A Synchrotron-Based Study of the Mary Rose Iron Cannonballs

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Abstract: Post-excavation iron corrosion may be accelerated by the presence of Cl⁻, leading to conservation methods designed to remove Cl. This study exploits a unique opportunity to assess 35 years of conservation applied to cast-iron cannon shot excavated from the Mary Rose. A combination of synchrotron X-ray powder diffraction (SXPD), absorption spectroscopy (XAS), and fluorescence (XRF) mapping have been used to characterise the impact of conservation on the crystalline corrosion products, chloride distribution, and speciation. The chlorinated phase akaganeite, β-FeO(OH,Cl), was found on shot washed in corrosion inhibitor Hostacor IT with or without an additional reduction stage. No chlorinated phases were observed on the surface of shot stored in sodium sesquicarbonate (Na₃CO₃/NaHCO₃); however, hibbingite, β-Fe₂(OH)₃Cl, was present in metal pores. It is proposed that surface β-FeO(OH,Cl) formed in the early stages of active conservation owing to oxidation of β-Fe₂(OH)₃Cl at near-neutral pH.

For over 2000 years, iron has been used to manufacture weapons, tools, ceremonial items, and more. However, surviving artefacts are prone to permanent loss or damage through the action of corrosion. During burial, the metal oxidises by an electrochemical process, where the cathodic reaction and oxidising agent are dependent on environmental conditions. Commonly, this involves either H₂ evolution or O₂ reduction, with multiple pathways involved in the reaction, resulting in complex corrosion layers. Under favourable conditions, the corrosion rate may be sufficiently low to allow exceptional preservation of artefacts. One such case is the shipwreck of King Henry VIII’s flagship, the Mary Rose (1511–1545), which sunk off the coast of Portsmouth on July 19, 1545. Buried in sediment 14 m below the surface, the ship was held in an environment with dissolved O₂ concentration of 0 mg L⁻¹ and redox potential, E₉, between −34 and −110 mV. These conditions allowed the ship and ca. 19000 artefacts to survive until excavation between 1979 and 1982.

Iron objects from sites with good preservation conditions face a greater threat from corrosion that occurs after excavation. Exposure to air and water can cause oxidation of FeO to stable FeII, FeIII, and intermediate FeIIIII compounds leading to rapid deterioration (Figure 1a). Further

Figure 1. Mechanical damage to Mary Rose cast iron cannon shot: a) shot showing severe cracking and degradation in storage [photo credit: The Mary Rose Trust], b) typical structure observed during artefact sampling, as represented in c) with a very thin layer of surface corrosion and separation of original metal into two layers owing to internal voids and cracks.

more, in the presence of Cl⁻, the reaction rate increases, resulting in preservation challenges for objects buried in chlorine-rich environments, such as seawater. To mitigate this, several desalination treatments have been proposed that aim to remove as much Cl as possible from the artefact. These techniques can be divided into two categories: reduction-based, where Cl⁻ is removed by transformation of chorine-containing FeIII crystals, and washing methods that remove chlorine by diffusion into aqueous solution. Comparison of different conservation methods has been limited by the variability of both objects and burial environments. As a result, it is often not possible to attribute differences in treatment success to technique used, while studying material that accurately reflects an archaeological artefact. To overcome these issues, this work focuses on the collection of 1248 cast iron cannon shot from the Mary Rose.

Having been produced in bulk, the shot were buried together and their relative uniformity maintained until

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Immediately after excavation, all of the shot or during samples; Table 1).

Table 1: Details of samples and shot analysed in this study.

| Shot ID   | Dimensions d [mm] | Weight [g] | Treatment | No. of samples analysed |
|-----------|-------------------|------------|-----------|-------------------------|
| 81A1527   | 85.0              | 2410.8     | SS        | 2                       |
| 81A2310   | 82.6              | 2199.9     | SS        | 2                       |
| 81A3470   | 84.8              | 2107.0     | SS        | 2                       |
| 81A3550   | 84.1              | 2361.0     | SS        | 1                       |
| 81A839    | 86.0              | 2014.8     | SS        | 3                       |
| 82A2618   | 85.3              | 2012.5     | SS        | 4                       |
| 82A4365[1] | 99.0             | 3500.0     | SS        | 1                       |
| 82A4233[1] | 86.0             | 2802.6     | SS        | 2                       |
| 81A461[1] | 84.0              | 568.3      | SS        | 2                       |
| 81A6218[1] | 193.0            | 26000      | SS        | 1                       |
| 81A6219[1] | 192.0            | 25750      | SS        | 1                       |
| 81A6143   | 79.9              | 1818.1     | HWAS      | 1                       |
| 83A0161   | 83.6              | 1740.3     | HW         | 1                       |
| 83A0189   | 70.6              | 1263.7     | HWAS      | 1                       |
| 83A0446   | 80.0              | 1052.0     | HW         | 1                       |
| 81A0177   | 85.0              | 2410.8     | HWAS      | 1                       |
| 81A6102   | 83.7              | 2045.1     | HW         | 1                       |

[a] Diameter, d, and weight measurements from excavation record.
[b] Artefact in too many pieces for accurate measurement.

and dried in 2-stage acetone:water (1:1 and 1:0) series. Now stored in a controlled environment (20°C, 20% RH)

3) HWAS: same as (2) but underwent additional alkaline sulfide, NaOH/NaSO₃, pH 12–13 reduction treatment.[15] Now stored in controlled (20°C, 20% RH) environment

Two types of samples were collected: bulk corrosion powders from the object surface (-S samples) and cut cross-sections mounted in polyester resin (-S samples; Table 1). Crystalline phases were studied by SXPD of -S samples, while the chloride distribution and speciation of -S samples were probed by synchrotron XRF mapping and Cl k-edge X-ray absorption near-edge spectroscopy (XANES), respectively. Details of the method may be found in the Supporting Information.

During cutting, cracks were observed in HW and HWAS shot, presenting a structure (Figure 1b,c) that consists of a thin (< 0.5 mm) surface corrosion layer over the original Tudor metal. Corrosion around large cracks and casting voids is associated with severe degradation and mechanical failure. In some cases, this has led to fracturing, indicating that corrosion is occurring inside the artefact, rather than from the outside in.

The chlorinated phase most often associated with archaeological iron corrosion in chlorinated media is akaganeite,[22–24] commonly referred to as β-FeO(OH), though more closely defined as FeO₃(ΣH(OH))₂Cl₃.[23] Akaganeite has a monoclinic crystal structure (space group: P2/m), built from edge- and corner-sharing Fe(OO)₆ octahedra that form a tunnel structure similar to the hollandite crystal.[22,25,26] Two Cl sites may be distinguished:[23] within the tunnel structure, Clₓ, and adsorbed to the surface, Clᵧ of the crystal, Figure 4b. The size of individual β-FeO(OH) crystals depends on the growth conditions, but is typically small, around 0.15 × 0.03 μm, resulting in a large proportion of Clₓ.[22] During a washing-based conservation treatment, mobile Clₓ is removed, while Clᵧ is thought to be unaffected.[14,22,23,27] X-ray diffraction of akaganeite gives two low-angle peaks, which at the wavelength used in this study (λ = 0.82578 Å) appear at 2θ values 6.35° and 8.95°, corresponding to the (101) and (200) planes, respectively. The insets in Figure 2a highlight the location of these peaks (dotted grey lines) and show that, somewhat surprisingly, akaganeite is not observed in the surface corrosion products of any of the SS shot, while it is present on the surface of all HW and HWAS shot. Phase identification of the powder diffraction profiles, Figure 2b, instead shows a combination of phases from the burial environment: calcite (CaCO₃), quartz (SiO₂), and aragonite (CaCO₃); related to the microstructure of the metal: graphite and cementite (Fe₃C); and commonly reported[13,14] marine iron corrosion products: goethite α-FeOOH, magnetite Fe₃O₄ and lepidocrocite γ-FeOOH.

Reflecting the SXPD results, where no chlorinated corrosion products were observed on the surface of SS shot, Cl elemental maps of -S samples (Figure 3 and the Supporting Information, Figure S7) show no chlorine at the surface of SS shot, while a localised layer of Cl is present on the outer edges and around voids of HW and HWAS shot. However, in one SS shot, the example shown in Figure 3, an area of Cl in the inner region of the sample can be seen. Comparing the Cl k-edge XANES in this inner area to the chlorine species observed on a HW treated shot (Figure 4) it can be seen that the Cl species is different. To identify the chlorine species present in the Mary Rose samples, a library of Cl standards was prepared by a combination of chemical purchases and synthesis (see the Supporting Information). Cl XANES from the standards were used to fingerprint spectral features in the sample datasets. The library of standards included a lab-synthesised sample of hibbingite, β-Fe₂(OH)₃Cl, a precursor to akaganeite that has been observed on archaeological iron,[3,28,29] but rapidly oxidises[30,31] to akaganeite in storage[23] or during
conservation and a lab-synthesised standard of β-FeO(OH), prepared by hydrolysis of an Fe\(^{3+}\) chloride solution. To simulate the effect of a washing treatment, the akaganeite standard was immersed in 500 mL distilled H\(_2\)O for 1 month at ambient conditions, with solution changes every 48–72 hours, giving a series of incrementally washed standards AKA-1 (0 washes) to AKA-8 (7 washes). Comparing the spectra from the HW and SS shot, it can be seen that the HW spectrum is consistent with β-FeO(OH), Figure 4c, while the spectrum from beneath the surface of the SS shot, Figure 4d, is consistent with the precursor Fe\(^{2+}\) chloride, β-Fe\(_2\)(OH)\(_3\)Cl.

Looking at the pre-edge region (Figure 4a), a small feature is visible at 2819–2822 eV for the unwashed akaganeite that is decreased in amplitude for the washed standard. The XANES data from the series of washed standards, AKA1–8, were fitted with three peaks to compare the relative intensities of the observed features (Figure 5). While the contribution from the second and third peaks remains constant throughout the series (Figure 5c, squares), the contribution from the first peak, the pre-edge, decreases with an increasing number of washes (circles and stars). This feature arises from electronic transitions in partially-bound Cl\(^-\), demonstrating that chlorine is lost from this site during washing. For the HW sample, a reduced amplitude is observed, indicating that the phase has gone through several washing
stages to remove $Cl_{sur}$. From this, it may be inferred that $\beta$-$FeO(OH)$ formed prior to, or in the early stages of the washing treatment. Immediately before the HW shot underwent active conservation, it was stored at pH 10 and was analogous to SS shot, that is, no surface $\beta$-$FeO(OH)$, but subsurface chlorine present in pores as $\beta$-$Fe_2(OH)_3Cl$. Studies have shown that oxidation of hibbingite to akaganeite in solution is only thermodynamically feasible in the pH range 4–6, and that complete transformation can occur in about 7 hours. As a result, it is proposed that the sudden change in pH from 10 to near-neutral during active conservation, coupled with removal in tap water of adhering corrosion layers, led to exposure of previously-blocked pores and cracks, enabling mobilisation of sub-surface chlorine and subsequent oxidation to akaganeite at the object surface. This transformation would have occurred while the artefact was in the first washing bath, resulting in loss of $Cl_{sur}$ in successive washes. This conclusion is supported by a recent in situ study of hibbingite on archaeological iron, where akaganeite was not observed to form in NaOH, but was observed after drying at the end of the treatment. However, while this mechanism can be used to explain akaganeite formation on this sample, it only represents a single location on a single artefact. In cases where fracturing has occurred to an object and a new surface is exposed to the external environment, corrosion products can be observed to form while in storage or on display. Rather, this investigation has shown that, alongside its formation after conservation, there are additional opportunities for akaganeite to form on archaeological iron, such as during or in-between treatment stages.

In conclusion, this work has used a combination of synchrotron techniques to gain an unprecedented insight into the effect of conservation choices on iron corrosion. It has been shown that during multi-decade immersion in sodium sesquicarbonate solution, chlorine is removed from the outer surface of artefacts; however, Cl can remain trapped in pores within the metal, in the form of hibbingite, $\beta$-$Fe_2(OH)_3Cl$. On exposure to oxygen at near-neutral pH, this phase rapidly oxidises to $\beta$-$FeO(OH)$. In the case of the Mary Rose shot, it is proposed that this transformation occurred during treatment, owing to a combination of pH change and surface removal. Using chlorine XANES spectra, it has been shown that, years after conservation, it is possible to differentiate iron corrosion products formed during treatment. This reveals that post-conservation studies of artefacts, even decades after treatment, have an important role to play in the future development of conservation.
Keywords: archaeology · chlorine · corrosion · iron · X-ray absorption spectroscopy

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Conflict of interest

The authors declare no conflict of interest.
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