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Optimal design for a cylindrical gear with inclined teeth

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Abstract. Designing is an act of creation, which is a technical activity carried out for productive purpose, and which aims to provide all the data necessary for the implementation of correlated material and financial means, a theme or an idea in practice. Depending on the operating conditions of the machines and their technological destination, optimum reliability, maintainability and ergonomics must be ensured from the design stage. For some areas where toothed gears are used, such as the aerospace industry, the automotive construction etc., reduced gear mass (volume) can be an important parameter to become an optimization criterion. This paper aims to study the gearing mass and proposes to minimize this function.

\[ M_{gearing} = V_{gearing} \cdot \rho_{material} \rightarrow \text{min} \]

1. Introduction
The gear mechanism is made up of two gears, which are sequentially transmitted through the teeth and continuously contacting (engaging) - rotating movement and torque between the two shafts.

Gears are used to transmit the rotation movement from the drive shaft to the other driven, achieving a constant transmission ratio between speeds. Transmission of movement is always accompanied by the transmission of torque, which is a mechanical work, so a power.

A gear is made up of a pair of gears, one driving and the other driven. Relative sliding of the surfaces in contact is excluded because the movement is not transmitted by the frictional force but by a pushing force between the teeth.

Gears have a wide use in mechanical transmissions, due to their advantages: constant transmission ratio; safety in operation; high durability; high efficiency; reduced size; the possibility of using for a wide range of powers, speeds and transmission reports. As drawbacks, there can be mentioned: high execution and mounting precision; complicated technology; noise and vibration in operation.

In the modern construction of machines and appliances, gearing is the most important and most used mechanism. The construction of a car like that of a lathe contains dozens of gears.

Properly groomed and properly assembled can guarantee safe operation at speeds and reduced power up to thousands of kilowatts of power and at high speeds up to 100-150 m/s. At present, toothed wheels with dimensions between fractions of millimeters up to 10 m in diameter can be built.

When selecting the material, a number of factors must be taken into account: the load that loads the gear; the required service life; the mechanical characteristics of the materials; how to obtain the semi-finished product; execution technology; economic efficiency; operating conditions.
2. The optimisation problem
This paper is a study on the mass of a gear speed reducer single stage and the objective function is to minimize this value.

It is proposed to design a cylindrical gear with inclined teeth having the following input data:

- Power of the second shaft: $P_2 = 24 \text{ kW}$
- Total gear ratio: $i_R = 2$
- Speed of the second shaft: $n_2 = 1000 \text{ rot/min}$
- The mean time in service between two successive repairs: $L_h = 9000 \text{ hours}$
- Number of wheels in contact with the wheel gear: $\chi_{1,2} = 1$
- Difference in wheel width: $\Delta_b = 5 \text{ mm}$
- Toothed wheel materials:
  - Pinion: 41MoCr11 - improved steel: $HB_1 = 2800 \text{ MPa}$
  - Gear: 40Cr10 – improved steel: $HB_2 = 2500 \text{ MPa}$
  - Density materials: $\rho_{\text{max}} = 7.85 \cdot 10^{-6} \text{ kg/mm}^3$
 rollers: 

- \( \sigma_{H\text{ lim}1} = 720 \, \text{MPa} \)
- \( \sigma_{H\text{ lim}2} = 675 \, \text{MPa} \)
- \( \sigma_{F\text{ lim}1} = 460 \, \text{MPa} \)
- \( \sigma_{F\text{ lim}2} = 445 \, \text{MPa} \)

Safety factor for contact stress:
- \( S_H = 1.25 \)
- \( S_F = 1.5 \)

Flank hardness factor: \( Z_w = 1 \)

Elasticity factor of the wheel material: \( Z_E = 189.8 \, \text{MPa}^{1/2} \)

Material factor: \( Z_M = 271 \, \text{N/mm}^2 \)

Precision class (tolerance grade): 7 tooth milling with the snail cutter and grinding

Profile of generating rack:
- Pressure angle normal reference plane: \( \alpha_n = 20^\circ \)
- Tooth head height factor: \( h_{0a}^* = 1 \)
- Match factor at the head of the reference tooth: \( c^* = 0.25 \)

Factor of operating mode: \( K_A = 1 \)

Lubricant type: TIN 125 EP with kinematic viscosity 125÷140 \( \text{mm}^2/\text{s} \) at 50°C

Overloading coefficient \( c_s = 1 \)

3. Optimisation problem genes

In the broad sense, optimization means the action of determining, on the basis of a predetermined criterion, the best decision in a given situation where more than one decision is possible, as well as the action to implement the established decision as well as its outcome.

Narrow optimization simply means action establishing the right choice (solution) called Decision optimal (optimal solution).

Five variables are considered to optimize the problem.

- Variable 1 - \( a_w \) – the center distance, axial distance values are those standardized in the field 40÷315 mm
- Variable 2 - \( \psi_a \) – the coefficient ratio between the width and the axial distance (variable real continuous), taking values in the range of 0,1 ÷ 0,6
- Variable 3 - \( \beta \) – the inclination helix angle on the pitch cylinder (variable real continuous), with value in the field 7,25° ÷ 15°
- Variable 4 - \( z_1 \) – the number of pinion teeth (full variable), with values in range 24 ÷ 50
- Variable 5 - \( x_s \) – the profile displacement coefficient sum for both gears (real continuous variable), having values in the range -0,5 ÷ +1,1

4. Calculate the amount necessary for describing the problem of optimization

Taking into account the inputs and variables mentioned above, it is necessary to go through a series of steps to determine the essential dimensions for describing the objective function and the optimization problem constraints.

4.1. Determining the power of the electric motor

\[
P_c = \frac{P_2}{\eta_{tot}} = \frac{24}{0.949} = 25.29 \, \text{kW}
\]

\( \eta_{tot} = \eta_{12} \cdot \eta_{\eta} \cdot \eta_l = 0.97 \cdot 0.994^2 \cdot 0.99 = 0.949 \)
Where:
\[ \eta_{\text{tot}} \] - total efficiency of the drive mechanism
\[ \eta_{12} = 0.97 \] - efficiency of the gears
\[ \eta_b = 0.994 \] - a pair of bearings efficiency:
\[ \eta_l = 0.99 \] - the lubrication efficiency.

4.2. Choosing electric motor
From STAS we choose the EM type 225M-60-6 with:
- The nominal power: \[ P_{EM} = 30kW > 25,29kW \]
- The loaded speed: \[ n_1 = 2870rot/min > n_{12} = n_2 \cdot i_R = 1000 \cdot 2 = 2000 \text{ rot/min} \]

4.3. Determination of the torque moments of the shafts
The moments developed for the two shafts of the reducer are:
\[ M_{t1} = \frac{30 \cdot P_1}{\pi \cdot n_1} \cdot 10^6 = 99821Nmm \]
\[ M_{t2} = \frac{30 \cdot P_2}{\pi \cdot n_2} \cdot 10^6 = 229299Nmm \]

4.4. Calculating the normal module, the distance between the axes and the number of teeth
- The distance between axes \( a \)
\[
\begin{align*}
\alpha & \geq (1 + u) \sqrt{\frac{K_A \cdot K_V \cdot K_H \cdot M_{t2}}{2 \cdot u \cdot \psi_a} \left( \frac{Z_M \cdot Z_H \cdot Z_e}{\sigma_{H, \text{lim}} \cdot K_{HN} \cdot Z_R \cdot Z_W} \right)^2} = 122,761 \text{ mm}
\end{align*}
\]
Where:
\[ u = i_R = 2 \]

The center distance is standardized and is given in table 1 and we’ll choose the next superior value but whether the calculated value is less than 5% than the lower one, we may choose the lower one.

| I  | II | I  | II | I  | II | I  | II | I  | II | I  | II |
|----|----|----|----|----|----|----|----|----|----|----|----|
| 40 | 40 | 63 | 63 | 100| 100| 160| 160| 250| 250| 400| 450|
| 45 | 45 | 71 | 71 | 112| 112| 180| 180| 280| 280| 400| 450|
| 50 | 50 | 80 | 80 | 125| 125| 200| 200| 315| 315| 500| 560|
| 56 | 56 | 90 | 90 | 140| 140| 225| 225| 355| 355| 500| 560|

Table 1 shows the standard values for axle spacing between cylindrical and worm gears. The values of the I string are preferential.

We’ll take \( a_w = 125 \text{ mm} \)

- The normal module \( m_n \)
\[
m_n \geq \frac{M_{t2} \cdot (1 + u) \cdot K_A \cdot K_V \cdot K_H \cdot K_{F_H} \cdot Y_F \cdot Y_{\beta}}{\psi_a \cdot \alpha^2 \sigma_{F, \text{lim}} \cdot K_{F_H} \cdot Y_Z \cdot Y_{F_X}} = 0,927 \text{ mm}
\]

If the value is under 1 mm then \( m_n \) is selected 1 mm. Thus \( m_n = 1 \text{ mm} \)
Establishing the number of teeth for the driving gear

The maximum number of teeth is calculated taking into account the center distance and the normal module

\[ z_{1 \text{max}} = \frac{2 \cdot a_w \cdot \cos\beta}{m_n \cdot (1 + u)} = \frac{2 \cdot 125 \cdot \cos(15^\circ)}{35 \cdot (1 + 2)} = 80.49 \text{ mm} \]

\[ z_1 < z_{1 \text{max}} \Rightarrow z_1 = 30 \div 35 \text{ if } z_{1 \text{max}} = 45 \div 80 \text{ and more} \]

We’ll choose \( z_1 = 35 \)

4.5. The final selection of the normal module, the distance between the axes and the number of teeth

\[ m_n = \frac{2 \cdot a_w \cdot \cos\beta}{z_1 \cdot (1 + u)} = \frac{2 \cdot 125 \cdot \cos(15^\circ)}{35 \cdot (1 + 2)} = 2.30 \text{ mm} \]

The new module now is \( m_n = 2.25 \)

With this new value one may recalculate the number of teeth:

\[ z_1 = \frac{2 \cdot a_w \cdot \cos\beta}{m_n \cdot (1 + u)} = \frac{2 \cdot 125 \cdot \cos(15^\circ)}{2.25 \cdot (1 + 2)} = 35.77 \]

The new selected number is identical with the preliminary selected one \( z_1 = 35 \)

With \( z_1 \) final we may calculate the number of teeth for the driven gear

\[ z_2 = u \cdot z_1 = 2 \cdot 35 = 70 \]

The rational for selection of \( z_2 \) is recommended that the number of teeth of both gears not to divide exactly (relative prime number).

We’ll choose \( z_2 = 71 \)

The reference center distance is recalculated

\[ a_0 = \frac{m_n \cdot (z_1 + z_2)}{2 \cdot \cos\beta} = \frac{2.25 \cdot (35 + 71)}{2 \cdot \cos(15^\circ)} = 123.46 \text{ mm} \]

4.6. Geometrical elements calculation

► The frontal pitch pressure angle \( \alpha_t \)

\[ \alpha_t = \arctg \left( \frac{tg\alpha_n}{\cos\beta} \right) = \arctg \left( \frac{tg(20^\circ)}{\cos(15^\circ)} \right) = 20.65^\circ \]

► The pitch gearing normal angle \( \alpha_{wt} \)

\[ \alpha_{wt} = \arccos \left( \frac{a_0 \cdot \cos\alpha_t}{a_w} \right) = 22.45^\circ \]

► The profile displacement coefficient sum for both gears \( x_s \)

\[ x_s = x_1 + x_2 = (z_1 + z_2) \cdot \frac{\text{inv}(\alpha_{wt}) - \text{inv}(\alpha_t)}{2 \cdot tg(\alpha_n)} = 0.6931 \]
Where:

\[ \text{inv}(\alpha_{wt}) = \frac{\text{tg}(\alpha_{wt})}{\frac{\pi}{180}} \cdot \alpha_{wt} = 0.0212 \]

\[ \text{inv}(\alpha_t) = \frac{\text{tg}(\alpha_t)}{\frac{\pi}{180}} \cdot \alpha_t = 0.0164 \]

In order to distribute this sum on both gears we’ll use the chart (Figure 3).

From the chart we have \( x_1 = 0.4 \) so that \( x_2 = 0.293 \)

- **Pitch diameter** \( d_1; d_2 \)
  
  \[ d_1 = \frac{m_n \cdot z_1}{\cos \beta} = 81.515 \text{ mm} \]
  
  \[ d_2 = \frac{m_n \cdot z_2}{\cos \beta} = 165.359 \text{ mm} \]

- **Top land diameter** \( d_{a1}; d_{a2} \)
  
  \[ d_{a1} = d_1 + 2 \cdot h_{a1} = 87.815 \text{ mm} \]
  
  \[ d_{a2} = d_2 + 2 \cdot h_{a2} = 171.177 \text{ mm} \]

  Where addendum is:
  
  \( h_{a1} = m_n \cdot (h_{0a} + x_1) = 3.15 \text{ mm} \)
  
  \( h_{a2} = m_n \cdot (h_{0a} + x_2) = 2.909 \text{ mm} \)
  
  \( h_{0a} = 1 \)

- **Root diameter** \( d_{f1}; d_{f2} \)
  
  \[ d_{f1} = d_1 - 2 \cdot h_{f1} = 77.695 \text{ mm} \]
  
  \[ d_{f2} = d_2 - 2 \cdot h_{f2} = 161.053 \text{ mm} \]

  Where dedendum is:
  
  \( h_{f1} = m_n \cdot (h_{0f} - x_1) = 1.91 \text{ mm} \)
  
  \( h_{f2} = m_n \cdot (h_{0f} - x_2) = 2.153 \text{ mm} \)
  
  \( h_{0f} = 1.25 \)
Base circle diameter $d_{b1}$; $d_{b2}$

\[ d_{b1} = d_1 \cdot \cos(\alpha_t) = 76,277 \text{ mm} \]
\[ d_{b2} = d_2 \cdot \cos(\alpha_t) = 154,735 \text{ mm} \]

Figure 4 – Geometrical elements for gears

Rolling diameter $d_{w1}$; $d_{w2}$

\[ d_{w1} = d_1 \cdot \frac{\cos(\alpha_t)}{\cos(a_{wt})} = 82,543 \text{ mm} \]
\[ d_{w2} = d_2 \cdot \frac{\cos(\alpha_t)}{\cos(a_{wt})} = 167,425 \text{ mm} \]

Gear width $b_1$; $b_2$

\[ b_2 = a_w \cdot \psi_\alpha = 58 \text{ mm} \]
\[ b_1 = b_2 + m_n = 63 \text{ mm} \]

4.7. Equivalent gear elements

- The equivalent gear teeth number $z_{n1}$; $z_{n2}$

\[ z_{n1} = \frac{z_1}{\cos^3 \beta_3} = 38,83 \Rightarrow z_{n1} = 39 \]
\[ z_{n2} = \frac{z_2}{\cos^3 \beta_3} = 78,78 \Rightarrow z_{n2} = 79 \]

- The equivalent gear pitch diameter $d_{n1}$; $d_{n2}$

\[ d_{n1} = \frac{d_1}{\cos^2 \beta} = 87,367 \text{ mm} \]
\[ d_{n2} = \frac{d_2}{\cos^2 \beta} = 177,231 \text{ mm} \]

- The equivalent top land diameter $d_{an1}$; $d_{an2}$

\[ d_{an1} = d_{n1} + a_1 - d_1 = 93,667 \text{ mm} \]
\[ d_{an2} = d_{n2} + a_2 - d_2 = 183,049 \text{ mm} \]

- The equivalent base circle diameter $d_{bn1}$; $d_{bn2}$

\[ d_{bn1}=d_{n1} \cdot \cos \alpha_n = 82,098 \text{ mm} \]
\[ d_{bn2}=d_{n2} \cdot \cos \alpha_n = 166,543 \text{ mm} \]

- The equivalent distance between axes, [mm]$a_{wn}$

\[ a_{wn} \geq \frac{a_w \cdot \cos \alpha_n}{\cos \beta_b \cdot \cos \alpha_{wn}} = 110,045 \text{ mm} \]
Where:

\[ \beta_b = \arctg \left( \frac{d_b}{d_1} \cdot \tan \beta \right) = 14,07^\circ \]
\[ \beta_w = \arctg \left( \frac{d_w}{d_1} \cdot \tan \beta \right) = 15,18^\circ \]
\[ \alpha_{wn} = \arccos \left( \frac{\cos \alpha_{wt} \cdot \cos \beta_b}{\cos \beta_w} \right) = 21,78^\circ \]

From Table 1 we’ll take \( a_{wn} = 112 \, \text{mm} \)

- The equivalent normal module \( m_{nn} \)

\[ m_{nn} = \frac{2 \cdot a_{wn} \cdot \cos \beta_w}{z_{n1} + z_{n2}} = 1,83 \, \text{mm} \]

The new module now is \( m_{nn} = 1,75 \)

5. Calculating the gear mass (volume)
The gearing weight is:

\[ M_{gearing} = V_{gearing} \cdot \rho_{material} \]

Where:

\( V_{gearing} \) – gear unit volume
\( \rho_{material} \) – density of the gear wheel material: \( \rho_{max} = 7,85 \cdot 10^{-6} \, \text{kg/mm}^3 \)

The gear unit volume is:

\[ V_{gearing} = V_{z1} + V_{z2} \]

Where:

\( V_{z1} \) – pinion volume, [mm\(^3\)]
\( V_{z2} \) – gear volume, [mm\(^3\)]

- We write in generalized form the relationships for volume determination using the index “\( i \)” (\( i \)-1 for the pinion, \( i \)-2 for the gear). Based on this notation the volume of the cylindrical inclined teeth is:

\[ V_{z_i} = A_i \cdot b_i \]

Where:

\( A_i \) – area of the cylindrical front surface with inclined teeth, [mm\(^2\)]
\( b_i \) – width of cylindrical wheels with inclined teeth, [mm]

Area of the cylindrical front surface with inclined teeth is:

\[ A_i = A_{disc \, i} + A_{z \, i} \cdot z_i \]

Where:

\( A_{disc \, i} \) – front surface area of the disc
\( A_{z \, i} \) – area of the cylindrical tooth front surface

\[ A_{disc \, i} = \frac{\pi \cdot d_{fi}^2}{4} \]

Where:

\( d_{fi} \) – root diameter of the cylindrical wheel

For calculating the area of the front surface of the cylindrical toothed wheel tooth, its surface has been divided into several circular sectors of known rays and angles (Figure 5).
Figure 5 – Dividing the front surface of the gear wheel

With notation in Figure 5, the front surface area can be written as follows:

$$A_{Zi} = 2 \cdot A_{AEMi} + A_{AMNPi} + A_{EHKFi} + 2 \cdot A_{Ri}$$

Where:
- $A_{AEMi}$ – contour area defined by points A, E, M, $[mm^2]$
- $A_{AMNPi}$ – contour area defined by points A, M, N, P, $[mm^2]$
- $A_{EHKFi}$ – contour area defined by points E, H, K, F, $[mm^2]$
- $A_{Ri}$ – zone conection area (outline bounded by points E, G, H, $[mm^2]$

Contour area defined by points A, E and M is:

$$A_{AEMi} = A_{OI EABD} - A_{DOI BA} - A_{sect Oiem} = 3428,824 \text{ mm}^2$$

Contour area defined by points A, M, N and P is:

$$A_{AMNPi} = A_{sect OIAP} - A_{sect OIMN} = 2241,68 \text{ mm}^2$$

Contour area defined by points E, H, K and F is:

$$A_{EHKFi} = A_{sect OIEF} - A_{sect OIHK} = 3725,512 \text{ mm}^2$$

Zone conection area is:

$$A_{Ri} = A_{DOIIIE} - A_{sect OIGH} - A_{sect OGE} = 2231,278 \text{ mm}^2$$

Area of the cylindrical front surface with inclined teeth is:

$$A_{i} = A_{disc i} + A_{Zi} \cdot z_{i} = 17287,396 \text{ mm}^2$$

The volume of the cylindrical inclined teeth is:

$$V_{Zi} = A_{i} \cdot b_{i} = 1099910,57 \text{ mm}^3$$

The gearing weight is:

$$M_{gearing} = V_{gearing} \cdot \rho_{material} = 8,634 \text{ kg}$$
6. The objective of the optimization problem

For some areas where toothed gears are used, such as the aerospace industry, the automotive construction etc., reduced gear mass (volume) can be an important parameter to become an optimization criterion.

For this reason it was considered as a function gear unit mass. We want to minimize this function.

\[ M_{gearing} = V_{gearing} \cdot \rho_{material} \rightarrow \text{min} \]

The Mathcad 15 software was used to solve the optimal design problem. The values of the minimum mass variable are shown in Table 2.

Tabel 2 – Values of solution variables with minimum mass

| Nr. | Variable                                      | Symbol | Valoare |
|-----|----------------------------------------------|--------|---------|
| 1   | Distance between axes, [mm]                 | \(a_w\) | 112     |
| 2   | Coefficient of displacement in the normal plane for the pinion | \(x_s\) | 1       |
| 3   | Coefficient ratio between the width and the axial distance | \(\psi_d\) | 0,45   |
| 4   | Inclination helix angle on the pitch cylinder | \(\beta\) | 14,07° |
| 5   | Gear teeth number                            | \(z_1\) | 39      |

Table 3 presents a comparison of the main geometric elements of the gear in the two variants (classical and optimal respectively).

Tabel 3 - Comparison between the two variants of gears

| Nr. | Characteristic                                      | Classic version | Optimal version |
|-----|-----------------------------------------------------|-----------------|-----------------|
|     |                                                     | pinion  | wheel    | pinion  | wheel    |
| 1   | Normal module, [mm]                                | 2,25    | 1,75    |         |         |
| 2   | Distance between axes, [mm]                        | 125     | 112     |         |         |
| 3   | Number of teeth of gears                            | 35      | 71      | 39      | 79      |
| 4   | Width gears, [mm]                                  | 63      | 58      | 67      | 62      |
| 5   | Root diameter, [mm]                                | 77,695  | 161,053 | 69,925  | 145,558 |
| 6   | Pitch diameter, [mm]                               | 81,515  | 165,359 | 73,363  | 148,823 |
| 7   | Rolling diameter, [mm]                              | 82,543  | 167,425 | 74,288  | 150,682 |
| 8   | Top land diameter, [mm]                             | 87,815  | 171,177 | 79,033  | 154,059 |
| 9   | Base circle diameter, [mm]                          | 76,277  | 154,735 | 67,124  | 140,808 |
| 10  | Gearing weight, [kg]                               | 8,634   | 7,403   |         |         |

7. Conclusions

For over 20 years, Mathcad is the standard recognized performing, documenting and working collaboratively with engineering calculations, methods and algorithms in design. Unlike spreadsheet programs, where equations are expressed cryptic and conversion between systems of different units is impossible, or programming languages, accessible mainly programmers, Mathcad is a much better perform and manage engineering calculations, they being easy to achieve, understood, verified, communicated and followed logically.
Based on the values in Table 3, it can be noticed that in the optimal variant the wheels of gearing are wider (coefficient of ratio between the width and the axial distance increased from 0.46 – 0.59) but with smaller diameters. The gearing weight decreased from 8.634 to 7.403 kg (which represents a 14.25% decrease in mass) on the idea that the same conditions function for both variants.

References
[1] CĂLIMĂNESCU, I., POP, V., 1981 *Machine elements – Theory and Cad Induction* (Constanța) vol.I (Ed. Nautică)
[2] CHIȘIU, A., ș.a. 1981 *Organe de mașini* (București) (Ed. Didactică și Pedagogică)
[3] DRĂGHICI, A., 1981 *Îndrumar de proiectare în construcția de mașini* (București) vol.I (Ed. Tehnică)
[4] GAFIȚANU, M., ș.a., 1983 *Organe de mașini* (București) vol.I (Ed. Tehnică)
[5] JOHNSON, C.R., 1980 *Optimum design of mechanical elements* (New York) (Ed. John Wiley Inc)
[6] PAVELESCU, D., 1985 *Organe de mașini* (București) (Ed. Didactică și Pedagogică)
[7] POPVICI, M.M., 2003 *Proiectarea optimală a organelor de mașini* (București) (Ed. Tehnică)
[8] RĂDULESCU, O., 1984 *Sinteze optimale în construcția de mașini* (București) (Ed. Tehnică)
[9] RĂDULESCU, O., 1982 *Organe de mașini. Sinteze optimale* (București) (Ed. Academiei Militare)
[10] RĂDULESCU, O., ș.a., 2003 *Proiectarea optimală a organelor de mașini* (București) (Ed. Tehnică)
[11] ZIDARU, N., 2004 *Organe de mașini* (București) (Ed. Printech)