Strain-Induced Modulation of Resistive Switching Temperature in Epitaxial VO$_2$ Thin Films on Flexible Synthetic Mica

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ABSTRACT: The resistive switching temperature associated with the metal–insulator transition (MIT) of epitaxial VO$_2$ thin films grown on flexible synthetic mica was modulated by bending stress. The resistive switching temperature of polycrystalline VO$_2$ and V$_2$O$_5$ thin films, initially grown on synthetic mica without a buffer layer, was observed not to shift with bending stress. By inserting a SnO$_2$ buffer layer, epitaxial growth of the VO$_2$(010) thin film was achieved, and the MIT temperature was found to vary with the bending stress. Thus, it was revealed that the bending response of the VO$_2$ thin film depends on the presence or absence of the SnO$_2$ buffer layer. The bending stress applied a maximum in-plane tensile strain of 0.077%, resulting in a high-temperature shift of 2.3 $^\circ$C during heating and 1.8 $^\circ$C during cooling. After $10^4$ bending cycles at a radius of curvature $R = 10$ mm, it was demonstrated that the epitaxial VO$_2$ thin film exhibits resistive switching temperature associated with MIT.

1. INTRODUCTION

Vanadium dioxide (VO$_2$), exhibiting a metal–insulator transition (MIT), has attracted attention as a promising material for oxide electronics. VO$_2$ has a monoclinic phase and is an insulator at room temperature, whereas it transforms to a metallic rutile phase at approximately 67 $^\circ$C.$^{1,2}$ The phase transition of VO$_2$ is reversible and dramatically changes the electrical conductivity and infrared transmittance.$^{2-6}$ Furthermore, the MIT of VO$_2$ can be induced by various stimuli such as electricity,$^{7-9}$ light,$^{10,11}$ and strain$^{12,13}$ in addition to heat. Hence, VO$_2$ has been studied for applications in nonvolatile memory,$^{14-16}$ smart windows,$^{17-21}$ flexible strain sensors,$^{12}$ optical temperature sensors,$^{22}$ and gas sensors.$^{23}$

One major research interest pertaining to VO$_2$ is to alter its MIT temperature. Various methods have been proposed to tune the MIT temperature. Doping has been reported to change the phase transition temperature of VO$_2$. Dopants like W, Mo, and Nb decrease the MIT temperature.$^{24-26}$ Conversely, dopants like Cr and Fe increase the MIT temperature.$^{27-29}$ Straining VO$_2$ thin films is also known to change its MIT temperature. For example, Breckenfeld et al. demonstrated that straining heterostructured VO$_2$/TiO$_2$ reduces its MIT temperature to $\sim$44 $^\circ$C.$^{30}$ Kim et al. reported that a 50 nm epitaxial VO$_2$ thin film grown on a sapphire substrate with a SnO$_2$ (001) buffer layer reduced the transition temperature to 52 $^\circ$C.$^{31}$ In addition, Muraoka and Hiroi studied the effect of uniaxial stress on the MIT of epitaxial VO$_2$ thin films grown on (001) and (110) TiO$_2$ substrates. As a result, they reported that the MIT temperature of VO$_2$ thin film grown on (001) TiO$_2$ decreases and that of VO$_2$ thin film grown on (110) TiO$_2$ increases.$^{32}$ Hong et al. investigated the in-plane strain directions using different orientations of VO$_2$ thin films on (001), (110), and (101) TiO$_2$ substrates and revealed that the MIT temperature depends on the strain state of the dimetric vanadium (V–V) atomic chain.$^{33}$ In particular, a compressive strain of V–V chains decreases MIT temperature, whereas a tensile strain increases MIT temperature.

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Epitaxial strain allows large MIT temperature modulation; however, the stress—strain relation is determined by the lattice mismatch with the substrate, and the stress cannot be altered after film formation. To alter the stress state (and consequently the MIT temperature), the deposited VO$_2$ could instead be deformed by bending and/or stretching. Cao et al. reported that the MIT temperature of VO$_2$ nanobeams could be altered by bending and stretching them. However, the difficulty of bending single nanostructures is a barrier to their use in device applications.

Although it is challenging to induce bending stress in nanostructures because of their small size, it is relatively simple to induce bending stress in thin films because of their larger size. Thus, by growing single-crystal VO$_2$ thin films on flexible substrates, it would be possible to change the MIT temperature by straining them. In this study, we focused on van der Waals epitaxy as a technique for attaching VO$_2$ thin films to flexible substrates on muscovite mica and synthetic mica. Mica is an inorganic two-dimensional (2D) material that can be thinned by mechanical cleavage. Although 2D materials have no dangling bonds at the cleavage surface, epitaxial thin films are grown by van der Waals epitaxy. Heteroepitaxial growth of various oxide thin films, such as VO$_2$, MoO$_3$, ZnO, NiO, In$_2$O$_3$, Al-doped ZnO (AZO), e-Fe$_2$O$_3$, and κ-Ga$_2$O$_3$ on muscovite mica and synthetic mica has been previously demonstrated. Furthermore, it has been shown that inducing bending stress in epitaxial thin films grown by van der Waals epitaxy changes the resistivity of ZnO and the magnetic anisotropy of e-Fe$_2$O$_3$.

Mist chemical vapor deposition (CVD) was utilized to grow epitaxial VO$_2$ thin films on flexible synthetic mica. In previous studies, we have demonstrated van der Waals epitaxy of various oxides, such as ZnO, NiO, In$_2$O$_3$, and κ-Ga$_2$O$_3$ by mist CVD. In addition, VO$_2$ thin films grown on rigid quartz substrates by mist CVD had high visible transmittance and exhibited large changes in the infrared transmittance with MIT. However, few reports exist on the epitaxial growth of VO$_2$ on flexible substrates using mist CVD. In this study, epitaxial VO$_2$ thin films were grown on flexible synthetic mica using van der Waals epitaxy via mist CVD and were then stressed by bending.

During the growth of VO$_2$ thin films, attention should be paid to the formation of V$_2$O$_3$, which is the most stable form of vanadium oxide. Furthermore, since the strain along the dimeric V–V atomic chain affects the MIT temperature, epitaxial growth is necessary to modulate the properties of VO$_2$ thin films by bending stress. Therefore, to obtain the VO$_2$ thin film with desired orientation, we inserted SnO$_2$ as a buffer layer. SnO$_2$ has the same rutile structure as the metallic phase of VO$_2$. SnO$_2$ has previously been utilized as a buffer layer for the epitaxial growth of VO$_2$. The epitaxial growth of highly crystalline SnO$_2$ thin films on sapphire substrates via mist CVD has also been reported. Hence, to grow epitaxial VO$_2$ thin films, we proposed to utilize SnO$_2$ buffer layers on synthetic mica. In this study, VO$_2$ thin films were grown on synthetic mica with and without SnO$_2$ buffer layers by mist CVD, and their electrical properties and MIT behavior were subsequently investigated. Furthermore, to clarify the effect of bending-induced in-plane tensile strain on the resistive switching temperature, the electrical characteristics of the VO$_2$ thin films were measured in the bent state.

## 2. RESULTS AND DISCUSSION

A (010) VO$_2$ layer was first grown on the synthetic mica substrate containing a (100) SnO$_2$ buffer layer. Figure 1a shows X-ray diffraction (XRD) 2θ–ω scan profiles of VO$_2$ thin films grown on synthetic mica substrates with and without SnO$_2$ buffer layers. For reference, the 2θ–ω scan profile of the synthetic mica substrate is depicted in Figure 1a. The diffraction peaks corresponding to the (011), (010), (100), and (210) planes of monoclinic VO$_2$ were observed when the SnO$_2$ buffer layer was absent. In addition to this, the diffraction peak of the (011) plane of tetragonal V$_2$O$_3$ was also observed. Thus, in the absence of a SnO$_2$ buffer layer, the deposited polycrystalline thin film consisted of a mixture of VO$_2$ and V$_2$O$_3$. On the other hand, diffraction peaks corresponding to the (010) plane of VO$_2$ and the (100) plane of SnO$_2$ were observed when the SnO$_2$ buffer layer was present, indicating that (010)-oriented monoclinic VO$_2$ was grown on the (100)-oriented SnO$_2$ buffer layer. To investigate the in-plane orientation of the VO$_2$ (010) thin film, we performed ϕ scanning of the VO$_2$ (210) reflection with the buffer layer, as...
shown in Figure 1b. Six diffraction peaks were observed at intervals of 60°, indicating that the VO₂ thin film exhibited a fixed in-plane orientation unlike a randomly oriented polycrystal. Thus, by inserting the SnO₂ buffer layer, epitaxial VO₂ thin film could be successfully grown on synthetic mica by mist CVD.

Next, we investigated impacts of the buffer layer and bending stress on the MIT characteristics of VO₂ thin films. Figure 2 shows the electrical resistance of VO₂ thin films grown without and with buffer layers as a function of temperature. First, we discuss the difference in MIT characteristics due to the presence of the buffer layer. The temperature dependence of the electrical resistance of VO₂ thin films without bending stress is indicated by the blue dots in Figure 2. The MIT temperatures calculated from the peaks of the derivative curves of the relationship between the sample temperature and the electrical resistance are also highlighted in Figure 2. The resistive switching derived from the MIT was observed in both VO₂ thin films with and without a buffer layer. The resistive change of MIT with the buffer layer was smaller than without the buffer layer. This is because the SnO₂ buffer layer has higher conductivity than the insulator phase of VO₂, resulting in lower resistance below the MIT temperature than without the buffer layer. On the other hand, although both thin films showed hysteresis during the cooling and heating processes, their MIT temperatures were different. The MIT temperatures of the VO₂ thin film without the buffer layer were 64.2 °C during heating and 61.8 °C during cooling, whereas those of the thin film with the buffer layer were 68.0 °C during heating and 60.8 °C during cooling. We believe that this difference may be due to smaller crystallites in the polycrystalline thin film and larger crystallites in the epitaxial thin film.

Now, we discuss the impact of bending stress on the MIT characteristics of VO₂ thin films. We utilized a brass rod with a radius of 10 mm to bend the thin films. The blue dots in Figure 2 correspond to the measured resistances of the bent films. A shift in the resistive switching temperature was more prominently observed in the epitaxial VO₂ thin film with the buffer layer than in the polycrystalline VO₂ thin film without the buffer layer. The shift due to bending was higher by 2.3 °C during heating and 1.8 °C during cooling. By stretching VO₂ nanonecms and applying epitaxial strain to VO₂ thin films, it has been reported that tensile strain along the a-axis increases the MIT temperature of monoclinic VO₂. On the other hand, as shown in Figure 1b, the epitaxial VO₂ (010) thin film grown on the synthetic mica formed three domains. By bending in one direction, the tensile strain can be applied to the a-axis direction of each VO₂ domain as long as it is not perpendicular to the bending direction. The strain effect is not canceled, and all domains stretched along the a-axis lead to an increase in the MIT temperature. Therefore, epitaxial VO₂ (010) thin films with three domains increased MIT temperature due to bending stress. Our result depicting a shift of the MIT temperature of the epitaxial VO₂ (010) thin film to a higher temperature by applying in-plane tensile strain through bending is consistent with these reports. Since the VO₂ thin film without the buffer layer was randomly oriented, the a-axis strain was not perfectly aligned along the bending direction, and the shift in MIT temperature derived from the strain was not significant. Thus, it was demonstrated that the MIT temperature of the epitaxial VO₂ thin film containing a SnO₂ buffer layer grown on a mica substrate could be altered by bending it.

We varied the amount of bending of the thin films to investigate the impact of bending stress on the MIT temperature. For a sample with thickness t bent at a radius of curvature R, the in-plane strain ε developed on the thin film surface is

$$\varepsilon = \frac{t}{2R}$$

Figure 3 shows the variation in the MIT temperature of the VO₂ thin film grown on synthetic mica with the buffer layer as a function of the in-plane tensile strain ε. Herein, the red and blue dots indicate the transition temperatures during heating and cooling, respectively. As the in-plane tensile strain increases, the MIT temperature of VO₂ gradually increases.

![Figure 2](https://pubs.acs.org/journal/acsodf41770)

**Figure 2.** Variation of the electrical resistance of VO₂ thin films grown (a) without and (b) with a buffer layer with temperature. The blue and red dots indicate the properties of the sample in unbent and bent states, respectively, at a radius of curvature of 10 mm. The values of the transition temperatures for each state are also highlighted. Schematics of measurements without and with bending are also shown.
For example, the application of an in-plane tensile strain of 0.077% increased the MIT temperature by 2.3 °C during heating and 1.8 °C during cooling. Moreover, the MIT temperature of the VO$_2$ thin film on the mica substrate was observed to vary linearly with the tensile strain. Assuming that such a linear relationship is valid even at larger strains, a 1% in-plane compressive strain can be expected to lower the MIT temperature by 32.7 °C during heating and 26.2 °C during cooling, allowing MIT to occur at room temperature.

To investigate the bending endurance, the epitaxial VO$_2$ thin film on the mica substrate was repeatedly bent, and the MIT temperature was measured in the unbent state. The bending tests were performed for $1 \times 10^4$ cycles with a radius of curvature of 10 mm. Figure 4a,b shows the MIT temperature of the epitaxial VO$_2$ thin film during heating and cooling and the electrical resistance at 40 °C (the insulating phase) and 80 °C (the metallic phase), respectively, in the unbent state after bending. After the bending test, the transition temperature was maintained during both heating and cooling cycles in the unbent state. Furthermore, the electrical resistance of the epitaxial VO$_2$ thin film remained more or less constant with bending cycles, as shown in Figure 4b. Figure 4c shows the temperature dependence of the electrical resistance of the epitaxial VO$_2$ thin film after $10^9$ bending cycles. Herein, the blue and red dots indicate the measurements performed without and with bending, respectively, at a radius of curvature of 10 mm. After $10^9$ bending cycles, the temperature-dependent MIT behavior without and with bending was mostly maintained. These results indicate that the epitaxial VO$_2$ thin film on synthetic mica exhibits high bending durability.

Raman scattering measurements were performed to investigate the effect of in-plane strain due to bending. We focused on the peak wavenumber at 607 cm$^{-1}$, corresponding to the V–O bond vibration, which has been reported to exhibit a continuously higher wavenumber shift due to tensile strain along the a-axis of monoclinic VO$_2$.

We analyzed the peak wavenumber shift of V–O phonons with in-plane tensile strain due to bending at different radii of curvature by measuring the Raman scattering. Figure 5a shows the Raman spectra in the range of 590–630 cm$^{-1}$ under various strains of the VO$_2$ thin film epitaxially grown on synthetic mica. Figure 5b shows the variation of the V–O phonon peak wavenumber and the in-plane tensile strain by bending. The V–O phonon with a peak at 607 cm$^{-1}$ in the unbent state was shifted to a higher wavenumber as the tensile strain of the thin film increased.
plane tensile strain due to bending. Raman measurements also indicate the V–O phonon peak in the unbent state. The dashed line indicates the V–O phonon peak in the unbent state. (b) Variation of the peak wavenumber of V–O phonons (607 cm$^{-1}$) without bending) with in-plane tensile strain due to bending.

Figure 5. (a) Raman spectra of the epitaxial VO$_2$ thin film grown on synthetic mica with a SnO$_2$ buffer layer in the unbent state. The peak wavenumber of the V–O phonon exhibited a shift of 0.8 cm$^{-1}$ due to an in-plane tensile strain of 0.077%. Thus, the stress induced by bending in the epitaxial VO$_2$ thin film caused the V–O phonon shift.

Atkin et al. reported shifts toward larger V–O phonons with tensile strains (0–2%) applied to the VO$_2$ microbeam, which is consistent with our observations. The peak wavenumber of the V–O phonon exhibited a shift of 0.8 cm$^{-1}$ due to an in-plane tensile strain of 0.077%. Thus, the stress induced by bending in the epitaxial VO$_2$ thin film caused the V–O phonon shift.

3. CONCLUSIONS

Epitaxial VO$_2$ thin films were grown on flexible synthetic mica with a SnO$_2$ buffer layer utilizing mist CVD. Focusing on the electrical properties of the VO$_2$ thin film, the resistive switching temperature associated with the MIT was modulated by bending stress. The polycrystalline VO$_2$ and V$_2$O$_3$ thin films grown without a SnO$_2$ buffer layer showed no modulation of the MIT temperature by bending. On the other hand, the epitaxial VO$_2$ thin film grown by inserting a SnO$_2$ buffer layer exhibited a shift in MIT temperature due to the tensile strain along the $a$-axis direction. Therefore, the effect of bending stress on VO$_2$ thin films grown on flexible synthetic mica can be altered with a SnO$_2$ buffer layer. The resistive switching temperature could be continuously modulated by varying the bending-induced in-plane tensile strain applied to the epitaxial VO$_2$ thin film. Even after $10^4$ bending cycles, the epitaxial VO$_2$ thin film exhibited MIT and a shift in resistive switching temperature due to the in-plane tensile strain, demonstrating excellent bending durability. Raman measurements also demonstrated that tensile strain applied to the VO$_2$ thin film with a SnO$_2$ buffer layer induced bending stress. These results are expected to promote further development of strain engineering for epitaxial VO$_2$ thin films and their application to flexible switching devices.

4. METHODS

The epitaxial growth of VO$_2$ thin films and the insertion of a SnO$_2$ buffer layer by mist CVD were demonstrated using cleaved flexible synthetic mica as a substrate. The synthetic mica substrate surface obtained by cleavage was fresh and did not require cleaning to remove contamination. Sn(IV) chloride pentahydrate (SnCl$_4$·5H$_2$O) was utilized as the Sn precursor and dissolved in a mixture of de-ionized water and hydrochloric acid (HCl). Vanadyl acetylacetonate (VO($\text{C}_5\text{H}_7\text{O}_2$)$_2$) was utilized as the V precursor and dissolved in de-ionized water. The concentrations of the Sn and V precursors were fixed at 0.5 and 0.03 M, respectively. The precursor solution was atomized by ultrasonic transducers (2.4 MHz) and transported by nitrogen (N$_2$) gas at a flow rate of 6.5 L/min during the growth of the SnO$_2$ buffer layer. During the growth of VO$_2$ thin films, the mist was transported by introducing oxygen (O$_2$) gas at a flow rate of 0.1 L/min and N$_2$ gas at a flow rate of 7.9 L/min. The respective growth temperature and time were 475 °C and 0.5 min for the SnO$_2$ buffer layer and 500 °C and 60 min for the VO$_2$ thin films.

The structural characterization of VO$_2$ thin films grown on synthetic mica with and without a SnO$_2$ buffer layer was performed by XRD (Bruker, D8 Discover) analysis using Cu K$_\alpha$ radiation as the X-ray source. The crystal structure and out-of-plane orientation were analyzed by XRD 2θ–ω scans, and the in-plane structure was characterized by a φ-scan. The resistive switching associated with the MIT of VO$_2$ thin films was demonstrated by two-terminal measurements, while measuring the sample temperature using K-type thermocouples. Ti/Au ohmic contacts were deposited on the thin film surface for electrical measurements using electron beam evaporation (ULVAC, CV-200). In addition, to analyze the resistance change characteristics of the bent film owing to MIT, electrical measurements were obtained by attaching samples to brass rods of different radii ($R = 10, 25, 50$, and $100$ mm) using polymide tape. The thickness of each layer required for strain estimation of the epitaxial VO$_2$ thin film was measured using a micrometer (Mitutoyo MDH-25MB) and a scanning electron microscope (SEM, Hitachi S-5200). The thickness values of the thin film with the buffer layer and the synthetic mica substrate were 440 nm and 15 μm, respectively. The bending endurance of the flexible VO$_2$ thin films was investigated by attaching the sample to an automated stage with a jig and evaluating its MIT behavior after repeated bending. The maximum number of bending cycles was $10^2$. A laser Raman spectrophotometer (Nihon Spectroscopy, NRS-S100) was used to obtain the Raman spectra of the unbent and bent VO$_2$ epitaxial thin films. The excitation laser wavelength was 532 nm, and the output power was 0.6 mW.

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Notes
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