1 Introduction

The study of tribology, including friction, wear, and lubrication, has recently attracted significant attention because numerous mechanical system failures originate from wear and most non-renewable energy resource exhaustion results from friction. The most effective approach to controlling or reducing friction and wear is to use a lubricant. The preparation of lubricating materials with the simultaneous functions of friction reduction, anti-wear, and repair by combining micro/nanomaterials and lubrication is currently a hot research topic in lubrication science.

Graphene (GP), a 2D structure of single-atom-thick carbon, has attracted significant attention because of its unique properties (including its superior strength, good thermal conductivity, good mechanical properties, and remarkable electron-transporting properties) in addition to its lubricating potential. The tribological properties of different types of GP nanosheets as effective solid lubricants were studied by Peng et al. Klemenz et al. performed nanoindentation and scratching of GP-covered Pt (111) surfaces in computer simulations and experiments and revealed the mechanisms of friction reduction and wear protection by GP on the atomic scale. Eswaraiah et al. observed that the addition of ultrathin GP significantly improved the lubricating performance of engine oil. The frictional characteristics, anti-wear abilities, and extreme pressure properties of the GP-dispersed oil were improved by 80%, 33%, and 40%, respectively.

More recently, organically modified GP and GP–inorganic nanocomposites have been widely studied. Graphene oxide was modified with ionic liquids and ethylene glycol, and its tribological properties were evaluated by Kumar et al. In addition, Su et al. prepared Ni and Ag nanoparticle-decorated GP nanocomposites using a chemical reduction approach. Many studies have demonstrated that GP is a good supporter of nanoparticles, and as-prepared nanocomposites usually exhibit better lubricating performances than GP alone.

Previous studies have also shown that nanocomposites of GP and GP-like layered metal dichalcogenide nanoparticles exhibit remarkable physical and chemical properties, which is probably because of their structural compatibility and synergistic interactions. However, research on the lubricating potential of these nanocomposites has rarely been reported. As a typical GP-like layered metal dichalcogenide, WS2 has been widely studied because of its low cost, effectiveness in reducing friction and wear, environmental compatibility, and excellent oxidation resistance.

Motivated by the above considerations, we prepared WS2 nanoparticle-decorated GP composites by adopting a facile and scalable approach and evaluated their lubricating performance on sliding steel-on-steel contacts using a UMT-2 ball-on-plate tribotester.

2 Experimental details

2.1 Materials

The GP used in this study was purchased from Jinan Graphene New Materials Co., Ltd. (Jinan, China) and was used as received. Commercial bulk WS2 (purity \( \geq 99.9\% \), particle size < 1 \( \mu \text{m} \)) was
2.2 Synthesis and characterization of WS₂/GP nanocomposites

To produce WS₂/GP nanocomposites, we first prepared WS₂ nanoparticles from bulk WS₂ using a mechanochemical treatment method. In a typical procedure, 0.5 g WS₂ and 5.0 g NaCl were added to the agate grinding bowl of a planetary ball mill (JC-2, Nanan Jiacheng Electronic Technology Co., Ltd., Nanan, China) with a ball-to-feed ratio of 1 : 7. Ball milling was performed for 2 h at a rotation rate of 450 rpm at room temperature (RT). In this process, WS₂ was uniformly mixed with NaCl and became nanostructured after ball milling. The samples were then repeatedly washed with deionized water and ethanol before being dried under vacuum at 80 °C for 8 h to obtain the exfoliated WS₂ (exf-WS₂) nanoparticles.

In the subsequent step, the GP and exf-WS₂ were dispersed in deionized water with a mass ratio of 1 : 9; the mixture was then sonicated and stirred at RT for 1 h each using a KQ-700E ultrasonic system (Kunshan Ultrasonic Instruments Co., Ltd., Kunshan, China) and a REX magnetic stirrer (REX, Shanghai, China). To generate active functional sites, we dropped two drops of concentrated hydrochloric acid into the reaction mixture. We then stirred the mixture and sealed it in a 50 ml autoclave, which was maintained at 240 °C for 24 h. Finally, the resulting product, WS₂/GP, was filtered using a TG-16 high-speed centrifuge (Gongyi Yuhua Instrument Co., Ltd., Gongyi, China) and transmission electron microscopy (TEM, JEM-2100F, JEOL, UK) to characterize the morphologies and microstructures. X-ray diffraction (XRD) measurements were performed using an X’Pert Pro X-ray diffractometer (PANalytica, Holland) with an X-ray source of Ni Kα radiation (1.54 Å) in the 2θ range 10–80° with a step size of 0.016°. Raman spectra were recorded in the range 4000–400 cm⁻¹ using a 532 nm laser as the excitation source on a Raman microscope system (LabRam HR, Renishaw, UK).

2.3 Tribological evaluation of WS₂/GP nanocomposites

In this study, GP, exf-WS₂ nanoparticles (nano-WS₂), and WS₂/GP nanocomposites (WS₂/GP) were dispersed into PAO4 oil as a lubricant under ultrasonication for 1 h. Inorganic nanoparticle additives are infamous for having poor dispersion stability in organic liquids, so the same concentration of surfactant Span-80 (C₃₂H₆₄O₆, Chengdu Changzheng Glass Co., Ltd.) was used as a dispersing agent. Fig. 1 presents digital pictures of different nano-additive dispersions with and without addition of Span-80 immediately after sonication and after 7 days undisturbed at 100 °C after sonication: (0) pure PAO4, (1) PAO4 + 0.1 wt% GP + 0.1 wt% SP, (2) PAO4 + 0.1 wt% GP, (3) PAO4 + 0.1 wt% nano-WS₂ + 0.1 wt% SP, (4) PAO4 + 0.1 wt% nano-WS₂, (5) PAO4 + 0.1 wt% WS₂/GP, and (6) PAO4 + 0.1 wt% WS₂/GP.

![Image: Images of different nano-additive dispersions with and without addition of Span-80 immediately after sonication and after 7 days undisturbed at 100 °C after sonication.](image)

Fig. 1 Images of different nano-additive dispersions with and without addition of Span-80 immediately after sonication and after 7 days undisturbed at 100 °C after sonication: (0) pure PAO4, (1) PAO4 + 0.1 wt% GP + 0.1 wt% SP, (2) PAO4 + 0.1 wt% GP, (3) PAO4 + 0.1 wt% nano-WS₂ + 0.1 wt% SP, (4) PAO4 + 0.1 wt% nano-WS₂, (5) PAO4 + 0.1 wt% WS₂/GP, and (6) PAO4 + 0.1 wt% WS₂/GP.

3 Results and discussion

3.1 Morphology and microstructure

SEM images of GP, nano-WS₂, and WS₂/GP nanocomposites are presented in Fig. 2. The SEM image of GP reveals a wrinkled and
layered morphology (Fig. 2a), whereas nanoscale patchy particles are observed in the nano-WS2 image (Fig. 2b). The image of WS2/GP in Fig. 2c reveals overlapping and interweaving of sheets of GP and nano-WS2, which is further confirmed by the EDX results in Fig. 2d.

Fig. 3 presents TEM and HRTEM images of GP, nano-WS2, and WS2/GP. The GP image reveals a few-layered and wrinkled structure (Fig. 3a), with an interlayer distance of 0.34 nm, corresponding to the (002) plane (Fig. 3b). A nanoscale patchy structure of nano-WS2 with a size distribution of below 100 nm is visible in Fig. 3c. Fig. 3d indicates that the interlayer distance is 0.62 nm, corresponding to the (002) plane. In Fig. 3e, loading of nano-WS2 on the surfaces of GP is observed, resulting in a layer-by-layer hybrid structure of WS2/GP. Moreover, two different interlayer distances of 0.34 and 0.62 nm are simultaneously observed, as labeled in Fig. 3f.

To examine the fine microstructure, bulk WS2, GP, nano-WS2, and WS2/GP samples were characterized using XRD and Raman analyses. Fig. 4 presents the XRD patterns of the samples. All the peaks of bulk WS2 can be attributed to the hexagonal phase (JCPDS no. 08-0237), indicating its high purity. Strong (002) diffraction peaks of the bulk WS2, nano-WS2, and WS2/GP are observed at 14.4°, indicating their well-stacked layered structure. However, both the nano-WS2 and WS2/GP display much less intense (002) peaks than the bulk WS2, indicating that their crystallite size and the number of layers are much smaller. For GP, the C (002) characteristic peak of GP appears at 25.9°. Furthermore, all the peaks of nano-WS2 are detected in the WS2/GP XRD pattern, and a new peak at 25.9°, corresponding to the C (002) peak, is also observed.

Fig. 5a presents the Raman spectra of the GP, nano-WS2, and WS2/GP. Two dominant peaks of nano-WS2 are observed at 353 and 419 cm⁻¹, corresponding to the E1²g and A1g modes of the hexagonal WS2, respectively. For GP, the GP characteristic D, G, and 2D peaks are observed. The appearance of the D peak proves that a significant number of defects exist. In the spectrum of WS2/GP, the E1g modes, G, and 2D peaks as well as the D and G peaks can be detected. Additionally, the D peak of GP corresponds to sp³/sp² hybridized defects, whereas the G peak.
corresponds to vibration in all of the sp$^2$-bonded carbon atoms. Thus, magnification and Gaussian fitting of the D and G peaks of GP and WS$_2$/GP as well as the intensity ratio of the D peak to the G peak ($I_D/I_G$) are compared in Fig. 5b. The $I_D/I_G$ of WS$_2$/GP was significantly reduced (from 1.088 to 0.426), revealing that the GP defects were repaired by nano-WS$_2$.

In summary, these findings confirm the successful preparation of WS$_2$/GP nanocomposites; it is reasonable to conclude that the GP and nano-WS$_2$ are chemically linked by $\pi$-$\pi$ interactions.

### 3.2 Friction and wear

We first investigated the lubricating abilities of GP and nano-WS$_2$ separately. Fig. 6 shows a plot of the average friction coefficients when lubricated with different concentrations of GP-dispersed oil and nano-WS$_2$-dispersed oil. The friction coefficient (COF) was effectively reduced after adding GP or nano-WS$_2$, and the COF reduction reached a maximum at the same concentration of 0.01 wt%, which was considered to be the optimal concentration of these two additives and was thus selected for investigation of the lubricating potential of WS$_2$/GP nanocomposites. However, further increase in the concentration increased the COF, especially for nano-WS$_2$, which was probably because the inhomogeneity of the lubricant resulted from unstable dispersion.

The friction coefficient curves of the PAO4 base oil and oils dispersed with 0.01 wt% GP, nano-WS$_2$, and WS$_2$/GP are presented in Fig. 7a. A physical mixture of GP and nano-WS$_2$ with a mass-ratio of 1 : 9 (WS$_2$ + GP) was also used at the same concentration for comparison. All the dispersed oils exhibited smaller and more stable friction coefficients than the base oil. However, the additives resulted in different friction-reducing efficiencies. The WS$_2$/GP-dispersed oil exhibited the lowest friction coefficient, followed by the WS$_2$ + GP-dispersed oil.
Comparisons of the average friction coefficients and wear rates using these oils are shown in Fig. 7b. All the nano-additives improve the lubricating performance of the base oil. However, the oil dispersed with WS$_2$/GP exhibits the most outstanding potential; its friction coefficient and wear rate were reduced by 70.2% and 65.8%, respectively, compared with the base oil. Fig. 7b also suggests that WS$_2$/GP has a better lubricating performance than GP or nano-WS$_2$ alone. This finding may originate from the synergistic lubricating action of the two components. Additionally, a certain degree of friction and wear reduction was also caused by WS$_2$ + GP compared with GP or nano-WS$_2$ alone; however, this was far less significant than that of WS$_2$/GP. This finding also confirms that WS$_2$/GP is a new composite material rather than a simple physical mixture.

Fig. 8a shows the friction coefficient curves of the WS$_2$/GP dispersed oils with different concentrations. The average friction coefficients and corresponding wear rates are compared in Fig. 8b. Similar “deep valley” shapes were observed for the variations; the lowest friction coefficient and wear rate appear at 0.02 wt% and 0.04 wt%, respectively. The optimal concentration of WS$_2$/GP is considered to be in the range 0.02–0.04 wt%. It cannot be overlooked that this optimal concentration is considerably higher than that of GP or nano-WS$_2$, which is probably because of the better dispersion of WS$_2$/GP. In summary, an excellent lubricating performance can be achieved with WS$_2$/GP-dispersed oil, which is maximized at concentrations of 0.02–0.04 wt%.

### 3.3 Worn surface characterization

After the tests, the worn surfaces of the plates using the PAO4 base oil and dispersed oils containing 0.01 wt% GP, nano-WS$_2$, WS$_2$ + GP, and WS$_2$/GP were analyzed using SEM, and the results are shown in Fig. 9. In Fig. 9a and b, the wear scar of the plate lubricated with the base oil is the largest; the worn surface is very rough and displays deep machining marks and severe
material spallation. After adding GP, the width of the wear scar was reduced, the defects became relatively shallower and narrower, and the worn surface became smoother despite the presence of machining marks (Fig. 9c and d). The worn plate lubricated with the nano-WS$_2$-dispersed oil displays slightly rough surfaces with certain machining marks (Fig. 9e and f). GP and nano-WS$_2$ are considered to have similar lubricating ability. As observed in Fig. 9g and i, the plates lubricated with the WS$_2$ + GP- and WS$_2$/GP-dispersed oil display much smaller wear scar widths than those using GP or nano-WS$_2$ alone; their worn surfaces are significantly smoother, and the defects are not obvious (Fig. 9h and j). However, it is apparent that WS$_2$/GP had
better lubricating ability than WS$_2$ + GP; the worn surface lubricated with the WS$_2$/GP-dispersed oil is very smooth without obvious defects.

Fig. 10 presents Raman spectra of the wear scars of the plates lubricated with the PAO4 base oil and the dispersed oils containing 0.01 wt% GP, nano-WS$_2$, and WS$_2$/GP. For the wear scar of the plate lubricated with the base oil, a typical peak of iron oxide was detected at 668 cm$^{-1}$. Considering that severe wear occurred, adhesive wear was the dominant mechanism of wear. After adding GP, it can be concluded that the GP layers adsorbed on the sliding interfaces during the frictional process as evidenced by the appearance of D and G peaks. A protective film may have been formed, which explains the friction and wear reduction. In addition, the typical peak of iron oxide was also observed, indicating that severe oxidation occurred. For the wear scar of the plate lubricated with the nano-WS$_2$-dispersed oil, typical peaks at 353 and 419 cm$^{-1}$, which were attributed to the E1 2g and A$_{1g}$ modes of nano-WS$_2$, were observed. However, two new peaks at 267 and 491 cm$^{-1}$ emerged after friction, which were attributed to the reaction products of nano-WS$_2$, indicating that nano-WS$_2$ reacted with the substrate or molecules of the base oil. Remarkably, the typical peak of iron oxide was obviously weakened. This finding indicates that the deposition, self-repair, and formation of the chemical reaction film may be the main causes of the friction-reduction and anti-wear properties of nano-WS$_2$. When the surface was lubricated with the WS$_2$/GP-dispersed oil, the characteristic peaks of nano-WS$_2$ at 353 and 419 cm$^{-1}$ and the characteristic peaks of GP at 1350 and 1576 cm$^{-1}$ could be simultaneously detected. Additionally,

no clear peaks of the reaction products of nano-WS$_2$ were observed, suggesting that GP helps to protect nano-WS$_2$ from tribochemical reactions. Furthermore, the typical peak of iron oxide was undetectable. Remarkably, the intensity reduction of the characteristic peaks of GP was not obvious compared with that of the GP-dispersed oil, which is unexpected even though the concentration of GP was one order of magnitude lower.

Fig. 11 shows the elemental distribution in the wear scars of the plates lubricated with these oils, as detected by SEM-EDX. The lowest Fe content was observed for the wear scar generated with the base oil and a strong peak for O was detected, which indicated that severe tribo-oxidation of the substrate occurred. After adding GP, a strong peak for C was observed, indicating that the GP layers adsorbed on the sliding interfaces. After adding nano-WS$_2$, peaks of W and S as well as relatively high O and Fe contents were observed. Most likely, a deposited film and a chemical reaction film of nano-WS$_2$ were formed on the sliding interfaces. When the plate was lubricated with the WS$_2$/GP-dispersed oil, peaks of W and S were also detected. In addition, the lowest O and highest Fe contents were observed, and a strong C peak was detected. These findings further demonstrate the synergistic effect of these two nano-additives on reducing the friction and wear.

XPS analysis was performed to explore the lubricating mechanism of this composite additive. Fig. 12 presents the full spectrum and curve-fitted XPS spectra of C1s, O1s, Fe2p, W3d, and S2p on the wear scar of the plate lubricated with 0.01 wt% WS$_2$/GP-dispersed oil. In Fig. 12b, the two C1s peaks, which matched well with the sp$^2$-C (C–C/O) and sp$^3$-C (C=C/O)31
signals, may originate from the WS<sub>2</sub>/GP nanocomposites. Therefore, we can reasonably conclude that the GP of the nanocomposites was deposited on the contact surfaces and formed a physical protective film. The O1s peak at 532.1 eV in Fig. 12c was indexed to sulfates, suggesting that a chemical transfer film may have been formed on the worn surfaces.

This conjecture is further authenticated by the WO<sub>3</sub> signal in the W3d peak (Fig. 12e) and S<sup>4+</sup> signal in the S2p peak (Fig. 12f). In addition, the other O1s peak at 530.4 eV was attributed to Fe<sub>3</sub>O<sub>4</sub>. The Fe<sub>2</sub>p<sub>3/2</sub> and Fe<sub>2</sub>p<sub>1/2</sub> signals positioned at 711.1 and 724.7 eV, respectively, belonged to the Fe2p of the Fe<sub>3</sub>O<sub>4</sub> groups. These findings confirm that the tribo-oxidation of the substrate cannot be prevented completely. Furthermore, the WS<sub>2</sub> signals in the W3d peak and S2p peak can only originate from the WS<sub>2</sub>/GP nanocomposites, which might be due to the deposition of nano-WS<sub>2</sub> of the WS<sub>2</sub>/GP nanocomposites.

### 3.4 Synergistic lubricating mechanism

In order to intuitively compare the lubricating abilities of the nano-additives, a simplified polar coordinate method was used, based on the above characterization and analysis results, as shown in Fig. 13. Three lubricating mechanisms, self-repairing, adsorption, and tribochemistry, as well as the dispersibility were used as evaluation indexes and were roughly divided into three grades: I, II, and III, where I is inferior and III is superior. In the GP-dispersed oil, the GP layers sheared at the sliding interfaces and adsorbed, which is attributed to its 2D structure;<sup>32–34</sup> a protective film may be formed, which results in low friction and wear. In the nano-WS<sub>2</sub>-dispersed oil, the main lubricating mechanism was a frictional chemical reaction and deposition and self-repair of the nano-WS<sub>2</sub>. When lubricated with the WS<sub>2</sub>/GP-dispersed oil, a combined effect of GP and nano-WS<sub>2</sub> in the WS<sub>2</sub>/GP nanocomposites was observed during the frictional process. This phenomenon resulted in enhanced adsorption of GP layers and deposition of nano-WS<sub>2</sub>, which played a role in the protection and restoration and yielded a synergistic lubricating mechanism.

![Fig. 13](Image) Comparison of the lubricating mechanisms of the GP, nano-WS<sub>2</sub>, and WS<sub>2</sub>/GP nano-additives using a simplified polar coordinate method.

### 4 Conclusions

In summary, composites of GP anchored with WS<sub>2</sub> nanoparticles were successfully prepared, and these displayed better dispersion in the base oil than GP or nano-WS<sub>2</sub> alone. The addition of WS<sub>2</sub>/GP significantly improves the lubricating performance of the base oil. The friction coefficient and wear rate were reduced by 70.2% and 65.8%, respectively, when 0.02–0.04 wt% WS<sub>2</sub>/GP was dispersed. The friction-reducing and anti-wear abilities of WS<sub>2</sub>/GP were also superior to those of GP or nano-WS<sub>2</sub> alone as well as to a physical mixture of those of GP or nano-WS<sub>2</sub> alone. These results not only suggest the use of WS<sub>2</sub>/GP nanocomposites as potential additives to improve the lubricating performance of oil-based lubricants but also provide new ideas for research on the lubricating potential of nanocomposites of GP and GP-like nanoparticles.

### Acknowledgements

This study was supported by the National Science Foundation of China (51375407 and U1530136).

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