A measurement of the attenuation of radiation from F-18 by a PET/MR scanner

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Abstract
The attenuation of 511 keV photons by the structure of a PET/MR scanner was measured prior to energizing the magnet. The exposure rate from a source of fluorine-18 was measured in air and, with the source placed at the isocenter of the instrument, at various points outside of the scanner. In an arc from 45 to 135 degrees relative to the long axis of the scanner and at a distance of 1.5 m from the isocenter, the attenuation by the scanner is at least 5.6 half-value layers from the MR component alone and at least 6.6 half-value layers with the PET insert installed. This information could inform better design of the radiation shielding for PET/MR scanners.

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KEY WORDS
PET/MR, self-attenuation

1 | INTRODUCTION

During the planning for the installation of a PET/MR scanner (Signa, General Electric Healthcare, Chicago, IL), no information was available on the attenuation of radiation from PET radionuclides by the scanner itself. As a consequence, the facility was shielded conservatively against ionizing radiation by ignoring any attenuation by the instrument itself. Prior to energizing the magnet during the installation of the scanner, the attenuations by the MR portion alone and by the MR portion along with the PET insert of the radiation from a source of fluorine-18 were measured. Those measurements demonstrate that including the structure of the PET/MR scanner in a radiation shielding design could obviate an appreciable amount of structural shielding compared to that which is called for when treating the radioactive patient as a bare point source in air.

Abbreviations: ALARA, as low as reasonably achievable; CT, (x-ray) computed tomography; MR, magnetic resonance (imaging); PET, positron emission tomography.
Three calibrated ionization survey meters (451B, Fluke Biomedical, Cleveland, OH) were used. Each was operated by a different medical physicist. A string with a plumb bob at the free end was tied around each meter and its length was adjusted so that the center of the chamber of the meter was in the horizontal plane of the isocenter when the tip of the plumb bob just touched the floor. Another medical physicist recorded the reading of each meter at each point on the polar grid (i.e., with the tip of the plumb bob just grazing each marked point on the floor) along with the time of day of the measurement as determined by a cellular telephone. All of the measurements were decay-corrected to the time at which the source had been assayed. The background was negligible in all cases. The three measurements at each grid point were averaged, corrected to a distance of 1 m by the inverse square law and then normalized by the average of the in-air measurements of the source at 1 m. They were then converted to half-value layer values by taking their logarithms to the base $\frac{1}{2}$ (i.e., by dividing their natural logarithms by the natural logarithm of one-half).

An in-house-written computer program that the authors use for designing radiation shielding in nuclear medicine and PET was employed to estimate the weekly doses from a busy workload consisting of an average activity of 3.4 mCi (126 MBq) of F-18 for 87.5% of the patients and an average activity of 10.2 mCi (377 MBq) of F-18 for 12.5% of the patients. The 3.4 mCi (126 MBq) average activity while the patient is in the scanner room assumes an 11 mCi (407 MBq) administered activity, a 64% patient transmission factor, a 1 h uptake time, voiding of 15% of the administered activity, and a 1 h scanning time. The higher activity was used to simulate anticipated Zr-89 studies. The patient was modeled as a point source that was located on the patient handling system outside of the magnet for 10% of the work week and at seven locations along the central axis of the scanner for a total of 70% of the work week, simulating the movement of the patient during image acquisition. It was assumed that the scanner room would not contain radioactivity for 20% of the work week. An occupancy factor of unity was assumed. The scanner was modeled as an annular cylinder of lead with a thickness of 33.7 mm. For 511 keV photons, this is 6.6 times the broad-beam half-value layer of 5.1 mm, which is the average of the values in two recent references.\textsuperscript{1,2}

### RESULTS

The gamma ray exposure constant from F-18 in syringes suspended in air was measured to be 0.573 mR-m\textsuperscript{2}/mCi-hr in the first measurement session and 0.656 mR-m\textsuperscript{2}/mCi-hr in the second measurement session.
The measured half-value layers of the attenuation afforded by the MR component alone are shown in Fig. 1 and are tabulated in Table 1. These measurements have been previously reported in a preliminary form. The measurements from the scanner after the PET insert and the patient handling system had been installed are shown in Fig. 2 and are tabulated in Table 2.

The estimated weekly dose distribution from the simulated work week in the absence of any shielding from the PET/MR itself is shown in Fig. 3. The estimated weekly dose distribution from the simulated work week including an approximation of the shielding afforded by the scanner is shown in Fig. 4.

**Table 2** Half-value layers of the MR and PET insert.

| Radial distance (m) | 0°  | 22.5° | 45° | 67.5° | 90° | 112.5° | 135° | 157.5° | 180° | 225° | 270° | 315° |
|-------------------|-----|-------|-----|-------|-----|--------|------|--------|------|------|------|------|
| 1.5               | 0.0 | 7.2   | 7.8 | 8.0   | 9.1 | 6.6    | 1.9  | 6.9    | 8.1  | 7.5  |      |      |
| 2                 | 0.0 | 0.26  | 5.8 | 7.8   | 7.9 | 8.3    | 5.5  | 1.6    | 5.9  | 7.6  | 6.1  |      |
| 2.5               | 0.0 | 0.54  | 5.3 | 6.9   | 7.2 | 5.2    | 1.8  | 1.0    | 5.5  | 5.3  |      |      |
| 3                 | 0.0 | 0.63  | 4.7 | 7.2   | 4.8 | 1.3    | 1.1  | 5.4    | 5.3  | 4.8  |      |      |
| 3.5               | 0.3 | 0.60  | 4.4 |       | 0.91 | 0.96   |      |        |      |      |      |      |

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**4 | DISCUSSION AND CONCLUSION**

The gamma ray exposure constants of 0.573 and 0.656 mR·m²/mCi·hr that were measured in the two sessions differ by about 14%, which is more than the expected uncertainty in the dose calibrator readings. It is possible that the assay of the second source was not correctly performed or recorded. However, both measured constants fall within the range of values from 0.568 to 0.710 mR·m²/mCi·hr that are found in the literature. The latter value was converted from the original dose units using a calculated f-factor of 0.965 cGy/R based on previous studies. This discrepancy does not adversely affect the attenuation values, which are based upon the ratio of two measurements of the same source.

Although measurements were made only in the horizontal plane that passed through the isocenter of the scanner, a visual inspection of the scanner with the covers removed indicated that that plane intersected the fewest ancillary components and that the parts such as the cold head above the magnet dewar and the supporting structure below the dewar might offer some additional shielding. The effect of extra components was observed in the horizontal plane where the patient handling system, which had been installed between the first and second measurements, introduced an additional half-value layer of shielding along the central axis beyond it, although only over a very small solid angle.

This report complements the work of Nye, et al., who found the effective attenuation of a General Electric Discovery LS PET/CT to be two half-value layers along the line perpendicular to the long axis of the scanner and passing through the isocenter and of Busse who, for several PET/CT scanners, found the attenuation by a PET...
scanner perpendicular to the long axis to be between 1.5 and 2.3 half-value layers, depending upon the manufacturer. The present measurements suggest that the attenuation of the PET insert of the PET/MR scanner is between 1.5 and two half-value layers.

The structure of the PET/MR scanner itself provides a substantial amount of shielding. It is at least 6.6 half-value layers at a distance of 1.5 m from the isocenter around an arc from 45 to 135 degrees with respect to the long axis. The thickest structural shielding that the authors have ever recommended for a PET/CT installation is five half-value layers.

Structural shielding for PET is both heavy and expensive. When designing the installation described here, the weight of the shielding as well as that of the scanner itself was a significant concern to the structural engineers. Had this information been available then, less structural shielding would have been recommended and siting would have been easier.
CONFLICT OF INTEREST

The authors have no conflicts of interest with respect to this work.

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