A Hybrid Approach for Cardiac Blood Flow Vortex Ring Identification Based on Optical Flow and Lagrangian Averaged Vorticity Deviation

Ke Yang1,2, Shiqian Wu3, Oluwarotimi W. Samuel4, Hui Zhang5, Dhanjoo N. Ghista6, Di Yang1,2 and Kelvin K. L. Wong*

1 Key Laboratory of Metallurgical Equipment and Control Technology, Ministry of Education, Wuhan University of Science and Technology, Wuhan, China, 2 Hubei Key Laboratory of Mechanical Transmission and Manufacturing Engineering, Wuhan University of Science and Technology, Wuhan, China, 3 School of Information Science and Engineering, Wuhan University of Science and Technology, Wuhan, China, 4 Shenzhen Institutes of Advanced Technology, Chinese Academy of Sciences, Shenzhen, China, 5 Ultrasound Department, The Third Affiliated Hospital of Sun Yat-sen University, Guangzhou, China, 6 University 2020 Foundation, Inc., California City, CA, United States

Objective: The measurement of cardiac blood flow vortex characteristics can help to facilitate the analysis of blood flow dynamics that regulates heart function. However, the complexity of cardiac flow along with other physical limitations makes it difficult to adequately identify the dominant vortices in a heart chamber, which play a significant role in regulating the heart function. Although the existing vortex quantification methods can achieve this goal, there are still some shortcomings: such as low precision, and ignoring the center of the vortex without the description of vortex deformation processes. To address these problems, an optical flow Lagrangian averaged vorticity deviation (Optical flow-LAVD) method is proposed.

Methodology: We examined the flow within the right atrium (RA) of the participants’ hearts, by using a single set of scans pertaining to a slice at two-chamber short-axis orientation. Toward adequate extraction of the vortex ring characteristics, a novel approach driven by the Lagrangian averaged vorticity deviation (LAVD) was implemented and applied to characterize the trajectory integral associated with vorticity deviation and the spatial mean of rings, by using phase-contrast magnetic resonance imaging (PC-MRI) datasets as a case study. To interpolate the time frames between every larger discrete frame and minimize the error caused by constructing a continuous velocity field for the integral process of LAVD, we implemented the optical flow as an interpolator and introduced the backward warping as an intermediate frame synthesis basis, which is then used to generate higher quality continuous velocity fields.

Results: Our analytical study results showed that the proposed Optical flow-LAVD method can accurately identify vortex ring and continuous velocity fields, based on optical flow information, for yielding high reconstruction outcomes. Compared with
INTRODUCTION

The vortex formation in blood flow within the heart plays an important role in characterizing the function of the blood flow mechanism and energy transfer to the heart chamber, which are important indicators that can be used to quantify the overall heart function. The fluid flow transported by the vortex formation is observed to be more efficient than that transported by a steady, straight jet flow of fluid, in terms of aiding the circulation of blood to the various regions of the heart chamber (Dabiri and Gharib, 2005; Kheradvar and Gharib, 2007, 2009; Kheradvar et al., 2007; Wong et al., 2009a). As we know, the cardiac myocardium has inter-twined helical fibers. So when they contract, the heart chamber twists, and this is how blood is efficiently ejected out of the chamber. Now this heart chamber twisting causes the formation of vortex rings of high vorticity in blood flow in the chamber. In contrast, cardiomyopathic hearts have impaired contractility, and hence less twisting; hence, they have smaller vortex rings with lower vorticity (Sengupta et al., 2006). So, the formation of vortex rings is closely associated with cardiac function, and the health status of an individual. This is why, in conjunction with the structural parameters of the heart, the vortex flow analysis provides an insight into its functional analysis, and helps distinguish normal subjects from patients with heart disease (Kheradvar et al., 2019). Therefore, developing a method that can enable quantification of the vortex ring characteristics and its dynamic changes during the cardiac cycle can enable understanding of the vortex ring’s physiological functions and facilitate exploration of heart diagnostics and its pathological changes (Kräuter et al., 2020).

Interestingly, phase-contrast magnetic resonance imaging (PC-MRI) allows three-dimensional MR velocity mapping based on the intrinsic sensitivity of MRI to flow, and provides a unique tool for measuring complex blood flow patterns in vivo (Markl et al., 2007; Dyverfeldt et al., 2015). Earlier Wong et al. (2009a) conducted a study in which the vorticity of vortex flow was measured by using the flow field obtained from scanned PC-MRI, to characterize the location and strengths of vortices within a cardiac chamber. A major limitation of this study is that it is based on global estimation, and does not include extraction of localized information from the vortex region to elucidate the function of dominant vortexes. The identification of the dominant vortex ring is the key for the comprehensive description of the resulting swirling blood flow within a heart chamber (such as the left ventricle) resulting in blood outflow.

Since there is no uniform definition of vortex (Epps, 2017; Günther and Theisel, 2018), different vortex criteria have been used to extract vortex flow information within the heart chamber (Wong et al., 2010; Töger et al., 2012; Elbaz et al., 2014; Kräuter et al., 2020). Elbaz et al. (2014) adopted the criterion $\lambda_2$ for left ventricular (LV) vortex detection in early and late diastolic inflow. Kräuter et al. (2020) computed the divergence-free part of the velocity vector for Q criterion-based identification vortex throughout the cardiac cycle. The above-mentioned methods are region-based and used to extract instantaneous vortex rings in a single frame, which hinders proper exploration of vortex formation processes. Töger et al. (2012) considered Lyapunov exponent values higher than 50% as the Lagrangian vortex ring to identify vortex boundaries. The Lagrangian vortex ring can more accurately describe the developmental process, but the method is conservative and does not include the vortex core (Kräuter et al., 2020). In Yang et al. (2021), we have employed Lagrangian averaged vorticity deviation (LAVD) to identify the cores and regions of the Lagrangian vortices and Eulerian vortices, for measuring the vortex volume and vorticity in the LV blood flow for more accurate quantification of the vortex formation. Wong et al. (2010) identified two dominant vortices of opposite rotation in the right atrium (RA), but they applied an unsupervised data clustering algorithm without considering the characteristics of blood flow. This is what has led to our preparing this paper, to improve the description of the vortex characterization in the RA by employing LAVD for more accurate identification and quantification of blood flow vortex rings.

Therefore, for accurate identification and tracking of the cardiac vortex ring characterization, this study presents a novel method (Optical flow-LAVD), which is precise in the extraction of Lagrangian vortex core and associated regions within the heart, based on the PC-MRI data. The proposed algorithm implements the trajectory integral of the normed deviation of vorticity from its spatial mean, for LAVD-based identification and tracking of the cardiac Lagrangian vortex rings (Haller et al., 2015). At the same time, we adopt the Horn-Schunck (Horn and Schunck, 1981) brightness constraint to synthesize the intermediate PC-MRI data for yielding high quality continuous velocity fields to reduce the error caused by the integral process of LAVD. Additionally, we have extensively validated the accuracy of the
The displacement gradient of $\mathcal{F}^t_{t_0}$ can describe the distance of two particles from time $t_0$ to $t_1$, one at $x_0$ and the other is adjacent to it at $x_0 + \delta x(t_0)$. Using mathematical representation, we have the following function

$$\Delta \mathcal{F}^t_{t_0}(x_0) = \frac{dx(x_0, t_0, t)}{dx_0} t \in [t_0, t_1].$$

It is to be noted that the $\Delta \mathcal{F}^t_{t_0}$ tensor does not provide an objective indication of the rotational component of the deformation, because the polar rotation angle extracting from this mapping depends on the observer (Haller, 2016). To address this issue, Haller et al. (2015) used a technique based on the Dynamic polar Decomposition (DPD) to decompose $\mathcal{F}^t_{t_0}$ into the dynamic rotation tensor $O^t_{t_0}$ and the right dynamic stretch tensor $M^t_{t_0}$, and this is denoted as follows

$$\Delta \mathcal{F}^t_{t_0} = O^t_{t_0} M^t_{t_0} t \in [t_0, t_1].$$

Then, $O^t_{t_0}$ can be further factorized into two tensors. Specifically, we have

$$\Delta \mathcal{F}^t_{t_0} = \Phi^t_{t_0} \Theta^t_{t_0} M^t_{t_0} t \in [t_0, t_1],$$

wherein, $\Phi^t_{t_0}$ is relative rotation and $\Theta^t_{t_0}$ describes the mean rotation (Haller et al., 2015). The $\Phi^t_{t_0}$ has a dynamic consistency, which implies that the total angle swept by this tensor around its axis of rotation is dynamically consistent. Because of the feature of any physical rigid body motion, this angle will satisfy the relationship

$$\psi^t_{t_0}(x_0) = \psi^t_{t_0}(x_0) + \psi^t_{t_0}(x_0) s, t \in [t_0, t_1],$$

where $\psi^t_{t_0}$ is the intrinsic rotation angle. Using the result obtained in Haller (2016), it can be computed as

$$\psi^t_{t_0}(x_0) = \frac{1}{2} \int_{t_0}^t |\omega(x(x_0, s), s) - \sigma(s)| ds,$$

where $\omega(x(x_0, s), s)$ is the vorticity along a material trajectory, and $\sigma$ describes the spatial mean of vorticity. The LAVD is defined by an integral component of the above Eq. (7), as follows

$$LAVD^t_{t_0}(x_0) = \int_{t_0}^t |\omega(x(x_0, s), s) - \sigma(s)| ds.$$

Based on this Eq. (8), a rotationally coherent Lagrangian vortex is defined as a nested set of outward decreasing tubular level sets of LAVD. The LAVD is objective, and we note that this measure is relative to its neighborhood, and its value-range depends on the flow domain. In this study, the region relative to the vortex is large, and of the size of RA, based on manual segmentation. The boundary of the Lagrangian vortex is the outermost closed convex level surface of LAVD, satisfying convexity deficiency, while the vortex core is the local maxima of LAVD enclosed by the boundary (Haller et al., 2015; Yang and Melissa, 2015). Hence, we define the boundaries of Lagrangian vortex within the heart as the outermost members of closed families of LAVD level curves falling below a convexity deficiency threshold.

The LAVD also leads to a difficulty: The Lagrangian vortex is intrinsically tied to a specific finite time interval over which
they exert their influence on nearby trajectories (Eppe, 2017; Katsanoulis et al., 2017). Short-time variability of flow within a cardiac chamber is often seen as significant in computing the LAVD values. Therefore, we adopt the Horn-Schunck (Horn and Schunck, 1981) optical flow to synthesize the intermediate PC-MR velocity data in time and space, for producing a more accurate continuous velocity field $v(x, t)$.

**Intermediate PC-MR Velocity Data Synthesis**

As expressed in Eq. (8), the computation of LAVD represents an integral process, but the PC-MR velocity data are obtained within the large discrete frames and have a limited temporal resolution. So in this study, we innovatively introduce the optical flow-based intermediate PC-MR velocity data synthesis to compute LAVD.

**Horn-Schunck Optical Flow**

Recent optical flow assessment methods (Wulff et al., 2017; Xu et al., 2017) take on the variational approach introduced by Horn and Schunck (HS) (Horn and Schunck, 1981). The HS optical flow can perform on consecutive frames and predict the motion of pixels from one frame to the other, by iteratively settling an optimization issue formulated from two constraints (Afrashteh et al., 2017). The first constraint is “brightness constancy,” and it assumes that a pixel has the same brightness level in two frames after movement,

$$I(x + u, y + v, t + dt) = I(x, y, t), \quad (9)$$

where (i) $I(x, y, t)$ is the pixel brightness in the first frame at spatial location $(x, y)$ and time $t$, and (ii) $I(x + u, y + v, t + dt)$ is the pixel brightness in the next frame at $t + dt$ after $(u, v)$ displacements from $(x, y)$ in $x$ and $y$ directions, respectively. The second constraint is “spatial smoothness,” which prevents discontinuities in the flow field, as follows

$$|\nabla u|^2 = \left(\frac{\partial u}{\partial x}\right)^2 + \left(\frac{\partial u}{\partial y}\right)^2 \text{ and } |\nabla v|^2 = \left(\frac{\partial v}{\partial x}\right)^2 + \left(\frac{\partial v}{\partial y}\right)^2. \quad (10)$$

These two constraints are combined to use the first-order form of Tikhonov’s formulation for solving the minimization problem (Horn and Schunck, 1981; Liu and Shen, 2008). Mathematically,

$$\min_{u, v} \left\{ \int (I_t + I_x u + I_y v)^2 dx dy + \alpha \int (|\nabla u|^2 + |\nabla v|^2) dx dy \right\}, \quad (11)$$

where (i) $I_t$, $I_x$, and $I_y$ are derivatives of $I(x, y, t)$ with respect to time, spatial direction $x$ and $y$, respectively, and (ii) $\alpha$ is the ratio of weights of the brightness constancy integral to that of spatial smoothness. This equation is solved numerically to estimate the values of $u$ and $v$ (Akemann et al., 2012).

**Intermediate PC-MRI Synthesis**

Given two input PC-MRI $I_0$ and $I_1$ and a time $t \in (0, 1)$, our purpose is to estimate the intermediate PC-MRI $\hat{I}$ at time $T = t$. Based on HS optical flow and inspired by intermediate video frame interpolation (Meyer et al., 2015; Jiang et al., 2018), we propose fusing the warped input PC-MRI at time $T = t$. Let $(u, v)_{t \to 0}$ and $(u, v)_{t \to 1}$ represent the optical flow from $I_t$ to $I_0$ and $I_t$ to $I_1$, respectively. We can synthesize the intermediate PC-MRI $\hat{I}$ as follows

$$\hat{I} = \alpha_0 \bigodot g(I_0, (u, v)_{t \to 0}) (1 - \alpha_0) \bigodot g(I_0, (u, v)_{t \to 1}), \quad (12)$$

where $\bigodot$ denotes the element-wise multiplication (Horn and Schunck, 1981).
where $g(\cdot, \cdot)$ is a backward warping function, which can be executed using bilinear interpolation and is differentiable (Zhou et al., 2016). The parameter $\alpha_0$ controls the contribution of the two input PC-MRI images, and depends on two factors: temporal consistency and occlusion reasoning (Jiang et al., 2018). The $\Theta$ represents element-wise multiplication, implying content perception weighting of input PC-MRI. For temporal consistency, the closer the time step $T = t$ is to $T = 0$, the greater contribution of $I_0$ makes to $I_1$; a similar property holds for $I_1$ (Jiang et al., 2018). On the other hand, considering the particularity of PC-MRI acquisition process, the occlusion question can be neglected. As a result, we can obtain the intermediate PC-MRI on consecutive frames based on Eq. (12) to produce a continuous velocity field for detecting LAVD.

The pipeline for Optical flow-LAVD based identification of Lagrangian vortex ring consists of four steps, and these steps are presented in Figure 2. First, the HS optical flow computation on consecutive frames is carried out. Second, based on the HS optical flow, the intermediate PC-MRI can be synthesized to produce a continuous velocity field. Third, the segmentation of the interested cardiac chamber is performed. Finally, the LAVD is computed and used to detect the Lagrangian vortex core and region within the cardiac chamber.

RESULTS OF ANALYTICAL STUDIES

Optical Flow-LAVD Based Vortex Ring Identification and Analysis

The proposed algorithm successfully identifies large-scale Lagrangian vortex rings that appear in the RA and analyzes their changes and evolution during selected time frame indices from $N_t = 8$ to $18$. As expressed in our previous research, vortex within the RA is formed and deformed during this period (Wong et al., 2009a). The variation of the Lagrangian vortex ring core and region can be visually examined by using the red circular markers as shown in Figure 3. The computation of the LAVD within the RA is based on Eq. (8), and the convexity deficiency of a closed curve in the plane is defined as the ratio of the area difference between the curve and its convex hull to the area enclosed by the curve (Haller et al., 2015). Then we can refer to our work in Yang et al. (2021) and visualized analysis, for the convexity deficiency threshold $d_{max} = 1$, to ensure the tubular characteristics in the heart (Yang et al., 2021). In addition, the volume of each Lagrangian vortex ring can be computed as the product of the area inside the delineation and the slice thickness, which is in line with an earlier study by Töger et al. (2012).

Figure 3 illustrates the temporal evolution of vortex volume within the RA of the healthy subject.

Horn-Schunck Optical Flow Based Intermediate PC-MRI Synthesis Analysis

Impact of Different Components on the Quality of PC-MRIs

For evaluation, we performed a number of ground-truth comparisons using the leave-some-out method (Meyer et al., 2015), i.e., the intermediate PC-MRIs are synthesized and compared to the original ones. We reported the Structural Similarity Index (SSIM) scores of predictions and ground-truth, as well as the interpolation errors (IE) (Meyer et al., 2015). To prevent noise and irrelevant content interference, we just computed SSIM and IE of the interested cardiac chamber.

We analyzed the impact of leaving out an increasing number of intermediate PC-MRI on decaying in image quality. The plot in Figure 4A visualizes the variation of IE of synthesized PC-MRI when skipping increasing frames. At the same time, we derived the SSIM and IE at different algorithm steps, as shown in Table 1. It can be seen that the optical flow computed before segmentation can obtain better intermediate images. Based on Eq. (11), we also carried out an experimental analysis of the influence of the main parameter $\alpha$ on the quality of reconstructed intermediate PC-MRI, as shown in Figure 4B.

Comparison With Other Interpolation Methods

We compared three different views including optical flow interpolation, phase-based interpolation, and linear interpolation to deal with the construction of the intermediate PC-MRI. The most popular methods for finding pixel correspondences across images are based on optical flow (Sun et al., 2010; Baker et al., 2011), while using image phase information directly to replace image brightness in the data term of standard optical flow formulations has been noticeable (Fleet and Jepson, 1990; Meyer et al., 2015). The phase-driven frame interpolation concept was applied to the discrete Fourier transform of an image, and it decomposes the input images into several oriented frequency bands $R_{\omega, \theta}$ by steerable pyramid filters (Meyer et al., 2015).

Then, Linear interpolation in time and space has been adopted to produce a continuous velocity field based on PC-MR velocity data (Töger et al., 2012). We have detailed the comparison of SSIM and IE during the selected time frame indices from $N_t = 8$ to $18$, as shown in Figures 4B,C. By comparing SSIM and IE, we find that the HS optical flow method has higher prediction quality, especially in the case of existence of a large-scale vortex. Hence, combined with HS optical flow based Intermediate PC-MRI synthesis to recover a more accurate continuous velocity field, the LAVD can describe precisely the evolution of Lagrangian vortex rings within the RA, to help medical experts enhance their understanding of the physiological functions of swirling blood flow.

Visual Analysis and the Experiment on Segmentation Dependence

We have carried out a visualization analysis of the difference between Optical flow-LAVD and linear interpolation-LAVD, as shown in Figure 5. The identification results of vortex rings within the RA based on different methods are represented by red and orange circular markers, respectively. In order to clearly reveal the distinction of the visual results, we selected time frame indices of large-scale vortex existent from $N_t = 8$ to $10$. It is found that the Optical flow-LAVD can more accurately describe the complexity of the Lagrangian vortex ring boundary.
Two consecutive PC-MRI
A-P Orientation

Nt=7

Nt=8

HS Optical flow Computation

Optical flow from Nt = 7 to Nt=8 (A-P)

Nt=7

Nt=8

F-H Orientation

Nt=7

Nt=8

Intermediate PC-MRI synthesis based on optical flow

Construction of continuous velocity field (X-orientation)

Nt=7

Nt=8

Intermediate PC-MRI

Construction of continuous velocity field (Y-orientation)

Nt=7

Nt=8

Right atrial segmentation

The cycle describes right atrial contour

Continuous velocity field

Continuous velocity plot after segmentation

LAVD computation

The Lagrangian vortex core and region can be extracted by LAVD

FIGURE 2 | The pipeline of the proposed Optical flow-LAVD based identification of Lagrangian vortex ring.
In order to assess the sensitivity of Optical flow-LAVD based vortex ring extraction using different segmentation masks, we have derived the Dice similarity coefficient (DSC) as

$$\frac{2TP}{TP + FP + FN}$$

where the TP, FP, TN, and FN represent the number of true positives, false positives, true negatives, and false negatives, respectively. We applied two different masks to selected time frame indices from $N_t = 8$ to $18$ and computed the DSC of the identification results of vortex rings under manual segmentation and automatic segmentation. Table 2 provides the DSC and segmentation time to verify the robustness of the Optical flow-LAVD to different segmentation masks.

**DISCUSSION**

We have presented a novel method for the identification of Lagrangian vortex rings core and region within the RA from PC-MRI data to allow for quantitative vortex volume. In particular, we have demonstrated (i) the variation in Lagrangian vortex rings within the RA during the diastolic phase from time frame indices $N_t = 8$ to $18$ of one cardiac cycle with 25 phases. (ii) the characteristics of the PC-MRI by constructing accurate continuous velocity fields, based on an image-optical flow algorithm for computing LAVD.

**Lagrangian Vortex Rings Within RA Identification and Analysis**

We have extracted the large-scale Lagrangian vortex rings that appear in the RA, and have analyzed their development and changes during selected time frame indices from $N_t = 8$ to $18$, which is in accordance with the previous publications (Wong et al., 2009a,b, 2010). The development of the vortex rings core and region can be visually examined using red circular as shown in Figure 3. In addition, we superimposed the corresponding MR images onto these LAVD maps to give an indication of the location of the vortex features with respect to the chamber walls. In the beginning during time frame $N_t = 8$ to $10$, two large-scale Lagrangian vortex rings exist in the chamber simultaneously, and we can note from Figure 3 that one counter-clockwise (CCW) Lagrangian vortex ring exists in the atrium along with a second clockwise (CW) Lagrangian vortex ring approximately to the upper-left of it. At the same time, the consequences of LAVD based identification are asymmetric, subject to the asymmetry of the heart as a whole (Kilner et al., 2000). Then later during time frame $N_t = 12$ to $14$, two typical vortex rings are partly dissipated, and they cannot remain strictly toroid and change over time. In particular, the CCW Lagrangian
vortex ring decomposes into two vortex rings of different scales, one of which moves toward the chamber wall regions. Eventually during time frame $N_t = 16$ to $18$, we identified two dominant vortex rings of opposite rotation to grow in scale until the CCW vortex ring becomes slightly larger than the CW one.

The relative rotation region variation of two vortex rings is demonstrated by plotting the vortex volume with respect to cardiac time frames, as shown in Figure 3. Toward the end-systole from $N_t = 8$ to $10$, the flow slows down and a corresponding dilation of the RA induces the flow in the inferior and superior vena cava to accelerate (Kilner et al., 2000). We note that the volume of two vortex rings of opposite rotation is increased, and the volume of the CW vortex ring and CCW vortex ring grow from $6.26$ to $7.74$ ml and $3.28$ to $3.84$ ml, respectively. With the opening of the atrioventricular valves, the blood surges into the relaxed ventricle from $N_t = 12$ to $14$ (Kilner et al., 2000). The volume of the two vortex rings is decreased, and declines from $1.36$ to $0.31$ ml and $1.22$ to $0.90$ ml (the volume sum of two CCW vortex rings), respectively. From time frame $N_t = 16$ to $18$, the volume of CW and CCW vortex rings change successively and range from $2.66$ to $1.35$ ml and $0.73$ to $3.13$ ml, respectively. The enlarged vortex rings can minimize stasis and thereby facilitate the flow of blood into the ventricle (Töger et al., 2012). After $N_t = 18$, we do not extract the Lagrangian vortex ring within RA, as a large amount of blood had flowed into the ventricle and there was no strict toroid flow. We set the convexity deficiency threshold to 1 in order to ensure the tubular characteristics (Haller, 2016; Yang et al., 2021). In conclusion, based on the statistics of the volume plot, we can describe the Lagrangian vortex ring development in a quantitative manner. Lagrangian vortex rings are distinctive material curves that organize the blood flow (Günther and Theisel, 2018). They present steady swirling scale flow, and manifest the persistence of Lagrangian vortex rings within the heart, to enable understanding of the role of evolution of vortices in the blood flow. We have also visualized the stretching and diffusion of vortex rings, which give deeper insight into vortex dynamics, revealing how vortex rings are weakened or reinforced by the cardiac flow field.
Intermediate PC-MRI Synthesis Analysis
Impact of Different Components on the Quality of PC-MRIs

We first investigated whether leaving out an increasing number of intermediate PC-MRI decays the synthesis quality. We computed IE under four different conditions: skipping single, two, three, and four frames. Figure 4A shows the degradation in the quality of interpolated PC-MRI with increased motion between frames. In order to estimate it more reliably and accurately, we simply use two consecutive frames to construct a continuous velocity field. We have also investigated the contribution of segmentation in our method, as shown in Table 2. By applying the step of computing optical flow first and then segmentation, better interpolated PC-MRI can be acquired, which is caused by the variation of RA contours and globality of HS optical flow (Afrashteh et al., 2017). We further studied the influence of the main parameter $\alpha$ on the quality of interpolated PC-MRI. We can observe from Figure 4B that as the parameter $\alpha$ increases, the SSIM score improves. However, there is a specific threshold, such that over-sizing using larger $\alpha$ has little effect on reliability.

Comparison With Existing Interpolation Methods

We have compared the HS optical flow-based Intermediate PC-MRI synthesis method with other methods including linear interpolation (Töger et al., 2012) and phase-based interpolation (Meyer et al., 2015). They are derived from different understandings of images. The IE scores and SSIM scores on each selected time frame from three methods are shown in Figures 4C,D, and the overall evaluation is shown in Table 3. Our Optical flow-LAVD model achieves the best performance on selected time frame indices. Particularly, the HS optical flow can achieve the best IE and SSIM during the large-scale vortex existent periods from $N_t = 8$ to $10$. In comparison, the quality of phase-based interpolated PC-MRI is slightly worse. This interpolation method captures phase information, but the irrelevant content and noise of PC-MRI have a negative effect. The variation in IE and SSIM during selected time frame indices is typically declining. This is due to larger pixel displacement and weakly turbulent flow pattern during the end of RA diastole period (Kheradvar et al., 2019).

Visual Analysis and Segmentation Dependence

Between the Optical flow-LAVD and linear interpolation-LAVD, visual analysis finds the differences in their Lagrangian vortex ring identification results. During the large-scale vortex existence period, the Optical flow-LAVD detected vortex ring region is wide and its boundary fits a complex ellipse, especially in the case of CW vortex rings shown in Figure 5. It can be found that the Optical flow-LAVD can more realistically describe the Lagrangian vortex rings formation. Furthermore, the computation of LAVD is an integral process. Two different vortex ring identification results boil down to the accumulation of

| Method                          | DSC   | Segmentation time (s) |
|---------------------------------|-------|-----------------------|
| Automatic segmentation          | 0.89  | 18                    |
| Manual segmentation             | 1     | 52                    |

| Method                          | IE    | SSIM     |
|---------------------------------|-------|----------|
| HS optical flow interpolation   | 8.29  | 0.67     |
| Linear interpolation            | 8.56  | 0.65     |
| Phased-based interpolation      | 9.17  | 0.62     |

Bold values highlight the highest scores.
numerical integration errors, which also indicates the importance of the high-performance interpolation method.

Regarding the vortex ring identification results under the manual segmentation as the reference condition, we compute the overlap of vortex regions under automatic segmentation and compare the segmentation time. The automatic segmentation masks are seen to yield poor agreement for Lagrangian vortex ring extraction, as shown in Table 2, which demonstrates the sensitivity of Optical flow-LAVD when using different segmentation approaches. While the LAVD is objective, we note that this measure is relative to its neighborhood, and its value-range depends on the neighborhood size (Günther and Theisel, 2018). Thus, the precision of automatic segmentation to achieve our algorithm speed-up is needed.

In summary, the HS optical flow-based interpolation method achieves the best results over the PC-MRI sequence, in generating a more accurate continuous velocity field. This is remarkable and interesting. Considering the characteristics of the PC-MRI, we combine the image-interpolation algorithm to compute the Lagrangian features of cardiovascular blood flow.

Limitations
There are several works that need to be improved in the proposed purpose method. Firstly, no reference standard exists for Lagrangian vortex rings within the cardiac chambers. However, the numerical simulation model we used is in excellent agreement with the model of Haller et al. (2015). There are no comparison experiments between healthy controls and patients. Nevertheless, the focus of this study is to provide a proof of concept of Optical flow-LAVD based vortex ring identification and, as discussed previously, combining optical flow can improve the accuracy of describing vortex evolution. In our following investigations, we will consider obtaining the synthetic data based on fluid dynamics simulations (Rispoli et al., 2015; Rajat et al., 2016) and diagnosis of additional pathological patients, in order to further validate the performance of our method, based on Optical Flow-LAVD. Vortices within the ventricular chambers reflect the pathophysiological link between the diastolic filling and systolic ejection, and present a better reproducibility because of their higher intensity field (Hong et al., 2013; Kheradvar et al., 2019). For that purpose, identification of vortices within the ventricular chambers by Optical flow-LAVD is to be the focus of our future work. Secondly, the blood flow in the heart is accompanied by the formation of vortex rings which dynamically occupy the 3D space of the heart chamber (Kräuter et al., 2020). The 3D vortex ring extraction is significant for a more accurate description of vortex formation (Wong et al., 2009a). In fact, the computation of LAVD to identify the 3D vortex ring in the heart has not been investigated, and remains a topic for our future research. Thirdly, we have strictly set the convexity deficiency threshold to ensure the tubular characteristics, leading to ignoring some vortices with a relative ring shape (Yang et al., 2021). So, future work is required to establish an adaptive method instead of setting threshold artificially. We also recognize that LAVD is relative to its neighborhood, and its value-range depends on the neighborhood size (Günther and Theisel, 2018). Thus, a high demand is placed on the method of high-precision segmentation of the heart chamber. Finally, we have used the HS optical flow-based interpolation method to achieve the best results over the PC-MRI sequence. However, the IE scores and SSIM scores on each selected time frame highlight the insufficiency of the interpolation model’s capacity to deal with the challenging motion regions of the heart; the temporal sampling in medical image sequences are lower than that of natural scene videos (Guo et al., 2020; Samuel et al., 2020), and the computation of optical flow is expensive (Meyer et al., 2015; Samuel et al., 2017). Improving the optical flow-based interpolation performance, and decreasing the computation time are also key factors for our future research.

CONCLUSION
In this study, we have proposed a novel cardiac Lagrangian vortex rings identification method, based on a combination of LAVD and optical flow. We first estimate the optical flow between two consecutive PC-MRI, and the intermediate optical flow fields can be approximated by warping the procedure for constructing continuous velocity fields. We then compute LAVD by using the synthesized velocity field to accurately extract the Lagrangian vortex core and region within RA. The temporal evolution of Lagrangian vortex rings within RA is described for the first time; it is found that the optical flow-based interpolation method achieves the best results over the PC-MRI sequence. Our method provides a solution for the cardiac vortex ring formation analysis, and improves understanding of blood flow dynamics within the heart.

DATA AVAILABILITY STATEMENT
The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

ETHICS STATEMENT
The studies involving human participants were reviewed and approved by the Royal Adelaide Hospital Committee and the Institutional Review Board. The patients/participants provided their written informed consent to participate in this study.

AUTHOR CONTRIBUTIONS
KY, SW, OS, HZ, DG, DY, and KW processed the data for analysis and performed the statistical analysis. All authors contributed to the study design, data interpretation, and writing of the report.

FUNDING
This work was funded by the National Natural Science Foundation of China (Grant Number 81771927).
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Conflict of Interest: DG was employed by company University 2020 Foundation, Inc.

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