Research Article

Study on Permeability of Soil-Rock Mixture in Water-Blocking Layer of Open-Pit Coal Mine Dump Site

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Constructing a water-blocking layer in the dump sites of an open-pit coal mine is of great significance to improve the water retention capacity of the reclamation area. The permeability law of the water-blocking layer is costly to be analyzed and researched by means of field tests. In this study, the soil-rock mixture samples similar to the water-blocking layer were prepared, and the rock block proportion (RBP) and hydraulic pressure were adopted as test variables to conduct a permeability test, which provided theoretical support for on-site construction. The results show that when the hydraulic pressure is less than the confining pressure, the permeability increases at a steady rate as the rock block proportion increases. When the hydraulic pressure is close to or equal to the confining pressure, penetrating cracks are easily formed between the soil-rock interfaces of the sample with a higher rock block proportion, resulting in a rapid increase in permeability. With the increase of hydraulic pressure, the migration of the internal fine particles in the sample with a rock block proportion of 40% or less leads to the partial cracks closure, which gradually reduces the permeability. The internal structure of the sample with a rock block proportion more than 40% experiences a process in which the permeability decreases with the crack closure to a significant increase due to the penetrating crack formation. In summary, the soil-rock mixture with about 30% rock block proportion is characterized by suitable permeability and stability, which guarantees the construction cost on-site at the same time. In addition, increasing the rolling times of the truck can increase the compaction of the water-blocking layer and reduce the permeability. The roughness and gradation of the rock blocks can improve the permeability and stability of the water-blocking layer.

1. Introduction

The new open-pit coal mine reclamation process in China divides the topsoil adopted for ecological restoration from top to bottom into humus, aquifers, and water-blocking layer, as shown in Figure 1. The permeability of the water-blocking layer directly affects the soil and root environment required for plant growth [1–3]. The current process adopts compacted clay mined in open-pit coal mines as water-blocking layer. However, as shown in Figure 2, the water-blocking layer is facing the problem of rock inclusion. This material is called a soil-rock mixture. It is of practical significance to study variables such as rock block proportions and thickness of water-blocking layer on permeability through an on-site test, but the economic and time costs are high. Therefore, a rough prediction of the on-site test results can be obtained through the laboratory tests of the soil-rock mixture, which can guide the on-site test design.

Soil-rock mixture exists in many natural geological and artificial civil engineering projects [4–6]. Because of its different existence conditions and compositions [7, 8], many scholars have different research methods and focuses on soil-rock mixtures under different engineering backgrounds. Ding [9] aimed at the soil-rock mixture in the dump site of an open-pit coal mine. Based on the CT images of the samples, numerical models of different rock block proportions and porosity were established for penetration simulation experiments. The result shows that increasing the
rock block proportion and compaction rate of the soil-rock mixture can improve the water retention capacity of the water-blocking layer. Zhao [10] established a numerical model consisting of soil, rocks, and water to reveal the water inrush mechanism of a fault tunnel and simulated the migration of water at different initial and dynamic velocities. Both of them are studied by numerical simulation. The advantage is that the seepage inside the soil-rock mixture can be clearly observed, but the research on the contact model of the soil-rock interface is not yet mature, so the correctness of some conclusions cannot be determined.

Zhou et al. [11] improved the existing soil-rock mixture seepage model. The improved model considered the influence of voids and fine particles on permeability, and they verified the accuracy of the model based on the experimental results. In [12], in order to solve the problem that the compacted clay that acts as a water-blocking layer in the landfill is prone to dry and crack in a dry environment, the hydraulic conductivity of sand-clay mixtures, threshold gradient, and bound forms of pore water were studied. The results show that changing the sand content of the soil can change the effective pore size of the soil. Wang [13] studied the compressibility and permeability characteristics of sandstone-mudstone mixtures. It shows that the compaction degree of soil-rock mixture is positively correlated with permeability. Wang [14] studied the porosity and particle damage of the compacted soil-rock mixture during the vibration compaction test. The results show that proper particle size distribution can effectively fill the voids between the framework particles and reduce the porosity. These researches related to the relationship between voids and permeability through laboratory experiments show that the internal structure of the soil-rock mixture has a strong correlation with permeability, and it is also an important idea for studying the cause of permeability change in this paper.

The construction of the water-blocking layer of open-pit coal mines in China has only been proposed in recent years, so there is currently little research on the water-blocking layer of open-pit coal mine dump sites. This study simulated the environment of the water-blocking layer to prepare soil-rock mixture samples and tested the effects of rock block proportion and hydraulic pressure on permeability. By comparing with other scholars’ researches, the analysis carried out from materials and microstructure draws the conclusions which are beneficial to ensure a balance between permeability and construction difficulty.

2. Materials and Methods

2.1. Samples Preparation. In the context of water-blocking layer of open-pit coal mine dump site, clay, a by-product produced during the coal mining process, contains rocks of different sizes and shapes mixed in it, which is impossible to avoid. In order to simulate the similar engineering situation, the clay (0–1 mm) collected on-site and sandstone were adopted to prepare soil-rock mixture samples. The materials are dried with a drying box before sample preparation. Sandstone shown in Figure 3 is sieved by using 1–2 mm, 2–5 mm, 5–8 mm, and 8–10 mm classifying sieves. A certain amount of water will be mixed with the dried clay, so that the moisture content is 20%.

The test set contains four kinds of samples with rock block proportions (weight proportions) of 30%, 40%, 50%,
and 60% (the samples are called A30, A40, A50, and A60 in this paper). Considering that the compaction of the water-blocking layer is carried out by repeated rollings of the truck, the compaction method of the samples was chosen to adopt a consolidometer to compact all the samples under the same conditions. According to the results of Wan-Jun [15], 400 kPa pressure was adopted to simulate the compaction process of the clay water-blocking layer in an open-pit coal mine with 48 hours consolidation time. The graded soil-rock mixtures (the particle gradation is shown in Figure 4) were filled into a consolidometer for drainage consolidation. According to experience, the quality of each filling is about 460 g, which can ensure that every consolidated sample is basically a 50 × 100 mm sample. The sample preparation process is shown in Figure 5.

2.2. Permeability Test. For the permeability test equipment, the British GDS triaxial test machine shown in Figure 6 was adopted. This machine provides confining pressure through water pressure. The principle of the permeability test is that when the seepage velocity measured by the two seepage sensors above and below the sample should be consistent, and the seepage velocity is the permeability. The structural diagram is shown in Figure 7.

Permeability test process is conducted as follows: (1) Install the sample wrapped with rubber film and permeable stone into the testing machine to ensure the tightness of the sample. (2) Fill the cell pressure chamber with water, pay attention to the change in permeability, ensuring the sample is still sealed. (3) Apply 50 N axial pressure to ensure close contact between the sample and the machine. (4) Apply a 300 kPa confining pressure, and then conduct the permeability test.

Each sample with different rock block proportions was tested for permeability at 100 kPa, 150 kPa, 200 kPa, 250 kPa, and 300 kPa hydraulic pressures. The hydraulic pressure \((P) = \text{back pressure} – \text{base pressure}\). And the base pressure was set to 0.

3. Results and Discussion

Rock block proportion and hydraulic pressure are the two common variables to study the permeability of soil-rock mixtures [16–18]. At the same time, these two variables are with good engineering significance in this study:

3.1. Rock Block Proportion Influence on Permeability. From the test results reflected in Figure 8, the soil-rock mixtures with different rock block proportions have a positive correlation with the permeability. The analysis and comparison with related tests or simulations are as follows:

![Figure 3: Sieved soil and sandstone](image)

![Figure 4: Particle gradation of soil-rock mixture](image)

![Figure 5: Sample preparation process](image)

![Figure 6: British GDS triaxial test machine](image)

![Figure 7: Structural diagram of permeability test](image)

![Figure 8: Test results](image)
The numerical simulation of Chen [19] and Xu [20] only considered the two phases (soil and rock). Ding [9] considered the three phases (soil, rock, and pores) but could not achieve the expansion of cracks under the influence of simulation principles. The soil-rock interface is the main factor that affects the permeability of the soil-rock mixture. Under hydraulic pressure, the soil-rock interface is prone to cracks leading to the increase in permeability. In this study, uniform compaction conditions were carried out for all samples, so the rock block proportion and the compaction degree were negatively correlated, which further increased the permeability [13].

From Figures 8(a), 8(b), and 8(c), the signs of the inflection point can be seen slightly at the position with a 40% rock block proportion. When the hydraulic pressure is equal to the confining pressure, from Figure 8(e), the sudden change in permeability at the 40% rock block proportion position can be clearly seen. In Wang’s study [16], the 40% rock block proportion point was the point corresponding to the minimum permeability. In Chen’s study [21], a curve similar to that of Figure 8(e) was obtained. It shows that 40% rock block proportion is a key point for the internal structure of soil-rock mixture. Based on the results from Figure 8, on the one hand, when the hydraulic pressure is less than the confining pressure, the confining pressure performs a strong hindrance to hydraulic damage and hinders the crack development. With the increase of the rock block proportion, the soil-rock interface increases, and the permeability maintains a steady growth rate. On the other hand, when the hydraulic pressure is close to or equal to the confining pressure, the protective effect of confining pressure becomes weaker, and cracks begin to develop. As shown in Figures 8(d) and 8(e), when the rock block proportion exceeds a certain limit (Figure 8(d): $P = 250$ kPa, RBP = 50%; Figure 8(e): $P = 300$ kPa, RBP = 40%), the distance between the rocks is shortened, and soil-rock interfaces are prone to form

Figure 5: Sample preparation process with consolidometer. (a) Filling. (b) Compacting. (c) Removing the sample.

Figure 6: GDS triaxial test machine.
penetrating cracks, resulting in a significant increase in permeability. At this time, the rock itself becomes the main factor affecting the internal structure. In addition to the influence of rocks, the decrease in the proportion of clay which plays a dominant role in the water-blocking layer also leads to the permeability increases.

To sum up, first, during the construction of the water-blocking layer, the rolling times of the truck should be increased to improve the compaction. Second, no more than 30% rock block proportion on-site can better avoid the increase in permeability caused by the increase in hydraulic pressure. At the same time, a certain rock block proportion for engineering can effectively reduce the construction costs.

3.2. Influence of Hydraulic Pressure on Permeability. As shown in Figure 9, with the increase of hydraulic pressure, the permeability of the A30 and A40 samples gradually decreased, and in the permeability curves of the A50 and A60 samples, an inflection point appeared. The A30 sample permeability under different hydraulic pressures varies between $1.28 \times 10^{-6} \text{ cm/s}$ and $3.83 \times 10^{-6} \text{ cm/s}$, with a variance of 0.9, which is less affected by the hydraulic pressure. The A60 sample permeability varies from $8.98 \times 10^{-6} \text{ cm/s}$ to $13.5 \times 10^{-6} \text{ cm/s}$ with the variance of 2.4, which is greatly affected by the hydraulic pressure. A detailed analysis is given follows:

(1) Combined with the analysis in Section 3.1, and according to Ma [22], the penetration of soil-rock mixture samples is the process that the fine particles migrate with water to rebalance. Because the top and bottom of the sample are blocked by permeable stone in this study, the fine soil particles cannot migrate out of the sample with hydraulic erosion. Therefore, when the rock block proportion is less than or equal to 40%, the fine particles migrate from top to bottom under the hydraulic pressure. Part of the soil cracks closes, and the cracks at the soil-rock interface slightly develop. Overall, the permeability decreases. When the rock block proportion reaches 50%, the soil-rock interface increases. As the hydraulic pressure increases, firstly, the sample permeability decreases with further compaction caused by the particle migration process. Then, as the hydraulic pressure approaches the confining pressure, the internal structure is damaged with a penetrating crack developing between the soil-rock interface, leading to a significant increase in permeability. The schematic diagram is shown in Figure 10.

(2) One of the reasons that the soil-rock interface is the weak face of the soil-rock mixture is that the fine particles and the surface of the rock blocks do not fit well due to the fractal shape, resulting in larger pores. Wang’s study [16] also adopted clay, but the permeability obtained was relatively large. In addition to confining pressure, the difference in rock blocks also caused the result. Figure 11 shows the rock block adopted in this paper and Wang’s study. The simple parameter comparison of the two rock blocks are shown in Table 1. Wang’s study adopted marble, which has the characteristics of smooth movement during measurement without a sense of stagnation. The sandstone surface used in this study is relatively rough.

As the most vulnerable part of the internal structure of the soil-rock mixture, the cracks affect the resistance to hydraulic pressure. According to Wang’s research [14] on...
the compaction of soil-rock mixtures with different particle sizes, the size distribution of rock blocks adopted in this paper is wider, and it is more possible to form an excellent gradation similar to sand and stone in concrete, forming the most dense state with minimum porosity.

At the same time, the relatively rough surface of the rock blocks increases the friction between the materials and reduces the effect of hydraulic pressure, making the soil-rock interface difficult to be damaged and finally improving the stability of the internal structure.

Similar to test conditions, the water-blocking layer is laid above the dump site which acts like a permeable stone hindering the migration of fine-grained clay. The following conclusions can be made from the analysis: (1) Hydraulic

![Variation curve of rock block proportion and permeability](image)

**Figure 8:** Variation curve of rock block proportion and permeability. (a) $P = 100$ kPa; (b) $P = 150$ kPa; (c) $P = 200$ kPa; (d) $P = 250$ kPa; (e) $P = 300$ kPa; (f) summary.
pressure changes the internal structure through the migration of fine particles in the soil-rock mixture. The 30% rock block proportion can better prevent the formation of penetrating crack with the increase of hydraulic pressure. (2) The roughness and gradation of rock blocks affect the permeability and stability of the water-blocking layer.

**Figure 9:** Curve of hydraulic pressure and permeability of soil-rock mixtures: (a) RBP = 30%; (b) RBP = 40%; (c) RBP = 50%; (d) RBP = 60%; (e) summary.
4. Conclusions

In this study, the soil-rock mixture samples with conditions similar to the water-blocking layer of an open-pit coal mine were prepared to conduct permeability tests to study the permeability under different rock block proportions and hydraulic pressure. The following conclusions are drawn from this study:

(1) Under the method of compaction by the truck, the rock block proportions will reduce the degree of compaction and increase the permeability. Therefore, during the construction of the water-blocking layer, the number of rolling times of the truck should be increased as much as possible to improve the compaction.

(2) With the increase of rock block proportions, the shortening of the distance between rock blocks makes it easy to form penetrating cracks at the soil-rock interface, resulting in a great increase in permeability.

(3) The migration of fine particles under hydraulic pressure changes the internal structure of the soil-
rock mixture. With the increase of hydraulic pressure, the internal structure of the sample with a rock block proportion more than 40% experienced a process in which the permeability decreases with the crack closure to a significant increase due to the penetrating crack formation.

(4) The soil-rock mixture with no more than 30% rock block proportion is characterized by suitable permeability and stability. At the same time, a certain rock block proportion for engineering can effectively reduce the construction costs.

(5) The roughness of the rock blocks can increase the friction between the soil and the rock and improve the stability of the soil-rock mixture. At the same time, reasonable gradation can make the soil-rock mixture form a more dense internal structure and reduce its permeability.

Permeability is an important index for evaluating the performance of water-blocking layer. In addition to the rock block proportions and hydraulic pressure, the shear failure caused by the uneven settlement of the dump site makes the shear resistance an important factor affecting the permeability. Rock block helps us to improve the shear resistance of the soil-rock mixture. Therefore, a comprehensive consideration of the effects of rock block grading and rock block proportions on the shear strength and permeability can provide a more comprehensive theoretical guidance for the stability of the water-blocking layer in an open-pit coal mine, and it is also the direction for further research.

Data Availability

The data used to support the findings of this study are included within the article.

Conflicts of Interest

The authors declare that there are no conflicts of interest regarding the publication of this article.

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