Ultra-high dynamic range electro-optic sampling for detecting millimeter and sub-millimeter radiation

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Time-domain spectroscopy using coherent millimeter and sub-millimeter radiation (also known as terahertz radiation) is rapidly expanding its application, owing greatly to the remarkable advances in generating and detecting such radiation. However, many current techniques for coherent terahertz detection have limited dynamic range, thus making it difficult to perform some basic experiments that need to directly compare strong and weak terahertz signals. Here, we propose and demonstrate a novel technique based on cross-polarized spectral-domain interferometry to achieve ultra-high dynamic range electro-optic sampling measurement of coherent millimeter and sub-millimeter radiation. In our scheme, we exploit the birefringence in a single-mode polarization maintaining fiber in order to measure the phase change induced by the electric field of terahertz radiation in the detection crystal. With our new technique, we have achieved a dynamic range of 7 × 106, which is 4 orders of magnitude higher than conventional electro-optic sampling techniques, while maintaining comparable signal-to-noise ratio. The present technique is foreseen to have great impact on experiments such as linear terahertz spectroscopy of optically thick materials (such as aqueous samples) and nonlinear terahertz spectroscopy, where the higher dynamic range is crucial for proper interpretation of experimentally obtained results.

Recent years have witnessed significant successful developments of techniques related to static and transient terahertz (THz) time-domain spectroscopy (THz-TDS) and imaging. The versatility of these techniques has been demonstrated in a wide range of applications in many disciplines, such as in spectroscopic imaging and tomography1–3, label-free genetic diagnostics and analysis4, biomolecular spectroscopy5, and biomedical applications such as T-ray biosensor6. Such remarkable progress has undoubtedly been accelerated by the incredible advances in both generating and detecting coherent THz radiation. For example, the recent surge in the availability of intense THz radiation sources is allowing new solutions to long-standing challenges, as well as opening up new avenues in both science and technology. For instance, intense THz sources have the potential to enable THz-TDS of aqueous samples, such as those related to biology and medicine7, with high signal-to-noise ratio (SNR)8. Due to the high absorption of THz radiation by water, such experiments have been difficult to perform up to now. However, the availability of THz sources with high flux is opening the possibility to perform THz-TDS of aqueous and other highly absorptive media in transmission configuration. Humidity also has significant influence in THz applications such as large-scale object imaging and remote sensing for security purposes9,10, and wireless communications11,12, in which the THz pulse may need to propagate long distances through the atmosphere. Intense THz sources are also enabling the observation of fascinating nonlinear phenomena in light-matter interaction processes13–20. For example, THz nonlinear spectroscopy offers a unique characterization method of novel materials for future THz electronics, such as graphene21–23 and topological insulators24,25. In turn, such demand is pushing

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the limits of tabletop, intense, and ultrafast broadband THz emitting sources, resulting in peak THz electric fields of sub-MV/cm to several MV/cm\(^2\)–30.

For such applications to be fully implemented, it is of crucial importance to have coherent THz detection techniques with both high dynamic range (DR) and high SNR\(^3\). High DR measurement is especially important in many of the above applications, where one needs to compare the waveform of intense THz pulses with relatively weak THz signals (such as the THz signal after experiencing strong absorption, or the nonlinear THz signal). Large DR is also required in THz-TDS measurements in order to avoid misinterpretation of experimentally obtained data\(^3\). However, electro-optic sampling (EOS)\(^32–34\), which is currently one of the most popular methods for THz detection, has achieved DR of only a few hundred. This limited DR of conventional EOS technique can be attributed to the mechanism by which the THz field is measured. In EOS, a linearly polarized femtosecond laser pulse co-propagates with a picosecond THz pulse in an electro-optic (EO) detection crystal\(^32\). The THz-electric-field-induced birefringence in the EO crystal (due to the Pockels effect) changes the polarization of the co-propagating optical probe pulse. The resulting ellipticity of the probe pulse is measured by using a detection system that consists of a quarter-wave plate, a polarizer and a pair of balanced photodiodes placed after the detection crystal. The change in phase, which is proportional to the THz electric field, is manifested as a modulation in the intensity of the two polarization components of the optical probe pulse. However, if the induced phase change in the probe pulse components is more than \(\pi/2\), a reversal in the intensity modulation of the probe pulse will take place. This in turn results in ambiguities in measuring THz fields that induce phase differences of more than \(\pi/2\)\(^3\) in the conventional EOS configuration. This limitation is known as over-rotation\(^35\) and hence severely limits the DR of conventional EOS. In addition, over-rotation poses several other restrictions. For example, higher spectral resolution in THz-TDS requires thicker EO detection crystals\(^35\). However, a thicker crystal increases the possibility of over-rotation, as induced birefringence in the EO crystal is proportional to both the THz electric field and the thickness of the crystal. One could use thin (less than 50 \(\mu\)m) detection crystals, but the DR will still suffer from lower THz electric field modulation on the optical probe pulse.

Techniques such as air-biased-coherent-detection (ABCD)\(^36,37\) and spectral-domain interferometry (SDI)\(^35,38\) have been proposed and demonstrated as alternatives to the conventional EOS technique, to overcome such limited DR in THz-TDS. Improved DR of 4,400 has been reported with the ABCD technique, but this came with the cost of the need for expensive equipment and a much more complex setup, requiring the use of a high voltage source and a photomultiplier tube\(^36\). Meanwhile, with the SDI technique in THz detection, over-rotation and its consequent restrictions could be easily eliminated by unwrapping the phase induced by the intense THz signal when it is more than \(\pi/2\), by using certain algorithms\(^35\). However, the standard SDI technique suffers from low SNR and limited temporal scan window, the latter being limited by the fixed optical path difference (OPD) between the two probe pulses\(^35,38\).

In the present work, we propose and demonstrate a new interferometric technique called cross-polarized spectral-domain interferometry (CP-SDI). Using this new technique, we have demonstrated a tremendous DR of \(7 \times 10^6\) for the EOS detection of THz electric fields, while avoiding the limitation of over-rotation. Moreover, the limit in the temporal scan window suffered in the standard SDI technique in THz detection has been avoided, thus achieving SNR that are comparable to conventional EOS detection technique. This new technique makes use of the birefringence in polarization maintaining (PM) single-mode optical fiber in order to measure the phase change due to the THz electric field.

**Results**

**Concept of the CP-SDI scheme.** The major breakthrough of the present work is the design and demonstration of an effective scheme for improved THz electric field measurement with higher DR and SNR, which is crucial for various applications of THz technology, including spectroscopic measurements. In this new technique, we exploit the intrinsic phase delay between the fast and the slow axes of the birefringent fiber\(^39\) (see Fig. 1). The s- and p-polarization components of the probe pulse experience different refractive indices in the PM fiber, which results in the modification of the polarization state at its output, depending on the length of the fiber. In other words, the PM fiber creates two pulses; one propagating along the fast axis and the other propagating along the slow axis of the PM fiber, resulting in an OPD between the two. This is in addition to the OPD between the s- and p- components of the probe pulse that results from the birefringence introduced by the detection crystal, when the THz pulse and the probe pulse overlap in space and time. Then, we choose a common polarization direction that is neither of s- nor p-polarization (by using, for example a polarizer), to allow these two pulses to interfere. The OPD introduced by the THz electric field is measured from the interference signal of the two probe pulses as a change in the phase. The measured phase can be unwrapped by certain algorithms described in ref. 35, leading to ultra-high DR for this technique.

The two orthogonal components of the probe pulse exiting the fiber cannot interfere, as they are cross polarized. In order to enable their interference, a polarizer is placed at the exit end of the PM fiber with its transmission axis at 45° with respect to the fast and slow axes. This allows a component of both s- and p-polarizations to pass through and to interfere in the spectrometer. At the CCD camera plane, the spectral components of the two pulses interfere, thus allowing one to measure the phase difference between them. Just as in the conventional EOS methods, the THz electric field induces birefringence in the ZnTe detection crystal, which is read out by the probe pulse when it overlaps with the THz pulse within the crystal in space and time. However, in the CP-SDI method, this birefringence is converted into a change in the OPD (or the phase) between the two probe pulses using a PM fiber and a polarizer. Using the interference signal between the spectral components of these two pulses, one can measure the THz electric field as a change in the phase difference introduced by the THz pulse.

The parameters of the PM optical fiber used in this study are summarized in Table 1.
THz electric field measurement. Here we experimentally compare THz electric field measurements obtained with the conventional EOS, the standard SDI, and the CP-SDI techniques. For the CP-SDI measurement, we have used the experimental set up shown in Fig. 2.

The resulting interference between the two component signals at the plane of the CCD camera can be expressed as

\[ I(k) = I_p(k) + I_s(k) + 2 \sqrt{I_p(k)I_s(k)} \cos \left[ \phi_o + kl + \phi_{THz} \right] \]  

(1)

Here, \( k = 2\pi/\lambda \) is the wave number and \( \lambda \) is the central wavelength of the probe pulse, \( I_p \) and \( I_s \) are the intensities of the \( p \)-polarization and \( s \)-polarization components of the probe pulse, respectively, \( \phi_o \) is the phase constant, \( l \) is the optical path difference introduced between \( s \)- and \( p \)-polarization components by the PM fiber and \( \phi_{THz} \) is the phase introduced by the THz signal. The interference is recorded using a (2D) CCD camera and rescaled from wavelength space to wave-number \( (k) \) space and Fourier transformed to obtain the corresponding FFT spectrum. The instantaneous phase difference between the two signals is calculated using the relation

| Parameter                      | Value                        |
|--------------------------------|------------------------------|
| Numerical aperture             | 0.12                         |
| Core diameter                  | 4.5 μm                       |
| Attenuation                    | \( \leq 4 \) dB/km @ 850 nm  |
| Operating wavelength           | 770–1100 nm                  |
| Second mode cut-off            | 710 ± 60 nm                  |
| Mode field diameter (1/e2 fit – near field) | 5.3 ± 1.0 μm @ 850 nm |
| Beat length                    | 2.4 mm @ 850 nm              |
| Birefringence                  | \( 3.5 \times 10^{-4} \)     |

Table 1. Parameters of the PM fiber used in the experiment.
\[ \varphi = \tan \left( \frac{\bar{H}(L)}{I(L)} \right) \]

(2)

Here, \( \bar{H}(L) \) and \( I(L) \) are the Hilbert transform and the interference signal intensity of equation (1) at an OPD of \( L \).

The change in the OPD over time can be traced by monitoring the phase change in equation (2). For a fixed length of the PM fiber, this phase changes only due to the birefringence induced by the THz electric field in the ZnTe detection crystal, which is proportional to the THz electric field strength. Hence the temporal shape of the THz electric field can be reconstructed by varying the delay time between the THz pulse and the optical probe pulse using a delay stage.

We show in Fig. 3a the long temporal scans (>30 ps) for the traces of the THz electric field measured using the conventional EOS and the CP-SDI techniques. The trace obtained with the CP-SDI technique using an optical fiber length of 80 cm. At this length, the OPD between the two probe pulses will be \(~400\mu m\) (a temporal separation of \(~1.3\) ps) at a central wavelength \( \lambda_o = 790\) nm when they exit the fiber. Worth to note that in contrast to common interferometric methods in SDI the two separated pulses in time interfere as two waves with different frequencies beat in time domain. Despite being temporally separated by more than the pulse duration, their spectral interference can be detected. The mode locked laser pulse is transformed into individual spectral components owing to the linear dispersion of the diffraction grating in the spectrometer. Several different directions will be taken by the different propagating spectral components, which in turn creates a frequency-dependent time delay\(^3\), therefore individual spectral components are spatially separated and hence are not mode locked anymore after the diffraction grating, consequently the two temporally separated pulses exiting the PM fiber can physically overlap on the CCD camera plane i.e. pulses interfere for much longer time scales.

For both THz traces in Fig. 3a, the main peak of the THz pulse is at 7.3 ps, while the second peak at 28.3 ps is the first reflection of THz pulse from the ZnTe detection crystal. For the sake of comparison we show in Fig. 3b a THz trace obtained with the standard SDI technique, where a 300 \( \mu m \)-thick glass plate was utilized to introduce a fixed OPD between the two probe pulses reflecting from its front and the back surfaces. One can see that the temporal scanning window is limited to only 3 ps owing to the fixed glass plate thickness in this version of SDI technique.

**Over-rotation limitation.** In order to compare the shape of the THz main pulse obtained with the conventional EOS and the CP-SDI techniques, short temporal scans (5 ps-long each) at different THz electric fields are shown in Fig. 4a,b. One can see that the THz pulse obtained at high THz electric fields (64 kV cm\(^{-1}\) – 54 kV cm\(^{-1}\)) with the conventional EOS in Fig. 4a suffers from over-rotation in the parts indicated by arrows, which alter the shape of the pulse. At lower THz electric fields (\(\leq 47\) kV cm\(^{-1}\)) the THz pulse obtained with the conventional EOS technique returns to its normal shape. Meanwhile when using the CP-SDI technique for the same THz electric fields, over-rotation is always avoided even at higher values of THz electric field, as shown in Fig. 4b.
Signal-to-noise ratio. The inset in Fig. 3a shows the corresponding power spectra of the THz electric field obtained from the conventional EOS and the CP-SDI techniques. From these spectra, we find that the measured SNR is 48.97 dB for the CP-SDI technique compared to 52.17 dB for conventional EOS technique. Meanwhile, the inset in Fig. 3b shows the spectrum of THz pulse obtained with the standard SDI technique. The SNR measured to be 38.12 dB for the standard SDI technique compared to 48.97 dB for the CP-SDI technique.

We could also evaluate the SNR from the temporal shape of the THz pulse, by taking the ratio of the THz peak to the standard deviation of the baseline (signal that is before 1 ps) in the THz temporal trace. Following such approach, the SNR of the THz pulse measured with the CP-SDI technique (Fig. 3a) is ~279 compared to ~418 for the THz pulse obtained with the conventional EOS technique (Fig. 3a). At the same time, the SNR of THz pulse obtained with the standard SDI (Fig. 3b) is ~45.

Dynamic range. For a Gaussian profiled spectrum, the maximum OPD that can be measured using the CP-SDI technique is given by

\[
d_{\text{max}} = \frac{2 \ln 2 N \lambda^2}{\pi} \frac{\lambda^2}{2 \Delta \lambda}
\]

Applying the parameters of our system (central wavelength \(\lambda_o = 790\) nm, bandwidth \(\Delta \lambda = 40\) nm, and number of pixels of the CCD camera \(N = 640\)) in equation (3) yields a theoretical OPD range of 2.203 mm. Considering a change of \(2\pi\) in the phase for one wavelength change in the OPD, the maximum overall phase change that we can measure with our CP-SDI system is 5,577 \(\pi\). In the conventional EOS technique, the maximum measurable phase change is \(\pi/2\), which is approximately 11,000 times smaller than the maximum measurable phase change obtained with the CP-SDI technique. Moreover, the maximum achievable DR for our technique with our current setup is measured to be \(7 \times 10^6\), which is 4 orders of magnitude higher than the maximum achievable DR for our conventional EOS configuration of \(6 \times 10^2\). Meanwhile in the standard SDI the maximum achievable DR is \(6 \times 10^5\) when using the same spectrometer and laser source.

Fiber length choice. We further investigate the effect of fiber length on the SNR of our THz electric field measurement. For this purpose, PM fibers of different lengths, ranging from 40 to 240 cm (with corresponding

Figure 3. Terahertz electric field detection using the conventional EOS, the CP-SDI, and the Standard SDI techniques. A comparison between THz electric field traces obtained with (a) conventional EOS (blue dashed line), and the CP-SDI (red solid line), and (b) the standard SDI (wine solid line) techniques. The temporal scanning window in the case of the standard SDI is limited to 3 ps due to the thickness (300 μm) of the glass plate used in the technique. The inset in (a) shows the corresponding power spectra of the THz traces obtained with the conventional EOS and the CP-SDI techniques and in (b) shows the corresponding power spectrum of the THz trace obtained with the standard SDI technique.
OPD between the probe pulses at the exit end of the fiber of 200 to 1200 μm) were used. At each fiber length, a THz temporal trace was recorded for the same THz peak electric field (64 kVcm⁻¹). Figure 5 shows the SNR measured using the CP-SDI THz detection technique for various OPD between the probe pulses. Our experimental findings show that the SNR increases as the OPD between the probe pulses decreases from 1200 μm to 400 μm. However, further decreasing the OPD from 400 μm to 200 μm reduces the SNR.

One could attribute this reduction in the SNR to the fact that working closer to the DC component of the interference signal (that is, closer to zero-OPD) will result in the signal subject to many low-frequency noises in the laboratory environment. On the other hand, the reduction in the SNR for OPD above 400 μm could be attributed to the reduced contrast of the interference fringes when working far away from zero-OPD where the sensitivity of the SDI technique is minimal. (See Supplementary Note1 and Supplementary Figure S1 online).

Discussion

The conventional EOS technique suffers from over-rotation, which was observed in our experiment design as well. However, by using our newly designed CP-SDI, we could circumvent this limitation while maintaining comparable SNR. By eliminating over-rotation, we could achieve a dynamic range of $7 \times 10^6$. On the other hand, the standard SDI technique in THz electric field measurement presented in our earlier work achieved inferior SNR and the DR compared to SNR and DR of the new CP-SDI technique. In the standard SDI technique one of the major sources of phase noise is angular vibration in the glass plate owing to the angular variation between its two surfaces. Furthermore the OPD between the two pulses reflecting from the glass plate surfaces was relatively large (900 μm) which results in working relatively far from zero-OPD which in turn cause a loss in interference signal of the two pulses and consequently lowers the SNR and the DR. However in the new CP-SDI technique,
introducing the PM fiber increases the SNR in THz measurement primarily because of working closer to zero optical path difference where sensitivity of the technique is maximal. Moreover, by using the PM fiber, the noises associated with glass plate vibrations which change the optical path difference between two interfering signals, are eliminated. A change in optical path difference because of glass plate vibration in the standard SDI technique will result in an additional change in phase, on top of the phase change introduced by the THz electric field, and appears as noise. This noise is eliminated in our new CP-SDI technique, since both interfering signals are traveling through the same fiber and any change in OPD is common to both signals. The PM fiber also enables higher dynamic range since the interfering signals are generated after the detection crystal where as in the standard SDI technique, the interfering signals are generated before the detection crystal, limiting the scan length to the temporal thickness of the glass plate. Consequently the CP-SDI technique has achieved higher SNR and dynamic range compared to the standard SDI technique.

Furthermore, the new CP-SDI technique in THz measurement eliminates the limit in the temporal scan length - crucially required for any spectroscopic application - which was a drawback of the standard SDI technique\(^3\) in THz detection due to limit imposed by the thickness of the glass plate, however in the new technique the PM fiber imposes no limit in the scan length. Indeed the PM fiber plays a critical role in adjusting a suitable working point on the OPD where the detection sensitivity is high and at the same time the noises are minimal. Alternatively this effect could be also achieved by using a birefringent crystal with appropriate dimensions; however that comes with the expenses of growing such crystal, whereas PM fibers are commercially available at affordable prices and can be manipulated easily in small size set ups.

In order to evaluate the capability of our technique to measure different THz peak electric fields with reasonable SNR, the THz peak electric field was varied from \(~4\,\text{kVcm}^{-1}\) to \(~64\,\text{kVcm}^{-1}\) by using two wire-grid polarizers. The amplitude THz electric field (\(E_{\text{THz}}\)) is measured with conventional EOS technique using the modulation formula in equation (4)\(^2\).

\[
\frac{A - B}{A + B} = \sin \theta = \frac{2\pi r_{41} n_o L t_{\text{ZnTe}} N E_{\text{THz}}}{\lambda_o}
\]

Here \(A\) and \(B\) are the signals from the balanced photodetectors in EO detection configuration, \(\theta\) is the phase shift induced by the THz peak electric field, \(r_{41}\) is the electro-optic coefficient of the ZnTe detection crystal, \(n_o\) is the refractive index of ZnTe, \(L\) is the ZnTe thickness, Fresnel transmission coefficients \(t_{\text{ZnTe}}\) for ZnTe and \(t_s\) for the silicon wafer, \(N\) is the number of silicon wafers, and \(\lambda_o\) is the central wavelength.

At THz peak electric field of \(64\,\text{kVcm}^{-1}\) we could measure SNR of 48.97 dB for the THz electric field measurement obtained with CP-SDI technique compared to 52.17 dB obtained with conventional EOS technique. Meanwhile at THz field of \(4\,\text{kVcm}^{-1}\) we could measure SNR of 28.45 dB for the CP-SDI technique compared to 34.77 dB for the conventional EOS technique. These experimental findings are indicative of the potentials of the new technique in measuring higher THz electric fields as well as lower fields. Further enhancement in SNR of the new CP-SDI technique could be achieved if self-referencing is implemented in the setup, which has been proven to enhance the SNR considerably by reducing the noise due to vibration and laser fluctuations in the set up\(^3\).

In summary, we propose and demonstrate a new EOS based technique using PM optical fiber and SDI. The new technique has a dynamic range that is 4 orders of magnitude higher than the conventional EOS technique, while maintaining comparable SNR. The technique is promising and has the potential to significantly advance new areas of THz science and technology, such as nonlinear THz spectroscopy, thus opening new avenues in THz-TDS and imaging techniques that require large dynamic range.
Methods
CP-SDI scheme. Here we use the experimental set up illustrated in Fig. 2 where a femtosecond 800 nm laser beam is split by a beam splitter (BS) into two arms: the pump arm and the probe arm. The pump arm is used to generate the THz pulse. The probe beam is focused by a spherical plano-convex lens (L1), and then propagates through a hole in a parabolic off-axis mirror (PM4) and onto a 1-mm-thick <110> ZnTe detection crystal, where it overlaps with the focused THz pulse. Another spherical plano-convex lens (L2) is used to collimate the optical probe beam after the ZnTe detection crystal. A quarter-wave plate is used before a single-mode PM optical fiber (Thorlabs, PM 780-HP) to convert the linear polarization state of the probe pulse to circular polarization without the presence of the THz pulse. Then the probe pulse is coupled into the PM fiber, with its polarization components (s- and p-) set along the two orthogonal birefringent axes of the PM fiber depending on the birefringence introduced in the ZnTe crystal by the THz electric field. The wire grid polarizers are used to vary THz peak electric field. The custom-made spectrometer consists of a diffraction grating (1200 grooves/mm), a plano-convex cylindrical lens CL3 (f = 150 mm), and a two-dimensional (2D) CCD camera (Dalsa Inc., CR-GM00-H6400, 480 × 640 pixels). We measure the phase change between the spectral components of the two polarization signals exiting the single mode PM fiber at a fixed length, which is proportional to the THz electric field strength only. By varying the delay time between the THz pulse and the optical probe pulse using a delay stage the temporal shape of the THz electric field can be plotted. Worth to mention that the experimental data extraction is straightforward and carried out in real time by a LabVIEW code that is developed in our group, moreover the experiment does not require any longer time than that taken by the conventional EOS technique.

Standard SDI scheme. Here we use the experimental setup described in our earlier work35 with a different CCD camera in the spectrometer (Dalsa Inc., CR-GM00-H6400, 480 × 640 pixels).

THz generation and peak electric field calculation. THz generation throughout this work was achieved via the tilted-pulse-front technique in a LiNbO3 crystal41,42 pumped with 0.96 mJ pulses from Ti:Sapphire laser (repetition rate of 2.5 kHz, wavelength of 800 nm, pulse width of 40 fs, and pulse energy up to 4 mJ). Single cycle THz pulses with energies up to 0.3 μJ are generated with bandwidth extending from 0.1 to 3 THz. In order to evaluate the THz peak electric field, an electro-optical signal $I_{THz}$ using the equation $\sin^{-1}(|\Delta I|/I) = \frac{2n_{THz}E_{peak}r_{ZnTe}}{\lambda_{THz}r_{Si}}$ (ref. 26). Here, $n_{THz} = 2.87$ (ref. 43) is the refractive index of ZnTe crystal, $r_{Si} = 4.04$ pm V$^{-1}$ (ref. 44) is the electro-optical coefficient of ZnTe, $r_{ZnTe} = 2/(n_{THz}+1) = 0.479$ is Fresnel transmission coefficients of ZnTe crystal where $n_{THz} = 3.17$ (ref. 45) is the refractive index of ZnTe crystal at 1 THz, $r_{Si} = 0.7$ (ref. 26) is Fresnel transmission coefficients of one silicon wafer, $L$ (= 1 mm) is the thickness of ZnTe crystal, $N$ (= 7) is the number of high-resistivity silicon attenuators used to reduce the THz field amplitude before ZnTe detection crystal, and $\lambda_{THz}$ (= 790 nm) is the central wavelength.

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Author Contributions

A.I. designed, carried out the experiment, and wrote the manuscript. D.F. helped in designing, carrying out the experiment, and contributed in writing the manuscript. G.S. and K.S. equally proposed the CP-SDI idea and contributed in writing the manuscript. M.K.-T. helped in carrying out the experiment and writing the manuscript. A.I. designed, carried out the experiment, and wrote the manuscript. D.F. helped in designing, carrying out the experiment, and contributed in writing the manuscript.

Additional Information

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