Evaluation of Respiratory Dynamics in an Asymmetric Lung Compliance Model

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Background: Unilateral lung hyperinflation develops in lungs with asymmetric compliance, which can lead to vital instability. The aim of this study was to investigate the respiratory dynamics and the effect of airway diameter on the distribution of tidal volume during mechanical ventilation in a lung model with asymmetric compliance.

Methods: Three groups of lung models were designed to simulate lungs with a symmetric and asymmetric compliance. The lung model was composed of two test lungs, lung1 and lung2. The static compliance of lung1 in C15, C60, and C120 groups was manipulated to be 15, 60, and 120 ml/cmH₂O, respectively. Meanwhile, the static compliance of lung2 was fixed at 60 ml/cmH₂O. Respiratory variables were measured above (proximal measurement) and below (distal measurement) the model trachea. The lung model was mechanically ventilated, and the airway internal diameter (ID) was changed from 3 to 8 mm in 1-mm increments.

Results: The mean ± standard deviation ratio of volumes distributed to each lung (V₁/V₂) in airway ID 3, 4, 5, 6, 7, and 8 were in order, 0.10 ± 0.05, 0.11 ± 0.03, 0.12 ± 0.02, 0.12 ± 0.02, 0.12 ± 0.02, and 0.12 ± 0.02 in the C15 group; 1.05 ± 0.16, 1.01 ± 0.09, 1.00 ± 0.07, 0.97 ± 0.09, 0.96 ± 0.06, and 0.97 ± 0.08 in the C60 group; and 1.46 ± 0.18, 3.06 ± 0.41, 3.72 ± 0.37, 3.78 ± 0.47, 3.77 ± 0.45, and 3.78 ± 0.60 in the C120 group. The positive end-expiratory pressure (PEEP) of lung1 was significantly increased at airway ID 3 mm (1.65 cmH₂O) in the C15 group; at ID 3, 4, and 5 mm (2.21, 1.06, and 0.95 cmH₂O) in the C60 group; and ID 3, 4, and 5 mm (2.92, 1.84, and 1.41 cmH₂O) in the C120 group, compared to ID 8 mm (P < 0.05).

Conclusions: In the C15 and C120 groups, the tidal volume was unevenly distributed to both lungs in a positive relationship with lung compliance. In the C120 group, the uneven distribution of tidal volume was improved when the airway ID was equal to or less than 4 mm, but a significant increase of PEEP was observed.

Key Words: airway obstruction; lung compliance; positive-pressure respiration, intrinsic; ventilation.

Introduction

Lung hyperinflation lowers the efficiency of the respiratory muscles by expanding the thorax and moves the diaphragm downwards, thus aggravating respiratory muscle fatigue [1]. In obstructive lung disease, the positive end-expiratory pressure (PEEP) is increased by airway obstruction during expiration, which leads to lung hyperinflation [2,3]. However, the mechanism of unilateral lung hyperinflation is more complex than bilateral lung hyperinflation. Unilateral...
lungs hyperinflation is mainly caused by dynamic hyperinflation which is influenced by the lung compliance, tidal volume, airway resistance, and respiratory rate [1,4]. Asymmetric lung compliance aggravates unilateral lung hyperinflation. It may lead to mediastinal shift, giant bullae rupture, and acute vital instability. A typical example is native lung hyperinflation, which is one of the major complications associated with unilateral lung transplantation [5]. In addition, there have been reports of unilateral lung hyperinflation during mechanical ventilation of patients with chronic obstructive pulmonary disease (COPD), who had asymmetrical lung compliance due to fibrosis or pneumonia of a single lung [6,7]. Here, changes in ventilatory distribution caused by asymmetric lung compliance accelerated unilateral lung hyperinflation particularly in patients who had airflow obstruction [6]. To the best of our knowledge, little is known about the respiratory dynamics during mechanical ventilation of lungs with asymmetric compliance.

In the present study, we aimed to investigate the distribution of ventilatory volume during inspiration and the influence of airway internal diameter (ID) change, by measuring respiratory variables in an asymmetric lung compliance model.

Materials and Methods

1) Lung model

The lung model was set to simulate a patient mechanically ventilated under general anesthesia. An air filter, endotracheal tube with an ID of 8 mm, connector with a variable diameter, Y-type breathing circuit, and two test lungs (Test lung 190; Maquet, Rastatt, Germany) were serially connected (Figure 1). The connector was placed to represent variable grades of distal airway obstruction. To implement asymmetrical lung compliance, one of the test lungs (lung1, L1) was manipulated to represent a normal lung (C60, static compliance 60 ml/cmH2O), a lung with low compliance (C15, static compliance 15 ml/cmH2O) or high compliance (C120, static compliance 120 ml/cmH2O). The compliance of the other test lung (lung2, L2) was set to that of a normal lung. In total, three lung models were constructed. To measure the respiratory parameters of total lung and L1, two spirometers (D-Lite™; Datex-Ohmeda, Madison, WI, USA) were set between the breathing circuit and air filter (proximal measurement) and between the Y-type breathing circuit and L1 (distal measurement), respectively. The method described by Park et al. [8] was used to introduce compliance changes to L1. At first, the cover plates of both test lungs were manipulated to establish a static compliance at 15 ml/cmH2O, 60 ml/cmH2O, and 120 ml/cmH2O. As a result, both plastic cover plates of the test lungs were either opened or fixed to establish a static compliance of 120 or 60 cmH2O, respectively, and 10 rubber bands were wound around the center of the fixed plastic cover plates to establish a static compliance of 15 cmH2O. Then, these conditions were applied to L1 of each group. Before measuring respiratory mechanics, proximally placed spirometer was used to observe static compliance. During the experiment, preset compliance changes were
applied to L₁. First, tidal volume of total lung and volumes distributed to each lung were measured proximally and distally, respectively. Second, other respiratory variables such as PEEP, plateau pressure time (P₁-P₂ time), and flow were measured proximally and distally.

2) Intervention

The lung model was ventilated using a mechanical ventilator (Dräger Fabius GS, Lübeck, Germany). Mechanical ventilation was performed using the volume-controlled mode with an inspiration to expiration ratio 1:2, an oxygen flow of 4 L/min, a tidal volume of 600 ml, a respiratory rate of 10 “breaths” per minute, and a maximum inspiratory pressure <80 cmH₂O. To observe the inspiratory plateau pressure, the inspiratory pause was set as 50% of the inspiration time (1 second). To measure the effect of airway ID change on the distribution of tidal volume during mechanical ventilation, the ID of the connector was decreased by 1-mm intervals from 8 to 3 mm. Every time the ID was changed, the new conditions were maintained for at least 1 min (10 cycles) before and 3 minutes (30 cycles) during data collection. A total of 36 conditions (three lung models, proximal and distal measurement, six IDs) were measured per cycle, and the mean values of 30 measurements at each condition (30 cycles) were calculated. Three additional cycles were measured with a spirometer distally placed at L₂ to calculate the compliance ratio between the two lungs. The compliance ratio was calculated by dividing the mean values of L₁ compliance by L₂ compliance.

3) Data collection

A data collection computer program (S5 collect®; Datex-Ohmeda Co., Helsinki, Finland) was used to obtain physical variables at a frequency of 25 Hz. Respiratory dynamics were analyzed based on this collected data. Flow, volume, and pressure were recorded as values measured by the spirometer, and static compliance was derived using the following equation:

\[ C_{\text{static}} = \frac{V_T}{P_{\text{plateau}} \cdot \text{PEEP}} \]  

\( C_{\text{static}} \) static compliance; \( V_T \) tidal volume; \( P_{\text{plateau}} \) inspiratory plateau pressure; and PEEP, positive end-expiratory pressure. The time from the start (P₁) to the end (P₂) of the inspiratory plateau phase (P₁-P₂) was calculated to evaluate the flow during the inspiratory pause.

4) Statistical analysis

Statistical analyses were performed using SPSS version 18.0 (SPSS Inc., Chicago, IL, USA). Differences between and within groups were analyzed using two-way and one-way analysis of variance (ANOVA), respectively. Post-hoc analyses were performed if the ANOVA results showed statistically significant differences. Depending on the results of Levene’s test, a Bonferroni correction for equal variance or a Tamhane’s T2 for unequal variance was used as the post-hoc test. The threshold for statistical significance in all tests was set at \( P < 0.05 \).

Results

The ratio of the volume distributed to the two lungs \( (V_{L1}/V_{L2}) \) was proportionate to the ratio of lung compliance \( (C_{L1}/C_{L2}) \) in all groups (Table 1). \( V_{L1}/V_{L2} \) and \( C_{L1}/C_{L2} \) were similar among the different airway IDs in C15 and C60 groups. However, in C120 group, \( V_{L1}/V_{L2} \) (P < 0.001) and \( C_{L1}/C_{L2} \) (P < 0.001) were significantly reduced at airway ID of 3 and 4 mm when compared with airway ID 8 mm. The total tidal volume (volume proximally measured) and volume distributed to L₁ is summarized in Table 2.

The distally measured (P₁-P₂) times were significantly shorter than those measured proximally in C15 and C60 group, except for an airway ID of 3 mm (Figure 2). The proximally measured (P₁-P₂) times were comparable between groups (Figure 3A) and the distally measured (P₁-P₂) time durations were negatively correlated to lung compliance (Figure 3B).

In the C120 group, a PEEP >1 cmH₂O was observed for all IDs. PEEP was significantly increased for an
Table 1. Comparison of $V_{L1}/V_{L2}$ and $C_{L1}/C_{L2}$ according to the airway internal diameter

| ID (mm) | C15 group | C60 group | C120 group |
|---------|-----------|-----------|------------|
|         | $V_{L1}/V_{L2}$ | $C_{L1}/C_{L2}$ | $V_{L1}/V_{L2}$ | $C_{L1}/C_{L2}$ | $V_{L1}/V_{L2}$ | $C_{L1}/C_{L2}$ |
| 3       | 0.10 ± 0.05 | 0.10     | 1.05 ± 0.16 | 1.05          | 1.46 ± 0.18 | 1.67          |
| 4       | 0.11 ± 0.03 | 0.12     | 1.01 ± 0.09 | 1.03          | 3.06 ± 0.41 | 2.74          |
| 5       | 0.12 ± 0.02 | 0.12     | 1.00 ± 0.07 | 1.02          | 3.72 ± 0.37 | 3.08          |
| 6       | 0.12 ± 0.02 | 0.13     | 0.97 ± 0.09 | 1.00          | 3.78 ± 0.47 | 3.32          |
| 7       | 0.12 ± 0.02 | 0.13     | 0.96 ± 0.06 | 1.00          | 3.77 ± 0.45 | 3.26          |
| 8       | 0.12 ± 0.02 | 0.13     | 0.97 ± 0.08 | 1.00          | 3.78 ± 0.60 | 3.39          |

Values are presented as mean ± standard deviation or mean, as appropriate.

$V_{L1}$: volume distributed to lung1; $V_{L2}$: volume distributed to lung2; $C_{L1}$: static compliance of lung1; $C_{L2}$: static compliance of lung2; ID: internal diameter.

*Static compliance of lung1 was manipulated as 15 ml/cmH$_2$O; Static compliance of lung1 was manipulated as 60 ml/cmH$_2$O; Static compliance of lung1 was manipulated as 120 ml/cmH$_2$O; Three additional cycles were measured with a spirometer distally placed at lung2 to calculate the compliance ratio between the two lungs; $P < 0.05$ vs. airway internal diameter of 8 mm.

Table 2. Difference of lung1 volume between groups at increasing internal diameters of airway

| ID (mm) | C15 group | C60 group | C120 group |
|---------|-----------|-----------|------------|
|         | Total lung | Lung1     | Total lung | Lung1     | Total lung | Lung1     | Total lung | Lung1     |
| 3       | 524.6 ± 25.8 | 59.4 ± 17.9 | 530.5 ± 19.0 | 272.1 ± 16.4 | 551.0 ± 17.1 | 307.9 ± 12.1 |
| 4       | 535.2 ± 27.8 | 55.2 ± 10.2 | 541.6 ± 21.8 | 272.4 ± 9.3  | 519.9 ± 15.8 | 401.6 ± 16.0 |
| 5       | 541.5 ± 28.8 | 56.3 ± 9.7  | 549.3 ± 24.4 | 274.8 ± 9.2  | 534.8 ± 17.1 | 428.2 ± 15.8 |
| 6       | 544.2 ± 27.9 | 60.4 ± 4.7  | 552.9 ± 24.2 | 272.6 ± 8.9  | 543.3 ± 18.1 | 432.7 ± 18.9 |
| 7       | 544.7 ± 27.8 | 60.2 ± 6.4  | 557.3 ± 23.4 | 274.2 ± 10.7 | 547.2 ± 19.0 | 434.3 ± 18.5 |
| 8       | 549.8 ± 28.6 | 59.3 ± 8.1  | 557.2 ± 24.2 | 274.9 ± 10.0 | 549.3 ± 18.2 | 433.7 ± 20.4 |

Values are presented as mean ± standard deviation.

ID: internal diameter.

*Static compliance of lung1 was manipulated as 15 ml/cmH$_2$O; Static compliance of lung1 was manipulated as 60 ml/cmH$_2$O; Static compliance of lung1 was manipulated as 120 ml/cmH$_2$O; $P < 0.05$ vs. airway internal diameter of 8 mm.

ID ≤5 mm (cross sectional area ≤19.6 mm$^2$) compared with an ID of 8 mm in the C120 (P < 0.001) and C60 (P < 0.001). In the C15 group, a statistically significant increase of PEEP occurred in ID 3 mm (cross sectional area, 7.1 mm$^2$), compared to ID 8 mm (P < 0.001). When the distal measurements of PEEP values were compared between lungs, C15 and C60 groups were comparable, while C120 group was significantly higher than that in the other models (Figure 4). Flow-time curve of distal measurement in the three groups are shown in Figure 5. The inspiratory flow of L1 in C15 and C60 groups was maintained ≤5 and ≤10 ml/s, respectively. This value was between 10 and 20 ml/s in the C120 group, showing the larger volume distributed to L1 compared to other groups. Flow limitation was observed in smaller airway IDs, which was most significant in C120 group.

Discussion

Without airway obstruction, the tidal volume was distributed to each lung according to its compliance (Table 1). However, in the C120 group, although the total tidal volume was achieved, the volume distributed to L1 was significantly decreased at ID 3 and 4 mm, compared to ID 8 mm (Table 2). In visual inspection, a significant reduction of flow was observed in airway ID 3 and 4 mm in C120 group (Figure 5).

https://doi.org/10.4266/kjccm.2016.00738
While other groups did not show a significant reduction in the tidal volume distributed to $L_1$, the distal measurement in C120 did show indications of statistically significant decreases at airway ID values of 3 and 4 mm (Table 2). The proportion of tidal volume distributed to $L_1$ in the C120 group was reduced at airway ID 3 and 4 mm. This signifies amelioration of the asymmetry of ventilatory distribution, which can be explained by a few factors. First, differences in the expansion rates of both lungs can be inferred by the differences of the time constants according to their compliance. The time constant is a product of the compliance and resistance and is therefore proportional to both compliance and resistance. Assuming that the resistances of both lungs are similar, the time constants of both lungs are proportional to their compliance. Having a small time constant means increased speed and pressure since the equilibrium volume is reached more quickly, and flow to that compartment will stop earlier. Meanwhile, having a larger time constant means that the time to reach the equilibrium volume is longer, and flow to that compartment will persist longer until equilibrium volume is reached [9-11]. Differences in time constants according to the differences in compliance can be confirmed by the $(P_1-P_2)$ time results (Figure 3B). When distally measured, $(P_1-P_2)$ times were significantly longer than proximally measured values in C15 and C60 groups; however, distally measure $(P_1-P_2)$ times of C120 group were comparable with proximally measured times.

**Figure 2.** Change of plateau pressure time in (A) C15, (B) C60, and (C) C120 groups. $P_1$: start point of plateau pressure; $P_2$: end point of plateau pressure; C15: static compliance of lung1 was manipulated as 15 ml/cmH$_2$O; C60: static compliance of lung1 was manipulated as 60 ml/cmH$_2$O; C120: static compliance of lung1 was manipulated as 120 ml/cmH$_2$O. *P < 0.05 vs. proximal measurement.

**Figure 3.** Change of plateau pressure time at (A) proximal and (B) distal measurements during change of internal diameter. $P_1$: start point of plateau pressure; $P_2$: end point of plateau pressure; C15: static compliance of lung1 was manipulated as 15 ml/cmH$_2$O; C60: static compliance of lung1 was manipulated as 60 ml/cmH$_2$O; C120: static compliance of lung1 was manipulated as 120 ml/cmH$_2$O. *P < 0.05 vs. airway internal diameter of 8 mm.
measured values (Figure 2). From this finding, it can be inferred that the flow at L₁ stops earlier than proximal measurement in the C15 and C60 groups. But in the C120 group, the flow at L₁ persists until the flow at the proximal measurement stops, indicating that L₁ in this group may not have enough time to reach the equilibrium volume distributed according to the compliance.

Second, a decrease in the airway ID causes a limitation of flow and increases the time required for the lungs to reach their equilibrium volume. When the flow rate decreases, the time required to fill a certain lung volume is increased, which makes it more difficult for the lung with the larger time constant (i.e., the lung with higher compliance if the airway resistance is the same) to fill the same volume. The flow-time curve of the three distally measured groups (Figure 5) shows that at an airway ID was equal to or less than 4 mm, all groups failed to reach the tidal volume within the inspiration period.

It is widely known that reducing the tidal volume and respiration rate ameliorates lung hyperinflation, and these variables can be controlled by mechanical ventilators [12-14]. This is true even in the asymmetrical lung compliance cases in COPD patients reported by Kollef and Turner [6]. However, little is known about how airway diameter changes, such as those in airway obstruction, affect unilateral lung hyperinflation. Anglès et al. [15] reported that after unilateral lung transplantation, the incidence of hyperinflation in the remaining native lung reached 64% during hospitalization. Lung hyperinflation led to longer ICU stays and higher mortality rates (67%

![Figure 4](https://example.com/image4.png)

**Figure 4.** Distal measurements showing response of positive end-expiratory pressure according to internal diameter change. C15: static compliance of lung1 was manipulated as 15 ml/cmH₂O; C60: static compliance of lung1 was manipulated as 60 ml/cmH₂O; C120: static compliance of lung1 was manipulated as 120 ml/cmH₂O. aP < 0.05 vs. airway internal diameter of 8 mm. Cross section area: internal diameter of 3, 4, 5, 6, 7 and 8 mm were measured to be 7.1, 12.6, 19.6, 28.3, 38.5, 50.3 mm² respectively; bP < 0.05 vs. C60 group.

![Figure 5](https://example.com/image5.png)

**Figure 5.** Flow-time curve of distal measurement in (A) C15, (B) C60, and (C) C120 groups. The area under the curve represents volume distributed to lung1. ID: internal diameter; C15: static compliance of lung1 was manipulated as 15 ml/cmH₂O; C60: static compliance of lung1 was manipulated as 60 ml/cmH₂O; C120: static compliance of lung1 was manipulated as 120 ml/cmH₂O.
vs. 20%) compared with patients without lung hyperinflation.

The results of the present study can be applied to patients under these conditions. However, improving the ventilatory distribution by reducing the airway ID ≤4 mm is not a desirable treatment for the mechanical ventilation of COPD patients with asymmetrical lung compliance. Because PEEP was significantly increased for an airway ID ≤5 mm, reducing the airway ID ≤4 mm may further exacerbate auto-PEEP. Clinical applications to limit volume redistribution in lungs with asymmetric compliance should focus on appropriate flow limitations that can maximize the time constant difference between the two lungs or on reducing the inspiratory pause time. The appropriate inspiratory flow rate for a patient may vary depending on the ratio of inspiration to expiration, respiratory rate, appropriate tidal volume, and lung compliance. As such, additional clinical studies are required to elucidate the appropriate values of these variables.

The limitation of our experimental model is that the model does not reflect the airway obstruction that occurs during expiration in obstructive lung disease. As such, our results should be limited to demonstrating the mechanism of unilateral lung hyperinflation during inspiration. Moreover, although the effects of respiratory muscles were not taken into account by assuming mechanical ventilation under general anesthesia, the interactions that may occur between both lungs due to the limited space of the thoracic cavity were not considered. Therefore, the measured values in the present study should be regarded as relative values showing the relationship between respiratory mechanical variables rather than absolute values. On the other hand, the fact that the respiratory variables were measured separately in unilateral lungs is a significant advantage of the present study as compared with animal studies or clinical trials.

In conclusion, we were able to show that the distribution of volume during inspiration was positively correlated to lung compliance. The uneven distribution of volume might be reduced by changing the airway diameter equal to or less than 4 mm (cross sectional area, 12.6 mm²); however, this may exacerbate auto-PEEP.

Acknowledgments

This study was presented at the Critical Care Symposium of the World Federation of Societies of Intensive and Critical Care Medicine (WFSICCM) on August 31, 2015 in Seoul, Korea.

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