Surface double coating of a LiNi$_a$Co$_b$Al$_{1-a-b}$O$_2$ ($a > 0.85$) cathode with TiO$_x$ and Li$_2$CO$_3$ to apply a water-based hybrid polymer binder to Li-ion batteries

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Recently a water-based polymer binder has been getting much attention because it simplifies the production process of lithium ion batteries (LIBs) and reduce their cost. The surface of LiNi$_a$Co$_b$Al$_{1-a-b}$O$_2$ ($a > 0.85$, NCA) cathode with a high voltage and high capacity was coated doubly with water-insoluble titanium oxide (TiO$_x$) and Li$_2$CO$_3$ layers to protect the NCA surface from the damage caused by contacting with water during its production process. The TiO$_x$ layer was at first coated on the NCA particle surface with a tumbling fluidized-bed granulating/coating machine for producing TiO$_x$-coated NCA. However, the TiO$_x$ layer could not coat the NCA surface completely. In the next place, the coating of the TiO$_x$-uncoated NCA surface with Li$_2$CO$_3$ layer was conducted by bubbling CO$_2$ gas in the TiO$_x$-coated NCA aqueous slurry on the grounds that Li$_2$CO$_3$ is formed through the reaction between CO$_2$ ions and residual LiOH on the TiO$_x$-uncoated NCA surface, resulting in the doubly coated NCA particles (TiO$_x$/Li$_2$CO$_3$-coated NCA particles). The Li$_2$CO$_3$ coating is considered to take place on the TiO$_x$ layer as well as the TiO$_x$-uncoated NCA surface. The results demonstrate that the double coating of the NCA surface with TiO$_x$ and Li$_2$CO$_3$ allows for a high water-resistance of the NCA surface and consequently the TiO$_x$/Li$_2$CO$_3$-coated NCA particle cathode prepared with a water-based binder possesses the same charge/discharge performance as that obtained with a “water-uncontacted” NCA particle cathode prepared using the conventional organic solvent-based polyvinylidene difluoride binder.

1. Introduction

In recent years, water-soluble and aqueous polymer binders, i.e., water-based polymer binders, have become of great interest as alternatives to the poly(vinylidene difluoride) (PVdF) binder dissolved in N-methyl-2-pyrrolidone (NMP) for the cathodes of lithium ion batteries (LIBs) from the viewpoints of environmentally friendly electrode fabrication processes and reducing the cost of LIBs. However, cathode materials such as LiNi$_{0.5}$Mn$_1.5$O$_4$,$^{11}$ LiNi$_a$Co$_b$Al$_{1-a-b}$O$_2$ (NCA)$^{12}$ and Li-rich solid-solution layered cathodes,$^{12}$ which are promising candidates as next generation positive-electrode active materials with high energy density for LIBs, are not stable in water-based slurry solutions because they contain a small amount of alkaline species such as LiOH as aresidue in their production process$^{14}$ and when they are dispersed in a water-based coating slurry, their surfaces are dissolved and its pH is increased, resulting in the corrosion of the Al foil current collectors and the falling off of active cathode materials from the current collector surfaces.$^{12}$ To prevent such a damage of cathode materials some ways have been proposed including the use of buffer agents to inhibit the increase in pH in the water-based slurry$^{15}$ and a stainless steel foil current collector$^{16}$ and the surface coating of cathode materials by carbon,$^{11}$ metal oxides$^{12}$ and Li$_2$CO$_3$.$^{17,18}$

In a series of our studies on surface coating of cathode materials,$^{11,12,19}$ we have found that Li$^+$ ions can relatively smoothly pass through the thin layers of carbon, Al$_2$O$_3$ and TiO$_2$ on NCA particles and the thin layer coating of NCA particles by
TiO$_x$ significantly suppresses, though not completely, the degradation in charge/discharge cyclability which is caused by contacting their surfaces with water, i.e., TiO$_x$-coated NCA cathode particles possess a water-resistant property when kept in the water-based slurry. The TiO$_x$ coating process in this case is a so-called batch process and thus it is not suitable for the mass production of TiO$_x$-coated cathode materials.

Recently, Yanagida et al.$^{17,18}$ have developed a simple continuous method to decrease the pH value of the NCA cathode aqueous slurry with CO$_2$ gas treatment using a cavitation effect in which the NCA particle surfaces are covered with the Li$_2$CO$_3$ layer formed by reacting the LiOH dissolved in the cathode slurry with the CO$_2$ gas introduced into it and the Li$_2$CO$_3$ layer prevents the electrolyte decomposition and reaction of the NCA particle surfaces with the electrolyte, resulting in improvement of the cyclability, coulombic efficiency and high-capacity retention rate of the Li$_2$CO$_3$-coated NCA cathode. They have claimed that their CO$_2$ gas treatment can be a continuous process for mass production. The CO$_2$ gas treatment of cathode particles is thus effective to protect their surface against water.$^{21,23}$ Thus, a suitable Li$_2$CO$_3$ layer coating is desirable. In addition, as mentioned later based on our examination on the water-resistance of NCA cathode particles coated with Li$_2$CO$_3$ layer by the CO$_2$ gas treatment, CO$_2$ gas-treated NCA samples could not exhibit full charge/discharge capacities because they suffered from a small surface damage (surface dissolution) by contacting with water owing to the uncomplete coating of the whole surface of NCA particles by the Li$_2$CO$_3$ layer, i.e., the NCA surface coating only by the Li$_2$CO$_3$ layer was not adequate for the present purpose.

In order to protect the NCA surfaces from the damage caused by contacting them with water during their production process using water-based binder, in this study, we aimed at doubly coating the NCA particle surfaces with TiO$_x$ and Li$_2$CO$_3$ layers, by using a surface coating procedure which may be applicable for the mass production of surface-coated NCA particles for commercially available LIBs, i.e., by first coating the NCA surface with TiO$_x$ layer using a tumbling fluidized-bed granulating/coating machine, which is used to form coating
layers in a wide range of industries including pharmaceuticals, foods and battery materials,\textsuperscript{24} (producing TiO\textsubscript{2}-coated NCA particles which are not coated completely by the TiO\textsubscript{2} layer) and then by coating the TiO\textsubscript{2}-coated as well as TiO\textsubscript{2}-uncoated NCA surfaces with Li\textsubscript{2}CO\textsubscript{3} layer by bubbling CO\textsubscript{2} gas in the TiO\textsubscript{2}-coated NCA aqueous slurry (finally producing the doubly coated NCA particles, abbreviated as TiO\textsubscript{2}/Li\textsubscript{2}CO\textsubscript{3}-coated NCA particles), as schematically shown in Fig. 1. We found that the TiO\textsubscript{2} layer does not coat the NCA surface completely and thus there are some TiO\textsubscript{2}-uncoated parts, but such TiO\textsubscript{2}-uncoated surfaces are covered with the subsequent Li\textsubscript{2}CO\textsubscript{3} layer coating and consequently the TiO\textsubscript{2}/Li\textsubscript{2}CO\textsubscript{3}-coated NCA particles have a high water-resistance and that the charge/discharge performance of the TiO\textsubscript{2}/Li\textsubscript{2}CO\textsubscript{3}-coated NCA cathode prepared using the water-based binder is significantly superior to those of the TiO\textsubscript{2}- or Li\textsubscript{2}CO\textsubscript{3}-coated cathodes and almost comparable to that obtained with “water-uncontacted” NCA cathode prepared using the conventional organic solvent (NMP)-based PVdF binder. The samples of un-, TiO\textsubscript{2}-, Li\textsubscript{2}CO\textsubscript{3}- and TiO\textsubscript{2}/Li\textsubscript{2}CO\textsubscript{3}-coated NCA particles that are prepared and treated with water are named by changing the concentration of TTIP, the spray speed and the total amount of the solution sprayed. After coating the TiO\textsubscript{2} precursor, the NCA particles were sintered at 450 °C for 2 h under argon atmosphere to form the TiO\textsubscript{2} layer on their surface, resulting in TiO\textsubscript{2}-coated NCA particles. TiO\textsubscript{2}-coated NCA samples C-1–C-5 were prepared at different spray conditions as summarized in Table 1.

TiO\textsubscript{2}-coated NCA cathode was prepared as follows: 910 mg of accurately weighed TiO\textsubscript{2}-coated NCA particles and 50 mg of acetylene black (AB, Denka Black, Denki Kagaku Gogyo, Japan) were mixed on a mortar with a pestle, and 10 mg of carboxymethyl cellulose (CMC, Polyscience Inc, cat.#6139) and 30 mg of water-based hybrid polymer binder (TRD202A, JSR, Japan) were mixed in Milli-Pore water (1.1 g, >18 MΩ). Then, the mixture of TiO\textsubscript{2}-coated NCA particles and AB was added to the CMC/TRD202A-mixed aqueous solution. The resulting mixed solution containing TiO\textsubscript{2}-coated NCA particles, TRD202A, AB and CMC was further mixed with a planetary mixing equipment (Mazerustar, KK-2505, KURABO, Japan) until it became a homogenous slurry. The weight% of TiO\textsubscript{2}-coated NCA powder : TRD202A : AB : CMC in the slurry was 91 : 3 : 5 : 1. The homogenous slurry was casted on Al current collector (thickness: 20 μm) with a doctor-blade having the gap of 100 μm. The slurry layer on the Al current collector was dried by evaporating water at 130 °C for 5 h in a vacuum drying oven. For comparison, polyvinylidene difluoride (PVdF, KF9130, Kureha, Japan) was also used as a binder. The weight% of the cathode films was kept as pristine NCA : PVdF : AB = 91 : 4 : 5. In every case, the loading amount of the cathode material on the Al current collector was 3.0–3.4 mg cm\textsuperscript{-2}.

2.2 Preparation of Li\textsubscript{2}CO\textsubscript{3} and TiO\textsubscript{2}/Li\textsubscript{2}CO\textsubscript{3}-coated NCA cathode electrodes

Li\textsubscript{2}CO\textsubscript{3}-coated NCA cathode electrode was prepared using the homogeneous aqueous slurry containing NCA particles, TRD202A, AB and CMC with the same weight% as in the preparation of TiO\textsubscript{2}-coated NCA cathode, by bubbling CO\textsubscript{2} gas into the slurry for 3 min and then flowing CO\textsubscript{2} gas over the slurry for a specified time of 1 h or 7 days. The samples of Li\textsubscript{2}CO\textsubscript{3}-coated NCA particles prepared by flowing CO\textsubscript{2} gas for the specified time of 1 h, 1 day, 3 days and 7 days will be named E-1, E-2, E-3 and E-4, respectively. Immediately after stopping the CO\textsubscript{2} gas flow, the slurry was casted on an Al current collector

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**Table 1** Spray conditions of TiO\textsubscript{2} precursor to prepare TiO\textsubscript{2}-coated NCA particles using a tumbling fluidized bed granulating/coating machine

| Sample number | C-1 | C-2 | C-3 | C-4 | C-5 |
|---------------|-----|-----|-----|-----|-----|
| Concentration of TTIP (wt%) | 5.3 | 36 | 36 | 36 | 36 |
| Spray speed (g min\textsuperscript{-1}) | 20 | 20 | 2.0 | 2.0 | 20 |
| Total amount of the solution sprayed (g) | 0.50 | 0.50 | 0.50 | 0.25 | 0.25 |

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**Fig. 2** Schematic drawing of a tumbling fluidized-bed granulating/coating machine to prepare TiO\textsubscript{2}-coated NCA particles.
with a doctor blade and was dried at 130 °C for 5 h in a vacuum drying oven.

In the case of the preparation of TiO₂/Li₂CO₃-coated NCA cathode electrodes, at first, the slurry composed of TiO₂-coated NCA particles, TRD202A, AB and CMC was prepared at the same mixing percentages of NCA, TRD202A, AB and CMC as in the preparation of TiO₂- and Li₂CO₃-coated NCA cathodes and then CO₂ gas was bubbled into the slurry as in the preparation of Li₂CO₃-coated NCA cathode electrode. When TiO₂/Li₂CO₃-coated NCA samples, G-1 and G-2, were prepared by bubbling CO₂ gas into the slurry for 1 h and 7 days, respectively. The casting of the slurry on an Al current collector and the subsequent drying process were conducted in a similar way as above.

2.3 Characterization of TiO₂-, Li₂CO₃-, and TiO₂/Li₂CO₃-coated NCA cathode materials

The atomic percentages of Ti atom on TiO₂-coated NCA particle samples were determined by X-ray fluorescence (XRF, ZSX Primus IV, Rigaku). Particle size and surface morphology of the TiO₂-coated NCA particles and the distribution of Co, Ni, Al and Ti atoms on the particles were observed with a field-emission scanning electron microscope (FE-SEM, S-4000, Hitachi) equipped with an X-ray dispersive spectrometer (EMAXEvolution X-Max80), HORIBA). The crystal structures of TiO₂ and Li₂CO₃ layers and NCA were characterized with powder X-ray diffraction (pXRD, RINT-Ultima III diffractometer). As an X-ray source, CuKα (λ = 0.1548 nm) was used. The equipments for STEM, STEM-EELS and STEM-EDX measurements and their measurement conditions are mentioned in the Experimental section of ESL.

The amounts of Li₂CO₃ formed on the Li₂CO₃- and TiO₂/Li₂CO₃-coated NCA electrodes were determined by a Warder titration, i.e., the amounts of both hydroxide and carbonate ions in a given titration solution were determined. 2.0 g of Li₂CO₃- and TiO₂/Li₂CO₃-coated NCA particles were dispersed in 50 mL water for 60 min to dissolve the Li₂CO₃ layer. The concentration of CO₃²⁻ ions dissolved in it was quantified by a titration with hydrochloric acid using phenolphthalein and methyl orange pH indicators. Phenolphthalein and methyl orange indicate the ends of the following reactions, i.e., eqn (1)–(3), respectively. Hydroxide ions originate from LiOH residua on the NCA particles’ surface.14,26

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\text{(1) } \text{OH}^- + \text{HCl} \rightarrow \text{Cl}^- + \text{H}_2\text{O} \\
\text{(2) } \text{CO}_3^{2-} + \text{HCl} \rightarrow \text{Cl}^- + \text{HCO}_3^- \\
\text{(3) } \text{HCO}_3^- + \text{HCl} \rightarrow \text{Cl}^- + \text{H}_2\text{O} + \text{CO}_2
\]

The concentration of CO₃²⁻ ion was determined from the volume of HCl titrant used to complete the reaction (3). The amounts of Li₂CO₃ on Li₂CO₃- and TiO₂/Li₂CO₃-coated NCA particles (2.0 g) were calculated using the thus-determined concentration of CO₃²⁻ ion. Finally, the amount of Li₂CO₃ in each case was expressed as the surface concentration (mg cm⁻²) using the Brunauer–Emmett–Teller (BET) surface area of NCA particles evaluated with a TriStar 3000 (Micromeritic Instrument Corporation).

2.4 Cell preparation and electrochemical tests

Charging/discharging cycle and rate performance tests of the cathode materials prepared were performed using a CR2032 coin-type cell. In the test cell, each cathode was paired with a lithium metal anode and both electrodes were separated by a porous polypropylene film (Celgard 3401). The electrolyte solution containing 1 M LiPF₆ in the mixture of ethylene carbonate (EC)/dimethyl carbonate (DMC) (1/2 volume ratio) (Ube Chemicals, Japan) was impregnated into the separator. The charge/discharging cycle and rate performance tests were carried out using a multi-channel battery tester (HJ1001SD8, Hokuto Denko Corporation, Japan) in thermostatic oven at room temperature (25 ± 1 °C). A constant-current/constant-voltage (CC–CV) mode was used for the charging/discharging cycle processes. The upper and lower voltage limits for the charging/discharging cycle processes were 4.25 and 2.5 V (vs. Li/Li⁺), respectively. The charge/discharging capacities (mAh g⁻¹) were calculated using the weight of NCA particles loaded on the Al current collector in which the weight of the TiO₂ and Li₂CO₃ coating was neglected. The charging/discharging cycle tests were done with 0.1C-rate for 3 cycles and then 0.5C-rate for 30 cycles, and finally the charging/discharging performance was checked at 0.1C-rate. The C rate was calculated using the specific capacity of 200 mA h g⁻¹ which was obtained with the cathode prepared from pristine (i.e., uncoated) NCA, PVdF binder and AB at a low C-rate of 0.1C. In the case of high C-rate performance tests, discharge capacity retentions were evaluated assuming that the discharge capacity obtained at 0.1C corresponds to 100% of discharge capacity retention.

3. Results and discussion

3.1 Characterization of TiO₂-, Li₂CO₃-, and TiO₂/Li₂CO₃-coated NCA materials

Fig. 3 shows the SEM images of (A) pristine NCA particles and (B, D, F and H) NCA particles exposed to water (in each case NCA particles (50 mg) were exposed to 5 mL water for 1 h and then dried at 130 °C for 1 h in a vacuum drying oven). The image B was obtained for the uncoated NCA particles, while the images D, F and H for TiO₂-, Li₂CO₃- and TiO₂/Li₂CO₃-coated NCA particles, respectively. When compared with SEM images of NCA particles prior to water treatment (Fig. S1†), we can see that the uncoated NCA (B) is damaged significantly due to the dissolution of the surface into water. The TEM image of the damaged NCA surface has been reported in our previous paper.22 On the damaged NCA surfaces, a Li-poor layer (2–3 nm in thickness) could be observed. On the other hand, the coated ones (D, F and H) seem not to be damaged. Fig. S1† shows SEM images of NCA particles prior to water treatment. The Li₂CO₃ coating (Fig. S1(E)†) smooths the NCA surface, while the surface coating by TiO₂ (Fig. S1(C)†) produces the rough surface. Also in the TiO₂/Li₂CO₃ coating (Fig. S1(G)†), the NCA surface is rough probably reflecting TiO₂ coating and interesting the roughness is larger than in the case of TiO₂ coating.

The TEM-EDX elemental mapping images of TiO₂-coated NCA samples C-1–C-5 prepared at different spray conditions.
and NCA, powder X-ray diffraction (pXRD) peaks for TiO$_2$-coated NCA particles were also obtained (Fig. S4†). The pXRD patterns of NCA samples C-1, C-3 and C-4, suggesting that the former samples are coated with higher amount of TiO$_2$. The thickness of TiO$_2$ coating on NCA particle surfaces is controlled by the concentration and spray speed of TTIP solution, i.e., the high concentration and spray speed of TTIP solution resulted in the increased thickness of TiO$_2$. In addition, in order to confirm a thin and uniform coating of the NCA particles with TiO$_2$ layer, SEM-EDX images for typical particles of samples C-3 and C-4 which showed better cathode performance among the TiO$_2$-coated NCA samples tested as described below were also obtained (Fig. S4†). They indicated that NCA particles are uniformly covered with TiO$_2$ layer even at the low coating amount of TiO$_2$.

In order to identify the crystal structures of TiO$_2$-coated layer and NCA, powder X-ray diffraction (pXRD) patterns of TiO$_2$-coated NCA samples C-1–C-5 were measured and the results are shown in Fig. 4. The pXRD profiles obtained matched that of a layered α-NaFeO$_2$-type structure with the space group R$\bar{3}$m, in which the Na sites are occupied by Li$^+$ ions and the Fe sites by transition metal (Ni, Co and Al) ions. It was found that the pXRD peaks corresponding to the layered α-NaFeO$_2$-type structure do not shift even at high degree of TiO$_2$ coating (e.g., samples C-2 and C-5), indicating that the TiO$_2$ layers formed on the NCA surfaces do not affect the crystal structure of the NCA particles themselves. On the other hand, the pXRD peaks for TiO$_2$ layer could not be observed in the pXRD patterns of NCA samples C-1–C-5 as found in recent studies in which the TiO$_2$ crystal structure is considered to grow “epitaxially” on the NCA particle surface based on the high angle annular-dark-field (HAADF)-scanning transmission electron microscopic (STEM) measurements.

Fig. 5 (I) shows the pXRD patterns of Li$_2$CO$_3$-coated (E-1) and pristine (A) NCA samples. As mentioned above, the pXRD peaks for NCA particles could be observed, but there was no difference in pXRD peaks of both samples. In the expanded pXRD profile (|I| in (II)), as expected, three peaks for Li$_2$CO$_3$ could be observed clearly at 21.5, 30.1 and 32.0°. On the other hand, also in the pristine NCA, the peaks for Li$_2$CO$_3$ could be observed ((A) in (II)) probably because a small amount of Li$_2$CO$_3$ was formed by exposing the pristine NCA sample to air.

The pristine and Li$_2$CO$_3$-coated NCA samples had the Brunauer–Emmett–Teller (BET) surface areas of 0.11–0.12 m$^2$ g$^{-1}$, i.e., the NCA surface areas are almost the same in both samples. In order to calculate the surface coating (in a unit of mg cm$^{-2}$) and layer thickness of Li$_2$CO$_3$, 0.155 m$^2$ g$^{-1}$ and 2.11 g cm$^{-3}$ were used as a surface area of NCA particles and a density of Li$_2$CO$_3$ layer, respectively. From the Warder titration experiments, the Li$_2$CO$_3$-coated NCA samples prepared by bubbling CO$_2$ gas for 1 h (E-1) and 7 days (E-4) were found to have the average Li$_2$CO$_3$ thicknesses of 16 and 22 nm, respectively. As can be seen from this, the thickness of Li$_2$CO$_3$ coating layer could be controlled by the period of bubbling of CO$_2$ gas into the sample solutions. The Li$_2$CO$_3$ coating layer grew slowly over several hours.

Fig. 6 shows the typical TEM images of (A) pristine, (E-1 and E-2) Li$_2$CO$_3$-coated, (C-3) TiO$_2$-coated and (G-1 and G-2) TiO$_2$/Li$_2$CO$_3$-coated NCA samples. The water-based Li$_2$CO$_3$-coated and TiO$_2$/Li$_2$CO$_3$-coated NCA slurries were kept under CO$_2$ atmosphere for 1 h (E-1 and G-1) and 7 days (E-4 and G-2). When the slurry solution of NCA particles was kept under CO$_2$ atmosphere for 1 h (E-1 and G-1) and 7 days (E-4 and G-2), the Li$_2$CO$_3$ layer could be observed clearly on their surfaces as can be seen.
from the comparison with the TEM image of pristine NCA (A), i.e., the average thicknesses of the Li$_2$CO$_3$ layer were 13.5 (E-1) and 15.8 (E-4) nm. In addition, needle-like crystals were found to be formed when kept under CO$_2$ atmosphere for 7 days (E-4) in the case of the water-based Li$_2$CO$_3$-coated NCA slurry. In this case, it is though that water invades into the coarse Li$_2$CO$_3$ layer and Li$^+$ ions extracted from the NCA surfaces react with CO$_3^{2-}$ to form needle-like crystals of Li$_2$CO$_3$ on the Li$_2$CO$_3$ layer. The whole surface of NCA particles seems to be coated with the TiO$_x$ layer. When the slurry composed of TiO$_x$-coated NCA particles, water-based hybrid polymer binder (TRD202A), AB and CMC was kept under CO$_2$ atmosphere for 1 h or 7 days, Li$_2$CO$_3$ layer may be formed on the TiO$_x$ layer (as it is not dense) as well as the TiO$_x$-uncoated part in which LiOH as a residue on the NCA surface is the source of Li$^+$ ions for the formation of Li$_2$CO$_3$. The average thicknesses of the Li$_2$CO$_3$ layer prepared on TiO$_x$-coated NCA particles under CO$_2$ atmosphere for 1 h (G-1) and 7 days (G-2) were 12.5 and 13.2 nm, respectively. However, needle-like crystals could not be observed being distinct from the case (E-4).

In order to confirm the formation of Li$_2$CO$_3$ layer on the NCA surface and TiO$_x$ layer, the STEM-EELS images of Li$_2$CO$_3$- and TiO$_x$/Li$_2$CO$_3$-coated NCA particles were measured and the typical results are shown in Fig. 7-9. In the case of TiO$_x$/Li$_2$CO$_3$-coated NCA sample (G-1, Fig. 7), the signals corresponding to Li, O and C elements could be observed over the whole surface, indicating that the NCA surface is on a whole coated by the TiO$_x$ layer. The average thickness of the Li$_2$CO$_3$ layer evaluated from the TEM image was ca. 15.7 nm, which was comparable to that calculated from the amount of Li$_2$CO$_3$ layer on the NCA surface estimated with a Wader titration using the density of Li$_2$CO$_3$ (d = 2.11 g cm$^{-3}$). The STEM-EELS images of TiO$_x$/Li$_2$CO$_3$-coated NCA particle (G-1, Fig. 8) confirmed Fig. 6 (G-1), i.e., the Li$_2$CO$_3$ layer is formed on the TiO$_x$ layer the average thickness of which was evaluated to be ca. 12.4 nm. From Fig. 9, it was further speculated that the needle-like crystals (shown in Fig. 6 (E-4)) observed after keeping the slurry solution containing pristine NCA particles under CO$_2$ atmosphere for 7 days correspond to NiCO$_3$ and Li$_2$CO$_3$. This fact suggests that the Li$_2$CO$_3$ layer formed on NCA particle surfaces is insufficient as a water-proof layer and as a result Ni$^{2+}$ ions of NCA dissolve to form NiCO$_3$. On the contrary, the TiO$_x$ layer on NCA particle surfaces inhibited the formation of the needle-like crystals under the same exposure to the CO$_2$ atmosphere, indicating...
that the double coating of NCA surface by TiO\textsubscript{x} layer and then Li\textsubscript{2}CO\textsubscript{3} layer is effective for giving a water-resistance to it.

3.2 Charging/discharging performance tests with TiO\textsubscript{x}-, Li\textsubscript{2}CO\textsubscript{3}- and TiO\textsubscript{x}/Li\textsubscript{2}CO\textsubscript{3}-coated NCA materials

Fig. 10 shows the charging/discharging cycle performance obtained with the cathodes prepared from pristine NCA and TiO\textsubscript{x}-coated NCA samples C-1–C-5. The charge/discharge was conducted with the 0.1C-rate for first 3 cycles and then with 0.5C-rate for 30 cycles and again with 0.1C-rate for 3 cycles to confirm the initial charge/discharge performance. Clearly, the pristine NCA (A) cathode prepared with PVdF binder exhibited the highest discharge performance among the NCA samples tested. The cycle performance is in the order of pristine > sample C-1 = sample C-3 > sample C-4 > sample C-2 > sample C-5. The performance order of the TiO\textsubscript{x}-coated samples is similar to the order of atomic ratio of Ti to Ni (Fig. S3†), indicating that an excessive TiO\textsubscript{x} coating reduces the discharge capacity because the TiO\textsubscript{x} retards the intercalation/deintercalation of Li\textsuperscript{+} ion to/from the NCA cathode active material. The samples C-1 and C-3 exhibited the highest discharge performance among the TiO\textsubscript{x}-coated NCA samples, but their performance was a little inferior to that obtained with the pristine NCA. This small decrease in the discharge capacity of samples C-1 and C-3 is considered to reflect that they are damaged by contact with water in the course of their preparation. The NCA particle surfaces of samples C-1 and C-3 might be partly uncoated with the TiO\textsubscript{x} layer and/or coated with the coarse TiO\textsubscript{x} layer and consequently the NCA surface might partially suffer from the damage by contact with water. From the discharge capacities obtained at 0.1C-rate after 30 cycles at 0.5C-rate, the discharge capacity retentions (%) which are defined as (discharge capacity at the 34\textsuperscript{th} cycle)/(discharge capacity at the 3\textsuperscript{rd} cycle) × 100 of the pristine and TiO\textsubscript{x}-coated NCA samples C-1–C-5 were calculated to be 93, 92, 83, 94, 89 and 78%, respectively. The samples C-2 and C-5 coated with larger amount of TiO\textsubscript{x} are considered to suffer from larger damage by the discharge at 0.5C-rate because thicker TiO\textsubscript{x} layers of these samples more significantly retard the intercalation/deintercalation of Li\textsuperscript{+} ions. In addition, the high rate performance of TiO\textsubscript{x}-coated NCA samples was examined with the C-rate of 0.1, 0.2, 0.5, 1, 2, 3 and 5C (Fig. S5†). The samples C-1, C-3 and C-4 exhibited nearly the same
performance as that obtained with the pristine NCA sample, while the samples C-2 and C-5 indicated significantly lower performance especially at higher C-rates. These results are similar to those obtained at the charging/discharging cycle tests at 0.1 and 0.5C (mentioned above). That is, the thick TiO$_x$ layer retarded actually the transfer of Li$^+$ ions from/to cathode.

Fig. 7  (a and b) Typical TEM images of Li$_2$CO$_3$ (CO$_2$ bubbling for 1 h)-coated NCA (E-1) and (c) STEM-EELS mapping of C, Li and O elements and their mixed mapping.

Fig. 8  (a) Typical TEM image of TiO$_x$/Li$_2$CO$_3$ (CO$_2$ bubbling for 1 h)-coated NCA (G-1) and (b) STEM-EELS mapping of Ti, C and Li elements and their mixed mapping.
particle surfaces and consequently degraded the cathode performance. The samples C-1, C-3 and C-4 exhibited the charging/discharging cycle performance and high rate performance comparable to that obtained with the TiO\textsubscript{x}-coated NCA samples prepared by reacting TiO\textsubscript{x}-precursor with NCA surface in beaker,\textsuperscript{12,19} indicating that the present TiO\textsubscript{x} coating using a tumbling fluidized-bed granulating/coating machine enables to prepare the NCA particles coated with TiO\textsubscript{x} layer which rarely inhibit the transfer of Li\textsuperscript{+} ions from/to NCA particle surfaces by suitably adjusting the concentration of TiO\textsubscript{x} precursor solution which is sprayed in the reaction camber.

The effect of Li\textsubscript{2}CO\textsubscript{3} coating on NCA cathodes on their cycle performance was examined and the results are shown in Fig. 11, in which the slurry solution containing pristine NCA particles, TRD202A binder, CMC and conductive additive (AB) was kept under CO\textsubscript{2} atmosphere for 1 h (E-1), 1 (E-2), 3 (E-3) and 7 (E-4) days. The reason why the CO\textsubscript{2} treatment of 1 h to 7 days was examined in this study is that slurry solutions of electrode active materials are used, once prepared, typically for 7 days in the production line of commercially available LIBs. The discharge capacity decreased largely with increasing the CO\textsubscript{2} treatment period. As mentioned above, longer CO\textsubscript{2} treatment may produce thicker Li\textsubscript{2}CO\textsubscript{3} and consequently leads to lower discharge capacity. Here we should also consider the damage of NCA particles by contact with water during the CO\textsubscript{2} treatment for the
Li$_2$CO$_3$ formation in the CO$_2$-saturated aqueous slurry solution containing NCA particles. Interestingly, the NCA samples CO$_2$-treated for 1 h (E-1) and 1 day (E-2) gave almost the same charge/discharge performance, although it is thought that the NCA sample CO$_2$-treated for 1 h is less damaged by contact with water and the Li$_2$CO$_3$ layer formed is thinner compared with the 1 day CO$_2$-treated one. Thus, under the present CO$_2$ treatment condition the CO$_2$ treatment of 1 h is enough to form the Li$_2$CO$_3$ layer.

Fig. 12 shows the charge/discharge performance obtained with the cathodes prepared from the slurry containing pristine NCA, PVdF and AB as well as the water-based slurries containing TiO$_x$(C-3), Li$_2$CO$_3$(E-1)- or TiO$_x$/Li$_2$CO$_3$(G-2)-coated NCA, TRD202A, CMC and AB. The pristine NCA (A) cathode prepared with PVdF binder exhibited the discharge capacities of 199 and 186 mA h g$^{-1}$ at the 1$^{\text{st}}$ and 30$^{\text{th}}$ cycles, respectively and the discharge capacity retention was 93% at the 30$^{\text{th}}$ cycle. On the other hand, the discharge capacities of the TiO$_x$-coated (Li$_2$CO$_3$-coated) NCA cathodes at the 1$^{\text{st}}$ and 30$^{\text{th}}$ cycles are 195 (196) and 177 (177) mA h g$^{-1}$, respectively. The discharge capacity retentions for TiO$_x$- and Li$_2$CO$_3$-coated NCA samples were 91 and 88% at the 30$^{\text{th}}$ cycles, respectively. The TiO$_x$/Li$_2$CO$_3$-coated NCA cathode, which was prepared by keeping the water-based slurry for 7 days under CO$_2$ atmosphere which means that the cathode was actually exposed to water for 7 days, exhibited the discharge capacities of 196 and 187 mA h g$^{-1}$ at the 1$^{\text{st}}$ and 30$^{\text{th}}$ cycles, respectively and the discharge capacity retention of 95% at the 30$^{\text{th}}$ cycle. Thus, it is obvious that the TiO$_x$/Li$_2$CO$_3$-coated NCA cathode is superior in both the discharge capacity and capacity retention to TiO$_x$- and Li$_2$CO$_3$-coated NCA cathodes and the discharge capacity retention of the former is comparable to that of the pristine NCA cathode prepared with PVdF binder. The TiO$_x$/Li$_2$CO$_3$-coated NCA cathodes gave, even though the NCA particles were exposed as the water-based slurry to water for 7 days, high charge/discharge capacities as a result of the surface double coating with TiO$_x$ and Li$_2$CO$_3$. In Fig. S6†, the SEM images of NCA cathodes after the charging/discharging cycles of 30 times (done in Fig. 12) are shown. In this case, the NCA particles are covered with PVdF and AB or TRD202A, CMC and AB and thus their surfaces look rough due to the adsorption of PVdF and AB or TRD202A, CMC and AB. The difference of surface morphology could not be observed among the four samples examined. Also in the comparison of the SEM images of the four samples before and after the charging/discharging cycles of 30 times (the SEM images obtained after the cycles are not shown in this paper), the surface morphology change could not be observed. Moisture contents of the cathode electrodes after drying NMP or water solvent were measured with thermogravimetry (TG) (Experimental in ESI and Fig. S7†). The cathode (a) composed of pristine NCA, PVdF and AB did not exhibit the change in weight of its scratched layer, indicating that the water content is almost zero. The TiO$_x$/Li$_2$CO$_3$-coated NCA (G-2) particles just after synthesis of the coated powder was showed a significantly large weight loss in the temperature region from 100 to 200 °C. However, the sample powder obtained from the cathode prepared with the TiO$_x$/Li$_2$CO$_3$-coated NCA (G-2) particles exhibited only a very small loss, i.e., the weight loss was 0.23 wt% because the TiO$_x$/Li$_2$CO$_3$-coated NCA particles on the cathode was dried well in the fabrication processes of cathodes. It can be considered that such a low content of water in the TiO$_x$/Li$_2$CO$_3$-coated NCA cathode do not influence the cathode
performance. The charge/discharge voltage–capacity curves of pristine (A), TiO$_x$- (C-3), Li$_2$CO$_3$- (E-1)- and TiO$_x$/Li$_2$CO$_3$ (G-2) -coated NCA cathodes are shown in Fig. S8.† These curves are, though there is a small difference in the charge/discharge capacity, typical for the NCA and show several small shoulders corresponding to the redox reaction of Co and Ni ions in NCA, indicating that the samples tested have the essentially same charge/discharge property except for the individual capacities.

The rate performance of the above-mentioned cathodes of typical four types was examined and the results are shown in Fig. 13. As predicted, the pristine NCA (A) without a coating layer exhibited the highest C-rate performance. The rate performance of the coated NCA cathodes was in the order of the TiO$_x$- (C-3), TiO$_x$/Li$_2$CO$_3$- (G-2) and Li$_2$CO$_3$-coated (E-1) ones. These results are considered to reflect the different degree of the inhibition of Li$^+$ ion transfer in the intercalation/ deintercalation processes by the individual coatings. In order to check the conductivity change after the coating of NCA particles, the direct current internal resistance (DC-IR) drop which can be seen in the early stage of the discharging process was compared. Fig. S9-(a)† shows the discharge voltage–discharge capacity curves of pristine (A), TiO$_x$- (C-3), Li$_2$CO$_3$- (E-1) and TiO$_x$/Li$_2$CO$_3$ (G-2)-coated NCA cathodes obtained at 5C-rate in the rate performance test of Fig. 13. The DC-IR drop can be related to the conductivity of coated NCA particles. In the enlarged discharge voltage–discharge capacity curves shown in Fig. S9-(b),† no difference in the DC-IR drop could be observed. Thus, the change of conductivity before and after the coating with TiO$_x$, Li$_2$CO$_3$, and TiO$_x$/Li$_2$CO$_3$ was not seen in the samples used in the rate performance test in Fig. 13. As mentioned in our previous paper, it is found that when thin TiO$_x$ coating layers are formed on NCA surface, they scarcely block the Li$^+$ transportation through them. Certainly, also in Fig. 13, the rate performance of TiO$_x$-coated NCA particles is almost the same as that of the pristine NCA particles within the experimental error. Li$_2$CO$_3$ coating, on the contrary, blocks somewhat the Li$^+$ transportation through its layer because the discharge capacity retention obtained at the TiO$_x$/Li$_2$CO$_3$-coated NCA cathode is lower than that obtained at the pristine and TiO$_x$-coated ones. Therefore, we think that un-coated the gaps left by incomplete TiO$_x$ coating are infilled by Li$_2$CO$_3$ coating and thus the TiO$_x$/Li$_2$CO$_3$-coated NCA cathode is inferior in the rate performance to the TiO$_x$-coated NCA ones.

4. Conclusions

In this study, we originally proposed the surface double coating of NCA cathode with water-stable TiO$_x$ and Li$_2$CO$_3$ layers with a view of applying water-based binders to the preparation of the cathodes for LIBs because the use of water-based binders simplifies their production process and reduces their cost. NCA cathodes possess a high voltage and high charge/discharge capacity, but they are heavily damaged when contacted to water during their preparation processes. The NCA surface was coated firstly with TiO$_x$ layer by spraying TiO$_x$ precursor slurry using a tumbling fluidized-bed granulating/coating machine followed by sintering at 450 °C under argon atmosphere (producing TiO$_x$-coated NCA particles) and then with Li$_2$CO$_3$ layer by bubbling CO$_2$ gas in the TiO$_x$-coated NCA aqueous slurry and consequently the NCA particles coated doubly with TiO$_x$ and Li$_2$CO$_3$ layers (TiO$_x$/Li$_2$CO$_3$-coated NCA particles) were prepared. The TEM and STEM-EELS measurements confirmed that the whole surface of NCA particles is actually coated doubly with TiO$_x$ and Li$_2$CO$_3$ layers. The TiO$_x$/Li$_2$CO$_3$-coated NCA cathode possessed a significantly higher charge/discharge performance compared with the TiO$_x$- or Li$_2$CO$_3$-coated NCA cathodes and almost the same charge/discharge capacities as obtained at the NCA cathode prepared using the conventional organic solvent-based PVdF binder although the high rate discharge performance was a little inferior to the latter due to a small resistance of Li$^+$ ion transfer through the coated layers. In addition, it should be noted that the present double coating procedure using a tumbling fluidized-bed granulating/coating machine and CO$_2$ gas bubbling is promising at a viewpoint of the mass production of surface-coated cathode materials for LIBs using water-based binders. Further study along with this line is progress.

Author contribution

T. W. and K. H. performed charge/discharge test and preparation of coated cathode materials. F. A. and T. G. characterized the synthesized materials with STEM, EELS and EDS. S. K., S. U. and H. I. performed coating treatment of cathode materials with
coating machine. Y. I. and F. M. (Nihon Kagaku Sangyo) performed a preparation of bare cathode material. J. W., T. O. and F. M. (Kanagawa University) wrote the manuscript, summarized the work.

Conflicts of interest

The authors declare no competing financial interest.

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