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MULTIBODY SYSTEMS AND SIMULATION IN MATLAB

Urgency of the research. Computer modeling changes the teaching methodology, the way of thinking and the possibilities of applications. It helps to move from external to internal properties and from individual to related properties. The development of the product is accelerated by experimenting with a computer model.

Target setting. Kinematic analysis in Matlab and MSC Adams View. The aim is to investigate the rotation of individual members of the robotic system and to determine the spatial movement of the end effector.

Actual scientific researches and issues analysis. MSC Adams represents dynamic simulators of virtual prototypes of mechanical systems. Virtual prototypes allow to model, analyze and optimize the future products and to examine their properties before building a real prototype. This approach is suitable for developing miniature mechatronic elements as well as complex systems.

Uninvestigated parts of general matters defining. Virtual prototypes represent a suitable resource for testing of control and regulation procedures.

The research objective. Compilation of a virtual prototype of a mechanical system that has all the decisive features and is computationally stable.

The statement of basic materials. Virtual model is a mathematical representation of real-world structures, simulating all its physical properties virtually.

Conclusions. The aim was to determine the kinematic properties and also to evaluate the influence of the parameters of the mechanism which influence these kinematic properties. The matrix method was used. The process of the solution consisted of determining the transformation matrices of the coordinate systems, the kinematic analysis of the industrial robot and the graphical representation of the effector handling space.

Keywords: virtual model; open kinematic chain; robotic system; software simulation; end-effector; transformation matrices.

Fig.: 11. References: 17.

Introduction. The development of technology and mechanization has led to the development of the theory of planar and spatial mechanisms. Spatial mechanisms are used in various production machines, for example, in robots and manipulators. Analytical analysis of mechanisms describes the movement of driven members or some points of these members depending on the known or prescribed movement of the driving members. It means the determination of the position, speed and acceleration of the studied members and points depending on the movement of the driving member. It is possible to use the vector method for kinematic solution of spatial mechanisms, which was described by V. A. Zinovev. This method, however, is quite complicated for scalar notation of vector equations. More suitable is the usage of the matrix notation. The fourth order matrices were introduced by J.Denavit and R.S.Hartenberg. Similarly, G.S.Kalicin solved some problems of planar and spherical mechanisms by the matrix notation. The possibility of using quaternions or biquaternions in kinematics of the rigid bodies was pointed out by J. Novák. General methods of analytical analyses were studied by S.G. Kislicin and J. F. Moroshkin. The czech author V. Brat introduced into practice the usage of a matrix notation in analysis of kinematics of spatial mechanisms. Individual simultaneous movements can be described by matrix equations. There are relationships derived for both simple and simultaneous movements. The suitability and widespread usage of the matrix method is given not only by the possibility to describe the directly the space of the individual members, but it is also appropriate for use in computers with advanced methods of numerical solution of systems of equations.

This paper presents the application of the matrix method in the kinematic analysis of a simple manipulator model. Manipulators are composed of open kinematic chains. Matlab and MSC Adams - View computer programs were used in their analysis.

Model of manipulator with 2 degrees of freedom of movement R-R.

The mechanical system representing the open kinematic chain consists of two members 2 and 3 and the base 1 (Fig. 1). The member 2 with length $l_2$ rotates around the axis $z_1 ≡ z_2$ by the angle $\varphi_2$ and the member 3 with length $l_3$ rotates around the axis $z_3$ by the angle $\varphi_3$. We investigate the absolute motion of the member 3 and its point M, determine the position

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vector $\mathbf{r}_{1M}$ (position of the point M relative to the base 1) using the matrix method, using the transformation matrices of the basic movements. We also express the velocity $\mathbf{v}_{1M}$ and the acceleration $\mathbf{a}_{1M}$ of point M relative to the base 1.

Fig. 1. Coordinate systems of the manipulator with 2 DOF ($q_1=\phi_2$, $q_2=\phi_3$)

We introduce the coordinate systems of individual members (Fig. 1). The movement of the member 2 with respect to the base 1 is rotational, the coordinate system $O_2$, $x_2$, $y_2$, $z_2$ of the member 2 is rotated with respect to the base coordinate system $O_1$, $x_1$, $y_1$, $z_1$ by the angle $\phi_2$ around the base axis while $z_1=z_2$. The coordinate system $O_3$, $x_3$, $y_3$, $z_3$ of the member 3 is shifted by the length of the first element $l_2$ along the $x_2$ axis and rotated by angle $\phi_3$ around the $z_3$ axis. Generalized coordinates for rotational movement of members are: $q_1=\phi_2$ and $q_2=\phi_3$. We search: $\mathbf{r}_{1M}$, $\mathbf{v}_{1M}$, $\mathbf{a}_{1M}$.

The motion of the member 3 with respect to the base 1 is determined by the movement of the point M and described by the equation:

$$\mathbf{r}_{1M} = \prod_{i=1}^{2} \mathbf{T}_{i,i+1} \cdot \mathbf{r}_{3M} \quad (1)$$

the relative spherical motion is described by the transformation matrix:

$$\mathbf{T}_{i3} = \prod_{i=1}^{2} \mathbf{T}_{i,i+1} \quad (2)$$

The matrix equation of the trajectory of the point M relative to the coordinate system of the base 1 is:

$$\mathbf{r}_{1M} = \mathbf{T}_{12} \cdot \mathbf{T}_{23} \cdot \mathbf{r}_{3M} \quad (3)$$

where:

$$\mathbf{T}_{12} = \mathbf{T}_{Z6}(\phi_2) \quad (4)$$

$$\mathbf{T}_{23} = \mathbf{T}_{Z6}(\phi_3) \mathbf{T}_{Z1}(l_2) \quad (5)$$

and:

$$\mathbf{r}_{3M} = \begin{bmatrix} l_3 & 0 & 0 \end{bmatrix}^T \quad (6)$$

then
Position vector of point M with respect to the base coordinate system $O_1, x_1, y_1, z_1$:

$$\mathbf{r}_{1M} = \begin{bmatrix} x_{1M} \\ y_{1M} \\ z_{1M} \end{bmatrix} = \begin{bmatrix} (c \varphi_2 c \varphi_3 - s \varphi_2 s \varphi_3) l_3 + c \varphi_2 c \varphi_3 l_2 - s \varphi_2 s \varphi_3 l_2 \\ (s \varphi_2 c \varphi_3 + c \varphi_2 s \varphi_3) l_3 + s \varphi_2 c \varphi_3 l_2 + c \varphi_2 s \varphi_3 l_2 \\ 0 \end{bmatrix}$$

The matlab script (Fig.2a) for the calculation of the position vector in symbolic form and the matlab script (Fig.2b) to determine the trajectory of point $M$:

```matlab
<editor-fold defaultstate="collapsed" desc="Example 1">
parameters q1 q2 15
T12=[cos(q2) -sin(q2) 0 0;sin(q2) cos(q2) 0 0] % 0 0 0 1
T23=[cos(q1) -sin(q1) 0 0;sin(q1) cos(q1) 0 0] % 0 0 0 1
T23T=[1 0 0 1;0 1 0 0;0 0 1 0;0 0 0 1]
T23T=T23*T23
T31=T31*T31
x1M=x1M'cT31T23T
y1M=y1M'T31T23T
z1M=z1M'
end
end
</editor-fold>
```

```matlab
% file for a) position vector of the manipulator r_{1M}, b) trajectory
% of the manipulator y_{1M} = y_{1M}(x_{1M}) and position x_{1M} = x_{1M}(t), y_{1M} = y_{1M}(t)

Solution of the position vector $r_{1M}$, position $x_{1M}$ and $y_{1M}$ in symbolic form in Matlab are shown in Figure 3.

$$\mathbf{r}_{1M} = T_{12} \cdot T_{23} \cdot r_{3M} = T_{Z6}(\varphi_2) \cdot T_{Z6}(\varphi_3) \cdot T_{Z1}(l_2) \cdot r_{3M} = \begin{bmatrix} c \varphi_2 & -s \varphi_2 & 0 & 0 \\ s \varphi_2 & c \varphi_2 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c \varphi_3 & -s \varphi_3 & 0 & 0 \\ s \varphi_3 & c \varphi_3 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & l_2 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} c \varphi_2 c \varphi_3 & s \varphi_2 s \varphi_3 & -s \varphi_2 c \varphi_3 & c \varphi_2 s \varphi_3 \\ c \varphi_3 & -s \varphi_3 & 0 & 0 \\ s \varphi_3 & c \varphi_3 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} l_3 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

(7)

Position vector of point M with respect to the base coordinate system $O_1, x_1, y_1, z_1$:

$$\mathbf{r}_{1M} = \begin{bmatrix} x_{1M} \\ y_{1M} \\ z_{1M} \end{bmatrix} = \begin{bmatrix} (c \varphi_2 c \varphi_3 - s \varphi_2 s \varphi_3) l_3 + c \varphi_2 c \varphi_3 l_2 - s \varphi_2 s \varphi_3 l_2 \\ (s \varphi_2 c \varphi_3 + c \varphi_2 s \varphi_3) l_3 + s \varphi_2 c \varphi_3 l_2 + c \varphi_2 s \varphi_3 l_2 \\ 0 \end{bmatrix}$$

(8)

Fig. 2. M – file for a) position vector of the manipulator $r_{1M}$, b) trajectory of the manipulator $y_{1M} = y_{1M}(x_{1M})$ and position $x_{1M} = x_{1M}(t)$, $y_{1M} = y_{1M}(t)$

Solution of the position vector $r_{1M}$, position $x_{1M}$ and $y_{1M}$ in symbolic form in Matlab are shown in Figure 3.
Fig. 3. Solution in Matlab of the position vector $r_{1M}$ of the manipulator

The trajectory of the manipulator $y_{1M}=y_{1M}(x_{1M})$, position $x_{1M} = x_{1M}(t)$, $y_{1M} = y_{1M}(t)$ of the point M is shown in Figure 4.

Fig. 4. Trajectory of the manipulator $y_{1M}=y_{1M}(x_{1M})$, position $x_{1M} = x_{1M}(t)$, $y_{1M} = y_{1M}(t)$
Model of manipulator with 3 degrees of freedom of movement.

The manipulator in Fig. 5 is an open kinematic chain of four members 1, 2, 3, and 4. The chain is four-dimensional with 3 degrees of freedom of movement. The member 2 is rotated about the z₁ axis, the member 3 is moved along the member 2 in the z₂= z₃ direction and the member 4 moves along the member 3 in the direction of the axis x₃= x₄. We investigate the absolute movement of the member 4 and its point M. The movement of the member 4 is expressed by means of the basic decomposition to the reference point M. It is necessary to determine by the matrix method, by means of transformation matrices of basic movements the position vector $\mathbf{r}_{1M}$ (position of point M relative to base 1) velocity $\mathbf{v}_{1M}$ and acceleration $\mathbf{a}_{1M}$ of the point M relative to base 1.

We introduce the coordinate systems of individual members (Fig 5). The movement of the member 2 with respect to the base 1 is rotational, the coordinate system $O₂$, $x₂$, $y₂$, $z₂$ of the member 2 is rotated with respect to the base coordinate system $O₁$, $x₁$, $y₁$, $z₁$ by the angle $\varphi_{12}$ around the axis $z₁ ≡ z₂$. The coordinate system $O₃$, $x₃$, $y₃$, $z₃$ of the member 3 is offset by the value $ξ_{23}$ in the direction of the $z₂$ axis of the member 2. The member 4 moves on the member 3 by the value $η_{34}$ in the $x₃$ direction of the member 3. The length of the member 4 is $d₄$ and the goal is to determine the movement of the end point M.

The generalized coordinate of the rotational motion of the member 2 is $q₁=\varphi_{12}$ and the generalized coordinate of the translational motion of the member 3 is $q₂=ξ_{23}$ and the generalized coordinate of the translational motion of the member 4 is $q₃= η_{34}$. In the initial position, the coordinate systems of members 1, 2, 3, 4 coincide $q=[0 \ 0 \ 0]ᵀ$.

The position $\mathbf{r}_{1M}$, the velocity $\mathbf{v}_{1M}$ and the acceleration $\mathbf{a}_{1M}$ of the point M relative to the base coordinate system are investigated.

The motion of the member 4 with respect to the base 1 is determined by the motion of the point M and described by the equation:
The relative spherical motion is described by the transformation matrix:

$$T_{14} = \prod_{i=1}^{3} T_{i,i+1}$$

We express the individual transformation matrices using the basic matrices. In each member, we introduce coordinate systems (Fig. 5) and mark the dimensions and coordinates. Then we write the transformation matrices using the transformation matrices of the basic movements in the form:

$$T_{12} = T_{Z6}(\phi_{12})$$
$$T_{23} = T_{Z3}(\xi_{23})$$
$$T_{34} = T_{Z1}(\eta_{34})$$

Then we obtain the equation of the trajectory of the point M of member 4 in the coordinate system of the base 1 by means of the basic matrices:

$$r_{1M} = T_{12} \cdot T_{23} \cdot T_{34} \cdot r_{4M}$$

where

$$r_{4M} = [d_4 \ 0 \ b \ 1]^T$$

and

$$r_{1M} = T_{Z6}(\phi_{12}) \cdot T_{Z3}(\xi_{23}) \cdot T_{Z1}(\eta_{34}) \cdot r_{4M} =$$

$$= \begin{bmatrix}
\cos(\phi_{12}) & -\sin(\phi_{12}) & 0 & 0 \\
\sin(\phi_{12}) & \cos(\phi_{12}) & 0 & 0 \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{bmatrix} \begin{bmatrix}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & \xi_{23} \\
0 & 0 & 0 & 1
\end{bmatrix} \begin{bmatrix}
1 & 0 & 0 & \eta_{34} \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{bmatrix} \begin{bmatrix}
d_4 \\
d_4 \cos(\phi_{12}) + \eta_{34} \cos(\phi_{12}) \\
d_4 \sin(\phi_{12}) + \eta_{34} \sin(\phi_{12}) \\
\xi_{23} + b \\
1
\end{bmatrix} =$$

$$= \begin{bmatrix}
\cos(\phi_{12}) & -\sin(\phi_{12}) & 0 & 0 \\
\sin(\phi_{12}) & \cos(\phi_{12}) & 0 & 0 \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{bmatrix} \begin{bmatrix}
\xi_{23} \\
0 \\
0 \\
0
\end{bmatrix} =$$

$$= \begin{bmatrix}
x_{4M} \\
y_{4M} \\
z_{4M} \\
1
\end{bmatrix} =$$

$$\begin{bmatrix}
dx_4 \cos(\phi_{12}) + \eta_{34} \cos(\phi_{12}) \\
dx_4 \sin(\phi_{12}) + \eta_{34} \sin(\phi_{12}) \\
b + \xi_{23} \\
1
\end{bmatrix} =$$

Velocity vector of point M with respect to the base coordinate system O1, x1, y1, z1:

$$v_{1M} = \dot{r}_{1M} =$$

$$\begin{bmatrix}
\dot{x}_{4M} \\
\dot{y}_{4M} \\
\dot{z}_{4M} \\
0
\end{bmatrix} =$$

$$\begin{bmatrix}
\eta_{34} \cdot \cos(\phi_{12}) \cdot \dot{x}_4 + \eta_{34} \cdot \sin(\phi_{12}) \\
\eta_{34} \cdot \sin(\phi_{12}) + \dot{x}_4 + \eta_{34} \cdot \cos(\phi_{12}) \\
\dot{\xi}_{23} \\
0
\end{bmatrix} =$$

Acceleration vector of point M with respect to the base coordinate system O1, x1, y1, z1:

$$a_{1M} = \ddot{r}_{1M} =$$

$$\begin{bmatrix}
\eta_{34} \cdot \cos(\phi_{12}) \cdot \dot{z}_{4M} - \eta_{34} \cdot \phi_{12} \cdot \sin(\phi_{12}) + \dot{\phi}_{12} \cdot (\dot{d}_4 + \eta_{34}) \cdot \cos(\phi_{12}) \\
\eta_{34} \cdot \phi_{12} \cdot \sin(\phi_{12}) + \dot{\phi}_{12} \cdot (\dot{d}_4 + \eta_{34}) + \eta_{34} \cdot \cos(\phi_{12}) - \phi_{12}^2 \cdot (\dot{d}_4 + \eta_{34}) \cdot \cos(\phi_{12}) \\
0 \\
0
\end{bmatrix} =$$

$$= \begin{bmatrix}
\eta_{34} \cdot \cos(\phi_{12}) \cdot \dot{z}_{4M} - \eta_{34} \cdot \phi_{12} \cdot \sin(\phi_{12}) + \dot{\phi}_{12} \cdot (\dot{d}_4 + \eta_{34}) \cdot \cos(\phi_{12}) \\
\eta_{34} \cdot \phi_{12} \cdot \sin(\phi_{12}) + \dot{\phi}_{12} \cdot (\dot{d}_4 + \eta_{34}) + \eta_{34} \cdot \cos(\phi_{12}) - \phi_{12}^2 \cdot (\dot{d}_4 + \eta_{34}) \cdot \cos(\phi_{12}) \\
\dot{\xi}_{23} \\
0
\end{bmatrix} =$$

$$= \begin{bmatrix}
\eta_{34} \cdot \cos(\phi_{12}) \cdot \dot{z}_{4M} - \eta_{34} \cdot \phi_{12} \cdot \sin(\phi_{12}) + \dot{\phi}_{12} \cdot (\dot{d}_4 + \eta_{34}) \cdot \cos(\phi_{12}) \\
\eta_{34} \cdot \phi_{12} \cdot \sin(\phi_{12}) + \dot{\phi}_{12} \cdot (\dot{d}_4 + \eta_{34}) + \eta_{34} \cdot \cos(\phi_{12}) - \phi_{12}^2 \cdot (\dot{d}_4 + \eta_{34}) \cdot \cos(\phi_{12}) \\
\dot{\xi}_{23} \\
0
\end{bmatrix} =$$
Solution of the position of the point M in the Matlab program is performed by m-files (Fig. 6a, b):

```matlab
figure(5)
set(gca,'Name','Position x1M=x1M(t), y1M=y1M(t), z1M=z1M(t)')
del0=0.5;  % m
b=0.5;  % m
omega=0.35;  % rad/s,
v0=1.0;  % m/s
v04=0.1;  % m/s
v04=0.1;  % m/s


t(1:0.001:30)
x1M=x0*cos(omega*t)+v04.*t;   %m
y1M=x0*sin(omega*t)+v04.*t;   %m
z1M=x0+v04.*t;   %m

subplot(2,2,1)
plot(x1M,y1M,z1M,'w','LineWidth', 1.5);
title('Trajectory of point M of the member 4');
xlabel('x1M [m]');
ylabel('y1M [m]');
grid on
hold on

subplot(2,2,2)
plot(x1M,y1M,'w','LineWidth', 1.5);
title('Position x1M=x1M(t) of the member 4');
legend(['x1M(t)']);
xlabel('t [s]');
ylabel('x1M [m]');
grid on

subplot(2,2,3)
plot(x1M,y1M,'w','LineWidth', 1.5);
title('Position y1M=y1M(t) of the member 4');
legend(['y1M(t)']);
xlabel('t [s]');
ylabel('y1M [m]');
grid on

subplot(2,2,4)
plot(x1M,z1M,'w','LineWidth', 1.5);
title('Position z1M=z1M(t) of the member 4');
legend(['z1M(t)']);
xlabel('t [s]');
ylabel('z1M [m]');
grid on
```

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**Fig. 6.** M-file of the trajectory and a) position $x_M = x_M(t)$, $y_M = y_M(t)$, and $z_M = z_M(t)$, b) position $y_M = y_M(x_M)$, $z_M = z_M(y_M)$, $z_M = z_M(x_M)$.

The trajectory and position $x_{1M}=x_{1M}(t)$, $y_{1M}=y_{1M}(t)$, $z_{1M}=z_{1M}(t)$ of the point M is shown in Fig. 7.

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**Fig. 7.** Trajectory and position $x_{1M}=x_{1M}(t)$, $y_{1M}=y_{1M}(t)$, $z_{1M}=z_{1M}(t)$ of the manipulator.
The trajectory and position $y_{1M}=y_{1M}(x_{1M})$, $z_{1M}=z_{1M}(x_{1M})$, $z_{1M}=z_{1M}(y_{1M})$ of the point $M$ is shown in Figure 8.

**Computer simulation in MSC Adams software.** An example of how to use Adams to simulate the movement of a R-R-T-R model manipulator is in the following section.

We create a model of the R-R-T-R manipulator with the basket according to Fig. 9a)-c) using modeling elements and procedures for building body, geometric and kinematic links in MSC.ADAMS/View and verifying its functionality. The manipulator consists of the base part on which is mounted the stand. There is an arm with a basket at the end. Once the model is assembled, another task is to investigate the endpoint movement. The solution is shown in graphical form. A preview of the assembled model of the manipulator and the simulation of its movement is shown in Fig. 9a)-f).
The trajectory of the end-effector during the simulation is shown in the Fig. 10.

![Fig. 10. Model of the manipulator- trajectory of the end-effector](image)

Movement is depicted using the Postprocessor in Fig. 11.

![Fig. 11. Position $x_M$, $y_M$, $z_M$ and position vector $r_M$ of the end effector](image)

The position $x_M=x_M(t)$, $y_M=y_M(t)$, $z_M=z_M(t)$ and magnitude of the position vector $r_M=r_M(t)$ of the point M of the end effectors in Postprocessor is shown in Figure 11.

**Conclusion.** This work deals with the problem of kinematic analysis of an open kinematic chain of an industrial robot. The aim was to determine the kinematic properties and also to evaluate the influence of the parameters of the mechanism which influence these kinematic properties. The matrix method was used. The process of the solution consisted of determining the transformation matrices of the coordinate systems, the kinematic analysis of the industrial robot and the graphical representation of the effector handling space. The analysis also includes graphical representations of the kinematic properties of the mechanical system.

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Аналіз останніх досліджень і публікацій. MSC Adams представляє динамічні симулятори віртуальних прототипів механічних систем. Віртуальні прототипи дозволяють моделювати, аналізувати і оптимізувати майбутні продукти і вивчати їхні властивості, перед ніж створювати реальний прототип. Цей прийом підходить для розробки мініатюрних мехатропних елементів, а також складних систем.

Виділення недосліджених частин загальної проблеми. Віртуальні прототипи становлять собою відповідний ресурс для тестування процедур контролю і регулювання.

Постановка завдання. Компіляція віртуального прототипу механічної системи, яка має всі вирішальні особливості і є стабільною з точки зору обчислень.

Висновки відповідно до статті. Мета полягала в тому, щоб визначити кінематичні властивості, а також оцінити вплив параметрів механізму, які впливають на ці кінематичні властивості. Був використанний матричний метод. Процес рішення складався з визначення матриць перетворення систем координат, кінематичного аналізу промислового робота і графічного представлення простору маніпулювання виконавчого пристрою.

Ключові слова: віртуальна модель; відкритий кінематичний ланцюг; роботизована система; програмне моделювання; виконавчий пристрій; матриці перетворення.

Рис.: 11. Бібл.: 17.

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