An approach for solving an inverse spherical two-phase Stefan problem arising in modeling of electric contact phenomena

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1 | INTRODUCTION

Partial differential equations play an important role for the development of models in heat conduction and investigated in various aspects (see, for example, literature$^{1-3}$ and the references therein). To realize the physical changes, some models need to be expressed as free or moving boundary problems. The theory of free boundaries has seen great progress in the last half century. For the general literature up to 2015, we refer to Friedman$^4$ and Chen et al.$^5$ Also, a long list of studies and literature therein are devoted to Stefan-type problems and their analytical and numerical solutions.$^6-13$

Arcing processes are very rapid and include phase transformations. Thus, it is reasonable to use Stefan-type problems for mathematical modeling of this phenomena. Worth to say that exact solution of the problem allows to elucidate and enhance understanding of arcing processes and contribute to the development of the arc theory. Present study is devoted to theoretical investigation and mathematical modeling of arc phenomena in electrical contacts and appears as a continuation of recent studies where mathematical modeling of short arcing is considered.$^{14,15}$ While in 2 studies,$^{14,15}$ the analytical solutions of the one- and two-phase (direct) Stefan problems are found, in this paper, we consider an inverse Stefan problem for which along with unknown temperature functions, heat flux function has to be determined. In the considered model, heat flux depends on time variable; however, it is well known that besides time variable, heat flux...
depends on numerous factors like electron bombardment and diverse electric contact effects like tunnel, Joule, Thomson, and Peltier effects. Thus, this model does not claim to be universal for all electric contact phenomena occurring during opening or switching electric contacts.

In this study, we consider spherical model that agrees with Holm’s so-called ideal sphere usually applied for electric contacts with small contact surface (radius of $b < 10^{-4} \text{m}$) and low electric current.\textsuperscript{16}

1.1 Problem statement

In a spherical model, the contact spot is given by the spherical surface of radius $b$. The heat flux $P(t)$ entering this surface melts the electric contact material (liquid zone $b < r < a(t)$) and then passes further through the solid zone $a(t) < r < \infty$ (for the illustration of the model, see Figure 1).

The heat equations for each zone are

$$\frac{\partial \theta_1}{\partial t} = a_1^2 \left( \frac{\partial^2 \theta_1}{\partial r^2} + \frac{2}{r} \frac{\partial \theta_1}{\partial r} \right), \quad b < r < a(t), \quad t > 0,$$

$$\frac{\partial \theta_2}{\partial t} = a_2^2 \left( \frac{\partial^2 \theta_2}{\partial r^2} + \frac{2}{r} \frac{\partial \theta_2}{\partial r} \right), \quad a(t) < r < \infty, \quad t > 0,$$

subjected to boundary condition at $r = b$

$$-\lambda_1 \frac{\partial \theta_1(b, t)}{\partial r} = P(t)$$

and to free boundary

$$\theta_1(a(t), t) = T_m.$$
\[ \theta_2(a(t), t) = T_m, \]  

the Stefan's condition

\[ -\lambda_1 \frac{\partial \theta_1(a(t), t)}{\partial r} = -\lambda_2 \frac{\partial \theta_2(a(t), t)}{\partial r} + L \gamma \frac{da}{dt}, \]

as well as the condition at infinity

\[ \theta_2(\infty, t) = 0. \]

Here, \( \theta_1 \) and \( \theta_2 \) are unknown heat functions, \( P(t) \) is an unknown heat flux coming from electric arc, \( T_m \) is a melting temperature of electric contact material, \( f(r) \) is a given function, and \( a_1, a_2, \lambda_1, \lambda_2, L, \) and \( \gamma \) are given constants. In the equation, power balance is described by Stefan's condition (9). The function \( a(t) \) describing the interphase location is given in the inverse problem under consideration.

## 2. Problem Solution

Suppose that the initial and free boundary conditions are analytic functions and they can be expanded in Taylor series as

\[ f(r) = \sum_{n=0}^{\infty} \frac{f^{(n)}(b)}{n!} (r - b)^n, \quad a(t) = b + \sum_{n=1}^{\infty} a_n t^{n/2}. \]  

We represent the solution of (1) to (10) in the following form

\[ \theta_1(r, t) = \frac{1}{r} \sum_{n=0}^{\infty} \left( 2a_1 \sqrt{t} \right)^n \left[ A_n t^n er f c \frac{r-b}{2a_1 \sqrt{t}} + B_n t^n er f c \frac{b-r}{2a_1 \sqrt{t}} \right], \]

\[ \theta_2(r, t) = \frac{1}{r} \sum_{n=0}^{\infty} \left( 2a_2 \sqrt{t} \right)^n \left[ C_n t^n er f c \frac{r-b}{2a_2 \sqrt{t}} + D_n t^n er f c \frac{b-r}{2a_2 \sqrt{t}} \right], \]

where coefficients \( A_n, B_n, C_n, \) and \( D_n \) have to be found. Here, \( i^n er f c \) is integral error function determined by the following recurrent formulas:

\[ i^n er f c = \int_x^\infty i^{n-1} er f c \, dv, \quad n = 1, 2, \ldots, \]

\[ i^n er f c = er f c = \sqrt{\pi} \int_x^\infty \exp(-v^2) dv. \]

**Lemma 1.** The integral error function holds the following properties:

1. \( \lim_{x \to \infty} \frac{i^n er f c(-x)}{x^n} = \frac{2}{n!}, \)
2. \( \lim_{x \to 0} \left( 2a_1 \sqrt{t} \right)^n C_n t^n er f c \frac{r-b}{2a_1 \sqrt{t}} = 0, \)
3. \( \lim_{x \to 0} \left( 2a_2 \sqrt{t} \right)^n D_n t^n er f c \frac{b-r}{2a_2 \sqrt{t}} = \frac{2}{n!} D_n (r - b)^n. \)

The proof of the lemma can be given by the L'Hopital's rule and properties of \( i^n er f c \) function.

**Theorem 2.** Let \( f \) be \( n \) times differentiable analytic function. Then

\[ \lim_{t \to 0} \theta_2(r, t) = \frac{1}{r} \sum_{n=0}^{\infty} \frac{2}{n!} D_n (r - b)^n. \]

**Proof.** Using Lemma 1, it is easy to see that

\[ \lim_{t \to 0} \theta_2(r, t) = \lim_{t \to 0} \frac{1}{r} \sum_{n=0}^{\infty} \left( 2a_2 \sqrt{t} \right)^n D_n t^n er f c \frac{b-r}{2a_2 \sqrt{t}} \]

\[ = \frac{1}{r} \lim_{t \to 0} \sum_{n=0}^{\infty} D_n (r - b)^n \frac{i^n er f c \left( \frac{r-b}{2a_2 \sqrt{t}} \right)^n}{\left( \frac{r-b}{2a_2 \sqrt{t}} \right)^n} = \frac{1}{r} \sum_{n=0}^{\infty} \frac{2}{n!} D_n (r - b)^n. \]
2.1 Calculation of coefficients

By the theorem and equations (4) and (11), we can write

$$\lim_{t \to 0} \theta_2(r, t) = f(r) = \sum_{n=0}^{\infty} \frac{f^{(n)}(b)}{n!} (r-b)^n.$$  

Using Theorem 2 and letting $F(r) = rf(r)$, we have

$$\sum_{n=0}^{\infty} \frac{2}{n!} D_n(r-b)^n = \sum_{n=0}^{\infty} \frac{F^{(n)}(b)}{n!} (r-b)^n,$$

$$D_n = \frac{F^{(n)}(b)}{2}.$$  

(12)

From (8), when we put $r = a(t)$, then $b$ will be canceled and there left only series $a(t) = \sum_{n=1}^{\infty} a_1 t^{n/2}$. In integral error function, if we take $\sqrt{t}$ out of the brackets,

$$i^n er f c \frac{\sqrt{t}(a_1 + a_2 \sqrt{t} + a_3 t + \ldots)}{2a_1 \sqrt{t}} = i^n er f c \frac{a(t)}{2a_1},$$

where $a(t)$ becomes

$$a(t) = a_1 + a_2 \sqrt{t} + a_3 t + \ldots = \sum_{n=1}^{\infty} a_n t^{n-1}.$$  

Let us take $\sqrt{t} = \tau$, and we obtain from Equation 8

$$\frac{1}{a(\tau)} \sum_{n=0}^{\infty} \left( 2a_1 \sqrt{\tau} \right)^n \left[ C_n i^n er f c(\tau) + D_n i^n er f c(-\delta(\tau)) \right] = T_m.$$  

(13)

where $\delta(\tau) = \frac{a(\tau)}{2a_1}$.

To calculate coefficient $C_n$, we apply Leibniz and Faa Di Bruno formulas and Bell polynomials. Using Leibniz formula, we have

$$\frac{\partial^k [i^n er f c(\pm \delta)]}{\partial \tau^k} \bigg|_{\tau=0} = \begin{cases} 0, & \text{for } k < n \\ \frac{n^k}{(k-n)!} [i^n er f c(\delta)]^{(k-n)}, & \text{for } k \geq n \end{cases}.$$  

Using Faa Di Bruno formula and Bell polynomials for a derivative of a composite function, we have

$$\frac{\partial^{k-n}[i^n er f c(\pm \delta)]}{\partial \tau^{k-n}} \bigg|_{\tau=0} = \sum_{m=1}^{k-n} (i^n er f c(\pm \delta))^{(m)} \bigg|_{\delta=0} B_{k-n,m}(\delta^{(k-n-1)}(\tau)) \bigg|_{\tau=0},$$

where

$$B_{k-n,m} = \sum_{j_1, j_2, \ldots, j_{k-n-m+1}} \frac{(k-n)!}{j_1! j_2! \ldots j_{k-n-m+1}!} \frac{1}{\delta^1 \delta^2 \delta^3 \ldots \delta^{k-n-m+1}}.$$  

and $j_1, j_2, \ldots$ satisfy the following equations

$$j_1 + j_2 + \ldots + j_{k-n-m+1} = m,$$

$$j_1 + 2j_2 + \ldots + (k-n-m+1)j_{k-n-m+1} = k-n$$

for $m \geq n$. Since

$$[i^n er f c(\pm \delta)]^{(m)}|_{\delta=0} = (-1)^m i^{n-m} er f c 0 = (\mp 1)^m \frac{\Gamma \left( \frac{n-m+1}{2} \right)}{(n-m)! \sqrt{\pi}}$$
by taking $k$th derivatives of both sides of (13) at $\tau = 0$, we have

$$
\sum_{n=0}^{k} C_n (2a_2)^n \frac{k!}{(k-n)!} \sum_{m=1}^{k-n} (-1)^m t^{m-1} e^{r f \left( \xi_1 \right)} \sum_{j_1, j_2, \ldots, j_{k-n-m+1}} \frac{(k-n)!}{j_1! j_2! \cdots j_{k-n-m+1}!} \delta_{j_1} \delta_{j_2} \cdots \delta_{j_{k-n-m+2}}
$$

$$
= T_m \alpha_k - \sum_{n=0}^{k} D_n (2a_2)^n \frac{k!}{(k-n)!} \sum_{m=1}^{k-n} \left( -1 \right)^m t^{m-1} e^{r f \left( \xi_1 \right)} \sum_{j_1, j_2, \ldots, j_{k-n-m+1}} \frac{(k-n)!}{j_1! j_2! \cdots j_{k-n-m+1}!} \delta_{j_1} \delta_{j_2} \cdots \delta_{j_{k-n-m+2}}
$$

(14)

for $k = 0, 1, 2, \ldots$.

From expression (14), we express coefficients $C_n$. From (7), we have

$$
\frac{1}{a(\tau)} \sum_{n=0}^{\infty} (2a_1 \sqrt{t})^n \left[ A_n t^{n} e^{r f \left( \xi_1 \right)} + B_n i^{n} e^{r f \left( -\xi_1 \right)} \right] = T_m,
$$

where

$$
\xi_1 = \frac{a(\tau)}{2a_1}.
$$

(15)

In the same manner, we get recurrent formula from (15) where we express $A_n$ in terms of $B_n$ as

$$
\sum_{n=0}^{k} A_n (2a_2)^n \frac{k!}{(k-n)!} \sum_{m=1}^{k-n} \left( -1 \right)^m t^{m-1} e^{r f \left( \xi_2 \right)} \sum_{j_1, j_2, \ldots, j_{k-n-m+1}} \frac{(k-n)!}{j_1! j_2! \cdots j_{k-n-m+1}!} \delta_{j_1} \delta_{j_2} \cdots \delta_{j_{k-n-m+2}}
$$

$$
= T_m \alpha_k - \sum_{n=0}^{k} D_n (2a_2)^n \frac{k!}{(k-n)!} \sum_{m=1}^{k-n} \left( -1 \right)^m t^{m-1} e^{r f \left( \xi_2 \right)} \sum_{j_1, j_2, \ldots, j_{k-n-m+1}} \frac{(k-n)!}{j_1! j_2! \cdots j_{k-n-m+1}!} \delta_{j_1} \delta_{j_2} \cdots \delta_{j_{k-n-m+2}}
$$

(16)

where

$$
\xi_1 = \frac{a_1}{2a_2}, \xi_2 = \frac{a_2}{2a_2}, \ldots, \xi_{k-n-m+2} = \frac{a_{k-n-m+2}}{2a_2}.
$$

We can express coefficients $A_n$ from this expression. In Stefan’s condition (9), we take first derivative of

$$
\frac{da}{dt} = a_1 \frac{1}{2\sqrt{t}} + a_2 + \frac{3}{2} a_3 \sqrt{t} + 2a_4 t + \cdots = \sum_{n=1}^{\infty} a_n t^{n-2},
$$

and we take $\sqrt{t} = \tau$. So

$$
\lambda_1 \frac{1}{a^2(\tau)} \sum_{n=0}^{\infty} (2a_1 \tau)^n \left[ A_n t^{n} e^{r f \left( \xi_1 \right)} + B_n i^{n} e^{r f \left( -\xi_1 \right)} \right]
$$

$$
- \lambda_1 \frac{1}{a(\tau)} \sum_{n=0}^{\infty} (2a_1 \tau)^{n-1} \left[ -A_n t^{n-1} e^{r f \left( \xi_1 \right)} + B_n i^{n-1} e^{r f \left( -\xi_1 \right)} \right]
$$

$$
= \lambda_2 \frac{1}{a^2(\tau)} \sum_{n=0}^{\infty} (2a_2 \tau)^n \left[ C_n t^{n} e^{r f \left( \xi_2 \right)} + D_n i^{n} e^{r f \left( -\xi_2 \right)} \right]
$$

$$
- \lambda_2 \frac{1}{a(\tau)} \sum_{n=0}^{\infty} (2a_2 \tau)^{n-1} \left[ -C_n t^{n-1} e^{r f \left( \xi_2 \right)} + D_n i^{n-1} e^{r f \left( -\xi_2 \right)} \right] + a(\tau) L \beta,
$$

(17)

where $a(\tau) = \sum_{n=1}^{\infty} a_n \tau^{n-2}$.

If we multiply both sides of (17) by $\tau a(\tau)$ and use (7) and (8), we get the following expression

$$
- \lambda_1 \sum_{n=0}^{\infty} (2a_1 \tau)^{n-1} \left[ -A_n t^{n-1} e^{r f \left( \xi_1 \right)} + B_n i^{n-1} e^{r f \left( -\xi_1 \right)} \right]
$$

$$
= T_m \left( \lambda_2 - \lambda_1 \right) - \lambda_2 \sum_{n=0}^{\infty} (2a_2 \tau)^{n-1} \left[ -C_n t^{n-1} e^{r f \left( \xi_2 \right)} + D_n i^{n-1} e^{r f \left( -\xi_2 \right)} \right] + \beta(\tau) L \beta,
$$

(18)
where
\[ \beta(\tau) = \sum_{n=1}^{\infty} (b + a_n \tau^n) \sum_{n=1}^{\infty} a_n \tau^n. \]

Taking k-times derivative of both sides of (18) at \( \tau = 0 \), we get recurrent formula for \( B_n \) coefficients.

By using all these expression on condition (6), we express coefficient of heat flux. From (6), we get
\[ \frac{\lambda_1}{B} \sum_{n=0}^{\infty} \left( 2a_1 \sqrt{t} \right)^n \left[ A_n t^n e^{rfc0} + B_n t^n e^{rfc0} \right] + \frac{\lambda_3}{B} \sum_{n=0}^{\infty} \left( 2a_1 \sqrt{t} \right)^{n-1} \left[ A_n t^{n-1} e^{rfc0} - B_n t^{n-1} e^{rfc0} \right] = \sum_{n=0}^{\infty} P_n t^{n/2}, \]

\[ \begin{cases} P_0 = \frac{\lambda_1}{b} t^n e^{rfc0}[A_1 - B_1 + \frac{1}{b} A_0 + \frac{1}{b} B_0], \\ P_1 = \frac{\lambda_1}{b} (2a_1) t^n e^{rfc0}[A_2 - B_2 + \frac{1}{b} A_1 + \frac{1}{b} B_1], \\ P_2 = \frac{\lambda_1}{b} (2a_1)^2 t^n e^{rfc0}[A_3 - B_3 + \frac{1}{b} A_2 + \frac{1}{b} B_2], \\ \vdots \\ P_n = \frac{\lambda_1}{b} (2a_1)^n t^n e^{rfc0}[A_{n+1} - B_{n+1} + \frac{1}{b} A_n + \frac{1}{b} B_n]. \end{cases} \]

Remark 3. For the convergence of temperature functions \( \Theta_1, \Theta_2 \), it is possible to follow the idea proposed in Holm.\(^{15}\)

### 3 | APPROXIMATE SOLUTION OF A TEST PROBLEM

In this section, the collocation method that is practical for engineers is applied using 3 points \( t_0 = 0, t_1 = 0.5 \), and \( t_2 = 1 \).

To show the effectiveness of the method, we proposed the following problem. Solution is found both exactly and approximately.

Let us consider
\[ \frac{\partial \theta_1}{\partial t} = a_1^2 \left( \frac{\partial^2 \theta_1}{\partial r^2} + \frac{2}{r} \frac{\partial \theta_1}{\partial r} \right), \quad \text{for } b < r < a(t), \]
\[ \frac{\partial \theta_2}{\partial t} = a_2^2 \left( \frac{\partial^2 \theta_2}{\partial r^2} + \frac{2}{r} \frac{\partial \theta_2}{\partial r} \right), \quad \text{for } a(t) < r < \infty, \]
\[ \theta_1(b, 0) = T_m, \]
\[ \theta_1(r, 0) = f(r), \]
\[ -\lambda_1 \frac{\partial \theta_2(b, t)}{\partial r} = P(t), \]
\[ \theta_1(a(t), t) = \theta_2(a(t), t) = T_m, \]
\[ -\lambda_1 \frac{\partial \theta_1(a(t), t)}{\partial r} = -\lambda_2 \frac{\partial \theta_2(a(t), t)}{\partial r} + L \frac{d \alpha}{dt}, \]
\[ \theta_2(\infty, t) = 0. \]

We represent solution of the problem in the following form
\[ \theta_i(r, t) = \frac{1}{r} \sum_{n=0}^{\infty} \left( 2a_i \sqrt{t} \right)^n \left[ A_n(C_n) t^n e^{rfc} + B_n(D_n) t^n e^{rfc} \right], \]

It is clear that from (20), we get \( D_n \) and from (21), we get \( C_n \). Also, using (21), we can express \( A_n \) in terms of \( B_n \). Thus, we can find \( B_n \) by (22).

Let \( \alpha(t) = b + a \sqrt{t} \) and \( \theta_i = \frac{1}{r} \Phi(r, t) \) where \( i = 1, 2 \). Taking derivative, we get
\[ \frac{\partial \theta_i}{\partial r} = \frac{1}{r} \Phi'(r, t) - \frac{1}{r^2} \Phi(r, t). \]
Let \( f(r) = r \). Using (21), we have

\[
\begin{align*}
C_0 i^0 e^{c \frac{1}{2a_2} r} + D_0 i^0 e^{c \left( -\frac{1}{2a_1} \right)} + 2a_2 \sqrt{i} \left[ C_1 i^1 e^{c \frac{1}{2a_2} r} + D_1 i^1 e^{c \left( -\frac{1}{2a_2} \right)} \right] + (2a_2 \sqrt{i})^2 \left[ C_2 i^2 e^{c \frac{1}{2a_2} r} + D_2 i^2 e^{c \left( -\frac{1}{2a_2} \right)} \right] + \ldots &= T_m(b + a \sqrt{i}),
\end{align*}
\]

\[
C_0 = \frac{b T_m - D_0 i^0 e^{c \left( -\frac{1}{2a_2} \right)}}{i^0 e^{c \left( -\frac{1}{2a_2} \right)}},
\]

\[
C_1 = \frac{a T_m - D_1 i^1 e^{c \left( -\frac{1}{2a_2} \right)}}{i^1 e^{c \left( -\frac{1}{2a_2} \right)}},
\]

\[
C_n = -\frac{D_n i^n e^{c \left( -\frac{1}{2a_2} \right)}}{i^n e^{c \frac{1}{2a_2}}} \text{, where } i = 2, 3, \ldots.
\]

Let us transform (22) to obtain

\[
-\lambda_1 \left[ \frac{1}{r} \Phi'_1(r, t) - \frac{1}{r^2} \Phi_1(r, t) \right] = -\lambda_2 \left[ \frac{1}{r} \Phi'_2(r, t) - \frac{1}{r^2} \Phi_2(r, t) \right] + \frac{L \gamma}{2 r},
\]

\[
-\lambda_1 \left[ \alpha(r) \sum_{n=0}^{\infty} (2a_1 r)^{n-1} \left[ -\alpha_1 i^{n-1} e^{c \left( \frac{1}{2a_1} \right)} + B_n i^{n-1} e^{c \left( -\frac{1}{2a_1} \right)} \right] \right]
- \sum_{n=0}^{\infty} (2a_2 r)^{n-1} \left[ C_n i^{n-1} e^{c \left( \frac{1}{2a_2} \right)} + D_n i^{n-1} e^{c \left( -\frac{1}{2a_2} \right)} \right]
- \sum_{n=0}^{\infty} (2a_2 r)^{n} \left[ C_n i^n e^{c \left( \frac{1}{2a_2} \right)} + D_n i^n e^{c \left( -\frac{1}{2a_2} \right)} \right] + \frac{L \gamma}{2 a_2 r}.
\]

Multiply both sides on \( r \), we get

\[
-\lambda_1 \left[ \alpha(r) r \Phi'_1 - r \Phi_1 \right] = -\lambda_2 \left[ \alpha(r) r \Phi'_2 - r \Phi_2 \right] + \frac{L \gamma}{2 a_2 r}.
\]

For \( r = 0 \),

\[
-\lambda_1 \left[ b A_0 i^{-1} e^{c \left( \frac{1}{2a_1} \right)} + b B_0 i^{-1} e^{c \left( -\frac{1}{2a_1} \right)} \right] = -\lambda_2 \left[ b C_0 i^{-1} e^{c \left( \frac{1}{2a_2} \right)} + b D_0 i^{-1} e^{c \left( -\frac{1}{2a_2} \right)} \right] + \frac{L \gamma}{2 a_2},
\]

and from (21), we get

\[
A_0 = \frac{T_m - B_0 i^{0} e^{c \left( -\frac{1}{2a_1} \right)}}{i^{0} e^{c \left( -\frac{1}{2a_1} \right)}}.
\]

Let

\[
- A_0 (C_n) i^{n-1} e^{c \left( \frac{1}{2a_1} \right)} + B_n (D_n) i^{n-1} e^{c \left( -\frac{1}{2a_1} \right)} > = \Psi_i,
\]

\[
A_0 (C_n) i^n e^{c \left( \frac{1}{2a_1} \right)} + B_n (D_n) i^n e^{c \left( -\frac{1}{2a_1} \right)} = \Psi_i
\]

and
Let \( f(r) = r \), \( T_m = 0 \), \( \lambda_1 = \lambda_2 = 1 \), \( a_1 = a_2 = 1 \), \( L = \alpha = \gamma = 1 \). Mathcad 15 is used for computations, and we get approximate values for \( A_0 = 2.96 \times 10^{-6} \), \( A_1 = 0.341 \), \( A_2 = -9.72 \), \( B_0 = -9.335 \times 10^{-7} \), \( B_1 = -0.057 \), and \( B_2 = 1 \) whereas exact values are \( A_0 = 2.96 \times 10^{-6} \), \( A_1 = 0.341 \), \( A_2 = -9.72 \), \( B_0 = -9.335377 \times 10^{-7} \), \( B_1 = -0.05678483 \), and \( B_2 = 1.00000000001 \).

In Figure 2, the graphs of both reconstructed exact \((\text{exact Flux P(0,t)})\) and approximate \((\text{approx Flux P(0,t)})\) flux functions are shown.

**FIGURE 2** Exact and approximate values of flux function [Colour figure can be viewed at wileyonlinelibrary.com]
In Figures 3 and 4, we illustrate the graph of relative error function calculated by following formula that is less than 0.0032% at point $x = 0, 0 \leq t \leq 0.025$

$$\text{Error}_{\text{rel}} = \left| \frac{\text{exact flux-approximate flux}}{\text{exact flux}} \right| \cdot 100.$$

### 4 | CONCLUSION

A mathematical model describing heat propagation in electric contacts is constructed on the base of two-phase spherical inverse Stefan problem. The heat source $P(t)$ which is occurred by arcing, bridging, etc. can be determined from Equation 19. Temperature functions $\Theta_1, \Theta_2$ that are given in the form of series are determined whose coefficients $A_n, B_n, C_n,$ and $D_n$ are also determined from Equations 14, 16, and 17. In the test problem, we used maximum principle for error estimate; the deviation does not exceed $3.2 \times 10^{-5}$ for 3 points. For better precision, more points has to be taken and better computer characteristics are required.

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