Probing Solar Convection

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ABSTRACT

In the solar convection zone acoustic waves are scattered by turbulent sound speed fluctuations. In this paper the scattering of waves by convective cells is treated using Rytov’s technique. Particular care is taken to include diffraction effects which are important especially for high-degree modes that are confined to the surface layers of the Sun. The scattering leads to damping of the waves and causes a phase shift. Damping manifests itself in the width of the spectral peak of p-mode eigenfrequencies. The contribution of scattering to the line widths is estimated and the sensitivity of the results on the assumed spectrum of the turbulence is studied. Finally the theoretical predictions are compared with recently measured line widths of high-degree modes.

Key words: convection, turbulence, waves, Sun: oscillations.

1 INTRODUCTION

In the solar convection zone thermal instabilities give rise to turbulent convection as the predominant heat transport mechanism. Turbulence is one of the unsolved puzzles of modern physics, and the lack of a fundamental theory of turbulence requires a variety of phenomenological models. This constitutes a serious limitation to the predictiveness of many astrophysical models and very often leads to a built-in uncertainty (Canuto & Christensen-Dalsgaard 1996). Theoretical modelling of convection in the Sun is extremely difficult. Solar convection is highly turbulent and occurs on a vast range of scales. The material is compressible and magnetic fields can play an important role. Consequently, various parametrizations have been invented to describe the properties of the convection. At the same time vast efforts
are being undertaken to numerically simulate solar convection. These simulations are still at an early stage and their results are not yet conclusive. One of the prime motivations for studying solar and stellar structure in great detail is to improve and test these models of convection.

Statistically significant differences between the observed and theoretically predicted eigenfrequencies of the Sun persist (Gough et al. 1996). The differences between computed adiabatic eigenfrequencies of the standard solar model and measured p-mode frequencies for any given order $n$ increase with frequency when scaled with the mode inertia (with the model frequencies being bigger). Higher frequencies of modes of a given radial order correspond to greater values of the spherical degree $l$, and hence to modes that remain increasingly confined to the surface layers of the Sun. This suggests that the cause for the discrepancy between theory and observation lies in an inadequate modelling of the surface layer of the Sun. It is this surface layer where convection is important and constitutes the greatest uncertainty in the model.

Helioseismic inferences are not reliable unless details of stellar structure and wave propagation within the acoustic cavity are correctly treated. It has been noted elsewhere (Canuto & Christensen-Dalsgaard 1996) that the errors in the computed frequencies caused by uncertainties in the equation of state (EOS) are large compared to the observational errors. The variation in the average wave propagation properties inside the Sun caused by turbulent convection and temperature fluctuations constitute yet another process that will affect the eigenfrequencies. This influence is difficult to assess and has not received as much attention as the errors introduced by uncertainties in the EOS or the opacity. Since helioseismic inferences are dependent on the detailed treatment of turbulence, the Sun could serve as a laboratory to study turbulence under conditions unattainable on Earth.

Turbulence enters the theory of solar oscillations in two places: it changes the model of solar structure mainly through the turbulent pressure that provides additional support against gravity, and secondly it interacts with the waves themselves. The waves interact with the turbulence via two mechanism: The turbulent velocity advects the acoustic waves (Brown 1984; Swisdak & Zweibel 1998) and the temperature fluctuations cause fluctuations
in the refractive index and thus in the local phase speed of the waves.

The good quality of solar oscillation data does not only allow an accurate determination of the eigenfrequencies but also contains detailed information such as the width of the spectral peak.

The observed line width of acoustic modes is caused by absorption and other non-adiabatic effects (e.g., Gough 1980; Goldreich & Kumar 1991; Bahmforth 1992), as well as by scattering by turbulent velocity fluctuations in the solar convection zone.

The scattering contribution to the line width has been studied by Goldreich & Murray (1994) in the framework of normal modes. Using a simple model of scattering of standing waves in a box and within the strict limits of geometrical acoustics, they derived a scattering width for radial modes of \( \Gamma_s \simeq \omega M^2 / \pi (n + 1) \), where \( \omega \) is the angular frequency of the mode, \( M = u/c \) is the Mach number of the turbulent velocity and \( n \) the order of the mode. However, geometrical acoustics is a poor approximation for non-radial high-degree modes, because at the top of the acoustic cavity the correlation length of the perturbations becomes comparable to the wavelength of the waves.

In this paper the scattering contribution to the line width is calculated, explicitly taking diffractive effects into account. Recently measured line widths of high-degree modes are compared with results of this calculation. Thus, one of the aims of this study is to investigate to what extent the structure of solar convection can be probed by seismic methods. For this purpose a formalism to describe the propagation of waves through random fluctuating media is introduced. For the sake of clarity I start by deriving the formalism for a homogeneous medium before generalising it to inhomogeneous media in Sec. 2.2.

## 2 WAVE PROPAGATION THROUGH FLUCTUATING MEDIA

Let us write down a wave equation with a scattering term on the rhs:

\[
\hat{L}\psi = (\nabla^2 + k^2)\psi = \epsilon V(\mathbf{r})\psi,
\]  

(1)

where \( V \) is sometimes called the ‘scattering potential’. For a homogeneous medium \( \epsilon V(\mathbf{r}) = 2k^2 \delta c(\mathbf{r})/c(\mathbf{r}) \), where \( \delta c \) is the rms of the sound speed perturbation. As the scattering is assumed to be weak, \( \epsilon \) is a small number. Thus one can solve equation (1) perturbatively.
An approximate solution can be written in terms of a Born expansion (e.g. Nayfeh, 1973) by writing

\[ \psi = \sum_{m=0}^{\infty} \epsilon^m \psi_m. \]  

(2)

Substituting into equation (1) yields

\[ (\nabla^2 + k^2)(\psi_0 + \epsilon \psi_1 + ...) = \epsilon V(\mathbf{r})(\psi_0 + \epsilon \psi_1 + ...). \]  

(3)

Equating equal powers of \( \epsilon \) yields for \( m = 0 \):

\[ \hat{L} \psi_0 = 0 \]  

(4)

and recursively for \( m > 0 \)

\[ \hat{L} \psi_m = V(\mathbf{r}) \psi_{m-1}. \]  

(5)

Equations (4) and (5) can be solved successively using Green’s function

\[ \psi_m(\mathbf{r}) = \int d^3 \mathbf{r}_1 V(\mathbf{r}_1) \psi_{m-1}(\mathbf{r}_1) G(\mathbf{r}; \mathbf{r}_1), \]  

(6)

where the Green function, \( G \), is defined by

\[ (\nabla^2 + k^2)G(\mathbf{r}; \mathbf{r}_1) = \delta^3(\mathbf{r} - \mathbf{r}_1). \]  

(7)

For a homogeneous medium \( G(\mathbf{r}; \mathbf{r}_1) = \exp(ik|\mathbf{r} - \mathbf{r}_1|)/4\pi|\mathbf{r} - \mathbf{r}_1|. \) From equation (8) one can write

\[ \psi_1(\mathbf{r}) = \int d^3 \mathbf{r}_1 V(\mathbf{r}_1) G(\mathbf{r}; \mathbf{r}_1) \psi_0(\mathbf{r}_1). \]  

(8)

and successively

\[ \psi_m(\mathbf{r}) = \int d^3 \mathbf{r}_1 \cdots \int d^3 \mathbf{r}_m V(\mathbf{r}_1) \cdots V(\mathbf{r}_m) G(\mathbf{r}; \mathbf{r}_1) \cdots G(\mathbf{r}; \mathbf{r}_m) \psi_0(\mathbf{r}_1). \]  

(9)

An alternative and possibly more intuitive technique to calculate phase and amplitude fluctuations, known as Rytov’s method, starts by recasting the wavefield into an exponential (see, e.g., Ishimaru 1978):
\[ \psi(\mathbf{r}) = e^{\Psi(\mathbf{r})}. \]  

Hence one can write

\[ \nabla^2 \psi = \psi \left[ \nabla \Psi \cdot \nabla \Psi + \nabla^2 \Psi \right], \]  

and equation (10) becomes

\[ \nabla^2 \Psi + \nabla \Psi \cdot \nabla \Psi + k^2 - \epsilon V = 0, \]  

which is a nonlinear first-order differential equation known as Riccati’s equation. Denoting \( \Psi_0 := \Psi \) in the absence of fluctuations, i.e. when \( V = 0 \), and writing \( \Psi = \Psi_0 + \Psi_1 \), one obtains

\[ \nabla^2 \Psi_1 + 2 \nabla \Psi_0 \cdot \nabla \Psi_1 = -[\nabla \Psi_1 \cdot \nabla \Psi_1 - \epsilon V]. \]  

With the identity

\[ \nabla^2 (\psi_0 \Psi_1) = (\nabla^2 \psi_0) \Psi_1 + 2 \psi_0 \nabla \Psi_0 \nabla \Psi_1 + \psi_0 \nabla^2 \Psi_1, \]  

one obtains the following inhomogeneous equation for \( \psi_0 \Psi_1 \)

\[ (\nabla^2 + k^2)(\psi_0 \Psi_1) = [\nabla \Psi_1 \cdot \nabla \Psi_1 - \epsilon V]\psi_0, \]  

which can be solved using Green’s function, yielding

\[ \Psi_1(\mathbf{r}) \simeq \frac{1}{\psi_0(\mathbf{r})} \int G(\mathbf{r} - \mathbf{r}') [\nabla \Psi_1 \cdot \nabla \Psi_1 - \epsilon V]\psi_0(\mathbf{r}') d^3\mathbf{r}'. \]  

To first order, \( \Psi_1 = 0 \) in the integrand, so that

\[ \Psi_1(\mathbf{r}) \simeq -\frac{1}{\psi_0(\mathbf{r})} \int \epsilon V G(\mathbf{r} - \mathbf{r}') \psi_0(\mathbf{r}') d^3\mathbf{r}'. \]  

Thus the first Rylov solution is given by

\[ \psi(\mathbf{r}) = \psi_0(\mathbf{r}) e^{\Psi_1(\mathbf{r})}. \]  

It has been shown that the first term in the Rylov expansion is superior to the first Born approximation (Keller 1969), and I shall employ Rylov’s technique in the following analysis. The two methods discussed above, the Born series and Rylov’s technique, are the most commonly used techniques dealing with scalar wave propagation through random media. More recently, Samelsohn & Mazar (1996) have treated this problem using a path-integral
analysis on the basis of the parabolic wave equation. For a detailed review of stochastic wave propagation and scattering in random media, see, e.g. Ishimaru (1978) and Klyatskin (1980).

Here it will be assumed that the sound speed fluctuations, and consequently the $\Psi_1$ fluctuations are Gaussian with zero mean, i.e. $\langle \Psi_1 \rangle = 0$, where the brackets denote the mean over time. The mean of equation (18) has the form of a characteristic function and one can write

$$\langle e^{\Psi_1} \rangle = e^{\frac{1}{2} \langle \Psi_1^2 \rangle},$$

where $\langle \Psi_1^2 \rangle$ is the correlation function defined in equation (24) (see Munk & Zachariasen 1976, Panchev 1971).

Whenever waves interact with obstacles or inhomogeneities in the medium, diffraction effects may occur. Most problems in diffraction theory cannot be solved exactly, so that a number of techniques have been invented to find approximate solutions. One of these techniques is Huygen’s principle, which states that every point of a wave front can be considered as a source of secondary wavelets which mutually interfere. The application of this principle to diffraction problems leads to the Fresnel zone construction. The textbook example for the application of Fresnel zones is the problem of diffraction by a small aperture in an infinite screen as sketched in Fig. 1. A wave propagates from a point source at point S through an opening in an opaque screen to point R. According to Huygen’s principle the total disturbance at R due to a source at point S is given by the integral over the aperture

$$\psi(R) = \int \frac{e^{ik(r+s)}}{r+s} dS,$$

where $s = SP$ and $r = PR$. In equation (20) I have neglected a so-called obliquity factor, which describes the angular variation of the secondary wavelets. Rays that connect S and R via a point P in the plane now have a phase at R that is different from the phase of the stationary ray.

The envelopes of all the rays of length $a + b + \lambda/2, a + b + \lambda, ..., a + b + j\lambda/2$, divide the aperture into a number of zones, which are called Fresnel zones ($a$ and $b$ are defined in Fig. 1, $\lambda$ is the wavelength and $j$ an integer). The contributions from successive Fresnel zones to the total wavefield alternate in sign. Those rays whose phase differs from the stationary phase by $\pi$ form the boundary of the first Fresnel zone in the plane of the obstacle. In our
Generally, the first Fresnel zone in a plane intersecting the raypath is defined as the area bounded by all those rays whose phase differs by $\pi$ from the phase of the stationary ray which joins two fixed points. This can now be repeated for all planes intersecting the ray path and the entirety of these zones yields a tube surrounding the stationary ray path: this tube I call the Fresnel tube. The Fresnel zone provides an estimate of the size of an irregularity that would give rise to diffraction effects. If the size of the irregularity is much bigger than the Fresnel zone, diffraction effects are negligible. It is straightforward to calculate the Fresnel zone for waves in a homogeneous medium. Let me consider a wave propagating from S to R as before. If the wave now follows the path SPR instead of the stationary ray, the corresponding change in phase, $\phi$, is given by

$$
\delta \phi = k[(a^2 + \delta z^2)^{1/2} + (b^2 + \delta z^2)^{1/2} - (a + b)] \approx \frac{k(a + b)}{2ab} \delta z^2, \tag{21}
$$

where $k$ denotes $2\pi/\lambda$. Hence the size of the Fresnel zone is given by

$$
\sqrt{2\pi} \left( \frac{\partial^2 \phi}{\partial z^2} \right)^{-1/2} = \left[ \frac{2\pi ab}{k(a + b)} \right]^{1/2}. \tag{22}
$$

### 2.1 Homogeneous medium

I begin by considering the case of wave propagation in a fluctuating homogeneous medium. In this case the ray paths are straight lines and the turbulent correlation function is a function of separation only, i.e.

$$
\epsilon^2 \langle V(r_1)V(r_2) \rangle = \zeta(r_1 - r_2). \tag{23}
$$

As stated in equations (18) and (19) the time-averaged wavefield at $r$ due to a source at the origin is given by the unperturbed wavefield times $\exp\left(\frac{1}{2}\langle \Psi_1^2 \rangle\right)$, where

$$
\langle \Psi_1^2 \rangle = (16\pi^2)^{-1} \int d^3r_1 \int d^3r_2 \frac{r^2}{|r - r_1| |r_2 - r|} \zeta(r_1 - r_2)
\times \exp[ik(r_1 + |r - r_1| - r)] \exp[ik(r_2 + |r - r_2| - r)]. \tag{24}
$$

It is convenient to convert to relative and centre-of-mass coordinates:
\[ \mathbf{\tilde{r}} = \mathbf{r}_1 - \mathbf{r}_2 \]  

(25) and

\[ \mathbf{R} = \frac{1}{2}(\mathbf{r}_1 + \mathbf{r}_2). \]  

(26)

I assume that \( \zeta \) is negligible when \( \tilde{r} \) is bigger than the correlation length of the sound speed perturbations, which are taken to be smaller than \( R \). Then one can expand the integrand in (24) in \( \tilde{r}/R \) yielding

\[
\langle \Psi_1^2 \rangle = \frac{1}{16\pi^2} \int \frac{d^3\mathbf{R}}{R^2|\mathbf{r} - \mathbf{R}|^2} \exp[2ik(R + |\mathbf{r} - \mathbf{R}| - r)] 
\int d^3\tilde{\mathbf{r}} \zeta(\tilde{\mathbf{r}}) \exp \left[ \frac{ik}{4} \left( \frac{\tilde{\mathbf{r}}^2 - (\tilde{\mathbf{r}} \cdot \mathbf{R})^2}{R} + \frac{\tilde{\mathbf{r}}^2 - [\tilde{\mathbf{r}} \cdot (\tilde{\mathbf{r}} - \mathbf{R})]^2}{|\mathbf{r} - \mathbf{R}|} \right) \right],
\]  

(27)

where the hat denotes a unit vector. Assuming that the radius of the Fresnel zone is smaller than \( s \), i.e. \( (r - s)/kr_s \ll 1 \), one can expand equation (27) in \( R_\perp/R_\parallel \) about its stationary path, which is the straight line from 0 to \( r \). Here \( s \) stands for \( R_\parallel \). The subscripts \( \perp \) and \( \parallel \) denote the vector components perpendicular and parallel to \( \mathbf{r} \). Thus one can write

\[ R + |\mathbf{r} - \mathbf{R}| - r \simeq \frac{R_\perp^2 r}{2s(r - s)}. \]  

(28)

Moreover,

\[ \frac{\tilde{\mathbf{r}}^2 - (\tilde{\mathbf{r}} \cdot \mathbf{R})^2}{R} \simeq \frac{\tilde{\mathbf{r}}^2}{s} + O \left( \frac{\tilde{\mathbf{r}}^2 R_\perp}{s^2} \right) \]  

(29)

and

\[ \frac{\tilde{\mathbf{r}}^2 - [\tilde{\mathbf{r}} \cdot (\tilde{\mathbf{r}} - \mathbf{R})]^2}{|\mathbf{r} - \mathbf{R}|} \simeq \frac{\tilde{\mathbf{r}}^2}{r - s} + O \left( \frac{\tilde{\mathbf{r}}^2 R_\perp}{s^2} \right). \]  

(30)

Substituting (28) into (27) and evaluating the integral over \( R_\perp \) by stationary phase, one finds that

\[
\int \frac{d^3\mathbf{R}}{R^2|\mathbf{r} - \mathbf{R}|^2} \exp[2ik(R + |\mathbf{r} - \mathbf{R}| - r)] \simeq \frac{i\pi}{k} \int_0^r \frac{r}{s(r - s)} ds.
\]  

(31)

Neglecting terms of order \( \tilde{r}^2 R_\perp/s^2 \) in equation (27) one is left with the integral over \( \tilde{\mathbf{r}} \) which after substitution of (29) and (30) becomes
\[
\langle \Psi_1^2 \rangle \simeq \frac{i}{16\pi k} \int_0^r ds \int d^3 \tilde{r} \frac{r}{s(r-s)} \times \exp \left[ \frac{ik}{4} \left( \frac{1}{s} + \frac{1}{r-s} \right) \tilde{r}_\perp^2 \right]. \tag{32}
\]

It is convenient to use the Fourier transform of the correlation function, which is defined as

\[
\tilde{\zeta}(\mathbf{q}) = \int \zeta(\tilde{\mathbf{r}}) e^{i\mathbf{q} \cdot \tilde{\mathbf{r}}} \, d^3 \tilde{\mathbf{r}}. \tag{33}
\]

Substituting the inverse transform into equation (32), using the relation

\[
\int \zeta(\tilde{r}_\parallel, 0) d\tilde{r}_\parallel = (2\pi)^{-2} \int \tilde{\zeta}(0, \mathbf{q}_\perp) d^2 \mathbf{q}_\perp, \tag{34}
\]

and integrating over \( d^2 \mathbf{r}_\perp \) by stationary phase, one obtains:

\[
\langle \Psi_1^2 \rangle \simeq -\frac{1}{(4\pi)^2 k^2} \int d^2 \mathbf{q}_\perp \tilde{\zeta}(0, \mathbf{q}_\perp) \int_0^r ds \ \exp \left[ \frac{iq_\perp^2 (s-r)s}{kr} \right]. \tag{35}
\]

The reader will recognise that the argument in the exponential in equation (35) is essentially the ratio of the size of the Fresnel zone to the correlation length of the fluctuations. The exponential takes account of the diffraction effects; its argument vanishes if the size of the inhomogeneities is much bigger than the Fresnel zone. The geometrical acoustics result is recovered by expanding the exponential in the previous equation. This is valid only if

\[
q_\perp^2 (s-r)s/kr \ll 1, \tag{36}
\]

which is the well-known Fresnel condition. Then the integral in (35) is simply

\[
\langle \Psi_1^2 \rangle \simeq -(2k)^{-2} r \int_0^r \zeta(r') \, dr', \tag{37}
\]

which is the geometrical acoustics result, and, unlike (35), does not account for diffraction.

Here, for simplicity, I confine myself to isotropic turbulence so that the three-dimensional Fourier transform becomes

\[
\tilde{\zeta}(q) = \frac{4\pi}{q} \int_0^\infty \zeta(r) r \sin qr \, dr. \tag{38}
\]

This now completes the description of the propagation of waves through a homogeneous turbulent medium, the main result being equation (32). This subsection serves to illustrate the evaluation of equation (18), which is most clearly demonstrated in a homogeneous medium. The Sun is, of course, inhomogeneous; hence in the following subsection I will generalise this
formalism to inhomogeneous media following the same principles and methods that were outlined above.

### 2.2 Inhomogeneous medium

For an inhomogeneous medium the correlation function $\zeta$ is a function of position as well as relative separation, i.e. $\zeta = \zeta(\tilde{r}, R)$. Furthermore, in an inhomogeneous medium the amplitude is no longer simply proportional to the inverse of the distance from the source, as for spherical waves in a homogeneous medium. In general, one can write the Green function as follows:

$$G(r, r_1) = A(r, r_1) \exp[iS(r, r_1)],$$

where the phase is given by

$$S(r, r_1) = \int_{r}^{R_1} k[r(s)] \cdot ds.$$  \hspace{1cm} (40)

It was shown by Munk & Zachariasen (1976), for example, that the ‘normalisation’ can be expressed as

$$A(r, R) = \frac{1}{4\pi} \left[ \det \frac{\partial}{\partial r_{\perp i}} \frac{\partial}{\partial R_{\perp j}} S(r, R) \right]^{1/2},$$

where the derivatives are evaluated at $r_{\perp} = R_{\perp} = 0$. Now, the exponent $\langle \Psi_1^2 \rangle$ reads

$$\langle \Psi_1^2 \rangle = \int d^3R \left[ \frac{A(r, R)A(R, 0)}{A(r, 0)} \right]^2 \int d^3\tilde{r} \zeta(\tilde{r}, R) \exp[i(S(r, R + \tilde{r}/2) + S(r, R - \tilde{r}/2) + S(R + \tilde{r}/2, 0) + S(R - \tilde{r}/2, 0) - 2S(r, 0))].$$

Expanding the exponent in powers of $\tilde{r}$, the linear terms vanish, so that one is left with the zero- and second-order term in $\tilde{r}$. Thus one can write

$$\langle \Psi_1^2 \rangle \simeq \int d^3R \left( \frac{A(r, R)A(R, 0)}{A(r, 0)} \right)^2 \exp[2i(S(r, R) + S(R, 0)) - S(r, 0))] \int d^3\tilde{r} \zeta(\tilde{r}, R) \exp[\frac{1}{2}i\tilde{r}_i\tilde{r}_jC_{ij}(R)],$$

where $C_{ij}$ denotes the ‘phase curvature’ defined as

$$C_{ij}(R) = \frac{\partial}{\partial R_i} \frac{\partial}{\partial R_j} [S(r, R) + S(R, 0)].$$

\hspace{1cm} (44)
The argument of the exponential in (43) is summed over the indices $i$ and $j$, each of which can take the values 1, 2 and 3. The phase curvature, $C_{ij}$, can be visualised as follows: Imagine displacing a ray which leads from 0 to $R$ and from $R$ onwards to $r$ by a small amount $\delta R$ so that the perturbed ray consists of a segment from 0 to $R + \delta R$ and a segment from $R + \delta R$ to $r$. The second derivative of the phase measured at $r$ due to a source at the origin with respect to perpendicular displacements at a point $R$ is called phase curvature. Since the ray follows a path of stationary phase, one finds that $C_{ij} = 0$ if $i \neq j$. Moreover, one can choose coordinates relative to the stationary ray from 0 to $r$ such that the only non-zero components of $C$ are the second derivatives in two perpendicular directions to the stationary ray at any point. The phase curvature is closely related to the concept of Fresnel zones and will be discussed further in Sec.[3].

Evaluating the integral over $d^3R$ by the method of stationary phase, selects the unperturbed path from 0 to $r$ as in the homogeneous case. The integral over $d^3\tilde{r}$ can again be simplified by introducing the Fourier transform of $\zeta$:

$$\langle \Psi_1^2 \rangle \simeq -\int_0^r ds \left[ \frac{A(r, R(s))A(R(s), 0)}{A(r, 0)} \right]^2 C_{11}^{-1/2}C_{22}^{-1/2} \int d^2q_{\perp}(s) \tilde{\zeta}[q_{\perp}(s), R(s)] \exp[iq_{\perp}^2 C_{jj}^{-1}(R(s))],$$

(45)

where the argument of the exponential is summed over $j$ ($j = 1, 2$). It is found that it is an excellent approximation, instead of using the normalisation of the Green function as given by equation (41), to simply write $A(r, R) = (4\pi|r - R|)^{-1}$, as in the homogeneous case. The deviations from homogeneity become only important in the phase. It is verified numerically (by using the correct Green function for a polytropic envelope, see Fan et al. 1995) that equation (45) can approximately be written as

$$\langle \Psi_1^2 \rangle \simeq -(4\pi)^{-2} \int_0^r ds k(s)^{-2} \int d^2q_{\perp}(s) \tilde{\zeta}[q_{\perp}(s), R(s)] \times \exp[iq_{\perp}^2 C_{jj}^{-1}(R(s))],$$

(46)

which is the expression that one would obtain using the amplitudes of the Green function for a homogeneous medium. Again equation (46) is much more accurate than the corresponding expression in the geometrical limit, which is given by
\[ \langle \Psi_1^2 \rangle \simeq - \int_0^r ds \ [2k(s)]^{-2} \int d\tilde{r}_\parallel \ \zeta(\tilde{r}_\parallel, s). \]  

Equation (45) is the most important equation of this paper. Within the assumptions made in its derivation, it describes the interaction of waves with the turbulent medium. My aim is now to evaluate (45) for acoustic waves in the Sun. In the following sections I will seek expressions for the various ingredients of (45), such as the scattering potential, the phase curvature and the correlation of the turbulence.

3 AN INHOMOGENEOUS WAVE EQUATION

First I derive the wave equation for solar acoustic oscillations in the presence of turbulence. This involves dividing the physical quantities into statistical averages and random fluctuations. The averages determine the mean properties of the envelope, whereas the fluctuations describe the turbulent convection and form the inhomogeneous term in the wave equation. For a sketch of the derivation of the linearized adiabatic wave equation in the absence of turbulence the reader is referred to the appendix.

Assuming that the Mach number of the turbulent flow is small, one can linearize in the perturbed variables. For simplicity I neglect the advection of the waves by the turbulent velocity and solely consider the effect of the perturbations in the sound speed. The perturbed quantities are denoted by a prime. As usual, \( c \) denotes local sound speed, \( \rho \) matter density and \( p \) pressure. Thus equation (A6) becomes

\[ (c + c')^2 \frac{D\rho}{Dt} = \frac{Dp}{Dt}, \]  

with equations (A1) and (A5) unchanged. Now I repeat the steps outlined in the appendix to eliminate \( p' \) and \( \rho' \) to find an equation for the scalar \( \chi := \text{div}\xi \), where \( \xi \) denotes the displacement of the fluid. Hence, in the presence of sound speed perturbations to first order in \( c' \), equation (A8) becomes

\[ \frac{\partial^2 \chi}{\partial t^2} = \nabla^2 (c^2 \chi - g_\theta \xi \cdot n) - \nabla (\Gamma \chi) \cdot n + \nabla^2 (2c' \chi) - \nabla (H^{-1} c' \chi) \cdot n \]  

Again making the substitution \( c^2 \chi = \rho^{-1/2} \psi \), and neglecting the buoyancy frequency, one obtains
\[ c^2 \left( \frac{\partial^2}{\partial t^2} + \omega_c^2 \right) \psi - \nabla^2 \psi = \nabla^2 \psi \ 2\delta c + 4(n \cdot \nabla \delta c)(n \cdot \nabla \psi) \]
\[ + (2\nabla^2(\delta c) - 2\delta c \omega_c^2/c^2)\psi, \quad (50) \]

where \( \delta c \) is the fractional sound speed fluctuation \( c'/c \). On the lhs I have written the familiar wave equation, modified by the cut-off frequency, \( \omega_c \), in the absence of sound speed perturbations, and on the rhs I have written all the scattering terms proportional to the perturbation \( \delta c \). On the rhs I can now substitute the unperturbed values for the spatial derivatives of \( \psi \) by treating the waves as locally plane, i.e. \( \nabla^2 \psi = -k^2 \psi = -\psi(\omega^2 - \omega_c^2)/c^2 \) and \( n \cdot \nabla \psi = ik_z \psi \). This brings the wave equation into the form of equation (1) with a rhs of the form \( \epsilon V(r) \psi \).

The treatment of the waves as locally plane is based on a wave-like decomposition of the normal modes. In this approximation the modes are represented as standing waves which in turn are formed by mutually interfering inward and outward propagating waves. Strictly speaking, this approximation is only valid when the order of the mode is large and many wavelengths fit in any scale height of the background medium. In practice, however, it turns out that this is a good approximation even for moderate order. For further reference see the appendix of this paper and Gough (1993).

Before proceeding to apply this formalism to the propagation of acoustic waves in the solar convection zone, I should recapitulate the assumptions made in this section: Plane-parallel geometry was assumed; as the rays that are most affected by convection are those confined to the surface layers of the Sun, they will feel the curvature of the Sun only as a small perturbation. Hence this assumption is fairly accurate. As customary, the gravitational acceleration is treated as a constant and the buoyancy frequency, \( N \), is ignored. Furthermore, perturbations in the gravitational acceleration \( g \) were neglected ("Cowling"-approximation). For linearization to be valid, the sound speed fluctuations and the Mach number of the turbulent flow are assumed to be small. Here, I only considered the scattering by the sound speed perturbations, i.e. by the perturbations in the refractive index. For a complete treatment of the interaction of waves with the turbulence one would also have to include those terms that arise from the advection by the turbulent velocity. Finally, for simplicity, I ignore the spatial derivatives of the pressure scale height \( H \) in the expression of the cut-off frequency and simply write it as \( \omega_c = c/2H \).
4 FRESNEL TUBES

In this section the phase curvature, which was introduced in Sec. 2, is calculated. At each point P on the wave path one can calculate how the phase of the wave due to a source at a fixed point Q varies when the raypath is slightly displaced from its stationary path. The first derivative of the phase with respect to small displacements of the ray path is zero, as expected by Fermat’s theorem. The second derivative, also called ‘phase curvature’, is defined in equation (44). It is inversely proportional to the square of the linear extent of the Fresnel zone which was introduced in Sec. 2.

Now, one can calculate the Fresnel tube for sound waves in the Sun. For simplicity one may assume that the solar envelope can be described by a plane-parallel polytrope. Then \( c^2 = c_0^2 z \) is linear with depth and \( c_0 \) is a constant. Indeed it is found that a polytrope of index \( \mu \simeq 3 \) yields a good fit to the observed frequencies. I should remark that this is not globally a good fit to the envelope, which is closer to a polytrope with \( \mu = 3/2 \), but rather a consequence of the fact that the frequencies are dominated by the uppermost layers of the Sun. The ray equations for a plane-parallel polytrope can easily be solved and I briefly quote the results here. If \( x \) denotes the horizontal coordinate and \( z \) depth below the surface, a ray that originates at the origin \( (x = z = 0) \) and propagates in the positive \( x \)-direction satisfies

\[
x = a \left[ \sin^{-1}(z/a)^{1/2} - (z/a)^{1/2} (1 - z/a)^{1/2} \right], \tag{51}
\]

where \( a \) is the depth of the lower turning point, \( a = \omega^2/c_0^2 k_x^2 \), where \( \omega \) is the angular frequency of oscillation and \( k_x \) is the horizontal wavenumber and a constant. The phase is given by

\[
\phi = 2 \omega a^{1/2} c_0^{-1} \sin^{-1}(z/a)^{1/2}. \tag{52}
\]

So for the full arc between two photospheric reflections the ray has traversed a horizontal distance \( x = \pi a \) and acquired a phase \( \phi = 2 \omega (\pi x)^{1/2}/c_0 \). In order to find the phase curvature at any given point along the ray, one perturbs the ray at \( x = x_0 \), while keeping the endpoints of the ray fixed. The second derivative of the total phase with respect to this displacement of the ray is the phase curvature as introduced in Sec. 2. The vertical extent of the first Fresnel zone is given by \( \sqrt{2\pi(\partial^2 \phi/\partial z^2)^{-1/2}} \). In Fig. 3 the extent of the first Fresnel zone in the direction perpendicular to the ray is shown as a function of depth for a ray with \( a = 0.001 R_\odot \). The Fresnel zone increases with depth until approximately 2/3 of the depth.
of the lower turning point from whereon it shrinks again to a smaller value at the lower turning point (see also Jenson et al. 1998).

However, it should be noted that the lower turning point is a caustic of the ray where the asymptotic ray theory breaks down. Nevertheless, this does not considerably affect the calculation presented here, since the damping of the waves occurs predominantly in the uppermost layer of the solar envelope. In deeper regions, the turbulent Mach number is too small to have any effect. If one assumes that the convective cells have a typical size of a pressure scale height, one can note that the size of the Fresnel zone is of the same order of magnitude as the size of the convective cell. Therefore, diffractive effects are important when the acoustic waves interact with the convection.

Since the Sun is horizontally stratified (i.e. the sound speed being a function of \( z \) only), the phase curvature in the direction perpendicular to the plane of the ray is the same as for a ray of the same length in a homogeneous medium. The phase curvature for this case was already calculated at the beginning of this section, and hence I can write

\[
\frac{\partial^2 \phi}{\partial y^2} \bigg|_{z=z_0} = \frac{2ka}{s(z_0)[2a - s(z_0)]},
\]

where \( 2a \) is the total length of a ray between two photospheric reflections (in a plane-parallel polytrope), and \( s(z_0) \) is the length of the arc from 0 to \( r(z_0) \).

5 SIMPLE MODELS OF CONVECTION

The simplest parametrization of convection is the mixing-length theory (MLT) first devised by Taylor (1915, 1932). It describes turbulence by a single length scale \( l_m \) which represents the dominant scale of coherent motion. The mixing length \( l_m \) can be the characteristic height of a convective cell or a mean free path. One imagines either an ensemble of rising and falling turbulent elements that break up after having traversed a distance \( l_m \) or a set of eddies of typical diameter \( l_m \). Vitense (1953) adopted a mixing length that was proportional to the pressure scale height, \( l_m = \alpha H \), where \( H = -(\partial \ln p/\partial r)^{-1} \) is the pressure scale height and \( \alpha \) is the proportionality constant which has to be determined by calibrating the theory. This is done by evolving solar models with different values of \( \alpha \). The resulting one parameter family of mixing-length models is then calibrated against the known radius of the Sun. Thus
Gough & Weiss (1976) found a value of $\alpha = 1.1$.

Ignoring pressure fluctuations the convective heat flux can be written as

$$F_c \approx \rho c_p \bar{w}T', \quad (54)$$

where the overbar denotes horizontal average. Now consider the dynamics of the buoyant fluid. The vertical component of the turbulent velocity $w$ can be estimated by equating the work done by the buoyancy forces as the fluid rises through a height $l_m$ to the kinetic energy gained by the fluid, i.e.

$$\rho w^2 \approx |\rho'| gl \approx g \rho \delta l_m |T'|/T, \quad (55)$$

where $\delta = - (\partial \ln \rho / \partial \ln T)_p$. Depending on the geometry of the flow considered there may be another factor of order unity in equation (55).

When the convection is very efficient, thermal diffusion may be ignored. The temperature fluctuations are then given by

$$|T'| \approx \beta l_m, \quad (56)$$

where $\beta = - [dT/dz - (\partial T/\partial p)_{ad} dp/dz]$ is the superadiabatic gradient. Again I am neglecting factors of order unity depending on the particular theory. Combining equation (56) with (55) gives

$$w^2 \approx g \delta \beta l_m^2 / T. \quad (57)$$

To calculate the convective heat flux one notes that the temperature fluctuation is positive for rising fluid and negative for falling fluid, so that all motion contributes positively to $F_c$. So combining (56) and (57) with (54) one obtains

$$F_c \approx \rho c_p \bar{w}T' = Al_m^2, \quad (58)$$

where $A = \rho c_p \beta^{3/2} (g \delta / T)^{1/2}$. This result was first obtained by Prandtl (1932).

The sound speed perturbations are given by $|c'|/c = |T'|/2T$. $|T'|/T$ can be calculated using equation (53), where the values of $w$ and $l_m$ are taken from a detailed model; the
resulting sound speed perturbations are shown in Fig. 4.

Now one can extend the simple mixing-length approach beyond the assumption that all eddies are of the same size, by introducing an eddy spectrum or distribution, $\Phi(l_m)$, that describes the density of eddies of size $l_m$. In mixing-length theory $\Phi(l_m) = \delta(l_m - l_0)$, where $l_0$ now denotes the mixing length of the standard MLT. Since there is no fundamental theory of turbulence which would apply to conditions inside the Sun, one has to choose a convenient spectrum. However, this eddy spectrum has to be normalised to yield the same convective heat flux as obtained by the calibrated mixing-length result. Therefore, $F_c$ is integrated over the entire eddy distribution to yield a total convective heat flux of

$$F_c = \int_0^\infty A l_m^2 \Phi(l_m) dl_m.$$  \hfill (59)

For instance, one might decide to choose an eddy distribution of the form

$$\Phi(l_m) = B l_m^{-2} e^{-l_m/l_0}.$$  \hfill (60)

Performing the integral in equation (59) and equating it to the calibrated MLT result, yields the normalisation to be $B = 1/6$.

6 RESULTS AND DISCUSSION

Finally, I proceed to numerically evaluate the integrals in equation (45) using the phase curvature calculated in Sec. 4 and the turbulent spectrum given by equation (60). The integrals in the correlation function $\epsilon^2 \langle V(r_1)V(r_2) \rangle$ can be simplified by expanding the terms that depend only on the static background state about their centre-of-mass coordinate $R$ assuming that all quantities related to the static background do not vary substantially over a correlation length of the turbulent perturbation.

The remaining correlation between the sound speed perturbations is then taken to be

$$\langle \delta c(r_1)\delta c(r_2) \rangle \approx \delta c^2(R) \tilde{r} \Phi(\tilde{r}),$$  \hfill (61)

and similarly for the correlations involving the derivative of $\delta c$. Here $\Phi(\tilde{r})$ is given by equation (60) and $\delta c(R)$ is shown in Fig. 4. In general, the exponent $\langle \Psi^2_1 \rangle$ is complex. The real
part leads to damping of the waves, and the imaginary part represents a phase shift.

The real part of $\langle \Psi^2_1 \rangle$ as a function of degree $l$ with the lower turning point kept fixed is shown in Fig. 5. Since the lower turning point is kept fixed, frequency increases with increasing $l$. One can note that the real part of $\langle \Psi^2_1 \rangle$ is negative, which means that the waves are damped, and the damping increases rapidly with $l$ (or $\omega$). This does not come as a surprise as one would expect the scattering to become stronger with decreasing wavelength. One may quote, for example, scattering by small spheres (Rayleigh scattering), where the scattering cross section is proportional to the fourth power of $k$. Clearly, the scattering increases with the thickness of the scattering medium and thus with increasing depth of the lower turning point as demonstrated in Fig. 5. Shown are the results based on three different correlation functions for the sound speed perturbations. The solid line assumes a spectrum of the form given by equation (60). The dashed line corresponds to

$$\Phi(l_m) = (2l_0)^{-1}e^{-l_m/l_0},$$

and the dotted line is based on

$$\Phi(l_m) = l_m^2(96l_0^3)^{-1}e^{-l_m/2l_0}.$$  

All three spectra are normalised according to equation (59). The dependence of the damping on the form of the convective spectrum can be relatively significant.

Fig. 6 shows the imaginary part of $\langle \Psi^2_1 \rangle$ for lower turning points of depths $a = 0.01 R_\odot$ and $a = 0.001 R_\odot$ as a function of degree. The results shown were calculated on the basis of the spectrum given by equation (60). The phase shift is negative which implies that the phase of the scattered wave is advanced over the phase of the unperturbed wave. At first sight it may seem surprising that scattering leads to an advancement of the phase. A simple qualitative explanation for this result is given by Codona et al. (1985). They showed that a continuous random medium can cause an average advance of the arrival time of a pulse, and I will briefly summarise their argument in the following.

Consider a wave propagating through a homogeneous medium from a point S to a point R, and assume that the random medium is concentrated in a “phase screen” at a distance $s$ from the source. This screen has the effect of shifting the time of the wavefront by a small
random amount \( t(x) \), where \( x \) is the position on the screen and \( t(x) \) is a random distribution with zero mean. The travel time for a path through \( x \) is

\[
\tau(x) = \tau_0 + \frac{p x^2}{2c} - t(x),
\]

(64)

where \( \tau_0 \) is the travel time of the unperturbed wave, \( p = r/s(r - s) \), \( r \) being \( \sqrt{\mathbb{R}} \), and \( c \) the wave speed in the medium. By Fermat’s principle the ray assumes a path such that \( \tau \) is stationary. Expanding \( t(x) \) as follows

\[
t(x) = t_0 + t'x + \frac{1}{2}t''x^2 + ..., \]

(65)

one finds that the ray crosses the screen at \( x_s = pct' \). The travel time of the ray is then given by

\[
\tau(x_s) \simeq \tau_0 + \frac{1}{2}cpt'^2 - t_0 - cpt'^2.
\]

(66)

Since \( t \), and hence \( t_0 \) and \( t' \), are by construction random variables with zero mean, the only contribution to the average travel time comes from the squared terms. The first term is positive corresponding to a delay, and represents the effect of geometry: The perturbed path is geometrically longer than the unperturbed one. The second term (called Fermat term) is negative and corresponds to a pulse advance. It is also twice as big as the first one resulting in an overall pulse advance. One can imagine that the rays governed by Fermat’s principle seek out regions with a pulse advance. Thus the average travel time is given by

\[
\tau = \tau_0 - cpt'^2/2.
\]

The phase shifts displayed in Fig. 6 are too small (corresponding to about 1/100th of a second at a frequency of 3 mHz) to be detected directly as a time delay in a time-distance analysis.

Having calculated the change of amplitude of the wave between two photospheric reflections one can convert this attenuation into a damping rate, \( \eta \), using the equation \( A/A_0 = e^{-\eta \tau} \), where \( \tau \) is the travel time for a single traverse of the ray, and \( A/A_0 \) the fractional change in amplitude per skip. Thus one finds that \( \eta = -\tau^{-1} \ln(A/A_0) \), where the amplitude ratio \( A/A_0 \) is given by \( \text{Re}[\exp(\frac{1}{2}\langle\Psi^2\rangle)] \). Observationally this damping manifests itself as a line width in the measured frequency of a solar eigenmode. It is straightforward to show that the line width (full width at half maximum) of the acoustic eigenmodes of the Sun, \( \Gamma \),
is equal to twice the damping rate $\eta$.

With the advent of long time-series of solar oscillation data as obtained, for example, by the ground-based GONG network and the Michelson-Doppler Interferometer on board the spacecraft SOHO, the line widths of high-degree modes can be measured with good accuracy. Recently, line widths of high-degree modes were reported by Duvall, Murawski, & Kosovichev (1998) and their results for the $p_1$ modes are reproduced in Fig. 7 a. In Fig. 7 b I have plotted the fractional contribution to the line width as predicted by the method presented here. The results shown in Fig. 7 b are based on the spectrum given by equation (62). It is found that scattering by sound speed perturbations contributes $\simeq 15\%$ to the line width of the high-degree modes. However, the model presented here can only be regarded as a toy model since the spectrum of the turbulence and the model of the surface layers of the Sun were chosen for convenience rather than for accuracy. But it is interesting to note that this model correctly predicts the variation of the line width with $\omega$ and $l$. The fractional contributions shown in Fig. 7 b are constant within the errors of the measurements.

Another caveat that I should mention concerns the assumed structure of the turbulence. In Sec. 5 the convection has been described by a local mixing-length theory which presumes that the convection can be characterised by a locally defined spectrum. This description of turbulence was used in the computations in order to demonstrate the capabilities of this method. However, recent numerical simulations and laboratory experiments suggest that the local mixing-length picture is a poor description of convection in stellar envelopes (e.g. Nordlund & Stein 1996). Instead there are indications that the turbulent flow is extremely non-local, non-isotropic and hence poorly represented by a local power spectrum. Some simulations show that heat is transported primarily through thin threads that extend all the way from the bottom to the top of the solar convection zone. Nevertheless, since Rytov’s technique is an even better approximation if the perturbations are confined to thin threads, the method of this analysis will in principle remain valid and useful.
7 CONCLUSIONS

To summarise, I have presented an analytical description of the interaction of waves with the turbulent medium following a similar treatment used in oceanography. The inhomogeneous wave equation was solved using Rytov’s technique, and several of the integrals in the ensuing expression could be evaluated analytically using a stationary-phase approximation; the remaining integrals could be solved numerically. Thus, in the framework of ray theory, one obtains a quantitative assessment of the scattering contribution to the line width of acoustic modes.

Previous studies of the line widths of solar modes have focused on radial modes and generally neglected the effect of diffraction. However, diffraction becomes important for shallow waves for which the size of the Fresnel zone is comparable with the size of the convective cells.

Scattering is not the only source of line widths. Other sources include non-adiabatic effects associated with the radiative and convective energy transport, mechanical absorption of the sound waves (Gough 1980; Goldreich & Keeley 1977; Christensen-Dalsgaard, Gough, & Libbrecht 1989; Balmforth 1992) and partial reflection at the upper turning point (Balmforth & Gough 1990). The latter showed in a simple analytical model that, for radial modes, partial reflection contributes significantly to the line width.

In this paper I have isolated the effect of scattering by sound speed perturbations from other effects that contribute to the line width. Using a simple semi-analytical model I studied one of the physical processes that determine the line widths of high-degree modes. Once the remaining contributions to the line width are well understood chances will be excellent that one will be able to constrain the convective spectrum seismically.

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APPENDIX A: LINEARIZED ADIABATIC WAVE EQUATION

The linearized adiabatic wave equation has been derived by various authors (e.g. see Gough 1986). In this appendix I briefly sketch its derivation, which is referred to in Sec. 3.

Neglecting viscosity, the momentum equation for a fluid moving with velocity $u$ can be written in the form

$$\rho \frac{Du}{Dt} = -\nabla p + g\rho + F,$$  \hspace{1cm} (A1)

where the Lagrangian derivative $D/Dt$ is defined as

$$\frac{D}{Dt} := \frac{\partial}{\partial t} + u \cdot \nabla.$$

$F$ denotes all other forces except gravity, $p$ is pressure and $\rho$ matter density. $g$ is the gravitational acceleration which is related to the gravitational potential $\phi$ by

$$g = \nabla \phi,$$  \hspace{1cm} (A3)

where $\phi$ satisfies Poisson’s equation

$$\nabla^2 \phi = -4\pi G \rho,$$  \hspace{1cm} (A4)

with $G$ being the gravitational constant.

The continuity equation is given by

$$\frac{D\rho}{Dt} + \rho \nabla \cdot u = \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho u) = 0.$$  \hspace{1cm} (A5)

Moreover, I make the assumption that the changes in pressure and density are adiabatic, i.e.

$$\frac{Dp}{Dt} = \frac{\Gamma_1 p}{\rho} \frac{D\rho}{Dt} = c^2 \frac{D\rho}{Dt}.$$  \hspace{1cm} (A6)

Here $\Gamma_1$ denotes the first adiabatic exponent, which is defined as

$$\Gamma_1 \equiv \left( \frac{\partial \ln p}{\partial \ln \rho} \right)_s.$$  \hspace{1cm} (A7)
and which needs to be derived from an assumed equation of state; $c$ denotes the local sound speed.

Now, equations (A1), (A4), (A5) and (A6) are perturbed around the equilibrium state in terms of the displacement $\xi$ of the fluid. Perturbing the equilibrium state – $p = p_0 + p'$, $\rho = \rho_0 + \rho'$, and $\phi = \phi_0 + \phi'$ – and by eliminating $p'$ and $\rho'$ from the momentum equation (A1) using equations (A4) and (A5), and after some rearrangement one obtains

$$\frac{\partial^2 \xi}{\partial t^2} = \nabla (c^2 \chi - g \mathbf{n} \cdot \xi) - \Gamma \mathbf{n}$$

(A8)

with $\Gamma = H^{-1} c^2 - g$, where $H$ is the density scale height $H := - (\partial \ln \rho / \partial \ln r)^{-1}$. The scalar $\chi$ is defined as $\chi := \text{div} \xi$.

Equation (A8) is an equation for the components of a vector. However, a vector is coordinate dependent so that it would be more convenient to find an equation for the scalar $\chi$. This is achieved by first taking the divergence of (A8):

$$\frac{\partial^2 \chi}{\partial t^2} = \nabla^2 (c^2 \chi - g \mathbf{n} \cdot \xi) - \mathbf{n} \cdot \nabla (\Gamma \chi).$$

(A9)

The vertical component of $\xi$, $\mathbf{n} \cdot \xi$, can be reexpressed by taking the double curl of equation (A8)

$$\mathbf{n} \cdot \frac{\partial^2}{\partial t^2} \nabla \times (\nabla \times \xi) = \frac{\partial^2}{\partial t^2} (\mathbf{n} \cdot \nabla \chi - \nabla^2 \mathbf{n} \cdot \xi) = -g \nabla^2_h (\Gamma \chi),$$

(A10)

where $\nabla^2_h$ is the horizontal Laplace operator. Solving (A10) for $\mathbf{n} \cdot \xi$ and substituting into (A9) yields the fourth-order equation:

$$\frac{\partial^4 \chi}{\partial t^4} - \frac{\partial^2}{\partial t^2} [\nabla^2 (c^2 \chi) - \mathbf{n} \cdot \nabla (H^{-1} c^2 \chi)] - N^2 \nabla^2_h (c^2 \chi) = 0,$$

(A11)

where $N$ is the buoyancy frequency given by

$$N^2 = g \left( \frac{1}{H} - \frac{g}{c^2} \right).$$

(A12)

Eliminating odd derivatives of the dependent variable by the substitution $c^2 \chi = \rho^{-1/2} \psi$, yields

$$c^{-2} \left( \frac{\partial^2}{\partial t^2} + \omega_c^2 \right) \frac{\partial^2 \psi}{\partial t^2} - \frac{\partial^2}{\partial t^2} \nabla^2 \psi - N^2 \nabla^2_h \psi = 0,$$

(A13)
where the quantity $\omega_c = \frac{c}{2H} (1 - 2n \cdot \nabla H)^{1/2}$ is the critical cut-off frequency. For acoustical oscillations one can simplify equation (A13) by neglecting the buoyancy frequency $N$:

$$\left( \frac{\partial^2}{\partial t^2} + \omega_c^2 \right) \psi - c^2 \nabla^2 \psi = 0.$$  \hfill (A14)

Aside from the term containing the critical cut-off frequency this is essentially a wave equation. The cut-off frequency $\omega_c$ modifies the wave equation in the sense that in the region where $\omega < \omega_c$ the waves become evanescent.
**Figure A1.** Fresnel zone construction.

**Figure A2.** Diagram to the calculation of the Fresnel tube in the Sun.

**Figure A3.** Extent of the Fresnel tube (perpendicular to the ray) as a function of depth in a plane-parallel polytrope for a ray with $a = 0.001$. All lengths are measured in units of solar radii.

**Figure A4.** Sound speed fluctuations in the solar envelope.

**Figure A5.** Real part of $-\langle \Psi_1^2 \rangle$ as a function of $L$ for lower turning points of $a = 0.01 \, R_{\odot}$ (a) and $a = 0.001 \, R_{\odot}$ (b) assuming different turbulent spectra (see text).

**Figure A6.** Imaginary part of $-\langle \Psi_1^2 \rangle$ as a function of $L$ for lower turning points of $a = 0.01 \, R_{\odot}$ (solid line) and $a = 0.001 \, R_{\odot}$.

**Figure A7.** Panel (a) shows line widths of solar modes as measured by Duvall, Kosovichev, & Murawski (1998) using the MDI instrument. On panel (b) are shown the corresponding (fractional) contributions to the line width from sound speed scattering as predicted by my model.
Figure 1:
Figure 2:
Figure 3:
Figure 4:
Figure 5:
Figure 6:
Figure 7: