Blast Load Analysis on Bridge Subjected to Various Standoff Distance

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Abstract: Need for designing important buildings to resist blast masses is growing in the recent time due to the increasing terrorist operations. A bomb explosion can cause very serious injury on the bridge pier. Collapse of one structural member in the vicinity of the source of explosion can also then create integral stress redistributions and lead to crumple of different members and at the end of the entire structure. Due to threat from such extreme loading conditions, efforts have been made to develop methods of structural analysis and design to resist blast loads. The evaluation and layout of systems subjected to blast loads require an in depth understanding of blast phenomena and its consequences on numerous structural elements. Blast loads Dynamic masses that want to be cautiously calculated similar to earthquake and wind loads. The study of effect of blast loading on a Bridge pier is carried out. Effects of variable blast source weight are calculated by considering various distances from point of explosion for bridge pier. The calculations of blast load on bridge pier for all cases are carried out by using IS 4991. The blast load is analytically determined as a pressure-time history and structural response predictions are performed with ANSYS using non-linear direct integration time history analyses. The influence of the lateral load response due to blast in terms of peak deflections, normal stress and bending stress is determined. The performance level of bridge pier under blast load is under collapse level for given blast load.

Keywords: Dynamic analysis, bridges, blast, explosion, time history, ANSYS

1. INTRODUCTION

Impact burdens are viewed as one of the outrageous burdens influencing structures, and even a limited quantity of hazardous can deliver extreme confined harm to the structure. Now and again, this confined extreme harm can possibly advance to worldwide breakdown of the whole structure. A blast begins when a high unstable material is exploded shaping an explosion wave in the material. The explosion wave commonly moves at speeds of 18,000 ft/s to 20,000 ft/s and is pressurized at up to 4x106 psi with temperatures in the scope of 8,000°F. This hot gas is extended, as a fast arrival of vitality happens.

A stun front moving at supersonic speed is framed before this gas and is known as the impact wave or stun front. This wave proliferates outward every which way from the explosion focus. The front of the wave, or the stun front, ventures quicker that the speed of sound. The progression of the air mass behind the stun brings about an outward development of air and flotsam and jetsam causing drag stacking on the structure and is known as the dynamic weight. This dynamic weight stacking is a component of the auxiliary shape, occurrence weight, air thickness, and the touchy material. Figure 1.2 demonstrates a normal bend for episode weight and the dynamic weight after some time. The number and power of residential and global psychological militant exercises, including the September 11, 2001 assault on World Trade Center towers in New York, have increased our worries towards the security of our foundation frameworks. Psychological militants assault targets where human losses and financial outcomes are probably going to be generous. Transportation frameworks have been viewed as alluring targets on account of their openness and potential effects on human lives and monetary action.

A. Blast on Bridges

The study of the structural and material response of bridges under blast loads are conducted either by experiments or numerical simulations. However, experiments are difficult to be done in full scale and are costly to perform. In addition to that, the other important factor is the difficulty of measuring the various parameters in the field for close-in detonations where the instrument is often destroyed and the failure process is difficult to document. Therefore, numerical solutions are considered an attractive approach to evaluating bridge response to explosions and are very important to support any blast experiments on bridges.
B. Objectives of study
1. To study effect & damage pattern of blast on bridge pier.
2. Study of Blast mechanism as per IS 4991
3. Bridge pier analysis with various cross sections such as circular, rectangular using ANSYS workbench.
4. To study stress distribution after blast load is applied and to study load deflection curve

II. LITERATURE REVIEW
Shuichi Fujikura[1] This paper reports the exploratory and expository examination of these two kinds of segments under impact stacking. The seismically structured RC and steel jacketed RC segments did not display pliable conduct under impact stacking and bombed in shear at their base as opposed to flexural yielding.

Eric B. Williamson For testing under these conditions, enormous impact burdens should be produced, which are exorbitant and require working with faculty that are fittingly able to complete this work.[2] Exploratory perceptions were utilized to assess the exhibition of a few plan parameters and to decide the limit and disappointment farthest point conditions of strengthened solid pathway connect sections exposed to huge impact loads.

Kiger, Sam[3] A. One-fourth of the straightforward range scaffold and half scale for the nonstop framework were demonstrated considering the fitting limit balance conditions

Z. Yi, A. K.[4] Agrawal To maintain a strategic distance from dock pull-outs and improve the exhibition of impact stacked sections A base measure of containment support ought to be expanded by half over the whole segment tallness.

S.K. Hashemi[5] the consequences of the limited component re-enactments are utilized to evaluate the potential dynamic breakdown reaction of a link stayed scaffold subject to different impact stacking situations.

Mohamed H. Mussa,[6] A thickness of 750 mm gave off an impression of being exceptionally impervious to the blast of a SDT or compartment for all the examined profundities, and the best opposition was accomplished at a profundity of 8 m, which ought to be considered by architects to guarantee the wellbeing of an underground box burrow when exposed to a fantastic surface blast.

S.K. Hashemi, M.A. Bradford †, H.R. Valipour 2016. In the course of recent decades, impact burdens have been perceived as one of the extraordinary stacking occasions that must be considered in the plan of significant structures, for example, link stayed spans

III. METHODOLOGY WORK STUDY
The impact burden relies on two central point characterized by the bomb size or charge weight W, and the standoff separation (R) between the impact source and the objective. Consider the structures exposed to a shoot proportional in respect some kg of TNT at a specific standoff separation

IV. PROBLEM STATEMENT
- Type of structure: Bridge Structure
- Height of bridge: 5 M
- Total span: 19 M
- Width: 12 M
- Circular Pier Dia.: 1M
- Rectangular Pier: 1x0.9M
- Explosive charge weight: 200kg, 500kg, 800kg, 1000kg
- Support: Fixed

V. RESULT AND DISCUSSION
A. ANSYS model For Circular Pier

Numerical Model
Because of the multifaceted nature of cement, its constitutive relations contrast from the diverse burden case. For this situation, a few diverse constitutive models of cement were proposed. The elastoplastic constitutive model dependent on the addition

Hypothesis is utilized to depict the constitutive relations of cement. This model sessile-Warnke's five-parameter yield paradigm, uniform quality foundation and related stream rule. Due to the extraordinary structure style of the steel-solid composite bar to concrete-filled steel rounded segment joints, the conduct varies in the better place of cement. The solid in the center territory of cement filled steel rounded limited by the steel cylindrical is under triaxial burden cases. As per the numerical investigation and test results, the Han-linhai model is sensible and solid by utilizing the repression record to characterize the solid limited by the steel cylindrical.
Table 1. Total Deformation for 200kg

| TIME (sec) | 15 FEET | 30 FEET | 50 FEET | 100 FEET |
|------------|---------|---------|---------|----------|
| 0.1        | 0       | 0       | 0       | 0        |
| 0.2        | 0.01332 | 0.01047 | 0.00314 | 0.00523  |
| 0.3        | 0.02663 | 0.02093 | 0.00628 | 0.00105  |
| 0.4        | 0.03995 | 0.0314  | 0.00942 | 0.00157  |
| 0.5        | 0.05327 | 0.04186 | 0.01256 | 0.00209  |
| 0.6        | 0.06659 | 0.05233 | 0.0157  | 0.00262  |
| 0.7        | 0.0799  | 0.06279 | 0.01884 | 0.00314  |
| 0.8        | 0.09322 | 0.07326 | 0.02198 | 0.00366  |
| 0.9        | 0.10654 | 0.08373 | 0.02512 | 0.00419  |
| 1          | 0.11985 | 0.09419 | 0.02825 | 0.00471  |

Graph 1. Deformation for Blast Load 200kg

Table 2. Total Deformations For 500 Kg

| TIME      | 15 FEET | 30 FEET | 50 FEET | 100 FEET |
|-----------|---------|---------|---------|----------|
| 0.1       | 0       | 0       | 0       | 0        |
| 0.2       | 0.02131 | 0.02094 | 0.00837 | 0.00094  |
| 0.3       | 0.04262 | 0.04187 | 0.01675 | 0.00188  |
| 0.4       | 0.06392 | 0.0628  | 0.02512 | 0.00283  |
| 0.5       | 0.08523 | 0.08174 | 0.03349 | 0.00377  |
| 0.6       | 0.10654 | 0.10467 | 0.04186 | 0.00471  |
| 0.7       | 0.12784 | 0.12561 | 0.05023 | 0.00566  |
| 0.8       | 0.14915 | 0.14654 | 0.05861 | 0.00659  |
| 0.9       | 0.17046 | 0.16748 | 0.06698 | 0.00753  |
| 1         | 0.19177 | 0.18841 | 0.07535 | 0.00848  |

Graph 2. Total Deformations for 500 Kg

Table 3. Total Deformation for 800 Kg

| TIME      | 15 FEET | 30 FEET | 50 FEET | 100 FEET |
|-----------|---------|---------|---------|----------|
| 0.1       | 0       | 0       | 0       | 0        |
| 0.2       | 0.02131 | 0.02094 | 0.00837 | 0.00094  |
| 0.3       | 0.04262 | 0.04187 | 0.01675 | 0.00188  |
| 0.4       | 0.06392 | 0.0628  | 0.02512 | 0.00283  |
| 0.5       | 0.08523 | 0.08174 | 0.03349 | 0.00377  |
| 0.6       | 0.10654 | 0.10467 | 0.04186 | 0.00471  |
| 0.7       | 0.12784 | 0.12561 | 0.05023 | 0.00566  |
| 0.8       | 0.14915 | 0.14654 | 0.05861 | 0.00659  |
| 0.9       | 0.17046 | 0.16748 | 0.06698 | 0.00753  |
| 1         | 0.19177 | 0.18841 | 0.07535 | 0.00848  |

Graph 3. Total Deformations for 800 Kg

Table 4. Total Deformations for 1000 Kg

| TIME      | 15 FEET | 30 FEET | 50 FEET | 100 FEET |
|-----------|---------|---------|---------|----------|
| 0.1       | 0       | 0       | 0       | 0        |
| 0.2       | 0.02131 | 0.02094 | 0.00837 | 0.00094  |
| 0.3       | 0.04262 | 0.04187 | 0.01675 | 0.00188  |
| 0.4       | 0.06392 | 0.0628  | 0.02512 | 0.00283  |
| 0.5       | 0.08523 | 0.08174 | 0.03349 | 0.00377  |
| 0.6       | 0.10654 | 0.10467 | 0.04186 | 0.00471  |
| 0.7       | 0.12784 | 0.12561 | 0.05023 | 0.00566  |
| 0.8       | 0.14915 | 0.14654 | 0.05861 | 0.00659  |
| 0.9       | 0.17046 | 0.16748 | 0.06698 | 0.00753  |
| 1         | 0.19177 | 0.18841 | 0.07535 | 0.00848  |
Graph 4. Total Deformations for 1000 Kg

VI. CONCLUSION

1) It is observed that in circular pier maximum deformation is obtain at 15ft and minimum deformation at 100ft. Also observed that for all weight of blast, there is some reduction in deformation. Normal strain, equivalent strain, strain energy, and normal stress. Also studied blast resistant bridge pier theories, the enhancement of building security against the effects of explosives in both architectural and structural point of view and the analysis techniques that should be carried out. In the present, studied about Blast mechanism for different terms related to blast and characteristics of blast. Also studied various types of blast such as commonly used blast TNT and Blast Mitigation Techniques and their applications. Blast can create significant effect on bridge. So, it’s necessary to design important bridges for blast load. However, for 15 ft and 30 ft the deformation values are nearly same in circular pier for 800 kg.

2) It is also observed that in Rectangular pier, maximum deformation is obtained at 15ft and minimum deformation at 100ft Also observed that for all weight of blast, there is some reduction in deformation. Normal strain, equivalent strain, strain energy, and normal stress.

3) All model having maximum total deformation at 15 feet for circular and rectangular.

4) All model having minimum total deformation at 100 feet for circular and rectangular.

5) Circular pier has maximum deformation which is 22.01% at 15 feet as compared to rectangular pier for 200kg and 500kg TNT weight.

6) Circular pier has maximum deformation which is 23.74% at 15 feet as compared to rectangular pier for 800kg and 1000kg TNT weight.

7) The comparison between circular pier and rectangular pier, it is observed that in circular pier has maximum total deformation as compared to rectangular pier.

8) After comparing all the result of a circular pier and rectangular pier, rectangular pier will become better for future use in construction as compared to circular pier under the blast load condition.

9) It is observed that deformation is more when its standoff distance is near to pier.

10) According to validation it is observed that both deformations is near about same so it concludes that this project work in right path.

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