Interference Cancellation in MIMO NLOS Optical Camera Communication-based Intelligent Transport Systems

NAVID BANI HASSAN1*, ZABIH GHASEMLOOY1, STANISLAV ZVANOVEC2, MAURO BIAGI3, ANNA MARIA VEGNI4, MIN ZHANG5, AND YINGJIA HUANG6

1Optical Communication Research Group, Department of Physics, Mathematics, and Electrical Engineering, Northumbria University, Newcastle upon Tyne, UK, NE1 8ST
2Department of Electromagnetic Field, Czech Technical University in Prague, Technicka 2, 16627 Prague, Czech Republic
3Department of DIET engineering, Sapienza University of Rome, Via Eudossiana 18, Rome, Italy
4Department of Engineering, Roma Tre University, Rome, Italy
5State Key Laboratory of Information Photonics and Optical Communications, Beijing Univ. of Posts & Telecom, Beijing, China
6Department of Engineering, Durham University, Durham, UK, DH1 3LE

*Corresponding author: navid.hassan@northumbria.ac.uk

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The ever-increasing number of vehicles at a global level signifies the need for communications between vehicles and the surrounding environment. Visible light communications (VLC) is a viable complementary technology to the congested radio frequency-based wireless systems. In order to increase the reliability of the VLC link, in this paper we propose two novel algorithms based on (i) channel inversion (CI), and (ii) frame subtraction and CI (FSCI) schemes are proposed to successfully extract the data in a non-line-of-sight multiple-input multiple-output spatial division multiplexing optical camera communications system. We have adopted differential modulation and frame subtraction schemes and proposed a unique packet structure to mark the packet and the position of the footprint of transmitters (Txs) in the image frame. We show that, the FSCI scheme with much simpler receiver structures can offer almost the same bit error rate (BER) performance compared with the hybrid selection/equal gain combining (HS/EGC) technique at lower transmit power (illumination) levels of < 13 dBm for a single transmitter (Tx) and improved performance at higher illumination levels of > 20 dBm for multiple Txs. Compared with HS/EGC, CI schemes have a higher tolerance to the spacing between Txs, where the payload threshold level can be set to a fixed value of 0.5. © 2019 Optical Society of America

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1. INTRODUCTION

Intelligent transportation systems (ITS) enables sharing of safety and traffic-related information between vehicles and/or vehicles and road infrastructures. The current ITS technologies are radio frequency (RF) based under the name of dedicated short-range communications (DSRC) [1]. However, there are a number of drawbacks related to DSRC including (i) sharing the same carrier frequency with a number of RF-based services such as fixed satellite and wireless services, mobile services, radiolocation, amateur radio, etc., thus resulting in both experiencing and introducing interference; (ii) increased costs due to the need for the RF-based on-board unit (OBU) and road-side unit (RSU) on vehicles and roadside infrastructure, respectively; (iii) vulnerability to the so-called broadcast storm, where several vehicles transmitting at the same time, which may lead to packet collision [2]; and (iv) potential hazards to the environment and human health [3]. As a viable alternative solution, the visible light communications (VLC) technology [4] could be adopted in vehicular communications by simply using lighting fixtures (i.e., front, back and internal), which are based on light emitting diodes (LEDs), organic LEDs (OLEDs), or laser diodes (LDs).

In VLC systems two types of detectors are commonly used: (i) photodiodes (PD) with a wide bandwidth (i.e., a few MHz to beyond a GHz depending on the PD’s size), which is the most widely used due to their high-speed [5, 6]; and (ii) image sensors (ISs) (i.e., multi-array PDs) as in cameras with much lower data
rates $R_p$. PD-based VLC systems are complex to implement for multiple access-based schemes and suffer from a high-level of ambient light-induced noise especially in outdoor environments in the presence of sunlight. Cameras, on the other hand, are considered as an imaging massive multiple-input multiple-output (MIMO) receiver (Rx), thus offering spatial separation of multiple light sources and spatial diversity [7, 8]. In addition, cameras can be used for multiple purposes such as vision and positioning [9]. Complementary metal-oxide semiconductor (CMOS) based cameras can offer a higher data rate than the frame rate of the camera by employing rolling-shutter (RS)-based sensor readout [10, 11]. However, in ITS there are a number of issues with RS-based communication including (i) very low exposure time, which can lead to poor SNR particularly over a longer transmission spans when operating at night times with streetlights of given illumination levels; (ii) a very small footprint of the light source at longer distances, which highly limits the performance of RS-based communications; and (iii) shorter size data packets and repetitive over a frame period given that the footprint of the light source only covers a small portion of the image sensor.

Most camera-based (i.e., IS) VLC, or commonly known as optical camera communications (OCC), systems reported are based on the line-of-sight (LOS) transmission mode. However, in some scenarios the transmitters (Txs) may not be within the LOS’s field of view (FoV) such as: (i) two vehicles approaching a crossroad where vehicles are not in the FoV of each other but the light beams and its reflections from the road surface are; (ii) two vehicles travelling on a motorway side-by-side where the camera can only pick reflections of the headlight of the other car from the road surface; (iii) taller SLs (SLs) high lampposts in highways, which can be outside the camera’s FoV but the light reflections from the road surface can be picked up by the camera; (iv) blocking of the LOS of the vehicle by a heavy goods vehicle, where the camera can still pick up off-axis projected optical illuminations induced reflections; and (v) blocking of the SLs by tall trees in urban areas, where camera can only capture reflected lights.

In [12], a $2 \times N$ non-LOS (NLOS) OCC system with a small overlap illumination region was proposed for SL-to-vehicle communications. It was shown that, for an overlap area above a certain level the information could not be extracted. Hence, in scenarios where the overlap region increases provided all the lights transmit data simultaneously then the information cannot be retrieved successfully. In [13], a space- and time- division multiplexing (STDMM) was proposed for NLOS OCC with large overlaps of the illumination footprints. However, using time division multiplexing (TDM) the system throughput is reduced [14], more specifically in urban areas with a large number of light sources (i.e., SLs, vehicles, display signs, etc.), see Fig. 1. In this situation, since the camera frame rate is low, selecting TDM as a multiple access technique is not the most efficient option. In addition, in cameras the IS, which is a massive matrix of photodiodes, channel inversion (CI) can be used, while the channel access is based on space division multiplexing (SDM).

CI, which eliminates the interference by directly forcing the interference terms to be zeros, has been investigated within the context of VLC for interference cancellation under the name of zero forcing (ZF) in multi-colour based MIMO and multiple-input single-output (MISO) links [6]. In [15], the performance of CI was compared with a combination of CI and successive interference cancellation (SIC) for a $3 \times 3$ MIMO wavelength division multiplexing (WDM) VLC system. It was shown that, for the optical band-pass filter and for signals having the same full

Fig. 1. Lighting sources in a typical urban environment showing overlapping illumination areas. The dark area within the dashed lines is the area where the vehicle’s camera observe.
In this paper, to the best of authors knowledge, for the first time we have adopted CI for OCC and propose two detection schemes of (i) CI; and (ii) frame subtraction and CI (FSCI) for NLOS MIMO-based OCC in order to mitigate the impact of crosstalk. We investigate the performance of CI-based NLOS OCC by considering the non-linearity of the camera, i.e., gamma correction. We show that, (i) error-free transmission is possible even under a high-level of crosstalk compared with hybrid selection/equal gain combining (HS/EGC); (ii) at a distance of 5 m and an ISO of 6400, CI offers improved performance compared with HS/EGC and FSCI by ~1.1 and 1.2 normalized eye-height, respectively at the cost of increased processing time (i.e., by 3 times); and (iii) for the Txs located close to each other, both CI and FSCI offer improved performance compared with HS/EGC.

The rest of the paper is organized as follows. In Section II, the system model is presented and in Section III, the proposed detection algorithms are described. Section IV outlines experimental test setup and results. Finally, Section V concludes the paper.

2. SYSTEM SETUP

The schematic system block diagram of the proposed system is illustrated in Fig. 2(a). M independent pseudo-random binary sequences in the on-off keying return-to-zero format are modulated to an Nl-bit length, where l = 1, . . . , M, and M is the number of Txs, as is generated as the payload. At the packet detector module, where preamble and pilot with the lengths of Npr-bit preamble and M-bit pilot are added to the payload, see Fig. 2(b), to indicate the start of the packet and obtain the channel coefficient matrix at the Rx, respectively. The role of preamble and pilot is to find start of the packet and to obtain channel coefficient matrix in the Rx side, respectively. The generated packet stream is differentially encoded as Xl×M = [x0,x1, . . . ,xM−1]T, where x0 = b0 and x1 = x0 ⊕ b1, and x0 is set to “0”. Note that, if the pilot signals are not interference-free, then the channel coefficient matrix will be inaccurate. Therefore, in order to ensure interference-free pilots, for the l-th Tx only the l-th bit is assigned “1” and remaining bits are set to “0” for the pilot signal. The output of the differential signalling block is then used for intensity modulation of the light sources for transmission over the NLOS channel with an impulse response given by [12]:

$$H_{N_{pr}×M}^{ch} = \left[ H_{N_{pr}×1}^{chj} \right]_{1×M} $$

where

$$H_{N_{pr}×1}^{chj} = \left[ h_{chj}(u,v) \right]_{N_{pr}×1} $$

with

$$h_{chj}(u,v) = \int_{y_{u−1}}^{y_u} \int_{x_{v−1}}^{x_v} R_{ij}(x,y) a_{t,ij}(x,y) \times R_{ij}(x,y) a_{t,ij}(x,y) \times \cos(\alpha_j(x,y)), $$

where $R_{ij}(x,y)$, $R_{ij}(x,y)$ and $\alpha_j(x,y)$ denote Lambertian patterns of the l-th Tx, reflections from the floor and the angle of incidence, respectively. $U$ and $V$ are the number of pixels in the horizontal and vertical directions in the image, respectively. In

$$a_{t,ij}(x,y) = \frac{dA}{d\alpha_j(x,y)} $$

and

$$a_{t,ij}(x,y) = A_{\text{lens,eff}} / d\alpha_j(x,y)^2 \times \rho, $$

where $dA$, $A_{\text{lens,eff}}$, $a_{t,ij}(x,y)$, and $a_{t,ij}(x,y)$ are the surface element

\[\text{on the floor, effective area of camera lens, distance from the l-th Tx to dA, and the distance from dA to the Rx, respectively. Moreover, the symbols in } H_{N_{pr}×1}(kT) \text{ and } N_{N×1}(kT) \text{ are the matrices of channel coefficients and the additive white Gaussian noise (AWGN) with the mean value } \mu_{\text{AWGN}} \text{ and variance } \sigma^2_{\text{AWGN}}, \text{ respectively, with } l = 1, \ldots , M. H_{N_{pr}×1}(kT) = P_t \times H_{N_{pr}×1}^{ch} \times H_{N_{pr}×1}(kT) \text{ where } P_t \text{ is the transmit power of the Tx.}

Note that, in cameras, non-linear functions of debayering, down-sampling and gamma correction, which are independent of the input signal, are applied to the RAW images to convert them to the JPEG format as given by:

$$Y_{N×1}(kT) = H_{N×M}(kT)X_{N×M}(kT) + N_{N×1}(kT),$$

where $H_{N×M}(kT) = [H_{l×N}(kT)]^T$ and $N_{N×1}(kT)$ are the matrices of channel coefficients and the additive white Gaussian noise (AWGN) with the mean value $\mu_{\text{AWGN}}$ and variance $\sigma^2_{\text{AWGN}}$, respectively, with $l = 1, \ldots , M$. $H_{l×N}(kT) = P_t \times H_{N_{pr}×1}^{ch} \times H_{N_{pr}×1}(kT) \times P_t$ is the transmit power of the Txs.

Note that, in cameras, non-linear functions of debayering, down-sampling and gamma correction, which are independent of the input signal, are applied to the RAW images to convert them to the JPEG format as given by:

$$Y_{N×1}(kT) = H_{N×M}(kT)X_{N×M}(kT) + N_{N×1}(kT),$$

where $g(.)$ is debayering function, $H_{N×M}(kT) = H_{N×M}(kT)^T$, $N_{N×1}(kT)$ is the noise matrix, and $Y_{N×1}$, $Y_{N×1}$, $Y_{N×1}$, $Y_{N×1}$, $Y_{N×1}$, and $Y_{N×1}$ are red, green and blue components of the image, respectively. Note that, since typical SLs are phosphor-coated LEDs, in this work we do not consider the colours, therefore following selection of odd/even frames all frames are converted.
to the grayscale as given by [23]:

\[
\hat{Y}_{N \times 1}(kT) = 0.2989Y_{N \times 1}^R(kT) \\
+ 0.5870Y_{N \times 1}^G(kT) \\
+ 0.1140Y_{N \times 1}^B(kT) \\
= \hat{H}_{N \times M}(kT) [X_{1 \times M}(kT)]^T \\
+ \hat{N}_{N \times 1}(kT).
\]

(7)

In order to reduce the complexity of processing of the received data, we apply an \(m \times n\) binning to \(Y_{N \times 1}(kT)\) as given by:

\[
\hat{Y}_{N' \times 1}(kT) = [b_i]_{N \times 1} \\
= \hat{H}_{N' \times M}(kT) [X_{1 \times M}(kT)]^T + \hat{N}_{N' \times 1}(kT),
\]

(8)

where \(b_i = \frac{1}{mn}1_{1 \times mn}A_{m \times n \times 1}, A_{m \times n \times 1} = \begin{bmatrix} y \end{bmatrix}_{m \times n \times 1}, j = \text{mod} (i - 1, \sqrt{m}) n + o_1 + (\lfloor \frac{(i - 1)n}{m} \rfloor + o_2 - 1) V, o_1 = 1, \ldots, n, o_2 = 1, \ldots, m, 1_{1 \times mn}\) is the matrix of ones and \(N' = \frac{N}{mn}\). Based on Lyapunov central limit theorem, when \(mn\) is a large number, \(b_i\) is a Gaussian distributed random variable with mean of \(\mu_{b_i} = \frac{1}{mn} \sum_{j=1}^{m} 1 \sum_{o_2=1}^{n} \mu_{y_i}\) and variance of \(\sigma_{b_i}^2 = \frac{1}{mn} \sum_{j=1}^{m} 1 \sum_{o_2=1}^{n} \sigma_{y_i}^2\). Note, following binning the number of pixels cannot be less than the number of Txs.

3. PROPOSED ALGORITHMS

We propose two detection schemes in order to extract the payload from captured video streams and compare them with the HS/EGC algorithm in [12]. The operations of the algorithms are best described by the flowchart shown in Fig. 3. For the entire captured video, the proposed algorithms, which are first applied to the odd and then to even frames of \(Y_{N \times 1}\) and \(\hat{Y}_{N \times 1}\), respectively have three stages of (i) preamble detection; (ii) pilot detection; and (iii) payload extraction, which are controlled by two flags, i.e., \(Flag_{pr}\) and \(Flag_{pi}\). Here, the subscript “pr” and “pi” refer to preamble and pilot, respectively. Note, at the start of the algorithm, both flags are set to “0”. In order to reduce the level of ambient light, each frame is subtracted from the previous frame as given by:

\[
\Delta Y_{N \times 1}(kT) = Y_{N \times 1}(kT) - Y_{N \times 1}((k - 1)T) \\
= \hat{H}_{N \times M}(kT) [\Delta X_{1 \times M}^0(kT)]^T + \Delta N_{N \times 1}(kT),
\]

(9)

where \(\Delta X_{1 \times M}^0(kT) = X_{1 \times M}^0(kT) - X_{1 \times M}^0(k - 1)T\) and \(\Delta N_{N \times 1}^0(kT) = N_{N \times 1}^0(kT) - N_{N \times 1}^0((k - 1)T)\) is an AWGN with zero mean and variance of \(2\sigma_x^2\). Note, elements of \(\Delta Y_{N \times 1}(kT)\) can have any integer values within the range of -255 to +255.

At the preamble detection stage, which is the same for all three schemes, since Txs are synchronized and share the same preamble, \(\Delta Y_{N \times 1}^0(kT)\) is averaged as given by:

\[
S_k = |\text{mean}(\Delta Y_{N \times 1}^0(kT))|,
\]

(10)

where \(|\cdot|\) is the absolute value. This procedure is performed \(N_{pr}\) times. \(S_k\) is then applied to a preamble hard threshold module the output of which is compared with the preamble. When matching is achieved, \(Flag_{pr}\) is toggled to “1” and detection proceeds to the next stage.

In the following subsections, we describe each of the proposed detection techniques.

Fig. 3. The flowchart of the proposed detection algorithms.

A. Frame Subtraction and Channel Inversion (FSCI)

Following preamble detection, \(\hat{H}_{N \times M}(kT)\) is generated for even values of \(k\) using pilot bits of the Txs. Since pilots are unique and only with a single bit set to “1” for each Tx, the frame related to each pilot is used to construct each row of the FSCI matrix of coefficients, i.e., \(\hat{H}_{N \times M}(kT)\), and on completion \(Flag_{pi}\) is toggled to “1”. Finally, in the payload extraction stage, in order to estimate the values of \(\hat{X}_{M \times 1}^0\) (both sides of \(9\) are multiplied with \(\hat{H}_{N \times M}(kT)\)). Note, for \(N' \neq M, \hat{H}_{N' \times M}\) is rank deficient, thus no inverse matrix. Instead, a pseudo inverse matrix can be used, which is given as [24]:

\[
\hat{H}^+_{M \times N'} = \left(\hat{H}_{M \times N'}^H \hat{H}_{N' \times M}^N\right)^{-1} \hat{H}_{M \times N'}^H,
\]

(11)

where \(\hat{H}_{M \times N'}^H\) is Hermitian transpose of \(\hat{H}_{N' \times M}\). Accordingly, the transmitted signal can be estimated as:

\[
\hat{\Delta X}_{M \times 1}^0(kT) = \hat{H}^+_{M \times N'} \Delta X_{1 \times N'}^0(kT)^T \\
- \hat{H}^+_{M \times N'} \Delta N_{1 \times N'}^0(kT)^T,
\]

(12)

However, this approach also leads to noise amplification (i.e., reduced SNR).

Finally, \(\Delta X_{M \times 1}^0(kT)\) is passed through a hard threshold module \(th_{psa}\) to estimate \(D_{M \times 1}\). With the upper and lower levels of \(\Delta X_{M \times 1}^0(kT)\) being “1” and “0”, respectively \(th_{psa}\) is set to 0.5. This stage is repeated for \(N_d\) iterations.

B. Channel Inversion (CI)

The CI algorithm is very similar to FSCI except for \(\hat{H}^+_{M \times N'}\) that is applied to \(\tilde{Y}_{N \times 1}\) as:

\[
\hat{X}_{M \times 1}^0(kT) = \hat{H}^+_{M \times N'} \left[\tilde{Y}_{N \times 1}^0(kT)\right]^T \\
- \hat{H}^+_{M \times N'} \left[\Delta N_{N \times 1}^0(kT)\right]^T.
\]

(13)

\(\hat{X}_{M \times 1}^0(kT)\) is then compared with \(th_{psa}\) and successively subtracted to estimate \(D_{M \times 1}\). In CI, the detection is carried out on each received frame. As a result, the output of CI is not affected by defects in frame subtraction due to gamma correction. Note,
Fig. 4. (a) The experimental testbed and (b) normalized light intensity on the floor for $D = 1$ m.

the only key difference between CI and FSCI is that, in FSCI, similar to HS/EGC, the inverse matrix of channel coefficients is applied to the subtracted frames, whereas in CI it is applied to each frame directly. In addition, as mentioned the pilot bits create the pattern of the Txs’ footprint in the image corresponding to a set of channel coefficients, which are later used to extract the information from the captured video stream at the Rx. In general, however, geometric distortions effects originating from the motion of the users, unfocused images, bad weather conditions, etc. have to be solved within OCC. In the proposed algorithms, as long as the shape of the footprint does not change significantly within the packet duration, the impact of geometric distortions will be negligible as the pilot and payload bits experience the same pattern of light. In [25, 26], different techniques are discussed to mitigate the image distortion.

4. EXPERIMENTAL RESULTS

Figure 4(a) illustrates the experimental setup for the performance evaluation of the proposed system. A 1066-bit packet composed of payload, pilot, and preamble of 1000, 2 and 64 bits long, respectively was generated in the OOK-NRZ format. Note, for a payload of length 1000, the probability of a 64-bit preamble repeating within the payload is $5 \times 10^{-17}$, i.e., extremely low [13]. Two Txs each composed of two cheap-on-board LEDs (COBLED) consisting of 48 small LEDs mounted on a heat sink were located on a frame at the height of $H_t = 2$ m above the floor level. COBLEDs on each Tx are spaced apart by 6 cm (see the inset in Fig. 4(a)), and have Lambertian beam profiles with the order of $m = 1$ and 2/3 in the horizontal and vertical directions, which is equivalent to the viewing angles of $\phi_{t,h} = 60^\circ$ and $\phi_{t,v} = 70^\circ$ in the horizontal and vertical directions, respectively. The normalized illumination profile of both Txs are projected on to the floor covered with a white sheet of paper with a reflection coefficient of $\sim 0.67$, where the distance between two Txs $D = 1$ m, was measured using a lux meter, see Fig. 4(b). Note, in the case of non-uniform reflection (e.g., wet road, which results in a more shiny surface), there will be very little interference in the NLOS link. Therefore, the problem of interference is inherently resolved. In this work, we use a matt surface to explore the worst-case scenario. A camera (Canon EOS 100D, with a sensor size of $22.3 \times 14.9$ mm and a Canon EF-S 18-55 mm lens) positioned at a distance $L_c$ of 5 m from the centre of the illumination plan on the floor with an elevation angle of $20^\circ$ were used to capture reflected lights. For the camera with $R_f$ of 60 fps (i.e., a data rate of 30 bps), we set ISO, exposure time $T_{\text{exp}}$ and aperture f-stop to 6400, 0.01 s, and $f/4$, respectively. For each experiment, a 3 minutes long RGB video stream with a 720p resolution was recorded for processing off-line in Matlab. Note that, in the detection process we used 10 binning. A camera-based Rx (with IS) offers a spatial diversity capability given that the pixel size in the IS is in the order of $\sim \mu$m, which is larger than the lights’ half wavelength.

Figures 5 show the measured eye diagrams of the received LSs considering non-linear gamma correction for: (a) the existing HS/EGC, and the proposed, (b) FSCI, and (c) CI.
Fig. 6. State diagrams for multi-levels eye diagrams of two interfering Txs: (a) HS/EGC, and (b) FSCI.

signals for HS/EGC, CI, and FSCI before \( t_{\text{thp}} \), where \( R_b \) is reduced ten times in order to have 10 samples per symbol. Note, with high levels of interference it is not possible to establish an error-free transmission with HS/EGC. We observe the followings for all eye diagrams: (i) the eye symmetry is maintained thus indicating very little contributions due to channel distortion; (ii) sharp slopes indicate good tolerance to the timing jitter; (iii) the wide eye width for some cases (i.e., reduced interference and noise, thus lower BER); (iv) multi-levels; and (v) higher SINR levels for some cases. As shown in Figs. 5(a), and (b), for HS/EGC and FSCI, there are 7 and 4 levels, respectively, which are best explained with reference to state diagrams shown in Fig. 6. In the case of HS/EGC, \( L_2 \) is the main reason that causes error in the data extraction, which happens when Txs have different initial stage and they toggle at the same time. In this situation the signal of one Tx is subtracted from the signal of the other Tx in the overlapping region. In case of FSCI, due to using the channel inversion to recover the data, the impact of interference is mitigated. Additionally, for the CI scheme, 3-level shown is based on the states of desired and interfering Txs as outlined in Table 1. Multi-levels observed in the eye-diagrams for CI and FSCI are mainly due to gamma correction, while for HS/EGC it is due to both gamma correction and interference. In the presence of gamma correction, the intensity of light in the overlapping area is not due to superposition of light rays; hence following CI, new levels are evident in the eye diagrams.

Figure 7(a) shows the simulated normalized eye-height (i.e., normalized to the widest eye opening \( w_{\text{eye,1}}/w_{\text{eye,2}} \) as a function of \( D/H_t \) for HS/EGC, CI and FSCI and for two Txs with the viewing angle of 60°. Note that, CI and FSCI have almost flat responses over all \( D/H_t \) up to 2 m/m, which outperforms HS/EGC. The negative value of the normalized eye opening for HS/EGC shows that \( L_2 \) is less than \( L_3 \), hence data cannot be recovered. Figure 7(b) depicts the normalized eye-height against the normalized ambient light illumination level \( \gamma \) (i.e., normalized to the peak illumination level of the Tx\(_k\)) for the proposed algorithms, \( P_t \) of 20 dBm, and \( D/H_t = 0.5 \) m/m. Here as well, HS/EGC display the worse normalized eye-height of \(< -0.3 \) compared with the average normalized heights of 0.8 and 0.9 for FSCI and CI, respectively for \( 0.5 < \gamma < 4 \). Note, HS/EGC display an almost flat response and for FSCI and CI algorithms, the normalized heights of the eyes are higher by 0.75 and 0.85 (on average), respectively compared with HS/EGC. For FSCI and CI the increase in the eye width beyond \( \gamma = 0.5 \) is due to the increase in the intensity of low-level pixels, hence the entire image is shifted to the more linear region of the gamma correction curve.

Figure 8(a) depicts the measured BER performance as a function of the transmit power for the proposed algorithms and for the ISO levels of 3200 and 6400, \( T_{\text{exp}} = 0.01 \) s, \( L_c = 5 \) m and f-stop of \( f/3.5 \) with only a single Tx in the absence of ambient light. The results show almost the same BER performance for HS/EGC and CI with a marginal power penalty of 0.1 dB irrespective of the ISO. Note, for ISO of 6400, a 3 dB lower transmit power is required compared with the ISO of 3200 for all schemes at BERs lower than the forward error correction (FEC) limit of \( 3 \times 10^{-3} \). In addition, there is a \(< 1\) dB power penalty between CI and HS/EGC irrespective of ISO. Finally, Fig. 8(b) demonstrates the BER as a function of the transmit power for the three schemes and for the link spans of 5 and 10 m, ISO of 6400, \( T_{\text{exp}} \) of 0.01 s and f-stop of \( f/4 \) displaying a same profile as in Fig. 8(b). Note, for a link span of 5 m the transmit power level is 3 dB lower compared with the link span of 10 m at the BER below the FEC limit for all schemes.

5. CONCLUSION

In this paper, we proposed two algorithms based on CI for NLOS MIMO OCC systems for interference cancellation and for extracting the payload in the presence of gamma correction, noise, and interference. We showed that, the proposed algorithms tolerate higher levels of interference compared with HS/EGC. For the OOK-NRZ signalling format, we showed that the eye diagrams displayed multiple-levels due to gamma correction and interference. We also showed that for a higher transmit power level of 20 dBm CI-based algorithms outperformed HS/EGC because of higher tolerance to the ambient light and a ratio of spacing to the height of Txs (i.e., 0.25 m/m). However, for lower transmit power levels (i.e., 6 dBm < \( P_t \) < 13 dBm) HS/EGC offered almost the same BER performance as FSCI (i.e., below the FEC limit). Moreover, HS/EGC showed \(~ 1.1\) dB worse performance compared with CI due to the increased level of noise as a result of frame subtraction. Although FSCI showed \(< 1.2\) dB power penalty compared with CI, \( t_{\text{thp}} \) in this scheme was fixed to 0.5. Compared with HS/EGC, which is limited to few scenarios, the proposed CI and FSCI algorithms offered higher tolerance to the spacing between Txs, but at the cost of increased computation time (i.e., three times for 10 binning) for obtaining the inverse

| Table 1. State of Txs for Each Level of The Eye-Diagram for CI. |
|-----------------|-----------------|-----------------|
| ine ine CI      | Desired Tx      | Interfering Tx  |
| ine L1          | “0”             | “0”             |
| ine L1          | “0”             | “1”             |
| ine L3          | “1”             | “0”             |
| ine L2          | “1”             | “1”             |
| ine ine         |                 |                 |
Fig. 7. The normalized eye height as a function of: (a) $D$ in the absence of ambient light; and (b) $\gamma$ at $D = 2$ m for the proposed algorithms considering two interfering LSs, $P_t$ of 20 dBm, $L = 5$ m, and a Tx’s viewing angle of 60°. The inset is the average intensity of a pixel as a function of total received power at the camera for ISO of 3200, $T_{\text{exp}}$ of 0.004 s, focal length of 55 mm and aperture f-stop of f5.6.

channel matrix. The work presented in this paper considered a relaxed situation of the static communications environment. However, in practice, mobility and the issues it cause such as near-far problem [27] should be considered, which will be the subject of our future works.

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