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AUTHOR(S):
Onoda, Yusuke; Schieving, Feike; Anten, Niels P.R.

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RESEARCH PAPER

A novel method of measuring leaf epidermis and mesophyll stiffness shows the ubiquitous nature of the sandwich structure of leaf laminas in broad-leaved angiosperm species

Yusuke Onoda1,2,*, Feike Schieving1, and Niels P.R. Anten1,3

1 Section of Plant Ecology and Biodiversity, Institute of Environmental Sciences, Utrecht University, P.O. Box 800.84, 3508TB, Utrecht, The Netherlands
2 Department of Agriculture, Kyoto University, Kyoto 606-8502, Japan
3 Centre for Crop Systems Analysis, Wageningen University, P.O. Box 430, 6700 AK, Wageningen, The Netherlands

* To whom correspondence should be addressed. E-mail: yusuke.onoda@gmail.com

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Abstract

Plant leaves commonly exhibit a thin, flat structure that facilitates a high light interception per unit mass, but may increase risks of mechanical failure when subjected to gravity, wind and herbivory as well as other stresses. Leaf laminas are composed of thin epidermis layers and thicker intervening mesophyll layers, which resemble a composite material, i.e. sandwich structure, used in engineering constructions (e.g. airplane wings) where high bending stiffness with minimum weight is important. Yet, to what extent leaf laminas are mechanically designed and behave as a sandwich structure remains unclear. To resolve this issue, we developed and applied a novel method to estimate stiffness of epidermis- and mesophyll layers without separating the layers. Across a phylogenetically diverse range of 36 angiosperm species, the estimated Young’s moduli (a measure of stiffness) of mesophyll layers were much lower than those of the epidermis layers, indicating that leaf laminas behaved similarly to efficient sandwich structures. The stiffness of epidermis layers was higher in evergreen species than in deciduous species, and strongly associated with cuticle thickness. The ubiquitous nature of sandwich structures in leaves across studied species suggests that the sandwich structure has evolutionary advantages as it enables leaves to be simultaneously thin and flat, efficiently capturing light and maintaining mechanical stability under various stresses.

Key words: Biodiversity, biomechanics, cuticle, epidermis, evolution, leaf anatomy, mechanical design, mesophyll, sandwich structure, turgor pressure.

Introduction

The primary function of plant leaves is recognized as photosynthesis and has been studied intensively from various points of view (Lambers et al., 2008; Blankenship, 2014). However, it is much less recognised that a large fraction (i.e. 14–77%) of leaf dry mass is in structural components i.e. cell walls (Onoda et al., 2011). The large investment in structural mass is considered to physically protect the photosynthetic leaf function from a suite of stressors including gravity, wind and herbivory (Read and Stokes 2006). Elucidating how the leaf anatomical structure is built in relation to these basic physical requirements is essential to better understand the functioning of leaves.

Leaves typically have a flat, thin structure, which is associated with a large leaf surface area per unit biomass, and is thus ideal for efficient light interception (Givnish, 1986; Braybrook and Kuhlemeier, 2010), but are concomitantly prone to
mechanical failure due to their thin structure (Niklas, 1999; Read and Stokes, 2006). Therefore leaves should be designed in a way that they are not only thin but also reasonably stiff and strong. In engineering, such demands are typically met by designing objects as sandwich structures.

A typical sandwich structure is composed of stiff outer surfaces and a lightweight core, which greatly increases specific stiffness (stiffness per unit mass) in bending and has been used in many engineering constructions such as airplane wings and surfboards (Gibson et al., 1988; Gere and Timoshenko, 1999). Leaf laminas resemble a sandwich structure in that they are composed of two layers of epidermis tissue and intervening mesophyll tissues (Vincent, 1982; Gibson et al., 1988; Niklas, 1991, 1992, 1999; Moulia et al., 1994; Moulia and Fournier, 1997). This design may be an evolutionary solution to increase lamina robustness with minimum biomass investment. It has been shown that the lamina (as well as veins) plays a significant role in whole leaf mechanical stability. For instance, Moulia et al. (1994) reported in maize that the lamina itself contributed about 50% to leaf bending stiffness at the middle of leaves and more towards the leaf tips. Similar importance of lamina stiffness in leaf bending stiffness was shown by a finite element method (Kobayashi et al., 2000, 2002). In addition to the importance of leaf lamina in maintaining whole leaf plane structure, a sandwich structure has also advantages in protecting leaves from herbivory and pathogen attack by its stiff and strong surface (Grubb, 1986).

Even though the sandwich structure of leaf lamina has been alluded to in several studies and its potential advantage for plants is recognized (Vincent, 1982; Gibson et al., 1988; Niklas 1991, 1992, 1999; Moulia et al., 1994; Moulia and Fournier, 1997; Niinemets and Fleck, 2002), to our knowledge no study has actually determined to what extent leaf lamina are indeed designed as a sandwich structure. It is therefore also unknown how common this design is among different plant species. Such an assessment requires knowledge of the mechanical properties of the epidermis and mesophyll layers. However, we know of only one study that evaluated the mechanical properties of the epidermis and mesophyll layers (Gibson et al., 1988). They indirectly estimated the Young’s modulus (intrinsic material stiffness) of each layer by assuming stiffness of the epidermis and mesophyll layers to be proportional to their respective cell wall cross-sectional areas in Iris leaves. The lack of knowledge for stiffness of leaf epidermis and mesophyll layers may be due to the practical difficulty in isolating leaf epidermis layers from other tissue. Furthermore, separating tissues from a turgid leaf may release tissue stress (also called residual stress in engineering), and could have confounding effects on the estimate of Young’s modulus of tissues (Hejnowicz and Sievers, 1995a).

In this study, we first quantified the extent to which leaf laminae behave as sandwich structures. To do so, we developed a novel method to quantify the Young’s moduli of the epidermis and mesophyll layers without separating these layers, based on linear elastic theory (Gere and Timoshenko, 1999). As discussed later, biological materials are much more complicated than an ideal material that follows linear elastic theory (Baskin and Jensen, 2013), yet we believe that this approach is an important first step to evaluate the mechanical properties of the epidermis and mesophyll layers. By applying this method to a diverse set of 36 species, we determined to what extent sandwich structures are common across species (i.e. herbaceous, woody deciduous or woody evergreen) and across phylogeny. Furthermore, the variation in the Young’s moduli of the epidermis and mesophyll layers was analysed with respect to leaf morphology (e.g thickness and tissue density) and anatomy (e.g. mesophyll, epidermis, cuticle and cell walls) to better understand how leaf structures are functionally built in relation to the multiple requirements for photosynthesis, mechanical stability and defence.

### Materials and methods

#### Model

In the present study, we use a few material terms that may not be commonly used in plant science, so first we explain these terms to avoid possible confusions. Young’s modulus is an intrinsic mechanical property of the material independent of its geometry (see equation 9 for the calculation). Tensile stiffness and bending stiffness are structural properties of a material, which depend on the Young’s modulus and geometry of the material (see also equations 1 and 2, Gere and Timoshenko 1999).

Many leaves have a flat plane structure consisting of two layers of epidermis and an intervening mesophyll core, which could be approximated by a sandwich structure as described below. Some other leaves have more complicated structures such as cylinder or shell structure, which require a more complicated mechanical modelling and are not considered in this study.

For a simple sandwich structure, such as a plane leaf lamina, longitudinal tensile stiffness of the sandwich structure in the tensile test can be expressed as a sum of the longitudinal Young’s moduli of the face (\(E_f\)) and core (\(E_c\)) weighted by the cross-section area of each layer, according to the superposition principle under the linear elastic theory (Gere and Timoshenko, 1999) (Fig. 1).

\[
E_T A = E_f A_f + E_c A_c
\]  
(1)

where \(A\) is cross-section area of the composite sandwich structure, and \(A_f\) and \(A_c\) are respectively the cross-section area of the face (i.e. epidermis) and core (i.e. mesophyll) layers (\(A = A_f + A_c\)).

Similarly, bending stiffness of the sandwich structure can be expressed as a sum of \(E_f I_f\) and \(E_c I_c\) weighted by the second moment of area of each layer (Gere and Timoshenko, 1999). The second moment of area is a geometrical property of a beam and depends on cross-section area and shape (described later).

\[
E_B I = E_f I_f + E_c I_c
\]  
(2)

where \(I\) is the second moment area of the composite sandwich structure, and \(I_f\) and \(I_c\) are the second moment area of the epidermis and mesophyll layers relative to the neutral axis of the leaf (\(I = I_f + I_c\)).

\(A_f/A\) is equal to relative thickness of the mesophyll in the whole lamina thickness, \(\alpha(0 < \alpha < 1, \text{Fig. 1})\) and \(A_f/A\) is thus equal to 1-\(\alpha\). From these, equation 1 can be rewritten as follows:

\[
E_T = (1 - \alpha)E_f + \alpha E_c
\]  
(3)

For the bending test, the second moment area of a layer (full and symmetric relative to the neutral axis) is proportional to the third power of its thickness (Gere and Timoshenko, 1999). Therefore the second moment area of the mesophyll layer (\(I_c\)) is equal to \(\alpha^3 I_f\),
and by the principle of superposition, the second moment of area of the epidermis layer ($I_f$) is equal to $(1-\alpha^3)I$. Therefore equation 2 can be expressed as follows:

$$E_B/E_T = -\frac{(1-\alpha^3)E_f + \alpha^2 E_c}{1-\alpha^3}$$  \hspace{1cm} (4)

From equations 3 and 4, $E_B/E_T$ can be determined as follows:

$$E_B/E_T = \frac{1-\alpha^2(1-\beta)}{1-\alpha(1-\beta)}$$  \hspace{1cm} (5)

where $\beta$ is $E_f/E_c$.

The relationship between $E_B/E_T$, $\alpha$ and $\beta$ is shown in Fig. 2. If a material is homogeneous ($\beta=1$), $E_B/E_T$ is equal to 1. This was validated through measurements on filter paper samples (No. 595, Whatman, Maidstone, UK), a homogenous material, showing $E_B/E_T = 0.996 \pm 0.17$ (mean ± SD, $n=12$). By contrast, if the face layers are stiffer than the core ($\beta<1$) as would be expected for an efficient sandwich structure, $E_B/E_T$ is higher than 1 (Fig. 2). Note that the optimal $\alpha$ that maximises $E_B/E_T$ increases with decreasing $\beta$ (Fig. 2). In the extreme case, where the face layers are exclusively stiffer than the core ($\beta=0$), equation 5 can be expressed as follows:

$$E_B/E_T \approx 1 + \alpha + \alpha^2$$  \hspace{1cm} (6)

This equation shows that the theoretical maximum of $E_B/E_T$ for an ideal sandwich structure with an extremely thin and stiff face layers ($\alpha=1$, $\beta=0$), the $E_B/E_T$ ratio can increase up to 3.

In equations 3 and 4, $E_c$ and $E_f$ cannot be directly measured, however because there are two equations and only two unknowns, these two variables can be solved analytically (see SI for the full derivation).

$$E_f = \frac{E_B - \alpha^2 E_T}{1-\alpha}$$  \hspace{1cm} (7)

$$E_c = \frac{(1+\alpha^2)E_T - E_B}{\alpha(1+\alpha)}$$  \hspace{1cm} (8)

Equations 7 and 8 show that Young’s moduli of the epidermis layers ($E_f$) and that of the mesophyll layer ($E_c$) can be estimated from only three measurable variables: (i) Young’s modulus of the lamina measured by tensile tests ($E_T$), (ii) Young’s modulus of the lamina measured by bending tests ($E_B$) and (iii) the fraction of lamina cross-section composed of the mesophyll layer ($\alpha$), which can be determined microscopically (see Methods section ‘Anatomy analysis’).

One may argue that when the bulk core material is too compliant, there is a possibility of buckling and subsequent delamination of the faces upon bending. This effect may be negligible in leaves since the mesophyll tissues are turgid and the bundle sheath extensions, which resemble a honeycomb structure, keep a distance between the two epidermis layers.

**Plant materials**

We collected leaves from 36 broad-leaved species (33 different families) including 15 herbaceous species, 12 deciduous woody species and 9 evergreen woody species (Table 1) that were grown outdoors.
Filled circles denote the optimal approaches to the value of $3$ as calculated from $E_T/E_f$ at variable $\alpha$ ($\alpha$ is the fraction of mesophyll layer in leaf lamina) at variable $\beta$ ($\beta$ is the ratio of the mesophyll layer Young's modulus to the epidermis layer Young's modulus) that maximizes $E_T/E_f$ at a given $\beta$. Note that when the epidermis layer is extremely thin and stiff compared to the mesophyll layer ($\alpha=1$, $\beta\approx0$), $E_T/E_f$ approaches the value of 3.

In the Utrecht University Botanical Garden (latitude=52.087N, longitude=5.167W) on 13 September 2006. All sampled leaves were fully developed without any visual damage or senescence. These species were collected to cover a wide range of angiosperm species including magnolids, monocots and a wide variety of eudicots (Supplementary Fig. S1). However very small, highly dissected or twisted leaves were avoided as these leaves could not be used for the mechanical measurements. Each sampled leaf was wrapped in a wet paper towel, and five or more leaves per species were combined and used for the calculations of $E_f$ and $E_c$.

Mechanical tests

From each sampled leaf, three intercostal lamina strips in total were excised avoiding primary veins (and also secondary veins when they were very distinct) by a pair of razor blades that were fixed in parallel and 0.52 cm apart. These samples were then used for the following mechanical tests; one strip was used for the tensile test, and the other two for the bending test on both the adaxial and abaxial sides of the leaves. Each lamina strip was excised just before the measurement so that the test specimen was kept as fresh as possible. When leaves were too small to excise enough strips, adjacent leaves were also used. Here five replicates per species for each measurement. One set of replicates (tensile and bending tests of 36 species) was completed in one day. In total five consecutive days were required to complete the measurements of five replicates of 36 species. Neither apparent deterioration nor systematic change in leaf mechanical properties was observed during the measurement period.

The tensile and bending tests were conducted with a general testing machine (5542, INSTRON, Canton, MA, USA) at room temperature ($\sim$23°C) and relative humidity (50–70%). In the tensile tests, the specimens were clamped by a pair of pneumatically controlled grips, and the free length between the clamps was $\sim$5 cm. Before the measurements, width ($w$) and free length ($l_0$) of the strips were measured by a caliper and the thickness at the middle of the strips ($d$) was measured by a thickness gage (7313, Mitsutoyo, Japan). Tension was applied at a constant speed of 25 mm min$^{-1}$. Force ($F$, N) and displacement ($\delta$, mm) were measured every 100 milliseconds until the specimen was torn (Supplementary Fig. S2). The Young’s modulus in the tensile tests ($E_T$) was estimated from the initial slope of the relationship between force ($F$) and displacement ($\delta$) based on the following relationship (Gere and Timoshenko, 1999) (Fig. 1):

$$ F = E_T A \frac{\delta}{l_0} \quad (9) $$

where $A$ is the cross-section area of the specimen and $l_0$ is the original length of the specimen between the clamps. Tensile strength (the maximum force per unit cross-section area of the specimen) was also recorded.

In the bending tests, a leaf strip was placed on two supports 15 mm apart, and force was applied at the middle of the specimen at a speed of 25 mm min$^{-1}$. Force ($F$) and displacement ($\delta$) were measured as in the tensile test (Supplementary Fig. S2). The Young’s modulus in the bending test ($E_B$) was estimated from the initial slope of the relationship between force and displacement based on the following relationship (Gere and Timoshenko, 1999) (Fig. 1):

$$ F = \frac{48 E_B I}{L^3} \delta \quad (10) $$

where $L$ is the span length and $I$ is the second moment of area of the specimen. In a specimen with a rectangular cross-section, $I$ is typically calculated as $1/12aw^3$, where $w$ is width and $d$ is thickness of specimen. The span-thickness ratio was reasonably high (53±20), thus shear deformation was negligible. Adaxial $E_B$ and abaxial $E_B$ measures were strongly correlated with each other (R$^2$=0.97) with a slope close to 1 (slope=1.024, 95% confidence interval of the slope=0.95–1.10, standardised major axis slope; Warton et al., 2006). Therefore adaxial $E_B$ and abaxial $E_B$ were combined and averaged per each leaf sample, and used for the calculations of $E_f$ and $E_c$.

Anatomy analysis

Small segments ($\sim1\times2$ mm) of lamina were excised for anatomical analyses from all measured leaves ($n=5$ for each species). The segments were fixed with 2.5% glutaraldehyde in 100 mM phosphate buffer (pH=7.0) and kept at 4°C until analysis. Leaf segments were sliced at a thickness of $\sim$10 μm and stained with Nile blue, a lipophilic dye. UV fluorescence images of the section were taken with a microscope (AX-LH 100 Olympus Optical, Japan) and used to measure thicknesses of each layer (epidermis, palisade, spongy parenchyma, cuticle, and cell walls of the epidermis) with image analysis software (analySIS, Olympus, Japan). Intercellular airspace was calculated from leaf fresh mass, dry mass and thickness with an assumption that specific gravity of water and leaf solid tissue were 1 and 1.5 g cm$^{-3}$ respectively (Roderick et al., 1999).

Calculation and statistical analysis

The Young’s moduli of the epidermis layers ($E_e$) and mesophyll layer ($E_m$) were calculated with equations 7 and 8. In this study, ‘epidermis layer’ means epidermis tissues plus cuticle membranes, and ‘mesophyll layer’ means intervening tissues between the epidermis layers (mostly mesophyll cells and some minor veins). Data were log-transformed before the statistical analysis when the data were not normally distributed (Shapiro-Wilk test, P<0.05). Differences in the values among functional groups were tested with ANOVA. Multiple comparisons were done with a Bonferroni correction. Pearson’s test was used to test correlation (r) among traits. Standardized major axis slope (Warton et al., 2006) was fitted to bivariate trait relationships. A phylogenetic tree was constructed for all measured species from the APG III (2009) with a program, Phylomatic (http://phylo diversity.net/phylomatic/).
Results

The Young's moduli measured by tensile tests ($E_T$) or bending tests ($E_B$) were positively correlated to lamina tissue density, meaning that stiff leaves were made of dense tissues (Fig. 3A). The Young's moduli measured by bending tests ($E_B$) were consistently higher than $E_T$ across 36 species, meaning that not only tissue density but also tissue arrangement, i.e. sandwich structue, affect the Young's modulus when it is measured in bending (Fig. 3A). There was a strong correlation between $E_T$ and $E_B$ across species ($R^2=0.93$, $P<0.0001$, Fig. 3B). The relationship was clearly different from the 1:1 relationship ($E_B/E_T=2.59 \pm 0.48$, $n=36$) and close to the theoretical maximum ($E_B/E_T=3$), meaning that leaf lamina of these plant species behaved as nearly ideal sandwich structures. Among growth forms, leaves of evergreen species were significantly stiffer (both $E_T$ and $E_B$) than those of deciduous species. The $E_B/E_T$ ratio was 2.77 in deciduous herbaceous species, 2.89 in evergreen herbaceous species, 2.28 in deciduous woody species and 2.67 in evergreen woody species.

Lamina thickness varied from 0.159 mm in *Fagus sylvatica* to 0.973 mm in *Talinum paniculatum*. Among functional
Evergreen woody species had slightly but significantly higher Young’s modulus to the epidermis layer Young’s modulus, indicating that many leaf laminas had a nearly ideal sandwich structure. Mean and SD (for B) were calculated by applying the measured values of $E_B$, $E_T$, and the mesophyll fraction ($\alpha$) to equations 7 and 8. $E_T$ was much higher than $E_c$, ranging from 11 MPa in Arabidopsis thaliana to 463 MPa in Eucalyptus pauciflora (Table 1; Fig. 6). On the other hand, $E_c$ was much lower (0.61 ± 0.61 MPa, n=36). The relatively large SD for the mean (i.e. high coefficient of variation) in $E_c$ was partly due to the structure of the data. For example, $E_c$ was calculated from $E_B$ and $E_T$ (equation 8) and therefore variation in $E_c$ was comparable in magnitude to the variation of $E_B$ and $E_T$, whereas the mean value of $E_c$ was much smaller than those of $E_B$ and $E_T$. While the accurate estimate of $E_c$ might not be possible in this method (see Discussion), qualitatively it is evident that the longitudinal stiffness of leaf laminae was largely determined by the stiffness of the epidermis layers. Among functional groups, $E_T$ was higher in evergreen woody species than in deciduous woody and herbaceous species (Fig. 6B, P<0.01).

The variation in the epidermis Young’s modulus ($E_t$) was significantly correlated with the fraction of outer cell walls and cuticles within the epidermis layers ($R^2=0.56$, $P<0.001$, n=36) (Fig. 7A). Each component, i.e. cuticle fraction or outer cell wall fraction in the epidermis layers, significantly correlated to the epidermis Young’s modulus ($P<0.001$), but the cuticle fraction rather than the cell wall fraction correlated more strongly with the epidermis Young’s modulus ($R^2=0.43–0.50$ versus 0.13–0.23, Table 2). The thickness of the epidermis layer itself was not significantly correlated to the epidermis Young’s modulus ($P>0.05$), while leaf mass per area (LMA) was significantly correlated to the epidermis Young’s modulus (Fig. 7C, Table 2, $R^2=0.52$). The Young’s moduli of mesophyll layers were not significantly correlated with any leaf morphological or anatomical traits unless phylogeny was considered (Table 2). When phylogeny was considered, the Young’s moduli of mesophyll layers were slightly
negatively correlated to water content and positively correlated to the mesophyll fraction.

Phylogenetic autocorrelations were weak and were not significant in most of the measured traits (Supplementary Table S2). Furthermore, a consideration of phylogenetic divergences did not strongly alter levels of correlations among traits (Table 2). The interpretation of these results is that the trait associations observed in this study were a result of repeated evolution across different clades of plants rather than a phylogenetic bias in the selection of studied species.

**Discussion**

In this study, we developed and applied a novel method to estimate the Young’s moduli of epidermis and mesophyll layers. Our model based on linear elastic theory has a number of simplifying assumptions, and there were some phenomena that cannot be fully explained by this model (as discussed later). Yet, our approach showed that leaf laminas were designed as efficient sandwich structures in which the epidermis tissues were much stiffer and thinner than the mesophyll tissues. In addition, we showed that this sandwich structure was found in a wide range of studied angiosperm species, suggesting that a sandwich structure has general advantages for many land plants. In this discussion, we discuss anatomical and ecological considerations of leaf sandwich structures and also discuss future challenges including technical issues.

**Anatomical considerations**

Across species, the epidermis Young’s modulus was strongly correlated with the fraction of cuticles and outer cell walls in

![Fig. 4. Leaf anatomy characteristics of 36 angiosperm species. (A) Thickness fraction of each layer. (B) Thickness of epidermis cell walls, cuticles and the rest of epidermis layer (upper and lower layers pooled together). Functional groups are abbreviated as H/D deciduous herbaceous species; H/E evergreen herbaceous species; W/D deciduous woody species; W/E evergreen woody species. Mean of five replications is shown for each species. (This figure is available in colour at JXB online.)](image)
the epidermis layer (Fig. 7), suggesting that the cuticles and epidermis outer cell walls played major roles in determining the surface stiffness. In particular, evergreen leaves had stiffer epidermis regions (Fig. 6) and thicker cuticles than deciduous leaves (Fig. 4), suggesting cuticles are mechanically important for long-lived leaves. This implication is also supported by studies on isolated leaf cuticle membranes (Wiedemann and Neinhuis, 1998; Bargel et al., 2006; Onoda et al., 2012), which found that leaf cuticles were made of very stiff material (50–1,500 MPa). Furthermore, $E_t$ increased more than proportionally with the fraction of cuticles and outer cell walls in the epidermis layer, indicating that thicker cuticles were made of stiffer materials (Onoda et al., 2012).

The mesophyll tissues were much softer than the epidermis tissues, which should be due to the thin mesophyll cell walls, small longitudinal continuity and the presence of intercellular airspaces. Mesophyll cells generally have much thinner cell walls (0.05–0.4 μm, Terashima et al., 2011) than epidermis cells (1.4–9.2 μm, Fig. 4B). Mesophyll layers also contain larger intercellular airspaces; our calculation showed that 7–41% of the leaf volume was occupied by air (Supplementary Table S1). The thin cell walls of mesophyll and the presence of intercellular airspaces are primarily important to facilitate a high rate of CO$_2$ diffusion for photosynthesis (Parkhurst, 1977; Terashima et al., 2001), but our study suggests that air spaces can also contribute to higher bending stiffness (i.e., the product $E_B I$) by increasing the second moment of area ($I$) in the sandwich structure.

There were minor veins in our test specimens, but their contribution to bending stiffness were likely small, as indicated by low $E_c$. This was in part due to their location close to the neutral axis, i.e., under bending, minor veins located close to the neutral axis deform much less than outer tissues (i.e. epidermis). Thus minor veins geometrically cannot contribute much to $E_B$. Such negligible contribution of minor veins to maintain a leaf horizontal position was also reported by a finite element analysis (Kobayashi et al., 2000, 2002).

Studies on hypocotyls of *Helianthus annuus* (Asteraceae) also showed that 86% of tensile stiffness came from the epidermis (Hejnowicz and Sievers, 1995b). Similarly, in turged tulip stems the epidermis was found to contribute up to 50% of stem bending stiffness (Niklas and Paolillo, 1997). Minor leaf veins are however important for water and photosynthate transport (Brodribb et al., 2007; Sack et al., 2013) and shear resistance (Lucas et al., 1991).

**Ecological significance**

Some leaves, especially herbaceous ones, are turgid i.e. hydrostatically inflated. They rely on turgor pressure to increase bending stiffness without much investment of resources in cell walls. It was intriguing that herbaceous species had significantly higher $E_B / E_T$ values than woody species (2.80 ± 0.48 versus 2.45 ± 0.44, t-test, $P<0.05$) as well as higher water content (0.79 ± 0.10 versus 0.64 ± 0.07, t-test, $P<0.05$), suggesting that turgor pressure can increase efficiency of the sandwich structure. In turgid leaves, epidermis and mesophyll layers are maintained in states of tension and compression respectively because the hydrostatically inflated ‘core’ mesophyll is accommodated by the much stiffer ‘face’ epidermis layers (Hejnowicz and Sievers, 1995a; Kutschera and Niklas 2007). This ‘pre-stressed sandwich structure’ may increase efficiency of sandwich structure in at least two ways. First, the hydrostatic pressure increases lamina thickness and thus widens the distance between two epidermis layers. This increases the second moment of area of the epidermis layers in relation to the neutral axis and contributes to more efficient sandwich structure. Second, the epidermis tissue may be ‘strain-stiffening material’ (Hejnowicz and Sievers, 1996). While this phenomenon cannot be explained by the linear elastic theory, if the epidermis layers become stiffer under hydrostatic pressure, they can increase efficiency of a sandwich structure by decreasing $\beta$ ($E_B / E_t$). Such mechanical efficiency should enable herbaceous plants to maintain a larger leaf area for a given...
biomass, which could contribute to them having relatively fast growth rates compared to woody species (Poorter et al., 2009), although other factors play a role as well. On the other hand, due to their reliance on water, hydrostatically inflated leaves tend to wilt sooner than leaves of woody species when water is limited. Leaf wilting is also an important function for plants as they can avoid strong sunlight and reduce water loss from leaves. Thus, the hydrostatically controlled-sandwich structure may be a quite efficient mechanism enabling plants to both acquire and avoid light energy depending on water availability.

In terms of leaf mechanical stability, a sandwich structure may be particularly beneficial for plants growing under light limited conditions because they are often carbon-limited and produce thinner leaves (as compared to the same species growing under stronger light) to achieve high efficiency of light interception per unit biomass (Terashima et al., 2001; Poorter et al., 2009). These shaded leaves tend to have a larger fraction of intercellular airspace (e.g. Lee et al., 2000). Indeed in Plantago major, the fraction of intercellular airspace was found to increase by 28% with a shading treatment (Onoda et al., 2008). The relatively large airspace in shade leaves was more likely associated with demands on mechanical stability than with the necessity for rapid intracellular CO₂ diffusion for photosynthesis, since photosynthesis under shade is hardly limited by the intercellular CO₂ diffusion resistance (Terashima et al., 2001). Bending stiffness scales to the third power of lamina thickness and, for example, a 10% larger lamina thickness due to an increase intercellular space can increase lamina bending stiffness by 33% without adding biomass. Therefore a larger intercellular space is likely important to maintain larger light interception area for a given mass which is advantageous in shaded environments.
Overall we observed a large interspecific variation in leaf lamina stiffness indices i.e. 36-fold in $E_B$ and 790-fold in bending stiffness ($= E_B \times I$) (Table 1), while the interspecific variation in fresh leaf mass per unit leaf area was much smaller (7-fold) (Supplementary Table S1). The much larger variation in bending stiffness than in fresh leaf mass may suggest that some leaves (especially evergreen leaves) may be too stiff (over-engineered) relative to the need to resist gravity or moderate wind, although an integrative approach including leaf weight, material properties and leaf dimensions is needed to

![Fig. 7](image-url)

**Fig. 7.** The Young’s moduli of the epidermis layers were plotted against (A) the fraction of cuticle and outer cell walls within the epidermis layers, (B) thickness of the epidermis layers (both upper and lower layers pooled together) and (C) leaf mass per area (LMA) across 36 angiosperm species. Mean and SD are shown for each species ($n=5$). Curvilinear regressions are used as they fit better than linear regressions. Regression lines; (A) $y=6451x^{2.41}$, $R^2=0.56$, $P<0.001$; (C) $y=0.1004x^{1.65}$, $R^2=0.52$, $P<0.001$ Note that ’epidermis layer’ in this study includes epidermis tissues and cuticles. (This figure is available in colour at JXB online.)

**Table 2.** Cross-species correlations (Pearson’s test) and phylogenetic independent contrast (PIC) correlations among leaf traits across 36 species. Abbreviations: $E_f$ and $E_c$ are Young’s modulus of epidermis and mesophyll layers respectively. $E_B$ and $E_T$ are Young’s modulus measured by the tensile test and bending test respectively. Log$_{10}$-transformation was applied when data were not normally distributed (Trans = 1). Bold letters indicate the level of significance ($P<0.05$).

| Traits                               | Trans | $E_f$ |       |       | $E_c$ |       |
|--------------------------------------|-------|-------|-------|-------|-------|-------|
|                                      |       | Cross-species | PIC   | Cross-species | PIC   |
| Lamina thickness                     | 1     | 0.206 | 0.059 | 0.118 | -0.049|
| Fresh LMA                            | 1     | 0.265 | 0.139 | 0.126 | -0.049|
| Dry LMA                              | 1     | 0.722 | 0.595 | 0.263 | 0.13  |
| Water content                        | 0     | -0.735| -0.717| -0.31 | -0.353|
| Dry mass density                     | 0     | 0.757 | 0.767 | 0.316 | 0.34  |
| Air fraction                         | 0     | 0.008 | -0.065| 0.074 | 0.183 |
| $E_T$                                | 1     | 0.908 | 0.894 | 0.239 | 0.436 |
| $E_B$                                | 1     | 0.958 | 0.964 | 0.087 | 0.252 |
| $E_B/E_T$                            | 0     | 0.246 | 0.181 | -0.673| -0.723|
| Tensile strength                     | 0     | 0.86  | 0.858 | 0.054 | 0.279 |
| Bending stiffness per unit width     | 1     | 0.731 | 0.607 | 0.151 | 0.111 |
| Upper cuticle thickness              | 1     | 0.653 | 0.447 | 0.204 | 0.031 |
| Upper epidermis thickness            | 0     | -0.397| -0.522| -0.251| -0.357|
| Palisade thickness                   | 1     | 0.274 | 0.244 | 0.281 | 0.161 |
| Spongy thickness                     | 1     | 0.224 | 0.196 | -0.124| -0.213|
| Lower epidermis thickness            | 0     | -0.096| -0.295| -0.245| -0.387|
| Lower cuticle thickness              | 1     | 0.708 | 0.53  | 0.22  | 0.121 |
| Upper epidermis cell wall thickness  | 1     | 0.354 | -0.09 | -0.087| -0.184|
| Lower epidermis cell wall thickness  | 1     | 0.477 | -0.079| -0.179| -0.276|
| Total epidermis thickness            | 0     | -0.018| -0.272| -0.117| -0.351|
| Mesophyll fraction ($\phi$)          | 0     | 0.398 | 0.626 | 0.245 | 0.386 |
| (Cuticle + cell wall)/epidermis      | 0     | 0.762 | 0.632 | 0.155 | 0.174 |
| Leaf area                            | 1     | -0.18 | -0.268| -0.065| -0.077|
| $E_I$                                | 1     | ---   | ---   | 0.069 | 0.196 |
| $E_B$                                | 0     | 0.069 | 0.196 | ---   | ---   |
understand whole leaf elastic stability (e.g. Fournier et al., 2013; Tadrist et al., 2014). These leaves were nevertheless designed as sandwich structures as indicated by their high \( E_y/E_T \) ratios, suggesting that a sandwich structure has benefits beyond being efficient in resisting gravitational and wind forces. Relatively thick cuticles may act as stiff and tough barriers against attacks from herbivores and microorganisms e.g. pathogens and bacteria (Grubb, 1986), and leaf toughness is a key element for longer leaf lifespan (Coley, 1983; Kitajima and Poorter, 2010; Onoda et al., 2011). Actually, in the present study, the Young’s moduli of the epidermis layers were strongly correlated with LMA (leaf mass per area), which is a good indicator of leaf lifespan (Wright et al., 2004). These observations suggest that sandwich structures may be beneficial not only for maintaining leaf plane structure against gravity or moderate wind, but also for long lifespan by protecting leaf functions from various external stresses.

While bending stiffness is important for leaves, leaves should be also deformable to reduce drag during strong winds (Vogel, 1989). This requirement may sound contradictory with the requirement for stiffness, but it may be possible because leaf surfaces (i.e. cuticles) are highly extensible materials in spite of their stiffness (Onoda et al., 2012). The requirement for deformation is likely to increase with leaf size because drag force is proportional to surface area (Vogel, 1989). In other words, small leaves do not necessarily deform much under wind. This may accord with the general pattern that very stiff leaves (e.g. sclerophyll leaves) tend to be small (Grubb, 1986).

**Technical issues and future challenges**

In this study, we show that the \( E_y/E_T \) ratio is a useful indicator of the extent to which leaves are designed as sandwich structures. Our method seems to be applicable to plant leaves since the \( E_y/E_T \) ratio of filter papers, which were more or less homogeneous material, was close to 1 (0.996±0.17) while most leaves had the ratios much higher than 1 (2.59±0.48, n=36). However, there were some species that exceeded the theoretical threshold of \( E_y/E_T (=3) \), albeit by a relatively small margin. Similarly, some mesophyll tissues had slightly negative Young’s moduli while the Young’s modulus should be a positive value. These may be artifacts possibly resulting from assumptions made in this study. We have at least three possible explanations for these phenomena. (i) The effective thickness of the stiff epidermis layer may be smaller than the total thickness of the epidermis layer. This is because the cuticle and outer cell walls largely determine the epidermis Young’s modulus (Fig. 7), whereas the inner part of the epidermis may behave more like the mesophyll tissues (Fig. 5B). (ii) If so, our mesophyll Young’s modulus values were underestimated and this could have resulted in negative values. Actually, recalculating the Young’s modulus of the mesophyll layer in this way, two-thirds of species that initially had negative moduli switched to positive values. However, this issue cannot explain why some leaves had \( E_y/E_T \) values larger than 3 (Fig. 5). (ii) There was a possible technical issue with the measurement. If leaf laminas were not completely flat in a direction perpendicular to the longitudinal direction (although we tried to exclude non-flat leaves), the effective second moment of area could be higher than the calculated second moment of area that assumed a rectangular cross-section. If so, this would result in an over-estimation of \( E_y \) while \( E_T \) would be unaffected. Similarly, if lamina thickness was not homogeneous within a leaf specimen, a slight underestimation of lamina thickness might result in an over-estimation of \( E \) and this effect would have been larger in the bending test than in the tensile test. These technical issues can result \( E_y/E_T \) values ≥3 and, consequently, result in apparent negative mesophyll Young’s moduli. (iii) As mentioned earlier, biological materials are quite complicated and do not always behave according to the linear elastic theory. It is known that soft tissues like mesophyll behave like ‘Fung materials’, which have a larger resistance to compressive strain than to tensile strain (Fung, 1993; Vandiver and Goriely, 2008). Furthermore, the epidermis tissue may be ‘strain-stiffening material’ (Hejnowicz and Sievers, 1996). There are also other effects including viscoelasticity, interactions between stress and moisture content, geometric non-linearity produced, e.g. by the Poisson’s effect (Mouila, 2013). These effects together may lead to \( E_y/E_T \) values ≥3 and, consequently, result in apparent negative mesophyll Young’s moduli. While our aim was to understand the basic principle underlying the leaf mechanical design across species, these complicating factors cannot be ignored and could be important for mechanical stability of leaves.

In this study, we focused on leaf laminas and did not consider mechanical properties of major veins or petioles. The mechanical contribution of major veins to whole leaf bending stiffness is important, especially near the leaf base, while lamina stiffness has a major role in leaf bending stiffness toward the leaf tips (Mouila et al., 1994; Kobayashi et al., 2000, 2002). Integrating the geometry and mechanical properties of laminas, veins and petioles will be an important challenge to understand mechanical stability of whole leaves (Tadrist et al., 2014).

**Conclusions**

Our novel approach indicates that many leaf laminas are designed as ideal sandwich structures, with the exclusively thin and stiff epidermis layers enveloping a thicker and softer mesophyll core. We showed that this design principle is commonly found in broad-leaves across a wide range of angiosperm taxa. This structure enables land plants to produce thin flat leaves with a high light interception per unit invested mass and yet resistant to buckling under gravitational forces and moderate wind. The stiff surface should also be important as a barrier against external biotic and abiotic stresses such as herbivory, pathogen attacks and rainfall. Anatomical features such as stiff cuticles, thin mesophyll cell walls, large intercellular airspace and hydrostatic pressure within leaves seem to be elegantly coordinated to optimize multi-functions of leaves, such as photosynthesis, mechanical stability and defence. These results provide new insights into the functional significance of leaf structure and have implications for plant sciences and biomimetic studies.
Supplementary material

Supplementary material is available at JXB online.

Supplementary Text S1. A full derivation of equations 7 and 8.

Supplementary Table S1. A phylogenetic tree of 36 species.

Supplementary Table S2. Additional leaf traits of 36 species.

Supplementary Fig. S1. A phylogenetic tree of 36 species.

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References

Angiosperm Phylogeny Group III. 2009. An update of the Angiosperm Phylogeny Group classification for the orders and families of flowering plants: APG III. Botanical Journal of the Linnean Society 161, 105–121.

Bargel H, Koch K, Cerman Z, Neinhuis C. 2006. Evans Review No. 3: Structure, function relationships of the plant cuticle and cuticular waxes. A smart material? Functional Plant Biology 33, 893–910.

Baskin TJ, Jensen OE. 2013. On the role of stress anisotropy in the growth of stems. Journal of Experimental Botany 64, 4697–4707.

Blankenship RE. 2014. Molecular mechanisms of photosynthesis. John Wiley & Sons.

Braybrook SA, Kuhlemeier C. 2010. How a plant builds leaves, The Plant Cell 22, 1006–1018.

Brodbibb TJ, Feild TS, Jordan GJ. 2007. Leaf maximum photosynthetic rate and venation are linked by plant characteristics. Plant Physiology 144, 1890–1898.

Coley PD. 1983. Herbivory and defensive characteristics of tree species in a lowland tropical forest. Ecological Monographs 53, 209–234.

Felsenstein J. 1985. Phylogenies and the comparative method. The American Naturalist 125, 1–15.

Fournier M, Dlouhá J, Jaouen G, Almeras T. 2013. Integrative biomechanics for tree ecology: beyond wood density and strength. Journal of Experimental Botany 64, 4799–4815.

Fung YC. 1993. Biomechanics: Mechanical properties of living tissues. New York: Springer-Verlag.

Gere JM, Timoshenko SP. 1999. Mechanics of materials 4th edn edition. Cheltenham: Taylor Thornes (Publisher) Ltd.

Gibson LJ, Ashby MF, Easterling KE. 1988. Structure and mechanics of the iris leaf. Journal of Materials Science 23, 3041–3048.

Günish TJ. 1986. Biomechanical constraints on crown geometry in forest herbs. In: Günish TJ, ed. On the economy of plant form and function. Cambridge: Cambridge University Press, pp 525–583.

Grubb PJ. 1986. Sclerophylls, pawpawhylls and pycnohylls: the nature and significance of hard leaf surfaces. In: Juniper B, Southwood R, eds. Insects and the plant surface. London, UK: Edward Arnold, 137–150.

Hejnowicz Z, Sievers A. 1995a. Tissue stresses in organs of herbaceous plants I. Poisson ratios of tissues and their role in determination of the stresses. Journal of Experimental Botany 46, 1035–1043.

Hejnowicz Z, Sievers A. 1995b. Tissue stresses in organs of herbaceous plants II. Determination in three dimensions in the hypocotyl of sunflower. Journal of Experimental Botany 46, 1045–1053.

Hejnowicz Z, Sievers A. 1996. Tissue stresses in organs of herbaceous plants III. Elastic properties of the tissues of sunflower hypocotyl and origin of tissue stresses. Journal of Experimental Botany 47, 519–528.

Kitajima K, Poorer L. 2010. Tissue-level leaf toughness, but not lamina thickness, predicts sapling leaf lifespan and shade tolerance of tropical tree species. New Phytologist 186, 708–721.

Kobayashi H, Daimaru M, Kubota M. 2002. Mechanical contribution of veins in a London plane leaf. ESDA 2002 (6th Biennial Conf. on Eng. Systems Design and Analysis). Istanbul Technical University, Istanbul, Turkey, B10-004.

Kobayashi H, Daimaru M, Kuribayashi K. 2000. Venation pattern of butterbur leaf and its mechanical contribution. Journal-Society of Materials Science Japan 49, 1318–1323.

Kutschera U, Niklas KJ. 2007. The epidermal-growth-control theory of stem elongation: an old and a new perspective. Journal of Plant Physiology 164, 1395–1409.

Lammers H, Chapin FS III, Pons TL. 1998. Plant physiological ecology. New York: Springer-Verlag.

Lee DW, Oberbauer SF, Johnson P, Krishnapalay B, Mansor M, Mohamad H, Yap SK. 2000. Effects of irradiance and spectral quality on leaf structure and function in seedlings of two Southeast Asian Hopea (dipterocarpaceae) species. American Journal of Botany 87, 447–455.

Lucas PW, Choong MF, Tan HTW, Turner IM, Berrick AJ. 1991. The fracture toughness of the leaf of the dicotyledon Calophyllum inophyllum L. (Guttiferae). Philosophical Transactions: Biological Sciences 334, 95–106.

Moran PA. 1950. Notes on continuous stochastic phenomena. Biometrika 37, 17–23.

Mouli B. 2013. Plant biomechanics and mechanobiology are convergent paths to flourishing interdisciplinary research. Journal of Experimental Botany 64, 4617–4633.

Mouli B, Fournier M. 1997. Mechanics of the maize leaf: a composite beam model of the midrib. Journal of Materials Science 32, 2771–2780.

Mouli B, Fournier M, Guiltard D. 1994. Mechanics and form of the maize leaf: in vivo qualification of flexural behaviour. Journal of Materials Science 29, 2359–2366.

Niinemets Ü, Fleck S. 2002. Leaf biomechanics and biomass investment in support in relation to long-term irradiance in Fagus. Plant Biology 4, 523–534.

Niklas KJ. 1991. Bending stiffness of cylindrical plant organisms with a core-rind construction: evidence from Juncus effusus leaves. American Journal of Botany 78, 561–568.

Niklas KJ. 1992. Plant biomechanics: an engineering approach to plant form and function. Chicago: University of Chicago Press.

Niklas KJ. 1999. A mechanical perspective on foliage leaf form and function. New Phytologist 143, 19–31.

Niklas KJ, Paolillo DJ. 1997. The role of the epidermis as stiffening agent in Tulipa (Liliaceae) stems. American Journal of Botany 84, 735–744.

Onoda Y, Richards L, Westoby M. 2012. The importance of leaf cuticle for carbon economy and mechanical strength. New Phytologist 196, 441–447.

Onoda Y, Schieving F, Anten NPR. 2008. Effects of light and nutrient availability on leaf mechanical properties of Plantago major: a conceptual approach. Annals of Botany 101, 727–736.

Onoda Y, Westoby M, Adler PB, et al. 2011. Global patterns of leaf mechanical properties. Ecology Letters 14, 301–312.

Paradis E. 2012. Analysis of macroevolution with phylogenies. Analysis of phylogenetics and evolution with R. Springer, 203–312.

Parkhurst DF. 1977. A three-dimensional model for CO2 uptake by leaves. Journal of Theoretical Biology 67, 471–488.

Poorter H, Niinemets U, Villar R. 2009. Causes and consequences of variation in leaf mass per area (LMA): a meta-analysis. New Phytologist 182, 565–588.

Read J, Stokes A. 2006. Plant biomechanics in an ecological context. American Journal of Botany 93, 1546–1565.

Roderick ML, Berry SL, Noble IR, Farquhar GD. 1999. A theoretical approach to linking the composition and morphology with the function of leaves. Functional Ecology 13, 683–695.

Sack L, Scoffoni C, John GP, et al. 2013. How do leaf veins influence the worldwide leaf economic spectrum? Review and synthesis. Journal of Experimental Botany 64, 4053–4080.
Tadrist L, Saudreau M, de Langre E. 2014. Wind and gravity mechanical effects on leaf inclination angles. *Journal of Theoretical Biology* **341**, 9–16.

Terashima I, Hanba YT, Tholen D, Niinemets U. 2011. Leaf functional anatomy in relation to photosynthesis. *Plant Physiology* **155**, 108–116.

Terashima I, Miyazawa SI, Hanba YT. 2001. Why are sun leaves thicker than shade leaves? Consideration based on analyses of CO₂ diffusion in the leaf. *Journal of Plant Research* **114**, 93–105.

Vandiver R, Goriely A. 2008. Tissue tension and axial growth of cylindrical structures in plants and elastic tissues. *Europhysics Letters* **84**, 58004.

Vincent JFV. 1982. The mechanical design of grass. *Journal of Materials Science* **17**, 856–860.

Vogel S. 1989. Drag and reconfiguration of broad leaves in high winds. *Journal of Experimental Botany* **40**, 941–948.

Warton DI, Wright IJ, Falster DS, Westoby M. 2006. Bivariate line-fitting methods for allometry. *Biological Reviews* **81**, 259–291.

Wiedemann P, Neinhuis C. 1998. Biomechanics of isolated plant cuticles. *Botanica Acta* **111**, 28–34.

Wright IJ, Reich PB, Westoby M, et al. 2004. The worldwide leaf economics spectrum. *Nature* **428**, 821–827.