An Investigation on Strength Degradation of Gfrp Laminates Under Environmental Impact

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Abstract The usage and replacement of conventional materials with polymer composite materials for engineering applications is always questioned by the end user, unless otherwise supported by the authentic published research. The reinforcement materials are highly hygroscopic; the matrix material provides protection to the reinforcement. Since the edges of composite components and surface are exposed to environment, water molecules travel along the reinforcement, which can damage the interfacial bonding, further the performance of the composite laminate may get affected. In this scenario the investigation related to this aspect, requires quantitative assessment which is carried out to estimate the damage associated by accelerated simulation of the real time situation provides information to extrapolate the effects of the moisture associated damage to the composite laminate. In this present work an attempt has been made in establishing the investigation procedure to estimate the influence of moisture absorption on strength degradation coupled with temperature. To estimate the life cycle time of polymer composite components such as marine boats and components related to submarine applications. From the test results, it is established reduced that the tensile strength and flexural modulus were reduced significantly, of the specimens subjected to water soaking and varying temperature.

Keywords Glass Fibre Reinforced Polymer Composite (GFRP), Resin Transfer Moulding (RTM), Tensile and Bending Test

1. Introduction

Glass fibre reinforced plastic materials are of low cost, light in weight, have good mechanical properties thus having potential to use them for structural applications such as equipment for chemical plants and pipelines which are subjected to aggressive environment. Therefore, the information comprising the effects of moisture absorption at higher temperatures on the mechanical properties of glass reinforced composites is very essential. Glass fibre reinforced polymer composites (GFRP) show relatively low degradation in various corrosive environments in the unstressed state, however, they are very susceptible to stress corrosion, especially in dilute mineral acid environment[1,2]. Krystyna Imlinska discussed in detail about the environmental stress cracking characteristics of GFRP and (A-G) FRP which were studied using CT (fracture mechanics) samples under.

Constant tensile load and water environment. For GFRP the characteristics of crack length as a function exposure time (upto3 months). Ductile aramid fibres seemed to protect the glass fibre reinforcement from stress cracking due to higher chemical resistance and complex failure mechanisms[3]. Accelerated environmental ageing study of polyester/glass fibre reinforced composites (GFRPCs) were studied based on two kinds of alternating cycles, which provided humidity, temperature and ultraviolet radiation. The study dynamic mechanical analysis, for a range of temperatures and frequencies under tensile and three-point bending loadings, revealed that the aged materials gained in stiffness, whereas a small deterioration in strength was found[6]. Tensile and flexural strength of bamboo fibre reinforced polypropylene composite and bamboo-glass fibre reinforced polypropylene hybrid composite were reduced[8]. On similar way experimental work has been done with polyester-glass fibre reinforced composites. The environmental stress cracking failure due to temperature and moisture has been studied for glass fibre reinforced composites[9]. Moisture does not only affect the adhesive bond of the bonded system in service, but also during the application of FRP on concrete surface. Tests on CFRP bonded to concrete with initially damp surface using a modified cantilever beam indicated reduction in bond strength when compared to specimens with initially dry concrete surface[11]. Since the failure under effect of moisture generally occurs by either concrete delaminating
or concrete-epoxy interface separation. The effects of variable moisture conditions on the fracture toughness of concrete/FRP bonded system are studied by means of the peel and shear fracture toughness determined from the conditioned test specimens. Moisture conditions can result in strength degradation [13]. The main objective of this work is to investigate the effects of hydro aging and hydrothermal aging environmental (constant temperature water bath) conditions on the performance and durability of glass fibre reinforced polymer.

2 Experimental Setup

2.1. Preparation of Test Samples

The specimens for the present work are prepared using RTM Machine. The specifications for the laminate preparation are (i) injection pressures, 30-40 psi. (ii) Curing Temperature – room temperature. The laminates obtained by RTM is the size 300mm x 300mm x 8mm. These laminates are sliced to standard ASTM 638 tensile specimens of dimensions 250 mm x 30 mm x 8 mm (as shown fig.1). These Specimens are immersed in the water bath at room temperature for a period of 180 days and other set of specimens immersed in constant temperature water bath which is maintained at 60°C for a period of 60 days (as shown fig.2&3).

Specifications of materials used in the composite laminate:

- Matrix: General purpose polyester resin (commercial Grade)
- Glass fibre: Saint Gobain makes E-Glass
- Chopped strand mat (stitched) 450g/s-m, the laminates are prepared with RTM process. The volume fraction of the reinforcement loading about 40% which is found by Burn test the remaining is matrix About 60%

2.2. Experimentation

The present work is focused to understand influence of the water soaking time which leads to reduce GFRP composite laminate’s tensile strength. The experiments were carried out on number of specimens moulded by
RTM and exposed to water bath which is maintained at room temperature and constant temperature at 60°C. Every 30 days specimens are taken from bath which are exposed to room temperature and for every 10 days specimens are taken from bath which is maintained at 60°C temperature, and carried out tensile tests, 3-point bending tests to determine the young’s and flexural modulus which are exposed to various periods.

3. Results-Tensile and Flexural Modulus

The laminates are exposed to water bath at room temperature, and are tested with tensile and 3-point bending test. This is repeated for every 30 days, the results are noted and the same displayed in graphs 1&3. The laminates are exposed at constant temperature 60°C, tested with tensile and 3-point bending test. This is repeated for every 10 days, and plotted graphs 2&4 with the obtained results. From stress-strain graphs tensile young’s modulus of the specimens are calculated with in the elastic limits choosing three points in a straight line portion and shown in graphs 5and 6. The specimen exposed for 60°C for 10 days tensile modulus is calculated as

Young’s Modulus (10 Days),

\[ E_t = \frac{8}{0.7+10/0.9+10.5/1} \times 100 \text{ N/mm}^2 \]

= 1.101 Gpa

Flexural modulus of elasticity is calculated with graphs 3 and 4 for specimens exposed at room temperature and constant temperature 60°C with different exposure times by using following equation and the results are shown in graphs 5 and 6.

\[ E_f = \frac{L^3 m}{4bd^3} \]

\[ L = \text{Support span (lamine length), (mm)} \]
\[ m = \text{slope of the deflection curve in initial straight portion (N/mm)} \]
\[ b = \text{Width of test beam, (mm)} \]
\[ d = \text{Depth of tested beam, (mm)} \]

The specimen exposed at room temperature for 180 days flexural modulus is calculated as

\[ E_f = \frac{L^3 M}{4bd^3} \]
\[ E_f = 220\times 0.0333\times 10^3/4\times 30\times 8 \]

= 5.7764 Gpa

![Figure 5. Tensile testing on UTM](image)

![Figure 6. Three point bending testing on UTM](image)

Graph 1. Tensile test—specimens exposed to room temperature (stress VS Strain at various exposed time 30 to 180 days)

Graph 2. Tensile test—Specimen exposed to constant temperature 600°C (stress VS Strain at various exposed time 10 to 60 days)
4. Discussions

The experimental results reveal that the GFRP (E-Glass/Polyester) samples subjected to water absorption at room temperature (results as shown in Graph 5) the tensile modulus has been rapidly reduced till 90 days and there a moderate reduction in it, whereas the flexural modulus has sharp reduction in the first 60 days and then a gradual reduction is observed. The samples subjected to aging at the constant temperature water bath (60°C) showed a hyperbolic decrement in the tensile strength and the flexural modulus (as shown in Graph 6). On the whole it was observed that tensile modulus decreased to some extent with the presence of moisture and temperature.

There is significant reduction in modulus because of loosing bonding strength of the polyester resin and fibre inter phase at room temperature. It is clear that the flexural modulus rapidly decreases with hydro aging and hydrothermal aging, because moisture generally affects any property which is dominated by the matrix and/or interface. However the flexural strength being a fibre dominated property the strength reduction occurs only if the fibres themselves are affected by hydrothermal environmental conditions.

The GFRP specimen showed a 66.7% reduction in the Young’s modulus due to the increase in the water bath temperature, i.e., there is a considerable effect of the bath temperature on the mechanical properties of the GFRP composites.

5. Conclusions

From the investigation it is observed that there is a remarkable reduction in mechanical strength (Young’s and flexural modulus) is observed in GFRP composite laminates which are subjected to different environmental conditions a exposure time. The flexural strength values of the specimens are decreased with exposure period of 60days in water at constant temperature. As per the results initially rapid reduction in mechanical properties is observed and
gradual decrease is observed during next phase.

The following important conclusions were drawn from test results.

a). The presence of moisture or water particles in the matrix, fibre-matrix interface and also attack on the glass fibres are all the reason for reduction of properties is due to interfacial bond damage.

b). The tensile and flexural modulus reduction is more in Hygrothermal aging when compare to hydro aging because the Temperature accelerated the aging processes.

c). It is worth noticing that aging at higher temperatures caused colour change in samples.

d). The change in tensile properties of laminates during aging are due to of Hygrothermal degradation of glass fibre, matrix interface.

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