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Chapter

Diffusion Hydrodynamic Model
Theoretical Development

Theodore V. Hromadka II and Chung-Cheng Yen

Abstract

In this chapter, the governing flow equations for one- and two-dimensional unsteady flows that are solved in the diffusion hydrodynamic model (DHM) are presented along with the relevant assumptions. A step-by-step derivation of the simplified equations which are based on continuity and momentum principles are detailed. Characteristic features of the explicit DHM numerical algorithm are discussed.

Keywords: unsteady flow, conservation of mass, finite difference, explicit scheme, flow equations

1. Introduction

Many flow phenomena of great engineering importance are unsteady in characters and cannot be reduced to a steady flow by changing the viewpoint of the observer. A complete theory of unsteady flow is therefore required and will be reviewed in this section. The equations of motion are not solvable in the most general case, but approximations and numerical methods can be developed which yield solutions of satisfactory accuracy.

2. Review of governing equations

The law of continuity for unsteady flow may be established by considering the conservation of mass in an infinitesimal space between two channel sections (Figure 1). In unsteady flow, the discharge, \( Q \), changes with distance, \( x \), at a rate \( \frac{\partial Q}{\partial x} \), and the depth, \( y \), changes with time, \( t \), at a rate \( \frac{\partial y}{\partial t} \). The change in discharge volume through space \( dx \) in the time \( dt \) is \( \frac{\partial Q}{\partial x}dxdt \). The corresponding change in channel storage in space is \( Tdx \left( \frac{\partial y}{\partial t} \right)dt = dx \left( \frac{\partial A}{\partial t} \right)dt \) in which \( A = Ty \). Because water is incompressible, the net change in discharge plus the change in storage should be zero, that is

\[
\left( \frac{\partial Q}{\partial x} \right)dxdt + Tdx \left( \frac{\partial y}{\partial t} \right)dt = \left( \frac{\partial Q}{\partial x} \right)dxdt + dx \left( \frac{\partial A}{\partial t} \right)dt = 0
\]
Simplifying

\[ \frac{\partial Q}{\partial x} + T \frac{\partial y}{\partial t} = 0 \]  
(1)

or

\[ \frac{\partial Q}{\partial x} + \frac{\partial A}{\partial t} = 0 \]  
(2)

At a given section, \( Q = VA \); thus Eq. (1) becomes

\[ \frac{\partial (VA)}{\partial x} + T \frac{\partial y}{\partial t} = 0 \]  
(3)

or

\[ A \frac{\partial V}{\partial x} + V \frac{\partial A}{\partial x} + T \frac{\partial y}{\partial t} = 0 \]  
(4)

Because the hydraulic depth \( D = A/T \) and \( \partial A = T \partial y \), the above equation may be written as

\[ D \frac{\partial V}{\partial x} + V \frac{\partial y}{\partial x} + \frac{\partial y}{\partial t} = 0 \]  
(5)

The above equations are all forms of the continuity equation for unsteady flow in open channels. For a rectangular channel or a channel of infinite width, Eq. (1) may be written as

\[ \frac{\partial q}{\partial x} + \frac{\partial y}{\partial t} = 0 \]  
(6)

where \( q \) is the discharge per unit width.
3. Equation of motion

In a steady, uniform flow, the gradient, $\frac{dH}{dx}$, of the total energy line is equal to magnitude of the “friction slope” $S_f = \frac{V^2}{(C^2R)}$, where C is the Chezy coefficient and R is the hydraulic radius. Indeed this statement was in a sense taken as the definition of $S_f$; however, in the present context, we have to consider the more general case in which the flow is nonuniform, and the velocity may be changing in the downstream direction. The net force, shear force and pressure force, is no longer zero since the flow is accelerating. Therefore, the equation of motion becomes

$$-\gamma A\Delta h - \tau_0 P\Delta x = \rho A\Delta x \left( V \frac{\partial V}{\partial x} + \frac{\partial V}{\partial t} \right)$$

that is

$$\tau_0 = -\gamma R \left( \frac{\partial h}{\partial x} + \frac{V}{g} \frac{\partial V}{\partial x} + \frac{1}{g} \frac{\partial V}{\partial t} \right)$$

$$-\gamma R \left( \frac{\partial H}{\partial x} + \frac{V^2}{C^2R} \right)$$  \hspace{1cm} (7)

where $\tau_0$ is the same shear stress, $P$ is the hydrostatic pressure, $h$ is the depth of water, $\Delta h$ is the change of depth of water, $\gamma$ is the specific weight of the fluid, $R$ is the mean hydraulic radius, and $\rho$ is the fluid density. Substituting $\frac{\partial z}{\partial x} = \frac{V}{C^2g}$ into Eq. (7), we obtain

$$\frac{\partial H}{\partial x} + \frac{1}{g} \frac{\partial V}{\partial x} + \frac{V^2}{C^2R} = 0$$  \hspace{1cm} (8)

and this equation may be rewritten as

$$S_e + S_a + S_f = 0$$  \hspace{1cm} (9)

where the three terms of Eq. (9) are called the energy slope, the acceleration slope, and the friction slope, respectively. **Figure 2** depicts the simplified representation of energy in unsteady flow.

By substituting $H = \frac{V^2}{2g} + y + z$ and the bed slope $S_o = -\frac{dz}{dx}$ into Eq. (8), we obtain

$$\frac{\partial H}{\partial x} = \frac{\partial z}{\partial x} + \frac{\partial y}{\partial x} + \frac{V}{g} \frac{\partial V}{\partial x}$$

$$= -S_o + \frac{\partial y}{\partial x} + \frac{V}{g} \frac{\partial V}{\partial x}$$

$$= -\frac{1}{g} \frac{\partial V}{\partial t} - S_f$$  \hspace{1cm} (10)
Hence Eq. (8) can be rewritten as

\[ S_f = S_0 \frac{\partial v}{\partial x} - \frac{v}{g} \frac{\partial v}{\partial x} - \frac{1}{g} \frac{\partial v}{\partial t} = \frac{v^2}{c^2 R} \]  

This equation may be applicable to various types of flow as indicated. This arrangement shows how the nonuniformity and unsteadiness of flows introduce extra terms into the governing dynamic equation.

4. Diffusion hydrodynamic model

4.1 One-dimensional diffusion hydrodynamic model

The mathematical relationships in a one-dimensional diffusion hydrodynamic model (DHM) are based upon the flow equations of continuity (2) and momentum (11) which can be rewritten [1] as

\[ \frac{\partial Q_x}{\partial x} + \frac{\partial A_x}{\partial t} = 0 \]  
\[ \frac{\partial Q_x}{\partial t} + \frac{\partial (Q_x^2/A_x)}{\partial x} + gA_x \left( \frac{\partial H}{\partial x} + S_{f0} \right) = 0 \]
where $Q_x$ is the flow rate; $x,t$ are spatial and temporal coordinates, $A_x$ is the flow area, $g$ is the gravitational acceleration, $H$ is the water surface elevation, and $S_{fx}$ is a friction slope. It is assumed that $S_{fx}$ approximated from Manning’s equation for steady flow by [1].

$$Q_x = \frac{1.486}{n} A_x R^{2/3} S_{fx}^{1/2}$$  \hspace{1cm} (14)

where $R$ is the hydraulic radius and $n$ is a flow resistance coefficient which may be increased to account for other energy losses such as expansions and bend losses. Letting $m_x$ be a momentum quantity defined by

$$m_x = \left( \frac{\partial Q_x}{\partial t} + \frac{\partial (Q_x^2/A_x)}{\partial x} \right)/gA_x$$  \hspace{1cm} (15)

then Eq. (13) can be rewritten as

$$S_{fx} = \left( \frac{\partial H}{\partial x} + m_x \right)^{-1}$$  \hspace{1cm} (16)

In Eq. (15), the subscript $x$ included in $m_x$ indicates the directional term. The expansion of Eq. (13) to two-dimensional case leads directly to the terms ($m_x, m_y$) except that now a cross-product of flow velocities is included, increasing the computational effort considerably.

Rewriting Eq. (14) and including Eqs. (15) and (16), the directional flow rate is computed by

$$Q_x = -K_x \left( \frac{\partial H}{\partial x} + m_x \right)$$  \hspace{1cm} (17)

where $Q_x$ indicates a directional term and $K_x$ is a type of conduction parameter defined by

$$K_x = \frac{1.486}{n} A_x R^{2/3} \left| \frac{\partial t}{\partial x} + m_x \right|^{1/2}$$  \hspace{1cm} (18)

In Eq. (18), $K_x$ is limited in value by the denominator term being checked for a smallest allowable magnitude (such as $\left| \frac{\partial t}{\partial x} + m_x \right|^{1/2} > 10^{-3}$).

Substituting the flow rate formulation of Eq. (17) into Eq. (12) gives a diffusion type of relationship

$$\frac{\partial}{\partial x} K_x \left[ \frac{\partial H}{\partial x} + m_x \right] = \frac{\partial A_x}{\partial t}$$  \hspace{1cm} (19)

The one-dimensional model of Akan and Yen [1] assumed $m_x = 0$ in Eq. (18). The $m_x$ term is assumed to be negligible when combined with the other similar terms—that is, they are considered as a sum rather than as individual directional terms that typically have more significance when examined individually. Additionally, the term “diffusion” routing indicates assuming that several convective and other components have a small contribution to the coupled mass and energy balance equations and therefore are neglected in the computational formulation to simplify the model accordingly. Thus, the one-dimensional DHM equation is given by
A Diffusion Hydrodynamic Model

\[
\frac{\partial}{\partial X} K_X \frac{\partial H}{\partial X} = \frac{\partial A_X}{\partial t} \tag{20}
\]

where \( K_X \) is now simplified as

\[
K_X = \frac{1.486}{n} A_x R^{2/3} \left( \frac{\partial H}{\partial X} \right) \tag{21}
\]

For a channel of constant width, \( W_X \), Eq. (20) reduces to

\[
\frac{\partial}{\partial X} K_X \frac{\partial H}{\partial X} = W_X \frac{\partial H}{\partial t} \tag{22}
\]

Assumptions other than \( m_X = 0 \) in Eq. (19) result in a family of models:

\[
m_X = \begin{cases} 
\frac{\partial (Q_x^2/A_x)}{\partial X} / gA_x & \text{(convective acceleration model)} \\
\frac{\partial Q_X}{\partial t} / gA_x & \text{(local acceleration model)} \\
\left[ \frac{\partial Q_X}{\partial t} + \frac{\partial (Q_x^2/A_x)}{\partial X} \right] / gA_x & \text{(fully dynamic model)} \\
0 & \text{(DHM)}
\end{cases} \tag{23}
\]

4.2 Two-dimensional diffusion hydrodynamic model

The set of (fully dynamic) 2D unsteady flow equations consists of one equation of continuity

\[
\frac{\partial q_x}{\partial x} + \frac{\partial q_y}{\partial y} + \frac{\partial H}{\partial t} = 0 \tag{24}
\]

and two equations of motion

\[
\begin{align*}
\frac{\partial q_x}{\partial t} + \frac{\partial}{\partial x} \left( q_x \frac{q_x}{h} \right) + \frac{\partial}{\partial y} \left( q_x q_y \frac{q_x}{h} \right) + gh \left[ S_{fx} + \frac{\partial H}{\partial X} \right] &= 0 \\
\frac{\partial q_y}{\partial t} + \frac{\partial}{\partial x} \left( q_y \frac{q_y}{h} \right) + \frac{\partial}{\partial y} \left( q_x q_y \frac{q_y}{h} \right) + gh \left[ S_{fy} + \frac{\partial H}{\partial Y} \right] &= 0
\end{align*} \tag{25, 26}
\]

where \( q_x \) and \( q_y \) are flow rates per unit width in the x and y directions; \( S_{fx} \) and \( S_{fy} \) represents friction slopes in x and y directions; H, h, and g stand for water surface elevation, flow depth, and gravitational acceleration, respectively; and x, y, and t are spatial and temporal coordinates.

The above equation set is based on the assumptions of constant fluid density without sources or sinks in the flow field and of hydrostatic pressure distributions. The local and convective acceleration terms can be grouped, and Eqs. (25) and (26) are rewritten as

\[
m_z + \left[ S_{fz} + \frac{\partial H}{\partial Z} \right] = 0, z = x, y \tag{27}
\]
where $m_Z$ represents the sum of the first three terms in Eqs. (25) or (26) divided by $gh$. Assuming the friction slope to be approximated by the Manning’s formula, one obtains, in the US customary units for flow in the $x$ or $y$ directions,

$$q_Z = \frac{1.486}{n} h^{5/3} S_{f0}^{1/2}, z = x, y$$  \hspace{1cm} (28)

Eq. (28) can be rewritten in the general case as

$$q_Z = -K_Z \frac{\partial H}{\partial Z} - K_Z m_Z, z = x, y$$  \hspace{1cm} (29)

where

$$K_Z = \frac{1.486}{n} h^{5/3} \left[ \frac{|\partial H / \partial S| + m_S}{C_0} \right]^{1/2}, z = x, y$$  \hspace{1cm} (30)

The symbol $s$ in Eq. (30) indicates the flow direction which makes an angle of

$$\theta = \tan^{-1} \left( \frac{q_y}{q_x} \right)$$

with the positive $x$ direction.

The $m_z$ term is assumed to be negligible [1–5] when combined with the other similar terms, i.e., they are considered as a sum rather than as individual directional terms that typically have more significance when examined individually. Additionally, the term “diffusion” routing indicates assuming that several convective and other components have a small contribution to the coupled mass and energy balance equations and therefore are neglected in the computational formulation to simplify the model accordingly. Neglecting this term results in the simple diffusion model

$$q_Z = -K_Z \frac{\partial H}{\partial Z}, z = x, y$$  \hspace{1cm} (31)

The proposed 2D DHM is formulated by substituting Eq. (31) into Eq. (24)

$$\frac{\partial}{\partial X} K_x \frac{\partial H}{\partial X} + \frac{\partial}{\partial Y} K_y \frac{\partial H}{\partial Y} = \frac{\partial H}{\partial t}$$  \hspace{1cm} (32)

If the momentum term groupings were retained, Eq. (32) would be written as

$$\frac{\partial}{\partial X} K_x \frac{\partial H}{\partial X} + \frac{\partial}{\partial Y} K_y \frac{\partial H}{\partial Y} + S = \frac{\partial H}{\partial t}$$  \hspace{1cm} (33)

where

$$S = \frac{\partial}{\partial X} (K_x m_x) + \frac{\partial}{\partial Y} (K_y m_y)$$

and $K_x$ and $K_y$ are also functions of $m_x$ and $m_y$, respectively.

5. Numerical approximation

5.1 Numerical solution algorithm

The one-dimensional domain is discretized across uniformly spaced nodal points, and at each of these points, at time $t = 0$, the values of Manning’s $n$, an
elevation, and initial flow depth (usually zero) are assigned. With these initial conditions, the solution is advanced to the next time step \((t + \Delta t)\) as detailed below:

1. Between nodal points, compute an average Manning’s \(n\) and average geometric factors.

2. Assuming \(m_X = 0\), estimate the nodal flow depths for the next time step \((t + \Delta t)\) by using Eqs. (20) and (21) explicitly.

3. Using the flow depths at time \(t\) and \(t + \Delta t\), estimate the mid time step value of \(m_X\) selected from Eq. (23).

4. Recalculate the conductivities \(K_X\) using the appropriate \(m_X\) values.

5. Determine the new nodal flow depths at the time \((t + \Delta t)\) using Eq. (19), and

6. Return to step (3) until \(K_X\) matches mid time step estimates.

The above algorithm steps can be used regardless of the choice of definition for \(m_X\) from Eq. (23). Additionally, the above program steps can be directly applied to a two-dimensional diffusion model with the selected \((m_X, m_Y)\) relations incorporated.

### 5.2 Numerical model formulation (grid element)

For uniform grid elements, the integrated finite difference version of the nodal domain integration (NDI) method [6] is used. For grid elements, the NDI nodal equation is based on the usual nodal system shown in Figure 3. Flow rates across the boundary \(\Gamma\) are estimated by assuming a linear trial function between nodal points.

For a square grid of width \(\delta\)

\[
q|\Gamma_E = -[K_X|\Gamma_E] [H_E - H_C]/\delta
\]

where

\[
K_X|\Gamma_E = \begin{cases} \frac{1.486}{n} h^{5/3} & \frac{H_E - H_C}{\delta \cos \theta}^{1/2}; |H_E - H_C| \geq E \\ 0 & |H_E - H_C| < \epsilon \end{cases}
\]

In Eq. (35), \(h\) (depth of water) and \(n\) (the Manning’s coefficient) are both the average of their respective values at \(C\) and \(E\), i.e., \(h = (h_C + h_E)/2\) and \(n = (n_C + n_E)/2\). Additionally, the denominator of \(K_X\) is checked such that \(K_X\) is set to zero if \(|H_E - H_C|\) is less than a tolerance \(\epsilon\) such as \(10^{-3}\) ft.

The net volume of water in each grid element between time step \(i\) and \(i + 1\) is \(\Delta q_C^i = q|_{E}^r + q|_{w}^r + q|_{N}^r + q|_{S}^r\) and the change of depth of water is \(\Delta H_C^i = \Delta H_C^i + \Delta t/\delta^2\) for time step \(i\) and \(i + 1\) with \(\Delta t\) interval. Then the model advances in time by an explicit approach

\[
H_C^{i+1} = H_C^i + \Delta H_C^i
\]

where the assumed input flood flows are added to the specified input nodes at each time step. After each time step, the hydraulic conductivity parameters of Eq. (35) are reevaluated, and the solution of Eq. (36) is reinitiated.
5.3 Model time step selection

The sensitivity of the model to time step selection is dependent upon the slope of the discharge hydrograph \(\frac{\partial Q}{\partial t}\) and the grid spacing. Increasing the grid spacing size introduces additional water storage to a corresponding increase in nodal point flood depth values. Similarly, a decrease in time step size allows a refined calculation of inflow and outflow values and a smoother variation in nodal point flood depths with respect to time. The computer algorithm may self-select a time step by increments of halving (or doubling) the initial user-chosen time step size so that a proper balance of inflow-outflow to control volume storage variation is achieved. In order to avoid a matrix solution for flood depths, an explicit time stepping algorithm is used to solve for the time derivative term. For large time steps or a rapid variation in the dam-break hydrograph (such as \(\frac{\partial Q}{\partial t}\) is large), a large accumulation of flow volume will occur at the most upstream nodal point. That is, at the dam-break reservoir nodal point, the lag in outflow from the control volume can cause an unacceptable error in the computation of the flood depth. One method that offsets this error is the program to self-select the time step until the difference in the rate of volume accumulation is within a specified tolerance.

Due to the form of the DHM in Eq. (22), the model can be extended into an implicit technique. However, this extension would require a matrix solution process which may become unmanageable for two-dimensional models which utilize hundreds of nodal points.

6. Conclusions

The one- and two-dimensional flow equations used in the diffusion hydrodynamic model are derived, and the relevant assumptions are listed. These equations, which are the basis of the model, are based on the conservation of mass and momentum principles. The explicit numerical algorithm and the discretized equations are also presented. The ability of the model to self-select the optimal time step is discussed.
Author details

Theodore V. Hromadka II* and Chung-Cheng Yen

1 Department of Mathematical Sciences, United States Military Academy, West Point, NY, USA
2 Tetra Tech, Irvine, CA, USA

*Address all correspondence to: tedhromadka@yahoo.com

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