Lithium-boro-tellurite glasses with ZnO additive: Exposure Buildup Factors (EBF) and Nuclear Shielding Properties

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Abstract

The effect of ZnO increment on lithium boro tellurite (Li$_2$O-B$_2$O$_3$-P$_2$O$_5$-ZnO) glass structure was investigated with the study of gamma and neutron attenuation properties. The gamma-ray shielding effectiveness of materials can be understood with the help of several different shielding parameters that play an important role in understanding the shielding capacities of the material. The mass attenuation coefficients ($\mu/\rho$) for Li$_2$O-B$_2$O$_3$-P$_2$O$_5$-ZnO glass samples were calculated by using the XCOM program based on the DOS-based compilation XCOM. To compare the theoretical and simulation results of the mass attenuation coefficients of the samples, MCNPX (Monte Carlo N-Particle) simulation code was handled with the XCOM program in the energy range of 0.02 MeV - 20 MeV. In addition, effective atomic numbers ($Z_{eff}$), electron densities ($N_e$), effective removal cross-section ($\Sigma_R$) and the transmission factor (TF) for sample glasses, have also been examined in that energy range. In addition to these parameters the Half-value layer (HVL), tenth value layer (TVL) and also mean free path (MFP) values were calculated by using the $\mu/\rho$. Moreover, exposure buildup factors (EBF) was calculated at 0.015–15 MeV up to 15 mfp by utilizing the G-P fitting approach. The glass having 20 mol% ZnO was found to has better gamma-ray shielding properties among the investigated glass samples. As a result, sample ZL5 among studied glasses has marvelous attenuation effectiveness whereas sample ZL1 has the best neutron radiation shielding performance. The outcomes of the present extended research can provide significant information for the comparison of new generation shielding materials with conventional shielding materials used in ionizing radiation facilities.

Keywords: ZnO; gamma shielding; EBF; neutron shielding; MCNPX;

ZnO Katkılı Lityum-Boro Tellürit Camlar: Maruz Kalma Faktörü (EBF) ve Nükleer Zırhlama Özellikleri

Özet

Lityum boro tellürit (Li$_2$O-B$_2$O$_3$-P$_2$O$_5$-ZnO) cam yapısı üzerinde ZnO katkısının etkisi, gama ve nötron zayıflatma özelliklerinin incelenmesi ile araştırılmıştır. Malzemelerin gama işini zırhama etkiliği, malzemelerin zırhama kapasitelerinin anlaşılmamasında önemli bir rol oynayan birkaç farklı zırhama parametreinin gündeme gelmesi beklenmiştir. Li$_2$O-B$_2$O$_3$-P$_2$O$_5$-ZnO cam örnekleri için kütle zayıflatma katsayısı ($\mu/\rho$), DOS-tabanlı XCOM’u temel alan XCOM programı kullanılarak hesaplanmıştır. Numunelerin kütle zayıflatma katsayısının teorik ve simulasyon sonuçlarını karşılaştırmak için, 0.02 MeV - 20 MeV enerji aralığında XCOM programı ile MCNPX (Monte Carlo N-Parçacık) simulasyon kodu kullanıldı. Ek olarak, etkili atom numarası ($Z_{eff}$), elektron yoğunluğu ($N_e$), etkili çıkarma hafifliği ($\Sigma_R$) ve numune camları için iletim faktörü (TF) değerleri de bu enerji aralığında incelenmiştir. Bu parametrelere ek olarak Yarı-değer kalınıtı (HVL), onuçu değer kalınıtı (TVL) ve ayrıca ortalama serbest yol (MFP) değerleri $\mu/\rho$ kullanılarak hesaplanmıştır. Ayrıca G-P fişleme yaklaşımları kullanılarak maruz kalma faktörü (EBF) değerleri de 0.015–15 MeV’de 15 mfp’ye kadar hesaplanmıştır. İncelenen cam örnekleri arasından % 20 mol ZnO katkısına sahip cam örnekinin daha iyi gama işını koruyucu özelliklerine sahip olduğu bulunmuştur. Sonuç olarak, incelenen cam örnekleri arasında ZL5, en iyi zayıflatma etkiliğine sahipken ZL1 cam örneği, en iyi nötron radyasyon zırhama performansına sahiptir. Mevcut araştırmanın bu yeni sonuçları, yeni nesil zırhama

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malzemeleri ile ıyonlaştırıcı radyasyon tesislerinde kullanılan geleneksel zırhlama malzemelerinin karşılaştırılması için önemli bilgiler sağlayabilir.

Anahtar Kelimeler: ZnO; gamma zırhlama; EBF; nötron zırhlama; MCNPX.

1. Introduction

In recent years, an increase has been observed in nuclear research laboratories and nuclear power plants. On the other hand, with the spread of radiation diagnosis-treatment methods, the number of personnel exposed to high energy radiation is increasing, especially in the field of medicine. Glasses, one of the radiation shielding materials, is a new groundbreaking application. These glasses have a wide range of applications such as nuclear medicine, radiology, imaging units, radiation oncology and nuclear physics research laboratories etc. They are produced especially because they absorb the photon radiation well. A familiar inorganic glass-composing oxide, B₂O₃ has a low melting point and well thermal stability because between heavy-metal oxide based glasses, tellurite-glasses become prominent with the possibility of modifying the glass composition with a large number of components, which can contain rare-earth elements (REE), highly polarized ions (Pb⁴⁺, Bi³⁺, Ti⁴⁺) and transition-metal oxides with a high proportion. And thus offers better non-linear optical properties [1-2]. Tellurite glasses; thanks to the high refractive index (>2), high insulating constants, high electrical conductivity, superior mechanical properties, high chemical and thermal stabilization, low glass-transition and defrost temperatures are suitable for optoelectronic applications, for example, optical fibers, microrels, data storing devices, lasers, sensors, optical imager, optic modulators and spectroscopic devices [3-6]. These important features promote the research specialist and engineers for using tellurite-glasses in several applications. TeO₂ is a conditional glassmaker; does not have the ability to make glass alone. Therefore, it makes the glass by adding a small amount of a second constituent (modifier) for example heavy metal oxide, alkali oxide or halide to modify the network structure [1]. Adding a small amount of TeO₂ to the borate glass system increases the stabilization and the capability to form a glass. Lithium oxide (Li₂O) plays a role in modifying the glass network structure. By adding Li₂O to the boro telluride glass system, mechanical, physical, transport and structural features are varied. Oxide glasses with Li₂O are commonly used in solar cell applications, solid-state batteries, and superionic conductors. Studies on boro-telluride glass samples having ZnO are quite exotic owing to their eminent refractive point and optical ethereality [7]. As a promising material for fiber optic technology, lasers, solar-cells and sensor studies, boro tellurite zinc glasses are largely used in the application of gas sensors, optoelectronic memory changing tools and optical waveguide practices [8-10]. Previous studies in literature on the Tellurite glass samples are TeO₂–ZnO Dutta et al. [11], TeO₂–Li₂O–ZnO Mohammed et al. [12], TeO₂–Li₂O–B₂O₃ Saddeek et al. [13], ZnO–B₂O₃–P₂O₅–TeO₂ Mosner et al. [14]. Ghada E. El Falaky et al. [15] examined the impact of ZnO on the mechanical and physical features of borate glass systems. Y.B. Saddeek et al. [16] examined mechanical, thermal and structural features of B₂O₃–TeO₂–B₂O₃ and Li₂O–TeO₂–B₂O₃ [17] glasses. G.Lakshminarayana et al. [18] worked on the TeO₂–B₂O₃–BaO–ZnO–Na2OEr2O3–Pr6O11 glass samples for gamma ray shielding features by using the thermal and vibrational spectroscopic studies. N. Elkhoshkhany et al. [19] examined the constitutive and optical behavior of TeO₂–Li₂O–ZnO–Nb2O₅–Er3O₃–B₂O₃ glass system. S. Rani et al. [20] examined the role of Li₂O on the physical, optical and constitutive features of zinc boro-tellurite glasses. M. G. Dong et al. [21] examined the role of Li₂O on the gamma radiation shielding properties of lithium-zinc-bismuth-borate glass system using the XCOM program and MCNPX code. The purpose of this study is to estimate the role of ZnO on the gamma shielding parameters in lithium boro-tellurite glasses. Molar fractions and the densities of the glass samples mentioned in this work are listed in Table 1 [22]. We estimate the mass attenuation coefficients (µ/ρ), total electronic (σₑ,e), atomic (σₑ,a) and molecular (σₑ,m) cross sections, effective atomic numbers (Zeff), electron densities (Nel) of the stated glass samples. The estimated values have been likened with the theoretical ones computed with the XCOM program. Some concerning parameters effective removal cross-section (Σₑ) and the transmission factor (TF) for sample glasses have also been examined in the energy range from 0.02 MeV to 20 MeV. The outcomes of the present extended research can provide significant information for the comparison of new generation shielding materials with conventional shielding materials used in ionizing radiation facilities.

| Sample Code | B₂O₃ | ZnO | TeO₂ | Li₂O | Density (g/cm³) |
|-------------|------|-----|------|------|----------------|
| ZL1         | 60   | 0   | 10   | 30   | 3.32           |
| ZL2         | 60   | 5   | 10   | 25   | 3.08           |
| ZL3         | 60   | 10  | 10   | 20   | 3.14           |
| ZL4         | 60   | 15  | 10   | 15   | 3.07           |
| ZL5         | 60   | 20  | 10   | 10   | 3.44           |
2. Material and Method

2.1. MCNPX and WinXCom Program

The issue of radiation absorption in the fields of nuclear energy and medicine remains important. There are various equations and studies in the literature for the absorption of α, β radiations and n (neutron), p (proton) particles. MCNPX is a very useful program and has a general object Monte Carlo N-Particle code and used for the transmission of model radiation such as Gamma-ray, X-ray, neutron or electron radiations via matter [23]. In this study, NaI (Tl) detector was used to detect gamma rays and the verification with the MCNPX code was done by Tekin [24]. The simulation setup used in the study is shown in Figure 1. This setup consists of five different elements. These are isotropic radioactive spot source, Pb collimator for original radiation rays, glass sample, Pb blocks for protection against scattered photons, and NaI (Tl) detector. In order to calculate the μ/ρ of the sample glasses in this study, the XCOM program [25, 26] together with the MCNP program was also used by using the fractions stated in Table 1.

Figure 1. (a) MCNPX simulation setup obtained MCNPX Visual Editor (VE X_22S) for mass attenuation coefficients studies (b) MCNPX simulation setup obtained from MCNPX Visual Editor (VE X_22S) for photon transmission factor (TF) studies
2.2. Calculation method of shielding parameters

As a high-energy photon passes through a substance of \( x \) thickness, its energy is absorbed and passes to the other side as its intensity is weakened exponentially. This reduction in radiation intensity is directly proportional to the \( x \)-thickness and linear reduction coefficient of the absorber in reference to the Lambert-Beer law Eq. 1 [27]:

\[
I = I_0 e^{-\mu x}
\]

where \( I \) and \( I_0 \) are specifying the transmitted and primary intensity of gamma radiation, \( \mu \) specify the linear attenuation coefficient and \( x \) is the thickness (cm) of the shielding material. The linear attenuation coefficient is defined as the energy reduction fraction per unit thickness on the unit surface. Although the linear attenuation coefficient is only associated with thickness, this coefficient is attached to the energy of the photons and on the structure of the absorbent. The proportion of the linear attenuation coefficient to the material density is the reduction per unit mass on the unit time and is expressed as the coefficient of mass reduction.

The experimental mass attenuation coefficient \( \mu/\rho \) of elements is expressed by:

\[
\mu_m = \frac{\mu}{\rho}
\]

The theoretical mass attenuation coefficient \( \mu/\rho \) (cm\(^2\)/g) of lithium boro-tellurite glasses containing ZnO can be specified as Eq.3:

\[
\frac{\mu}{\rho}_{\text{glass}} = \sum w_i \left( \frac{\mu}{\rho} \right)_i
\]

where \( w_i \) and \( (\mu/\rho)_i \) are the fraction by weight and mass attenuation coefficient of the examined element in the sequence. To calculate the \( (\mu/\rho) \) value of the examined glasses for a determined energy region XCOM and MCNP code should be used [28]. Additionally, the fraction by weight \( w_i \) should be calculated by considering the number of element \( n_i \) and atomic weight of the \( i \)th element \( A_i \) in a chemical compound as:

\[
w_i = \frac{n_i A_i}{\sum_i n_i A_i}
\]

The \( \mu/\rho \) values of the examined glasses were examined by using the XCOM program based on the DOS-based compilation XCOM [28].

In nuclear physics, the possibility of radiation interacting with matter is considered a cross-section. The cross-section is considered to be the total cross-section of the whole material, rather than the interaction with a single atom. According to the experimental studies and the results obtained, the area of the total cross-section can be calculated. In line with these experimental data, the area of the total cross-section has been determined theoretically and formulated and approximate results have been obtained. Total cross-sections can be specified as the following equations[29];

\[
\sigma_{t,m} = \frac{\mu M}{N_A}
\]

\[
\sigma_{t,a} = \frac{1}{N_A} \sum_i f_i A_i \left( \frac{\mu}{\rho} \right)_i = \frac{\sigma_{t,m}}{\sum_i n_i}
\]

\[
\sigma_{t,el} = \frac{1}{N_A} \sum_i f_i A_i \left( \frac{\mu}{\rho} \right)_i = \frac{\sigma_{t,a}}{Z_{\text{eff}}}
\]

\( \sigma_{t,m} \): Total molecular cross-section;
\( \sigma_{t,a} \): Total atomic cross-section
\( \sigma_{t,el} \): Total electronic cross-section of the individual elements
\( M = \sum_i (n_i A_i) \): Molecular weight
\( N_A \): Avogadro constant
\( f_i \): Fractional abundance of \( i \)th element
\( n_i \): Number of element
\( A_i \): Atomic weight of the \( i \)th element of samples
\( Z_i \): Atomic number of the \( i \)th element
The effective atomic number \((Z_{eff})\) is a significant parameter for radiation absorptions of compounds, mixtures and alloys. Based on the variation of photon interaction cross section of the composite material element does not display the characteristic energy of the atomic number of the elements in all energies. Therefore, it has used the term atomic number for composite materials and it is stated that this value changes depending on the energy. The effective atomic number is theoretically the proportion of the total \(\sigma_{t,a}\) (atomic cross-section) to the \(\sigma_{t,el}\) (total electronic cross-section) given in Eq. 8 [30].

\[
Z_{eff} = \frac{\sigma_{t,a}}{\sigma_{t,el}}
\]  
(8)

The \(Z_{eff}\) is a commonly used parameter for diagnosis and treatment, especially in nuclear medicine, for dose calculations and for radiation protection. The effective electron number, such as the electron density, is used for similar purposes [31]. The effective electron number indicates the number of electrons interacting with the substance in the unit mass.

\[
N_e = \frac{(\mu/\rho)}{\sigma_{t,el}} = \frac{N_A Z_{eff}}{M} \sum_i n_i = \frac{N_A Z_{eff}}{(A)}
\]  
(9)

The average atomic mass in other words average atomic weight \((A)\) [32,33] can be specified as;

\[
(A) = \frac{M}{\Sigma_i n_i}
\]  
(10)

Half-value layer (HVL) is the thickness of the material required to reduce the beam intensity to the half value of the principal intensity. The HVL shows that as the photon energy increases, energetic photons have the ability to permeate the sample. For the sample glasses, HVL can be examined by using the equation below,

\[
HVL = x_{1/2} = \frac{0.693}{\mu}
\]  
(11)

The tenth value layer TVL is the thickness of material required to reduce the beam intensity to one-tenth of the initial intensity.

\[
TVL = x_{1/10} = \frac{\ln 10}{\mu}
\]  
(12)

HVL, TVL and also (Mean free path) MFP are the most widely used theoretical parameters for radiation shielding efficiency for glass samples [34,35] and there is a correlation between them: \(1\ HVL \cong 0.3\ TVL\ .\) The average free path is the average distance the sample passes through before the single-particle interacts with the material and is calculated by the following equation.

\[
MFP = \frac{1}{\mu}
\]  
(13)

The transmission factor of gamma-ray (TF), defined as \((I/I_0)\) can be determined using the attenuation coefficient and density of the material. In this case, certain thicknesses are selected for the shielding material or the thickness is selected to achieve a certain degree of attenuation at the source energies to use in the MCNP simulation program. Permeability based on material thickness and initial photon energy.

The probability of reaction by neutrons diminishes quickly as the neutron energy increases. However, scattering is very significant in a collision since it can pass on pretty much energy to the neutron. That’s why it is of great importance to investigate the neutron blocking capacity of the shielding materials. The status of fast neutron attenuation is defined by a parameter named the "removal cross-section", unitized by \((cm^{-1})\). The effective removal cross-section, \(\Sigma R\) \((cm^2/g)\) is used to qualify the fast neutrons attenuation in glass samples and obtained by adding the individual mass removal cross-section of its components [33]:

\[
\Sigma R = \sum_i W_i (\Sigma R/\rho)_i
\]  
(14)

where \(W_i\) is the partial density and equal to \(W_i = w_i \rho_s\)

\(\Sigma R/\rho\): Mass removal cross-section of the \(i\) th constituent

\(w_i\): Weight fraction of the \(i\) th component
Density of the sample.

The exposure buildup factor (EBF) is a central parameter in determining the quality of radiation shielding features of glasses. To compute the EBF values we used G-P fitting method developed by Harima [36-38]. In the calculation processes, the $Z_{eq}$ values are derived by matching the $\left( \frac{\mu_m}{\mu_{m, \text{Total}}} \right)_{\text{Compton}}$ ratio of the specific energy with the appropriate ratio of the element with the help of the following equation.

$$\left( \frac{\mu_m}{\mu_{m, \text{Total}}} \right)_{\text{Compton}} = \frac{Z_1 (\log R_2 - \log R_1) + Z_2 (\log R - \log R_2)}{\log R_2 - \log R_1}$$

(17)

where $Z_1$ and $Z_2$ indicates the atomic numbers of the samples.

At the later stage, using the ANSI / ANS-6.4.3 [39] standard reference database, the values of G-P fitting parameters in the 0.015-15 MeV energy region for the selected samples were then calculated. Finally, all these parameters obtained in the previous steps are utilized in order to calculate EBF values. Detailed information about calculations can be accessed from previous studies [40-44].

3. Results and Discussion

For studying the shielding features of glass samples having the compound $x\text{ZnO}(30-x)\text{Li}_2\text{O}-60\text{TeO}_2 \text{B}_2\text{O}_3$ ($x=0, 5, 10, 15$ and 20mol%), the mass attenuation coefficient (MAC) ($\mu/\rho$) in the energy range from 0.02 MeV to 20 MeV were calculated applying XCOM program and the outcomes are drawn according to the photon energy (see Figure 2). As can be easily understood from Figure 2, $\mu/\rho$ values are dropped rapidly to 0.06 MeV as the photon energy increased since the photoelectric effect is dominant at low lying photon energy region and become constant after the energy range of 0.06 MeV mid-level energies where the Compton effect is dominant. Additionally, it is easy to see that the reduction of the Li$_2$O contribution and the increment of the ZnO contribution in sample glasses leads to the increment of $\mu/\rho$ values. In this case, it is clear that the ZL5 has the largest value of $\mu/\rho$ among the glass samples.

![Figure 2: Mass attenuation coefficients ($\mu/\rho$) of the sample glasses with photon energy from 0.02 to 20 MeV.](image)

The MCNPX simulation code and XCOM program were used to compare the simulation and theoretical results of the mass attenuation coefficients of the samples. The values compared between 0.02 MeV - 20 MeV energy range are shown in Table 2. As is evident from Table 2, when gamma energies increase for glass samples it was determined that the mass attenuation coefficients go down and run up with the rise of ZnO contribution. This demonstrates that an increase in photon interactions in low photon energies with the increase of ZnO contribution in samples varies by $-Z^4/E^3$. Table 2 also shows that the results obtained by the XCOM program and MCNPX code are consistent with each other.
| Energy (MeV) | ZL1          | ZL2          | ZL3          | ZL4          | ZL5          |
|-------------|--------------|--------------|--------------|--------------|--------------|
|             | MCNPX | XCOM     | MCNPX | XCOM     | MCNPX | XCOM     | MCNPX | XCOM     | MCNPX | XCOM     |
| 0.020       | 5.17685   | 5.026482   | 6.612855   | 6.593171   | 8.125587   | 8.047543   | 9.546587   | 9.401257   | 11.253304   | 10.644414  |
| 0.122       | 0.325504   | 0.319874   | 0.332007   | 0.322427   | 0.338521   | 0.324798   | 0.342235   | 0.327005   | 0.345216   | 0.329064   |
| 0.356       | 0.105054   | 0.104144   | 0.105214   | 0.104229   | 0.107877   | 0.104307   | 0.110042   | 0.104381   | 0.112581   | 0.104449   |
| 0.515       | 0.087622   | 0.085436   | 0.087714   | 0.085455   | 0.088021   | 0.085473   | 0.085490   | 0.086824   | 0.085505   |
| 0.665       | 0.075320   | 0.074942   | 0.075412   | 0.074943   | 0.075996   | 0.074943   | 0.076120   | 0.074944   | 0.076216   | 0.074945   |
| 1.173       | 0.057004   | 0.056076   | 0.057116   | 0.056063   | 0.057598   | 0.056052   | 0.057419   | 0.056041   | 0.057516   | 0.056031   |
| 1.250       | 0.054672   | 0.054252   | 0.054712   | 0.054241   | 0.054991   | 0.054231   | 0.055114   | 0.054222   | 0.055201   | 0.054213   |
| 1.330       | 0.052722   | 0.052530   | 0.052789   | 0.052522   | 0.052901   | 0.052514   | 0.052991   | 0.052507   | 0.052824   | 0.052500   |
| 5.000       | 0.028831   | 0.028228   | 0.028851   | 0.028475   | 0.028755   | 0.028704   | 0.028854   | 0.028917   | 0.029459   | 0.029115   |
| 8.000       | 0.025335   | 0.024392   | 0.025651   | 0.024793   | 0.025810   | 0.025166   | 0.026115   | 0.025512   | 0.026710   | 0.025836   |
| 10.000      | 0.023530   | 0.023279   | 0.023945   | 0.023759   | 0.024511   | 0.024205   | 0.024901   | 0.024619   | 0.025698   | 0.025006   |
| 15.000      | 0.022846   | 0.022192   | 0.023004   | 0.022815   | 0.023759   | 0.023394   | 0.024511   | 0.023933   | 0.025204   | 0.024436   |
| 20.000      | 0.022914   | 0.022003   | 0.022988   | 0.022730   | 0.023810   | 0.023405   | 0.024357   | 0.024033   | 0.025881   | 0.024620   |

The HVL, TVL and MFP values of the sample glasses are shown in Figures 3 and 4 (a, b). These values are very small in the low energy region of photon and these values are reduced by the increasing concentration of ZnO. HVL and TVL values were almost constant up to 0.1 MeV energy for all glass samples, after which a quick increase occurred in these values and reached the peak value of 15 MeV. The differences in these values for existing glass samples can be specified as the domination of varied photon interaction types in varied energy zone. In addition, these values decrease with the increasing densities of the subject glass samples. It is important to note that the low MFP, HVL and TVL values are necessary for a preferable gamma ray protection material since the possibility of photon interaction by the material is higher. According to this result, when we compare glass samples, it is understood that the ZL5 glass sample with minimum HVL, TVL, MFP and maximum density and mass attenuation coefficient has the best protection features among the glass samples.

![Figure 3. Mean free path (MFP) of investigated glass samples.](image-url)
**Figure 4.** a) Half (HVL) and b) tenth value layer (TVL) of investigated glass samples.

**Figure 5** indicates the changes in the effective atomic number ($Z_{\text{eff}}$) of the ZnO doped lithium boro-tellurite glasses according to the gamma-ray energies in the region of 0.02 MeV to 20 MeV. As shown in **Figure 5**, a quick jump occurred at the 0.06 MeV energy range with the increment of the Zn contribution in glass structures except for the glass sample ZL1. The reason is photoelectric cross-section dependence on the $Z^{4.5}$. Moreover, a remarkable decrease of $Z_{\text{eff}}$ values in the region of 0.04 MeV - 0.1 MeV takes place with the increment of the photon energy for the glass samples. When the photon energy rice further, the $Z_{\text{eff}}$ becoming virtually stand-alone from photon energy. The prevailing of the Compton scattering case can be one of the main reasons. When the value is higher than 2.0 MeV, the $Z_{\text{eff}}$ demonstrates a slow increment and this indicates that pair production is dominant. As can be understood from **Figure 5**, the $Z_{\text{eff}}$ is highest for sample ZL5. The alteration of electron density for examined sample glasses with photon energy indicates the same action as in $Z_{\text{eff}}$, can be seen in **Figure 6**.
The calculated gamma-ray transmission factors (TFs) depending on thickness (x) are shown in Figure 7, calculated by the MCNPX program for specific energies. As one can see from the figure the TF values drop rapidly with the increase in mass thickness and better attenuation (minimum values of TFs) is achieved in high energy regions. The difference between the TF values of the samples changes from 0.87% to 0.11%. ZL5 is the best absorbent between the glass samples for both neutron and gamma radiation. Figure 7 shows that the transmission factor for the glass samples aligns considering the following order: ZL1>ZL2>ZL3>ZL4>ZL5. Effective removal cross-section (ΣR), Mass removal cross-section of the ith compound (ΣR/ρ), the weight fraction of the ith component and partial densities of the samples are listed in Table 3 for examined glass samples. According to Table 3, a slight increase in ΣR values was determined as the amount of Zn increased in glass samples. On the other hand, there was no significant difference between the ΣR values of the examined glass samples. Changes in values are owing to the density differences of the glass samples, so it is educated that density plays an important role in fast neutron protection.
Figure 7. Transmission factors (TFs) as a function of shielding thickness.

Table 3. Effective removal cross sections for the glass samples

| Element | \( \frac{\Sigma R}{\rho} \) (cm²/g) | Fraction by weight (%) | Partial Density (g cm⁻³) | \( \Sigma R \) (cm⁻¹) | Fraction by weight (%) | Partial Density (g cm⁻³) | \( \Sigma R \) (cm⁻¹) | Fraction by weight (%) | Partial Density (g cm⁻³) | \( \Sigma R \) (cm⁻¹) |
|---------|-----------------------------------|------------------------|--------------------------|-------------------|------------------------|--------------------------|-------------------|------------------------|--------------------------|-------------------|
| B       | 0.0575                            | 0.194511               | 0.645777                 | 0.037132          | 0.187280               | 0.576821                 | 0.033167          | 0.180566               | 0.566979                 | 0.032601          |
| Zn      | 0.0183                            | 0.000000               | 0.000000                 | 0.047198          | 0.145370               | 0.002660                 | 0.091013          | 0.285779               | 0.005230                 |
| O       | 0.0405                            | 0.551733               | 1.831754                 | 0.074186          | 0.531221               | 1.636160                 | 0.066264          | 0.512179               | 1.608241                 | 0.065134          |
| Te      | 0.0134                            | 0.191315               | 0.635165                 | 0.008511          | 0.184202               | 0.567342                 | 0.007602          | 0.177599               | 0.557661                 | 0.007473          |
| Li      | 0.0840                            | 0.062441               | 0.207305                 | 0.017414          | 0.050100               | 0.154307                 | 0.012962          | 0.038643               | 0.121339                 | 0.010193          |
| TOTAL   | 0.137243                          | 0.122656               | 0.120630                 |                   |                        |                          |                   |                        |                          |                   |

Table 3 continued...

| Element | \( \frac{\Sigma R}{\rho} \) (cm²/g) | Fraction by weight (%) | Partial Density (g cm⁻³) | \( \Sigma R \) (cm⁻¹) | Fraction by weight (%) | Partial Density (g cm⁻³) | \( \Sigma R \) (cm⁻¹) | Fraction by weight (%) | Partial Density (g cm⁻³) | \( \Sigma R \) (cm⁻¹) |
|---------|-----------------------------------|------------------------|--------------------------|-------------------|------------------------|--------------------------|-------------------|------------------------|--------------------------|-------------------|
| B       | 0.0575                            | 0.174318               | 0.535156                 | 0.030771          | 0.168487               | 0.579597                 | 0.033327          |
| Zn      | 0.0183                            | 0.131795               | 0.404609                 | 0.007404          | 0.169849               | 0.584279                 | 0.010692          |
| O       | 0.0405                            | 0.494455               | 1.517976                 | 0.061478          | 0.477916               | 1.644033                 | 0.066583          |
| Te      | 0.0134                            | 0.171453               | 0.526361                 | 0.007053          | 0.165719               | 0.570072                 | 0.007639          |
| Li      | 0.0840                            | 0.027979               | 0.085897                 | 0.007215          | 0.018029               | 0.062020                 | 0.005210          |
| TOTAL   | 0.113922                          | 0.123451               |                         |                   |                        |                          |                   |                        |                          |                   |

The \( \Sigma R \) value of Sample ZL1 has been shown to have a maximum value between the other glass samples (Figure 8). This can be explained by its higher Li₂O content among the glass samples since Li's effective removal cross-section is bigger than Zn. In this study, we have calculated the EBF values of the selected glasses in 0.015–15MeV up to 15 MFP by utilizing the G-P fitting approach. The EBF values are plotted in Figure 9.
Figure 8. Effective removal cross-section values of the glasses with density.

Figure 9. (a–e) The exposure buildup factors in the energy region 0.015–15 MeV at the 1–15 mfp for glass samples.
The figure shows us that EBF values remain very low at first, and start rising fast as the energy level rises [40,41]. That indicates an inverse relationship between energy and EBF. Yet, at 0.6 MeV, the EBF values extended to its maximum and after that peak, it keeps decreasing even if the energy level rises. That is simply because we have different processes derived from the energy and matter interaction at different (low, mid and high) levels. Photoelectric effect grows into dominance at the low energy levels yielding an inverse effect with \( E^{3.5} \). The sample of glasses absorbs the maximum level of low energy photons as the build-up for the photons are constricted at this energy region. Compton scattering is the process that becomes a dominant incident at the intermediate energies yielding high EBF. The high EBF is because of the multiple scattering processes rather than MFP. Pair production becomes dominant when it comes to high energies yielding lower EBF as the photon energy rises [42,44]. With the highest \( Z_{eq} \) value, ZL5 yields the minimum EBF values (Figure 10).

![Figure 10. Equivalent atomic numbers of the glass samples with photon energy](image)

4. Conclusions

In summary, the modifier role of ZnO in for lithium boro-tellurite glass samples was determined by calculating mass attenuation coefficient (\( \mu/\rho \)) by XCOM software and MCNPX code. Comparing the values of XCOM and MCNPX, it can be easily seen that \( \mu/\rho \) values are in compliance with each other. In addition to the mass attenuation coefficient, \( Z_{eq} \), \( N_{el} \), HVL, TVL, MFP, TF, \( \Sigma_R \), \( Z_{eq} \), EBF shielding parameters were also calculated. According to the results of this study, \( \mu/\rho \) and \( Z_{eq} \) values are go up with increasing ZnO contribution. ZL1 glass sample has the minimum \( Z_{eq} \). Also, HVL, TVL and MFP values of the worked glass samples are increased as the photon energy goes up and decreased as the amount of ZnO additive increases. Sample ZL5 has the smallest value among the other glass samples. \( \Sigma_R \) values together with transmission factors were also examined for the glass samples. Sample ZL5 has the smallest TF values, whereas Sample ZL1 has the biggest \( \Sigma_R \) values among the glass samples. Moreover, among the selected glasses (i.e. ZL1), the one with the lowest \( Z_{eq} \) has the maximum EBF, as the one (i.e. ZL5) with the highest \( Z_{eq} \) provide the minimum EBF. In this sense, ZL5 is better than ZL1 as a radiation attenuator in terms of EBF values. The hypothesis of this study is to observe an improvement in the radiation attenuation properties of glass samples with increasing ZnO ratio. The results of this study prove the accuracy of the proposed hypothesis. The amount of increase in the ZnO additive is not very high in glass samples. Therefore, the presented results of the samples can be shed light on radiation physics medical applications and shielding research for future studies.

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