Optimal baseplate position in reverse shoulder arthroplasty in small-stature Japanese women: a cadaveric study

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Abstract: The purpose of this study was to determine the optimal position of the baseplate on the small glenoid of female Japanese. Two sets of 3D scapular models were made according to the CT data of 7 female cadavers. We set two scenarios of the baseplate placement: A and B. In scenario A, the baseplate was placed on the glenoid face centrally in the anteroposterior direction. In scenario B, the baseplate was implanted at the point where the baseplate post was contained within the glenoid vault. Whether or not the baseplate post perforated the scapular neck was recorded. In scenario A, the central post penetrated the scapular neck posteriorly in 5 scapulae. In scenario B, the average distances from the guide pin position to the anterior glenoid rim was 9.7 ± 1.7 mm and the optimal position of the guide pin was 1.9 ± 1.7 mm anterior from the glenoid center. The central post was contained within the scapula without breakage of the cortex. This study demonstrated that shifting the center of the baseplate slightly anterior to the anatomic center is necessary to avoid perforation of the scapular neck in small female Japanese. J. Med. Invest. 68: 175-180, February, 2021

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Reverse shoulder arthroplasty (RSA) was developed by Paul Grammont in 1985 to restore shoulder function in patients with cuff tear arthropathy (CTA) (1). The basic concept of RSA is reversal of glenohumeral joint anatomy by replacing the glenoid cavity with large-diameter convex metallic glenosphere and humeral head with concave polyethylene socket to cause distalization and medialization of the center of rotation of the shoulder. This prosthetic design increases the lever arm and force of the deltoid muscle, which acts as a stabilizer and main muscle of the shoulder.

RSA has been proven to provide satisfactory pain relief and functional improvement for patients with rotator cuff deficiency (2, 3). Recently, first-line surgical treatment for cuff tear arthropathy and its indications have been expanded to include fracture of the proximal humerus (4), rheumatoid arthritis (5), primary osteoarthritis, tumors of the proximal humerus (6) and revision surgeries for failed anatomical shoulder arthroplasty (7).

Optimal positioning and secure initial fixation of the glenoid baseplate are critical for long-term and excellent clinical outcomes of RSA. Lower positioning of the glenoid baseplate on the glenoid surface is recommended to avoid scapular notching, which is the most common radiographic complication after RSA (8). In the anteroposterior plane, the pilot hole should also be positioned optimally to eliminate penetration of the central post outside the glenoid vault (9). Kelly et al. (9) developed a computed tomography (CT)-template protocol to determine the position of the pilot hole by superimposing a virtual baseplate on the axial image 12 mm above the inferior glenoid rim. They reported that the optimal position determined by their protocol was slightly posterior in anteroposterior dimensions. Their study did not state the sex and race of the specimens; however, the size of the scapulae in their study was similar to those of other published anatomical studies. Conversely, in our current clinical practice, we have found it necessary to shift the center of the baseplate slightly anterior to the anatomic center of the glenoid to avoid the posterior cortex of the scapular neck from breaking in small-stature Japanese women (10).

The purpose of this study was to determine if the preoperative planning protocol proposed by Kelly et al. (9) could be applied to Japanese shoulders, which are considerably smaller than those of Caucasians. We hypothesized that the optimal position of the baseplate would differ in women with a glenoid fossa that is smaller than the baseplate. We sought to demonstrate the optimal baseplate position to avoid the central peg from perforating the glenoid fossa bone of small-stature women.

METHODS

Seven fresh frozen cadavers were used in this study. All specimens were Japanese women, (mean age, 82.4 years; range, 48 to 100) years. All the cadavers were donated to Tokushima University for research purposes. The study was approved by the Institutional Review Board of Tokushima University.

For all cadaveric specimens, CT scans were obtained with a 16-slice scanner (Somaton Emotion-16; Siemens Japan, Tokyo, Japan). The scanning parameters were as follows: 130 kV; 134 mAs; slice thickness, 0.75 mm; screw pitch, 0.5 mm; and matrix, 512 × 512. None of the specimens showed signs of previous surgery, trauma, abnormal osseous anatomy, or severe osteoarthritis. Multiplanar reconstructions were made using the OsiriX DICOM shareware viewer (www.osirix-viewer.com). The optimal positioning of the baseplate was determined to be 12 mm above the inferior glenoid rim, as described by Kelly et al. (9) The optimal baseplate position in the anteroposterior plane was then de-
determined according to the template protocol. The baseplate was positioned either anteriorly or posteriorly from the central position, where the central post was contained within the scapular neck (Fig. 1). The distance from the center post to the anterior glenoid rim were measured and identified as an entry point for the baseplate guide pin in the anteroposterior plane.

CT data were exported in Digital Imaging and Communication in Medicine (DICOM) file format and imported into the medical imaging software Mechanical Finder (Research Center of Computational Mechanics, Inc., Tokyo, Japan). A three-dimensional (3D) model of the scapula was constructed by extracting the regions of interest from the imported DICOM data and then saving these in stereolithography (STL) file format. The STL file of the scapula data was processed with the free software Meshmixer (Autodesk, San Rafael, CA), which allows for virtual sectioning of the rendered model intended for 3D printing. Each 3D scapular model was evaluated for file quality, detection performance of bad edges, flipped triangles, and multiple shells and then repaired to transform the complex geometry of the cancellous bone into a compatible model for printing. The 3D scapular model was then loaded to a 3D printer (Lepton2 ; GENKEI LLC, Tokyo, Japan). Print parameters were set to a layer thickness of 0.2 mm, filling rate of 15.0%, and filling speed of 58 mm/s. The scale was set at 1 : 1, and polylactic acid was used as the 3D printing material (Fig. 2).

Two sets of 3D scapular models were printed for each specimen. Glenoid height, glenoid width, scapular height, and scapular width measurements were obtained on 3D models and compared with measurements on 3D-CT (Fig. 3).

The glenoid component of a Trabecular Metal Reverse Shoulder System™ (Zimmer Biomet, Warsaw, IN) was implanted in

Figure 1. Preoperative planning of the baseplate placement. (A) Baseplate positioning at the anatomic center of a small glenoid introduces risk for posterior cortex breakage (white arrow). (B) Slight anterior placement can avoid this risk, but results in extra overhang of the baseplate anteriorly from the glenoid rim (black arrow).

Figure 2. Three-dimensional model of the scapula. (A) Anterior view. (B) Lateral view.
all specimens. This glenoid component comprises a 28-mm flatback baseplate that is affixed to the glenoid with a central post 15 mm in length and 8 mm in diameter, and two locking screws in the superior and inferior positions.

We set up two scenarios of baseplate placement, A and B. In scenario A, the central post of the baseplate was placed on the glenoid surface centrally in the anteroposterior direction, as described in the surgical technique guide provided by the manufacturer. In scenario B, the central post was placed at the point determined by the preoperative template protocol. The entry point of the guide pin was marked with a marker pen and a 2.5-mm guide pin was inserted without any tilt relative to the native glenoid using a unidirectional drill guide. The version of the baseplate was set to match that of the native glenoid. The glenoid surface was reamed using a 28-mm cannulated reamer placed over the guide pin until it flattened. Peripheral reaming was also performed if necessary. The central hole was enlarged using a 7.5-mm drill and the baseplate was inserted until the baseplate was flush with the reamed surface of the glenoid. Then, whether the baseplate post was contained within the glenoid vault was recorded. The overhang of the baseplate from the glenoid rim was measured using calipers.

RESULTS

Glenoid height, width, scapular height, and width were measured on 3D printed models and compared with scapular measurements on CT scans (Table 1). Each measurement on both 3D printed models and CT scans was similar.

In scenario A, the target position of the guide pin was centered in the anteroposterior dimension. The average overhang of the glenoid baseplate was 2.5 ± 1.3 (range, 1.0-4.4) mm from the anterior glenoid edge. The central post was contained within the scapula without cortex breakage in all scapulae (Fig. 4).

In scenario B, the target position of the guide pin was determined by the CT-templating protocol. The average distances from the guide pin position to the anterior glenoid rim was 9.7 ± 1.7 (range, 7.6-11.8) mm (Table 2). Thus, the optimal position of the guide pin was 1.9 ± 1.7 (range, 0.6-3.2) mm anterior in the anteroposterior dimension. The average overhang of the glenoid baseplate was 4.3 ± 1.7 (range, 2.2-6.4) mm from the anterior glenoid edge. The central post drill penetrated the scapular neck posteriorly in 5 scapulae (Fig. 5).

Figure 3. Measurements of glenoid and scapular sizes. A: glenoid height B: glenoid width C: scapular height D: scapular width

Table 1. Glenoid and scapular size measured on 3D printed models and CT scans

| Specimen no. | CT measurements | 3D models |
|--------------|-----------------|-----------|
|              | Glenoid length  | Glenoid width | Scapular length | Scapular width | Glenoid length | Glenoid width | Scapular length | Scapular width |
| 1            | 35.6 mm         | 25.2 mm      | 133.3 mm       | 94.1 mm        | 34.5 mm        | 26.9 mm      | 127.0 mm       | 93.5 mm        |
| 2            | 25.5 mm         | 19.3 mm      | 111.7 mm       | 84.1 mm        | 29.7 mm        | 18.8 mm      | 114.5 mm       | 93.5 mm        |
| 3            | 30.7 mm         | 20.1 mm      | 111.6 mm       | 88.9 mm        | 31.5 mm        | 21.0 mm      | 115.0 mm       | 89.0 mm        |
| 4            | 33.8 mm         | 24.7 mm      | 96.0 mm        | 91.3 mm        | 34.0 mm        | 24.5 mm      | 93.5 mm        | 89.5 mm        |
| 5            | 29.0 mm         | 22.8 mm      | 97.6 mm        | 92.9 mm        | 30.0 mm        | 23.0 mm      | 98.0 mm        | 91.0 mm        |
| 6            | 32.3 mm         | 23.5 mm      | 113.4 mm       | 89.2 mm        | 32.0 mm        | 23.0 mm      | 115.5 mm       | 90.5 mm        |
| 7            | 33.9 mm         | 26.0 mm      | 121.4 mm       | 90.9 mm        | 32.0 mm        | 26.0 mm      | 118.5 mm       | 91.5 mm        |
| Average      | 31.5 mm         | 23.1 mm      | 112.1 mm       | 90.2 mm        | 32.0 mm        | 23.3 mm      | 111.7 mm       | 91.2 mm        |
Table 2. Preoperative planning of the baseplate position

| Specimen no. | Scenario A        | Scenario B        |                  |                  |                  |
|--------------|-------------------|-------------------|------------------|------------------|------------------|
|              | Position of the   | Anterior overhang | Position of the  | Anterior overhang | Position of the  |
|              | guide pin         | of the base plate | guide pin        | of the base plate | guide pin from   |
|              |                   |                   |                  |                  | the center of the |
| 1            | 12.6 mm           | 1.4 mm            | 9.4 mm           | 4.8 mm           | 3.2 mm           |
| 2            | 9.7 mm            | 4.4 mm            | 7.6 mm           | 6.4 mm           | 2.1 mm           |
| 3            | 10.0 mm           | 4.0 mm            | 9.5 mm           | 4.5 mm           | 0.6 mm           |
| 4            | 12.4 mm           | 1.6 mm            | 11.8 mm          | 2.2 mm           | 0.6 mm           |
| 5            | 11.4 mm           | 2.6 mm            | 7.8 mm           | 6.2 mm           | 3.6 mm           |
| 6            | 11.7 mm           | 2.3 mm            | 9.7 mm           | 4.3 mm           | 2.1 mm           |
| 7            | 13 mm             | 1.0 mm            | 11.8 mm          | 2.2 mm           | 1.2 mm           |
| Average      | 11.5 mm           | 2.4 mm            | 9.7 mm           | 4.3 mm           | 1.9 mm           |

Position of the guide pin was expressed as the distance from the anterior glenoid rim.
Anterior overhang of the base plate expressed as the distance from the anterior glenoid rim to the anterior edge of the base plate.
DISCUSSION

When inserting RSA implants, the baseplate should be positioned inferiorly and be aligned to the inferior edge of the glenoid to avoid scapular notching. The 12-mm rule proposed by Kelly et al. (9) has been widely accepted as a practical recommendation for the ideal location of the pilot hole. Their theory proposes that the baseplate pilot hole be placed 12 mm above the inferior glenoid rim, and slightly posterior from the anatomic center of the glenoid surface.

Although age, sex, and ethnicity of specimens in the study by Kelly et al. (9) were unknown, their specimens were similar in size to other published scapular measurements of Caucasians (11, 12, 13). Previous studies analyzing normal scapular geometry and morphology have demonstrated racial differences in glenoid size. Iannotti et al. (11) measured the dimensions of the glenoid surface and found an average glenoid height of 39 ± 3.5 mm and a width of 29 ± 3.2 mm. Von Schroeder et al. (12) reported that glenoid height and width were 36 ± 4 mm and 29 ± 3 mm, respectively. However, compared with these measurements, Asian shoulders are smaller. Matsumura et al. (14) analyzed 160 healthy Japanese shoulders and reported an average glenoid height of 31.5 ± 2.8 mm and glenoid width of 23.1 ± 2.4 mm.

Another study in a Japanese population demonstrated that the average glenoid height and width were 33.3 ± 5.3 mm and 25.9 ± 4.3 mm, respectively (15). The glenoid size in the women of our study was close to that reported in these Japanese studies.

In addition to ethnic variations, the glenoid is known to be larger in men than in women. Sex differences in glenoid morphology were not considered when inserting baseplate guide pin at the glenoid surface. In a Korean population, Ji et al. (16) noted that insertion of a standard 29-mm baseplate was technically challenging in small-stature patients, especially in small-stature women. For a small glenoid, the standard-sized 29-mm baseplate is larger than glenoid bone stock, which results in insufficient bone-implant contact and anterior and posterior screw fixation. The authors suggested that smaller implants may be required for proportionally small-stature patients.

With increased use of RSA in several countries worldwide including in Asia, some manufacturers have made available baseplates with a diameter < 29 mm. RSA use has thus been increasing, especially in small-stature Asian women. Athwal et al. (17) reported favorable short-term outcomes with the Mini 25-mm baseplate in small-stature patients with demonstrable implant safety and effectiveness. Chase et al. (18) demonstrated that smaller baseplates improve primary stability and greater impingement-free range of motion in a relatively small glenoid fossa, compared with the regular 29-mm baseplate. Previous studies have focused on proper placement of the standard 29-mm baseplate. It is still unclear whether these guidelines for the 29-mm baseplate can be applied to the Mini 25-mm baseplate.

In this study, we determined the ideal position of the guide pin in a small glenoid fossa using the same CT-templating protocol described by Kelly et al. (9). We found that the target position of the guide pin was located slightly anterior from the center of the glenoid, which was contrary to their theory. This discrepancy may be related to the relative height of the CT image used for templating. If the glenoid size is similar to the baseplate size, the shape of the glenoid vault is an isosceles triangle. Conversely, a baseplate positioned 12 mm above the inferior glenoid rim is higher than the center of the glenoid fossa, and the CT slice passes near the spinoglenoid notch. At this level, the glenoid vault is narrow posteriorly. Therefore, shifting the position of the guide pin slightly anteriorly may prevent breakage of the posterior wall of the scapular neck. Anterior shifting of the baseplate leads the anterior overhang from the anterior glenoid edge, which may cause insufficient fixation of the anterior screw. A biomechanical comparative study demonstrated that the most important screws for glenoid-baseplate fixation were the superior and inferior screws. Anterior overhang of the baseplate exerts less influence on the initial stability of the baseplate. It is unclear how central post perforating the scapular neck affects the initial press-fit fixation of the baseplate. Further biomechanical testing is required to clarify this. There are certain limitations of this study. First, the sample size was small. Second, biomechanical testing was not performed to compare the initial fixation strength of these two scenarios. Third, our specimens had no severe deformity or bony erosions. Kelly et al. (9) reported that the 12-mm rule would not apply to scapulae with severe bone defects. On an abnormal glenoid version, the target point may differ from that of this study. Fourthly, shifting of the guide pin position could be applied to only a flat-back baseplate. A round-back baseplate is not suitable for a small glenoid fossa because the baseplate should be placed in the centrally on the glenoid surface.

CONCLUSION

This study demonstrated that shifting the center of the baseplate slightly anterior to the anatomic center is necessary to avoid the posterior cortex of the scapular neck from breaking in small-stature Japanese women. Our results in this Japanese women cohort were contrary to those of Western cadavers described by Kelly et al. (9); however, their CT-template protocol is still useful for obtaining better stability of the glenoid component, even in a small glenoid fossa.

COI DISCLOSURE

Shoji Fukuta: The author, their immediate family, and any research foundation with which they are affiliated have not receive any financial payments or other benefits from any commercial entity related to the subject of this article.

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