Measurement of thin film interfacial surface roughness by coherence scanning interferometry

H. Yoshino, A. Abbas, P. M. Kaminski, R. Smith, J. M. Walls, and D. Mansfield

Citation: Journal of Applied Physics 121, 105303 (2017); doi: 10.1063/1.4978066
View online: http://dx.doi.org/10.1063/1.4978066
View Table of Contents: http://aip.scitation.org/toc/jap/121/10
Published by the American Institute of Physics

Articles you may be interested in

Time resolved small angle X-ray scattering experiments performed on detonating explosives at the advanced photon source: Calculation of the time and distance between the detonation front and the x-ray beam
Journal of Applied Physics 121, 105902105902 (2017); 10.1063/1.4978036

Ion distribution and ablation depth measurements of a fs-ps laser-irradiated solid tin target
Journal of Applied Physics 121, 103301103301 (2017); 10.1063/1.4977854

Breakdown electric fields in dissociated hot gas mixtures of sulfur hexafluoride including teflon: Calculations with experimental validations and utilization in fluid dynamics arc simulations
Journal of Applied Physics 121, 103302103302 (2017); 10.1063/1.4977864

Electrode material dependence of two-dimensional electron and vapour density distribution over vacuum arc discharge
Journal of Applied Physics 121, 103304103304 (2017); 10.1063/1.4977066

The effect of residual stress on photoluminescence in multi-crystalline silicon wafers
Journal of Applied Physics 121, 085701085701 (2017); 10.1063/1.4976328

Resonant optical properties of AlGaAs/GaAs multiple-quantum-well based Bragg structure at the second quantum state
Journal of Applied Physics 121, 103101103101 (2017); 10.1063/1.4978252
Coherence Scanning Interferometry (CSI), also referred to as Scanning White Light Interferometry (SWLI) or full-field OCT, have been widely used for three dimensional surface topographical measurement. These methods are generally unsuitable for determining the film thickness where there is an interfacial surface roughness (ISR) between deposited films and the substrate. Nevertheless, many studies have been carried out on film thickness determination using CSI. Some methods treat the interference signals in the time domain when each thin film has a thickness in a certain range ($\geq 1.5 \mu m$), while others make use of the spectral phase or amplitude of the signals in the frequency domain to allow measurement in the thin film range ($\leq 1.5 \mu m$).

The use of the CSI-methods for thin film thickness measurements based on time domain analysis is limited to film thickness ($\geq 1.5 \mu m$). This is because as the surfaces of the film assembly get closer, the peaks in the interference signal overlap more in the time domain. Even so, this method provides a three dimensional presentation of interfacial surface topography and film thickness without difficulty. In contrast, those measurements which use frequency analysis work well in the thin film regime. For example, methods using the Helical Complex Field (HCF) function are able to accurately measure the film thickness less than 100 nm. There is, however, difficulty using this method in determining the film structure on a pixel by pixel basis owing to noise in the signal. For this, the conventional HCF method normally computes the thin film thickness by averaging the signals over an area occupied by a few hundreds of pixels.

Mansfield proposed applying the HCF function to three dimensional pixel-by-pixel thin film thickness determination together with Interfacial Surface Roughness (ISR).
computation by introducing a first order approximation of the function $^{17}$ and then demonstrated this capability in terms of comparing the resultant top surface of a dielectric-coated glass substrate with AFM measurements. $^{18}$ This paper aims to verify the ISR methodology using actual measurement results by testing samples with dielectric films of Zirconium dioxide and Silicon dioxide on Silicon wafers with etched pits and measuring the roughness and the pits depth of the buried interfaces and comparing these measurements with those of the original substrate prior to thin film deposition. Theoretic consideration shows the ISR method works for perturbations of up to $\pm 10$ nm depending on the materials used. We have analyzed the pits ranging from $-2.5$ to $-16.4$ nm and have proven a good agreement with those original surfaces measured by CSI before deposition of the dielectric films.

II. METHODOLOGY

A. Coherence scanning interferometry

In a typical CSI hardware configuration, a LED is often preferred as a light source over a halogen light for its intensity, lower heat production, and an appropriate bandwidth for surface inspection. The bandwidth of the light source and the numerical aperture (NA) of the objective lens mainly determines the coherence length. $^{19,20}$

Although a white light source such as a halogen light creates a shorter coherence length than those from LEDs making detection of the interference fringes on test surfaces less easy, a halogen light is used in this method. This is because this methodology involves a numerical optimization in the frequency domain, and thus a wider bandwidth in the region between 400 and 750 nm leads to a more accurate solution.

The interference signal, interferogram denoted by $I$, observed by a photo-detector can be approximated as a combination of a DC part and an oscillatory part with respect to the incident light angle averaged over the numerical aperture $\langle h \rangle$. The symbol $h$ also denotes the observed interference signal, which is normally about $2\pi f Z / \cos \theta$, where $Z$ is the data-sampling interval $Z_{\text{step}}$, $f$ is the frequency of the interference signal, which is normally about 60–70 nm, corresponding to one eighth of the mean effective wavelength (see Fig. 2(a)). The distortion due to the thin film assembly is finally interpreted as the change in phase and amplitude in the frequency domain. Note that normally a known flat surface such as Si or SiC is used as a reference sample with its field reflectance averaged over the numerical aperture of the objective lens $I_{\text{ref}}$. The symbol $\theta$ also denotes the incident light angle averaged over the numerical aperture (see Appendix A).

FIG. 1. Interference signal of (a) the bare Si substrate, (b) the 560 nm SiO$_2$ on Si with respect to the scanning direction $Z [\mu m]$.

B. Helical complex field (HCF) function

A general interferogram consists of a DC component and a symmetric oscillation as shown in Fig. 1(a). The presence of transparent films on a substrate will distort the shape of the interference signal as shown in Fig. 1(b). This distortion is determined by the amplitude reflection coefficients of the thin film assembly.

The HCF theory $^{12,15,16}$ can be used to estimate the film thickness based on the distortion, where the positive side-band of the Fourier transform with respect to the frequency $\nu$, denoted by $F_{\nu} [I_{SB+}]$, of the interference signals from the film assembly $I$ and reference sample $I_{\text{ref}}$ are computed. The HCF function is theoretically and experimentally derived. Let $HCF^d$ be the HCF function derived from an actual measurement and $HCF^l$ be the one that is theoretically synthesized, respectively, with its film thickness vector $d = \{d_1, \ldots, d_l\}^T$, then they are expressed by $^{22,23}$

\[
HCF^d(\nu; d) = \frac{F_{\nu} [I(Z)]_{SB+}}{F_{\nu} [I_{\text{ref}}(Z)]_{SB+}},
\]

\[
HCF^l(\nu; d) = \frac{\tilde{r}_{\text{ref}}(\nu)}{I_{\text{ref}}} \exp(2\pi i \Delta Z_{\text{HCF}} \cos \theta),
\]

where the unknown parameter $\Delta Z_{\text{HCF}}$ satisfies $-2\Delta Z_{\text{step}} < \Delta Z_{\text{HCF}} < 2\Delta Z_{\text{step}}$. Here, $\Delta Z_{\text{step}}$ is the data-sampling interval of the interference signal, which is normally about 60–70 nm, corresponding to one eighth of the mean effective wavelength (see Fig. 2(a)). The distortion due to the thin film assembly is finally interpreted as the change in phase and amplitude in the frequency domain. Note that normally a known flat surface such as Si or SiC is used as a reference sample with its field reflectance averaged over the numerical aperture of the objective lens $I_{\text{ref}}$. The symbol $\theta$ also denotes the incident light angle averaged over the numerical aperture (see Appendix A).

FIG. 2. (a) Cross-sectional view of the film thickness $d$ determined by the HCF curve fitting and real topography in each film and (b) top view of the global HCF function and the local HCF function at a pixel.
The set of the film thickness $d$ is numerically determined by minimizing the least squares error between $HCF^d$ and $HCF^d$ with respect to $d$ and $\Delta z_{HCF}$. This procedure is broken down to a curve fitting between the HCF functions with respect to the real and imaginary parts.

As is apparent from Figs. 3(b) and 3(c), a single pixel HCF function suffers significantly from noise (dominated by photo-electron noise) in the frequency domain. The global determined HCF function denoted by $HCF^d$, consists of an HCF function generated from an ensemble of pixel intensity sequences. This global function typically corresponds to an area with $M$ pixels say, $200 \times 200$ as shown in Fig. 2(b), and exhibits dramatically a better signal/noise as shown in Fig. 3(a). Following the preceding film thickness measurement method using the HCF function, the optimal set of the HCF functions due to the noise as illustrated in Fig. 2(a). With this method, computation to determine $d + \Delta d$ at all the pixels would require $M$ non-linear optimizations. This would require an excessive and time-consuming computing particularly when the number of pixels in a measurement area is large. Also, the optimization itself may well be compromised because of the significant noise apparent in the frequency domain.

C. Extension of HCF function to interfacial surface roughness measurement

A large number of optimizations might be required even if the application of $J_{HCF}$ to each pixel by substituting $HCF^d$ with the corresponding local determined HCF function $HCF^d_m$ was effectively feasible. It is also very difficult to achieve a good fit between the synthesized and the determined HCF functions due to the noise as illustrated in Fig. 3(b) and thus this may lead to spurious results.

The ISR method provides a solution to this difficulty by effectively avoiding the noise effect in the optimization process. The ISR method uses such a relatively smooth $HCF^d$ as in Fig. 3(a) to approximate such a rough $HCF^d_m$ as in Figs. 3(b) and 3(c) by means of the first order partial derivative of the synthesized HCF function. This approach brings two advantages: first a smooth local HCF function can be established; second a linear least squares error optimization will be conducted rather than a non-linear one.

1. First order approximation of the synthesized HCF function

Considering small deviations $\Delta d$ from the global film thickness $d$ determined by the method discussed in Section II B, a primarily approximated expression for the local synthesized HCF function $HCF^d_m$ can be presented by using $HCF^d$.

\[
HCF^d_m(\nu, \mathbf{d} + \Delta \mathbf{d}) \simeq HCF^d(\nu, \mathbf{d}) + \{ \nabla_d HCF^d(\nu, \mathbf{d}) \}^\top \Delta \mathbf{d} \\
\simeq HCF^d + j4\pi\nu \cos \theta \cdot HCF^d \\
\times \left\{ \Delta d_{\text{sub}} + \sum_{l=1}^L G_l(\nu; \mathbf{d}) \Delta d_l \right\},
\]

where the set of the film thickness $d$ is understood hereafter to be $\mathbf{d} = \{ d_{\text{sub}}, d_1, \ldots, d_L \}^\top$ including a perturbation of the substrate $\Delta d_{\text{sub}}$ as shown in Fig. 2(a). $G_l$ is defined as a gain of the perturbation in the $l$-th layer and is analytically provided in advance (see Appendix B). Note that $\Delta d_l$ cannot be obtained explicitly from $J_{HCF}$ although, this will not cause problems because what is essential in the following calculations is $\Delta d_{\text{sub}}$. The value of each $\Delta d_l$ should be small enough ($\leq 10$ nm) to approximate the partial derivatives.

The perturbations in the film thickness $\Delta d$ are determined by minimizing the least-square based error function $J_{px} = \int |HCF^d_{px} - HCF^d(\nu; \mathbf{d} + \Delta \mathbf{d})|^2 d\nu$ with respect to the perturbations $\Delta d$, where $HCF^d_{px}$ represents a locally determined HCF function provided by the corresponding actual measurement. This locally determined HCF function apparently contains too much noise to be used for the non-linear optimization of $J_{HCF}$. Perturbations to be determined by means of $J_{px}$ should be less than $\sim 10$ nm to maintain the quality of approximation depending on the structure of the film assembly.

2. Linear least-squares optimization

In the actual computation, the variables and functions are treated in a discrete manner such that $\mathbf{v} = [\nu_1, \nu_2, \ldots, \nu_m]^\top$, and thus the merit function $J_{px}$ is effectively re-written
\[ J_{px} = \sum_{i=1}^{m} \left[ \text{HCF}_{px}^d (\nu_i) - \text{HCF}_{px}^d (\nu_i; \mathbf{d} + \Delta \mathbf{d}) \right]^2, \]
\[ = \left| \text{HCF}_{px}^d - \left( \text{HCF}^d + \text{Diag}[\text{HCF}^d] \mathbf{G} \Delta \mathbf{d} \right) \right|^2, \quad (3) \]

where

\[ \mathbf{G} = j4\pi \cos \tilde{\theta} \begin{bmatrix} \nu_1 & \nu_1 \cdot G_1 (\nu_1) & \cdots & \nu_1 \cdot G_L (\nu_1) \\ \nu_2 & \cdots & \cdots \\ \vdots & \cdots & \cdots \\ \nu_m & \nu_m \cdot G_1 (\nu_m) & \cdots & \nu_m \cdot G_L (\nu_m) \end{bmatrix}, \]

\[ \text{Diag}[\text{HCF}^d] = \begin{bmatrix} \text{HCF}^d (\nu_1) & \cdots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \cdots & \text{HCF}^d (\nu_m) \end{bmatrix}, \]

\[ \text{HCF}^d_{px} = \left[ \text{HCF}^d (\nu_1), \ldots, \text{HCF}^d (\nu_m) \right]^\top, \]

\[ \text{HCF}^d = \left[ \text{HCF}^d (\nu_1), \ldots, \text{HCF}^d (\nu_m) \right]^\top. \]

As in Eq. (3), the function \( \text{HCF}_{px}^d \) depends linearly on \( \Delta \mathbf{d} \). Thus, the optimal solution \( \Delta \mathbf{d} \) of the linear least squares error problem in Eq. (3) is explicitly determined in the well-known form as follows:\textsuperscript{25}

\[ \Delta \mathbf{d} = (\mathbf{G}^\top \mathbf{G})^{-1} \mathbf{G}^\top \mathbf{u}, \quad (4) \]

where

\[ \mathbf{u} = \text{Diag}[\text{HCF}^d]^{-1} \left[ \text{HCF}^d_{px} - \text{HCF}^d \right]. \]

This gives the Best Linear Unbiased Estimators (BLUE) for solving over-determined linear problems. It follows that the thin film thickness, or the interfacial surface roughness at a pixel is finally obtained as \( \mathbf{d} + \Delta \mathbf{d} \).

This optimization avoids such a time-consuming non-linear optimization as \( J_{HCF} \), and thus enables the determination of interfacial surface topographies in realistic timescales.

### III. EXPERIMENT

#### A. Experimental setup

The CSI instrument, CCI HD (Taylor Hobson Ltd), was used to observe the interference signals. As in the specification sheet,\textsuperscript{26} the 4 M pixel camera of the instrument allows noise-robust signal acquisition by averaging the signals over four pixels to obtain one signal with high lateral resolution maintained. This four-pixel unit is henceforth regarded as a single pixel for purposes of the model.

As discussed in Section II A, a light source with a broad bandwidth in the visible region is necessary for this technique. In this experiment, a halogen lamp is used and its nominal characteristic light intensity is shown in Fig. 11(a). For the assumption discussed in Section II A to be satisfied, a \( \times 10 \) objective lens shown in Table I is used for the data acquisition.\textsuperscript{26} A Si optical flat surface is used as a reference sample. Note that any reference material can be used here but its refractive index \( N_{ref} \) must be known in advance.

#### B. Test sample fabrication

The test samples were fabricated by etching a square pit on a Silicon wafer substrate using a 30 kV gallium Focused Ion Beam (FIB/SEM dual beam system). An example is shown in Fig. 4(a). The thin film oxide layers were then deposited using reactive magnetron sputtering with metal targets, an oxygen plasma source, and a pulsed DC power supply. A 20 μm × 20 μm pit was created by FIB etching,

\[ \begin{array}{|c|c|}
\hline
\text{Item} & \text{Specification} \\
\hline
\text{Magnification} & \times 10 \\
\text{Field of view (mm²)} & 1.65 \times 1.65 \\
\text{Optical resolution (μm)} & 1.3 \\
\text{Numerical aperture} & 0.3 \\
\text{Design} & \text{Mirau} \\
\hline
\end{array} \]

This experiment avoids such a time-consuming non-linear optimization as \( J_{HCF} \), and thus enables the determination of interfacial surface topographies in realistic timescales.
and its depth was controlled by timing the FIB etching and prior knowledge of the etching rate.

Three types of oxide thin films were deposited on the Silicon wafers using the reactive magnetron sputtering as shown in Table II: producing 514.4 nm for SiO$_2$, 308.6 nm for a second SiO$_2$ thin film, and 338.9 nm for a ZrO$_2$ thin film, which correspond to the Quarter Wavelength Optical Thickness (QWOT), respectively. The refractive index of the etched areas will be slightly modified due to surface amorphisation and Gallium ion implantation. In this study, we have ignored any such changes in the substrate refractive index.

### C. Measurement result and analysis

Measurements were obtained from the samples listed in Table II using the CSI system. The measurement data was post-processed: using the ISR method and a conventional CSI surface measurement. The latter method detects the peak positions of the interference signals (CCI method$^{27}$). Comparisons between the results of the two methods were then made to verify the performance of the ISR method.

| Sample number | Target QWOT$^a$ | Film  | Film thickness (nm)$^b$ | FIB etching depth (nm)$^c$ |
|---------------|----------------|-------|------------------------|---------------------------|
| #1-1          | 5 SiO$_2$      | 536.8 | 3.2                    |
| #1-2          | 5 SiO$_2$      | 544.9 | 7.2                    |
| #1-3          | 5 SiO$_2$      | 540.4 | 16.4                   |
| #1-4          | 5 SiO$_2$      | 547.7 | 9.4                    |
| #2-1          | 3 SiO$_2$      | 317.5 | 15.3                   |
| #2-2          | 3 SiO$_2$      | 316.3 | 9.7                    |
| #2-3          | 3 SiO$_2$      | 319.6 | 8.7                    |
| #2-4          | 3 SiO$_2$      | 320.2 | 2.5                    |
| #3-1          | 5 ZrO$_2$      | 309.5 | 15.5                   |
| #3-2          | 5 ZrO$_2$      | 309.5 | 12.1                   |
| #3-3          | 5 ZrO$_2$      | 314.1 | 9.0                    |
| #3-4          | 5 ZrO$_2$      | 313.6 | 4.3                    |

$^a$QWOT is at the wavelength of 600 nm.

$^b$A global film thickness is obtained by numerical optimization.

$^c$The depth of the pits of the samples were measured before deposition with the CCI HD (Taylor Hobson Ltd).

1. **Result: Depth of the FIB etched square pit**

The depth of the etched pits measured by the ISR method will be compared with those obtained using the conventional CSI method. The depths are computed by comparing the average height of the pits and that of the rest of the measured area. Note that roughness on the surfaces involved is not considered for this evaluation.

While the conventional CSI method only considers the light reflection from the whole thin film/substrate assembly to measure a three dimensional surface, the ISR method successfully separates the contribution of the substrate from the complete thin film/substrate signal. As a result, the ISR method reproduces the buried surface roughness more faithfully comparing (a) with (b) and (c) in Figs. 4–6.

2. **Analysis: Correlation of the determined surfaces**

The correlation coefficients between $S_o$ and $S_{ISR}$ and $S_{CSI}$ are provided in Fig. 8. The Correlation coefficient...
operator Cor is defined here to be the maximum value of the correlation function of two different surfaces as follows:

\[
\text{Cor}[S_1, S_{\text{mtd}}] = \max_{x,y} \left\{ \frac{S_1(x, y) \otimes S_{\text{mtd}}(x, y)}{\| S_1(x, y) \| \cdot \| S_{\text{mtd}}(x, y) \|} \right\},
\]

where \( S_1 \otimes S_2 \) denotes the cross-correlation function between surfaces \( S_1 \) and \( S_2 \), and \( \| \cdot \| \) implies the \( L^2 \) norm; \( mtd \) represents the method to be used, chosen as either ISR or CSI.

It is clearly seen that the correlation coefficients decline in an inverse proportion to the depth of the corresponding square pit. This is because the measurements and images obtained using the ISR method contain spurious features which are associated with the signal to noise in the local pixel.

Root Mean Square (RMS) errors between \( S_o \) and \( S_{\text{ISR}} \) and between \( S_o \) and \( S_{\text{CSI}} \) are shown in Figs. 9(a) and 9(b), respectively. As shown, the RMS errors between \( S_o \) and \( S_{\text{ISR}} \) are almost all smaller than 1 nm regardless of the thin film type and the depth of the etched pit, whereas the conventional CSI method results in larger errors as shown in Fig. 9(b). The root cause of the RMS errors in Fig. 9(a) is related to the various sources of noise in the signal. The noise stems from several sources not only including uncertainty in the measurement of optical constants using spectroscopic ellipsometry, but also from noise generated in the CSI system and its surrounding environment. Although the ISR method results in a larger level of RMS error with the #2 SiO\(_2\) sample compared to the #3 ZrO\(_2\) sample as shown in Fig. 9(a), it provides the #2 sample with a higher correlation coefficient for the depth than #3 sample as shown in Fig. 8. This implies that the #2 SiO\(_2\) sample is more susceptible to random noise.

3. Analysis: Surface roughness comparison between pre- and post-deposition

The surface roughness determined by the ISR method is expected to increase from the original due to the noise induced by the system, surrounding environment, and uncertainty in the physical constants. A Silicon wafer is used as the substrate in this experiment such that its surface should be regarded to be “flat.” The original surface roughness (\( S_q \)) of the areas surrounding the pit is 0.63 ± 0.11 nm.
expected, those determined by the ISR method resulted in an increased $S_q$ as shown in Fig. 10. This roughness is also visually apparent in a comparison between the surfaces in Figs. 4(a) and 4(b). As in Fig. 10, the roughness values are evenly increased slightly depending on the type of the film and its thickness.

IV. DISCUSSION

As far as determination of the pit depth is concerned, the ISR method works best for #1 SiO$_2$ samples with $QWOT = 5$, followed by #2 SiO$_2$ with 3 and #3 ZrO$_2$ with 3 as in Fig. 7(a). $QWOT$ is known to be proportional to the number of peaks and valleys found in a spectral reflectance as shown in Fig. 11(b).$^{28}$ The HCF function has such spectral features corresponding to its field reflectance. Therefore, an HCF function with a small $QWOT$ might have difficulty in numerical optimization because the smaller number of the features of the function results in less accurate curve-fitting. This implies that the value of $QWOT$ has a significant impact on the performance of the HCF based techniques. The ISR method is not an exception because the HCF function introduced in this method is a first order approximation of the original HCF function. The difference in the performance of the ISR method shown in Fig. 7(a) is considered to be the values of the $QWOT$s, which are effectively 5.27 for #1 samples, 3.09 for #2, and 4.59 for #3 as shown in Table III.

Reflection from the thin film assembly influences the signal to noise ratio under the assumption that the noise level is unchanged throughout the measurements. It follows that the increases in the roughness values, which is discussed in Section III C 3, are thought to be negatively proportional to the product between the intensities of light $L_I$ and an averaged reflection $R(\nu) = |\bar{R}(\nu)|$ such that $g(\nu) = R(\nu) \cdot L_I(\nu)$ and $G = \int g(\nu) d\nu$. Let $G$ be the integration of the product $g(\nu)$, then this is proportional to the number of signal photo-electrons, this can be considered as an indication of the robustness of the measurement to the noise effect.

Figures 11(b) and 11(c) show the spectral reflectance of the samples with a mean film thickness and the computations of their $g(\nu)$, respectively. In Table III, the $G$ values, mean $g$ over the effective bandwidth (from 430 to 750 nm), and effective $QWOT$ values of the samples with the mean
thickness are presented. As expected, the $G$ value for the #2 SiO$_2$ sample is the smallest among the three groups, and so is the mean values of $g$ by 10%–20% compared with the rest of the groups. From these, one reasonable explanation for the level of roughness induced on the substrate is the signal to noise ratio associated with the spectral product between a reflection of a film structure and the intensity of a light source. Evidently, an error arises from the approximation in Eq. (B3) and uncertainties in refractive indices also influence the signal to noise ratio.

V. CONCLUSIONS

Application of the conventional CSI techniques to thin film metrologies such as film thickness and interfacial surface roughness, is limited by the film thickness because the interferogram is generally analysed in the time domain where the peaks of the signal should be separated. The general requirement for the film thickness is over 1.5 $\mu$m. The introduction of the HCF function to the thin film regime (from 0.05 to 1.5 $\mu$m) enabled the measurement of global film thickness over hundreds of pixels. For thin films of significant optical thickness (such as a SiO$_2$ layer of a few hundred nanometers), the HCF signature is easily sufficient to allow interfacial topographies to be determined on a pixel-by-pixel basis using this approach; as the optical thickness of the film(s) is further reduced, this capability becomes progressively less viable. Nevertheless, the HCF function used in the ISR method, derived from a first order approximation of the HCF function, extends the HCF method’s capability to determine the local interfacial or buried surfaces and provide a three dimensional representation. In addition, heavy computation for numerical optimization can be avoided as this method uses a linear approximation of the HCF function.

The Silicon wafer samples having an etched pit depth ranging from 2.5 to 16.4 nm were deposited with Silica and Zirconia oxide. These pits were measured through a thin film layer by using the ISR method and the existing CSI method (CCI). Prior theoretic consideration showed the ISR method held for perturbations of up to $\sim$10 nm and the substrate surfaces determined by the ISR method were almost identical to the original surfaces. Together with the experimental results presented in the earlier top surface ISR publication, these results provide a substantive experimental evidence for the ISR theory.

The roughness of the substrate surfaces measured by the ISR method tends to be larger than those of the original surfaces. This approach numerically determines the local film thickness including the substrate surface profile by establishing a synthesized HCF function by means of the global HCF counterpart and compares it with a relatively noisy local HCF function. It follows that the smaller the noise, the less is the roughness induced on the surface measurement. Standard noise reduction techniques such as signal accumulation or post-analysis filtering could be applied to minimize this roughness.

The CSI technique is a powerful well-established tool for the precise measurement of surface topography. The development of the HCF function has already extended its capability for the determination of refractive index. This paper extends its capability further to include the three-dimensional measurement of buried interfaces.

ACKNOWLEDGMENTS

The authors are grateful to RCUK for financial support through the SuperSolar Hub (EPSRC Grant No. EP/J017361/1).
APPENDIX A: REFLECTION FROM A MULTI-LAYER FILM ASSEMBLY

Let $N(\nu) = n(\nu) - j\kappa(\nu)$ be a spectral complex refractive index of the frequency $\nu$, then this index consists of the index of refraction $n$ and the extinction coefficient $\kappa$.

The optical admittance $\eta$ is a function of the polarisation-state $(p,s)$, the complex refractive index $N$ and the incident angle $\theta$ for each layer. The optical admittances for the $p$ and $s$ planes are given by $\eta_p = N \gamma / \cos \theta$ and $\eta_s = N \gamma / \cos \theta$, where $\gamma = (\epsilon_0 / \mu_0)^{1/2}$, $\epsilon_0$ and $\mu_0$ are the permittivity and magnetic permeability of vacuum, respectively. The mean complex amplitude reflection coefficient, $r$, of the multi-layer film structure shown in Fig. 2(a) (where the $i$th layer has thickness $d_i$, refractive index $N_i$, and incident angle $\theta_i$) is then represented by

$$r(\nu, d, \theta) = \frac{1}{2} \left( r_p(\nu, d, \theta) + r_s(\nu, d, \theta) \right),$$

where

$$r_{p,s}(\nu, d, \theta) = \frac{\eta_{air}^{p,s} - \eta_{p,s}}{\eta_{air}^{p,s} + \eta_{p,s}}, \quad d = \{d_1, \ldots, d_L\}^\top.$$  \hspace{1cm} (A1)

Here $\eta_{air}^{p,s}$ and $\eta_{p,s}^{i}$ are the optical admittances of the air and the substrate, respectively. $L$ is the number of layers in the multi-layer model, and $Y_{p,s}$ is the input optical admittance of assembly for each polarisation plane, which is derived from the characteristic matrix of the assembly $[B_{p,s}, C_{p,s}]^\top$ as follows:

$$Y_{p,s}(d) = \frac{C_{p,s}}{B_{p,s}},$$

where

$$[B_{p,s}, C_{p,s}] = \prod_{i=1}^{L} \left[ \begin{array}{cc} \cos \delta_i & j \sin \delta_i / \eta_{p,s}^{i} \\ j \eta_{p,s}^{i} \sin \delta_i & \cos \delta_i \end{array} \right] \left[ \begin{array}{c} 1 \\ \eta_{p,s}^{i} \end{array} \right].$$

and where

$$\delta_i = 2\pi\nu N_i d_i \cos \theta_i, \quad \cos \theta_i = \frac{1}{N_i} \sqrt{N_i^2 - \sin^2 \theta_i}. \hspace{1cm} (A2)$$

Considering the passage of the incident light through an objective lens, the overall complex reflection coefficient of the layer structure $\bar{r}$ is defined by averaging $r$ over the numerical aperture ranging from $\theta_{\text{min}}$ to $\theta_{\text{max}}$ multiplied by the weighting function $w(\theta)$ such that $\bar{r}(\nu, d, \theta) = \int_{\text{min}}^{\text{max}} \int_{\text{w}}(\theta) (\nu, d, \theta) \cdot w d\theta$ where $\int w d\theta = 1$. Likewise the averaged incident angle $\bar{\theta}$ is determined as $\bar{\theta} = \int_{\text{min}}^{\text{max}} \theta \cdot w d\theta$.

The underlying assumption to justify this approach of determining the mean field-reflectance $\bar{r}$ is that for a randomly polarised CSI instrument with a low to medium numerical aperture (NA), we regard the $s$ and $p$-plane reference mirror (RM) field-reflectance to be approximately equal such that $r_{RM}^{p}(\nu, \theta) \approx r_{RM}^{s}(\nu, \theta)$.

APPENDIX B: GAIN COMPUTATION

Terms in 2 can be expressed by partial derivatives

$$\left\{ \nabla_d HCF^s(\nu, \hat{d}) \right\}^\top \Delta d = \frac{\partial (HCF^s)}{\partial d_{\text{sub}}} \Delta d_{\text{sub}} + \sum_{i=1}^{L} \frac{\partial (HCF^s)}{\partial d_i} \Delta d_i.$$  \hspace{1cm} (B1)

Following this, the second and third terms in Eq. (B1) are analytically determined, respectively, as follows:

$$\frac{\partial (HCF^s)}{\partial d_{\text{sub}}} = j 4\nu \cos \theta \cdot \bar{r} \exp \left( j 4\nu \Delta HCF \cos \bar{\theta} \right),$$

$$\frac{\partial (HCF^s)}{\partial d_i} = \left( j 4\nu \cos \theta \cdot \bar{r} + \frac{\partial \bar{r}}{\partial d_i} \right) \exp \left( j 4\nu \Delta HCF \cos \bar{\theta} \right),$$

$$\frac{\partial \bar{r}}{\partial d_i} = \frac{\partial \bar{r}}{\partial r_i}, \quad e^{j\theta} = j \frac{\partial \bar{r}}{\partial d_i}, \quad \text{where} \quad \arg(r) = \chi,$$

$$\Delta HCF = d_{\text{sub}} + \sum_{i=1}^{L} d_i - \Delta d_{\text{ref}}.$$  \hspace{1cm} (B2)

By substituting the terms in Eq. (B2) into Eq. (B1), Eq. (B1) is finally expressed as follows:

$$\left\{ \nabla_d HCF^s(\nu, \hat{d}) \right\}^\top \Delta d = +j 4\nu \cos \theta \cdot HCF^s \left( \Delta d_{\text{sub}} + \sum_{i=1}^{L} G_i(\nu, \hat{d}) \Delta d_i \right),$$

where

$$G_i(\nu, \hat{d}) = 1 + \frac{1}{4\nu \cos \theta} \frac{\partial \bar{r}(\hat{d})}{\partial d_i}. \hspace{1cm} (B3)$$

Then, the partial derivative of $\chi$ is expressed by

$$\frac{\partial \chi}{\partial d_i} = \frac{1}{|\hat{d}|^2} \left( \frac{\partial \text{Re} \bar{r}}{\partial d_i} \frac{\partial \text{Im} \bar{r}}{\partial d_i} - \frac{\partial \text{Im} \bar{r}}{\partial d_i} \frac{\partial \text{Re} \bar{r}}{\partial d_i} \right),$$  \hspace{1cm} (B4)

where Eq. (B4) is effectively computed in advance by approximating the real and imaginary parts of the partial derivative of the amplitude reflection coefficient as follows:

$$\frac{\partial \text{Re} \bar{r}}{\partial d_i} \approx \frac{\text{Re} \bar{r}(\nu, \hat{d}_i)}{2 \Delta d_i},$$

$$\frac{\partial \text{Im} \bar{r}}{\partial d_i} \approx \frac{\text{Im} \bar{r}(\nu, \hat{d}_i)}{2 \Delta d_i},$$

where $\hat{d}_i = \{\hat{d}_{\text{sub}}, \hat{d}_1, \ldots, \hat{d}_i + \Delta d, \ldots, \hat{d}_L\}^\top$, $\hat{d}_i = \{\hat{d}_{\text{sub}}, \hat{d}_1, \ldots, \hat{d}_i - \Delta d, \ldots, \hat{d}_L\}^\top$. \hspace{1cm} (B5)

1. A. F. Fercher, J. Biomed. Opt. 1, 157 (1996).
2. S. K. Debnath, S.-W. Kim, M. P. Kothiyal, and P. Hariharan, Appl. Opt. 49, 6624 (2010).
3. ISO, ISO 25178-604:2013(en), Geometrical Product Specifications (GPS)—Surface Texture: Areal—Part 604: Nominal Characteristics of Non-Contact (Coherence Scanning Interferometry) Instruments (ISO, International Organization for Standardization, Geneva, 2013).
4. P. de Groot, in Optical Measurement of Surface Topography (Springer, 2011), Chap. 9, pp. 187–208.
5. E. Beaurepaire, A. C. Boccara, M. Lebéc, L. Blanchot, and H. Saint-Jalmes, Opt. Lett. 23, 244 (1998).
6. B. S. Lee and T. C. Strand, Appl. Opt. 29, 3784 (1990).
7 P. J. De Groot and X. C. de Lega, in *Optical Engineering-Applications* (International Society for Optics and Photonics, 2008), p. 70640L.
8 A. Bosseboeuf and S. Petitgrand, in *Optical Metrology* (International Society for Optics and Photonics, 2003), pp. 1–16.
9 S.-W. Kim and G.-H. Kim, *Appl. Opt.* 38, 5968 (1999).
10 S. Kim and G. Kim, “Method for measuring a thickness profile and a refractive index using white-light scanning interferometry and recording medium therefore,” U.S. patent application 6,545,763 B1 (2003).
11 Y. Ghim and S. Kim, *Appl. Opt.* 48, 799 (2009).
12 D. Mansfield, “Apparatus for and a method of determining characteristics of thin-layer structures using low-coherence interferometry,” WO patent application PCT/GB2005/002,783 (2006).
13 P. J. de Groot, “Interferometry method for ellipsometry, reflectometry, and scatterometry measurements, including characterization of thin film structures,” U.S. patent application 7,403,289 B2 (2008).
14 I. Abdulhalim, *Meas. Sci. Technol.* 12, 1996 (2001).
15 I. Abdulhalim, *Proc. SPIE* 6186, 61860O (2006).
16 B. Maniscalco, P. M. Kaminski, and J. M. Walls, *Thin Solid Films* 550, 10 (2014).
17 D. I. Mansfield, “Apparatus for and a method of determining surface characteristics,” U.S. patent application 13/352,687 (2012).
18 I. Abdulhalim, *J. Mod. Opt.* 48, 279 (2001).
19 D. Mansfield, *Proc. SPIE* 7101, 71010U (2008).
20 I. Abdulhalim, *J. Opt. A: Pure Appl. Opt.* 8, 952 (2006).
21 A. Safrani and I. Abdulhalim, *Appl. Opt.* 50, 3021 (2011).
22 D. Mansfield, “Apparatus for and a method of determining a characteristic of a sample,” WO patent application PCT/GB2015/052,339 (2016).
23 H. Yoshino, P. M. Kaminski, R. Smith, J. M. Walls, and D. Mansfield, *Appl. Opt.* 55, 4253 (2016).
24 H. Yoshino, R. Smith, J. M. Walls, and D. Mansfield, *Proc. SPIE* 9749, 97490P (2016).
25 T. Lewis and P. Odell, *J. Am. Stat. Assoc.* 61, 1063 (1966).
26 Taylor Hobson Ltd., *CCI System Specifications* (Taylor Hobson Ltd, 2012).
27 A. Bankhead and I. McDonnell, “Interferometric surface profiling,” GB patent application 2,390,676 (2008).
28 H. Macleod, *Thin-Film Optical Filters*, 3rd ed., Series in Optics and Optoelectronics (Taylor & Francis, 2001).