The role of interaction between low molecular weight neutral organic compounds and a polyamide RO membrane in the rejection mechanism†

Muxue Zhang, a Lauren Breitner, b Kerry J. Howe b and Daisuke Minakata a,*

Reverse osmosis (RO) is a membrane technology that separates dissolved species from water. RO has been applied for the removal of chemical contaminants from water and is employed in wastewater reclamation to provide an additional barrier to improve the removal of trace organic contaminants. The presence of a wide variety of influent chemical contaminants and the insufficient rejection of low molecular weight neutral chemicals by RO calls for the need to develop a comprehensive model that predicts the rejection of various chemicals in RO. Yet the role of the interaction between neutral organic compounds and a RO membrane, and how the functional groups of organic compounds affect the interaction have not been fully elucidated. In this study, we first constructed a molecular model for a reference polyamide (PA) membrane. We then investigated the impact of explicit water molecules and PA membrane functionality on the membrane structure using quantum mechanical calculations. We examined solvent–membrane interactions and then solvent–membrane–solute interactions using two neutral test solutes, arsenic and boron, by comparing the theoretically calculated aqueous-phase free energies of interaction with their experimental values. Finally, the validated PA membrane model was used to calculate the free energies of interaction for a wide variety of organic compounds such as haloalkanes, haloalkenes, alkybenzenes and halobenzenes, which correlated with the experimentally obtained mass transfer coefficients. The correlation indicates that the interaction between organic compounds and PA membranes plays a critical role in the rejection mechanism.

Introduction

The presence of a wide variety of trace chemicals called chemicals of emerging concern (CECs) in effluents of wastewater1–4 presents challenges to the practice of direct potable reuse, in which reclaimed wastewater is introduced directly to the potable water supply distribution system, or indirect potable reuse, in which reclaimed wastewater is introduced to the potable water supply system after passing through an environmental buffer.5

Reverse osmosis (RO) is an attractive and promising membrane-based treatment process that can be applied for the removal of CECs and employed after microfiltration (MF)/ultrafiltration (UF) processes in typical wastewater reclamation schemes.6–9 While RO rejects a wide variety of CECs with greater than 99% rejection efficiency, neutral compounds with a molecular weight (MW) less than 200 g mol−1 have poor rejection efficiencies.7

The rejection of organic compounds by non-porous dense RO membranes is explained by two major factors: (1) solute–membrane interactions and (2) the diffusion of solute through the membrane active layer.10 The former interaction refers to the thermodynamic properties of solute–membrane interactions, i.e., the coefficient describing the partitioning of solute between membrane and water. The latter factor, diffusion, refers to the kinetics of solute movement in membranes. In general, strong interactions between organic compounds and membranes are dominant for the mass transfer of small molecules from water to membranes11 and increase the concentration of the solute within the membrane, which decreases the rejection efficiency.12,13 Three major solute–solvent–membrane interactions that have been distinguished are (1) steric exclusion, (2) electrostatic interactions, and (3) an affinity between the solute and membrane.12,14,15 The affinity component includes hydrophobic attraction, hydrogen bonding, and the dielectric effect of water molecules and is described by the free energy of interaction between the solute.
and the membrane in the aqueous phase.\textsuperscript{14} In the non-porous solid RO membrane, the diffusion of an organic compound occurs mainly through polyamide rich domains than through the water-filled voids of membrane\textsuperscript{11} and is also affected by the membrane–solute interaction. In general, an independent measurement of each parameter in very thin-film composite materials used for RO is technically challenging.\textsuperscript{11}

Molecular mechanics- and quantum mechanics (QM)-based computational chemistry tools are robust techniques that can be used to characterize membrane properties and provide mechanistic insights into solute–solvent–membrane interactions. Classical molecular modeling and dynamics (MM/MD) have been used to construct RO membrane structures and characterize the membrane properties to engineer the design of membrane materials and simulate the rejection of solute.\textsuperscript{15–20} Studies using MD techniques have been very successful at simulating cross-linked polyamide (PA) membranes and related polymer materials. Xiang et al. (2013) found the critical role of carboxylate group of a polyamide membrane surface for binding with a foulant, alginate, through their MD study.\textsuperscript{21} Ghoufi et al. (2017) has recently used MD simulation to qualitatively show the significant contributions from solute–membrane (−4 to −3 kJ mol\textsuperscript{−1} of interaction energy) and solute–water (−5 to −2 kJ mol\textsuperscript{−1}) interactions to the experimentally determined partition coefficients (e.g., 0.09 for 4aminopiperidine, 0.15 for pinacolone, and 0.81 for methylisobutyl ketone) based on the FTIR spectroscopy measurement with SWC4+ RO membrane at 21.0 °C and 11–17 bar of trans-membrane pressure differences.\textsuperscript{22} Among compounds that have the same $M_W$, a compound that strongly interacts with membranes has the largest partition coefficient (i.e., lowest rejection by the membrane). However, energies determined by MM/MD only provide qualitative measures and those energies may not be used for the prediction of organic compounds’ rejections. In contrast, \textit{ab initio} and density functional theory (DFT) QM calculations provide reliable thermodynamic properties based on statistical thermodynamics.\textsuperscript{23} If a membrane segment is properly assigned and simulations of solute–solvent–membrane interactions are performed with a reasonable computational demand, this approach can be used to systematically calculate interaction energies between the membrane and a wide variety of CECs, which are then fed into a predictive model.

In this study, we use QM calculations to construct various segments of a PA membrane by cross-linking 1,3-diaminobenzene (MPD) and 1,3,5-benzenetricarbonyl trichloride (TMC) and examining the impacts of hydrogen bonds on the functional groups of the PA molecular model membrane. We use arsenic acid (H$_3$AsO$_3$) as a test neutral chemical to study the membrane–solute–solvent interaction because of the availability of its experimental parameters and use a similar compound of boron (H$_3$BO$_3$) to enhance the findings. We also calculate the aqueous-phase free energies for interactions of the membrane–water–solute interaction for a wide variety of organic compounds and compare the resultant thermodynamic properties with the mass transfer coefficients obtained from our previous experiments.

### Materials and methods

#### Mass transfer coefficients of solutes

The rejection of organic compounds, $Re_j$, by RO can be quantified using the ratio of organic compound concentrations in permeate, $C_p$, and feed solution, $C_f$, as shown in eqn (1)\textsuperscript{24}

$$Re_j = 1 - \frac{C_p}{C_f}$$

where $C_p$ is the ratio of the flux of solute to that of water and can be expressed as

$$C_p = \frac{J_k}{J_w} = \frac{k_s (\beta C_p - C_f)}{k_w (\Delta P - (\beta \Pi_f - \Pi_p))}$$

where $k_s$ and $k_w$ are the solute and water mass transfer coefficients, respectively, $\beta$ is the concentration polarization factor, $\Delta P$ is the pressure applied across the membrane, $\Pi_f$ and $\Pi_p$ are the osmotic pressures of feed and permeate solutions. Given that $\beta$, $\Delta P$, $\Pi_f$ and $\Pi_p$ are determined by the operating conditions and $k_w$ is a membrane property, $k_s$ is the fundamental property that reflects the rejection of a target organic compound resulting from the partition and diffusion. The partition coefficient of an organic compound between the membrane matrix and aqueous-phase has a proportional relationship with the aqueous-phase free energy of interaction\textsuperscript{24,25,26}

$$K = \frac{C_{\text{mem}}}{C_{\text{aq}}} \exp\left(-\Delta G_{\text{intr}}^{\text{ff}}\right)$$

where $K$ is the partition coefficient, and $C_{\text{mem}}$ and $C_{\text{aq}}$ are the concentrations of organic compound in the membrane matrix and in the aqueous phase, respectively. The diffusion of an organic compound in the membrane matrix is also affected by the interaction,\textsuperscript{23} and therefore, the $k_s$ values for organic compounds might thus have a proportional relationship with the aqueous-phase free energy of interaction if the solute–membrane interaction mechanism corresponds to the rejection trend.

$$\ln k_s \propto \Delta G_{\text{intr}}^{\text{ff}}$$

The aqueous-phase free energy of interaction, $\Delta G_{\text{aq}}^{\text{intr}}$ (kcal mol\textsuperscript{−1}), is the free energy difference associated with the differences in the interactions of the solute in the aqueous phase and in the membrane matrix

$$\Delta G_{\text{aq}}^{\text{intr}} = G_{\text{aq}}^{\text{solvent-membrane-H2O}} - (G_{\text{membrane-H2O}} + G_{\text{solvent}})$$

where $G_{\text{solvent-membrane-H2O}}$, $G_{\text{membrane-H2O}}$, and $G_{\text{solvent}}$ is the aqueous-phase free energy of the membrane with the solute in the presence of $n$ explicit water molecules ($0 \leq n$), the membrane interacting with $n$ explicit water molecules, and the solute, respectively.\textsuperscript{27}

For the detailed calculation procedure see the ESI, Text S1.\textsuperscript{‡} We use the subscripts ‘calc’ and ‘exp’ to indicate the theoretically calculated and experimentally obtained aqueous-phase free energies of interaction, respectively. The experimentally determined $k_s$ values for various organic compounds were determined from a bench-top laboratory scale experiment and...
reported in our other publications.\textsuperscript{28,29} Briefly, the experiments were done with a bench-top system containing multiple flat sheet membranes at three operational pressures, constant solution temperature (20 °C), and a constant pH of 6.5. The concentrations of feed and permeate after the steady-state condition were measured for organic compounds and the rejection efficiencies were determined. Using eqn (1) and (2), the $k_s$ values were determined for various RO membrane products. In this study, we only used the $k_s$ values obtained through a ESPA2-LD PA brackish water RO membrane (Hydranautics) because this was used as a reference membrane. The detailed descriptions of $k_s$ values about the organic compounds will be given below.

Conformer search and geometry optimization

The energetically stable conformers of our PA membrane model structure and their interactions with solute and water were first searched with molecular mechanics using the Merck Molecular Force Field (MMFF)\textsuperscript{30} employed in the Spartan’16 Parallel Suite (Wavefunction Inc.),\textsuperscript{31} which has been widely used for various conformer searches including our previous study,\textsuperscript{32–33} and the global minimum energies of the conformers were then calculated. Second, the structures of the top five conformers were further optimized at the B3LYP\textsuperscript{34,35} level with the 6–31*G basis set using Spartan’16. Third, each optimized conformer structure was used as the input gaseous-phase geometry for optimization and frequency calculations at the M06-2X/cc-pVDZ level\textsuperscript{36} using Gaussian 09, revision D.1.\textsuperscript{37} Finally, using the optimized gaseous-phase structure as a starting point, the aqueous-phase structure was optimized, and the frequencies were calculated at the same level (\textit{i.e.}, M06-2X/cc-pVDZ)\textsuperscript{38} using an implicit universal solvation model (SMD)\textsuperscript{40} at 20 °C (293.15 K). The detailed procedures for the structural optimization and frequency calculations are given in ESI Text S2.\textsuperscript{†}

Results and discussions

Membrane structures

Based on previous research, we built the base molecular models for the PA membrane active layer by connecting TMC and MPD monomers in a ratio of 1 : 1 to generate cross-linked ring and linear structures with four-units.\textsuperscript{15,16,42} Models consisting of two- and six-unit TMC and MPD cross-linked monomers, elemental composition of the membrane model, and the impact of side chains resulting from larger PA membrane structures were also investigated [ESI Text S3]. To maintain acceptable computational time consumption for the subsequent QM calculations and focus on the effects of the solute–membrane interactions on the critical membrane structure, we used the four-unit model for the following study. The four-unit PA membrane model contained two TMC and two MPD molecules with two carboxylic functional groups, which can dissociate depending on the solution pH.\textsuperscript{43–45} The charge of the carboxylic functional groups of the PA membrane model affects the membrane structure. To evaluate the impact of the dissociation of carboxylic functional group(s) on the PA membrane structure, we thus built three models: (1) a PA membrane containing two non-dissociated carboxylic functional groups (PA-0), (2) a PA membrane containing one dissociated and one non-dissociated carboxylic functional group (PA-1), and (3) a PA membrane containing two dissociated carboxylic functional groups (PA-2).

Water–membrane interactions and the free energy of interaction

To investigate the water–membrane interaction, we added several explicit water molecule(s) that interact with the PA membrane in addition to the implicit solvation model. In general, the implicit solvation model does not account for long-range dispersion interactions in the outer solvation shell and the addition of explicit water molecule(s) is therefore recommended to explicitly account for H-bonds.\textsuperscript{46} A detailed discussion on the impact of water molecules on the three PA membrane structures is provided in the ESI Text S4.\textsuperscript{†} Fig. S8 in ESI† plots the calculated gaseous- and aqueous-phase free energies of interaction ($\Delta G_{\text{gas,calc}}$-H2O and $\Delta G_{\text{aq,calc}}$-H2O) against the number, $n$, of explicit water molecule(s) for the PA-0, PA-1, and PA-2 membrane models. We found that as more explicit water molecules were added, both the gaseous- and aqueous-phase free energies of interaction for PA-1 and PA-2 decreased. For example, the aqueous-phase free energy of interaction per mole of 4-unit membrane model with/without explicit water molecules decreased from $–0.41$ kcal mol$^{-1}$ for PA-1 with 1 explicit water molecule to $–3.52$ kcal mol$^{-1}$ with 6 explicit water molecules. In contrast, the free energy of interaction for PA-0 increased as a greater number of explicit water molecules were added. A similar trend was observed for the gaseous-phase free energy of interaction. Since greater negative values of free energy of interaction indicate greater stability, these results suggest that dissociated carboxylic functional groups were stabilized with the addition of explicit water molecules by forming additional hydrogen bonds. An increase in the $\Delta G_{\text{aq,calc}}$-H2O value when $n = 6$ for PA-0 (both carboxylic functional groups are non-dissociated) because the addition of extra explicit water molecules created a cluster and decreased the resultant $\Delta G_{\text{aq,calc}}$-H2O, which increases the $\Delta G_{\text{aq,calc}}$-H2O for PA-0 based on the eqn (5).

To validate the theoretically calculated aqueous-phase free energy of interaction for the membrane–water system, we calculated the free energy of interaction using eqn (6) based on the literature-reported, experimentally obtained partition coefficient of water in a PA membrane.\textsuperscript{46}

$$\phi = (1 – \lambda)^2 \exp \left( -\frac{\Delta G_{\text{gas}}}{R T} \right) \quad (6)$$

Here, the partition coefficient, $\phi$, is defined as the ratio of the solute concentration in the membrane matrix (membrane pores) to that outside the membrane (\textit{i.e.}, in the solvent) with the dimensionless unit. The parameter $\lambda$ is the ratio of the solute radius to the membrane pore radius, $R$ is the gas constant (0.001987 kcal K$^{-1}$ mol$^{-1}$), and $T$ is the absolute temperature (K). Although eqn (6) was developed for porous NF membranes\textsuperscript{44} and no governing equation incorporates size-based exclusion for non-porous RO membranes, the sizes of the solute and
Solvent molecules also play a critical role in their partitioning in non-porous membranes. We thus used eqn (6) to estimate the free energy of interaction for the non-porous RO membrane. The radius of a water molecule was calculated (1.95 Å) based on the volume of water (18.8 cm$^3$ mol$^{-1}$) estimated using the LeBas method, and we used a membrane pore radius of 3 Å, which was calculated from a MD study. A partition coefficient of 0.275 was obtained for the FT-30 membrane from Suzuki et al. (2015), which also used a membrane model with a TMC to MPD ratio of 1:1 to simulate PA membrane hydration. The experimental partition coefficient was reported as 0.29. Using these data described above, we obtained a value of $-0.47$ kcal mol$^{-1}$, which is very close to the values obtained from our theoretical calculations with various membrane structures in the presence of explicit water molecules. For example, we obtained $-0.41$ kcal mol$^{-1}$ for the aqueous-phase free energy of interaction for the PA membrane PA-1 in the presence of one explicit water molecule. Based on 1.39 g cm$^{-3}$ of a total mass density of waters reported by Suzuki et al. (2015), we calculated the number of water molecules in the membrane interior as 474 within the total width 48.7 Å of the slab membrane model. The observed number of amide bonds in the bulk membrane was measured as 479 ± 10 at a 1:1 ratio of MPD and TMC. Given that the number of carboxylate functional groups equals the number of amide functional groups in a 1:1 TMC-MPD unit, approximately one water molecule is present around the carboxylate functional group. Our PA membrane molecular model in the presence of one explicit water molecule therefore reproduces the properties of a bulk membrane system simulated by the molecular model, and the theoretically calculated free energy of interaction validates the use of this model.

**Solute–membrane–water interaction and the free energy of interaction**

The validation of the PA1 membrane model for the solute–membrane–water interaction is given in Text S5 in ESI.

**Correlation of mass transfer coefficients with free energy of interaction for organic compounds**

**Overall results.** Approximately 50% of the carboxylic functional groups in the PA membrane are dissociated in solution with a neutral pH and our previous experiment was done at 6.5, we use the PA-1 model to investigate the correlation of experimentally determined $k_s$ values obtained by a reference membrane, ESFA2-LD, with the free energies of interaction for various organic compounds. Only four-ring PA membrane model was used for alkanes and both four-ring and -linear models were investigated for alkenes and benzenes because a C–C double bond of organic compounds interacts with the ring of a PA membrane model. When multiple $\Delta G_{aq,calc}$ values were obtained from the ring and linear membrane models, the lowest value was used for the correlation. Fig. 1 shows the correlations: $\ln k_s = -0.381 \Delta G_{aq,calc} + 3.611$ for 9 haloalkanes ($r^2 = 0.739$) and $\ln k_s = -0.367 \Delta G_{aq,calc} + 4.538$ for 6 haloalkenes ($r^2 = 0.778$). Fig. 2 shows the correlation: $\ln k_s = -0.410 \Delta G_{aq,calc} + 4.035$ for 23 alkylbenzenes and halobenzenes ($r^2 = 0.774$). Overall the reasonable linear correlation was observed. In general, ±2.0 kcal mol$^{-1}$ of accuracy in calculating the energy was reported with the M06-2X/cc-pVDZ and the SMD solvation model. However, the accuracy in calculating the free energy of interaction may be tradeoff because the value was the difference between a complex and two independent systems as shown in eqn (5). Using the estimated ±2.0 kcal mol$^{-1}$ of accuracy in calculating the $\Delta G_{aq,calc}$ value, the accuracy in calculating the $k_s$ value using the correlation for haloalkane would be within ±2.0 L m$^{-2} \cdot$ h of the $k_s$ value and this corresponds to less than 4% of rejection efficiency. Given that the estimated experimental accuracy in obtaining the rejection efficiency within ±10%, our observed correlation is accurate enough to estimate the rejection within the experimental error. Tables S8 and S9 in ESIF summarize the experimentally determined $k_s$ values and theoretically calculated $\Delta G_{aq,calc}$ values for all compounds. Three data points (1,1,2,2-tetrachloroethane for data point no. 6, 1,2,3-trichloropropane for no. 9, and 1,2-dibromo-3-chloropropane for no. 14) were not included in the correlation for haloalkanes because of two potential reasons: (1) experimental error and (2) contribution of molecular size to diffusion. When the $k_s$ values were close to 2.0 L m$^{-2} \cdot$ h, which correlated to more than 95% rejection and may be affected by
Haloalkanes and haloalkenes

In the following section, we will investigate the relationships between the structures of haloalkanes and haloalkenes, their free energies of interaction, and the $k_s$ values in more detail. This approach will provide more insight into the impact of a single functional group on a compound with the same base structure. A comparison of chloroform (compound no. 1) and tetrachloromethane (no. 2) revealed that the substitution of a H atom by a chlorine atom decreased the $k_s$ value (i.e., increased the rejection) due to the decreased interaction with the membrane. The $\Delta G_{\text{aq,calc}}^{\text{int}}$ values of chloroform and tetrachloromethane are 3.16 kcal mol$^{-1}$ and 4.48 kcal mol$^{-1}$, indicating that the interaction corresponds to the rejection trend. A comparison of 1,2-dichloropropane (no. 7) and 1,3-dichloropropane (no. 8) revealed that a chlorine functional group adjacent to a terminal carbon resulted in a lower $k_s$ value than a chlorine atom at a medial carbon, as shown by the $k_s$ values for 1,2-dichloropropane (3.79 L m$^{-2}$ h) and 1,3-dichloropropane (15.6 L m$^{-2}$ h), which indicate decreased rejection of the latter compound. Because these two compounds have identical MWs and very similar sizes, the 4.12 kcal mol$^{-1}$ $\Delta G_{\text{aq,calc}}^{\text{int}}$ value for 1,2-dichloropropane and 1.16 kcal mol$^{-1}$ $\Delta G_{\text{aq,calc}}^{\text{int}}$ value for 1,3-dichloropropane indicate the critical role of the interaction with membrane. Replacing a chlorine atom with a bromine atom in aliphatic haloalkanes increased the $k_s$ value from 8.38 L m$^{-2}$ h for bromodichloromethane (no. 12) to 11.2 L m$^{-2}$ h for chlorodibromomethane (no. 13) (i.e., decreased rejection) due to the greater hydrophobicity resulting from the bromine atom. Although this trend does not follow the expected trend of $k_s$ values (i.e., chloroform > bromodichloromethane > chlorodibromomethane > bromoform), the $\Delta G_{\text{aq,calc}}^{\text{int}}$ value of 4.98 L m$^{-2}$ h for bromodichloromethane and 4.66 L m$^{-2}$ h $\Delta G_{\text{aq,calc}}^{\text{int}}$ value for chlorodibromomethane showed that the trend in the interaction corresponds to the rejection.

Overall, the $k_s$ values for haloalkenes were slightly larger than those for haloalkanes (i.e., less rejection of haloalkenes). This trend is because of the well-known favorable interaction of the $\pi$-bond of an unsaturated C–C double bond with the benzene ring structure of TMC. Both linear and ring structures of a PA membrane model with 4 chains were used for haloalkanes and halobenzenes to account for all possible interactions of a C–C double bond of an organic compound with TMC. A chlorine functional group on an alkene base structure decreased the $k_s$ values (i.e., increased the rejection). The $k_s$ value for trichloroethene (no. 5) was 44.4 L m$^{-2}$ h and much larger than the 9.05 L m$^{-2}$ h $k_s$ value for tetrachloroethene (no. 6). The hydrophobic nature of the chlorine functional group increases the $\Delta G_{\text{aq,calc}}^{\text{int}}$ value from 3.06 kcal mol$^{-1}$ for trichloroethene to 5.84 kcal mol$^{-1}$ for tetrachloroethene. This result indicates that the interaction trend corresponds to the rejection. Being a cis- or trans-isomer significantly affected reaction. The $k_s$ values were 41.9 L m$^{-2}$ h for cis-1,3-dichloropropene (no. 8) and 99.5 L m$^{-2}$ h for trans-1,3-dichloropropene (no. 9). The $\Delta G_{\text{aq,calc}}^{\text{int}}$ value was 2.35 kcal mol$^{-1}$ for cis-1,3-dichloropropene and 1.04 kcal mol$^{-1}$ for trans-1,3-dichloropropene. While these two isomers have almost identical $M_w$.
and molar volumes, the location of the functional group affected the ability of these isomers to permeate the PA membrane, and the free energy of interaction corresponds to the rejection trend.

**Allylbenzenes and halobenzenes**

The type of functional groups and their positions on a benzene ring significantly affect the rejection of allylbenzenes and halobenzenes, and we found the interaction between an organic compound and the PA membrane plays a critical role for the rejection of these compounds. Longer mono-alkyl functional groups decreased the $k_s$ values (i.e., increased the rejection), probably due to greater interactions between the alkyl side chain and the PA membrane. For example, the $k_s$ value decreased from 8.94 L m$^{-2}$ h for toluene (compound no. 1 in benzene group) to 6.05 L m$^{-2}$ h for ethylbenzene (no. 4), 5.80 L m$^{-2}$ h for propylbenzene (no. 6), and 4.60 L m$^{-2}$ h for n-butylbenzene (no. 10). In comparison, the $\Delta G_{aq,calc}$ values increased from 2.34 kcal mol$^{-1}$ for toluene to 2.47 kcal mol$^{-1}$ for ethylbenzene, 2.86 kcal mol$^{-1}$ for propylbenzene, and 3.14 kcal mol$^{-1}$ for n-butylbenzene. The chlorine functional group on a benzene ring increased the $k_s$ value from its value in the presence of an alkyl functional group due to hydrophobic interactions with PA membrane (i.e., decreased rejection). For example, the $k_s$ value was 8.94 L m$^{-2}$ h for toluene, 23.26 L m$^{-2}$ h for chlorobenzene (no. 15), and 29.02 L m$^{-2}$ h for bromobenzene (no. 23). The $\Delta G_{aq,calc}$ value was 2.34 kcal mol$^{-1}$ for toluene, $-0.36$ kcal mol$^{-1}$ for chlorobenzene, and $-1.13$ kcal mol$^{-1}$ for bromobenzene. Thus, even though the base benzene ring structure interacts with membrane ring structures such as benzene, the functional group significantly affects the rejection and the interaction of the functional group with the PA membrane. Noteworthy that the role of a chlorine functional group is complex: while the chlorine functional group is significantly increased the rejection and the interaction of the functional group, the presence of an alkyl functional group due to hydrophobic interactions with PA membrane (i.e., decreased rejection). Noteworthy that the role of a chlorine functional group is complex: while the chlorine functional group is significantly increased the rejection and the interaction of the functional group, the presence of an alkyl functional group due to hydrophobic interactions with PA membrane (i.e., decreased rejection).

**Conclusion**

This study highlights the novel approach to using *ab initio* QM-based computational chemistry calculations to investigate the interaction between a wide variety of neutral organic compounds and polyamide RO membrane for water treatment application. Our molecular model constructed in this study was validated with the experimentally determined water–membrane and solute–water–membrane interactions. We determined linear correlations between the theoretically calculated free energies of interaction for a wide variety of organic compounds and the experimentally obtained mass transfer coefficients. The correlation indicates that the interaction between organic compounds and RO membranes plays a critical role in the rejection mechanism.

**Conflicts of interest**

There are no conflicts to declare.

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