Application of Cauchy (Lipschitz) Criterion for Obtaining Theoretical Models of Atmosphere Striking Overvoltages

Slobodan N. Bjelić
Faculty of Technical Sciences, Kosovska Mitrovica, Serbia
E-mail: slobodanbjelic49@yahoo.com

Nenad A. Marković
Higher Technical School of Professional Studies Urosevac, in Leposavic, Serbia
E-mail: nen.mark74@yahoo.com

Zorica S. Bogićević
Higher Technical Professional School, Zvecan, Serbia
E-mail: zocabogi@gmail.com

Igor S. Bjelić
The National Archaeological Institute of Serbia, Belgrade, Serbia
E-mail: igor_bjelic@yahoo.com

Received: 25 May 2019; Accepted: 14 June 2019; Published: 08 September 2019

Abstract—In investigation of consequences of atmosphere and commutating striking voltages, for simulation of the overvoltage are used the models of generators whose RC circuits have standard passive parameters of the elements upon which the form of striking overvoltage depends.

According to IEC 62 305-1 standard, these formulas in the theoretical model serve for dimensioning the RC circuit of the generator of striking voltages although the definitions of time constants and passive parameters have only axiomatic character. Related to classical solution, this paper presents the model formed by mathematical procedure the solutions of which give sufficiently accurate values of time constants and essential parameters of RC circuit as well as the shape of striking voltage wave. The formulas for voltages and currents in model contain parameters of passive elements, and their accuracy has been confirmed by diagrams obtained in simulation by means of adapted psbtrnsrg.mdl part of MATLAB program. Theoretical model is suitable for simulation of standard wave forms of striking atmospheric and commutating overvoltages which replace laboratory testing.

Index Terms—Atmospheric voltage, Cauchy (Lipschitz) criterion, RC generator, Simulation, Theoretical model.

I. INTRODUCTION

There is no universal method for calculation of transient processes of switching and atmospheric overvoltages. Approximate solutions can be obtained by applying methods from the theory of electrical circuits, that is method of projection of one modification (Finite Element Method-FEM, of Ric, Galerkin [1]). The method in based on testing approximations of solutions of differential equations in order to determine “projection”, that is an approximate solution defined in spatial and time domain. The striking voltages which are many times higher than the values of drive voltages are short-time high voltages occurring due to atmospheric influence (external) or to commutations in electricity networks (internal) [2,3].

This paper presents the model formed by mathematical procedure the solutions of which give sufficiently accurate values and shape of striking voltage wave.

The paper has been organized in the following manner: Section 2 gives a review of the literature of related works in the field of atmosphere and commutating striking voltages. Section 3 gives amounts and forms of overvoltage as well as classical solution and correction of the classical solutions according to Cauchy-Lipschitz criterion. In Section 4 equations are derived for voltages and currents in RC circuit of striking voltage generator with sparking, depending upon the number of elements and their structure. Approximate solution of the form of striking voltage wave is given in Section 5. Section 6 shows the results of simulation and discussion of the model suggested for obtaining transient overvoltages. Finally, section 7 gives some concluding considerations.
II. RELATED WORKS

Testing the effects of shock voltages is not a new phenomenon. Many studies have been conducted on this subject and a number of papers have dealt with this issue [2,4].

Wilson [5] claims that the amount of electricity in storm clouds is \((10-50)\text{C},\) while intensity \(E = -\text{grad}\phi\) rapidly decreases in the zone of maximum potential gradient.

The claim is also that the leader comprises less than 2 km of active zone.

Simpson, [6] claims to have measured intensities of fields close to the ground of 200 kV/m and that the voltages before the lightning flash were \(V = 10^6 \text{kV}\). Majority of the energy was spent on ionization of the path of movement of the leader. Potentials of the body at strokes of atmospheric discharges are \(V \approx (1-10)\text{MV}\), but polarity of the voltage is disputable. The currents between the cloud and the Earth were measured to be at the value of \(I \approx 150\text{kA}\).

Simpson [6] also considers “the positive discharges” to be 1-10 times more frequent than negative; the authors of USA detect higher number of occurrence of negative discharges. Contradiction is apparent since negative strokes reach the Earth at one point through the leader; therefore they are stronger than positive strokes whose path to the ground goes through streamers which transfer only a part of the charge. Model of the process is \(LC\) circuit, and time of the process and aperiodic character determine parameter values. This theory is rejected because air can be more or less conductive if ions and electrons accidentally appear in it, and cloud is a perfect isolated ambient - \(H_2O\) molecules bind free ions from the surrounding atmosphere.

In the opinion of N. Marković et al. [7] the theory also did not explain the phenomenon of the path of leader tracer of ghost lightning depending upon some source of radiation in the universe. New investigations show that the lightning strikes at the points of geological discontinuity which are ionized due to action of radioactive masses.

III. FORMS OF OVERVOLTAGE, CHARACTERISTIC AMOUNTS AND CLASSICAL SOLUTIONS BY CAUCHY-LIPSCHITZ CRITERION

The amounts and form of atmospheric striking voltage are defined by IEC standard, Fig. 1.a,b,c [8,9,10,11]. Standard voltage value is described by the relation \(\tau_f / \tau_1 = T_1 / T_2 = 1.2/50\mu\text{s}\), duration time of the front \(T_1 = 1.2\mu\text{s}(\pm 30\%)\) and achieving \(1/2\) of amplitude value of the back for \(T_2 = 50\mu\text{s}(\pm 20\%)\). According to IEC standard [8] \(T_1\) is effective time of wavefront between two relative voltage values denoted by point \(A\) (30% amplitude) and point \(B\) (90% amplitude), Fig. 1.b, magnified 1.67 times, since duration time of the wavefront is by that amount longer than that corresponding to the voltages at points \(A\) and \(B\). \(T_2\) is effective time within voltage is reduced down to \(1/2\) value of amplitude.

Overvoltage is any voltage between a phase conductor and the Earth of phase conductors whose amplitude is in accordance with the definition of overvoltage [12]. Atmospheric and switching overvoltage-transient overvoltage is short-time overvoltage of the order (\(\text{ms}\)) or shorter that oscillates or does not oscillate, and it is usually strongly damped and achieves the full value at various times [13].

![Fig.1. Real and general form: a) striking voltage, b) striking voltage of atmospheric origin, c) switching overvoltage.](image)

Transient overvoltages are of the same polarity and are categorized as follows [14]:

- a) slower front growth: front time \(t_f\) from \(20\mu\text{s} < t_f < 5000\mu\text{s}\) and back time from \(t_r < 20\text{ms}\);

Copyright © 2019 MECS
b) rapid front growth: front time \( t_f \) from 0.1 \( \mu s < t_f < 20 \mu s \), and back duration from \( t_i < 300 \mu s \);

c) very rapid front growth (overvoltages of one polarity with front time \( t_f < 0.1 \mu s \), duration \( T < 3 \mu s \)).

They have shorter time of voltage growth \( T_1 \) to amplitude value in relation to the time of achieving \( \frac{1}{2} \) of amplitude value at the back \( T_2 \). Cutting of striking voltage occurs due to breakdown and is described by time of cutting voltage \( T_c \). Time to amplitude of voltage \( T_e \) with switching striking overvoltages is the time between initial condition \((0,0)\) and \(V_m\). In addition to back time \( T_2 \) for achieving \( \frac{1}{2} \) of amplitude value, the characteristic quantity is also the duration time of maximum \( T_d \) within which the voltage exceeds 90% of amplitude value \( V_m \).

According to references [8,10,15,16] the standard form of atmospheric overvoltage impulse is \(1.2/50 \mu s\) while of switching it is \(100/1000 \mu s\). For both impulses, duration time of voltage growth to amplitude value \( T_1 \) greatly exceeds \( t_f \).

Fig. 2 shows the basic characteristics of overvoltage.

![Fig. 2. Basic characteristics of overvoltage.](image)

The parameters given in Fig. 2 are: amplitude \( V_{\text{max}} (kV) \), front time \( t_f (\mu s) \), back time \( T, t_i (\mu s) \), and their approximate values are: \( t_f \approx (1-10) \mu s \), \( t_i \approx 20 \mu s \) and sometimes also \( t_i \approx (200-300) \mu s \).

Standard waveform of induced atmospheric voltage wave is defined by hypotheses in the references [4,10] where it is stated that the wave is the difference of two exponential functions \( v(t)=V_m\left( e^{-\alpha t} - e^{-\beta t} \right) \). Parameter \( \beta \) is joined to the time of wave front growth \( t_f \) and parameter \( \alpha \) is joined to the time of wave back \( t_i \). By choosing the values \( \alpha \) and \( \beta \) the given waveform is obtained with two exponential members and relation \( t_f / t_i \) [3,11,12]. Such a presentation does not correspond to the facts because:

- the solution \( v(t)=V_m\left( e^{-\alpha t} - e^{-\beta t} \right) \) is not mathematically correct and does not have an adequate physical explanation and it does not satisfy the condition of equivalency of original of the function and its first derivative,

- analytical method can provide formulas for shaping transient atmospheric of switching striking voltage in RC circuit of \( n \) order with minimal number of elements of the second order which will be the basis for designing the generator of assigned form of voltage/current wave (the example is given in the paper).

Cauchy condition is satisfied if the function \( y=f(x,y) \) has partial differential \( df/dy \) in the region, and, if it is not, then Lipschitz condition is used [17,18]. For an isolated singular point \((0,0)\) Cauchy conditions are disturbed if they are satisfied at any other point. Course of the curve around the singular point depends upon the root of the characteristic equation. For continuous function \( f(x,y) \) around the point \( M(x_0,y_0) \), \( |x-x_0|<a \) and \( |y-y_0|<b \) there is at least one solution for the equation \( y'=f(x,y) \) which is defined and continuous in the interval around the point \( x=x_0 \) which is also the solution \( y=y_0 \).

Lipschitz condition \( |f(x,y)-f(x_0,y_0)|<N|y_1-y_2| \) is fulfilled if \( N \) does not depend upon \( x,y_1,y_2 \), and the solution is continuous function of \( y=y_0 \). If through the point \( M(x,y) \) goes the graph of the solution \( y'=f(x,y) \), of the equation \( y'=f(x,y) \), coefficient of the direction of tangent upon the graph at that point determines the expression \( dy/dx \).

All straight lines in the field in the plane, parallel to that tangent on the graph at the set point have equal directions (other straight lines apart from it are not tangent). Other directions belonging to remaining straight lines do not satisfy the condition to be the first derivatives of the graph at the set point since Cauchy conditions for linear homogenous differential equations of the second order with constant coefficients have not been fulfilled:

\[
\Leftrightarrow ay''+by'+cy = 0, \quad a\lambda^2 + b\lambda + c = 0. \tag{1}
\]

Solution of the previous equation has two exponential components \( y_1(x)=Ae^{\lambda_1 x} \) and \( y_2(x)=Be^{\lambda_2 x} \) and it depends upon coefficients, that is the root value of the characteristic equation. Three cases can be distinguished:

- a) \( \lambda_1 \) and \( \lambda_2 \) are real and different, then \( y = y_1(x) + y_2(x) = Ae^{\lambda_1 x} + Be^{\lambda_2 x} \). If due to initial conditions \( B = -A \) then \( y = y_1(x) + y_2(x) = Ae^{\lambda_2 x} - e^{\lambda_2 x} \);
b) \( (\lambda_1) \) and \( (\lambda_2) \) are real and equal, then:
\[
y(x) = y_1(x) + y_2(x) = Ae^{\lambda_1x} \cos \lambda_1m + xBe^{\lambda_1x} \sin \lambda_1m x.
\]

Cauchy-Lipschitz theorem about the existence of solution for differential equation of the first order and the principle of equivalency of function and its first derivative states: Function is equivalent to its derivative only if it can be obtained by integration from that derivative [3]. The analysis is valid for both exponential components. For case a) it is true: \( \lambda_1 \) and \( \lambda_2 \) if and are real and different, the first derivative of the first component at a point \( x \) is \( y_1'(x) = dy/dx = \lambda_1e^{\lambda_1x} \).

Differential equation determines at each point the direction of tangent on the graph of solution. That direction is identical to directions of all straight lines parallel to belonging tangent on the graph at the specified point within a field in the plane.

Other straight lines of the same directions are not tangent because they do not touch the straight line, and other directions of remaining straight lines do not fulfill the condition to be the first derivatives of the graph at the set points (Cauchy conditions). A set of directions creates a field of directions, and one point and direction at that point is only one element of direction of the field. Integration of the equation involves connecting geometrical location of the points of integral curve, and direction of the tangent at each point of the curve coincides with direction of the field.

In some equations for solving processes of technical matters there are vertical directions, i.e. \( f(x, y) \rightarrow \infty \). Then, in solving the roles of dependent and independent variables can be interchanged. Operation of differentiation is used, principle of equivalency introduced and it is considered that \( dx/dy = f^{-1}(x, y) \) is equivalent to \( f(x, y) \) (equations are equivalent if they have the same roots [3]).

In the domain where Cauchy conditions for equations under a) and b) are met through each point \( M(x_0, y_0) \) passes only one integral curve. The set of curves depends upon one parameters and the equation of family of curves-integral of equation of the first order has one liberally chosen constant \( C \). Particular integral \( y = \phi(x) \) which satisfies the condition \( y_0 = \phi(x_0) \) obtained is from the integral \( F(x, y, C) = 0 \) if \( C \) is determined from \( F(x_0, y_0, C) = 0 \).

Variable \( x \) in the equation (1) is replaced by the time \( x = t \) quantity and dependent variable \( y \) by voltage \( y = v \):

\[
\frac{d^2v(t)}{dt^2} + \frac{b}{a} \frac{dv(t)}{dt} + \frac{c}{a} v(t) = 0.
\]

Classical solution for the variable \( x = t \) is [3]:

\[
v = v_1(t) + v_2(t) = A(e^{\lambda_1 t} - e^{\lambda_2 t}).
\]

If \( v_1(t) = Ae^{\lambda_1 t} \) and \( v_2(t) = Be^{\lambda_2 t} \) are continuous functions within the rectangle \( P \), if elements of the set \( \mathbb{R} \) are real numbers, then functions \( v_1(t) \) and \( v_2(t) \) belong to the field (domain) \( \mathbb{R}^2 \), and \( s \) corresponds to the maximum \( \mu > 0 \).

A. Classical solution

When the functions \( v_1(t) \) and \( v_2(t) \) satisfy Lipshitz condition [3], in accordance with theorem about existence of \( \eta \) numbers as a unit within the set \( \mathbb{R} \), we obtain:

\[
\begin{align*}
|\eta| &< \frac{1}{\mu(x - \xi)}, \exists \eta \in \mathbb{R} \\
|v(t) &- v(t)| \leq \eta |s_1 - s_2| &\in P
\end{align*}
\]

If \( \xi_1 < \min \left( \xi, \frac{1}{\mu}, \frac{1}{\eta} \right) \), it is proved that there is only one differential function \( v = v(t) \) in the domain \( P = [0 - \xi, t_0 + \xi] \) which is the solution of the differential equation \( \frac{dv}{dt} = f(v, t) \) (*), at the segments \( [t_0 - \xi_1, t_0 + \xi] \) and satisfies the initial condition \( v(t=0) = v_0 \) . Solutions of the equation (*), with the initial condition \( v(t=0) = v_0 \) are continuous solutions of the equation [3]:

\[
v(t) = v_0 + \int_{t_0}^{t} f(v, \tau) d\tau \quad \tau \in [0 - \xi, t_0 + \xi_1].
\]

B. Correction of classical solution

The solution where the first derivative and original equivalent is obtained by Cauchy-Lipschitz criterion makes it easier to determine voltage constants because the time constants define passive \( RC \) parameters:

\[
v_1(t) = \int_{0}^{t} \frac{dv(t)}{dt} - v(t)_{t=0^+} = A(t - e^{\lambda_1 t}).
\]


\[ v_H(t) = \int_0^t \frac{dv_2(t)}{dt} dt - v_2(t)|_{t=0^+} = B\left(1 - e^{-2\beta t}\right). \]  \(7\)

For \( B = -A \), \( v(t)|_{t=0} = 0 \) and \( e^{2\beta t} v_0 = e^{2\beta t} \), then new solution is obtained very similar to the known classical solution \( v(t) = A e^{\beta t} - A e^{\beta t} \):

\[ v(t) = A(1 - e^{\beta t}) - A(1 - e^{\beta t}). \]  \(8\)

The solution with \( B = -A \) and two components \( v(t) = v_I(t) + v_H(t) \) should satisfy the equation and equivalency condition of the first derivative and original. Also, by analytical method, integration of the first derivative gives:

\[ v_I(t)|_{t=0} = -A\left(1 - e^{-\tau_1}\right) = A\left(1 - e^{-\tau_1}\right). \]  \(9\)

\[ v_H(t)|_{t=0} = -B\left(1 - e^{-\tau_2}\right) = B\left(1 - e^{-\tau_2}\right). \]  \(10\)

\[ v(t) = v_I(t) + v_H(t) = A\left(1 - e^{-\tau_1}\right) - A\left(1 - e^{-\tau_2}\right). \]  \(11\)

\[ \frac{dv(t)}{dt} = A\left(\frac{1}{\tau_1} e^{-\tau_1} - \frac{1}{\tau_2} e^{-\tau_2}\right). \]  \(12\)

\[ \frac{dv(t)}{dt}|_{t=0} = A\left(\frac{\tau_2 - \tau_1}{\tau_2 \tau_1} - \frac{C}{a} = \frac{V_k}{a}\right) \]  \(13\)

Solution of the equation (13) satisfies homogeneous differential equation of the second order and can be used for determining parameters for the generator for simulation of atmospheric and switching striking overvoltages. Graph shapes of the components are different classical solution, Fig.3.a,b. They also differ for the corrected solution, Fig. 3.c, for voltages \( v(t) \) in RC circuit of the second order, which in accordance with IEC standard [8] has specified monotonous and aperiodic course.

From the moment \( t = 0_+ \) the shape asymptotically approaches the course of stationary state \( v(t) = v_I(t) + v_H(t) \).

Classical solutions are disputable because for both components the first derivatives are not tangents but straight lines parallel to tangents. Per abscissa these are curves of variables displaced by \( t_1 \) and \( t_2 \) which leads to an error in determining time constants of voltage forms defined by the parameters of RC circuit. The new solution is determined by analytical method in which Cauchy and Lipshitz condition for the first derivative on the function graph is met for all abscissa values \( 0 < t < \infty \).
IV. GENERATOR OF STRIKING OVERVOLTAGE WITH PASSIVE PARAMETERS OF ELEMENTS AND SPARKING

Generator of striking voltages with sparking, depending upon number of elements and structure is made with RC circuit of the first second and higher n order-Marks generator with multiple RC circuits. Amplitude $V_m$ and constants $\tau_1, \tau_2, t_m, C, C_k$ are adjusted according to the requirement of IEC standards [8]. $r_f, r_r, R$ are determined depending upon number and values of parameters.

Breakthrough of sparking that influences waveform is defined by Streamers theory of channel and Paschen’s law. Multiple Streamers occur in homogenous fields and further ionization creates the channel of high temperature plasma-leader.

Breakthrough time $t = t_0 \ (t \approx t_0 = 10 \div 20 \text{ns} \equiv 0_+)$, is the time from the moment voltage occurs to breakthrough.

In Fig. 4.a the circuit has at input the capacitor of capacitance $C_k$ under voltage by circuit $V_k$. After breakthrough of sparking through a combination of damping resistor $r_i$ and resistor $r_f$ (wave-front), capacitance $C$ of the object tested is loaded and at the same time discharged through discharge resistor $R$. Capacitance $C$ value is often not known when determining shape of the voltage. In the diagram of RC circuit of striking voltage in Fig. 4.a the currents are:

$$i = -C_k \frac{dv_k}{dt}, \quad i_2 = C \frac{dv}{dt} \quad (14)$$

The wave form of striking voltage is obtained as follows:

$$a \frac{d^2v(t)}{dt^2} + \frac{b}{c} \frac{dv(t)}{dt} + v(t) = 0. \quad (15)$$

$$\tau_1 \tau_2 \frac{d^2v(t)}{dt^2} + (\tau_1 + \tau_2) \frac{dv(t)}{dt} + v(t) = 0. \quad (16)$$

The same shape is obtained also in analog way:

$$\frac{d^2v(t)}{dt^2} + \frac{b}{a} \frac{dv(t)}{dt} + \frac{c}{a} v(t) = 0 \quad (17)$$

$$\frac{d^2v(t)}{dt^2} + \frac{1}{\tau_1 \tau_2} \frac{dv(t)}{dt} + \frac{1}{\tau_1 \tau_2} v(t) = 0$$

where is the equation:

$$\tau_{1,2} = \frac{b \pm \sqrt{b^2 - 4ac}}{2c}, \quad \tau_{1,2} = \frac{a}{c} \quad (18)$$

The solution with two components in equations (9-13), for $B = -A$ should satisfy value of parameters (18) and equivalency condition of the first derivative and original. Differentiation of the equation (12) gives:

$$\frac{dv(t)}{dt} \bigg|_{t=0} = A \left( \frac{1}{\tau_1} e^{-\frac{t}{\tau_1}} - \frac{1}{\tau_2} e^{-\frac{t}{\tau_2}} \right) = A \frac{\tau_2 - \tau_1}{\tau_1 \tau_2}. \quad (19)$$

The expression $v(t) = A \left[ (1 - e^{-t/\tau_1}) - (1 - e^{-t/\tau_2}) \right]$ satisfies the equation and can be used for choosing parameters in simulation of atmospheric and switching striking overvoltages.

IEC standard determines parameters of RC circuit of the model through time constants $T_1$ and $T_2$:

- wave front time $T_1 = t_f$ defined by time difference at the points with values $0.3V_m$ and $0.9V_m$.
- back time $T_2 = t_2$ as the time at which voltage value at the back reduces to $(1/2)V_m$. 

Copyright © 2019 MECS
Wave form theoretical model is defined by mathematically determined time constants $t_1$ and $t_2$, which are in different correlations in regards to standard values $t_f, t_r$. When choosing the shape, possible solution variants are:

- set value $t_1 \leq T_1$ or $t_1 \geq T_1$ and then can be determined and $k = V_m / A = f(T_1)$ and $t_2 = f(T_2, k)$,
- set value $t_2 \leq T_2$ or $t_2 \geq T_2$ then can be determined and $k = V_m / A = f(T_2)$ and $t_1 = f(T_1, k)$,
- after determining $t_1, t_2, k$ and adopting necessary values $C_k, R, C$ according to derived equations, parameters of $RC$ circuit, $r_f, r_p$ are determined.

V. APPROXIMATE SOLUTION OF STRIKING VOLTAGE WAVEFORM

If there is no data about capacitance of tested object $C$, in order to calculate parameters of $RC$ it is necessary to adopt values $C, C_k$ and to determine relation of the value $r_f, R$. To obtain expected waveform of the striking voltage, all parameter values should be in accordance with specified constants $V_m, r_1, r_2, k$.

According to IEC standard the value [8] $\frac{t_2}{t_2 - t_1} \geq r_1$ hence follows the expression:

$$\frac{dv(t)}{dt}_{t=0} = A \frac{t_2 - t_1}{t_1 t_2} = \frac{A}{r_1}.$$  \hspace{1cm} (20)

Constant $A$ which defines time constants is determined from $V_m$ and the values $k < 1, V_m = kA$ [8]. Atmospheric wave is characterized by amplitude $V_m$ and relation $T_1 / T_2$:

$$t_f = T_1 = 1.67(t_2 - t_1), \hspace{0.5cm} t_2 - t_1 = T_1 / 1.67.$$  \hspace{1cm} (21)

Since $t_1, t_2 < (t_f = T_1) \ll (r_1 = T_2) < t_2$ , both exponential members are: $e^{-t_1 / t_2} \cong 1, e^{-t_2 / t_2 - t_2} \cong 1$.

Value $t_1$ of striking voltage of the generator

$$v(t) = A \left[ e^{-t / t_1} + e^{-t / t_2} \right]$$ per IEC standard [8] and

axiomatic definitions $e^{-t_1 / t_2} \cong 1, e^{-t_2 / t_2} \cong 1$ is determined from:

$$v(t)_{0.3V_m} = A \left[ e^{-t / t_1} + e^{-t / t_2} \right] = 0.3V_m$$ \hspace{1cm} (22)

$$v(t_1)_{0.9V_m} = A \left[ e^{-t / t_1} + e^{-t / t_2} \right] = 0.9V_m.$$ \hspace{1cm} (23)

So if

$$e^{\frac{t}{t_1}} = 1 - 0.3k, e^{\frac{t}{t_2}} = 1 - 0.9k \Rightarrow e^{\frac{-t_2 + t}{t_1}} = \frac{1 - 0.3k}{1 - 0.9k} \Rightarrow$$

$$t_f - t_1 = ln \frac{1 - 0.3k}{1 - 0.9k} = 1.67 \frac{t_1}{t_1, t_1} = 1.67 \frac{1 - 0.3k}{1 - 0.9k} .$$  \hspace{1cm} (24)

Back time $t_2$, is determined from equation (23)

$$v(t)_{t_2} = V_m \left[ e^{-t / t_1} + e^{-t / t_2} \right]$$, so if

$$e^{-t_2 / t_1} \approx 10^{-4} \rightarrow 0 \hspace{0.5cm} v(t)_{t_2} = V_m \left[ e^{-t / t_2} \right].$$

$$k \equiv e^{-t_2^2}, \hspace{0.5cm} t_2 \equiv T_2 \frac{T_2}{ln(2/k)}$$ and $t_m = \frac{t_f t_2}{t_2 - t_1} ln \frac{t_2}{t_1}$.

VI. CALCULATION, SIMULATION AND ANALYSIS OF TRANSIENT PROCESS

Solution for $v_k(t) = V_{ck}$ is determined from state within the circuit of the simulation model, Fig. 5 when the switch is closed and sparking open (there is no breakthrough of the sparking)

$$v_k = V_{ck} \frac{T_1}{T_f} + \frac{1 + R}{R}$$ \hspace{0.5cm} (25)

and solution for

$$v(t) = V_{csurge} \hspace{0.5cm} and \hspace{0.5cm} i_2(t) = I_{csurge}$$ from the state within
the circuit when breakthrough of the sparking occurs

\[ v(t) = A \left[ -e^{-\frac{t}{\tau_1}} + e^{-\frac{t}{\tau_2}} \right], \quad i_2 = I_{c,\text{surge}} = C \frac{dv}{dt}. \]

In order to check derived equations of transient process simulation was made in the part of the program MATLAB psbtransient.mdl Power Sym package titled psbtrsrg.mdl. Fig. 5 [19]. The diagrams obtained, Fig. 6, confirm that derived relations are in accordance with the set values in Simulation model.

Fig. 5. Diagram of simulation model for transient process in striking voltage generator: a) before breakthrough of sparking, b) after breakthrough.

Fig. 6. Transient processes in linear RC circuit of generator current voltage: a) Values A and \( V_{ck} \), b) diagram \( V_{ck} \), c) diagram \( V_c \), d) diagrams of current and \( I_c \), and e) detail of striking voltage wavefront.
Results and diagrams obtained, Fig. 6, show variations of currents and voltages and indicate possibility of applying the model of RC circuit in the generator to obtain expected striking voltage waveforms.

For RC circuit of striking voltage generator with specified $V_{\text{cm.surge}}(kV)$, given shape; front and back times $T_1/T_2 = 1.2\mu s/50\mu s = 41.7$ and adopted values $k = \frac{V_m}{A}; C_k, (\mu F)$, it is necessary to determine $V_{ck} = A$, mathematical time constants $\tau_2, \tau_1$ and resistance values $R, r_f, r_T (\Omega)$.

As mentioned earlier in the paper, this is an example where formulas for shaping transient atmospheric or switching striking voltage within RC circuit can be obtained by analytical method.

**Example:**

$V_{\text{cm.surge}} = 300.94kV$

$k = 0.948 \pm 0.95$

$A = \frac{V_m}{0.948}$

$A = 317.36kV$

$V_{ck} = A = 317.36kV$

$\tau_1 = \frac{T_1}{1.67 \ln 1-0.3k} = \frac{1.2}{1.67 \ln 1-0.3 \cdot 0.95} \approx 0.46\mu s$

$\tau_2 - \tau_1 = \frac{30.82}{\ln (2/k)} = \frac{50}{\ln (2/0.948)} = 66.99 \approx 67\mu s$

$\tau_2 \tau_1 = \frac{30.82(\mu s)^2}{66.54}\mu s$

$\tau_2 - \tau_1 = 66.54\mu s$

$\tau_2 + \tau_1 = 67.46\mu s$

$\tau_m = \frac{\tau_2 \tau_1}{\tau_2 - \tau_1} = \frac{0.46 \cdot 67.0}{67.16 - 0.46} = 2.3\mu s$

Checking:

$V_m = A \left( -e^{\frac{t}{\tau_1}} + e^{\frac{t}{\tau_2}} \right) = 317.33 \left[ -e^{\frac{2.3}{0.46}} + e^{\frac{2.3}{67}} \right] = 317.36[-0.00674 + 0.966] = 317.33 \cdot 0.959 \approx 304.3kV \approx 300.03kV \approx 300.94kV$

From specified parameter values of input branch of $RC_k$, electric circuit $C_k = 0.125 \cdot 10^{-3} \mu F$ and $R = 1110\Omega$ is determined time constant $RC_k$ which amounts to:

$RC_k = 1110\Omega \cdot 0.125 \cdot 10^{-3} F \approx 0.13875\mu s$

From adopted value $C = 2.5\mu F$ and time constants of the back $\tau_2 = 67\mu s$ we obtain:

$r_f = \frac{67 \cdot 10^{-6}}{2.5 \cdot 10^{-6}} = 26.8\Omega$

Then, value $r_T$ is calculated as:

$r_T = \frac{r_f R}{r_f + R(RC_k^{-1})} = \frac{26.8 \cdot 1110}{26.8 + 1110 \cdot 0.46} \approx 60.62\Omega$

Checking:

$\tau_1 = RC_k \left[ \frac{r_f}{r_f + (1 + \tau_T/R)} \right] = 0.13875 \left[ \frac{60.62}{60.62 + 1 \cdot 1100} \right]$

$= 0.13875 \cdot 0.322621 = 0.4608\mu s$

For analysis of transient process with specified waveform of striking voltage is used diagram of the model that contains specified values: $V_{source} = 400kV$ , $k = 0.95$ , $V_m = 300kV$ , $T_1/T_2 (\mu s/\mu s) = 41.7$ , switch, sparking and passive elements: $C_k = 0.125 \cdot 10^{-9} F$ , $C \approx 2.5 \cdot 10^{-6} F , R = 1110\Omega$.

Resistances calculated are $r_T = 60.62\Omega$ and $r_f = 26.8\Omega$. Opening and closing the switch and sparking start the simulation and activate program psbtrsg.mdl, with chosen circuit parameters. Measured currents and voltages are:

$i_2 = I_{c.surge} = C \frac{dv}{dt} = C \cdot A \left( \frac{1}{\tau_1} - \frac{1}{\tau_2} \right)$

$v_k = V_{ck} = r_f C \left[ \frac{r_f}{r_f + (1 + \tau_T/R)} \right] \frac{dv}{dt}$

$\nu(T) = V_c = A \left[ -e^{\frac{-t}{\tau_1}} - e^{\frac{-t}{\tau_2}} \right]$

**VII. Conclusion**

Established equations and expressions can be used to determine values of standard parameters of striking voltage shapes and time constants in the generator models with electric RC circuits. The example shown and its checks show that the errors occurring in calculation of parameter values and constants are very small.
Advantages of MATLAB Simulink are a great number of possible Simulations and the results of these simulations, forms and characteristic values of obtained wave diagrams verify the method suggested for obtaining the parameters of voltages and currents of striking voltages waves.

Ready-made MATLAB Simulink programs simulate changes of frequencies pretty well, but own development both of models and programs gives special advantages, such as detailed insight into all components of the models and programs and introduction of various alterations that otherwise could not be introduced into available program package.

Application of auxiliary time constants \( \tau_1 \), \( \tau_2 \) which are in correlation with constants \( T_1 \), \( T_2 \) gives correct parameter values and that is confirmed also by diagrams obtained by simulation using the innovated part of the program psbtsrsg.mdl MATLAB. The results of the simulation also confirm that the solutions obtained by application of the analytical method shown are correct and applicable. A high correlation can be the result of the third variable influence, which caused the appearance of their interdependence. This phenomenon is left to the authors to examine and explain in some of the following work.

REFERENCES

[1] N. Marković, S. Bјelić, J. Љivanić, V. Miličević, Z. Miličević, “Model of Transient Process Where Three-Phase Transducer Feeds Induction Motor Equivalented as a Variable Active-Inductive Load”, Mathematical Problems in Engineering, Vol. 2016, Article ID 6740261, Research Article, 2016, http://dx.doi.org/10.1155/2016/6740261.

[2] P. Vukelja, J. Mrvić, D. Hrvić, “The Experimental Investigation of Overvoltages Transferred From High to Low Voltage Side of 420 kV/15.75 kV/15.75 kV Transformer Made by Asea and Located in Hydroelectric Power Plant Djeđarić 1”, UDK: 621.3.015: 621.314.222.6, Vol. 18, 2007, pp. 161–173.

[3] И.Н. Бронштеин, К.А. Семендьев, “Справочник по математике”, Moskva, Nauka, 1973, pp. 154.

[4] S. Bјelić, P. Spalević, Z. Bogićević, B. Prlinčević, “Generating Control Signals in the Electro-energy Networks Using Passive Elements”, Journal of Multidisciplinary Engineering Science and Technology (JMEST), Vol. 1, Issue 4, 2014, pp. 248–253.

[5] C.T.R. Wilson, “Investigations on lightning discharges and on the electric field of thunderstorm”, Philosophical Transactions of The Royal Society, pp. 73–115.

[6] I.G.C. Simpson, “Proceeding Royal Society (GB)”, No. 114, pp.114.

[7] N. Marković, S. Bјelić, Protection against hazardous electrical current, Higher Technical School of Professional Studies Urosevac in Leposavic, 2018.

[8] Standards: IEC 60071-1, IEC 61024-1: Protection against lightning. Part I: General principles IEC 62305-1.

[9] L. Van der Sluis, “Transients in Power Systems”, John Wiley & Sons Ltd, 2001.

[10] B. Jovanović, S. Bјelić, N. Marković, “Transient Processes on the Elements of Underground Installations”, International Journal of Information Technology and Computer Science IJITCS 2017, Vol. 9, No. 9, pp. 1–10, DOI: 10.5815/ijitcs.

[11] L.L. Grigsby, “The Electric Power Engineering Hand book”, Chapter 10 Power System Transients, 10.6 Transient Voltage Response of Coils and Windings, CRC Press LLC, 2001.

[12] N. Marković, S. Bјelić, J. Љivanić, U. Jakišić, “Numerical simulation and analytical model of electrical arc impedance in the transient processes”, Elektronika, Energetika, Elektrotehnika, Przegląd Elektrotechniczny, 2013-2a2013, pp. 113–117.

[13] S. Bјelić, Z. Bogićević, “Computer Simulation of Theoretical Model of Electromagnetic Transient Processes in Power Transformers”, Information Technology and Computer Science, IJITCS 2013, Vol. 6, No. 1, pp. 1–12, DOI: 10.5815/ijitcs.2014.01.01.

[14] N. Mohan, T.M. Undeland, W.P. Robbins, “Power Electronics: Converters, Applications, and Design”, John Wiley & Sons. Inc., Section 8.4.1., New York, 1995.

[15] A. Veverka, “Technika Vysokých Napeti” SNTL/ALFA, Praha 1982, pp. 283–292.

[16] V. Miličević, S. Bјelić, N. Marković, U. Jakišić, “Simulation of transient process in distributive networks middle voltage (10-35 kV), BizInfo. UDK: 621.316.027.6:519.876.5, Vol. 1, 2014, pp. 83-93.

[17] J.C. Meyer, D.J. Needham, “The Cauchy Problem for Non-Lipschitz Semi Linear Parabolic Differential Equations”, London Mathematical Society, Cambridge, 2000.

[18] M. Pierre, R. Shigui, “Theory and Applications of Abstract Semilinear Cauchy Problems”, Springer, Switzerland, 2018.

[19] MATLAB SIMULINK Sim Power System, Copyright 1984–2002 The Math Works, Version 6.5.0,180913a, June 2, 2000.

Authors’ Profiles

Slobodan N. Bјelić: Full-time professor at Faculty of Technical Sciences in Kosovska Mitrovia, University of Pristina. He received his Ph.D. degree in 1982, field of interest: Electrical Engineering-Computer Science-Protective Relays-Electrical Installation and Illumination Engineering-Electrical Power Converters. He is author or coauthor of 10 textbooks and over 200 scientific and professional papers published in international and Serbian journals.

Nenad A. Marković: Assistant Director for Education at High Technical School of Professional Studies Urosevac with temporary seat in Leposavic, and professor at study programs Mechanical engineering and Road Traffic in mentioned school. He has received his Ph.D. degree from Faculty of technical Sciences in Cacak-University of Kragujevac and is author or coauthor of many textbooks, exercises and over 120 papers published in international and Serbian journals.
Zorica S. Bogićević: Professor of vocational study in Higher Technical Professional School in Zvecan, Serbia. She is received her Ph.D. degree in 2016, field of interest: Electrical Engineering-Computer Science. Her disertation teses was: “Development of algorithms and simulation of transitional process in transformer windings with computer supports”. She is author of textbook Electric drivers and over 60 scientific and professional papers published in international and Serbian journals.

Igor S. Bjelić: Her disertation teses was: “Typology and structural characteristics of arches and vaults of sacral buildings in the medieval Serbia”, Faculty of Civil Engineering and Architecture, University of Nis, September 2016. She is author of 36 scientific and professional papers published in international and Serbian journals.

How to cite this paper: Slobodan N. Bjelić, Nenad A. Marković, Zorica S. Bogićević, Igor S. Bjelić, "Application of Cauchy (Lipschitz) Criterion for Obtaining Theoretical Models of Atmosphere Striking Overvoltages", International Journal of Information Technology and Computer Science(IJITCS), Vol.11, No.9, pp.20-30, 2019. DOI: 10.5815/ijitcs.2019.09.03