures 7 - 9 is the trajectory tracking performance of the nonlinear Lyapunov-based controller for the mobile robot with initial state error \([0.3, -0.5, \pi/6]\), where the linear displacement unit is meters and radians is the unit of the angular displacement. Figure 7 is the result of an underdamped control system due to low damping ratio, whereas Figure 8 is the result of an overdamped control system due to high damping ratio. The result of a critically damped control system with unity damping ratio is shown in Figure 9, whereas Figure 10 is the corresponding trajectory tracking output performance of the NN-optimized controller. It can be observed, as the case is in the previous example, that the NN-optimized controller of Figure 14 showed better comparative control performance than the different variations of traditional Lyapunov-based controllers of Figures 11 - 13.

To further show the performance advantage of the NN-optimized controller, the average linear and angular tracking errors over the entire trajectory are presented in Table 1 as it applies to the different initial state errors. It can be seen that both the resultant linear and angular tracking errors are minimized using the NN-optimized controller.
The desired positioning of the 2-DOF helicopter pitch and yaw angular orientations over time are defined as,

\[
\theta_d(t) = \begin{cases} 
0.8r^5 - 8r^3 + 10r + 6, & r = 0.05t, \ t \leq 47 \\
-16.9, & r > 47 
\end{cases}
\]  

(28)

\[\varphi_d = 5\]  

(29)
The LQR-based controller performance is shown in Figures 15 and 17 with initial pitch and yaw angular orientations of -40.5 and 0 degrees. The Q and R parameters were selected as diag([3e5 3e5 1 1 1 1]) and diag([1 1]) where Q is associated with both the state and error feedback signals. The performances of the NN-optimized controller are shown in Figures 16 and 18 for pitch and yaw angle control respectively. Since the system is linearized, modest performance improvement is observed with respect to response speed and steady-state error minimization. Table 2 shows the comparative tracking errors.

5. Conclusion

A neural network optimized control system design for autonomous vehicle navigation has been proposed in this study. The design consists of an inner error loop integrated with an outer loop for estimating the controller parameters utilizing a neural network trained on samples from test navigation. Comparative studies of the proposed scheme with traditional methods were presented. In the first case, the neural network optimized control system was shown to outperform a Lyapunov-based controller in terms of faster convergence to the desired trajectory and better steady-state performance for an eight-shaped maneuver. A second illustrative simulation example was conducted for the control of pitch and yaw angles of a 2-Degree-Of-Freedom helicopter model, where improved transient and steady-state performances were observed for NN-optimized controller over a Linear Quadratic Regulator-based controller.

Because the neural network structure allows complex and nonlinear mapping of variables, the trained estimator is able to learn the behavior of both linear and nonlinear systems. Furthermore, since the proposed scheme is sample-based, it can compensate for plant modelling errors that degrades the performance of traditional controllers in real-life applications.

Conflict of Interest

The authors declare no conflict of interest.

Acknowledgment

The research work presented in this article is supported in part by the US National Science Foundation award 1464387, 1736196 and by the U.S. Office of the Under Secretary of Defense for Research and Engineering (OUSD(R&E)) under agreement number FA8750-15-2-0119. The U.S. Government is authorized to reproduce and distribute reprints for governmental purposes notwithstanding any copyright notation thereon. The views and conclusions contained herein are those of the authors and should not be interpreted as necessarily representing the official policies or endorsements, either expressed or implied, of the US National Science Foundation or the Office of the Under Secretary of Defense for Research and Engineering (OUSD(R&E)) or the U.S. Government.

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