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Nitrogen plasma surface treatment for improving polar ink adhesion on micro/nanofibrillated cellulose films

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Abstract We find that nitrogen plasma treatment of micro/nanofibrillated cellulose films increases wettability of the surface by both liquid polar water and nonpolar hexadecane. The increased wetting effect is more pronounced in the case of polar liquid, favouring the use of plasma treated micro/nanofibrillated cellulose films as substrates for a range of inkjet printing including organic-based polar-solvent inks. The films were formed from aqueous suspensions of progressively enzymatic pretreated wood-free cellulose fibres, resulting in increased removal of amorphous species producing novel nanocellulose surfaces displaying increasing crystallinity. The mechanical properties of each film are shown to be highly dependent on the enzymatic pretreatment time. The change in surface chemistry arising from exposure to nitrogen plasma is revealed using X-ray photoelectron spectroscopy. That both polar and dispersive surface energy components become increased, as measured by contact angle, is also linked to an increase in surface roughness. The change in surface free energy is exemplified to favour the trapping of photovoltaic inks.

Keywords DBD plasma · Nitrogen plasma surface treatment · Nanocellulose films · Enzymatic nanocellulose · Printing of organic-based polar inks

Introduction and background

Sustainability is one of the key targets for industrial practice today. The related research aimed at new biobased materials derived from renewable sources, is relevant for the sustainable economy. In the bioproducts industry, micro/nanofibrillated cellulose (MNFC) has attracted attention in a number of potential applications (Hubbe et al. 2017a). It can be used in standard wood products, such as paper and boards. However, most of the benefits derived from MNFC stem from its wider uptake in a range of industrial value chains, such as biodegradable packaging films and laminates. MNFC has interesting intrinsic properties derived from large specific surface area and its
alternate regions of crystallinity. The hydroxylated surface chemistry is readily suitable for chemical modification. Films formed from MNFC are considered smart materials and studied for functional materials applications. Enzyme-treated fibres used to produce cellulose nanofibrils provide higher crystallinity in the resulting nanocellulose, as enzymes digest amorphous cellulose, which acts as the glue between crystalline cellulose regions. Direct hydrogen bonding of crystalline cellulose, therefore, gives a stronger material film. An example of an important application of MNFC is as a substrate for printed solar cells based on organic inks (Zhu et al. 2014). The surface properties of MNFC films, such as wettability by liquid, topography, chemistry, surface charge, the presence of hydrophobic and hydrophilic domains, density and conformation of functional groups, all play a crucial role in printability and barrier properties. Their ability to support controlled migration of solvent ink vehicle and chromatographic differentiation of ink components is important in the printing of inkjet printable (IP) inks, and especially for production of bio-based printed functionality in a wide range of applications, such as printed electronics and printed diagnostics (Hoeng et al. 2016; Jutila et al. 2018).

Solar panel IP photovoltaic (PV) inks contain a complex mix of materials, including the organic electron acceptor (p-type) and negative electron donor (n-type) suspended in solvent together with specific surfactant(s) intended to keep the p-type and n-type components de-mixed (Kumar and Chand 2012). Although drop-on-demand (DoD) inkjet printing is a very competitive candidate for printing PV inks on film substrates, there are limitations in respect to mutual compatibility between the surface of MNFC films and mixed polar-dispersive solvents constituting the PV ink (Singh et al. 2010; Yinhua et al. 2013). Electrolyte is highly polar, for example, and so sufficient wettability is needed by providing a polar surface, despite the parallel requirement for wettability by organic species (Schultz et al. 1977; Özkan et al. 2016). This complex polar-dispersive surface energy balance is, therefore, critical (Hansson et al. 2011).

Exposure to plasma is a convenient method to modify the surface properties of polymeric materials, while keeping their bulk properties intact, making a material better adapted for printing (Möller et al. 2010; Kramer et al. 2006; Catia et al. 2015). Furthermore, as we demonstrate, it is a convenient way to introduce desired groups onto the surface of materials (Mihailovic et al. 2011). Surface properties depend on parameters of plasma treatment such as applied electrical field energy, type of feed gas, pressure, exposure time, and reactor geometry (van de Vyver et al. 2011; Jun et al. 2008).

In this work, we modify enzyme pretreated fibre-derived MNFC film surfaces using nitrogen plasma to enhance their amphiphilic surface affinity to polar and non-polar IP PV inks. Measurements of the surface free energy, surface roughness (atomic force microscopy (AFM)) and material composition [X-ray photoelectron spectroscopy (XPS)] were used to characterise the MNFC film surface before and after plasma treatment. The affinity for IP PV ink was assessed visually after inkjet printing. We also identify a correlation between the observed change in free surface energy of the MNFC film, arising from the plasma treatment, with the effect of the enzymatic pretreatment. This is related to the level of residual crystallinity increasing as a function of progressive enzymatic pretreatment (Galagan et al. 2011; Cernakova et al. 2006; Pertile et al. 2010; Vanneste et al. 2017).

To meet the requirement of sufficient tensile strength of MNFC films for the application exemplified, the rheological properties of enzymatically pretreated MNFC fibrillar suspensions were compared with the mechanical properties of corresponding obtained films, so that rheology can be used as a predictor of film strength (Maloney 2015; Zhu et al. 2014).

Materials and methods

Preparation of MNFC

For the manufacture of short MNFC fibrils, the pulp was first washed to create the sodium form by adding sodium hydroxide to a 2 w/w% fibre suspension until the pH reached 10, and then re-washed with deionised water to a conductivity of 8.2 lS. The enzymatic treatment was performed with a commercial enzyme ECOPULPx R (Ecopulp Finland Oy), produced by a genetically modified strain of Trichoderma reesei fungus (Rantanen et al. 2015). The activity properties of the enzyme are reported to be 17,700 nkat cm$^{-3}$ cellulase with a protein level of 93 mg cm$^{-3}$
An amount of 3 mg of enzyme per gram of pulp fibre was added to a 2.5 w/w% suspension and the temperature was increased to 57 °C at pH 5.5 during hydrolysis, whilst keeping under constant agitation. The period of digestion was increased for each subsequent sample in 30 min steps, Table 1. The enzymatic activity was terminated by adjusting the pH to 9–10 by sodium carbonate and increasing the temperature to 90 °C. After cooling the suspension overnight in cold storage, the samples were refined using an homogeniser (model M-110P, Microfluidics, USA), passing the material under a pressure of 2000 bar through a 100 μm flow gap. The solids content of the MNFC suspension after the fluidisation was 1.65 w/w%.

The enzymatic pretreatment of pulp as a route for producing low-charged MNFC resulted in the production of short fibrils, which, in the case studied here, have much lower aspect ratio than MFC and NFC produced via chemical oxidative pretreatment or mechanical refining alone, as illustrated in Fig. 1 comparing MNFC/300/ and MNFC/0/ suspensions (Table 1), revealing much shorter fibrils obtained upon 300 min of enzymatic hydrolysis.

**MNFC film preparation**

With increasing enzymatic treatment time, the resulting MNFC suspension viscosity decreased significantly, and the solid content for preparation of the respective films ranged from 0.6 to 1.9 w/w% to meet the target film grammage of 60 g m⁻² produced under conditions of 23 °C and relative humidity (RH) 50%. Films were made on a sheet-former according to ISO standard 5269-1, with some modification of the screen to aid fines retention. Due to the very strong water retention of MNFC, and its fine size, a polyamide monofilament open mesh fabric SEFAR NITEX® 03-1/1 with a pore size of 1 μm was placed on top of a 125 μm metal screen. The pulp suspension was poured at high viscosity onto the former without adding water or stirring the slurry. The system was pressurised to 0.3 bar and the sealing lid was used on the sheet-former. Double-sided adhesive tape, of 5 mm width, was attached to the edges of the drying plate between plate and formed film, with purpose of fixing the edge of the film to prevent it shrinking during drying (Fig. 2).

**Material treatment and characterisation**

*Optical microscopy* was used to study the fibrillar sample suspensions and films using an Olympus BX 61 microscope equipped with a DP12 camera. *Water retention* the water retention value (WRV) of the MNFC was determined in accordance to the standard SCAN-C 102XE with a slight modification in that 10 w/w% suspension of the MNFC was added in various ratios to a suspension of bleached unrefined pulp. The pulp matrix helps the MNFC dewater and remain retained on the screen. The WRV of neat MNFC can be evaluated by extrapolating to zero pulp, not including the swelling of the pulp fibres (Möller et al. 2010). The experiment was performed in triplicate for each sample.

*Dielectric barrier discharge (DBD) plasma* operates in a thermodynamically non-equilibrium condition (so-called cold plasma) in which the ion and molecular translational temperature is much lower than the electron temperature, such that excessive gas heating can be suppressed (Kostic et al. 2009; Prysiazhnyi et al. 2013). The advantage is that the plasma can be generated at atmospheric pressure, either in open or closed environment. In an open atmosphere, the plasma discharges can be produced with a gas flow between the electrodes (Mihailovic et al. 2011; Chu et al. 2002; Jens et al. 2017).

Table 1 Materials used in this study: bleached hardwood Kraft pulp treated with enzymes under controlled conditions, with progressive increase in enzymatic digestion time by 30 min steps for each subsequent sample

| Enzymatic treatment time/ min | 0 (reference) | 30 | 60 | 90 | 120 | 150 | 180 | 210 | 240 | 270 | 300 |
|-----------------------------|--------------|----|----|----|-----|-----|-----|-----|-----|-----|-----|
| Sample label                | MNFC/0/      | MNFC/30/ | MNFC/60/ | MNFC/90/ | MNFC/120/ | MNFC/150/ | MNFC/180/ | MNFC/210/ | MNFC/240/ | MNFC/270/ | MNFC/300/ |
A further attractive characteristic of the DBD plasma at atmospheric pressure is that it can be used to modify or activate surfaces of a wide range of materials, from polymers, textile fibres to biological tissues, without damaging them (Kostic et al. 2009; Pertile et al. 2010; Mihailovic et al. 2011). To generate the DBD plasma we used a home-made device built at the Faculty of Physics, University Belgrade, Fig. 3. The DBD is assembled in a chamber with nitrogen gas injected into the discharge volume (6 dm$^3$ min$^{-1}$) through ten equidistant holes to ensure homogeneous gas flow. MNFC films were treated for 0 s, 30 s and 60 s, respectively. The device was operated at 6 kV DC and 300 electric field pulses per second (Hz) for the prescribed durations of time, for all the films, as a higher voltage resulted in burning of the thin MNFC films, especially for those made from pulp exposed to long enzymatic pretreatment time.

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Determination of free surface energy (FSE) components

For the evaluation of any change in free surface energy of MNFC films arising from nitrogen plasma treatment, the contact angle (CA) is determined.

Most liquids are rapidly spreading on a high energy surface, and so a representative contact angle (CA) cannot be readily measured, Schultz et al. (1977) developed a method where CA can be measured by submerging the surface in one liquid and using a second liquid to measure the contact angle. In this case a hydrocarbon n-hexadecane is used as the submerging liquid having the purely dispersive liquid–vapour surface tension of $\gamma_{LV}^h = 27.4 \text{ mJ m}^{-2}$, much lower than the expected surface free energy of the MNFC samples, and water as the contact angle liquid with the highly polar liquid–vapour surface tension $\gamma_{LV}^w = 72.8 \text{ mJ m}^{-2}$ (Hansson et al. 2011). A sessile drop of water is lowered into contact with the horizontal film immersed under hexadecane using a precise pipette delivering 70 µl of liquid and the progressive change in drop shape due to the change in CA recorded with a Nikon camera (D5000) in time steps of 1 ms. The CA of water is also recorded separately to represent the print challenge of a highly polar ink (Özkan et al. 2016; Dimic-Misic et al. 2015). For each given MNFC sample and given liquid data variation is within 10%. The identification of contact line geometry and evaluation of CA uses numeric software tools, as presented visually in Fig. 4. For a parallel optimal method for polar FSE determination with water alone, the Girifalco and Good approach (1957), combined with the Neumann equation of state was used. This latter allowed the polar contribution to FSE be estimated and thus can be added to the formerly measured dispersive component. Each measurement was conducted five times. For each given MNFC sample, the relative error of measured FSE was shown to be $\sim 10\%$.

Surface topography

Plasma action on the film surface can lead to a degree of debonding of fibrils as well as electrostatic charging and potential for subsequent additional moisture adsorption. Such changes can lead to re-conformation of the surface, even though no mechanical forces have been applied (Kostic et al. 2009; Chu et al. 2002). The change in topography of the MNFC films was investigated by Atomic Force Microscopy (AFM) (Veeco Instruments, model Dimension V). Using a MultiMode 8 with Bruker NanoScope V controller. Each MNFC film sample was dry-cast onto a Mica support for AFM imaging. Micrographs were obtained in trapping mode under ambient conditions, using TAP 300 tips (resonant frequency 300 kHz, line force being kept constant at 40 N m$^{-1}$ and the AFM images were processed and analysed with the Bruker NanoScope Analysis 1.5 software.
Mechanical properties

Mechanical properties of the MNFC films were measured by an MTS 400/M vertical tensile tester equipped with a 20 N load cell. The instrument was controlled by a TestWorks 4.02 program. Specimen strips with dimensions of $60 \times 15 \text{ mm}^2$ were clipped from the MNFC films with a lab paper cutter (Afshahi et al. 2018). The thickness of the strips was separately measured with an L&W micrometer SE 250. The gauge length was 40 mm and the testing velocity was $0.5 \text{ mm min}^{-1}$. The results are presented as an average value obtained from five parallel specimens.

Surface chemical composition

Surface composition of the MNFC films was evaluated with X-ray photoelectron spectroscopy (XPS), using a Kratos AXIS Ultra electron spectrometer, with monochromatic Al K$\alpha$ irradiation at 100 W and under charge neutralisation. Both the untreated MNFC films and plasma treated specimens were analysed. For the preparation, samples were pre-evacuated for at least 12 h, after which wide area survey spectra (for elemental analysis) as well as high resolution regions of C1$s$ and O1$s$ were recorded from several locations, and an in situ reference of pure cellulose was recorded for each sample batch (Johansson and Campbell 2004). With the parameters used, XPS analysis was recorded on an area of $1 \text{ mm}^2$ and the analysis depth is less than 10 nm. Carbon high resolution data were fitted using CasaXPS and a four component Gaussian fit tailored for cellulosics.
**MNFC suspension rheology**

The rheological properties of MNFC suspensions were analysed at 2 w/w% concentration at 23 °C with an Anton Paar MCR 300 shear rheometer. The dynamic viscosity (η) was determined by steady shear-flow measurements, using the bob-in-cup geometry (Mohataschemi et al. 2014). Due to the potential for wall depletion (apparent slip) and thixotropic behaviour of MNFC suspensions, the “bob” was a four-bladed vane spindle with a diameter of 10 mm and a length of 8.8 mm, while the metal cup had a diameter of 17 mm. A pre-shear protocol was applied using constant shear at a shear rate \( \dot{\gamma} = 100 \, \text{s}^{-1} \) for 5 min, followed by a rest time of 10 min prior to recording the flow curves. Flow curves of MNFC suspensions were constructed under decreasing shear rate of \( \dot{\gamma} = 1000–0.01 \, \text{s}^{-1} \), with a logarithmic spread of data points (Dimic-Misic et al. 2013). To distinguish the MNFC suspensions in terms of their colloidal interactions as an effect of hydrolysis time, aspect ratio, crystallinity and friction between nanofibrils during the flow (Paakkonen et al. 2016; Dimic-Misic et al. 2018), the log–log plot flow curves were fitted to a power law according to the Oswald–de Waele empirical model, as shown in Eq. (1)

\[
\eta = k \dot{\gamma}^{1-n}
\]

where \( k \) and \( n \) are the flow index and the power-law exponent, respectively: \( n = 1 \) indicates a Newtonian fluid and \( n > 1 \) indicates pseudo-plastic (shear thinning) behaviour.

The Herschel–Bulkley equation describes the dynamic yield stress \( \tau_d^0 \) as

\[
\tau = \tau_d^0 + k \dot{\gamma}^n
\]

where \( \tau \) is the shear stress.

**Printing**

The photovoltaic (PV) inkjet printing inks (IP) contain a complex mix of materials, solvent and surfactants that keep the p-type and n-type components de-mixed (Hashmi et al. 2015; Özkan et al. 2016). A piezoelectric laboratory scale drop-on-demand (DoD) materials inkjet printer (Dimatix 2831-DMP) was used to test the printability of the plasma treated MNFC films (Dimic-Misic et al. 2015). The solvent of the IP ink is 3-methoxypropionitrile, which is highly polar and non-volatile (boiling point 164 °C), viscosity 1.2 mPa s and density 0.937 g cm\(^{-3}\), as stated by the supplier, Sigma Aldrich. The surface tension measurement was performed on the ink with an optical tensiometer (CAM 200 from KSV instruments) in pendant drop mode, giving a value of 29.2 mN m\(^{-1}\) (mJ m\(^{-2}\)).

**Results and discussion**

The rheological properties of the MNFC suspensions are given in Table 2, showing the change in dewatering, dynamic yield point and flocculation/water trapping gel-like structure (consistency coefficient, \( k \)) and shear thinning properties (index, \( n \), expressed as the positive difference \( n - 1 \)) and change in fibre morphology expressed as the fines content using the dynamic drainage jar (DDJ).

It is clear to see that with increase in enzymatic hydrolysis time, dewatering decreases as fibrils become thinner and smaller, and suspensions become more gel-like rheologically (Rantanen et al. 2015). At the same time, crystallinity of fibrils increases and water trapping structure/flocculation within the matrix with contrasting increased mobility in the flow regime once the structure is broken (Paakkonen et al. 2016). The dynamic yield point, the minimum stress needed to be induced to set the suspension into flow increases as the suspensions become more gel-like, but, also, breakage of that suspension induces greater shear thinning as fibrils are smaller and more crystalline, orienting easily in the flow direction (Paakkonen et al. 2016; Hubbe et al. 2017b).

The mechanical and optical properties of MNFC films are presented in Table 3, where it is evident that the sheet density of the films increases with increase in hydrolysis time, while the packing density of the smaller crystalline particles increases. The permeability of those films created with the finer nanofibrils obtained after 120 min hydrolysis in turn falls rapidly, and it was not possible to measure using air flow techniques. The light scattering coefficient decreases also as the packing density is increased and the amorphous parts of the cellulose fibres were reduced, while, due also to higher packing density, the elasticity modulus increases, showing that films had improved strength.
Table 2 Properties of MNFC suspensions

| Enzymatic treatment time (min) | WRV (cm³ g⁻¹) | Yield point, ε₀ (Pa) | Consistency coefficient, k (Pa s⁻¹) | Shear thinning coefficient, \( l(1 - n) \) | DDJ fines value (%) |
|--------------------------------|--------------|---------------------|-------------------------------|---------------------------------|-------------------|
| MNFC suspension properties     |              |                     |                               |                                 |                   |
| 0                              | 1.25         | 34.12               | 431.23                        | 0.82                            | 93.8              |
| 30                             | 1.61         | 47.34               | 241.3                         | 0.81                            | 88.8              |
| 60                             | 1.83         | 54.23               | 139.65                        | 0.81                            | 79.5              |
| 90                             | 2.19         | 68.45               | 89.67                         | 0.81                            | 62.4              |
| 120                            | 2.55         | 91.45               | 69.45                         | 0.84                            | 27.0              |
| 150                            | 2.85         | 438.34              | 57.23                         | 0.84                            | 21.0              |
| 180                            | 2.98         | 29.82               | 35.15                         | 0.86                            | 11.8              |
| 210                            | 3.33         | 19.64               | 19.67                         | 0.86                            | 9.6               |
| 240                            | 3.37         | 12.67               | 14.34                         | 0.87                            | 6.5               |
| 270                            | 3.32         | 8.99                | 9.97                          | 0.89                            | 1.5               |
| 300                            | 3.34         | 4.74                | 5.45                          | 0.91                            | 0.2               |

Table 3 Mechanical and optical properties of MNFC films

| Enzymatic treatment time (min) | Film weight (g m⁻²) | Density (g cm⁻³) | Permeability [µm(Pa s)⁻¹] | Light scattering coefficient (m² kg⁻¹) | E-Modulus (GPa) |
|--------------------------------|---------------------|------------------|--------------------------|--------------------------------------|-----------------|
| Film properties                |                     |                  |                          |                                      |                 |
| 0                              | 73.91               | 0.637            | 69.86                    | 37.43                                | 2.53            |
| 30                             | 76.12               | 0.794            | 9.96                     | 22.83                                | 4.16            |
| 60                             | 71.35               | 0.910            | 1.06                     | 16.12                                | 5.12            |
| 90                             | 72.31               | 1.016            | NA                       | 9.94                                 | 7.02            |
| 120                            | 70.53               | 1.090            | NA                       | 6.93                                 | 8.59            |
| 150                            | 70.81               | 1.127            | NA                       | 5.81                                 | 9.13            |
| 180                            | 69.57               | 1.145            | NA                       | 4.48                                 | 8.95            |
| 210                            | 71.08               | 1.178            | NA                       | 3.74                                 | 11.26           |
| 240                            | 70.10               | 1.179            | NA                       | 3.08                                 | 9.17            |
| 270                            | 71.18               | 1.226            | NA                       | 3.11                                 | 9.76            |
| 300                            | 65.27               | 1.187            | NA                       | 3.31                                 | 10.03           |

*Roughness* colour contour and profile plots of the surface of MNFC/30/150/300 films before and after plasma treatment are presented in Fig. 5. Before plasma treatment, the roughness of the films is directional, being different in in the two measured directions (red and blue profile lines). The map for MFC/30/indicates that there are voids present between 1 and 2 µm wide, while in the case of MFC/300/the surface is flatter with less voids and of much smaller size. This means that the degree of enzyme hydrolysis directly increases the resulting smoothness due to the ever finer fibrillar elements produced, as the crystalline parts are separated due to breakdown of the amorphous constituent. After plasma treatment, the amorphous material containing surfaces, e.g. MNFC/30/, are also seen to become relatively rougher than the highly hydrolysed crystalline films, e.g. MNFC/300/. The action of the plasma is to increase voyage in the courser particulate systems, as previously described, due to effects of charge, fibril debonding etc. (Jun et al. 2008). In MNFC/30/, it is possible to identify irregular both small and large voids appearing after plasma
treatment, while in MNFC/300/, the surface of the film has almost no such jagged appearance with voids only smaller than 1 μm. Nitrogen plasma treatment, thus, obviously changes the morphology of the films, on both the micro (nano) and macro level, which is likely also to have an influence on the wetting behaviour and decrease in CA due to the increased meniscus liquid–solid wetting line length (Prysiazhnyi et al. 2013; Pertile et al. 2010).

Fig. 5 Surface morphology and roughness of a MNFC/30/, b MNFC/150/ and c MNFC/300/before and after DBD nitrogen plasma treatment

The surface chemical species are revealed by the XPS spectra, from which the atomic % of C–C, C–O, O–C=O and N can be derived, Fig. 6. The effect of surface modification after nitrogen plasma can be clearly seen as the level of N attachment increasing as a function of the enzymatic removal of amorphous content (Johansson and Campbell 2004). The samples with increased crystalline proportion after longer enzymatic treatment nonetheless show similar C–C bond content. Similarly, with reduction of the
amorphous part with increased hydrolysis, the number of C–O groups decreases while C=O groups and other C and N containing groups are formed.

The results shown in Fig. 7 reveal that with the increase in enzymatic treatment of the raw material pulp there is a reduction of total FSE in the corresponding MNFC films in both polar and dispersive energy (green and blue unfilled symbols, respectively). A reversal of the decline in FSE as a function of enzymatic treatment can be observed resulting from nitrogen plasma treatment, showing compensating increases in both polar and dispersive measured components (green and blue filled symbols, respectively). Thus, an increase in wettability for water and n-hexadecane is reflected by a decrease in CA as the plasma treatment acts on the more crystalline samples (Johansson and Campbell 2004). However, as the roughness is also seen to increase as a function of plasma treatment for the lower crystalline samples (less exposure to enzymatic breakdown), one would expect from the Wenzel model that the wettability would increase. That we see a recorded increase in n-hexadecane CA, and thus decrease in dispersive FSE, we can conclude that the action of the plasma
discharge on the amorphous part is initially to reduce the dispersive energy component, and so likely act, at least partially, to breakdown first the amorphous content resulting in debonding and hence roughening (Hansson et al. 2011). This effective etching of amorphous parts of fibrils is then replaced by the action of nitrogen attachment, such that the higher average FSE values regained in the more crystalline samples after plasma treatment are significantly higher than the theoretical FSE 59.4 mJ m\(^{-2}\) of cellulose, and this is achieved via the major contribution of the plasma-induced increase in polar component.

The increased contribution of the polar component in the FSE donated by the cationic N adsorption under plasma exposure is, therefore, expected to enhance the compatibility with the application of highly polar inks, especially if their components are anionic (Vanneste et al. 2017; Ma et al. 2010; Hoth et al. 2008). The images in Fig. 8 confirm this expectation, where the improved wetting of the surface by water as a function of plasma exposure time is paralleled by the greater pick-up (trapping) of ink colorant (Hoeng et al. 2016).

**Summary and conclusions**

Micro nanofibrillated cellulose films formed from aqueous suspension can be made stronger by pretreatment of the raw fibre using enzymatic hydrolysis. However, the wettability by ionic liquids, including functional inkjet printing inks, such as are suitably used for printed electronics, solar cells etc., decreases as a result, limiting the use of such films in practice. Nitrogen plasma treatment, however, enables wettability by such formulations to be improved. The mechanism by which this occurs has been studied in this work presented in this paper and the following conclusions can be drawn:

- Total free surface energy increases with nitrogen plasma treatment of highly enzymatically hydrolysed fibrillar films (contact angle decreases), with a major increase in the polar component.
- Nitrogen is also included into the surface.
- Upon exposure to nitrogen plasma, dispersive surface energy initially decreases on those films made of pulp that was not treated or undergone short enzymatic treatment time, whereas the polar surface energy component remains relatively unchanged on such films.
- This effect is related to the interaction of the nitrogen plasma with the amorphous cellulose component in the non-hydrolysed fibrils.
- The dispersive energy component can once again be increased by exposure to nitrogen plasma in the case of the more crystalline fibrillar material derived from increased hydrolysis via enzymatic pretreatment.
- The surface area per unit mass was increased by the plasma treatment, apparently due to increased roughness on a nanometre scale.
- Highly ionic liquids, water and solvents typically used to disperse surfactant-containing organic-

![Fig. 8](image-url) IP ink printed on MNFC/300/film showing the dependence on wettability of the surface after nitrogen plasma treatment (see also Fig. 4); lower water droplet CA on the film corresponds with a significant increase in print colour density: a) untreated film, b) plasma treated for 30 s and c) plasma treated for 60 s.
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