Heavy Metals Removing from Municipal Solid Waste Incineration Fly Ashes by Electric Field-Enhanced Washing

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Received: 4 January 2020; Accepted: 7 February 2020; Published: 10 February 2020

Abstract: Municipal solid waste incineration (MSWI) fly ash contains chlorides, heavy metals, and organic pollutants, which requires appropriate disposal to eliminate this risk. In this study, the effects of agents on heavy metals removal from MSWI fly ash by electric field-enhanced washing were systematically studied. The results show that when these fly ashes were washed at a current density of 35 mA/cm², polarity switching frequency of 40 Hz, Ethylenediaminetetraacetic acid (EDTA) dosage of 0.5 mol/L, and a pH of 2 for 4 h, almost all of the Cd and Ni could be removed, with a removal efficiency of 100.00% and 99.59%, respectively. Meanwhile, it also shows a significant effect on Cu and Zn, with a removal efficiency higher than 85%. After washing, the results of the sequential extraction procedure showed that the residual forms of Pb, Cu, Zn, Cd, Ni, and As increased obviously. According to GB5085.3-2007, the toxicity of the treated MSWI fly ash were below their thresholds of 5 and 1 mg/L for Pb and Cd, respectively. Thus, a novel technology for heavy metals removal from MSWI fly ash is proposed.

Keywords: MSWI fly ash; electric field; heavy metals; harmless

1. Introduction

As the sharp increasing growth of economy and the significant acceleration of urbanization, about two-thirds of Chinese cities are suffering from “garbage siege” [1]. Statistically, in 2017, the municipal solid waste (MSW) produced by 202 large and medium-sized cities nationwide amounted to 20 million tons, increasing by approximately 8–10% annually. Incineration is widely used to deal with MSW, owing to its advantages of good capacity reduction, high degree of harmlessness, and high energy efficiency [2]. It is reported that China has built and operated 220 MSWI plants in large and medium-sized cities over the past decades, with an incineration capacity of 219,000 tons/day, 62 million tons per year, accounting for 26.9% of China’s annual waste disposal volume. However, in the process of incineration, about 3–5% municipal solid waste incineration (MSWI) fly ash will be produced [3]. Due to its fine size and large specific surface area, MSWI fly ash is prone to enrich not only heavy metals in high concentrations, but also dioxins, which are highly toxic and powerful carcinogenic organic pollutants, thus posing serious risk to the environment and human beings [4]. Therefore, MSWI fly ash has been classified as a hazardous waste and requires effective treatment prior to landfill or comprehensive utilization.
MSWI fly ash disposal are mainly “solidification/stabilization + landfill”. Various treatment techniques, including cement solidification, chemical stabilization, and vitrification, etc., must be adopted before landfill to alleviate the toxicity. Cementitious materials, such as cement [5], asphalt [6], or stabilizing chemicals [7], are mixed and reacted with MSWI fly ash, and heavy metals are wrapped into hard solidified bodies. Solidification/stabilization, as a mature technology, has become the dominant method for the disposal of MSWI fly ash in most countries. However, solidification results in an increase of 1.5–2.0 times in final landfill volume and 30% in mass. The long-term environmental safety assessment of treated MSWI fly ash needs to be further verified [8].

Generally, it is significant to pre-treat the MSWI fly ash before hazard-free treatment or recycling, for mitigating the corrosion of disposal equipment or the adverse effect on the quality of resource products. With the popularization and application of electrochemical technology, substantial progress has been made: it has gradually expanded from soil remediation [9] to clay [10], copper tailings [11], electrolytic manganese residue [12], converter vanadium slag [13], refractory ores [14], and refractory gold ores [15]. Meanwhile, electrons could also be used as “cleaners” under a low-intensity electric field [16]. As a highly-porous hazardous waste, MSWI fly ash contains a large number of micropores, which is beneficial to the moisture transport in the reaction system. The large amount of metal ions contained in the micropores is also advantageous for improving the ion-exchange capacity of MSWI fly ash. Therefore, the electrochemical technique is thought to be an effective method to remove heavy metals from MSWI fly ash. To improve this removal efficiency, assistant agents were adopted since they could form a stable compound with heavy metals contained in MSWI fly ash, favoring to be removed [17]. In addition, such an assistant agent must be mobilized by an electric field such as Ethylenediaminetetraacetic acid (EDTA), which was applied in contaminated soil and heavy metals waste water [18,19].

Thus, four pivotal parameters of pH, current density, extraction time, and polarity switching frequency for heavy metals removal from MSWI fly ashes by electric enhanced washing were studied. Meanwhile, the effect of EDTA during this washing process was also discussed. The results show that EDTA-assisted electric washing could effectively remove heavy metals from MSWI fly ashes, providing a perspective approach for MSWI removing, while also bringing a new application for electrochemistry.

2. Materials and Methods

2.1. Materials

MSWI fly ash used was collected from a certified MSWI plant in Beijing, China, under the bag filter, which was first dried to a constant weight at 80 °C. The chemical reagents such as NaOH, H₂SO₄, HNO₃, HCl, HF, CH₃COOH, HONH₂Cl, H₂O₂, CH₃COONH₄, and EDTA used in this study were of analytical grade expect specific claim. Deionized water was provided by the Water Purification System (Advantage A10, Millipore, Burlington, MA, USA), and all experiments were carried out at room temperature.

2.2. Electric Enhanced Washing

The experimental apparatus used in this study is shown in Figure 1. The reactor used in the experiment was a 500 mL beaker, and the anode and cathode were graphite plates (Qingdao BaoFeng graphite products Co., Ltd., Qingdao, China), having a surface area of 45 cm² (4.5 × 10 cm). The two were fixed at a distance of 10 mm. For a typical experiment, 20 g of MSWI fly ash sample was added into the beaker and blended with 0.5 mol/L EDTA, while the liquid-to-solid (L/S) ratio was fixed at 15 mL/g. In addition, a direct current power supply (KRT-3005, Shenzhen JinRang electronic technology Co. Ltd., Shenzhen, China) with a current range of 0–3 A and voltage of 0–30 V was used to provide the electric field. The beaker was placed on a thermostatic magnetic stirrer (HJ-6A, Chanzhou Ronghua instrument manufacturing Co. LTD, Chanzhou, China), stirring at an appropriate stirring speed for a set time. During this process, pH value of the reaction system was monitored by a pH meter timely which was
kept at a constant value by HNO₃ or NaOH. After extracting, the supernatant was separated from the residue by vacuum filtration and determined by Inductively Coupled Plasma Optical Emission Spectrometer (ICP-OES, Optima 8300, PerkinElmer, Waltham, MA, USA). The remaining residue was dried at 65 °C for further analysis. The removal efficiency of heavy metals in MSWI fly ash is calculated according to Equation (1):

$$\eta = (M_{\text{origin}} f_{\text{origin}} - M_{\text{residue}} f_{\text{residue}})/M_{\text{origin}} f_{\text{origin}} = 1 - (M_{\text{residue}} f_{\text{residue}}/M_{\text{origin}} f_{\text{origin}})$$  (1)

where $\eta$ means the removal efficiency of heavy metals from MSWI fly ash (%); $M_{\text{origin}}$ and $M_{\text{residue}}$ means the dry basis quality of MSWI fly ash before and after treatment (kg); and $f_{\text{origin}}$ and $f_{\text{residue}}$ means the heavy metal content in MSWI fly ash before and after treatment (mg/kg).

![Figure 1. The experimental apparatus of enhanced extracted by electric field.](image)

Heavy metal removal efficiency was investigated by examining the parameters of pH, current density, duration, and polarity switching frequency as well as EDTA dosage. The experimental arrangements are given in Table 1.

| Factors                     | Levels                |
|-----------------------------|-----------------------|
| pH                          | 2, 4, 6, 8, 10        |
| Current density (mA/cm²)    | 0, 15, 25, 35, 45     |
| Duration (h)                | 2, 4, 8, 16, 32       |
| Switching frequency (Hz)    | 0, 20, 40, 60, 80     |

2.3. Total Heavy Metal Content

Microwave digestion refers to “The technical specification for soil environmental monitoring” (HJ/T 166-2004), and it is used to digest the fly ashes before and after the leaching. First, 0.2000 g of MSWI fly ash was weighed and added into the digestion tube; then, it was blended with 6 mL of HNO₃ (69%), 2 mL of HCl (72%) and 2 mL of HF (48%). After covering lids, they were placed in the digestion tubes and treated by a microwave dissolver (Multiwave PRO, Anton Paar, Graz, Austria). After digesting according to the set temperature control procedure, they were cooled and filtered. Heavy metals such as Pb, Cu, Zn, Cd, Cr, Ni, As, and Ba in the filtrate were determined by ICP-OES.

2.4. Toxicity Characteristic Leaching Procedure

The toxicity leaching procedure specified in the standard of “Solid waste-extraction procedure for leaching toxicity—Sulphuric acid & nitric acid method” (HJT299-2007) was applied to assess the leaching toxicity of heavy metals. First, a 100 g sample was weighed and placed in an extraction bottle. According to the moisture content of the sample, the extraction agent was mixed evenly with the sample at a solid–liquid ratio of 10:1 (kg/L). Therein, an extraction agent was prepared from sulfuric
acid and nitric acid with a mass ratio of 2:1 and a pH of 3.20 ± 0.05. After that, it was fixed on an inverted oscillation device after the lid is tightened, and it was overturned at a speed of 30 ± 2 r/min for 18 ± 2 h at 23 ± 2 °C. The concentration of heavy metals in the extracting solution was determined by ICP-OES.

2.5. Sequential Extraction Procedure

Heavy metals in different chemical forms were analyzed by selective extractors. According to the extractors, it can be extracted in three steps to minimize its mutual influence. (1) Soluble and Exchangeable: 40 mL 0.11 mol/L CH₃COOH for 1.0000 g sample, oscillated for 16 h at room temperature. After being centrifuged for 20 min (4000 r/min), the liquid supernatant was filtered through a 0.45 µm membrane and retained for testing. Then, the remaining residue was added with 20 mL of deionized water, oscillated for 20 min, centrifuged for 20 min, and the liquid supernatant was discarded. (2) Reducible: using the remaining residue from the previous step as the subject, 40 mL 0.5 mol/L NH₂OH·HCl was added; then, it was oscillated at room temperature for 16 h, and the same operation as the previous step was repeated. (3) Oxidizable: 10 mL of H₂O₂ was slowly added to the residue in the centrifuge tube; then, it was covered and dissolved at room temperature for 1 h. After that, the solution was dissolved in a water bath for 1 h (85 °C); then, the lid was removed, and the water bath was heated until the solution was less than 3 mL. Afterwards, we added H₂O₂ 10 mL again and repeated the above operation. (4) Residual: the residue of the previous step was evaporated, transferred to the digestion tank, and digested.

2.6. Characterization

The sample was analyzed using an X-ray fluorescence spectrometer (XRF, UltimaIV, Rigaku, Tokyo, Japan). The mineral phase was determined by an X-ray diffractometer (XRD, Axios MAX, PANalytical B.V., Almelo, Netherlands). The micromorphology was observed by a field emission scanning electron microscope (FESEM, S-3400N, HITACHI, Tokyo, Japan). Cl⁻ was determined by an automatic potentiometric titration (888Titrando, Metrohm, Herisau, Switzerland).

3. Results and Discussion

3.1. Characteristics of MSWI Fly Ash

As can be seen from Table 2, the dominating elements in MSWI fly ash are Ca, Cl, Si, S, Na, and K, accounting for 87.01 wt %. The high Ca content in MSWI fly ash is mainly caused by the excessive lime slurry injected into the flue gas to reduce the emission of acidic gases (SO₂, HCl) [20]. Meanwhile, the plastic products, kitchen waste, and other chlorine components volatilize–condense during the incineration, so that there is a higher content of Cl (18.38 wt %) in MSWI fly ash in the form of soluble chlorine salts [21].

Table 2. Chemical composition of municipal solid waste incineration (MSWI) fly ash by X-ray fluorescence spectrometer (XRF) (wt %).

| Compound | CaO | Cl | SiO₂ | SO₃ | Na₂O | K₂O | Al₂O₃ | MgO | Fe₂O₃ | Other |
|----------|-----|----|------|-----|------|-----|-------|-----|-------|-------|
| Original Sample | 39.18 | 18.38 | 10.02 | 8.97 | 5.99 | 4.47 | 3.81 | 3.75 | 2.11 | 3.32 |

The mineralogical components of MSWI fly ash are shown in Figure 2a, and the main mineral phases of MSWI fly ash are KCl, NaCl, CaSO₄, CaClO₄, CaCO₃, SiO₂, and Ca(OH)₂, which are consistent with the results of other research studies [22,23]. It indicates that MSWI fly ash is a mixture of chloride, calcium compounds, and silicate. However, the high content of amorphous substance enhances the background position of the XRD pattern, obscuring some crystal characteristic peaks, which could not reflect the mineral phase of the metal in the MSWI fly ash [24].
The micromorphology of MSWI fly ash is shown in Figure 2b. In Figure 2b, a large amount of amorphous substances is arranged loosely with a few spherical particles and floccule. Therein, non-mineral particles are dark in color, loose and porous in structure, with spherical particles of different particle sizes and nodular calcite (CaCO$_3$) embedded on the surface, which is speculated to be secondary minerals congealed and generated in flue gas.

![Figure 2. XRD patterns (a) and SEM images (b) of MSWI fly ash.](image)

3.2. Characteristics of Heavy Metals in MSWI Fly Ash

A large amount of heavy metals is enriched in MSWI fly ash. Table 3 shows the heavy metal in MSWI fly ash and their leaching toxicity based on the extraction procedure of HJ/T 299-2007. It can be seen from Table 3 that the heavy metals in the MSWI fly ash are mostly Zn, Pb, Ba, and Cu, and their content reach to 3610.76 mg/kg, 1143.64 mg/kg, 1047.00 mg/kg, and 546.12 mg/kg, respectively. This means that the heavy metals in MSWI fly ash are not inert substances, showing a serious of extraction toxicity. Pb and Cd extracted reached 12.82 mg/L and 1.21 mg/L, which exceeded the threshold of GB 5085.3-2007 of 5 and 1 mg/L. Moreover, the leaching toxicity of Pb is more than double the standard threshold [25].

| Heavy Metals | Pb (mg/kg) | Cu (mg/kg) | Zn (mg/kg) | Cd (mg/kg) | Cr (mg/kg) | Ni (mg/kg) | As (mg/kg) | Ba (mg/kg) |
|--------------|------------|------------|------------|------------|------------|------------|------------|------------|
| Original sample | 1143.64 | 546.12 | 3610.76 | 132.48 | 176.65 | 19.35 | 123.12 | 1047.00 |
| Extraction toxicity (mg/L) | 12.82 | 1.86 | 14.12 | 1.21 | 0.28 | 0.06 | ND | 2.77 |

Table 3. Heavy metals content and their leaching toxicity in MSWI fly ash.

Annotation: “ND” Not detected.

Figure 3 shows the chemical distribution of different heavy metals in MSWI fly ash. The proportion of soluble to exchangeable forms of Cd is as high as 63.63%, and the proportion of residual form is relatively low, only 2.47%. This could be attributed to Cd being a kind of volatile heavy metal, which is easy to react with chloride to form chloride in the incineration process. It finally adsorbs to MSWI fly ash in the condensation phase. Although its total content is only 132.48 mg/kg, its mobility and bioavailability in the environment are so high that it poses a serious risk to the environment [26]. The proportions of an oxidizable form of Pb, Cu, and As reach 55.34%, 47.82%, and 70.40%, respectively, which are relatively stable. However, it still faces the risk of leaching in a strong oxidizing environment. The residual form of Ni is 50.01%, which is a much lower risk to the environment when compared to other heavy metals. The difference of heavy metal chemical distribution is mainly related to its physicochemical characteristics (volatility, melting point, boiling point); it is hardly related to the total content of heavy metal, and these results are also consistent with other research studies [27].
3.3. Effect of pH

Previous research studies show that pH is an important factor that affects the extraction of heavy metals from MSWI fly ash [28,29]. As shown in Figure 4, pH has a significant effect on the removal efficiency of heavy metals in MSWI fly ash. For Pb, Cu, Zn, Cd, and Ni, the removal efficiencies increase with the decrease of pH value, and reach the maximum at a pH of 2, which are 97.78%, 94.26%, 81.17%, 100%, and 99.59% respectively. The leaching characteristics of heavy metals in MSWI fly ash are bound up with the compounds formed. When the pH value changes, it would enhance/weaken the conversion of heavy metal to free ions in the system [30]. Under acidic conditions, heavy metals generally form metal oxides that are soluble in water, making the leaching characteristics more obvious. However, As in MSWI fly ash could only be effectively removed at a high pH value. It may be related to As existing as a stable complex of calcium or a transition metal of iron hydroxyl arsenate hydrate ($M^{2+})_2Fe_3(AsO_4)_3(OH)_4$ $\cdot$ 10H$_2$O. The complexes are degraded as the pH increases, where As is removed with the release of Ca$^{2+}$ [31].

![Figure 3. Heavy metal forms of MSWI fly ash.](image)

![Figure 4. Effect of pH on heavy metals efficiency (0.5 mol/L EDTA, 25 mA/cm$^2$, 4 h, 0 Hz).](image)

3.4. Effect of Current Density

The removal efficiency of heavy metals in MSWI fly ash, under different current densities, is shown in Figure 5. With the increasing of current density, the removal efficiency of Cu and Ni increase...
first and then plateau. When the current density is 35 mA/cm² and pH is 2, the removal efficiency of Cu can reach 94.26%, while Ni in the MSWI fly ash is basically removed, about 99.59%. The removal efficiency of As increases from 49.48% to 67.69% when the current density increases from 0 to 35 mA/cm². By changing the surface charge distribution on the face of MSWI fly ash and accelerating electron transfer in solution, the electric field can improve the removal efficiency of heavy metal [32]. However, an excess current density would cause energy waste and reduce the current efficiency.

Figure 5. Effect of current density on heavy metals efficiency (0.5 mol/L EDTA, pH = 2, 4 h, 0 Hz).

3.5. Effect of Extraction Time

In order to investigate the effect of extraction time on the removal efficiency of heavy metals in MSWI fly ash, the time intervals were selected as 2 h, 4 h, 8 h, 16 h, and 32 h. Figure 6 shows that Cd and Ni can be removed quickly: more than 90% in 2 h. The removal efficiency curves of Pb and Cu increase first and then tend to flatten as the extraction time increases. When the extraction time is 4 h, the removal efficiency of Pb and Cu reach 97.78% and 96.01%, respectively. By contrast, Zn and As require a long extraction time, and the curves do not reach equilibrium, even extending the extraction time to 32 h. It would be related to the residual forms of Zn and As, since they are higher than 34.89% and 50.00%, making it difficult to transfer from the solid phase to the liquid phase. The interaction time between MSWI fly ash and agent affects the dissolution and diffusion of heavy metals directly. If the extraction time is too short, a sufficient dissolution cannot be guaranteed. By contrast, the disposal costs will rise.
3.6. Effect of Polarity Switching Frequency

The removal efficiency of heavy metals in MSWI fly ash was investigated by periodically switching the polarity of cathode and anode. The results are shown in Figure 7. For Pb and Cu, the removal efficiency goes up with the increase of polarity switching frequency, and tends to plateau after 40 Hz. With the increase of polarity switching frequency, the removal efficiency of Ni and As increase first and then decrease, reaching their maximum at frequencies of 40 Hz and 60 Hz with values of 99.59% and 74.69%, respectively. Without polarity switching, during the extraction process, a large amount of Ca\(^{2+}\) and Mg\(^{2+}\) in the system would generate a dense oxide film adsorbing on the surface of the plate, which causes the plate to be passivated, thereby reducing the current efficiency [33]. This phenomenon was also reported by other researchers [34,35]. Polarity switching could alleviate this passivation. Under electric field, before the heavy metal ions are adsorbed on the electrodes, the motion direction will be changed due to the electrode switching.

Figure 6. Effect of extraction time on heavy metals efficiency (0.5 mol/L EDTA, 35 mA/cm\(^2\), pH = 2, 0 Hz).

Figure 7. Effect of periodically switched polarity on heavy metals efficiency (0.5 mol/L EDTA, 35 mA/cm\(^2\), pH = 2, 2 h).
3.7. Characterization of Soluble Salts in MSWI Fly Ash During Extraction Process

It can be seen from Figure 8 that Cl\(^-\) can be quickly dissolved in solution and stabilized in about 10 to 30 min. The concentration of salt in MSWI fly ash during the extraction process was as follows: Cl\(^-\) > Na\(^+\) > K\(^+\), about 0.38 mol/L, 0.08 mol/L, and 0.18 mol/L respectively. The dissolution of Cl\(^-\), K\(^+\), and Na\(^+\) is related to the rapid dissolution of soluble components, such as NaCl, KCl, K\(_2\)Ca(SO\(_4\))\(_2\)-H\(_2\)O, and the partial dissolution of insoluble aluminosilicate (K\(_2\)O·Al\(_2\)O\(_3\)·3SiO\(_2\)), Na\(_2\)O·Al\(_2\)O\(_3\)·3SiO\(_2\)·2H\(_2\)O) and chloroaluminates (3CaO·Al\(_2\)O\(_3\)·CaCl\(_2\)·10H\(_2\)O).

![Figure 8](image_url)

**Figure 8.** Composition changes in the extracting solution at different extraction times (mol/L).

3.8. Characterization of the MSWI Fly Ash under Different Conditions

The chemical composition of the original samples and samples treated by the electric field are shown in Table 4. As shown in Table 4, compared with the original sample, the proportion of CaO, Cl, Na\(_2\)O, and K\(_2\)O in MSWI fly ash decreases obviously after treated by electric field. The mass of these four before and after the treatment decrease from 68.02 wt % to 28.82 wt %. This phenomenon indicates that the soluble salts in MSWI fly ash are effectively removed after being treated.

| Compound            | CaO  | Cl   | SiO\(_2\) | SO\(_3\) | Na\(_2\)O | K\(_2\)O | Al\(_2\)O\(_3\) | MgO  | Fe\(_2\)O\(_3\) | Other |
|---------------------|------|------|-----------|----------|-----------|----------|----------------|------|----------------|-------|
| Original samples    | 39.18| 18.38| 10.02     | 8.97     | 5.99      | 4.47     | 3.81          | 3.75 | 2.11           | 3.32  |
| Electric field      | 20.35| 1.65 | 32.71     | 1.04     | 3.11      | 3.71     | 20.52         | 0.83 | 6.61           | 9.47  |

As can be seen from Figure 9a, the position of the diffraction peak of MSWI fly ash is significantly different before and after extraction. The primary mineral phases in the treated MSWI fly ash are SiO\(_2\), CaSO\(_4\), CaCO\(_3\), Ca\(_3\)Si\(_2\)O\(_7\), NaHSO\(_4\), and Al(OH)\(_3\). The diffraction peaks of KCl and NaCl in the sample treated by electric field disappear, while the diffraction peaks of SiO\(_2\) and CaSO\(_4\), which are hardly soluble in water, are present obviously. In addition, CaCO\(_3\) in MSWI fly ash reacts with H\(^+\) generated by the plate to produce CO\(_2\), which may explain the absence of Ca(OH)\(_2\) and CaClOH in treated MSWI fly ash.

\[
\text{Ca(OH)}_2 + \text{CO}_2 \rightarrow \text{CaCO}_3 + \text{H}_2\text{O} \\
2\text{CaClOH} + \text{CO}_2 \rightarrow \text{CaCl}_2 + \text{CaCO}_3 + \text{H}_2\text{O}
\]

SEM analysis of the samples is shown in Figure 9b,c. The distribution of the original sample is disordered, and a few spherical particles and floccule are overlapped (Figure 9b). As shown in
Figure 9c, the irregular particles are significantly reduced. Most of the particles in treated MSWI fly ash are smooth clumps that are about less than 10 μm in size. These results show that the shape and size of MSWI fly ash particles can be changed by the electric field.

![XRD patterns and SEM images of treated MSWI fly ash](image)

**Figure 9.** XRD patterns (a) and SEM images (b) and (c) of treated MSWI fly ash.

It can be seen from Table 5 that the extraction toxicity of Pb and Cd in the original samples is 12.82 mg/L and 1.21 mg/L, respectively, exceeding the maximum permissible concentration of GB 5085.3-2007, 5, and 1 mg/L. After the treatment, various elements in the toxicity characteristic leaching procedure are reduced. The extraction toxicity of Pb and Cd are reduced by 94.58% and 100%, respectively, which are lower than the threshold specified in the standard. In addition, the extraction toxicity of most elements, such as Zn, Cd, Cr, Ni, and As in MSWI fly ash are lower than the detection limit.

| Heavy Metals | Pb  | Zn  | Cu  | Cd  | Cr  | Ni  | As  | Ba  |
|--------------|-----|-----|-----|-----|-----|-----|-----|-----|
| Original sample | 12.82 | 1.86 | 14.12 | 1.21 | 0.28 | 0.06 | ND  | 2.77|
| Electric field strengthening | 1.78 | ND  | 1.12 | ND  | ND  | ND  | ND  | 0.49|
| GB 5085.3-2007 | 5   | 100 | 100 | 1   | 15  | 5   | 5   | 100 |

Table 5. Extraction toxicity of treated MSWI fly ash (mg/L).

Annotation: “ND” Not detected.

As can be seen from Figure 10, after the treatment, compared with original samples, the residual form of Pb, Cu, Zn, Cd, Ni, and As are increased by 46.54%, 33.47%, 34.37%, 45.27%, 52.09%, and 18.02%, respectively. When the electric field was applied, other forms of heavy metals, except residual, are continuously removed. Therefore, the electric field can not only improve the extraction ability of heavy metals in the reaction system, but also increase the proportion of stable form of heavy metals, which reduces the harm to the environment.
was 40 Hz and EDTA dosage was 0.5 mol/L, at a pH value of 2 for 4 h, the removal efficiency of Cd, Ni, and Pb is up to 100.00%, 99.59%, and 97.78%, while Cu and Zn removal efficiency is higher than 85% and As is about 74.69%. The sequential extraction procedure showed that the residual forms of Pb, Cd, and As is about 74.69%. The removal process of heavy metal in MSWI fly ash are illustrated in Figure 11. In the reaction system, MSWI fly ash is affected by the liquid diffusion and electrostatic attraction, and it is restricted by the pore solution, cations, and other substances. The surface charge polarity of MSWI fly ash will change under a certain pH, which be concerned with the reaction at the Equations (4) and (5). During this process, heavy metals release from the MSWI fly ash into the solution and react with the assistant agents to form a stable complex, as shown in Equations (6) and (7). The main reactions are as follows:

\[
2H_2O - 4e^- \rightarrow O_2↑ + 4H^+ \quad (4)
\]

\[
2H^+ + 2e^- \rightarrow H_2↑ \quad (5)
\]

\[
M^{2+} + H_2Y^2- \rightarrow MY^- + 2H^+ \quad (6)
\]

\[
M^{3+} + H_2Y^2- \rightarrow MY^- + 2H^+ \quad (7)
\]

3.9. The Main Mechanism of Pollutant Migration

The removal process of heavy metal in MSWI fly ash are illustrated in Figure 11. In the reaction system, MSWI fly ash is affected by the liquid diffusion and electrostatic attraction, and it is restricted by the pore solution, cations, and other substances. The surface charge polarity of MSWI fly ash will change under a certain pH, which be concerned with the reaction at the Equations (4) and (5). During this process, heavy metals release from the MSWI fly ash into the solution and react with the assistant agents to form a stable complex, as shown in Equations (6) and (7). The main reactions are as follows:

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\[
2H^+ + 2e^- \rightarrow H_2↑ \quad (5)
\]

\[
M^{2+} + H_2Y^2- \rightarrow MY^- + 2H^+ \quad (6)
\]

\[
M^{3+} + H_2Y^2- \rightarrow MY^- + 2H^+ \quad (7)
\]

4. Conclusions

The results of this research indicated that heavy metals could be efficiently removed by electric field enhanced washing. When the current density was 35 mA/cm², polarity switching frequency was 40 Hz and EDTA dosage was 0.5 mol/L, at a pH value of 2 for 4 h, the removal efficiency of Cd, Ni, and Pb is up to 100.00%, 99.59%, and 97.78%, while Cu and Zn removal efficiency is higher than 85% and As is about 74.69%. The sequential extraction procedure showed that the residual forms
of Pb, Cu, Zn, Cd, Ni, and As increased obviously. In addition, almost all of the K\(^+\), Na\(^+\), and Cl\(^-\) was removed at the same time as proven by XRD, XRF, and SEM. After the electric field-enhanced washing, the leaching toxicity of MSWI fly ash is greatly reduced when compared with the original samples, and metal leaching toxicity of all the elements is below all their thresholds. Therefore, electric field-enhanced washing has a perspective future in the removal of harmful substances from MSWI fly ash.

**Author Contributions:** For research articles with several authors, a short paragraph specifying their individual contributions must be provided. Methodology, Y.T. and M.C.; formal analysis, R.W. (Rui Wang) and Z.L.; investigation, X.X.; resources, X.X.; data curation, R.W. (Rong Wang); writing—original draft preparation, Y.T.; writing—review and editing, M.C., J.S. and F.Y.; supervision, M.C.; project administration, Z.W. All authors have read and agreed to the published version of the manuscript.

**Funding:** This research was funded by “State Key Laboratory of Solid Waste Reuse for Building Materials, grant number SWR-2017-004”, “National Natural Science Foundation of China, grant number 51974262” and “National Key R&D Program of China, grant number 2018YFC1903500”.

**Conflicts of Interest:** The authors declare no conflict of interest.

**References**

1. Li, X.; Zhang, C.; Li, Y.; Zhi, Q. The Status of Municipal Solid Waste Incineration (MSWI) in China and its Clean Development. *Energy Procedia* **2016**, *104*, 498–503. [CrossRef]

2. Zhang, B.; Zhou, W.; Zhao, H.; Tian, Z.; Li, F.; Wu, Y. Stabilization/solidification of lead in MSWI fly ash with mercapto functionalized dendrimer Chelator. *Waste Manag.* **2016**, *50*, 105–112. [CrossRef]

3. Yang, Z.; Tian, S.; Liu, L.; Wang, X.; Zhang, Z. Application of washed MSWI fly ash in cement composites: Long-term environmental impacts. *Environ. Sci. Pollut. Res.* **2018**, *25*, 12127–12138. [CrossRef]

4. Pesonen, J.; Yliniemi, J.; Ilikainen, M.; Kuokkanen, T.; Lassi, U. Stabilization/solidification of fly ash from fluidized bed combustion of recovered fuel and biofuel using alkali activation and cement addition. *J. Environ. Chem. Eng.* **2016**, *4*, 1759–1768. [CrossRef]

5. Aubert, J.E.; Hussen, B.; Sarramone, N. Utilization of municipal solid waste incineration (MSWI) fly ash in blended cement Part 1: Processing and characterization of MSWI fly ash. *J. Hazard. Mater.* **2006**, *136*, 624–631. [CrossRef] [PubMed]

6. Xue, Y.; Hou, H.; Zhu, S.; Zha, J. Utilization of municipal solid waste incineration ash in stone mastic asphalt mixture: Pavement performance and environmental impact. *Constr. Build. Mater.* **2009**, *23*, 989–996. [CrossRef]

7. Chen, C.G.; Sun, C.J.; Gau, S.H.; Wu, C.W.; Chen, Y.L. The effects of the mechanical–chemical stabilization process for municipal solid waste incinerator fly ash on the chemical reactions in cement paste. *Waste Manag.* **2013**, *33*, 858–865. [CrossRef]

8. Jin, M.; Zheng, Z.; Sun, Y.; Chen, L.; Jin, Z. Resistance of metakaolin-MSWI fly ash based geopolymer to acid and alkaline environments. *J. Non-Cryst. Solids* **2016**, *450*, 116–122. [CrossRef]

9. Wei, X.; Guo, S.; Wu, B.; Li, F.; Li, G. Effects of reducing agent and approaching anodes on chromium removal in electrokinetic soil remediation. *Front. Environ. Sci. Eng.* **2016**, *10*, 253–261. [CrossRef]

10. Li, X.; Li, H.; Yang, G. Electric fields within clay materials: How to affect the adsorption of metal ions. *J. Colloid Interface Sci.* **2017**, *501*, 54–59. [CrossRef]

11. Rojo, A.; Hansen, H.K.; Monárdez, O.; Jorquera, C.; Santis, P.; Inostroza, P. Electrical Behavior of Copper Mine Tailings during EKR with Modified Electric Fields. *Bull. Environ. Contam. Toxicol.* **2017**, *98*, 304–309. [CrossRef] [PubMed]

12. Yang, T.; Shu, J.; Chen, M.; Wang, J.; Wang, Y.; Luo, Z.; Wang, R.; Yang, F.; Xiu, F.; Sun, Z. Manganese and ammonia nitrogen recovery from electrolytic manganese residue by electric field enhanced leaching. *J. Clean. Prod.* **2019**, *236*, 117708.

13. Liu, Z.; Nueraihemaiti, A.; Chen, M.; Du, J.; Fan, X.; Tao, C. Hydrometallurgical leaching process intensified by an electric field for converter vanadium slag. *Hydrometallurgy* **2015**, *155*, 56–60. [CrossRef]

14. Kim, R.; Gahreman, A. The effect of ore mineralogy on the electrochemical gold dissolution behavior in various cyanide and oxygen concentrations; Effect of sulfidic ores containing heavy metals. *Hydrometallurgy* **2019**, *184*, 75–87. [CrossRef]
15. Bas, A.D.; Safizadeh, F.; Ghali, E.; Choi, Y. Leaching and electrochemical dissolution of gold in the presence of iron oxide minerals associated with roasted gold ore. *Hydrometallurgy* 2016, 166, 143–153. [CrossRef]

16. Liu, L.; Li, W.; Song, W.; Guo, M. Remediation techniques for heavy metal-contaminated soils: Principles and applicability. *Sci. Total Environ.* 2018, 633, 206–219. [CrossRef]

17. Ferreira, C.; Jensen, P.; Ottosen, L.; Ribeiro, A. Removal of selected heavy metals from MSW fly ash by the electrodialytic process. *Eng. Geol.* 2005, 77, 339–347. [CrossRef]

18. Lu, C.-C.; Hsu, M.H.; Lin, Y.-P. Evaluation of heavy metal leachability of incinerating recycled aggregate and solidification/stabilization products for construction reuse using TCLP, multi-final pH and EDTA-mediated TCLP leaching tests. *J. Hazard. Mater.* 2019, 368, 336–344. [CrossRef]

19. Jiang, Y.; Liu, C.; Huang, A. EDTA-Functionalized Covalent Organic Framework for the Removal of Heavy-Metal Ions. *ACS Appl. Mater. Interfaces* 2019, 11, 32186–32191. [CrossRef]

20. Jiao, F.; Zhang, L.; Dong, Z.; Namioka, T.; Yamada, N.; Ninomiya, Y. Study on the species of heavy metals in MSWI fly ash and their leaching behavior. *Fuel Process. Technol.* 2016, 152, 108–115. [CrossRef]

21. Zhao, K.; Hu, Y.; Tian, Y.; Chen, D.; Feng, Y. Chlamin removal from MSWI fly ash by thermal treatment: Effects of iron/aluminum additives. *J. Environ. Sci. Sci.* 2020, 88, 112–121. [CrossRef] [PubMed]

22. Zhou, J.; Wu, S.; Pan, Y.; Zhang, L.; Cao, Z.; Zhang, X.; Yonemochi, S.; Hosono, S.; Wang, Y.; Oh, K.; et al. Enrichment of heavy metals in fine particles of municipal solid waste incinerator (MSWI) fly ash and associated health risk. *Waste Manag.* 2015, 43, 239–246. [CrossRef] [PubMed]

23. Wongsa, A.; Boonserm, K.; Waisurasingha, C.; Sata, V.; Chindapasrirt, P. Use of municipal solid waste incinerator (MSWI) bottom ash in high calcium fly ash geopolymer matrix. *J. Clean. Prod.* 2017, 148, 49–59. [CrossRef]

24. Alphen, C.V. Automated mineralogical analysis of coal and ash products—Challenges and requirements. *Miner. Eng.* 2007, 20, 496–505. [CrossRef]

25. Gong, B.; Deng, Y.; Yang, Y.; Tan, S.N.; Liu, Q.; Yang, W. Solidification and Biotoxicity Assessment of Thermally Treated Municipal Solid Waste Incineration (MSWI) Fly Ash. *Int. J. Environ. Res. Publ. Health* 2017, 14, 626. [CrossRef] [PubMed]

26. Lu, L.; Liu, G.; Wang, J.; Wu, Y. Bioavailability and mobility of heavy metals in soil in vicinity of a coal mine from Huaibei, China. *Hum. Ecol. Risk Assess. Int. J.* 2017, 23, 1164–1177. [CrossRef]

27. Chen, P.; Sun, X.; Gao, M.; Ma, J.; Guo, Q. Transformation and migration of cadmium during chemical-looping combustion/gasification of municipal solid waste. *Chem. Eng. J.* 2019, 365, 389–399. [CrossRef]

28. Wang, H.; Fan, X.; Wang, Y.N.; Li, W.; Sun, Y.; Zhan, M.; Wu, G. Comparative leaching of six toxic metals from raw and chemically stabilized MSWI fly ash using citric acid. *J. Environ. Manag.* 2017, 208, 15. [CrossRef]

29. Zhang, Y.; Cetin, B.; Likos, W.J.; Edil, T.B. Impacts of pH on leaching potential of elements from MSW incineration fly ash. *Fuel* 2016, 184, 815–825. [CrossRef]

30. Chen, W.; Kirkelund, G.M.; Jensen, P.E.; Ottosen, L.M. Electrodialytic extraction of Cr from water-washed MSWI fly ash by changing pH and redox conditions. *Waste Manag.* 2018, 71, 215. [CrossRef]

31. Ke, Y.; Li, P.; Chan, W.P.; Dou, X.; Wang, J.Y. Characteristics of heavy metals leaching from MSWI fly ashes in sequential scrubbing processes. *J. Mater. Cycles Waste Manag.* 2018, 20, 604–613.

32. Shu, J.; Liu, R.; Liu, Z.; Chen, H.; Tao, C. Enhanced extraction of manganese from electrolytic manganese residue by electrochemical. *J. Electroanal. Chem.* 2016, 780, 32–37. [CrossRef]

33. Ng, Y.S.; Gupta, B.S.; Hashim, M.A. Remediation of Pb/Cr co-contaminated soil using electrokinetic process and approaching electrode technique. *Environ. Sci. Pollut. Res. Int.* 2016, 23, 546. [CrossRef] [PubMed]

34. Zhu, Y.E.; Zhang, Q.R.; Zhang, W.R.; Jiang, K.Q.; Hou, H.B.; Li, L.; Li, H. Historical verication of chromium-contaminated soil remediation in the past 15 years based on the bibliometric analysis (2001–2015). *J. Agro-Environ. Sci.* 2017, 36, 409–419.

35. Tao, Z.; Zou, H.; Ji, M.; Li, X.; Li, L.; Tang, T. Enhanced electrokinetic remediation of lead-contaminated soil by complexing agents and approaching anodes. *Environ. Sci. Pollut. Res.* 2014, 21, 3126–3133.

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