Heating rate measurement and characterization of a prototype surface-electrode trap for optical frequency metrology

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Abstract
We present the characterization of a prototype surface-electrode trap as a first step towards the realization of a compact, single-ion optical clock based on Yb+. The use of a SE trap will be a key factor to benefit from clean-room fabrication techniques and technological advances made in the field of quantum information processing. We successfully demonstrated trapping at a 500 μm electrodes distance and characterized our trap in terms of lifetime and heating rate. This is to our knowledge the highest distance achieved for heating rates measurements in SE traps. This simple 5-wire design realized with simple materials yields a heating rate of 8 × 10³ phonons/s. We provide an analysis of the performances of this prototype trap for optical frequency metrology.

1 Introduction
While the frame for single-ion optical clocks and trapped-ion quantum computing was set in the late twentieth century [1, 2], experimental progress accelerated drastically during the past 15 years. Single-ion optical frequency standards have reached stunning levels of accuracy [3, 4], and the realization of optical time scales and optical clocks networks is becoming a reality [5–7]. On the other hand, technological progress of SE traps has allowed tremendous advances both for quantum computation [8] and for the integration of advanced features in compact physical packages [9].

We are developing a compact single-ion clock based on a SE trap [10] using the 435.5 nm quadrupole transition in ¹⁷¹Yb+. Our target fractional frequency stability of < 10⁻¹⁴ τ⁻¹/₂ is ten times below commercial masers performances. With robust continuous operation and high output power at 2 × 435.5 = 871 nm, it would constitute a perfect optical flywheel for an operational all-optical timescale. Low systematic shifts and reproducibility would further enable the use of such a clock as a mobile reference in an optical clock network, and accuracy on the order of 10⁻¹⁷ would be attractive for relativistic geodesy campaigns.

We have tested a simple SE geometry using a printed circuit board (PCB) trapping chip on an FR4 substrate. FR4 (Flame Retardant 4) is a fiber glass reinforced epoxy resin with low outgasing properties [11]. Several teams have developed PCB traps [12–14] as a simple, low cost way to test a trapping configuration. To our knowledge, we are the first team developing such an SE trap for optical frequency metrology. Moreover, we have specifically chosen to work at a large trapping distance in order to prevent anomalous heating, which approximately scales as 1/d⁴ where d is the ion to electrodes distance. The use of a prototype PCB trap has allowed us to perform a pre-characterization of the potential performances of such a setup.

In this manuscript, we first describe our single-ion trap setup, and the trapping potential experimental characterization. We then present our heating rate measurements and a theoretical estimation of the performances of a single-ion clock based on such a trap.

2 Experimental setup
The trap used in this manuscript is a FR4 PCB circuit with a 5-wire geometry [15] using mini-SD in-vacuum electrical connection, described in [10, 16]. Figure 1 shows the electrodes layout. Electrodes are made of gold-plated copper,
Fig. 1 Drawing of the trap electrodes (5-wire geometry). Yellow: DC electrodes. Orange: RF electrodes. Violet arrow: laser beam direction. T: connection of a bias tee outside the chamber for modulation of the corresponding DC electrode voltage.

with a 25 μm thickness and a 120 μm inter-electrodes gap. The RF electrodes are 630 μm and 1200 μm wide. With the 330 μm wide ground RF electrode, this results in a 500 μm trapping distance. The RF electrodes asymmetry tilts the RF pseudopotential axes (x’, y’) in the (x, y) plane by about 10° [15], and lifts the trapping frequencies degeneracy.

RF electrodes connected to a low-loss RF inductance form a resonant LC circuit with resonance angular frequency $\Omega_{RF} = 2\pi \times 5.7$ MHz. Peak-to-peak voltages up to $V_{RF} = 280 V_{pp}$ can be obtained at the RF electrodes, resulting in theoretical trapping frequencies of up to 350 kHz for a single $^{176}$Yb$^+$ ion (all experiments presented in this article were performed with the $^{176}$Yb isotope for simplicity). Theoretical values are computed using an analytic model [17].

A set of DC voltages between −8.8 V and 6 V provides confinement in the z-direction and is fine-tuned to minimize excess micromotion (EMM) as described below. This results in an 85 kHz axial trap frequency.

The trap is housed in an octagonal titanium chamber [16]. A commercial ytterbium dispenser$^1$ outputs the atoms, and ions are produced by a two-stage photo-ionization process [18] using an isotopically selective 399 nm laser [19] and the 369.5 nm laser also used for Doppler cooling. Two additional lasers at 935.5 nm and 638 nm are used to repump the ions from the $^2D_{5/2}$ and $^2F_{7/2}$ states, respectively.

All four lasers are commercial extended cavity diode lasers (ECDL), and are brought to the experiment by a single endlessly monomode photonic crystal fiber$^2$ that outputs the beam at a 45° angle in the x–z plane shown Fig. 1. This provides a non-zero projection along all trap axes in order to cool down all three degrees of freedom [20]. The cooling laser is focused on a 60 μm waist spot close to the center of the trap, providing saturation parameters of several tens with powers of just a few tens of microwatts while limiting any charging of dielectric material from UV lasers. All lasers are frequency stabilized using a commercial wavemeter [21].

We detect the trapped ions fluorescence at 369.5 nm using a photomultiplier (PM) and a high quantum efficiency electron-multiplying CCD (EMCCD) camera.

### 3 Trap characterization

One of the fundamental requirements for an ion trap setup is to keep ions long enough for an experiment to be conducted. Trapping times up to several weeks or months are regularly reported in 3D traps [22], and trapping times of the order of several hours with cooling lasers are common with SE traps [23–25].

The background pressure is $5.5 \times 10^{-10}$ mbar, maintained by a hybrid ion-getter pump. The resulting lifetime, with cooling lasers on, is about 25 min. This is comparable with some other PCB traps lifetimes [12, 13]. This lifetime is compatible with a local partial pressure of order $10^{-10}$ mbar in the ion vicinity for species susceptible of molecule formations. Collisions can indeed lead to the formation of charged molecules such as YbO$^+$ or YbH$^+$ [26, 27]. It is remarkable that such a low background pressure could be achieved with a standard FR4 PCB and a non UHV-graded mini-SD slot.

We have measured the trap secular frequencies with relative uncertainty below $5 \times 10^{-5}$ by modulating the DC field amplitude [28] through a corner electrode (indicated by a “T” on Fig. 1). The axial frequency is measured to be 85 kHz, in agreement with the theoretical prediction. We also find a very good agreement between theoretical predictions and experimental measurements, with radial frequencies ranging from 225 to 350 kHz for RF amplitudes between 200 and 275 V.

One of the main challenges of ion trapping experiments is the ability to minimize excess micromotion (EMM) driven by the RF potential [29]. EMM affects clock operation through the relativistic second-order Doppler shift [30]. Experimental imperfections that cause EMM, like residual electric fields or RF electrodes phase mismatches for instance, also lead to an increase of the DC Stark shift associated to the time averaged squared electric field sensed by the ion [29]. It is, therefore, crucial to deterministically move the trapping position to the RF null and to measure the residual EMM.

When using a camera to image the ions, it is common with linear Paul traps to increase the RF peak-to-peak amplitude to observe the trap position converge towards the RF null [29]. This method has also been used to very precisely compensate EMM with SE trap geometries [31]. We have used this method as an initial coarse tuning, by positioning a single ion such that its spot center position, focus and fluorescence level stay identical when varying the RF

$^1$ Alvatec, now AlfaVakuo.

$^2$ NKT Photonics.
peak-to-peak amplitude over the entire range (100–270 V). With a resolution of 2.7 μm pixel⁻¹ and ion spots full width at half maximum (FWHM) of 7 μm, we can expect to position the ion within Δu = 3 μm of the RF null in each transverse direction. The SE trap simulations indicate a corresponding micromotion amplitude upper bound of ARF,rad ≈ 370 nm. We can evaluate the maximum residual static electric field to be \( E_{\text{trans}} = \left( \sqrt{2} \Delta u \right) \frac{M_{\text{ion}}}{e} < 37 \text{ V/m} \) with \( e \) the elementary charge.

A reduction below 10 V/m is required for clock operation with systematic shifts at the 10⁻¹⁷ level [32]. In order to enhance further the micromotion compensation, standard techniques rely on photon-correlation or sideband spectroscopy [29, 33]. We rather modulate the RF voltage amplitude at the trap secular frequencies so that the ion motion is resonantly excited and scan the ion position to find the least sensitive spot [34].

The influence of the RF voltage on the trap axial position is very low, but the presence of experimental stray fields can introduce non-negligible EMM along this direction. We have measured the single ion spot width as a function of its axial position while modulating the RF amplitude at the axial secular frequency. With this method, it is possible to position the ion within Δz = ±5 μm of the RF null in the axial direction, corresponding to a residual electric field \( E_z = \Delta z \frac{M_{\text{ion}}}{e} \leq 2.6 \text{ V/m} \). According to simulations, this is also equivalent to a maximum micromotion amplitude along the axis \( A_{\text{RF,ax}} \leq 5 \text{ nm} \).

We move the ion in the transverse plane around the RF null position by using alternatively the ground RF electrode and a set of ground DC electrodes. We directly observe the PM fluorescence level detected while slowly sweeping the RF modulation frequency on a 5 kHz range around one of the transverse secular frequencies. When the modulation frequency hits the secular frequency, the excitation of the ion motion is detected as a dip in the fluorescence spectrum. By minimizing the amplitude of this excitation alternatively in each tuning direction, the ion can be positioned to the RF null with a resolution of ±5 × 10⁻³ V on the control voltages. According to simulations, this corresponds to a maximum distance from the RF null \( |\Delta r| \leq 0.7 \text{ μm} \) (mostly along the \( y \) axis), with a maximum micromotion amplitude \( A_{\text{RF,rad}} \leq 60 \text{ nm} \). The maximum residual static electric field is evaluated to be \( |E_{\text{rad}}| = \Delta r \frac{M_{\text{ion}}}{e} \leq 6.2 \text{ V/m} \) in the transverse plane. This is below the required limit of 10 V/m mentioned above.

### 4 Heating rate measurements

When using trapped ions for coherent spectroscopy and for quantum information applications, the ions vibrational state should ideally be preserved during a probing sequence even in absence of cooling. The heating rate induced by electric noise at the trap electrodes [35] is thus another fundamental parameter that needs characterization and has led to numerous works where it is quantified and minimized [36]. The heating rate is quantified through the measurement of the temperature change of a single trapped ion using techniques such as the Doppler-recoupling method [37, 38], Raman spectroscopy [36] and the analysis of the ion spot pictures [39, 40].

We have used ion spot pictures measurements and the Doppler recoupling method. In both cases, we estimate the ion temperature after a controlled warm-up time where all lasers are turned off. Measuring the temperature of the ion as a function of this “dark time” provides an experimental value of the heating rate.

Experimentally achievable dark times are limited by the beam waist of our cooling laser at the trap position and the axial frequency of 85 kHz. Taking into account the 45° projection of the probe laser on the secular axis, we limit the highest measurable temperatures to 500 mK in order to neglect the influence of the spatial transverse variations of the beam intensity. This upper bound for temperature measurements also induces a limitation on the timescale of measurable Doppler-recoupling dynamics.

#### 4.1 Ion spot picture analysis

For temperatures down to the Doppler limit in the weak binding regime, the root mean square (RMS) value \( \sigma_u \) of the Gaussian position distribution of the ion is, in any of the secular axis direction \( u \) [41–43]:

\[
\sigma_u = \sqrt{\frac{k_B T_u}{M \omega_u^2}}
\]

with \( T_u \) the temperature along the secular direction, \( k_B \) the Boltzmann constant and \( \omega_u \) the trapping angular frequency along direction \( u \). The imaged fluorescence spot represents the ion position distribution convoluted with the imaging Point Spread Function (PSF). Assuming the PSF to be Gaussian with RMS value \( \sigma_{\text{PSF}} \), the detected spot is also Gaussian with RMS value \( \sigma_{\text{im}} \) [41]:

\[
\sigma_{\text{im}}^2 = \sigma_{\text{PSF}}^2 + \sigma_u^2.
\]

A difference \( \Delta T_u \) between temperatures \( T_{u,1} \) and \( T_{u,2} \) is easily expressed as a function of the corresponding measured spot sizes \( \sigma_{\text{im},1} \) and \( \sigma_{\text{im},2} \):

\[
\Delta T_u = T_{u,1} - T_{u,2} = \frac{M \omega_u^2}{k_B} \left( \sigma_{\text{im},2}^2 - \sigma_{\text{im},1}^2 \right).
\]

The heating rate can be extracted from the measurements of the ion spot size as a function of the dark time, and results
will, therefore, be presented as total image Gaussian variance $\sigma_{\text{im}}^2$ for simplicity and clarity.

The pictures exposure time needs to be long enough to ensure good signal-to-noise ratio (SNR) but short enough in regards of the cooling dynamics. We use the maximum available laser power at a detuning $\delta_{\text{pic}} \approx -5 \text{ MHz}$ small compared to the cooling transition natural linewidth $\Gamma_{\text{cool}} \approx 23 \text{ MHz}$, so that the cooling dynamics stay slow according to Doppler-recooling simulations, and the fluorescence level is close to its maximum while remaining on the cooling side of the transition. According to Doppler-recooling simulations with our experimental parameters, at the end of a 50$\mu$s exposure time, the temperature should not have dropped to less than 80% of its initial value. By measuring the ion spot size as a function of the picture exposure time, we have also checked experimentally that we cannot detect any reduction from the initial temperature with this value of 50$\mu$s. As a conservative estimate, 25% will still be added to the heating rate results to account for the temperature reduction caused by the exposure time.

In the experimental sequence, the 370 nm laser is kept ON only during the 50 $\mu$s exposure time, and shut down for a safety duration using an AOM during the camera readout. After the picture has been taken, the ion is cooled down for 50 ms by dropping the power of the 370 nm laser to 2.5 $I_{\text{sat}}$ and increasing the detuning to $\delta_{\text{cool}} \approx -20 \text{ MHz}$. These parameters are chosen experimentally as a compromise to protect the ion against high-energy collisions, at the expense of a relatively high temperature at the end of this cooling period. All lasers are then shut down using mechanical shutters to let the ion warm up for a controlled dark time.

In order to free oneself from the minimum resolution determined by the aberrated PSF, a set of data has also been recorded when artificially warming up the ion for 750$\mu$s before the dark time, by detuning the 370 nm laser to $\delta_{\text{cool}} \approx +40 \text{ MHz}$ with maximum available power. Under these conditions, we ensure $\sigma_\alpha \gg \sigma_{\text{PSF}}$.

Averaged images of 4000 sequences are fitted by a 2D Gaussian function inside an elliptical contour, as illustrated Fig. 2. A baseline plane is obtained and subtracted by fitting the background noise outside the ellipse to reject slow fluctuations.

Figure 3a displays the final data results for the axial direction after a simple dark time sequence as full blue squares, and with an initial warm-up pulse as full red disks. The corresponding open symbols are the results of the pictures taken just before the dark time for reference. These confirm that cooling is efficient, and are used to determine the measurements ordinate offset. A linear fit of the data returns slopes of $30 \pm 4$ and $22 \pm 4 \text{ mK s}^{-1}$, respectively. The heating rate is independent of the ion initial temperature within our error bars, which confirms that the measurement is not impaired by the imaging resolution.

The results for the $x$ direction are displayed on Fig. 3b using the same denotation. Because of the higher secular frequency in this direction, ion spot sizes are smaller and data barely exceed the measurement resolution. Similar linear fits return $52 \pm 45$ and $156 \pm 90 \text{ mK s}^{-1}$, respectively, but must only be considered as a conservative upper bound.

We have checked that these values are independent of residual excess micromotion, as it could be the case in presence of spurious noise around angular frequencies $\Omega_{\text{RF}} \pm \omega_\alpha [36]$. To do so, we have voluntarily introduced a supplementary voltage on the ground DC electrodes up to 10 times our minimum resolution for compensation and in both directions. According to trap simulations, this represents a translation of the ion out of the RF null in a composite direction of the two trap axes of up to $\pm 1.2 \mu$m, when operating the trap at $V_{\text{RF}} \approx 275 \text{ V}$. This corresponds to micromotion amplitudes up to 100nm. In this range, no evolution of the heating rate could be detected within our error bars.

In conclusion, this method allows to conservatively estimate the heating rate to be $33 \pm 4 \text{ mK s}^{-1}$ in the axial direction (average of the two measured slopes with added 25%) and provides an upper bound of $308 \text{ mK s}^{-1}$ for the transverse direction (maximum possible value of the slope with added 25%).
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4.2 Doppler-recooling method

The Doppler-recooling method was theoretically introduced in [37] side to side with the experimental results presented in [38]. The method relies on measuring the onset of the fluorescence signal when cooling lasers are shined onto a single ion. The mean dynamics of the fluorescence signal can be fitted with a simple 1D model to return a value of the temperature of the ion at the beginning of the cooling time.

We have also implemented this technique, as it is both widely used in the community and simple to setup. We used a 5 s dark time and two different detunings, and inferred the heating rate assuming a negligible initial temperature.

For $\delta v_{\text{cool}} = -5$ MHz, the data fit returns a temperature of $0.63 \pm 0.04$ K after 5 s without cooling, and of $0.37 \pm 0.07$ K for $\delta v_{\text{cool}} = -20$ MHz. They correspond to heating rates of $130$ mK s$^{-1}$ and $75$ mK s$^{-1}$, respectively.

The discrepancy between the ion spot analysis and the Doppler recooling method supports a non-negligible transverse heating rate. This points out that the simple Doppler-recooling method is not directly applicable in our case, because the single dimensionality assumption is not verified. In this regime, the Doppler-recooling method tends to an over-evaluation of the initial temperature [37]. The upper bound on the heating rate in the transverse direction can safely be reduced to $130$ mK s$^{-1}$.

Our results illustrate the fact that this method becomes inappropriate when the heating rate is comparable in two directions. In this case, only an upper bound can be obtained, as the theoretical model fails. This can mistakenly be overlooked if the Doppler-recooling method is not combined with another, direction-sensitive technique.

5 Discussion

Using the combined results of the two methods presented Sect. 4, we can infer the heating rate to be $33 \pm 4$ mK s$^{-1}$ in the axial direction and below $130$ mK s$^{-1}$ in the transverse direction. In order to put our results into perspective, we calculate the electric noise spectral density [44]:

$$\omega_u S_{E}(\omega_u) = \frac{4M \omega_u}{e^2} k_B T_u,$$

to obtain in the axial direction $\omega_u S_{E}(\omega_u) \approx 1.1 \times 10^{-5} \text{V}^2 \text{m}^{-2}$ and in the transverse direction $\omega_u S_{E}(\omega_u) \approx 1.9 \times 10^{-4} \text{V}^2 \text{m}^{-2}$. Given our $500 \mu$m trapping distance, these results add up rather well to the point clouds found in the literature [44]. The presence of a non-negligible transverse heating rate combined with the measured trap lifetime and the observation of high-energy collisions at a 2 min$^{-1}$ rate during Doppler-recooling sequences is a strong indication of a rather high background pressure at the trap location. This could be a source of collisional heating, which will be removed in a next experiment by using better materials.

It can be useful when investigating clock operation to use the axial and transverse secular frequencies, 85 kHz and 350 kHz respectively, to express the heating rate

$$\dot{\theta}_u = \frac{k_B T_u}{\hbar \omega_u},$$

measured with this work in both directions close to $8 \times 10^3$ phonons s$^{-1}$.  

![Fig. 3](image-url)
Table 1 Summary of the motion-related shifts that would impair our trapping geometry

| Shift           | Prototype trap | Prototype trap advanced | State-of-the-art materials |
|-----------------|----------------|-------------------------|---------------------------|
| 2nd order Doppler | $1.3 \times 10^{-17}$ | $1.3 \times 10^{-17}$ | $\approx 10^{-18}$ [54]   |
| Stark           | $2.7 \times 10^{-17}$ | $0.9 \times 10^{-17}$ | $\approx 10^{-18}$ [55]   |
| Quadrupole      | $10^{-15}$      | $10^{-16}$         | $\approx 10^{-17}$ [55]   |

See text for details

This value can be used to discuss our prototype trap properties regarding a hypothetical clock operation. As a reminder, the prospect of the experiment is to use the $^3S_{1/2} \leftrightarrow ^3D_{3/2}$ quadrupolar transition at 435.5 nm in $^{171}$Yb$^+$ as the clock transition. The upper state $^3D_{3/2}$ of this transition has a lifetime of $\tau \approx 52$ ms [45, 46].

During clock interrogation, the ion temperature should stay as unaffected as possible. Ideally, the heating rate $\dot{\bar{n}}$ should satisfy $\dot{\bar{n}} \tau_c \leq \bar{n}$, where $\bar{n}$ is the mean phonon number and $\tau_c$ is the period spent without cooling during the sequence [32]. With our upper bound estimate for the heating rate of $\dot{\bar{n}} \sim 8 \times 10^3$ phonons s$^{-1}$, this would limit $\tau_c$ to a few ms only when probing in the transverse direction. This corresponds to a quantum-projection-noise limited fractional frequency stability of $5 \times 10^{-14} \tau^{-1/2}$ assuming a 1 s cycle time. To bypass this limitation, the heating rate should be reduced below $\dot{\bar{n}} < 10^3$ phonons s$^{-1}$ in the transverse direction and be negligible compared to the axial heating rate we measured with our prototype chip. These values are well within reach with state-of-the-art setups.

The ion heating can also induce a loss of contrast when fringes are washed out by the wavefunction spread-out over many motional states [47–50]. This is prevented when the Lamb–Dicke criterion $\eta^2 \bar{n} \ll 1$ is verified, where $\eta^2 = \left( \frac{2\tau_c}{\lambda \cos \theta_{sec}} \right)^2 \frac{\hbar}{2M_0\omega_{sec}}$ with $\lambda$ the laser wavelength, $\theta_{sec}$ the angle between the laser direction and the secular axis and $\omega_{sec}$ the trap secular frequency.

The Doppler cooling limit for ytterbium is $T_D = \frac{\hbar \omega_{sec}}{2k_B} \approx 0.47$ mK. Along the transverse directions, our trapping frequencies lead to $\eta^2 \bar{n} \approx 0.25$ at 0.5 mK. The access to higher secular frequencies would enable to work even deeper in the Lamb–Dicke regime.

Table 1 summarizes the estimated motion-related shifts that could be observed with the current performances of our trap. First, this includes the 2nd order Doppler shift from secular and micromotion. Since all motional frequencies and the trap field frequency are much lower than the frequency of the optical transition, this also includes the static Stark shift from the time averaged squared electric field seen by the ion [29, 30, 51]. The estimated maximum EMM amplitude $A_{RF, rad} \leq 60$ nm is used to estimate both the maximum kinetic energy and electric fields sensed by the ion. For Doppler temperatures and our level of micromotion compensation, the 2nd order Doppler shift is indeed mainly determined by the EMM and can be estimated directly as $\frac{\Delta v_{\text{emm}}}{v_{\text{2ndDopp}}} = \frac{\Omega_{RF}^2 k_B T_c}{4c^2}$. The DC Stark shift stems from both secular motion, ordinary micromotion and excess micromotion [29]. Using the fact that the differential scalar and tensor polarizabilities of the quadrupole transition $\Delta \alpha_S$ et $\Delta \alpha_T$ are of opposite signs [52], a conservative upper bound can be calculated with:

$$\hbar |\Delta v|_{\text{max Stark}} = \frac{1}{2} \left( \frac{M\alpha^2 k_B T_c}{e^2} + \sum_{\text{mm}} \frac{M\Omega^2_{RF} k_B T_u}{e^2} \right) + \frac{1}{2} \left( \frac{M\Omega^2_{RF} A_{RF,ax}}{e} \right)^2 + \left( \frac{M\Omega^2_{RF} A_{RF,rad}}{e} \right)^2 \cdot |\Delta \alpha_S - \Delta \alpha_T|.$$  

which is also dominated by the EMM terms in the transverse direction. We use experimental values found in [53] for $\Delta \alpha_S$ and $\Delta \alpha_T$.

The spatial spread caused by the heating rate will not contribute to an increase of the EMM, neither regarding the 2nd order Doppler shift nor the related static Stark shift term. The noise spectral density leading to the measured heating rate, by itself, leads to completely negligible static Stark shift.

Our trap uses a quadrupole trap geometry. For this reason, electric field gradients are intrinsically present and lead to a quadrupole shift of the clock transition [30, 51]. The RF field contribution averages to 0 at first order. The second order can be significant [56], but cancels out when using the right Zeeman sublevels [53].

Table 1 first column shows the shifts we expect given the results of our prototype trap characterization. The second column takes into account the potential use of rejection-schemes that can be implemented to reduce the Stark shift by a factor of three and the quadrupole shift by an order of magnitude [22, 30, 57]. With such schemes, a clock based on such a simple 5-wire trap geometry and inexpensive materials would exhibit trap-related shifts on the order of a few $10^{-17}$.

We can evaluate the hypothetical performances of a clock based on the same trapping geometry with state-of-the-art materials from the literature [30, 54, 55]. For such an estimation, we rely on figures measured with 3D trap geometries, where the use of a 2D trap should not induce a difference. Exclusive use of ultra-high vacuum compatible, low outgassing materials will enable much longer trapping lifetimes, and might also reduce collisional heating if present. Moreover, electrodes surface quality have an influence on anomalous heating, and will also be improved with state-of-the-art
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6 Conclusion

We have developed and characterized a PCB prototype SE trap as a first test towards the development of a compact single-ion optical clock. We have successfully trapped ions at a $500 \mu\text{m}$ trapping distance for the electrodes, which is to our knowledge the highest distance used in a surface ion trap for heating rate measurements.

The measured lifetime of 25 min and heating rate of $8 \times 10^3$ phonons/s are compatible with the literature, and are most likely limited by the background pressure in the trap vicinity. Given these results, we estimate that such a simple trap would lead to a fractional frequency instability of around $5 \times 10^{-14}$ using Rabi spectroscopy, while trap-related fractional frequency shifts would be below $10^{-16}$. Such a clock would already constitute a considerable achievement.

A trap based on the simple five-wire geometry with high trapping distance is, therefore, compatible with optical frequency metrology. For improved performances, the use of better materials and a lower background pressure are necessary. To both reduce the heating rate and work deeper in the Lamb–Dicke regime, higher trapping frequencies ($> 500 \text{kHz}$) in the transverse plane should be used, which is compatible with state-of-the-art ion trapping techniques. Under such conditions, fractional frequency stability would be improved by the higher achievable contrasts. We estimate that trap related fractional frequency shifts (2nd-order Doppler, Stark and quadrupole shifts) would be reduced to about $10^{-17}$. Further reduction would be obtained by working with the octupole transition at 467 nm.

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Author contributions T. Lauprêtre and C. Lacroûte wrote the main manuscript text. T. Lauprêtre was involved in all experimental works and results analysis, and prepared the figures. B. Achi was involved in the data taking, results analysis, and setup of the experiment automated control. C. Lacroûte was involved in setting up the ion trap and optical bench, in the data taking and results analysis. All authors reviewed the manuscript.

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Declarations

Conflict of interest The authors declare no competing interests.

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