ABSTRACT: We present a new assessment method for driver visibility based on reaction time measurement and workload in real driving situations from the most relevant accident scenario involving pedestrians. The procedure was validated in a balanced trial to compare a wet flatblade windshield washing system to a conventional Fluidic nozzles system. The test cohort comprised 204 subjects who form a representative sample of German driving license holders. The average reaction time gain of wet flatblade over Fluidic nozzles is 315 ms for pedestrian detection and 270 ms for the recognition of critical traffic situations.

KEY WORDS: Human engineering, Safety, Reaction time, Workload, Wiping systems, Washing function, Fluidic nozzle, Wet flatblade (C2)

1. Introduction

To date, current regulations of the U.S. DoT Federal Motor Carrier Safety Administration (1), the SAE International (2),(3), and the ISO (4) define minimum standards for windshield wiping and washing systems based on the geometric design of the driver’s outlook, and on technical features such as wiper speeds and reliability (e.g. number of cycles, temperature ranges and rubber aging). None of the test procedures described in the regulations takes into account the perception of dynamic traffic scenes by the driver.

The assessment method we present in this contribution bridges this gap by presenting a perception test design that is based on a relevant accident scenario, namely crossing pedestrians. The scenario is represented by three pairs of uncritical and critical situations that are displayed in order to measure reaction times for pedestrian detection, and for the classification of the situations' criticality.

The method is designed to measure the impact of visual perturbances on the windshield upon drivers’ reaction times. In this contribution, we use the method to assess visual disturbances during windshield washing with two windshield wiping and washing systems.

The method can also be applied to assess other sources of visual disturbances such as dirt on the windshield and rubber quality including ageing effects.

The remainder of this contribution is structured as follows. In Section 2, we describe the assessment method. Section 3 describes the method’s application, i.e. devices under test, test Kohort and Balanced Trial. Results are described in Section 4, Section 5 draws a conclusion. Section 6 contains an Ethics declaration which is due to the involvement of human subjects.
The first and most important reason is safety: if a car is heading north in Germany, i.e. on the northern hemisphere, then the windshield is not directly exposed to sunlight. We therefore avoid the corresponding glare during the test runs.

The second reason for the orientation of the test track in a northern direction is to maintain constant test conditions. The opacity of spray on a windshield is greatly affected when it is directly exposed to a light source.

By avoiding direct exposure of the windshield to the sun, we avoid varying opacity of the spray, and hence varying test conditions.

When the test drivers pass Light barrier 1, a pump is activated to spray a contamination liquid onto the car, thus decreasing the driver’s visibility.

For the contamination of the windshield, a mixture of water, road salt and dust is used. The mixture ratio is 120 l water, 1 kg of dust and 3 kg of salt. For the dust, a standardised, synthetically produced industry dust is used (Arizona-dust fine SAE J726). After the windshield contamination, the drivers are tasked to drive on until they reach a small bump and then to start windshield washing. The bump is referred to as “Haptic feedback” in Fig. 1.

Upon activation of the washing pump, a controller on board of the car sends a trigger signal to the Ground Control Station (GCS) via a radio link. In Fig. 1, a dashed arrow from the car to the GCS illustrates the radio link. The second light barrier at the position of the bump is used for tests with clean windshield and neither wiping nor cleaning to replace the trigger signal derived from the washing pump.

Upon reception of the trigger signal, the GCS starts sending video images of traffic situations to an 80 inch display which is large enough to show pedestrians in their natural size. At that moment, the distance between the car and the display is 24 m, which corresponds to 1.7 s at urban speed (50 kph).

Fig. 2 shows an overview of the video images used during the tests. Each row corresponds to one pair of uncritical and critical traffic situations. Key frames at defined positions in the video sequence are used as temporal reference for the detection and recognition tasks, see the indications in Fig. 2. The images of each pair of video sequences are pairwise identical except for the last frame which is key to determining whether the video sequence represents a critical or an uncritical situation.

The key frames for situation recognition show the pedestrians with eye contact to the driver to indicate an uncritical situation, or they show the pedestrians’ back to indicate a critical situation.

The test drivers are tasked to release the throttle pedal as soon as they see a person on the display. By means of a sensor on the pedal, the on-board controller detects the release and sends a corresponding message to the GCS.

Upon appearance of the key frame for an uncritical situation, the test persons are tasked to re-accelerate, they are tasked to brake if they see the pedestrians’ back. The sensor on the throttle is also used to detect re-acceleration; for the detection of braking, the on-board controller is connected to the brake light. The measurement of reaction times is done in the
GCS. Detection and recognition times are based on the time difference between sending the respective key frame to the display and receiving the corresponding messages from the onboard controller.

One complete set of test runs contains the three pairs of critical and uncritical traffic situations, and three runs with an empty scene. “Critical”, “uncritical” and “empty” video sequences are displayed in random order. Otherwise, the detection task would be trivial. While the test drivers perform six detection tasks during a run with one system, they perform only three recognition tasks. Only the three critical scenes count into them. The purpose of the uncritical scenes is to validate the reactions in the critical scenes and to prevent the test person to brake in any case.

2.2. Definition of the assessment procedure

As mentioned above, we applied the above described method to compare two windshield washing and wiping systems. A safety benefit of a wiper system can be assumed when it enables drivers to react faster in critical situations. Our assessment procedure foresees that a large number of test drivers is involved on a test parcours where their performance is measured while they have to react to the six above-mentioned traffic scenes.

A qualitative statistics aims to answer if most people are able to react faster with one of the two systems. For each driver we note whether he or she performed better more often with one system. Also, we analysed the reaction time difference between the systems for statistical significance.

In a quantitative statistic for each system, the mean reaction times for the detection and recognition tasks are determined together with their standard errors. The same analysis is done for the reaction time differences between the washing systems in each of the six situations. The results give a precise idea to which extent the reaction time is affected by visual disturbance.

Eventually, the results of the reaction time measurements are compared to feedback given by drivers about their subjective performance differences between both systems, and the tests without windshield contamination. Feedback was collected using the standard NASA TLX method (8).

3. method application

3.1. The systems under test

In order to validate our method, we measured reaction times during washing cycles using wet flatblade and Fluidic nozzles. For control, we measured reaction times also with neither washing nor wiping activity.

Initially, wiper and washer systems were separate devices. The washer system applied water onto the windshield through hood mounted nozzles and the wiper removed rain. Nozzle developments went from single jet nozzles to triple jets nozzles, the disadvantage being that the application of the washer fluid was limited to a few distinct spots. In the 90’s, Fluidic nozzles were introduced, which distribute washer fluid into droplets over a larger area, to improve cleaning efficiency. Unfortunately, with this system the view of the driver is disturbed for a time period, which may create a safety risk. Mid of the 90’s Integrated Cleaning appeared (nozzles on wiper arms or wiper blades) to improve efficiency at high speed. The systems were further improved for safety and liquid consumption up to now.

For the tests, we used one of the most advanced Integrated Cleaning systems, a wet flatblade introduced in 2012 with nozzles all along the blade and software controlled liquid depletion1.

Fig. 3 Windshield washing with hood Fluidic nozzles (above) and wet flatblade (below). Note the difference in the amount of spray on the windshield.

3.2. Selection and number of test drivers

The tests being performed in Germany, we decided to make a statement about the potential gain in safety for holders of a German driver’s license. Therefore, the persons selected for the test drives should be representative of the population the statement is targeted at in terms of gender and age distribution.

The subjects were grouped with respect to their age as follows:
- 18-30 years,
- 31-50 years,
- 51-80 years.

When we looked into the German demographic data, we recognised differences between the resident population and our target population, i.e. holders of a driving license.

Table 1 shows the percentage of the three age groups in the resident and in the driving population, separately for male and female subjects (M18-30 through F51-80). The statistics are from 60.000 questionnaires of the 2008 MiD census about mobility in Germany (5).

1 The wet flatblade system we used was provided by Valeo, it is commercially known under the name AquaBlade®.
Table 1  Percentage of women (F) and men (M) in the 18-30, 31-50, and 51-80 age groups of the resident, and of the driving population in Germany.

| Age Group | Resident Population | Driving Population |
|-----------|---------------------|--------------------|
| M18-30    | 10.59%              | 10.24%             |
| F18-30    | 9.21%               | 9.06%              |
| M31-50    | 18.62%              | 19.96%             |
| F31-50    | 19.83%              | 20.87%             |
| M51-80    | 19.72%              | 20.84%             |
| F51-80    | 22.03%              | 19.04%             |

As can be seen from the line labelled “F51-80”, the percentage of female drivers between 51 and 80 years is significantly lower (19.04%) than the share that 51-to-80-year old women have of the resident population (22.03%).

3.3. Balanced trial

Following a theoretical instruction and a set of 9 training runs, each test person carried out 27 test runs as described above, one set of 9 without windshield washing, one set with Fluidic nozzles (F), and one set with wet flatblade (W). Tests without windshield washing are referred to as “no wiping” (N) in Table 2.

Table 2  Distribution of numbers of test persons over gender and age groups, and over orders, in which tests with wet flatblade (W), no wiping (N) and Fluidic nozzles (F) were carried out.

| Order | M18-30 | F18-30 | M31-50 | F31-50 | M51-80 | F51-80 | Total |
|-------|--------|--------|--------|--------|--------|--------|-------|
| WFN   | 4      | 3      | 7      | 7      | 7      | 6      | 34    |
| NWF   | 4      | 3      | 7      | 7      | 7      | 6      | 33    |
| FNW   | 4      | 3      | 7      | 7      | 7      | 6      | 33    |
| WNF   | 4      | 3      | 7      | 7      | 7      | 6      | 34    |
| FWN   | 4      | 3      | 7      | 7      | 7      | 6      | 35    |
| NFW   | 4      | 3      | 7      | 6      | 7      | 6      | 33    |
| Total | 24     | 18     | 42     | 42     | 38     | 204    |

There are six possible orders in which the three sets can be carried out. In order to establish fair conditions for the comparison of Fluidic nozzles and wet flatblade, we took care that each of the possible orders was carried out by the same number of test persons. An additional constraint was that the groups M18-30 through F51-80 needed to be represented according to the percentage values contained in the “driving population” column of Table 1. Table 2 shows the resulting test plan which we executed according to the rules of a balanced trial, i.e. before having a second subject of the M18-30, M18-30 age groups execute a test in the order WFN, we took care that all other orders NWF through NFW were followed by one person of that same group, and before any of the orders was followed by a second subject of the M18-30 and W18-30 groups, we took care that in each of the other groups each order had been followed by two subjects already.

Table 3  Representative and achieved actual sample of the German driving population.

| Age Group | Driving Population | Actual Share |
|-----------|--------------------|--------------|
| M18-30    | 10.24%             | 11.76%       |
| F18-30    | 9.06%              | 8.82%        |
| M31-50    | 19.96%             | 20.59%       |
| F31-50    | 20.87%             | 19.61%       |
| M51-80    | 20.84%             | 20.59%       |
| F51-80    | 19.04%             | 18.63%       |

As can be seen in Table 2, we released, for the groups F31-50 and F51-80, the constraint that each of the permutations WFN through NFW be represented equally, see Column “actual share” of Table 3 for the resulting composition of the test cohort.

4. Results

This chapter contains the objective and subjective results of the test drives. The test drive measurements show the objective performance, for example reaction time. On the basis of a questionnaire we obtained subjective preference values.

4.1. Bernoulli process of results

The Bernoulli process (reference (6), see Fig. 4) shows the objective and subjective performance of the test drivers. Over progressing test person IDs, it indicates the rate of drivers who performed better with the wet flatblade than with the fluidic system (objective performance) and who preferred wet flatblade (subjective preference).

After tests with about 150 persons, the Bernoulli process shows a stable result. The actual number of test persons involved in the study was 204 which is more than enough for the analysis.
4.2. Answers from test drivers

Objective performance measurements do not always correlate with user’s acceptance and satisfaction. For this reason, two questionnaires were designed for the test drivers to receive feedback on the different systems.

The first questionnaire is a standardised NASA TLX\(^8\), which the participants were to fill in after each set of nine test runs with one of the three selected “systems” N, W, and F.

The most important topics of the first questionnaire are mental demand, physical demand, temporal demand, performance, effort and frustration. As can be seen in Fig. 5, wet flatblade is rated better (smaller values) in nearly all topics.

The second questionnaire requests additional information and a personal assessments after completion of all test drives. 55% of the participants used a visual aid in general and 91% used a visual aid for the actual test drives. 84% own a car and 53% already had at least one accident. See Fig. 6 for some more results from the second questionnaire.

Fig. 5 Summary of the NASA TLX questionnaire.

The second questionnaire requests additional information and a personal assessments after completion of all test drives. 55% of the participants used a visual aid in general and 91% used a visual aid for the actual test drives. 84% own a car and 53% already had at least one accident. See Fig. 6 for some more results from the second questionnaire.

How often do you drive a car?

| Frequency   | Seldom | Sometimes | Often | Very often |
|-------------|--------|-----------|-------|------------|
| %           | 4      | 19        | 35    | 42         |

How do you rate your eyesight?

| Visual Acuity | Good | Medium | Bad |
|---------------|------|--------|-----|
| %             | 72   | 27     | 1   |

Which system was for you the safest?

| System        | Wet flatblade | Fluidics | No difference |
|---------------|---------------|----------|---------------|
| %             | 82            | 10       | 8             |

Do you think systems like wet flatblade could prevent accidents?

| Opinion      | Yes | No | Not sure |
|--------------|-----|----|---------|
| %            | 70  | 22 | 8       |

4.3. Reaction time measurements

Sample measurements for the recognition task in the critical situation with the fluidic system are shown in Table 4. There exist two more of these data sets for the two other “systems” (wet flatblade and no wiping) and three more data sets for the detection task with six columns each (critical and uncritical situations).

Table 4 Sample measurements from Fluidic nozzles, recognition task (reaction times in ms).

| Fle, Rec | Scene 1 | Scene 2 | Scene 3 |
|----------|---------|---------|---------|
| Driver 1 | 1528    | 1002    | 1368    |
| Driver 2 | 801     | 684     | 680     |
| Driver 3 | 726     | 920     | 922     |
| Driver 4 | X       | 965     | 1208    |
| ...      | ...     | ...     | ...     |
| Driver 204| 966    | 1094    | -       |

Fig. 7 and Fig. 8 at the end of the article show the reaction time histograms.

4.3.1. Quality of the measurements

The “X” in Scene 1 of Driver 4 indicates that the test driver did pass the detection task but not the recognition task in this case. The “-” in Scene 3 of Driver 204 indicates that already the detection task was not passed in that case.

The quality of source data is rated by the amount of misbehavior in the reaction tasks. A misbehavior is (a) to not release the throttle pedal in a non-empty scene, (b) to release the throttle pedal in an empty scene, (c) to not break in a critical scene, (d) to break or not to reaccelerate in an uncritical scene, (e) to react too slow on an event, or (f) to react too soon to an event.

Basically, (e) means to brake after the passenger has already passed and for (f) the lower bound for plausible reaction times, see reference (7). Note that the recognition task was not evaluated in scenes where the detection task remained unaccomplished.

Table 5 shows the overall detection and recognition rates observed during our study. The reading of the detection rates is as follows. For non-empty scenes, the numbers indicate the percentage of test runs in which the test persons correctly released the throttle pedal. For the empty scenes, the numbers indicate the percentage of test runs in which the test persons correctly remained on the throttle pedal.

The recognition rates for the non-empty scenes indicate the percentage of test runs in which the test persons correctly braked in critical situations and re-accelerated in uncritical situations.

Knowing that in 84.64% and 92.81% of the tests in empty scenes, test persons correctly remained on the throttle validates the detection rates observed for the non-empty scenes.

Formally, we obtained recognition rates also for the empty scenes, these can be explained as follows. For the 15.36% and
7.19% of false detections with Fluidic nozzles and wet flatblade, respectively, the percentage of test persons that correctly re-accelerated is 95.45% and 92.31%, respectively, see Table 5.

Table 5 Overall detection and recognition rates with Fluidic nozzles (FLC) and wet flatblade (WFB) for test runs critical, uncritical and empty.

|                  | DetRate  | RecRate  | DetRate  | RecRate  |
|------------------|----------|----------|----------|----------|
|                  | FLC      | FLC      | WFB      | WFB      |
| Critical         | 90.20%   | 93.48%   | 90.36%   | 94.76%   |
| Uncritical       | 82.84%   | 84.81%   | 82.35%   | 92.66%   |
| Empty            | 84.64%   | 95.45%   | 92.81%   | 92.31%   |

Table 5 shows that the vast majority of the tests were performed correctly.

4.3.2 Model assumptions
Each driver $x$ has per system and per task its own random distribution of reaction times with its own expectation $\mu_x$ and variance $\sigma^2_x$. Let

$$\mu = \frac{1}{n} \sum_x \mu_x$$

be the overall mean of the individual expectations over all $n$ drivers in the base population and the parameter of interest. Let

$$\sigma^2_{\text{ind}} = \frac{1}{n} \sum_x \sigma^2_x$$

be the mean individual variance in the base population and

$$\sigma^2 = \frac{1}{n} \sum_x (\mu_x - \mu)^2$$

the variance of the individual expectations over the base population. Let $X$ be a random driver of the base population and let $T$ be a random reaction time of $X$ (or a reaction time difference between two systems under elsewise identical conditions). With the notation above it holds that

$$E[T|X] = \mu_x$$

and

$$V[T|X] = \sigma^2_x.$$

By the law of total expectation it holds further

$$E[T] = E[E[T|X]] = E[\mu_x] = \mu$$

and by the law of total variance

$$V[T] = E[V[T|X]] + V[E[T|X]]$$

$$= E[\sigma^2_x] + V[\mu_x] = \sigma^2_{\text{ind}} + \sigma^2 = \sigma^2.$$

Taking $k$ test drivers $X_i$ and performing $r_i$ measurements $T_{i,j}$ on the $i^{th}$ driver yields an estimator

$$m = \frac{1}{k} \sum_i \left( \frac{1}{r_i} \sum_j T_{i,j} \right)$$

of $\mu$ with variance

$$\sigma^2_m = \frac{1}{k} \left( \frac{\sigma^2_{\text{ind}}}{r} + \sigma^2 \right)$$

where $\bar{r}$ is the harmonic mean of valid values per test driver. The rest of this paragraph proofs equation (2) and can safely be skipped on the first read:

Let

$$t_i = \frac{1}{r_i} \sum_j T_{i,j}$$

be the mean reaction time of driver $X_i$. By the iterated law of total expectation and variance conditioned on $r_i$ it holds

$$E[t_i|X_i] = E[E[t_i|X_i] | X_i] = E[\mu_{X_i} | X_i] = \mu_{X_i}$$

and

$$V[t_i|X_i] = E[V[t_i|X_i] | X_i] + V[E[t_i|X_i] | X_i]$$

$$= E[\frac{\sigma^2_{X_i}}{r_i}] + V[\mu_{X_i}] = \frac{\sigma^2_{X_i}}{\bar{r}} + 0$$

where

$$\frac{1}{\bar{r}} = E[\frac{1}{r_i}]$$

is assumed to be independent of $X_i$. This assumption might not exactly be true as a driver with a small reaction time variance performs very similar on each turn and can be considered a “good” driver who will likely pass all tests whereas a driver with high reaction time variance has very unpredictable behavior and one would expect it to be more likely that the test driver misses one or two tests. However, the effect is small and was neglected here. To compensate for it one could slightly decrease $\bar{r}$.

By the total law of variance it follows further:

$$V[t_i] = E[V[t_i|X_i]] + V[E[t_i|X_i]]$$

$$= E[\frac{\sigma^2_{X_i}}{r_i}] + V[\mu_{X_i}] = \frac{\sigma^2_{\text{ind}}}{\bar{r}} + \sigma^2$$

and finally

$$\sigma^2_m = V[m] = V \left[ \frac{1}{k} \sum_i t_i \right] = \frac{1}{k} V[t_i] = \frac{1}{k} \left( \frac{\sigma^2_{\text{ind}}}{\bar{r}} + \sigma^2 \right)$$

since the $t_i$ are independent.

4.3.3 Mean estimators
The mean estimators for the different washing systems and tasks are shown in Table 6.

The lower half shows the mean estimators of the paired time differences. They are not equal to the differences of the mean estimators in the upper half of the table since the reaction
times are weighted differently and reaction times that have no corresponding partner in the paired difference do not count into the difference estimators.

4.3.4 Estimator of Variances

For test drivers who passed at least two scenes it is possible to estimate the individual variance with the usual empirical variance estimator. Taking the mean over all test drivers yields to estimate the individual variance with the usual empirical

\[ \text{variance estimator} \]

But the benefit of the difference estimators is that they have lower variance than the differences of the individual estimators (see Table 7).

\[ \text{flc} - \text{wfb} \]

\[ \text{fluidic} \]

\[ \text{no wiping} \]

\[ \text{wfb} - \text{now} \]

\[ \text{flc} - \text{now} \]

\[ \text{flc} - \text{wfb} \]

\[ \text{wfb} - \text{now} \]

4.3.4 Estimator of Variances

For test drivers who passed at least two scenes it is possible to estimate the individual variance with the usual empirical variance estimator. Taking the mean over all test drivers yields an estimator \( \sigma_{\text{ind}}^2 \) for \( \sigma^2 \). Assuming that the number of passed tests is independent of the individual variance and neglecting the kurtosis of the individual brake time distributions, it would be optimal to weight the individual estimators by \( r - 1 \) where \( r \) is the number of passed tests of the test driver. This assumption might not hold exactly in this setting but using this weighted mean should still be beneficial and yield a better estimator as the unweighted sum. On the other hand calculating the empirical variance by scene and taking their mean yields an estimator \( s^2 \) for \( \sigma^2 \). Their difference is an estimator \( s_{\text{ind}}^2 \) for \( \sigma^2 \). Together, the variance of the estimators in Table 6 is obtained accordant to equation (2) by

\[ s_{\text{m}} = \frac{1}{k} \left( s_{\text{ind}}^2 + s_{\mu}^2 \right). \]

The results for the estimators are given in Table 7.

The variances of the mean estimators in the detection task are much lower than the variances of the estimators in the recognition task since each test driver performed six detection tasks but only three recognition tasks.

Confidence intervals can be constructed with the estimators of Table 7 using the quantiles of the standard normal distribution. This is legitimate as the mean reaction times are nearly normally distributed as they consist of the sum of around 200 independently distributed individual reaction times and the assumption was verified by bootstrapping \(^{60}\) from the data.

The one-sided 95% confidence interval on the lower bound for the true reaction time difference between fluidic and wet flatblade can be calculated as \( m - z_{0.95} s_{m} = 315 \text{ ms} - 1.645 \times 18.0 \text{ ms} = 285 \text{ ms} \) for the detection task and \( 278 \text{ ms} - 1.645 \times 26.6 \text{ ms} = 234 \text{ ms} \) for the recognition task. Other confidence intervals can be concluded analogously.

Table 6 Mean estimators for the different systems and tasks

| Mean Estimators       | Detection Task | Recognition Task |
|-----------------------|----------------|------------------|
| no wiping (now)       | 809 ms         | 943 ms           |
| wet flatblade (wfb)   | 1042 ms        | 1038 ms          |
| fluidic (flc)         | 1319 ms        | 1311 ms          |
| flc – wfb             | 315 ms         | 278 ms           |
| wfb – now             | 245 ms         | 49 ms            |
| flc – now             | 519 ms         | 371 ms           |

Table 7 Variance estimators for the different systems and paired differences. \( s_{\text{ind}}^2 \) estimates the mean variance of reaction times of a randomly chosen (but fixed) test driver. \( s_{\mu}^2 \) estimates the variance of the expected reaction times across different test drivers. \( s^2 \) estimates the overall variance of random reaction time of a random test driver. \( s_{\text{m}}^2 \) estimates the variances of the mean estimators given in Table 6.

| Recognition        | Detection | s     | \( s_{\text{ind}} \) | \( s_{\mu} \) | \( s_{m} \) |
|--------------------|-----------|-------|---------------------|-------------|-----------|
| no wiping          | 384 ms    | 264 ms| 279 ms              | 8.1 ms      |
| wet flatblade      | 421 ms    | 295 ms| 301 ms              | 9.6 ms      |
| fluidic            | 549 ms    | 415 ms| 359 ms              | 13.4 ms     |
| flc – wfb          | 550 ms    | 502 ms| 225 ms              | 18.0 ms     |
| wfb – now          | 455 ms    | 399 ms| 217 ms              | 13.7 ms     |
| flc – now          | 561 ms    | 472 ms| 303 ms              | 16.4 ms     |

Table 7 Variance estimators for the different systems and paired differences. \( s_{\text{ind}}^2 \) estimates the mean variance of reaction times of a randomly chosen (but fixed) test driver. \( s_{\mu}^2 \) estimates the variance of the expected reaction times across different test drivers. \( s^2 \) estimates the overall variance of random reaction time of a random test driver. \( s_{\text{m}}^2 \) estimates the variances of the mean estimators given in Table 6.

| Recognition        | s     | \( s_{\text{ind}} \) | \( s_{\mu} \) | \( s_{m} \) |
|--------------------|-------|---------------------|-------------|-----------|
| no wiping          | 267 ms| 185 ms              | 193 ms      | 15.9 ms   |
| wet flatblade      | 380 ms| 241 ms              | 294 ms      | 23.5 ms   |
| fluidic            | 512 ms| 353 ms              | 371 ms      | 31.0 ms   |
| flc – wfb          | 475 ms| 425 ms              | 213 ms      | 26.6 ms   |
| wfb – now          | 326 ms| 272 ms              | 180 ms      | 18.7 ms   |
| flc – now          | 472 ms| 409 ms              | 235 ms      | 26.4 ms   |

4.4. Safety assessment

As a result of our study we can state a significant advantage of wet flatblade over fluidic nozzles, both in terms of objective perception performance and subjective assessment by the test drivers. A detailed statistical analysis confirmed that with a confidence level of 95%, the gain in recognition time is 234 milliseconds or better. The average gain was 315 milliseconds for pedestrian detection and 270 milliseconds for the recognition of critical traffic situations.

A rough estimate shows the safety relevance of the results. Assuming 15,000 km per year at an average speed of 80 km/h makes 11,250 minutes on the road a year. Using 4 fillings of a washing liquid reservoir of 4 liters at a pump flow of 2 liters per minute makes 8 minutes of windshield washing time in a year. Based on these assumption, windshield cleaning is effectuated 0.07% of the time on the road.

Assuming an annual 68,000 road fatalities in the G7 countries \(^{39}\) lead to the assumption that, statistically, the reaction time gain due to the wet flatblade technology could have improved the chances of 68,000 + 0.07% ≈ 48 people that were killed in an accident that occurred during or shortly after windshield washing, by reducing the reaction time by up to 315 ms.

5. Conclusion

We propose a new methodology to assess windshield systems that complements existing regulations. The assessment is based on driver reaction times which makes it possible to
determine the impact of windshield washing technologies upon road safety. For illustration, we applied the methodology by conducting comprehensive with 204 individuals who form a representative sample for the holders of a German driver’s license. Both objective and subjective evaluations demonstrate that new washing systems, such as wet flatblade, can offer additional safety to drivers and pedestrians and provide more comfort to drivers.

6. Ethics Declaration

Our research and its results were accepted by an Ethics Review Board (Betriebsrat of the Fraunhofer IOSB). Our research results were obtained through informed consent and the contents have ethical validity.

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