LONGITUDINAL WAKEFIELD FOR AN AXISYMMETRIC COLLIMATOR* 

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Abstract

We consider the longitudinal point-charge wakefield, \( w(s) \), for an axisymmetric collimator having inner radius \( b \), outer radius \( d \), inner length \( g \) and taper length \( L \). The taper angle \( \alpha \) is defined by \( \tan \alpha = (d - b)/L \). Using the electromagnetic simulation code ECHO, we explore the dependence of the wakefield on a collimator’s geometric parameters over a wide range of profiles: from small-angle tapers to step-function transitions.

INTRODUCTION

In this paper, using the 2-D electromagnetic simulation ECHO code [1,2], we carry out an investigation of the longitudinal point-charge wakefield for a collimator having inner radius \( b \); the length of the inner section of the collimator by \( g \); and the length of the taper by \( L \). The longitudinal wakefield produced by a point charge is denoted \( w(s) \), where \( s \) is the distance of the test particle behind the driving particle.

Figure 1: a) Step Collimator. b) Tapered Collimator.

We consider the highly relativistic limit in which a particle traveling at the speed of light \( c \) passes through a step-function or tapered collimator illustrated in Figs. 1a,b. We denote: the smaller pipe radius by \( b \); the larger radius by \( d \); the length of the inner section of the collimator by \( g \); and the length of the taper by \( L \). The taper angle \( \alpha \) is defined by \( \tan \alpha = (d - b)/L \). The longitudinal wakefield produced by a point charge is given in the form

\[
 w(s; b, d, g, L) = \frac{eZ_0}{\pi} \log(d/b) \delta(s) + D(s; b, d, g, L),
\]

(1)

where \( Z_0 \) is the impedance of free space. The delta function term corresponds to the result in the optical regime [5]. The causal function \( D(s) \), vanishes for \( s < 0 \), and is discontinuous at \( s = 0 \). Since the impedance vanishes at zero frequency, it follows that

\[
 \int_0^\infty ds D(s) = -\frac{eZ_0}{\pi} \log(d/b).
\]

(2)

In this paper, in order to facilitate the illustration of the behavior of the wakefield of a collimator over a wide range of parameters and for larger \( s \), we prefer to introduce the normalized causal function \( u(s) \), via

\[
 w(s; b, d, g, L) = \frac{eZ_0}{\pi} \log(d/b) \delta(s) - u(s; b, d, g, L),
\]

(3)

where

\[
 \int_0^\infty ds u(s) = 1.
\]

(4)

Using this normalized function, the ratio of the loss factor \( k_{loss} \) to that in the optical regime \([5,6]\) \( k_{loss}^{opt} \) is easily expressed. For a Gaussian bunch of rms width \( \sigma \), this ratio is given by

\[
 k_{loss}(\sigma)/k_{loss}^{opt}(\sigma) = 1 - \int_0^\infty ds u(s) \exp(-s^2/4\sigma^2),
\]

(5)

where \( k_{loss}^{opt}(\sigma) = (cz_0/2\pi^{3/2}) \log(d/b) \).

For a small-angle tapered collimator \((sat)\), it is shown in ref. [4] that,

\[
 D^{sat}(0) = -\frac{cz_0}{\pi b \alpha},
\]

(6)

and for a step collimator \((st)\), it follows from the work of Okamoto, Jiang and Gluckstern [7] that

\[
 D^{st}(0) = -\frac{0.6 c z_0}{\pi b (\pi/2)}.
\]

(7)

We now note that to within \( \pm 10\% \) accuracy,

\[
 \frac{1}{\pi b} \approx \frac{\log(d/b)}{d}, \quad \text{(for} \ 1.5 \leq d/b \leq 6 \text{).}
\]

(8)

In this paper, we shall restrict our attention to collimators with parameters within the range \( 1.5 \leq d/b \leq 6 \). In this case, Eqs. (6,8) imply that for small-angle tapers,

\[
 u^{sat}(0) \approx \frac{\pi}{d \alpha},
\]

(9)

and Eqs. (7,8) show that for a step collimator,

\[
 u^{st}(0) \approx \frac{0.6 \pi}{d (\pi/2)}
\]

(10)

The short-range wakefield depends predominantly on the two length scales \( ba \) and \( da \). In illustrating its behavior, one can plot the wakefield versus the variable \( s/\alpha a \) or \( s/da \). In this paper, in order to illustrate more clearly the behavior of the wakefield at longer distances, we prefer to utilize the variable \( s/da \).

For the short-range wakefield \((s/da \leq 0.3)\), our numerical calculations demonstrate that the dependence on \( g \) is very weak and they support the approximate validity of the scaling relation,

\[
 w(s; b, d, g, L) \equiv \frac{eZ_0}{\pi} \log\left(\frac{d}{b}\right) \delta(s) - \frac{1}{da} f\left(\frac{s}{da}, \frac{b}{a}\right).
\]

(11)

With the wakefield approximated by Eq. (11), it follows from Eq. (5) that the departure of the loss factor from the optical approximation for short bunches \( (\sigma/da \leq 0.15) \) can be estimated by

\[
 k_{loss}(\sigma)/k_{loss}^{opt}(\sigma) \approx 1 - \sqrt{\pi} f\left(0, \frac{b}{a}ight) \frac{\sigma}{da}.
\]

(12)

with \( f\left(0, \frac{b}{a}\right) \) varying from \( \sim 3 \) for small-angle tapers to \( \sim 1.8 \) for step collimators. Eq. (12) is a more accurate expression for the loss factor than the similar relation given in Eq. (12.26) of ref. [8].
DIMENSIONAL ANALYSIS

We motivate our discussion by using dimensional analysis and the longitudinal scaling relation introduced in ref. [9]. From dimensional analysis, we can write,

\[ u(s; b, d, g, L) = \frac{1}{a} u_1 \left( \frac{s}{a}, \frac{b}{d}, \frac{d}{a}, \frac{L}{a} \right). \]

(13)

In the special case of a step collimator, for which \( L=0 \),

\[ u^{st}(s; b, d, g) = \frac{1}{a} u_2 \left( \frac{s}{a}, \frac{b}{d}, 0 \right). \]

(14)

We have determined that when \( g \) is not too large, the field depends very weakly on \( g \), so we can simplify Eq. (14) to read,

\[ u^{st}(s; b, d, g) \approx \frac{1}{a} u_2 \left( \frac{s}{a} \right). \]

(15)

The corresponding weak dependence of the impedance of a step collimator on \( g \) was found in the analysis of Ref. [7].

Our ECHO calculations have uncovered the surprising result that in the parameter range we are considering [see Eq. (8)], and for \( s/d \approx 0.5 \), the dependence on \( b/d \) is very weak (see Fig. 2), so to a reasonable approximation,

\[ u^{st}(s; b, d, g) \approx \frac{1}{a} u_3 \left( \frac{s}{a} \right). \]

(16)

Clearly, in Eq. (13), we could have chosen to set the length scale with any of the lengths in the problem. Eq. (16) provides one motivation for our choice to single out the dependence on the larger radius \( d \).

For a small-angle tapered collimator, it has been shown [9] that an important longitudinal scaling relation holds for the short-range wakefield,

\[ w^{sat}(s; b, d, g, L) = \lambda w^{sat} \left( \frac{sl}{\alpha}, \frac{b}{d}, \frac{d}{\alpha}, \frac{L}{\alpha} \right). \]

(17)

where \( \lambda \) is a dimensionless parameter. The scaling relation (17) holds trivially for the delta function term in Eq. (3). It therefore follows from Eqs. (13) and (17) that

\[ u_1^{sat} \left( \frac{s}{a}, \frac{b}{d}, \frac{d}{a}, \frac{L}{a} \right) = \lambda u_1^{sat} \left( \frac{sl}{\alpha}, \frac{b}{d}, \frac{d}{\alpha}, \frac{L}{\alpha} \right). \]

(18)

We now choose \( \lambda = L/(d-b) \), obtaining

\[ u_1^{sat} \left( \frac{s}{a}, \frac{b}{d}, \frac{d}{a}, \frac{L}{a} \right) = \frac{L}{d-b} u_1^{sat} \left( \frac{sl}{d-b}, \frac{b}{d-b}, \frac{d-b}{d}, \frac{L}{d-b} \right). \]

(19)

and hence,

\[ u^{sat}(s; b, d, g, L) = \frac{L}{d-b} u_2^{sat} \left( \frac{sl}{d-b}, \frac{b}{d-b}, \frac{d-b}{d}, \frac{L}{d-b} \right). \]

(20)

Recall that the taper angle \( \alpha \) is defined by \( \tan \theta = (d-b)/L \). We can rewrite Eq. (20) in the form

\[ u^{sat}(s; b, d, g, L) = \frac{1}{d \tan \theta} u_2^{sat} \left( \frac{s}{d \tan \theta}, \frac{b}{d \tan \theta}, \frac{d-b}{d}, \frac{L}{d} \right). \]

(21)

Based on the ECHO calculations, we have found that the dependence on \( g \) is weak for \( s/d \alpha \lesssim 0.3 \). Neglecting the dependence on \( g \), and replacing \( \tan \\theta \) by the angle \( \alpha \) in the first argument of \( u_2^{sat}(s) \), we obtain the approximate scaling relation

\[ u^{sat}(s; b, d, g, L) \approx \frac{1}{d \tan \alpha} u_2^{sat} \left( \frac{s}{d \tan \alpha}, \frac{b}{d}, \frac{d-b}{d} \right). \]

(22)

Let us note that Eq. (22), which we have just introduced for the tapered collimator, has a form consistent with Eq. (15) found for the step collimator \( (\alpha = \pi/2) \). Therefore, we can hope that Eq. (15) will have an approximate validity for large collimator angles. Our numerical calculations show that replacing the tangent by the angle extends the range of usefulness of Eq. (15). In the context of the derivation of the scaling relation of Ref. [9], replacing \( \tan \alpha \) by the angle \( \alpha \) corresponds to moving out of the region of validity of the paraxial approximation, which is only applicable for a smooth, slowly-varying wall. Once the taper angle approaches \( \pi/2 \), the scaling is broken and the function \( f \) begins to depend also on the angle \( \alpha \) itself. The special case of the wakefield of the step collimator \( (\alpha = \pi/2) \) turns out to exhibit very interesting behavior deserving individual attention.

APPROXIMATE CALCULATION OF THE POINT-CHARGE WAKEFIELD

Using ECHO, we cannot directly calculate the point-charge wakefield. In Ref. [4], an approximate method for determining the point-charge wake has been introduced. Following this approach, we use ECHO to calculate the wakefield \( W^{\alpha}(s) \) produced by a Gaussian bunch of rms width \( \sigma_0 \). We choose \( \sigma_0 \) small enough so that the wake is resistive. We then approximate Eq. (3) by

\[ W^{\alpha}(s; b, d, g, L) = \frac{c^2 \omega^2}{\pi \alpha} \log(d/b) \left[ \frac{1}{\sqrt{1+4\pi \alpha}} \exp \left( \frac{-s^2}{2d^2} \right) - U^{\alpha}(s; b, d, g, L) \right]. \]

(23)

For \( s \gg \sigma_0 \), the point-charge wake is well-approximated by Eq. (23), hence

\[ u(s; b, d, g, L) \approx U^{\alpha}(s; b, d, g, L) \quad (s \gg \sigma_0). \]

(24)

In this manner, we approximate the scaling function introduced in Eq. (11) by

\[ f \approx d\alpha U^{\alpha}(s; b, d, g, L) \quad (s \gg \sigma_0). \]

(25)

STEP COLLIMATORS

In Fig. 2, we plot \( f \approx d\alpha U^{\alpha} \) versus \( s/d \alpha \) for step collimators with \( b=3\)mm and \( d=6\)mm (black), \( 12\)mm (green) and \( 18\)mm (orange), and with \( b=6\)mm and \( d=12\)mm (red). The rms length of the charge distribution \( \sigma_0 = 50\mu m \) is chosen to be small enough to assure that the wake field is resistive. The close agreement of the wakefields for these different parameters is striking. These results clearly show that the dependence of the scaling function \( f \) on the ratio \( b/d \) is surprisingly weak, as noted in Eq. (16).

Figure 2: For step collimator, we plot \( (\pi d/2) U^{\alpha}(s; b, d, g) \) versus \( 2s/rd \) for \( \sigma_0 = 50\mu m \) and: \( d=12\)mm, \( b=3\)mm, \( g=10\)mm, \( \sigma_0 = 50\mu m \); \( d=12\)mm, \( b=6\)mm, \( g=10\)mm (green); \( d=12\)mm, \( b=6\)mm, \( g=50\)mm (orange); \( d=6\)mm, \( b=3\)mm, \( g=50\)mm (red); \( d=6\)mm, \( b=3\)mm, \( g=50\)mm (black).

TAPERED COLLIMATORS

We note that for \( s/d \alpha \lesssim 0.3 \), \( f \) is quite independent of \( g \). In Fig. 3, we plot the function \( f \approx d\alpha U^{\alpha} \) versus \( s/d \alpha \) for collimators with \( d=6\)mm and \( b=3\)mm. The cases with taper length \( L \approx 6.25\)mm (red, blue, orange) satisfy the
longitudinal scaling (17) very accurately. The longitudinal scaling is seen to be broken when \( L \leq 3.125 \text{mm} \). The accuracy of the approximation of Eq. (11) for the cases of \( L=3.12 \text{mm} \) (aqua) and \( L=1.56 \text{mm} \) (green) has been significantly improved by the replacement of tan \( \alpha \) by the angle \( \alpha \) as suggested following Eq. (21). Even in the case of the step collimator (black), Eq. (11) provides a rough approximation for small \( s \). In Fig. 4, we plot the function \( f = \frac{d a U_{\alpha \theta}}{s d a} \) for collimators with \( d=12 \text{mm} \) and \( b=3 \text{mm} \). The cases with taper length \( L \geq 12.5 \text{mm} \) (pink, black, orange) satisfy the longitudinal scaling (17) very accurately. The longitudinal scaling is seen to be broken for the cases of \( L \leq 6.25 \text{mm} \) (red, aqua, green). In Fig. 5, we plot the function \( f = \frac{d a U_{\alpha \theta}}{s d a} \) for collimators with \( d=6 \text{mm} \), \( b=3 \text{mm} \), \( L=25 \text{mm} \) (red); \( d=12 \text{mm}, b=3 \text{mm}, L=50 \text{mm} \) (black); and \( d=18 \text{mm}, b=3 \text{mm}, L=50 \text{mm} \) (green) for values of \( L \) sufficiently large to assure longitudinal scaling (17) is accurately satisfied. We see that for \( s d a \approx 0.3 \), there is approximate agreement between the curves corresponding to different values of \( b/d \), illustrating the weak dependence on the ratio \( b/d \) in the approximate scaling relation (11).

**SUMMARY**

For a tapered collimator, we have shown that the short-range wakefield, for \( s d a \leq 0.3 \) and \( \alpha \leq \pi / 3 \), is well-approximated by Eq. (11). Having factored out the \( \log (d/b) \) term, we have found that in the range \( 1.5 \leq \frac{d}{b} \leq 6 \) of Eq. (8), the scaling function \( f \) depends only weakly on \( b/d \). For small taper angle, \( \alpha \leq \pi / 4 \), the ECHO calculations confirm that the longitudinal scaling [9] relation (17) is accurately satisfied. The approximation of Eq. (11) properly satisfies Eq. (17) for small taper angle. The longitudinal scaling is broken for angles large compared with \( \pi / 4 \). We have found that using the taper angle \( \alpha \) in Eq. (11), rather than its tangent, allows Eq. (11) to remain a good approximation for larger angles \( (\alpha \sim \pi / 3) \), beyond the regime where Eq. (17) is satisfied. As the taper angle increases further, Eq. (11) becomes less accurate, and the function \( f \) begins to depend on the angle \( \alpha \) itself.

The case of a step collimator (\( \alpha = \pi / 2 \)) is quite interesting. For the parameters that we have considered, its wakefield is well-approximated by,

\[
w_{\text{step}}(s; b, d, g, L) \approx \frac{e^{\alpha}}{\alpha} \log \left( \frac{d}{b} \right) \left[ f(s) - \frac{1}{d} f_{\text{step}} \left( \frac{d}{b} \right) \right],
\]

where the dependence on \( b/d \) is very weak for \( s/d > 0.5 \) (see Fig. 2). The very weak dependence of \( f_{\text{step}} \) on \( b/d \) is quite remarkable, and we did not anticipate this simple behavior.

![Figure 3](image-url)  
**Figure 3:** For tapered collimators, we plot \( da U_{\alpha \theta} \) versus \( s/d a \) for \( d=6 \text{mm} \), \( b=3 \text{mm} \) and: \( g=3.12 \text{mm}, L=1.56 \text{mm}, \sigma_0=32 \mu \text{m} \) (green); \( g=6.25 \text{mm}, L=3.12 \text{mm}, \sigma_0=32 \mu \text{m} \) (aqua); \( g=12.5 \text{mm}, L=6.25 \text{mm}, \sigma_0=32 \mu \text{m} \) (red); \( g=25 \text{mm}, L=12.5 \text{mm}, \sigma_0=16 \mu \text{m} \) (blue); \( g=50 \text{mm}, L=25 \text{mm}, \sigma_0=8 \mu \text{m} \) (orange). The black curve corresponds to a step collimator. We see that longitudinal scaling is only accurately satisfied for \( L \geq 6.25 \text{mm} \).

![Figure 4](image-url)  
**Figure 4:** For tapered collimators, we plot \( da U_{\alpha \theta} \) versus \( s/d a \) for \( d=12 \text{mm} \) and \( b=3 \text{mm} \) and: \( g=3.12 \text{mm}, L=1.56 \text{mm}, \sigma_0=30 \mu \text{m} \) (green); \( g=6.25 \text{mm}, L=3.12 \text{mm}, \sigma_0=30 \mu \text{m} \) (aqua); \( g=12.5 \text{mm}, L=6.25 \text{mm}, \sigma_0=30 \mu \text{m} \) (red); \( g=18.8 \text{mm}, L=9.4 \text{mm}, \sigma_0=30 \mu \text{m} \) (blue); \( g=25 \text{mm}, L=12.5 \text{mm}, \sigma_0=20 \mu \text{m} \) (orange); \( g=12 \text{mm}, L=50 \text{mm}, \sigma_0=10 \mu \text{m} \) (black); \( g=100 \text{mm}, L=50 \text{mm}, \sigma_0=10 \mu \text{m} \) (purple).

![Figure 5](image-url)  
**Figure 5:** For small-angle tapered collimators satisfying longitudinal scaling, we plot \( da U_{\alpha \theta} \) versus \( s/d a \) for: \( d=6 \text{mm}, b=3 \text{mm}, L=25 \text{mm} \) (red); \( d=12 \text{mm}, b=3 \text{mm}, L=50 \text{mm} \) (black); and \( d=18 \text{mm}, b=3 \text{mm}, L=50 \text{mm} \) (green).

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