Calibration of Estimated BER from Error Vector Magnitude with Carrier Phase Recovery

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Abstract
This paper presents the estimation of bit error ratio (BER) from error vector magnitude (EVM) for the quadrature phase shift keying (QPSK) modulation format with the Viterbi & Viterbi algorithm and differential decoding to compensate for laser phase noise. It is demonstrated analytically and through simulation that a calibration is necessary when using the established relationship between EVM and BER to take into account the implementation penalty associated with the carrier phase recovery algorithm. Simulation results using the proposed calibration technique are presented for different combined linewidth symbol duration product in a QPSK coherent system. The impact on the number of symbols used to estimate the BER from EVM analysis is also investigated and compared to error counting. An estimation with lower uncertainty is demonstrated to be achievable with EVM analysis compared to error counting for different number of symbols. Finally, the estimation of BER for a 16-ary quadrature amplitude modulation (16-QAM) optical coherent system is investigated using the blind phase search algorithm for carrier phase recovery.

Keywords
Error Vector Magnitude (EVM), Quadrature Phase Shift Keying (QPSK), Carrier phase recovery

Introduction
Advanced modulation formats are currently receiving renewed interest for the next-generation of optical communication systems [1]. In particular, the quadrature phase shift keying (QPSK) modulation format has attracted a lot of research interest to increase data capacity due to its robustness to linear impairments and optical signal-to-noise ratio requirements [2,3]. With information encoded on both the amplitude and phase of the optical carrier, accurate metrological tools need to be developed to quantify the performance of optical QPSK coherent systems. A plethora of performance metrics can be used in optical communications to assess the quality of spectrally-efficient modulation formats [4-8]. The performance of the transmitted signal can be evaluated using metrics such as bit error ratio (BER), Q-factor, eye diagram and, more recently, error vector magnitude (EVM) [9]. BER is the most conclusive figure of merit compared to the other performance metrics. However, it requires a known pattern, e.g. a training sequence, to be transmitted for continuous performance monitoring in optical networks. EVM is a popular performance metric in wireless digital communication systems and is commonly used to evaluate the quality of vector-modulated signals [10] and is a more suitable figure of merit at high optical signal-to-noise ratio (OSNR) in coherent systems where a large number of symbols will otherwise be required for accurate error counting.

In this paper, the estimation of BER from EVM analysis is first presented for the QPSK modulation format with the Viterbi & Viterbi algorithm and differential decoding for different combined linewidth symbol duration product, $\Delta \nu T_s$. A calibration is shown to be necessary when using the established relationship between EVM and BER to take into account the implementation penalty associated with the carrier phase recovery algorithm in optical coherent systems. The EVM analysis is shown to give better accuracy than error counting for different number of symbols. Finally, the estimation of BER from EVM analysis is presented for a 16-ary quadrature amplitude modulation (16-QAM) optical coherent system.

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Error Vector Magnitude and BER Estimation

Error vector magnitude is extensively applied as a performance metric for digital wireless communication systems and is commonly defined as the root-mean-square (rms) value of the difference between a collection of ideal transmitted symbols and the received symbols in the I-Q plane \([11,12]\). The rms EVM can be expressed as \([12]\)

\[
EVM_{\text{rms}} = \sqrt{\frac{1}{N} \sum_{k=1}^{N} \left| r_k - t_k \right|^2} \tag{1}
\]

Where \(P_a\) is the average transmitted power for the chosen modulation, \(t_k\) is the transmitted vector, \(r_k\) is the received signal vector, and \(N\) is the number of symbols over which the EVM is estimated. The vector \(r_k\) can either be a known reference pattern for data-aided EVM calculation or computed relative to the closest symbol in the constellation for non data-aided EVM calculation. EVM is related to signal-to-noise ratio (SNR) as follows \([11]\)

\[
EVM_{\text{rms}} = \frac{1}{\sqrt{\text{SNR}}} \tag{2}
\]

for data-aided calculation. For the QPSK modulation format and differential decoding, where the EVM is caused only by amplified spontaneous emission (ASE) noise, the BER can be estimated using \([11]\)

\[
\text{BER} = \text{erfc} \left[ \sqrt{2 \cdot \text{EVM}_{\text{rms}}^2} \right] \tag{3}
\]

where a factor of 2 has been included for the differential coding penalty and erfc is the complementary error function. Although the relationship (3) is valid for data-aided EVM calculation, it can also be applied to non data-aided EVM calculation for BER \(< 10^{-2}\) as discussed in \([6]\). The performance of (3) with carrier phase recovery is discussed in the next section.

BER Estimation with Carrier Phase Recovery

The feed forward Viterbi & Viterbi algorithm (VVA) is the widely adopted scheme for the QPSK modulation format in digital coherent receivers for carrier phase recovery. The estimated phase, \(\phi\), using the VVA can be obtained using \([13]\)

\[
\phi = \frac{1}{4} \arg \sum_{k=1}^{N_b} r_k^4 \tag{4}
\]

where \(N_b\) is the averaging block size. The VVA is typically followed by differential decoding to solve the four-fold phase ambiguity and also to avoid cycle slips. The analytical expression for the BER of a differentially encoded QPSK signal using the VVA with block averaging can be approximated as \([14]\)

\[
P_e \approx \int_{-\infty}^{\infty} \text{erfc} \left[ \sqrt{\frac{\gamma_s}{2}} \left( \cos(\epsilon) - \sin(\epsilon) \right) \right] P_{\phi\epsilon}(\epsilon) d\epsilon, \tag{5}
\]

where \(\gamma_s\) is the SNR, \(P_{\phi\epsilon}(\epsilon)\) is the Gaussian probability density function of the phase estimation error with zero mean and variance \([14]\)

\[
\sigma_{\phi}^2 \approx \frac{2\pi \Delta v T_s (N_b^2 - 1)}{6N_b} + \frac{\sigma_n^2 (1 + 4.5\sigma_n^2)}{2N_b}, \tag{6}
\]

where \(\sigma_n = \sqrt{1/\gamma_s}\).

The optimum block size, \(N_{\text{opt}}\), to minimize the standard deviation of the phase estimation error is given as \([14]\)

\[
N_{\text{opt}} = \text{round} \left[ \sqrt{\frac{3(1 + 4.5\sigma_n^2)}{2\pi \Delta v T_s}} - 1 \right] \tag{7}
\]

The above analytical approximation for the BER with the optimum block size is compared in Figure 1 with the estimated BER from EVM analysis and error counting for different values of \(\Delta v T_s\). The theoretical limit with differential decoding is also shown for comparison. The phase noise in the simulation was modeled as the Wiener process \([15]\)

\[
\theta_k = \sum_{i=-\infty}^{k} v_i \tag{8}
\]

where \(v_i\)’s are independent and identically distributed (i.i.d) random Gaussian variables with zero mean and variance

\[
\sigma_p^2 = 2\pi \Delta v T_s \tag{9}
\]

The simulation was performed over 200,000 symbols with non data-aided EVM calculation. The theoretical BER with phase noise was found to be in good agreement with error counting except for \(\Delta v T_s = 10^{-3}\) due to the assumption of small phase estimation error in (5). The BER estimated from EVM analysis, however, can be seen to deviate from error counting as the implementation penalty associated with the carrier phase recovery algorithm is not included in (3). Similar results were reported in \([8]\) for QPSK transmission experiments where the BER obtained from EVM analysis was found to be underestimated compared to error counting. It is noted that similar underestimation is also observed for non-differential decoding; however it is anticipated that installed systems will employ differential decoding to mitigate cycle slips.

The BER obtained from EVM analysis using (3) must

\[\int_{-\infty}^{\infty} \text{erfc} \left[ \sqrt{\frac{\gamma_s}{2}} \left( \cos(\epsilon) - \sin(\epsilon) \right) \right] P_{\phi\epsilon}(\epsilon) d\epsilon, \tag{5}\]
therefore be calibrated to reliably estimate the actual BER
with carrier phase recovery. From (2) and (3), it can be
seen that the calibration can be achieved by scaling the
estimated SNR from EVM analysis when calculating the
BER as follows

\[ BER_{cal} = \operatorname{erfc} \left( \frac{10^{-\frac{-\Delta P}{10}}}{2 \cdot EVM_{rms}^2} \right) \]  \hspace{1cm} (10)

where \( \Delta P \) is the implementation penalty in dB associ-
ated with the carrier phase recovery algorithm at the cali-
bration point. Figure 2 shows the required SNR to achieve
the target BER of \(10^{-4}, 10^{-3}, \) and \(10^{-2}\) using the analytical
approximation (5). The block size was optimized accord-
ing to (7) for the different values of \(\Delta vT_s\). Figure 3 shows
the corresponding implementation penalty, \( \Delta P \), relative
to the theoretical limit with differential decoding for the
respective target BER. Calibration results using (10) with
the analytical approximation of \( \Delta P \) are presented in the
next section for different values of \( \Delta vT_s \).

**Calibration Results**

The results shown in Figure 1 reveal that the relation-
ship (3) underestimates the BER depending on the val-
ue of \(\Delta vT_s\). Calibrating the BER estimated from EVM
analysis is thus necessary to reliably monitor the perfor-
mance of QPSK coherent systems. The calibrated BER is
compared to the estimated BER from EVM analysis and

![Figure 1: Theoretical BER (5) compared to estimated BER from EVM analysis and error counting for (a) \(\Delta \nuT_s = 10^{-5}\), (b) \(\Delta \nuT_s = 10^{-4}\), and (c) \(\Delta \nuT_s = 10^{-3}\).](image1)

![Figure 2: Required SNR to achieve target BER of \(10^{-4}, 10^{-3}, \) and \(10^{-2}\) using analytical approximation (5) with the optimum block size for the Viterbi & Viterbi algorithm.](image2)

![Figure 3: Implementation penalty, \( \Delta P \), of the Viterbi & Viterbi algorithm relative to theoretical limit with differential decoding for target BER of \(10^{-4}, 10^{-3}, \) and \(10^{-2}\).](image3)
error counting in Figure 4 for different values of $\Delta \nu Ts$. The required SNR shown in Figure 2 was used to achieve the target BER of $10^{-4}$, $10^{-3}$, and $10^{-2}$ in the simulation. The estimated BER from EVM analysis using (3) can be seen to deviate from error counting for $\Delta \nu Ts > 10^{-3}$ where the implementation penalty $\Delta P$ associated with the carrier phase recovery should be considered for accurate results. The calibration technique (10) with the analytical values of $\Delta P$ can be seen to significantly improve the accuracy of the estimated BER from EVM analysis in Figure 4 except for $\Delta \nu Ts = 10^{-4}$ where the analytical approximation is less accurate. Nevertheless, the calibrated BER can be seen to give a closer estimate to error counting, in particular, at the target BER of $10^{-2}$ and $10^{-3}$ compared to the estimated BER from EVM analysis without calibration.

It should be noted that the value of $\Delta P$ can also be obtained by comparing the performance of (10) with error counting as part of a calibration process instead of using the analytical approximation. Such approach would be useful, for example, when the implementation penalty in the transmission system is higher than the analytical value of $\Delta P$ associated with the carrier phase recovery algorithm. Figure 5 shows the performance for $\Delta \nu Ts = 10^{-4}$ where the optimum value of $\Delta P$ was determined by minimizing the difference between the BER estimated from (10) and error counting at the target BER of $10^{-4}$. As it can be seen, the calibration technique (10) can reliably monitor the optical performance over an SNR range of at least 3 dB with $\Delta P$ determined by comparing (10) and error counting at the calibration point.

Next, the simulation was performed over 1000 trials to investigate the impact of using different number of symbols on the estimation of the BER from EVM analysis and error counting at the target BER of $10^{-3}$ as shown in Figure 6. The mean BER values, $\mu$, over the 1000 trials can be seen to be similar for both estimators with $N > 10,000$. However, from the curve bands, $\mu \pm \sigma$, where $\sigma$ is the standard deviation, it can be seen that an estimation with lower uncertainty can be achieved from EVM analysis compared to error counting. The standard deviation of the estimated BER from EVM analysis is compared to error counting in Figure 7 for different number of symbols. As it can be seen, the estimation of BER from EVM analysis is significantly better than error counting. The above simulation results demonstrate that the calibrated BER can potentially be a useful figure of merit to reliably monitor the optical performance of coherent systems with EVM analysis as opposed to the large number of symbols that may be required for accurate error counting.

![Figure 4: Performance of calibrated BER with the analytical values of $\Delta P$ compared to the BER estimated from EVM analysis and error counting at the target BER of $10^{-4}$, $10^{-3}$, and $10^{-2}$.](image1)

![Figure 5: Performance of calibrated BER compared to the BER estimated from EVM analysis and error counting. The inset shows the recovered QPSK constellation at the SNR of 10.5 dB ($\Delta \nu Ts = 10^{-4}$ and $\Delta P = 0.245$ dB).](image2)

![Figure 6: Impact on the number of symbols used to estimate the BER from EVM analysis and error counting at the target BER of $10^{-3}$ ($\Delta \nu Ts = 10^{-4}$ and $\Delta P = 0.245$ dB).](image3)
For QPSK and 16-QAM, the values of $F$ can thus be set to 2 and 1.67, respectively, to include the expected differential decoding penalty for the different modulation formats. Note that equation (11) reduces to (3) for the QPSK modulation format. The carrier phase recovery was implemented using the feed forward blind phase search algorithm [15] which is applicable to arbitrary M-QAM constellations and suitable for real-time implementation with high linewidth tolerance. The number of test phases was set to 32 with a filter half width of 9 as discussed in [15] for 16-QAM. The simulation was performed over 200,000 symbols.

Figure 8 shows the estimated BER from EVM analysis for the 16-QAM coherent system with $\Delta\nu Ts$ set to $10^{-4}$. As it can be seen, the BER is also underestimated for 16-QAM with carrier phase recovery. Following a similar calibration approach as (10) for QSPK, the implementation penalty, $\Delta P$, can also be included in (11) to calibrate the estimated BER for 16-QAM. The calibrated BER with $\Delta P = 0.4$ dB can be seen to be in good agreement with error counting in Figure 8. The value of $\Delta P$ was determined by comparing the estimated BER from EVM analysis with error counting at the target BER of $10^{-3}$. The above calibration approach is thus equally applicable to 16-QAM optical coherent systems with carrier phase recovery when estimating the BER from EVM analysis.

Conclusions

The estimation of BER from error vector magnitude analysis has been demonstrated for the QPSK modulation format with carrier phase recovery and differential decoding. The laser phase noise was compensated using the widely adopted Viterbi & Viterbi algorithm with block averaging. Analytical and simulation results demonstrate that a calibration is necessary for accurate BER estimation with $\Delta\nu Ts > 10^{-5}$ to take into account the implementation penalty associated with the carrier phase recovery algorithm. The impact on the number of symbols used to estimate the BER from EVM analysis has also been presented. An estimation with lower uncertainty can be achieved with EVM analysis compared to error counting. Finally, the calibration approach was shown to be equally applicable to 16-QAM optical coherent systems.

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