The AC conductivity and dielectric permittivity for PVA-treated MWCNT electrolyte composite

Huda AlFannakh1,* and S. S. Ibrahim2

1Physics Department, College of Science, King Faisal University, P.O. Box 400, Al-Ahsa, Saudi Arabia
2Physics Department, Faculty of Science, Cairo University, Giza, Egypt

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ABSTRACT

Three-phase polymer electrolyte nanocomposite composed of polyvinyl-alcohol (PVA), manganese(II) chloride (MnCl2), and multiwall carbon nanotubes (MWCNTs) were prepared using the cast techniques. Impedance spectroscopy was used to investigate the AC electrical conductivity (\(\sigma_{ac}\)) of two- and three-phase samples with different weight ratios of multiwall carbon nanotubes (MWCNTs) over a wide frequency range and at various fixed temperatures (30 °C to 120 °C). The frequency-dependent nature of \(\sigma_{ac}\) was seen to follow Jonscher’s power law. The redistribution of accumulated charges was used to explain the change in the pre-exponent (n) and the constant (A) after the percolation threshold. As the temperature approached the glass transition temperature, the mobility of ions and polymeric chains also played an important role in this change. The Correlated Barrier Hopping (CBH) model was considered as the most predicted model for the samples at temperatures below 100 °C. However, the Quantum Mechanical Tunneling (QMT) model was predicted to be the most prevalent conduction model for temperatures greater than 100 °C. The values of the activation energy calculated from both \(Z''\) and \(M''\) are mostly close. Equivalent circuits were used to analyze the impedance spectra of the two- and three-phase samples. An attempt was made to explain the impedance behavior of the samples through the elements participating in the equivalent circuits.

1 Introduction

Electrolytic polymers represent one of the materials which attract the interest of many researchers because of their potential applications in solid-state batteries, chemical sensors, solar cells, and electrolyte gate transistors [1–16]. The electrolytic polymers are characterized by their high ionic properties, good mechanical properties, low electrochemical stability, low cost, ease of handling, easy manufacturing as thin films, and it is environmentally friendly. The development of polymers is not only by the addition of some kind of salts for polymers to form polymer electrolyte, but also the researchers have observed

Address correspondence to E-mail: halfannakh@kfu.edu.sa

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that the addition of nanomaterials (metals, semiconductors, organic and inorganic, fibers, and oxides, as well as carbon nanotubes) can contribute to improving some physical and/or chemical properties of the polymer electrolyte. This three-phase electrolytic nanocomposite may have specific properties which will be useful in technological applications such as supercapacitors sensors and actuators [17–21].

The improvement of the physical properties of the polymer electrolyte can be through adding carbon nanomaterials (Carbon nanoparticles [22, 23], Carbon nanofibers [24–26], multiwall carbon nanotubes MWCNTs [27–30], etc.[31, 32]), or by addition of ceramic nanomaterials (ZnO [33, 34], TiO2 [35, 36], BaTiO3 [37, 38], MnO2 [39, 40], etc.) or using a conductive polymer as third phase (PANI [41], P3OT [42], etc.).

Polyvinyl alcohol (PVA) electrolyte has been used as basic material for the preparation of three-phase nanocomposite. In the field of energy-storage devices, polyaniline-based electrodes are solidified in the H2SO4-polyvinyl alcohol gel electrolyte. This two-phase electrolyte was used to construct paper-like polymer supercapacitors using MWCNTs (as the third phase) [43]. Pan et al. [44] investigate the effect of CNTs on the ionic conductivity of the potassium hydroxide (KOH)-doped PVA/CNT membrane. The ionic conductivity increased by adding the functionalized CNT. They found that the methanol permeability was suppressed in the three-phase samples (PVA/KOH/CNTs) compared with the polymer electrolyte two-phase samples (PVA/KOH). Tu et al. [45] used PVA/Li2SO4/BMIMI gel polymer electrolyte to construct activated carbon-based supercapacitors. They investigate the prepared supercapacitors using cyclic voltammetry, galvanostatic charge–discharge, impedance spectroscopy techniques, and mechanical performance. Such flexible supercapacitors show better cyclic durability and excellent mechanical implementation. A wearable electronic textile three-phase nanocomposite based on PVA/SWCNTs humidity sensor was investigated by Zhou et al. [46]. For the application of Lithium-ion capacitors (LICs), poly(vinylidene fluoride-hexafluoropropylene) (PVDF-HFP) co-doped with multiwalled carbon nanotubes (MWCNT) via weak bond interactions of gel polymer electrolytes (GPEs) was investigated by Shengrui Yu et al. [47]. MWCNTs/PANI electrolyte composites were synthesized by the in situ polymerization technique. Under optimal conditions, the electrolyte with 4% MWCNTs/PANI and a salt concentration of 0.5 g showed a higher ionic conductivity of 197.4 μS/cm. The ionic conductivity of electrolytes affects the photovoltaic performance of fabricated dye-sensitized solar cells [48].

The dynamics of ionic transport and thermoelectric properties of a methacrylate-based polymer blend in combination with a lithium salt and MWCNTs was investigated by Maximilian Frank et al. [49]. The addition of MWCNTs to the polymer electrolyte allows for variation of the Seebeck coefficient as well as the ionic and electronic conductivities.

A remarkable increase in the electrical resistance of a fiber sensor increases significantly after spraying water. Samples prepared using 1:5 weight ratios of SWCNTs/PVA showed high sensitivity in high relative humidity. Three-phase system composed of MnCl2, PVA and PEG with different weight percentages of MnCl2 was prepared and investigated using Hall measurements [50]. Electrical conductivity of the composite increases with increasing the salt wt.%. The calculated activation energies were decreased with increasing salt wt.%. Dielectric measurement was also investigated for PVA: PEG/MnCl2 three-phase composites.

There is an issue usually discussed in the study of ac-conductivity, which concerns the link between the values of the parameters n and A when the Jonscher’s power law is applied [51], and the state of the material under study. Is there a direct relation between n and the state of the filler inside the sample (e.g., before and after percolation) or the sample morphology (e.g., two-phase, three-phase, filler aggregation or segregation process)? During this article, the authors aim to answer this question and link these parameters (n and A) with the state of the material under investigation, in addition to studying some other properties. Also, an attempt to improve the distribution of carbon tubes with polymer by grinding and soaking it in the salt solution (to reduce the attractiveness of the MWCNTs between each other) before adding to the polymer as a kind of physical treatment. Also, adding salt to the host polymer will contribute significantly to improving the electrical properties of the nanocomposite. Therefore, the research will investigate the ac-conductivity for a group of two-phase (polymer electrolytic sample) and three-phase samples (polymer electrolyte loaded with MWCNTs) before and after percolation.
2 Experimental

2.1 Materials

Analytical-grade PVA (with average Mwt. of 130,000 and 99% degree of hydrolysis) as host polymer and Manganese(II) chloride hydrate (Mwt. of 125.84) were purchased from Aldrich. Functionalized MWCNTs were purchased from Chengdu Organic Chemicals Co. Ltd., China (diameter > 50 nm, 10–20 mm length, and purity > 95%).

2.2 Sample preparation

Three-phase polymer electrolyte nanocomposite samples (PVA + 5% MnCl\textsubscript{2} + x wt.% MWCNTs) were prepared using the cast techniques according to the following steps:

1. Specific weight of the polymer was dissolved in 15 ml of distilled water at 85 °C. The solution was continuously stirred using a magnetic stirrer for 3 h.
2. Manganese chloride salt was weighted to be about 5 wt.% of the total sample weight. The salt was dissolved in 10 ml of distilled water and then added to different weight ratios of MWCNTs (0.1, 0.4, 0.8, 1.0, 2.0 wt. %). The mixture was manually ground in the MnCl\textsubscript{2} solution for 5 min (for MWCNTs untangling) and left for soaking (1 h) before adding the polymer solution. The three-phase solution was mixed using ultrasonicator for 2 h and transferred to a magnetic stirrer and stirred overnight (at ≈ 60 °C) to ensure the mixture homogeneity. The homogenous mixture was poured into flat glass plates and kept inside the thermal chamber (40–45 °C) and left to dry.

2.3 Dielectric measurements

The impedance (Z) and AC conductivity (\(\sigma_{ac}\)) of the composites were measured using a Keithly 4200 SCS (Semiconductor Characterization System) at frequencies varying from 100 Hz to 10 MHz. Both Z and \(\delta\) (phase angle) were collected automatically after averaging then Z’ (real part of impedance), Z” (imaginary part of impedance), and \(\sigma_{ac}\) (AC conductivity) were calculated. Copper conductive plates were used on both sides of the sample as conductive electrodes.

3 Discussion

Usually, pure polymers (other than conductive polymers) belong to the category of insulating materials due to the shortage of free-charge carriers. Therefore, their response to the applied AC field will be related to the dielectric relaxation effects which can be attributed to the transfer of space charges, the rotation of permanent dipoles in addition to the induced dipoles, segment mobility of polar groups, interfacial charge, as well as the relaxation due to transition of the materials from the glassy state to the rubber state. The addition of salts and/or nano-fillers may have an influence or impact on these relaxations process. Also, the interaction between the nano-fillers and polymer chains may cause a complex behavior for the relaxation process of the composite. The existence of induced polarization and interfacial polarization can also complicate the relaxation process.

The AC conductivity \(\sigma_{ac}\) can be calculated by the following relation:

\[
\sigma_{ac} = 2nf\varepsilon_0\varepsilon_\prime\tan(\delta)
\]  

(1)

where \(\varepsilon_0\) and \(\varepsilon_\prime\) are the dielectric constant of the free space and the material, respectively, and \(\tan(\delta)\) is the loss tangent or dissipation factor.

Figure 1 shows the frequency dependence of the AC conductivity \(\sigma_{ac}\) at different temperatures (from 30 to 120 °C) for PVA, PVA/MnCl\textsubscript{2}, and PVA/MnCl\textsubscript{2}/MWCNTs samples. It is found that \(\sigma_{ac}\) increases with the increase in temperature (typical behavior for most insulating polymer) [52]. The increase in the temperature increases the mobility of charge carriers in the polymer matrix and polymer composite and also, increases the number of transit sites [51]. This will increase the ability of the charge carrier to transfer from one transit site to another and the charge carrier will be able to overcome the potential barrier to contribute in the conduction. It is noted that the frequency at which the dispersion occurs (hopping frequency \(\omega_H\)) is shifted toward higher frequency as the temperature increases. In this case, it is possible to apply the Jonscher’s power law (JPL) [51]:

\[
\sigma_{ac}(\omega) = \sigma_{dc} + A\omega^n
\]  

(2)

where \(\omega\) is the angular frequency, \(\sigma_{dc}\) is the dc-conductivity (i.e., independent of frequency at \(\omega \approx 0\)), \(A\) is a temperature-dependent constant, and \(n\) is an
Both values ($A$ and $n$) depend on the temperature. The parameter $A$ represents the strength of polarizability in the sample, whereas the parameter $n$ represents the reactivity between the sample constituent (such as the interaction between the fillers with each other or the fillers with the polymeric chains or the interaction of the polymeric chains with each other in the case of the polymer blend).

The variation of $n$ with temperature depends on the type of conduction mechanism within the sample which depends on temperature, frequency, and...
sample constituent. Quantum mechanical tunneling (QMT), correlated barrier hopping (CBH), non-overlapping small polaron tunneling (SPT), and overlapping large polaron tunneling (OLPT) are theoretical models that can be used to identify the conduction mechanism in the case of AC conductivity [53].

For pure PVA samples, the general Jonscher power law equation (Eq. 2) did not give a good fitting when applying the following initial conditions: \( r_{ac} \geq 0 \) and \( 0 \leq n \leq 1 \); when using the modified Jonscher equation (Eq. 3) with the following initial conditions—\( r_{ac} \geq 0, 0 \leq n_1 \leq 1 \), and \( 0 \leq n_2 \leq 2 \)—a good fitting (Fig. 2) has been obtained.

\[
\sigma_{ac} = \sigma_{ac} + A_{10^{n_1}} + A_{20^{n_2}}
\]  

(3)

For the two-phase sample (PVA/MnCl\textsubscript{2}), Jonscher power law (Eq. 2) was applied and it gives a good fitting (between 0.998 and 1). The temperature dependence of \( n \) and \( A \) is represented in Fig. 3a for the two-phase sample. The values of \( n \) decrease as temperature increases and it varied between 0.88 and 0.72 with average of 0.80. The constant \( A \) increases gradually with temperature and reach its maximum value at about 80 °C and then the values changed between \( 4.35 \times 10^{-7} \) and \( 3.12 \times 10^{-7} \). The changes in the values of \( n \) and \( A \) (see Fig. 3a) indicate that, as the temperature increases (thermal activation), the polarizability increases (accumulation of the charge carriers and ions) in addition to the increase of the interfacial polarization. So, the ion–ion interaction and ion–polymer interaction decrease (i.e., \( n \) decreases). At near the glass transition temperature (\( T_g \)), the chain mobility increases which in turn allows the movement of ions and releases the accumulative charge carriers, which are reflected as reductions in the values of \( A \).

The sample loaded with 0.1 wt.% MWCNTs (Fig. 3b) behaves similarly to the electrolytic sample (PVA/MnCl\textsubscript{2}). The general behavior of the constant \( A \) with temperature is a gradual increase, and near the glass transition the values of \( n \) oscillate around 0.93 and then continue to increase (reach to 1 at 120 °C). Moreover, the values of \( n \) behave almost opposite to the behavior of the parameter \( A \). This behavior can be explained by following the same approach as the previous interpretation, as the sample is still before the percolation threshold.

Samples loaded with 0.4 wt.% and 0.8 wt.% MnCl\textsubscript{2} (Figs. 3c, d), which exceed the percolation threshold, have to some extent a different behavior where the value of \( n \) gradually decreased and then became almost constant over a wide range of temperatures (from 50 to 120 °C). For the sample loaded with 0.8 wt.%, \( n \) decreases gradually and increases dramatically above 100 °C. The constant \( A \) for both samples (0.4 wt.% and 0.8 wt.% MnCl\textsubscript{2}) shows a peak around 80 °C and is more symmetrical for the sample loaded with 0.8 wt.% MnCl\textsubscript{2}.

The behavior of samples after the percolation can be explained as follows:

1. Increasing the constant \( A \) with temperatures, below the glass transition temperature, may be due to the accumulation of ions and their lack of mobility. In addition, the presence of the

![Fig. 2](Image) The frequency dependence of ac-conductivity for pure PVA at 80 and 110 °C. The full lines is given by JPL (Eq. 2) and broken lines are given by modified JPL (Eq. 3) with
interfacial polarization around those ions will contribute to increasing the polarizability of the sample.

2. At temperatures above the glass transition, the mobility of the polymeric chains will increase, allowing more mobility for the ions to contribute to the conduction process. As well as, the leakage of charges carriers, which contributes to the interfacial polarization, causes a decrease in the value of the constant $A$ with temperature.

3. Also, at high temperatures ($T > T_g$) and as a result of the thermal expansion of the polymer in addition to the ease of movement of polymeric chains and charge carriers, the reactivity between the different elements will decrease, which is reflected as a decrease in the value of $n$. At temperatures greater than $100^\circ C$, sample loaded with 0.8 wt.% can be excluded from this behavior, where $n$ increases with increasing temperature. This can be attributed to the redistribution process of the filler and the formation of the filler aggregation.

By looking at the values of $n$ and its temperature dependence, one can assume that the CBH model (which assume the charge carriers hop between two sites above the Coulomb barrier) to be the most predominant model for the samples under test, especially during temperatures below $100^\circ C$, where the value of the parameter $n$ decreases, and its values range between 0.8 and 1. However, for temperatures greater than $100^\circ C$, the QMT model (which depends on phonon-assisted electron tunneling) is expected to be the most predominant conduction model.

Figure 4A–D represents the variation in AC conductivity versus frequency for pure, two-phase, and three-phase composite samples at 30, 60, 90, and $120^\circ C$. It is seeming that the addition of MnCl$_2$ to PVA increases the AC conductivity. Also $\sigma_{ac}$ increases with the increasing MWCNTs and there is an abrupt increase at 0.4 wt.% MWCNTs suggesting a percolation behavior. It is also noted that the addition of MWCNTs from 0.4 to 0.8 wt.% did not change the value of the AC conductivity particularly below $90^\circ C$. This can be attributed to the uniform distribution of fillers within the electrolytic polymer and
that the presence of salt helped increase the degree of freedom of movement of the MWCNTs, which caused a uniform distribution of those fillers and reduce the percolation threshold.

When the concentrations of the MWCNTs exceed the 0.8 wt.%, it is noticed that the AC conductivity decreases, and this can be attributed to the formation of aggregates (due to the interaction of the fillers with each other) and the formation of conductive fillers islands separated by an insulating medium of the electrolytic polymer.

As the temperature increases a plateau region which is an indicator to the dc-conductivity contribution increases. This gradual change from dc plateau to (ac) dispersive region designates the distribution of relaxation times. The frequency dependence of electrical conductivity can be divided into distinctive regions implying the existence of various dissipated effects [54].

Also, the increase of the AC conductivity at higher temperature (> 90 °C) can be attributed to the thermal expansion of the polymer matrix which leads to increase the chain mobility, encouraging the trapped ions to contribute in the conduction and hence increases the ionic conduction [52, 55]. The contribution of the segmental motion of the chains cannot neglect, since at temperatures above the glass transition the mobility of the chain increases and the chain segment contributes directly in the conduction mechanism.

It is known that the dielectric loss arises from the dissipation of the acquired energy during the charge or electric dipole movement in an alternating electric field. This energy loss is due to the phase lag between the charge or dipole response and the applied field.
Figure 5 shows the loss factor (tan δ) for the two-phase and three-phase samples at different temperatures. The dielectric loss curves for the samples follow the typical behavior, where the loss decreases gradually as the frequency increases. This behavior can be explained by considering the response of the charges and dipoles to the applied electric field at low and high frequencies. When the field frequency is low, the response of the charges (or dipoles) to the electric field will be high, so the loss factor is also high. The loss gradually decreases with increasing frequency, due to the weak response of field dipoles. This behavior depends on the nature of the sample, frequency range, and temperature. In the present case, Maxwell–Wagner–Sillars (MWS) interfacial polarization represents the main source of dielectric loss at low frequency [56].

The dielectric loss increases with increasing loading of MWCNTs up to 0.8 wt.% and then decreases sharply for 1 wt.% and 2 wt.% loaded samples. This change can be interpreted as follows:

1. Above the percolation threshold, the dielectric loss increases due to the formation of a network of capacitors and resistors through the sample, and these components are randomly connected in series and parallel [57].

2. When the loading of MWCNTs exceeds a certain level, the formation of MWCNTs aggregation (isolated islands) will occur and the number of micro-capacitors and resistors will decrease. Therefore, the dielectric loss will also decrease.

It is also noted that, for temperatures above Tg, the loss spectra were characterized by a definite peak for samples loaded with MWCNTs up to 0.8 wt.%. These
peaks shifted toward higher frequency with MWCNTs loading, indicating that the relaxation time decreases on increasing MWCNTs loading. This can be attributed to the fact that within the percolation region, the resistive and capacitive components of the networks decrease as the filler loading increases (before aggregation formation) reducing the relaxation time. A noticeable shift for the loss tangent peak toward the higher frequency side with temperature increase is attributed to the thermal activation of the charge and electric dipoles [58, 59].

Zsimwin program was used to find the equivalent circuit of the samples. Figures 6 and 7 show the fitting between the theoretical and experimental values of the two-phase (PVA/MnCl₂) and three-phase (PVA/MnCl₂/MWCNTs) samples at temperatures 60 °C and 100 °C as representative results.

The equivalent circuit depicted in Fig. 3 is employed to analyze the impedance.

The equivalent circuits depicted in Fig. 8A, B are employed to analyze the impedance spectra for the two- and three-phase samples. In both circuits, $R_1$...
Fig. 7 Cole–Cole fit of two-and three-phase samples at 100 °C; the open symbols are the experimental data and the solid lines are the fitted curves.

Fig. 8 Electrical equivalent circuit model representing impedance spectra to fit the experimental complex impedance, for two-and three-phase samples.

represents the electrode resistance, placed in series with the resistance of the polymer media \( (R_2) \). \( Q_1 \) is the imperfect capacitance due to the dielectric nature of the polymer media, \( R_3 \) is the resistance to the transfer of charge through the electrolytic media and \( Q_2 \) is a constant phase element representing the capacity of the interfacial polarization at the interface between the MWCNTs and the electrolyte, while \( R_4 \) and \( Q_3 \) represent the resistance to the transfer of charge between MWCNTs and the constant phase element (capacitance) between the MWCNTs aggregates at temperature \( 60 °C \). At 100 °C and due to thermal expansion the CPE connected with \( R_4 \) will change to \( W \) which represents the diffusion of charge between the MWCNTs aggregates.
4 Conclusion

Casting techniques has been utilized for the preparation of two-phase and three-phase electrolyte nanocomposite samples (PVA/MnCl2 and PVA/MnCl2/MWCNTs). The samples were loaded with different weight ratios of MWCNTs (0.1, 0.4, 0.8, 1.0, 2.0 wt. %). The results investigate the dielectric properties for the two- and three-phase samples within the frequency range of 100–1*10^6 Hz and at various temperatures (30 to 120 °C). The addition of MWCNTs to the electrolyte sample significantly improved the electrical conductivity of the composite (e.g., about three orders of magnitude at 500 Hz at 60°). A sudden increase was observed at 0.4 wt.% MWCNTs indicating leaching behavior. The ac–conductivity spectra were following Jonscher’s power law. For PVA/MnCl2 sample, the values of n (exponent) decreased as temperature increased and varied between 0.88 and 0.72 with an average of 0.80. Above the percolation threshold, the variation of n and A was interpreted by considering the redistribution of the accumulated charges (close to Tg) beside the change in the ions mobility and polymeric chains. The CBH model is the most predicted model for the samples under test, especially at temperatures below 100 °C, where the parameter n values decrease and range from 0.8 to 1. However, the QMT model is predicted to be the most prevalent conduction model for temperatures greater than 100 °C.

Data availability

The data that support the findings of this study are available from the corresponding author on reasonable request.

Declarations

Competing interest The authors have no relevant financial or non-financial interest to disclose.

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Author contributions

All authors contributed to the study conception and design. Material preparation, data collection, and analysis were performed by SSI. The first draft of the manuscript was written by HA and the two authors commented on previous versions of the manuscript. All authors read and approved the final manuscript.

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