Methods and Protocols for Reliable Electrochemical Testing in Post-Li Batteries (Na, K, Mg, and Ca)

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ABSTRACT: While less mature than the Li-ion battery, technologies based on Na, K, Mg, and Ca are attracting more and more attention from the battery community. New material (cathode, anode, or electrolyte) testing for these post-Li systems commonly involves the use of an electrochemical setup called a half-cell in which metal counter and reference electrodes are used. Here we first describe the different issues that become critical when moving away from Li with respect to the cell hardware (cell design, current collector, separator, insulator) and the nature of the counter and reference electrodes. Workarounds are given, and a versatile setup is proposed to run reliable electrochemical tests for post-Li battery materials in general, in a broad range of electrolyte compositions.

INTRODUCTION

Our modern society is battery dependent! The continuous growth of the worldwide battery market (around 70 billion US $ in 2016) is galvanized by the cost decrease (in $/kWh) of the Li-ion technology which has been divided by a factor of 10 since its first commercialization by Sony in 1991.  However, the Li-ion battery is slowly but surely reaching its limits (both in terms of energy density and cost reduction), and controversial debates on lithium supply cannot be ignored. Several other battery chemistries are being developed aiming at surpassing the Li-ion technology which has been divided by a factor of 10 in 2016) is galvanized by the cost decrease (in $/kWh) of the Li-ion technology which has been divided by a factor of 10 since its first commercialization by Sony in 1991. However, the Li-ion battery is slowly but surely reaching its limits (both in terms of energy density and cost reduction), and controversial debates on lithium supply cannot be ignored. The following properties should hold: (i) nonpolarizable, i.e., if current is flowing through the RE (depending on potentialstat electronics and cell’s leakage resistance) it should not affect its potential, and (ii) reliable and stable potential with time (ideally, reproducible to about one millivolt). Although these conditions are, at least satisfactorily, met in Li half-cells, recent studies point to several issues associated with the use of Na, Mg, and Ca metal CEs and REs. Considering the difficulty of the development of new battery chemistries in which both electrodes and electrolytes must be studied in parallel, the use of reliable electrochemical protocols is crucial in order not to discard potentially interesting material candidates. This paper presents an introduction to some of the most important parameters to be considered for the successful and unbiased electrochemical testing of new materials in Na, Mg, and Ca based batteries for researchers new to the field. The case of K is briefly discussed as well. Only systems involving liquid electrolyte are considered, and the cell geometry, nature of the current collectors, separators, and counter and reference electrodes are discussed. Examples of their impact on the electrochemical response in typical electrochemical characterization procedures (cyclic voltammetry (CV), galvanostatic cycling (GC), galvanostatic or...
potentiostatic intermittent titration techniques (GITT or PITT), and impedance spectroscopy (EIS)) are presented. Electrode formulation (procedure to prepare composite electrode containing the active material to be tested) or the specific requirements for in situ/in operando characterization techniques are not covered and the reader is referred to refs 10 and 11 for detailed procedures. Finally, considering all the requirements for achieving reliable electrochemical tests in non Li cells, a versatile, reliable, and easily implemented electrochemical setup is proposed and benchmarked against a challenging system: Ca cathode testing in an electrolyte in which Ca plating and stripping do not occur.

### DIFFERENT TYPES OF CELLS

Three common laboratory scale setups are used to test the electrochemical properties of materials (electrode and electrolyte) for different battery chemistries (Li, Na, K, Mg, and Ca): beaker, Swagelok, and coin cells. Pouch cells may eventually be employed in a second step, usually in the form of full cells, when promising results have been obtained in one of the configurations mentioned above.

The beaker cell uses standard labware and is easy to assemble; it is also compatible with large REs such as junction reference electrodes and luggin capillary allowing for minimizing ohmic drop (see discussion in the reference electrode section). The main counterparts are the high amount of electrolyte required, the absence of stack pressure, and the need to keep the cell in a glovebox for the whole duration of the experiment, and cell connections inside the glovebox are also required. Possible evaporation of solvents from the electrolyte can affect the atmosphere in the glovebox and consequently they commonly have to be kept in a glovebox. The tight sealing of coin cells might be seen as an advantage since it increases the electrolyte concentration during the test. These disadvantages might be avoided by placing the cell in an airtight box equipped with electrical connections such as in ref 12; we are, however, not aware of the use of this approach to test materials for battery applications given the advantages of the Swagelok-type cell in terms of dimensions and airtightness. The important volume of electrolyte in a beaker cell might be seen as an advantage since it increases the dilution of side-reaction products at the electrodes, which can artificially increase the cyclability of poorly stable systems. However, such side reactions will eventually have to be dealt with when moving to a more realistic setup application-wise.

Swagelok cells use gas tubing fittings as the cell body and simple “plungers” as the current collectors,13 resulting in an easily constructed setup that is widely used. The electrodes are separated by a porous separator impregnated by the electrolyte, and a compression spring maintains the pressure manually applied during cell assembly. Two-electrode cells can be built with straight fittings and three electrode cells either by welding a tube at their side13 or using a tee junction and a specifically machined plunger for the third electrode (Figure 1a). As both the plungers and the cell body are metallic, the use of an insulator is mandatory in order to prevent short circuit between the electrodes. This insulator can cover the plungers, e.g., polytetrafluoroethylene (PTFE) tape, which can be used until at least 100 °C. Alternatively, the insulator can take the form of a tube inside the cell body. The reference electrode is attached to a specifically machined plunger, shown in Figure 1b, presenting a dedicated groove in order to tightly tie a wire reference electrode. Other plunger designs may use a screw to hold the wire. In such cells, a few hundreds of microliters of electrolyte are sufficient to soak electrodes and separators.

Following a somewhat similar approach the two and three-electrode “Conflat” cells were recently introduced using standard ultrahigh vacuum fittings14 instead of gas tubing fittings (as in Swagelok cells). Operating temperatures as high as 200 °C are reported for these cells with an insulator and gasket made of PTFE.

Coin cells represent another widely employed cell configuration to test active materials for battery applications. The assembly of a full Li-ion coin cell with a thin separator and electrodes of equal diameter, aiming at improved cell performance and cycle life, is a very delicate task.15 Fortunately, it is simplified in the framework of testing active materials only, in which a thick separator and larger counter electrode than working electrode can be employed, though a minimal care should be taken in the alignment to ensure that all of the WE is faced by the CE. An unassembled coin cell is shown in Figure 1c). The inner parts are simply a current collector and a spring to maintain pressure on the electrodes stack. A polypropylene gasket ensures both functions of electrical insulation and air tightness; the sealing is performed by a specific crimping machine, which implies the need for a dedicated space in a glovebox. The tight sealing of coin cells makes them a setup of choice for long-term cycling at lab scale.

Examples of coin cells in three-electrode configuration can be found in refs 16−20. In the simplest cases, the supplementary RE consists of a thin wire passed between the gasket and the casing.17,19,20 The assembly of such cells is very tricky19 as breaking of the reference wire or shortage will easily happen. The presence of the wire can affect the air-tightness of the cell, and consequently they commonly have to be kept in a glovebox17 or sealed with epoxy after crimping,19 which can hardly be expected to be as reliable as a standard coin cell in the long term. An alternative consists of modifying the cell’s hardware to integrate the RE,18 in which a more reliable sealing would be expected at the cost of an important work in the cell design and manufacturing.

After characterization of the materials, it is of high interest to investigate the performance of the most promising ones as constituents of an actual battery, i.e., in a “full cell”
configuration. Coin cells are commonly used for this purpose, in which the lack of an RE is usually a secondary issue. Pouch cells are much closer to commercial cells and are therefore preferred for systematic studies at the cell level. They have the counterpart of being more demanding in terms of amount of active material and equipment to prepare homogeneous electrodes at larger scale and seal the cells. In the case of post-Li-ion technologies, the use of pouch cells for sodium-ion or magnesium—sulfur systems has been reported.

Several new cell designs have been reported mostly aiming at improving the quality of impedance spectroscopy measurements (see impedance section) or in order to facilitate in situ/in operando characterization tests. Each technique brings constraints to the design of an operando cell in terms of geometry, materials properties (such as transparency to certain wavelengths), or the positioning of actuators. Examples of cells developed for in operando techniques include X-ray diffraction or absorption, infrared spectroscopy, UV-visible spectroscopy, mass spectrometry, or NMR. The democratization of 3D printers broadens the possibilities to build custom cells, mostly using polylefins.

Cells dedicated to the electrochemical testing of materials for battery applications are also commercialized by a few companies and were used in some studies. Two- or three-electrode configurations are commonly available. Some of these cells were designed mostly for Li systems and their constituting materials might not be compatible with electrolytes based on alternative cations, but products made of the most resistant materials and ready to work with metallic or carbon quasi-reference electrodes are also offered.

## CURRENT COLLECTORS

Reactions at the current collectors may limit the operating window of the cell. In current-controlled techniques, such reactions can lead to endless and noisy voltage plateaus.

At the cathode side, corrosion of the cell’s hardware may occur, which may depend on the nature of the electrolyte salt. This can be exemplified by the corrosion of aluminum initiated in TFSI-based electrolytes, which can be prevented by adding LiPF$_6$ in the electrolyte to form an AlF$_x$-rich passivation layer. However, it is not always desirable to alter the composition of the electrolyte, and not all PF$_6^-$ or BF$_4^-$ based salts are easily available and/or dried. For instance, Mg(BF$_4$)$_2$, Mg(PF$_6$)$_2$, and Ca(PF$_6$)$_2$ are not commercially available, Ca(BF$_4$)$_2$ is not stable, and only hydrated Ca(BF$_4$)$_2$ can be purchased and needs extensive drying procedures. Overall, only TFSI-based Mg and Ca salts are available dry and are commonly used. In such cases, the current collector material used can significantly affect the voltage window, as shown in Figure 2, which informs on the anodic stability limit with Al, AISI 316 stainless steel, or Ni$_{80}$Cr$_{20}$ alloy used as the working electrode in 0.3 M Ca(TFSI)$_2$ ethylene carbonate (EC):propylene carbonate (PC) electrolyte. Among the three materials tested in Figure 2, AISI 316 offers the highest anodic stability. While stainless steel might bring a weight penalty in practical application because of its density nearly as high as that of copper, this is not a problem at the stage of materials testing.

Commercial coin cell casings are often made of AISI 304 stainless steel, which has significantly lower resistance to corrosion than 316. With such casings, an Al deposit or a disk of Al foil (or 316 stainless steel) at the working electrode side can be used to increase the maximum cell voltage. It needs to fully cover the inner surface of the can to ensure that the gasket takes place on the foil or Al deposit and no part of the WE casing is accessible to the electrolyte. While most of corrosion issues are due to the electrolyte, active material can also be problematic. For instance, elemental sulfur and polysulfides can lead to significant corrosion of common current collector such as stainless steel and copper. Such corrosion potentially has an impact on the overall electrochemical response through cycling of copper sulfide species.

At the anode side, the voltage window may be limited by the alloying of the current collector with the cation in solution. The typical example is the electrochemical formation of an alloy of Li and Al at ~0.3 V vs Li$^+$/Li, which is the reason for the use of copper current collectors in commercial Li-ion cells. A similar issue can occur in Na cells when low purity Al pluggers are used, which can contain traces of Pb that can alloy with Na. Calcium and magnesium can form thermodynamically stable alloys with aluminum or copper as well, however, several groups use these metals as current collectors at low voltages without reporting issues of electrochemical alloying, suggesting that their alloying with divalent cations might be kinetically limited. Since electrochemical quartz crystal microbalance and rotating disc electrodes commonly use Au and Pt as working electrodes, it is worth mentioning that Na, K, Mg, and Ca can all alloy with Au and at least Na and Ca can alloy with Pt, whereas we could not find data for the Mg—Pt and K—Pt systems. A systematic investigation on the possibility to form Ca or Mg based alloys with conventional metal substrates used in battery testing (Cu, Al, Pt, Au, or SS) is still lacking.

## INSULATOR

As mentioned above, an insulator material is required in order to prevent direct contact between the current collectors of the different electrodes, i.e., cell short circuit. It is only required for compact cell designs such as Swagelok or coin cells but not for the beaker type, as the electrolyte acts as the electronically insulating material between the electrodes. Li cells commonly use boPET (Mylar) foil as insulator, which displays good chemical compatibility with organic electrolytes commonly used in batteries. However, certain electrolyte decomposition products have been proposed to attack Mylar. This is the case
of sodium cells with glyme-based electrolytes producing both highly reactive radicals and strongly basic alkoxides. As Mylar is not resistant to highly alkaline media, polyether ether ketone (PEEK) is preferred in such applications.

As it is easily machined, PEEK is used to fabricate complete cells bodies apart from only insulating the electrodes. It is inert toward metallic lithium as well as toward Li-ion electrolytes and can operate at temperatures up to ~300 °C. PTFE is also widely employed, especially since it is available in the form of tapes that can be used to cover the plenums. However, it is not suitable for low potentials as it gets defluorinated in contact with alkali metals, forming carbon. After a long exposure, the carbon formed may even produce short circuits. In contact with sodium metal, the reaction is highly dependent on the solvent used: no evidence of PTFE decomposition is observed in carbonates, whereas it is important with diglyme. PTFE decomposition has also been proposed to be at the origin of capacity loss with graphite anodes when used as binder. This reaction seems to be less problematic in the case of Ca and Mg cells as no evidence of such decomposition has been reported so far.

Polyamide (Nylon) had been extensively used as sealing material for Ni–Cd and Ni–MH batteries (both cylindrical and coin cells) until shown to be incompatible with the alkaline media. Nylon can be machined to form specific cell designs. No big issues are reported regarding its stability against lithium anodes, but the temperature range is limited: the melting point is 220 °C but mechanical strength starts to get lost at temperatures as low as 50 °C. For this reason, Nylon ferrules and gaskets should be reserved to tests at room temperature or slightly above. Other more exotic polymers can be used as insulators for specific setup requirements. For instance, polyimide (Kapton) can be used for high temperature applications, being stable up to 400 °C. It can be found in several formats: Kapton HN is a plastic film of different thicknesses, and Kapton FN is an adhesive tape, in which the Kapton film is covered by a fluorocarbon resin to provide adhesion characteristics. Note, however, that the fluorocarbon resin is similar to PTFE and PVDF and its instability in lithium batteries at low potential has been reported.

Polyolefins (polypropylene, high-density polyethylene, etc.) form a very versatile family of polymers with higher stability at low potentials than the PTFE. However, they might be less resistant to dissolution and solvent uptake and could present low thermal stability depending on the polymer.

Overall, in our research on Na, Mg, and Ca we found the use of PTFE very convenient in terms of shape (available in the form of tapes) and temperature stability, some tests requiring temperatures up to 100 °C (for Ca plating for instance). However, alternatives such as PEEK must be used in glyme based electrolytes.

SEPARATOR

While insulating material is necessary in order to prevent short circuit by direct contact between the different current collectors and the metallic core of the cell (if Swagelok cells are being used), an electronic insulation is also needed between the WE and the CE. This is the role of the separator, usually consisting of a porous and electronically insulating structure which can be wet by the electrolyte, thus ensuring ionic transport through it. A large number of separators have been developed and are commercially available depending on the battery technology under test. However, at laboratory research scale there are mainly two types used: polyolefin membranes (e.g., commercial Celgard separators) and glass fiber.

Polyolefins, being thin (<30 μm) and highly chemically resistant, are extensively used in both laboratory and commercial cells. The preferred composition of a polyolefin separator is a three-layered membrane composed of polypropylene/polyethylene/polypropylene (PP/PE/PP). The outer PP layers provide high resistance to oxidation and reduction at the electrodes while the inner PE layer works as a thermal fuse. When the temperature of the cell goes above 130 °C the PE melts closing the pores of the separator and avoiding further heating and eventual thermal runaway. Polyolefins are very resistant to highly caustic or acidic media and have good compatibility with many organic solvents, but wettability issues are common with viscous electrolyte such as PC-based ones.

In laboratory cells, where the thickness is not as crucial, glass fiber is more extensively used. Based on borosilicate glass, it presents excellent chemical and thermal stability. An important exception is the susceptibility of borosilicate glass toward the attack by HF. In lithium-ion cells, HF is a known hydrolysis product of fluorinated anions, such as PF6− and BF4−. Therefore, special attention must be devoted when traces of water are present in the electrolyte which might generate HF which attacks the separator forming more water and soluble boron compounds.

We have found that the commercial glass fiber separators can also release corrosive products in the electrolyte solution. This is illustrated by Figure 3 which reports cyclic voltammograms of 316 stainless steel WE and 0.1 M Ca(TFSI)2 in PC electrolyte after different pretreatments of the WE or separators. In Figure 3a), without specific treatment of either WE or separators, an oxidation peak is observed around 3.1 V vs Ca2+/Ca, that grows for the different pretreatments of the WE or separators, an oxidation peak is observed around 3.1 V vs Ca2+/Ca, that grows for the maximum of more than 200°C and then vanishes. It is associated with important reduction current below 2.6 V and oxidation current above 3.5 V vs Ca2+/Ca, all three features following the same trend of reaching a maximum after 55 cycles and then decreasing. This response appears related to the passivation of the stainless steel electrode, as confirmed by Figure 3b for which the WE was passivated in 20% nitric acid prior to cell assembly. In this case the same features can be identified on the voltammograms, but their magnitude is decreased by an order of magnitude, which indicates that the associated process is inhibited by the pretreatment in nitric acid. However, the elimination of these parasitic electrochemical features is even more efficient by simply soaking the separator in the electrolyte at 100 °C and then rinsing with DMC (in Figure 3c). Indeed, in this case no parasitic process can be seen, even without pretreatment of the working electrode in nitric acid. Simple rinsing of the separators with DMC at room temperature also leads to the disappearance of these parasitic redox features (Figure 3d), yet the baseline of the cyclic voltammograms appears broader than in (c). These results point at the separators as the origin of the peaks observed in Figure 3a through the release of some corrosive product, the exact nature of which is not determined yet.
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20% HNO₃ after polishing, and the separators are used without further treatment; (b) the working electrode was passivated for 1 h in lower than 1 mA cm⁻², the lithium electrode is reproducible only at current densities lower than 1 mA cm⁻². The voltage of the metal/electrolyte interface, mass transport through the SEI, and electrode requires desolvation of the cation at the SEI/ materials in two-electrode cells (typically requiring few tens to hundreds of μA). For higher current densities, a third electrode will be needed as a reference versus which the potential can be reliably measured. In other battery chemistries, however, the operation of the metal electrode is not as trivial.

In the case of metallic sodium, in most electrolytes it works similarly by formation of a SEI, this SEI being more soluble in Na than in Li systems. Using conventional alkylcarbonate based electrolyte, continuous electrolyte decomposition will prevent from running any long-term cycling and leads to the production of electroactive species in solution. Though significantly decreased, continuous electrolyte decomposition is still observed with FEC additive. Upon plating, Na metal has a higher tendency than Li to grow dendrites, which may result in cell failure due to internal shorting. Upon stripping, voltage steps experienced by the Na CE can also misleadingly be attributed to the working electrode in two-electrode configuration. Altogether, given the extra polarization of the sodium electrode, its higher impedance, leading to unreliable potential, a three-electrode configuration is needed in most Na cells to avoid biased conclusions. As an example, low voltage anodes such as hard carbons can reach the lower cutoff voltage upon reduction before the full capacity can be accessed due to the polarization associated with the CE in a two-electrode configuration.

Given that the SEI stability is more problematic with Na than with Li and that the solubility of alkali salts in water increases when moving from Li to Na to K, significant issues associated with the use of K metal CE could also be expected. K cells are generally assembled in two-electrode configuration vs K metal, similarly to most Li half cells. However, in this configuration, part of the capacity lost after 120 cycles can be recovered by changing electrolyte and K electrode, which shows that it does not work as an ideal CE. Soluble products of the electrolyte decomposition on K metal can also diffuse toward the WE, potentially affecting the representativeness of the performance of the material tested. FEC is occasionally used in K cells, though it is not clearly stated whether the purpose is to limit electrolyte decomposition at the CE or build a better SEI on the WE. However, when comparing Li, Na, and K metal anodes in contact with perchlorate salts in PC solutions, a substantial amount of soluble decomposition products was only detected in Na cells suggesting a better stability of Li and K interfaces. Overall, solubility issues of passivation layers in K cells are not fully understood and a systematic investigation is needed.

Moving to the RE, it should ideally be “reversible, reproducible, constant in time and easy to prepare. Generally, the reference electrode is reversible to one of the ions in the solution to avoid liquid junctions.” Unlike aqueous systems where references are commonly reversible to an anion, in a lithium cell, voltage is determined by the activity of Li⁺ at the vicinity of the reference, which can safely be considered as constant. Electrodes reversible to the cation can be divided in three categories: the metal itself, metallic alloys, and insertion materials. Though these different types of REs work very well with Li, their applicability to other cation-based systems is not straightforward.

As discussed previously, unstable Na metal/electrolyte interfaces and partial dissolution of the SEI can affect the measure in alkylcarbonate electrolytes. Also, in the case of K cells, the addition of FEC tends to improve the stability of the metal/electrolyte interface in alkylcarbonate electrolytes.

In ether solvents (such as glymes) a stable operation of a K

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**Figure 3.** Cyclic voltammograms recorded at 20 mV s⁻¹ on a 316 stainless steel plunger as working electrode in 0.1 M Ca(TFSI)₂ in PC at room temperature with an activated carbon counter electrode. (a) Glass fiber separator and polished working electrode are used without further treatment; (b) the working electrode was passivated for 1 h in 20% HNO₃ after polishing, and the separators are used without treatment; (c) the separators were soaked for 5 days in the electrolyte at 100 °C and then rinsed with DMC before use, and the working electrode is as polished; and (d) the separators were rinsed with DMC only, and the working electrode is as polished.

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**COUNTER AND REFERENCE ELECTRODES FOR MONOVALENT SYSTEMS (Na AND K)**

Beginning with the CE, its basic requirements are to reversibly store charge (not involving electrolyte contamination) and to have sufficient capacity to sustain the current density arising from the redox processes occurring at the WE. For a given cathode the counter electrode having the highest theoretical gravimetric capacity is the corresponding metal, but its use is not always appropriate.

With lithium metal electrode an electronically insulating and ion-conducting surface layer forms in contact with the electrolyte: the solid electrolyte interphase (SEI). This interphase will undergo breakdown and repair cycles during charge and discharge of the cell. The working of this metal electrode requires desolvation of the cation at the SEI/electrolyte interface, mass transport through the SEI, and charge transfer at its interface with the metal. The voltage of the lithium electrode is reproducible only at current densities lower than 1 mA cm⁻², which is enough to test most active materials in two-electrode cells (typically requiring few tens to hundreds of μA). For higher current densities, a third electrode will be needed as a reference versus which the potential can be reliably measured. In other battery chemistries, however, the operation of the metal electrode is not as trivial.

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metal electrode depends greatly on the salt used, the KPF$_6$ being the worst performing—in opposition to the case of Li.$^{86}$ Altogether, it is clear that not all electrolyte systems commonly employed for lithium cells are directly transferable to Na or K and further research into SEI formation on metal electrodes is needed in these cases. It is highly recommended to evaluate the stability of the metallic electrode when used as CE and/or RE.

Aside from metal electrodes, metallic alloys and insertion materials can be used as REs reversible to the cation in solution. For such systems to be suitable, they need to be biphase and therefore display a constant voltage for a wide range of compositions. In Li-ion cells, several alloys such as Li$_x$Sn$^{17}$, Li$_x$Au$^{77}$, or Li$_x$Bi$^{78}$ as well as insertion materials such as lithium titanate and lithium iron phosphate$^{27,67}$ have been used. These REs are usually prepared in situ, possibly using composite electrodes. Alloys present the advantage that metallic wire can be used (Sn, Au, …), the alloy being formed at its surface, thus miniaturization, easy handling, and precise placement of the reference are possible. The counterpart is that dealloying can occur with time and the potential of such RE eventually drifts.$^{79}$ Most of the insertion type electrodes, on the other hand, operate within the stability window of most electrolytes resulting in a passivation free surface and improved potential stability. While alloys and insertion type references would be highly advantageous in Na and K cells and there is a large amount of potential material candidates, there is, to the best of our knowledge, no report on their use in Na and K half cells.

Additional to the nature of the reference electrode, its placement in the cell is also vital. REs made of soft metals such as Li or Na can be implemented in Swagelok cells by replacing the wire in Figure 1a by a piece of mesh onto which the metal is pressed or using a specifically designed plunger.$^{77}$ The simplest approach consists in using a second metal disk as the RE but may be poorly reliable. Indeed, to avoid the blocking of cation conduction through the cell the RE disk has to be located outside of the WE-CE stack, which can lead to voltage discrepancies between RE and CE of the same nature. For instance, in a Na cell with metal CE and RE the difference is commonly as high as 15 mV at open circuit when the RE is a 10 mm disk located 7 mm outside of the WE-CE stack (typical for a three-electrode Swagelok cell), whereas it is less than 2 mV when the RE is a 3 mm strip at the vicinity of the WE.

### COUNTER AND REFERENCE ELECTRODES FOR DIVALENT SYSTEMS (Ca AND Mg)

Regarding divalent cations, Ca and Mg anodes work only in limited combinations of temperature, salt, and solvent. To date, the metallic Mg anode can only work in ether-based electrolyte solutions for which the electrochemical stability window above 3 V remains a challenge.$^{3,80−82}$ Care should thus be taken when high voltage cathodes are investigated, as currently available electrolytes will most likely not allow for both efficient Mg plating/stripping and sufficient anodic stability. Unlike for Li metal, formation of the passive film on Mg metal tends to block divalent cation migration, preventing plating and stripping.$^{83}$ Thus, any presence of oxygen, water, or other impurities in the electrolyte (even at the ppm level) can lead to inactive passivating films. Several methods have been employed in order to overcome this issue, including the addition of Mg–chloride salts,$^{84}$ the use of magnesium powder for which an acceptable degree of Mg free surface could be maintained,$^{85,86}$ and the use of a so-called “conditioning” process,$^{85,88}$ which consists of performing several plating and stripping cycles until the stationary electrochemical response is obtained. Therefore, the use of the Mg metal electrode is far from being obvious, and if the nature of its interface with the electrolyte is not carefully considered during battery material testing it can lead to discarding promising electrode or electrolyte materials.

Moving to calcium, the use of the metal anode is even more challenging than for Mg. Indeed, this technology is still in its infancy and plating/stripping has only been demonstrated in very limited conditions: above 75 °C in carbonate based solvents and Ca(BF$_4$)$_2$ salt$^{66,87}$ or at room temperature with Ca(BH$_4$)$_2$ salt in THF, thus with limited anodic stability.$^{88,89}$ Outside of these specific combinations of salt, solvents, and temperature, Ca metal CE cannot be used in the half cell configuration.

The most obvious and versatile alternative to a metal (Na, K, Ca, or Mg) CE is a capacitive electrode such as activated carbon (AC), which is regularly used to test active materials for batteries based on Ca or Mg.$^{86−89}$ With such materials, ions are stored electrostatically on the carbon’s wide specific surface area. This mechanism, which does not involve charge transfer, brings high reversibility and works with a large variety of ions. It takes place in the voltage stability window of most electrolytes; hence, no passivation layer is formed which could affect mass transport. The counterpart is a relatively low specific capacity which requires careful sizing of the CE as a function of expected capacity of the WE. For example, for a 1.2 mA h WE which corresponds to 4.3 mg of active material with a specific capacity of 280 mA h g$^{-1}$, at least 48 mg of a carbon having a capacity of 25 mA h g$^{-1}$ are required. Such heavy counter electrodes can be easily obtained by piling several layers of self-standing electrode, either a bond with PTFE or in the form of cloth.

Using AC as the CE, care should also be taken as the cell will evolve differently whether the cation is initially present in the WE active material or not. In the first configuration, an example of which could be Ca$_3$Co$_2$O$_6$,$^{90}$ the experiment starts by oxidizing the WE to release cations in solution. At the CE, cations will be stored at the surface of the carbon and the cell is a “rocking-chair” system, which is schematized in Figure 4a. In the second configuration, as is the case with a material such as TiS$_2$, the experiment starts by a reduction at the working electrode, which will consume cations from the electrolyte. In order to maintain electroneutrality of the solution, anions will be stored at the CE, which overall leads to gradual dilution of the electrolyte (Figure 4b). This effect is usually negligible but can become significant in extreme cases and have a significant impact on the ionic conductivity. For example, the same 1.2 mA h electrode as above in 600 μL of 0.1 M solution of divalent cation as electrolyte will require 30% of the total quantity of cations in the electrolyte for a full reduction. In such cases, precharging of the CE might be necessary. Precharging of the carbon electrode can be done by charging a two electrode carbon/carbon cell at the required capacity, and then recovering the negative and rinsing it with the electrolyte. During the precharging step, it is recommended to use a heavier (1.5−2X) positive electrode to prevent electrolyte decomposition at that electrode. With this procedure the AC electrode becomes a source of cations as for metal CE and, if the AC is carefully oversized, a rocking
chair is achieved and no electrolyte dilution takes place (Figure 4c). Precharging the CE can also be a way to increase its available capacity and prevent it from reaching the anodic stability limit of the electrolyte, especially when the temperature has to be increased. Because the potential of the carbon electrode varies with the capacity, the use of an RE is mandatory. As a benchmark for the properties of a standard AC (YP17, Kuraray) when used as CE in a divalent cation based system, the capacity and rate capability of a 14.2 mg carbon electrode (with 5 wt % PTFE binder) and cycled in 0.1 M Ca(TFSI)₂ in PC electrolyte are shown in Figure 5. For current density below 20 mA·g⁻¹, a specific capacity of about 25 mAh·g⁻¹ is obtained. As mentioned before, since most active materials are tested with current density below 1 mA·g⁻¹ (especially true for divalent cation systems with low power performances), the value of 25 mA h·g⁻¹ can safely be considered for this carbon. Finally, it is advised to carefully wet the AC electrode with the electrolyte before cell assembly when working with high viscosity solutions. Indeed, since the capacity of the electrode is directly proportional to the surface in contact with the electrolyte, the wettability issue will result in capacity decrease. The electrode can be placed in the electrolyte overnight and/or placed in the electrolyte and

Figure 4. Schemes of cells using carbonaceous counter electrodes, after assembly and during cycling. In (a) and (b), a pristine CE is used in combination with a WE that is either (a) a cation source or (b) a cation host; (c) a cation host-type WE is combined with a previously charged CE.

Figure 5. (a–c) Galvanostatic charge and discharge profiles of Ca²⁺ in YP17 activated carbon from rest potential down to 2.1 V vs Ca²⁺/Ca (−1.3 V vs the Ag/Ag₂S RE employed) at room temperature in 0.1 M Ca(TFSI)₂ in PC. The current densities are 10, 20, and 100 mA·g⁻¹ in (a), (b), and (c), respectively. (d) Reversible capacity and Coulombic efficiency as a function of the current density. The CE is an overcapacitive (2.5× the mass of WE) YP17 electrode.
under vacuum in order to remove as many trapped gas bubbles as possible before cell assembly.

With respect to reference electrodes, significant potential shifts for Ca and Mg pseudo-REs have already been reported by a few groups, with amplitudes depending on the experimental conditions. The general trend being that ether-based electrolytes lead to relatively small potential shift, if any (below few hundreds of mV), while shift as large as 1 V can be measured in alkylcarbonate solutions. This suggests a significant influence of the nature of the passivation layer formed on the metal electrode on its potential. In the absence of formation of a passivation layer, the potential of the metal RE is most likely influenced by its initial surface chemistry such as for quasi-reference electrodes (QREs, thus, at least partly, depend on the electrolyte water content).

As for Na and K, the use of an alloy or insertion type RE in Mg and Ca cells has not yet been reported. However, electrochemical alloying with Mg was demonstrated with micrometric In, Bi, or sputtered Pb, which display characteristic voltage plateaus for a wide composition range. This suggests these alloys might be suitable as references in Mg cells, provided they do not passivate in the electrolyte used.

Figure 6. Scheme of a potentiostat connected to a two or three-electrode cell are represented in Figure 6a,b, respectively. Two cables are connected to the WE, one to the CE, and one to the RE. A fifth cable might be present allowing the voltage of the CE (not represented) to be recorded. The current i is applied between WE and CE, and the voltage V is measured between WE and RE: The current i flowing through the RE remains negligible thanks to the high input impedance of the potentiostat (>10 GΩ), and thus in the three-electrode configuration the processes occurring at RE have no contribution to the voltage V (WE potential vs RE plus the ohmic drop, discussed below).

Cyclic voltammetry (voltage controlled, CV) and galvanostatic cycling (current controlled, GC) are the two base techniques employed to test active materials. Details of the cyclic voltammetry experiment and analysis can be found in ref 99. GC is usually preferred over CV for battery tests because they can display important capacities over a narrow voltage window, thus saving time on less important potential regions, and enable for a more complete reactivity of the material. The capacity and Coulombic efficiency are also determined with better precision using galvanostatic cycling. In most cases, both CV and GC techniques are more reliable when performed in a three-electrode cell configuration in which the potential of the RE will remain stable during cycling. This is true for Li cells and often mandatory for Na, K, Mg, and Ca systems for which the metal RE is not reliable, especially if also used as the CE. An additional parameter that should be considered is the uncompensated ohmic drop (or IR drop) in the electrolyte that will always arise between the WE and the RE. Three parameters dictate the extent of this IR drop: the electrolyte ionic conductivity, the distance between the WE and the RE, and the current flowing through the WE (see Table 1 for estimation of IR drop values in various conditions). While the first two parameters are fixed for a given electrochemical setup, current density varies during a CV experiment and is fixed during a GC test. Therefore, while the IR drop will only shift the whole GC curve (to lower or higher potential values upon reduction or oxidation of the WE, respectively), it can significantly affect the CV curve shape. Due to the high ionic conductivity of the Li based electrolyte, the IR drop usually tends to be negligible and so is expected for Na and K systems which commonly present even better salt dissociation and mobility in solutions than for Li. However, Ca and Mg based electrolytes suffer from poor salt dissociation and mobility, which can result in a significant IR drop depending on the cell geometry (Table 1). A high uncompensated IR drop will lead to misinterpretations of electrochemical processes. Careful RE positioning in Ca and Mg cells is thus even more crucial than for monovalent systems in order to record reliable electrochemical data.

While CV and GC consist of varying linearly the potential or the total capacity passed through the sample, the potentiostatic intermittent titration technique (PITT) and galvanostatic intermittent titration technique (GITT) consist of stepwise variations of these parameters. For PITT the voltage varies by steps of a few mV and current decrease is monitored for a given time or until it reaches a given value, and then the voltage is incremented. Similarly, GITT involves increments of capacity in the form of galvanostatic pulses, followed by relaxation periods.

PITT and GITT serve two main purposes: obtaining the potential as a function of composition in conditions close to equilibrium (the titration curve) and estimating the diffusion coefficient of the cation inside the active material. Using reliable RE, the former is straightforward: potential and total capacity are taken right before every voltage step or current pulse to plot the titration curve. The latter relies on the analysis of the transient profiles, with underlying assumptions regarding the geometry of the diffusion medium and whether multiple phases or a solid solution are involved.

Originally, the equations permitting extraction of diffusion coefficients from the GITT and PITT techniques were derived
Table 1. Uncompensated Ohmic Drops in the Electrolyte for Various Working to Counter Electrode Distances, Electrolyte Conductivities, and Current Densities

| cell length (WE to RE) | 25 μm (polyolefin separator) | 450 μm (glass fiber separator) | 5 mm (beaker cell) |
|------------------------|-------------------------------|--------------------------------|-------------------|
| conductivity, mS cm⁻¹  | 10 μA cm⁻²                   | 220 μA cm⁻²                    | 5 mA cm⁻²         |
| areal resistance, Ω cm² | 1                            | 10                             | 1                 |
| ohmic drop at          | 25 μV                        | 550 μV                         | 12.5 mV           |
| 10 μA cm⁻²             | 5 μV                         | 110 μV                         | 2.5 mV            |
| 220 μA cm⁻²            | 550 μV                       | 110 μV                         | 225 mV            |
| 5 mA cm⁻²              | 12.5 mV                      | 2.5 mV                         | 2.5 V             |

for the case of 1D diffusion through a thin film or a pellet. Diffusion through a single solid solution is considered that may have a very narrow composition range, and infinitely fast reaction at the interface with the electrolyte is considered, in such a way that the process is purely diffusion controlled. Battery electrodes usually consist of a porous composite of the active material, a conductive additive, and a binder, which is impregnated with the electrolyte. In this case, the diffusion through the active material can hardly be considered as a 1D axisymmetric and may be closer to 1D radial diffusion in the case of spherical particles with a narrow size distribution. The concentration profiles in the active material and, therefore, the current (for GITT) or voltage (for Pitt) response, will also be altered if the reaction at the interface is not infinitely fast. In the case of divergent cations that have high solvation energies, desolvation at the interface might become the rate-determining step, in which case using equations derived in the case of an infinitely fast surface reaction will not be valid. For the Pitt technique, the influence of the rate of surface reactions was analyzed in refs 105 and 106 in the case of an electrode slab and spherical particles, respectively.

Using intermittent titration techniques to estimate a diffusion coefficient may require dedicated electrode formulation and cell constituents, especially regarding the separator, which should preferably be a thin polymeric membrane rather than a thick glass fiber layer. The estimation of diffusion coefficients in two-electrode cells implies the assumption that the cell voltage only reflects processes at the WE. This requires low polarization and fast relaxation at the CE side. This would hardly be the case for Ca and Mg metal.

Electrochemical impedance spectroscopy (EIS) is another widely employed technique to investigate battery materials. It consists of applying a sinusoidal voltage or current perturbation to the cell and varying its frequency. The perturbation needs to be sufficiently small for the system to give a linear response that will be a sinusoidal wave at the same frequency with a certain phase shift. Because of this phase shift the ratio between voltage and current is a complex impedance that can be reported as a Bode or a Nyquist plot. Impedance spectroscopy can bring information regarding the different processes occurring in the electrochemical cell, such as mass transfer in the electrolyte or through an SEI, charge transfer, or diffusion, since they will contribute more or less significantly to the conduction of electrical current depending on its frequency.

The impedance technique relies on the assumption that the response of the system studied is linear, causal, stable, and finite, which implies that the data should verify Kramers and Kronig transforms. The easiest way to check the linearity and stability of the response is to repeat the measurement with a different amplitude of the perturbation and verify that the impedance spectrum is unchanged. Fitting the data with a series of Voigt elements, which complies with Kramers and Kronig relations, is a relatively easy way to identify the frequency range over which the data is consistent. Modern electrochemical software may include a Kramers–Kronig module to do this test. Other methods to perform this verification are reviewed in ref 108.

Potentiostatic EIS (PEIS) may be considered more convenient because potentiostats usually offer various current ranges and can automatically switch to the most adequate to perform the measurement, whereas galvanostatic EIS (GEIS) requires some idea of the order of magnitude of the impedance to select the appropriate current. Apart from extreme cases of cells with very high (where PEIS should be preferred) or very low impedance (GEIS preferred), both techniques should be equivalent. Below we discuss the specificities of impedance measurements in two or three-electrode cells.

In the two-electrode configuration, symmetrical cells (same electrodes and state of charge) can be used in a measure that leads to twice the mean impedance of one of the electrodes in series with the resistance of the electrolyte. This procedure can produce reliable impedance spectra but requires twice the amount of active material and cell disassembly and reassembly in symmetrical cells that makes impedance study as a function of time or state of charge a laborious task. The two-electrode configuration can be used in order to evaluate the overall impedance of full cells during aging in conditions close to application. However, for materials testing in cells that are not symmetrical, there is hardly a way to discriminate the contribution of the WE from that of the CE. This is shown in Figure 7 in which the impedance of a symmetrical hard C/hard C cell is compared with that of a hard C/Ca cell, with 0.1 M Ca(TFSI)₂ in PC as the electrolyte. For the hard C/Ca cell, a huge loop is observed that has an amplitude of ~100 kΩ cm⁻². This corresponds to the contribution of the Ca electrode since the impedance of the hard C electrode is half that of the hard C/hard C cell (<30 kΩ cm⁻²). For cells that are not symmetrical, it is therefore mandatory to use a three-electrode configuration in order to remove the contribution of the CE.

In three-electrode configuration, artifact loops can easily appear that can originate from geometrical asymmetry (such as a difference in size or misalignment between WE and CE) or electrochemical asymmetry (WE and CE of different natures). Comparing the impedance obtained in a three-electrode configuration with that of a symmetrical cell is an efficient way to check the reliability of the experimental setup. To avoid issues with electrochemical asymmetry, the impedance of the CE should be at most equivalent to that of the WE, since the impedance spectrum displaying the lowest

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magnitude of the two electrodes will be distorted. As discussed above, Ca and Mg metals usually display very high impedance (>100s of kΩ cm²), even in conditions where plating and stripping are actually possible, and thus artifact loops are likely to appear in impedance spectra when Ca or Mg CEs are used. Regarding geometrical effects, several cells were designed with higher symmetry than the standard configuration having the RE placed at the side. While these cells were developed for Li systems, their design can inspire post-Li tests. Most of them use concentric RE and CE, with the CE punched at its center and the reference placed in the middle. Accordingly, such configuration limits the impact of both geometrical and electrochemical asymmetries. A ring shaped electrode can serve the same purpose, as seen in Figure 8. It reports the impedance at OCV of a PTFE-bond YP17 (activated carbon) electrode in a three-electrode configuration with Ag/AgS QRE either in the form of a wire located at the edge of the WE–CE stack or a ring placed between the two electrodes. With the tip-shaped electrode, an artifact loop is observed in the Nyquist diagram, which is partly located in the first quadrant of the complex plane. On the opposite, with the ring-shaped electrode the spectrum remains in the second quadrant. It consists of a semicircular loop (attributable to charge transfer at the current collector/composite active material interface) followed by a 45° slope (diffusion of ions in the porosity of the carbon) and then a quasi-vertical line (capacitive behavior), which is the expected shape for the impedance of an activated carbon electrode in an organic electrolyte without optimization of the interface between the current collector and active material.

While impedance techniques are very sensitive to cell asymmetry, they are less demanding in terms of potential stability for the WE. Since these measurements are usually shorter (typically a few minutes to 1 h) than other techniques such as galvanostatic cycling, the only requirement is that the voltage drift remains negligible with respect to the amplitude of the perturbation for the duration of the longest period (i.e., at the lowest frequency investigated). However, a high impedance of the RE (Z_RE) can be detrimental if the ohmic drop Z_RE × i (see Figure 6b) becomes significant with respect to the amplitude of the perturbation.

Overall, for impedance measurements, Ca and Mg metal electrodes should not be used as the CE and/or RE in both two- and three-electrode configurations due to their usually high impedance which could lead to significant error or artifact loops and alternative CE and RE or symmetric configuration should be preferred. Na and K metal impedance is also rather high (at least in alkyl carbonate electrolytes), and its impact on impedance measurements when used as the CE and/or RE should be carefully considered.

**VERSATILE ELECTROCHEMICAL SETUP FOR POST-LI SYSTEMS**

Alternative RE and CE electrodes should be used in post-Li cells, especially for Mg and Ca systems. With respect to the RE, an easily implemented alternative to a metal electrode is a QRE, which consists of a piece of another metal such as Ag or Pt. QREs are commonly used in ionic liquids, where no reversible electrode with respect to either ion in the electrolyte is available. The Ag or Pt wire is directly immersed in the test solution or in a dedicated compartment separated by a glass frit. The latter configuration limits the influence of the reactions occurring at the WE and CE on the potential of the RE but requires the test to be run in a glovebox unless a specific cell is developed. Activated carbon (AC) QREs were also suggested as viable potential references since the high surface area of this material makes it less sensitive to impurities that could be generated during the operation of the cell.

The main drawback of QREs is that their potential is governed by reactions that are not well-defined. As mentioned in ref 119, “the commonly used quasi-reference electrode (based on either silver or platinum wire) functions through the presence of various compounds (most likely oxides) on the metal surface. The exact identity of the ‘redox couple’ is never known with
any certainty.” Consequently, the potential of a QRE cannot be evaluated theoretically and needs to be calibrated versus a known redox couple, which is commonly done by adding an electroactive specie in the solution after the measurement. This procedure relies on the assumption that the potential of the RE was steady for the whole duration of the experiment. For the test of active materials that usually last for tens of hours to several days, this can become a strong assumption. Ferrocene (Fc) and cobaltocene (Cc) are the most common electroactive species employed to calibrate the voltage of QREs. The standard potentials of Fc+/Fc and Cc+/Cc are 0.4 and −0.92 V with respect to the normal hydrogen electrode, respectively, and are assumed to be independent of the nature of the solvent. This assumption is due to the structure of the ions that are “univalent, large, symmetrical […]”, with the charge deeply buried”, in such a way that their activity is the same as that of a neutral molecule with the same shape and independent of the solvent.

Since the potential of the QRE such as silver wire is controlled by its surface chemistry, one way of stabilizing/fixed its potential is by controlling its surface chemistry by coating it with a metallic salt, leading to a Ag/AgX reference (X ideally being the anion used in the electrolyte tested, so that the reference is reversible to the anion in solution). However, solubility of silver salts can be significant in organic electrolytes and contaminate the electrolyte. Several PC-based electrolytes were prepared containing different silver salts, and then silver plating was investigated by linear sweep voltammetry (Figure 9). The solubility of AgBF₄ appears relatively important since at 0.6 M the solution is not saturated. In this solution a peak current as high as 25 mA cm⁻² is recorded. AgPF₆ is much less soluble, as only a few mg mL⁻¹ were dissolved in 0.1 M Ca(TFSI)$_2$ in PC electrolyte. However, the linear sweep in AgPF₆ saturated electrolyte displays a Ag plating peak at −33 mV vs Ag⁺/Ag with current of about 7% of the one observed in the case of 0.6 M AgBF₄ in PC, indicating significant silver contamination in the solution. By contrast, no Ag plating can be observed with electrolytes saturated in Ag₂S or AgCl; hence, these electrodes appear more suitable as reference systems.

Ag₂S is about 20 times less soluble than AgCl in 154 mM aqueous NaCl solution. Regarding organic solutions, we immersed 12 cm bare Ag wire or coated with Ag₂S (∼50 mg Ag in either case) in 1.5 mL of LP30 electrolyte for 10 days at room temperature. No Ag (<0.2 ppm) could be detected by ICP-MS after immersion of either Ag or Ag₂S in the electrolyte. Ag/Ag₂S can be easily prepared by dipping a Ag wire in ammonium sulfide. Though the oxidized form of the redox couple is identified, the voltage of the Ag/Ag₂S reference is not well-defined unless the concentration in S at the vicinity of the electrode is controlled.

In Figure 10 the potential stability of Ag and Ag/Ag₂S electrodes in EC:DMC with either 1 M LiPF₆ or 1 M LiTFSI as the electrolyte is reported. Their potential is obtained from the redox potential of Fc⁺/Fc, which was measured by cyclic voltammetry (20 mV s⁻¹) on the stainless steel plunger as a working electrode and YP17 activated carbon counter electrode. Two curves corresponding to two identical cells are plotted in each case.
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and discharge voltage profiles for TiS₂ cycled in 0.1 M Ca(TFSI)₂ in PC, with either a Ca metal or an AC CE. The cells are cycled at C/100 (C ≡ 1 Ca inserted in TiS₂) between −2 and 0.6 V vs Ag/Ag₃S with Δx in Ca₄Ti₅S₁₀ limited to 1.2. The potentials are reported versus the Ag/Ag₃S QRE, which has a potential of −40 ± 25 mV versus Fe⁺/Fe at 100 °C. First, a conventional half cell setup is used with a Ca metal disk as the CE, and upon first discharge its potential stabilizes around −1.65 V vs Ag/Ag₃S (Figure 11a). This value appears very high given that the voltage of the QRE is 3.42 V vs Ca²⁺/Ca at room temperature, suggesting that Ca stripping at the CE is very unfavored. As the current is reversed after 120 h, the CE potential drops below −4 V vs Ag/Ag₃S and keeps decreasing dramatically after a local minimum at −4.7 V. After 32 h of charge the voltage is higher than 11 V between the RE and the CE and the experiment is stopped for reaching a safety limit of the potentiostat. On the other hand, in Figure 11b an AC CE is used, which was previously calculated in a two-electrode carbon/carbon cell at room temperature. During the discharge of TiS₂, Ca²⁺ ions are released from the CE, the potential of which monotonously increases from −0.60 to 0.04 V vs Ag/Ag₃S. For subsequent TiS₂ charge and discharge, reversible charge storage at CE ensures that its potential remains in a safe window of [−0.35:0.05] V vs Ag/Ag₃S, thus permitting two complete cycles to be performed in more than 450 h.

Clearly, a large amount of side reactions occurs during cycling of the TiS₂ electrode at 100 °C since at every charge or discharge a capacity corresponding to the reaction of 1.2 Ca per formula unit is passed through the cell, which is 20% higher than the capacity corresponding to the Ti⁴⁺/Ti⁶⁺ redox process. Several voltage maxima at charge also look suspicious, though some of them might be associated with energy barriers for phase transitions. Nevertheless, Figure 11 shows that the use of a QRE such as Ag/Ag₃S in combination with a carbonaceous CE that relies on simple electrostatic charge storage allows the reactions occurring during cycling of an active material to be studied in electrolytes for which the plating of divalent cations is impossible. Such a setup significantly broadens the possibilities in comparison to the use of metallic CEs that hardly allow for more than the reduction of a material, which therefore must be a cation host rather than a cation source, and with possible release in the electrolyte of products of side reactions at the CE.

SUMMARY

To study materials for post-Li-ion batteries, the experimental setup used in Li cells cannot be simply transposed to other systems, especially regarding the use of a piece of metal as the RE or CE. Na and Ca or Mg illustrate two opposed cases: on Na a less stable SEI is formed than on Li, which brings problems related with extensive electrolyte decomposition and contamination with the soluble decomposition products; on Ca and Mg the surface layer is in most cases rather a passivation layer than an actual SEI, so that their rest potential does not correspond to the equilibrium potential that a pure metallic surface would theoretically have in the electrolyte and plating or stripping reactions are impeded. In either case, replacing metal electrodes by other types of REs and CEs improves the reliability of electrochemical tests. For a most reliable setup, such alternative RE and CE should operate within the voltage stability window of the electrolyte.

An example of the use of an AC as a CE in combination with a QRE (Ag/Ag₃S) as an alternative electrochemical setup for battery material (anode and cathode active material and electrolyte) testing is presented. The reliability of such a setup is demonstrated with the case of TiS₂ cycling in a Ca electrolyte, which does not allow for plating and stripping. However, such improved reliability in comparison to setups using the metal electrode as the RE and CE can only be achieved through careful consideration of the voltage stability and chemical compatibility of the electrolyte with the QRE and sizing of the AC electrode, the latter having relatively low capacity (<30 mAh g⁻¹). Depending on the configuration, precharging of the AC CE prior to material testing might be needed. Finally, three-electrode cell configuration should be
used in most cases and, similar to the Li system, cell geometry and positioning of the RE with respect to the WE and CE are crucial, especially for impedance measurements.

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Notes

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