The Effect of Toughening Combined with Microjet Cooling During Quenching (Solution Heat Treatment) of Calcium Carbide-modified CuAl10Fe4Ni4 Alloy on its Mechanical Properties

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Abstract

The work presents the results of the experimental research concerning the impact of a heat treatment (toughening) of aluminum bronze CuAl10Fe4Ni4 on its mechanical properties. The conditions of the experiments and selected results are described. A detailed description of the effects of individual heat treatment conditions namely low and high temperature aging is also presented in the work.

Keywords: Cast aluminum bronzes, Heat treatment

1. Introduction

Within the framework of long-lasting research of cast aluminum bronzes, recently the effect of heat treatment of CuAl10Fe4Ni4 alloy modified with calcium carbide and cooled in microjet during quenching was investigated.

Concurrent modification with C + Ca additives and calcium carbide (CaC2) was introduced. The aim was to produce an effect of the investigated factors on the mechanical properties (Rm, Rp0.2, A, Z, HBW).

2. Test conditions

Melting and casting of specimens for mechanical testing was investigated (Fig. 1).

Melting was carried out in a Radyne AMF145 induction crucible furnace of high frequency (2.3 kHz). The 40 kg charge consisted solely of BA 1044 alloy ingots. The process of molten metal preparation included the following steps: introducing the charge and refiner (Longgaz), melting, overheating, deslagging, deoxidising with CuP, refining with compressed nitrogen (8 minutes at a pressure of 0.1-0.2 bar), deslagging, deoxidation with magnesium, possibly modification. Mould for casting the specimens was poured at 1250°C. For the calculated charge, 46g CuP, 40g Mg and modifiers: 0.06% Ca+
0.15% C or 0.18% CaC$_2$ were applied. The disintegrated modifiers were wrapped in aluminium foil.

Table 1 gives the chemical analysis of individual melts: L (1) without modification, M (2) modification with Ca + C, and N (3) modification with CaC$_2$. A GDS 850A emission spectrometer (Leco) was used in the studies.

Table 1. Chemical composition of the examined specimens, wt.%

|          | Al | Fe | Mn | Ni | Si | Zn | Cu |
|----------|----|----|----|----|----|----|----|
| Melt L (1) | 9.5 | 4.45 | 0.17 | 4.2 | 0.22 | 0.3 | rest |
| Melt M (2) | 9.7 | 4.45 | 0.17 | 4.30 | 0.20 | 0.15 | rest |
| Melt N (3) | 10.3 | 4.45 | 0.18 | 4.5 | 0.18 | 0.15 | rest |
| Ingot     | 10  | 4.5 | 0.15 | 4.1 | 0.23 | 0.3 | rest |

EN 1982 (PN-91/H87026)

|          | Al | Fe | Mn | Ni | Si | Zn | Cu |
|----------|----|----|----|----|----|----|----|
| 9-11     | 3.5 | -5.5 | 3.5 | -5.5 | rest |

Figure 1 shows the cast sample with gating and feeding system (upper drawing) and sample after preliminary machining used for testing of the heat treatment effect (down drawing).

Studies of the heat treatment carried out with a microjet device during solutioning (quenching) are shown in Figure 2. The work stand consists of a microjet device, special furnace for high-temperature heat treatment, a digital recorder of temperature changes with a control computer and additional terminal feeding microjet module with the cooling medium.

Figure 4a shows the specimen after heat treatment, while Figure 4b shows the machined specimen for testing of mechanical properties. An example of microjet solution heat treatment is shown in Figure 5, while Figure 6 shows the course of an ageing treatment; ageing (tempering) was applied in two temperature variants, i.e. low-temperature (a) and high-temperature (b).
3. Mechanical properties

The following designations of the sample condition were introduced: L - as-cast, P – solution heat treated, S1 – low-temperature aged (350°C) and S2 – high-temperature aged (700°C).

Table 2 presents mean values of the results obtained during variant studies of the CuAl10Fe4Ni4 alloy. Table 3 gives the corresponding maximum values of the properties, demonstrating the potential these alloys can offer in different states.

| State      | Modification | Rm  | Rp0.2 | A5% | HBW  |
|------------|--------------|-----|-------|-----|------|
| as-cast    | unmodified   | 676 | 282   | 4.9 | 5.2  |
|            | Ca+C         | 640 | 314   | 9.1 | 8.3  |
|            | CaC2         | 618 | 317   | 9.6 | 7.6  |
| solution   | unmodified   | 816 | 289   | 4.1 | 3.9  |
| heat       | Ca+C         | 801 | 499   | 3.2 | 4.4  |
| treated    | CaC2         | 718 | 577   | 2.5 | 2.0  |
| aged at    | unmodified   | 849 | 420   | 1.5 | 2.0  |
| 350°C      | Ca+C         | 890 | 668   | 2.5 | 1.9  |
|            | CaC2         | 815 | 774   | 2.0 | 1.0  |
| aged at    | unmodified   | 719 | 367   | 11.7| 12.8 |
| 700°C      | Ca+C         | 756 | 394   | 16.7| 15.6 |
|            | CaC2         | 683 | 389   | 10  | 9.1  |

Table 3.

| State      | Modification | Rm  | Rp0.2 | A5% | HBW  |
|------------|--------------|-----|-------|-----|------|
| as-cast    | unmodified   | 678 | 287   | 5.6 | 5.2  |
|            | Ca+C         | 658 | 321   | 9.9 | 9.4  |
|            | CaC2         | 637 | 332   | 10  | 8.2  |
| solution   | unmodified   | 825 | 345   | 4.8 | 4.3  |
| heat       | Ca+C         | 826 | 556   | 3.4 | 5.1  |
| treated    | CaC2         | 783 | 602   | 3.4 | 4.0  |
| aged at    | unmodified   | 915 | 489   | 2.1 | 2.0  |
| 350°C      | Ca+C         | 930 | 700   | 3.0 | 2.4  |
|            | CaC2         | 828 | 805   | 2.3 | 1.2  |
| aged at    | unmodified   | 735 | 414   | 12.6| 12.8 |
| 700°C      | Ca+C         | 765 | 420   | 16.9| 15.8 |
|            | CaC2         | 690 | 404   | 11.0| 9.7  |

4. Summary

The effect of heat treatment when applied to the alloy in both unmodified and modified state is particularly well visible during toughening (solution heat treatment and ageing). The highest values of Rm are obtained in low-temperature annealing (350°C) but at the cost of plastic properties (A, Z) and at a relatively high hardness. On the other hand, the application of high-temperature annealing (700°C) during toughening leads to the, so-called, betatisation, i.e. obtaining at room temperature a partially transformed β phase at the expense of a brittle γ2 phase, which enables obtaining much higher plastic properties at lower values of Rm and HBW. Quite notable is the increase of Rp0.2 after this heat treatment as compared to as-cast state.

Differences in the properties of alloys unmodified and after variant modification are relatively small with respect to Rm in as-cast state, but with clear improvement in the value of Rp0.2 for alloy modified with the additions of Ca + C and CaC2.
In a similar way is behaving the alloy in a solution heat treated state and after toughening combined with low-temperature annealing.

The use of CaC$_2$ modifier yields the mechanical properties inferior in all states to those obtained with an addition of Ca + C. As regards R$_{p0.2}$, better results after solution heat treatment and toughening combined with low-temperature annealing are obtained when modification is done with an addition of CaC$_2$.

As regards plastic properties (A, Z), only in as-cast state the addition of CaC$_2$ gives better results compared to alloy unmodified. In multi-variant heat treatment, the preferred addition is Ca + C.

Modifying of CuAl10Fe4Ni4 alloy with additions of Ca + C and CaC$_2$ has a beneficial effect on plastic properties, while the effect on R$_m$ still remains ambiguous, making this property worse in as-cast state and after solution heat treatment, and improving it after toughening. The effect of the examined modifying additives is not significant, except for the values of R$_{p0.2}$ in the state after toughening combined with low-temperature annealing.

More clear is the effect of heat treatment. In terms of mechanical properties (R$_m$), special attention deserves toughening combined with low-temperature annealing, allowing in particular cases obtaining even the R$_m$ = 930 MPa. On the other hand, toughening combined with high-temperature annealing leads to a significant improvement of plastic properties (A, Z) with mechanical properties kept at a satisfactory level.

Fig. 7. Martensitic transformations in Cu-Al alloys [4]

A variant of the concept of high-temperature annealing during toughening is based on partial preservation of the β phase to room temperature at the expense of the γ$_2$ phase. Figure 7 shows the martensitic transformations occurring in Cu-Al alloys. In the eutectoid reaction there is a partial transformation of β phase (with A2 lattice) into a β$_1$ phase (with DO3 lattice), followed by a peritectoid reaction of β$_1$ phase transforming into a β'$_1$ phase (with DO22 lattice). In alloys containing up to 10 wt.% Al, the solution heat treatment often makes β phase transform directly into a disordered fcc β' martensite; this martensite is designated as an α' phase (with 3R lattice).

A characteristic feature of Cu-Al alloys is the reversibility of phase transformations:

$$\beta \rightleftharpoons \beta' \rightleftharpoons \beta_1 \rightleftharpoons \beta'_1$$

In these alloys, in the region of the β phase, also a bainitic transformation with participation of the β$_1$ phase can occur when high-speed cooling is applied during the solution heat treatment. In hypoeutectoid alloys (in the state of equilibrium at <11.8 wt.% Al), coarse bainite is forming (a mixture of coarse lamellar α’ + β’$_1$ phases). The eutectoid and hypereutectoid alloys can have a fine-grain bainite.

Partial transformation of the β phase into martensite or bainite stimulates changes in mechanical properties of the heat treated CuAl10Fe4Ni4 alloy.

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