Voltage Control Using Limited Communication

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Abstract—In electricity distribution networks, the increasing penetration of renewable energy generation necessitates faster and more sophisticated voltage controls. Unfortunately, recent research shows that local voltage control fails in achieving the desired regulation, unless there is communication between the controllers. However, the communication infrastructure for distribution systems is less reliable and less ubiquitous as compared to that for the bulk transmission system. In this paper, we design distributed voltage control that uses limited communication. That is, only neighboring buses need to communicate a few bits between each other for each control step. We investigate how these controllers can achieve the desired asymptotic behavior of the voltage regulation and we provide upper bounds on the number of bits that are needed to ensure a predefined accuracy of the regulation. Finally, we illustrate the results by numerical simulations.

Index Terms—Distributed Optimization, Smart Grid, Voltage Regulation, Reactive Power, Limited Communication.

I. INTRODUCTION

There is an increasing penetration of distributed energy resources such as renewable energy in distribution networks. Unfortunately, such a penetration causes faster voltage fluctuations than what today’s distribution networks can handle, see [1]. Therefore, to avoid overloading the distribution networks, the integration of renewable energy resources must be accompanied by faster and more sophisticated voltage regulation.

These challenges have motivated a growing research interest in voltage control, where fast voltage fluctuations are regulated through real-time reactive power injections to ensure that the voltage is maintained within an acceptable range. Such fast voltage control can be implemented in the emerging power devices such as inverters. The research efforts have focused on two main directions: local and distributed control strategies. In the local voltage control, control devices at each bus update the reactive power injections using only locally available information, such as local voltage measurements, see [2], [3], [4] and references therein. On the other hand, in distributed voltage control, control devices at each bus determine the reactive power injection with additional information communicated from its neighboring buses in the distribution network, see [5], [6], [7], [8], [9]. Local control strategies perform well in some cases, they may fail to ensure that the voltage is maintained within the accepted range in some cases, as proved by the impossibility result in [10]. Therefore, communication among the local controllers is needed to guarantee the performance of voltage regulation.

The communication capabilities of today’s distribution networks generally suffer from low data rates, [11], [12]. To compensate for this deficiency, power system operators and industries are currently investing heavily in integrating the distribution networks with a sophisticated communication infrastructure. However, even with the promising capabilities of the future low latency networks, fast real-time control applications, like voltage control, rely on short packages that carry coarsely quantized information, [13]. Therefore, it is important to develop voltage control with very limited communication for early integration of renewable resources using today’s grid limited communication capabilities and also for sustainable developments of the future smart grid.

Networked control systems with limited bandwidth communication have been well investigated [14], [15], [16]. However, standard algorithms used for stabilization of networked control systems are generally not applicable to the voltage regulation problem. Instead, most distributed voltage control algorithms in the literature are based on the tools of distributed optimization, e.g. [5], [6], [7], [8], [9]. Even though distributed optimization with limited bandwidth has received some attention [17], [18], [19], [20], none of these works fit the characteristics of the voltage control problem.

Other ways of limiting the communication of voltage control algorithms have been considered in the literature. The work in [21] proposes that the systems only communicates when there is an overvoltage in the system. Whereas the method in [22] proposes that the systems only communicates when there is an overvoltage in the system. Unlike our work, these papers do not consider bandwidth limited communication.

In this paper, we study a distributed voltage control where only a few bits of communication between neighboring buses are needed during each control step. In particular, the voltage control device on each bus determines the reactive power injection based on its local voltage measurement and current reactive power injection, in addition to a few bits of information communicated from its physical neighbors. We show that the algorithm can regulate the voltages to an acceptable range, for any predefined accuracy, in a finite number of iterations. We also provide an upper bound on the number of communicated bits (in the worst case) that are needed to ensure a predefined accuracy of the desired voltage level. Though the theoretical analysis is based on a linearized power flow model that is applicable for radial distribution...
network developed in [23], we use the nonlinear power flow model to numerically test the algorithm. Moreover, we test the performance under both static and dynamic operating conditions. Both the theoretical and numerical results confirm that reducing the communication to a few bits do not sacrifice the control performance. This opens up a large flexibility for implementing voltage control in practice. For instance it enables the use of power lines as the communication media for electricity distribution systems despite the limited bandwidth of power line communication [12].

Preliminary studies of this work appeared in [24]. However, in [24] most of the proofs are omitted (but they appear here) and all the numerical results especially with the nonlinear power flow model here are new. Moreover, the presentation and theoretical results here have been largely improved compared to [24].

A. Notation

Vectors and matrices are represented by boldface lower and upper case letters, respectively. The imaginary unit is denoted by i, i.e., \(i = \sqrt{-1}\). The set of real, complex, and natural numbers are denoted by \(\mathbb{R}\), \(\mathbb{C}\), and \(\mathbb{N}\), respectively. The set of real \(n\) vectors and \(n \times m\) matrices are denoted by \(\mathbb{R}^n\) and \(\mathbb{R}^{n \times m}\), respectively. Otherwise, we use calligraphy letters to represent represent sets. We let \(S^{n-1} = \{x \in \mathbb{R}^n | 1 = ||x||\}\) denote the unit sphere. The superscript \((\cdot)\) stands for transpose. \(\text{diag}(A_1, \ldots, A_n)\) denotes the diagonal block matrix with \(A_1, \ldots, A_n\) on the diagonal. We let ||\( \cdot ||\) denote the 2-norm. The distance between a point \(x \in \mathbb{R}^n\) and a set \(\mathcal{X} \subseteq \mathbb{R}^n\) is given by \(\text{dist}(x, \mathcal{X}) = \inf_{z \in \mathcal{X}} ||x - z||\). For a matrix \(A \in \mathbb{R}^{n \times N}\), we let \(\lambda_i(A)\), for \(i = 1, \ldots, n\) denote its eigenvalues (not in any particular order) and \(\lambda_{\max}(A) = \max_{i=1,\ldots,n} |\lambda_i(A)|\). We let \(\lfloor x \rfloor_+\) denote the projection of \(x \in \mathbb{R}^n\) into the positive orthant \(\mathbb{R}^n_+\).

II. System Model and Problem Formulation

In this section we present the power flow model, Section II-A, and the voltage regulation problem, Section II-B.

A. System Model: Linearized Power Distribution Network

Consider a radial power distribution network with \(N + 1\) buses represented by the set \(N_0 = \{0\} \cup N\), where \(N = \{1, \ldots, N\}\). Bus 0 is a feeder bus and the buses in \(N\) are branch buses. Let \(\mathcal{E} \subseteq N_0 \times N_0\) denote the set of directed flow lines, so if \((i,j) \in \mathcal{E}\) then \(i\) is the parent of \(j\). For each \(i\), let \(s_i = p_i + iq_i \in \mathbb{C}\), \(V_i \in \mathbb{C}\), and \(v_i \in \mathbb{R}_+\) denote the complex power injection, complex voltage, and squared voltage magnitude, respectively, at bus \(i\). For each \((i,j) \in \mathcal{E}\), let \(S_{ij} = P_{ij} + iQ_{ij} \in \mathbb{C}\) and \(z_{ij} = r_{ij} + iz_{ij} \in \mathbb{C}\) denote the complex power flow and impedance in the line from bus \(i\) to bus \(j\). To model the relationship between the variables, we use the linearized branch flow model from [23], which gives a good approximation in radial distribution networks:

\[
\begin{align*}
-p_i &= P_{\sigma,i} - \sum_{k : (i,k) \in E} P_{ik}, \quad i \in N, \\
-q_i &= Q_{\sigma,i} - \sum_{k : (i,k) \in E} Q_{ik}, \quad i \in N, \\
v_j - v_i &= -2r_{ij}P_{ij} - 2r_{ij}Q_{ij}, \quad (i,j) \in N,
\end{align*}
\]

where \(\sigma_i\) is the parent of bus \(i \in N\), i.e., the unique \(\sigma_i \in N_0\) with \((\sigma_i, i) \in \mathcal{E}\). By rearranging Equation (I) we get that

\[
\mathbf{v} = \mathbf{A}\mathbf{q}^\mathbf{t} + \mathbf{B}\mathbf{p}^\mathbf{t} + \mathbf{1}_0\mathbf{q},
\]

where \(\mathbf{v} = [v_1, \ldots, v_N]^\mathbf{t}\), \(\mathbf{q}^\mathbf{t} = [q_1, \ldots, q_N]^\mathbf{t}\), \(\mathbf{p}^\mathbf{t} = [p_1, \ldots, p_N]^\mathbf{t}\),

\[
\mathbf{A}_{ij} = \begin{cases} 
\frac{1}{2} \left( x_{\sigma,i}^{-1} + \sum_{k : (i,k) \in \mathcal{E}} x_{ik}^{-1} \right) & \text{if } i = j, \\
-\frac{1}{2} x_{ij}^{-1} & \text{if } (i,j) \in \mathcal{E} \\
0 & \text{otherwise,}
\end{cases}
\]

Proof: It is proved in [2] Lemma 1] that \(\mathbf{A}\) is a positive definite matrix whose inverse has the following structure

\[
\mathbf{A}^{-1} = \begin{pmatrix}
1 & \frac{1}{2} \left( x_{\sigma,i}^{-1} + \sum_{k : (i,k) \in \mathcal{E}} x_{ik}^{-1} \right) \\
\frac{1}{2} x_{ij}^{-1} & 0
\end{pmatrix}
\]

We now introduce the Voltage Regulation Problem.

B. Voltage Regulation Problem

Suppose that the real power injection \(\mathbf{p}^\mathbf{t}\) at each bus has been decided. Write the reactive power injection as \(\mathbf{q}^\mathbf{t} = \mathbf{q} + \mathbf{q}^\mathbf{U}\), where \(\mathbf{q}\) is the adjustable reactive power that can be used for voltage regulation and \(\mathbf{q}^\mathbf{U}\) denotes other reactive power injection that cannot be changed by the voltage control devices. Then the goal of the voltage regulation problem is to find feasible voltages \(\mathbf{v}\) and adjustable reactive powers \(\mathbf{q}\) so that the physical relationship (2) holds and that \(\mathbf{v}\) and \(\mathbf{q}\) are inside some feasible operation range \([\mathbf{v}^{\mathbf{\min}}, \mathbf{v}^{\mathbf{\max}}]\) and \([\mathbf{q}^{\mathbf{\min}}, \mathbf{q}^{\mathbf{\max}}]\), respectively. Formally, the voltage regulation problem is to find the reactive power injection \(\mathbf{q}\) so that,

\[
\begin{align}
\mathbf{v} &= \mathbf{A}\mathbf{q} + \mathbf{d}, \\
\mathbf{v}^{\mathbf{\min}} &\leq \mathbf{v} \leq \mathbf{v}^{\mathbf{\max}}, \\
\mathbf{q}^{\mathbf{\min}} &\leq \mathbf{q} \leq \mathbf{q}^{\mathbf{\max}},
\end{align}
\]

where \(\mathbf{d} := \mathbf{A}\mathbf{q}^\mathbf{U} + \mathbf{B}\mathbf{p}^\mathbf{t} + \mathbf{1}_0\mathbf{q}\). Throughout the paper we implicitly assume that the voltage regulation problem has a solution.

The results also directly apply to the linearized power flow model in [10]. The linearized model is for the purpose of deriving the control algorithm and analyzing the theoretical performance. The designed control algorithms can be applied to the nonlinear distribution networks. In Section V, we use the nonlinear power flow model to numerically test the algorithm performance.
Assumption 1. There exists \( q \in \mathbb{R}^N \) satisfying Equation (4).

Our problem of voltage control is to design a distributed control for finding the feasible reactive power injections and voltages that satisfy equation (4) that works under any operating condition denoted by \( d \). In particular, where each bus controls its reactive power based only on local information and a limited number of bits communicated from neighboring buses. That is, each bus \( i \in \mathcal{N} \) updates its reactive power injection according to

\[
q_i(t+1) = K_i(\text{Local}_i(t), \text{Comm}_i(t)),
\]

where \( t \) is the iteration index and \( K_i(\cdot) \) is the control law at bus \( i \). The function \( K_i(\cdot) \) depends on the local information

\[
\text{Local}_i(t) = (q_i(0), \ldots, q_i(t), v_i(0), \ldots, v_i(t)),
\]

and the communicated information that bus \( i \) has received from its neighbors

\[
\text{Comm}_i(t) = ((b_j(0))_{j \in \mathcal{N}_i}, \ldots, (b_j(t))_{j \in \mathcal{N}_i}),
\]

where \( \mathcal{N}_i = \{ j \in \mathcal{N} | (i, j) \in \mathcal{E} \text{ or } (i, j) \in \mathcal{E} \} \) and \( b_j(t) \) is the information that bus \( j \) communicates to its neighbors at iteration \( t \). We study how such control laws can be achieved when \( b_j(t) \) contains a limited number of bits.

Note that the problem can generally not be solved without communication, i.e., with \( \text{Comm}_i(t) \) empty for all \( i \) and \( t \), as proved by the impossibility result in [10]. Some authors have proposed distributed solution algorithms where only neighbors in the power networks communicate, see [5], [6], [7], [8]. This is challenging in practice because the communication infrastructure for distribution systems is less reliable and less ubiquitous as compared to that for the bulk transmission system. To compensate for that, we study limited communication voltage control algorithms where controllers only communicate a few bits to their neighbors. These algorithms are based on combining the ideas from the voltage control algorithms in [7], [8] and the limited communication gradient methods in [19]. However, the algorithms and results in [19] are not directly applicable here because the communication structure is different and some of the assumptions in [19] do not hold for the voltage regulation problem.

III. VOLTAGE CONTROL WITH LIMITED COMMUNICATION

We present our limited communication algorithm for the voltage control problem in Section III-A. We highlight the convergence properties of the algorithm in Section III-B.

A. Algorithm

The following algorithm is an instance of the control algorithm in Equation (5) where each bus communicates only 2-bits per iteration.

**VC-LB Algorithm: Voltage Control - Limited Bandwidth**

\[ \text{a) Initialization: Set } t = 0, \text{ and for each bus } i \in \mathcal{N} \text{ set} \]

\[
\lambda_i(0) = (\lambda_i^{\min}(0), \lambda_i^{\max}(0)) = (0, 0),
\]

\[
\mu_i(0) = (\mu_i^{\min}(0), \mu_i^{\max}(0)) = (0, 0).
\]

where the variables \( \lambda_i(t), \lambda^{\max}_i(t), \mu^\min_i(t), \) and \( \mu^{\max}_i(t) \) are dual variables related to violating the bounds in equations (4c) and (4d), see Section IV for details.

\[ \text{b) Local Computation: Each bus } i \in \mathcal{N} \text{ computes its next reactive power injection as follows} \]

\[
q_i(t+1) = \lambda_i^{\min}(t) - \lambda_i^{\max}(t) + \sum_{j \in \mathcal{N}_i} a_{ij}(\mu_j^{\min}(t) - \mu_j^{\max}(t)).
\]

Bus \( i \) can then also compute the communicated signal

\[
b_i(t+1) = \text{sign}
\[
[ q_i(t+1) - \mu_i^{\max}, q_i^{\min} - q_i(t+1) ].
\]

\[ \text{c) Local Control: Each bus } i \in \mathcal{N} \text{ injects the reactive power } q_i(t+1) \text{ into the power network.} \]

\[ \text{d) Local Measurement: Each bus } i \in \mathcal{N} \text{ measures the voltage magnitude } v_i(q(t+1)), \text{ given by the physical relationship (4a).} \]

\[ \text{e) Communication: Each bus } i \in \mathcal{N} \text{ communicates } b_i(t+1) \text{ to each of its neighbours } j \in \mathcal{N}_i \text{ using a two bits.} \]

\[ \text{f) Local Computation: Each bus } i \in \mathcal{N} \text{ updates its dual variables} \]

\[
\lambda_i(t+1) = \left[ \lambda_i(t) + \alpha \left[ v_i(q(t+1)) - v_i^{\max} \right] \right]_+, \]

\[
\mu_i(t+1) = [\mu_i(t) + \beta b_i(t)]_+. \]

Bus \( i \) also updates a local copy of \( \mu_j(t+1) \) for each neighbour \( j \in \mathcal{N}_i \) using Equation (9).

\[ \text{g) Update Iteration Index: } t = t + 1 \text{ and go to step b).} \]

This algorithm satisfies the structure of Equation (5). This can be seen by noting that \( \lambda_i(t) \) is a function of \( \text{Local}_i(t) \) via Equation (8) and \( \mu_i(t) \) is a function of \( \text{Local}_i(t) \) and \( \text{Comm}_i(t) \) via Equations (7) and (9). The algorithm is easy to implement since the local computation step is based on a numerical operation, moreover, for the communication step each bus only needs to communicate 2 bits of information since \( b_i(t) \) can only take one of the \( 2^2 = 4 \) values \((-1, -1), (1, 1), (1, -1), \) and \((-1, 1)\). The parameters \( \alpha, \beta > 0 \) are step-sizes and are discussed further in the next section.

**Remark 1.** We have considered the extreme case when only 2-bits are communicated per iterations to make the algorithm analysis more manageable. It is possible that, using more bits, can improve performance and studying such trade-offs would be an interesting extension to this work. However, from both the theoretical results and numerical simulations, 2-bits communication voltage control can achieve a comparable performance as the non-quantized counterpart for our problem.

**B. Main Convergence Results**

We now study the converge of the VC-LB Algorithm to a solution to the voltage regulation problem. We show that in finite number of iterations the reactive power \( q(t) \) and voltage \( v(q(t)) \) satisfy Equation (4) approximately and exactly under mild additional assumptions. We measure the feasibility of
reactive power $q \in \mathbb{R}^N$ (and the associated voltage $v(q) \in \mathbb{R}^N$) as follows
\[
\text{fes}(q) = \text{dist}((q, v(q)), Q \times \mathcal{V}),
\]  
where $Q = [q_{\min}, q_{\max}]$ and $\mathcal{V} = [v_{\min}, v_{\max}]$.

The following theorem (proved in Section V-B) establishes that the VC-LB Algorithm can solve the problem up to any $\epsilon > 0$ accuracy in finite number of iterations if the step-sizes are chosen appropriately.

**Theorem 1. (Approximate Solution)** Let $\epsilon \in (0, 1]$ and choose the step-sizes $\alpha, \beta > 0$ such that
\[
\alpha = \frac{1}{L} \quad \text{and} \quad \beta = \frac{\epsilon}{4N^{3/2}L},
\]
where
\[
L = \max_{i=1,\ldots,N} \left( \lambda_i(A) + \frac{1}{\lambda_i(A)} \right).
\]
Then there exists $T \in \mathbb{N}$ such that $\text{fes}(q(T)) \leq \epsilon$ where $T$ is upper bounded by
\[
T \leq \left[ \frac{16N^3L\lambda_{\max}(A)}{\epsilon^2} \right],
\]
where $Q = \max \{ (q_{\min}^i)^2, (q_{\max}^i)^2 : i = 1, \ldots, N \}$.

Theorem 1 shows that the VC-LB Algorithm can solve the voltage regulation problem to any precision in finite number of iterations and using finite number of communicated bits. In particular, the theorem shows that any $\epsilon > 0$ accuracy can be reached by communicating $O(1/\epsilon^2)$ bits. This is comparable to convergence rate without quantization. This follows from the fact that the VC-LB Algorithm is a quantized version of a dual gradient method where the primal variable is $q$ and the dual gradient is Lipschitz continuous. See Section V. Under these assumptions the feasibility of the primal iterates $q(t)$ of dual gradient methods (with constant step-size) is $O(1/\epsilon^2)$, see, for example [22]. We note that to compute $L$ requires the knowledge of $A$. However, since $A$ is generally not changing $L$ needs to be computed once and can then be used every time when the algorithm runs.

In practice, we often like to run the algorithm over an extended period of time. Therefore, it is desirable that once the algorithm converges to some $\epsilon > 0$ accuracy then it does not oscillate much away from that accuracy. We show this numerically in Section V. However, it is hard to prove this analytically due to technical difficulties explained in Section IV-C. Nevertheless, the following theorem (proved in Section V-C) shows that there exist step-sizes that ensure that any $\epsilon > 0$ accuracy is held for all sufficiently large $t$.

**Theorem 2.** Suppose that the voltage regulation problem is strictly feasible, i.e., there exists some $q \in \mathbb{R}^N$ such that
\[
q \in (q_{\min}^i, q_{\max}^i) \quad \text{and} \quad v(q) \in (v_{\min}^i, v_{\max}^i).
\]
Then for any $\epsilon > 0$ there exist step-sizes $\alpha, \beta > 0$ and $T \in \mathbb{N}$ such that
\[
\text{fes}(q(t)) \leq \epsilon, \quad \text{for all} \quad t \geq T.
\]

We can also use the VC-LB Algorithm to solve the voltage regulation problem exactly provided a mild additional assumption. In particular, if we use the VC-LB Algorithm to solve the restricted voltage regulation problem of finding reactive power $q$ that solves
\[
q \in [q_{\min}^i + 1\rho, q_{\max}^i - 1\rho], \quad v(q) \in [v_{\min}^i + 1\rho, v_{\max}^i - 1\rho],
\]
for some $\rho > 0$. Then any $\epsilon = \rho$ accurate solution to the voltage regulation problem in Equation (14) is an exact solution to the original problem. Hence, we can apply Theorem 1 to find an exact solution in finite number of iterations where each bus communicates finite number of bits.

**Corollary 1.** (Exact Solution). Let $\rho > 0$ be given and consider the VC-LB Algorithm for solving the restricted voltage regulation problem in Equation (14). Moreover, suppose restricted the voltage regulation problem in Equation (14) is feasible. Choose the step-sizes $\alpha, \beta > 0$ such that
\[
\alpha = \frac{1}{L} \quad \text{and} \quad \beta = \frac{\rho}{4N^{3/2}L}.
\]
Then there exists $T \in \mathbb{N}$ such that $\text{fes}(q(T)) \leq 0$ where $T$ is upper bounded by
\[
T \leq \left[ \frac{16N^3L\lambda_{\max}(A)}{\rho^2} \right].
\]

The parameter $\rho$ should be chosen so that the intervals in Equation (14) are not empty. Also note that increasing $\rho$ restricts the set of feasible voltages $v(q) \in [v_{\min}^i + 1\rho, v_{\max}^i - 1\rho]$, which must be non empty for the theorem to hold.

**C. Implementation without Violating Capacity Constraint**

As shown in Section III-A and III-B while the VC-LB algorithm can guarantee that the reactive power $q(t)$ will reach the capacity constraint $[q_{\min}^i, q_{\max}^i]$ (approximately), $q(t)$ may still violate these limits during the transient. This can be problematic since many physical control devices do not allow violating the capacity constraint for an extended amount of time. One way to reduce this violation is to use a smaller step size $\alpha$. By doing this, the voltage constraint multiplier $\lambda(t)$ will update slower compared to the capacity constraint multiplier $\mu(t)$, hence putting more priority on enforcing the capacity constraint. We illustrate this in simulations, see Section V.

We now propose an alternative implementation of the VC-LB algorithm that meets the reactive capacity constraint during the transients inspired by [26, 27]. At time $t$, instead of implementing $q_i(t)$ that may violate the capacity constraint, we implement $q_i^{phy}(t)$, defined to be the projection of $q_i(t)$ in terms of available parameters.

\[2\text{Similar convergence results can be ensured for any step-size } \alpha, \beta > 0 \text{ giving in Proposition 2 in Section IV-B in which case the upper bound in Equation (12) is replaced by (23). However, we present the results here using these particular step-sizes to get an explicit form on the upper bound in (12) in terms of available parameters.}

\[3\text{Note that this is a stronger requirement that given by Assumption 1.} \]
onto the capacity constraint set \([q_i^{\min}, q_i^{\max}]\). Mathematically, we implement \(q_i^{phy}(t + 1) = \max(\min(q_i(t + 1), q_i^{\max}), q_i^{\min})\). Here the superscript in variable \(q_i^{phy}(t)\) refers to “physical”, which is to emphasize that \(q_i^{phy}(t)\) is the amount of reactive power this is physically implemented. Clearly, \(q_i^{phy}(t)\) will always satisfy the capacity constraint. We formally introduce the revised VC-LB below.

**VC-LB with Projection (VC-LB-P)**

\(a\) **Initialization:** The same as VC-LB Algorithm.

\(b\) **Local Computation:** The same as VC-LB Algorithm.

\(c\) **Local Control:** Each bus \(i \in \mathcal{N}\) implements \(q_i^{phy}(t + 1) = \max(\min(q_i(t + 1), q_i^{\max}), q_i^{\min})\) into the power network.

\(d\) **Local Measurement:** Each bus \(i \in \mathcal{N}\) measures the voltage magnitude \(v_i(q_i^{phy}(t + 1))\), given by the physical relationship (4a).

\(e\) **Communication:** The same as VC-LB Algorithm.

\(f\) **Local Computation:** Each bus \(i \in \mathcal{N}\) updates its dual variables

\[
\lambda_i(t+1) = \left[ \lambda_i(t) + \alpha \left( v_i(q_i^{phy}(t + 1)) - v_i^{\min} \right) \right] + \frac{1}{\beta} \; (16)
\]

\[
\mu_i(t+1) = [\mu_i(t) + \beta b_i(t)] +. \quad (17)
\]

Bus \(i\) also updates a local copy of \(\mu_j(t + 1)\) for each neighbor \(j \in \mathcal{N}_i\) using Equation (17).

\(g\) **Update Iteration Index:** \(t = t + 1\) and go to step b).

The difference between VC-LB-P with the original VC-LB lies in step c), d), f). In step c), we implement \(q_i^{phy}(t + 1)\) instead of \(q_i(t + 1)\). As a result, in step d) the measured voltage becomes \(v_i(q_i^{phy}(t + 1))\) instead of \(v_i(q_i(t + 1))\), and correspondingly in step f), update equation (16) uses \(v_i(q_i^{phy}(t + 1))\) instead of \(v_i(q_i(t + 1))\).

We now explain the rationale behind the new implementation VC-LB-P. Note that in VC-LB-P, the update equation for Lagrangian multiplier \(\mu_i(t)\) and variable \(q_i(t)\) is kept the same as VC-LB. This means that \(\mu_i(t)\) still reflects the capacity constraint violation of \(q_i(t)\), so \(q_i(t)\) will still meet the capacity constraint asymptotically. And therefore \(q_i(t) - q_i^{phy}(t) \rightarrow 0\), i.e., the projection step will not substantially change the convergence results established in Section III-B. We note that similar projection steps have been done in [26, 27] and WC has theoretically shown that under the projection step, a modified primal-dual algorithm can still converge. Though we cannot rigorously prove the convergence of VC-LB-P in this paper, we will conduct extensive simulation to verify the convergence of VC-LB-P.

## IV. Convergence Analysis

The goal of this section is to prove the convergence results from the previous section. We give preliminary results in Section IV-A and then prove Theorems 1 and 2, respectively, in Sections IV-B and IV-C. Readers that not interested in these proofs can go straight to Section V with no loss of information.

### A. Preliminaries: Duality Theory

We prove that the algorithm converges to an approximate solution to the following optimization problem

\[
\begin{align*}
\text{minimize} & \quad \frac{1}{2} q^T A q \\
\text{subject to} & \quad v^{\min} \leq v(q) \leq v^{\max} \\
& \quad q^{\min} \leq q \leq q^{\max}.
\end{align*}
\]

Problem (18) is convex because of Proposition 1. Its dual is

\[
\begin{align*}
\text{maximize} & \quad D(z) \\
\text{subject to} & \quad z = (\lambda, \mu) \\
& \quad \lambda \geq 0,
\end{align*}
\]

where \(\lambda = (\lambda^{\min}, \lambda^{\max})\) and \(\mu = (\mu^{\min}, \mu^{\max})\) are the dual variables associated to the constraints \(v^{\min} \leq v(q) \leq v^{\max}\) and \(q^{\min} \leq q \leq q^{\max}\), respectively, and \(D : \mathbb{R}^{4N} \rightarrow \mathbb{R}\) is the dual function, see Chapter 5 in [28] for the details. The dual gradient is

\[
\nabla D(z) = \left[ \nabla^\lambda D(z) \quad \nabla^\mu D(z) \right] \quad (19)
\]

where

\[
\nabla^\lambda D(z) = \left[ v^{\min} - v(q(z)) \quad v(q(z)) - v^{\max} \right], \quad \nabla^\mu D(z) = \left[ q^{\min} - q(z) \quad q(z) - q^{\max} \right],
\]

and

\[
q(\lambda, \mu) = \lambda^{\min} - \lambda^{\max} + \lambda^{-1} \mu^{\min} - \lambda^{-1} \mu^{\max}. \quad (20)
\]

In Lemma 1 we show that \(\nabla D(\cdot)\) is L-Lipschitz continuous, with L given in the lemma. Therefore, the gradient descent method

\[
\begin{align*}
\lambda(t+1) &= [\lambda(t) + \gamma \nabla^\lambda D(\lambda(t), \mu(t))]_+ \quad (22a) \\
\mu(t+1) &= [\mu(t) + \beta \text{sign}(\nabla^\mu D(\lambda(t), \mu(t)))]_+. \quad (22b)
\end{align*}
\]

converges to the set of optimal dual variables for appropriate step-size \(\gamma\) [29, Chapter 2]. The work in [7], [8], [10] shows how the dual gradient iterations in Equations (22a) and (22b) can be implemented in a distributed manner among the buses so that only neighbouring buses need to communicate per iteration. However, these algorithms communicate real numbers, which is challenging in practice as communication among controllers is generally constrained to low data rates. To compensate for that, we have presented the VC-LB Algorithm in Section III which can be equivalently be written as follows:

\[
\begin{align*}
\lambda(t+1) &= [\lambda(t) + \alpha \nabla^\lambda D(\lambda(t))]_+ \quad (23a) \\
\mu(t+1) &= [\mu(t) + \beta \text{sign}(\nabla^\mu D(\mu(t)))]_+. \quad (23b)
\end{align*}
\]

where \(\alpha, \beta > 0\) are step-sizes and the primal variables are updated according to (21). We now prove Theorem 1 and 2 by considering the VC-LB Algorithm on the form in Equation (23).
B. Proof of Theorem 1

We now prove Theorem 1. The main step of the proof is illustrated in the following result (proved in Appendix B).

**Proposition 2.** Suppose $\epsilon > 0$ and $z = (\lambda, \mu) \in \mathbb{R}_+^N$ are such that $V(z) > \epsilon$ where

$$V(z) = ||z - [z + \nabla D(z)]_+||.$$

Choose the step-sizes $\alpha, \beta > 0$

$$\alpha < \frac{2}{L}, \quad \beta < \min \left\{ \frac{\epsilon}{2N^{3/2} L^{2}}, \sqrt{\frac{\alpha(1 - L\alpha/2)^2}{2NL}} \right\}. \quad (25a) \quad (25b)$$

Then for

$$\bar{z} = (\bar{\lambda}, \bar{\mu}) = \left[ \begin{array}{c} \lambda \\ \mu \end{array} \right] + \frac{\alpha V^2 D(\lambda)}{\beta} \text{sign}(\nabla \mu D(\mu))$$

following holds

$$D(\bar{z}) - D(z) \leq D^*(z) + \delta(\alpha, \beta), \quad (26)$$

where

$$\delta(\alpha, \beta) = \min \left\{ \left( \frac{L^2}{2} \right) \frac{2NL\beta^2}{2N^{3/2} L^{2}} \right\} > 0 \quad (27)$$

where $L$ is a Lipschitz constant on $\nabla D(\cdot)$.

From Lemma 2 in Appendix A we have that $\text{fes}(q(z)) \leq V(z)$. Hence, Proposition 2 shows that for all $\epsilon > 0$, we can choose step-sizes $\alpha, \beta > 0$ such that if $V(z) > \epsilon$ then the dual objective function value is improved by taking a step of the algorithm in Equations (25a) and (25b). Using this intuition, we have the following result.

**Proposition 3.** Consider the VC-LB Algorithm and take some $\epsilon > 0$. Choose the step-sizes $\alpha, \beta > 0$ as in Equations (25a) and (25b). Then there exists $T \in \mathbb{N}$ such that $\text{fes}(q(T)) \leq V(z) \leq \epsilon$ where $T$ is upper bounded by

$$T \leq \left[ \frac{D^* - D(z(0))}{\delta(\alpha, \beta)} \right]. \quad (28)$$

Proof: Suppose that $V(z(t)) > \epsilon$, for $t = 0, \ldots, T_0 - 1$, where $T_0 := \left[ \frac{D^* - D(z(0))}{\delta(\alpha, \beta)} \right]$. Then by Proposition 2 we have that $D(z(t)) \geq D(z(t-1)) + \delta(\alpha, \beta)$ for $t = 0, \ldots, T_0$ or

$$0 \leq D^* - D(z(T_0)) \leq D^* - D(T_0 - 1) - \delta(\alpha, \beta) \leq D^* - D(z(0)) - \delta(\alpha, \beta) \leq 0,$$

where the last inequality comes by that $T_0 \geq \left[ \frac{D^* - D(z(0))}{\delta(\alpha, \beta)} \right]$. Hence, $z(T_0)$ is an optimal solution to the dual problem in Equation (19) and $q(z(T_0))$ is an optimal solution to the primal problem in Equation (18) implying $V(z(T_0)) = 0 \leq \epsilon$ from Lemma 2.

Theorem 1 follows from Proposition 3. Direct calculation shows that the step-sizes in Equation (11) satisfy the condition given in Equations (25a) and (25b). Therefore, we just have to show for $\alpha$ and $\beta$ in Equation (11) following holds

$$\frac{D^* - D(z(0))}{\delta(\alpha, \beta)} \leq \frac{16N^3 L^2 Q \lambda_{\max}(A)}{\epsilon^2} \quad (29)$$

to conclude the proof. Equation (29) follows directly from the following two identity (proved below):

$$\delta(\alpha, \beta) = \frac{3\epsilon^2}{16N^2 L^2}, \quad \text{and} \quad D^* - D(z(0)) \leq \lambda_{\max}(A) N Q,$$

for all $\hat{q} \in [q_{\min}, q_{\max}]$ such that $V(\hat{q}) \in [v_{\min}, v_{\max}]$. The equality is obtained by plugging $\alpha$ and $\beta$ from Equation (11) into Equation (27). To prove the inequality we note that

$$D^* = (q^*)^T A^T q^*$$

because of the strong duality and

$$D(z(0)) = \min_{\hat{q} \in \mathbb{R}^N} \frac{1}{2} (q^*)^T A q^* = 0,$$

yielding

$$D^* - D(z(0)) \leq (q^*)^T A q^* \leq \lambda_{\max}(A) \|q^*\|^2 \leq \lambda_{\max}(A) N Q.$$

C. Proof of Theorem 2

We now prove Theorem 2 due to space limitation the proof is given in the extended version of this paper found in [30].

**Proposition 4.** Suppose that the voltage regulation problem is strictly feasible, i.e., there exists some $q \in \mathbb{R}^N$ such that

$$q \in [q_{\min}, q_{\max}] \quad \text{and} \quad v(q) \in [v_{\min}, v_{\max}].$$

Define the set $\mathcal{E}(z) = \{ z \in \mathbb{R}_+^N | V(z) \leq \epsilon \}$ and the function $F(z) = \inf \{ D(z) | z \in \mathcal{E}(z) \}$. Then following holds:

a) There exists $\kappa > 0$ such that the set $\mathcal{E}(z)$ is bounded and $F(z) > -\infty$ for all $\epsilon \leq \kappa$.

b) We have $\lim_{t \rightarrow \infty} F(z(t)) = f^*$.

c) For any $\epsilon > 0$, step-sizes $\alpha, \beta > 0$ chosen as in Equations (25) and $T \in \mathbb{N}$ such that $V(z(T)) \leq \epsilon$ we have

$$D(z(t)) \geq F(z) - \frac{L}{2} \beta^2, \text{ for all } t \geq T. \quad (30)$$

From Proposition 3 and Proposition 4 we have that for any $\eta > 0$ there exist exit stepsizes $\alpha, \beta > 0$ and $T \in \mathbb{N}$ such that $D^* - D(z(t)) \leq \eta$ holds for all $t \geq T$. From Lemma 5 in Appendix A there exists $\eta > 0$ such that if $D^* - D(z) \leq \eta$ then $\text{dist}(z, z^*) \leq \epsilon/\phi$, where $\phi = ||G||$ and

$$G = \left( \begin{array}{cccc} 1 & -1 & A^{-1} & -A^{-1} \\ 0 & 0 & A & A^{-1} \\ 0 & 0 & -A & I \\ 0 & 0 & I & -I \end{array} \right).$$

Therefore, there exists $\alpha, \beta > 0$ and $T \in \mathbb{N}$ such that $\text{dist}(z(T), z^*) \leq \epsilon/\phi$ for all $t \geq T$. We also have for $z \in \mathbb{R}^N$, by setting $z^* = \min_{z \in z} ||z - z||$, that

$$\text{fes}(q(z)) \leq \frac{1}{2} ||(q(z), v(q(z))) - (q(z^*), v(q(z^*)))||,$$

$$= ||G(z - z^*)|| \leq \phi ||z - z^*|| = \phi \text{dist}(z, z^*),$$

where we have used that $(q(z), v(q(z))) = Gz + (0, d)$. Therefore, $\text{fes}(q(T)) = \text{dist}(z(T), z^*) \leq \epsilon$ for all $t \geq T$.
Fig. 1: The 56 bus network used in our simulation.

Fig. 2: Convergence of the $v(t)$ and $q(t)$ in the VC-LB Algorithm. Parameters are $\alpha = 0.2, \beta = 10^{-5}, \rho = 0$. Notice that during each iteration, each node uses 2-bits to communicate.

V. NUMERICAL RESULTS USING NON LINEAR POWER FLOW

We test our algorithm on the 56-bus radial distribution network in [31], as shown in Figure 1. Bus 1 is the feeder bus, and there are PVs installed at bus 33, 40, 45, 55. All quantities, when the nominal value of voltage is 12kV. Throughout the simulation we set $v_{\text{min}} = 11.4kV$, $v_{\text{max}} = 12.6kV \pm 5\%$ of the nominal value, and for each bus $i \in \mathcal{N}$, we set $q_i^U = 0$, $q_i^{\text{min}} = -0.5$ MW, and $q_i^{\text{max}} = 0.5$ MW. The power flow is calculated using MATPOWER [32] which uses the full nonlinear power flow instead of the linearized power flow in our analysis. We demonstrate the proposed algorithm in static and dynamic voltage control scenarios.

A. Static Voltage Control

We first test the case in which the real power injection $p_i$ is fixed and is from the load data in [31], except we have scaled up the load from bus 7 to bus 19 to make the problem more challenging. The parameters of the algorithm is set as $\alpha = 0.2, \beta = 10^{-5}$ and $\rho = 0$. Fig. 2 illustrates the voltage profile and the reactive power injection trajectory under VC-LB. The results show that the voltage converge to the feasible range within roughly 400 iterations, or 800 bits of communication. Similarly, the reactive power converges to the feasible range within roughly 1200 iterations, or 2400 bits of communication.

Fig. 3 demonstrates the convergence of VC-LB under different step-sizes $\alpha, \beta$ and parameter $\rho$ (recall $\rho$ is introduced to find an exact solution, see Corollary 1). It plots the feasibility measure $\text{fes}(q(t))$ in Equation (10) as a function of iteration counts. First of all, Fig. 3 shows that when $\rho = 0$, the algorithm converges to an approximately feasible point, within certain accuracy. Further, there is a trade-off between how high the accuracy is and how many communication bits are needed to achieve that accuracy. Secondly, for the $\rho > 0$ case, Fig. 3 demonstrates our algorithm is indeed driving the system towards an exact solution, consistent with Corollary 1.

We comment that the step-sizes in Equation (11) are conservative. For the parameters of this network, we can calculate $L \approx 7 \times 10^3$, so the step-sizes in Equation (11) are very small ($\alpha \approx 10^{-4}, \beta \approx 6 \times 10^{-7}$ using $\epsilon = 1$), leading to very slow convergence, as illustrated in the blue curve in Fig. 3. On the contrary, the results in Fig. 2 and Fig. 3 have shown that in practice fast convergence can be obtained for step-sizes that are much larger than (11). This is because to obtain the theoretical guarantees we must account for every potential worst-case behavior and also make some relaxations to make the mathematical derivations tractable. This is a typical trade-off between theoretical convergence guarantees and the convergence in practice, as discussed for example in [28].

We note that in Fig. 2 though the reactive power injection meets the capacity constraint asymptotically, it violates the constraint during the transient. As discussed in Section III-C we now test the two methods to deal with this. Firstly, we test the VC-LB algorithm with a small $\alpha$, which as discussed in Section III-C, will put more priority on enforcing capacity constraint. We use the same simulation setting and step sizes as Fig. 2 except that $\alpha$ is reduced to 0.08 ($\beta = 10^{-5}, \rho = 0$ are kept the same). Results are shown in Fig. 4. Compared
in Fig. 6, The figure shows that in all cases the VC-LB-P Algorithm regulates the voltage profile within the 500-iteration (1000-bit) limit and in the meanwhile not violating the reactive power capacity constraint at any time. We further note that the time it takes to conduct a 1-bit communication, when using protocols for extremely low latency communications [13] (at the cost of limited data-rate), can be made extremely small. This suggests that the VC-LB-P Algorithm in this paper can be used to provide fast voltage regulation in future smart grids.

VI. CONCLUSION

This paper studied distributed voltage control algorithms where only a few bits of communication between neighboring buses are needed. The convergence of these algorithms was studied and their practical applicability illustrated in simulations. Future work is to 1) study the trade-offs between the data rate and control performance, 2) characterize the online performance under dynamic operating scenarios, and 3) implement the algorithm on a real-world testbed.

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APPENDIX A

IMPORTANT LEMMAS

Lemma 1. We have $\nabla D(z) = Mz + r$, where

$$M = \begin{pmatrix}
-A & A & -I & I \\
A & -A & I & -I \\
-I & I & -A^{-1} & A^{-1} \\
I & -I & A^{-1} & -A^{-1}
\end{pmatrix}.$$ (31)

The eigenvalues of $M$ are

$$\lambda_i(M) = -2 \left( \lambda_i(A) + \frac{1}{\lambda_i(A)} \right), \quad \text{for } i = 1, \ldots, n \quad (32)$$

and $\lambda_1(M) = 0$ for $i = n + 1, \ldots, 4n$.

Proof: The fact that $\nabla D(z) = Mz + r$ follows from Equations (20) and (21). To find the eigenvalues of $M$, let $w_i \in \mathbb{R}^n$ be an eigenvector of the matrix $A$ associated to the eigenvalue $\lambda_i(A)$. Then direct calculations show that $Mv_i = \lambda_i(M)v_i$ with $\lambda_i(M)$ defined in Equation (32), where $v_i = (\lambda_i(A)w_i, -\lambda_i(A)w_i, w_i, -w_i)$.

To prove that 0 is an eigenvalue of $M$ with multiplicity $3n$, i.e., $\lambda_1(M) = 0$ for $i = n + 1, \ldots, 4n$, we note that $M$ is a rank $n$ matrix and hence has a $3n$ dimensional null space. This can be seen by noting that the rows 2, 3, and 4 of the block matrix $M$, see Equation (31), can be obtained from elementary row operations (Gauss elimination) on the first row of $M$. In particular, $R_2 = -R_1$, $R_3 = AR_1$, $R_4 = -AR_1$, where $R_i$ is the $i$-th row of the block representation of $M$ given in Equation (31).

Lemma 2. For $V(\cdot)$ defined in Equation (24) we have:

a) A feasible dual variable $z \in \mathbb{R}_{+}^{4N}$ is an optimal solution to the Dual Problem (19) if and only if $V(z) = 0$.

b) For all $z \in \mathbb{R}_{+}^{4N}$ $f_{es}(q(z)) \leq V(z)$, where $q(z)$ is defined in Equation (21).

Proof: a) Follows from [19, Lemma 3].

b) We have that

$$f_{es}(q(z)) = \begin{pmatrix}
\min (q(z)) \\
\min (q(z)) \\
\max (q(z)) \\
\max (q(z))
\end{pmatrix} = \|\nabla D(z)\|_+,$$

where the last equality comes from Equation (20). Using that

$$\|\nabla D(z)\|_+ \leq \|z_i - z_i + \nabla_i D(z)\|_+$$

for $i = 1, \ldots, 4N$, we get that

$$\|\nabla D(z)\|_+^2 = \sum_{i=1}^{4N} (\nabla_i D(z))^2_+ \leq \sum_{i=1}^{4N} [z_i - z_i + \nabla_i D(z)]_+^2 = V(z)^2,$$

which proves the result.
Lemma 3. For all \( \beta \in [0, 1] \), \( z \in \mathbb{R} \) and \( x, \alpha_1, \alpha_2 \in \mathbb{R}_+ \) with \( \alpha_1 \leq |x - [x + z]|_+ \) the following holds

\[
\begin{align*}
\beta|x - [x + z]|_+ &\leq |x - [x + \beta z]|_+ \quad (33) \\
\alpha_1 &\leq |x - [x + \alpha_1 \text{sign}(z)]_+| \quad (34) \\
0 &\leq z([x + \alpha_2 z]|_+ - x). \quad (35)
\end{align*}
\]

Proof: The proof follows similar steps as the proof of Lemma 9. In particular, the inequalities (33) and (34) are easily checked by using that for \( x \in \mathbb{R}_+ \) and \( z \in \mathbb{R} \) we have \( |x - z|_+ = |z| \) if \( x + z \geq 0 \) and \( |x - z|_+ = x \) if \( x + z \leq 0 \). The Inequality (35) comes by rearrange the inequality \( \text{sign}(z)[x + \alpha_1 z]_+ \leq \text{sign}(z)x \) and \( |z| \) on both sides. \( \blacksquare \)

Lemma 4. Suppose that the voltage regulation problem is strictly feasible, i.e., there exist some \( q \in \mathbb{R}^N \) such that \( q \in (q_{\min}, q_{\max}) \) and \( v(q) \in (v_{\min}, v_{\max}) \). Then the set \( \mathcal{Z}^* \) of optimizers of the dual problem given in Equation (29) is bounded.

Proof: Follows directly from Lemma 1 in [33]. \( \blacksquare \)

Lemma 5. For \( \epsilon > 0 \), there exists \( \eta > 0 \) such that if \( \|D^* - D(z)\|_\eta \leq \epsilon \) then \( d(z, \mathcal{Z}^*) \leq \epsilon \).

Proof: We prove this by contradiction. Suppose that no such \( \eta > 0 \) exists. Then we can generate a sequence \( z_k \in \mathbb{R}_+ \) such that \( \lim_{k \to \infty} D(z_k) = D^* \) and \( d(z_k, \mathcal{Z}^*) > \epsilon \) for all \( k \in \mathbb{N} \). The sequence \( z_k \) is bounded because \( \mathcal{Z}^* \) is bounded, see Lemma 4. Therefore, the level sets \( L(\kappa) = \{ z \in \mathbb{R}_+^N \mid |D(z)| \geq \kappa \} \) are also bounded, see Proposition B.9. As a result, \( z_k \) has a convergent subsequence \( z_{k_r} \) with \( \lim_{r \to \infty} z_{k_r} = z \in \mathbb{R}_+ \). Then \( D(z) = \lim_{r \to \infty} D(z_{k_r}) = D^* \), so \( z \in \mathcal{Z}^* \). This contradicts the fact that \( d(z_k, \mathcal{Z}^*) > \epsilon \) for all \( k \in \mathbb{N} \), since \( d(z_k, \mathcal{Z}^*) \leq |z_k - z| \leq \epsilon \) for sufficiently large \( r \), which yields the result. \( \blacksquare \)

APPENDIX B

PROOF OF PROPOSITION 1

The dual function \( D(\cdot) \) is concave and with \( L \)-Lipschitz continuous gradient so we have [29] Equation (2.1.6)

\[
D([z]^+) \geq D(z) + \langle \nabla D(z), [z]^+ - z \rangle - \frac{L}{2} \| [z]^+ - z \|^2,
\]

\[
= D(z) + \langle \nabla^\Lambda D(z), [\lambda]^+ - \lambda \rangle - \frac{L}{2} \| [\lambda]^+ - \lambda \|^2
\]

\[
+ \langle \nabla^\mu D(z), [\mu]^+ - \mu \rangle - \frac{L}{2} \| [\mu]^+ - \mu \|^2,
\]

\[
\geq D(z) + \alpha \left( 1 - \frac{L}{2} \alpha \right) \| \lambda - \lambda + \nabla^\Lambda D(z) \|^2
\]

\[
+ \langle \nabla^\mu D(z), [\mu]^+ - \mu \rangle - \frac{L}{2} \| [\mu]^+ - \mu \|^2,
\]

where the final inequality is proved below. From Lemma 2 we have \( V(z) \geq f_{\text{ess}}(q(z)) > 0 \), yielding

\[
\epsilon^2 \leq V(z)^2 = \| \lambda - \lambda + \nabla^\Lambda D(z) \|_+^2 + \| \mu - \mu + \nabla^\mu D(z) \|_+^2.
\]

Consider the two cases separately when (a)

\[
\| \mu - [\mu + \nabla^\mu D(\mu)]_+ \|^2 \geq \frac{\epsilon^2}{2}
\]

and (b)

\[
\| \mu - [\mu + \nabla^\mu D(\mu)]_+ \|^2 \leq \frac{\epsilon^2}{2}
\]

In case (a) we have (proved below)

\[
D([\bar{z}]^+) \geq D(z) + \left( \frac{\epsilon}{2N^{1/2}} - \beta \right) \mu \lambda,
\]

and case (b) we have (proved below)

\[
D([\bar{z}]^+) \geq D(z) + \alpha \left( 1 - \frac{L}{2} \alpha \right)^2 - NL\beta^2.
\]

Then Equation (26) is obtained by Equations (37) and (38).

Proof of Equation (36): We have

\[
\langle \nabla^\Lambda D(z), [\lambda]^+ - \lambda \rangle = \sum_{i=1}^{2N} \| \nabla^\Lambda_i D(z) \|_1 \| \lambda_i + \alpha \nabla^\Lambda_i D(z) \|_+ - \lambda_i \|
\]

\[
\geq \sum_{i=1}^{2N} \frac{1}{\alpha} (\| \lambda_i + \alpha \nabla^\Lambda_i D(z) \|_+ - \lambda_i)^2
\]

where the equality comes by using that each term of the sum is positive from Equation (35) and the inequality comes by using the non-expansiveness of the projection to get

\[
\| \nabla^\Lambda D(z) \|_1 - \lambda = \sum_{i=1}^{2N} (\| \lambda_i + \alpha \nabla^\Lambda_i D(z) \|_+ - \lambda_i)^2.
\]

We also have

\[
\| \langle \nabla^\Lambda D(z), [\lambda]^+ - \lambda \rangle \|_1 = \sum_{i=1}^{2N} (\| \lambda_i + \alpha \nabla^\Lambda_i D(z) \|_+ - \lambda_i)^2.
\]

By combining (39) and (40) we get

\[
\langle \nabla^\Lambda D(z), [\lambda]^+ - \lambda \rangle \leq \frac{L}{2} \| [\lambda]^+ - \lambda \|^2
\]

\[
\geq \left( \frac{1}{\alpha} - \frac{L}{2} \right) \sum_{i=1}^{2N} (\| \lambda_i + \alpha \nabla^\Lambda_i D(z) \|_+ - \lambda_i)^2
\]

\[
\geq \alpha^2 \left( \frac{1}{\alpha} - \frac{L}{2} \right) \| \lambda - \mu^\Lambda D(z) \|_+^2
\]

where the second inequality comes by using (33) and the fact that \( \alpha < 2L < 1 \) (see Lemma 1).

Proof of Equation (37): Suppose that

\[
\| \mu - [\mu + \nabla^\mu D(\mu)]_+ \|^2 \geq \frac{\epsilon^2}{2}.
\]

Then we have

\[
\langle \nabla^\mu D(z), [\mu]^+ - \mu \rangle
\]

\[
= \sum_{i=1}^{2N} \| \nabla^\mu_i D(z) \|_1 (\| \mu_i + \beta \text{sign}(\nabla^\mu_i D(z)) \|_+ - \mu_i)
\]

\[
\geq |\mu_j - [\mu_j + \nabla^\mu_j D(z)]_+| + |\mu_j - [\mu_j + \beta \text{sign}(\nabla^\mu_j D(z))]_+|
\]

\[
\geq \frac{\epsilon}{2N^{1/2}} \beta
\]

where \( j = \text{argmax}_{j=1, \ldots, 2N} |\mu_j - [\mu_j + \nabla^\mu_j D(z)]_+| \), the equality comes by using that each term of the sum is positive from Equation (35), the first inequality from the non-expansiveness.
of the projection [28 Proposition B.11], and the final inequality comes from the fact that \( ||\mu - [\mu + \nabla^\mu D(z)]_+||_\infty \geq \epsilon/(\sqrt{2N}) \), since \( ||\mu - [\mu + \nabla^\mu D(z)]_+|| \geq \epsilon/\sqrt{2} \), and Equation (34), together with the fact that \( \beta \leq \epsilon/(2\sqrt{N}) \leq |||\mu_j - [\mu_j + \nabla^j D(z)]_+|| \). We also have

\[
||\mu - [\bar{\mu}]_+||^2 = \sum_{i=1}^{2N} |\mu_i - [\bar{\mu}_i + \beta \text{sign}(\nabla^\mu_i D(z))]_+|^2 \\
\leq 2N\beta^2. \tag{42}
\]

Combining Equations (41) and (42) and rearranging yields

\[
\langle \nabla^\mu D(z), [\bar{\mu}]_+ - \mu \rangle - \frac{L}{2} \left[ ||\bar{\mu}_+ - \mu||^2 \right] \geq -\frac{\epsilon}{2N^{3/2}L} \beta LN,
\]

which proves Equation (37).

**Proof of Equation (38):** The result follows from that

\[
\langle \nabla^\mu D(z), [\bar{\mu}]_+ - \mu \rangle - \frac{L}{2} \left[ ||\bar{\mu}_+ - \mu||^2 \right] \geq -NL\beta^2, \tag{43}
\]

where inequality comes by that

\[
||\mu - [\bar{\mu}]_+||^2 = \sum_{i=1}^{2N} (\mu_i - [\bar{\mu}_i])^2 \leq 2N\beta^2.
\]

and \( \langle \nabla^\mu D(z), [\bar{\mu}]_+ - \mu \rangle \geq 0 \), from Equation (35).

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