CHANGES IN WOOD PROPERTIES OF CHESTNUT WOOD STRUCTURAL ELEMENTS WITH NATURAL AGING

Elif Topaloglu

https://orcid.org/0000-0003-4736-8702

Derya Ustaomer

https://orcid.org/0000-0003-0102-818X

Murat Ozturk

https://orcid.org/0000-0003-1405-036X

Emrah Pesman

https://orcid.org/0000-0003-0189-4715

ABSTRACT

Knowing the effects of natural aging on wood properties is important both for the conservation of historical wooden material and for reuse of aged wood. The aim of this study was to investigate the wood properties of old wooden elements not impregnated with any protective chemicals and taken from different parts of Zeytinlik houses in Giresun, Turkey. Test samples were prepared from old wooden elements and freshly cut chestnut timber. The anatomical, chemical, physical and mechanical properties were determined according to standard procedure, and the results were compared with those of recent wood specimen. As a result of the anatomical identification, it was determined that the wooden elements used in traditional Zeytinlik houses belong to species of Anatolian chestnut (*Castanea sativa*), and after an average service life of 88, 113 and 120 years, there was no change in the anatomical structure of the old wooden elements. Fourier transform infrared band characterization of old wood specimens revealed that hemicelluloses degraded and lignin structure changed on the surface of almost all specimens. Especially, the wood density values of the facade elements were smaller than that of recent wood specimen. Except for the modulus of rupture of window sill and rafter, all mechanical properties were significantly greater compared with those of recent wood specimen. The results of this research showed that old wood not damaged by fungi and insects could be evaluated for reuse.

Keywords: Natural aging, service life, wood anatomy, wood properties, wooden structural elements.

INTRODUCTION

Technological development of humanity from the primitive age to the present has been closely related to human dependence on wood. Most of the properties of wood enabled it to be used both as an industrial raw material and as a construction material (Panshin and Zeeuw 1970). Wood can have a nearly unlimited service life under ideal conditions (Williams 2005). Service life is defined as “the period of time after installation
during which a facility or its component parts meet or exceed the performance requirements” (ISO 15686-1 2011). The service life of wood can exceed thousands of years under conditions where the weathering and biodegradation is prevented. The main source of degradation is aging (Matsuo et al. 2011). Aging of wood is a process that starts with the cutting of a tree and depends on environmental conditions. The aging process can take place on the historical wood, archaeological wood, and fossilized wood under different conditions such as aerobic and anaerobic conditions (Fengel 1991). When unprotected wood is exposed to atmospheric conditions, its surface becomes rough and darkened (Panshin and Zeeuw 1970). Ultraviolet (UV) light, moisture, temperature, abrasion or mechanical actions are the important factors in this process, which is defined as weathering (Feist 1983).

The effect of aging on the physical and mechanical properties is frequently uncertain and depends on wood species, aging time and storage conditions (Sonderegger et al. 2015). In addition, the aging conditions, different test methods or difficulties in sample matching may have affected wood aging process. Changes in the physical and mechanical properties of wood with aging result from changes in its microstructure and chemical changes in the components (Kránitz et al. 2016). Borgen et al. (1975) investigated the mechanism of fracture of wood samples between the ages of 900 and 4400, and determined that the weakest parts of the wood structure are the middle lamella/S1 region and interfibrillar matrix. Kačík et al. (2014) observed that the cellulose in old fir wood beams samples increased by 13 %, both the lignin and holocellulose dropped by 4 % compared to the recent fir wood. Machado et al. (2019) concluded that the density values of old wood belonging to *Pinus sylvestris* and *Pinus pinaster* with a service life of about 250 years are compatible with the value of the new wood. However, some authors reported that a decrease in the density values and various mechanical properties such as compressive strength and static bending strength for salvaged wood of *Juniperus excelsa* and *Pinus sylvestris* (Bektas et al. 2004, Bektas et al. 2005, Yorur et al. 2014).

During the service life of wood materials, which carry out functions such as beam, wall, floor, and roof element in buildings, degradation in wood properties may occur due to some factors. If the wood materials used are not impregnated with protective chemicals, the damage may be higher. It is important to determine the physical, chemical and mechanical properties of the wood materials used in order to have more information about the service life of the wood materials used in traditional wooden structures and to decide whether the wood materials can be reused. The aim of this study is to investigate the changes in wood properties of old wood materials used in traditional Giresun-Zeytinlik houses with natural aging. Moreover, it is aimed to find answers to the questions about the durability of old wood materials by comparing with the findings obtained from recent wood specimen.

**MATERIALS AND METHODS**

**Materials**

Traditional Zeytinlik houses are located in Zeytinlik District of Giresun (40°55’ north latitude - 38°23’ east longitude), Turkey. A total of six old wood materials were extracted from three randomly selected houses from traditional Zeytinlik houses. The approximate ages of the houses where the old wood materials were extracted can be stated as follows: 120 years for the front support, rafter and roof ridge, 113 years for the window sill and window blinds, and 88 years for the column pillar. The front support, window sill and window blinds are the structural elements that act as facade elements, the rafter and roof ridge are the roof elements, and column pillar is the carrier elements. In addition, the front support, rafter, roof ridge and column pillar are the elements that serve as load carriers in the structure. Figure 1 shows the macroscopic appearance of old wood materials used in this study. It was found macroscopically that all the old wood materials extracted from the houses were produced from the heartwood part of the tree and the sapwood part was not very common. In addition, as a result of visual inspection, there are nails on the front support, rafter and roof ridge elements; window sill and window blinds elements were exposed to UV degradation and color change was observed on their surfaces.
Preparation of wood specimens

Wood specimens consist of a total of seven different wood materials, six old wood materials that were extracted from different building parts of selected houses and one wood material was obtained by cutting from recent wood. About 10 cm long pieces were cut in the transverse direction from the ends of each of the old wood materials. These pieces were used to determine the anatomical features of wood, FTIR-ATR (Fourier transform infrared- Attenuated total reflection) measurements, and the remaining parts were used to determine the physical and mechanical properties of wood. In order to compare the results of old wood specimens and recent wood specimens, one healthy and smooth-stem chestnut tree, 60-years-old and with diameter of 30 cm at breast height (1,30 m), was cut. All wood samples were conditioned in the air-conditioning chamber at 20 °C and 65 % relative humidity until they reached 12 % humidity.

Wood identification and determination of anatomical features

To determine anatomical features of wood, 1 cm × 1 cm × 1 cm cubic pieces of wood were extracted from all wood materials. Three sections of transverse, radial and tangential thickness of 15 to 20 microns were taken by using Reichert slide microtome. These sections were exposed to sodium hypochlorite for 5 to 10 minutes and then washed with distilled water. Before staining of the sections, 1 to 2 drops of acetic acid were added to equilibrate the pH and allowed to stand for 1 to 2 minutes and washed again with distilled water. After this procedure, the sections were stained for 5 minutes in safranin 0 solution. After staining, sections were taken into 50 % alcohol-water mixture. Permanent preparations were prepared by performing standard preparation procedures on the sections (Ives 2001). The microphotographs of the wood samples were taken with Olympus BX 50 digital photomicroscope and transferred to computer with Image Monitoring and Analysis System. Wood materials were identified by using comparisons method with the reference collection of the KATO (Karadeniz Technical University, Herbarium) wood collection, InsideWood database (InsideWood 2018) and Merev (1998). All anatomical descriptions conform to the IAWA Committee for microscopic features of heartwood (Wheeler et al. 1989). Wood anatomical features measured include: tangential and radial vessel diameter in early wood and late wood, vessel frequency (per mm²), ray height, ray width and ray frequency (per mm). Thirty measurements or counts were performed for each anatomical parameter. All measurements were taken using Bs200ProP Image analyze software (BAB 2000).

Fourier transform infrared (FTIR) spectroscopy analysis

The Shimadzu IR Prestige-21 FTIR equipped with ATR (attenuated total reflection) was used to determine the characterization of the old wood materials. Fourier transform infrared spectra were recorded between 600 cm⁻¹ and 1800 cm⁻¹, with a resolution of 8 cm⁻¹ and 16 scans per experiment. Spectrum scans were performed on the specimens taken from the surface part which is exposed to outdoor conditions and light radiation.
from the inner part which is not affected by these effects.

**Determination of wood density**

Density test was determined according to ISO 13061-2 (2014) standard. In order to determine wood density, small wood specimens with dimensions of 20 mm × 20 mm × 30 mm (tangential × radial × longitudinal) were cut from all wood materials. As the wood density varies according to the moisture content (MC) of wood, the density values were calculated in two different forms as oven dry (0 % MC) density and air-dry (12 % MC) density. Moisture content of wood specimens was determined according to ISO 13061-1 (2014) standard. Density value (kg/m³) was calculated by ratio of mass (kg) to volume (m³) at 0 % and 12 % MC.

**Determination of wood mechanical properties**

Modulus of rupture (MOR in MPa) and modulus of elasticity (MOE in MPa) were determined in a three-point bending test according to ISO 13061-3 (2014) and ISO 13061-4 (2014), respectively. The measurements were performed using a Zwick universal testing machine with 20 mm × 20 mm × 300 mm (tangential × radial × longitudinal) wood specimens. The load was applied to the radial section and the middle part of wood specimens. The crosshead speed was 15 mm/min and span length was 240 mm. For compression strength parallel to grain test, small wood specimens with dimensions of 20 mm × 20 mm × 30 mm (tangential × radial × longitudinal) were used. Compression test was carried out according to ISO 13061-17 (2014) standard using a Zwick universal testing machine with a crosshead speed of 10 mm/min.

**Statistical analysis**

Moisture content, wood density and mechanical properties of old and recent wood specimens were tested by One Way Anova test the basis of the 95 % confidence interval. Significant differences between the groups were determined by Duncan homogeneity groups. Statistical analysis was performed using the SPSS 22.0 program (IBM 2020).

**RESULTS AND DISCUSSION**

**Wood identification**

The old wood materials from traditional Zeytinlik houses were identified microscopically to *Castanea sativa* Mill. (chestnut wood). Microscopic photographs of three sections of old and recent wood specimens were shown in Figure 2, Figure 3 and Figure 4.

![Microscopic photographs of the wood anatomy of *Castanea sativa* Mill. used as the roof ridge, window blinds and window sills in traditional Zeytinlik houses.](image)

(a-b, f-g, k-l: transverse section, c-d, h-i, m-n: radial section, e, j, o: tangential section. — Scale bar for a, f, k = 250 µm, for b, c, g, h, j, l, n, o = 100 µm, for d, i, n = 50 µm).
Figure 3: Microscopic photographs of the wood anatomy of *Castanea sativa* Mill. used as rafter, front support and column pillar in traditional Zeytinlik houses.

(a-b, f-g, k-l: transverse section, c-d, h-i, m-n: radial section, e, j, o: tangential section.,
— Scale bar for a, f, k = 250 µm, for b, c, e, g, h, j, l, m, o = 100 µm, for d, ı, n = 50 µm).

Figure 4: Microscopic photographs of the wood anatomy of *Castanea sativa* Mill. was obtained from recent wood specimen.

(a-b: transverse section, c-d: radial section, e: tangential section.,
— Scale bar for a = 250 µm, for b, c, e = 100 µm, for d = 50 µm).

Its wood is ring-porous and growth rings boundaries are distinct. Vessels are arranged in diagonal and/or radial pattern. The apotracheal axial parenchyma is diffuse and paratracheal axial parenchyma is occasionally scanty (Figure 2, Figure 3 a, b, f, g, k and Figure 4 a, b). Vessel elements have a simple perforation plate. Homocellular rays cells are exclusively procumbent (Figure 2, Figure 3 c, d, h, i, m, n and Figure 4 c, d). Rays are exclusively uniseriate (Figure 2, Figure 3 e, j, o and Figure 4 e). Average values of anatomical features of old and recent wood specimens are given in Table 1.

Table 1: Average values of anatomical features of old and recent wood specimens.

| Anatomical features* | Old wood specimens | Recent wood specimen |
|----------------------|--------------------|---------------------|
| Vessel               | 199.32 (48.50)     | 219.52 (33.44)      |
| VRD (µm)             | 41.32 (38.60)      | 37.57 (32.46)       |
| VTD (µm)             | 57.91 (54.41)      | 59.99 (58.32)       |
| Frequency (per mm)   | 25 (7)             | 24 (7)              |
| Height (µm)          | 191.83 (51.72)     | 185.72 (39.37)      |
| Width (µm)           | 11.82 (0.83)       | 14.79 (1.69)        |
| Frequency (per mm)   | 10 (1)             | 10 (1)              |

*VTD: vessel tangential diameter, VRD: vessel radial diameter.
** Standard deviation is indicated in parentheses.
As shown in Table 1, VTD of old wood specimens was found to be 136.21 µm - 247.95 µm and 30.74 µm - 41.44 µm for early wood and late wood, and VRD of old wood specimens was found to be 161.83 µm - 322.58 µm and 32.58 µm - 53.74 µm for early wood and late wood, respectively. VRD of both early wood and late wood were wider than VTD. Vessel diameters of early wood and late wood of recent wood specimen were found to be close to vessel diameters of the window blinds element. It was determined that vessel frequency in 1 mm² of old wood specimens varied between 24 to 36 and this value of recent wood specimen was 28. The ray height and width of old wood specimens ranged between 185.72 µm - 281.83 µm and 11.82 µm - 19.12 µm, respectively. The number of ray per millimeter of old wood specimens was found to range between 8 to 10, and number of ray per millimeter of recent wood specimen was found to be the same as those window blinds and front support. In this study, the results of the anatomical features of both old and recent chestnut wood were found to be consistent with the results reported by Merev (2003). As a result of natural aging and after a service life of 88, 113 and 120 years, microphotographs also support that there is no change in the wood anatomy features of old wooden elements. Madhoushi (2016) reported that the wood species of structural elements removed from a historical building in Gorgan, Iran were identified as elm, lime tree, oak, sugar maple and scots pine. Dogu et al. (2017) determined that the wood of a very old timber building element that was used on the inside of a balcony and exposed to outdoor conditions for more than 400 years belongs to oak wood. They also stated that oak wood species is characterized by high durable heartwood since it contains high amount of tannins. Han et al. (2019) determined that the wood blocks taken from the beam of a historical building, which was first built in 1370 A.C., belong to the elm wood (Ulmus sp.) and they observed significant structural differences between sound aged wood.

FTIR-ATR spectra analysis

The FTIR spectra measured from the inner and surface parts of old wood specimens are given in Figure 5. The spectrum represented by blue is measured from the inner part of old wood specimens, and the spectrum represented by red is measured from the surface part of old wood specimens. It is seen in Figure 5 that there are differences between the peaks obtained from the surface parts of old wood specimens and those obtained from the inner parts. When we examined all the spectra in detail, it was observed that the peak in the 1732 cm⁻¹ band in the specimens taken from the inner part of the wood material was lost for almost all structural elements in the spectra measured from the surface part of the specimens. The peak in this wave number is associated with carbohydrates (Marchessault and Liang 1962). The reason for the reduction of this peak in specimens exposed to light and outdoor weather conditions can be explained by the breakdown of acetyl groups in the xylan and degradation of hemicelluloses (Esteves et al. 2013). It was determined that the intensity of aforementioned peaks either decreased or disappeared completely in the spectra measured from the surface part of most structural elements. The decrease in these bands can be explained by aging and deacetilization on the surface of the wood material (Mohebby 2008, Stefke et al. 2008). Similar results were determined by Tintner et al. (2016), and also observed in a study on fossil Sequoiadendron giganteum wood performed by Uçar et al. (2005). In the measurements made from inner parts, the peak of 1596 cm⁻¹ for roof ridge, front support, rafter, column pillar and window blinds disappeared with aging in the measurements made from surface parts, and a rather distinct new peak formed in 1643 cm⁻¹.
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According to these findings, it can be said that the structure of lignin and phenolic structures changed completely with light radiation and oxidation. The conjugation degree of lignin and multiple conjugated systems increased in aged wood samples due to oxidation and decreased acid soluble lignin (Borgin et al. 1975). It is possible to conclude that the disappearance of the peak in the 1505 cm$^{-1}$ band with aging supports these results. It was determined that the peak at 1318 cm$^{-1}$ band became evident in the spectra of the rafter and window blinds specimens. This peak indicates the C-H vibration in cellulose (Müller et al. 2009, Guo et al. 2018). However, the peak at 1367 cm$^{-1}$ had become more pronounced with the aging effect in some structural elements. The prominence in this peak was attributed to CH deformation in cellulose and hemicelluloses after aging (Liu et al. 2017, Tarmian and Mastouri 2019). However, during outdoor weathering, water mechanically corrodes the surface of wood material and hydrolyzes hemicelluloses on the surface, and the hemicelluloses become more vulnerable when lignin breaks down (Williams 2005).

Density values

Average values of moisture content and density of old and recent wood specimens are shown in Table 2. Fluctuations in the amount of water present in the wood considerably affect all the physical properties of wood, mechanical as well as nonmechanical (Panshin and Zeeuw 1970). As shown in Table 2, moisture content was found to be 11.69 % to 13.58 % and 14.54 % for old wood specimens and recent wood specimen, respectively. According to One Way Anova test results; there were statistically significant differences (P = significance level = 0.000), which are indicated in Table 2 by letters from a to e, between moisture content values of all wood specimens. The lowest moisture content was obtained in the wood specimens of roof ridge. Recent wood specimen had higher moisture content than old ones. Yokoyama et al. (2009) determined that equilibrium moisture content tends to decrease with age. Sonderegger et al. (2015) reported that the moisture content of aged oak wood at different relative humidity was lower than that of the recent wood. The decrease in amorphous cellulose or adsorption sites in hemicelluloses resulting in lower equilibrium moisture content values (Inagaki et al. 2008, Kránitz et al. 2016) may be the reason for this change in humidity of old wood specimens.

**Figure 5:** ATR-FTIR spectra for inner surface (blue line) and outer surface (red line) of old wood specimens ((a) front support, (b) rafter, (c) roof ridge, (d) column pillar, (e) window sill, (f) window blinds).
Table 2: Average values of moisture content and density of old and recent wood specimens.

| Wood specimens         | Moisture content (%) | Air-dry density (kg/m³) | Oven dry density (kg/m³) |
|------------------------|----------------------|-------------------------|--------------------------|
| Roof ridge             | 11.69 (0.99)**       | 570 (20)                | 540 (20)                 |
| Window blinds          | 13.09 (0.83)         | 540 (20)                | 510 (10)                 |
| Window sill            | 13.40 (0.70)         | 500 (20)                | 470 (20)                 |
| Rafter                 | 13.58 (0.76)         | 580 (20)                | 540 (20)                 |
| Front support          | 13.49 (0.64)         | 530 (10)                | 500 (10)                 |
| Column pillar          | 12.54 (0.37)         | 570 (30)                | 530 (30)                 |
| Recent wood specimen   | 14.54 (0.96)         | 570 (10)                | 530 (10)                 |

*The superscript letters in each column indicate a significant difference between the groups (p = 0.000).
** Standard deviation is indicated in parentheses.

Our range of air-dry density was 500 kg/m³ - 580 kg/m³ and of oven dry density was 470 kg/m³ - 540 kg/m³ for old wood specimens. As seen in Table 2, the density values were found for the recent wood are among these values. According to One Way Anova test results; there were statistically significant differences (p = 0.000), which are indicated in Table 2 by letters from a to e for air-dry density and from a to d for oven dry density, between density values of all wood specimens. The smallest density values were found in the wood specimens of window sill, while the greatest density values were determined in the wood specimens of rafter. In a study prepared by Ay and Şahin (2002a) air-dry and oven dry density values of chestnut wood (Castanea sativa) were reported to be as 540 kg/m³ and 510 kg/m³, respectively. Compared with the density values of old wood specimens, the air-dry and oven dry density values of recent wood specimens were greater than the values of the front support, window sill and window blinds wood specimens, on the other hand; density values of rafter, roof ridge and column pillar wood specimens gave the same and/or close results with the values of the recent wood. According to these results, it is possible to say that there is no decrease in density values of the rafter, roof ridge and column pillar structure elements until the present day during the natural aging. Contrary to this result, window sill, window blinds and front support elements may be smaller in density values because they are the facade elements of the building and exposed to outdoor weathering effects. However, some researchers are reported that the good correlation between wood density and the erosion rate occurring on the wood surface during weathering (Feist and Mraz 1978, Williams 2005). Han et al. (2019) reported that the decrease of carbohydrates and concentration of lignin in the fiber wall after aging may lead to lower rigidity, and a decrease of density and elastic modulus of the cell wall. Furthermore, Thaler et al. (2014) found that density value of old chestnut pole with a service life of approximately 35 years and density value of recent chestnut wood as 571 kg/m³ and 607 kg/m³, respectively.

**Mechanical properties**

In the literature, there are many studies on mechanical properties of aged wood, especially compression strength, bending strength and Young’s modulus. Table 3 shows the results of mechanical tests of old and recent wood specimens. Compression strength, MOR and MOE values were found to be between 51.41 MPa - 87.35 MPa, 56.09 MPa - 95.49 MPa and 7812.37 MPa - 10762.67 MPa for aged wood specimens, and 51.02 MPa, 66.11 MPa, 7235.33 MPa for recent wood specimen, respectively. The average of compression strength and MOR values of chestnut (Castanea sativa) wood are reported as 58.19 N/mm² and 79 N/mm², respectively (Ay and Şahin 2002b). One Way Anova test results showed that there were statistically significant differences (p = 0.000), which are shown in Table 3 by letters from a to e, between compression strength values of all wood specimens. It was determined that the wood specimens of column pillar and rafter were in the same homogeneity group with recent wood specimen, and compression strength values of the other old wood specimens were greater than that of recent wood specimen. This result may be due to the fact that column pillar in structures and rafter in roofs are used as a conventional bearing elements and these elements are faced with compression and bending load, respectively. Decreases in compression strength compared with control wood were reported for salvaged juniper wood by Bektas et al. (2004), for salvaged scots pine wood by Bektas et al. (2005) and for salvaged scotch pine wood by Yorur et al. (2014). In addition, Sousa et al. (2014) found that the compression strength parallel to grain of decayed sweet chestnut beam decreased by 33.1 %. Furthermore, Thaler and Humar (2013) found that the compressive strength of oak and beech wooden beams used more than 100 years no changed compared to control oak wood, but it decreased for old beech wood.
### Table 3: Average values of mechanical properties of old and recent wood specimens.

| Wood specimens         | Compression strength (MPa) | MOR (MPa) | MOE (MPa) |
|------------------------|-----------------------------|-----------|-----------|
| Roof ridge             | 87.35\(^*\) (3.08)         | 95.49\(^*\) (4.20) | 10762.67\(^*\) (608,79) |
| Window blinds          | 70.48\(^*\) (4.52)         | 85.60\(^*\) (4.80) | 9026.78\(^*\) (397,93) |
| Window sill            | 61.19\(^*\) (1.43)         | 56.09\(^*\) (2.70) | 7833.33\(^*\) (547,05) |
| Rafter                 | 53.08\(^*\) (3.11)         | 59.12\(^*\) (3.48) | 7812.37\(^*\) (406,41) |
| Front support          | 58.17\(^*\) (3.12)         | 71.50\(^*\) (3.65) | 8781.33\(^*\) (423,47) |
| Column pillar          | 51.41\(^*\) (3.05)         | 86.94\(^*\) (3.14) | 9365.33\(^*\) (411,60) |
| Recent wood specimen   | 51.02\(^*\) (1.57)         | 66.11\(^*\) (3.77) | 7235.33\(^*\) (347,17) |

*The superscript letters in each column indicate a significant difference between the groups (p = 0.000) ** Standard deviation is indicated in parentheses.

The effect of natural aging on MOR and MOE is summarized in Table 3. One Way Anova test results indicated that there were statistically significant differences (p = 0.000) between MOR and MOE values of wood specimens. It was determined that MOR values of rafter and window sill are smaller than that of recent wood specimen. When evaluated in terms of its use in the building among the old wooden elements in this study, the wooden element most exposed to bending is the rafter. For this reason, it is thought that the resistance of the rafter element to withstand an average bending load of 120 years gradually decreased over time. However, it was reported by Panshin and Zeeuw (1970) that the high flexural rigidity of wood is most effective in building elements such as beams. Window sill, which is among the facade elements in wooden structures, is one of the most exposed elements to outside weather conditions such as rain, snow, wind, and sun rays. Changes/decreases in chemical components of wood as a result of both outdoor weathering and natural aging may cause weakening of mechanical resistance of wood samples. However, as the hemicellulose is deteriorated, the woody cell wall begins to collapse and loss of strength occurs (Nilsson and Rowell 2012). MOR values of the front support, column pillar, roof ridge and window blinds were quite great compared to recent wood specimen, and also MOE values all old wood specimens were greater than that of recent wood specimen. According to these results, it is possible to say that the mechanical strength performance of these wooden elements during the natural aging period is very good. This result is attributed to the natural durability and sufficient strength of chestnut wood, which is an important source of tannin. However, Emmerich et al. (2019) stated that anatomical properties of wood had an important effect on the structural integrity of hardwoods. Vurdu et al. (2013) reported no significant difference in bending strength of antique pine and antique fir woods which are approximately 100 years old, compared to control samples, and modulus of elasticity of antique pine wood was higher than control pine sample, while an inverse result was obtained for antique fir wood. Sonderegger et al. (2015) found that the bending MOR and MOE values of aged spruce wood from historical buildings were higher than that of recent wood, and they also found a contradictory result for aged fir wood. Madhoushi (2016) determined that the mechanical properties of old structural members, and concluded that these old members were structurally good despite their appearance and may be kept for reuse. Furthermore, Thaler and Humar (2013) determined that the MOR and MOE of oak and beech wooden beams, which were used more than 100 years, with very minor differences compared to control oak wood, but both values decreased significantly for old beech wood. In another study, Thaler et al. (2014) determined MOR and MOE values as 113.5 MPa and 9379 MPa, and 94.5 MPa and 6708.6 MPa for old chestnut wood and recent chestnut wood, respectively. Yokoyama et al. (2009) investigated the change in mechanical properties of Hinoki (Chamaecyparis obtusa) wood taken from historical Japanese houses over time. They observed that no significant change in longitudinal and radial rigidity and longitudinal strength.

### CONCLUSIONS

The old wood specimens from the Zeytinlik houses were identified as *Castanea sativa* (chestnut wood), one of the native tree species grown in the Black Sea region of Turkey. As a result of the anatomical identification, it was determined that there was no change in the anatomical structure of old wooden elements after average service life of 88, 113 and 120 years. However, according to results of the FTIR-ATR spectra of old wooden elements, it was determined that hemicelluloses deteriorated and the structure of lignin changed on the surface part of almost all old wood specimens. There was a decrease especially in wood density values of the facade elements depending on the time. However, the mechanical strength performance of the chestnut wooden elements used in Zeytinlik houses are generally in good condition compared to recent chestnut wood specimen. Based on these results, it was concluded that these wooden elements, which are thought to be old in appearance, are structurally in good condition and can be evaluated for reuse. It is recommended to encourage the reuse of old wooden elements, which is thought to be unusable and disposed only by looking at its external appearance.
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