A corn dryer prototype was manufactured for Mexican small-scale farmers in order to avoid them paying fines for corn with a high-moisture content when selling their corn on to stores. The dryer comprised two large boxes perforated by round holes and containing stainless steel trays subjected to a hot air temperature of 45°C within the batch. The accumulated grain in both boxes was 200 mm and the airflow rate were 0.56 m³ s⁻¹. The corn ears layer was of 80 mm of depth in each of the boxes. The airflow rate was 0.34 m³ s⁻¹. Within eight hours, we sampled corn grain in nine points of each box and found that the mean corn grain moisture content was reduced from 30.36% to 10.47% for box 1 whereas for box 2 it was reduced until 14.72%. The fuel consumption for drying was 0.55 kg h⁻¹ of kerosene. In Box 1, the exponential regression model for corn grain moisture content had an R² of 0.9143 whereas Box 2 exponential regression model had an R² was of 0.6642. In Box 1, the exponential regression model for corn ear moisture content had an R² of 0.9616 whereas Box 2 had an R² was of 0.9400. Both models for corn cob moisture content had R² was of 0.9400. Two-layer corn dryers can be used to harness gas or fuel energy to speed up drying for storage.
in Japan (Kalamphastra, 1995). The grain dryer using far-infrared radiation reduced the electricity and kerosene (Hidaka et al., 2004). It was also developed a low-cost mobile flash dryer for rice grain in Philippines. It was found that the drying rate (0.03 kg moisture min\(^{-1}\)) was maximum at 70°C of air temperature and 40 m\(^3\) min\(^{-1}\) of airflow rate (Bulaong et al., 1996). It is also important to research about behavior of moisture contents and temperatures in vertical dryers with two or more corn boxes.

The objective of this project was to design and manufacture a dryer prototype using upper and lower boxes as an experimental machine, which might be used for corn grain and corn ear drying.

**Materials and Methods**

The design parameters were chosen to provide to small farmers a suitable, cheap, and durable corn dryer. The description of the manufacturing components of the dryer of two boxes (Figure 1) is as follows:

**Frame and Body of the Dryer**

The frame was constructed using an angle with a thickness of 5 mm and 50 mm in width, and two grid structures were made using an angle whose thickness was 2.5 mm and 30 mm wide. Finally, they were joined using electric arc welding. A steel plate with a thickness of 1.2 mm was used to form the body of the dryer. The dimensions of the dryer were 530 mm (width) × 900 mm (length) × 1735 mm (height).

**Box and Perforated Sheet**

The capacity of each box was 0.14 m\(^3\) (100 kg) with a layer of corn of 310 mm and a free space of 150 mm. The area of the perforated sheet is 4500 cm\(^2\). Each hole has an area of 36 mm\(^2\). The horizontal distance between successive perforations is 5 mm and the vertical distance is 4 mm (Figure 1). It also has a 254 cm\(^2\) gate to discharge the grain using a handle and a small shovel. This dryer has a mechanical system that allows the removal of the boxes as soon as the grain of corn is dry.

**Duct, Fan and Burner**

The conduit was 500 mm long and 390 mm in diameter. It was manufactured using a steel plate with a thickness of 1.2 mm. This steel plate was processed in a roller machine to form a cylinder that was then joined using clamps and weld. A cylinder was welded to a support base (Figure 2).

Finally, a fan and burner model FB-386 from Yamamoto C. Ltd. was mounted to the duct and the duct was screwed to the dryer (Figure 3).

**Performance Test**

The objective of this test was to determine the time required to dry corn grain at a temperature of 45°C inside the dryer. 45°C would not affect the final quality of dried kernels (Akowuah et al., 2018). The time required to dry corn cobs was also determined. The corn grain was placed in the boxes at an average initial moisture content of 30.36%. The amount of material was 40 kg in each of the boxes. The grain layer was almost 2000 mm since there was not enough material. The consumption of electrical energy was measured by installing a watt meter to the electric motor. The fan speed was measured using an electronic tachometer.

| Condition                   | Box 1 | Box 2 |
|-----------------------------|-------|-------|
| Outside Temperature (°C)    | 26.86 | 26.86 |
| Relative humidity (%)       | 64.68 | 64.68 |
| Mass of corn grain (kg)     | 40    | 40    |
| Hot air temperature(°C)     | 45    | 45    |
| Drying time (h)             | 8     | 8     |
| Kerosene consumption (kg h\(^{-1}\)) | 0.55 | 0.55 |
| Air flowrate (m\(^3\) s\(^{-1}\)) | 0.56 | 0.56 |
| Corn grain moisture content (%) | 30.36 | 30.36 |
| Moisture drying rate (% moisture h\(^{-1}\)) | 2.44 | 1.91 |
| Electrical energy consumption (kwh) | 2.13 | 2.13 |

Table 1. Parameters of performance test when drying corn grains.

| Condition                   | Box 1 | Box 2 |
|-----------------------------|-------|-------|
| Outside Temperature (°C)    | 17.83 | 17.83 |
| Relative humidity (%)       | 92.16 | 92.16 |
| Mass of corn ear (kg)       | 20    | 20    |
| Hot air temperature(°C)     | 45    | 45    |
| Drying time (h)             | 10    | 10    |
| Kerosene consumption (kg h\(^{-1}\)) | 0.91 | 0.91 |
| Air flowrate (m\(^3\) s\(^{-1}\)) | 0.34 | 0.34 |
| Corn ear grain moisture content (%) | 27.53 | 27.53 |
| Moisture drying rate (% moisture h\(^{-1}\)) | 1.60 | 1.44 |
| Electrical energy consumption (kwh) | 2.67 | 2.67 |

Table 2. Parameters of performance test when drying corn ear.

![Figure 1. Round holes stainless steel sheet.](image)

![Figure 2. Conceptual design of corn dryer.](image)
The temperature of the grain was measured in each box by 3 thermocouples (Kawaso, Co.) located in the upper, middle, and bottom, to the center of both upper and lower boxes. The temperature data was recorded by a microprocessor and plotter. The moisture content of the grain was sampled at total 9 points with 3 repetitions from the upper, middle, and lower parts of the grain layer in each box. The average data of outdoor air conditions were obtained with the weather station.

A second test was carried out to dry ears of corn, which were placed in the boxes until forming an 80 mm layer. A procedure very similar to that of the test for drying grain was applied, except for the sampling method because the grain was removed from the cob. The amount of material placed in each box was only 20 kg because density of ears and unavailability of them. The initial content of the corn ear was 27.53%.

**Equations of Air Flowrate, Moisture Content and Drying Time**

To estimate the air flowrate needed to dry the corn grain, the following equation was used:

\[
Q = \frac{q^e}{3600 T(1-T_o)}
\]  

(1)

Where:

- \( Q \) = Air flowrate, \( m^3 \) s\(^{-1} \)
- \( q \) = Caloric value of kerosene, 11,000 kcal kg\(^{-1} \)
- \( z \) = Fuel consumption, kg h\(^{-1} \)
- \( C \) = Specific heat, 0.25 kcal kg\(^{-1} \) °C\(^{-1} \)
- \( T \) = Mean temperature of dry air, °C.
- \( T_o \) = Mean atmospheric air temperature, °C.
- \( p \) = Air density, 1.2kg m\(^{-3} \)

To estimate the corn grain and ear moisture content, the following equation was used:

\[
H_{current} = H_{storage} e^{rt}
\]  

(2)

Where:

- \( H \) = Moisture content, %.
- \( t \) = Time, h.
- \( e \) = Napier number, 2.71828
- \( H_{storage} \) = Storage crop moisture content, %.
- \( H_{current} \) = Current crop moisture content, %.
- \( r \) = Intrinsic rate of decrease of moisture content.

To estimate the drying time, the following equations was used:

\[
t = \frac{H_{storage}}{H_{initial}} \frac{1}{r}
\]  

(3)

\( H_{initial} \) = Initial crop moisture content, %.

The predictive models were exponential regression models. To obtain the \( H_{initial} \) we linearized the exponential regression models and found \( H_{initial} \) value.

**Results**

**Performance Test**

The air flow required to dry the corn grain was 0.56 m\(^3\) s\(^{-1} \) and for corn cobs it was 0.34 m\(^3\) s\(^{-1} \) both at a speed of 1810 rpm. Tables 1 and 2 show the results of the performance test of the grain dryer and corn cob.

![Figure 3. Dryer prototype(a), Duct, fan and burner(b)](image)

![Figure 4. Temperatures versus time during the corn grain drying.](image)

![Figure 5. Temperatures versus time during the corn ears drying.](image)

The function test has shown that the temperature difference between box 1 and 2 was 4.31°C for the case of corn grain while for corn cob it was 0.01. The moisture content found at the end of the test showed a difference between boxes 1 and 2 of 4.27% in the case of corn grain and for grain removed from the corn cob this was 1.35%.

**Temperature**

Figure 4 shows the temperatures in corn grain boxes during the corn drying performance tests. The highest temperatures of corn grains for storage were reached out at 6 h (48.33°C) and 5 h (52.83°C) for Box 1 and Box 2, respectively. Figure 5 shows the changes in temperatures in corn ear during the corn drying performance tests. The highest temperature of corn ear for storage in both boxes were reached out at 5h with 49.07°C for Box 1 and 50.10°C for Box 2.
Moisture Content
Corn grain moisture was tested for drying time 5, 7 and 8 hours, and corn cobs for 5, 7 and 10 because laboratory time was limited.

Figure 6 shows the changes in moisture content in corn grain boxes during the corn drying performance tests. The moisture contents of corn grains for storage were reached out at 7h (MC 13.42%) and 8 h (MC 14.72%) for Box 1 and Box 2, respectively. Figure 7 shows the changes in moisture content in both corn ear and cob during the corn drying performance tests. The moisture contents of corn ear for storage in both boxes were reached out at 7h with 14.01% for Box 1 and 13.75% for Box 2. In the case of moisture contents of corn cobs for storage reached. Moisture content varies between 12.4% and 15.1% for storage of corn cobs.

Exponential Regression Models
Figure 6 shows the regression models fitted in corn grain moisture in Box 1 and Box 2. In Box1, the exponential regression model for corn grain moisture content had an R² of 0.9143 whereas Box 2 exponential regression model had an R² was of 0.6642. Figure 7 shows the regression models fitted in corn ear moisture in Box 1 and Box 2. In Box 1, the exponential regression model for corn ear moisture content had an R² of 0.9616 whereas Box 2 exponential regression model had an R² was of 0.9400. Figure 8 shows the exponential regression models fitted in corn cob moisture in Box 1 and Box 2. Both exponential regression models for corn cob moisture content had an R² of 0.9639.

Discussion
The corn grain moisture content was reduced from 30.36% to 14.72% within 8 hours. The fuel consumption for drying was 0.55 kg h⁻¹ of kerosene. The corn ears moisture content was reduced from 27.53% to 11.55% within 10 h, while fuel consumption was 0.91 kg h⁻¹ of kerosene.

The moisture contents of corn grains for storage were reached out at 5h and 7 h for Box 1 and Box 2, respectively. The moisture contents of corn earn for storage in both boxes were reached out at 7h. The highest temperatures of corn grains for storage were reached out at 6 h and 5 h for Box 1 and Box 2, respectively. The highest temperature of corn earn for storage in both boxes were reached out at 7 h (based on Figure 4).

In Box1, the exponential regression model for corn grain moisture content had an R² of 0.9143 whereas Box 2 exponential regression model had an R² was of 0.6642. In Box1, the exponential regression model for corn ear moisture content had an R² of 0.9616 whereas Box 2 exponential regression model had an R² was of 0.9400. Both exponential regression models for corn cob moisture content had an R² of 0.9639.

Conclusions
Based on drying experiments with the dryer prototype of corn grain and ears the following can be concluded:

- Two-layer corn dryer prototype can be used to harness gas or fuel energy in order to speed up drying for storage.
• The dryer batch kept a hot air temperature of 45° during drying tests of corn grain and ears.
• The accumulated grain in both boxes was 200 mm and the airflow rate was 0.56 m³s⁻¹. The airflow rate was 0.34 m³ s⁻¹. Within 8 hours, the corn grain moisture content was able to be reduced from 30.36% to 14.72%. The fuel consumption for carrying out the drying was 0.55 kg h⁻¹ of kerosene. In lower box (Box1), the exponential regression model for corn grain moisture content had an R² of 0.9143 whereas upper box (Box 2) had an R² was of 0.6642.
• The layer of corn ears was 80 mm in depth inside each of the boxes. Over 10 hours, results showed a reduction in moisture content of the corn ears of from 27.53% to 12.90%, with a respective fuel consumption of 0.91 kg h⁻¹ of kerosene. When carried out over 10 hours, Box 1, had an R² of 0.9616 whereas Box 2 had an R² was of 0.94.
• During drying test of ears both models for corn cob moisture content had an R² of 0.9639.
• It is desirable that the dryer be tested using different heights of the grain layers or corn cobs. It is also advisable to dry using different temperatures and quantities inside the dryer in order to establish best the relationship between them.

Acknowledgments

We thank to Scientific and Technological Research Support Program (PAICYT CT1519-21) from Universidad Autónoma de Nuevo León, Mexican Ministry of Education, Mexican Council for Science and Technology as well as Japanese International Cooperation Agency for their support.

Author contributions

AILM and HRF planned the experiments, interpreted the results, and made the write up of manuscript, JAV, HFB and WA interpreted the results, ULM made the write up of manuscript and UFGG statistically analyzed the data and made illustrations.

References

Akwuah JO, Maier D, Opit G, McNeill S, Amstrong P, Campabadal C, Obeng-Akrofi G. 2018. Drying temperature effect on kernel damage and viability of maize dried in a solar biomass hybrid dryer. Open Journal of Applied Sciences, 8(11): 506.