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A Sub-Threshold Differential CMOS Schmitt Trigger with Adjustable Hysteresis Based on Body Bias Technique

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Received: 8 April 2020; Accepted: 10 May 2020; Published: 14 May 2020

Abstract: This paper presents a sub-threshold differential CMOS Schmitt trigger with tunable hysteresis, which can be used to enhance the noise immunity of low-power electronic systems. By exploiting the body bias technique to the positive feedback transistors, the hysteresis of the proposed Schmitt trigger is generated, and it can be adjusted by the applied bias voltage to the bulk terminal of the utilized PMOS transistors. The principle of operation and the main formulas of the proposed circuit are discussed. The circuit is designed in a 0.18-µm standard CMOS process with a 0.6 V power supply. Post-layout simulation results show that the hysteresis width of the Schmitt trigger can be adjusted from 45.5 mV to 162 mV where the ratio of the hysteresis width variation to supply voltage is 19.4%. This circuit consumes 10.52 × 7.91 µm² of silicon area, and its power consumption is only 1.38 µW, which makes it a suitable candidate for low-power applications such as portable electronic, biomedical, and bio-implantable systems.

Keywords: differential Schmitt trigger; low voltage; sub-threshold; low power; body bias technique; positive feedback

1. Introduction

As the electronics world is heading toward the future, electronic devices require longer lifetime batteries. Hence, the IC designers are obliged to make use of some design techniques to provide a prolonged battery life. One of the common techniques is reducing the supply voltage to decrease the power consumption of the circuits by operating transistors in the weak inversion region. At low voltage, one of the main constraints faced is the device noise level. The weak inversion region is also known as the sub-threshold region because it occurs under the threshold voltage of transistors where very small currents can be provided. The current-voltage equation in this region is an exponential relationship, and although for a given power budget, the \( g_m/I_D \) ratio is at its maximum level; since the values of currents are so small, the circuit may become sensitive to noise [1,2]. Moreover, circuits which operate in the sub-threshold region face some limitations such as poor frequency response and poor linearity [2]. Thus, in general, these circuits are meant for low-frequency and low-current applications such as biomedical and biotelemetry devices and are not suitable for medium power applications [3,4].

A valuable solution to improve the robustness of the circuits to noise is using Schmitt triggers. Schmitt triggers can improve the sensitivity of electronic systems to electromagnetic interferences, i.e., they increase the static noise margin of the circuits but at the cost of more power consumption.
and delay [5,6]. Accordingly, in general, it is expected that the circuits based on Schmitt triggers operate more reliably in terms of noise immunity [7]. The Schmitt trigger is a bi-stable circuit that is utilized in both analog and digital signal processing systems [8]. The reason for the popularity of this circuit is its hysteresis characteristic or its ability to work in two different threshold levels, which enables the Schmitt trigger to suppress noise in various analog and digital circuits [9]. Indeed, the Schmitt trigger is a restoring signal circuit [10], which eliminates noise content from the input signal and extracts the original input signal information. The positive feedback that causes the circuit loop gain to be more than one is the most popular scheme in creating distinct threshold levels to provide the hysteresis characteristic. The feature that equips the Schmitt trigger with analog to digital conversion and therefore reshapes the pulses can be implemented by either internal or external positive feedback. The positive feedback can be controlled internally or externally according to the intended application and noise tolerance [11,12]. It is worth noting that since different threshold levels can cause different outputs, the hysteresis characteristic might not be desirable in some applications, such as ADC converters [13].

Hysteresis of a Schmitt trigger is directly affected by process variations and transistor mismatches. This issue is more problematic in applications where the level of noise and disturbances is not predictable [8]. To overcome this deficiency, Schmitt triggers with tunable hysteresis can be used as a helpful solution. Besides, the possibility of controlling the hysteresis levels in some applications such as power amplifier circuits [14] leads to lower power consumption and improves the overall performance of the circuit [15].

Generally, traditional single-output Schmitt triggers used to be realized by operational amplifiers and passive components, which had some significant defects such as high-power consumption, limited-gain bandwidth product, low-slew rate, and low-dynamic range. After Allstot, who designed a Schmitt trigger for wireless applications [16], implementing differential Schmitt triggers became widely common. Nowadays, Schmitt triggers, which can convert any periodic signal to its stable logic one, are the fundamental block frequently used in the areas of communication and measurement systems to generate basic waveforms such as square, triangular, pulse, and so on [17–19]. Furthermore, relaxation oscillators [20], function generators [21], mono-stable multi-vibrators [22], pulse width modulators [23], and switching power supplies [24] are the other several applications of Schmitt trigger circuits in the emerging areas of signal processing.

In this paper, a differential Schmitt trigger with adjustable hysteresis and transistors that are biased in the sub-threshold region is proposed. Hysteresis of this circuit is created by positive feedback and can be controlled by the body bias technique. In a body driven transistor, the input signal is applied to the bulk terminal to create conduction between the source and drain. Despite the smaller transconductance and bandwidth, this will enhance the application of fundamental analog building blocks in low-voltage environments [2]. In the presented work, by applying the body bias technique to the positive feedback transistors, no additional element is required to equip the circuit with hysteresis control capability. Basically, MOSFETs using the body bias technique are required to have isolated bulk terminals [2], which cause some percent of a larger active area. However, the proposed circuit structure helps to have a Schmitt trigger with fewer transistors and a smaller occupied chip area compared to the recently proposed topologies, which make it suitable for bio-implantable circuits. This paper is organized as follows: The proposed Schmitt trigger is described in Section 2; Section 3 presents the simulation results; finally, the paper is concluded in Section 4.

2. Proposed Schmitt Trigger Circuit Description

2.1. Differential Pair of the Circuit

The differential pair of the proposed low-voltage, low-power Schmitt trigger with tunable hysteresis is illustrated in Figure 1. Transistors of M_{1a} and M_{1b} are the differential inputs, and M_t is a controlled current source that provides the tail current of the differential pair by a bias voltage of V_{B1}. M_{2a} and M_{2b} implement positive feedback to create the hysteresis of the proposed Schmitt trigger.
Due to the tail current, when the DC voltage of the positive input, $V_{in}^+$, increases from 0 to positive voltages while $V_{in}^-$ is fixed at a mid-point (reference voltage), $I_{1a}$ will be increased, and inversely, $I_{1b}$ will be decreased, which are the drain currents of transistors $M_{1a}$ and $M_{1b}$, respectively. Thus, based on the differential behavior of the circuit, the drain voltage of $M_{1a}$ decreases and the drain voltage of $M_{1b}$ increases, and $V_{d-1a}$ switches from high to low in $V_2$. The DC transfer characteristics of $V_{d-1a}$ are shown in Figure 2 (gray curve).

It should be noted that because of $M_{3a}$, which is a voltage-controlled current source and provides a fixed current, an increase in $I_{1a}$ will increase the drain current of $M_{2a}$, i.e., $I_{2a}$. On the other hand, when $I_{1b}$ decreases, $I_{2b}$ reduces as well under the same circumstance. However, the reduction of $V_{d-1a}$ will force $I_{2b}$ to increase and retain its former situation. Therefore, $I_{1b}$ and accordingly $V_{d-1b}$ will not change either. Hence, $I_{2a}$ will also retain its former situation, and $I_{1a}$ and $V_{d-1a}$ will remain unchanged as well. This situation will continue until the difference between $V_{in}^+$ and $V_{in}^-$ becomes so large that $I_{1a}$ overcomes $I_{2a}$ and the state changes. At this point, $V_{d-1a}$ will change; its position is denoted as $V_3$ in Figure 2. In contrast, when $V_{in}^+$ becomes significantly smaller than $V_{in}^-$, the output current will change its state at the voltage of $V_1$, which is shown in the figure. This voltage shift from $V_2$ is caused by the positive feedback transistors; $M_{2a}$ and $M_{2b}$. In the absence of these transistors, the circuit will operate as a comparator. It is perceivable that the proposed Schmitt trigger operates at a current mode, and its operation analysis is described in the following.

![Figure 1. The differential pair of the proposed Schmitt trigger.](image1)

![Figure 2. Qualitative hysteresis characteristic of an inverting Schmitt trigger.](image2)

According to Figure 1, using KCL at the drain node of the positive input transistor $M_{1a}$ results in:

$$I_{1a} = I_{3a} + I_{2a}, \quad (1)$$

The drain current equation in the sub-threshold region has an exponential relationship and for a NMOS transistor equals to $I_d = I_0 \frac{W}{L} e^{\frac{V_{ds}}{V_{th}}} (1 - e^{-\frac{V_{th}}{V_{th}}})$ where $I_0 = \mu_c C_{ox} (n - 1) V_t^2 e^{-\frac{V_{th}}{V_{th}}}$. Then, $I_d$ can be
approximated as 

\[ I_d = I_0 \frac{W}{L} e^{\frac{V_{gs,1a} - V_{th,1a}}{nV_t}} \]

where \( n \) and \( V_t \) are sub-threshold coefficient and thermal voltage, respectively. Consequently, Equation (1) can be written as:

\[ I_{0,1a} \left( \frac{W}{L} \right) e^{\frac{V_{gs,1a} - V_{th,1a}}{nV_t}} = I_{3a} + I_{0,2a} \left( \frac{W}{L} \right) e^{\frac{V_{gs,2a} - V_{th,2a}}{nV_t}}, \]  

(2)

If we repeat the same path for the drain node of the negative input transistor \( M_{1b} \) and subtract \( V_{gs,1b} \) from \( V_{gs,1a} \), the voltage difference of input terminals becomes:

\[ \Delta V_{in} = (V_{gs,2a} - V_{gs,2b}) + (V_{th,2b} - V_{th,2a}). \]  

(3)

2.2. Two-Stage Schmitt Trigger Circuit

In Figure 2, voltage levels of \( V_1 \) and \( V_3 \) are LTP and UTP of the Schmitt trigger, respectively. As can be seen, the hysteresis curve will not reach to logical zero or one, which is because of the low gain of the circuit. To solve this problem, an output stage is added to the structure illustrated in Figure 3. After amplifying the signal by the second stage, the hysteresis characteristic will be consistent with Figure 4. In other words, immediately after \( V_{d-1a} \)’s decrease, the drain current of \( M_{4a} \) will also reduce. Then, because of the current mirror of \( M_{5a,b} \) and higher current of \( M_{4b} \), \( I_{out} \) will approach zero and a sharper transition will occur, as depicted in Figure 4.

![Figure 3](image1.png)

**Figure 3.** The proposed two-stage Schmitt trigger.

![Figure 4](image2.png)

**Figure 4.** Qualitative hysteresis characteristic of the two-stage Schmitt trigger.

A KVL from \( V_{dd} \) to the source terminal of \( M_{4b} \) will result in \( V_{gs,2a} = -V_{dd} + V_{gs,4b} \). Afterward, we can write:
where \( \gamma \) and \( \phi \) are the body-effect coefficient and surface potential, respectively. Equation (7) declares that by variation of \( V_{c1} \) and \( V_{c2} \) (bulk terminals of \( M_{2a,b} \)), hysteresis width can be tuned. It should be noted that \( V_c \) must be smaller than \( |2\phi| + V_{dd} \). Since the proposed circuit has a 0.6 V supply voltage, the value of \( V_c \) cannot exceed \( |2\phi| + 0.6 \) mathematically. To avoid leakage current, it is important to consider that \( V_c \) cannot be smaller than the supply voltage, and the corresponding voltage levels must be chosen optimally.

Figure 5. The proposed Schmitt trigger with adjustable hysteresis.
3. Post-Layout Simulation Results

The proposed sub-threshold differential Schmitt trigger with tunable hysteresis is designed and post-layout simulated in a standard 0.18 μm CMOS technology. The utilized technology allows bulk and body contacts to be different in the wafer fabrication process. Power consumption of the circuit is 1.38 μW, which makes it suitable for biomedical applications. The layout of the proposed Schmitt trigger is shown in Figure 6, which occupies the chip area of 10.52 × 7.91 μm². The aspect ratios of transistors are set according to Table 1.

| Transistor | W/L         |
|------------|-------------|
| M₁a,b      | 0.44 μm/0.18 μm |
| M₂a,b      | 0.88 μm/0.18 μm  |
| M₃a,b      | 0.44 μm/0.18 μm  |
| M₄a,b      | 0.44 μm/0.18 μm  |
| M₅a,b      | 0.88 μm/0.18 μm  |
| M₆        | 0.44 μm/0.18 μm  |

The DC voltage transfer characteristic of the proposed Schmitt trigger is shown in Figure 7 where \( V_{in}^+ \) is initially swept from 0 to 0.6 V and then from 0.6 V to 0 to observe the hysteresis curve, while \( V_{in}^- \) is fixed at 0.3 V. The UTP and LTP of the circuit are 380.1 mV and 254.1 mV, respectively, so the hysteresis width is 126 mV. A triangular waveform with the amplitude of 0.6 V and 500 kHz frequency is applied to \( V_{in}^+ \), and its corresponding transient output is illustrated in Figure 8.

Figure 9 shows the hysteresis characteristic of the proposed Schmitt trigger while \( V_{c1} \) is swept from 0.3 V to 0.6 V. It is clear that the hysteresis width can be varied in proportion to the bias voltage applied to the bulk terminal of the positive feedback transistors \( M_{2a} \) and \( M_{2b} \). Moreover, the variation of the transient response of the circuit according to the changes of the body bias voltage, i.e., \( V_{c1} \), is depicted in Figure 10. The voltage transfer characteristic of the proposed Schmitt trigger over different process corners at 27 °C is shown in Figure 11. Variations of the hysteresis width and the center of the circuit in three process corners over temperatures from −20 °C to 60 °C is simulated, and the result is illustrated in Figure 12a,b, respectively.

![Figure 6. The layout of the proposed Schmitt trigger in 0.18 μm CMOS technology.](image-url)
Figure 7. Voltage transfer characteristics of the proposed Schmitt trigger. $V_{in}^+$ is swept from 0 to 0.6 V and vice versa, while $V_{in}^-$ is set to 0.3 V, and $V_{B1}$ and $V_{B2}$ are 0.35 V and 0.3 V, respectively.

Figure 8. Time-domain response of the designed Schmitt trigger circuit to 500 kHz triangular input signal.

Figure 9. Dependence of the threshold voltages on the $V_{c1}$ variation. $V_{in}^+$ is swept from 0 to 0.6 V and vice versa, while $V_{in}^-$ is set to 0.3 V.
Figure 10. Variation of the time-domain response of the proposed circuit by changes of $V_{c1}$.

Figure 11. Variation of the hysteresis width in different process corners at 27 degrees Celsius.

Figure 13 shows the variation of the hysteresis width and its center versus the reference voltage for a constant value of control voltage. In addition to the hysteresis width variation of the circuit by changing $V_{c1}$, the width and the center of its hysteresis vary through sweeping $V_{in}^-$ from 250 mV to 450 mV. Figure 14 provides a more comprehensive review of the dependency of the hysteresis width on the control voltage and the reference voltage. It shows that by sweeping $V_{c1}$ from 400 mV to 600 mV and simultaneously changing $V_{in}^-$ from 250 mV to 350 mV, hysteresis width changes in a range of 116 mV.

To examine the effect of process variations and component mismatches on the transient response of the proposed Schmitt trigger, 100 runs of Monte Carlo analysis are performed for all employed transistors. Figure 15 shows the transient responses of input and output voltages for post-layout simulation of Monte Carlo analysis. Finally, in Figure 16a,b, post-layout simulated histograms for 100 runs of Monte Carlo for LTP and UTP of the circuit are presented. As can be seen, the majority of the iterations for LTP and UTP fit in about 254 mV ± 11% and 380 mV ± 15%, respectively. Moreover, the proposed circuit was simulated with ±10% variation in power supply, for which proper operation was observed (Figure 17).

Table 2 illustrates the comparison of the proposed and the recent CMOS Schmitt triggers which have almost common properties. The comparison is mainly considered in terms of supply voltage, single or differential input, voltage or current mode, static power consumption, occupied chip area, and hysteresis width. The proposed current mode CMOS Schmitt trigger operates at a voltage supply
of 0.6 V and its transistors are biased in the sub-threshold region. Therefore, this circuit has significantly lower power consumption and a smaller occupied chip area, which make it suitable for low-voltage and low-power applications.

Table 2. Performance comparison of Schmitt triggers.

|                      | This Work | [15] | [25] | [26] | [27] | [28] | [29] | [30] |
|----------------------|-----------|------|------|------|------|------|------|------|
| Technology           | 0.18 µm   | 0.18 µm | 0.18 µm | 0.18 µm | 0.18 µm | 0.18 µm | 40 nm | 0.18 µm |
| Power Supply         | 0.6 V     | 1.8 V | 0.8 V | 0.6 V | 0.4 V | 0.15 V | 1 V  | 0.4 V |
| Single/Differential Input | Diff. | Diff. | Diff. | Single | Diff. | Single | Single | Pseudo Diff. |
| V/I Mode             | Current Mode (I) | Current Mode (I) | Current Mode (I) | Voltage Mode (V) | Current Mode (I) | Current Mode (I) | Voltage Mode (V) | Current Mode (I) |
| Variable/Fixed Hysteresis | Variable | Variable | Variable | Fixed | Fixed | Fixed | Variable | Fixed |
| Wc 1/V2             | 19.4%     | 6.66% | 12.5% | 0     | 0     | 0     | 2.8% | 0     |
| Power Consumption    | 1.38 µW   | -     | 0.48–1.12 mW | 2.64 mW | -     | -     | -    | 150 nW |
| Chip Area            | (10.52 × 7.91 ¬1)/2 | - | (39 × 17.5 ¬1)/2 | - | (20.37 × 10.41 ¬1)/2 | - | (14.8 × 7 ¬1)/2 |
| No. of Transistors   | 11 + bias | 13    | 16 + bias | 9    | 14 + bias | 6    | 6    | 10 + bias |
| Simulation/Measurement | Post-layout Sim. | Sim. | Post-layout Sim. | Meas. | Sim. | Meas. | Sim. | Post-layout Sim. |

1 Wc: Hysteresis width variation.

Figure 12. Variation of hysteresis (a) width and (b) center of the proposed Schmitt trigger from −20 to 60 degrees Celsius in different process corners.

Figure 13. Variation of the hysteresis width and its center versus reference voltage of $V_{in}$ while $V_{C1}$ is set to 300 mV.
Figure 13. Variation of the hysteresis width and its center versus reference voltage of $V_{in^-}$ while $V_{C1}$ is set to 300 mV.

Figure 14. Dependence of the hysteresis width on the control voltage ($V_{C1}$) and the reference voltage ($V_{in^-}$).

Figure 15. Post-layout simulation for 100 runs of Monte Carlo on the transient response of the input and output voltages.

Figure 16. Post-layout simulated histogram for 100 runs of Monte Carlo for (a) LTP and (b) UTP.
Author Contributions: Conceptualization and design, S.R. and A.N.; formal analysis, A.N. and S.R.; software, A.N. and S.R.; investigation, M.H.M. and Y.B.; writing—original draft preparation, S.R.; writing—review and editing, M.N. and S.H.-H.; supervision, P.A. and M.H.M.; funding acquisition, S.H.-H. and M.N. All authors have read and agreed to the published version of the manuscript.

Conflicts of Interest: The authors declare no conflict of interest.

Funding: This research received no external funding.

Conflicts of Interest: The authors declare no conflict of interest.

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