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Determination of quartz on membrane filters by X-ray diffraction

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Recognition of the health hazards due to prolonged exposure to airborne respirable silica has prompted the development of analytical methods for quartz based upon spectrophotometric (3, 17, 18), infrared (13, 20), and X-ray diffraction (1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 14, 21) techniques. The diffractometric method is attractive because it uses a small sample, is nondestructive and rapid, and all the individual crystalline mineral phases in a sample are potentially identifiable. In environmental monitoring, for which dust samples are collected on filters, the direct analysis of the dust on the filter would be convenient. Such a technique omits the removal and preparation of the dust sample for separate analysis and avoids errors associated with these procedures.

The difficulties experienced in devising a suitable direct X-ray diffractometric method have identified a number of problem areas. Matrix effects such as mass absorption and interferences, particle orientation, size distribution and the quality of quartz standards are the most critical. Initial investigators (4, 19) limited the weight and composition of the loading on the filters so that the effect of sample mass absorption would be negligible and a linear relationship would exist between the quantity of the analyte and its diffraction line intensity.

The analysis of the thin layer specimens on organic membranes suffers from high X-ray background scatter. This problem has been overcome by Bumstead with the use of pure silver filters and internal standardization (5). Leroux and co-workers have developed a method in which the silver line intensity is used to compensate for mass absorption effects in the surrounding dust (14). The direct use of the silver filters for the routine sampling of workplace air has several disadvantages.
however. The most important of these are connected with the retention and shielding properties of the filter material and with the need for silver line intensity measurements for every filter before use.

Mixed ester or polyvinyl chloride (PVC) membrane filters can be used for dust collection, and, after ashing or other suitable treatment, the dust sample is redeposited on a silver filter for “direct” X-ray diffractometry (5, 12). This approach greatly increases the laboratory work as compared with quartz determination on the sampling filter.

Nuclepore polycarbonate filters are very thin membrane filters with a low diffraction background, low mass absorption, small pore size, and high surface retention for collected dust. The theory of Altree-Williams forms the basis of an improved diffractometric technique for the use of Nuclepore filters in monitoring airborne quartz (2). The tendency for quartz particles to exhibit preferred orientation in thin layers deposited on smooth surfaces such as PVC or Nuclepore filters is responsible for the high variation of quartz line intensities (8). This orientation effect can only partly be compensated for by the rotation of the sample holder during the spectrometric measurement.

Since the late 1960s the Finnish Institute of Occupational Health has used Millipore membrane filters for aerosol sampling. Its preferred method for determining the respirable quartz concentration in workplace air has been that of modified Andreasen liquid sedimentation combined with X-ray diffractometry (21). The method is limited to a sample size of over 10 mg. The present study was initiated with particular reference to the foundry industry, for which the determination of quartz content in smaller samples is often needed. The task was to combine the most convenient membrane filter sampling with an accurate and rapid analysis. Dust samples were collected on a filter without any size-selective classifier, and the filter was then subjected to X-ray diffraction measurement with digital line intensity calculation. The effects of mass absorption, interferences, particle orientation, and size distribution were assessed.

MATERIALS AND METHODS

X-ray apparatus

A Philips X-ray diffractometer was used comprising a generator (PW 1130), a vertical goniometer (PW 1050), a sample spinner (PW 1064), a graphite monochromator (PW 1152), an amplifier (PW 4280), a proportional counter (PW 1965), and a copper anode X-ray tube (PW 2103). A fixed divergence slit of 1° and a receiving slit of 0.25° were installed in the instrument. Membrane filters were mounted in the diffractometer and drawn taut with a concentric ring holder. The samples were analyzed at a tube power of 50 kV and 20 mA. Diffraction line intensity was measured with a Hewlett-Packard Integrator 3380 A, while the spectra were scanned at an angle rate of 1°/min. The α-quartz diffraction lines 4.26 Å, 3.34 Å and 1.82 Å appeared at 2θ angles of 20.85°, 26.67° and 50.15°, respectively. The integrator subtracted the background intensity using numerical peak fitting and interpolation. The net peak area reported by the integrator or the peak height measured by a recorder was alternatively used as the diffraction line intensity. A silicon blank was used as an external standard to correct for long-term instrumental drift.

Standard preparation

Both the samples and standards were collected on Millipore AAWP mixed cellulose ester membrane filters with a diameter of 37 mm and a pore size of 0.8 μm. The standards with known amounts of deposited material were prepared by liquid filtration. The dust suspension contained 100 mg of dried material in 100 ml of distilled water. The suspension was agitated with an ultrasonic stirrer which dispersed agglomerates. An aliquot of the stock suspension was pipetted and then filtered in a Millipore filtering apparatus (XX 15047). With 50 ml of added water the dust was smoothly deposited over a circular area of 34 mm in diameter, which is the same as the effective filtering diameter of an air sampling monitor Millipore M25W 037 AO. The membrane filters were then dried.
at 60°C for 2 h. The apparent dust amount was calculated from the aliquot volume, and the result was checked by the weighing of the dried filter before and after the deposition. The filters had an electrostatic charge, and a static eliminator Staticmaster Ionizing Unit Model 2U 500 was used to discharge them.

The quartz standards were made of fractionated Fyle quartz, which originated from Fyleverken Ltd. (Eriksdal, Sweden) and was kindly supplied by the Aerosol Section of Arbetarskyddsstyrelsen, Stockholm. Most of the particles were less than 10 μm in size, and the yield of those below 5 μm was about 85 w-%, as determined by liquid sedimentation. In Scandinavian countries this raw material is used by industrial hygiene laboratories as a standard for 100 % α-quartz. The calcium fluoride and iron oxide used as quartz matrices were analytical grade Merck chemicals.

RESULTS

Precision of standard preparation

The precision of preparing quartz standards is affected by variation in the weighing and drying of the membrane filters, in the pipetting and filtering of the dust suspension, and in the mounting of samples in the diffractometer. Sixteen replicate standards were made of a mixture which contained 10 % Fyle quartz in calcium fluoride. The calculated weights of the total deposits were 10 mg each. Table 1 shows the variation of the peak areas for the 20.85° and 26.67° quartz lines and for the 28.30° and 47.10° lines of calcium fluoride. The relative standard deviations of the intensities ranged from 9.0 to 12.1 % for the two quartz lines and from 4.4 to 5.7 % for the two calcium fluoride lines. No significant difference between the variation of peak heights and that of peak areas could be found.

The alteration of filter weight during preparation was determined after 50 ml of pure distilled water was sucked through ten separate filters. The weight difference caused by the treatment was less than ± 0.2 mg, a variation which corresponds to the imprecision of weighing a slightly hygroscopic filter. The water extractables are reported by the manufacturer to be less than 4 % of the filter weight, if voluminous amounts of water are used (15). When the apparent weights of deposited material were calculated from suspension volumes and compared with the weighings, an average material loss of 3 % was observed. The difference between the results ranged from −11 to +4 % for a series of 80 loaded filters. In the latter test the deposits varied from 1 to 50 mg of dust.

The analytical precision of the diffraction intensity measurements is also shown in table 1. The relative standard deviation of the quartz peak areas ranged from 8.0 to 10.3 % in the case of ten replicate determinations on one filter loaded with

| 2θ       | Average peak height (mm) | Preparing, mounting and measuring a standard filter | Mounting and measuring a standard filter |
|----------|---------------------------|---------------------------------------------------|-----------------------------------------|
| 20.85° quartz | 9                        | 12.1                                              | 10.3                                    |
| 26.67° quartz | 42                       | 9.0                                               | 8.0                                     |
| 28.30° calcium fluoride | 230            | 4.4                                               | 3.3                                     |
| 47.10° calcium fluoride | 150            | 5.7                                               | 4.1                                     |

Table 1. Precision of preparing a quartz standard and measuring its X-ray intensities. The filter was loaded with 1 mg of quartz mixed with 9 mg of calcium fluoride. (Number of replicate samples = 16, number of replicate measurements = 10)
1 mg of quartz and 9 mg of calcium fluoride. When a series of quartz standards was prepared by air filtration, no differences in diffractometric response could be observed in comparison to suspension filtrated samples.

**Mass absorption**

Filters were prepared with different loadings and varying compositions of quartz in calcium fluoride. The diffraction intensities were measured from the three highest quartz lines, of which the results for the 26.67° line are plotted in fig. 1. This family of curves can be used as calibration standards when the quartz concentrations of field samples are to be analyzed. At low loadings the relationship is linear. As the loading increases, a continuing deviation from linearity occurs due to the increasing absorption of the X-ray beam by the sample. For a diffractometer with a fixed divergence slit, line intensity \( I \) relates to total dust weight \( m \) and quartz concentration \( C \) as follows:

\[
I = aC(1 - e^{-bm}),
\]

where the parameters \( a \) and \( b \) should be evaluated separately for each dust composition. Their theoretical equations are (1, 12):

\[
a = k/\mu \quad \text{(b)}
\]

\[
b = (2\mu/A) \csc \Theta \quad \text{(c)}
\]

where \( k = \text{constant} \), \( \mu = \text{mass absorption coefficient of the sample} \), \( A = \text{dust deposition area (larger than the irradiated area)} \), and \( \Theta = \text{angle of incidence of the X-ray beam to the sample} \).

For the assessment of the effects of differing sample matrices, two series of ten samples were prepared with dust deposits ranging from 2 to 20 mg. In the first series the dust mixture contained 5 % quartz, 45 % iron oxide and 50 % calcium fluoride. The second mixture was composed of 15 % quartz, 35 % iron oxide and 50 % calcium fluoride. The quartz amounts on the filters were analyzed by the present direct method. The calibration curves (fig. 1), which are based on a pure calcium fluoride matrix, were used when the peak intensities were converted to concentrations. The results (mean ± standard deviation) for the two series were 4.9 ± 0.8 % and 17.7 ± 2.5 %, respectively.

These results confirm the assumption that the matrix effects do not seriously limit the usefulness of the method. The mass absorption properties of calcium fluoride can be considered as roughly similar to common silicate minerals and foundry dust. Iron compounds exhibit strong fluorescence and high mass absorption when CuKa radiation is used in the diffractometer. The iron content of foundry dust may vary from 2 to 20 % and, if so, the inaccuracies caused by mass absorption and enhancement effects are expected to be less than those found in the present experiment. Theoretically, for a 10-mg sample, a maximum relative error of 20 % can be caused by the variation of mass absorption coefficient from 40 to 100 cm²/g (equation a). This range includes calcium fluoride and common minerals such as calcite, dolomite, zircon, felspars, micas and mixtures thereof (10).
The diffractometry of thin layer specimens analyzed directly on collecting organic membranes suffers from high X-ray background scatter from the filter. However, the sloping and uneven base line was taken into account by digital peak recognition and integration. Some care has to be exercised to insure that the filter surface in the specimen holder is taut and unwaved. The nonuniformity of the dust deposit can cause a variation of about 0.05° in peak positions and, in addition, can cause an undue variation of line intensities. Rotation of the sample is helpful to even out the preferred orientation and nonuniform distribution, but their effects cannot be totally compensated for in this way.

The relative intensities of the bulk specimens agreed with the published values of Fyle quartz (6), while those for the filter deposits did not. The measured ratios of lines 20.85°, 26.67° and 50.15° were 18:100:12 for the bulk samples and 25:100:6 for the filter samples. It appeared that three phenomena accounted for the difference. The line intensities vary with the θ for thin samples as follows:

\[ I = (2 k C m / A) \csc \theta, \quad (d) \]

whereas equation a yields an invariable value for an infinitely thick layer:

\[ I = k C / \mu. \quad (e) \]

Accordingly, the calculated ratios for a thin sample are 23:100:7. Secondly, a thin layer of cleaved quartz crystals on a smooth surface may exhibit a preferred orientation favoring the 3.34 Å line (8). As the deposition depth increases or the filter material becomes more porous, the orientation approaches random. Thirdly, the rough surface of the membrane can cause shadowing of the X-ray beam at low 2θ angles. However, the relative line intensities remained practically unaltered and irrespective of the total loading or means of the dust deposition on the filter when the sample size was limited to less than 20 mg.

**Particle size**

An additional problem in diffractometric analysis is that the peak intensity from an unknown must be compared to some known material for a quantitative estimate. Particle size distribution, crystallographic properties, or the orientation of the standard sample may be different from that of the unknown and result in significant error (11). For the evaluation of the particle size effect, three fractions of Fyle quartz were separated by liquid sedimentation. The mean particle size of the sediments was 1—2, 2—5, and 5—10 μm when counted by optical microscopy. In comparison to the original standard filters, the 1—2 μm fraction yielded only about 75 % of the intensity for the quartz lines of 20.85°, 26.67° or 50.15°. About 100 % intensity was measured from the two coarse fractions.

Alteration in peak intensity was also found when quartz powders of different particle sizes were measured. The powders were mounted in the diffractometer by means of a bulk specimen holder 10 mm in diameter. The intensity was maximum for 2- to 3-μm particles. An intensity of about 90 % was measured from particles in the size range of 40—50 μm. The intensity from the coarse fraction was reduced because of the X-ray extinction within the particles, whereas the reduction of intensity from smaller particles was ascribed to their amorphous surface. The pulverizing process creates an amorphous surface layer on the quartz particles approximately 0.03 μm thick (3). The mass of this noncrystalline material comprises a significant percentage only in small particles less than 1 μm in size.

A proportion of the X-ray intensity reduction from smaller particles can be accounted for by line broadening. The 26.67° line width was increased by 15 % in the 1—2 μm fraction as compared to the coarse fractions. Therefore the peak area measurement is recommended for the quantitative analysis in order to compensate for this phenomenon.

**Field samples**

Foundry dust was collected on membrane filters with an open face monitor and by means of personal and stationary samplers. The dust samples represented different iron foundry operations, namely,
Table 2. Quartz concentrations in foundry samples. Comparison of the direct method with internal standardization.

| Total dust amount on filter (mg) | Quartz in total dust, analyzed directly on a filter (%) | Quartz in total dust, analyzed by internal sedimentation and internal standardization (%) | Quartz in respirable dust, analyzed by internal standardization (%) |
|----------------------------------|--------------------------------------------------------|----------------------------------------------------------------------------------|------------------------------------------------------------------|
| 2.0                              | 15                                                     | 16                                                                               | too small a sample                                               |
| 3.8                              | 7                                                      | 7                                                                                |                                                                  |
| 4.8                              | 10                                                     | 9                                                                                |                                                                  |
| 5.5                              | 3                                                      | 3                                                                                |                                                                  |
| 6.7                              | 14                                                     | 11                                                                               |                                                                  |
| 7.5                              | 17                                                     | 20                                                                               |                                                                  |
| 8.3                              | 82                                                     | 80                                                                               |                                                                  |
| 14.8                             | 14                                                     | 13                                                                               | 10<sup>a</sup>                                                   |
| 15.7                             | 12                                                     | 11                                                                               | 7<sup>a</sup>                                                   |
| 17.8                             | 6                                                      | 7                                                                                | 6<sup>a</sup>                                                   |
| 19.0                             | 14                                                     | 14                                                                               | 11<sup>a</sup>                                                  |

<sup>a</sup> With 55 % respirable dust.

sand preparation, casting, molding, shake-out and fettling. A series of these samples was analyzed quantitatively by the present direct method and by a procedure in which the dust deposit is removed onto a cover glass and the quartz concentration is measured with calcium fluoride used as an internal standard (21). Table 2 shows a part of the results for comparison. In general the disagreement between the two methods was less than 10 % of the mean value. The fraction of respirable dust does not fluctuate much from one foundry operation to another, and therefore the concentration of respirable quartz could be estimated from the total content. A range of about 30—60 % of respirable dust is typical for a large series of samples (16).

In the case of foundry dust, diffraction line interference must be considered. In the present experiment the quartz line of 20.85° was used for the quantitation if the qualitative scan of a sample indicated the presence of graphite or zircon; otherwise the more intense 26.67° peak was preferable. The detection limit of the analytical method is dependent on the composition and amount of the matrix on the filter. For the iron foundry samples with a quartz content of about 10 %, a quartz amount of 0.1 mg can be detected. The lowest quartz concentration detectable in large samples is about 2 %.

DISCUSSION

The present work is primarily related to the X-ray analysis of quartz — that is, the last step of assessing its concentration in workplace air. Therefore the precision and accuracy of the analytical method should be compared with other sources of error. When a typical precision of 8 % for a direct quartz analysis (table 1) and that of 7 % for air flow measurements with personal samplers are added as squared, a total precision of 11 % for the concentration measurement is achieved. The imprecision of weighing the loaded filters is negligible, because at low loadings, where the dust weight determination is most imprecise, the mass absorption effects are minimal. The precision of the direct method is fully comparable with the results achieved by dust removal and internal standardization (21).

In practice particle orientation or non-uniformity of the filter samples are not significant limitations to the use of the calibration standards made by suspension filtration. However, all analytical methods for free silica share one common problem; the particle size distributions of the sample and the standard are important variables. If the size distribution of the dust sample is too fine, the X-ray response is low compared to a standard. In addition
the question remains of whether the amorphous layer of quartz particles should be included in the quantitation. When a standard material such as Fyle quartz with a known particle size distribution in the respirable range is selected, the results are consistent. The accuracy of analyzing total quartz content in foundry samples can thus be taken relatively to be about 10% when the chemical composition and size distribution is roughly known according to the type of dust-producing material or process.

The direct diffractometric method proved to be both convenient and accurate for analyzing quartz on membrane filters. Since dust removal from a filter is time consuming and prone to introduce additional error, it seems preferable to confine the techniques to cases where the respirable fraction of the dust sample must be determined or when severe interferences must be removed by ashing or re-deposition. Direct measurement is especially suited for total dust loadings ranging from 1 to 10 mg.

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