Linear Quadratic Regulator for Impulse Uncontrollable Singular Systems

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Abstract

This paper investigates the linear quadratic regulator problem for singular systems which may contain some impulse uncontrollable modes. By transforming to the Weierstrass form, impulse controllable and uncontrollable subsystems can be separated. Sufficient conditions are proposed, under which solutions to both state and costate equations for the linear quadratic regulator problem are impulse-free. The necessary conditions for the minimization of the quadratic cost function are converted to a two-point boundary value problem, which can be solved by either computing its back-time state transition matrix or solving a Riccati equation. Two examples are provided to illustrate the main results.

Keywords: Singular systems; Descriptor systems; Linear quadratic regulator; Optimal feedback

Introduction

Singular systems, also called descriptor systems, arise naturally in chemical processes, mechanical systems, and so on. Therefore, since the last seventies, singular systems have attracted intensive attention. Linear quadratic regulator (LQR) problems play an important role in the field of control engineering. Therefore the LQR problems for descriptor systems have been investigated in the literature. The earliest papers on this problem are those of [1] and [2]. This problem were also addressed in ref. [3,4], where a generalized Riccati equation is shown to result directly from the necessary conditions for the existence of an optimal control. The generalized Riccati equation proposed in [3] may not have solutions, which was shown in ref. [5]. Bender and Laub [5] approached this problem by performing a singular value decomposition (SVD) to isolate the dynamics from non-dynamic portion, and four equivalent Riccati equations were derived in the SVD coordinate system. [6] investigated that the robust properties of the LQR for singular systems with single input. A parametrization of the optimal feedback gains was used to show that certain robust properties can be achieved by an appropriate choice of the feedback gain. The LQR problem for linear time-varying singular systems was addressed in ref. [7], [8] derived a Riccati equation formulated in the original state parameters under which the problem has a solution. The LQR problem for non-regular singular systems was solved by converting a non-regular singular system into a regular one with index one in ref. [9].

It is worth pointing out that all the results on the LQR problem for singular systems mentioned above were obtained with an assumption that the singular systems are impulse controllable, that is, the impulsive modes can be removed by applying a state feedback. However, many practical systems, especially constrained mechanical systems (see Example 1), can not be modelled by an impulse controllable singular system. Therefore, the LQR problem for impulse uncontrollable singular systems is not only theoretically interesting but also practically important [10].

In this paper, the LQR problem for impulse uncontrollable singular systems is addressed. In order to guarantee the existence of the cost function, solutions to the singular systems should contain no impulse, which can be achieved by a feedback if the systems are impulse controllable or by choosing initial conditions properly for impulse uncontrollable cases [11]. Moreover, the final conditions should be properly chosen as well to guarantee that the optimal solution to the LQR problem is impulse-free. In order to facilitate the analysis, the singular system is assumed to be in the Weierstrass form [12].

Problem Formulation

Consider the problem of finding \( u(t) \) to minimize

\[
J(x,u,u_1) = \frac{1}{2} \int x^T Q x + u^T R u \, dt
\]

with the constraint

\[
E x(t) = Ax(t) + Bu(t), \quad E x(0) = E_0
\]

Where \( R > 0 \), \( Q = Q^T \geq 0 \), \( x(t) \in R^n \), \( u(t) \in R^m \), and \( E \) is a square matrix of rank \( q \leq n \). The pencil \((sE - A)\) is assumed to be regular, that is, \( \det(sE - A) \neq 0 \) for some \( s \). Let \( \rho = \deg(\det(sE - A)) \). Assume that there exist invertible matrices \( U \) and \( V \) so that

\[
UEV = \begin{pmatrix} I & 0 \\ 0 & N \end{pmatrix}, \quad UAV = \begin{pmatrix} A_1 & 0 \\ 0 & I \end{pmatrix}, \quad UB = B_1
\]

\[
V^T x = \begin{pmatrix} x_1 \\ x_2 \end{pmatrix}, \quad U^T p = \begin{pmatrix} p_1 \\ p_2 \end{pmatrix}, \quad V^T QV = \begin{pmatrix} Q_1 & Q_{12} \\ Q_{21} & Q_2 \end{pmatrix}
\]

\[
U^T Q U^{-1} = \begin{pmatrix} Q_{11} & Q_{12} \\ Q_{21} & Q_{22} \end{pmatrix}, \quad V^T x = \begin{pmatrix} x_1 \\ x_2 \end{pmatrix},
\]

where \( p \) is the costate variable defined in (7) or (14), \( x_1(t) \in R^n \), \( x_2(t) \in R^{n-q} \), \( p_1(t) \in R^{n-q} \), \( p_2(t) \in R^{m-r} \), \( A_1 \in R^{n-q} \times n-q \), \( B_1 \in R^{n-q} \times m \), \( Q_1 = Q_1^T \in R^{n-q} \times n-q \), \( Q_2 = Q_2^T \in R^{m-r} \times m-r \), \( Q_{21}, Q_{12} \in R^{m-r} \times n-q \), \( N \in R^{n-q} \times (n-q) \) is a nilpotent matrix of the nilpotency \( v \). Without loss of generality, assume that \( N \) takes a Jordan normal form of \( N = \text{diag}(N_1, \ldots, N_s) \) with the Jordan block \( N_i \) being a shift matrix of size \( v_i \times v_i \), and \( \forall z \in R^{n}, x_2 \in R^{m-r} \), \( x_2 = 0 \) implies \( x_2 = 0 \).

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It will prove useful to partition $x_2, p_2, Q_{21}, Q_{22}$ as follows:

$$x_2 = \begin{bmatrix} x_1 \ \ x_2 \end{bmatrix}, \quad p_2 = \begin{bmatrix} p_1 \ \ p_2 \end{bmatrix}, \quad Q_{21} = \begin{bmatrix} Q_{11} & \vdots & Q_{12} \end{bmatrix}, \quad Q_{22} = \begin{bmatrix} \vdots & \ddots & \vdots \ \ \vdots & \ddots & \vdots \ \ \vdots & \ddots & \vdots \ \ Q_{21} & \vdots & Q_{22} \end{bmatrix}$$

with $x_1 \in \mathbb{R}^n$, $p_1 \in \mathbb{R}^m$, $B_2 \in \mathbb{R}^{m \times n}$, $Q_{21} \in \mathbb{R}^{m \times n}$, $Q_{22} \in \mathbb{R}^{m \times m}$, $Q_{21} = (Q_{21})^\top \in \mathbb{R}^{n \times m}$, $Q_{12} \in \mathbb{R}^{n \times n}$, $Q_{12} = (Q_{12})^\top \in \mathbb{R}^{m \times n}$, and $i = 1, \ldots, \gamma$ for $j = 1, \ldots, \gamma$.

Furthermore, for $i = 1, \ldots, \gamma$, partition $x_2^i, p_2^i, B_2^i, Q_{21}^i, Q_{22}^i$ into $1 \times \rho x$.

Assumption 2: $N_i^2 Q_{21}^i = 0$ for $i = \gamma_1 + 1, \ldots, \gamma_2$. $N_i^2 Q_{22}^i = 0$ for $i = \gamma_1 + 1, \ldots, \gamma_2$.

Assumption 3: $N_i x_2^i = 0$ for $i = \gamma_1 + 1, \ldots, \gamma_2$.

Assumption 4: $N_i^2 Q_{21}^i = 0$ for $i = \gamma_1 + 1, \ldots, \gamma_2$. $N_i^2 Q_{22}^i N_j = 0$ for $i = \gamma_1 + 1, \ldots, \gamma_2$, $j = 1, \ldots, \gamma$.

In addition, in order to make the cost function finite for the case of an infinite horizon, the following assumption is necessary.

Assumption 6: The finite modes of $(2)$ are stabilizable, that is, $(A, B)$ is stabilizable.

### Necessary Conditions

The necessary conditions for $f$ to be minimized are

$$Ex(t) = \partial H / \partial q$$

$$E^c p(t) = -\partial H / \partial x$$

$$0 = \partial H / \partial u$$

with $H = x^T Q x + a^T R u + c^T (A x + B u)$ and the boundary conditions $E x(0) = E x_0$ and $E^c p(T) = E^c \dot{Q} E x(T)$, which, in the Weierstrass form, can be written as

$$x_1(0) = x_0$$

$$N_i x_2^i(0) = N_i x_2^i$$

$$p_1(t) = Q_{21} x_1(t) + \sum_{j=1}^\gamma N_i^2 Q_{21}^i \dot{x}_2^i(t)$$

$$N_i^2 p_1(t) = N_i^2 Q_{22}^i x_1(t) + \sum_{j=1}^\gamma N_i^2 Q_{22}^i N_i x_2^i(t)$$

where $i = 1, \ldots, \gamma$. It follows from (6)-(8) that

$$E x(t) = A x(t) + B u(t)$$

$$E^c p(t) = -Q x(t) - A^c p(t)$$

$$0 = R^c p(t) + R u(t)$$

which, in the Weierstrass form, can be expressed as

$$\dot{x}_1(t) = A x_1(t) + B u(t)$$

$$\dot{x}_2^i(t) = x_2^i(t) + B_2^i u(t)$$

$$\dot{p}_1(t) = -Q_{21} x_1(t) - \sum_{j=1}^\gamma N_i^2 Q_{21}^i \dot{x}_2^i(t) - A^c p_1(t)$$

$$\dot{p}_2^i(t) = -Q_{22}^i x_1(t) - \sum_{j=1}^\gamma N_i^2 Q_{22}^i N_i x_2^i(t) - p_2^i(t)$$

$$0 = R^c p_1(t) + \sum_{j=1}^\gamma (B_2^i)^\top p_2^i(t) + R u(t)$$

where $i = 1, \ldots, \gamma$.

### Solutions of the LQR Problem

This section is devoted to finding a solution to the two-point boundary value problem described by (16)-(20) with the boundary conditions (9)-(12). Before doing this, first let us examine the implication of Assumptions 2-3.

With the special structure of $N_i$ in mind, the following lemma can be verified using Assumption 2.

**Lemma 1:** If Assumption 2 is satisfied, then $(B_2^i)^\top = 0$ for $i = \gamma_1 + 1, \ldots, \gamma_2$, $i = \gamma_1 + 1, \ldots, \gamma_2$, where $(B_2^i)$ is the $j$-th row of $B_2^i$. 

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Proof. A simple calculation shows that
\[
N_t' = \begin{bmatrix} (B_t) \cdots (B_t) \end{bmatrix} = \begin{bmatrix} 0 \cdots 0 \end{bmatrix}
\]
for \(i = \gamma_i + 1, \ldots, \gamma_j\), from which the conclusion of the lemma can be directly drawn.

Assumptions 2-3 are sufficient for solutions of the subsystems corresponding to the Jordan blocks \(\gamma_i + 1, \ldots, \gamma_j\) to be impulse-free, which will be proved in the following lemma.

**Lemma 2:** If Assumptions 2 and 3 are satisfied, then \(\pi_i(t) = 0\) for \(i = \gamma_i + 1, \ldots, \gamma_j\).

Proof. Note that Assumption 3 implies \(N_{\gamma_i}(0) = N_{\gamma_i} = 0\) for \(i = \gamma_i + 1, \ldots, \gamma_j\). Applying this and Assumptions 2 to (5) gives
\[
x_i(t) = \pi_i(t) = -\sum_{k=1}^{\omega_i} e^{\gamma_i t} (N_{\gamma_i}(0) - B_{\gamma_i}(t)) - \sum_{k=1}^{\omega_i} e^{\gamma_i t} (N_{\gamma_i}(0) - B_{\gamma_i}(t)) = -\pi_{\gamma_i}(t)
\]
which, according to Lemma 1, means that \(\pi_i(t) = 0\) for \(i = \gamma_i + 1, \ldots, \gamma_j\).

Similar to the proof of Lemma 1, it is straightforward to prove the following lemma.

**Lemma 3:** If Assumption 4 is satisfied, then \((Q_{\gamma_i})_k = 0\) for \(k = 1, \ldots, \gamma_i - 1, i = \gamma_i + 1, \ldots, \gamma_j\), and \((Q_{\gamma_i})_k = 0\) for \(k = 1, \gamma_i + 1, \ldots, \gamma_j, i = \gamma_i + 1, \ldots, \gamma_j\), where \((Q_{\gamma_i})_k\) and \((Q_{\gamma_i})_k\) are the \(k\)-th rows of \(Q_{\gamma_i}\) and \(Q_{\gamma_i}\), respectively.

Proof. The conclusion can be drawn from the relations.

\[
N_{\gamma_i}^T Q_{\gamma_i} = \begin{bmatrix} (Q_{\gamma_i})_k \cdots (Q_{\gamma_i})_k \end{bmatrix} = \begin{bmatrix} 0 \cdots 0 \end{bmatrix}
\]
\[
N_{\gamma_i}^T Q_{\gamma_i} = \begin{bmatrix} 0 \cdots 0 \end{bmatrix}
\]

The following lemma indicates that the final values for \(\pi\) are zeros for \(i = \gamma_i + 1, \ldots, \gamma_j\) if Assumption 5 is satisfied.

**Lemma 4:** If Assumption 5 is satisfied, then \(\pi(t) = 0\) for \(i = \gamma_i + 1, \ldots, \gamma_j\).

Proof. Due to Assumption 5, (12) can be rewritten as
\[
\begin{bmatrix} \pi(t) \end{bmatrix} = N_{\gamma_i}^T Q_{\gamma_i} x_{\gamma_i}(t) + \sum_{k=1}^{\omega_i} N_{\gamma_i}^T Q_{\gamma_i} N_{\gamma_i} x_{\gamma_i}(t) = \begin{bmatrix} 0 \\ 0 \end{bmatrix}
\]

The following lemma shows that solutions to the costate subsystems corresponding to the Jordan blocks \(\gamma_i + 1, \ldots, \gamma_j\) are impulse-free if Assumptions 4-5 are satisfied.

**Lemma 5:** If Assumptions 4-5 are satisfied, then \(\pi(t) = 0\) for \(i = \gamma_i + 1, \ldots, \gamma_j\).

Proof. It can be proved that solutions to (19) is given by
\[
p_i(t) = -\sum_{k=1}^{\omega_i} e^{\gamma_i t} (t - t_r)^{-1} (-N_{\gamma_i}) p_i(t)
\]
for \(i = \gamma_i + 1, \ldots, \gamma_j\). It follows from Lemma 4 that \((-N_{\gamma_i}) p_i(t) = 0\) for \(i = \gamma_i + 1, \ldots, \gamma_j\). As a result, with Assumption 4, \(p_i(t)\) can be simplified as
\[
p_i(t) = -\sum_{k=1}^{\omega_i} e^{\gamma_i t} (t - t_r)^{-1} (-N_{\gamma_i}) p_i(t)
\]
which, together with Lemma 3, implies that the lemma holds.

A simple manipulation shows that for \(i = 1, \ldots, \gamma_j\), (17) and (19) can be expressed as
\[
\pi_i = A_i x_{\gamma_i} + A_{\gamma_i} x_{\gamma_i} + B u
\]
(21)
and
\[
0 = A_{\gamma_i} x_{\gamma_i} + B u
\]
(22)

Similarly, the final values for \(\pi\) are zeros and \(\pi\) for \(i = 1, \ldots, \gamma_j\), where
\[
\pi_i = A_i x_{\gamma_i} + A_{\gamma_i} x_{\gamma_i} + B u
\]
(23)

Similar to the proof of Lemma 1, it is straightforward to prove the following lemma.

**Lemma 6:** If Assumption 5 is satisfied, then \(\pi(t) = 0\) for \(i = 1, \ldots, \gamma_j\).

Proof. Due to Assumption 5, (12) can be rewritten as
\[
\begin{bmatrix} \pi(t) \end{bmatrix} = N_{\gamma_i}^T Q_{\gamma_i} x_{\gamma_i}(t) + \sum_{k=1}^{\omega_i} N_{\gamma_i}^T Q_{\gamma_i} N_{\gamma_i} x_{\gamma_i}(t) = \begin{bmatrix} 0 \\ 0 \end{bmatrix}
\]

The following lemma indicates that the final values for \(\pi\) are zeros for \(i = 1, \ldots, \gamma_j\) if Assumption 5 is satisfied.

**Lemma 7:** If Assumption 5 is satisfied, then \(\pi(t) = 0\) for \(i = 1, \ldots, \gamma_j\).

Proof. Due to Assumption 5, (12) can be rewritten as
\[
\begin{bmatrix} \pi(t) \end{bmatrix} = N_{\gamma_i}^T Q_{\gamma_i} x_{\gamma_i}(t) + \sum_{k=1}^{\omega_i} N_{\gamma_i}^T Q_{\gamma_i} N_{\gamma_i} x_{\gamma_i}(t) = \begin{bmatrix} 0 \\ 0 \end{bmatrix}
\]

The following lemma shows that solutions to the costate subsystems corresponding to the Jordan blocks \(\gamma_i + 1, \ldots, \gamma_j\) are impulse-free if Assumptions 4-5 are satisfied.
Lemma 6: If Assumption 1 is satisfied, then the matrix $\tilde{B}_2$ has full row rank.

Proof. This lemma can be easily verified by applying Assumption 1.

Assumption 7: $\tilde{R} - \tilde{R}^T \bigg[ -\tilde{q}^{11}_2 - \tilde{q}^{12}_2 \bigg] \tilde{q}^{22}_2 > 0$ and $\tilde{q}^{11}_2 > 0$.

Lemma 7: If Assumptions 1 and 7 are satisfied, then $\tilde{R}$ is invertible.

Proof. Note that

$$
\begin{bmatrix}
0 & 0 & I & \tilde{B}_2 \\
0 & \tilde{q}^{11}_2 & \tilde{q}^{12}_2 & 0 \\
I & \tilde{q}^{11}_2 & \tilde{q}^{12}_2 & 0 \\
I & \tilde{q}^{11}_2 & \tilde{q}^{12}_2 & 0
\end{bmatrix} = \tilde{R} \begin{bmatrix}
0 & 0 & I \\
0 & 0 & I \\
0 & 0 & I \\
0 & 0 & I
\end{bmatrix} \begin{bmatrix}
\tilde{E}_2 \\
\tilde{E}_2 \\
\tilde{E}_2 \\
\tilde{E}_2
\end{bmatrix} = \tilde{R}
$$

is invertible. Therefore, according to Lemma 6, $\tilde{R}$ is invertible.

Therefore, $\tilde{x}_t(t)$, $\tilde{p}_t(t)$, and $u(t)$ can be uniquely determined from (33), (35), and (36) as

$$
\begin{bmatrix}
\hat{p}_t(t) \\
\hat{x}_t(t) \\
u(t)
\end{bmatrix} = \tilde{R}^{-1} \tilde{S}^{-1} \begin{bmatrix}
\tilde{x}_t(t) \\
\tilde{p}_t(t) \\
\tilde{u}(t)
\end{bmatrix}
$$

This can then be substituted back into (32) and (34), which results in a usual two-point boundary value problem of linear-quadratic optimal control with $\tilde{x}_t(t)$ and $\tilde{h}_t(t)$ as the state and costate instead of $x(t)$ and $p(t)$.

(32) and (34) becomes

$$
\begin{bmatrix}
\hat{x}_t(t) \\
\hat{p}_t(t)
\end{bmatrix} = \begin{bmatrix}
\tilde{A}_t & -\tilde{R} \\
-\tilde{\tilde{Q}} & -\tilde{\tilde{A}}
\end{bmatrix} \begin{bmatrix}
\tilde{x}_t(t) \\
\tilde{p}_t(t)
\end{bmatrix}
$$

with the boundary conditions of (37) and (38) where $\tilde{A} = \tilde{A}_t - \tilde{R} \tilde{S}^{-1} \tilde{S}^{-1}$, $\tilde{h} = \tilde{h}_t$, and $\tilde{Q} = \tilde{Q}_t - \tilde{R} \tilde{S}^{-1} \tilde{S}^{-1}$.

The solutions to the two-point boundary value problem (40) can be solved by computing its back-time state transition matrix

$$
\begin{bmatrix}
\tilde{x}_t(t) \\
\tilde{p}_t(t)
\end{bmatrix} = \begin{bmatrix}
\tilde{Q}_t(t, t_{f}) \\
\tilde{P}_t(t, t_{f})
\end{bmatrix} \begin{bmatrix}
\tilde{x}_t(t_{f}) \\
\tilde{p}_t(t_{f})
\end{bmatrix}
$$

By following the approach proposed by Bender and Laub [5], the optimal feedback gain can be determined by solving the equation

$$
U(t) = K(t) X(t)
$$

for $K(t)$ with $X(t) = \begin{bmatrix} \tilde{x}_t(t) \\ \tilde{X}_t(t) \end{bmatrix}$. The general solutions is

$$
K(t) - U(t) X(t) + Y(t) \bigg[ I - X(t) X(t)^T \bigg] \tilde{x}_t(t)
$$

where $Y(t) = R^{*\infty}$ is an arbitrary real matrix and $U$ can be determined from

$$
\begin{bmatrix}
\hat{P}_t \\
\hat{X}_t \\
U
\end{bmatrix} = \begin{bmatrix}
\tilde{A}_t & 0 \\
\tilde{Q}_t & \tilde{B}_t
\end{bmatrix} \begin{bmatrix}
\tilde{E}_2 \\
\tilde{E}_2
\end{bmatrix}
$$
With $P$ being the solution of the following Riccati equation
\[ P = P \dot{A} + A^T P + \dot{Q} - P \dot{R}^T P, \quad P(t_0) = \dot{Q}(t_0). \] (45)

The main results can be summarized by the following theorem.

**Theorem 1.** Assume that the singular system is in the Weierstrass form. If Assumptions 1-7 are satisfied, then

1. there exists a unique, impulse-free solution of the necessary conditions (16)-(20), together with the boundary conditions (9)-(12), which can be found from (39) and (40);
2. the optimal feedback gain can be determined by (43);
3. the optimal cost $J$ from (1) is given by $J = \frac{1}{2} \dot{q}^T P(t_0) \dot{q}_0$.

**Examples**

**Example 1.** Consider a simple example of a planar manipulator constrained so that the end effector can only move along a straight line. The equations of motion [10] is given by
\[ \ddot{q}_1 = u_1 + f_1, \]
\[ \ddot{q}_2 = u_2 + f_2 \]
with a constraint equation of $q_1 + 2q_2 = 1$.

Thus, the forces of constraint are $f_1 = \lambda$ and $f_2 = 2\lambda$. Set $x_1 = 2q_1 - q_2$, $x_2 = 2\dot{q}_1 - \dot{q}_2$, $x_3 = 5\lambda$, $x_4 = \dot{q}_1 + 2\dot{q}_2$, $x_5 = q_1 + 2q_2 - 1$. Then, the manipulator can be expressed as the form of (3)-(4) with
\[ A_1 = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}, \quad B_1 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}, \quad N_1 = \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix}, \quad B_2 = \begin{bmatrix} 1 \\ 2 \\ 0 \\ 0 \\ 0 \end{bmatrix}. \]

This system is not impulse controllable with $y_1 = 0, y_2 = 1$. It can be verified that Assumptions 1-7 are satisfied with initial conditions $q_{10} + 2q_{20} - 1 = 0,$
\[ \dot{q}_{10} + 2\dot{q}_{20} = 0, \] and matrices $Q_1 = \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix}, \quad Q_2 = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$
\[ Q_{12} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}, \quad Q_{21} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}, \quad Q_{22} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}.$ It is simple to verify the following:
\[ \dot{B}_1 = B_1, \quad \dot{B}_2 = B_2, \quad \dot{Q}_1 = Q_1, \quad \dot{Q}_2 = Q_2, \quad \dot{Q}_{12} = Q_{12}, \quad \dot{Q}_{21} = Q_{21}, \quad \dot{Q}_{22} = Q_{22}. \]

\[ \dot{A}_1 = A_1, \quad \dot{Q}_1 = Q_1, \quad \dot{Q}_{11} = Q_{11}, \] and $A_2 = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}, \quad \dot{A}_2 = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$. Set $P = \begin{bmatrix} P_{11} & P_{12} \\ P_{21} & P_{22} \end{bmatrix}$. Then, the Riccati equation (45) for the case of $t_f = \infty$ has a unique positive definite solution of
\[ P = \begin{bmatrix} \frac{1}{5} \sqrt{0.5 \sqrt{2} + 25} \\ \frac{1}{5} \sqrt{0.5 \sqrt{2} + 5} \end{bmatrix}. \]

It follows from (44) that $\dot{X}_1(t) = 0$

and $U(t) = K_1 \dot{X}_1(t)$ with $K_1 = \begin{bmatrix} -\frac{2}{5} \sqrt{5} & -\frac{2}{5} \sqrt{0.5 \sqrt{2} + 5} \\ \frac{1}{5} \sqrt{0.5 \sqrt{2} + 5} & \frac{1}{5} \sqrt{0.5 \sqrt{2} + 5} \end{bmatrix}$. According to

(42), the feedback $K = [K_1, K_2]$ can be found with $K_2$ being arbitrary.

**Conclusion**

In this paper, the linear quadratic regulator problem has been solved for a linear time-invariant singular systems which may not be impulse controllable. The impulse controllable and uncontrollable subsystems have been separated by transforming the singular system into the Weierstrass form. The sufficient conditions have been proposed so that the impulse uncontrollable subsystems and their corresponding costate subsystems admit a unique impulse-free solution. The necessary conditions for the minimization of the quadratic cost function have been converted to the Riccati equation.

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