Interlinked Ac-Dc Microgrids by Fuzzy Based Tie-Converters for Autonomous Power Management

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Abstract – Several operational drawbacks for interlinked AC-DC microgrids to the existing schemes of power management. Designed with main objective on based of their loading conditions power sharing among interlinked microgrids for some existing control schemes, while other schemes without considering specific loading conditions of the interlinked microgrids to regulate voltage. However, cannot reach the existing schemes both objectives successfully. To control these problems an autonomous power management for interlinked AC-DC microgrids by fuzzy based tie-converters is proposed. Fuzzy is the advanced controller that will be used in tie converters. By replacing PI with Fuzzy Logic Controller better results will be found. It makes fuzzy logic an effective tool for the conception and design of intelligent systems. The fuzzy logic toolbox is easy to master and convenient to use. The hybrid control has been proposed for the interlinking or tie-converters of the AC-DC microgrids for autonomous power management with FLC. The proposed is fully autonomous scheme ,while for tie-converters and generators it retains plug-n-play features. Under different operating scenarios the performance has been validated for the proposed control scheme with FLC. Better voltage regulation maintaining autonomously in the DC microgrid managing the power deficit effectively can be done through proposed scheme. To demonstrate its effectiveness, the system is modelled and its performance will simulated on MATLAB.

Index Terms – Power management, autonomous control, interlinked microgrid, droop control, distributed control, hybrid control.

I. INTRODUCTION

A microgrid is a group of interconnected distributed energy resources and loads that acts as a single controllable entity with in clearly defined electrical boundaries with respect to grid. The technical improvement in action of bringing resources into effective of alternative energy technologies and renewables plays an important role in power electronics [1]-[3] which have clearly understand in different forms of combinations and network topologies [4],[5]. While meeting load requirements their overall aim of network topology and control to make as possible the benefits predominantly determined. Alternative energy and renewable technologies are bring into effective action extensively. These new technologies which are give effective action in the form of microgrid is tend to choose due to more superior, like increase reliable supply, best effective use of resources and advancement power quality [6]-[7]. At a recent time, more improved grid architectures including multi-microgrid [8]-[11], the zone based grid architectures [12], interlinked AC-DC microgrids [13]-[17] and interlinked AC-AC microgrids [18],[19] have become visible.

The main goal is to utilize more benefits from alternative energy and renewable resources of these improved network architectures. For example two or more interlinking microgrids, it will hold up frequency and voltage, flexibility of interlinked microgrids, make possible reserve sharing and finally overall reliability increase. The interconnecting between two or more microgrids arrangement or with beneficial grids depends on the overall goals mainly, and also used the management and control scheme in single microgrids. When different operating frequencies and/or voltages have two or more microgrids are mainly used the harmonizing tie-converters. The tie-converters are absolutely necessary if the microgrids have different overall control aim to be interconnected and power flow have to be regulated among them [18]. In similar way, tie-converters necessary for the interconnecting of DC microgrid with another AC microgrid or with beneficial grid to regulate power flow in other functionalities, and that has been discovered in the published literature under different kinds of situation [13]-[17]. In [13], for interlinking or tie-converters the demand-droop control scheme of AC-DC microgrids has been proposed. Interlinked droop controlled AC-DC microgrids on the bases of normalized terminal frequency and voltage the action of power flow decided. Relative loading based on their condition between two interlinked microgrids an autonomous power management is possible for this scheme. By connecting storage system to interlinked microgrids has been enlarged the same power sharing scheme [14]. This scheme been made better for interlinking converter to reduce the energy flow by developing gradually auto-tunning [15]. The existing auto-tuning make it possible for the power transfer only when one microgrid is lightly-loaded while other heavily-loaded. For different functional conditions for the intellinked AC-DC microgrids has been researched the power sharing on droop based scheme in [16]. In [17], presented a three-port system consist of DC, AC and a storage system for overall aim to power dealing. It is as presented in [15] that based on loading condition of interlinked microgrid for power sharing dealing is same. In [20], for interlinked AC-DC microgrid another power management scheme is used, it has an aim to regulate DC microgrid of voltage without any considering the generator of specific loading level. This scheme put into effect for only single-converter which the feature of plug-n-play limits. Based on relative loading condition the power sharing droop based schemes transfer power for interlinked microgrids. During uneven or contingency loading condition the power transfer does not regulate the frequency and/or voltage but supports frequency and voltage of the interlinked microgrids. Although these schemes allow for the interlinked microgrids plug-n-play feature. By using only PI controller it will get
II. CONTROL OF AC AND DC MICROGRIDS

The DC microgrid consist of dispatchable generators, non-dispatchable generator and loads, as shown in fig. 1. Non-dispatchable generator is solar-PV generator and dispatched generators are fuel-cell, microgrids. Dispatched generators are source of electricity that can be used on demand. It can turned ON or OFF, or can adjust their power output according to an order. Non-dispatched generators are not continuously available due to the weather condition. It does not rectify the load changes. Operate solar PV non-dispatchable system in current control mode and thus high power will extracts at all the times. The dispatched generators can be controlled by decentralized or centralized control scheme and are usually for resilient the renewable capacity. Due to reliable and simplicity, the decentralized droop scheme is more favour. Therefore, for dispatched generators the traditional group scheme is used, it is given by

\[
V_{dc,i} = V_{dc,max} - \partial_{dc,i}P_{dc,i}
\]

\[
\partial_{dc,i} = \frac{\Delta V_{dc}}{P_{dc,max,i}}
\]

(1)

Where, \(V_{dc,i}\) is \(i^{th}\) generator of reference voltage, \(i\) is the DC generator number, \((i = 1, 2, 3, \ldots)\); \(P_{dc,i}\) is the \(i^{th}\) generator of output power, \(P_{dc,max,i}\) is the \(i^{th}\) generator of rated or maximum power, \(V_{dc,min} = V_{dc,norm,TC1}\) and \(V_{dc,max}\) are the defined minimum and maximum voltage; \(\partial_{dc,i}\) is the \(i^{th}\) generator of droop gain.

On the bases of (1), the voltage reference of generator 1 and 2 for the droop controlled can be calculated by (2) and (3).

As DC bus voltage share generators 1 and 2 (i.e., \(V_{dc,ref,1} = V_{dc,ref,2}\)), (2) and (3) can be rewritten and equated by (4), which denotes that according to droop controlled generators of their rated power capacity will share proportional power.

\[
V_{dc,ref,1} = V_{dc,max} - \partial_{dc,1}P_{dc,1} + \partial_{dc,2}P_{dc,2}
\]

In (4) equality the generator terminal voltages is same.

Practically, due to which the generator terminal voltages are connected dissimilar lengths as they are not same through cable/feeder, precise sharing of power affect by mismatching the voltage at generator terminals, by using of any suitable compensation method it needs to be compensated.

The feeder voltage drop with compensation of droop equation can be rewritten by

\[
V_{dc,ref,i} = V_{dc,max} - \partial_{dc,i}P_{dc,i} + \partial_{dc,ref}X_i
\]

The droop controlled DC microgrid of the voltage will change with varying the load, but within of defined allowed range. The voltage is set between 395V to 420V, for the droop controlled generators, the generators will deliver 100% power at 395V and there is no power at 420V. The tie-converters will start when in large amount of loaded the DC generators (e.g., 80% generators loading at less than or equal to 402.4V), to meet the peak load demand the tie-converters bring power from AC microgrid and for example of interlinked microgrids in fig. 1, the DC microgrid of frequency and voltage is considered rigid. AC microgrid can be operate in grid-connected mode or secondary frequency and voltage regulation with droop controlled. In fig. 1, the AC microgrid characteristics are shown where the frequency and voltage at nominal value are constant (e.g., 415V and 50 Hz). In more, to send excess power to the DC microgrid and to meet its local demand AC microgrid has adequate generation capacity which has been exhibit through the proposed control of autonomous tie-converters. Also the voltage of DC microgrid regulate.
III. PROPOSED HYBRID CONTROL OF TIE-CONVERTERS

The rating power for strong the renewable capacity of storage systems or dispatchable generators depends on charging of loads and the renewable source in the microgrid. The excessive charging of loads and renewables with a high power rating needs storage systems or dispatchable generators, which expressing possibility or not be a feasible solution. Alternatively, directly or through harmonizing converters, could be interconnected with insufficient generation capacity to another microgrid or usefulness grid. It is only able to be done through tie-converters for interlinking of DC microgrid with a AC microgrid. DC microgrid is characterized with insufficient generation capacity due to excessive changing of the loads and renewable as a droop controlled system and AC microgrid is characterized with sufficient generation capacity as a frequency and voltage regulated system. By bringing the power from AC microgrid the power shortage in DC microgrid is controlled, during the less renewable power output or the peak load demand. Ideally, with the proposed tie-converter control it can be done autonomously and efficiently. Based on the following purposes the tie-converter of control scheme is developed: 1) To reduce the losses of power transfer, e.g., on based of power transfer demand the number of tie-converters should operate, and in the DC microgrid during peak-load demand only tie-converter should operate; 2) To achieve control of fully autonomous on the communication network without depending; 3) To transfer power during the peak load demand from the AC to DC microgrid or in the DC microgrid generation possibility; 4) To regulate the DC microgrid voltage of droop controlled; 5) To enable for generators and tie-converters the plug-n-play feature. Unlike in [13]-[17] for the interlinked AC-DC microgrid of existing schemes, voltage regulation mode control and a hybrid droop for tie-converters is proposed and the proposed control scheme of mathematical form is given by:

\[
V_{\text{con,T}=x} = \begin{cases} 
0; & V_{x}>V_{\text{ref,T}=x} \\
V_{\text{con,T}=x}\cdot (1-L)\% & 0 \leq V_{x}\leq L_{\%}\times P_{\text{max,T}=x} \\
V_{\text{con,T}=x}\cdot (1-H)\% & L_{\%}\times P_{\text{max,T}=x} < V_{x} < (100-H)\% \times P_{\text{max,T}=x} \\
V_{\text{con,T}=x}\cdot (100-H)\% & V_{x} \geq (100-H)\% \times P_{\text{max,T}=x}
\end{cases}
\]

Where TCx entitled the tie-converter (x = 1, 2, 3, ...); V_{dc,T}=x is the xth tie-converter of reference voltage; V_{dc,nom,TCx} is the nominal voltage by xth tie-converter to be regulated; V_{dc} is voltage of DC microgrid; V_{dc,nom,TCx} is the DC microgrid voltage when maximum power transfers of xth tie-converter; V_{dc,start,TCx} is the xth tie-converter of threshold voltage to start; P_{dc,max,TCx} is the xth tie-converter of maximum power limit; P_{dc,TCx} is the xth tie-converter of DC power output; L% and H% are the allocated for droop 1 and 2 mode respectively rated power percentage of tie-converter; \( \delta_{H,TCx} = (V_{dc,nom,TCx} - V_{dc,nom,TCx+1})/H\% \times P_{dc,max,TCx} \) is the xth tie-converter of droop 2 gain (at high power); \( \delta_{L,TCx} = (V_{dc,start,TCx} - V_{dc,nom,TCx})/L\% \times P_{dc,max,TCx} \) is the xth tie-converter of droop 1 gain (at low power). As shown in fig.1, when the DC microgrid voltage drops to the \( V_{dc,start,TCx} \) of threshold set tie-converter 1 starts in control mod of droop 1. This threshold voltage indicates that in the DC microgrid of all the generators are heavily-loaded (e.g. over 80% loaded). At the set condition to the voltage regulation mode a smooth transition enables in the droop control mode the start of the tie-converter i.e., \( P_{dc,TCx} > L% \times P_{dc,max,TCx} \). During the voltage regulation mode, to meet the peak demand power of DC microgrid the tie-converter from AC microgrid imports power and also its voltage regulate to the nominal value of \( V_{dc,nom,TCx} \) to be set. Furthermore, unlike all tie-converters of the parallel operation in the existing schemes, the operations of converters has been compute. The tie-converters only starts first when heavily-loaded in the DC microgrid of all the generators. Once the power capacity of first tie-converter near to saturation at \( P_{dc,TCx} = (100-H)\% \times P_{dc,max,TCx} \) from the voltage regulation to droop 2 control mode its control mode is changed to allow minor voltage drop. This minor voltage drop will enable its operation to start the next tie-converter which is caused by the droop 2 control mode. In case of the first tie-converter failure, automatically the second tie-converter starts its operation due to high load demand followed by the voltage drop. Therefore, the control strategy of proposed provides dynamic operation without compromising the inherited resilience during all operating conditions of the droop based scheme with fuzzy. Depending on L% and H% of chosen value the tie-converter’s power will allocate for droop 1 and droop 2 control modes, and while considering the power and voltage measurement errors between different modes should be smooth transition tuned to allow in the considered microgrid. Fuzzy logic controller is used in the controller of a PI before sending the signal to the PWM module. It has been outstanding in dealing with complex, undefined, non-linear or time-varying systems. It is comparatively simple to execute because the control system usually does not need a mathematical model. Fuzzy logic has rapidly turned out to be a standout amongst the present best innovations for advanced control frameworks improvement. Quickly become one of today’s most successful technologies for sophisticated control systems development. It is a mathematical tool for managing vulnerability. With the voltage regulation mode of proposed scheme, the DC microgrid of voltage regulation overall performance can be amended. During the peak load demand in peculiar, at nominal value of DC microgrid voltage is regulated, which is not the case for interlinked microgrids with the existing power management. Different scenarios has been justify for load operating of proposed scheme, as explained in section IV.

IV. PERFORMANCE VALIDATION

For two different scenarios the proposed scheme of performance of DC microgrid has been validated. In first scenario, the microgrid contains a fuel cell, dispatched microturbine and variable load.
A non-dispatched solar PV generator is added for scenario 1, in the second scenario. In table I-III the system parameters are encapsulated.

The logic flow diagram of tie-converter is shown in fig.2. The two scenarios at different load operating conditions have been tested to establish capability and durability of the proposed scheme.

The fuzzy logic controller is replaced with PI. The control block diagram of tie-converter is shown in fig.3. FLC is an appealing selection when precise mathematical formulations are not doable. Different focal points of the FLC are, it can work with led exact information sources, it need not bother with quick processors it is more strong than other non-linear controllers.

**TABLE I**

| Feature          | Control Mode                        |
|------------------|-------------------------------------|
| AC microgrid     | Islanded-microgrid with regulated   |
| Voltage and frequency | Grid-connected mode                  |
| Tie-converter    | Hybrid droop and voltage control mode|
| DC microgrid     | Non-dispatchable generators and current control mode with MPPT |

**TABLE II**

| Description    | Parameter | Value |
|----------------|-----------|-------|
| Voltage        | Vdc (V)   | 400 (+5%, -12.5%) |
| Microturbine   | Pdcm,1 (kW) | 10 |
|                | Qdc,1 (kW) | 2.5 |
| Fuel cell      | Pdcm,2 (kW) | 5 |
| Solar PV       | Pdcm,3 (kW) | 10 |
| Load           | PLoad,peak (kW) | 25 |

**TABLE III**

| Description     | Parameter | Value                  |
|-----------------|-----------|------------------------|
| AC microgrid    | Vnom (V)  | 415 (1 − i) 20         |
| Tie-converter   | Pdcm,TC1 (kW) | 10 |
|                 | Vnom,TC1 (V) | 402.5 |
|                 | Qnom,TC1 (V) | 400.0 |
|                 | Vnom,TC2 (V) | 397.5 |
|                 | I% = H% | 10% |

Fig. 3. Scenario 1: DC microgrid with microturbine, fuel cell and variable load

The DC microgrid contains fuel cell (Pdcm,2 = 5 kW) microturbine (Pdcm,1 = 10 kW), and variable DC load (Pload,peak = 20 kW) and through a tie-converter (Pdcm,TC1 = 10 kW) with AC microgrid these are interlinked, as shown in fig. 3.

The DC microgrid load from 5 kW to 20 kW is vary in steps. At load demand of 15 kW, the generator 1 and generator 2 of expected loadings are more than 80%, and the DC microgrid voltage is below the Vdcm,start,TC1 = 402.5 V set threshold. This condition will permits the tie-converter 1 from AC microgrid to import power and at the defined nominal value of Vdcm,nom,TC1 = 400.0 V the DC microgrid voltage regulate. These performance results are shown in Fig.5. When load changes from 10 kW to 15 kW the DC microgrid voltage decreases below 400 V. Tie-converter 1 to start in droop 1 control mode when this voltage drop triggers. When the tie-converter control mode is start in droop 1 control mode at the threshold (Pdcm,TC1 > 10%×Pdcm,max,TC1) the voltage regulation mode changeover immediately and satisfy the condition. At 1.2s, from 15KW to 20KW the DC microgrid load is further raised, and from the AC microgrid the power transferred is increased. From 8s to 12s in the DC microgrid all over the peak-load demand, tie-converter operate and regulate the DC microgrid voltage. At 16s the load demand is reduced in DC microgrid and automatically tie-converter turns off with a short delay. Therefore the proposed control scheme with fuzzy logic controller has good performance of voltage regulation and establish efficient operation.
Fig. 5. Results showing (a) tie-converter and generators power, (b) DC microgrid voltage and (c) tie-converter control signals for four different load operating conditions.

B. Scenario 2: DC Microgrid with Non-dispatchable Generator and Load profile

To scenario 1 solar PV system of a non-dispatchable generator is added, which is shown in fig.6. For proposed strategy effectiveness with renewable generator and load demand different operating conditions are developed further.

Fig. 6. Scenario 2: DC microgrid with microturbine, fuel cell, solar PV and load

The peak value 24.5KW is increases the DC microgrid load and then decreases, which is shown in fig.7. When loads of generators 1 and 2 increases 80% and DC microgrid voltage drops below to threshold set of $V_{dc,\text{set},TC1} = 402.5$ V. The solar PV output is lower with high of load demand. In voltage regulation mode the tie-converter operate from 8.5s to 14.2s. The DC microgrid load decreases when the output power of tie-converter is below $P_{dc,max,TC1}$. This condition requires before turns off the tie-converter in droop control mode operate.

Fig. 7. Scenario 2: Results showing (a) load demand of DC microgrid, (b) tie-converter and generators power, (c) DC microgrid voltage and (d) Tie-converter control signals at varying solar PV and load operating conditions.

V. CONCLUSIONS

For interlinked AC-DC microgrids have an autonomous power management scheme with different configurations has been presented. The proposed scheme with fuzzy logic controller manages the shortage of DC microgrid power autonomously and efficiently.
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To avoid unnecessary operational losses using the number of tie-converters has been reduced in operation. For better regulation of voltage in the DC microgrid the scheme has established. For two different scenarios the durability and performance has been validated at variable load conditions in the DC microgrid of proposed scheme with FLC.

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