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Vibrating Flexoelectric Micro-Beams as Angular Rate Sensors

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Abstract: We studied flexoelectrically excited/detected bending vibrations in perpendicular directions of a micro-beam spinning about its axis. A set of one-dimensional equations was derived and used in a theoretical analysis. It is shown that the Coriolis effect associated with the spin produces an electrical output proportional to the angular rate of the spin when it is small. Thus, the beam can be used as a gyroscope for angular rate sensing. Compared to conventional piezoelectric beam gyroscopes, the flexoelectric beam proposed and analyzed has a simpler structure.

Keywords: gyroscope; flexoelectric; beam; vibration

1. Introduction

Gyroscopes are key components for motion sensing. Early gyroscopes were based on the inertia of a rotating rigid body. Later, vibratory and optical gyroscopes were subsequently developed. This paper is concerned with vibratory gyroscopes in which vibrations are usually excited and detected piezoelectrically or electrostatically. The literature on vibratory gyroscopes is numerous. Early references can be found in a few review articles [1–3] and Ph.D. dissertations [4,5]. Relatively recent ones are, e.g., [6–10], among which, [10] is a review on micromachined and nano gyroscopes.

Specifically, for piezoelectric vibratory gyroscopes based on flexural vibrations of thin beams [11], since piezoelectric coupling produces strains rather than curvatures, either a composite beam or some complicated electrode configuration is typically needed to excite and detect flexural motions of beams [11–13].

Recently, there has been a growing interest in the flexoelectric effect [14–17], with which, flexural motion in a homogeneous beam [18–20] or plate [21] can be excited or detected with only electrodes. In particular, flexoelectric beams have already been used as actuators or sensors in electromechanical devices [22,23]. This offers the possibility of flexoelectric angular rate sensors. In this paper, we propose a flexoelectric beam vibratory gyroscope that is original. The flexoelectric beam in the proposed gyroscope functions as both an actuator and a sensor at the same time through two pairs of electrodes and flexural vibrations in perpendicular directions. We demonstrate how the proposed gyroscope works through modeling. The basic three-dimensional theory of flexoelectricity is gathered in Section 2, from which, a one-dimensional model for flexural motions of the gyroscope is established in Section 3. A theoretical analysis and numerical results are presented in Sections 4 and 5, respectively, to show the basic response of the beam when it is rotating about its axis. Finally, some conclusions are drawn in Section 6.
2. Theory of Flexoelectricity

The macroscopic theory of flexoelectricity [15–17] is summarized below for its notation. It is also the foundation for the one-dimensional (1-D) model to be developed in the next section. In Cartesian tensor notation [24], the field equations are

\[
T_{ij,j} - \tau_{ijk,jk} + F_i = \rho \ddot{u}_i, \quad (1a)
\]

\[
D_{ij} = 0, \quad (1b)
\]

where \( T \) is the stress tensor, \( \tau \) a higher-order stress, \( F \) the body force vector, \( \rho \) the mass density, which is a scalar, \( u \) the mechanical displacement vector, and \( D \) the electric displacement vector. A vector or tensor is written either in boldface or in component form with one index (vector) or more indices (tensor) [24]. A comma followed by an index denotes partial differentiation with respect to the coordinate associated with the index [24]. We limit ourselves to nonpiezoelectric materials. The constitutive relations accompanying Equation (1) describing material behaviors are

\[
T_{ij} = C_{ijkl} S_{kl}, \quad \tau_{ijk} = -f_{ijkl} E_i, \quad D_i = \varepsilon_{ij} E_j + f_{ijkl} \eta_{jkli}, \quad (2)
\]

where \( S \) is the strain tensor, \( E \) the electric field vector, \( \eta \) the strain gradient tensor, \( C_{ijkl} \) the elastic stiffness tensor, \( f_{ijkl} \) the flexoelectric constants (tensor), and \( \varepsilon_{ij} \) the dielectric constants (tensor). \( S, \eta, \) and \( E \) are related to \( u \) and the scalar electric potential \( \phi \) through

\[
S_{ij} = (u_{ij} + u_{ji})/2, \quad \eta_{ijkl} = S_{jkli}, \quad E_i = -\phi_{,i}. \quad (3)
\]

3. One-Dimensional Equations for a Flexoelectric Beam in Bending Vibrations

Consider the thin flexoelectric beam in Figure 1. Its lateral surfaces are traction free and are electroded. The voltage across the two electrodes at \( x_2 = \pm a \) for actuation is \( V_2(t) \), and that between the two electrodes at \( x_3 = \pm b \) for sensing is \( V_3(t) \).

![Figure 1. A thin flexoelectric beam and coordinate system whose origin is at the center of the left face.](image)

1-D equations for bending in the \((x_1,x_3)\) plane were derived from Equations (1)–(3) in [20]. For the gyroscope application to be studied in the next section, we need to generalize the 1-D equations in [20] to the case of simultaneous bending in both of the \((x_1,x_2)\) and \((x_1,x_3)\) planes. In this case, the displacement components are approximated by

\[
u_2 \cong u_2(x_1, t), \quad u_3 \cong u_3(x_1, t), \quad u_1 \cong -x_2 u_{2,1} - x_3 u_{3,1}, \quad (4)
\]
which produce the following axial strain and strain gradients:

\[ S_{11} = -x_2 u_{2,11} - x_3 u_{3,11}, \]
\[ \eta_{112} = -u_{2,11}, \quad \eta_{113} = -u_{3,11}. \]  

(5)

Since the lateral surfaces of the beam are electroded and the electric potential are functions of time only on ideal electrodes that we assume, the electric field is approximated by

\[ E_2 = -\frac{V_2}{2a}, \quad E_3 = -\frac{V_3}{2b}, \quad E_1 = 0. \]  

(6)

The equations for bending are obtained by integrating Equation (1a) with \( i = 2 \) and \( 3 \) over the beam cross section, which results in [20]

\[ Q_{2,1} + f_2 A = \rho A u_{2,11}, \]
\[ Q_{3,1} + f_3 A = \rho A u_{3,11}. \]  

(7)

where \( Q_2 \) and \( Q_3 \) are the transverse shear forces in the \( x_2 \) and \( x_3 \) directions, respectively, and \( A = 4ab \) is the area of the beam cross section. The integration of the products of Equation (1a) with \( x_2 \) or \( x_3 \) over the beam cross section yields the following shear force-bending moment relation [20]:

\[ M_2 = Q_{2,1}, \quad M_3 = Q_{3,1}. \]  

(8)

where \( M_3 \) and \( M_2 \) are moments associated with bending in the \((x_1,x_2)\) and \((x_1,x_3)\) planes, respectively. For thin beams, the rotatory inertia is neglected. The 1-D constitutive relations are obtained by integrating the relevant equations in Equation (2) and their products with \( x_2 \) or \( x_3 \) over a cross section. The results are

\[ M_3 = -\tau B_2 u_{2,1111} - f_{3113} A E_2, \]  

(9a)

\[ M_2 = -\tau B_3 u_{3,1111} - f_{3113} A E_3, \]  

(9b)

\[ D_2^{(0)} = \varepsilon_{11} A E_2 - f_{3113} A u_{2,1111}, \]  

(9c)

\[ D_3^{(0)} = \varepsilon_{11} A E_3 - f_{3113} A u_{3,1111}, \]  

(9d)

where

\[ \tau = \frac{(c_{1111} - c_{1122})(c_{1111} + 2c_{1222})}{c_{1111} + c_{1222}}, \]
\[ B_2 = \int_A x_2^2 dA, \quad B_3 = \int_A x_3^2 dA. \]  

(10)

\( D_2^{(0)} \) and \( D_3^{(0)} \) are needed to calculate the charge on the electrodes. Substitutions from Equations (8) and (9), we can write Equation (7) as two equations for \( u_1 \) and \( u_2 \):

\[ -\tau B_2 u_{2,1111} + F_2 A = \rho A u_2, \]
\[ -\tau B_3 u_{3,1111} + F_3 A = \rho A u_3. \]  

(11)

4. Analysis of a Flexoelectric Gyroscope

When the beam in Figure 1 is used as a gyroscope, it is rotating about the \( x_1 \) axis with an angular rate \( \Omega \) that is to be measured. We fixed the coordinate system to the rotating beam. In the rotating coordinate system, the effects of the centripetal and Coriolis accelerations can be taken into consideration through the following effective forces:

\[ F_2 = -\rho(-2\Omega u_3 - \Omega^2 u_2), \]
\[ F_3 = -\rho(2\Omega u_2 - \Omega^2 u_3). \]  

(12)
\( V_2 \) is the known applied voltage that drives the beam into bending with \( u_2 \). The effective Coriolis force then drives the beam into bending with \( u_3 \), which produces \( V_3 \), which is unknown. The charge on the electrode at \( x_3 = b \) is given by
\[
Q^e = 2e \left[ \frac{L}{2b} - D_3 x_3 \right] dx_1
= 2e \int_{0}^{L} f_{3113} [u_{3,1}(L) - u_{3,1}(0)]
\]
(13)

where Equation (9d) has been used. The current flowing out of this electrode is given by
\[
I_3 = -Q^e.
\]
(14)

Consider time-harmonic motions with the following complex notation
\[
(V_2, V_3, u_2, u_3, Q^e, I_3) = \text{Re} \left\{ (V_2, V_3, U_2, U_3, Q^e, I_3) \exp(i\omega t) \right\},
\]
(15)

where \( V_2, V_3, U_2, U_3, Q^e \), and \( I_3 \) are the complex amplitudes of \( V_2, V_3, u_2, u_3, Q^e \), and \( I_3 \). \( i \) is the imaginary unit. \( \omega \) is the time-harmonic frequency. The electrodes at \( x_3 = \pm b \) are connected by a circuit whose impedance is \( Z \) in harmonic motions, which provides the following circuit equation:
\[
I_3 = \frac{V_3}{Z}.
\]
(16)

The substitution of Equations (12)–(15) into Equations (11) and (16) results in the following three equations for \( U_2, U_3 \), and \( V_3 \):
\[
\begin{align*}
-\tau B_2 U_{2,1111} + \rho A(\omega^2 U_2 + i\omega 2\Omega U_3 + \Omega^2 U_2) &= 0, \\
-\tau B_3 U_{3,1111} + \rho A(\omega^2 U_3 - i\omega 2\Omega U_2 + \Omega^2 U_3) &= 0, \\
\frac{V_3}{Z} &= -2i\omega \left\{ \frac{L e_{11} V_3}{2b} + f_{3113} [U_{3,1}(L) - U_{3,1}(0)] \right\}.
\end{align*}
\]
(17)

Specifically, consider a simply supported beam with the following boundary conditions:
\[
\begin{align*}
u_2(0,t) &= u_3(0,t) = u_2(L,t) = u_3(L,t) = 0, \\
M_2(0,t) &= M_3(0,t) = M_2(L,t) = M_3(L,t) = 0.
\end{align*}
\]
(18)

Equation (18) represents the simplest and most basic mounting of a beam, which was used in the first piezoelectric vibratory gyroscope [11]. The purpose of the present paper is to show that a vibrating flexoelectric beam can also operate as a gyroscope. Other mountings, such as a cantilever, can also be used, which changes the mathematical analysis but not the mechanism of the device. Therefore, other boundary conditions are not pursued here.

Equation (17a,b) form a system of linear ordinary differential equations. We look for its solution in the following form:
\[
U_2 = \bar{U}_2 \exp(kx_1), \quad U_3 = \bar{U}_3 \exp(kx_1)
\]
(19)

where \( k \) is undetermined. The substitution of Equation (19) into Equation (17a,b) gives two linear homogeneous algebraic equations:
\[
\begin{bmatrix}
-\tau B_2 k^4 - \rho A(\omega^2 + \Omega^2) & 2\rho A i\omega \Omega \\
2\rho A i\omega \Omega & -\tau B_3 k^4 - \rho A(\omega^2 + \Omega^2)
\end{bmatrix}
\begin{bmatrix}
\bar{U}_2 \\
\bar{U}_3
\end{bmatrix}
= \begin{bmatrix}
0 \\
0
\end{bmatrix}.
\]
(20)

For nontrivial solutions, the determinant of the coefficient matrix has to vanish, i.e.,
\[
(\tau)^2 B_2 k^8 - \rho A(\omega^2 + \Omega^2) [c(B_2 + B_3) k^4 + [\rho A(\omega^2 + \Omega^2)]^2] + (2\rho A i\omega \Omega)^2 = 0.
\]
(21)
Equation (21) is a polynomial equation for \( k \). We denote its eight roots by \( k^{(N)} \), where \( N = 1, 2, \ldots, 8 \). The corresponding nontrivial solutions of \( U_2 \) and \( U_3 \) are denoted by

\[
\begin{bmatrix} U_2 \\ U_3 \end{bmatrix} = \begin{bmatrix} 2\rho A i\omega \Omega \\ -[\rho A(\omega^2 + \Omega^2) - \tau B_2(k^{(N)})^4] \end{bmatrix}.
\]

Then, the general solution of Equation (17a,b) can be written as

\[
U_2 = \sum_{N=1}^{8} (2\rho A i\omega \Omega) \Pi^{(N)} \exp(k^{(N)}x_1),
\]

\[
U_3 = -\sum_{N=1}^{8} [\rho A(\omega^2 + \Omega^2) - \tau B_2(k^{(N)})^4] \Pi^{(N)} \exp(k^{(N)}x_1),
\]

where \( \Pi^{(N)} \) are undetermined constants. The substitution of Equation (23) into Equations (17c) and (18) yields nine linear algebraic equations for \( \Pi^{(N)} \) and \( \Pi_3 \). These equations are solved on a computer using MATLAB R2021a (Xi’an, China).

5. Numerical Results and Discussion

As a numerical example, consider a ceramic beam of BaTiO$_3$ that is not poled and hence is nonpiezoelectric. The relevant material constants are \( C_{11} = 166 \) GPa, \( C_{12} = 77 \) GPa, \( C_{13} = 78 \) GPa, \( C_{33} = 162 \) GPa, \( C_{44} = 43 \) GPa, \( \epsilon_{33} = \epsilon_{22} = 12.6 \times 10^{-9} \) C$^2$/N·m$^2$, and \( f_{3113} = 10^{-6} $N/C. The elastic and dielectric constants are from [25]. The flexoelectric constant is from [18,26]. Examples of other materials that have been used for micro-beams are zinc oxide, barium sodium niobate, barium titanate [27], and strontium titanate [28], which, when unpoled, may be considered for flexoelectric gyroscope applications. In [29], a micro-beam of BaTiO$_3$ with dimensions of 1.5, 3.2, and 11 $\mu$m was fabricated for experimental investigation. For our modeling analysis with the goal of demonstrating the basic operation of the gyroscope, the geometric parameters were chosen to be \( a = b = 5 \mu$m, \( c = d = a/2 \), and \( L = 200 \mu$m. Material damping is described by complex elastic constants \( C_{pq}(1 + i/Q) \) with \( Q = 10^2 \). The amplitude of the driving voltage is \( V_2 = 100 $volts. \( Z = \infty \) is used for the open circuit output voltage. \( \Omega = 3.6 \times 10^4 $rad/s, which is much smaller than (approximately 1%) the first resonance frequency of the beam, which is \( 3.6 \times 10^6 $rad/s. Some of these parameters may be varied separately below. We introduced \( Z_2 \) as a unit for \( Z \):

\[
Z_2 = \frac{1}{2i\omega C_2}, \quad C_2 = \frac{L\epsilon_{11}}{2b}.
\]

Figure 2a shows \( |u_2(L/2)| \) versus the driving frequency \( \omega \) with three resonances. The third one is barely visible. For gyroscope application, we are mainly interested in the first resonance. \( |u_2(L/2)|, |u_3(L/2)| \) and the output voltage \( |V_3| \) near the first resonance are shown in Figure 2b–d, respectively. \( u_2 \) is driven by the applied \( V_2 \) through flexoelectric coupling and is called the primary motion. \( u_3 \) is due to the Coriolis force associated with \( \Omega \) and is called the secondary motion. \( V_3 \) is produced by \( u_3 \) through flexoelectric coupling. They all assume double-peak resonances because of flexural vibrations in both directions, which is typical for vibratory piezoelectric gyroscopes.

Figure 3 shows the effects of various parameters on the output voltage near the first resonance. Figure 3a shows that a larger flexoelectric coefficient leads to a higher output, which is as expected. Figure 3b shows that the output voltage drops when the cross section deviates somewhat from a square. This is because, for a beam with a cross section not close to a square, the resonance frequencies of flexural vibrations in the \( x_2 \) and \( x_3 \) directions are not close. Hence, the gyroscope is not working in the optimal condition (the so-called double-resonant condition). Figure 3c shows that, when the impedance of the output circuit increases, the output voltage increases too. At the same time, the output current decreases correspondingly. Figure 3d shows that the output voltage is linear in \( \Omega \) when \( \Omega \) is small,
which is ideal for angular rate sensing. For large values of $\Omega$, the linearity is lost because $\Omega$ appears in Equation (17) in a complicated and nonlinear way.

![Figure 2](image)

**Figure 2.** Behavior near the first resonance. (a) Primary motion showing resonances. (b) Primary motion near the first resonance. (c) Secondary motion near the first resonance. (d) Output voltage near the first resonance.

![Figure 3](image)

**Figure 3.** Effects of various parameters. (a) Flexoelectric coefficient. (b) Dimensions of the cross section. (c) Impedance of the output circuit. (d) Angular rate $\Omega$. $\omega = 3.7 \times 10^6 \text{ rad/s}$. 

- Figure 2 shows the effects of various parameters on the output voltage near the first resonance. The plots illustrate how the output voltage varies with different parameters such as the driving frequency $\omega$, the flexoelectric coefficient, and the dimensions of the cross section.
- Figure 3a demonstrates the behavior of the flexoelectric coefficient $V_2$ versus $\omega$ for different values of $b$. The curves show how $V_2$ changes as $\omega$ varies, highlighting the impact of the flexoelectric coefficient on the output voltage.
- Figure 3b illustrates the influence of the dimensions of the cross section on the output voltage $V_3$. The curves show how $V_3$ changes with $\omega$ for the given dimensions, indicating the importance of geometric parameters in determining the output characteristics.
- Figure 3c examines the effect of the impedance of the output circuit on the output voltage $V_3$. The curves demonstrate how $V_3$ varies with $\omega$ for different impedances, revealing the relationship between circuit impedance and sensor performance.
- Figure 3d explores the effect of angular rate $\Omega$ on the output voltage $V_3$. The plot shows the output voltage as $\Omega$ varies within a specified range, indicating the dependence of the output on angular rate.

These figures provide a comprehensive understanding of the behavior of the gyroscope, enabling a deeper insight into its operational characteristics and optimization for various applications.
The output signal $V_3$ for detecting $\Omega$ depends on several physical and geometric parameters; in particular, the driving frequency $\omega$ and the impedance $Z$ of the output circuit as shown in Figures 2 and 3, where $\omega$ and $Z$ were varied one at a time. For a more comprehensive understanding of the behavior of the gyroscope, we plot $V_3$ versus $\omega$ and $\Omega$ together in Figure 4a, and $V_3$ versus $\omega$ and $Z$ in Figure 4b, respectively. The curves in Figures 2 and 3 are formed by intersections of the surfaces in Figure 4 with different vertical planes. It can be seen from Figure 4a that, when $\Omega$ is fixed, there are two peaks as $\omega$ varies. The two peak values increase with $\Omega$ monotonically when $\Omega$ is small and saturate when $\Omega$ is large. The distance between the two peaks also increases with $\Omega$. In Figure 4b, when $Z$ is fixed, there are two peaks as $\omega$ varies. The two peak values increase with $Z$ monotonically. When $Z$ is small, the output circuit is nearly shorted, with a small $V_3$. When $Z$ is large, the output circuit is nearly open, with a large and saturated $V_3$. These agree with Figure 3c,d.

![Figure 4](image-url)

**Figure 4.** Three-dimensional views of the output voltage. (a) $V_3$ versus $\omega$ and $\Omega$. $Z = \infty$. (b) $V_3$ versus $\omega$ and $Z$. $\Omega = 105$ rad/s.

### 6. Conclusions

It is shown theoretically that a micro-beam in flexural vibrations excited and detected flexoelectrically can be used to make a gyroscope to detect an angular rate. Compared to conventional piezoelectric beam gyroscopes, the flexoelectric beam gyroscope proposed has a simpler structure or electrode configuration. The one-dimensional model developed is effective in describing the basic behaviors of the beam flexoelectric gyroscope.
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