Determination of Reference Values of Complex Fuel and Ecological Criterion as the Separate Independent Factor of Ecological Safety

In this study the approach and method on its basis for calculated assessment of reference values of complex fuel-ecological criterion of Prof. I. Parsadanov as separate independent ecological safety factor and as reference points of psychophysical scale of the partial desirability function when using it as the ecological safety factor of power plants with reciprocating internal combustion engines exploitation process was proposed. Also in the study calculated assessment of reference values of ecological indicators of reciprocating internal combustion engines as components of complex fuel-ecological criterion depending on magnitudes of effective power and coordinates of field of engine operating regimes for different levels of statutory ecological standards in force in Ukraine and previously in force was carried out. Thus, calculated assessment of reference values of complex fuel-ecological criterion and its components was performed and obtained the distribution of such reference values in field of 2Ch10.5/12 autotactor diesel engine operating regimes depending as well as dependences of such reference values on magnitudes of level of ecological standards EURO, engine effective performance and lower calorific value of engine fuel. So, the study for the first time proposes the approach to calculated assessment of reference values of the complex fuel-ecological criterion of Prof. I. Parsadanov as reference points of the psychophysical scale of the Harrington's partial desirability function when using it as the separate independent ecological safety factor of exploitation process of power plants with reciprocating ICE. The method, based on the proposed approach for calculative evaluation of reference values of the complex fuel-ecological criterion of Prof. I. Parsadanov as reference points of psychophysical scale of partial desirability function is suitable for obtaining necessary data for the complex criterion evaluation of the ecological safety level of operation process of power units with piston ICE using generalized Harrington desirability function, in the structure of which the complex fuel-ecological criterion acts as a distinct factor of environmental safety.

Key words: environment protection technologies; ecological safety; power plants; internal combustion engines; reference values; criteria-based assessment; EURO level.

Relevance of the study and problem statement

The relevance of the research presented in this study is due to the following. In the monograph [1] the analysis of 9 known mathematical apparatuses suitable for the implementation of complex calculated assessment of the level of ecological safety (ES) of the process of accident-free exploitation of power plants (PP) with reciprocating internal combustion engine (RICE). According to the results of analysis and systematization in the form of the corresponding classification it is established that the most suitable for achievement of the formulated purpose it is possible to accept the mathematical apparatus of complex fuel-ecological criterion of Prof. I. Parsadanov (NTU “KhPI”) \(K_E\) (described in the monograph [2]) and the Harrington generalized desirability function \(D\) (described in the work [3]). In the same source, a comparative analysis of the advantages and disadvantages of selected alternative criterion mathematical apparatuses is carried out and it is concluded that it is rational for further research to use both apparatuses with mutual strengthening of their advantages and weakening of disadvantages.

The first step in this way is to use the mathematical apparatus of the generalized desirability function with the structure of the considered influencing factors, identical to the complex fuel-ecological criterion. Since the main advantage of the \(K_E\) criterion is taking into account the mass hourly fuel consumption of RICE \(G_{fuel}\), then to use this advantage it is necessary to determine the ponderability of this ES factor in comparison with others — emissions of pollutants with exhaust gas (EG) flow \(G(k)\), which is done in the monograph [1], that also provides the improved classification of ES factors, the source of which is RICE in PP, which consists of 15 points, and also reveals the nature of the influence of the value \(G_{fuel}\) for all other ES factors in the specified classification. Therefore, given that the fuel component of the \(K_E\) criterion completely determines its ecological component, as established in the monograph [1], it is rational to explore the features of the application of another approach, namely the use of the \(K_E\) criterion as a separate independent influencing factor in the structure of the generalized desirability function \(D\). At the same time it becomes possible to consider indicators of vibration (degree of non-uniformity of rotation of crankshaft \(\phi_{cr}\), Klimov-Stechkin criteria \(\xi_a\) and \(\eta_a\), noise (equivalent \(L_{equiv}\) and maximum \(L_{max}\) noise level), thermal pollution (mass hourly fuel consumption \(G_{fuel}\) separately from the fuel component of the criterion \(K_E\), emissions of sulfur oxides \(G(SO_2)\), etc.

To implement this approach, it is necessary to have data on the magnitudes of such ES factor (i.e. the response of the local quality criterion \(r\), which can be correlated with the reference points of the psychophysical scale of desirability of magnitudes of the response \(r\) “good” and “bad”, and their corresponding magnitudes of the scale of values of basic assessment of the...
мagnitudes of the partial desirability function $d = 0.63...0.80$ and $d = 0.2...0.32$. Thus for reference values of indicators of ecological component of $K_{fe}$ criterion it is proposed to choose the emission magnitudes of legislatively normalized pollutants contained in the relevant standards (for example in [4,5]), for the current (mark of “good” and $d = 0.80$) and previous (mark “bad” and $d = 0.20$) levels of EURO.

However, different units of RICE, which are currently in operation, belong to different generations of such equipment and are in different current technical condition (corresponding to the degree of physical wear and compliance with the order of routine maintenance and repair) and therefore are characterized by different levels of fuel efficiency, i.e. the magnitude of RICE specific effective mass hourly fuel consumption $g_{fe}$. Therefore it is necessary to receive dependences of magnitude of $K_{fe}$ criterion, in the structure of which the indicators of ecological component acquire legislatively established magnitudes, from the magnitude of fuel component of the criterion for different levels of EURO standards. However, when analyzing the scientific and technical literature, authors did not find the results of such a study, so obtaining the set of magnitudes of the $K_{fe}$ criterion, which can be correlated with the reference points of the scale of the partial desirability function $d$, is a topical scientific and technical challenge with signs of scientific novelty and practical value.

It should be noted that RICE is a powerful source of environmental pollution by various physical factors, including non-renewable energy sources (engine fuel of petroleum origin) – this is a qualitative aspect of the relevance of topic of this study, they together produce up to 75 % of energy (mechanical and electrical) in our country [2] – this is a quantitative aspect of the relevance of topic of this study.

**Purpose of the study** is to determine the reference values of the complex fuel-ecological criterion of Prof. I. Parsadanov as the separate independent ES factor and as reference points of the psychophysical scale of the partial desirability function. **The task of the study** is to determine the necessary characteristics of the complex fuel-ecological criterion as the separate independent ES factor and as partial desirability functions for a complex assessment of the ES level exploitation process of PP with RICE based on the mathematical apparatus of the Harrington generalized desirability function. **Object of the study** is the quantitative characteristics of the fuel-ecological criterion as the separate independent ES factor. **Subject of the study** are the magnitudes of the reference values of the fuel-ecological criterion as a separate independent ES factor for different levels of legislatively established ecologi-
unique and universal indicator of the quality of the object under study, and is also characterized by adequacy and statistical sensitivity. The magnitude of generalized desirability function $D$ for the $i$-th representative operating regime of RICE in the model of its operation, in the structure of which as separate independent influencing ES factor there is complex fuel-ecological criterion $K_{fe}$, determined by the formula (1).

$$D_i = \sum_{k=1}^{n} d_{ki}^r = \left[ \sum_{k=1}^{n} \frac{1}{\gamma_1} \left( k_i - d_{ki}^r \right)^{\gamma_1} \right]$$

where $d_{ki}$ – partial desirability function that meets the $k$-th quality criterion, $d_{ki} = 0…1.0$, and $k_i = K_{fe}$; $n$ – number of quality criteria considered; $\gamma_1$ – weight factor of the $k$-th quality criterion considered, $0 < \gamma_1 \leq 1$, and $\gamma_1 = 38.4 + 245.3 = 283.7$ (see source [1]).

The mathematical apparatus of this function provides transformation of magnitudes of responses of local criteria of quality $r_i$ in the dimensionless scale of desirability – magnitudes of partial desirability functions $d_{ki}$ – according to the table of base mark of desirability scale, that is Table 1, which also contains a psychophysical scale [3].

| Mark of desirability of the response magnitude $r_{ki}$ | Quantitative magnitude according to the desirability scale $d_{ki}$ |
|--------------------------------------------------------|-------------------------------------------------|
| Very good                                              | $1.0 \ldots 0.8$                                 |
| Good                                                   | $0.8 \ldots 0.63$                                |
| Satisfactory                                           | $0.63 \ldots 0.37$                               |
| Bad                                                    | $0.37 \ldots 0.2$                                |
| Very bad                                               | $0.2 \ldots 0.0$                                 |

In this study as partial functions of desirability $d_{ki}$ or those that meet, firstly, the fuel-ecological criterion $K_{fe}$ (marked with index $k_1$ in the formula (1)), and secondly, the values that could potentially be indicators of other ES factors, included in the improved classification in the source [1], which, however, are not taken into account by the mathematical apparatus of the $K_{fe}$ criterion (that is, all but the mass hourly emissions of legislatively normalized pollutants – $G$(PM), $G$(NO$_x$), $G$(CO), $G$(C$_n$H$_m$), as well as indirectly – the mass hourly fuel consumption of diesel engine $G_{\text{fuel}}$, namely indicators of noise (equivalent $L_{\text{Aeq}}$ and maximum $L_{\text{max}}$ noise level), vibration (the degree of uneven rotation of the crankshaft $\delta_{\text{cr}}$, Klimov-Stechkin criteria $\xi_{\text{cr}}$ and $\eta_{\text{cr}}$), thermal pollution (mass hourly fuel consumption $G_{\text{fuel}}$), emissions of sulfur oxides $G$(SO$_x$) etc indicated by indexes $k_2 \ldots k_6$ in the formula (1)). ES factor in the structure of the desirability function $D$, criterion $K_{fe}$ is chosen as the main one, is a case of a real one-sided constraint and is described by the formula (2).

$$d_{ki} = \exp\left[\exp(d_{ki} + b_{ki} \cdot r_{ki})\right]$$

where $r_{ki}$ – actual magnitude of $k$-th quality criterion on the $i$-th representative regime of RICE operation in the model of its operation; $a_{ki}$ and $b_{ki}$ – coefficients determined on the basis of establishing correspondence between a pair of characteristic magnitudes $r_{ki}$ and $d_{ki}$ according to Table 1.

Data that allows to determine the parameters of compounds of formulas (2) for the partial desirability functions $d_{ki}$ are obtained by solving of system of two equations (see formulas (3) – (5)) for cases that put in accordance with one characteristic magnitudes $r_{ki}$ and $d_{ki}$, known from practice or normative documents.

$$\begin{cases}
    d_{kidn} = \exp[-\exp(a_{ki} + b_{ki} \cdot r_{kidn})] \\
    d_{kipup} = \exp[-\exp(a_{ki} + b_{ki} \cdot r_{kipup})]
\end{cases}$$

$$d_k = \frac{\ln(-\ln(d_{kipup})) \cdot r_{ldn} - \ln(-\ln(d_{kidn})) \cdot r_{kipup}}{r_{ldn} - r_{kipup}}$$

$$b_k = \frac{\ln(-\ln(d_{ldn})) - \ln(-\ln(d_{kipup}))}{r_{ldn} - r_{kipup}}$$

where indices $up$ and $dn$ marked characteristic magnitudes of $r_{ki}$ and $d_{ki}$, corresponding to the assessed marks on psychophysical scale “good” (i.e. $d_{kipup} = 0.63 \ldots 0.80$) and “bad” (i.e. $d_{kidn} = 0.20 \ldots 0.32$) taking into account the specific features of the quantities $r_{ki}$.

The essence of the proposed method is that as magnitudes of $r_{kipup}$ will be used the individual regime magnitudes of the $K_{fe}$ criterion (see formula (6)), the factors of the ecological component of which $(G$(PM), $G$(NO$_x$), $G$(CO), $G$(C$_n$H$_m$)) meet current legal standards (i.e. the level of EURO VI, the most stringent in terms of historical retrospect), and as magnitudes of $r_{kidn}$ – value of the $K_{fe}$ criterion, the factors of ecological component of which correspond to less rigid in terms of historical retrospect standards (i.e. levels of EURO I...VI). Such requirements in historical retrospect are summarized in Table 2.

$$K_{fei} = \frac{3600 \cdot N}{H_{\text{a}} \cdot G_{\text{fuel}}} \cdot \frac{1000 \cdot G_{\text{fuel}}}{\%},$$

In standards of toxicity indicators of EG of RICE [4,5] the maximum permissible magnitudes of specific effective mass hourly emissions of pollutants with EG flow are specified $(g$(PM), $g$(NO$_x$), $g$(CO), $g$(C$_n$H$_m$) in
kg/(kW-h)), rather than the value of their mass hourly emission (G(ПM), G(NOx), G(CO), G(CnHm) in kg/h), which appear in the formula to determine the magnitude of the Kc criterion. Such magnitudes are correlated by formula (7), i.e. the magnitude of mass hourly emission of k-th pollutant G(k), corresponding to the normatively established magnitude of the specific effective mass hourly emission of the same pollutant g(k), depends on the magnitude of RICE effective mass emission Nc in kW, and therefore from the coordinates of the field of its operating regimes (crankshaft speed n, in rpm and torque Msp in N·m) which is reflected in the formula (8).

Table 2. Diesel engine toxicity indicators [1, 2, 4, 5, 7–10]

| EURO level | Year of introduction | Specific effective mass hourly emission Gk, g/(kW-h) |
|------------|---------------------|--------------------------------------------------|
| I          | 1992                | PM: 0.612, NOx: 8.0, CnHm: 1.1, CO: 4.5          |
| II         | 1996                | PM: 0.25–0.15, NOx: 7.0, CO: 1.1, CnHm: 4.0      |
| III        | 2000                | PM: 0.10, NOx: 5.0, CO: 0.66, CnHm: 2.1          |
| IV         | 2005                | PM: 0.02, NOx: 3.5, CO: 0.46, CnHm: 1.5          |
| V          | 2008                | PM: 0.02, NOx: 2.0, CO: 0.25, CnHm: 1.5          |
| VI         | 2012                | PM: 0.01, NOx: 0.5, CO: 0.2, CnHm: 1.0           |

\[ G_k = g_k \cdot N_c, \text{ kg/h;} \quad (7) \]

\[ N_c = n_{max} \cdot M_{sp} / 9550, \text{ kW.} \quad (8) \]

2. Obtaining of reference values of indicators of ecological performance of RICE

Dependencies of magnitudes of reference values of emission G(ПM), G(NOx), G(CO), G(CnHm), total emission \( \Sigma(G(k)) \) and total reduced \( \Sigma(A(k)\cdot G(k)) \) and from magnitudes of effective power \( N_c \), described by formula (7) according to Table 2, for different levels of EURO are illustrated in the form of graphs in Fig. 1. Distribution of magnitudes of power \( N_c \), described by formula (8), in the field of operation regimes of diesel engine 2Ch10.5/12 is shown in Fig. 2. Distribution of magnitudes of reference values of emission G(ПM), G(NOx), G(CO), G(CnHm) and \( \Sigma(A(k)\cdot G(k)) \) on the field of operating regimes of that diesel engine for extreme levels EURO I and VI is illustrated in Fig. 3 and 4.

Fig. 1 shows that such dependences for any RICE are linear, the emission reference values increase with increasing magnitude of effective power. So with increasing magnitude of \( N_c \) from 0.05 to 25 kW: a) value \( G_k(\text{ПM}) \) increase from 0.03 to 15.3 g/h for EURO I and from 0.001 to 0.25 g/h for EURO VI; b) value \( G_k(\text{NOx}) \) – from 0.4 to 200 g/h (EURO I) and from 0.025 to 12.5 g/h (EURO VI); c) value \( G_k(\text{CnHm}) \) – from 0.055 for 27.5 g/h (EURO I) and from 0.01 to 5.0 g/h (EURO VI); d) value \( G_k(\text{CO}) \) – from 0.023 to 112.5 g/h (EURO I) and from 0.05 to 25.0 g/h (EURO VI); e) value \( \Sigma(A(k)\cdot G(k)) \) – from 23.0 to 11480.5 g/h (EURO I) and from 1.2 to 604.8 g/h (EURO VI); f) value \( \Sigma(G(k)) \) – from 0.71 to 355.3 g/h (EURO I) and from 0.09 to 24.8 g/h (EURO VI).

Fig. 2–4 shows that such distributions for diesel engine 2Ch10.5/12 have the form of planes inclined to the axes of both coordinates of the field of operation regimes of the engine: a) value \( G_k(\text{ПM}) \) varies from 0.001 (EURO VI) and 0.029 (EURO I) (at \( n_{max} = 800 \) rpm and \( M_{sp} = 0.56 \) N·m – regime A) to 0.207 (EURO VI) and 12.7 (EURO I) g/h (at \( n_{max} = 1800 \) rpm i \( M_{sp} = 110 \) N·m – regime B); b) value \( G_k(\text{NOx}) \) – from 0.023 (EURO VI) and 0.38 (EURO I) (regime A) to 10.4 (EURO VI) and 165.9 (EURO I) g/h (regime B);
c) value \( G_d(C_{H_m}) \) – from 0.009 (EURO VI) and 0.052 (EURO I) (regime A) to 4.1 (EURO VI) and 22.8 (EURO I) g/h (regime B); d) value \( G_d(CO) \) – from 0.047 (EURO VI) and 0.211 (EURO I) (regime A) to 20.7 (EURO VI) and 93.3 (EURO I) g/h (regime B); e) value \( \Sigma(A(k) \cdot G(k))_e \) – from 1.0 (EURO VI) and 2.2 (EURO I) (regime A) to 502 (EURO VI) and 9521 (EURO I) g/h (regime B).

\[
U = 3600 / H_u = \text{const};
\]

\[
V = \sigma \cdot f \sum_{k=1}^{h} (A_k \cdot g_{ki}) = f(\text{EURO})
\]

\[
\frac{U \cdot N_{ei}}{G_{fueli} + V \cdot N_{ei}} = \frac{U \cdot N_{ei}}{g_{ei} \cdot N_{ei} + V \cdot N_{ei}} = U
\]

\[
\eta = \frac{U}{g_{ei} \cdot V} = f(g_{ei}; \text{EURO})
\]

where \( U = 84.3 \text{ kg/(kW-h)} \) – constant value; \( V \) – substitution that is constant for a certain level EURO, kg/(kW-h).

Entered values \( U \) and \( V \) have the following physical meaning: \( U \) – magnitude of the specific effective mass hourly fuel consumption of diesel engine, provided that its effective efficiency coefficient \( \eta \) is equal to 1.0; \( V \) – magnitude of the specific reduced effective mass hourly emission of full set of legislatively standardized pollutants under certain conditions of RICE operation. Reference values of \( V \) and values of its relative change \( \delta V \) for different EURO levels for basic values \( \sigma = 1.0 \) and \( f = 1.0 \) and \( H_u = 42.7 \text{ MJ/kg} \) is illustrated in Fig. 5 in the form of a histogram. Value of \( U \) for different types of motor fuel, i.e. the value \( H_a \), and for basic values \( \sigma = 1.0 \) \( f = 1.0 \) illustrated in Fig. 4 in the form of a graph. Fig. 3 shows that the reference magnitudes of value \( V \) with increasing EURO (increasing the stringency of ecological requirements for RICE) decreases, for EURO VI by 95 % compared to EURO I.

\[
K_{fei} = \frac{3600 \cdot N_{ei}}{H_u \cdot G_{fueli} + \sigma \cdot f \cdot N_{ei} \cdot \sum_{k=1}^{h} (A_k \cdot g_{ki})}
\]

Fig. 2. Distribution of magnitudes of effective power \( N_e \) on field of operating regimes of diesel engine 2Ch10.5/12

3. Results of calculated assessment of reference values of complex fuel-ecological criterion and their analysis

For the study formula (6) was converted to the form of formula (9).

Fig. 3. Distribution of reference values of emissions \( G_d(\text{PM}) \) (a, b), \( G_d(\text{NOx}) \) (c, d) and \( G_d(C_{H_m}) \) (e, f) on the field of operating regimes of 2Ch10.5/12 diesel engine for extreme levels EURO I and VI

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Reference values of specific effective mass hourly fuel consumption of RICE $g_e$ for different types of engine fuel (with different magnitudes of calorific value $H_u$ in MJ/kg) depend on the value of engine effective efficiency coefficient $\eta_e$. Such dependences are illustrated in Fig. 6. Fig. 6 shows that such dependences have the form of family of hyperbolas, magnitude $g_e$ while varying from 1440 ($\eta_e = 0.1$, $H_u = 25$ MJ/kg) do 28.8 g/(kW·h) ($\eta_e = 1.0$, $H_u = 125$ MJ/kg).

Fig. 6 shows that the reference values of the value $U$ with increasing of value $H_u$ decrease according to the hyperbolic law and in the full range of changes of the influencing factor (from 25 to 125 MJ/kg) change on ±70 % compared to the basic value $H_u = 42.7$ MJ/kg, which is equal to 84.5 g/(kW·h).

Fig. 8 shows graphs of the dependence of the reference values of the value $g_e$ from the value of effective performance coefficient $\eta_e$ for different types of engine fuel and for basic values $\sigma = 1.0$ and $f = 1.0$.

Fig. 8 shows that such values $g_e$ fall according to the hyperbolic law of increasing value $\eta_e$. At value of $\eta_e = 0.5$, which reflects the objective limit of RICE modern possibilities, for conventional diesel fuel ($H_u = 42.7$ MJ/kg) value $g_e = 168.6$ g/(kW·h), while decreasing $\eta_e$ to 0.1 it grows by 400 %, and with growth of $\eta_e$ to 1.0 – decreases by 50 %.

Dependence of reference values of the $K_u$ criterion from the magnitudes of RICE specific effective mass hourly fuel consumption $g_e$ for different EURO levels and basic values $\sigma = 1.0$, $f = 1.0$ and $H_u = 42.7$ MJ/kg, described by formula (9), is shown in Fig. 9. Actually graphs in Fig. 9 are the basis for obtaining the desired values of the reference points of the corresponding partial desirability scale.

![Graph](image_url)
from 0 to 1000 %. The real limits of change in these magnitudes are as follows: \( g_e \) – from 150 to 350 g/(kW∙h) (see Fig. 6), \( K_{fe} \) – from 100 to 500 ‰ (see Fig. 8). Such graphs, constructed within the specified real limits of change of coordinates are given in Fig. 9.b. Fig. 9 shows that the graphs depicted on it are the family of hyperbolas, the reference values of the \( K_{fe} \) criterion decrease with increasing magnitude \( g_e \), and the difference between such values for the extreme values of the EURO level decreases from 1800 (at \( g_e = 0 \) g/(kW∙h)) to 83 % (at \( g_e = 500 \) g/(kW∙h)).

It is known that the physical meaning of the \( K_{fe} \) criterion is that it is effective performance coefficient of RICE taking into account its legislatively regulated EG ecological indicators. Thus, its limit values for any stationary engine mode are the values of the effective performance \( \eta_e \). These are the values it achieves when it is perfectly environmentally friendly, i.e. when there are no legally regulated pollutants in its EG stream. Distribution of magnitudes of \( \eta_e \) for 2Ch10.5/12 diesel engine in the field of its operating regimes are shown in Fig. 3.6. Fig. 3.6 shows that the magnitudes of \( \eta_e \) are distributed on a field of operating regimes of that diesel engine unevenly and acquire magnitudes within 0.08 (regime A) to 0.356 (regime B).

Distribution of reference values of \( K_{fe} \) criterion on field of operating regimes of 2Ch10.5/12 diesel engine for extreme levels of EURO – I and VI, and basic values \( \sigma = 1.0, f = 1.0 \) and \( H_n = 42.7 \) MJ/kg shown in Fig. 11.

Fig. 11 shows that such reference values of the \( K_{fe} \) criterion distributed over the field of operating regimes unevenly and reach maximum 61 and 200 ‰ respectively for EURO I and EURO VI on various steady regimes of RICE operation. The nature of the distribution differs significantly for different EURO levels. This difference is due to the peculiarities of the distribution of magnitude of \( \eta_e \) of this diesel engine and reference values of pollutant emissions in this field, presented in Fig. 2–4.
The results of calculations of the reference values of the $K_p$ criterion averaged over the field of operation regimes of the autotractor diesel engine 2Ch10.5/12 for all EURO levels are shown in Fig. 11, the dependence graph on it is described by the method of least squares in the form of a 4-degree polynomial – this is formula (10).

\[
K_{\text{fen}} = 0.735 \cdot \text{EURO}^4 - 8.325 \cdot \text{EURO}^3 + 34.366 \cdot \text{EURO}^2 - 50.346 \cdot \text{EURO} + 45.783, \% \quad (10)
\]

**Conclusions**

Thus, based on the analysis of the results of the study described in this paper, the following conclusions can be drawn.

1. Approach and method on its basis for calculating assessment of reference values of complex fuel-ecological criterion of Prof. I. Parsadanov as separate independent ES factor and as reference points of psychophysical scale of the partial desirability function when using it as the ES factor of PP with RICE operation process was proposed.

2. Calculated assessment of reference values of ecological indicators of RICE as components of complex fuel-ecological criterion depending on magnitudes of effective power and coordinates of field of engine operating regimes for different levels of legislative ecological standards in force in Ukraine and previously in force was carried out.

3. Calculated assessment of reference values of complex fuel-ecological criterion and its components was performed and obtained the distribution of such reference values in field of 2Ch10.5/12 diesel engine operating regimes depending as well as dependences of such reference values on magnitudes of level of ecological standards EURO, effective performance coefficient of engine and lower calorific value of engine fuel.

Identified dependences are described by formulas by the method of least squares.

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ВИЗНАЧЕНИЯ ЕТАЛОННИХ ЗНАЧЕНЬ КОМПЛЕКСНОГО ПАЛИВНО-ЕКОЛОГІЧНОГО КРИТЕРІЮ ЯК ОКРЕМОГО САМОСТОЯНЬОГО ЧИННИКА ЕКОЛОГІЧНОЇ БЕЗПЕКИ

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У цьому дослідженні запропоновано підхід і метод на його основі для розрахункового оцінювання еталонних значень комплексного паливно-екологічного критерію проф. І.В. Парсаданова як окремого незалежного фактора екологічної безпеки та як еталонних значень властивостей смислової дії часткових функцій бажаної ефективності при використанні його як факто-ра екологічної безпеки процесу експлуатації енергобезпеки з поршневими двигунами внутрішнього згорання. Також у дослідженні надано розрахункову оцінку еталонних значень екологічних показників поршневих двигунів внутрішнього згорання як складових комплексного паливно-екологічного критерію залежно від величин ефективної потужності та координат поля режимів роботи двигуна для різних рівнів в Україні екологічних норм – чинних та тих, що раніше діяли. Таким чином, було здійснено розрахунок оцінювання еталонних значень комплексного паливно-екологічного критерію та його компонентів і отримано розподіл таких значень по полю режимів роботи автотракторного дизеля 2Ч10.5/12, 22. Scale to a 150% height to fit the page.
Екологізація ДВЗ

а також залежності таких еталонних величин від рівня екологічних стандартів EURO, значень ефективного коефіцієнта корисної дії двигуна та нижньої теплотової здатності моторного палива. Отже, у дослідженні вперше запропоновано підхід до розрахункового оцінювання еталонних значень комплексного паливно-екологічного критерію проф. І.В. Парсаданова як реперних точок психофізичної шкали часткової функції бажаності Харрінгтона при використанні його у якості фактора екологічної безпеки процесу експлуатації енергоустановок з поршневим ДВЗ. Методика, побудована на запропонованому підході, для розрахункового оцінювання еталонних значень комплексного паливно-екологічного критерію проф. І.В. Парсаданова як реперних точок психофізичної шкали часткової функції бажаності прийнятна для отримання необхідних даних для здійснення комплексного критеріального оцінювання рівня екологічної безпеки процесу експлуатації енергоустановок з поршневим ДВЗ з використанням узагальненої функції бажаності Харрінгтона, у структурі якої комплексний паливно-екологічний критерій виступає, як окремий фактор екологічної безпеки.

Ключові слова: технології захисту навколишнього середовища; екологічна безпека; енергоустановки; двигуни внутрішнього згоряння; еталонні значення; критеріальне оцінювання; рівень EURO.

ОПРЕДЕЛЕНИЕ ЭТАЛОННЫХ ЗНАЧЕНИЙ КОМПЛЕКСНОГО ТОПЛИВНО-ЭКОЛОГИЧЕСКОГО КРИТЕРИЯ КАК ОТДЕЛЬНОГО САМОСТОЯТЕЛЬНОГО ФАКТОРА ЭКОЛОГИЧЕСКОЙ БЕЗОПАСНОСТИ

В этом исследовании предложен подход и метод на его основе для расчетного оценивания эталонных значений комплексного топливно-экологического критерия проф. И.В. Парсаданова как отдельного независимого фактора экологической безопасности и качестве эталонных значений психофизической шкалы частичной функции желательности при использовании его в качестве фактора экологической безопасности процесса эксплуатации энергоустановок с поршневыми двигателями внутреннего сгорания. Также в исследовании представлена расчетная оценка эталонных значений экологических показателей двигателей внутреннего сгорания как составляющих комплексного топливно-экологического критерия в зависимости от величин эффективной мощности и координат поля режимов работы двигателя для различных уровней экологических норм – действующих в Украине и тех, что ранее действовали. Таким образом, было осуществлено расчетное оценивание эталонных значений комплексного топливно-экологического критерия и его компонентов и получено распределение таких значений по полю режимов работы автотракторного дизеля 2Ч10,5/12, а также зависимости таких эталонных величин от уровня экологических стандартов EURO, значений эффективного коэффициента полезного действия двигателя и низшей теплотворной способности моторного топлива. Итак, в исследовании впервые предложен подход к расчетному оцениванию эталонных значений комплексного топливно-экологического критерия проф. И.В. Парсаданова як реперных точек психофизической шкалы частичной функции желательности Харрінгтона при использовании его в качестве фактора экологической безопасности процесса эксплуатации энергоустановок с поршневыми ДВС. Методика, построенная на предложенном подходе, для расчетного оценивания эталонных значений комплексного топливно-экологического критерия проф. И.В. Парсаданова як реперных точек психофизической шкалы частичной функции желательности пригодна для получения необходимых данных для комплексного критериального оценивания уровня экологической безопасности процесса эксплуатации энергоустановок с поршневым ДВС с использованием обобщенной функции желательности Харрінгтона, в структуре которой комплексный топливно-экологический критерий выступает как отдельный фактор экологической безопасности.

Ключевые слова: технологии защиты окружающей среды; экологическая безопасность; энергоустановки; двигатели внутреннего сгорания; эталонные значения; критериальная оценка; уровень EURO.