Biomechanical analysis of the acetabular buttress-plate: are complex acetabular fractures in the quadrilateral area stable after treatment with anterior construct plate-1/3 tube buttress plate fixation?

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OBJECTIVE: The acetabular buttress-plate has been widely used in treating difficult cases with satisfying clinical results. However, the biomechanical properties of a postoperative acetabular fracture fixed by the buttress-plate are not clear. The purpose of this study was to evaluate the biomechanical properties of stability after the anterior tube buttress-plate fixation of complex acetabular fractures in the quadrilateral area.

METHODS: A construct was proposed based on anterior construct plate - 1/3 tube buttress plate fixation for acetabular both-column fractures. Two groups of six formalin-preserved cadaveric pelvises were analyzed: (1) group A, the normal pelvis and (2) group B, anterior construct plate-1/3 tube buttress plate with quadrilateral area fixation. The displacements were measured, and cyclical loads were applied in both standing and sitting simulations.

RESULTS: As the load was added, the displacements were A>B, increasing in line. In the 600 N physiological loading, the differences were significant (standing position: p=0.013; sitting position: p=0.009) between groups A and B.

CONCLUSION: The anterior construct plate - 1/3 tube buttress plate fixation provided a better stable construct for early sitting. The standing mode yielded more significant differences between the groups. Placing a 1/3 tube buttress-plate via an anterior approach is a novel method of providing quadrilateral area support in this setting.

KEYWORDS: Acetabular Fractures; Quadrilateral Area; Articular Comminution; Internal Fixation; Biomechanics.

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INTRODUCTION

Treating acetabular fractures in the quadrilateral area is one of the most challenging problems in the orthopedic trauma department because such fractures often belong to the group of articular comminuted fractures. The bone in the quadrilateral area is thin, and the anatomical site is deep. The most difficult part of these bony deficits is that the screw can easily penetrate into the hip (1). Acetabular both-column fractures are the most common fracture in the quadrilateral area (1,2). We often select a multi-approach (3) or modified ilioinguinal approach (1) to expose this fracture during the operation. Due to the presence of many postoperative complications, the reduction and internal fixation of acetabular both-column fractures though a single anterior approach has been a direction sought by many orthopedic doctors (4,5).

The main problem is the difficulty involved in fixing the posterior column fracture block (quadrilateral area) through a single anterior approach. The lag screw through the anterior column to the posterior column would produce a certain clinical result (1,6), but its fixation is eccentric (partial posterior) and requires the fracture blocks of the anterior and posterior columns to not be crushed (6,7). The cerclage wires also produce some good results (8). However, more complex hardware combinations necessitate larger exposures, which are often associated with higher rates of infection and overall complications (9). Given these issues, the fixation technology of the bone surface (buttress-plate) was used to fix the posterior column.
fracture block. A titanium plate combined with 1/3 tube buttress-plate has been widely used and produces a better therapeutic effect (3,4). The stability of elastic fixation to the quadrilateral area by the tube buttress-plate has always been controversial (3,8). Stability is essential because an ingrowth component can only be successful if it is adequately stabilized against the host bone to allow host bone ingrowth to occur (9). There are currently no biomechanical evaluations in the literature comparing buttress-plate for the treatment of complex acetabular fractures. Therefore, this study evaluated the biomechanics of a tube buttress-plate in both standing (1) and sitting (10) simulations.

METHODS

Specimens
We selected six formalin-preserved cadaveric pelvices for this investigation. Six normal human specimens that included the fourth lumbar vertebra and proximal 1/3 of the femoral shaft were obtained from the Department of Anatomy of Southern Medical University. These specimens had no known metabolic bone disease or tumors. The trabecular appearance and bony quality were examined, and bone abnormalities were ruled out by a standard anteroposterior X-ray. The soft tissue was removed, except the sacrum, sacroiliac joint, hip joint capsule, ligaments of the sacral spine, sacral tubercle and obturator internus (Figure 1). Only one hip was used for testing for each hip surgery. We selected the reconstruction plate, 1/3 tube and titanium screws (3.5 mm) of AO, and ZWICKZ100 material machine (Germany ZWICKZ, a precision of 0.1%, Department of Mechanical Room of the Wuhan University of Technology).

Displacement measurement
The specimen was fixed in the position of standing or sitting (Figure 2) on the pelvis as previously described by Pierannunzii L (1) and Gao YC (10). Then, the specimen was treated repeatedly with loads from 400 to 700 Newtons. In the standing position, the lateral displacement of the posterior column wall was measured with a multifunctional digital dial gauge (Beijing Deli love Monitoring Technology, Beijing, China). In the sitting position, the lateral displacement of the posterior column wall was measured with a multifunctional digital dial gauge, and the overall axial displacement of the pelvis was measured with the beam sensor of the ZwickZ100 electronic universal testing machine. The stiffness of the specimens was calculated. First, we tested the six normal human pelvices in both the standing and sitting simulations as the control group. Then, we produced high both-column fractures using a wire saw on one hip (Figure 3) and fixed the fracture using anterior construct plate -1/3 tube buttress-plate fixation (group B, Figure 4). We tested the fractured pelvic again in the standing and sitting positions consecutively.

Analysis
According to the matta standard (2), the displacement of a fracture after internal fixation of less than 1 mm indicated anatomic reduction; if the lateral displacement of the posterior column wall was greater than 1 mm, the femoral head would appear central dislocation; and if the longitudinal displacement of the anterior inferior iliac spine was greater than 1 mm, the femoral head would appear upward dislocation.

The “Paired-Sample T Test” was used to assess the significance of the differences between the groups for each index of measurement. Initially, all conditions were considered together; subsequently, the tests were conducted separately for each position by the “2-Repeating Factor of ANOVA”. An alpha-level of 0.05 was used for each test to test the differences between the simulations.

All data were expressed as the means ± SE unless otherwise stated, and the statistical analysis was performed with SPSS 13.0 statistics software for Windows (SPSS, Chicago, IL).
RESULTS

The fracture blocks of the anterior and posterior columns in the specimens after internal fixation were firmly fixed immediately, resulting in anatomic reduction. The soft tissue (the sacrotuberous ligament, sacrospinous ligament and obturator internus) was taut. The screws and plates did not crack during the testing process. The maximum separation was less than 2 mm. After the removal of the load, the acetabular plate and fixation returned to their initial form or state.

The relationship between load and displacement

As the load was added, the displacements were \( A < B \), increasing in line. In the standing position, the displacement of the specimens in group B under the 400 N load was greater than 1 mm, indicating that the dislocation of the femoral head began to appear under the 400 N load. In the inner wall, horizontal displacement of more than 1 mm appeared at the following loads: 400 N in 1 case, 500 N in 1 case, 600 N in 1 case, and 700 N in 2 cases. In the anterior wall, longitudinal displacement of more than 1 mm appeared at the following loads: 400 N in 1 case, 500 N in 2 cases, 600 N in 3 cases, and 700 N in 3 cases. The statistical analysis showed that there was a significant difference between the horizontal and vertical displacements (\( p < 0.05 \)) in group A to group B (Tables 1 and 2).

In the sitting position, the lateral displacement of the posterior column-inner wall in group B was absolutely within 0.5 (mm and thus was without dislocation. The statistical analysis showed that although the numerical value of the lateral displacement of the posterior column-inner wall in group B was greater than that in group A, there was no significant difference (\( p > 0.05 \)) (Table 3).

Axial stiffness of the pelvis in group A was significantly larger than that in group B (\( p < 0.01 \)) (Table 4).

Quantitative analysis of the test results on the physiological load (600 N)

In the standing position, the longitudinal stiffness of the anterior wall was \( 2883.9 \pm 1901.2 \) N/mm in group A and \( 1015.5 \pm 365.3 \) N/mm in group B. We analyzed the two measuring indices (the lateral displacement of the inner wall and the longitudinal stiffness of the anterior) comprehensively using the statistical method of “2 Repeating Factor Of ANOVA”, which showed a significant difference (\( F = 14.3, p = 0.013 \)) between groups A and B. In the sitting position, we analyzed the two measuring indices (the lateral displacement of the inner wall and the axial stiffness of the pelvis) comprehensively, which showed a significant difference (\( F = 16.9, p = 0.009 \)) between groups A and B.

DISCUSSION

The acetabulum represents a basin-like anatomic structure that bears the body’s weight, receives the resultant force from the ground, and accommodates ambulatory activity and hip joint mobility (11). Open anatomic reduction of the articular surface combined with rigid internal fixation and early mobilization is the standard current treatment for injuries to this region (11,12). Maintaining stability of the joint is very important (9). The stability of the hip mainly depends on the blocking effect of the acetabular bone. The quadrilateral area (square area) is located in the inner side of the acetabular posterior column. Comminuted fractures are likely caused by strong violence to the longitudinal femoral neck. The femoral head with the fracture blocks would transpose to the intrapelvic direction.

### Table 1 - Different loading-lateral displacement of the posterior column inner wall in the standing position (x ± s mm).

| Group | 400  | 500  | 600  | 700  |
|-------|------|------|------|------|
| A     | 0.14 ± 0.04 | 0.15 ± 0.07 | 0.19 ± 0.06 | 0.24 ± 0.06 |
| B     | 0.65 ± 0.29 | 0.72 ± 0.29 | 0.76 ± 0.30 | 0.82 ± 0.32 |

Paired-Sample T Test: group A - group B (\( p < 0.012 \)).

### Table 2 - Different loading-lateral displacement of the anterior inferior iliac spine in the standing position (x ± s mm).

| Group | 400  | 500  | 600  | 700  |
|-------|------|------|------|------|
| A     | 0.14 ± 0.05 | 0.18 ± 0.07 | 0.26 ± 0.10 | 0.31 ± 0.12 |
| B     | 0.24 ± 0.18 | 0.29 ± 0.19 | 0.36 ± 0.18 | 0.40 ± 0.16 |

Paired-Sample T Test: group A - group B (\( p < 0.032 \)).
The plate was remodeled easily, resulting in the loss of its clinical study showed that elastic plate stability was reduced wall fracture downward in the pelvic side wall. A recent highlighted that an excessive correction plate, which is proximal end of the plate was fixed to the iliac bone. He fixation to resist the shear stress of the inner wall. The well as the 1/3 tube (3,4,12).

operation. The routine method is almost unable to achieve technology of the bone surface, is an ideal internal fixation. elastic buttress-plate, which is typically used as the fixation biomechanics, a reconstruction titanium plate-1/3 tube type interfragmentary lag screw (20).

the fracture may be displaced during tightening of the screw fixation was eccentric and could play a certain role in the surface fracture of the posterior column (16). The lag screw fixation was eccentric and could play a certain role in fixation. When the screw is away from the acetalubar fracture, the reliable degree of fixation decreases by approximately 50% (14), and the stability of the acetalubar decreases (15,16). In general, only the anterior reconstruction titanium plate-screw system shows difficulty in fully achieving reliable fixation (8,14,16).

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Historically, hip biomechanics suggested that the bearing force of the acetalubar could be divided into two components in the horizontal and vertical directions of the coronal plane (16,17). The shear stress in the horizontal direction often promoted the fracture block to emerge as a transverse separation (8,13,18,19). We should emphasize the reduction and stability of the quadrilateral area in the operation, not only paying attention to reducing and fixing the surface fracture of the posterior column (16). The lag screw fixation was eccentric and could play a certain role in fixation. However, not all acetalubar fractures are amenable to the placement of an interfragmentary lag screw (6,7,20), and the fracture may be displaced during tightening of the interfragmentary lag screw (20).

This study evaluated the tube buttress-plate. The horizontal displacement in the posterior column wall reflects the shear resistance of the internal fixator after the operation. Upward or slip displacements, which are produced by the push of the femoral head-acetalubar roof, reflect the overall standing stability of the hip. The longitudinal displacement of the sacroiliac joint mainly comprises the longitudinal stiffness of the complete pelvis. However, the stiffness of the entire pelvis is not equivalent to the stiffness of the sacroiliac joint (21). The stability of the hip also produces axial stiffness in the pelvis. In the same pelvis, the difference in the axial stiffness reflects the stability of the fixation. We selected cadaveric specimens to create a high both-column fracture model. According to the stress distribution of the hip after loading in the coronal plane, the results showed the following: 1. as the load increased from 400 N to 700 N, the displacement increased, which was consistent with the law of conventional dynamics; and 2. in the standing position, the displacements in group B were larger.

Given the characteristics of the anatomy and acetalubar biomechanics, a reconstruction titanium plate-1/3 tube type elastic buttress-plate, which is typically used as the fixation technology of the bone surface, is an ideal internal fixation. It has the advantage of a simple application during the operation. The routine method is almost unable to achieve fixation to the acetalubar fossa and quadrilateral area as well as the 1/3 tube (3,4,12).

Cole (19) first reported the use of elastic buttress-plate fixation to resist the shear stress of the inner wall. The proximal end of the plate was fixed to the iliac bone. He highlighted that an excessive correction plate, which is similar to a spring, was used to hold the pieces of a medial wall fracture downward in the pelvic side wall. A recent clinical study showed that elastic plate stability was reduced by postoperative turning during nursing care and that the plate was remodeled easily, resulting in the loss of its fixation role after fatigue. It also has the potential to cut pelvic organs. Farid (8) made some improvements with the addition of cerclage wire in the elastic steel plate to strengthen the fixation. To provide adequate pressure, the wire needed to be thread through the greater sciatic notch, and stripping during the operation was significant. All of these factors can easily injure the sciatic nerve and peripheral vascular system. Pan (3) added the 1/3 tubular plate under the anterior column reconstruction titanium plate and attempted to rely on the extrusion of the titanium plate to reinforce the elastomeric tube, thereby fixing the bone block. Laflamme (13) performed a follow-up study over 4.2 years in elderly people using a buttress-plate to fix fracture blocks in the quadrilateral area and found that the anatomical reduction rate was 90.5%. There are currently no biomechanical evaluations in the literature comparing buttress-plate for the treatment of complex acetalubar fractures. Therefore, this study evaluated the tube buttress-plate.

| Table 3 - Different loading-lateral displacement of the posterior column inner wall in the sitting position (x ± s mm). |
|---------------------------------------------------------------|
| **Group** | 400 | 500 | 600 | 700 |
| A | 0.18 ± 0.07 | 0.20 ± 0.06 | 0.21 ± 0.05 | 0.22 ± 0.06 |
| B | 0.26 ± 0.17 | 0.28 ± 0.18 | 0.32 ± 0.18 | 0.35 ± 0.20 |

Paired-Sample T Test: group A - group B (p<0.16).

Table 4 - Different loading-axial stiffness of the pelvis in the sitting position (x ± s N/mm).

| **Group** | 400 | 500 | 600 | 700 |
|-----------|-----|-----|-----|-----|
| A | 208.5 ± 54.3 | 213.0 ± 50.6 | 221.5 ± 59.4 | 222.0 ± 40.3 |
| B | 118.2 ± 10.5 | 125.6 ± 8.9 | 129.9 ± 7.5 | 132.5 ± 7.1 |

Paired-Sample T Test: group A - group B (p<0.01).
take care of the physiological conditions of fracture reduction after the operation (10). We tested the positions of sitting and standing in this experiment, retaining portions of the soft tissue. We also fully simulated the postoperative physiological status of the patients, which was close to the clinical status. In group B, the experimental results showed that the hip was prone to instability in the standing position. The shear force of the 1/3 tube type titanium plate was poor. Although the axial stiffness of the pelvic in the sitting position was poorer than that of the normal pelvis, acetabulum fractures showed a satisfactory reduction on physiological load. Thus, sitting early is safe.

In general, as long as the patient’s condition allows it, the operation of the acetabular fracture should be performed 3-7 days and no more than 2 weeks after the injury. Otherwise, the difficulty of the operation would increase (22). Thus, because the healing rate of acetabular fractures is very rapid, the fractures will tend to be stable after 2 or 3 weeks because they can easily form a localized scab. Along with the process of fracture healing, the fixation stability of an acetabular fracture will be enhanced, that is, the inner fixation would bear weight-stress for a short time only. Its main contribution of share the weight is going on in the initial 2 weeks. All of these factors may explain why single-point elasticity fixation (1/3 tube type titanium plate) can obtain satisfactory results in the fixing portion of the posterior column fracture.

In addition, the proper selection of the operation approach will reduce the degree of difficulty and improve the quality of the reduction (23). In the reduction of both column acetabular fractures, we often adopt the combination approach, which needs a wide range of stripping and a long operation time. Postoperative heterotropic ossification also occurs at a high rate. We selected a single ilioinguinal approach in the fixation of an anterior construct plate-1/3 tube buttress plate, fully utilizing the advantages of the anterior approach, which are essential to maximize the union rates and minimize the complications in these difficult cases (24). The ilioinguinal approach also could be able to fix most complex fractures of the acetabulum (25).

Therefore, the reduction and internal fixation of both-column fractures using a single anterior approach has been the direction taken by many orthopedic doctors (4,5). However, the main problem is that the block posterior column and the quadrilateral area are difficult to fix. The 1/3 tube plate had better results than palliative care (no fixation or indirect fixation) in weakening the shear stress on the inner wall but is poorer to prevent separation of the distal bone block. More work is needed to search for a suitable fixator.

A few points should be noted. First, we only used six specimens as representatives because human pelvis specimens are very precious. Second, we elected to pursue a repeated measures design rather than a matched pair design for this investigation. Six specimens were tested four successive times. To reduce the effect of the repeated test impacts, the experiments were performed randomly in the simulated positions. At the same time, the maximum load (700 N) was within the yielding point of the pelvis (26). The mechanical strength had no obvious effect on the elastic deformation. Third, although there are individual differences among the experimental samples, the experimental load was selected based on the characteristics of each specimen (16,20). Therefore, we selected a large observation range, from 400 to 700 N, and did not perform the analysis one by one, but rather only focused on the analysis of the 600 N physiological weight (10,16). In addition, Vailas (27) highlighted that the function of the soft tissue could not be ignored. The integrity of the articular capsule determined the stability of the hip joint. To be close to the actual clinical state, we retained the important ligaments and muscles for convenient measurements in this experiment, which was different from previous studies (9,20).

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**AUTHOR CONTRIBUTIONS**

Wu YD was responsible for the manuscript first draft and English version, prepared the figures, and conducted the literature search. Cai XH participated in the experimental design, analyzed the data and approved the final version of the manuscript. Liu XM reviewed the manuscript and checked the English journal for submission. Zhang HX revised the manuscript. Wu YD, Cai XH, Liu XM and Zhang HX performed part of the experiments.

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