Gentisides are a class of chemical compounds which is considered as potential therapeutic substance for treatment of neurodegenerative disorders. The heat reflux extraction conditions were optimized for seven kinds of gentisides from the root and rhizome of *Gentiana rigescens* Franch. ex Hemsl. by employing response surface method. Based on univariate test, a Box–Behnken design (BBD) was applied to the survey of relationships between response value (gentisides yield) and independent variables which were chosen from various extraction processes, including extraction temperature, extraction time, and solvent–material ratio. The optimized conditions for this extraction are as follows: extraction time of 3.40 h, extraction temperature of 74.33 °C, and ratio of solvent to raw material of 10.21:1 mL/g. Verification assay revealed that the predicted value (99.24%) of extraction parameters from this model was mainly conformed to the experimentally observed values (98.61 ± 0.61).
of associated control (or input) variables, which consists of a
group of mathematical and statistical techniques [12]. Com-
pared with traditional optimization method, major advantage
of RSM is that it can perform the interactive effects among
the studied variables. Full three-level factorial, Box-Behnken,
central composite, and Doehlert designs were used most
frequently for RSM of experimental design [13]. Compared
with central composite and three-level full factorial design,
the Box-Behnken design employed in this experiment and
Doehlert matrix design demonstrated slightly more efficiency
than others [14]. Previous researches about gentisides were
progressive and continuous; however, the knowledge of
extraction process about the active constituent has not been
described. Thus, we attempted to seek optimum conditions
for gentisides extraction according to RSM.

2. Materials and Methods

2.1. Materials and Reagents. The root and rhizome of G.
rigescens collected from Yunxian (Lincang City, Yunnan
Province, China) were identified by Professor Hang Jin
from Yunnan Academy of Agricultural Science (YAAS). The
herbariums were preserved in the Institute of Medicinal
Plants, YAAS. The material specimens dried at 50°C for a
week were ground through a 60-mesh sieve and then
utilized as test spares. HPLC grade methanol and acetonitrile
(Sigma Inc., USA) were used as eluents A and B for chromato-
graphic analysis. All the other reagents including ethanol,
trichloromethane, and cyclohexane were used in analytical
grade.

2.2. Heat Reflux Extraction. Samples of 2 g were extracted
by means of conventional heat reflux extraction using 90%
ethanol solvent in a given extraction temperature, extrac-
tion time, and solvent-material ratio. The above operations
repeated twice. The combined hot extracts of samples were
collected and filtered through filter paper. A process of
decompressing concentration was implemented with the
filtration liquid using a rotary evaporator (BUCHI, Flawil,
Switzerland) at 45°C until becoming highly enriched extrac-
tum.

2.3. Purification Process of Primary Extract. The previous
extractive liquor was loaded into SPE (Solid Phase Extract-
ion) silica gel column chromatography (500 mg/3 mL, Won-
daSep, SHIMADZU-GL, Tokyo, Japan). Eluents C and D
(ratios of cyclohexane to chloroform were 9:1 and 7:3, resp.)
were used for eluting the active ingredients from the silica gel
column, and usage amount was 1.5 mL and 5 mL, respectively.
Elution fractions of eluent D were collected and concentrated
to dry and then dissolved by ethanol absolute of 1 mL for
subsequent determination by HPLC [15].

2.4. Determination and Analysis of Gentisides by HPLC.
Chromatographic analysis was carried out on a Dionex
U3000 HPLC system (Dionex, Sunnyvale, USA) equipped
with DAD detector. A reversed-phase WondaCract ODS-2
column (5 µm, 4.6 mm × 250 mm; SHIMADZU-GL, Japan)
was used for separating the purified samples. The mobile
phase consisted of methanol as eluent A and acetonitrile as
eluent B which was performed with flow rate of 1.0 mL/min
for one hour. The ratio of eluent A to eluent B was 4:6,
column temperature was 30°C, and the injection volume
was 20 µL. UV detection wavelength of the monitor was
arranged at 210 nm [15]. Data processing was carried out with
Chromeleon 6.80 SR9a software.

Content of gentisides could be calculated by establishing
standard curve. The gentisides yield (GY) was calculated
using the following equation:

\[
\text{gentisides yield} (%) = \frac{\sum_{i=1}^{7} Y_i}{Y_0},
\]

\[
Y_{1-7} = Y_A, Y_B, Y_G, Y_H, Y_I, Y_J, Y_K,
\]
where $Y_i$ represented the value of gentisides content calculated by corresponding peak area sourced from HPLC and $Y_0$ was estimated value of sample, which was evaluated as 3 mg previously.

2.5. Univariate Test Design. Concentration of extraction solution (ethanol-water solution), extraction temperature, extraction time, and solvent-material ratio were considered as main influence factors to gentisides yield extraction. The parameters and their ranges were as follows: concentration of extracting solution of 60–90%, extraction temperature of 55–85°C, extraction time of 0.5–4 h, and ratio of liquid to material of 1:4–1:12 (g/mL).

2.6. Optimum Experiment Design and Statistical Analysis. The parameters of extraction conditions were optimized using response surface methodology. Based on the consequence of univariate test, a BBD (three factors, three levels) experiment was performed to elucidate the relationships between independent variables ($X_1$, $X_2$, and $X_3$), and exclusive response value ($Y$) [13]. The actual values were coded at three levels: −1, 0, and +1. Experimental design scheme derived from Design-Expert 8.0.6 software (Stat-Ease Inc., MN, USA) and response value (gentisides yield) were shown in Table 1. The four variables were coded according to the following equation:

\[
X_i = \frac{x_i - x_0}{\Delta x},
\]

where $X_i$ is the coded value, $x_i$ is the corresponding actual value, $x_0$ is the actual value in the center of the domain, and $\Delta x$ is the increment of $x_i$ corresponding to a variation of 1 unit of $X$ (Supplementary Material 2 in Supplementary Material available online at http://dx.doi.org/10.1155/2015/819067). Regression coefficients for intercept, linear, quadratic, and interaction terms and nonlinear quadratic polynomial model employed were as follows:

\[
Y = \beta_0 + \sum_{i=0}^{k} \beta_i x_i + \sum_{j=0}^{k} \beta_{ij} x_i^2 + \sum_{i=0}^{k} \sum_{j=0}^{k} \beta_{ij} x_i x_j,
\]

where $Y$ was the response function; $\beta_0$ was a constant; $\beta_i$, $\beta_{ii}$, and $\beta_{ij}$ were the linear, quadratic, and interactive coefficients, respectively; and $x_i$ represented the coded levels of independent variables. The terms $x_i x_j$ and $x_i^2$ were expressed as the interaction and quadratic terms, respectively.

3. Results and Discussion

3.1. Chromatographic Results. The HPLC chromatograms of standard substance and testing sample were shown in Figures 2(a) and 2(b). Absorption peaks of the target compounds were arisen at retention time of 15.180, 18.917, 21.040, 25.047, 26.610, and 29.783 min. The calibration curves were plotted...
by using five gradient concentrations of mixed standard substance (0.01, 0.05, 0.10, 0.50, and 1.00 mg/mL), which quantified the GY (expressed as %) by means of regressive equations: 

\[ Y = 735.88x + 0.9700 \]  

(gentiside A, \( R^2 = 0.9994 \))

\[ Y = 446.81x - 2.2227 \]  

(gentiside B, \( R^2 = 0.9976 \))

\[ Y = 419.66x - 0.1712 \]  

(gentiside G, \( R^2 = 0.9988 \))

\[ Y = 655.49x + 2.2037 \]  

(gentiside H, \( R^2 = 0.9989 \))

\[ Y = 630.77x + 1.2064 \]  

(gentiside I, \( R^2 = 0.9987 \))

\[ Y = 417.80x + 2.1768 \]  

(gentiside J, \( R^2 = 0.9985 \)), and 

\[ Y = 130.69x - 0.1592 \]  

(gentiside K, \( R^2 = 0.9995 \)),

where \( Y \) denoted peak area and \( x \) denoted concentration of sample (linear intervals were shown in Supplementary Material 3). HPLC conditions including precision, stability, and repeatability were summarized in Supplementary Material 4, which revealed that the experiment conditions performed well enough to carry on sample analysis.

3.2. Effect of the Ethanol Concentration on the Gentisides Yield. We selected, respectively, 60%, 70%, 80%, and 90% as the concentration of ethanol-water to investigate the effect of discrepant concentration of the extraction solvent on the gentisides yield when other extraction parameters were as follows: extraction temperature 75°C, extraction time of 3 h, and solvent-material ratio of 10 mL/g. As shown in Figure 3(a), the content of gentisides was rising straight along with increasing concentration of ethanol and finally we obtained the highest content of gentisides in concentration of 90%. Therefore, we selected 90% as concentration of solvent in this experiment.

3.3. Effect of the Extraction Temperature on the Gentisides Yield. The extraction temperature was set at 55, 65, 75, and 85°C, respectively, to examine the effect of different temperature on the gentisides yield when other extraction parameters were as follows: ethanol-water concentration of 90%, extraction time of 3 h, and solvent-material ratio of 10 mL/g. As shown in Figure 3(b), a distinct increase of the content of gentisides emerged in plate from 55 to 75°C, and then the content of gentisides dropped slightly from 75 to 85°C. It
could be explained that ester groups of effective components were resolved at high temperature [16, 17]. The statistical analysis showed that significant differences existed among 55, 65, 85, and 75°C, and the content of gentisides reached the highest temperature at 75°C. As a result, we selected 75°C as the center point of extraction temperature in this experiment.

3.4. Effect of the Extraction Time on the Gentisides Yield. The extraction time was set at 0.5, 1, 2, 3, and 4 h, respectively, to examine the effect of different extraction time on the gentisides yield when other extraction parameters were as follows: ethanol-water concentration of 90%, extraction temperature of 75°C, and solvent-material ratio of 10 mL/g. As shown in Figure 3(c), the content of gentisides was rising straight as extraction time from 0.5 to 1 h and then rose up slightly from 1 to 4 h. As a result, we selected 2 h as the center point of extraction time in this experiment.

3.5. The Effect of the Ratio of Liquid to Material on the Gentisides Yield. Respectively, 4, 6, 8, 10, and 12 mL/g were selected as the ratio of liquid to material of extraction parameter to investigate the effect of different extraction time on the gentisides yield when other extraction parameters were as follows: ethanol-water concentration of 90%, extraction temperature of 75°C, and solvent-material ratio of 10 mL/g. As shown in Figure 3(d), the content of gentisides was rising straight as solvent-material ratio rising from 4 to 10 mL/g, particularly at the beginning of solvent volume increase, and then rose up inconspicuously after 10 mL/g. To maximize gentisides yield, we selected 10 mL/g as the center point of solvent-material ratio in this experiment.

3.6. Optimization Parameters by Response Surface Method. The extraction of gentisides from Gentiana rigescens was optimized through response surface methodology. An optimum result could be obtained from optimized model according to statistical analysis. All the 17 of the designed experiments were disorderedly conducted (for the decrease of uncontrollable influence) on the basis of Table 1. Response variable $Y$ predicted and the test variables $(X_1, X_2, and X_3)$ were related by the following second-order polynomial equation:

$$Y = +98.08 - 0.49X_1 + 5.26X_2 + 1.82X_3 - 7.02X_1X_2$$
$$- 2.55X_1X_3 - 3.77X_2X_3 - 26.40X_1^2 - 6.71X_2^2$$
$$- 2.35X_3^2,$$


where $Y$ is function of the regression equation, namely, GY (%), and $X_1, X_2, and X_3$ are the coded variables for extraction temperature, extraction time, and the ratio of solvent to the raw material, respectively.

As shown in Table 2, the analysis of variance (ANOVA) was employed for statistical significance of response surface quadratic polynomial model. Here, model $F$-value of 12.68 (more than $F$-critical value of 8.81) and model $P$ value (95% confidence level) of 0.0015 (<0.01) indicated that the quadratic polynomial model was significant in order to suitably predict optimal experiment conditions. The lack of fit measures the failure of the model to represent the data in the experimental domain at points which are not included in the regression [18]. As listed in Table 2, $F$-value and $P$ value of the lack of fit were 0.39 and 0.7674, respectively, which indicated that it was not significant relative to the pure error and implied that the model equation was available. The higher the value of $R^2_{adj}$ is, the deeper the correlation between the observed and predicted values performs [19]. The value of $R^2$ (determination coefficient) was 0.9422, which indicated the satisfactory correlation between actual values and predicted ones [20, 21]. The value of $R^2_{adj}$ (adjusted determination coefficient) was 0.8679, which meant that at least 86.79% of the gentisides content could be predicted by the model, and only less than 1.3% of the total variations were not explained by model. Adequate precision compares the range of the predicted values at the design points to the average prediction error. A ratio greater than 4 indicated adequate model discrimination. As shown in Table 2, the value of adequate precision was 10.122, which indicated an adequate signal for model and could be used to navigate the design space. CV (coefficient of variation) indicates the degree of precision with which the experiments are compared. As shown in Table 2, a relatively low value of CV was 1.14, which showed a better precision and reliability of quadratic polynomial model [18].

The $P$ value is used as a tool to check the significance of each coefficient and the interaction strength between each independent variable [22]. According to the $P$ values of each model term summarized in Table 2, it could be concluded that these terms including an independent variable ($X_3$) and two quadratic terms ($X_1^2$ and $X_2^2$) were significantly affecting the yield of gentisides ("Prob > $F" less than 0.05), and among them quadratic terms were the most significant parameters.

| SD     | SS   | DF | MS   | $F$ value | $P$ value |
|--------|------|----|------|-----------|-----------|
| Model  | 3816.19 | 9  | 424.02 | 12.68     | 0.0015    |
| $X_1$  | 1.94  | 1  | 1.94  | 0.06      | 0.8165    |
| $X_2$  | 221.18 | 1  | 221.18 | 6.61      | 0.0369    |
| $X_3$  | 26.51 | 1  | 26.51  | 0.79      | 0.4029    |
| $X_1X_2$ | 196.93 | 1  | 196.93 | 5.89      | 0.0457    |
| $X_1X_3$ | 25.93  | 1  | 25.93  | 0.78      | 0.4078    |
| $X_2X_3$ | 56.99  | 1  | 56.99  | 1.70      | 0.2331    |
| $X_1^2$ | 2935.05 | 1  | 2935.05 | 87.74     | <0.0001   |
| $X_2^2$ | 189.85 | 1  | 189.85 | 5.68      | 0.0487    |
| $X_3^2$ | 23.24  | 1  | 23.24  | 0.69      | 0.4321    |

| $R^2$     | 0.9422 | Adeq. precision | 10.122 |
| $R^2_{adj}$ | 0.8679 | CV, %   | 7.11   |
| Pred. $R^2$ | 0.7208 | PRESS  | 1130.88 |
Figure 4: 2D contour plots and 3D response surface plots of the effects on relationships between independent variables and response value; ((a) and (b)) 2D contour and 3D plot of the interactions between extraction time and extraction temperature; ((c) and (d)) 2D contour and 3D plot of the interactions between extraction temperature and the ratio of liquid to material; ((e) and (f)) 2D contour and 3D plot of the interactions between extraction time and the ratio of liquid to material.
which influenced GY. It also shown that interaction between extraction temperature ($X_1$) and extraction time ($X_2$) was significant. Thus, the extraction temperature ($X_1$) was confirmed as the key condition affecting the GY.

### 3.7. Analysis of the Response Surface

The 2D contour plots and 3D response surface plots graphically represented the interactive effects of extraction temperature ($X_1$), extraction time ($X_2$), and solvent-material ratio ($X_3$) on GY. According to contour plots’ shapes produced by Design-Expert 8.0.6., response surface plots demonstrated whether the mutual interactions between the variables are significant or not, which were shown in Figure 4. Circular contour plot indicates that the interactions between the corresponding variables are negligible, while elliptical contour plot indicates that the interactions between the corresponding variables are significant [22]. As two variables were depicted in same plots while the other variable was kept at level 0, relationships between independent and dependent variables could be intuitively conveyed. Figures 4(b) and 4(d) showed the interaction relationships of extraction temperature ($X_1$) with the extraction time ($X_2$) and solvent-material ratio ($X_3$) on the yield of gentisides, respectively. The yield of gentisides increased rapidly with the increment of extraction temperature, while it declined rapidly with higher temperature after a critical value of 75°C. The yield of gentisides increased lightly along with extraction time extended (from 2 to 4 h) at extraction temperature lower than 80°C and even declined less obviously at extraction temperature higher than 80°C, which indicated that mutual interaction of extraction temperature and extraction time was significant on the increasing of the yields extraction. The response curves of extract variable $X_1$ in Figure 4(d) were smooth at all degree extraction temperatures indicating that solvent-material ratio was insignificant on the increasing of the yields extraction. In Figure 4(f), the response surface was smooth, which expressed that the mutual interaction of extraction time and solvent-material ratio had conspicuous significance on the extraction yield. Descriptions above were in general accord with data ($P < 0.05$) in Table 2.

3.8. Optimization of Extracting Parameters and Validation of the Model. A series of experiments were performed to obtain optimum conditions for independent variables and the predicted values of the responses by using Design-Expert 8.0.6 software. Optimal values of extraction parameters and maximum predicted yield of gentisides were given in Table 3 and also carried out as follows: extraction temperature of 73.33°C, extraction time of 3.40 h, solvent-material ratio of 10.21 mL/g, solvent concentration (ethanol) of 90%, and optimum predicted value of response of 99.24%, respectively. However, considering actual production, optimized solutions were modified slightly as follows: extraction temperature of 75°C, extraction time of 3.5 h, and solvent-material ratio of 10 mL/g. Under modified conditions, actual extraction yield was 98.61 ± 0.61%, which validated that the model was adequate for predicting the maximum extraction yield of gentisides.

### 4. Conclusions

This investigation in the successful uses of univariate test and Box-Behnken design forecasted optimal extracting parameters of gentisides (gentisides A, B, G, H, I, J, and K) from the root and rhizome of *G. rigescens*, which demonstrated that maximized gentisides yield of 99.24% could be achieved when solvent concentration of 90%, extraction temperature of 74.33°C, extraction time of 3.40 h, and solvent-material ratio of 10.21 mL/g were selected as extraction conditions. Considering feasible technical operations, solvent concentration of 90%, extraction temperature of 75°C, extraction time of 3.5 h, and solvent-material ratio of 10 mL/g were determined as final optimum extraction conditions.

### Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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