Non-synchronization of lattice and carrier temperatures in light-emitting diodes

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Pulse implementation or switching-off (PISO) of electrical currents has become a common operation in junction-temperature \(T\) measurements for semiconductor devices since 2004. Here we have experimentally discovered a substantial discrepancy between \(T\) values with, and without, PISO (e.g., 36.8 °C versus 76.5 °C above the ambient temperature at 25.0 °C). Our research indicates that methods associated with PISO are flawed due to non-synchronization of lattice temperatures and carrier temperatures in transient states. To scrutinize this discrepancy, we propose a lattice-inertia thermal anchoring mechanism that (1) explains the cause of this discrepancy, (2) helps to develop a remedy to eliminate this discrepancy by identifying three transient phases, (3) has been applied to establishing an original, accurate, and noninvasive technique for light-emitting diodes to measure \(T\) in the absence of PISO. Our finding may pave the foundation for LED communities to further establish reliable junction-temperature measurements based on the identified mechanism.

In designing light-emitting diodes (LEDs)\(^1\)\(^-\)\(^3\) that emit the light via recombination of holes and electrons and waste thermal energy through lattice vibration, we desire to extract photons \(P_{\text{opt}}\), must supply electrons \(P_{\text{elec}}\), and dislike phonons \(P_{\text{cond}}\) (Fig. 1a). In turn, characteristics of photons, electrons, and phonons are strongly associated with the temperature at the junction interface \(T_j\) between n-type and p-type semiconductors\(^4\)\(^-\)\(^7\). It is currently a challenge to accurately measure LED junction temperatures \(T_j\) under conditions of large currents\(^8\)\(^-\)\(^11\). The primary reason arises because LED chips are usually sealed, thus prohibiting direct contacts. Presently, the work related to pulse implementation or switching-off (PISO, Fig. 1b) has populated the literature in semiconductor areas, including forward voltages\(^16\)\(^,\)\(^17\), peak energy\(^18\)\(^,\)\(^19\), reverse currents\(^20\) and low forward currents\(^21\). Although these methods are capable of facing the challenge mentioned above, the discrepancy between results obtained with, and without, PISO has been found to be substantial.

In our laboratory, we have adopted both the forward voltage method (FVM, Fig. 1b) and confocal Raman spectroscopy (CRS, Fig. 1c). Using the former, we first obtain the steady-state linear relationship between \(T_j\) and \(I_α\) (inset of Fig. 2a), controlled by the heat sink at \(I_α\) \(=\) \(25\, \text{mA}\), and the forward voltage \(V\) at \(5\, \text{mA}\) with negligible thermal power input. Then we light the LED sample (e.g. blue InGaN/GaN) under a large steady-state current (e.g. \(I_β\) \(=\) \(350\, \text{mA}\)). Instantaneously, this current is switched down to \(I_β\) \(=\) \(5\, \text{mA}\) by the FVM instrument named T3ster (MicRed. Inc., Hungary), and the forward voltage is recorded. Utilizing the linear relationship at \(5\, \text{mA}\), we deduce the desired \(T_j\) to be 36.8 °C under 350 mA (Fig. 2a, time in logarithmic scale). Alternatively, when using CRS\(^22\)\(^-\)\(^24\), which excludes PISO, we obtain \(T_j\) to be 76.5 °C based on the peak location of Raman shift (Fig. 2b,c). Peaks of Raman-light-beam intensity shift to the left as \(T_j\) increases by an increment of 10.0 °C, whereas the peak at \(I\) \(=\) \(350\, \text{mA}\) and \(T_{\text{sink}}\) \(=\) \(25.0\, \text{°C}\) (the ▲ curve) is located at \(568.4\, \text{cm}^{-1}\) (Fig. 2d). This trend clearly suggests that \(T_j\) must be at least higher than approximately \(55.0\, \text{°C} + 10.0\, \text{°C}\). Had \(T_j\) been lower than \(55.0\, \text{°C}\), as measured by CRS, the peak should have been located between \(569.0\, \text{cm}^{-1}\) and \(569.4\, \text{cm}^{-1}\). Relative to the ambient temperature at 25.0 °C, the discrepancy amounts to \((51.5\, \text{°C} – 11.8\, \text{°C})/11.8\, \text{°C} = 336.4\%.

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To scrutinize this puzzling difference, we have additionally used thermocouples (TC)\(^{25}\) and a thermal imager (TI)\(^{26}\), which receive direct thermal signals from samples, and have obtained 73.5°C and 73.8°C (Fig. 2e–g), respectively (Supplementary S1). Nine exposed LEDs (1-W each) were further selected for conformations, including three blue InGaN/GaN (B1#, B2#, B3#), three green InGaN/GaN (G1#, G2#, G3#) and three red AlGaNp (R1#, R2#, R3#), also leading to substantial discrepancies (Supplementary S2). Finally, we propose the following mechanism to explain this discrepancy, and further develop an independent method that requires neither PISO nor intrusive contacts, and utilizes Shockley equation for diodes as well as the principle of thermal anchoring (to be described below).

**Lattice-inertia thermal anchoring (LITA)**

Consider the electron transport inside a doped semiconductor undergoing three transient phases: (1) PISO phase from state \(\alpha\) to state \(\beta\), (2) non-synchronization phase from state \(\beta\) to state \(\gamma\) (a delayed state replacing state \(\beta\)), (3) relaxation phase from state \(\gamma\) to \(\gamma\) (steady state). The electron velocity at steady state \(\alpha\) should equal the vector sum of the thermally-diffusive velocity and the drift velocity. After algebra, we can prove that the kinetic energy of electrons at state \(\alpha\) is greater than the counterpart at state \(\beta\) (\(v_\alpha^2 > v_\beta^2\)) (Supplementary S3), partly because the drift component diminishes upon PISO. Electrons with small drift velocities descend to combine with holes in the valence band, reducing potential energies relative to their nucleuses. Consequently, the carrier temperature \(T_c\)\(^{27–31}\) decreases from state \(\alpha\) to state \(\beta\). Next, there exist two types of external inputs, electrical power and thermal power that influence both \(T_\alpha\) and \(T_\beta\) (Fig. 3a). For the former which drives the electron transport, \(I\) and \(V\) change instantaneously after PISO, exerting impacts on the electrical field, which subsequently causes reductions of \(T_c\), or carrier potential energy. Because of lattice inertia \(\gg\) carrier inertia and the occurrence of PISO, we can conclude that \(T_\alpha - T_\beta \approx T_\alpha - T_\gamma \approx 0\). Consider a practical example, in which the electrical current of 350 mA (\(I_\alpha\)) is instantaneously switched down to 5 mA (\(I_\beta\)) within approximately 1 ms, along with a voltage reduction from \(V_\alpha = 3.1\ \text{V}\) to \(V_\beta = 2.6\ \text{V}\) (Fig. 3b). Complicated phenomena, including re-thermalization, radiative recombination, non-radiative Auger, and non-radiative Shockley-Reed-Hall deep-level recombinations, diminish as time elapses within the sample. Let us calculate dimensionless percentage changes of \(V\), \(I\), and \(T\) as \(\Delta V_\alpha / V_\alpha = 0.2\), \(\Delta I_\alpha / I_\alpha = 69.0\), \(\Delta T_\gamma / T_\gamma \approx 0\), and \(\Delta T_\beta / T_\beta \approx \Delta V_\beta / V_\beta\), \(\Delta I_\beta / I_\beta = 84.6\). These changes imply that \(\Delta V_\gamma\) and \(\Delta T_\gamma\) differ substantially, leading to the chaotic nature of state \(\beta\) and the difficulty of determining \(T_\gamma\) and \(V_\beta\) accurately. Hence, if possible, we should avoid utilizing data that belong to the uncertain \(\beta\) state, completely dismiss \(V_\beta\) that plays the primary role of the discrepancy-inducing

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**Figure 1. Experimental set-ups for forward voltage method (FVM).** (a) The LED sample consists of layers including LED chip, die attach, and copper slug. In steady state, the influx \(IV\) should equal out fluxes including \(P_{\text{conv}}, P_{\text{opt}}, P_{\text{rad}}\) (cond = conduction; opt = optical; conv = convection; rad = radiation). (b) Pulse-implementation or switching-off (PISO) of currents for FVM. \(I_\alpha\) = current at the steady state, e.g., 350 mA; \(I_\beta\) = a small fraction of \(I_\alpha\) to stay on, e.g., 5 mA; \(I_\gamma\) = the major portion of \(I_\alpha\) to be switched off. The subscript ‘\(r\)’ denotes ‘thermal’, suggesting that the current generates the thermal power. (c) Confocal Raman spectroscopy (CRS). The LED sample is mounted on a heat sink, and is lit by a current source. The peak of Raman shift has moved leftward minutely when temperatures of samples increase.

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Figure 2. Junction-temperature measurements of FVM, CRS, TC and TI. (a) Take blue InGaN/GaN LED (B1#) as the example. In reference to the linear relationship between $V$ and $T_j$, we deduce the value of $T_j$ to be 36.8°C. (b) Relationship between $T_j$ and Raman redshift for the B1# sample when the LED chip is lit at small currents (5 mA). The peak at $T_j = 55.0°C$ has shifted to the left slightly. (c) Relationship between $T_j$ and Raman redshift for B1# sample when the LED chip is lit at large currents. At steady state and $I = 350$ mA, for example, we measure Raman shift to obtain the peak location. Next, utilizing the $T_j$ and Raman shift relationship in (b), we obtain $T_j = 76.5°C$. (d) Correlation between peak location and $T_j$. (e) Junction temperature versus the current for B1# sample. In the absence of PISO, results obtained by CRS, TC and TI agree closely with one another, but differ appreciably from those obtained by FVM. Due to the disturbance of large noises, $T_j$ cannot be reliably measured in CRS for B1# sample at 450 mA. (f) Junction temperature versus the current for G1# sample. (g) Junction temperature versus the current for R1# sample.
culprit, and proceed to cool down the sample further till state $\beta'$. From state $\beta$ to state $\beta'$, $T_c$ is primarily influenced by the external cooling macroscopically or phonon propagation and lattice vibrations microscopically (Fig. 3a). By contrast, electrons continue to descend from higher to lower energy levels, but the descending distribution is additionally affected by the external cooling macroscopically or phonon propagation and lattice vibrations microscopically. Therefore, it is nonrigorous for FVM to apply this inter-relationship to situations when $\epsilon_\alpha > \epsilon_\beta$. In other words, in the remedial approach ($\alpha \rightarrow \beta'$), data between two end states are intentionally ignored. Because of dismissing $V_{\beta'}$ value, we need to produce another equation in substitution. Consequently, the next task is to obtain a relationship between $T_{j,\beta}$ and $T_{j,\beta'}$ based on the principle of thermal anchoring. Following the first law of thermodynamics, we identify all energy components crossing the boundary of the sample’s control volume (Fig. 1a), and write $P_{elec} = P_{opt} + P_{conv} + P_{rad} + P_{cond}$ (Supplementary S4). Finally, from state $\beta'$ to state $\gamma$, we are allowed to utilize the steady-state $V \& T_j$ relationship, which is approximately linear with a negative slope. If time between $\beta$ and $\beta'$ is taken to be 100 ms, we obtain $T_{j,\beta} = 75.0^\circ C$ for B1# sample (Supplementary S5). Since it remains uncertain to precisely locate the state $\beta'$, next we propose a previously-unreported method that adopts the principle of thermal anchoring and avoids PISO. In the steady-state Shockley equation for diodes, namely,
\[ I = I_s \left[ \exp \left( \frac{qV}{nkT} \right) - 1 \right] \]

Since \( I, I_s \) and \( V \) can be readily measured via experiments, we have only the ideality factor \( n \) and \( T_j \) left as unknowns, and need one more equation.

In analogy to casting the anchor when docking a ship in the harbor so that the anchor location reveals ships’ whereabouts, we maintain \( T_{\text{sink}} \) constant and attempt to determine \( T_j \). The overall thermal resistance of two layers, namely the die attach, and Cu slug, between the LED chip and the sink resembles the length of the anchoring steel wire.

In reference to the physical configuration of the sample (Fig. 1a), it is reasonable to idealize these layers as one-dimensional slabs. Consider a multi-layer system whose top and bottom are either heat sinks or sources. We further recognize the phenomenon that, when phonon waves propagate from the source to the sink, they excite oscillations of lattice inertia along the path, but do not alter basic lattice structures after they pass. When they reach the sink, \( T_{\text{sink}} \) remains constant, but vibration energy escapes to outside the sink, and thermal conductivities of intermediate layers remain unchanged. If the electrical input \( P_{\text{elec}} \) also remains unchanged (implying \( P_{\text{cond}} \) remains the same), so does \( T_j - T_{\text{sink}} \). Then, we select two states, 1 and 2, where 1 represents \( T_{\text{sink}} = 25.0^\circ\text{C} \); 2 represents \( T_{\text{sink}} = 35.0^\circ\text{C} \) (10.0 degrees higher than \( T_j \)). Other \( T_{\text{sink}} \) differences ranging from 5.0°C to 40.0°C with a 5.0°C increment have also been conducted. Under the iso-current condition (\( I = 350 \text{ mA} \)), we observe that \( P_{\text{elec}} \) equals \( P_{\text{cond}} \) (because \( V \) varies minimally) and that \( R_{\text{th1}} = R_{\text{th2}} \) (for example, \( k_{\text{Cu}} \) varies from 413.0 to 393.0 W/mK when its temperature varies from 200 K to 400 K). Therefore, we can safely deduce \( T_{j=1} - T_{\text{sink}1} \approx T_{j=2} - T_{\text{sink}2} \) (Fig. 4a,b). As a result, we obtain two nonlinear relations,
\[ I = I_j(T_{j01}) \exp \left( \frac{qV_1}{nkT_{j01}} \right), \]  

and

\[ I = I_j(T_{j01} + \Delta T_{\text{sink}}) \exp \left( \frac{qV_2}{nk(T_{j01} + \Delta T_{\text{sink}})} \right), \]

where \( \Delta T_{\text{sink}1} = T_{\text{sink}2} - T_{\text{sink}1} \). Equations (4) and (5) can be simultaneously solved using the Newton-Raphson method or its modified version (Supplementary S6). Values of \( T_j \) agree well with those obtained using CRS, TC and TI (Fig. 4c–e). Additionally, we have found this \( T_{\text{sink}} \) difference of 10.0 °C to be optimal among other \( T_{\text{sink}} \) differences. If \( T_{\text{sink}} \) becomes too large, \( R_g \) no longer remains constant, violating the nonlinear thermal anchoring principle. If \( T_{\text{sink}} \) becomes too small, two algebraic equations tend to be similar, leading to algebraic redundancy.

Steps of the procedure can be outlined as:

(a) Measure the reverse current versus the junction temperature to obtain \( I_j(T_j) \).
(b) Measure the \( I - V \) characteristic curve from 1 mA to 500 mA at \( T_{\text{sink}1} = 25.0 \) °C and \( T_{\text{sink}2} = 35.0 \) °C, respectively
(c) To solve equations (4) and (5) using Newton-Raphson method to obtain \( T_{j01} \) at \( T_{\text{sink}} = 25.0 \) °C.

In summary, the discrepancy between PISO and non-PISO is attributed to non-synchronization of lattice and carrier temperatures in transient states. Generally in PISO carrier transient behaviors are intentionally bypassed, rendering the voltage and the carrier’s temperature disengaged. To confirm and avoid this PISO-induced disengagement, we first discover the LITA mechanism and develop an original, accurate, and nondestructive technique to measure LED junction temperatures in steady state conditions. This principle of the nondestructive method involves \( I - V \) characteristic of LEDs and nonlinear thermal anchoring. Finally, NTA results exhibit close agreements with data of Raman spectroscopy, thermal couples, and thermal imagers (Fig. 4c–e, Fig. S3a,b).

**Methods**

**Forward voltage method.** FVM includes three primary steps: (a) obtain a steady-state linear relationship between the voltage and \( T_j \) (inset of Fig. 2a), (b) operate PISO from state \( \alpha \) to state \( \beta \), and (c) allow the sample to cool down from state \( \beta \) to state \( \gamma \) (steady state) (Fig. 2a). Take blue InGaN/GaN LED (B1#) as the example. At three sink temperatures (25.0 °C, 35.0 °C, and 45.0 °C) and \( I_\beta = 5 \) mA, we measure three different voltages (2.565 V, 2.555 V, and 2.543 V), and obtain a negative-sloped line representing the relationship between \( V \) and \( T_j \), with \( k_\nu = -1.2 \) mV/K (inset). Next, we run a steady state current at \( I_\alpha = 350 \) mA for 5 minutes. Instantaneously, the current is switched down to \( I_\beta = 5 \) mA with the duration lasting approximately 1 µs. At this instant, the voltage, \( V_\beta \), is recorded. After approximately 5 more minutes, the voltage is recorded to be \( V_\gamma \). In reference to the linear relationship between \( V \) and \( T_j \), we deduce the value of \( T_{j01} \) according to \( V_\beta - V_\gamma = k_\nu(T_{j01} - T_j) \) to be 36.8 °C, which is assumed to equal \( T_{j01} \) in FVM.

**Confocal Raman spectroscopy.** CRS includes two primary steps: (a) measure Raman shifts for various \( T_j \) values to obtain a relationship between Raman shift and \( T_j \) when LED is lit at small currents (5 mA). The LED sample is mounted on a heat sink, controlled by a temperature controller (Keithley Instruments, Inc., American, Keithley 2510), and is lit by a current source (Keithley Instruments, Inc., American, Keithley 2611). (b) measure Raman shifts to obtain desired \( T_j \) when LED is lit by large currents. Raman shift signals are collected by a confocal Raman microscope (XploRA, HORIBA Jobin Yvon, France) to yield a correlation between the wave-peak location and the junction temperature when the LED is lit at small currents (5 mA). After the acquisition of this shift and \( T_j \) relationship, we turn on the LED at large currents and measure the Stokes shift again. Because the B1 chip emits 400~550 nm light beams, we select the 633 nm laser, carefully maintain all parametric conditions the same as the small-current run at \( T_{\text{sink}} = 25.0 \) °C, and measure Raman shifts under currents of 150 mA, 250 mA, and 350 mA.

**Thermocouples.** TCs are placed on the sample surface for several random positions and take average values (Supplementary S1).

**Thermal imager.** TI aims at the chips surface and takes the average of measurements distributed within a pre-determined area (Supplementary Fig. S1b–d).

**Nonlinear thermal-anchoring.** NTA principle combined with Shockley equation generates two nonlinear equations which are solved by Newton-Raphson method. All first-order derivatives are discretized using the finite difference method, with the occasional necessary to adopt the under-relaxation algorithm to achieve convergences.
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Author Contributions

J.H.Z. and T.M.S. conceived the original concept, performed experiments, and wrote the manuscript. Y.J.L., H.M. and Z.C. participated in technical planning and discussions. R.R.C. and Z.C. provided useful consultations.

Additional Information

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