Performance Performance Analysis of Tubular PEM Fuel Cell Models and Thermal Analysis of Base Model using Ethylene Glycol-Water Mixture as a Coolant

Tejas Ambekar¹, Pratham Amle², Durgesh Chandangole³, Gopal Ghule⁴, Prof. Dr. L. D. Mangate⁵
¹, ², ³, ⁴Students, Mechanical Engineering, Vishwakarma Institute of Technology, Pune, India
⁵Faculty, Mechanical Engineering, Vishwakarma Institute of Technology, Pune, India

Abstract: This work aims towards the simulation of Various proton exchange membrane fuel cell (PEMFC) models to investigate the effects of operating parameters such as temperature, pressure, anode flow levels and cathode reactants, component types, cooling temperatures in the performance of a modified fuel cell. The basic model and the tubular model are developed in modelling software based on the size of the parameter later simulated using the addon module in the Ansys software. The Addon module is specifically designed to mimic a different type of fuel cell. The simulated model of cell power output showed positive compliance with experimental results taken from the literature and revealed that the operating pressure, temperature, and flow rate of reactants positively affect the function of the Fuel cell. The results also showed that the cooling temperature of the coolant indicates higher concentrations of current congestion compared to the base model without cooling. Corrective results obtained from the effect of temperature on cell function showed that the fuel cell temperature favor both cell function and efficiency. It can therefore be assumed that the efficiency of the cell is strongly influenced by operating temperature, pressure, cooling temperature, fuel flow rate and oxidant.

Keywords: PEM fuel cell, Current density, tubular fuel cell, addon-module.

1. INTRODUCTION

Over the years, the earth has relied heavily on the only source of energy known as fossil fuels and is limited to domestic and industrial use. This situation has created an imbalance in global oil production and demand, which has led to energy crisis due to a lack of supply and price volatility. Inflation and environmental pollution of fossil fuels are some of the major problems caused by over-reliance on this energy source. It has been widely documented that the burning of fossil fuels poses a threat to human health and the environment and that this has led to an increase in the search for a clean energy source to protect the environment and to protect one from inhaling toxic substances. For example, it is a well-known fact that combustion of fossil fuels emits harmful gases such as CO₂, CO, and SO₂ into the atmosphere. These gases pose a serious health and environmental risk and, therefore, create a major global environmental problem. Concerns about price volatility due to over-reliance on fossil fuels and increased awareness of the natural impact of fossil fuel fuels have led to an increase in calls for other energy sources that may not compete effectively with existing energy sources. Fuel cells defined as electrochemical tools that convert chemical reaction energy into electricity directly, with water as their product, are now considered a promising, economical, and sustainable energy source.

Fuel cells produce little or no pollution depending on the type of fuel used. They also have advantages that make them better than other industrial combustion channels which are capable of capturing the excess heat produced and using it in the same way as mixing or heating space / water. Other major advantages of fuel cells carried over combustible engines include high efficiency and lack of hazardous substances. Unless researchers and the government provide the recognition of fuel cells especially the proton exchange membrane fuel cell (PEMFC) as a non-environmentally friendly source of energy that can compete effectively with existing energy sources, the high cost of associated components and technological management is detrimental. commercial availability of fuel cells as an alternative energy source. Over the past few years, good progress has been made in achieving the sale of this unique energy source by reducing the cost of electrode components, flow field plate, and membranes. However, the lack of understanding of the impact of various parameters on the power output by the fuel cell system remains a critical issue to focus on in the current study.
In this note, the first and second rules of thermodynamics have been recognized as major tools for measuring the strength and power of fuel cell technology. The first law of thermodynamics (energy analysis) deals with the value of energy and states that energy cannot be created or destroyed. The law serves as a necessary tool for calculating power during the process and does not present challenges to the engineers. The second law (energy analysis), however, deals with energy quality, the deterioration of this energy during the process, the generation of entropy, and the loss of productivity and provides a large area for development. The second law of thermodynamics has been proven to be a powerful tool in the efficient operation of complex thermodynamic systems. In more recent times, energy analysis has become an important component in providing a better understanding of energy system processes analysis, inefficiency sources, and the differential quality of energy (or heat) used.

The purpose of this study is therefore to develop a predictable simulation model to determine how we can increase fuel cell performance especially by using a coolant such as an ethyl glycol water compound and how we can increase the current energy produced by fuel cell function parameters. Imitation of the improved model is expected to provide information on the interaction of various parameters affecting the functioning of the proton exchange membrane fuel cell.

Fig.1 Base model

II. LITERATURE SURVEY

[1] A calorimeter was used to measure the heat production in (PEM) fuel cells operated on hydrogen and oxygen at 50 °C and 1 bar. We thus conclude that the reversible heat of the anode and cathode of this cell are near 0 and -80 J K⁻¹ mol⁻¹, respectively.[2] The salient numerical features of the models are examined, and an overview of the most used computational fluid dynamic codes for the numerical modelling of proton exchange membrane fuel cells is given. [3] A three-dimensional, multi-phase, non-isothermal CFD model of a proton exchange membrane fuel cell has been developed and used to investigate the displacement, deformation, and stresses inside the whole cell, which developed during the cell operation due to the changes of temperature. [4] Increasing the width of the channels reduces the maximum temperature of the cooling plate surface. Increasing the distance between two channels leads to adverse effects on the thermal parameters as well as increased pressure drop. [5] The effects of different parameters on the performances of proton exchange membrane fuel cells were studied experimentally. [6] Full three-dimensional computational fluid dynamics models of planar and tubular-shaped air-breathing PEM fuel cell has been developed.

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III. GEOMETRY DEFINITION

Due to the fact that there are a number of different physical zones associated with the fuel cell, the following regions must be present in the fuel cell mesh:

1) Anode flow channel
2) Anode gas diffusion layer
3) Anode catalyst layer
4) Membrane layer
5) Cathode catalyst layer
6) Cathode gas diffusion layer
7) Cathode flow channel

8) The following zones have to be identified, if present in the fuel cell mesh:
9) Anode current collector
10) Cathode current collector
11) Coolant channel

We have selected Maruti Suzuki Ertiga for drive shaft calculations. The following are the specifications of it.

| TABLE I. | GEOMETRY DEFINITION FOR FUEL CELL AND ELECTROLYSIS MODEL |
|----------|----------------------------------------------------------|
| Cell dimension | Values (in mm) |
| Gas channel length | 10 |
| Height of gas channel | 1 |
| Width of gas channel | 1 |
| Width of cell | 2 |
| Thickness of catalyst layer | 0.014 |
| Thickness of gas diffusion layer | 0.0254 |
| Thickness of current collector | 2.5 |
| Thickness of membrane | 0.051 |
| Overall cell height | 5.1295 |
| Cooling channel width | 0.5 |
| Cooling channel height | 0.5 |

| TABLE II. | OPERATING CONDITIONS FOR FUEL CELL |
|----------|-----------------------------------|
| Parameters | Value |
| Cell operating temperature | 323 K |
| Cell operating pressure | 1 bar |
| Open-circuit voltage | 1.07 V |
| Anode Reference exchange current density | 10000 A/m² |
| Cathode Reference exchange current density | 20 A/m² |
| CL Electric conductivity | 5000 S/m |
| Current collector Electric conductivity | 1000000 S/m |
| GDL Electric conductivity | 5000 S/m |
| Anode exchange coefficient | 2 |
| Cathode exchange coefficient | 2 |
| Reference concentration of anode | 1 kmol/m³ |
| Reference concentration of cathode | 1 kmol/m³ |
| CL Porosity | 0.2 |
| GDL Porosity | 0.6 |
IV. SETUP

A. Boundary condition

TABLE III
BOUNDARY CONDITION

| Location   | Parameter               | values  |
|------------|-------------------------|---------|
| Cathode    | Velocity inlet          | 0.3 m/s |
|            | O2 mass fraction        | 0.6     |
|            | H2O mass fraction       | 0.4     |
|            | Pressure outlet         | 0 pa    |
|            | temperature inlet       | 353     |
| Anode      | Velocity inlet          | 0.2 m/s |
|            | O2 mass fraction        | 0.21    |
|            | H2O mass fraction       | 0.15    |
|            | Pressure outlet         | 0 pa    |
|            | temperature inlet       | 353     |
| Wall       | Cathode Collector       | 0.2-0.64|

B. Mesh Quality Parameter

TABLE IV
MESH QUALITY PARAMETER

| Quality Parameter | Max.     | Min.     | Avg.     |
|-------------------|----------|----------|----------|
| Aspects Ratio     |          |          |          |
| Base model FC     | 11.905   | Base model FC | 1 | Base model FC | 2.0058 |
| Base model FC with cooling | 11.905 | Base model FC with cooling | 1 | Base model FC with cooling | 2.0166 |
| Circular tubular FC | 36.283 | Circular tubular FC | 1.06 | Circular tubular FC | 4.9456 |
| Square tubular FC | 36.364   | Square tubular FC | 1.008 | Square tubular FC | 6.0151 |
| Triangular Tubular FC | 111.31 | Triangular Tubular FC | 1.079 | Triangular Tubular FC | 6.4955 |
| Element Quality   |          |          |          |
| Base model FC     | 1        | Base model FC | 0.154 | Base model FC | 0.89663 |
| Base model FC with cooling | 1 | Base model FC with cooling | 0.154 | Base model FC with cooling | 0.89076 |
| Circular tubular FC | 0.9973 | Circular tubular FC | 0.05 | Circular tubular FC | 0.67422 |
| Square tubular FC | 1        | Square tubular FC | 0.05 | Square tubular FC | 0.74809 |
| Triangular Tubular FC | 0.9972 | Triangular Tubular FC | 0.05 | Triangular Tubular FC | 0.66669 |
| Skewness          |          |          |          |
| Base model FC     | 0.00     | Base model FC | 0.05 | Base model FC | 0.00 |
| Model Type                | Value 1 | Value 2 | Value 3 |
|--------------------------|---------|---------|---------|
| Base model FC with cooling | 0.4659  | 0.05    | 0.00    |
| Circular tubular FC      | 0.8685  | 0.05    | 0.16208 |
| Square tubular FC        | 0.9008  | 0.05    | 0.16789 |
| Triangular Tubular FC    | 0.9872  | 0.05    | 0.35204 |

Fig. 2. Meshing of Base model

Fig. 3. Meshing of base model with cooling

Fig. 4. Meshing of tubular square model
C. Grid Independence Test

In this section, the resolution of the computational grid is evaluated. The appropriate number of grid points has a great impact on the accuracy of the numerical simulations. In order to test the effect of the number of grid points on numerical results, various grid resolutions are considered. The results are shown in Figure 3 in which the pressure drop is compared between the input and output of the fuel cell. The results show that the number of 25200 grid points is enough for the present simulation.

V. PROPERTIES OF ETHYL-GLYCOL MIXTURE

Ethylene glycol-water properties are observed at different temperatures and at different fraction. Properties observed are Thermal conductivity, density, viscosity, specific heat, electrical conductivity.

Fig. 5. Meshing of tubular circular model

Fig. 6. Grid Independence Test

Fig. 7. Thermal conductivity of ethylene glycol-water mixtures
VI. RESULTS AND DISCUSSION

A. Result for FC Base Model without Cooling

Fig. 8. Density of ethylene glycol-water mixture

Fig. 9. Viscosity of ethylene glycol-water mixtures

Fig. 10. Temperature distribution along the length of fuel cell

Fig. 11. Temperature distribution along the cross section of fuel cell
B. Identify Results for FC base model with cooling (Ethylene glycol-water 50:50).
Solution has monitor for current flux density and maximum temperature in fuel cell. It can be seen that solution is converged above 2500 iterations in case of non-cooling system of fuel cell.

Fig. 12. H₂ species fraction distribution along length of fuel cell

Fig. 13. O₂ species fraction distribution along length of fuel cell

Fig. 14. Vector showing Current density magnitude within cross section of fuel cell

Fig. 15. Temperature distribution along the length of fuel cell
Distribution of heat at anode and cathode side are different. Cathode reaction generated more fraction out of total heat. Temperature distribution along the height of the fuel cell has been plotted in figure.

![Temperature distribution along the length of fuel cell](image1.png)

**Fig. 16.** Temperature distribution along the length of fuel cell

![Vector showing Current density magnitude within cross section of fuel cell](image2.png)

**Fig. 17.** Vector showing Current density magnitude within cross section of fuel cell

C. Results for Tubular circular FC Base Model

![Temperature distribution along the length of circular fuel cell](image3.png)

**Fig. 18.** Temperature distribution along the length of circular fuel cell
D. Results for Tubular square FC Base Model

E. Graphs

Fig. 19. Temperature distribution along the length of square c/s fuel cell

Fig. 20. Effect of H2 specie mass flow rate variation on current density

Fig. 21. Effect of H2 species and o2 species mass flow rate variation on current density
F. Graphs With Respect to Tubular Circular Model

Fig. 22. Effect of cooling temperature variation on current density

Fig. 23. Effect of temperature variation on current density in tubular circular FC

Fig. 24. Effect of pressure variation on current density in tubular circular FC
G. Graphs With Respect to Tubular Square Model

![Operating temperature vs current density](image1)

Fig. 25. Effect of temperature variation on current density in tubular square FC

![Operating pressure vs current density](image2)

Fig. 26. Effect of pressure variation on current density in tubular square FC

![Polarization graphs](image3)

Fig. 27. Polarization graphs of base model with and without cooling
Maximum temperature vs output voltage in the PEM fuel cell has been plotted at different cooling inlet temperatures. It can be seen that increase in the voltage up to 0.7V will result in a sudden drop of temperature.
H. Max Temperature Graphs
1) W.r.t to H2 species

![Graph showing effect of cooling temperature with respect to max temp and H2 species](image1)

Fig. 31. Effect of cooling temperature with respect to max temp and H2 species

2) Validation

![Graph showing polarization graph with experimental data and analysis data](image2)

Fig. 33. Model validation

VIII. CONCLUSION
Simulation of single straight channel, PEM fuel cell is carried out with and without liquid cooling system. Under liquid cooling system maximum temperature in the membrane of fuel cell is dropped by 70K if coolant inlet temperature is 290 K to prevent fuel cell from excessive temperature. Fuel cell temperature distribution is not uniform at anode and cathode. Maximum temperature in cathode channel is greater than maximum temperature at anode channel. With the increase in output voltage up to 0.7V maximum temperature in fuel cell drop suddenly. Operating voltage above 0.7V is best to prevent excessive temperature. With increase in the H2 concentration at anode channel decreases the temperature in fuel cell. Hydrogen fraction in anode channel above 0.3 is best to prevent excessive temperature. Comparing polarity curves of Base model PEM Fuel cell with and without cooling. With cooling Configuration shows a good values of current density than base model without cooling.
Comparing the polarity curves indicated that circular tubular configurations propose higher current density compared to the square tubular configurations PEM fuel cell model. But the triangular tubular configuration shows a drop in current density, especially in the low voltages, in comparison with the base PEM fuel cell model and it has not converged to final values as well as iteration during the analysis. Counters of Mass fractions of species on base model shows uniform increase in fraction from gas diffusion layer to gas channel. Vectors of current density in both base model with and without cooling gives uniform formation of vector filed due to its non uniform the further you moved from the corners. Due to sharp angle small amount of water content was predicted in the corners of this architecture indicating the slowness of the reaction in these regions. Unlike that case, the circular figure demonstrated a uniform distribution of the exit water vapor due to the uniform distribution of the species. Square architecture power production is placed between the circular and triangular architectures. Temperature distribution contours in gas diffusion and the catalyst layers at the cathode indicated that rising temperature is concentrated away from of the corner regions of the square and triangular architectures due to their sharp angles and slowness of reaction. In the Circular architecture, due to the dispersion of reaction at all surfaces, distribution of rising temperature occurred in wider surfaces and therefore the maximum temperature for this architecture is low. But triangular geometry, due to its non-uniform reaction has the maximum temperature compared with the two other architectures. This damages the catalyst and diffusion layers which results in an undesirable increase in cost especially for the catalyst layer. So, this point should be considered when designing novel high temperature

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