Laser Processing of Tungsten Powder with Femtosecond Laser Radiation

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Laser irradiation of dispensed tungsten powder layers with grain sizes smaller than 1 µm was investigated using high-repetition femtosecond laser systems. Laser processing was performed line by line with repetition rates of 1 MHz and varying parameters such as laser power, processing speed, number of scans and pressure. In addition to the expected material ablation and melting, novel phenomena such as crystallisation, emergence of ripple structures, extensive agglomeration and the formation of nano-wires will be discussed qualitatively with the help of SEM photographs. Dependence on light pressure, pulse overlap and irradiated energy per unit section will be demonstrated. High-resolution microstructures will be discussed as a first application of innovative laser microsintering technology using high-repetition femtosecond laser pulses.

Keywords: femtosecond laser, high-repetition rate laser, laser microsintering, nano-ripple, tungsten

1. Introduction

Ultrashort pulses are commonly used for precise ablation of layers or for 3D microstructuring [1-3]. Glass welding is known also [4]. Further investigations demonstrate the possibility of targeted fabrication of nano- and microstructures on various material surfaces [5, 6]. However, fs laser irradiation of dispensed loose powder layers with the objective of producing sintered structures has not been investigated thus far. By varying the pulse energy and the scan velocity, it should be possible to find parameters under which radiation pressure and plasma effects bring about compaction of the powder layers, and the applied energy per unit section heats up the powder layer to just below the melting point. Other than the short exposure time, this would largely correspond to the classic sintering process.

2. Experimental principles

An existing laser microsintering facility was used for the investigations. It consists of a fs laser (Table 1), an adjustable attenuator for selecting the pulse energy, a pulse divider, a scanner for beam deflection and focussing, and a vacuum sintering chamber.

| Table 1 | General laser parameters |
|---------|--------------------------|
| Wavelength | Pulse duration | Pulse repetition rate | Focus spot radius |
| λ [nm] | t [fs] | f [MHz] | \( w_{36} [\mu m] \) |
| 1030 | 180 | 1; 0,125 | 18 |

The experiments used tungsten powder supplied by Goodfellow. It is specified by the manufacturer at a grain size < 1 µm. The measured bulk density \( \rho_p \) was 2.8 g/cm³, which corresponds to a relative powder density of ca. 15%. The powder’s surface was normally produced by means of a dispensing process. The thickness of the powder layer was ca. 1000 µm.

In order to prepare a defined powder surface, it was cleaned before every experiment through laser irradiation. To this end, the powder surface was irradiated line by line with a pulse energy of 0.7 µJ and a velocity of 4.5 m/s. With these parameters, a plasma was observed during the first scan but not during subsequent scans. No visual effect was observed on the powder’s surface. Based on scanning electron microscope (SEM) imaging, however, it became clear that the powder’s surface had already been slightly affected by the irradiation. The irradiated regions appeared lighter in the SEM images.

Scan velocity \( v \) and pulse repetition rate \( f \) were varied in order to investigate the effect of lateral pulse distance \( a \), and of energy per unit section \( Q_0 \), on the sintering process (Table 3). The applied energy per unit section is the ratio of mean laser power and scan velocity. The hatch distance \( l \) was 50 µm in all basic experiments.

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\begin{array}{cccc}
\text{Table 2} & \text{Laser pulse parameters} \\
\text{Pulse energy} & \text{Fluence} & \text{Pulse peak power} & \text{Max. intensity} & \text{Radiation pressure (R=1)} \\
Q_0 [\mu J] & H_0 [J/cm^2] & P_0 [MW] & I_{max} [W/cm^2] & p [Pa] \\
0.4 & 0.07 & 1.96 & 0.39 \times 10^{12} & 257 \times 10^5 \\
7.5 & 1.30 & 36.67 & 7.21 \times 10^{12} & 4787 \times 10^5 \\
\end{array}
\]

50 Pa. Helium was used as residual gas in selected experiments.
Table 3  Process parameters

| Laser power $P_a$ [W] | Pulse repetition rate $f$ [MHz] | Scan velocity $v$ [m/s] | Pulse distance $a$ [µm] | Energy per unit section $Q_S$ [J/m] |
|------------------------|-------------------------------|------------------------|--------------------------|-----------------------------------|
| 0.4                    | 1                             | 0.1                    | 0.1                      | 4                                 |
| 0.4                    | 1                             | 5                      | 5                        | 0.08                              |
| 7.5                    | 1                             | 0.1                    | 0.1                      | 75                                |
| 7.5                    | 1                             | 5                      | 5                        | 1.5                               |
| 0.875                  | 0.125                         | 0.3125                 | 2.5                      | 2.8                               |
| 0.875                  | 0.125                         | 5                      | 40                       | 0.175                             |

The formation of plasmons from the free electron gas is significant especially when irradiating solid body surfaces with fs lasers. The plasmons are resonant oscillation modes of the electron gas. One distinguishes between volume and surface plasmons. In the case of metallic nanoparticles whose dimensions are much smaller than the wavelength of light, the plasmons lead to unusual optical properties. Depending on the resonant frequencies, there occurs narrowband absorption of light and light scattering into the far field. In addition, there is an amplified near field (factor $10^6$) around the particle, with the typical spatial extent being several 10 nm [7].

Due to the short pulse duration, coupling of the laser beam energy occurs first in the free electron gas, and after an interval of a few ps the energy is transferred to the solid lattice (two-temperature model). The excitation of the plasmons and the coupling factor to the phonons are responsible for the qualitative formation of nanoripples [9].

When using the classical heat conduction equation, the irradiated powder grains would take on different temperatures depending on their size [11]. The temperature equalisation in the powder bed is likely to take place largely by through radiation processes, i.e. considerably faster than through heat conductance.

3. Results and discussion

3.1 Low intensity < $1.6 \times 10^{12}$ W/cm$^2$, low energy per unit section < 0.7 J/m, $f = 1$ MHz

When using low intensity and energy per unit section under multiple irradiation, the powder grains exhibited nanoripple formation (Fig.1). Due to the low applied energy per unit section and since the powder grains have largely retained their crystal structure, it can be assumed that direct nanostructuring of the tungsten particles without separate melt formation has taken place.

3.2 Low intensity < $1.6 \times 10^{12}$ W/cm$^2$, moderate energy per unit section 0.7...20 J/m, $f = 1$ MHz

Under multiple irradiation, and starting from 5 scans at the lowest intensity $I_{max} = 0.39 \times 10^{12}$ W/cm$^2$ with a low pulse distance $a = 0.1$–0.3 µm, the irradiated region exhibited the formation of large-area slabs. The thickness of the slabs was ca. 10 µm. They exhibited a curvature which increased with the number of irradiations. It appeared as though the powder layer had underwent large-area sintering and was under strong internal mechanical stress (Fig. 3). Thus far there is no clue as yet for an explanation of this effect. It is noteworthy that at a line spacing of 50 µm there was no overlapping of the focus spot diameter. At higher intensities, $I_{max} = 3.52 \times 10^{12}$ W/cm$^2$, the effect was also observed with greater pulse distances, $a > 1$ µm.

The formation of fibrous nanoparticle aggregates [12] was observed when conducting the experiments under a helium pressure $p = 0.5 \times 10^5$ Pa (Fig. 2).
3.3 Moderate intensity $1.6 \ldots 5 \times 10^{12} \text{W/cm}^2$, moderate energy per unit section $0.7 \ldots 20 \text{J/m}$, $f = 1 \text{MHz}$

When increasing the intensity and the energy per unit section, the tracks exhibited an increased formation of melts (Fig. 4). Due to the surface tension, the predominant effect was of spherical melt formations. Depending on the applied intensity and scan velocity, there was either formation of crystals (Fig. 5) or melt pearls with nanoripple structures (Fig. 6). The crystals formed preferentially at a pulse distance of 0.3 to 0.8 µm, and an increased intensity of $I_{\text{max}} = 4.05 \times 10^{12} \text{W/cm}^2$.

Evidently, with these parameters there is sufficient time for the formation of crystalline structures. The crystalline structure was absent when the scan velocity was decreased to 0.1 m/s and the intensity to $I_{\text{max}} = 1.76 \times 10^{12} \text{W/cm}^2$. Instead, nanoripples occurred on the amorphous melt pearls. The generally observed conditions for the formation were a relatively high pulse overlap or a multiple scan. It is noteworthy that ripple formation occurred in two different directions. Firstly, the deep laser-induced ripples are present. In addition, superficial ripples transverse to those can be seen (Fig. 6).

Significant reduction of energy per unit section by increasing the scan velocity led to a delicate melt track with a width of ca. 15 µm (Fig. 7). Under multiple scans, however, the melt strands were transected and the formation of individual melt pearls took place.

Increasing the intensity whilst simultaneously reducing the energy per unit section even further, led to a decrease in melt volume (Fig. 8). Only individual molten micro-regions were now present, with maximum dimensions of $5 \times 10 \mu\text{m}^2$. Cohesion was no longer exhibited.
3.4 High intensity > 5 \times 10^{12} \text{W/cm}^2, \text{moderate energy per unit section} 0.7...20 \text{J/m}, f = 125 \text{kHz}

Since the scan velocity was limited to \( v = 5 \text{ m/s} \), the effect of an increased pulse distance could only be investigated by reducing the laser’s pulse repetition rate to 125 kHz. This made possible the application of high intensity together with moderate to low energy per unit section. At a pulse distance of \( a = 2.5 \mu \text{m} \), the formation of highly fissured structures at the centre of the track was observed, and also melt and ripple formation at the edge (Fig. 10). This showed that on the one hand, the intensity was sufficiently high to cause compaction of the powder, but on the other, the applied energy – especially in the region of lower intensity at the edge – was still so high that disruptive secondary effects took place.

Increasing the pulse distance to 5-20 \( \mu \text{m} \) led to the disappearance of the melts (Fig. 11). The powder grains were firmly joined to each other. The structure is limited to a width of ca. 15 \( \mu \text{m} \). When the mean energy per unit section is reduced by increasing the pulse distance, this decreases the “superfluous” melt formation to such an extent that the resulting structures are similar to classic sintered formations. From a pulse distance of \( a > 20 \mu \text{m} \) onward, the compactness of the structures was markedly reduced. Decreasing the intensity to \( 5.81 \times 10^{12} \text{W/cm}^2 \) led, starting at a pulse distance of \( a > 10 \mu \text{m} \), to a decline in the sintered structures.

The high radiation pressure, \( p = 4787 \times 10^5 \text{ Pa} \), led to high forces acting on the particles, either 177 \( \mu \text{N} \) (diameter = 1 \( \mu \text{m} \)) or 17 \( \mu \text{N} \) (diameter = 0.3 \( \mu \text{m} \)). These forces were 9 orders of magnitude higher than the acting gravitational forces! Due to the ultrashort exposure time, however, these high forces did not lead to significant displacement of the particles (only ca. \( 10^{-16} \text{m} \)) or to significant kinetic energies (only ca. \( 10^{-14} \mu \text{J} \)). The radiation pressure, therefore, has no detectable effect on the sintering process.

The formation of the sintered structures at high intensities should, rather, be attributed to the same mechanisms as in laser microsintering with ns pulses. The vaporisation of material at the powder’s surface leads to a recoil, which accelerates the particles towards the powder bed. The expansion of the material vapour plasma also exerts a pressure on the forming surface of the sintered structure. When using ns pulses, this structure is characterised by melts. When sintering with fs laser pulses, it seems initially as though no melt is present. Future investigations will explore this effect in more detail, and a model for the formation of the sintered structures will be constructed.

Nanospikes appear to have formed at the surface of the sintered structure (Fig. 12), however not in association with
nanoripples as reported by other research groups [13]. The nanospikes will be investigated in greater detail by means of high-resolution SEM imaging.

![SEM Image 1](image1)

**Fig. 12** SEM image, $I_{\text{max}} = 6.74 \times 10^{12} \, \text{W/cm}^2$, $Q_s = 0.7 \, \text{J/m}$, $v = 1.25 \, \text{m/s}$, $a = 10 \, \mu\text{m}$, 10 scans.

### 3.5 High intensity > $5 \times 10^{12} \, \text{W/cm}^2$, high energy per unit section > $20 \, \text{J/m}$, $f = 1 \, \text{MHz}$

When maintaining the high intensity and increasing energy per unit section considerably by reducing scan velocity, significant melt formation could be observed. However, since at the same time the high intensity led to greater plasma formation, the melt was pushed into deeper regions of the powder. There was formation of relatively well-bounded molten trench structures, ca. $30 \, \mu\text{m}$ wide, with vertical walls (Fig. 13). The depth was up to $138 \, \mu\text{m}$.

![Optical Image 1](image2)

**Fig. 13** Optical image, $I_{\text{max}} = 6.97 \times 10^{12} \, \text{W/cm}^2$, $Q_s = 72 \, \text{J/m}$, $v = 0.1 \, \text{m/s}$, $a = 0.1 \, \mu\text{m}$, 1 scan.

### 3.6 Effects of pressure / gas

The structures of the experimental series created under a helium pressure of $p = 0.5 \times 10^5 \, \text{Pa}$, possessed lower resolution than those created in vacuum. In addition, higher laser power was needed in order to achieve structure sizes similar to those achieved in vacuum. The likely reason is the generated residual gas plasma, which is additional to the always present material vapour plasma. Under these conditions, it reduces process efficiency and the attainable resolution.

![SEM Image 2](image3)

**Fig. 14** SEM image, $I_{\text{max}} = 6.74 \times 10^{12} \, \text{W/cm}^2$, $Q_s = 0.7 \, \text{J/m}$, $v = 1.25 \, \text{m/s}$, $a = 10 \, \mu\text{m}$, $l = 10 \, \mu\text{m}$, $f = 125 \, \text{kHz}$, 10 scans.

![SEM Image 3](image4)

**Fig. 15** SEM image, $I_{\text{max}} = 6.74 \times 10^{12} \, \text{W/cm}^2$, $Q_s = 0.23 \, \text{J/m}$, $v = 3.75 \, \text{m/s}$, $a = 30 \, \mu\text{m}$, $l = 10 \, \mu\text{m}$, $f = 125 \, \text{kHz}$, 10 scans.

### 3.7 Sintering areas

By decreasing the line spacing to $l = 10 \, \mu\text{m}$, it proved possible to sinter continuous surfaces (Fig. 14 and 15). Sintered structures of varying sizes in the range 1-10 $\mu\text{m}$ were formed, depending on the scan velocity used.

![SEM Image 4](image5)

**Fig. 16** SEM image, $I_{\text{max}} = 6.74 \times 10^{12} \, \text{W/cm}^2$, $Q_s = 0.7 \, \text{J/m}$, $v = 1.25 \, \text{m/s}$, $a = 10 \, \mu\text{m}$, $l = 10 \, \mu\text{m}$, $f = 125 \, \text{kHz}$, 10 scans.

![SEM Image 5](image6)

**Fig. 17** SEM image, $I_{\text{max}} = 6.74 \times 10^{12} \, \text{W/cm}^2$, $Q_s = 0.23 \, \text{J/m}$, $v = 3.75 \, \text{m/s}$, $a = 30 \, \mu\text{m}$, $l = 10 \, \mu\text{m}$, $f = 125 \, \text{kHz}$, 10 scans.

### 3.8 Highly resolved structures

The first experiments designed to create defined grid-like structures demonstrate the fundamental suitability of the method and its ability to achieve high resolution (Fig. 16 & 17). The height of the applied structure was ca. $1 \, \mu\text{m}$. The carrier platform was not lowered during the 6 dispensing procedures. The grid spacing used was $50 \, \mu\text{m}$, the produced optical line width (Fig. 16) is ca. $17 \, \mu\text{m}$. However, the structures identified in the SEM image seem considerably wider (Fig. 17).
4. Summary and outlook

The fundamental feasibility of laser microsintering with a high-repetition fs laser was demonstrated. Lateral pulse distances of \( a = 5 \ldots 20 \, \mu m \) have proved to be advantageous at an applied intensity of \( I_{\text{max}} = 6.74 \times 10^{12} \, W/cm^2 \) and a pulse repetition rate of \( f = 125 \, kHz \). Sintered structures were created for the first time that resemble the classic sintered formations. The effect of the temporal pulse distance on the sintering outcome will be investigated in greater detail in the future by varying the pulse repetition rate.

The sintering of highly resolved structures is just as possible as that of thin layers. The fabrication of micro/nano-sieves using this method will be investigated in the future. Investigating the applicability of the method to other materials will also be focused upon.

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