High resolution measurements with miniature neutron scintillators in the SUR-100 zero power reactor

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Abstract—Three 1-mm$^3$ miniature fiber-coupled scintillators have been used to perform cm-wise resolution measurements of the thermal neutron flux within experimental channels of the SUR-100 facility, a zero power thermal reactor operated by the Institute of Nuclear Technology and Energy Systems at the University of Stuttgart. The detection system is developed at the École Polytechnique Fédérale de Lausanne in collaboration with the Paul Scherrer Institut. Thermal neutrons count rates were measured along the experimental channels I and II, which cross the reactor at the center and tangentially to the core, respectively. The reactor was modelled with the Monte Carlo neutron transport code Serpent-2.1.3.1. The comparison of experimental and computed reaction rate distributions showed a good agreement within the core region, with discrepancies within 2σ. An unexpected discrepancy, probably caused by a geometric inconsistency in the computational model of the reactor, was observed in the reflector region of the experimental channel I, where a 20% difference (i.e. 8σ) was found between experimental and simulated results. Significant discrepancies, respectively worth 10σ and 15σ, were noticed at distance, in the lead shielding region, for both experimental channels I and II. In addition, reaction rate gradients across the 2.6 cm and 5.4 cm diameters of both channels were measured. A horizontal reaction rate gradient of (9.09 ± 0.20)% was measured within 2.4 cm across the diameter of the experimental channel II, with a difference from computed results of 2%. The absence of a vertical reaction rate gradient inside the experimental channel I was confirmed by measurements.

Keywords — Scintillation detectors, Monte Carlo simulations, Reaction rate profiles.

I. INTRODUCTION

The objective of the campaign presented hereafter was to perform high spatial resolution measurements to characterize the neutron thermal flux distribution inside experimental channels of the SUR-100 reactor, and to compare the measurement results with Monte Carlo simulations. The study benefited of the innovative miniature detector developed by the Laboratory for Reactor Physics and Systems Behaviour (LRS) at EPFL in collaboration with the Paul Scherrer Institut (PSI) [1]. Three units of the fiber-coupled scintillator detector were used in different arrangements to perform the flux characterization of the experimental channels of the reactor. Their small size results in a neutron flux perturbation lower than any other conventional detector and allows for measurements with high spatial discretization. All the profile measurements presented in this paper are given in relative reaction rates units. In addition, a preexisting MCNP [2] model of the reactor has been converted into Serpent2 [3] and used to run particle transport simulations. Monte Carlo simulations have been performed both to design the experiments, and to compare their results to the acquired measurements. The experimental campaign is described in the first section, followed by the modelling of the reactor, and finally the comparison and discussion of experimental and simulation results are presented.

II. EXPERIMENTAL CAMPAIGN

A. The SUR-100 reactor

The Siemens Training Reactor SUR-100 (in Fig. 1) is a thermal zero-power reactor built in 1964 and located in the University of Stuttgart. It is used for mainly for educational purposes by the Institut für Kernenergetik und Energiesysteme (IKE). The reactor has a maximum thermal power output of 1 W, with a nominal power of 100 mW. It is equipped with a homogeneous core, composed of solid cylindrical slabs of moderator with fuel particles dispersed inside. The core is provided with a lifting mechanism which can move axially the lower core section away from the upper one. The core halves are separated for the shutdown and brought together for the startup of the reactor. The reactivity regulation is performed with two cadmium control plates, which are steered into the core from below. The reactor is provided with various
C. Detector arrangement

The experimental instrumentation consisted in a multiple acquisition neutron detection system: three fiber-coupled scintillators have been used as detectors, with minor modifications with respect to the initial design of past studies [4]. The main improvement regards the aluminum cap, which has been reshaped in a new two-diameter configuration to improve the coupling with the fiber. An aluminum holder housing the three detectors tips was manufactured at a diameter of 26 mm corresponding to the internal diameter of the experimental channel I. Given the difference in diameter of the experimental channels, the diameter of the holding tube had the possibility to be adapted to a larger diameter (54 mm) by means of aluminum spacer rings. To move the detectors along the experimental channels, the front-end holder was mechanically coupled to an aluminum tube manufactured by the IKE laboratory, which was graduated to select the detectors’ position inside the channels. The tube’s handle allowed to adjust the angular orientation of the detectors inside the experimental channels. The choice of aluminum for the holding equipment was straightforward, given its small influence on thermal neutron flux, its availability, its low neutron absorption cross section and rapid decay of the induced activity.

D. Conducted experiments

Steady-state and dynamic measurements were carried over along the campaign. We focus in the present article on the thermal flux characterization through the use of the miniature detectors, namely the measurements of thermal neutron flux profiles:

- along the central experimental channel I: [-40,40] cm around core center,
- along the tangential channel II: [-8,46] cm around core center,
- across the diameter of both channels I (vertically) and II (horizontally).

An explanatory scheme of the performed measurements is presented in Fig. 4. Depending on the experiment, the tube was...
slid into the channels with one of the possible configurations shown in Fig. 5.

The number of the detectors used was varied in dependence of the needs of each experiment. In most of the experiments, one of the miniature detectors (fiber 2) was removed from the holder and used for power monitoring. Count rates were recorded at each position for the time necessary to have statistical errors in the order of 0.1%.

An additional measurement of the thermal flux profile inside the central channel was obtained with a neutron activation experiment which is conducted on a regular basis for teaching purposes at the SUR-100 reactor. The flux profile was retrieved by measuring with a High-Purity Germanium (HPGe) semiconductor detector the gamma-radiation emitted by some manganese samples irradiated in the reactor central channel for about 45 minutes. A cylindrical holder with the same diameter as the experimental channel was used to position 16 samples of $^{55}$Mn inside the reactor core. The samples, consisting in tiny cylindrical rods of equal diameter with a length varying from 16.6 to 18.0 mm, were positioned in the 2 cm spaced housings of the holder. The stable $^{55}$Mn isotopes interact with thermal neutrons through the $^{55}$Mn($n,\gamma$) neutron capture reaction, leading to the measurable decay of $^{56}$Mn nuclei.

III. SERPENT 2 MODEL OF THE SUR-100 REACTOR

The Serpent2 model hereafter presented results from the conversion of an already existent MCNP input: all the geometrical and materials details of the reactor have been taken from this reference, thus the same assumptions are considered. The main simplifications of the computational model concern:

- the absence of all the drive mechanisms, as they are not impacting the neutron economy relevantly;
- the absence of the experimental channel 10/V, being it filled with graphite and therefore considered part of the reflector;
- the absence of the detector housings and the detectors themselves, since deemed non-impacting for the studies performed in this work because of their distance from the experimental channels;
- the absence of the aluminum coating of control plates, since they are assumed to not perturb the neutron flux in the thermal range of interest.

To improve its usability and its level of accuracy, the computational model has been adapted with minor modifications beyond its bare conversion, concerning shielding and control systems.

Despite its absence in the model provided by IKE, the concrete shielding has been modeled in Serpent2. Although the presence of the outermost layer of the shielding might not affect the neutronics in the center of the core, it is key for possible radiation protection studies e.g estimation of dose rate delivered to the operators. While the geometric dimensions of the concrete shielding have been taken from the official documentation from Siemens [7], its composition has been assumed “regular concrete” from the MCNP material compendium [8]. The concrete shielding has been shaped with a cylindrical shape, being this a simplification motivated by the absence of geometrical data on the real octagonal shape of the component at the time of the modeling procedure.

In addition, and to facilitate the modeling task of moving the control plates and the lower core section in different positions, the model is provided with a dedicated cell for each of them. This, together with the use of the translation command of Serpent2, enables to easily displace the elements without the need of a significant revision of the surfaces definition and opens to the use of apposite scripts to automatize the calculations. Thanks to these enhancements, the two control plates can be steered independently in the range [0, 250] mm and the lower core section (together with the lower section of the inner reflector) can be moved within the interval [0, 45] mm.

![Fig. 6 - Vertical cut view of the Serpent2 SUR-100 model.](https://doi.org/10.1051/epjconf/202125304029)
IV. RESULTS

A. Neutron thermal flux profile along central channel I

For this experiment, the miniature detectors 1 and 3 were moved along the length of channel I through the aluminum tube in the configuration (c) of Fig. 5, while the detector 2 was used as a monitor at a fixed position along the whole duration of the measurements in the tangential channel II. The results of the measurements recorded using detector 1 are depicted in Fig. 7. The count rates are normalized twice: first by detector 2, then by the maximum measured value. The profile is symmetric with respect to the core center, given the overall agreement of the data measured on each side of the core. A slight difference is found to exist between the points lying in the interval from 20 to 28 cm far from the core center, with a disagreement in the order of 10%.

![Fig. 7 - Comparison of normalized experimental count rates against 6Li reaction rates predicted by simulations along experimental channel I (top) and observed discrepancies (bottom).](image)

The measured data are then compared with computational results obtained through the Serpent2 model. The real configuration of the reactor (i.e. power level, control plates position and filling of experimental channels) of the day of the measurement is implemented in the computational model, in order to reproduce the experiments as faithfully as possible. Cylindrical virtual detectors with the same radius of the channel (26 mm) and a thickness of 1 cm are used to score the neutrons reaction rate with the Lithium-6 of the scintillator in every cm of the experimental channel in the range [-45,45] cm. The modeling of real-size detectors, given the miniature dimensions of the scintillators, was deemed to be unnecessary for the scope of the work at hand. Indeed, simulating real-size scintillator would cause a significant increase in the computational cost of the simulations, given the lower occurrence of neutrons interaction with a much smaller volume. Despite this, the smearing of the detectors is expected to introduce a discrepancy with the measured data, since the Monte Carlo results are in this way averaged on larger volumes. A depiction of the comparison of experimental and simulated data is also given in Fig. 7, as well as residuals.

![Fig. 8 - Direct comparison of the activation profile with measurements of miniature detector (top); Comparison of the activation profile with Serpent2 computed results (bottom).](image)

The experimental results are seen to be particularly in agreement with the simulated data in the spatial range [-30,18] cm, with a C/E-1 value lower than 10%. It is worth noting that this overall good agreement proves the negligible neutron flux perturbation induced by the miniature detectors, not modeled for the computational simulation.

An asymmetry in the radial profile is found in the zone of the graphite reflector between +20 and +30 cm away from the core, and it is not foreseen by the simulations. This discrepancy, which causes a disagreement of about 20%, could be caused by localized change in material composition or some geometric asymmetry not considered in the computational model. Further away from the core center, a higher discrepancy is found to exist symmetrically from 30 to 40 cm, with a C/E-1 value that reaches about 70%. Given the presence of the lead shielding in the zone of highest disagreement, such a discrepancy could be motivated with the uncertainties in material composition or in its cross section. Since the data series are normalized for their maximum values (which is located in the core center), the disagreement observed could not necessarily be attributed to the peripheral zones and therefore at the lead shielding region. Nevertheless, the main suspicions fall on the lead shielding area, as it is mechanically and chemically less known than the core center region.

The results are compared as well with the activation experiment in Fig. 8 (top), where a substantial disagreement is found between the fiber measurements and the count rates retrieved with the activation technique.
top), a meaningless comparison is obtained, with differences up to 50%. A fair comparison between the activation measurements and the Serpent2 results are performed by including in the computational model the activation holder. The comparison is shown in in Fig. 8 (bottom), where a good agreement is found between experimental and computational data, with C/E-1 values lower than 20%.

B. Neutron thermal flux profile along channel II

Similarly to the central channel I case above, the upper tangential channel was deployed to characterize the thermal neutron flux distribution along the length. No experimental data on the flux distribution was available beforehand, due to the difficulties to perform activation measurements in a region too far from the core center.

The detector 2 was used as a monitor as well, and it was positioned in the experimental channel I, approximately in correspondence of the core center. The remaining two detectors were configured as shown in Fig. 5(c). In addition, to fit the holder tube in a channel with larger diameter, apposite ring spacers made out of aluminum were used. The experimental results are shown in Fig. 9, together with a comparison against simulated data. For the Serpent2 simulation, virtual track-length detector of cylindrical dimension as big as the channel (54 mm diameter) are used to characterize the thermal flux profile.

The experimental results show excellent agreement with most of the simulated points, exception made for the data lying in the interval [20;35] cm, where the disagreement reaches values of about 50%. Again, the discrepancy is localized in the zone occupied by the lead shielding, which might have substantial differences in composition with respect to the modeled one.

Data from detector 2 are used for the central channel, with a power normalization using detector 1, since its position remains unchanged even after the 180° rotation. Data from detector 3 are used for the tangential channel, with a power normalization using detector 2 set in the core center.

For the central channel, both experimental and simulation results suggest the absence of a vertical gradient, being the reaction rate distribution almost flat in the core center. However, for the tangential channel II, the experiment shows the existence of a horizontal gradient of (9.09±0.20) % from the innermost to the outermost radial position measured with the miniature detectors.

V. CONCLUSIONS

High spatial resolution measurements of the thermal neutron flux have been performed with three 1-mm² miniature fiber-coupled scintillators within the experimental channels of the SUR-100 facility, a zero-power thermal reactor operated by the IKE of the University of Stuttgart. The miniature detection system was developed at EPFL in collaboration with PSI.

Relative flux distributions were measured along the experimental central (I) and tangential (II) channels of SUR-100 and compared against Monte Carlo simulations performed with Serpent2. The comparison of experimental and computed neutron distributions showed a good agreement within the core region, with discrepancies within 2σ. An unexpected discrepancy, probably caused by a geometric inconsistency in the computational model of the reactor, was observed in the reflector region of the experimental channel I, where a 20% difference (i.e. 8σ) was found between experimental and simulated results. Significant discrepancies, respectively worth 10σ and 15σ, were noticed at distance, in the lead shielding region, for both experimental channels I and II.

The results for the experimental central channel I are compared to neutron activation measurements, showing a strong perturbation of the neutron flux shape (35% increase of thermal neutron flux in the core region of experimental channel I) due to the plastic-graphite holder used for the samples irradiation. The negligible flux perturbations induced by the miniature fiber-coupled detectors has been found to be a great advantage compared to the previously used manganese activation technique. In addition, reaction rate gradients across the 2.6 cm and 5.4 cm diameters of the channels are successfully measured.

An horizontal reaction rate gradient of (9.09 ± 0.20)% was measured within 2.4 cm across the diameter of the experimental channel II, with a difference from computed results of 2%. The absence of a vertical reaction rate gradient inside the experimental channel I was confirmed by measurements.

In conclusion, the experimental campaign carried out in the SUR-100 zero-power reactor highlighted the suitability of the miniature fiber-coupled scintillators for high resolution thermal neutron flux distribution measurements and for the
characterization of highly localized gradients in the range of few cm.

REFERENCES

[1] F. Vitullo et al., “A mm3 Fiber-Coupled Scintillator for In-Core Thermal Neutron Detection in CROCUS,” IEEE Trans. Nucl. Sci., vol. 67, no. 4, pp. 625–635, Apr. 2020, doi: 10.1109/TNS.2020.2977530.

[2] C. J. Werner et al., “MCNP Version 6.2 Release Notes.”

[3] J. Leppänen, M. Pusa, T. Vaitanen, V. Valtavirta, and T. Kaltiaisenaho, “The Serpent Monte Carlo code: Status, development and applications in 2013,” Ann. Nucl. Energy, vol. 82, pp. 142–150, Aug. 2015, doi: 10.1016/J.ANUCENE.2014.08.024.

[4] F. Vitullo et al., “Developing and testing a miniature fiber-coupled scintillator for in-core neutron counting in CROCUS,” Adv. Nucl. Instrum. Meas. Methods Their Appl. (Animma 2019), vol. 225, p. 04018, Jan. 2020, doi: 10.1051/EPJCONF/202022504018.

[5] SCINTACOR, “SCINTACOR – Neutron Screens.” [Online]. Available: www.scintacor.com. [Accessed: 29-Jul-2021].

[6] ESKA, “High-Performance Plastic Optical Fiber Specification Sheet SH-8001.”

[7] H. Von Gunter and E. Schwartz, “Siemens-Uniterrichts-Reaktor SUR Part 2: Reactor description,” 1963.

[8] R. J. McConn, C. J. Gesh, R. T. Pagh, R. A. Rucker, and R. Williams III, “Compendium of Material Composition Data for Radiation Transport Modeling,” Mar. 2011, doi: 10.2172/1023125.