Grain Boundary Pop-in, Yield Point Phenomenon and Carbon Segregation in Aged Low Carbon Steel

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Nanoindentation measurements, tensile tests, and carbon concentration analyses were conducted to study yield behaviors in as-received, aged, and prestrained low carbon steel. In aged sample, steel showed both yield point phenomenon (YPP) and grain boundary (GB) pop-ins besides initial pop-in, while steels in other two states showed no YPP and only the initial pop-in. 3-dimensional atom probe (3DAP) analysis in both as-received and aged samples showed that carbon content in the matrix decreased significantly after aging treatment, which is believed to contribute to the occurrence of both YPP and GB pop-in.

KEY WORDS: yield point phenomenon; nanoindentation; grain boundary pop-in; low carbon steel.

1. Introduction

Low carbon steels are popular panel materials for both vehicles and appliances. These steels frequently suffer stress–strain defects caused by yield point phenomenon (YPP). YPP, a yielding feature showed in stress-strain curves, is visible as Lüders bands in annealed low carbon steels. This phenomenon has been a concern for a long time. Hence, understanding the mechanism of YPP is of high academic and commercial importance.

Most researchers relate YPP in steels to interstitial atoms such as C or N. Low et al.11) reported that removal of both C and N in mild steels by wet hydrogen treatment can make the yield point disappear. It is well accepted that the interaction between interstitial atoms and dislocations form “Cottrell atmosphere”,2) and the unpinning of dislocations from atmospheres causes the yield point. Hahn3) pointed out that YPP is a consequence of rapid dislocation multiplication after initial yield. Other researchers suggested that YPP is due to the fastening of dislocations by interstitial atoms at grain boundaries.4,5) This inconsistence in explanations of YPP calls for further studies by new technology that characterizes materials in small regions with high spatial resolution.

Recently, nanoindentation has been used to investigate the mechanical properties of materials at micro-scales. In load-displacement curves of nanoindentation, both “initial pop-in”,6,7) and “grain boundary (GB) pop-in”8–11) phenomena have been observed. In initial pop-in, a sudden increase in the displacement occurs during the early stage of mechanical contact, which is attributable to the nucleation or multiplication of dislocations.12,13) Ahn et al.14) related the initial pop-in to YPP. But, this connection was ruled out because in steel without YPP initial pop-in was also observed.7) GB pop-in occurs at higher load than initial pop-in. The GB pop-in was related to interfacial yielding near the grain boundary.15) The phenomenon was considered to be caused by the unpinning of dislocations from grain boundary.10) GB pop-in was observed in body-centered cubic metals (e.g. Iron and Niobium) which usually show YPP.8–11) Thus, it is of interest to study YPP and GB pop-in together using the same samples. This paper reports our measurements of YPP by tensile tests, and both initial pop-in and GB pop-in by nanoindentation in a commercial low carbon steel and our understanding of YPP mechanisms.

2. Experimental Methods

As-received samples are commercial low carbon steel sheets without YPP, and the average grain size is about 8 μm. The chemical composition of the steel is Fe-0.025C-0.0018N-0.047Al-0.18Mn-0.015Cr (wt%). An as-received sample was aged at 220°C for 6 h to create YPP. The aged sample was then deformed under a tensile strain of 5% to remove YPP. Tensile tests were performed on as-received, aged and deformed samples at a strain rate of 1×10−3/s at room temperature. The interstitial content of aged and as-received samples was measured in a 3-dimensional atom probe (3DAP; LEAP 4000x HR).

The specimens prepared for nanoindentation tests were mechanically polished using 2 500-grit SiC paper and then electropolished for about 1 min in a solution composed of 6% perchloric acid, 14% water, and 80% ethanol at 278 K under a potential of 40 V. Nanoindentation tests were performed using a Hysitron Triboindenter with a Berkovich diamond tip. The angle between Berkovich indenter and rolling direction of samples remained the same for all the tests. The maximum force was 10 mN and loading rate was 2 mN/s. Indentations in each sample were made in a 4×10 array with 20 μm intervals between indents. A Scanning Electron Microscopy (SEM) was used to examine the indentations.

3. Results and Discussions

The stress-strain curves of samples in as-received, aged, and 5% strained after aging are shown in Fig. 1. YPP occurs with upper and lower yield points in aged samples, but not in samples of as-received or 5% prestrained steels.

Figure 2 shows the representative load-depth curves of indentations in low carbon steels. Initial pop-in phenomena occur under loads less than 1.1 mN in most tests in as-
received (Fig. 2(a)), aged (Fig. 2(b)) and 5%-strained (Fig. 2(c)) samples. 14 of our 40 tests of aged samples exhibited GB pop-in that was triggered at higher load than that for initial pop-in plateau. Moreover, GB pop-in in aged sample was found when indentation was made in the proximity of a boundary (Fig. 3(a)). Indents in the grain interior showed no GB pop-in (Fig. 3(b)).

In our experiments, not all the indentations close to the boundaries showed GB pop-in in a given aged sample. This is not unusual because, according to previous researchers, several factors affect the occurrence of GB pop-in: distance between the indentation and nearest GB,8) dislocation density,10) orientation between two adjacent grains,11) and presence of impurities within grain boundaries.9,10) No test (out of 40 measurements), however, showed GB pop-in in as-received and prestrained samples. Since GB pop-in appeared only in sample with YPP, GB pop-in and YPP may be related to similar microstructure changes resulted from aging.

The load-depth curve can be converted into (P/h) vs. h curve, which was used to analyze the plastic deformation mechanisms for nanoindentation.16) The slope of (P/h) vs. h curve, d(P/h)/dh, can be used to describe work-hardening rate.11) In our aged sample, GB pop-in caused a discontinuity in slope at high load region in (P/h) vs. h curve (Fig. 4(a)). The slope of (P/h) vs. h plot decreases after GB pop-in, which suggests that the stress required to activate dislocation source at or near the boundary was reduced after initial yield of the GB.11) In addition, the slopes in as-received sample are hardly changed after the initial pop-in, whose values are lower than those before GB pop-in in aged
attributed to pinning of dislocations by interstitial atoms. Britton et al., on the other hand, pointed out that GB pop-in is due to interstitials pinning dislocations on or near the boundary.\textsuperscript{10} So the contributions of carbon segregation to YPP and GB pop-in need to be investigated further.

4. Conclusions

In low carbon steel samples, both GB pop-ins and YPP were observed only in aged sample, not in as-received and 5% prestrained samples. 3-dimensional atom probe (3DAP) analysis showed that carbon content in the matrix of the aged sample decreased significantly after aging treatment of the as-received sample, indicating carbon segregation to defects. Such segregation creates a strengthened barrier for slip transfer from the grain subject to indentation to the adjacent one so that GB pop-in occurs and for dislocation motion in the materials so that YPP happens.

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Table 1. Chemical compositions of the low carbon steel from 3DAP (atomic fraction in ppm).

| C   | S   | Al  | Mn  | P   | Cr  | Cu  |
|-----|-----|-----|-----|-----|-----|-----|
| As-received | 178±3  | 18±1 | 779±7 | 1734±11 | 238±4 | 268±4 |
| Aged  | 77±1 | 19±1 | 801±4 | 1650±6 | 216±2 | 247±2 | 243±2 |

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