Study of novel parallel H-bridge and common-emitter current-source inverters for photovoltaic power conversion system

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ABSTRACT

A novel operation of three-level H-bridge and common-emitter current source inverters (CSIs) proposed for photovoltaic power converters is presented in this paper. Two photovoltaic systems with two different inverter circuits, i.e. H-bridge and common-emitter CSIs, were connected in parallel to supply a sharing ac power load. In order to regulate the power supplied by each inverter system, proportional integral current controllers were employed. Triangular carrier and sinusoidal signals-based modulation techniques were implemented to both inverters. Some parameters such as load current, inverter’s output current, total harmonics distortion (THD), and efficiency were tested and analyzed. Test results showed that in the parallel operation of these inverters, the average THD percentage of the load current was 0.34% for load power factor 0.996 and 0.62% for load power factor 0.782. Minimum waveform distortion of inverter ac currents during parallel operation can be achieved if the current magnitudes of both inverters were set the same. In the case of efficiency, the maximum efficiency of the system was 89.07%. Operating the H-bridge CSI with a higher magnitude of the output current will result in higher efficiency of the system.

1. INTRODUCTION

Recently, the application of renewable energy sources especially photovoltaic systems has been increasing in many countries around the world. It is because of some merits introduced by the photovoltaic system, such as reducing environmental pollution, low operating cost, and availability from a few watt power to a larger megawatt-scale system [1]–[4]. Simplicity in installation such as on rooftop is a feature that attracts more interest to photovoltaic for residential application [5]–[7]. Even more so, some governments issued policies giving incentives for the development of renewable energy sources such as photovoltaic power generator to increase its application in their countries. Fortunately, the latest efficiency of a photovoltaic module has achieved 47.1%, realized by using multi-junction concentrator solar cells [8]. It will boost the total efficiency of solar energy conversion into electrical energy.

Moreover, the availability of supporting technologies such as photovoltaic power converters is also another important factor to increase the wider application of the photovoltaic system. Power electronic converters are essential parts of the development of renewable energy applications [9]–[11]. Some renewable energy sources generate electrical energy in the form of dc power, such as photovoltaic systems, and fuel cells. The generated power of other energy sources such as micro hydro power, wind power system, tidal, and sea wave energies are commonly in the form of ac power. They use an ac machine generator to produce electrical
energy. For the dc load system, the generated dc power can be used to supply power load after processed by the dc-dc converter to have stable dc voltage and current as required. In the case of an ac load system, the dc power should be converted into ac power by utilizing dc to ac power converter or power inverter [12]–[14]. The power inverter generates ac power with adjustable frequency, magnitude, and phase angle of its output voltage and current. In case the input of the inverter is dc voltage, and the output is a controllable ac voltage, the inverter is classified as a voltage source inverter (VSI). However, if the input is in dc current form, and the output is controllable ac current, the inverter is called a current source inverter (CSI) [15]–[17]. These two kinds of inverters are applicable for photovoltaic energy conversion systems.

A single-phase power inverter is suitable to be used in a residential PV system, i.e. rooftop installed photovoltaic, where most residential loads are single-phase systems. For a single-phase grid-tied inverter application, the current source inverter introduced some features compared to voltage source inverter such as more immune to short circuit fault, longer lifetime of its power inductors than capacitors, and better quality of ac output current [18]–[22]. Moreover, some circuit topologies of the current source inverter have inherent boost-up voltage capability. Hence, it will eliminate the need for a power transformer to raise the output voltage of the inverter [23]–[25]. For a higher power residential photovoltaic system, a single inverter may not be enough to proceed with the total generated power. The capacity of a commercially available single-phase inverter is limited. Moreover, a single inverter system is weak in reliability issues. Hence, operating some power inverters in parallel is a realistic option to address these issues. In fact, parallel operation of many inverters is an unavoidable situation when many residential photovoltaic systems are operated in grid-tied operation. These inverters can be many types with different circuits and characteristics [26]–[34].

The basic concept of paralleling inverters is shown in Figure 1. As shown in this figure, N number of photovoltaic systems with N number of inverters work in parallel. A study of operation parallel between two H-bridge current source inverters has been discussed in [17]. However, power transformers were applied in this system, and the inverter circuits were the same type. This paper investigates and presents a novel photovoltaic system constructed by two different types of current source power inverters, i.e. H-bridge and common-emitter current source inverters. Each inverter is connected with a different photovoltaic system working in parallel to supply a common ac power load. The proposed system introduces some features such as more immune to short circuit fault, higher power capacity, the possibility of backup operation mode, and better quality of load current. Computer simulation tests were performed to investigate the performance of the system.

![Figure 1. Parallel operation of inverters for photovoltaic systems](image)

2. PROPOSED PHOTOVOLTAIC SYSTEM

Figure 2 presents circuits of a three-level H-bridge current source inverter. The power inductor (L) is utilized to generate dc current source from the input power (V_in) for inverter circuits. Total five controlled power switches with four isolated gate drive circuits are required, including the switch for dc current generator circuit Q. Table 1 is the switching combination of power switches Q1, Q2, Q3, and Q4 to produce a three-level output current, i.e. +I, 0, and –I currents. Moreover, Figure 3 is a three-level common-emitter current source inverter circuit. It is also composed of five controlled power switches. The power inductors L1 and L2 in this circuit are employed to create two dc current sources of the inverter. These two inductors have a common core as shown in the figure. Four power switches are connected together of their emitter terminal at a common point, hence a single isolated power supply can be applied to supply four gate drive circuits of the inverter’s switches.
Moreover, because of the common-emitter connection of its power switches, a lower gradient voltage can be achieved. Hence this inverter is also more suitable for higher speed switching operation, compared to the H-bridge current source inverter. Both inverters need only a single dc current sensor for current controller function as shown in Figure 2 and Figure 3. Table 2 is the switching operation of this three-level common-emitter current source inverter circuit.

![Figure 2. H-bridge current source inverter [35]](image)

![Figure 3. Three-level common-emitter current-source inverter [36], [37]](image)

Table 1. Switching modes of H-bridge CSI

| $Q_1$ | $Q_2$ | $Q_3$ | $Q_4$ | $I_{out}$ |
|-------|-------|-------|-------|------------|
| ON    | OFF   | ON    | OFF   | +1         |
| ON    | OFF   | OFF   | ON    | 0          |
| OFF   | ON    | ON    | OFF   | 0          |
| OFF   | ON    | OFF   | ON    | -1         |

Table 2. Operation mode of common-emitter CSI [18]

| $Q_1$ | $Q_2$ | $Q_3$ | $Q_4$ | $I_{out}$ |
|-------|-------|-------|-------|------------|
| OFF   | OFF   | ON    | ON    | +1         |
| ON    | OFF   | OFF   | ON    | 0          |
| ON    | ON    | OFF   | OFF   | -1         |

In this paper, the three-level H-bridge and common-emitter inverter circuits are applied together to proceed the dc power delivered by two photovoltaic systems to be transformed into ac power to supply power load as depicted in Figure 4. The proposed parallel operation of these circuits is shown in Figure 4 (a). It can be a new alternative operation of inverters to proceed with two photovoltaic systems. Ten photovoltaic modules with a total capacity 1 kWp were applied as dc power source of each inverter circuit. Two arrays of photovoltaic systems were designed in the system. Five photovoltaic modules were connected in series to construct a photovoltaic array as shown in Figure 4 (b). A more number of photovoltaic systems of course will need more inverter circuits to achieve higher power. A common ac power load is connected to both inverters.

The current controlled operation mode was utilized to regulate the power delivered by photovoltaic via inverters to the load. Proportional integral (PI) current controllers were applied to both inverters as shown in Figure 5 and Figure 6. These controllers will adjust the output current and power of each inverter. In the case of a common-emitter inverter, two power inductors with a single core were implemented to generate two dc input current sources for inverter circuits. However, even two inductors were used, only a single sensor was applied to regulate the currents in inductor 1 and inductor 2 as shown in Figure 5. Hence it can simplify the required sensor number. In the case of the H-bridge CSI, the dc current source was created by a single power...
inductor. Hence, a single sensor was required to sense the inductor current for control purpose. The action of a current control signal, and maximum power point tracking (MPPT) was realized by power switch $Q_c$ that will regulate the magnitude of dc current thru changing its duty cycle. Diode $D_f$ was required to ensure the current path for the inductor’s current during switch $Q_c$ turn-off.

To generate a pulse width modulation (PWM) ac current, two triangular carrier signals with opposite offset value plus a single sinusoidal signal were applied to the modulator system as shown in Figure 7. These signals feed in two comparators to generate PWM switching signals. The frequency of carrier signal provides the working frequency of the inverter’s power switches, and the main frequency of ac current is assigned by the frequency of modulating signal. The sinusoidal modulating signal will work also to synchronize the frequency of the two inverters. The comparators will produce PWM signals from the comparison between the carrier and modulating signals. The produced PWM signals will be amplified by gate drive, and on-off controller circuits to operate power switches turn-on and turn-off.

Figure 4. Proposed inverter system (a) proposed parallel system of H-bridge and common-emitter inverters and (b) configuration of photovoltaic system for each inverter

Figure 5. Control of CE-CSI

Figure 6. Control of H-bridge CSI

Figure 7. PWM modulation strategy of inverters

3. RESULTS AND DISCUSSION

To investigate the performance of the proposed inverter system, computer simulation tests were performed using PSIM software. The tested inverter circuits and PV system is shown in Figure 4. Table 3
presents test parameters of the common-emitter inverter circuit, while Table 4 lists test parameters of the H-bridge inverter circuit. The common-emitter inverter utilizes a transformer with the same winding number on both sides functioned as power inductors. The primary winding of a transformer is applied as the first inductor $L_1$, while the secondary winding is set as the second inductor $L_2$. The inductance of inductor $L_1$ and $L_2$ are the same as 0.01 mH with a winding resistance value of 0.1 mΩ. The magnetizing inductance of this transformer is 0.5 mH. In the case of H-bridge CSI, a single power inductor 0.01 mH was applied to generate the input dc current.

The switching operation of both inverters was set the same as 20 kHz, while the modulation index in this test was adjusted at a value of 0.9. A filter capacitor 10 µF was connected to each inverter’s output terminal to filter the harmonics components of its PWM ac current. The two inverters shared a common inductive power load with resistance and inductance connected in series. To investigate different load power factor operations, two inductors with different values were tested with inductance 1 mH and 10 mH. These inductors were connected with resistor 4 Ω which gave load power factors of 0.996 and 0.782, respectively. Moreover, the specification of a photovoltaic module is indicated in Table 5. Ten photovoltaic modules with a capacity per module of 100 Wp were utilized for each inverter system. A constant light intensity of 1000 W/m² was applied to all photovoltaic modules.

| Table 3. Parameters of common-emitter inverter |
|-----------------------------------------------|
| Parameters | Value |
| Inductance $L_1$ and $L_2$ | 0.01 mH |
| Resistance of inductors | 0.1 mΩ |
| Magnetizing inductance | 0.5 mH |
| Filter AC capacitor | 10 µF |
| Working frequency of power switches | 20 kHz |
| Modulation index | 0.9 |
| Main output frequency | 50 Hz |
| Load | $R = 4 \, \Omega$, $L = 1 \, \text{mH}$, and $10 \, \text{mH}$ |

| Table 4. Parameters of H-bridge inverter |
|------------------------------------------|
| Parameters | Value |
| Power inductor | 0.01 mH |
| Filter AC capacitor | 10 µF |
| Working frequency of power switches | 20 kHz |
| Modulation index | 0.9 |
| Main output frequency | 50 Hz |
| Load | $R = 4 \, \Omega$, $L = 1 \, \text{mH}$, and $10 \, \text{mH}$ |

| Table 5. Parameters of PV system |
|----------------------------------|
| Parameters | Value |
| Light intensity | 1000 W/m² |
| Temperature | 25 °C |
| Series resistance | 0.0032 Ω |
| Parallel resistance | 2000 Ω |
| Short circuit current | 12.14 A |
| Number of modules | 10 |
| Capacity per module | 100 Wp |

The system was tested by varying the current controller reference value of the inverter’s output currents from 1 A to 9 A, based on the photovoltaic system capacity. Three possible operating conditions of the inverter system were evaluated to approach the real probable operation as follow:

- The current magnitude of H-bridge CSI was lower than the common-emitter CSI, $I_{cs1} < I_{cs2}$.
- The magnitude of two inverter currents were the same, i.e. $I_{cs1} = I_{cs2}$.
- The current magnitude of H-bridge CSI was higher than the common-emitter CSI, $I_{cs1} > I_{cs2}$.

Figure 8 presents the injected current by H-bridge CSI ($I_{cs1}$), common-emitter inverter ($I_{cs2}$), and load current ($I_{load}$) waveforms when the reference magnitude of H-bridge CSI current was lower than the common-emitter CSI, $I_{cs1} < I_{cs2}$, i.e. 1 A and 9 A. As can be observed, the output currents of the two inverters are sinusoidal currents. High-frequency ripples were more visible for common-emitter inverter current ($I_{cs2}$) where its magnitude is lower than $I_{cs1}$. Figure 9 shows the current waveforms of H-bridge CSI ($I_{cs1}$), common-emitter inverter ($I_{cs2}$), and load current ($I_{load}$) when the magnitude of two inverter currents was adjusted the same, i.e.
I_{csi1} = I_{csi2}. The current waveform of $I_{csi1}$ was a sinusoidal current with a smaller distortion than the first test condition. Furthermore, current waveforms when the current magnitude of H-bridge CSI is higher than the common-emitter CSI, $I_{csi1} > I_{csi2}$ were depicted in Figure 10. The high-frequency current ripples appeared in the current generated by H-bridge CSI ($I_{csi2}$). Current waveforms of $I_{csi1}$ and load current ($I_{load}$) were closely sinusoidal current waveforms.

![Figure 8](image_url)

Figure 8. Injected current by H-bridge CSI ($I_{csi1}$), common-emitter inverter ($I_{csi2}$), and load current ($I_{load}$) waveforms when $I_{csi1} < I_{csi2}$

![Figure 9](image_url)

Figure 9. Injected current by H-bridge CSI ($I_{csi1}$), common-emitter inverter ($I_{csi2}$), and load current ($I_{load}$) waveforms when $I_{csi1} = I_{csi2}$

![Figure 10](image_url)

Figure 10. Injected current by H-bridge CSI ($I_{csi1}$), common-emitter inverter ($I_{csi2}$), and load current ($I_{load}$) waveforms when $I_{csi1} > I_{csi2}$

To make a more detailed analysis of the waveform distortion, Figure 11 presents the harmonics profile of currents $I_{csi1}$, $I_{csi2}$, and $I_{load}$ for different magnitudes at load power factor 0.996. As can be noticed in Figure 11,
in the case of an H-bridge inverter, if the magnitude of output current increases, the THD of output current will decrease. The minimum THD value of H-bridge CSI was 0.50% at output current 5 A, and its maximum value was 21.27% at output current 1 A. In contrast, in the case of a common-emitter inverter, if the magnitude of output current increases, the THD will increase. The minimum THD value of I_{c12} was 0.81% CSI at output current 5 A, and its maximum value was 21.3% at output current 9 A. However, as can be seen in the graph, the THD values of load current were almost constant at around 0.34%. Even the THD value of both inverters varied, the THD value of the load current did not change. Figure 12 is the THD profile for different magnitudes of ac current at power factor 0.782. The minimum THD value of load current was 0.617% when output current H-bridge and common-emitter CSIs were 1 A and 9 A, respectively.

Total harmonics distortion (THD) profile for different load conditions with the same current magnitudes of common-emitter and H-bridge CSIs, i.e., 5 A, is described in Figure 13. As can be viewed in the figure, if the resistance of load increases, the THD of the inverter’s output current will also increase. The lowest THD value of load current was 0.38% when the load was 4 Ω, and the maximum THD was 0.51% when the load was 8 Ω. Moreover, the efficiency profile of the inverter system for different current magnitude operations is shown in Figure 14. The power inductors and diodes count of common emitter CSI is larger than H-bridge CSI. It will cause more power losses in the circuits. Hence, the efficiency of common-emitter CSI is basically lower than H-bridge CSI. Operating the H-bridge CSI in a larger current magnitude will give higher efficiency to the system. Compared to the system applying voltage source inverters, a lower efficiency is a limitation of the proposed current source inverter system. From the data, the minimum waveform distortion of inverter ac currents during parallel operation can be achieved if the current magnitudes of both inverters were set the same.

4. CONCLUSION

A novel photovoltaic energy conversion system constructed using H-bridge and common-emitter current source inverter circuits connected in parallel has been proposed and presented. In the case of dc current source generation, the H-bridge CSI circuit is less complex than the common-emitter CSI because it needs a single power inductor only. However, for gate drive circuit requirements, the common-emitter CSI is simpler because of the common-emitter connection of its power switches. The proposed system can be a new alternative for a photovoltaic system with a high-quality load current waveform. Test results have shown that the distortion
of load current was less than 1%. Higher efficiency of the inverter system can be achieved by operating the H-bridge CSI with a higher magnitude of output current than the common-emitter CSI.

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REFERENCES

[1] J. Jurasz, F. A. Canalesc, A. Kiesd, M. Guezgouze, and A. Belucof, “A review on the complementarity of renewable energy sources: Concept, metrics, application and future research directions,” Solar Energy, vol. 195, pp. 703-724, 2020, doi: 10.1016/j.solener.2019.11.087.

[2] S. Wang, “Current status of PV in China and its future forecast,” CSEE Journal of Power and Energy Systems, vol. 6, no. 1, pp. 72-82, 2020, doi: 10.17775/CSEEJPS.2019.03170.

[3] A. Gholami, M. Ameri, M. Zandi, R. G. Ghoachani, S. Eslami and S. Pierfederci, “Photovoltaic Potential Assessment and Dust Impacts on Photovoltaic Systems in Iran: Review Paper,” IEEE Journal of Photovoltaics, vol. 10, no. 3, pp. 824-837, 2020, doi: 10.1109/JPHOTOV.2020.2978851.

[4] J. C. Blakesley, T. Huld, H. Muellehans, A. Gracia-Amilllo, G. Friessen, T.R. Betts, and W. Hermann, “Accuracy, cost and sensitivity analysis of PV energy rating,” Solar Energy, vol. 203, pp. 91-100, 2020, doi: 10.1016/j.solener.2020.03.088.

[5] F. Luo, G. Ranzi, C. Wan, Z. Xu and Z. Y. Dong, “A Multistage Home Energy Management System With Residential Photovoltaic Penetration,” IEEE Transactions on Industrial Informatics, vol. 15, no. 1, pp. 116-126, 2019, doi: 10.1109/TII.2018.2871159.

[6] L. Callegaro, G. Konstantinou, C. A. Rojas, N. F. Avila and J. E. Fletcher, “Testing Evidence and Analysis of Rooftop PV Inverters Response to Grid Disturbances,” IEEE Journal of Photovoltaics, vol. 10, no. 6, pp. 1882-1891, 2020, doi: 10.1109/JPHOTOV.2020.3014873.

[7] R. Panigrahi, S. K. Mishra, S. C. Srivastava, A. K. Srivastava and N. Schulz, “Grid Integration of Small-Scale Photovoltaic Systems in Secondary Distribution Network-A Review,” IEEE Transactions on Industry Applications, vol. 56, no. 3, pp. 3178-3195, 2020, doi: 10.1109/TIA.2020.2979789.

[8] J. F. Geisz, M. A. Steiner, N. Jain, K. L. Schulte, R. M. France, W. E. McMahon, E. E. Perl, and D. J. Friedman, “Building a six-junction inverted metamorphic concentrator solar cell,” IEEE Journal of Photovoltaics, vol. 8, no. 2, pp. 626-632, 2018, doi: 10.1109/JPHOTOV.2017.2777567.

[9] S. B. Kjaer, J. K. Pedersen and F. Blaabjerg, “A review of single-phase grid-connected inverters for photovoltaic modules,” IEEE Transactions on Industry Applications, vol. 41, no. 5, pp. 1292-1306, 2005, doi: 10.1109/TIA.2005.853371.

[10] K. Alluhabii, I. Barsaleh and H. Hu, “Comprehensive Review and Comparison of Single-Phase Grid-Tied Photovoltaic Microinverters,” IEEE Journal of Emerging and Selected Topics in Power Electronics, vol. 8, no. 2, pp. 1310-1329, 2020, doi: 10.1109/JESTPE.2019.2904013.

[11] J. M. Carrasco et al., “Power-Electronic Systems for the Grid Integration of Renewable Energy Sources: A Survey,” IEEE Transactions on Industrial Electronics, vol. 53, no. 4, pp. 1002-1016, 2006, doi: 10.1109/TIE.2006.878356.

[12] S. W. Shmeen, F. N. Abdullah, and D. H. Shaker, “Simulation model of single phase PWM inverter by using MATLAB/Simulink”, International Journal of Power Electronics and Drive Systems, vol. 12, no. 1, pp. 212-216, 2021, doi: 10.11591/ijece.v12i1.pp212-216.

[13] Z. Bai and Z. Zhang, “Conformation of Multilevel Current Source Converter Topologies Using the Duality Principle,” IEEE Transactions on Power Electronics, vol. 23, no. 5, pp. 2260-2267, 2008, doi: 10.1109/TPEL.2008.2001893.

[14] N. Vazquez, H. Lopez, C. Hernandez, E. Vazquez, R. Osorio and J. Arau, “A Different Multilevel Current-Source Inverter,” IEEE Transactions on Industrial Electronics, vol. 57, no. 8, pp. 2623-2632, 2010, doi: 10.1109/TIE.2009.2030814.

[15] N. F. N. Ismail, N. A. Rahim, S. R. S. Rainah, and Y. Al-Turki, “Parallel inductor multilevel current source inverter with energy-recovery scheme for inductor currents balancing,” IET Power Electronics, vol. 9, issue 11, pp. 2298-2304, 2016, doi: 10.1049/iet-pel.2015.0909.

[16] K. Gnanasambandam, A. K. Rathore, A. Edpuganti, D. Srinivasan, and J. Rodriguez, “Current-fed multilevel converters: an overview of circuit topologies, modulation techniques, and applications,” IEEE Transactions on Power Electronics, vol. 32, no. 5, pp. 3382-3401, 2016, doi: 10.1109/TPEL.2016.2585576.

[17] Suroso, D. T. Nugroho, Amran, and T. Noguchi, “Parallel operation of current-source inverter for low-voltage high-current grid-connected photovoltaic system,” International Journal of Electrical and Computer Engineering, vol. 9, no. 4, pp. 2220-2229, 2019, doi: 10.11591/ijece.v9i4.pp2220-2229.

[18] Suroso and T. Noguchi, “A new three-level current-source PWM inverter and its application for grid connected power conditioner,” IEEE Transactions on Industrial Electronics, vol. 64, no. 7, pp. 5449-5459, 2017, doi: 10.1109/TIE.2017.2674595.

[19] X. Guo, N. Wang, J. Zhang, B. Wang and M. Nguyen, “A Novel Transformerless Current Source Inverter for Leakage Current Reduction,” IEEE Access, vol. 7, pp. 50681-50690, 2019, doi: 10.1109/ACCESS.2019.2908287.

[20] H. Keyhani, and H. A. Toliyat, “Single-stage multistage PV inverter with an isolated high-frequency link and soft-switching operation,” IEEE Transactions on Power Electronics, vol. 29, no. 8, pp. 3919-3929, 2014, doi: 10.1109/TPEL.2013.2288361.

[21] S. V. Araujo, P. Zacharias and R. Mallwitz, “Highly Efficient Single-Phase Transformerless Inverters for Grid-Connected Photovoltaic Systems,” IEEE Transactions on Industrial Electronics, vol. 57, no. 9, pp. 3118-3128, 2010, doi: 10.1109/TIE.2009.2073654.

[22] P. G. Barbosa, H. A. Carvalho Braga, M. D. Carvo Barbosa Rodrigues and E. C. Teixeira, “Boost current multilevel inverter and its application on single-phase grid-connected photovoltaic systems,” IEEE Transactions on Power Electronics, vol. 21, no. 4, pp. 1116-1124, 2006, doi: 10.1109/TPEL.2006.876784.

[23] L. S. Garcia, G. M. Buatti, L. C. de Freitas, E. A. A. Coelho, V. J. Farias and L. C. Gomes de Freitas, “Dual Transformerless Single-Stage Current Source Inverter With Energy Management Control Strategy,” IEEE Transactions on Power Electronics, vol. 28, no. 10, pp. 4644-4656, 2013, doi: 10.1109/TPEL.2012.2234139.

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