Kinetics based on the base-catalyzed mechanism of a click reaction between glycol dimercaptoacetate and glycidyl phenyl ether†

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The kinetics model of the thiol–epoxy reaction was built, and the parameters of elementary reactions were obtained according to the well-defined base-catalyzed mechanism. Through the comparison of rate constants, the rate-controlling step was proven to be the deprotonation of thiol by the base catalyst, instead of the nucleophilic attack of thiolate anion on the epoxy functional group, as previously commonly believed. Moreover, alkoxide anions tend to deprotonate unreacted thiol, rather than the conjugate acid of the base catalyst with increasing temperature. Finally, the kinetic model and its parameters have been validated using the experimental data with different initial concentrations of base catalyst, thiol and epoxy functional groups.

The concept of “Click Chemistry” has drawn intensive attention from worldwide researchers since it was raised by Sharpless and his colleagues in 2001. “Click Chemistry” is a collection of carbon-heteroatom bond-forming reactions that possess a fast reaction rate and high selectivity, under mild conditions. Thiol “Click Chemistry”, including thiol–ene, thiol–isocyanate, thiol–halogen and thiol–epoxy reactions, has attracted much attention in the last decade. While the thiol–epoxy reaction has been applied widely, the fundamental research has mainly focused on the efficiency of various base catalysts and the structure effects of thions and epoxides. Inorganic bases like LiOH have strong basicity, leading to high catalytic efficiency in the thiol–epoxy reaction. However, inorganic bases cannot dissolve completely in organic solvents, which limits their application as homogeneous catalysts in thiol–epoxy reactions. Although having weaker basicity, organic bases such as 1,5,7-triazabicyclo[4.4.0]dec-5-ene (TBD), trimethylamine (TEA) and tetrabutylammonium fluoride (TBAF) are also frequently used in thiol–epoxy reactions due to their excellent solubility in organic solvents. To widen the application fields of the thiol–epoxy reaction, it is necessary to undertake a thorough investigation of its mechanism.

The well-acknowledged base-catalyzed mechanism of the thiol–epoxy reaction is a simple nucleophilic ring-opening reaction. In this mechanism, the thiol group is deprotonated by the base catalyst to form thiolate anion. Under the nucleophilic attack of the thiolate anion, the epoxy functional group is ring-opened to generate the alkoxide anion, which has strong basicity and forms the final product after proton transfer. The first step is an acid–base reaction that is usually considered to be a fast reaction. Therefore, the nucleophilic attack of the thiolate anion on the epoxy functional group is assumed to be the rate-controlling step of the thiol–epoxy reaction, resulting in a second-order reaction mechanism.

In this study, 1,8-naphthalenediamine was selected as the base catalyst to avoid the influence of the nucleophile-initiated mechanism because it is a well-known non-nucleophilic organic base. Moreover, 1,8-naphthalenediamine is an organic base with strong basicity and it is expected to trigger the thiol–epoxy reaction at a fast rate in the acid–base step. Kinetic parameters of elementary reactions involved in the base-catalyzed mechanism of the thiol–epoxy reaction were obtained by fitting experimental data. Rate constants were compared to determine the rate-controlling step of the thiol–epoxy reaction.

Even though the epoxy functional group is very active with its structure of a strained three-membered ring, it cannot react with thiol directly. In the well-established base-catalyzed mechanism of the thiol–epoxy reaction, thiol is deprotonated by the base catalyst and loses its active hydrogen ion to generate the thiolate anion, which is an acid–base reaction in a broad sense. The thiolate anion has much stronger nucleophilicity than that of thiol. The epoxy functional group is opened under the nucleophilic attack of the thiolate anion. The thiolate anion prefers to attack the less sterically hindered carbon of the epoxy functional group to form the alkoxide anion. Alkoxide anion has high basicity, with a pKₐ of around 17. It can deprotonate all hydrogen sources in the reaction system, including the conjugate acid of
the catalyst and unreacted thiol to generate the final product of the thiol–epoxy reaction. The base-catalyzed mechanism of the thiol–epoxy reaction is illustrated in Scheme 1.

According to the abovementioned mechanism, there are a total of five elementary reactions involved. These are as follows: (1) deprotonation of thiol by the base catalyst to form the thiolate anion and the conjugate acid of the catalyst (Reaction 1); (2) the reverse of Reaction 1 (Reaction −1); (3) nucleophilic attack of the thiolate anion on the epoxy functional group to generate the alkoxide anion (Reaction 3); (4) deprotonation of unreacted thiol by alkoxide anion to generate the final product and the thiolate anion (Reaction 4); (5) deprotonation of unreacted thiol by the alkoxide anion to generate the final product and base catalyst (Reaction 5). The rate constants of these five elementary reactions are set as $k_1$, $k_{−1}$, $k_2$, $k_3$, and $k_4$. There are seven substances or functional groups appearing in the mechanism; they are the thiol functional group, the base catalyst, the thiolate anion, the conjugated acid of the catalyst, the epoxy functional group, the alkoxide anion and the final product. All of the elementary reactions are bimolecular ones. The differential equations of consumption or generation rates of the substances can be obtained according to the mechanism (see ESI†). The kinetic model has been built combining the differential equations and initial concentrations of substances. Kinetic experiments were carried out under different conditions to obtain epoxy concentration curves. Experimental data with a molar ratio fixed at 1 : 1 of thiol and epoxy functional group was fitted using this model to obtain kinetic parameters.

The experimental points and fitting curves are compared in Fig. 1. It can be seen that the fitting curves at every reaction temperature from 60–130 °C match the experimental points well. The rate constants of the five elementary reactions at each temperature were obtained and are listed in Table 1. The ln $k$–1/T curves of each rate constant show fine linearity, which means that all elementary reactions satisfy Arrhenius’ equation well in this temperature range (Fig. S1 in ESI†). The activation energies and pre-exponential factors have been obtained by the intercepts and slopes of the fitting lines according to Arrhenius’ equation. The results are listed in Table 2.

The value of the rate constant $k_1$ reflects the deprotonation rate of thiol by base catalyst 1,8-naphthalenediamine, whereas the value of rate constant $k_{−1}$ corresponds to the rate of the reverse reaction of this acid–base reaction. The organic base 1,8-naphthalene-diamine is a strong base with a $pK_a$ of 12.1.20 From the comparison between $k_1$ and $k_{−1}$ listed in Table 1, it can be found that $k_1$ is two orders of magnitude greater than $k_{−1}$. This means that reaction −1, namely the reverse reaction of the acid–base reaction, hardly takes place in the entire mechanism. This is also in agreement with the high basicity of the catalyst. In addition, the activation energy of reaction 1 ($E_a$) is 17.8 kJ mol$^{−1}$ while $E_{a−1}$ is only 4.95 kJ mol$^{−1}$, indicating that Reaction 1 is more sensitive to temperature changes compared to Reaction −1.

### Scheme 1  Base-catalyzed mechanism of the thiol–epoxy reaction.

### Fig. 1  Experimental points and fitting curves of thiol–epoxy reaction under different temperatures: (a) 60/80/100/120 °C (b) 70/90/110/130 °C.

### Table 1  Rate constants of elementary reactions in the temperature range from 60 °C to 130 °Ca

| Temperature/°C | $k_1$  | $k_{−1}$ | $k_2$  | $k_3$  | $k_4$  |
|----------------|--------|----------|--------|--------|--------|
| 60             | 4.746  | 0.04001  | 257.6  | 1398   | 1176   |
| 70             | 5.591  | 0.04242  | 327.6  | 2454   | 1464   |
| 80             | 6.614  | 0.04555  | 442.1  | 3757   | 1478   |
| 90             | 7.777  | 0.04775  | 591.8  | 5649   | 1990   |
| 100            | 8.906  | 0.04882  | 646.9  | 8150   | 2356   |
| 110            | 10.23  | 0.05216  | 739.5  | 10 170 | 3141   |
| 120            | 11.68  | 0.05347  | 884.3  | 14 390 | 3709   |
| 130            | 15.58  | 0.05408  | 1233   | 23 340 | 3950   |

a The unit of each rate constant is g mol$^{−1}$ min$^{−1}$.
The traditional simplified kinetic equation of the thiol–epoxy reaction was raised on the condition that the nucleophilic attack was the slowest step in the entire mechanism. Then, the apparent kinetic equation could be written in the following form:

$$-\frac{dc_E}{dt} = k_2c_Gc_E$$

where $k_2$ is the rate constant of the nucleophilic attack step, and $c_G$ and $c_E$ are the concentration of thiolate anion and epoxy functional group, respectively.

However, the condition mentioned here is not always corrected in every reaction system. Taking our reaction system as an example, the rate-controlling step of the entire mechanism is the deprotonation step of thiol and not the nucleophilic attack step. Then, the kinetic equations could not be simplified to one in the form of a second order reaction.

In other reaction systems using more active thiol and a catalyst with stronger basicity, the rate of Reaction 1 may be fast at certain temperatures and the acid–base equilibrium can be reached in a short time as well. Moreover, if the $k_3$ is far greater than $k_4$, then Reaction 4 could be neglected in the mechanism. Therefore, the base-catalyzed mechanism could be simplified and presented in the following form, as shown in Scheme 2, under these two assumptions.

Only under this condition will the nucleophilic attack be the rate-controlling step of the entire mechanism and will the thiol–epoxy reaction satisfy the requirements of a second order reaction. However, according to the analysis of elementary reactions involved in the mechanism, not all reaction systems will satisfy these two assumptions at an arbitrary temperature.

Due to the strong basicity of the alkoxide anion, the reaction rates of Reaction 3 and Reaction 4 are both rapid. Therefore, the concentration of the alkoxide anion remains very low in the reaction system throughout the reaction time (Fig. S2 in ESI†). The low concentration of the alkoxide anion also explains the absence of epoxy homopolymerization in the reaction system and confirms the thiol–epoxy reaction as a click reaction.²¹

According to the analysis mentioned above, the concentration of the base catalyst can directly influence the initiation rate of the thiol–epoxy reaction, namely the rate of Reaction 1. Kinetic experiments with different base catalyst concentrations were carried out to obtain the epoxy concentration points. In addition to the experimental points, the predicted epoxy concentration curves were obtained from the kinetic model using the parameters shown in Table 1. Both the experimental results and predicted curves are presented in Fig. 2. The predicted epoxy concentration curves given by the kinetic model fit the experimental points well. It can be concluded that the kinetic model and parameters obtained above could predict kinetic curves well within a base catalyst concentration range of 1–5 mol%.

![Scheme 2](Image)

**Scheme 2** Simplified form of thiol–epoxy reaction under certain assumptions.

Table 2 Activation energies and pre-exponential factors of each elementary reaction

| Reaction $i$ | $i = 1$ | $i = 2$ | $i = 3$ | $i = 4$ |
|-------------|----------|----------|----------|----------|
| $E_a$/kJ mol$^{-1}$ | 17.8 | 4.95 | 23.4 | 42.6 |
| $A_0$/g·mol$^{-1}$ (mol min)$^{-1}$ | 2.88 × 10$^3$ | 0.242 | 1.24 × 10$^6$ | 7.24 × 10$^9$ | 3.29 × 10$^{16}$ |
Moreover, kinetic experiments with a different initial molar ratio of functional groups were carried out to validate the kinetic model. Similarly, it can be concluded that the kinetic model and parameters obtained herein can predict the kinetic curves well in the range of molar ratios of thiol and epoxy functional groups from 1 : 1 to 1.5 : 1.

The present study establishes the kinetic model of the thiol–epoxy reaction according to the well-acknowledged base-catalyzed mechanism. Experimental points are fitted in the kinetic model to obtain kinetic parameters of elementary reactions including rate constants at different temperatures, activation energies and pre-exponential factors. Through the analysis of kinetic parameters of each elementary reaction, the slowest reaction in the mechanism is proven to be the deprotonation reaction of thiol by base catalyst, instead of the nucleophilic attack of thiolate anion on the epoxy functional group. Under certain conditions, the nucleophilic attack step will be the rate-controlling step of the thiol–epoxy reaction, and the entire reaction will satisfy the requirements of a second order reaction. Kinetic experiments with different initial concentrations of base catalyst, thiol and epoxy functional group were carried out. All the predicted epoxy concentration curves fit the experimental points well, validating the kinetic model and its parameters.

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Notes and references

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