Model of charge transport in Semi-Insulating Undoped GaAs microstrip detectors

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Abstract

In this paper we present a method for simulating the response of microstrip detectors to minimum ionizing particles, making use of a program for field calculation, a program for carrier drift and SPICE for circuit response. A knowledge of the electric field is essential for any further improvement of the program. A simple model involving EL2 levels in the metastable state is proposed to explain some measurements of electric field.

Presented by S. D’Auria at the 4th workshop on GaAs detectors and related compounds
San Miniato (Italy) 19-21 March 1995
1 Introduction

Microstrip detectors made of GaAs will be used in a part of the forward tracker detector in ATLAS at the LHC because of their larger radiation hardness when compared to silicon devices. Test beam results are reported elsewhere in these proceedings. In order to optimise the parameters of the devices, such as total thickness, strip pitch and aspect ratio for a required spatial resolution, we are developing a program which is able to calculate the current signal from the various geometrical configurations and crystal properties. A more detailed study will be published later; in the following we describe the method and stress the importance of a detailed knowledge of the electric field inside the detector.

The second part of this paper deals with a model for the electric field. Semi-Insulating-Undoped (SIU) GaAs has a resistivity of the order of $10^7 \, \Omega \, \text{cm}$ which is achieved through a compensation by deep levels. These levels are mainly of the intrinsic type called EL2, which is due to the non perfect stoichiometric ratio between Ga and As. In detectors made of this material the region which is active for detection has a thickness which increases with bias. At a bias of 200 V about 180 $\mu$m are active [1, 2, 3]. Various models [4, 5, 6] have been proposed to calculate the electric field, and two measurements have been made [7, 8]. The measurements show that the electric field is approximately uniform at high voltages, which means that the sensitive region has a very low fixed charge density. This observation is very difficult to explain in homogeneous materials, where the fixed charge density is constant over the depth. A possible explanation of such a field shape is that some of the EL2 defects, under the influence of a strong electric field, make a transition to a normally metastable state featuring no energy levels in the forbidden gap. The existence of such a level has been reported [9], but neither evidence nor exclusion of a voltage-induced transformation has yet been reported.

2 Microstrip detector simulation

SIU GaAs is characterized by an imperfect drift of charge carriers, due probably to trapping [10] and to the peculiar shape of the electric field. Double-sided microstrip detectors show a marked asymmetry in charge response from the two sides [11]. Therefore a full 2-dimensional simulation of the charge drift in the device is needed in order to calculate the signal induced on the strips.

The chain of programs used is shown schematically in fig. 1. The three main parts are: a
2.1 Field calculation

In simulating a device two or more electric fields have to be considered. They are the physical field which is driving the motion of charges and the so called weighting field which has dimensions \([L^{-1}]\) and is a purely geometrical function of space position. It is a measure of the coupling between the moving charge and the electrode considered. For instance, in the simple case of parallel-plate diode electrodes separated by a distance \(d\) the weighting field is a vector of length \(1/d\) perpendicular to the surface. In the case of devices with more electrodes, as in microstrip detectors, the weighting field for the \(j^{th}\) electrode is calculated by holding it at +1 V and maintaining all the other electrodes at ground. All the fixed charge has to be neglected.

In the first stage of work reported here we have used the code GARFIELD to calculate the electric fields. This program was written to simulate gas operated multiwire drift chambers. A part of it performs a 2-dimensional calculation of electric field in a configuration where electrodes have a wire shape or are infinite planes.

Each microstrip was simulated as an array of neighbouring wires with a distance between centres 1% larger than their diameter. We then checked that the resulting field was independent of the wire diameter and we chose a diameter of 1 \(\mu m\) as a good compromise. A clear limitation of this method is the lack of simulation of surface effects with dielectric materials such as silicon nitride and air. Also, we expect that results are reliable only on a scale larger than a few times the wire diameter. This is acceptable if signals from minimum ionising particles (m.i.p.s) have to be simulated, but a more accurate calculation of the field is needed if details have to be looked at or if signals from alpha particles are to be simulated.

A plot of the modulus of the weighting field for one strip is shown in fig. 2. The major contribution to the signal for that particular strip is due to holes or electrons moving in proximity of it. Due to the geometry, however most of the signal is due to holes.
The drift field was calculated by GARFIELD and then multiplied by the following function:

\[ f(x) = \frac{1}{1 + e^{\frac{-x}{W_t}}} \]  

where \( x \) is the distance from the strip plane, \( W = W(V) \) is the thickness of the active region, \( W_t \) is the thickness of the transition region. A low overall constant field of 100 V/cm was then added. The result is an approximation to the field measured in ref. [7], (fig. 3). It was assumed that \( W = \alpha V \) with \( \alpha = 1\mu m/V \), as reported in [4].

As an example, a zone of 550 \( \mu m \) in width for a 200 \( \mu m \) thick detector was simulated. The strip pitch was 50 \( \mu m \) and the metal width was 40 \( \mu m \). Only the part comprising 5 central strips was used for further analysis corresponding to a grid of 90 \( \times \) 90 points. Interpolation of the electric field was used between points.

### 2.2 Drift of charge carriers

The initial distribution of charge is assumed to be uniform along the linear track of a minimum ionizing particle. Generation of delta rays and charge spreading has not yet been implemented, but is assumed to be not essential at the present stage. A constant number of electron-hole pairs is generated for each track. A time-slice approach is used in simulation, as a current signal is required. Each individual carrier is followed during its drift. Trapping probabilities are calculated from the trap concentrations, \( N_k \), cross sections \( \sigma_k \) and drift velocity \( v(x(t)) \). A flag associated with each carrier indicates its status, which can be: free, trapped, reached the electrode. The probability of being trapped by the \( k^{th} \) type of trap is given by:

\[ P_k(\sigma_k, N_k, x, \Delta t) = 1 - \exp(-v(x)\sigma_k N_k \Delta t) \]  

where \( \Delta t \) is the time step.

Detrapping is also taken into account as a possible process. We assume that there is a mean trapped time \( \tau_k \) and that both \( \tau_k \) and \( \sigma_k \) are independent of electric field.

The carrier drift velocity is calculated from the electric field using parametrizations of the experimental data [14] [15], as shown in fig. 4. We note that provided the field is high enough, the details of its shape have a negligible influence on carrier velocity for the larger part of the
device, as saturation is reached. If drift in a magnetic field and diffusion have to be considered, however, an exact knowledge of the electric field is essential.

The current signal on the $j^{th}$ electrode is calculated from the Ramo-Shockley theorem:

$$i_j(t) = \sum_{n=1}^{N_c} q_n \bar{v}_n(t) \bar{E}_{w_j}(\bar{x}_n(t))$$

where $N_c$ is twice the number of electron-hole pairs generated, $\bar{E}_{w_j}(\bar{x}_n(t))$ is the weighting field and $q_n$ the charge of the carrier. The charge signal is obtained by integration of $i(t)$ and gives the charge collection efficiency. An example of a current signal is shown in fig. 5 and is used as input for SPICE.

### 2.3 SPICE calculation

In order to calculate the signal reaching each preamplifier the front-end and bias coupling network was simulated using SPICE. The parameters depend mainly on the detector geometry. The main parameters are the inter-strip capacitance, depending on pitch, aspect ratio and strip length, the strip to back contact capacitance and the decoupling capacitance. The biasing structure, based on punch-through was also included as a 10 GΩ resistor with a 20 fF capacitance in parallel. A schematic is shown in fig. 6. Resistors had to be used to ensure a DC path to nodes.

The signals from two neighbouring strips were included as two independent piece-wise linear current generators. The current values were calculated with the drift code described previously, simulating tracks impinging perpendicularly on the strips; the hit position was varied from the centre of the central strip to the centre of the neighbouring one on the right. It was assumed that all strips were read-out. In simulating the signal a symmetry relation was assumed, i.e. $i_j(t)|_{y=y_0} = i_{j+1}(t)|_{y=p-y_0}$ where $p$ is the pitch, and $y_0$ is the distance of the track from the centre of the $j^{th}$ strip.

The current signal at the preamplifier input was calculated and then integrated to give the total charge detected by each channel. An $\eta$ function $\eta(x)$, related directly to spatial resolution.
Figure 5: An example of the simulated current signal generated by minimum ionizing particles traversing a 200\,µm thick detector in the middle of the considered strip, which in this case is 30\,µm wide. The bias voltage was 180\,V. The major contribution is due to holes which approach the area where the weighting field is high. The electron contribution is shown in the shaded curve.

Figure 6: Schematic of the circuit used in the SPICE simulation. $C_{is}$ is the inter-strip capacitance, $C_{bp}$ is the capacitance to the backplane, $R_L$ is the load resistance of the amplifier. The biasing structure is represented by a parallel RC. Current sources from two neighbouring strips are taken into account. An array of seven strips was simulated.
Figure 7: Plot of the $\eta$ variable defined as: $\eta(x) = \frac{Q_{\text{left}}(x)}{Q_{\text{left}}(x) + Q_{\text{right}}(x)}$, where $x$ is the distance from the centre of the strip. The detector is 200$\mu$m thick, pitch is 50$\mu$m, metal width is 30$\mu$m.

could be calculated for the given configuration. An example is shown in fig. 7.

3 A model for the electric field

The present simulation chain can be a starting kernel for further improvements. However, a more detailed simulation, including effects of magnetic field and diffusion, is possible if a definite shape of electric field is generally accepted. Measurements made at UMIST indicate that the field is uniform in the vicinity of the reverse biased contact, as shown in fig. 3. This a clear experimental result. Most calculations result instead in a linearly decreasing electric field. This arises naturally if a uniform doping concentration is assumed. Although some of the defects are not ionized due to quasi-Fermi-level shifting by the reverse bias current, the main trend is a field decreasing monotonically to the back contact. A constant electric field is quite difficult to explain. A correlation between reverse current and charge collection efficiency for alphas has been reported as evidence supporting the calculations. This correlation has not been found by us for m.i.p.s, as we have several examples of detectors with a low reverse current density (20 nA/mm$^2$) and high charge collection efficiency (90 %) over a large thickness (500 $\mu$m) (fig. 8).

Another model proposes a neutralization of deep levels by field-enhanced trapping of the electrons of the reverse current. In this model, too, a high current is required to obtain a high charge collection efficiency.

The nature of the reverse current is not yet clear. Thermionic emission would require a really low barrier height, while if a generation mechanism is assumed, saturation could normally be explained only if most of the current is generated in the first few micrometers below the reverse-biased contact. Otherwise the current density is expected to increase with the volume in which the electric field is high.

Commercial SIU-GaAs usually contains a concentration of about $10^{16}$ cm$^{-3}$ of EL2 defects. This defect is believed to be due to an As substitutional ($\text{As}_{\text{Ga}}$) plus an As interstitial ($\text{As}_i$) as second nearest neighbour. The material is naturally compensated and shows a resistivity of $10^7\Omega\text{cm}$ which is ideal in a substrate for electronic and optical circuits.

The EL2 defect has been reported to have a metastable state EL2$^*$ which has very little or no electrical and optical activity. It is therefore believed that the corresponding energy level
Figure 8: Charge collection efficiency for m.i.p.s and leakage current density at 20.0°C for the SIU-GaAs pad detector G114-5. The thickness is 500 µm, area is 7 mm², with guard-ring.

is split and shifted into the conduction and valence bands. One proposed microscopic structure of EL2* is similar to EL2, but with the As_i atom as nearest neighbour. The transition is:

\[ EL2 \rightarrow EL2^* \implies As_{i(II)} \rightarrow As_{i(I)} \]  \hspace{1cm} (4)

The EL2* can be generated via optical absorption, involving different charge states [18]. The decay rate to the stable state has an activation energy of 0.3 eV so that at room temperature the metastable state has a lifetime of about 1.5 µs. It is generally observed at fairly low temperatures, (about 77K) and in the presence of a low electric field.

If the transition could happen at room temperature, under the effect of a high electric field, for example, the measurements of electric field shape in [19] could be qualitatively explained in the following way: as reverse bias is applied, deep donors start to become ionized; some are neutralized by trapping electrons from the leakage current, as in [20]; this lowers their effective concentration, in such a way that the electric field can extend for several micrometres. This process continues until the field at the contact reaches a critical field, \( E_c \), of about 10 kV/cm, at a bias voltage between 20 and 50 V. At this point the transition \( EL2 \rightarrow EL2^* \) starts to take place, so that the field remains roughly constant, as deep levels are no longer active. We should assume that the transition is not complete, leaving some compensating EL2+. The region where the field drops is shifted rigidly towards the back contact as bias is increased. In this transition region the electric field is non-zero and most of the EL2 defects are active. Thus the reverse current can be efficiently generated there and is constant to the extent that the transition region has a constant thickness while moving across. This is to be expected in a homogeneous material. A sketch of the proposed model is shown in fig. 9.

From the point of view of charge transport, three regions of electric field can therefore be distinguished: one constant, one linearly decreasing and one with an extremely low residual electric field. This is quite similar to that shown in fig. 3. In the third region transport is mainly
due to charge relaxation, with a typical time of $\epsilon \rho \approx 10\mu s$, giving a slow signal component. In
the transition region the field is decreasing. Thus the electron velocity initially increases then
decreases and trapping can be enhanced. The charge collection efficiency and the medium-slow
components of the signal depend on the shape of the field. In the region where a constant field
is present the charge transport is good, as the concentration of active traps is lower. Little
contribution to trapping is expected from this zone.

The shape of electric field used in the simulation now has also a theoretical (although
qualitative) explanation and is not based only on empirical data. While the validity of this
model is not proved, it enables to explain consistently many features of SIU-GaAs detectors.
$C-V$ characteristics would not characterise this model, as the transition region where charge
can move has the same features as in normal semiconductors. The saturation of reverse current
can be explained in this model, assuming that the current is generated mainly in the transition
region where the electric field is non negligible and the concentration of active levels is high.

A possible way to test the model is with OBIC measurements $^2$ using a focused light beam
at a wavelength which is unable to separate directly an electron-hole pair. In this way only
deep levels will be probed and the photocurrent at a distance from the front contact will be
proportional to the number of active levels at that point and to the electric field. A region
of constant width where the photocurrent is higher is expected to move across the detector as
the reverse bias is increased. If the model is incorrect the region with high photoresponse will
simply increase in width. We propose to carry out this measurement in the near future.

4 Conclusions

A code has been set up to simulate the response of GaAs microstrip detectors to $m.i.p.s$. From
preliminary results it is evident that charge sharing is possible in principle also in SIU-GaAs
detectors where the charge transport is not perfect, provided that the strip parameters and
noise performances are optimized. More extensive results on various geometry and parameters
will be presented soon. Limitations of the present code are in the calculation of details of the
electric field near the strip and at the interface with passivating layers. This will be improved
using a more suitable package for the field calculation. Further developments will also aim at including the possibility of drift in a magnetic field and the effects of diffusion. Because of the peculiar band structure of GaAs these processes are strongly dependent on the local intensity of the electric field even when the drift velocity is saturated. A detailed knowledge of the electric field is needed to improve the simulation.

A possible explanation of the measured electric field profile has been proposed, based on a transition of the EL2 defects which makes them electrically and optically inactive. This model can explain consistently a variety of features of SIU-GaAs, like the slow transients and a saturation in generation current.

Acknowledgements

We wish to thank PPARC and the EC (via an H.C.M. contract) for support and our host for organizing this workshop.

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