Deformation and Thermal Histories of Ordinary Chondrites: Evidence for Postdeformation Annealing and Syn-Metamorphic Shock

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Deformation and thermal histories of ordinary chondrites: Evidence for post-deformation annealing and syn-metamorphic shock

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1 Table, 7 Figures, Electronic Annex.

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Abstract-- We show that olivine microstructures in seven metamorphosed ordinary chondrites of different groups studied with optical and transmission electron microscopy can be used to evaluate the post-deformation cooling setting of the meteorites, and to discriminate between collisions affecting cold and warm parent bodies. The L6 chondrites Park (shock stage S1), Bruderheim (S4), Leedey (S4), and Morrow County (S5) were affected by variable shock deformation followed by relatively rapid cooling, and probably cooled as fragments liberated by impact in near-surface settings. In contrast, Kernouvé (H6 S1), Portales Valley (H6/7 S1), and MIL 99301 (LL6 S1) appear to have cooled slowly after shock, probably by deep burial in warm materials. In these chondrites, post-deformation annealing lowered apparent optical strain levels in olivine. Additionally, Kernouvé, Morrow County, Park, MIL 99301, and possibly Portales Valley, show evidence for having been deformed at an elevated temperature (≥800-1000 °C). The high temperatures for Morrow County can be explained by dynamic heating during intense shock, but Kernouvé, Park, and MIL 99301 were probably shocked while the H, L and LL parent bodies were warm, during early, endogenically-driven thermal metamorphism. Thus, whereas the S4 and S5 chondrites experienced purely shock-induced heating and cooling, all the S1 chondrites examined show evidence for static heating consistent with either syn-metamorphic shock (Kernouvé, MIL 99301, Park), post-deformation burial in warm materials (Kernouvé, MIL 99301, Portales Valley), or both. The results show the pitfalls in relying on optical shock classification alone to infer an absence of shock and to construct cooling stratigraphy models for parent bodies. Moreover, they provide support for the idea that "secondary" metamorphic and "tertiary"
shock processes overlapped in time shortly after the accretion of chondritic
planetesimals, and that impacts into warm asteroidal bodies were common.

1. INTRODUCTION

Collisions affected all solar system bodies and could have played a possibly
complex and important role in the geological evolution of low-gravity, asteroidal-sized
planetesimals (Scott et al., 1989; Stöffler et al., 1988). Chondritic meteorites are
samples of such planetesimals that potentially can record evidence in their
microstructures for collisional shock, during and shortly after accretion and in much later
events. The L chondrite parent body evidently suffered a major impact ~0.5 Ga ago that
largely destroyed it, and which caused much debris to be delivered to Earth shortly
thereafter (Haack et al., 1996; Schmitz et al., 2001; Greenwood et al., 2007; Swindle et
al., 2014). There is radiometric evidence that, based on H chondrites of low optical
shock stage (S1 and S2—Stöffler et al., 1991), the H-group parent body initially cooled
in an onion-shell structure (Trieloff et al., 2003; Kleine et al., 2008) and that this body
was preserved intact during cooling from peak metamorphism. However, there is also
evidence that chondrite parent bodies experienced early collisions while they were
thermally metamorphosed (e.g., Ruzicka et al., 2005; Hutson et al., 2009; Friedrich et
al., 2013, 2014; Tait et al., 2014; Scott et al., 2014). Impact redistribution could have
placed chondrites of different metamorphic grades (petrographic types) at different
depths, accounting for an overall lack of correlation between these grades and cooling
rates based on metallographic techniques (Scott and Rajan, 1981; Grimm, 1985; Taylor
et al., 1987; Scott et al., 2014). Especially large early impacts could have resulted in
destruction and reassembly of the parent bodies (Grimm, 1985; Taylor et al., 1987;
Optical petrographic properties of olivine provide the main way to assess the shock histories of chondrites (and other meteorites) with the Stöffler et al. (1991) shock stage scheme, which is used widely. However, generally fast diffusion in olivine might allow deformation features to preferentially "heal" in this mineral during annealing (Rubin 1992, 1994, 1995, 2002, 2003, 2004). If so, the shock stage of olivine alone might lead to erroneous inferences.

This study was designed to better understand the role and effect of collisions in the early solar system, especially the relationship between deformation and thermal processing. Transmission electron microscopy (TEM) studies of olivine in ordinary chondrites was our main focus, given the usefulness of TEM to probe shock and thermal histories in chondrites (e.g., Ashworth and Barber, 1975, 1977; Joreau et al., 1997; Langenhorst et al., 1995; Leroux, 2001), and given knowledge of how olivine responds to deformation and annealing (e.g., Raleigh, 1968; Carter et al., 1968; Phakey et al., 1972; Goetze and Kohlstedt, 1973; Green, 1976; Guegen and Nicolas, 1980; Druiventak et al., 2011). Ordinary chondrites of different groups but similar petrographic type were selected for study, including L6 (Bruderheim, Leedey, Morrow County, Park), H6 (Kernouvé), H6/7 (Portales Valley), and LL6 (Miller Range 99301, hereafter abbreviated MIL 99301). The L6 chondrites were chosen as reference (baseline) samples, to understand the effects of differing shock intensity ranging from shock stage S1 (Park) to S5 (Morrow County). If the L6 chondrites were shocked late in a parent body break-up event, they could have experienced a simple shock history involving deformation and heating of cold materials followed by rapid cooling. In contrast, the chosen H (Kernouvé, Portales Valley) and LL (MIL 99301) chondrites, all weakly
deformed (S1), were selected based on evidence that they could have experienced a more complex shock history, involving warm ambient conditions during or after shock. Each contains features that could be relicts of shock metamorphism which were not obliterated during annealing (Rubin, 2004). Coarse metal veins in the H chondrites such as Portales Valley and Kernouvé likely formed by impact melting and mobilization of metal (Hutson, 1989; Kring et al., 1999; Rubin et al., 2001) before or during metamorphism (Hutson, 1989; Ruzicka et al., 2005; Friedrich et al., 2013). Other potential relict shock features include chromite-plagioclase assemblages in all three meteorites (although these are present in most ordinary chondrites) (Rubin, 2003, 2004), silicate darkening in MIL 99301 and Portales Valley, low-Ca clinopyroxene in MIL 99301, and polycrystalline (recrystallized) troilite in MIL 99301 (Rubin, 2002, 2004).

Preliminary data were reported previously (Hutson et al., 2007, 2009; Ruzicka and Hugo, 2011, 2014).

2. SAMPLES AND METHODS

Samples were studied at Portland State University with optical microscopy using a Leica DM 2500 petrographic microscope, and with TEM using an FEI Tecnai G3 transmission electron microscope. Sample designations for meteorites studied with these techniques are given in Tables EA-1 and EA-2 (Electronic Annex). For each meteorite, optical and TEM data were acquired from the same polished thin section. Optical microscopy was used to perform a grain-by-grain assessment of olivine deformation for a representative sampling of grains ≥50 µm across using the method of Jamsja and Ruzicka (2010). Based on the works of Stöffler et al. (1991), Schmitt and Stöffler (1995) and Schmitt (2000), olivine grains were assigned to different shock
stages based on intragranular misorientation and the presence of parallel straight planar fractures or planar deformation features (Table EA-1). Misorientation angles were the primary categorization tool, and were determined in cross-polarized transmitted light by the difference in extinction position between the main extinction portion of the grains and their remaining portions. These data were used to determine the conventional shock stage (the highest category shown by at least 25% of grains, as given by Stöffler et al., 1991), the “weighted shock stage” (the mean of all grain shock stages), and the non-uniformity of deformation (variation of grain shock stages).

The TEM, operated at 200kV, was used to study all electron transparent areas of olivine grains in ion-milled 3-mm-diameter discs cored from polished thin sections. Amplitude contrast imaging in both bright field (bf) and g-3g weak beam dark field (wbdf) mode was used. Parameters were measured that have been found to be related to extent and temperature of deformation, and the extent of annealing. Deformation temperature is indicated by dislocation Burgers vector (b), screw/edge character, and curvature. Long, straight b=[001] screw dislocations in olivine are characteristic of low-temperature (and also high strain-rate) deformation, whereas b=[001] dislocations with more edge or mixed components, dislocation loops, and especially dislocations with slip direction b=[100] are characteristic of higher temperature (and also low strain-rate) deformation (Raleigh, 1968; Carter et al., 1968; Phakey et al., 1972; Blacic and Christy, 1973; Green, 1976; Ashworth and Barber, 1975, 1977; Guegen and Nicolas, 1980; Gaboriaud et al., 1981; Sears et al., 1984; Töpel-Schadt and Müller, 1985; Langenhorst et al., 1995; Druiventak et al., 2011; Demouchy, et al., 2013). Impact-related deformation involves high strain rates (e.g., Spray, 2010), so temperature is probably
the main variable that determines which slip system will be activated in chondritic
olivine. The ratio of “free” dislocations (not “bound” in subgrain boundaries) to the total
number of dislocations (free/(free+bound) or FFB ratio) is related to annealing extent
(Goetze and Kohlstedt, 1973). For each discrete olivine grain in our specimens we
determined the dislocation density (number per area); b where possible using the
conventional g·b =0 criterion; for b=[001] dislocations, the apparent length in screw
orientation compared to other orientations (% b=[001] screw sense); qualitative
dislocation curvature and symmetry; and the presence of dislocation loops, jogs, and
kink bands. For each meteorite specimen we also report the geometric average
dislocation density of all olivine grains (ρ\textsubscript{g}) rather than arithmetic average because
dislocation densities in some specimens vary by orders of magnitude from grain to

3. RESULTS

3.1. Optical petrography

Optical data are summarized in Table EA-1 (Electronic Annex) and by shock
stage histograms in Fig. 1. The meteorites fall into two overall groups: weakly deformed
S1 (Portales Valley, Kernouvé, Park, MIL 99301) and more strongly deformed S4
(Leedey, Bruderheim) and S5 (Morrow County) chondrites (Fig. 1). Leedey is
reclassified as shock stage S4, revised from the literature value of S3 (Rubin, 1994).
MIL 99301 is evidently a breccia, containing mostly weakly deformed (S1) but also
some more deformed and even recrystallized (S6) grains (Fig. 1). Some meteorites
(e.g., Leedey) show less dispersion in shock stages, and on this basis provide no
evidence for being breccias or for having been impacted more than once. Morrow
County is a definite S5 based on olivine data, consistent with the presence in this meteorite (alone among the samples studied) of all feldspar as maskelynite, a hallmark of shock stage S5 (Stöffler et al., 1991). Morrow County also contains numerous chromite-plagioclase (maskelynite) assemblages, a proposed shock indicator (Rubin, 2003), as well as prominent shock veins.

All the S1 meteorites contain otherwise unstrained olivine grains that have sharply defined low-angle misorientation boundaries observable with optical microscopy, with orientation mismatches of a few degrees from one side of the boundary to the other. Fig. 2 shows an example of such a grain from Portales Valley. These grains do not fit readily into shock stage categories: misorientation of this extent should be accompanied by planar fractures or planar deformation features, and/or by strain present throughout the grains. Sharp, localized changes in orientation could be produced by annealing, either by adjacent olivine grains growing together in nearly the same crystallographic orientation during metamorphism, or by deformed single grains generating orientation domains as a result of dislocation climb during annealing (to form subgrain boundaries). Sharp changes in orientation also could be a manifestation of kink bands produced by deformation (Raleigh, 1968; Carter et al., 1968). As noted below, olivine TEM data indicate that subgrain boundaries are common in Kernouvé, Portales Valley, and MIL 99301, and that kink bands are present in Park and MIL 99301. Thus the olivine misorientation features noted optically in these meteorites are probably subgrain boundaries in Kernouvé, Portales Valley, and MIL 99301, and kink bands in Park.
Fig. 1. Shock stage histograms for the meteorites in this study, arranged according to increasing weighted shock stage (values in brackets; the conventional shock stage from the 25% rule is shown outside the brackets). N= number of grains.

[Color in web, b/w in print]
Fig. 2. Cross-polarized transmitted light images of an otherwise weakly strained olivine grain in Portales Valley (CML0056-3) for two stage positions (part b rotated 15° clockwise relative to part a), showing a low angle (~5°) misorientation boundary between areas 1 and 2. The misorientation boundary is invisible in part a, but visible in part b as a sharp and slightly curved feature; fringes suggest a dipping contact. Area 3 is another orientation domain within the grain. Scale bar is 40 µm long. [color in web, black/white in print]

3.2. TEM petrography

TEM results are summarized in Table 1 and reported for individual olivine grains in Table EA-2 (Electronic Annex). Representative TEM micrographs are shown for L6 chondrites in Fig. 3, and for H and LL chondrites in Fig. 4.

3.2.1. Leedey and Bruderheim (L6 S4)

Leedey and Bruderheim have similar olivine microstructures. Both are heavily deformed (average geometric dislocation density $\rho_g \sim 3 \times 10^9$ and $\sim 1 \times 10^{10}$ cm$^{-2}$, respectively) with a strong prevalence of $b$-[001] dislocations, and only rare subgrain boundaries (Table 1; Fig. 3a-d). Dislocations are relatively straight, and include both screw and edge components, typically forming a rectilinear pattern (Fig. 3a, c). In many cases the individual dislocations take the form of a larger glide loop, with parallel $b$-[001] screws and more rounded edge segments. “Walls” of dislocation tangles are present across which misorientation of the crystal lattice occurs, forming patchy domains ($\leq$1 µm across) of differing crystal orientation between the walls (Fig. 3b). The
walls themselves can be straight, curved, or en echelon (Fig. 3g). Leedey also contains
kink bands that produced lamellar misorientation domains (Fig. 3d). The kink band
boundaries are narrower than other misorientation boundaries such as those composed
of tangles.

3.2.2. Morrow County (L6 S5)

Olivine microstructures in Morrow County resemble those in Bruderheim and
Leedey in some ways but differ significantly in other ways. As in Bruderheim and
Leedey, olivine in Morrow County is heavily deformed ($\rho_g \sim 5 \times 10^9$ cm$^{-2}$) and contains
only rare subgrain boundaries (Table 1). Also like Bruderheim and Leedey, a rectilinear
pattern of dislocations including $b=[001]$ screws and edge dislocations was observed
(Fig. 3e). Common dislocation tangles (Fig. 3f) form planar and en echelon
misorientation boundaries, and micrometer-sized orientation domains are well-
developed (Fig. 3g). Unlike Bruderheim and Leedey, Morrow County contains many
extensively curved and bowed dislocations and many small dislocation loops (Table 1,
Fig. 3f). $b=[001]$ dislocations with mixed screw/edge character are typical (Fig. 3f).
$b=[100]$ dislocations are common (Table 1), and sometimes form arrays that intersect
with $b=[001]$ dislocations to form dense tangles (Fig. 3f).
| Meteorite        | Geometric mean dislocation density ($\rho_g$) (cm$^{-2}$) | Geometric standard deviation dislocation density (cm$^{-2}$) | Maximum dislocation density (cm$^{-2}$) | Typical dislocation microstructure                                                                 | Subgrain boundaries | Average FFB dislocation ratio (%)$^a$ | b vector summary                      | Average % [001] screw dislocations$^b$ | N               |
|------------------|----------------------------------------------------------|------------------------------------------------------------|----------------------------------------|--------------------------------------------------------------------------------------------------|---------------------|----------------------------------------|-----------------------------------------|------------------------------------------|----------------|
| Bruderheim       | $1.3 \times 10^{10}$                                     | 4.1                                                        | $1.5 \times 10^{11}$                   | Parallel straight screw segments, other areas a mix of parallel screws & intersecting or curved; tangles & tangles. | rare / none         | 100 ± 0                                | [001] prevalent.                         | 29 ± 22                                   | 12             |
| Leedey           | $3.2 \times 10^9$                                        | 2.7                                                        | $2.1 \times 10^{10}$                   | Straight $b=[001]$ segments in 3 directions, some bowing; tangles & kink bands.                  | infrequent          | 96 +4/-10                              | [001] prevalent, [100] infrequent.       | < 50                       | 11             |
| Morrow County    | $4.9 \times 10^9$                                        | 3.2                                                        | $2.4 \times 10^{10}$                   | Extensively curved & bowed with many loops; common tangles.                                      | rare                | 99 +1/-3                               | [001] prevalent, [100] common.           | 10 ± 12                                   | 13             |
| Park             | $3.3 \times 10^8$                                        | 3.4                                                        | $1.3 \times 10^9$                      | Many parallel straight segments; extensively curved, bowed, common loops; tangles & kink bands.  | rare / none         | 100 ± 0                                | [001] prevalent, [100] somewhat common. | 36 ± 17                                   | 18             |
| Kernouvé         | $1.1 \times 10^6$                                        | $4.2 \times 10^3$                                        | $6.8 \times 10^8$                      | Bowed individual dislocations.                                                                  | common              | 84 +16/-29                             | [001] prevalent, [100] common.           | 2 +7/-2                                   | 20             |
| Portales Valley  | $4.4 \times 10^6$                                        | $6.8 \times 10^3$                                        | $1.4 \times 10^{11}$                   | Parallel straight; some intersecting, curved; some tangles.                                    | common              | 88 +22/-28                             | [001] prevalent, [100] prevalent, [101] rare in subgrain boundaries. | 32 ± 27                                   | 30             |
| MIL 99301        | $2.2 \times 10^7$                                        | $6.2 \times 10^2$                                        | $1.4 \times 10^8$                      | Parallel straight; frequent intersecting or curved; kink bands.                                | common              | 74 +26/-36                             | [001] prevalent, [100] somewhat common, [101] rare in subgrain boundaries. | 56 ± 26                                   | 9              |

$^a$ 100 x (number free dislocations) / (number free + bound dislocations), arithmetic average and standard deviation.

$^b$ Length of $b=[001]$ dislocations that are in screw sense, arithmetic average and standard deviation. For Morrow County, two sets of values are shown, one set for all 13 areas examined and one set excluding an atypical area.
Fig. 3. TEM images of olivine in L chondrites obtained in weak beam dark field (\textit{wbdf}) and bright field (\textit{bf}) modes. (a, b) \textit{Wbdf} images of Bruderheim, showing rectilinear pattern of $b=\langle 001 \rangle$ screw and edge dislocations (part a), and $b=\langle 001 \rangle$ screw dislocations and a misoriented domain (part b). The intense contrast of the latter domain is caused by overlapping strain fields produced by strong deformation. (c, d) \textit{Wbdf} images of Leedey showing rectilinear pattern of $b=\langle 001 \rangle$ screw and edge dislocations (part c), and kink bands producing lamellar misorientation domains (part d). (e) \textit{Wbdf} image of Morrow County showing presence of $b=\langle 001 \rangle$ screw dislocations and other dislocations with a vaguely rectilinear pattern; curved dislocations are also present. (f) Morrow County observed in \textit{wbdf} mode showing typical curved, mixed $b=\langle 001 \rangle$ dislocations, and a dislocation tangle composed in part of $b=\langle 100 \rangle$ dislocations. (g) Morrow County observed in \textit{bf} mode showing planar and en echelon misorientation boundaries, defined by dislocation tangles. Numerous curved dislocations (small dark features) are present throughout. (h) Park observed in \textit{bf} mode showing $b=\langle 001 \rangle$ screw dislocations, bowed dislocations and small loops, as well as a dislocation tangle composed in part of an array of $b=\langle 100 \rangle$ dislocations. (i) \textit{Wbdf} image of Park showing curved and looped $b=\langle 001 \rangle$ dislocations and a dislocation tangle composed of both $b=\langle 100 \rangle$ and $b=\langle 001 \rangle$ dislocations. [b/w in web and in print]
Fig. 4. TEM images of olivine in H and LL chondrites. (a, b, c) Wbdf images of Kernouvé showing relatively low dislocation density, and subgrain boundaries that range from poorly developed (part a, one set of dislocations) to well-developed two-set “picket fence” (part c). Both \( \mathbf{b} = [001] \) and \( \mathbf{b} = [100] \) dislocations are present. (d) Wbdf image of Portales Valley showing moderate density of \( \mathbf{b} = [001] \) screw dislocations and no subgrain boundaries. (e) Bf image of Portales Valley showing virtually all dislocations present in subgrain boundaries, composed of both \( \mathbf{b} = [001] \) and \( \mathbf{b} = [101] \) dislocations. The inset shows a wbdf image close-up of a subgrain boundary in Portales Valley composed of one set of parallel and nearly straight dislocations. (f) Bf image of a relatively deformed area of Portales Valley including \( \mathbf{b} = [001] \) screw dislocations. (g) Wbdf image of MIL 99301 showing both \( \mathbf{b} = [100] \) and \( \mathbf{b} = [001] \) dislocations as well as some \( \mathbf{b} = [101] \) dislocations and a subgrain boundary. (h) Bf image of MIL 99301 showing \( \mathbf{b} = [001] \) dislocations including many in screw configuration, as well as a kink band with a terminal \( \mathbf{b} = [100] \) dislocation. The box shows the location of part i. (i) Wbdf image showing a close up of the kink band in part h; \( \mathbf{b} = [001] \) dislocations are jogged across the kink band. [b/w in web and print]
3.2.3. Park (L6 S1)

Olivine in Park is less deformed ($\rho_g \sim 3 \times 10^8$ cm$^{-2}$) than in the previously described L chondrites. As with these other chondrites, subgrain boundaries are essentially absent (Table 1). Dislocations include many straight $b=[001]$ screws, as in Bruderheim and Leedey, but also many extensively curved or bowed dislocations and some small loops (Fig. 3h, 3i), as in Morrow County. $b=[100]$ dislocations, though not as common as in Morrow County, are also present in Park, and as in Morrow County, such $b=[100]$ dislocations are found in dislocation tangles (Fig. 3h, i). Kink bands were observed.

3.2.4. Kernouvé (H6 S1)

This chondrite contains the least deformed olivine, on average, of those studied ($\rho_g \sim 1 \times 10^8$ cm$^{-2}$), with many grains nearly devoid of dislocations and others having only a modest number (Fig. 4a-c). Unlike the other chondrites mentioned so far, subgrain boundaries are prominent in olivine from Kernouvé. These subgrain boundaries range in their configurations from those with only one set of loosely arranged, non-intersecting dislocations (Fig. 4a) to those with two sets of intersecting dislocations forming a curvilinear “picket fence” (Fig. 4c). Intermediate cases of subgrain boundaries with only a few intersecting dislocations are present (Fig. 4b). Some parallel $b=[001]$ screws are found in Kernouvé (Fig. 4b), but most dislocations are bowed or curved, or are present in subgrain boundaries. $b=[100]$ dislocations are common, and are often found in subgrain boundaries (Fig. 4b, c).
3.2.5. Portales Valley (H6/7 S1)

Olivine grains in Portales Valley have diverse microstructures. Dislocation densities vary greatly in grains, from nil to \(10^{10}\ \text{cm}^{-2}\). Averaging over many (30) grains, the overall dislocation density is low in Portales Valley (\(\rho_g \sim 4 \times 10^6\ \text{cm}^{-2}\)) and only slightly more than in Kernouvé (Table 1). Dislocations with \(b=[001]\) are most common, but infrequent \(b=[100]\) were observed. Rare \(b=[101]\) dislocations were found in subgrain boundaries. In some grains, straight \(b=[001]\) screws are present in moderately (Fig. 4d) or heavily deformed grains (Fig. 4f), whereas other grains contain curved or tangled dislocations, or subgrain boundaries (Fig. 4e). In some subgrain boundaries, dislocations are notably straight and parallel and contained in a tight band (inset Fig. 4e), indicating better developed subgrains than in Kernouvé. Some subgrain boundaries consist mainly of \(b=[001]\) dislocations, whereas others consist mainly of \(b=[101]\) dislocations (Fig. 4e). The \(b=[101]\) dislocations likely formed by the combination of \(b=[001]\) and \(b=[100]\) dislocations during climb.

3.2.6. MIL 99301 (LL6 S1)

Olivine in MIL 99301 has a low overall dislocation density (\(\rho_g \sim 2 \times 10^7\ \text{cm}^{-2}\)) (Table 1). Dislocations include straight \(b=[001]\) screws (Fig. 4h), somewhat common \(b=[100]\) dislocations (Fig. 4g), rare \(b=[101]\) dislocations in areas close to \(b=[001]\) and \(b=[100]\) dislocations (Fig. 4g), and curved dislocations of all types (Fig. 4g, h). As with Portales Valley, the \(b=[101]\) dislocations likely formed by the combination of \(b=[001]\) and \(b=[100]\) dislocations during climb. Some dislocations are jogged, evidence for the movement of one dislocation through another. MIL 99301 olivine also contains a kink band (Fig. 4h) whose terminus is marked by a \(b=[100]\) dislocation. \(b=[001]\) screw
dislocations are jogged where they intersect with the kink band (Fig. 4i), evidence for the movement of one or more dislocations through the screws. Subgrain boundaries in MIL 99301 include “picket fence” and single dislocation sets (Fig. 4g), as in Kernouvé and Portales Valley, and contain \( b = [001] \) and \( b = [101] \) dislocations, as in Portales Valley.

4. DISCUSSION

4.1. Annealing (recovery) during and after shock

Microstructures in olivine can be used to evaluate annealing (microstructural recovery) effects, both as a result of dynamic heating (during shock deformation) and as a result of static heating (post-impact heating). Features produced by annealing include curved dislocations, small dislocation loops, “picket fence” subgrain boundaries, annihilation of dislocations, and healing of cracks (e.g., Phakey et al., 1972; Goetze and Kohlstedt, 1973; Ashworth and Mallinson, 1985).

Fig. 5 shows a large difference in olivine between the reference L6 chondrites (Park, Leedey, Bruderheim, Morrow County) and those that were purportedly annealed (Kernouvé, Portales Valley, MIL 99301), in terms of such parameters as the average dislocation density, the weighted shock stage, and the FFB dislocation ratio. The reference L6 chondrites show a crude correlation between dislocation density and shock stage, but the annealed chondrites have low dislocation densities that do not correlate with shock stage (Fig. 5a). In addition, the FFB ratio for the reference chondrites lies close to 1 (0.96-1.0, i.e., there are few subgrain boundaries in them), whereas the FFB ratio is significantly lower in the annealed chondrites (0.74-0.88) (Fig.
5b). Among all the meteorites, dislocation density and FFB ratio are correlated, with the annealed chondrites having both low FFB and low dislocation density (Fig. 5b).

The latter correlation is the trend expected for microstructural recovery involving dislocation climb and annihilation (Fig. 5b). This implies that the low dislocation densities in Kernouvé, Portales Valley, and MIL 99301 were produced by significant recovery, and supports the identification of these chondrites as extensively annealed. The subgrain boundaries that are present in Kernouvé, Portales Valley, and MIL 99301 must be the result of post-shock annealing not directly related to their impact heating, because the annealing effects associated with even strongly shocked (S4 and S5) chondrites are minor. This implies that annealing was caused by endogenic heat.

The dislocation climb necessary for subgrain boundary formation is thermally activated and related to both the time and temperature of annealing (see below). As there is no relationship between FFB ratio and shock stage or dislocation density for the reference L6 chondrites, which were presumably shocked to different temperatures, annealing time must be the critical variable, and longer annealing times for Kernouvé, Portales Valley, and MIL 99301 can be surmised. Thus, one can infer rapid cooling after deformation for the L6 chondrites, and slow cooling after deformation for the annealed chondrites. The extended post-deformation annealing for Kernouvé, Portales Valley, and MIL 99301 implies deep burial from a cooling surface, and possibly emplacement in a large mass of warm materials. In contrast, all the L6 chondrites evidently cooled more rapidly after deformation, as a result of shallow burial from a cooling surface.
Fig. 5. Relationship between geometric average dislocation density and (a) weighted shock stage, and (b) average free/(free+bound) dislocation ratio in olivine. Reference L6 chondrites show a crude correlation between dislocation density and weighted shock stage, and all have a large proportion of free dislocations. In contrast, the annealed chondrites Kernouvé, Portales Valley and MIL 99301 contain a distinctly lower dislocation density and lower proportion of free dislocations, as expected for dislocation climb and annihilation.

In principle, the time-temperature conditions necessary to create subgrain boundaries in Kernouvé, Portales Valley, and MIL 99301 can be evaluated using the experimental data of Goetze and Kohlstedt (1973), but in practice it appears no firm conclusion can be drawn from these data. The experiments related a decrease in free/bound dislocation ratio to annealing temperatures and times through an Arrhenius expression. Although these data have been utilized by others to interpret the thermal
histories of shocked chondrites (Ashworth and Mallinson, 1985), the validity of the
Arrhenius constants are uncertain, and other work suggests possibly slower rates of
recovery, by roughly 1-2 orders of magnitude (Guegen and Nicholas, 1980). Allowing for
two orders of magnitude slower recovery, annealing durations of tens of hours (at
1000°C) to hundreds of years (at 800 °C) are implied for the annealed chondrites,
assuming a decrease in FFB of 25% (from 1 to 0.75). This is much less than the millions
of years cooling time needed for a parent body heated by $^{26}$Al decay (Trieloff et al.,
2003; Kleine et al., 2008), which at face value implies that a $^{26}$Al radiogenic heat source
cannot be responsible for the post-deformation annealing experienced by the annealed
chondrites. However, the result is uncertain. Moreover, in apparent contrast to the
natural samples, the experimental charges showed little dislocation annihilation during
recovery (Goetze and Kohlstedt, 1973), suggesting the experiments may not be
applicable to the annealed chondrites.

Although olivine grains in the strongly shocked chondrites (Leedey, Bruderheim,
Morrow County) do not have many subgrain boundaries, there is evidence for significant
dislocation climb in Morrow County, including the presence of extensively curved and
bowed dislocations and small dislocation loops. These features in Morrow County (S5)
compared to Leedey and Bruderheim (both S4) can be explained by higher
temperatures during deformation (Phakey et al., 1972), as thermal activation allows
dislocations to bow away from the linear configurations defined by Peierls barriers. This
explanation is plausible because there is a sharp increase in shock temperature and
post-shock temperature with an increase in shock pressure from shock stage S4 to S5
(Stöffler et al., 1991; Schmitt, 2000).
Annealing experiments of shock-deformed olivine show that annealing for 90 hours at 800-900 °C does not produce subgrain boundaries, but that annealing for this amount of time at 1000 °C does (Ashworth and Mallinson, 1985). Further, deformation experiments from 600-1250 °C showed only limited recovery at temperature <1000 °C (Phakey et al., 1972). Thus, Morrow County must have experienced a combination of either low shock temperatures (<1000 °C) or short post-shock annealing times (<90 hours), or both. For the other rapidly cooled L6 chondrites (Leedey, Bruderheim, Park), post-shock annealing temperatures and durations were even less, probably <<800 °C and <<90 hours.

Thermal histories of chondrites during and after shock can be evaluated also based on metallographic techniques (e.g., Smith and Goldstein, 1977). For example, Scott et al. (2014) provided an account of cooling histories of low-shock H chondrites derived from studies of metal, including quantitative estimates of cooling rates based on the central taenite method. This method reflects cooling at temperatures (~500 °C) that are probably much lower than those needed to produce significant recovery in olivine. Thus, metallographic cooling rates might or might not directly correspond to the annealing effects discussed here. Nevertheless, metallographic cooling rates for Kernouve (10 °C/Ma) and Portales Valley (25 °C/Ma), although not unusual, are on the low side for low-shock H chondrites (Scott et al., 2014). This is consistent with deep burial of these meteorites during cooling. These cooling rates could correspond to depths of ~10-15 km in the H chondrite parent asteroid (Scott et al., 2014).

4.2. Shock stages of quickly cooled and annealed chondrites
The correlation between shock stage and average dislocation density for the L6 chondrites (Fig. 5a) is what one would expect for a shock history uncomplicated by extensive post-deformation recovery. The data imply characteristic dislocation densities in olivine for substantially unannealed and quickly cooled S4 and S5 chondrites of ~3 x $10^{8}$ to $1 x 10^{10}$ cm$^{-2}$, and for S1 chondrites of ~3 x $10^{8}$ cm$^{-2}$. These densities are generally consistent with literature values (Ashworth and Barber 1975, 1977; Madon and Poirier, 1983; Töpel-Schadt and Müller, 1985; Ruzicka, 1990; Langenhorst et al., 1995; Leroux et al. 1996; Joreau et al. 1996, 1997).

The highest average dislocation densities were found in Bruderheim, despite this meteorite having a lower conventional shock stage than Morrow County and a lower weighted shock stage than Leedey (Fig. 1, 5). This probably indicates that the region in Bruderheim observed with TEM was slightly more deformed than average for Bruderheim. This variation is not unexpected, as the passage of a shock wave in rocks will produce local variations in shock pressures and temperatures owing to the heterogeneous nature of the rocks (e.g., Sharp and DeCarli, 2006). It is also possible that Morrow County experienced some amount of dislocation annihilation during a limited recovery period.

If the low average dislocation densities for Kernouvé, MIL 99301, and Portales Valley were the result of recovery that destroyed many dislocations (Sec. 4.1), the question arises as to how many dislocations were removed and what shock stage these meteorites may have had originally. Two approaches using dislocation densities in olivine, together with comparisons to the reference chondrites, can be used as guides to the original deformation: the maximum dislocation density (approach 1) and the
dislocation densities of areas that contain dislocations but no subgrain boundaries (approach 2). Using approach 1, the maximum dislocation densities (cm\(^{-2}\)) in Kernouvé, MIL 99301, and Portales Valley are \(~7 \times 10^6\), \(~1 \times 10^9\), and \(~1 \times 10^{10}\), respectively (Table 1). These densities are respectively similar to those in Park (S1), between Park and Leedey (i.e., S2-S3), and between Morrow County and Bruderheim (i.e., S4-S5).

Using approach 2, the densities are \(~6 \times 10^6\) – \(~5 \times 10^8\) in Kernouvé and \(~6 \times 10^7\) – \(~1 \times 10^9\) in MIL 99301, both similar to that in Park, whereas Portales Valley has too large a spread (\(~1 \times 10^6\) – \(~1 \times 10^{10}\)) to provide a useful constraint (Fig. EA-1).

Based on these comparisons, we suggest that post-deformation annealing lowered apparent optical strain levels in olivine from Kernouvé, MIL 99301, and (especially) Portales Valley. Kernouvé probably was S1 originally, though a more deformed S1 than it is now. MIL 99301 originally could have been shock stage S2-S3 or a more deformed S1, less than the S4 inferred by Rubin (2002) based on other potential shock indicators. Portales Valley could have been shock stage S4-S5 originally, which is more than the initial S3 inferred by Kring et al. (1999) and Rubin et al. (2001), and less than the S6 mentioned by Rubin (2004).

We have no reason to doubt that among the three annealed chondrites, Kernouvé was the least deformed initially, MIL 99301 next most deformed, and Portales Valley the most deformed, but the estimates of initial shock stages should be considered uncertain. Too little is known still about the correspondence of deformation between TEM and optical methods. The real possibility of multiple impacts or heterogeneous impact effects also can complicate interpretations. In addition, although recovery of modestly deformed (S2 or S3) olivine to produce S1 olivine seems
reasonable, less clear is whether more strongly deformed grains (S4 or S5) could be effectively recovered. For such heavily deformed grains, significant annealing might result in recrystallization instead (Scott et al., 2014).

4.3. Temperatures during shock

Three independent temperature proxies that relate to thermally activated processes during slip can be used to assess temperatures during deformation (Sec. 2). These include 1) the length of $b=[001]$ dislocations in screw sense compared to other orientations (% $b=[001]$ screw sense, lower at higher temperature), 2) the relative number of $b=[100]$ dislocations (higher at higher temperature), and 3) the presence of jogged dislocations (more prevalent at higher temperature) and kink bands (those with [100] slip are active at higher temperature—Carter et al., 1968; Green and Radcliffe, 1972a, b; Boland and Buiskool Toxopeus, 1977).

Fig. 6 shows for all meteorites studied the % $b=[001]$ screw sense and the relative number of $b=[100]$ dislocations. Both parameters suggest elevated temperature during deformation for Morrow County and Kernouvé (Fig. 6). Based on the $b=[100]$ data, MIL 99301 and Park were probably deformed at somewhat elevated temperature (Fig. 6), consistent with the presence in these meteorites of jogged dislocations and kink bands (Table 1). In MIL 99301, at least one well-studied kink band (Fig. 4h, i) seems to be of the type activated at high temperature. At relatively low laboratory strain rates ($\sim 10^{-2}$ to $10^{-8}$ s$^{-1}$), $b=[100]$ dislocations begin to appear above 800 °C and become prevalent above 1000 °C (Green, 1976; Gueguen and Nicolas, 1980). These transition temperatures increase at the higher strain rates that are expected for shock (Raleigh, 1968; Carter et al., 1968; Green, 1976; Gueguen and Nicolas, 1980). In none of the
samples studied here are $b=[100]$ dislocations prevalent. This suggests that those meteorites that contain moderately common (Park, MIL 99301) to common $b=[100]$ dislocations (Kernouvé, Morrow County) were deformed at a temperature of ≥800-1000 °C, probably warmer for Kernouvé and Morrow County than for Park and MIL 99301.

Fig. 6. Relationship between two different proxies for deformation temperature in olivine, including $b=[100]$ dislocation prevalence, and the percentage of $b=[001]$ dislocations present in a screw orientation. For the latter, points show the mean values among TEM areas examined (excluding one atypical area in Morrow County) and the error bars show the standard deviation of these values. Symbols as in Fig. 5.

For Morrow County, elevated deformation temperature is almost certainly the result of intense shock, consistent with evidence for some dynamic heating (Sec. 4.1). Assuming the applicability of shock loading experiments (Schmitt, 2000), and a best estimate for shock stage S5 of 35-45 GPa (Stöffler et al., 1991), a temperature increase of ~700-900 °C can be inferred for shock stage S5. This is similar to the ≥800-1000 °C temperature implied for Morrow County based on $b=[100]$ dislocations.
For Kernouvé, Park, and MIL 99301, strong heating during intense shock is not viable, and shock deformation must instead have occurred when the parent bodies were hot at the time of impact deformation. Inferred temperatures of ≥800-1000 °C based on dislocation microstructure are similar to the peak metamorphic temperatures experienced by chondrites during thermal metamorphism (e.g., Huss et al., 2006). Thus, deformation for Kernouvé (H6), Park (L6), and MIL 99301 (LL6) probably occurred during thermal metamorphism when the parent bodies were being metamorphosed to type 6 grade. This conclusion holds for three different parent bodies (H, L, LL) among the three studied, suggesting a not uncommon process of impact into warm asteroidal bodies.

Shock deformation of an already warm target was suggested also for the Kobe CK4 chondrite based on the presence of extensive silicate darkening caused by small metal-sulfide inclusions in silicate such as olivine (Tomoeka et al., 2001). Such inclusions can form by shock injection of metallic melts into fractures (Leroux et al., 1996), and injection is enhanced when the target materials are warm (Schmitt, 2000; Nakamura et al., 2000). Limited silicate darkening is seen in both MIL 99301 and Portales Valley (Rubin et al., 2001; Rubin, 2002, 2004). This weakly supports the idea of impacting a warm target.

Also characteristic of shock deformation in a warm chondritic target is recrystallized troilite (Schmitt, 2000). If the pre-shock temperature is elevated (i.e., ~650 °C), troilite recrystallizes readily during shock to form polycrystalline troilite even under conditions that result in little deformation of olivine and plagioclase (Schmitt, 2000). Polycrystalline troilite is not prevalent in any of the S1 chondrites but has been reported
The dearth of polycrystalline troilite provides little support for a warm target, but such troilite would not form if it had melted (Schmitt, 2000). This might be expected either for higher pre-shock temperatures or high temperatures associated with stronger shock. In Portales Valley at least, troilite was probably impact-melted along with metal (Ruzicka et al., 2005). Thus, the significance of not finding much polycrystalline troilite in the annealed chondrites is not clear.

### 4.4. Implications for collisional events affecting ordinary chondrite parent bodies

Fig. 7 summarizes for olivine in all chondrites studied the amount of post-deformation annealing based on the FFB ratio, and temperature during shock based on the prevalence of $b=[100]$ dislocations. This diagram can be used as a guide to understand the impact histories of the chondrites and their parent bodies.

For the L6 chondrites (Leedey, Bruderheim, Park, Morrow County), low FFB ratios imply rapid cooling following deformation and shallow burial beneath a cooling surface (Fig. 7; Sec. 4.1). All could have originated as ejecta of some sort. $^{39}$Ar-$^{40}$Ar ages of ~500 Ma for Bruderheim (Turner, 1969; Bogard et al., 1987) and ~450-470 Ma for Morrow County (Patricia Clay, University of Manchester, pers. comm.) are consistent with the postulated break-up event of the L chondrite parent body, and both meteorites could have cooled in one or more of the break-up fragments. $^{39}$Ar-$^{40}$Ar data for Leedey imply an older reheating event and collision at ~3.8 Ga (Bogard et al., 1987), suggesting Leedey cooled in near-surface regolith ~3.8 Ga ago and was not strongly shocked in the ~0.5 Ga event. Park has an unusually low shock stage for an L chondrite, with no evidence it ever was significantly shocked. Still, it shows evidence for weak shock occurring at an elevated temperature, while the parent body was warm (Sec. 4.3),
followed by minimal post-shock annealing (Fig. 7). Park has an ancient $^{39}$Ar-$^{40}$Ar plateau age of 4492.6 ± 9.5 Ma (Patricia Clay, University of Manchester, pers. comm.). The microstructure and age data for Park are consistent with syn-metamorphic impact excavation of warm interior materials from the parent body, and emplacement of these materials near the surface of the parent body where cooling was rapid.

Kernouvé olivine has both common $\mathbf{b}=[100]$ dislocations and low FFB ratios, suggesting shock near peak metamorphic temperature followed by slow cooling at depth (Fig. 7; Sec. 4.1, 4.3). The meteorite has an ancient $^{39}$Ar-$^{40}$Ar age of ~4.46 Ga (Turner et al., 1978), consistent with early cooling. Kernouvé was never significantly shocked (Sec. 4.2), so it probably was minimally disturbed during metamorphism and could have cooled slowly as warm sub-regolith (basement) material in the H chondrite parent body. Still, the meteorite shows evidence for a weak shock occurring at high ambient temperatures. Coarse metal veins in Kernouvé have been interpreted as a manifestation of an early shock disturbance (Hutson, 1989; Rubin, 2003; Friedrich et al., 2013), which probably occurred in the same event that weakly deformed olivine at high temperatures. Evidently, only a weak (S1) shock at high temperatures was needed to mobilize metal into veins.
Fig. 7. Diagram summarizing thermal and deformation histories of meteorites as inferred from TEM data for olivine. Post-shock annealing is related to the value of average free/(free+bound) dislocation ratio and should correspond to cooling rate, whereas temperature during deformation is related to the prevalence of \(b=[100]\) dislocations. There is no simple correspondence between post-shock annealing and deformation temperature. All the reference L6 chondrites (circles) can be explained by rapid cooling following shock, whereas the annealed chondrites (squares) can be explained by deeper burial from a cooling surface. As discussed in the text, elevated temperatures during deformation can be explained by either intense shock metamorphism (for Morrow County) or warm target materials (for Kernouvé, MIL 99301, Park).

[432]

[433] As with Kernouvé, MIL 99301 was shocked at elevated temperature and cooled at depth (Fig. 7; Sec. 4.1, 4.3). However, \(^{39}\text{Ar}-{^{40}\text{Ar}}\) data for MIL 99301 suggest two shock events, one at 4.52 ± 0.08 Ga and another at 4.23 ± 0.03 Ga (Dixon et al., 2004).

[434] Although Dixon et al. suggested slow cooling for MIL 99301 in the second event, this
seems unlikely. MIL 99301 has a wide range of shock stages including a small admixture of more highly shocked material (Fig. 1), possibly caused by impact mixing or heterogeneity introduced during a shock event. The first possibility is favored by a comparatively narrow range of shock effects seen in other chondrites such as Leedey, Bruderheim, and Morrow County (Fig. 1), which suggests that single shock events do not produce an overly large range of shock stages. In any case, given the evidence for strain obliteration in olivine during extended annealing of the sort that affected much of MIL 99301 (Sec. 4.2), it seems unlikely that olivine with highly different shock stages would be preserved during such annealing. Slow cooling more likely occurred before the introduction of highly shocked grains. Thus, the first degassing event ~4.52 Ga ago could have entailed slow cooling, while the parent body was undergoing thermal metamorphism, and a second shock event at ~4.23 Ga ago could have either excavated and mixed materials of diverse deformation and thermal histories or created heterogeneous shock effects.

Portales Valley also cooled slowly at depth (Fig. 7). Like Kernouvé, the meteorite contains coarse metal veins that probably formed by impact mobilization of metal (Kring et al., 1999; Rubin, 2003; Ruzicka et al., 2005). Unlike Kernouvé, Portales Valley could have been strongly shocked before extensive annealing (Sec. 4.2), consistent with formation directly below an impact crater (Kring et al., 1999; Rubin, 2003; Ruzicka et al., 2005) in well-insulated H-chondrite basement. The Portales Valley source region could have been hot (possibly ~900-950 °C) during impact (Ruzicka et al., 2005), but at face value a relatively low proportion of $b=[100]$ dislocations in olivine suggests a lower deformation temperature (Fig. 7). However, microstructure data do not exclude the
possibility of Portales Valley having been slightly cooler but still warm (T<800 °C) at the
time of impact, and many $\mathbf{b}=[100]$ dislocations may have been destroyed during
annealing, leading to an erroneously low estimate of deformation temperature. The
latter possibility is supported by the presence in Portales Valley of $\mathbf{b}=[101]$ dislocations
in well-formed subgrain boundaries that were likely produced by the combination of
$\mathbf{b}=[001]$ and $\mathbf{b}=[100]$ dislocations during dislocation climb (Sec. 3.2.5). Thus, Portales
Valley may indeed have been shocked while the parent body was warm and undergoing
thermal metamorphism, although the temperature at the time of impact is uncertain. An
old $^{39}\text{Ar}^{40}\text{Ar}$ age for Portales Valley of 4477 ± 16 Ma (Garrison and Bogard, 2001)--
indistinguishable from Kernouvé and the older age for MIL 99301-- is consistent with
early shock. Thus, it is possible that all of the slowly-cooled S1 meteorites (Kernouvé,
MIL 99301, Portales Valley) were deformed and annealed at depth in parent bodies that
were undergoing early thermal metamorphism.

4.5. Breaking paradigms

The traditional view of chondrite formation is that 1) “secondary” thermal
metamorphism pre-dated “tertiary” shock processes, and that 2) thermal metamorphism
caused by endogenic heating resulted in an onion-shell stratigraphy, with higher
metamorphic grades at greater depths (Dodd, 1981; Hutchison, 2004). However, each
of these paradigms may not be entirely valid. Our data support the idea that thermal
metamorphism and shock likely overlapped in time during and shortly after the accretion
of the H, L, and LL chondrite parent bodies (Grimm, 1985; Ganguly et al., 2013;
Friedrich et al., 2013, 2014; Swindle et al., 2014). Moreover, impact cratering occurring
concurrently with endogenic metamorphism could have redistributed material from
different depths in the parent bodies, locally excavating hot and burying cold material. An onion shell structure would tend to be reconfigured by impacts, destroying an expected inverse correlation between cooling rate and metamorphic grade (Scott et al., 2014), and possibly including an extensive scrambling caused by collisional disruption and reaccretion (Grimm, 1985; Taylor et al., 1987; Ganguly et al., 2013). However, the structure could be reformed during continued endogenic heating. This would lead to a complex parent body stratigraphy that was non-axisymmetric and temporally variable. Furthermore, our results indicate pitfalls in using the shock stage of olivine alone as a guide to whether chondrites were significantly affected by shock. Some shock stage S1 chondrites (e.g., Portales Valley) were significantly shocked prior to thermal annealing that partly obliterated strain effects in olivine. Thus, it might not be straightforward to use the properties of chondrites to reconstruct simple thermal models of their asteroidal parent bodies. Olivine microstructures investigated with transmission electron microscopy can provide additional key evidence to aid in such reconstructions.

5. CONCLUSION

Detailed optical and electron petrographic studies for olivine in various ordinary chondrites provide a wealth of information related to collisional and metamorphic processes. The L6 chondrites Park, Leedey, Bruderheim and Morrow County show the effects of varying shock intensity and all could have cooled quickly in ejecta fragments. In contrast, the S1 chondrites Kernouvé (H6), Portales Valley (H6/7), and MIL 99301 (LL6) all show good evidence for extensive recovery during protracted annealing that lowered optical strain in olivine as a result of burial at depth, probably within warm parent bodies. In addition, there is good evidence that some S1 chondrites from each of
the three ordinary chondrite groups, including Kernouvé, MIL 99301, and Park, were shocked at elevated temperature (≥800-1000 °C), while the parent bodies were undergoing endogenic thermal metamorphism. Portales Valley may also have been shocked while the parent body was warm. The data show the pitfalls in relying on optical shock stage alone to infer an absence of shock and to construct cooling models for parent bodies. For example, Park, although never shocked significantly, shows evidence for an impact scrambling process that transported hot interior materials to a cooling surface. On the other hand, Kernouvé, also never shocked significantly, is more likely to have cooled in place at depth in the parent body and to provide a record of original parent body thermal metamorphic structure. Finally, the data for L6 chondrites, all evidently rapidly cooled following shock and lacking evidence for much olivine recovery, suggest that impact heating alone was not solely responsible for thermal metamorphic effects in these or other chondrites. Burial at depth inside warm, insulating bodies was necessary to result in significant olivine recovery.

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ELECTRONIC ANNEX

Includes: Table EA-1, Table EA-2, Fig. EA-1

For the paper “Deformation and thermal histories of ordinary chondrites: Evidence for post-deformation annealing and syn-metamorphic shock”
Table EA-1. Olivine shock stage data based on optical microscopy; meteorites are arranged according to increasing weighted shock stage.\(^a\)

| Meteorite       | Sections\(^b\) | Number of grains | % S1  | % S2  | % S3  | % S4  | % S5  | % S6  | Conventional shock stage | Weighted shock stage | Comment                                                                 |
|-----------------|-----------------|------------------|-------|-------|-------|-------|-------|-------|---------------------------|---------------------|-------------------------------------------------------------------------|
| Kernouvé        | 0666-1, 0666-2A, USNM 1054-2 | 115               | 91.3  | 7.0   | 0     | 0     | 0     | 0.9   | S1                        | S1.13               | Irregular metal veins; low angle boundaries.                            |
| Portales Valley | 0056-3, 0056-4  | 100              | 84    | 16    | 0     | 0     | 0     | 0     | S1                        | S1.16               | Metal veins; low angle boundaries.                                     |
| Park            | 0617-1A, 0617-1B, 0617-2A | 153              | 76.5  | 15.0  | 6.5   | 1.3   | 0     | 0     | S1                        | S1.35               | Low angle boundaries.                                                  |
| MIL 99301       | 0422-1, 0422-B  | 65               | 73.8  | 13.8  | 1.5   | 4.6   | 1.5   | 4.6   | S1                        | S1.60               | Breccia; low angle boundaries.                                         |
| Holbrook        | 0302-5B, 0302-6A | 94               | 30.9  | 18.1  | 26.6  | 24.5  | 0     | 0     | S3                        | S2.45               | Breccia; not used for TEM owing to large dispersion of shock stages.    |
| Bruderheim      | 0618-1A, 0618-1B, 0618-2A | 136             | 0     | 1.5   | 30.9  | 55.9  | 11.8  | 0     | S4                        | S3.78               | Minor melt pockets.                                                    |
| Leedey          | 0504-1A, 0504-1B, ASU 489-A-1 | 162              | 0     | 0.6   | 16.0  | 72.2  | 11.1  | 0     | S4                        | S3.94               | Strong S4. Minor melt pockets.                                         |
| Morrow County   | 0497-2A, 0497-6A, 0497-6B | 149             | 0     | 0     | 3.4   | 47.0  | 49.7  | 0     | S5                        | S4.46               | Maskelynite; shock veins; chr-plag\(^c\).                              |

\(^a\) Criteria for assigning olivine shock stages as follows: S1 <2° misorientation; S2 2-3° misorientation; S3 2-3° misorientation and at least one set of parallel planar fractures (PFs) or planar deformation features (PDFs); S4 3-5° misorientation and ≥2 sets of PFs/PDFs; S5 >5° misorientation and ≥3 sets of PFs/PDFs; and S6 recrystallized.

\(^b\) CML section number except where noted. ASU = Arizona State University, USNM = U.S. National Museum.

\(^c\) Abundant chromite-plagioclase (maskelynite) assemblages.
Table EA-2 (next three pages). Olivine microstructure data for individual areas examined with transmission electron microscopy.

| Meteorite / sections | Area   | Dislocation character                                                                 | \( \rho \) (cm\(^{-2}\)) | Burgers vector \( \mathbf{b} \) | % FFB | % \([001]\) | % \([100]\) |
|----------------------|--------|---------------------------------------------------------------------------------------|-----------------------------|-----------------------------|-------|-------------|-------------|
| Bruderheim / 0618-1B | 1A10   | [001] screws with straight edges, few [100]                                          | 5.4E+09                     |                             | 100   | 51          |             |
| 1A11                 | long   | [001] screws with straight edges                                                      | 2.8E+09                     |                             | 100   | 66          |             |
| 1A12                 | long   | [001] screws with straight edges                                                      | 2.0E+09                     |                             | 100   | 32          |             |
| 1A13c                | long   | [001] screws with straight edges                                                      | 2.4E+09                     |                             | 100   | 43          |             |
| 1A13e                | long   | [001] screws with straight edges                                                      | 7.1E+09                     |                             | 100   | 58          |             |
| B3-ol                | straight & jogged [001]                                                               | 2.3E+10                     |                             | 100   | 27          |             |
| 2A1                  | slightly curved & jogged [001], few screws                                           | 6.4E+10                     |                             | 100   | 4           |             |
| 2A2                  | slightly curved & jogged [001], few screws                                           | 8.0E+10                     |                             | 100   | 5           |             |
| 2A2a                 | slightly curved & jogged [001], few screws                                           | 1.5E+11                     |                             | 100   | 3           |             |
| 2F1                  | slightly curved & jogged [001], some screws                                          | 1.0E+10                     |                             | 100   | 9           |             |
| 2D1                  | slightly curved & jogged [001], some screws                                          | 1.5E+10                     |                             | 100   | 25          |             |
| 2A3                  | curved & jogged [001], some screws, [100]                                           | 1.6E+10                     | [001], [100]                | 100   | 20          |             |
| Leedey / 0504-1B     | 4A2    | long [001] screws, others, some curved                                                | 5.53E+09                    |                             | 100   | 12          |             |
| 4A3                  | long   | [001] screws, others, some curved                                                     | 1.98E+09                    |                             | 100   | 21          |             |
| 4A4                  | [001] screws & bowed edges, curved [100]                                             | 3.08E+09                    | [100], [001]                | 93    | 46          |             |
| 4A5                  | long   | [001] screws                                                                         | 5.30E+09                    |                             | 100   | 78          |             |
| 4B1                  | long   | [001] screws, others, some curved                                                     | 1.02E+10                    |                             | 100   | 39          |             |
| 4B3                  | long   | [001] screws, others, some curved                                                     | 2.14E+10                    |                             | 100   | 39          |             |
| 4C1                  | long   | [001] screws, others, some curved                                                     | 2.90E+09                    | [100], [001]                |       |             |             |
| 4C2                  | long   | [001] screws, arrays, kink bands                                                     | 7.05E+08                    |                             | 70    | 73          |             |
| 4E1                  | straight 3 vectors, many short curved                                                | 8.16E+08                    |                             | 100   | 36          |             |
| 4E2                  | long   | [001] screws, others, some curved                                                     | 2.42E+09                    |                             | 100   | 72          |             |
| 4F1                  | long   | [001] screws, others, some curved                                                     | 2.07E+09                    |                             | 100   | 55          |             |
| 4D2                  | frequent kink bands                                                                  |                             |                             |       |             |             |
| Morrow County / 0497-6B| 1A2    | curved, loops, few straight segments                                                 | 1.37E+09                    |                             | 100   | 18          |             |
| 1A4                  | curved | loops                                                                                | 1.21E+10                    |                             | 100   | 8           |             |
| 1A10                 | curved | loops                                                                                | 2.40E+10                    |                             | 100   | 0           |             |
| 1B1                  | curved | loops                                                                                | 4.30E+09                    | [001], [100]                | 100   | 16          |             |
| 1B2                  | curved | loops                                                                                | 1.15E+10                    | [001], [100], others?       | 92    |             |             |
| 1B3                  | curved | loops                                                                                | 3.91E+09                    |                             | 93    | 9           |             |
| 1B6                  | curved | loops                                                                                | 8.31E+09                    |                             | 100   | 11          |             |
| 1C1                  | curved | loops                                                                                | 9.99E+09                    | [001], [100]                | 100   | 0           |             |
| 2A1                  | curved | loops                                                                                | 3.41E+09                    | [001], [100]                | 100   | 5           |             |
| 2A2                  | curved | loops                                                                                | 9.96E+09                    |                             | 100   | 6           |             |
| 2A4                  | curved | loops                                                                                | 2.30E+08                    |                             | 100   | 43          |             |
| FIB-1                | curved | loops                                                                                | 4.13E+09                    | [001] predominant, [100]    | 100   | 0           |             |
| FIB-2                | curved | loops                                                                                | 5.09E+09                    | [001] predominant, [100]    | 100   | 0           |             |
| Park / 0617-1B       | 2A2    | curved, straight [001] screws                                                        | 1.39E+08                    |                             | 100   | 49          |             |
| 2A3                  | straight screws from kink band                                                        | 1.87E+07                    |                             | 100   | 62          |             |
| 2B1                  | curved, straight [001] screws                                                        | 3.55E+08                    | [001], [100]                | 100   | 45          |             |
| Park continued | 2B1a | curved [001], straight [001] screws | 1.58E+08 | [001] | 100 | 60 |
| 2B3 | curved, straight screws from kink band | 3.09E+08 | 100 | 19 |
| 2B4 | curved, straight [001] screws | 6.96E+08 | 100 | 17 |
| 2B2R | straight screws from kink band, small loops | 2.75E+08 | [001], [100] | 100 | 28 |
| 2D1-ol | array of short [100] segments | 8.82E+07 | [100], [?]| 100 | 28 |
| 2G1 | curved [001], few [001] screws, tangle | 3.12E+07 | [001], [100] | 100 | 6 |
| 1A1a | [001] with long screws and bowed edges | 8.57E+08 | 100 | 60 |
| 1A1 | curved [001], straight [001] screws | 1.26E+09 | 100 | 24 |
| 1A2 | curved, looped, long [001] from kink band | 7.20E+08 | 100 | 32 |
| 1A3a1 | curved [001], straight [001] screws | 1.13E+09 | 100 | 45 |
| 1A3a | curved [001], straight [001] screws | 9.26E+08 | 100 | 18 |
| 1A3b | curved [001], straight [001] screws | 8.32E+08 | 100 |
| 1A3c | curved [001], straight [001] screws | 3.10E+08 | 100 | 46 |
| 1A4 | curved [001], straight [001] screws | 3.54E+08 | 100 | 24 |
| 1A5 | curved [001], straight [001] screws | 1.10E+09 | 100 | 47 |

| Kernouvé / 0666-1 | 4A1 | [001] well formed array, loose array of [100] | 1.6E+08 | [001] and [100] | 42 | 0 |
| 4A2 | random bowed + 2 well-formed arrays | 1.8E+08 | 54 | 0 |
| 4A3 | [001] screws, curved [001] in array | 1.6E+08 | 79 | 26 |
| 4A4 | none | 1.0E+00 | 100 | 0 |
| 4A5 | none | 1.0E+00 | 100 | 0 |
| 4A6 | isolated | 9.3E+07 | 100 | 0 |
| 4A7 | none | 1.0E+00 |
| 4A8 | curved arrays ([100] and [001]) | 4.6E+08 | [001] and [100] | 100 | 0 |
| 4A9 | [001] curved into a poorly formed array | 3.3E+08 | [001] | 100 | 0 |
| 4A10 | well & poorly formed intersecting arrays | 2.8E+08 | 0 | 0 |
| 3A1 | none | 1.0E+00 |
| 3A2a | loosely formed [001] & [100] arrays | 4.0E+08 | mostly [001], some [100] | 100 | 0 |
| 3A3a | slightly curved, some intersections | 2.2E+08 | 100 | 0 |
| 3A3b | slightly curved, very low density | 6.7E+06 | 100 | 0 |
| 3A3c | slightly curved, some intersections | 7.7E+07 | 100 | 0 |
| 3A3d | slightly curved very low density | 6.7E+06 | 100 | 0 |
| 3A3e | none | 1.0E+00 |
| 3A3f | slightly curved, loosely formed array | 6.0E+07 | 100 | 0 |
| 3A10 | slightly curved & intersecting, one array | 6.8E+08 | mostly [001], some [100] | 74 | 0 |
| 3A10a | straight, possibly pure edge | 6.4E+07 | [001] edge | 100 | 0 |

| Portales Valley / 0056-3, 0056-4 | AA | none | 1.0E+00 |
| Ab | isolated & curved | 3.6E+08 | [001] | 100 | 0 |
| Ac | isolated | 9.6E+07 | 100 |
| Ba | none | 1.0E+00 |
| E | isolated & curved, arrays | 8.6E+08 | [001], some [100] and [101] | 12 |
| F | none | 1.0E+00 |
| Fb | isolated | 3.0E+06 | 100 |
| H | none | 1.0E+00 |
| Hh | none | 1.0E+00 |
| Portales Valley continued | K | intersecting & curved | 5.5E+08 | 100 | 0 |
|--------------------------|---|----------------------|--------|-----|---|
| K                        | Kb | isolated             | 1.1E+06| 100 |   |
|                          | Kk | intersecting & curved | 4.5E+07| 100 | 0 |
|                          | Ki | intersecting & curved, parallel straight | 1.8E+08| 100 | 67 |
|                          | L  | parallel straight, intersecting & curved | 2.8E+09| 100 | 68 |
|                          | Lb | parallel straight, intersecting & curved | 2.9E+09| 100 | 52 |
|                          | Lb2| parallel straight     | 3.5E+08| 100 | 71 |
|                          | Lb3| parallel straight, intersecting & curved | 2.5E+08| [001] screws | 96 | 64 |
|                          | Mb | parallel straight, tangles | 8.3E+09| 100 | 51 |
|                          | Mc | parallel straight, tangles | 2.5E+09| 100 |   |
|                          | Md | parallel straight     | 1.4E+10| 100 | 30 |
|                          | Me | parallel straight, tangles, arrays | 1.9E+09| 82  | 16 |
|                          | Na | isolated & curved     | 7.3E+07| 100 |   |
|                          | Nb | none                  | 1.0E+00|     |   |
|                          | Nc | none                  | 1.0E+00|     |   |
|                          | O  | many                  | 1.2E+10|     | 37 |
|                          | Oa | isolated & curved, arrays | 2.6E+08| 43  | 30 |
|                          | Ob | intersecting & curved, tangles | 1.8E+08| 100 | 9 |
|                          | Oc | isolated & curved     | 1.1E+09| 13  | 0 |
|                          | Od | intersecting & curved, tangles, arrays | 2.1E+09| 95  | 18 |
|                          | Oe | intersecting & curved, tangles, arrays | 1.5E+09| 100 |   |
| MIL 99301 / 0422-B       | F3 | straight [001] screws | 1.4E+09| 100 | 90 |
|                          | F4 |                       | 1.0E+00|     |   |
|                          | G1 |                       | 3.9E+07| 38  |   |
|                          | G1a| free curved; straight on array | 3.0E+08| 20  | 50 |
|                          | G1b|                       | 8.7E+07| 100 | 37 |
|                          | G5a| kink band with jogged 001 screws | 1.8E+08| [001], [100], [101] | 100 | 73 |
|                          | G6a| jogged cutting through 001 screws | 1.0E+08| 100 | 31 |
|                          | G6b|                       | 6.3E+07| 100 | 85 |
|                          | G7 | straight, curved, arrays | 6.0E+08| [001], [100], [101] | 37 | 27 |

a CML section number. b Dislocation density; areas with no dislocations assigned an arbitrary small value to permit calculation of a geometric average. c FFB = free / (free + bound) dislocation ratio. d Length of b=[001] dislocations in screw orientation compared to other orientations; includes more dislocations than in areas with formal determination of Burgers vectors (listed in Burgers vector column), as b=[001] dislocations can usually be identified by their morphology (i.e., extended loop structure).
Fig. EA-1. Microstructure data (dislocation density, and free/(free+bound) = FFB dislocation ratio) for individual olivine TEM areas in (a) reference L6 chondrites and (b) annealed H and LL chondrites. Contrary to the situation for meteorites as a whole, there is no correlation between dislocation density and FFB ratio on the scale of individual TEM areas. If dislocation annihilation occurred during the formation of subgrain boundaries, the dislocation densities of areas with lower FFB would have been higher initially. Together with maximum dislocation densities and dislocation densities in regions with high FFB, these data can be interpreted to indicate that overall dislocation densities prior to recovery were higher initially for the annealed S1 chondrites.