RobotGreen. A Teleoperated Agricultural Robot for Structured Environments

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Abstract

This paper presents the development of a remote robotic platform to monitor and take care of urban crops. The agricultural robot performs activities such as sowing, irrigation, fumigation, and pruning activities on a small scalable structured crop. The generalities of the design of an anthropomorphic robot with five degrees of freedom, the description of the development of a multi-purpose end effector for the development of agricultural tasks, the implemented architecture of the teleoperation system of the robot is presented, including a visual support system and the employment of a low-cost master robot that allows the slave robot to be controlled more intuitively. Finally, some experimental results that show the functioning of the system are presented.

Keywords: Robot, agriculture, teleoperation, urban, remote sensors, eco-friendly design.

1. Introduction

With the passage of time humanity is becoming aware of the preservation of natural resources. In retrospect, many cases in which industrial processes prevailed even over harmful environmental effects could be noted. Nowadays man has realized that natural resources are very limited and that it is necessary to comply with a series of rules to protect the environment. In this new wave of conservationism and sustainability, several companies have proposed a large number of alternatives in favor of the protection of the environment. Some of them are the use of renewable energies on a large scale, clean or environmentally friendly industrial production [1], use of recyclable or natural materials, minimization and waste management, the proper storage or disposal of waste, among others.

Although large and medium-sized industries generate large environmental impacts [2], the need to promote the same culture spreads to small businesses and even to the population in general. Following this last idea it is conceivable to see how in recent years ideas such as energy generation on a domestic scale, architectural designs that take advantage of thermodynamic effects [3], collection of rainwater for toilets [4, 5], green roofs [6], vertical crops in buildings [7, 8], among many others have emerged.

These latest applications demonstrate how humanity is radically changing the conception that industrial developments and technology go against the environment, these on the contrary could guarantee the care of it, making them sustainable. A good example is the incorporation of new technologies such as robots in agricultural activities performing a wide variety of tasks [9]. These activities include fruit harvesting [10], monitoring [11], loading and unloading of agricultural material [12], transport assistance for harvested fruits [13], irrigation [14], fumigation, fertilization [15], weeding, automatic grafting, plowing [16], and sowing [17].

For the development of these activities, the agricultural robots have been equipped with advanced features compared to those of other robots, to guarantee their efficiency and effectiveness. e.g. for the collection of delicate fruits there are robots with deformable clamps [18], they have been equipped with the ability to interact and cooperate with other robots [19], pH measurement, humidity, automatic location of plants [20], wide range navigation [21, 22], guided by vision to avoid obstacles [23], land surveys for its displacement [24], some can even be reconfigure to achieve complex manipulations [25], others implement redundancy strategies [26], to perform tasks too complex or where you want a robot to do the work of a man to avoid exposure to hazardous environments as in the case of fumigation, teleoperated robots are implemented [15].

This project is aimed at the development of small structured crops or for interiors. The general idea is that citizens may have small crops in their own homes for the production of some types of food or infusions. Since the general population is used to doing a lot of work, they cannot afford to go constantly to their homes, which is why it is proposed that these crops be monitored or tended remotely by means of a robot, which will be responsible for carrying out the main tasks.

This teleoperation can be developed on different levels, which range from a supervised control using a smart phone to perform basic and repetitive tasks such as irrigation, to an advanced teleoperation that requires the use of a master robot (MR) for the development of complex tasks such as planting. This last case is contemplated when an urban crop is located on a roof, a terrace, or in a vertical garden in order to keep users from having to go to them avoiding possible accidents.
This article is organized as follows. In Section 2, the technological development is presented, in it; the generalities of the robot's design are described, it is then followed by the architecture of teleoperation systems; the results are analyzed and discussed in Section 3, and finally, the conclusions are presented in Section 4.

2. Technological Development

Generalities of Design of the Robotic Structure. For the study phase and design of the agricultural robot, the methodology of Quality Function Developed (QFD) is used as a method to define the development of its activities. This methodology compiles the requirements and needs of the robot and displays them in a set of technical and operative characteristics conducive to creating a concept that meets them. The methodology, rather than providing quantitative data, provides information of a fundamental qualitative nature to generate the design concept and explore solutions that adapt to the tools available for the execution of this project [27].

The requirements of the project represent the needs to be solved with the manufacturing of the robot. Some needs demand a higher level of attention, therefore; the degree of importance for each project requirement must be established correctly. The Mudge diagram is a tool that allows the comparison of project requirements aiming to generate a hierarchy among them according to the degree of importance and relevance in the project. The comparison in the Mudge diagram is done by attributing a value in each evaluation of two functions. The scale used to define the degree of importance considering values between 1 and 5, where 5 is the highest and 1 the lowest degree of importance. These values are represented by the letters A, B, C, D, E with respective values of 5, 4, 3, 2, 1.

In Fig. 1 the result of applying the Mudge diagram is presented. The scale and degree of importance that define the relevance of the requirements in the project can be appreciated [28].

The requirements of the project derived from the needs after applying the Mudge diagram are presented in Fig. 2 through the Pareto diagram. The bars represent each of the requirements defined for the robot with the value resulting from the comparison with other requirements. The curve indicates accumulations that go up to the value of 100 percent. An analysis of the diagram allows us to deduce that if efforts and resources are focused on satisfying the first 6 requirements, the project approaches the solution 60 percent for the needs raised by the users of the agricultural robot.

The solution concept obtained for the requirements mentioned in the agricultural robot project establishes the best solution for the robotic configuration in that of an anthropomorphic structure. Compared to closed chain robotic configurations, this arrangement provides greater work area, and a high degree of maneuverability. With the right selection of motors, precision, torque and correct operation of the position and trajectory control are guaranteed.

![Mudge Diagram for Agricultural Indoor Robot](image1)

![Pareto diagram of the robot for agricultural applications.](image2)

![Anthropomorphic robot structure with 5 DF.](image3)

![Design of Anthropomorphic robot with 5 DoF](image4)
Once the type of structure was proposed, the kinematic model of the robot was made by the traditional method of Denavit-Hartenberg, as well as by the successive displacement of screws using the Rodrigues equation [29] in its denotation of homogeneous transformation matrix for each joint (\(A_i\)), to find the closing equation of the end effector with respect to the origin (\(A_e\)) given its initial position (\(A_{e0}\)). In the latter case, the screw axes (\(s_i\)) coincide with the \(Z_{i-1}\) (with \(i\) from 1 to 5) and the normal vector from the origin to the screw axis is denoted as \(s_o\).

\[
A_e = A_1A_2A_3A_4A_5A_{e0} = A_{e0}
\]  

(1)

The conventional Jacobian matrix is obtained by horizontally concatenating the vectors \(J_i\) defined by the Eq. (2) for \(i\) from 1 to 5 (since all the joints of the robot are rotational), where \(A^{-1}_n\) \(p_n\) are the vectors of the articulation system unto the end effector of the robot.

\[
J_i = \begin{bmatrix}
    Z_{i-1}\times & p_n^T
\end{bmatrix}
\]

(2)

This robot basically has two types of singularities. Those of the outer limits (\(q_i = 0\), see section 2.3 and Fig. 17) and the internal ones that occur when the end effector is on the \(Z_0\) axis (coordinates \(x_c\) and \(y_c\) null). To solve this second singularity in terms of inverse kinematics, a choice was made to keep a record of the joint coordinate \(q_i\) (memory) and take the last one when passing through a singular point. In regards to the velocity level, the left-side pseudo-reverse method is implemented minimizing the quadratic error (\(J_i^* = [J_i^T]^T\)), another alternative is to use the Singularity Isolation plus Compact QP (SICQP) method described in [30].

In Fig. 4 the arrangement of the drives in the robot are illustrated, in it, it can be noted that the second joint has two motors in parallel position given that these are ones that must exert a greater torque. For the selection of the motors, the inverse dynamic model of the robot was estimated by means of the Lagrangian formulation, see Eqs. (3) and (4)

\[
\frac{d}{dt} \frac{\partial L}{\partial \dot{q}_i} - \frac{\partial L}{\partial q_i} = \tau
\]

(3)

\[
L = E_c - E_p
\]

(4)

where \(q_i\) are the generalized or articulate coordinates, \(\tau\) is the applied pair vectors, \(L\) is the Lagrangian function, \(E_c\) is the kinetic energy, and \(E_p\) is the potential energy.

When replacing the masses, inertias, frictions and dimensional parameters of the robot, the expressed model equation was obtained an expressed as follows.

\[
\tau = D(q)\ddot{q} + H(q, \dot{q}) + C(q) + F_c \dot{q}
\]

(5)

where \(D\) is the inertial matrix, \(H\) is the vector of coriolis and centrifugal forces, \(C\) is the vector of gravity force, and \(F_c\) is the robot’s friction coefficient matrix.

Subsequently, with the inverse dynamic model (see Fig. 5), a simulation of the robot was made, placing it in the most demanding configuration and applying to each of the joints a trapezoidal trajectory according to the parameters of acceleration times and maximum speed required. In this way the data was obtained to select the appropriate motors.
dispersing element is coupled). It must be stressed that the robot has the ability to easily attach various tools which will allow you to expand its applications.

Fig. 7. End effector multifunctional and attachable.

To satisfy the requirement of the project that sets the working space of the robot as important, the solution concept defines an additional mechanism that allows the robot to be moved in one direction. The mechanism is a motorized rail system which can be modified to reach different distances and allow the inclusion of new crop sections [31]. In Fig. 8 a photograph of the device can be seen.

Fig. 8. Translation mechanism for the robot. Architecture of the teleoperation system

The system can be divided into two zones, local and remote. The first is where the user or operator is located, which through the use of input devices (keyboard, mouse, master device, and smart phone) generates directives or commands to operate the system. The user in turn has feedback devices which allow him to handle information related to the remote environment; in this case he has a screen that displays the images captured by a camera in the remote environment, as well as information coming from sensors. Since a master device was implemented, a controller was required in the local area which is responsible for controlling the actuators of this device, when a particular force is required to be executed. In Fig. 9 we can see the general architecture of the teleoperation system implemented for remote cultivation.

Fig. 9. Teleoperation system architecture

In the remote area the devices to be controlled can be found, which in this case are: the agricultural robot and the displacement rail, the control box can be a PC, the environment is composed by the crop, the sensors including the electronic devices involved and the communications system.

In Fig. 10 the elements that make up the local area of the teleoperation system can be seen. The user has a computer that illustrates the information captured by the sensors in the remote environment. In turn, the user can enter the operation commands in various ways. You can use the mouse to press buttons in a graphical interface (quite intuitive) with specific commands such as the watering of a certain plant, the change of position of the end effector of the robot on the axes x, y, z, changes of orientations, among others. If you open the remote console application you can write and execute textual commands (higher level of platform control). And finally it has an operation mode based on a haptic device (master robot) that has a homothetic structure of the agricultural robot, by moving this device the remote robot will follow them. The control system is implemented in the computer, which then communicates via User Datagram Protocol (UDP) through a router with the remote area.

Fig. 10. Local teleoperation system zone

As for the remote area, it was divided into two parts in order to better illustrate its components. The first part consists of the agricultural robot which has 4 AX12 motors, 3 high torque MX64 motors, a displacement rail that significantly increases the working space of the robot which is driven by an AX12 motor. Since these two devices have actuators from the company Dynamixel, a USB2 Dynamixel card is used for its operation, which is commanded by means of a computer, as can be seen in Fig. 11.

Fig. 11. Remote teleoperation system zone

It can also be seen in this Fig. that there is an IP camera that communicates via WIFI or Ethernet to perform a visual feedback of the remote area. Optionally, the robot can have a high resolution web camera in its end effector in case it needs to visualize more clearly any object in the environment.

The second part of the remote zone (see Fig. 12) is composed of an Arduino Mega card equipped with an Ethernet Shield that allows you to send and receive...
information via UDP, a digital temperature humidity sensor (DTH11) that allows you to estimate the temperature of the environment and relative humidity, a light sensor or light dependent resistor (LDR), two level sensors to know the state of the liquids in the water and fertilizer storage tanks (or fumigation liquid) and a module of two opto-coupled relays that control the drive of the electronic pumping devices [31].

Fig. 12. Remote teleoperation system zone (part 2).

In Fig. 13 we can see a general and summarized diagram of the architecture of the system. It should be noted that the communications channel was proposed for a local area network, however it can be easily expanded to the Internet in order to increase the distance between the local and remote area. Since the universal protocol of datagrams was used for the sending of commands, the possibility of generating mobile applications for the control of the agricultural platform from a smartphone or a tablet is open.

Fig. 13. General diagram and summary of the system’s architecture.

**Preliminary Approaches for the Teleoperation of the Robotic Arm.** Moving the robot by specifying the joint coordinates can be an uncomfortable task for the user, because the new location (position and orientation) of the robot end effector cannot be calculated intuitively (calculations corresponding to the direct kinematics of the robot). On the other hand, specifying a new reference location for the robot is not as trivial a task as thought given that the robot has only 5 degrees of freedom having some limitations related to movement. In the same way there are some mechanical and electrical restrictions that prevent the robot from moving to a large number of locations. In order to solve this problem, a kinematic study of the working space of the robot is carried out and a series of aids are generated to illustrate the user about the allowed movements that the robot can make.

The robot’s workspace corresponds to the points at which its end effector can be accessed. It must be taken into consideration that although the robot is capable of reaching a certain position, this does not mean that it may be able to do it with any kind of orientation. For this reason, contemplating which points are those in which the robot’s wrist can access should be the first thing to do (remember that the wrist is in charge of changing the orientation of the end effector). The point of the robot’s wrist corresponds to the origin of system 3, which can be seen in Fig. 14.

Fig. 14. Inner limit of the robot's wrist workspace without taking collisions into account.

The blue sphere corresponds to the inner limit that the robot’s wrist can reach. This sphere’s center is the robot’s shoulder (System 1) and has as radius the distance between the origins of the systems 3 and 1 when joint 2 takes the value of 90 degrees (maximum mechanical limit of this articulation defined by the geometries of the links 2 and 3 of the robot).

In an analogous way, the outer limit of the workspace of the robot’s wrist is calculated. It can be seen that it is coincident when links 2 and 3 are aligned. In Fig. 15 the robot is illustrated in this type of configuration.

Fig. 15. Outer limit of the workspace of the robot's wrist.

In order to make the operation of the robot more intuitive, the workspace of the end effector is calculated from its current orientation. The cross section of this space corresponds to the same as the wrist but displaced to a
distance equivalent to the difference between the positions of the systems’ coordinates 4 and 5, as shown in Fig. 16.

In an analogous manner, the relationship between the outer limit of the working space of the wrist and the end effector is illustrated in Fig. 17. It should be noted that these workspaces revolve around the \( z \) axis according to joint position number one. From these preliminary approaches, the operating ranges of the robot end effector can be established. Additionally the robot's designed kinematic control system restricts the boundary angles of each of the joints to prevent the links from colliding with each other.

The teleoperation of the agricultural robot can be performed by the user using 4 different modes.
- Trajectory planning using an isochronous mode.
- Movement in the task space mode.
- Tracking of a master robot mode.
- Pre-loaded routines mode

Fig. 18 shows the local zone control scheme of the system including the input devices that the user can use in each of the teleoperation modes of the robot. In this Fig. it can be seen that the user may use a keyboard to send preset commands (e.g. go to home position or go to a specific joint coordinates), a mouse to interact with a graphical interface by moving the robot end effector (movement in the space of the task), a master robot (Tracking Mode) or a mobile device (cell phone, tablet, laptop) to activate preloaded routines from a web page.

Fig. 19 shows the three-dimensional representation of the execution of an example of this type of trajectories is illustrated. It must be taken into account that the profile implemented in each of the joints is a trapezoidal type.

As can be seen in Fig. 20 all the joints begin to move at the same time and finish at the same moment.

**Teleoperation of the Robot Using the Movement in the Task Space Mode.** This mode of teleoperation is based on the operator being able to change the position of the end effector according to the coordinate axes \( x \), \( y \) and \( z \) at the base of the robot as well as specifying the slope of the end
devices that facilitate the establishment of references. This slope is controlled by the fourth degree of freedom.

Given that there are several mechanical restrictions that prevent the robot from moving in some directions, the need to provide the user with information on the robot’s current position and the movements it can make from it was detected, evidencing the limitations.

To provide a better guide to the operator of the teleoperated system, visual signals are generated to indicate when the robot reaches one of its limits or how close it is to them. For example, in Fig. 21 the inner and outer limits of the workspace allowed for the robot are illustrated. In the case that the reference indicated by the user reaches one of its workspace limits, this limit will change color informing the user of this event.

![Fig. 21. Indication of arrival at the outer limit of the workspace](image)

Even with guide signals, it is very common for the user to generate references that the robot is not able to achieve, which is why an algorithm that detects whether or not the robot reaches the reference was generated, if it does not reach it, it calculates a solution that is viable for the robot and executes it. This allows a more comfortable handling of the robot without generating interruptions.

In Fig. 22 this case can be seen, where the solidarity sphere coordinated with the end effector system indicate the reference or objective proposed by the user for the robot end effector.

![Fig. 22. Reference exceeding the inner limit of the workspace.](image)

### Teleoperation of the Robot Using the Tracking of a Master Robot Mode.

Despite the visual indications provided to the user, teleoperation of the robot is not very intuitive for some of them using the mouse and / or the keyboard as input devices. For this reason, the use of master devices that facilitate the establishment of references was proposed, however, as is well known, this type of devices are of considerable cost, so the design and implementation of a device using the same type of robot servomotors as actuators (AX12 motor) was proceeded since they are relatively low cost bearing in mind the great benefits they provide.

The general idea was to develop a device that reflects the user guiding forces allowing him to estimate in an intuitive way when the links of the real robot are close to colliding in order to avoid sending erroneous references or crashes of the robot.

The developed device offers the user comfort to reflect a homothetic behavior to the anthropomorphic structure of the slave robot (SR) (agricultural robot), see Fig. 23. This implies that the user does not need to know by means of visual signals the limits of the workspace of the robot end effector, you just have to guide the end of the MR with your hand and the SR will follow the established reference.

![Fig. 23. Master robot implemented for teleoperation.](image)

Since the two robots have very similar kinematic constraints, they allow the user to easily interpret the logic of SR movements. For this reason it is not necessary to perform any kinematic transformation between them (only scaling). Although the movement ranges of the joints of the MR are greater than those of the SR, they were limited via software to make them coincide fully.

The use of this device makes the operation of the system very intuitive. When the user tries to point out references that the agricultural robot is not able to reach, it activates its actuators by exerting pairs and forces that allow it to detect the event. For example, with this device the user can detect when trying to exceed the limit of ± 60° of the joint 4 (one of the biggest limitations of the SR), every time that tries to exceed this range, activates the joint 4 of the MR exerting a force that forces the user to comply with the restriction, in addition to preventing the SR from colliding with itself, in addition it indicates the user the event and allows him to easily correct the reference. The Fig. 23 shows the MR with 5 degrees of freedom.

To verify the operation of the teleoperated system, experiments were proposed where the user had to perform typical operations of an agricultural process such as planting, irrigation and fertilization of plants. In Fig. 24 a photograph of the SR and two pots where the plants that are under its care are housed.

![Image](image)

In Fig. 25 the user can be seen moving the MR to generate the references that are sent to the controller of the SR. The similarity between the SR and the MR can be

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clearly distinguished. It should be noted that the articulations of the MR are normally de-energized and only act when the user tries to make an erroneous movement that the robot in reality cannot do, avoiding collisions.

Fig. 24. Agricultural robot in the remote area of the teleoperation system.

Fig. 25. User moving the low cost MR.

To get better feedback of the environment, the user has access to an IP camera located in the remote area which allows him to clearly visualize the robot's actions and, if desired, the visual aids created for it, as shown in Fig. 26.

Fig. 26. Robot teleoperation interface.

If the user wishes, the activation of the supply of information from the sensors is available, with this feature he can verify the temperature, humidity and luminosity of the crop so that he may be able to confirm that there is water or fertilizer in the storage tanks and carry out irrigation or fertilization tasks.

Teleoperation of the Robot Using Pre-Loaded Routines Mode. The teleoperation method based on the task space was designed to perform non-repetitive operations of a simple or medium degree of difficulty, for example the fumigation of a particular section of a plant. The teleoperation mode by means of the MR is planned for cases in which performing complex tasks that require greater skill of the user is desired, such tasks could be opening holes, planting plants or weeding. It should be noted that these activities were thought for the robot and not for a human since there is the possibility of having crops in places that are difficult to access such as vertical crops, roofs or terraces. In this way regular care can be provided to the crop without the user being subjected to dangerous situations (slippage, falls, among others).

In addition to the mentioned teleoperation methods, another mode has been generated to control the robot. This method is based on the execution of previously established routines which can be activated by the network sending high level commands via UDP. This method allows performing repetitive tasks such as irrigation and fertilization of plants or reading the information coming from the sensors from a mobile device (cellphones, tablets among others) or a computer. It must be taken into account that if the user wishes it, he can generate a repetitive schedule of tasks for the robot to execute based on or not based on criteria presented by the sensors. For example, water the plants every day at 5 a.m. except for the days when the temperature is lower than a predetermined value. In the same way conditions could be created according to luminosity and humidity, which can be very useful in countries with seasons.

3. Results

As for the design of the robot, it was possible to show that the torque calculation and the selection of the motors was correct considering that the robot achieves the pre-established speeds even in the most demanding configuration according to the gravitational effects. The functioning of the sensors is validated by comparison with the readings obtained by means of external equipment.

Agricultural robot joint level teleoperation results. To corroborate the functioning of the robot's teleoperation, a mono-articular study was used. Each of the joints was taken and their PID controllers were tuned (case MX64 motors) these are embedded in each of its drives. The control of each one of the drives is composed of two cascade systems which allow to define both the target position and the required speed.

Once the motors were calibrated, a comparative study was performed, emulating the position reference given by the articulation of the MR (step signal equivalent to a 30 degree offset) versus the response of the articulation of the SR implementing different speed levels. In Fig. 27 we can see the results corresponding to joint number 2 (the one that requires greater torque). These show the response to speeds ranging from 1 to 11 revolutions per minute (RPM). The results with higher speeds were not contemplated given that they gave a response with a peak value of over-oscillation which is not recommended in the case of teleoperated systems to avoid collisions. Since the idea is for the system is to respond as quickly as possible, it was selected to work with 11 RPM.
In Fig. 28 the results obtained for the same joint are illustrated, in an experiment where the user-directed MR was used executing relatively fast oscillatory movements for a time of 20 seconds. It can be seen how the articulation of the SR follows the reference adequately. It is necessary to emphasize that these experiments were carried out using a local network to guarantee low delays in the communications channel (provided for the tracking mode of the MR).

In order to quantify the performance of the system before delays (variables) occurred in the communication channel an experiment was proposed which emulates the position reference given by the articulation of the MR by a sinusoidal type signal with a unit frequency, a amplitude of 40 and a midpoint of 150 degrees. By sending the same reference, the evaluation of responses to different delays that occurred in the communications channel is allowed. To emulate the different levels of delay and to preserve the variable characteristics of the communications system, a buffer of variable amplitude (2 to 6 data) was created so that it delayed the sending of a data until the buffer was completely filled. It must be emphasized that non-blocking sockets were used via UDP to avoid possible inconveniences in the case of loss of information.

In Fig. 29, the response obtained with the same reference can be seen using a delay buffer of level 2 to 6. It can be clearly seen that the system responds correctly despite the various variable delays. In Fig. 30, the delays produced in all communications established for the experiment called Slave R4 (amplitude buffer 4) are illustrated, where the average value of the delays was 207, the maximum value of 31 and the standard deviation of 22 milliseconds.

As is evident, the delay in the communications channel increases, the response developed by the articulation of the SR is more differentiated from that of the MR. In order to better parameterize the quality of the response developed, an identification of the response is employed using the form given by Eq. (6) and the error is verified with respect to it.

$$q_e = 40\sin(t - \text{lag}) + 150$$

In this equation, the lag variable represents the estimated delay time that the articulation of the SR takes to perform the trajectory proposed by the MR; this time involves the delay in communications and the dynamics of the system and controller. In Fig. 31 the error obtained in position of the SR with respect to the offset sinusoidal signal (0.657 seconds) of the experiment called Slave R4 is presented. Table 1 shows the metrics obtained for experiments where the buffer varies between 2 and 6, which implies delays in the communications channel between approximately 100 and 300 milliseconds.

Additionally, if the user wishes to perform a task in which he must guarantee an error smaller than a certain value, he can activate a feature that enables a locking system of the joints of the MR to avoid significant differences between the MR and the SR, or in the event that large delays occur. Under normal conditions when the SR reaches the
reference the joints are unlocked. In Fig. 32, an example of this type of actions is illustrated.

Table 1. Metric of the experiments performed with different delays.

| Delay level in buffer | Estimated Lag [s] | Communications Channel delay [s] | Error regarding estimated signal [degrees] |
|-----------------------|-------------------|---------------------------------|------------------------------------------|
|                       | Average           | Maximum                         | STD Absol - Average | Absolute Maximum | STD |
| 2                     | 0.390             | 0.103                           | 0.18                        | 0.015 | 1.40 | 10.05 | 2.03 |
| 3                     | 0.517             | 0.159                           | 0.29                        | 0.035 | 1.55 | 8.98  | 2.09 |
| 4                     | 0.657             | 0.207                           | 0.31                        | 0.022 | 1.97 | 6.59  | 2.52 |
| 5                     | 0.797             | 0.258                           | 0.37                        | 0.037 | 2.56 | 8.42  | 3.27 |
| 6                     | 0.969             | 0.309                           | 0.43                        | 0.029 | 3.78 | 11.27 | 4.69 |

Fig. 31. Error in position of the SR with respect to the sinusoidal signal phase experiment called Slave R4.

Fig. 32. Lock of the joints of the MR in face of a significant difference of positions regarding those of the SR or significant delays.

Descriptive results of the operation of the agricultural robot. Once the operation at the joint level of the agricultural robot is corroborated, tests in relation to the execution of the tasks for which it was designed were performed. For these tests the elements of the crop, the multipurpose effector, the displacement rail and the robot accessories were used.

In Fig. 33 we present the teleoperation system corresponding to the remote area, where we can see cultivation, the SR with all accessories attached which, apart from the sensors, the use of an on-board camera that improves perception is highlighted. The user has access to an IP camera that allows a visual feedback of the environment.

In these tests, a user was asked to perform typical tasks that must be executed in the implementation of an urban crop. These tasks consisted in the teleoperation of the agricultural robot by means of the MR, which had the multipurpose manipulator on it. The tasks included the removal of a dry plant, the opening of a hole, and the sowing by transplant, in this case it can be observed that the plant is carried in a paper bag which degrades with time facilitating the planting process and lastly a cutting or pruning operation as it can be appreciated in Figs. 34 to 36. As expected, the irrigation and fertilization operations were trivial, so they were destined to be executed in repetitive and continuous sequences through the use of mobile devices.

Fig. 33. Robot operation using guide signals of in the robot's workspace.

Fig. 34. Process of weeding or removal of plants.

Fig. 35. Realization of the sowing process by transplant.
The teleoperation system is fundamental for the execution of this project it can be concluded that it is viable to tend a crop remotely in an urban environment. The teleoperation system is fundamental for the development of operations. Many variables must be taken into account to reduce dependence on supervision of the same. Within these variables, emphasize system supplies such as electricity, water, fertilizer, soil, among others.

The sensors play a very important role in the teleoperation processes of this project, the cameras are transcendental since they allow to observe the behavior of the robot and the elements with which it interacts. On the other hand, the luminosity, temperature and humidity sensors can be used to generate optimal irrigation conditions according to the criteria established by the agronomist, as well as to avoid material waste and possible damage.

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