Fundamental Understanding of the Di-Air System: The Role of Ceria in NO\textsubscript{x} Abatement

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Abstract Temporal analysis of product (TAP) is used to investigate the effectiveness of CO, C\textsubscript{3}H\textsubscript{6}, and C\textsubscript{3}H\textsubscript{8} in the reduction of a La–Zr doped ceria catalyst and NO reduction into N\textsubscript{2} over this pre-reduced catalyst. Hydrocarbons are found to be substantially more effective in the reduction of this catalyst at high temperature (above 500 °C) as compared to CO. NO decomposes over oxygen anion defects created upon catalyst reduction. Deposited carbon, in case the catalyst is reduced by C\textsubscript{3}H\textsubscript{6} or C\textsubscript{3}H\textsubscript{8}, acts as a delayed or stored reductant and is not directly involved in NO reduction. Instead the oxidation of deposited carbon by an oxygen species derived from lattice oxygen (re)creates the oxygen anion defects active in NO reduction. In situ Raman, in which NO is flown over C\textsubscript{3}H\textsubscript{6} pre-reduced La–Zr doped ceria at 560 °C, additionally shows that re-oxidation of the La–Zr doped ceria catalyst starts prior to the oxidation of deposited carbon, which confirms our TAP findings that firstly NO re-oxidized the La–Zr doped ceria catalyst and that secondly the oxidation of deposited carbon only commences at a higher ceria oxidation state. These findings create a new perspective on the operating principle of Toyota’s Di-Air system.

Keywords NO reduction · Di-air · Ceria · TAP · Hydrocarbon oxidation

1 Introduction

Customer demand and legislation, e.g., the introduction of mandatory CO\textsubscript{2} emission targets of 95 g/km by the year 2020 in the EU for the complete model range of car manufacturers, drives the development of more fuel efficient cars. Introduction of the current Euro 6 emission standard has seen the development of highly efficient lean-burn turbo-charged gasoline engines and catalytic deNO\textsubscript{x} systems (Urea-Selective Catalytic reduction (SCR) and Lean NO\textsubscript{x} Traps (NSR)) for the diesel engines. Euro 7 is anticipated to involve a further reduction of the NO\textsubscript{x} emissions to 0.04 g/km, while particulate matter emissions remain at 0.005 g/km. In addition, the more realistic Worldwide Harmonized Light Vehicles Test Procedures (WLTP) is expected to replace the outdated and non-realistic New European Driving Cycle (NEDC).

The composition of diesel engine exhaust gas is approximately 200 ppm NO, 5 % CO\textsubscript{2}, 5 % O\textsubscript{2}, 4 % H\textsubscript{2}O. To meet the future Euro 7, it is anticipated that this small concentration of NO has to be further reduced to 10 ppm in the competing presence of O\textsubscript{2}, CO\textsubscript{2}, and H\textsubscript{2}O. To meet the Euro 7 standard new technologies may be required. The three-way catalyst (TWC) works efficiently under stoichiometric conditions and loses its activity in the presence of oxygen. Urea-SCR has a complex dosing system and might be too voluminous to fit into most of the small passenger diesel cars. The NSR still needs further improvement to achieve high NO\textsubscript{x} conversion at higher temperatures and space velocity. Recently, Bisaiji et al. (Toyota Company) developed the Di-Air system in which short fuel rich and long fuel lean periods are created by a direct injection of fuel into the exhaust upstream of a NSR catalyst (Pt/Rh/Ba/K/Ce/Al\textsubscript{2}O\textsubscript{3}) \cite{1,2}. By using the same amount of fuel the optimal NO\textsubscript{x} reduction was achieved.
when large fuel injection pulses were used as compared to small fuel injection pulses and/or post injection directly into the engine. The Di-Air system can retain high NO\textsubscript{x} conversion (above 80 %) up to 800 °C and, therefore, could be a promising technology to meet the future NO\textsubscript{x} emission standards under realistic driving test conditions. The unique performance of this system is ascribed to the formation of stable isocyanate and isocyanide intermediates on the catalyst surface evidenced by FTIR observations at 250 °C [2, 3]. How this system can achieve this performance remains largely unresolved. In order to further develop and optimize this system, we started a detailed investigation into the operating principle of the Di-Air system. Initially we will primarily use the TAP technique (a vacuum pulse-response technique) [4] to investigate what the role of each Di-Air catalyst component.

Ceria is well-known as an important ingredient in automotive soot filters [5, 6] due to ceria’s ability to rapid and reversibly change oxidation state: Ce\textsuperscript{4+} + e\textsuperscript{-} ↔ Ce\textsuperscript{3+} + ⬜ (⬜ represents an oxygen anion vacancy). Depending on the oxidative or reductive nature of the atmosphere, it acts as an oxygen buffer, but in principle also as an oxidiser or reductant. A lot of fundamental reports on soot oxidation by using ceria base catalyst, although the origination of the active oxygen species for soot oxidation remains controversy [7, 8].

To study the role of the ceria component in Di-Air system we selected a commercial La–Zr doped ceria catalyst for its thermal stability [9]. Surprisingly, this catalyst turned out to be capable of performing all tasks required for an effective automotive emission reduction catalyst, fuel (HC hydrocarbon) oxidation, CO oxidation, and NO\textsubscript{x} reduction. Here, we present the results of the reduction–oxidation behaviour of the La–Zr doped ceria catalyst, using CO, C\textsubscript{3}H\textsubscript{6}, and C\textsubscript{3}H\textsubscript{8} in the absence of gas-phase oxygen and its re-oxidation by NO. The performed experiments provide a clear picture of the product evolution as a function of the oxidation state of the catalyst.

2 Experimental

The BET surface area of the catalyst is determined by N\textsubscript{2} adsorption using a Tristar II 3020 Micromeritics outgassing after 16 h outgassing at 200 °C. Inductive coupling plasma-optical emission spectrometer (ICP-OES, PerkinElmer Optima 5300) is applied to obtain the catalyst composition. The surface composition of the catalyst is measured by the X-ray photoelectron spectroscopy (XPS, K-alpha Thermo Fisher Scientific spectrometer). Powder X-ray diffraction (XRD) was recorded by using Bruker AXS D5005 with Co K\textalpha{} source. In-situ Raman spectra (Renishaw, 2000) were recorded using a temperature controlled in situ Raman cell (Linkam, THMS 600). Ten scans were collected for each spectrum in the 100–4000 cm\textsuperscript{-1} range using continues grating mode with a resolution of 4 cm\textsuperscript{-1} and scan time 10 s. The spectrometer was calibrated daily using a silicon standard with a strong band at 520 cm\textsuperscript{-1}.

The main technique used in the study is on a home-made advanced temporal analysis of products (TAP). TAP is a vacuum pulse-response technique. Reactant gas pulses are introduced to a small finite volume upstream of a packed catalyst bed. These introduced reactant molecules and eventually formed products upon interaction with the catalyst diffuse through the packed catalyst bed until they leave the packed bed, where they are recorded versus time (response) by a mass spectrometer. TAP experiments were performed using 21.2 mg of the La–Zr doped ceria (BASF) catalyst packed between two quartz particle beds in the temperature range 200–600 °C. In all experiments a starting pulse size of approximately 1.6 × 10\textsuperscript{15} molecules was used, the pulse size gradually decreases during an experiment as the reactant is pulsed from a constant calibrated volume. Prior to an NO (20 vol. % in Ar, internal standard) or \textsubscript{15}NO pulse experiment: (1) the catalyst was oxidized using an O\textsubscript{2} (20 vol% in Ar) pulse train; (2) a pre-reduction using either CO (80 vol% in Ar), C\textsubscript{3}H\textsubscript{6} (20 vol% in Ne) or C\textsubscript{3}H\textsubscript{8} (20 vol% in Ne) pulses was performed until the product distribution did not change.

The hypothetical ceria layers concept is introduced in order to obtain insight in the reactivity of the actual surface as a function of the degree of reduction (surface oxidation state). As the ceria (111) crystal plane is a stoichiometric O–Ce–O tri-layer stacked along the [111] direction, we regard each O–Ce–O tri-layer as one hypothetical ceria layer (0.316 nm). Assuming a perfect cubic crystal structure (size 5.0 nm), the total amount of hypothetical ceria layers was determined to be 16 (111) layers. The total number of hexagonal surface units (Fig. 1) on the (111) surface is calculated to be 3.6·10\textsuperscript{18} using the following equation:

\[N = \frac{s_{\text{BET}} \times W_{\text{sample}}}{s_{\text{hexagonal \ unit}}}\]

where the \(s_{\text{BET}}\) is 65 m\textsuperscript{2}/g, \(W_{\text{sample}}\) is 21.2 mg, \(s_{\text{hexagonal \ unit}}\) of the hexagonal surface unit is 0.38 nm\textsuperscript{2}.

The total amount of O in each crystal layer can be calculated to be 2.2·10\textsuperscript{19} using the following equation:

\[N_{\text{Total\,O}} = N \times n\]

where the \(n\) represents the number of oxygen atoms in one hexagonal unit. As shown in Fig. 1, the number of oxygen atoms one hexagonal unit is 6. Assuming that Zr and La are Ce, a maximum of 25 % of the number of O ions in each
crystal layer can be reduced, the amount of reducible oxygens in one hypothetical ceria layer is calculated to be $5.4 \times 10^{18}$.

3 Results and Discussion

3.1 Catalyst Characterization

The BET surface area of the La–Zr doped ceria is 65 m$^2$/g. The bulk composition of the La–Zr doped ceria sample is Ce$_{0.22}$Zr$_{0.07}$La$_{0.05}$O$_{0.66}$, as determined by inductively coupled plasma mass spectrometry (ICP). According to XPS, the surface ratio of Ce, Zr, and La is 170:92:1. Compared to the bulk composition the surface is enriched in Zr and there is hardly any La on the surface. XRD patterns (Fig. 2) shows the cubic structure, the crystal size is 5.0 nm based on the Scherrer equation:

$$D = \frac{K \lambda}{\beta \cos \theta}$$

where $\lambda$ is X-ray wavelength 0.1789 nm, $K$ is the particle shape factor 0.94, and $\beta$ is the full width at half height of the (111) peak.

3.2 Comparison of Reductant Activity Over the La–Zr Doped Ceria

In order to investigate the effectiveness of CO, C$_3$H$_6$, and C$_3$H$_8$ in the reduction of the La–Zr doped ceria catalyst, CO, C$_3$H$_6$, and C$_3$H$_8$ TAP pulse experiments were carried out, the obtained results are shown in the Figs. 3 and 4.

As shown in Fig. 3, until 0.4 reduced catalyst layers, CO is essentially completely converted to CO$_2$. After this period CO conversion and CO$_2$ production progressively decrease, but never reaching a zero level during the duration of the experiment. The total amount of consumed oxygen atoms during the whole CO pulse experiment at 580 °C is 6.3 $\times 10^{18}$, i.e., CO can only reduce the catalyst to approximately 1.2 layers. Below 200 °C, CO shows negligible activity in the reduction of ceria.

Figure 4a shows the result of a TAP single pulse experiment using C$_3$H$_6$ as a reductant over a pre-oxidized La–Zr doped ceria at 580 °C. In phase I, up to 0.25 reduced catalyst layers, a high activity is observed where predominantly total oxidation products, i.e., CO$_2$ and H$_2$O are formed. H$_2$ formation is observed from the start of the experiment, while CO production is initially zero. H$_2$ as well as CO production increases during this phase I. In phase II the C$_3$H$_6$ conversion rapidly declines. In phase III pre-dominantly partial oxidation takes place and CO and H$_2$ are observed. In phase II and III the C$_3$H$_6$ conversion is low with exponentially increasing H$_2$ and CO production, but in phase IV, corresponding to 1.5–2.7 reduced catalyst layers, the C$_3$H$_6$ conversion increases to full conversion. In
phase V, when the ceria is reduced to more than 2.5 layers, C₃H₆ conversion and H₂ production decline. H₂ production remains persistent even when no CO is observed to evolve. Some carbon (determined from the carbon mass balance) starts to deposit on the surface when CO evolution is observed (phase II). Large amounts of carbon deposition are observed when the CO formation declines while H₂ formation persists (phase IV). C₃H₆ can reduce the catalyst as far as 2.7 layers and deposits 3.1 × 10¹⁹ carbon atoms on the surface. Below 400 °C C₃H₆ shows negligible activity in ceria reduction and carbon deposition.

Figure 4b shows the result of a TAP single pulse experiment using C₃H₈ (model saturated hydrocarbon) as a reductant over pre-oxidized La–Zr doped ceria at 580 °C. In phase I, predominantly total oxidation products, i.e., CO₂ and H₂O are formed. H₂ formation is observed from the start of the experiment, while CO production is initially zero. H₂ as well as CO production increases during this phase I. C₃H₈ conversion declines in phase II and increases again during phase III. During phase II and III, partial oxidation takes place and CO, H₂ and C₃H₆ are observed. The C₃H₆ conversion over the whole experiment is substantially lower as compared to that of C₃H₆. In phase IV, when the ceria is reduced to more than 1.5 layers, C₃H₈ conversion and H₂ production decline. H₂ production remains persistent even when no CO is observed to evolve. Some carbon (carbon mass balance) starts to deposit on the surface, when CO evolution is observed (phase I). Large amounts of carbon deposition are observed when the CO formation declines while H₂ formation persists (phase IV). C₃H₈ can reduce the catalyst up to 2.5 layers and deposits 1.5 × 10¹⁹ carbon atoms on the surface. Below 500 °C C₃H₈ shows negligible activity in ceria reduction and carbon deposition. As compared to C₃H₆ and C₃H₆, CO has a higher catalyst reduction ability at lower temperatures, but it cannot compete with the reduction potential of hydrocarbons at temperatures above 500 °C.

3.3 NO Reduction Over the Pre-reduced La–Zr Doped Ceria by CO and Hydrocarbons

In order to investigate the roles of different reductants in the reduction of NO into N₂ over the La–Zr doped ceria catalyst, NO is pulsed over CO and C₃H₆ pre-reduced La–Zr doped ceria. Figure 5 displays the obtained results for the CO pre-reduced sample at 540 °C. Full NO conversion is obtained, while N₂ is the only product for 1.2–0.5 hypothetical reduced ceria layers. After that, NO conversion starts declining, accompanied by a parallel decrease in the N₂ production. The amount of oxygen atoms taken up by the catalyst during the NO pulse experiment is around 6.6 × 10¹⁸, which is similar to the total oxygen atom consumption during the CO pre-reduction at 540 °C. Initially
N accumulation (from the N mass balance) is observed and the initially accumulated N is released as N\textsubscript{2} later. Neither N\textsubscript{2}O nor NO\textsubscript{2} are observed during this NO titration.

Figure 6 shows the result of the TAP titration experiment with NO over C\textsubscript{3}H\textsubscript{6} pre-reduced La–Zr doped ceria at 540 °C. In phase I, corresponding to 1.9–0.5 reduced catalyst layers, the performance is roughly identical to the results obtained for the CO pre-reduced sample: oxygen is accumulated thereby re-oxidizing the catalyst. N\textsubscript{2} is the main observed product while CO or CO\textsubscript{2} are hardly formed. In phase II, the evolution of CO\textsubscript{2} is observed. This evolution of CO\textsubscript{2} is shortly followed by a decrease in the NO conversion. During phase III, NO conversion increases again. In phase IV, NO achieves full conversion, while only N\textsubscript{2} and CO\textsubscript{2} are observed, per 2 NO molecules approximately 1 N\textsubscript{2} and 1 CO\textsubscript{2} molecule are produced. In phase V a progressive decrease in the NO conversion is observed which ceases, when it approaches 0 %. The N\textsubscript{2} and CO\textsubscript{2} production follow the same trend as the NO conversion. The initial absence of oxidation products CO and CO\textsubscript{2} during the first NO pulses in phase I indicate that the carbonaceous residues left on the surface after C\textsubscript{3}H\textsubscript{6} pre-reduction do not directly participate in the reduction of NO into N\textsubscript{2}. CO\textsubscript{2} formation is observed until catalyst is re-oxidized to 0.5 reduced layers (phase II). The formation of CO\textsubscript{2} at this point suggests that at a specific catalyst oxidation state the catalyst becomes active for the oxidation of the deposited carbonaceous residues left behind during the C\textsubscript{3}H\textsubscript{6} pre-reduction. A temporary NO conversion decrease is observed around the same point of 0.5 reduced layers, the onset of this NO conversion decrease is caused by the depletion of oxygen anion defect sites. The formation of CO\textsubscript{2} proceeds the temporary NO conversion decline. The oxidation of carbonaceous deposits by an oxygen species derived from lattice oxygen to CO\textsubscript{2} (re)creates oxygen anion defect centers capable of NO dissociation into N\textsubscript{2}. Therefore, these carbonaceous deposits can be seen as a stored reductant with a delayed function. The presence of the carbonaceous deposits allow for a prolonged period of NO reduction as compared to the CO pre-reduced case. Neither N\textsubscript{2}O and NO\textsubscript{2} nor HCN (cyanides) and HNCO (cyanate) are observed during this NO titration.

As TAP is a vacuum technique, in situ Raman (at atmospheric pressure) is applied to confirm the results obtained from TAP. NO reduction is performed over C\textsubscript{3}H\textsubscript{6} pre-treated La–Zr doped ceria both at 560 °C and is shown in Fig. 7.

The band at 460 cm\textsuperscript{-1} is attributed to the symmetric stretch mode of Ce-O\textsubscript{8} crystal unit, which is characteristic for the reduced fluorite ceria structure [13]. This peak disappears during the C\textsubscript{3}H\textsubscript{6} pre-treatment, while under NO flow the increase in the intensity of the band at 460 cm\textsuperscript{-1} indicates that the pre-reduced La–Zr doped ceria catalyst is re-oxidised by NO. The bands at 1575 and 1350 cm\textsuperscript{-1} are assigned to G band and D band of carbon in the form of graphene or graphite. The G band is usually assigned to zone centre phonons of $E_{2g}$ symmetry of the perfect...
graphite structure and the D peak is a breathing mode of $A_{1g}$ symmetry, this mode is forbidden in a perfect graphite structure and only becomes active in the presence of structural defects and disorders [14]. The intensity of D band and G band of graphene/graphite remains constant during the first 270 min of NO/N$_2$ flow, this indicates that the oxidation of carbon commences much later than the re-oxidation of the ceria. This observation also points out that the oxidation of carbon is via an oxygen species derived from lattice oxygen and not by gas phase NO, this is in line with previous findings in the oxidation of soot on ceria based catalysts [5].

The inventors of the Di-Air system attribute the exceptional behavior of their catalyst to the formation of cyanate and cyanide type intermediates [2, 3]. In the current study, where the presence of hydrocarbons and NO is decoupled, we find similar exceptional behavior. At 580 °C, hydrocarbon pre-reduced La–Zr doped ceria (21 mg) outperforms CO pre-reduced La–Zr doped ceria by a factor of 13. The amount of extracted oxygen during C$_3$H$_6$ is 1.5·10$^{19}$ atoms and the deposited carbon additionally extracts 3.1·10$^{19}$ oxygen atoms, which is 13 times more as compared to the amount of extracted oxygen atoms during CO reduction. We find no evidence that hydrocarbon residues or carbonaceous residues play a direct role in NO conversion. These residues, however, allow for a delayed reduction action during lean conditions, where they recreate oxygen anion defects that are responsible for further NO decomposition into N$_2$.

### 3.4 Significance to the Di-Air system

Fuel is used to reduce ceria and, thereby, creating oxygen anion vacancies required for NO decomposition into N$_2$. When a fuel injection policy is applied which will keep the ceria in an partial reduction corresponding to the total reduction state between zero and 0.25 reduced layers, all the oxygen vacancies will be refilled rapidly by the oxidizing gases (NO, CO$_2$, O$_2$, and H$_2$O) during this fuel lean condition and there will be no benefit from the delayed reduction action of the deposited carbon. Therefore, a high frequency of fuel injections is required to create locally a rich hydrocarbon environment. When using this fuel injection policy that includes the partial oxidation period (0–2.5 reduced hypothetical ceria layers), the fuel decomposition activity is not only higher, also the carbonaceous deposits act as reductant reservoir and the reduction of the ceria is deeper (up to 2.5 reduction layer). When a fuel pulse has passed and the catalyst is exposed to lean conditions, this deeper reduction degree might be more selective for the NO ceria re-oxidation in competition with O$_2$ and the other milder oxidizers (CO$_2$ and H$_2$O) and once more these carbonaceous deposits keep re-creating lattice oxygen anion vacancies, on which NO can dissociate to form N$_2$. Our other work shows NO is able to reduce to N$_2$ in the presence of excess oxygen [15]. The observed phenomena can have a great impact on the fuel injection policy and the total fuel consumption due to these fuel injections.

### 4 Conclusion

The hydrocarbon activation activity of the La–Zr doped ceria is limited and requires high temperatures, especially when saturated hydrocarbons will be used. The addition of suitable dopants to the La–Zr doped ceria catalyst is recommended in order to improve its (saturated) hydrocarbon activation capability. Oxygen anion defect centers in the lattice of ceria are responsible for NO decomposition into N$_2$, while hydrocarbons deposit carbon species. The oxidation of these deposited carbon species by oxygen species from the lattice can maintain a reduced surface state of the ceria during actual operation under lean conditions, thereby extending the effectiveness of the hydrocarbon injections.

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