A Promising Technological Approach to Improve Indoor Air Quality

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Abstract: Indoor Air quality (IAQ) in private or public environments is progressively recognized as a
critical issue for human health. For that purpose the poor IAQ needs to be mitigated and immediate
drastic measures must be taken. In environmental science and especially in advanced oxidation
processes and technologies (AOPs-AOTs), photocatalysis has gained considerable interest among
scientists as a tool for IAQ improvement. In the current study an innovative paint material was
developed which exhibits intense photocatalytic activity under direct and diffused visible light for
the degradation of air pollutants, suitable for indoor use. A laboratory and a real scale study were
performed using the above innovative photo-paint. The lab test was performed in a special design
photo-reactor while the real scale in a military’s medical building. Nitrogen Oxide (NO) and Toluene
concentration was monitored between “reference” rooms (without photo paint) and “green” rooms
(with photo-paint) in order to estimate the photocatalytic efficiency of the photo-paint to degrade the
above pollutants. Results of the study showed a decrease up to 60% and 16% for NO and toluene
respectively under lab scale tests while an improvement of air quality up to 19% and 5% under real
world conditions was achieved.

Keywords: IAQ improvement; photo-paint; NO; Toluene degradation

1. Introduction

Indoor air quality (IAQ) is an important determinant of human health, comfort and productivity.
For that purpose, high quality indoor air is desirable. Indoor air pollution can be addressed through
the two approaches of prevention and removal. The latter includes the use of air cleaning technologies
especially in buildings where ventilation rates are being reduced in order to save energy. Indicative
air cleaning technologies which have been developed during the recent years are: filtration and
adsorption, electrostatic air purification, air filtration and gas adsorption filtration [1–3], ozonation [4–7],
non-thermal plasma [8,9] and photocatalytic oxidation (PCO) [10–13]. PCO is a general air cleaning
technology, which is able to degrade Volatile Organic Compounds (VOCs), such as aromatics, alkanes,
odor compounds etc. Air cleaning photocatalytic technology is based on the principle that radiation
of suitable wave-lengths can be absorbed by semiconductors, which leads to the creation of reactive
oxygen species (ROS) that can degrade air pollutants. TiO₂ is the most commonly-used semiconductor
in PCO research. However, over the last years, scientists have combined TiO₂ with other materials
such as activated carbon and zeolite hybrid catalysts in order to enhance the PCO degradation of air
pollutants [14–16]. Furthermore, numerous TiO₂ photocatalysts with different morphological designs
have been developed: nanoparticles, nanotubes, hollow fibers and mesoporous. To this end, the need to evaluate the photocatalytic performance of the above materials in a common methodological approach has been raised and extensive research efforts have been devoted to it [17,18].

However, in most of these studies, only a single compound was tested, using a photocatalytic reactor and a methodological approach, which have been developed by the same lab that produced the material. It is well known that indoor air contains numerous contaminants; thus, tests of only one compound may be misleading. Furthermore, many studies proved the generation of by-products during the photocatalytic processes, such as formaldehyde, ozone, benzaldehyde, acetaldehyde etc. It is obvious that in some cases, by-products could be more harmful than the target pollutant [19–22]. For that purpose, and although photocatalytic technology is promising, the synthesis route of a photocatalytic material should be designed carefully in order to avoid contaminants which could lead to the formation and emission in the gas phase of intermediate products as they can be more hazardous than the target pollutant. The latter is clearly demonstrated during the evaluation of two photocatalytic air-purification in a mock-up air cabin. Although two symptoms, dizziness and claustrophobia, were reported to decrease when either one of the photocatalytic air-purification devices was operated, intermediates (acetaldehyde and formaldehyde) were detected as a result of ethanol photodegradation [23,24].

The present research addresses the indoor air purification study using a photocatalytic paint, which was tested under both laboratory and real world indoor conditions (application in building walls). A modified TiO$_2$ was chosen as photocatalyst in order to be activated by visible light which is the dominant spectrum in indoor environments. Traditional TiO$_2$ is activated only under UV light. More specifically a Mn-doped TiO$_2$ photocatalyst (powder) was used in the synthetic route of a photocatalytic paint production. The powder named TCM-1 [25] has already been successfully tested for the oxidation of air pollutants under indoor-like illumination conditions and when mixed either with calcareous or cementitious base matrices demonstrated a unique ability to efficiently degrade volatile organic compounds (VOCs) such as BTX (Benzene, Toluene, Xylene), formaldehyde and nitrogen oxides (NOx) [26–28]. Additionally, it has been proven effective on eliminating bacteria such as E. coli and Klebsiella pneumoniae and phages such as MS2 [29–32]. Furthermore, no dangerous by-products were produced during the degradation process. In a previous work, in order to demonstrate the photocatalytic effectiveness of TCM-1, the powder has been incorporated in/on different construction matrices such as glass, plywood, wood, ceramic and concrete substances, which were, subsequently, tested indicating very promising results [33].

In the current study TCM-1 incorporated into paint production process in order to produce paint with the ability to photocatalytically improve IAQ by degraded indoor air pollutants. NO and toluene were chosen as the target pollutants since they are typical indoor air pollutants that can be emitted from various indoor sources, such as cooking, tobacco smoke, furniture, building materials and fireplaces, as well as from outdoor sources, e.g., traffic, domestic heating. These indoor pollutants can have significant health impacts and for that purpose their elimination from the indoor environment should be appropriately addressed. In order to simulate the real indoor air conditions, visible light was used as the source for the PCO reaction in the current study. The latter is different from what we usually find in the literature. More specifically, UV light is the most commonly used parameter in the experimental procedures, which usually applied to test the efficiency of a photo-material.

The experimental study of the current work was carried out using the European Committee for Standardization (CEN) Technical Specification (TS) 16980:2016 as a basic reference to perform the lab scale experiments, while the real scale experiments were based on the comparison between the concentration level of a pollutant in a reference and the “green” room, respectively. The latter was performed at the military medical center of the Cadets Training Camp in Heraklion Crete.
2. Materials and Methods

2.1. Materials

Chemicals for the preparation of the photocatalytic powder such as Titanium (IV) oxysulfate hydrate (TiOSO₄·xH₂O), manganese (II) acetate tetrahydrate Mn(CH₃COO)₂ and ammonium hydroxide (25% NH₄OH) purchased from Aldrich were applied. Chemicals for the preparation of the photo-paint were purchased from VINAVIL EGYPT (New Cairo, Egypt), DOW chemicals (Midland, Michigan, MI, United States), BYK (Wesel, Germany), DuPont (Midland, Michigan, MI, United States) and Dionyssos Marbles (Penteli, Greece) and are readily available raw materials mainly used at the coating industry.

2.2. Methods

2.2.1. Preparation of Photo-Material (powder)

In the present study, an optimum powder (0.1% Mn-doped) named TCM-1 was used for the preparation of photocatalytic paint. TCM-1 was synthesized by a co-precipitation method with 0.1% of manganese. TCM-1 was precipitated at pH ∼ 7 from aqueous solution of titanium (IV) oxysulfate hydrate and manganese by the addition of ammonia. After aging the suspension overnight, the precipitate was filtered and dried under air at 373 K. The residue was crushed to a fine powder and calcined in a furnace at 973 K for 3 h. More details in the synthesis procedure and the characterization are given in previous work along with the preparation details [25].

2.2.2. Preparation of Photo-Paint

TCM-1 powder (0.1% Mn-doped) was added to a specially formulated architectural coating. The paint was consisted 10% w/w of the TCM-1 powder partly replacing the Titanium Oxide (normally used as a white pigment). The raw materials for the preparation of the photo-paint are commonly used in the coating industry. A polyvinyl acetate copolymer binder was used and the Pigment Volume Content (PVC) was adjusted, but kept below its critical value in order for the paint to have a high quality, matte finish.

The production process of the photo-paint was consisted of three discreet phases. At phase 1, the mill-base (the minimum amount of liquid that can wet the solid particles of the paint, added at phase 2) was produced. Water was used as solvent with additives, such as sodium hexametaphosphate (dispersion agent), propylene glycol (antifreezing agent), silica modified surfactant (defoaming agent), cellulose (rheology modifier), isothiazolinone based mixture (biocide agent) and a mixture of Alkanol-amines (pH adjusting agent). At phase 2, we applied high shear forces to the mill-base by using a disperser equipped with a blade dissover disc and gradually added the solid phase of the paint [Calcium carbonate powder (20 µm), Titanium Oxide (0.2–0.5 µm), Talc Powder (6 µm) and TCM-1 powder]. The goal of this phase is to maximize dispersion by eliminating the presence of any agglomerate in the final paint. At phase 3, we added the Polyvinyl Acetate copolymer binder emulsion and a coalescent solvent mixture, necessary for the final product to have a smooth surface (filmer). The dispersion was achieved by using low shearing forces and the pigment dispersion was stabilized in order to prevent the formation of uncontrolled flocculates by using non-ionic urethane rheology modifiers.

2.3. Characterization

Powder X-ray diffraction patterns were obtained by a Rigaku D/MAX-2000H rotating anode diffractometer (CuKα radiation) equipped with a secondary pyrolytic graphite monochromator operating at 40 kV and 80 mA over the 2θ collection range of 20–80° (scan rate was 0.05° s⁻¹). The grain
size (nm) of TCM-1 was calculated from the line broadening of the X-ray diffraction peak according to the following Scherrer formula:

\[ D = \frac{k\lambda}{\beta\cos\theta} \]  

(1)

where \( k \) is the Scherrer contact (~ 0.9), \( \lambda \) is the wavelength of the X-ray radiation (1.54 Å for CuK\(\alpha \)), \( \beta \) is the full width at half maximum (FWHM) of the diffraction peak measured at 2\(\theta \), and \( \theta \) is the Bragg angle. The morphology and elemental analysis were performed using scanning electron microscopy (SEM) and energy dispersive X-ray spectroscopy (EDX), on a JSM-6390LV microscope (Jeol, Tokyo, Japan).

The photo-paint was evaluated through typical quality control measurements. Viscosity was measured using a Brookfield KU-2 viscometer (Brookfield Engineering Laboratories, INC. Middleboro, MA, USA) at a temperature of 25 °C with the help of a laboratory water bath and the measurements were conducted according to ASTM D 562-10 (2018) standard test method. Density was measured using a 100 ml pyknometer (density cup) by Elcometer (Manchester, United Kingdom) and an analytical scale, and the measurements were conducted according to ISO 2811-1:2016 standard. Fineness of Grind was evaluated using a Hegman gauge and the evaluation was conducted according to ASTM D 1210-05 (2014) standard test method. Lastly, pH was measured using a Hanna HI 83141V pH meter (Hanna Instruments, Greece) and the measurements were conducted according to ISO 787-7:2009 standard.

2.4. Photocatalytic Evaluation Lab-Scale

The experimental methodology that was applied and the required scientific equipment were based on CEN Technical Specification (TS) 16980:2016. The photocatalytic effect of the optimized material studied in a continuous flux photocatalytic reactor (Figure 1), which consists of a) a gas transfer and mixing unit in order to adjust the concentration and humidity levels; b) the photocatalytic reactor main body made of special plastic so as radiation intensity and wavelength of the radiation is not affected; (c) the sample irradiation system (OMICRON FS LED Rodgau-Dudenhofen, Germany) consisting of an LED device connected via software to a computer in order to achieve the optimum efficiency and accuracy in measuring the radiation; d) a NOx and VOCs analyzer installed on line with the reactor for continuous monitoring of the pollutant concentration.

Furthermore, in order to ensure optimum mixing of atmospheric pollutants in the reactor, a fan is installed inside the chamber, while its intensity is adjusted externally to ensure the stability of the experimental conditions throughout the experiments. The NO concentration is set to (0.50 ± 0.05) ppmv, while the relative humidity to 40 ± 5%. The illumination provided an average irradiance to the test specimen surface within the range of wavelengths that are mostly adsorbed by the photocatalyst, equal to (10.0 ± 5%) W/m².

![Figure 1. Photocatalytic reactor.](image-url)
2.5. Photocatalytic Evaluation_Real-Scale

A building of the Hellenic Army in Crete was used to test the de-polluting efficiency of the photo-paint under real scale application. In general, the photocatalytic efficiency of a material while applied in a real scale environment and more specifically in indoor building environment could be estimated through two approaches:

a) A first approach could be the installation of air quality and environmental monitoring systems (passive inorganic (NO) and organic (BTX) samplers, temperature and humidity recorders) in the buildings prior to the application of the photo-paint. To that end, a reliable record on the concentration levels of air pollutants in the case study building (without the photo paint) for at least 12 months should be obtained. Accordingly, the photo-paint should be applied in the buildings and environmental parameters should be monitored through passive sampling techniques for another 12 months. The potential changes in the indoor air quality due to the photocatalytic action of the photo-paint will be recorded and quantified to illustrate the capability of the photo-paint to improve IAQ. A restriction of this approach could be the variations in outdoor air quality and meteorological conditions during the different sampling periods. In order to eliminate the effect of the above restrictions, the experiments has to take place the same season (e.g., winter) and the outdoor concentration should be considered on the final results.

b) A second approach to evaluate the efficiency of the photo-paints is to estimate the IAQ differences between “reference” rooms (without photo paint) and “green” rooms (with photo-paint), which are located on the same level (in a raw) and where the same activities take place. The current approach overcomes the restrictions of the previous one and for that purpose was used in the current study. More specifically a room of 120 m$^2$ in the ground floor was paint with the innovative photocatalytic paint (“green room”) and compared with a same size and usage room (“reference room”) located very close to the “green” one. The outcome of this approach was compared with the outcome of the lab tests in order to estimate the differences of the photocatalytic performance of a material when studied in a control experimental reactor and under real world environmental conditions. Passive samplers for NO and Toluene were applied. More specifically, four passive samplers/pollutants were installed in each of the rooms for 30 days and then analyzed in the lab using the well-established Saltzmann spectrophotometric method for NO, while the Toluene samplers were and desorbed by carbon disulphide and analysed by gas chromatography (GC/FID).

3. Results

3.1. Physical and Chemical Properties

Figure 2 shows the X-Ray Diffraction (XRD) pattern of TCM-1(dopant concentration 0.1 wt%), calcinated at 700 °C for 3 h 1. The peaks at $2\theta$ values of 25.3°, 37.6°, and 48.2° correspond to the (101), (004) and (200) planes, respectively, and they are all anatase signature peaks. The grain size for the TCM-1 was 38.69 nm and it was determined from the full width at half maximum (FWHM) of the (101) anatase peak according to the Scherrer’s formula. In our previous work, it was proven that the doping and the role of Mn in TiO$_2$ in the case of 0.1 wt% manganese shows only 2+ oxidation state in comparison with high concentrations [34].
Figure 2. Powder XRD patterns of TCM-1.

Figure 3 shows the UV-Vis absorption as a function of wavelength for TCM-1 and exhibited an absorption edge in the visible light range (400–800 nm). The band gap energy was 2.87 eV for Mn doped catalyst.

Figure 3. UV-vis absorption of TCM-1 and energy gaps calculated from Kubenka–Munk plots.

Figure 4a shows the morphology of the photocatalyst were investigated with SEM, without specific morphology, while the spherical shape particles of all the samples demonstrated some degree of agglomeration and the diameter ranged from 0.1 to 40 μm. Figure 4b shows the characteristic peaks of Mn and Ti atoms.
Figure 4. (a,b) SEM image of TCM-1 and EDX analysis.

As far as the photo-paint is concerned, the main physicochemical properties are listed in Table 1. The measured values are typical for an indoor emulsion architectural paint, and although TCM-1 was used at 10% w/w, TCM-1 behaved as expected from a Titanium Oxide white pigment. A paint formulated with the process described in Section 2.2.2 and with the use of Ti Pure 902+ Titanium Oxide white pigment instead of TCM-1 has identical physicochemical properties.

Table 1. Physicochemical Properties of photo-paint.

| Property                           | Value   | Test Method          |
|------------------------------------|---------|----------------------|
| Viscosity at 25°C (KU)             | 100–110 | ASTM D 562           |
| Density at 25°C (kg/l)             | 1.55    | ISO 2811             |
| Fineness and Dispersion            | <40 μm  | ASTM D1210           |
| pH at 25°C                         | 8.5–9   | ISO 787-9            |
| PVC (%)                            | 66      | Calculated           |
| Usage rate for a 50 μm dry film thickness (m²/kg) | 5.95 | Calculated |

3.2. Lab and Real-Scale Photocatalytic Performance

In order to estimate the background, experiments in the absence of the photocatalytic paint were performed. The photocatalytic experiments determine the total pollutant degradation involving both UV photolysis and photocatalysis on the photo-paint. The net photocatalytic effect is calculated by the subtraction of the background contribution from the photocatalytic experiments. More specifically, blank tests were carried out by polluting the reactor with NO and Toluene in the absence of the
photocatalyst without and with irradiation, respectively; then, the same experiments were carried out in the presence of the photocatalysts.

Figure 5a,b present the elimination of NO and toluene under the irradiation of the photo-paint from Vis-light. It is obvious that just after the irradiation of the sample (Time 30), a sharp decrease in NO and a smaller but significant decrease in toluene concentration is observed, which demonstrate the immediate response of the photocatalytic system and provide the photo-efficiency of the paint.

Adsorption of NO onto the chamber’s wall area and photolysis are the main sinks of NO during blank tests. Calculations have shown that both these mechanisms did not contributed to the total NO and toluene removal during the photocatalytic experiments.

The photocatalytic activity was evaluated by the calculation photocatalytic yield (% \( \eta \), Equation (2)) and photodegradation rate (\( r \), Equation (3)). The corresponding equations were used for toluene. The results in Table 2 showed the possibility of developing a very promising and highly active to air pollutants photocatalytic paint (Table 2).

The losses in the system are minimal, and as a consequence the fraction \( \frac{\eta_{\text{dark}}}{1-\eta_{\text{NO}}} \) is zero.

| Table 2. Photocatalytic parameters for lab and real scale tests. |
|---------------------------------------------------------------|
| **Parameter** | **Lab Scale** | **Real Scale** |
|----------------|--------------|---------------|
| \( \eta \) NO  | 59.08        | 18.8          |
| \( \eta \) Toluene | 16.7         | 5.26          |
| \( r_{\text{photo}} \) (\( \mu \text{g/m}^2\text{s} \)) | 3.89         | -             |

\[
\% \eta_{\text{NO}} = \frac{C_{\text{NO}}^{\text{IN}} - C_{\text{NO}}^{\text{OUT,light}}}{C_{\text{NO}}^{\text{IN}}} \times 100 \tag{2}
\]

where:
- \( C_{\text{NO}}^{\text{IN}} \): the concentration of NO at reactor inlet
- \( C_{\text{NO}}^{\text{OUT,light}} \): the concentration of NO at reactor outlet under stable conditions with irradiation (lamp on)

\[
r_{\text{NO}}^{\text{photo}} = \frac{613F}{S} \left( \frac{\eta_{\text{total}}}{\eta_{\text{NO}}} - \frac{\eta_{\text{dark}}}{\eta_{\text{NO}}} \right) \tag{3}
\]

where
- \( F \): the gas flow (m\(^3\) h\(^{-1}\))
- \( S \): The area of the test surface (m\(^2\))

The photodegradation rate provides a more accurate measure of the photocatalytic activity of the material in comparison with the % photocatalytic decomposition. The latter is attributed to the fact that \( r \) is taking into consideration the initial concentration of the pollutant, the sample’s area and the irradiation time. It is expressed as \( \mu \text{g} \) of converted NO/toluene per m\(^2\) of material per second of irradiation. The current parameter was calculated only for the lab tests, where the pollutant flow rate in the chamber was known.

The photodegradation rate is calculated by the formula below (Equation (3)) and expressed in \( \mu \text{g/m}^2 \text{s} \).
The variations on NO and Toluene concentrations during the experimental procedure of photocatalysis are presented in Figure 5a and Figure 5b, respectively. At first, the pollutant was introduced into the photo-reactor and the system remained in equilibrium for 30 min. Then, irradiation was followed and a sharp reduction in NO and significant but less intense than NO elimination in toluene concentration is observed, which stabilized after 3 h and remained stable for approximately 2 h where the irradiation stopped. The results from the laboratory tests showed that for both pollutants, the photocatalytic paint gave very promising results. It is worth to note that in the case of toluene, the degradation efficiency is significantly lower than NO. However, a reduction of VOCs even at that level could have significant effects in the improvement of IAQ. Furthermore, the lower degradation efficiency in VOCs compared with NO is in line with the results of various studies [35–38]. The latter could be attributed to the low adsorption capacity of toluene molecules at the catalyst surface. The extremely hydroxylated surface of the paint material due to physically or chemically bound water, could constrain its interaction with the active radicals through surface diffusion [39,40].

3.3. Real-Scale Photocatalytic Performance

As far as the real scale application is concerned, the deppolution efficiency was calculated by the absolute difference in the concentration levels of NO and toluene, which was measured in the two
rooms of the military building: the “green” and the “reference” rooms. Results are shown in Table 2. It is observed that real scale tests showed significant lower values of NO and toluene degradation than in the lab-scale application. The latter was also observed in other studies [41–45]. The control environment of the laboratory versus the more complex and polyparametric environment of a real application could be the main reason that led to significant differences in the values that characterize the photocatalytic efficiency of the paint. However, they provide an indication of the photocatalytic efficiency of the paints to degrade pollutants in situ and a basis for photo-paint applications in order to improve IAQ.

4. Discussion

The effect of photocatalytic paint in the improvement of IAQ has been studied in both laboratory and real scale tests. It is interesting to note that NO could be effectively converted by the photocatalytic paint, while toluene showed lower photocatalytic removal in the same photocatalytic process (lab and real scale). A possible explanation of the different photocatalytic performance of NO and toluene under the same application could be explained as follows: the dominant oxidants in a photocatalytic reaction are hydroxyl radicals (OH•) and hydroperoxyl radicals (HO₂•), which are generated from the redox reactions of positive holes (h⁺) and electrons (e⁻) with O₂, H₂O or OH⁻. The kinetic coefficients of gas phase reactions for HOₓ radicals and targeted gas (NO and toluene in this case) have only minor differences [46,47]. However, NO is better adsorbed by the alkaline constituents of the paint due to its acidic property. This significantly increases their reaction potential with HOₓ radicals. On the other hand, the adsorption capacity of toluene is lower than NO due to the extremely hydroxylated surface of the paint, which constrain its interaction with the active radicals. Toluene is absorbed more easily in a less hydrophilic TiO₂ surface than a more hydroxylated one [41]. It is obvious that different gaseous pollutants present significant variations in their photocatalytic activity due to the difference in their diffusion in the paint matrix. Efficient adsorption of the pollutant molecules at the catalyst surface could promote the photocatalytic reaction.

Comparing lab versus real scale experiments results, it is observed that laboratory tests showed significant higher values of both pollutants (NO and toluene) degradation than in real scale application. The translation from the laboratory results to “real” site efficiency is difficult because of the great number of parameters involved such as traffic and environmental parameters (temperature, light intensity, relative humidity wind speed). For that purpose, the more complex and polyparametric environment of a real application lead to significant differences in the values, which characterize the photocatalytic efficiency of the paint. In any case, precaution has to be taken with the interpretation of data obtained from the real scale experiments since these results are limited over time. However, they provide an indicative picture of the efficiency of the photocatalytic paints to eliminate air pollutants under real world conditions and a basis on which to improve their photocatalytic capacity for future applications. The need for large scale applications is more imperative nowadays, as many photo-materials have indicated very promising results during lab scale tests, but their capacity under real world conditions has not been proven. The latter is critical and proven by the outcome of the current work, which showed significant differences between the photo-efficiency of the same material under two different scales. Additionally, the demonstration of the effectiveness of photocatalytic materials on site should also include negative effects, such as the formation and emission of by-products during the photocatalytic reactions, as well as the durability of the photo-paint mechanical properties. The latter is of high importance, as in most of the cases, TiO₂ oxidizes not only the air pollutants on the photo-material surface, but also their organic and inorganic components. For that purpose, special attention is given in the formulation of such materials in order to avoid it. As it is not in the scope of the current manuscript to study the durability of the photo-paint mechanical properties, measurements to characterize the mechanical durability of the paint were not performed. However, it is worth mentioning that almost two years after the photo-paint application, cracks or other surface damages have not been observed. Nevertheless, beyond the visual observation, the latter should be certified by analytical measurements,
which should be the topic of future study. Furthermore, better results could be obtained by using mathematical models to simulate the photocatalytic processes, validating the model using the outcomes of the lab measurements and then implement various parameters in order to assess the real life effects [48].

5. Conclusions

This article addresses the effect of a photocatalytic paint on the elimination of air pollutants, and more specifically NO and toluene, for application in indoor environments. The following conclusions can be drawn:

- The physicochemical properties (including the mechanical parameters) of the photo-paint does not seem to be affected from the introduction of the photocatalytic powder (TCM-1) in the synthesis route.
- The photocatalytic efficiency of the paint on NO removal was significantly higher than toluene. The potential of a pollutant removal depends on the intrinsic properties of gas and the chemical nature of the paint in which the TiO$_2$ particles are embedded. However, the removal rate of toluene was very promising for the improvement of IAQ while using the studied photo-paint.
- Lab tests showed better photocatalytic properties of the paint than the results from the real scale application due to the great number of parameters involved in the case of real scale application.
- There is a need for large scale applications to demonstrate the effectiveness of photocatalytic materials on site, including any negative effects of the application, such as the emission of by-products (e.g., carbonyl compounds, O$_3$ etc.).

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