Article

Optimal Phase Arrangement of Distribution Transformers for System Unbalance Improvement and Loss Reduction

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Abstract: This paper presents an efficient strategy for transformer planning to reduce the system losses by means of transformer rearrangement. The customer connected to the distribution transformer are first investigated by the field survey, and the loads of the various customers are collected from the customer information system (CIS) and distribution database system (DAS) to derive their load patterns. The objective function is to minimize the total line loss in the 24 intervals. An improved bacterial foraging algorithm (IBFO) is proposed herein to find the optimal phase combination of distribution transformers to minimize the total line loss by considering operating constraints. A three-phase load flow program with Equivalent current injection (ECT) is used to solve the total line loss and system unbalance factor on a Taipower distribution system. The results can help operators not only perform the proper installation phase selection of distribution transformers, but also reduce the system losses, decrease the system unbalance factor, and improve the voltage profiles of the buses.

Keywords: unbalance factor; distribution system; bacterial foraging optimization; taipower system

1. Introduction

In Taiwan, the Taiwan Power Company (Taipower) usually uses two single-phase transformers to connect to an Open-Wye/Open Delta transformer for serving both the single-phase and three-phase loads, and it is more economical for transformer management [1]. In Taipower distribution system, there exist a number of Open-Wye/Open-Delta transformers for the sake of economic and future expansion considerations [2,3]. A distribution feeder inherently produces the three-phase unbalance due to the lack of a third transformer and the two kinds of load served. This causes the phase voltage and current along a distribution feeder to become unbalanced. The unbalanced situations will lead to extra line losses, communication obstruction, and shorter service life of equipment [4,5]. A serious issue is that the grounding relay will trip due to the phase unbalance. The power quality and operation efficiency in the distribution system will also be reduced.

In general, the capacity selection of a distribution transformer is mostly based on the peak of the load. An Open-Wye/Open Delta transformer or three-phase transformer may simultaneously serve both the single-phase loads and three-phase loads. The loads changed in the three phases try to balance the current of three phases by using a transformer connected rearrangement. The process of transformer rearrangement ensures distribution loads on three phases to balance the current flow in the distribution system. It makes the neutral current the lowest, thereby having minimal line loss in the distribution feeder. Due to Open-Wye/Open Delta transformer’s reconnection on the secondary side is not easily implemental, and field operators may not know how the changes will reflect on the prime side. This research tried to resolve the problem by load re-assignment through prime phase re-sequencing. Both the system balance and line loss problems were considered in this paper.
In the past, there is not much research literature on transformer rearrangement. Genetic algorithm (GA) was used to optimize the phase arrangement of distribution transformers connected for improving the system unbalance and loss reduction [6]. By considering the voltage-dependency of loads, particle swarm optimization (PSO) is applied for the phase-balancing of distribution feeder [7]. An NSGA-II application for phase balancing of primary distribution circuits by the reconnection of circuit laterals and distribution transformers was implemented to minimize both line losses and unbalance factor [8]. An expert system is proposed to take the rephase strategy of distribution transformers to improve the three-phase balancing of the distribution system [9]. Bird-mating is adopted to assist in the coordinated switching of phase connection in Open-Wye/Open Delta transformers to achieve better voltage balance [10]. An automatic phase load balancing methodology is proposed herein which can balance the load on three phases of the distribution transformers [11]. Linear programming and dynamic programming were integrated to find the optimal phase arrangement of a distribution transformer for a feeder [12,13]. A three-phase load flow program is used to calculate the line losses in cases of transformer rearrangement, optimal load diversity, and mixed-type.

The problem for the phase arrangement of a distribution transformer can be formulated as a non-linear mixed-integer combinatorial optimization problem, which can be obtained by a complete enumeration of all feasible combinations. It involves high complexity in the search space, which manifests itself in the form of complicated constraints imposed on variables and the probable large number of variables in the searching process. To determine the best operating system, an efficient tool is needed to solve this problem. The purpose of this paper is to propose an improved bacterial foraging algorithm (IBFO) as a new approach in solving the optimal phase arrangement of the distribution transformers problem. Bacterial foraging optimization (BFO) is a nature-inspired optimization algorithm, which introduces the foraging behavior of bacteria based on competitive–cooperative mechanism [14]. In the past, BFO was successfully applied to various fields of power system optimization [15–19]. Improved BFO has also been successfully applied to optimize some problems in engineering and scientific fields [20–24]. The integration of gradient particles swarm (GPSO) and BFO was proposed to solve the optimization of distributed generation [20]. The standard benchmark problems with a large number of local optimal solutions are used for examples and solved by Chaotic BFO [21] and effective BFO [22]. Particle swarm optimization and BFO were integrated to solve the optimal schedule strategy for the active distribution network problem [23]. A GA-BFO algorithm was proposed to improve the security of the heterogeneous network routing protocols [24]. By combining BFO and stochastic weight trade-off (SWT) [25], this paper proposed another version of IBFO in order to refine the solution quality. For the first time, the proposed IBFO is applied to the phase arrangement of distribution transformers. A three-phase load flow program with the equivalent current injection (ECI) [26] is used to analyze the effect of the IBFO on a practical distribution feeder. Simulation results can help operators to improve the system unbalance and voltage profile, as well as enhance the operating efficiency of the distribution system.

2. The Problem Description

2.1. Transformer Connection Types

Figure 1 shows loads of the Open-Wye/Open Delta transformers meant to serve both the single-phase and three-phase loads. The loads at the secondary lateral consist of the single-phase and three-phase loads, which are equivalently represented by two individual phases ($S_A$ and $S_B$) at the primary lateral. The load at each phase is expressed as Equations (1)–(3). As it does not matter what type of transformer needs to be connected to the feeder, many schemes can be selected to connect to the phases A–C of the primary lateral in the various connected arrangements. The possible connection schemes for the various types of each transformer are listed in Table 1.

$$S_A = S_{AN} + S_{BN} + S_{AB} + S_{AC} < 60^\circ + \frac{S_{AB}}{\sqrt{3}} < 30^\circ$$ (1)
\[ S_B = S_{BC} + S_{AC} < -60^\circ + \frac{S_{3\phi}}{\sqrt{3}} < -30^\circ \]  

(2)

\[ S_C = 0 \]  

(3)

In Table 1, the arrangement of the equivalent loads in the primary lateral has 6 connection types, 3 connection types, and 3 connection types for the \( 3\phi \) transformers, Open-Wye/Open Delta transformer, and single-phase transformer. The main purpose of this paper is to find the optimal scheme for the transformer connection to minimize the real power line losses and improve the voltage unbalance factor.

### 2.2. Transformer Equivalent Load

In the Taipower distribution system, the record of each customer in the Customer Information System (CIS) must be connected to a transformer secondary side in the Distribution Database System (DAS). The power consumption of each customer is recorded in the CIS. Since a distribution transformer may simultaneously serve the mixed loading of various customers, the transformer loads can be estimated based on each customer type. By using CIS and DAS, the phase hourly loads in the primary side can be derived based on the connection of the transformer, the loads on the secondary side, and their corresponding load patterns. In this paper, the phase hourly load of each distribution transformer is calculated by the field survey and typical load patterns. The percentage of hourly energy consumption over one day is calculated by Equation (4) and the hourly real power consumption of each load customer is solved by Equation (5). Therefore the transformer loading can be easily obtained by summing the hourly loading of each customer served by the transformer as expressed in Equation (6). By considering the load growth of customers:

\[ PART_{it} = \frac{PAR_{it}}{\sum_{i=1}^{n} PAR_{it}} \]  

(4)
\[ P_{it} = \text{PART}_{it} \times \frac{PKWH}{N\text{DAY}} \times (1 + r)^m \] (5)

\[ P_{tr} = \sum_{i=1}^{n} P_{it}. \] (6)

2.3. The Objective Function for Phase Rearrangement of Transformers

The objective function for phase rearrangement of transformers is to minimize the total line loss during the 24 intervals. The loss-minimizing problem can be formulated as:

\[ \text{Min. Obj}(\bullet) = \sum_{t=1}^{24} P_{loss}^t(T_S). \] (7)

The objective function of \( P_{loss}^t \) is defined as follows:

\[ P_{loss}^t = \frac{1}{2} \sum_{i=1}^{NB} \sum_{j=1}^{NB} \text{Re}[Y_{ij}] |V_i|^2 + |V_j|^2 - 2|V_i||V_j|\cos \theta_{ij}. \] (8)

The voltage and current constraints are considered in Equations (9)–(11). Any combination which violates the following constraints is no longer selected:

\[ V_{\text{min}} \leq V_i \leq V_{\text{max}} \] (9)
\[ |I_{ij}| \leq I_{\text{max}} \] (10)
\[ |I_n| \ll I_{n\text{max}}. \] (11)

The fitness function is defined as:

\[ \text{Fit}_i(x_i) = \text{Obj}(x_i) + \sum_{n=1}^{\text{ineq}} \lambda_{\text{ineq},n} \left| g(x_i) - g_{\text{lim}} \right|^2, \] (12)

where \( \text{Obj} \) is the objective function, \( g(x_i) \) is the inequality constraints such as Equations (9)–(11); \( x_i \) is the state value of \( i \)-th bacterium; \( \text{ineq} \) is the number of inequality constraints; \( \lambda_{\text{ineq},n} \) is the penalty factor that can be adjusted in the optimization procedure; and \( g_{\text{lim}} \) is defined by:

\[ g_{\text{lim}} = \begin{cases} 
  x_i & \text{if } x_{i,\text{min}} \leq x_i \leq x_{i,\text{max}} \\
  x_{\text{min}} & \text{if } x_i < x_{i,\text{min}} \\
  x_{\text{max}} & \text{if } x_i > x_{i,\text{max}} \end{cases}. \] (13)

In accordance with IEEE ANSI standard, the voltage unbalance factor of the \( i \)-th bus is defined as Equation (14):

\[ VU = \frac{3 \times (V_i^{\text{max}} - V_i^{\text{min}})}{(V_i^A + V_i^B + V_i^C)} \times 100\%. \] (14)

3. Solution Algorithm

BFO was developed by [14] for numerical optimization in 2005; this search algorithm is based on the mechanism of bacterial foraging behavior. BFO is similar to random search methods, but does not contain complicated mechanisms such as crossover or mutation. BFO generates a set of initial solutions, known as E. coli, and then searches for the optimal value through iteration evolution. More importantly, every bacterium has a memory capacity, and can provide a one-way message to the population. Thus, the search process of BFO is the process of following the current optimal solution. For example, if the
bacterium meets a good environment, it will continue to swim in the same direction. Otherwise, it will use the tumble method to seek another direction. Bacteria must constantly move in the process of evolution and gradually tend to move to a better environment for a better solution. This paper proposes IBFO, which integrated the Stochastic Weight Trade-off (SWT) in BFO to improve the local searching ability of individuals. The concept of IBFO is to preserve the balance between global exploration and local exploitation by trading off stochastic weight with using dynamic acceleration coefficients trade-off. The mechanism increased the diversity of bacterial chemotaxis to avoid premature convergence. IBFO was developed as follows.

3.1. Bacterial Chemotaxis

Traditional bacterial chemotaxis is described as Equation (15).

\[ x'_{j,n} = x_{j,n}^p + AD \times C_p, \ j = 1, \ldots, J \ \text{and} \ n = 1, \ldots, N \]  

(15)

\[ x_{j,n}^{p+1} = \begin{cases} x_{j,n}^p & f_{it_n} < f_{it_n}^p \\ x_{j,n}^p & \text{otherwise} \end{cases} \]  

(16)

In the process of bacterial chemotaxis, it simply relies on the moving distance \( C_p \) and the tumble direction \( AD \); the useful chemotaxis messages are not transmitted between the bacteria. This could lead to a local minimum. Thus, Equation (15) is modified by Equation (17):

\[ x'_{j,n} = x_{j,n}^p + C_p' \times \xi_j r_1 \text{Sign}(r_2) \Delta D, \]  

(17)

where \( r_1, r_2 \): Random number between 0 and 1 and \( \text{Sign} \) is a freak factor, which is defined as:

\[ \text{Sign}(r_2) = \begin{cases} 1 & r_2 > P_{let} \\ -1 & r_2 \leq P_{let} \end{cases} \]  

(18)

where \( P_{let} \): The probability of “lethargy”, \( C_p' \) is the distance factor, which is varied with the stage of the optimization process [27]:

\[ C_p' = (C_{p_{\max}} - C_{p_{\min}}) \frac{S}{S_{\max}} + C_{p_{\min}}' \]  

(19)

where \( \xi_j \) is a control parameter used to reduce the stochastic effect linearly, \( \xi_j \) also varies with the stage of optimization process:

\[ \xi_j = (\xi_{min} - \xi_{max}) \frac{S}{S_{\max}} + \xi_{max} \]  

(20)

The bacterial chemotaxis in Equation (17) is controlled by a factor of \( \xi_j r_1 \text{Sign}(r_2) \). This term is referred to as the “stochastic trade-off control factor.” Using the linearly decreasing method would take longer global exploration than the nonlinearly decreasing method, and reduce the individual’s risk of missing the promising area. The values of maximum iterations \( \xi_{min}, \xi_{max} \) and \( P_{let} \) are set to 0.5, 2.5, and 0.5, respectively.

3.2. Bacterial Reproduction

After a period of bacterial chemotaxis, there is an obvious difference in the fitness value of the bacterium. For the reproduction process, the bacteria are sorted in order of ascending fitness value and the healthiest bacteria is split into two bacterium, which are placed at the same location. A bacterium with a better fitness value replicates a bacterium identical to itself. In this paper, the reproduction
process is set at 20% bacterial replication after 20 times of the chemotaxis process. The formulation of bacterial reproduction is described as follows:

\[
\text{if } k_1 < P_{re} \text{ then } k_1 = k_1 + 1 \\
\text{else } \\
\hat{f}t_{N_{re}} = \text{sort} \{ \hat{f}t_{1}^{p}, \hat{f}t_{2}^{p}, \ldots, \hat{f}t_{N}^{p} \} \text{ and } k_1 = 0.
\]

(21)

3.3. Elimination-Dispersal

The elimination-dispersal of the bacteria in the population is set on the number of chemotaxis \(P_{ed}\). A set \(P_{e} = [j \times N]\) is randomly generated after the \(P_{ed}\) chemotaxis. If the generated random variable \((\text{rand})\) is less than the elimination-dispersal rate \(N_{ed}\), the state value of the bacterium is eliminated, and a new bacterium is generated by Equation (22).

\[
\text{if } k_2 > P_{ed} \text{ then } k_2 = k_2 + 1 \\
\text{else} \\
\text{if } P_{ed} \leq N_{ed} x_{j,n}^p = x_{j,\text{min}} + \text{rand} \times (x_{j,\text{max}} - x_{j,\text{min}}) \text{ and } k_2 = 0.
\]

(22)

The phase rearrangement of distribution transformers is expressed in discrete state, so the initial solution is obtained by assigning an integer value for the operating status of each bacterium. The feasibility status is assured by the following equations:

\[
x_{j,n}^p = x_{j,\text{min}} + \text{round} \left( \text{rand} \times (x_{j,\text{max}} - x_{j,\text{min}}) \right),
\]

(23)

where \(x_{j,n}^p = [x_{j,1,n}^p, x_{j,2,n}^p, \ldots, x_{j,n,n}^p, \ldots, x_{j,N-1,n}^p, x_{j,N,n}^p]\) is the \(n\)-th connected status of distribution transformers corresponding to the \(j\)-th bus. The bacterial chemotaxis is re-defined as in Equation (24):

\[
\text{if } r \geq 0.5 \text{ then } x_{j,n}^p = x_{j,n}^p + \text{round}(\Delta D \times (x_{j,\text{gbest}} - x_{j,n}^p)) \\
\text{else} \text{ then } x_{j,n}^p = x_{j,n}^p + \text{round}(\Delta D \times C^p)
\]

(24)

Figure 2 is the flowchart of IBFO applied.
4. Case Study

To demonstrate the effectiveness of the IBFO, a practical feeder with 27 buses was selected for analyzing the efficiency, as shown in Figure 3. The load, which is served by this feeder, includes residential, commercial, and several small-industrial customers. There were about 2952 different customers planning to be connected with this feeder. The total capacity of connected transformers was 8600 KVA and a summary of these transformers is listed in Table 2.
Table 2. Summary of distribution transformer.

| Transformer Type         | The No. of Transformer | Total Capacity (KVA) |
|--------------------------|------------------------|----------------------|
| Three-phase              | 7                      | 3500                 |
| Open-Y/open-Δ            | 10                     | 5000                 |
| Single-phase             | 1                      | 100                  |
| Total                    | 18                     | 8600                 |

4.1. Voltage Profile Improvement

Table 3 is the optimal phase connection of distribution transformers after the IBFO. The load phase of the transformer connections of busses 3, 6, 7, 12, 18, 25, 26 do not need to be changed, while the busses 13, 15, 20, 27 need to change the load phase of the transformer once, and busses 4, 8, 10, 11, 17, 21, 24 require changing twice, while only bus 17 needs to change the load phase three times.
Table 3. The optimal phase connected to distribution transformers.

| Bus No. | Transformer Type | Original Connected | Phase Rearrangement |
|---------|------------------|--------------------|---------------------|
| 3       | $2\phi$          | A,B                | -                   |
| 4       | $2\phi$          | A,B                | B to C, C to A      |
| 6       | $3\phi$          | A,B,C              | -                   |
| 7       | $2\phi$          | A,B                | -                   |
| 8       | $3\phi$          | A,B,C              | A to C, - C to A    |
| 10      | $3\phi$          | A,B,C              | A to C, - C to A    |
| 11      | $3\phi$          | A,B,C              | A to C, - C to A    |
| 12      | $3\phi$          | A,B,C              | -                   |
| 13      | $2\phi$          | B,C                | - C to A           |
| 15      | $2\phi$          | A,B                | A to C, -          |
| 17      | $3\phi$          | A,B,C              | A to B, B to C, C to A |
| 18      | $2\phi$          | B,C                | -                   |
| 20      | $3\phi$          | A,B,C              | - B to C           |
| 21      | $2\phi$          | A,C                | A to C, C to B     |
| 24      | $2\phi$          | B,C                | B to A, C to B     |
| 25      | $1\phi$          | B                  | -                   |
| 26      | $2\phi$          | A,B                | -                   |
| 27      | $2\phi$          | A,B                | A to C, -          |

Note: A to C is changed from phase-A connection to phase-C connection.

Figures 4 and 5 show the three-phase voltage profiles of each bus before and after phase rearrangement at the light load period (6 am), respectively. In the Figures 4 and 5, the minimum voltage of each bus is operated from 0.958 p.u. to 0.976 p.u. before the phase rearrangement and from 0.972 p.u. to 0.985 p.u. after the phase rearrangement, respectively. It is obvious that the voltage profiles can be improved after the phase rearrangement.

Figure 4. The three-phase voltage profiles of each bus before phase rearrangement at the light load period.
Figures 6 and 7 show the three-phase voltage profiles of each bus before and after the phase rearrangement at the heavy load period (2 pm), respectively. In Figure 6, the minimum voltage of phase A is about 0.943 p.u., which violates the operational constraints. After the phase rearrangement, the minimum voltage of phase A is promoted to 0.976 p.u. and the three-phase voltage profiles of each bus are simultaneously improved to safe operation.

Figure 5. The three-phase voltage profiles of each bus after phase rearrangement at the light load period.

Figure 6. The three-phase voltage profiles of each bus before the phase rearrangement at the heavy load period.

Figure 7. The three-phase voltage profiles of each bus after the phase rearrangement at the heavy load period.
4.2. Unbalance and Loss Improvement

Figure 8 demonstrates the daily system unbalance profiles at the swing bus (bus 1) and Figure 9 is the total line loss profiles at each hour. The unbalance factor between 9 am and 5 pm is much larger than the other periods. The unbalance factor at the peak load was from 23%–24% to 2%–7% by using the phase arrangement of distribution transformers. In Figure 8, it is clearly observed that phase rearrangement introduces a lower unbalance factor than that without phase rearrangement. At the same time, the total line loss is improved and total line loss was also reduced from 980.09 kW to 659.01 kW.

![Figure 8](image_url)

**Figure 8.** The daily system unbalance profiles at the swing bus (bus 1).

![Figure 9](image_url)

**Figure 9.** The total line loss profiles.

4.3. Convergence Test

Figure 10 illustrates the convergence characteristics of GA, PSO, BFO, and IBFO. The tests were carried out on an Intel i5-7300HQ 2.5 GHz CPU and 16 GB DRAM memory. We set 100 iterations as the stopping condition for each algorithm. In Figure 10, the fitness value of IBFO can converge to a lower value than other algorithms. The operational time of the IBFO is slightly longer than that of the BFO but faster than GA. Regarding the calculation stability of the optimal solutions, IBFO reach convergence after about 82 iterations and has better convergence than the other algorithms. Table 4 shows the maximum, minimum, and average optimized loss with 100 test runs. In the 100 times of
repeated resilience testing, the average converged loss of IBFO, BFO, PSO, and GA are 730.84 kW, 761.16 kW, 826.08 kW and 869.46 kW, respectively. It shows the capacity of IBFO to explore a more likely global optimum than other algorithms. The results show that it is better than the PSO, BFO, or GA, which demonstrates that the IBFO is best.

![Fitness value x10^3](image)

**Figure 10.** The convergence characteristics of genetic algorithm (GA), particle swarm optimization (PSO), bacterial foraging optimization (BFO), and IBFO.

|                         | GA    | PSO   | BFO   | IBFO  |
|-------------------------|-------|-------|-------|-------|
| Maximum converged loss (kW) | 1031.12 | 969.09 | 906.98 | 854.80 |
| Minimal converged loss (kW)    | 695.57  | 677.11 | 667.68 | 659.01 |
| Average converged loss (kW)     | 869.46  | 826.08 | 761.16 | 730.84 |
| CPU time (sec)                | 84.81   | 48.67  | 60.82  | 69.94  |

**Table 4.** The comparison of GA, PSO, BFO, and IBFO.

5. Conclusions

This paper presents an efficient strategy-based IBFO algorithm to find out the optimal phase assignment for the overall transformers in a distribution feeder. The minimal total line loss is formulated as the objective function. IBFO process swaps the phase-type of transformers to accomplish the appropriate arrangement of transformers. According to the optimal phase assignment of the transformer and an actual Taipower distribution feeder, the system losses and unbalance factor are solved by the three-phase load flow analysis. With the advantages of heuristic ideals, IBFO supersedes the conventional ideals threefold: the complicated discrete problem is solvable with better performance and the more likelihood of deriving a global optimum than AI methods. By comparing the other algorithms, IBFO is sufficient evidence to show that the transformer rearrangement method is both effective and efficient. The results show that the unbalance factor and total line loss can be improved by the IBFO algorithm. The IBFO algorithm has great potential for further applications to many other mixed-integer combinational optimization problems in power system planning and operation.

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Nomenclature

\( S_A, S_B, S_C \) the equivalent loads for A, B, C phase

\( S_{AN}, S_{BN} \) the A-phase and B-phase loads connected to the neutral wires

\( S_{AB}, S_{AC}, S_{BC} \) the single-phase loads connected to the two-wire

\( S_{3∅} \) the three-phase load

\( P_{AR} \) per unit load at hour \( t \) of load customer \( i \)

\( PARt \) percentage of hourly energy consumption over a daily period of load customer \( i \)

\( PKWH_i \) monthly energy consumption of customer \( i \) in CIS

\( NDAY \) the number of monthly days

\( P_{it} \) hourly real power demand of customer \( i \)

\( P_{tr} \) transformer hourly loading at hour \( t \)

\( n \) the number of customers

\( r \) the rate of load growth of the customer

\( m \) the time period of load forecasting

\( P_{loss} \) The total line loss of distribution feeders at \( t \)-th time

\( T_{S} \) the status of phase arrangement

\( NB \) the total number of branches in the feeder

\( V_i \) the voltage of \( i \)-th bus

\( Y_{ij} \) the admittance of branch

\( \theta_{ij} = \theta_i - \theta_j \) the voltage phase angle difference between bus-\( i \) and bus-\( j \)

\( I_{max} \) upper limit of branch current magnitude

\( V_{min}/V_{max} \) lower/upper limit of bus voltage magnitude \( (V_{min} = 0.95/V_{max} = 1.05) \)

\( I_{n} \) the neutral line current

\( I_{maxn} \) the maximal value of \( I_{n} \) current

\( x_j^{p,n} \) the \( j \)-th state value of \( n \)-th bacterium at the \( p \)-th chemotaxis.

\( j \) the \( j \)-th state value of the bacterium, a bacterium combined by \( J \) state values into a complete solution

\( N \) The total number of bacteria

\( \Delta D \) the tumble direction vector of the bacterium \( \Delta D \in [-1, 1] \)

\( C_p \) The distance for the bacterium at each step

\( x_{j,n}^{p} \) State value of the \( n \)-th bacterium after the \( p \)-th chemotaxis

\( f_{n}^{p} \) The fitness value of the \( n \)-th bacterium at the \( p \)-th chemotaxis

\( f_{fitr}^{p} \) The fitness value of the \( n \)-th bacterium after the \( p \)-th chemotaxis

\( x_{j,n}^{p+1} \) State value of the \( n \)-th bacterium after the \((p+1)\)-th chemotaxis

\( k_1 \) The count of the bacterial reproduction

\( P_{re} \) The number of chemotaxis process

\( N_{re} \) The number of bacterial reproduction

\( sort \) The fitness values sorted after the chemotaxis procedure

\( k_2 \) The count of bacterial elimination

\( P_{ed} \) The number of chemotaxis

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