Effects of Flowable Composite Resin and curing method on Microleakage

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INTRODUCTION

Resin composite are routinely used as restorative materials in anterior and posterior teeth due to their excellent elastic qualities (1).

However, polymerization shrinkage of resin matrix is still considered highly relevant in unsuccessful resin composite direct restoration (2).

The forces generated by polymerization shrinkage may induce stresses that could break the bonding at the cavity walls. which is one of the main causes of marginal failure ad subsequent, microleakage (3).

Marginal microleakage is defined as the penetration of acid, enzymes, ions, bacteria and bacterial products between...
cavity wall and the restorative material, and its responsible for marginal discoloration, post operative sensitivity, secondary, secondary caries and pulp damage\(^4\).

In modern adhesive dentistry, a number of different materials and clinical procedures have been advocated to minimize some of most trouble some problems with direct posterior composites, and among several protocols, the use of flowable resin composite has been suggested as a means to reduce the possibility of microleakage \(^5,6\).

The flowable resin materials have low viscosity, high flowability and are richer in resin than traditional composites, their elastic modulus is low, (it is about 50% of the conventional resins composite) so their tenacity values are better than those of conventional one \(^7\). It acts as buffer against the contraction forces of the overlying composite resin during the curing process, so the flowable composites have been indicated as liners \(^8\).

The use of resin liner with flow, has been suggested as a mean to reduced the possibility of microleakage \(^9\).

Co-curing the adhesive and flowable composite has also been occasionally recommended, although supporting evidence is sparse \(^10,11,12\).

The objective of this invitro study was to investigate the microleakage in Cl V composite restoration using flowable resin composite associated with an adhesive, either light cured separately or co-cured.

**MATERIALS AND METHODS**

Sixty, caries-free, restoration-free extracted human premolars were selected and stored in distilled water prior to the study, teeth thoroughly cleaned, then polished with a slurry of non fluoridated pumice and water in a rubber prophylaxis cup at a low speed, in order to obtain a clean, smooth and hard surface. The teeth were examined by fiber optic light to exclude crakes.

In each tooth a standardized box shaped class V cavity of 3.0 mm (mesial-distal), 2.0mm (occlusal-gingival) and 2.0mm depth was prepared using a cylindrical diamond bur No.556 in a high speed hand piece with air/water coolant on buccal surface, just below the cementoenamel junction, with enamel and dentin margins.

Each bur was used for Four preparation and then replaced. Cavities were received 0.5mm bevel at a 45 angle on their occlusal margins, cervical margins ended at a 90 angle with the longitudinal surfaces of the teeth.

Preparation of the teeth, restoration and finishing were performed by one operator.

In all groups the total etch technique was performed prior the establishment of the adhesive layer. A 35% phosphoric acid (Scothbond Etchant Gel, 3M - ESPE, st. paul, MN, USA) was applied initially to the enamel margins and then extended from the superficial to deep dentin for 20 sec. washing and drying, leaving moist dentin (avoid dentinal dehydration). The teeth were randomly assigned into three groups of twenty cavities each, according to the restorative technique used:

Group 1- Single bond Excite adhesive system (Ivoclar, Vivadent AG, 9494 Schaan/Liechtenstein) was applied according to the manufacturer's instructions and light cured with visible light source (Viva dent, Schaan Liechtenstein, Austria) for 20 second with a standard light at 480 mw/cm\(^2\) assessed with a radiometer every 5 restorations. Then a hybrid composite resin (tetric ceram) (Ivoclar Vivadent AG, lot H29498 Schaan/Liechtenstein) was placed and light cured for 40 second (control group).

Group 2- Single bond was applied in one layer that was gently air dried and covered with flowable resin composite (Tetric flow) (Ivoclar Vivadent CE, Lot H 31291 Schaan/ Liechtenstein), which was inserted with a needle provided by the manufacturer. This two-component layer was co-cured (light cured simultaneously) for 40 sec, then tetric ceram hybrid composite was applied and light cured for 40 sec to restore the cavity.

In group 3- Bond was applied and light cured for 20 sec, flowable composite was placed with its special needles in the cavity and cured for 40 sec. Finally, a hybrid composite was placed and cured for 40 sec, to complete the restoration.

The specimens maintained in distilled water for 1 week at 37 °C
(± 1 °C) after this period, the restorations were finished and polished with soft-lex sequential disks (3m Brasil Ltda., sumar, sp, Brazil).

All of the specimens were thermocycled for 300 cycles at temperature ranging from 5 °C ± 2 °C to 55 °C ± 2 °C, each cycle lasted 45 sec with a dwell time of 15 sec, in each path, and 15 sec. intervals between paths. The root apices of the teeth were sealed with an acrylic resin and the entire tooth surfaces were painted with two coats of nail varnish except the restorations and one millimeter beyond the margins. The teeth were then immersed in buffered 2% methylene blue solution at 37 °C for 24 hours, thoroughly rinsed with running water and stored in humidor. For evaluation, each tooth was longitudinally sectioned with a slow speed diamond sectioning disks in a buccal lingual direction through the middle of the restoration, the sections were evaluated by two independent calibrated examiners on the stereomicroscope (Hamilton by Altaly international Italy) at a magnification level of x 40 to determine the extend of dye penetration on the gingival and occlusal walls of the restorations.

The following criteria were used to score the extend of the leakage at both enamel and dentin margins.

- 0 - No dye penetration
- 1- Dye penetration up to half of the cavity depth.
- 2- Dye penetration more than half of the cavity depth.
- 3- Dye penetration arriving to the cavity floor. (Fig 1)

Data were subjected to the Fisher Freeman Halton statistical test at a confidence level of 95% (p<0.05).

**RESULTS**

The frequency of microleakage score at enamel and dentin surfaces of the tested groups are reported in Tables (1) and (2).
Table (1) The frequency of microleakage scores at enamel margins.

| Groups | Site of leakage | Total |
|--------|-----------------|-------|
|        | 0               |       |
|        | 1               |       |
|        | 2               |       |
|        | 3               |       |
| G1     | 4               | 20.0  |
|        | 10              | 50.0  |
|        | 6               | 30.0  |
|        | 0               | 0.0   |
|        | 0               | 0.0   |
|        | 20              | 100   |
| G2     | 8               | 40.0  |
|        | 10              | 50.0  |
|        | 2               | 10.0  |
|        | 0               | 0.0   |
|        | 0               | 0.0   |
|        | 20              | 100   |
| G3     | 14              | 70.0  |
|        | 6               | 30.0  |
|        | 0               | 0.0   |
|        | 0               | 0.0   |
|        | 20              | 100   |

Groups 2 and 3 has significant difference from group 1 at \( p < 0.05 \) and \( p < 0.001 \) respectively and group 3 has significant difference from group 2 at \( p < 0.05 \).

Table (2) The frequency of microleakage scores at enamel margins.

| Groups | Site of leakage | Total |
|--------|-----------------|-------|
|        | 0               |       |
|        | 1               |       |
|        | 2               |       |
|        | 3               |       |
| G1     | 0               | 0.0   |
|        | 0               | 0.0   |
|        | 12              | 60.0  |
|        | 8               | 40.0  |
|        | 20              | 100   |
| G2     | 0               | 0.0   |
|        | 4               | 20.0  |
|        | 10              | 50.0  |
|        | 6               | 30.0  |
|        | 20              | 100   |
| G3     | 0               | 0.0   |
|        | 8               | 40.0  |
|        | 8               | 40.0  |
|        | 4               | 20.0  |
|        | 20              | 100   |

Groups 2 and 3 has significant difference from group 1 at \( p < 0.05 \) and \( p < 0.001 \) respectively and group 3 has significant difference from group 2 at \( p < 0.05 \).

Non parametric Fisher Freeman Halton test revealed a significant differences in microleakage score between the tested groups for both enamel and dentin margins.

In most of the sections, the cervical margins presented higher leakage score than occlusal margins (Fig. 1).

Fig. (2) Sectional tooth see the degree of dye penetration.

E = Enamel, D= Dentin, C = Composite and P = Pulp

Differences in microleakage patterns and scores were observed between Group 1 (control group) and Group 3 at \( p < 0.001 \) and Group 2 with Group 3 at \( p < 0.05 \) for both enamel and dentin margins.

That is mean in the present study the marginal adaptation of the resin composite restorative system was improved by the use of flowable resin composite as liner.
Group 3 (adhesive and flowable composite cured separately) yield the best results, and provided better marginal seals.

**DISCUSSION**

Composite resin still presented with relevant draw backs such as inherent polymerization shrinkage, which result contraction gaps at the tooth/restoration interface that lead to microleakage (13). When composite resin are the material of choice for cervical defects or class V cavi ties this represents a challenge and technically demanding situation because the gingival margins usually located in the dentin or cementum, which is considered a critical factor governing the marginal adaptation (14).

In the present study, higher leakage was detected in dentin when compared to enamel. These differences might be related to the compositions of these tissues, while the enamel is almost completely mineralized, dentin present with a lower mineral content, with an organic matrix having a moist surface which impairs the bonding mechanism (15,16).

Therefore the bond strength to enamel is typically stronger and more stable than that obtained with dentin, and leakage along the enamel/restoration interface is less than that of dentin (17,18).

The restorative technique with resin elastic liners and rigid restorative composites might be suitable alternative to reduce stress at the dentin/composite interface, flowable resin composite can used as an intermediate layer and this methods proposed to increase the longevity of composite restorations, especially those with margins in dentin (19).

The main rationale behind the use of flowable resin composite is the formation of an elastic layer that may compensate for polymerization shrinkage stress. Montes et al (20) suggested that the use of an intermediate low elastic modulus layer would function as an shock absorber or a "stress-breaker"

The results of the present study showed that the use of flowable resin composite (with adhesive cured separately under hybrid composite Group 3) exhibited less microscopical leakage than control group. This finding are in agreement with the finding of other studies (6, 8, 9, 21 and 22).

The low viscosity of tetric flow with its handling characteristic, allow the material to readily adapt to the prepared tooth structure creating an intimate union with the microstructural defects of the of the prepared cavities.

Li Q et al (8) studied the influences of flowable materials as an intermediate layer in class V cavities, his results showed that composite fillings could be improved by the use of flowable composite materials.

Group 2, (the adhesive system co-cured with the flowable composite simultaneously) has been advocated as a mean to improve the marginal sealing of adhesive restorations (11).

As the oxygen inhibition layer could prevent the adequate polymerization of the adhesive, a flowable composite may ensure this oxygen inhibition layer is blocked out prior to polymerization of the dentin bonding agent (3).

In this study the use of a flowable composite light cured simultaneously with the adhesive did not improved the marginal sealing like the teeth in group 3 (when the flowable resin and adhesive cured separately). This result in agreement with Sensi et al. (3) who concluded that adhesive system should not be co-cured with flowable composite.

This might be related to the displacement of the bonding agent leaving unprotected zone that may cause adhesive failure and subsequent increase in the microleakage score.

Despite the methodological and criterial differences, the results achieved with this study is in accordance with similar studies (3,9).

From clinical point of view, the tooth/composite restoration interface in class V cavities could improved by the use of flowable resin materials with rigid composite resin such as hybrid resin.

Although, in this study an effort was made to simulate the clinical situation, but, ideally, long term clinical studies should by performed to evaluate the performance of the flowable resin composite when used with hybrid composite.
Conclusion

- The dentin margins demonstrated more leakage as compared to enamel margins.
- Non of the restorative techniques or materials completely sealed the tooth/restoration interface especially in the cervical margins.
- The use of flowable resin material may be advantageous in reducing the microleakage level.
- It is not preferable to co-cured the flowable composite with the adhesive system.

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