1. Introduction

Printed flexible electronics is one of the fastest-growing technologies in the world, which is of great significance to industries as diverse as healthcare, electronics, consumer goods and mobility. This technology is a direct additive deposition process to print the ink material onto various flexible substrates, which greatly simplifies the fabrication process of electronic devices. Besides, it offers a number of attractive new virtues to electronic products such as being wearable, flexible, bendable, more lightweight and even transparent.1,2 It is improving existing electronics by creating products with new features or replacing existing components with higher performance alternatives in a simpler, faster, more cost-effective and eco-friendly way.

Conductive inks play a central role for printed flexible electronics since they find application in a wide range of newly-emerged electronic and energy devices.3,4 Currently, a number of inks based on silver,5–9 copper,10–16 graphene,17–21 carbon,22,23 and conductive polymers,24–26 have been explored for printed flexible electronics. Among them, silver-based inks have been the favored metal inks because they are more cost-effective than Au-based metal inks, more stable than Cu-based inks and highly competitive ink for flexible printed electronics.41 This type of ink exists in a solution form so that problems...
such as nozzle clogging occurred in the printing process are avoided. In this regard, features with fine resolutions can be printed. After post-treatment, desired conductivity can be achieved on a wide range of flexible substrates.

Up to now, although much research on silver particle-free inks has been performed, there are still some drawbacks: (1) in some cases, the obtained ink is less stable and decomposes to silver particles over time such as silver carbonate ink and silver oxide ink. This is mostly due to the utilization of volatile solvents and ligands with weak reducibility. In other cases, the obtained ink has a lower sintering temperature in the range of 70–90 °C. These inks may not be suitable for a long-term inkjet printing process because it may lead to the formation of silver particles in the nozzle and clog it due to the quick decomposition of the ink. Also, due to the fast evaporation of the components in ink, the quality of silver films is usually decreased; (2) some of the synthetic methods of these inks are not economically feasible and not easy to make because of cost and safety concerns. For instance, the silver precursors for β-diketonate silver particle-free ink and silver(I) 2-[2-(2-methoxy-ethoxy)ethoxy]acetate ink are required a complex and time-consuming process to synthesize, and the precursor for silver hexafluoroacetylacetonate cyclooctadiene ink are expensive and need to be formulated in glove box due to the usage of toxic solvents and ligands with weak reducibility. In other cases, the silver acetate-based particle-free inks, formic acid and ethyamine are usually adopted. Both chemicals are not safe, especially the latter which has higher toxicity. Besides, a 12-aging time is required for such inks to avoid any particle formation when using the ink. Although some of the developed silver particle-free inks are cheap in terms of material cost, they are not easy to print due to the stability issue and unmatched fluid parameters required by a specific printer. (3) The influences of changes in fluid parameters on the printability of the formulated ink and the performance of the resultant film are rarely examined. Therefore, we see a certain need to develop a stable, low-cost and printable silver-particle-free ink using nontoxic solvents and simple synthetic procedure.

Sols are the majority of the silver particle-free ink. They have two functions; one is to increase the solubility of the silver precursor and the other is to provide the ink with essential fluid properties for printing. Selection of appropriate solvents, therefore, is important to the ink formulation. Alcohols with low boiling point and low molecular weight are by far the most popular choice since they have lower toxicity and less organic residues after post-treatment. Besides, some alcohols are reductive, which is conducive to the film formation. However, alcohols also have negative effects when using as the ink solvents.

Two phenomena often occur during the sintering/annealing/ drying of alcohol-based inks, the solvent shrinkage effect (Marangoni effect) and the coffee ring effect. The former will result in a film with a structure that has a thin edge and thick center, while the latter will produce a film that has a thick edge, thin center, or even no particulate at the center. Both phenomena seriously affect the electrical and mechanical performance of the sintered films or patterns, limiting the wide device applications of the inks. However, the two effects coexist and which one dominates depends on the physical properties of the solvent. Some solvents are dominated by the shrinkage effect such as water. Some are dominated by coffee ring effect such as ethanol, and for some solvents, the two phenomena are not obvious.

On the other hand, in order to achieve good printing on specific substrates, the ink should have certain fluid properties. These properties are also determined by the type of solvents selected. However, some alcohols, such as methanol, ethanol and isopropanol, have very low viscosity and contact angle, which spread rapidly on the glass and polymer substrates. Therefore, control of spreading is an issue to be solved. Besides, the volatility of these alcohols can cause printing issues such as causing the crystal precipitation in ink and clog the printhead. Moreover, these alcohols are prone to resulting in a non-uniform surface structure on the substrate after post-treatment, which should also be avoided. Therefore, it is necessary to study the solvent effects of the silver particle-free inks before formulating an ink that can be printed.

Currently, most research towards silver particle-free inks mainly concentrated on the enhancement of conductivity and adhesion of the resultant metal silver films, the decomposition mechanism of the metal–ligand complex and the effects of the ligand’s type on the ink properties and the morphology of the associated films. For solvent effects on silver particle-free ink, to our knowledge, no research reports.

In this work, a stable, transparent and printable silver particle-free ink was developed using a facile alcohol-based synthesis route. The fluid property, thermal property, stability and electrical performance of the inks based on different alcohols were investigated and characterized, where mixed alcohols with a proper ratio were chosen to obtain the final ink for printing. Conductive silver patterns with a flat surface and compact structure as well as high resolutions were printed on both flexible polymer and glass substrates successfully using industrial scale printheads. Additionally, we assessed the cost and performance of our ink.

2. Experimental section

2.1 Preparation of silver ink and film

Silver nitrate (AgNO₃), oxalic acid (H₂C₂O₄), sodium hydroxide (NaOH), 1,2-diamino propane (C₃H₆N₂, 1,2-DAP), ethanol (C₂H₅OH, EA), 2-methoxylethanol (C₃H₈O₂, 2-MEA), butanol (C₅H₁₂O, BA) and hexanol (C₆H₁₄O, HA) were purchased from Sigma-Aldrich. Methanol (CH₃OH, MA), 2-propanol (C₃H₇OH, IPA) and ethylene glycol (C₂H₂(0H)₂EG) were purchased from Honeywell and Roth respectively. All chemicals were used without further purification. Polyimide films (PI, 127 μm thick, obtained from DuPont) and glass were used as substrates. Before application, 15 mm × 15 mm of PI films and 25 mm × 25 mm of glass sheets were cleaned using deionized water and ethanol respectively and then dried.

The silver particle-free inks used in this study were prepared in alcohols using silver oxalate and 1,2-diaminopropane. The silver oxalate was prepared using the method described in our previous work. For ink preparation, 0.152 g of silver oxalate.
powder was first dispersed in 0.75 ml of alcohol and stirred for 5 minutes. Then, 0.172 ml of 1,2-diaminopropane amines was added. The mixture was stirred for 60 minutes to form the ink. To make a reasonable comparison, the weight of silver oxalate (0.152 g) was the same in each ink and the Ag/amine molar ratios were kept at a constant value of 1:2. The silver content in the ink was about 10 wt%. Here, we tried to load more silver in the ink but it has a solubility issue. This is because the silver oxalate is sparingly soluble in alcohol and needs amine to increase its solubility by forming a soluble silver–amine complex. If we want to increase the silver content in the ink, we also need to use more amines and solvents to ensure the solubility and printability.

The silver films or silver patterns on glass and PI substrates were obtained separately by spin coating (1000 rpm, 30 s) and drop-casting with a subsequent sintering process at selected temperatures for up to 60 minutes. Printing of the ink was conducted using a PixDro LP50 inkjet printer (SÜSS MicroTec) equipped with industrial-scale Fujifilm Dimatix Spectra SE128 piezoelectric printheads. The drops were generated by a single bias pulse with a voltage of 100 V and a pulse width of 10 μs. The jetting frequency was set to 1 kHz. Different resolutions in the range of 300 dpi to 1050 dpi were adopted to print the square films. The patterns and lines with different widths were printed in 750 dpi. Before printing, the ink was filtered with a PTFE filter (0.45 μm).

2.2 Characterization

The UV/vis absorption spectra were obtained on a Lambda 950 UV-vis spectrophotometer. DI water was used as the solvent. The surface tension and contact angle of each ink on the PI substrate were measured using a drop-shape analyzer (Krüss DSA100, Germany). The viscosity of inks was measured by using a Haake rotational viscometer. X-ray diffraction (XRD) analysis was conducted on a Bruker D8 Advance X-ray diffractometer with a Cu Kα1 radiation (λ = 0.15406 nm). The diffraction patterns were collected at 25 °C and over a range of 20° to 90°. The thermal behaviors of the inks were investigated with a differential scanning calorimeter (Netzsch DSC 204 F1) and a thermogravimetric analyzer (Netzsch TG 209 F1) at a heating rate of 10 °C min⁻¹ under an argon atmosphere and a nitrogen atmosphere, respectively. Aluminum pans with pierced lids were used to load the inks. The gas outlet of the thermogravimetric analyzer was directly coupled with a mass spectrometer (Netzsch QMS 403C) to monitor the gaseous products evolved during heating. The surface morphologies and chemical composition of the obtained silver films were observed via a scanning electron microscope (HTACH S-4100) and a surface energy disperse spectrometer (EDX). The sheet resistivity was measured using a 4 point probe system (Jandel Engineering). The average thickness of the film was measured by SEM to calculate its resistivity.

3. Results and discussion

3.1 Ink design, synthesis and characterization

The properties of the silver particle-free ink vary primarily with the type of silver precursor, the ligand and the solvent used to solubilize them. The key point in formulating an ideal ink, therefore, lies in the careful selection of these components.

Silver oxalate was chosen as the core of our ink because it has a high silver content (71 wt%), a simple synthetic process and easily decomposes to silver without leaving organic residues. 1,2-Diaminopropane, a bi-dentate aliphatic amine with a boiling point of 119 °C was used as the ligand for silver oxalate. Five types of alcohols with small molecular weight were selected as the ink solvents respectively because they are less toxic and easily available.

Silver particle-free inks were prepared by simply dissolving the synthesized white silver oxalate powder into the different alcohols using 1,2-diaminopropane (1,2-DAP) as the ligand (Fig. 1a). The silver oxalate was produced through the reaction of sodium oxalate and silver nitrate directly. As expected, sparingly soluble silver oxalate powder gradually dissolved in each alcohol containing 1,2-DAP, mainly via the complexing process proposed in Fig. 1b, resulting in a transparent ink. Compared to the synthetic methods of inks based on β-diketone silver or silver(1) 2-[2-(2-methoxyethoxy)ethoxy]acetate or silver hexafluoroacetacetonate cyclooctadiene, our one-pot approach is easy to handle and the process is facile, quick and cost-effective. In comparison with inks based on silver acetate, we don’t require an overnight aging time of 12 hours to let the produced particle settle and the utilization of pungent formic acid and toxic ethyamine are avoided, which is relatively safe. In other words, a facile synthesis route was developed by simply mixing the selected chemicals together to make your own silver particle-free conductive ink.

Here, it should be noted that the dissolution rate of silver oxalate powder varies with the selected alcohols containing 1,2-DAP. The powder dissolved within 5 minutes in methanol (MA), 2-methoxyethanol (2-ME) and ethylene glycol (EG) inks. However, in the solvent of ethanol and 2-propanol, the dissolvable rate was slow and more time was necessary, especially for the 2-propanol. The dissolution behavior of the silver oxalate powder in butanol and hexanol containing 1,2-DAP was also observed. Both inks showed slow dissolution rate and precipitation occurs over time (see Fig. S1 in ESI†).

To realize the printing on specific substrates, the ink should have certain fluid properties compatible with the utilized printhead. These properties relate to viscosity, surface tension, evaporation rate and wettability with the substrate, which are...
determined by the solvents used. Considering this, the fluid parameters of the five silver inks were investigated to check the printability of each ink; the results are listed in Table 1. The surface tension and contact angle images are given in Fig. S2 in ESI†.

As seen, the ink from ethylene glycol has higher surface tension and viscosity in the five types of inks, with a value of 47.88 mN m⁻¹ and 16.62 mPa s, respectively. On the contrary, the ink from methanol has a lower value, especially in the viscosity (0.758 mPa s). For printing, an ink with high surface tension helps to suppress the formation of satellite droplets and increase the printing velocity, thereby resulting in a good print quality.57 The typical values for industrial printheads are in the range of 25–35 mN m⁻¹. As for viscosity, a low value is easier to print with an inkjet head. However, it should be compatible with the printhead. For piezoelectric printheads, the value should be in the range of 8–15 mPa s. From Table 1, it can be seen that the viscosity values of the five inks are all out of this range.

In terms of volatility, ethylene glycol has a high boiling point of 197.6 °C, followed by 2-ME. The remaining three are all volatile, which might lead to nozzle clogging which is one of the most common failure modes of drop-on-demand inkjet printers. In the aspect of wettability, the methanol ink spreads strongly on the PI substrate and a contact angle of 15.72° is measured. For printing fine features on hydrophobic substrates such as glass or polymer films, a large contact angle may be beneficial to achieve patterns with high resolutions. Especially ethylene glycol ink has a relatively large contact angle of 40.33°, which would contribute to the well-defined printed structures and reliable adhesion on the substrate.

The dimensionless number Z, the inverse of the Ohnesorge number, is often used to predict whether a liquid can be printed. It is defined as the ratio between the Reynolds number and a square root of the Weber number, as shown below,

\[ Z = \frac{N_{Re}}{(N_{we})^{1/2}} = \frac{(\gamma \rho)}{\eta} \]

where \( \gamma \), \( \rho \) and \( \eta \) are the surface tension, the density and the viscosity of the liquid, respectively, and \( z \) is the diameter of the nozzle (in our case 35 μm). According to Jang et al., the liquid with a Z value in the range from 4 to 14 can be used for inkjet printing.58 Based on the measured fluid parameters, the Z values of the five inks were calculated and listed in Table 1. Only the ink from IPA may be suitable for printing.

Apart from the fluid properties, we also investigated the stability, thermal property, and electrical performance of the as-prepared five silver inks, see Section S1 in ESI† from Fig. S3–S7 (ESI†). The results show that the solvent type has little effect on the thermal behaviour of the ink but mainly affects the morphology and electrical performance of the associated films. Each ink has its advantages and disadvantages either in the fluid properties or in the stability and electrical performance. To get a balance between these properties, we targeted a mixture of solvents as the ideal choice for an optimal ink, which can not only provide the essential fluid properties for the inkjet printing but also can result in highly conductive films with good quality at low temperature.

### 3.2 Film structure from inks based on mixed alcohol solvents

In Section 3.1, we investigated the structural and electrical properties of the films produced from the five silver inks (see ESI† Fig. S5 and S6). Together with the stability and the fluid properties of each ink, we found that the ink from methanol (MA) has better stability and uniform surface structure as well as lower resistivity but shows the obvious coffee-ring effect and non-ideal fluid properties such as fast evaporation rate and stronger wetting behavior; the ink from ethylene glycol (EG) has a structure consisting of big silver crystals and good fluid properties for print quality but the film has a higher resistivity. After consideration, a mixture of these two solvents was selected as the ink solvent. Inks with different MA/EG ratios that are varied from 0:5 to 5:0 were formulated and characterized.

In terms of fluid properties, the inks in 4:1 and 3:2 spread easily on the glass substrates, showing good wettability and flowability. The sintered films from these two inks are slightly yellow, and the film from the ink in 4:1 shows a coffee-ring effect. For the inks in 1:4 and 2:3, they flow and evaporate slowly, and cannot cover the whole glass after sintering at 150 °C, and the resultant films are dark yellow. With a mixed solvent in a proper MA/EG ratio, the fluid properties required by a printer and the film morphology could be guaranteed.

XRD, SEM and four-probe analyses were employed to investigate the physical phase, morphology and resistivity of the resultant films to determine the optimal mixing ratio; the results are given in Fig. 2. Clearly, the X-ray diffraction patterns of all the films exhibit a crystalline silver structure (JCPDS card no. 04-0783, Fig. 2a), indicating that the silver-amine complex in each ink has been transformed into metallic silver. Small peaks relative to the PI substrates were also observed, which indicates that the films are thin. As the MA concentration increases, the intensity of the (111) diffraction peak reaches its maximum at 3:2, meaning an increased crystallization of the silver particles in the film.

Fig. 2b shows the corresponding surface morphology of the silver films on PI substrates (the SEM images on glass substrates
were given in Fig. S8a and b in ESI†. As seen, the film quality is significantly improved with the increase of the MA concentration, with a surface change from loose to dense. The surface morphology of the film from inks with MA/EG in 1:4, 2:3 and 1:1 revealed a microstructure that was composed of silver particles with big and small sizes, where the latter was covered on the top of the former. Meanwhile, these films all have varying degrees of solvent shrinkage effect in appearance and the ink in 1:4 is most serious. By contrast, the film from the ink in 3:2 and 4:1 presented a microstructure that was composed of hollow silver nanoparticles in a good connection. The film produced from the 4:1 ink shows an obvious coffee-ring effect in appearance with a smooth part and roughness part. These microstructure differences are associated with the physical characteristics of the MA and EG.

The resistivity data is given in Fig. 3. As the MA content increases, the resistivity of the silver film decreases drastically. This can be easily understood. When the MA/EG is 1:4, the MA content is small, the viscosity of the ink is large, mass transfer is hindered during the sintering, and silver ions cannot be completely reduced and the EG cannot be completely volatile, thereby making the resistivity relatively high. On the contrary, when the MA/EG is 4:1, the EG content is relatively small, the reduction of silver ions is complete and there are fewer organic residues left in the produced films, thereby resulting in a lower resistivity. Here, considering that the fast evaporation of MA will not be beneficial to the printing, we chose 3:2 as the optimal ratio to formulate the ink for the later printing.

The surface tension, the contact angle and the density of the optimal ink (MA/EG 3:2) were measured to be 31.09 mN m⁻¹, 27.9° and 1.02 g cm⁻³, respectively. The viscosity is about 8–9 mPa s. These values are within the range of fluid parameters required by a piezoelectric printer, indicating that the ink can be printed.

3.3 Stability and conductivity of the optimal silver ink
Stability is always an important concern for ink performance. For silver particle-free ink, there’s a possibility that its components could react with each other over time, leading to the formation of silver particles, precipitation and phase separation, which is not good for long shelf-life and printing. This is especially true when the inks contain reductive components such as reducible alcohols or amines or formic acid. In our case, the inks with different
MA/EG ratios were found to be visually and chemically stable over time. After storing in a fridge at 5 °C for 60 days, all of them are still transparent without color change and particle precipitation (Fig. 4a), indicating good shelf life.

The electrical performance of the optimal silver ink as a function of sintering time and the temperature was studied and the results are given in Fig. 4b. It can be seen that the resistivity is largely independent of sintering temperature above 180 °C and the sintering time is more than 30 minutes, with a value (15.46 \( \mu \Omega \text{cm} \)) equivalent to 10 times of bulk silver (1.59 \( \mu \Omega \text{cm} \)). Although this value is higher than that of bulk silver, it can meet the electrical requirements of most electronic products. As for the reason, it might be associated with the low content of silver in the ink and the sintering parameters as well as the degree of organic residues from EG. We tried to sinter the ink at 100 °C for 2 to 3 hours. However, due to the inadequate evaporation and decomposition of EG (bp = 197 °C), a resistivity close to 15.46 \( \mu \Omega \text{cm} \) cannot be achieved.

The cross-section images show that the thickness of the film decreases with the increase of the sintering temperature (Fig. 4c-e), indicating that more solvents have evaporated. After sintering at a temperature in the range of 180–200 °C for 5 or 30 minutes, the average thickness of the silver film shows a stable 370–380 nm.

Here, we also performed the printing experiment with an ink stored at 5 °C for more than 90 days to check its stability. The printing process is still smooth without any crystal precipitation or particle formation issues, further confirming the good stability of the ink. We also investigated the resistivity of the films from the ink stored at 5 °C for 90 days, which is about 15.72 \( \mu \Omega \text{cm} \), a slight change, indicating the stability of the printed film.

### 3.4 Printability of the optimal silver ink

The printing of the optimal ink was conducted using a PixDro LP50 inkjet printer, using Spectra S-class printheads. The drop images of the ink at different times after the ejection from the printhead are given in Fig. 5a. After 60 \( \mu \text{s} \), the drop is still connected with the nozzle via a filament. At a time of 80 \( \mu \text{s} \), the drop detaches from the nozzle, and the filament flows into the main drop. After 120 \( \mu \text{s} \), a spherical drop is obtained, which is free from a satellite drop or a filament, meaning good printability.

As expected, squares in 20 mm × 20 mm were printed smoothly on glass substrates. Based on the results of Section 3.3, we chose 200 °C to sinter the square films printed with different resolutions in the range of 300 dpi to 1050 dpi. SEM and four-probe analyses were used to investigate the effect of resolution on the film morphology, thickness and resistivity, see Fig. 5b and Fig. S10 (in ESI†). The films printed with 300 dpi and 450 dpi have a discontinuous morphology, where the number of silver particles is small and the interconnections between them are poor. The films printed using a resolution of 600 dpi and 750 dpi show good quality with uniform morphology. When higher resolution such as 900 or 1050 dpi was used, the morphology of the film is less uniform. The cross-section images of the printed square films show that the film thickness increases with the increase of the printing resolution, and there is a drastic increase when the resolution is 1050 dpi. The film achieved in 750 dpi shows the best quality and the lowest resistivity of 15.28 \( \mu \Omega \text{cm} \). As for the reason, it is associated with the particle numbers generated in the film and the amount of the organic residues. The higher the resolution, the more ink dots per inch that the printer deposits. Therefore, to the squares with the same size, a higher resolution will bring more organic residues in the films and the silver ions cannot be transformed to silver in full amount under the same sintering time, resulting in a high resistivity. However, there is an optimal value, where the numbers of particles are just right which can produce a continuous film.
3.5 Cost and performance assessment

Apart from the excellent electrical performance and favorable processability, cost is also a key factor to be considered for optimal inks, which should be as low as possible to serve low-cost printed electronics. We made a comparison of the developed silver particle-free inks in terms of type, cost (materials consumption), advantages and disadvantages respectively, see Table S1 in ESI†.

As shown in Table S1 (ESI†), the reported silver particle-free inks are not expensive and have a silver loading in the range of 10–25%. A temperature around 150 °C is usually required to achieve a low resistivity in the order of $10^{-6}$ Ω cm. These inks are compatible with most of the temperature-sensitive flexible substrates, which is a key advantage over nanoparticle silver inks. Even so, some of these inks are less stable and have sediment over time, while others decompose quickly and are not suitable for a long-term inkjet printing process, despite these inks possessed the best conductivity. Besides, an ink with multiple ingredients could decrease the quality of the silver film due to the decomposition and evaporation of these components. Moreover, in most cases, the detailed printing information such as printing parameters, printing quality and the smallest line width are not provided. From Table S1 (ESI†), it can be seen that our ink has a simple synthetic route, low cost, excellent printability and favorable conductivity. Further study will be focused on the conductivity and adhesion improvement on flexible substrates.

4. Conclusions

In summary, a stable, cheap and printable silver-particle free ink was formulated and characterized by using selected alcohols as the solvents. It was found that the alcohol type mainly affects the fluid properties of the ink, the morphology and electrical performance of the associated films. A mixture of solvents was a good choice, which not only provides the essential fluid properties for the inkjet printing but also results in highly conductive films with good quality. The obtained ink showed long-lasting stability without the occurrence of turbidity at lower temperatures (5 °C). It also exhibited compatibility with the inkjet printing technique. The printed Ag features yielded favorable conductivities (15.46 μΩ cm), about 10 times of bulk silver after annealing at 180 °C. The research offers a low-cost, reliable and highly demanding material for flexible printed electronics, which can be made easily following a simple recipe.

Conflicts of interest

All authors declare that they have no conflict of interest.

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References

1 M. A. Leenen, V. Arning, H. Thiem, J. Steiger and R. Anselmann, Phys. Status Solidi A, 2009, 206, 588–597.
2 W. Li, Q. Sun, L. Li, J. Jiu, X.-Y. Liu, M. Kanehara, T. Minari and K. Suganuma, Appl. Mater. Today, 2020, 18, 100451.
3 Q. Huang and Y. Zhu, Adv. Mater. Technol., 2019, 4, 1800546.
4 W. Wu, Nanoscale, 2017, 9, 7342–7372.
5 A. Kosmala, R. Wright, Q. Zhang and P. Kirby, Mater. Chem. Phys., 2011, 129, 1075–1080.
6 K. R. Zope, D. Cormier and S. A. Williams, ACS Appl. Mater. Interfaces, 2018, 10, 3830–3837.
7 W. Yang, C. Wang and V. Arrighi, J. Electron. Mater., 2018, 47, 2824–2835.
8 M. Vaseem, G. McKerricher and A. Shamim, ACS Appl. Mater. Interfaces, 2016, 8, 177–186.
9 S. B. Walker and J. A. Lewis, J. Am. Chem. Soc., 2012, 134, 1419–1421.
10 T. Araki, T. Sugahara, J. Jiu, S. Nagao, M. Nogi, H. Koga, H. Uchida, K. Shinozaki and K. Suganuma, Langmuir, 2013, 29, 11192–11197.
11 D. Deng, T. Qi, Y. Cheng, Y. Jin and F. Xiao, J. Mater. Sci.: Mater. Electron., 2014, 25, 395–397.
12 Y. Dong, Z. Lin, X. Li, Q. Zhu, J.-G. Li and X. Sun, J. Mater. Chem. C, 2018, 6, 6406–6415.
13 Y. Farraj, M. Groucho and S. Magdassi, Chem. Commun., 2015, 51, 1587–1590.
14 N. N. Jason, W. Shen and W. Cheng, ACS Appl. Mater. Interfaces, 2015, 7, 16760–16766.
15 D.-H. Shin, S. Woo, H. Yem, M. Cha, S. Cho, M. Kang, S. Jeong, Y. Kim, K. Kang and Y. Piao, ACS Appl. Mater. Interfaces, 2014, 6, 3312–3319.
16 F. Hermerschmidt, D. Burmeister, G. Ligorio, S. M. Pozov, R. Ward, S. A. Choulis and E. J. List-Kratchivil, Adv. Mater. Technol., 2018, 3, 1800146.
17 A. Al Shboul, C. Trudeau, S. Cloutier, M. Siaj and J. Claverie, Nanoscale, 2017, 9, 9893–9901.
18 C.-L. Lee, C.-H. Chen and C.-W. Chen, Chem. Eng. J., 2018, 230, 296–302.
19 D. Sinar, G. K. Knopf and S. Nikumb, Proc. SPIE, 2013, 8612, 861204.
20 T. S. Tran, N. K. Dutta and N. R. Choudhury, Adv. Colloid Interface Sci., 2018, 261, 41–61.
21 W. Yang and C. Wang, J. Mater. Chem. C, 2016, 4, 7193–7207.
22 S. H. Chae and Y. H. Lee, Nano Convergence, 2014, 1, 15.
23 J.-W. Han, B. Kim, J. Li and M. Meyyappan, Mater. Res. Bull., 2014, 50, 249–253.
24 N. Perinka, C. H. Kim, M. Kaplanova and Y. Bonnassieux, Phys. Procedia, 2013, 44, 120–129.
25 R. Brooke, D. Evans, M. Dienel, P. Hojati-Talemi, P. Murphy and M. Fabretto, J. Mater. Chem. C, 2013, 1, 3353–3358.
26 A. Chioleroi, S. Bocchini, F. Scaravaggi, S. Porro, D. Perrone, D. Beretta, M. Caironi and C. F. Pirri, Semicond. Sci. Technol., 2015, 30, 10.
27 C. N. Chen, C. P. Chen, T. Y. Dong, T. C. Chang, M. C. Chen, H. T. Chen and I. G. Chen, Acta Mater., 2012, 60, 5914–5924.
28 S. Magdassi, M. Groucho, O. Berezin and A. Kamysnhy, ACS Nano, 2010, 4, 1943–1948.
29 S. Jeong, H. C. Song, W. W. Lee, Y. Choi, S. S. Lee and B.-H. Ryu, J. Phys. Chem. C, 2010, 114, 22277–22283.
30 R. Shankar, L. Groven, A. Amert, K. W. Whites and J. J. Kellar, J. Mater. Chem. C, 2011, 21, 10871–10877.
31 D. J. Finn, M. Lotya and J. N. Coleman, ACS Appl. Mater. Interfaces, 2015, 7, 9254–9261.
32 H. Lu, J. Lin, N. Wu, S. Nie, Q. Luo, C.-Q. Ma and Z. Cui, Appl. Phys. Lett., 2015, 106, 093302.
33 Q. Huang, K. N. Al-Milaji and H. Zhao, ACS Appl. Nano Mater, 2018, 1, 4528–4536.
34 J. Liang, K. Tong and Q. Pei, Adv. Mater., 2016, 28, 5986–5996.
35 W. J. Scheideler, J. Smith, I. Deckman, S. Chung, A. C. Arias and V. Subramanian, J. Mater. Chem. C, 2016, 4, 3248–3255.
36 O. Huang and Y. Zhu, Sci. Rep., 2018, 8, 1–10.
37 S. F. Jahn, T. Blaudeck, R. R. Baumann, A. Jakob, P. Ecorchard, T. Rüffer, H. Lang and P. Schmidt, Chem. Mater., 2010, 22, 3067–3071.
38 A. J. Kell, C. Paquet, O. Mozeno, I. Dijavani-Tabarzii, B. Deore, X. Y. Liu, G. P. Lopinski, R. James, K. Hettak, J. Shaker, A. Momciu, J. Ferrigno, O. Ferrand, J. X. Hu, S. Lafreniere and P. R. L. Malenfant, ACS Appl. Mater. Interfaces, 2017, 9, 17227–17238.
39 X. Nie, H. Wang and J. Zou, Appl. Surf. Sci., 2012, 261, 554–560.
40 Y. Chang, D.-Y. Wang, Y.-L. Tai and Z.-G. Yang, J. Mater. Chem., 2012, 22, 25296–25301.
41 W. Yang, E. J. W. List-Kratchivil and C. Wang, J. Mater. Chem. C, 2019, 7, 15098–15117.
42 Y. Dong, X. D. Li, S. H. Liu, Q. Zhu, M. Zhang, J. G. Li and X. D. Sun, Thin Solid Films, 2016, 616, 635–642.
43 S. P. Chen, Z. K. Kao, J. L. Lin and Y. C. Liao, ACS Appl. Mater. Interfaces, 2012, 4, 7063–7067.
44 Y. Mou, Y. Zhang, H. Cheng, Y. Peng and M. Chen, Appl. Surf. Sci., 2018, 459, 249–256.
45 S. P. Chen, Z. K. Kao, J. L. Lin and Y. C. Liao, ACS Appl. Mater. Interfaces, 2012, 4, 7063–7067.
46 M. Vaseem, G. McKerricher and A. Shamim, ACS Appl. Mater. Interfaces, 2016, 8, 177–186.
47 C.-N. Chen, T.-Y. Dong, T.-C. Chang, M.-C. Chen, H.-L. Tsai and W.-S. Hwang, J. Mater. Chem. C, 2013, 1, 5161–5168.
48 K. Black, J. Singh, D. Mehta, S. Sung, C. J. Sutcliffe and P. R. Chalker, Sci. Rep., 2016, 6, 7.
49 K. S. Bhat, R. Ahmad, Y. Wang and Y. B. Hahn, J. Mater. Chem. C, 2016, 4, 8522–8527.
50 H. Hu and R. G. Larson, J. Phys. Chem. B, 2006, 110, 7090–7094.
51 W.-D. Yang, C.-Y. Liu, Z.-Y. Zhang, Y. Liu and S.-D. Nie, J. Mater. Chem. C, 2012, 22, 23012–23016.
52 R. D. Deegan, O. Bakajin, T. F. Dupont, G. Huber, S. R. Nagel and T. A. Witten, Nature, 1997, 389, 827–829.
53 E. Tekin, B.-J. de Gans and U. S. Schubert, *J. Mater. Chem.*, 2004, **14**, 2627–2632.
54 F. Girard, M. Antoni and K. Sefiane, *Langmuir*, 2008, **24**, 9207–9210.
55 P. J. Smith and D. H. Shin, *Inkjet-based micromanufacturing*, John Wiley & Sons, 2012.
56 F. Mathies, E. J. List-Kratochvil and E. L. Unger, *Energy Technol.*, 2020, **8**, 1900991.
57 B. He, S. Yang, Z. Qin, B. Wen and C. Zhang, *Sci. Rep.*, 2017, **7**, 1–7.
58 D. Jang, D. Kim and J. Moon, *Langmuir*, 2009, **25**, 2629–2635.
59 W.-d. Yang, C.-h. Wang, V. Arrighi, C.-y. Liu and D. Watson, *J. Mater. Sci.: Mater. Electron.*, 2015, **26**, 8973–8982.