Determination of Temperature Gradient in TIG Welding of Duplex Stainless Steel

Alptekin KISASÖZ, Rıdvan GECÜ, Ahmet KARAASLAN

Yıldız Teknik Üniversitesi, Kimya Metalurji Fakültesi, Metalurji ve Malzeme Mühendisliği Bölümü, 34210 İstanbul/TÜRKİYE; email: akisasoz@gmail.com

Abstract: In welding of DSS, austenite/ferrite phase ratio can vary and various intermetallic phases may occur in weld metal due to excessive heat input. Especially, HAZ is very sensitive against the variation of austenite/ferrite phase ratio and formation of intermetallic phases. Thus, determining the temperature gradient in welding is very crucial. In this study ANSYS workbench was used for defining the temperature gradient in HAZ. The peak temperature in HAZ generated during the welding was determined and also, cooling rates of the analysis were compared with theoretical cooling rate values.

Keywords: Finite element modelling, ANSYS, TIG welding.

1. Introduction

Duplex stainless steels (DSS) have equal amount of austenite and ferrite phases. DSS have higher mechanical properties, corrosion resistance in chloride media and general corrosion resistance owing to dual phase structure [1-3].

In welding of DSS, austenite/ferrite phase ratio can vary and various intermetallic phases may occur in weld metal due to excessive heat input. Especially, HAZ is very sensitive against the variation of austenite/ferrite phase ratio and formation of intermetallic phases. Thus, mechanical properties and corrosion resistance of DSS will decrease. Therefore, determination of heat input during the welding and heat flow into the weld metal are critical for identifying the weld metal microstructure. Finite element modelling (FEM) method is used for determining the heat flow and temperature.
gradients into weld metal during the welding process. In FEM, a solid model of weld metal is created and heat flow analysis is run depending on the welding and specimen parameters [3-5].

Various softwares are used in FEM of welding. In this study, FEM was studied in TIG welding of DSS. Also, ANSYS workbench was adapted for determination of heat flow into DSS weld and temperature gradient into HAZ was determined.

2. Experimental

ANSYS Workbench 14.5 was used in modelling of heat flow in DSS welding. A solid model of DSS plates were created with 400x150x10 mm dimension and heat flow analysis were performed in “transient thermal” module. ANSYS Workbench starting page was given in Figure 1.

![Figure 1. ANSYS workbench starting interface](Image)

After selecting the transient thermal module, transient thermal project including material data, solid model and analysis set up was seen as given in Figure 2.
Analysis were performed with transient thermal module by defining the material properties into software engineering data. Defined material properties were density, specific heat and thermal conductivity values of DSS. After defining the material properties into software library, a solid model of DSS weld was uploaded and also, temperature gradients occurred during the welding was calculated and analysis time was determined depends on the welding time. Welding power was calculated from Equation 1.

\[ Q = E \times I \times f1 \]  

(1)

Where, Q is heat power (W), E is welding voltage (V), I is welding current and f1 is welding efficiency determined from welding method.

By creating solid model of DSS, defining the material data into software and determining the analysis time, the welding and material parameters mentioned below was counting into welding FEM analysis:

- Material properties,
- welding current and welding voltage,
- welding method,
- welding speed and time.

3. Results and Discussion

Modelling of TIG welding with 200 A welding current, 15 V welding voltage and 900 s welding time was performed. Welding efficiency (f1) of TIG is between 0.50-0.60 and also, f1 was determined as 0.60 in FEM analysis. Welding power in TIG welding was calculated as 1800 W. The temperature gradient generated into HAZ structure was given in Figure 3.

According to FEM analysis, the peak temperature generated into HAZ was 803 °C. The peak temperature values were 681 °C, 706 °C, 757 °C and 784 °C during the 588 seconds, 646 seconds, 774 seconds and 844 seconds analysis time, respectively.

Also, cooling rates of the analysis were compared with theoretical cooling rate values as seen in Figure 4. Theoretical cooling rate values were calculated from Equation 2.
Figure 3. Temperature gradient formed into HAZ

Figure 4. Comparison of theoretical and analysis cooling rates

\[ R = 2 \times \pi \times K \times \rho \times c \left( \frac{h}{H_{net}} \right)^2 (T_c - T_0)^3 \]  

(2)

where, \( R \) is cooling rate (°C/s), \( K \) is thermal conductivity (J/mm-s °C), \( T_c \) and \( T_0 \) is temperature (°C), \( \rho \) is density (g/mm³), \( c \) is specific heat (J/g °C), \( h \) is thickness (mm).

The slope of linear characteristics of theoretical and analysis cooling rates are similar.
4. Conclusion

In TIG welding of DSS, HAZ is very sensitive against the variation of austenite/ferrite phase ratio and formation of intermetallic phases. Thus, determination of temperature gradient is important.

In this study, the peak temperature value and temperature gradient in HAZ generated during the welding was determined. Moreover, theoretical and analysis cooling rates were calculated. Slope of the linear characteristics of both cooling rate values was similar.

According to experimental results, ANSYS workbench is useful for determining the temperature gradients in welding of DSS, especially in HAZ.

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