Electric Field Breakdown of Polymer Based Nano-Composite at Room 
and Cryogenic Temperatures

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Abstract. Electrical breakdown field measurements on Polymethylmethylacrylate (PMMA) and a 
nano-composite of PMMA/Barium Titanate (BTA) by 10% wt are presented. The measurements 
were made using uniform field electrode configuration under high voltage DC. The electrodes were 
made of stainless steel, each having a Bruce profile, and diameter 25 mm. The measurements were 
made at room temperature (293 K) and liquid Nitrogen temperature (77 K). Using Weibull statistics 
it shows that both PMMA and the nano-composite have breakdown electrical field strengths much 
higher at 293 K than at 77 K. It has been shown that there was very marked improvement in the 
reliability of results for both compounds at 77 K over those at 293 K. The SEM micrographs have 
shown very distinct differences in the behavior of the nano-compound between 293 K and 77 K, 
PMMA also exhibit some clear differences.

Introduction
The rapid progress on HTS power applications has boosted research on cryogenic dielectrics, as 
they require tailored insulation for each purpose. Research into nanotechnology has grown 
exponentially over the last decade. The development of nanocomposites represents a very attractive 
route to upgrade and diversify properties of “old” polymers without changing polymer compositions 
and processing [1-2]. Results obtained from researchers on nanometric dielectrics have shown 
some improvement in the breakdown characteristics, when compared with base polymers, [3-7]. 
Preliminary results have shown that the nanocomposites made from PMMA (Polymethyl 
Methacrylate) and BTA (Barium Titanate) 5% by weight have the same or slightly better 
breakdown characteristics as that of neat PMMA. PMMA was selected because it has better 
electrical properties at cryogenic temperature [8]. The nanocomposites were tested for AC and 
Impulse breakdown at room and cryogenic temperature [9]. In this paper we present our 
investigations on nanocomposites with BTA 10% by weight in base polymer PMMA. The materials 
were manufactured by Anti solvent Precipitation method (ASP) which gives good dispersion of
nanoparticles in the matrix. The characterizations were carried out for DC voltages at room and cryogenic temperatures.

EXPERIMENTAL ARRANGEMENT AND PROCEDURE

Sample Preparation

Fig. 1 shows a flow chart for fabrication of samples. Brief descriptions are given for methods used for neat PMMA and PMMA/BTA (10% wt).

![Fabrication process for PMMA and PMMA/BTA samples](image)

**Pure PMMA:** Neat PMMA (Polymethylmethacrylate) was weighed and placed on a hot die press; the temperature was raised gradually until the temperature reached 220° C. Pressure was then applied on the press (4.5 Ton). The pressure was maintained and the sample was allowed to cool for between 7 and 10 hours. The clear sheet of PMMA whose thickness was approximately 0.1mm was then removed from the press and cut using a laser cutter to the required size.

**PMMA/BTA (10% by wt.):** A novel method was used to manufacture nanocomposites, which has the promise to give good dispersion of nanoparticles in the matrix. The method is known as Anti solvent Precipitation (ASP), in which an agglomerate of the polymer and nanoparticles were precipitated from the solvent. 13.5 g of PMMA crystals were dissolved in 150 ml of Chloroform. 1.5 g of BTA was mixed with 600 ml of Chloroform on sonicator for 2 hours. The two solutions were mixed and left on a sonicator for a further 20 minutes. The resulting solution was then mixed with about 1.5 liters of methanol. The solution was continuously stirred with a mechanical stirrer to enable co-precipitation of PMMA and the nanoparticles. The solids were filtered from methanol and were allowed to dry for between 10 and 12 hours in a vacuum oven. The semi-solid was then placed on a hot press and the temperature was gradually raised until it reached 220° C, a pressure of
4.5 Tons was then applied to the sample. The press was allowed to cool for between 7 and 10 hours. The resulting sheet (thickness ~ 0.1mm) of PMMA/BTA was then removed and cut to required size using a laser cutter.

**Laboratory Procedure:**

There were two experiments performed for each sample material: DC breakdown at 293 K and 77 K. For each test, the samples were cleaned with isopropyl alcohol and the thicknesses measured with Vernier calipers.

**Experimental Setup:**

For the room temperature measurements, two 25 mm diameter Bruce Profile electrodes were cleaned with alcohol. One electrode was inserted into an acrylic cup and then attached to the steel rod at the bottom of the G10 sample holder. The other electrode was attached onto a stainless steel rod inserted at the top of the sample holder. The sample material was placed on the bottom electrode and the top electrode was lowered onto the sample. The stainless steel rod was then locked into place with a G10 bolt at the top of the sample holder. The ground connection was attached to the steel extending out of the side of the bottom of the sample holder, and the cup was filled with silicon transformer oil. The entire setup was placed on a G10 platform in a splash container, and connected to the DC generator. Fig. 2 shows a schematic of the experimental set up.

![Schematic of the experimental procedure for DC measurements.](image)

**Figure 2:** Schematic of the experimental procedure for DC measurements.

For tests performed in liquid nitrogen, the lower electrode was attached to the sample holder without the acrylic cup. The stainless steel rod was not locked in place immediately, but was instead held pressing down onto the sample with a welding clamp, and the ground connection was attached to the steel rod at the bottom of the sample holder. The entire assembly was immersed in a bath of liquid nitrogen. After the temperature equalized, the stainless steel rod was locked into place with the G10 bolt and the welding clamp was removed. Care being taken that the pressure exerted on the sample was always the same for each sample under test.
DC Breakdown Measurements

The electrode assembly with the sample was connected to a DC power supply, rated at 100 kV, 16 kW (Glassman Model SH100R160). The power supply was controlled using a computer programmed by LabView (version 8.2). The voltage was ramped at 500 volts per second until a breakdown occurred. The breakdown voltage and waveform were recorded. The samples used were approximately 0.15 mm thick, and fifteen samples were tested at each temperature.

Results:

The threshold field value, \( E_{63.2\%} \), given in table 1 is where each line of probability crosses the dashed horizontal line on the plot above. If neat PMMA is used as a base line, then the threshold value of neat PMMA at 77 K is 45.5% of that at the room temperature. Similarly, the threshold values of PMMA/BTA (10% wt.) are 84.6% and 64.9%, for the 293 K and 77 K measurements, respectively, of the room temperature neat PMMA measurements.

The slope of each line, \( \beta \) (shape factor), in the table is representative of how reliable the data is. It is represented by the steepness of the slope of the fit line on the probability chart. More reliable results are represented by steeper slopes. Using neat PMMA as the base line, neat PMMA at 77 K has improved by a factor of 3.56. Similarly the slopes for PMMA/BTA (10% wt.) at 293 K and 77 K have improved by a factor of 3.21 and 5.65 respectively.

|                | \( E_{63.2\%} \) (kV/mm) | \( \beta \) |
|----------------|-------------------------|----------|
| PMMA Neat      | 282.15                  | 128.39   |
| PMMA/BTA (10%wt.) | 238.73                  | 183.06   |

Table1: Threshold field values & shape factors values.
Fracture Surface Analysis

Fig. 4 shows the DC breakdown area of the base polymer (PMMA) at 293K and 77K. The SEM images show that the damage to the dielectric was similar at both temperatures except for the cracks formed on the surface of the sample at 77K. When the voltage was applied and the breakdown occurred, the polymer in that region was burned in each case. But at cryogenic temperature, because of the very low temperature around it, the material was rapidly quenched. Due to this rapid quenching of the material, there were cracks formed at the breakdown area. Similar cracks were also observed for the fabricated nanocomposites, after breakdown occurred at 77K. In the case at 293K, the experiment was carried out in a bath of transformer oil. After the breakdown of the material (PMMA/BTA), it took a longer time for the melted polymer to cool. During that period the nano-particles migrated out of the bulk material sticking out of the surface. Due to surface tension, brought about by the fact that the surface area of the nano-particles being larger, thus resulting in cluster formation. These clusters were not formed at 77K, due to the fact that after melting there was very rapid cooling of the material which trapped the nano-particles. As shown in Fig. 4(d), the nano-particles are on the surface of the polymer in the form of clusters, covered by the host polymer PMMA.
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References:

1. D. R. James, I. Sauers, M. O. Pace, and A. R. Ellis, IEEE Dielectrics and Electrical Insulation Society, pp. 542 (2002).
2. E. Tuncer, I. Sauers, D. R. James, A. R. Ellis, M. P. Paranthaman, T. Aytug, S. Sathyamurthy, K. L. More, J. Li, and A. Goyal, Nanotechnology, Vol. 18, p. 025703, (2007).
3. J. K. Nelson and Y. Hu, J. Phys. D: Appl. Phys., Vol. 38, pp. 213 (2005).
4. Y. Cao, P. C. Irwin, and K. Younsi, IEEE Trans. Dielect. Electr. Insul., Vol. 11,, pp. 797 (2004).
5. M. F. Frechette, M. L. Trudeau, H. D. Alamdari, and S. Boily, IEEE Trans. Dielect. Electr. Insul., Vol. 11, pp. 808 (2004).
6. J. K. Nelson and J. C. Fothergill, Nanotechnology, Vol. 15, pp. 586 (2004).
7. E. Tuncer, I. Sauers, D. R. James, A. R. Ellis, M. P. Paranthaman, A. Goyal, and K. L. More, Nanotechnology, Vol. 18, pp. 325704, (2007).
8. Kosaki, M., IEEE Electrical Insulation Magazine, 12(5): p. 17-24 (1996).
9. H. Rodrigo, W. Baumgartinger, A. Ingrole, Z (Richard) Liang, D. G. Crook and S. L. Ranner, Proceedings of Materials Research Society, Symposium BB paper number BB3.10 (2009).