Catalyst tolerance to SO2 and water vapor of Mn based bimetallic oxides for NO deep oxidation by ozone

Fawei Lin, Zihua Wang, Jiaming Shao, Dingkun Yuan, Yong He, Yanqun Zhu and Kefa Cen

Improving the catalyst stabilities under different conditions (water vapor, SO2, both water vapor and SO2) is important for industrial applications regarding catalytic NO deep oxidation by ozone. In this paper, Ce–Mn/SA and Fe–Mn/SA catalysts were selected to investigate the stabilities. The results showed that the Ce–Mn/SA exhibited excellent stability and resistance to SO2, while the Fe–Mn/SA only displayed excellent stability without moisture and SO2. Almost a 50% drop in efficiency was observed after deactivation by water vapor and water vapor together with SO2 for the two catalysts. The Fe–Mn/SA displayed inferior resistance to SO2. After stability testing with water vapor, the surface area, pore volume, and average pore diameter all decreased. The low adsorption energy of the H2O molecule resulted in the superior adsorption of water vapor, which occupied large amounts of active sites. XPS results showed that the ratio of Mn4+ and chemisorbed oxygen decreased after deactivation. Mn3+ favors NO oxidation, while Mn5+ is favorable for ozone decomposition. Therefore, better performance in NO deep oxidation by ozone requires relative balance distribution between Mn4+ and Mn5+. Interestingly, the TPD results showed that the NO desorption peak was unaffected and even increased a lot after water vapor stability testing. This could be attributed to the nitrates, formed by the N2O5 and H2O in liquid phase, that were adsorbed on the catalyst surface prior to NO, which contributes to a bigger NO desorption peak with lower NO adsorption ability. The trace of sulfate formed after SO2 stability testing was verified from TPD and TGA results, but it was not observed from the FTIR spectra, indicating the sulfate species formed during the ozonation process may not exist on the catalyst surface.

1. Introduction

With the increasing threat to human health of air pollution, more and more strict emission standards are being issued worldwide. As well known, the combustion of fossil fuels (e.g. coal, petroleum) and municipal solid waste are the major anthropogenic source of air pollution. Several emission control technologies have been proposed and applied for the flue gas treatment. Hereinto, catalysts are becoming the critical part of these emission control technologies, including NOx reduction, NO oxidation, Hg oxidation, soot combustion, VOCs combustion, etc. The catalyst stability is a crucial factor when evaluating its feasibility for industrial applications. Furthermore, many components such as SO2, water vapor, ash, alkali metals (e.g. K, Na) and other harmful species (e.g. Pb, As, P) brought by flue gas from combustion of coal, petroleum, and municipal solid waste, would seriously deactivate the catalysts. Therefore, improving the catalyst resistance to these components is an important topic.

Contrary to reduction method, oxidation method is regarded as a promising NOx control option for industrial boilers. Especially for the ultra-low emission, oxidation method can achieve extreme low emission concentration. Furthermore, Hg0 and VOCs can also be removed together with NOx by oxidation method. In the oxidation process, NO, the major species of nitrogen oxides in the flue gas, is oxidized into NO2 and N2O3; Hg0 is oxidized into Hg22; VOCs can be oxidized into small molecule compounds. Then these oxidation products can be removed together with SO2 in typical WFGD (wet flue gas desulfurization) device. Ozone, characterized by long life time, strong oxidation ability, short reaction time, and large scale production, has always been regarded as the preferred oxidizing agent. However, the relatively high investment and running cost are becoming the biggest obstacles in promoting this technique. Therefore, catalysts are introduced to improve the oxidation efficiency with low ozone usage.

The catalytic ozonation is usually carried out at low temperature due to the thermal accelerated ozone decomposition process. The previous works on catalytic ozonation...
reported that the catalyst was easily to be deactivated due to the accumulation of intermediate species. The SA (spherical alumina) instead of powder sample was selected as the catalyst support in our previous work\(^2\) to achieve the dispersive arrangement, which can enhance the desorption and decomposition of intermediate species. The manganese oxides supported on SA indeed exhibited good stability and resistance to SO\(_2\). However, it has been widely reported that water vapor will lead to catalyst deactivation for ozone decomposition.\(^2\),\(^3\) In this article, water vapor was introduced to investigate its influence on catalyst stability. Since SO\(_2\) is excluded in most of the ozone involved applications, no other previous works have studied the catalyst resistance to SO\(_2\) for catalytic ozonation and ozone decomposition to the best of our knowledge. In this study, the catalyst stabilities without moisture and SO\(_2\), with water vapor, with SO\(_2\), and with SO\(_2\) and water vapor were investigated, respectively. Ce–Mn/SA and Fe–Mn/SA, two catalysts displayed excellent activity, were selected to conduct these tests. Meanwhile, several kinds of characterization measurements were carried out to study the physicochemical properties before and after stability tests.

2. Experimental section

2.1 Catalyst preparation

The two catalyst samples were prepared by the wet coimpregnation method. The detailed procedures have been reported previously.\(^2\)\(^8\) Mn(CH\(_2\)COO\(_2\))\(_2 \cdot 4H_2O\) (Aladdin, \(\geq 99.0\)%), Ce(NO\(_3\))\(_3 \cdot 6H_2O\) (Sinopharm, \(\geq 99.0\)%), and Fe(NO\(_3\))\(_3 \cdot 9H_2O\) (Sinopharm, \(\geq 98.5\)%) were used as the precursor. The Mn loading was 5 wt%, and the molar ratio of Ce/Mn and Fe/Mn were 1/5, respectively. The catalyst samples are labelled as M–Mn/SA in this article. The M represents the Ce and Fe, respectively.

2.2 Catalyst characterization

XRD (X-ray diffraction), XPS (X-ray photoelectron spectroscopy), TGA (Thermal gravimetric analysis), TPD (Temperature programmed desorption), FTIR (Fourier transform infrared spectroscopy) and N\(_2\) adsorption–desorption isotherms were detected for these catalyst samples. These samples that had undergone various stages of use are labelled as listed in Table 1.

XRD patterns were recorded on a Rigaku D/max 2550PC diffractometer with a scan rate of 4° min\(^{-1}\) using Cu K\(_\alpha\) radiation. XPS spectra were collected on a photoelectron spectrometer (Thermo Scientific Escalab 250Xi) with a standard Al K\(_\alpha\) source (1486.6 eV) after referencing to the C 1s line at 284.5 eV. The XRS results of fresh samples are listed in the other articles but the distribution molar ratios are mentioned for reference.

The weight loss at different temperatures can be used to estimate the mass of nitrogen species and sulfur species formed on the catalyst surface. Therefore, TGA and DTA (differential thermal analysis) curves were detected through a thermo-gravimetric analyzer (TA-Q500 TGA). 10 mg of each sample was loaded onto the reactor without any pretreatment. Then sample was heated up to 1000°C at a rate of 10°C min\(^{-1}\) under N\(_2\) atmosphere. The TGA and DTA curves from 50°C to 1000°C were obtained.

TPD patterns were obtained using an automatic temperature programmed chemisorption analyzer (Micromeritics AutoChem II 2920) together with a mass spectrometer (Hiden QIC20). 50 mg of each sample were loaded into a U type quartz tube, then the furnace was heated to 100°C at a rate of 10°C min\(^{-1}\) under He atmosphere and maintained for 30 min to remove adsorbed water and some other impurities. After pretreatment, the mass spectrometer began testing. Sequentially, the furnace was heated to 1000°C at a rate of 10°C min\(^{-1}\) under He atmosphere. The TCD signals of NO, O\(_2\), and SO\(_2\) were obtained from the mass spectrometer.

FTIR spectra detected by a Nicolet 5700 FTIR spectrometer with 0.09 cm\(^{-1}\) resolution can be used to evaluate the formed species on the catalyst surface after ozonation process.

N\(_2\) adsorption–desorption isotherms were recorded in a Micromeritics ASAP 2020 equipment under liquid N\(_2\) (77 K). Prior to analysis, the samples were degassed at 473 K for 5 h.

2.3 Stability testing procedure

The stability testing was carried out in the same reactor mentioned in ref. 28. The total gas flow rate was kept at 2 L min\(^{-1}\), with oxygen concentration of 2.5 vol%, and the corresponding residence time in the reactor about 0.12 s. The initial NO concentration was fixed at 410 mg N\(^{-1}\) m\(^{-3}\) with small amount of NO\(_2\) residual in the cylinder. The O\(_3\)/NO molar ratio was fixed at 1.5 with ozone injection amount of 642 mg N\(^{-1}\) m\(^{-3}\). In addition, SO\(_2\) and water vapor were added into the reactor when assaying the catalyst stability with SO\(_2\) and water vapor. SO\(_2\) was from bottled gas supplied by Jingong Gas Co., Ltd. (SO\(_2\)-5%/balance N\(_2\)) and the concentration was controlled by MFC (mass flow controller) at 285 mg N\(^{-1}\) m\(^{-3}\). Water vapor was added by bubbling through heating water and the concentration was ~10 vol%. The concentrations of SO\(_2\) and water vapor were also measured by an FTIR (Fourier transform infrared spectroscopy) gas analyzer. The other instruments and testing procedure have been mentioned in previous work.\(^2\)

For each testing, after 15 min ozone injection, the concentrations of NO + NO\(_2\) tends to be stable. Thus, SO\(_2\) and water vapor were added into the reactor after 15 min ozone injection. For comparison, these stabilities testing without SO\(_2\) and water vapor were also recorded after 15 min ozone injection.

| Denotation | Sample | Description |
|------------|--------|-------------|
| Ce–Mn/SA-a | Fe–Mn/SA-a | Fresh catalyst |
| Ce–Mn/SA-b | Fe–Mn/SA-b | Catalyst after stability testing for 120 min |
| Ce–Mn/SA-c | Fe–Mn/SA-c | Catalyst after stability testing with water vapor for 120 min |
| Ce–Mn/SA-d | Fe–Mn/SA-d | Catalyst after stability testing with SO\(_2\) for 120 min |
| Ce–Mn/SA-e | Fe–Mn/SA-e | Catalyst after stability testing with SO\(_2\) and water vapor for 120 min |
3. Results and discussion

3.1 Catalytic stabilities testing

The Ce–Mn/SA and Fe–Mn/SA were used to investigate the catalyst stability. As the blank results shown in Fig. 1, the concentrations of NO + NO₂ were stable with catalytic reaction time of 0.12 s at 100 °C. However, the stabilities with SO₂ showed obvious difference for these two samples. The introduction of SO₂ almost had no effect on Ce–Mn/SA during the 120 min testing, which means the Ce–Mn/SA had strong resistance to SO₂. But the concentration of NO + NO₂ increased quickly after SO₂ addition for Fe–Mn/SA. Only after 80 min, more than 200 mg N⁻¹ m⁻³ of NO + NO₂ was detected, which means the Fe–Mn/SA was deactivated seriously by SO₂. Generally, the NO adsorption ability will be inhibited seriously after the addition of SO₂. This was attributed to the oxidation between ozone and NO, which could greatly enhance the chemical adsorption of NO₂. Therefore, the catalyst activity could be maintained even with SO₂ for Ce–Mn/SA. But the resistance was no longer appeared when the Fe–Mn/SA was used. According to the XPS results showed below, the valance state of Mn species of Fe–Mn/SA was changed obviously after stability testing with SO₂, while the Ce–Mn/SA was maintained, which can be the explanation for the worse resistance to SO₂ of Fe–Mn/SA. Therefore, the metal interaction resulted in distinct resistance to SO₂.

Several previous works have pointed out that the presence of water vapor can lead to catalyst deactivation for catalytic ozone decomposition and catalytic ozonation. The adsorption energy of water vapor is lower than other reactants, indicating stronger adsorption. Then the H₂O molecule adsorbed on the catalyst surface is hard to desorb. As shown in Fig. 1, the concentration of NO + NO₂ increased significantly after the addition of water vapor for the two catalysts. After nearly 20 min, the concentration trended to be stable. In comparison, the stable concentration was about 200 mg N⁻¹ m⁻³ for Ce–Mn/SA, and about 150 mg N⁻¹ m⁻³ for Fe–Mn/SA, indicating the Fe–Mn/SA resistance to water vapor was higher than Ce–Mn/SA.

Finally, the SO₂ and water vapor were introduced into the reactor together. Generally, the coexistence of SO₂ and water vapor will promote the formation of sulfur species on the catalyst surface. Thus, the catalyst deactivation will be more serious in this condition. It can be observed from the results of Ce–Mn/SA in Fig. 1 that the concentration of NO + NO₂ after the addition of SO₂ and water vapor was similar with the addition of single water vapor. For Fe–Mn/SA, after the addition of SO₂ and water vapor, the concentration of NO + NO₂ increased sharply to nearly 250 mg N⁻¹ m⁻³ after 15 min. Then it decreased and stabilized at nearly 200 mg N⁻¹ m⁻³, which was similar with stable concentration after addition of SO₂. This illustrates that except for the initial sharply deactivation, the final stable results were not enhanced by the coexistence of SO₂ and water vapor.

3.2 Crystallite structures

The Ce–Mn/SA was selected to investigate the crystallite structures change after stabilities testing. The results can be found in Fig. 2 there was no new peaks after these four stabilities testing. The only change was the peak intensity. The main peak between 60 deg and 70 deg can be used for analysis. After deep oxidation stability testing, the peak intensity increased (from Ce–Mn/SA-a to Ce–Mn/SA-b), indicating the stronger crystallization. According to the main reaction pathway of catalytic NO deep oxidation by ozone proposed in our previous work, the active metals were firstly oxidized by ozone and then forwarded to oxidize nitrogen oxides, which accounted for the stronger crystallization after deep oxidation by ozone. After the stability testing with water vapor (Ce–Mn/SA-c), the peak intensity went back to the same level as fresh catalyst (Ce–Mn/SA-a). This also verifies the significant deactivation in the presence of water vapor. For Ce–Mn/SA-d, the peak intensity was similar with Ce–Mn/SA-b, which was corresponding to the similar results between blank stability testing and with SO₂. However, the peak intensity of Ce–Mn/SA-e had almost no difference with Ce–Mn/SA-d.
Mn 2p signals exhibited a spin orbit doublet with Mn 2p_{3/2} and Mn 2p_{1/2}. After peak-fit processing through the optimum combination of Gaussian peaks method, two main peaks could be obtained in the Mn 2p_{3/2} region, which were ascribed to Mn^{4+} and Mn^{3+} species.\textsuperscript{33,34} Only one region could be detected for the O 1s spectra. And it could be deconvoluted into two main peaks represent lattice oxygen O_l and chemisorbed oxygen O_s.\textsuperscript{35,36} respectively. The specific binding energy of Mn and oxygen species were shown in Tables 3 and 4. Meanwhile, the molar ratio of Mn^{4+} and O_s were calculated by quantitative area integration method and listed in Tables 3 and 4 for comparison.

For Ce–Mn/SA, the ratio of Mn^{4+} decreased (Ce–Mn/SA-b) after stability testing (the Mn^{4+}/Mn is 0.55 for Ce–Mn/SA-a). Eqn (1) depicts the main reaction pathway for catalytic NO deep oxidation by ozone,\textsuperscript{28} indicating Mn^{4+} played as the intermediate oxidant in the reaction process. This explains the observed decrease of Mn^{4+} after stability testing. According to eqn (2), the consumed Mn^{4+} would be continuously replenished by ozone. Meanwhile, in light of eqn (1), the observed conversion from lattice oxygen (O_l[Mn^{4+}]) to chemisorbed oxygen (NO_3–Mn) would resulting in the increase of O_s after stability testing shown in Table 3 (the O_s/O_l is 0.43 for Ce–Mn/SA-a). After the stability testing with water vapor (Ce–Mn/SA-c, with SO_2 (Ce–Mn/SA-d, and with both SO_2 and water vapor (Ce–Mn/SA-e), the ratios of Mn^{4+} all decreased when compared with Ce–Mn/SA-b, which might be relevant to the agglomeration of manganese oxides. Mn^{4+} favors for NO oxidation, while Mn^{3+} is favorable for ozone decomposition. Therefore, the relative balance distribution between Mn^{4+} and Mn^{3+} is beneficial to catalytic NO deep oxidation by ozone. The ratios of Mn^{4+} for Ce–Mn/SA-c and Ce–Mn/SA-e were lower than Ce–Mn/SA-b and Ce–Mn/SA-d, which might cause the catalyst deactivation in the presence of water vapor and water vapor together with SO_2. The ratios of chemisorbed oxygen decreased after stabilities testing with water vapor (Ce–Mn/SA-c, Ce–Mn/SA-d, Ce–Mn/SA-e) compared with Ce–Mn/SA-b. The decrease of Ce–Mn/SA-d indicates that the sulfur species were not accumulated on the catalyst surface, which agrees with the FTIR results shown below. The decreases of Ce–Mn/SA-c and Ce–Mn/SA-e resulted in the lower NO deep oxidation efficiency.

\[
O^\cdot [Mn^{4+}] + NO_2–Mn \rightarrow NO_3–Mn + [Mn^{3+}] \tag{1}
\]

\[
O_3 + [Mn^{3+}] \rightarrow O^\cdot [Mn^{4+}] + O_2 \tag{2}
\]

For Fe–Mn/SA, due to the deactivation in the presence of SO_2, the ratio of Mn^{4+} for catalyst after stability testing (Fe–Mn/SA-d) decreased from 0.44 (Fe–Mn/SA-b) to 0.37, which was different from Ce–Mn/SA (decreased from 0.41 (Ce–Mn/SA-b) to 0.40 (Ce–Mn/SA-d)). This phenomenon can explain the worse resistance to SO_2 of Fe–Mn/SA than Ce–Mn/SA. The other samples had the same variation tendency with Ce–Mn/SA because of the similar stability results. The chemisorbed oxygen distributions were almost the same among these four samples. When the catalyst was exposed to water vapor, the adsorption of H_2O molecule could increase the chemisorbed oxygen, while the deactivation would lead to the decrease of chemisorbed oxygen. The
A synthetic effect would therefore result in a tiny change of chemisorbed oxygen.

The Ce 3d spectra of Ce–Mn/SA after stabilities testing are also shown in Fig. 4. The characteristic peaks included 3d_{5/2} states (labelled as v) and 3d_{3/2} states (labelled as u). After peak-fit processing, the XPS spectra were deconvoluted into several peaks. The v’ and u’ represented Ce^{3+} species, and the others represented Ce^{4+} species. The binding energies and molar ratio of Ce^{4+} calculated by quantitative area integration method are listed in Table 5. After stability testing (Ce–Mn/SA-b), the ratio of Ce^{4+} increased compared with fresh catalyst (Ce–Mn/SA-a, 0.47). After exposure to water vapor (Ce–Mn/SA-c), the ratio of Ce^{4+} decreased slightly compared with Ce–Mn/SA-b, corresponding to the catalyst deactivation. For Ce–Mn/SA-d, the decrease of Ce^{4+} might be related to the reduction of Ce^{4+} to Ce^{3+} by SO_{2}. The higher ratio of Ce^{4+} for Ce–Mn/SA-e compared with Ce–Mn/SA-c was corresponding to slightly better performance in presence of water vapor together with SO_{2} than single presence of water vapor shown in Fig. 1.

The Fe 2p XPS spectra shown in Fig. 4 included two main peaks, Fe^{3+} and Fe^{2+}. While for Fe–Mn/SA-d and Fe–Mn/SA-e, the satellite peak appeared. The binding energies and molar ratio of Fe^{3+} are listed in Table 6. The variation tendency of Fe^{3+} was similar with Ce^{4+} mentioned above after stabilities testing. It can be observed that the ratio of Fe^{3+} for Fe–Mn/SA-d was much lower than Fe–Mn/SA-c, which was corresponding to the better resistance to water vapor than SO_{2} shown in Fig. 1. When the catalyst was exposed to water vapor together with SO_{2}, the ratio of Fe^{3+} became the lowest among all these samples. It can be found that the ratio of Fe^{3+} was corresponding to the performance of stability testing.

### Table 2 Pore structure parameters of Ce–Mn/SA and Fe–Mn/SA after stabilities testing with and without water vapor

| Catalyst       | BET surface area/m² g<sub>cat</sub><sup>-1</sup> | Pore volume<sub>a</sub>/cm³ g<sub>cat</sub><sup>-1</sup> | Average pore diameter<sub>b</sub>/nm |
|----------------|---------------------------------------------|-----------------------------------------------|----------------------------------|
| Ce–Mn/SA-a     | 318.7                                       | 0.43                                          | 4.8                              |
| Ce–Mn/SA-b     | 239.1                                       | 0.32                                          | 4.9                              |
| Ce–Mn/SA-c     | 236.1                                       | 0.31                                          | 4.8                              |
| Fe–Mn/SA-a     | 228.9                                       | 0.32                                          | 5.0                              |
| Fe–Mn/SA-b     | 225.8                                       | 0.35                                          | 5.4                              |
| Fe–Mn/SA-c     | 223.7                                       | 0.31                                          | 5.4                              |

<sup>a</sup> BJH desorption cumulative volume of pores. <sup>b</sup> BJH desorption average pore diameter.

3.5 Temperature programmed desorption

As the TPD profiles for these catalysts after stabilities testing shown in Fig. 5, desorption of NO, O<sub>2</sub>, and SO<sub>2</sub> can be detected during the heating process. Because the major desorption...
specie of nitrogen oxides is NO, the NO$_2$ profiles were ignored. It should be mentioned that the TCD signals of NO, O$_2$, and SO$_2$ for Fe–Mn/SA in Fig. 5 are all 1/2 compared with Ce–Mn/SA.

For NO-TPD, only one peak around 365 °C could be observed for all samples, which can be ascribed to the desorption of monodentate and bidentate nitrate species.$^{41,42}$ However, the...
shown below. At the reaction temperature of 100 °C, the NO desorption peak became slightly bigger for Mn/SA-c), the TCD signal of NO between 150 °C and 300 °C was associated with the weakly adsorbed nitrogen species on the catalyst surface. After stability testing without moisture and SO2, the NO desorption of Fe–Mn/SA-b was extremely lower than Ce–Mn/SA-b. This indicates the NO adsorption ability of Ce–Mn/SA was quite higher than Fe–Mn/SA. Furthermore, the TCD signal of NO between 150 °C and 300 °C was very weak for Fe–Mn/SA, indicating less weakly adsorbed nitrogen species on the catalyst surface. After stability testing with water vapor (Ce–Mn/SA-c), the NO desorption peak became slightly bigger compared with Ce–Mn/SA-b, which agrees with TGA results shown below. At the reaction temperature of 100 °C, some H2O in liquid phase would easily react with N2O5, the major products after catalytic reaction. Therefore, the slightly bigger NO desorption peak could be attributed to the interaction between N2O5 and H2O, which would give rise to more adsorbed nitrates on the catalyst surface. Therefore, rather than better NO adsorption ability, more nitrates formed and adsorbed on the catalyst surfaces can be predicted from the enhanced NO desorption peak due to the serious catalyst deactivation. Above all, the nitrates grabbed the adsorption active sites for NO, which led to lower NO adsorption. The deactivation was also attributed to the atom state change and pore blocking, which severely inhibit ozone decomposition process. Previous works on catalytic NO oxidation also pointed out that the NO adsorption ability would be reduced by water vapor. Therefore, it can be concluded that the coexistence of ozone and water vapor enhanced the nitrates formation on the catalyst surface while the NO adsorption ability was inhibited. Interestingly, Fe–Mn/SA had even better performance for NO deep oxidation by ozone despite the lower NO adsorption ability compared with Ce–Mn/SA. The abundant oxygen vacancies of cerium oxides are beneficial to NO adsorption. After stabilities testing in the presence of SO2 (Ce–Mn/SA-d and Ce–Mn/SA-e), the TCD signals of NO decreased obviously, which agreed with the results obtained in previous work. However, although the NO adsorption ability decreased seriously with SO2, the catalyst performance seemed to be unaffected. When the water vapor was added together with SO2, the NO desorption peak became feebler. This inhibition effect could be attributed to sulfates formation, which took precedence over nitrates formation. Thus, the coexistence of water vapor and SO2 led to the greatest breakage for catalyst activity. More interestingly, almost no discrepancy of the NO-TCD signals was observed for all the four Fe–Mn/SA samples, while the catalyst performance was greatly affected by the introduction of water vapor and SO2. This illustrates that the NO adsorption ability of Fe–Mn/SA was unaffected by SO2, and the deactivation might be related to the change of ozone decomposition activity.

There were two main desorption peaks associated with two weak desorption peaks in the O2-TPD profiles. The first big desorption peak at 366 °C (similar with 363 °C and 365 °C of NO-TPD) was mainly ascribed to the decomposition of nitrate species. The second big desorption peak at 929 °C (similar with 929 °C and 927 °C of SO2-TPD) was mainly ascribed to the decomposition of sulfate species. The weak desorption peak at lower temperature was attributed to desorption of physical adsorption water. The release of chemisorbed oxygen species and surface lattice oxygen species corresponded to the desorption region between 200 °C and 300 °C. The weak desorption peak at higher temperature was attributed to the release of lattice oxygen species and metal phase transformation. The variation tendency of O2-TPD was the same with NO-TPD.

| Sample      | Mn3+ (eV) | Mn3+ (eV) | Mn4+/Mn | O2 (eV) | O2/ O |
|-------------|-----------|-----------|---------|---------|-------|
| Ce–Mn/SA-b  | 642.1     | 644.3     | 0.41    | 530.6   | 531.6 | 0.60  |
| Ce–Mn/SA-c  | 642.0     | 644.1     | 0.34    | 530.4   | 531.3 | 0.53  |
| Ce–Mn/SA-d  | 642.1     | 644.0     | 0.40    | 530.6   | 531.5 | 0.49  |
| Ce–Mn/SA-e  | 642.2     | 645.4     | 0.26    | 530.4   | 531.4 | 0.48  |

| Sample      | Fe3+ (eV) | Satellite (eV) | Fe3+ (eV) | Fe3+/Fe total |
|-------------|-----------|----------------|-----------|---------------|
| Fe–Mn/SA-b  | 712.1     | —              | 725.1     | 0.56          |
| Fe–Mn/SA-c  | 711.9     | —              | 724.9     | 0.54          |
| Fe–Mn/SA-d  | 711.5     | 717.1          | 725.7     | 0.48          |
| Fe–Mn/SA-e  | 711.5     | 715.7          | 725.5     | 0.42          |

| Sample      | Ce 3d binding energies (eV) and valance composition on Ce–Mn/SA after stabilities testing |
|-------------|------------------------------------------------------------------------------------------|
| Ce–Mn/SA-b  | v (eV) | v’ (eV) | v” (eV) | u (eV) | u’ (eV) | u” (eV) | Ce4+/Ce |
| Ce–Mn/SA-c  | 882.4  | —       | 885.0   | 898.8  | 901.4  | 903.7  | 916.9   | 0.53    |
| Ce–Mn/SA-d  | 882.2  | —       | 885.3   | 898.5  | —      | 902.9  | 916.8   | 0.47    |
| Ce–Mn/SA-e  | 882.7  | 883.6   | 885.4   | 899.1  | —      | 903.7  | 917.3   | 0.46    |

The Ce 3d binding energies (eV) and valance composition on Ce–Mn/SA after stabilities testing.
The SO$_2$ desorption peak could be detected only when the catalyst was tested in the presence of SO$_2$. Compared with our previous work,$^{28}$ the SO$_2$ desorption temperature increased after doping with second transition metal oxides. Generally, the thermal decomposition of sulfate includes two steps: initial decomposition with the formation of oxysulfates and second

Fig. 5 TPD profiles of NO, O$_2$, and SO$_2$ for catalysts after stabilities testing. (a) and (b) NO-TPD; (c) and (d) O$_2$-TPD; (e) and (f) SO$_2$-TPD.
decomposition with the formation of metal oxides and SO$_2$.\textsuperscript{46} Undoubtedly, the second step corresponding to the SO$_2$-TPD results occurs at higher temperature. It has been mentioned that the bulk MnSO$_4$ and Al$_2$(SO$_4$)$_3$ decomposition temperatures are 850 °C and 770 °C,\textsuperscript{14} respectively. The decomposition of bulk sulfates of cerium and evolution of SO$_2$ occurs at 750 °C.\textsuperscript{48} The

Fig. 6 TGA and DTA profiles for catalysts after stabilities testing.
The thermal decomposition of sulfates of iron to Fe₂O₃ and SO₂ occurs at 658 °C. It can be observed that the SO₂ desorption peak temperature in Fig. 5 was much higher than these sulfates decomposition temperature, which might be attributed to the synthetic effects between metal oxides. It can be also observed that the SO₂ desorption peak became smaller for sample-e compared with sample-d. This illustrates that the coexistence of SO₂ and water vapor decreased the formation of bulk sulfates.

3.6 Thermal gravimetric analysis

The thermal gravimetric analysis was carried out to investigate the weight loss along with temperature. The weight loss at different temperature region can be used to compare the amounts of species formed after stabilities testing. Therefore, the TGA/DTA curves were divided into four regions as shown in Fig. 6, and the weight loss amounts in different region were also listed for comparison.

The first region from 50 °C to 150 °C contributed the major weight loss for all samples, which was the dehydration process. Interestingly, for both Ce–Mn/SA and Fe–Mn/SA, the weight losses of the dehydration process decreased after stabilities testing (Ce–Mn/SA-b and Fe–Mn/SA-b) compared with fresh catalysts (Ce–Mn/SA-a and Fe–Mn/SA-a). Even the catalysts were tested in presence of water vapor (Ce–Mn/SA-c and Fe–Mn/SA-c), the weight losses of the dehydration process decreased as well. It can be speculated that some radicals related to H₂O would participate in the catalytic reaction to form the nitrates and nitrites.

The second region from 150 °C to 500 °C could be ascribed to the nitrates and nitrites desorption region as the NO-TPD results, which exhibited a weight loss peak at 365 °C. Some residual chemisorbed radicals which were not desorbed in the first region would also contribute to the weight loss. That’s why there were also more than 2.8% weight loss for these two fresh catalysts. It could be seen that the weight losses in the second region increased after stabilities testing with water vapor even the catalyst deactivation had occurred. This results agree with the NO-TPD and O₂-TPD results. For Fe–Mn/SA, the weight losses in the second region stayed at about 4.05% in all the explored conditions.

The third region from 500 °C to 800 °C was corresponding to the transformation of MnO₂ to Mn₂O₃ as mentioned above.

Finally, the fourth region from 800 °C to 1000 °C was the sulfates decomposition region, which was corresponding to the SO₂-TPD results. The weight losses decreased in this region for catalysts that were exposed to water vapor together with SO₂ (Ce–Mn/SA-e and Fe–Mn/SA-e) compared with only exposure to SO₂ (Ce–Mn/SA-d and Fe–Mn/SA-d). This indicates that the coexistence of water vapor and SO₂ inhibited the sulfates formation to some extend during the catalytic process. As mentioned above, the adsorption energy of H₂O molecule is very low, resulting in the superior adsorption ability compared with SO₂.

3.7 Surface properties

As shown in Fig. 7, the FTIR technique was used to detect the species formed on the catalyst surface after stabilities testing. The bands at 3439 cm⁻¹ stood for the O–H stretching modes of hydrogen-bonded H₂O molecules on alumina support. The bands at 1634 cm⁻¹ were ascribed to bridging nitrate. Almost no discrepancy could be detected between these samples. Therefore, the bridging nitrate may be the undecomposed nitrate from the precursors. The bands at 1381 cm⁻¹ were the main formation species on the catalyst surface: free nitrates, including bidentate nitrate, monodentate nitrate, and ionic nitrate. This band appeared only for the samples after stabilities testing. Interestingly, even after catalyst deactivation induced by the introduction of water vapor and SO₂, the intensity of this band showed no obvious change. Meanwhile, no sulfates bands could be detected in Fig. 7. It can be therefore
speculated some bulk nitrates and sulfates that produced during the ozonation process cannot be detected on the catalyst surface.

4. Conclusions

The catalyst stabilities under different conditions (water vapor, SO$_2$, both water vapor and SO$_2$) were conducted for catalytic NO deep oxidation by ozone. It was found that the Ce–Mn/SA exhibited excellent stability and resistance to SO$_2$, but a 50% drop in efficiency was observed after catalyst deactivation by water vapor and water vapor together with SO$_2$. The Fe–Mn/SA also displayed excellent stability while showed inferior resistance to SO$_2$ and water vapor. Almost 50% drop in efficiency was observed when the catalyst was exposed to water vapor and SO$_2$ (single or together).

XRD, $N_2$ adsorption–desorption isotherms, XPS, TPD, TGA, and FTIR were conducted to investigate the poisoning mechanism. After stabilities testing with water vapor, the surface area, pore volume, and average pore diameter all decreased. Meanwhile, the ratio of Mn$^{6+}$ and chemisorbed oxygen decreased after deactivation. The low adsorption energy of H$_2$O molecule results in the preferential adsorption of water vapor, which occupied large amounts of active sites. Furthermore, the nitrates, formed by the NO$_2$ and H$_2$O in liquid phase, were adsorbed on the catalyst surface prior to NO, which contributes to bigger NO desorption peak with lower NO adsorption ability. No sulfate species were detected on the FTIR spectra while SO$_2$ desorption peaks were observed from the TPD and TGA analysis, indicating that the sulfate species formed during the ozonation process may not exist on the catalyst surface. Above all, the key to increase the catalyst resistance to water vapor is to intensify the ozone decomposition activity in the presence of water vapor.

Acknowledgements

This work was supported by the National Natural Science Foundation of China (51422605), and the Zhejiang Provincial Natural Science Foundation (LR16E060001).

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