Experimental study on flame propagation over overload-wire under varying inclination Angle

Hu Wen¹, Xiangtao Zhao¹*, Qing Tian¹, Weifeng Wang¹, He Jian²

¹School of Safety Science and Engineering, Xi’an University of Science and Technology, Xi’an 710054, China
²State grid Shaanxi province power company maintenance company, Xi’an 710054, China

Abstract. To better understand the process of fire caused by conducting wire, based on the study of overload of the low-voltage wire, the theoretical analysis of flame spread mechanism of overload-wire was proposed, and the functional relationship between flame shape characteristics and flame spread speed, current, and inclination angle was studied. The results show that: (1) the theoretical model of flame propagation can well reflect the changes of thermodynamic parameters in the process of flame propagation, and it is in better agreement with the experimental results. (2) When the current value is constant, with the increase of the inclination angle of the wire (0°-90°), the flame is elongated along the wire direction, the width of the flame base increases, and the angle between the flame front and the wire decreases. When the inclination angle is fixed, with the increase of the inclination angle of the conductor, the flame shape becomes more "high and wide" and the flame height increases at the same time. (3) When the current is constant, the flame spread rate increases with the increase of wire inclination angle; when the inclination angle is constant, the flame spread rate decreases sharply with the increase of current.

1 Introduction

Many related studies have shown that the inclination angle has a significant effect on the fire spread characteristics of the solid surface. Quintiere et al. [1] used hardened RPU plates to carry out upward and downward fire spread experiments and found that the inclination angle of the experimental samples has a significant effect on the fire spread rate. Great influence. Zhang Ying [2] discussed the influence of the tilt angle on the spread of flame on the surface of the wood and studied the mechanism of flame spread acceleration. Drysdale and Macmillan et al. [3] conducted upward fire propagation experiments in "hot thin" and "hot thick" PMMA, and found that when the sample placement angle changes from horizontal 0° to 75°, the average flame propagation rate is almost No change; when the inclination angle is changed from 75° to 90°, the flame spread rate increases greatly. Hu Longhua et al. [4] studied the influence of the tilt angle on the flame spread rate (FSR) on wires with high thermal conductivity and derived a simplified FSR calculation model. Zhu Keke [5] studied the flame rate of horizontal, upward, and downward spreading of the wire under the inclination angle of -75° to +75°, and conducted an in-depth discussion from the basic flame shape. In actual scenes such as building fires, the wire is not only placed horizontally, but the inclined state of the wire also has a significant impact on its combustion behavior [6-9]. The buoyancy acting on the pyrolysis gas will affect the flame shape and the unburned molten insulation layer through gravity [10-13]. Buoyancy will have a more complex effect on the forward propagation of the flame. Therefore, it can be inferred that the flame shape and flame spread rate of the overcurrent wire with a certain inclination angle are quite different from the horizontal and vertical spread.

For wires placed at a certain angle, increasing the current through the wire will increase the Joule heat generated by the inner core of the wire and change the heat conduction of the wire to the insulating layer. At the same time, the natural convection between the insulating layer and the outside air will strengthen, and the induced buoyancy will also The increase will further affect the basic flame shape and flame spread rate. Therefore, this article will study the flame spread characteristics of wires passing different currents under different inclination angles.

2 Experimental

This experimental system consists of four parts: (1) The power rectifier circuit system, through which the current and voltage output is controlled by the current output regulation system; (2) The current output regulation system, through which the voltage can be adjusted and output Voltage 220V/380V, voltage acquisition frequency 1.5×104Hz; current adjustment range is 30~300A DC or AC, current output accuracy can be controlled within ±0.1A; and the control system has two modes: automatic mode and manual mode; (3) over Electric current test bench system. The test bench system is composed of upper and lower parts: the upper prism-shaped smoke exhaust device; the lower part is a 1500mm (D) × 1200mm (W) × 233
2000mm (H) rectangular parallelepiped closed test bench space, inside the space. The test bench and insulated wooden blocks are 1200mm high for over-current experiments; (4) The connection device adopts a quick-release structure to connect the experimental samples and the power supply terminal. The schematic diagram of the experimental system is shown in Figure 1.

This article mainly focuses on the study of the combustion characteristics of low-voltage conductors. Wire (PVC) is selected. As shown in Table 1. The wires are measured to a length of 540mm, and the length of the insulation layer of about 20mm at both ends of the wire is removed. The experimental wire parameters are shown in Table 1.

### Table 1. Basic physical parameters of experimental wires

| Sample | Core diameter (mm) | Insulation thickness (mm) | Sample diameter (mm) | The ratio of Core section area $A_c/A_0$ (%) | The ratio of insulation section area $A_p/A_0$ (%) | Rated current (A) $I_e$ |
|--------|-------------------|--------------------------|-----------------------|--------------------------------------------|---------------------------------------------|----------------------------|
| Cu-PVC | $d_c$ 1.38        | $\delta_p$ 0.8           | $d_0$ 2.98            | 21.44                                      | 78.56                                      | 32                         |

During the stable phase of the wire flame spread, the CCD camera (1000fps, 1920 × 1280 pixels, 72 pixels/inch) was used to record the burning phenomenon at a shooting rate of 1000 frames per second, and the position of the flame front was marked. Figure 4 shows the position of the flame front. By drawing the time history curve of the flame front position, the slope of the curve is fitted and calculated, and the fire spread rate (unit: m/s) is obtained through proportional conversion (the actual length is 5cm = 2.8pix).

### Figure 2. Change in the position of the leading edge of the wire

#### 3 Theoretical analysis of flame spreading process

The PVC insulation material of the wire in this study is considered to be a kind of thermal thin material ($\delta p = 0.8\text{mm} << 1\text{mm}$) [14]. Therefore, the temperature profile of the entire PVC insulation layer or the inner core cross-section can be considered uniform, the spread rate of the flame mainly depends on the thermal feedback of the combustion zone in the front of the flame to the preheating zone. As shown in Figure 3, by $\dot{Q}_1$, $\dot{Q}_2$ and $\dot{Q}_3$ respectively represent the heat convection between the flame and the exposed part of the core, the heat convection between the flame and the insulating layer, and the heat conduction through the inner core constitute the thermal feedback of the flame front combustion zone. The heat radiation and heat conduction are mainly controlled by the heat input of the flame, and the heat conduction $\dot{Q}_3$ is mainly caused by the Joule heating effect of the wire during the electrification process. Therefore, the heat balance of the combustion zone can be expressed as follows [15,16]:

$$\frac{\pi}{2} d_0^2 d_0 \rho_l c_v (T_e - T_c) + S \frac{\pi}{2} d_0^2 \rho_0 c_p (T_e - T_0) = \dot{Q}_1 + \dot{Q}_2 + \dot{Q}_3.$$  
(1)
\[
\dot{Q}_1 = h_j(T_f - T_p) \\
\dot{Q}_2 = (1 - \exp(-k\lambda))\sigma(T_f^4 - T_p^4) \\
\dot{Q}_3 = \lambda_p(T_f - T_p) \\
\dot{Q}_4 = h_p(T_f - T_p) \\
\dot{Q}_5 = \lambda_p(T_f - T_p)^2 = \lambda_p(T_f - T_p)/(\lambda_k, d^+ + 4h_k(F_i - F_s))/4k_h(F_i - F_s)
\]

Among them \( \rho_p, c_p \) and \( V_f \) respectively represent the density of the PVC insulation layer, the specific heat of the PVC insulation layer, and the flame spread rate of the PVC insulation layer; \( \gamma_s, h_p, \text{ and } \lambda_p \) respectively represent the pyrolysis latent heat, convective heat transfer coefficient, and thermal conductivity of the insulation layer; \( k, l, \text{ and } \sigma \) respectively Soot absorption coefficient, characteristic length and Boltzmann constant; \( T_e, T_p, \text{ and } T_f \) respectively represent the ambient temperature, insulation temperature, flame temperature; \( T_c \) represent the metal core temperature; \( h_c, F_i, \text{ and } F_s \) respectively the heat transfer coefficient of the inner core of the combustion zone, flame width, and length.

Therefore, through (1), (2), (3), (4), and (5) equations, we can get the flame spread rate as follows:

\[
V_f = \frac{h_p(T_f - T_p)^2}{4\pi d^+ \rho_p c_p (T_p - T_e)^2 + \lambda_p(T_f - T_p) + \lambda_p(T_f - T_p)^2}
\]

4 Results and discussion

4.1 Flame characteristics

Figure 4 shows the flame shape corresponding to varying overcurrent conductors at the same time under varying inclination angles of copper core (Cu-PVC). The Figure 4 shows the flame image corresponding to the inclination angle of the wire in the experimental conditions from 0° to 90°, and the values of overcurrent are 4.0 Ie, 4.5 Ie, 5.0 Ie, 5.5 Ie, 6.0 Ie. It can be found from the Figure 4:
For a wire with a certain inclination angle: (1) The flame shape becomes more "high and wide" under the condition of higher overload current, and the flame height also increases at the same time. This is because the wire is under the same environmental conditions, the higher overload current makes natural Convection increases, and induced buoyancy increases. At the same time, the diffusion rate of the insulating layer accelerates, and the burning rate of the flame increases. As the overload current value increases, the flame will be stretched due to the increase in buoyancy, the flame profile gradually becomes sharp, and the flame height increases as a whole Trend, the width of the flame base is gradually widening; (2) When the overload current value is higher, due to the enhancement of the buoyancy driving effect, the pyrolysis gas at the flame base burns more fully and the burning rate is faster, and the area of the light yellow flame area is larger. With the increase of the current value, the proportion of bright yellow flame area gradually decreases, and the proportion of light yellow flame area gradually increases.

For a certain overload current condition: (1) As the inclination of the wire gradually increases (0°~75°), the flame is elongated along the direction of the wire, and the width of the flame base becomes larger. The width of the flame base when the wire is placed horizontally is the smallest. At the same time, the angle between the flame front and the wire becomes smaller, and the distance between the flame and the wire surface is smaller (flame height), which is more conducive to the thermal feedback between the flame and the wire surface, and accelerates the spread of the flame from the combustion zone to the preheating zone. Speed; (2) With the gradual increase of the inclination of the wire (0°~75°), the area of the light yellow flame area becomes larger and the area of the bright yellow area increases, indicating that the combustion is more complete.

It is worth noting that when the inclined spreading at a low angle (15°), it is found that the flame shape has periodic spreading changes. Due to the particularity of the angle, the liquid melt of the insulating layer that cannot be burned and consumed will move towards the wire under the action of gravity. Flow distribution in the opposite direction of flame spread.

From the above discussion, it is found that at the inclination angle (75°), the angle between the flame and the wire becomes smaller, and the flame is more "flat", approaching 0°. Therefore, compare the vertical spread (90°) shape of the wire with the dip spread (75°), as shown in Figure 5 below.

| Inclination angles | 4.0le | 4.5le | 5.0le | 5.5le | 6.0le |
|-------------------|------|------|------|------|------|
| 75°               | ![ Flame image ] | ![ Flame image ] | ![ Flame image ] | ![ Flame image ] | ![ Flame image ] |
| 90°               | ![ Flame image ] | ![ Flame image ] | ![ Flame image ] | ![ Flame image ] | ![ Flame image ] |

**Figure 5.** Vertical spread (90°) shape and oblique spread (75°) flame shape under different current conditions

From Figure 5, it is found that when the current is constant, the flame spreading at an inclination angle (75°) is more "slender" than the flame spreading vertically (90°), and the miscellaneous flame is accompanied at the top of the flame, while the flame spreading vertically (90°) has no miscellaneous Flame, flame propagation is also more stable.

### 4.2 The effect of inclination on flame spread

Figure 6 shows the variation of the flame spread rate of copper core wire with the wire inclination angle under different inclination angle condition.
It can be found in Figure 6:

(1) For wires with different inclination angles, the thickness of the insulating layer is the same, and the current is constant, the flame spread rate increases as the inclination angle of the wire increases. Under different energized current conditions, the flame spread rate changes with the inclination angle the same, the flame spread rate is the smallest at the horizontal inclination angle, and the flame spread rate reaches the maximum at the vertical inclination angle. Due to the gradual increase of the inclination angle of the wire (0°~75°), the flame is elongated along the direction of the wire, the width of the flame base becomes significantly larger, and the angle between the flame front and the outer surface of the wire becomes smaller, which is more conducive to the flame and the insulating layer. Thermal feedback between the time, increasing the rate of flame spread.

(2) Data fitting of angle and flame spread speed found: when using ExpDec1 mathematical model equation for different energized current values and inclination angles, the goodness of fitting is higher, and the fitting equation can be used to calculate the difference in different inclination angles. The flame spread rate is predicted and judged.

4.3 The effect of electric current on flame spread rate

Figure 7 shows the variation of flame spread speed with inclination angle under different current conditions.
Figure 7. Variation Law of Flame Spreading Speed with Current under Different Inclination Angle

It can be seen from Figure 7:

(1) When the inclination angle is constant, as the current increases, the flame spread rate drops sharply, mainly because the energized wire starts to pyrolyze due to the Joule heating effect, and the generated pyrolysis gas and air form a preliminary Diffusion of mixed gas, as the current increases, the rate of pyrolysis gas generation in the insulating layer continues to increase, thereby affecting the flame spread rate;

(2) When the Lorentz mathematical model equation is used between the flame spread rate and the current, the goodness of fit is high, and the flame spread rate under different current conditions can be predicted and judged by the fitting equation.

5 Conclusions

(1) The theoretical model of flame propagation can well reflect the changes of thermodynamic parameters in the process of flame propagation, and it is in better agreement with the experimental results.

(2) When the current value is constant, with the increase of the inclination angle of the wire (0°- 90°), the flame is elongated along the wire direction, the width of the flame base increases, and the angle between the flame front and the wire decreases. When the inclination angle is fixed, with the increase of the inclination angle of the conductor, the flame shape becomes more "high and wide" and the flame height increases at the same time.

(3) When the current is constant, the flame spread rate increases with the increase of wire inclination angle; when the inclination angle is constant, the flame spread rate decreases sharply with the increase of current.

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