Influence of Interface Morphology on Hysteresis in Vapor-Deposited Perovskite Solar Cells

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Metal halide perovskite materials show great promise for photovoltaic devices, with power conversion efficiencies (PCE) based on this class of materials having recently exceeded 22%.[1] However, organic-inorganic perovskite photovoltaic devices have been beset by anomalous hysteresis, whereby the current–voltage (I–V) characteristics are dependent upon both scan rate and direction.[2] Furthermore, discrepancies have been reported between the initial measured solar cell efficiency and measurements taken after holding the device at a sustained bias over a period of time.[3–5] Both ion migration in the bulk of the thin film and charge trapping at the perovskite surface have been proposed as causes of the anomalous hysteresis.[6–8]

In this systematic study we use a single batch of vapor-deposited CH$_3$NH$_3$PbI$_3$ (MAPbI$_3$) on a range of device architectures to show that the cause of hysteresis in planar heterojunction MAPbI$_3$ solar cells originates from the interface between the perovskite and the electron transport layer, and that interface engineering can be used to eliminate hysteresis in these devices. Furthermore, we show using transmission electron microscopy (TEM) and scanning transmission electron microscopy (STEM) that under identical growth conditions the interface affects perovskite morphology and crystallinity. We link devices incorporating amorphous regions of MAPbI$_3$ at the perovskite-electron transport layer (ETL) interface, with hysteresis and poor stabilized performance of solar cell devices.

The perovskite methylammonium lead triiodide (MAPbI$_3$) has been intensively studied since its initial breakthrough as a photoabsorber.[9] It has been shown to possess material properties ideally suited for photovoltaic devices such as a high absorption coefficient, long electron–hole diffusion lengths,[10] high-energy carrier mobilities,[11] and a favorable bandgap of ≈1.6 eV.[12,13] Organic–inorganic metal halide perovskite materials can be processed by a diverse range of deposition techniques and on a variety of substrates.[14–17] Solution coating techniques and vapor deposition are the two key approaches that have produced highly efficient solar cells.[18,19] Dual source vapor deposition was used to create the earliest high-efficiency planar heterojunction perovskite solar cell using an MAPbI$_{1-x}$Cl$_x$ perovskite.[20] Solution processing techniques have been used to further explore the planar heterojunction device architecture by changing both the charge transport layers and the perovskite photoactive layer.[21,22] However, planar heterojunction solar cells based on both vapor-deposited and solution-processed MAPbI$_3$ have been reported to exhibit significant hysteresis in their I–V characteristics.[2–4]

In this study we focus on vapor-deposited perovskite solar cells, as vapor deposition allows us to deposit a perovskite film simultaneously on multiple devices with different planar architectures under identical conditions. Vapor deposition involves heating precursor solids in high vacuum, allowing the sublimed material to uniformly condense on the substrate.[23] While vapor deposition is currently less commonly used compared with solution processing, it considerably reduces the amount of independent variables, leading to highly uniform and pinhole-free thin films on a consistent basis.[24] As a technique widely used in industry for organic light emitting diodes and inorganic semiconductors, thermal vapor deposition has also been shown to have a high rate of batch-to-batch reproducibility.[24] There are two main methods to create an MAPbI$_3$ thin film by thermal vapor deposition: co-evaporation, by which the precursor materials methyl ammonium iodide and lead iodide (PbI$_2$) are evaporated simultaneously[25] and a two-step evaporation, whereby the precursors are deposited sequentially.[17] In this study, we focus on films produced by dual source thermal co-evaporation.

To establish a link between device J–V hysteresis and architecture we first present statistics from 186 planar heterojunction solar cells produced from 17 deposition batches, where deposition parameters and annealing conditions were optimized for the particular architecture. In order to understand the underlying cause of hysteresis we will then concentrate on a subset of architectures where the perovskite was deposited in the same vapor deposition run, without any post-deposition thermal annealing.
A clear link between $J$–$V$ hysteresis and device architecture can be seen by examining Figure 1 which summarizes the performance of 186 devices with four common device architectures labeled A–D. For types A–C the MAPbI$_3$ perovskite layer was evaporated onto an ETL, a geometry that is common for most published perovskite solar cells and which we will refer to as a “regular” device architecture.\[26\] The ETLs for types A, B, and C were TiO$_2$, C$_{60}$, [6,6]-phenyl C$_{61}$ butyric acid methyl ester (PCBM), respectively, while the hole transport layer (HTL) was 2,2$'$,7,7$'$-tetrakis(N,N-di-4-methoxyphenylamino)-9,9$'$-spirobifluorene (Spiro-OMeTAD). In contrast, for the type D, which we will refer to as an “inverted” device architecture, the PCBM ETL was deposited after the MAPbI$_3$ was evaporated on a poly(4-butylphenyl-diphenyl-amine) HTL.\[27\]

Figure 1a shows the $J$–$V$ characteristics of the champion devices for each architecture type A–D. For the type A (c-TiO$_2$ ETL) a clear hysteresis can be seen between the forward and reverse $J$–$V$ sweep. While the standard method to determine the PCE of a solar cell is based on analysis of the $J$–$V$ curve,\[28\] it has been proposed that an alternate method measuring the “stabilized power output” (SPO) may be more appropriate in assessing the working efficiency of hysteretic cells.\[2\] In this method PCE is measured as a function of time, by holding the device at a load corresponding to the maximum power point. Maintaining the device at constant bias more closely simulates the operation of a solar cell under load, thus measurements of SPO and stabilized current density at maximum power point ($J_{mpp}$) can be more representative indicators of the true device efficiency.

Device architectures, B and C, show a good agreement between the PCE and SPO. Interestingly for the type B device, in which the c-TiO$_2$ ETL was entirely replaced by C$_{60}$, there is significant $J$–$V$ hysteresis yet a good agreement between PCE (15.4%) and SPO (15.0%). Type C devices, which incorporate a

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**Figure 1.** a) Schematics for different planar heterojunction device architectures with varying n-type layers (type A–C) and an inverted device architecture (type D), with the corresponding current–voltage ($J$–$V$) curves for the champion devices. The arrows denote the scan direction of the $J$–$V$ sweep. The inset in each $J$–$V$ curve shows the stabilized power output (SPO) after 50 s under a constant bias. Histograms showing the statistical variation for the different device types. b) Stabilized power output (SPO). c) Stabilized current density ($J_{mpp}$). Type A devices (blue) have very poor stabilized currents and efficiencies compared to devices which use n-type layers used in the device types B (orange), C (green), and D (purple). Type B devices show hysteresis, yet the stabilized device parameters are significantly higher compared to type A devices. Evaporation conditions were individually optimized for each device architecture; detailed information on layer thicknesses and fabrication methods can be found in the Supporting Information.
layer of PCBM on top of c-TiO$_2$ as ETL, show minimal hysteresis. Finally, the inverted device (type D) shows no observable hysteresis with again the SPO being representative of the PCE. This is in good agreement with previous results, where inverted devices employing evaporated MAPbI$_3$ thin films show no hysteresis.[19]

The improved SPO after changing the ETL from c-TiO$_2$ (type A) to C$_{60}$ (type B) is consistent with C$_{60}$ being a more effective electron extraction material.[30] Furthermore the hysteresis observed in the type B devices, can be attributed to formation of pinholes in the spin coated C$_{60}$ thin films, due to its low solubility in solvents.[31] In the pinhole regions of type B devices the MAPbI$_3$ makes direct contact with the transparent electrode, fluorine doped tin oxide (FTO), as shown in Figure S8 in the Supporting Information. We have shown previously that devices with FTO/MAPbI$_3$ interfaces exhibit severe hysteresis and poor SPO.[3] The good SPO and $J_{mpp}$ for type B devices can thus be attributed to steady-state photocurrent being shunted around these pinhole regions. However, to achieve devices with both high SPO and low $J$–$V$ hysteresis it is important to ensure that MAPbI$_3$ does not make direct contact with the FTO.

The statistics of SPO and $J_{mpp}$ for all devices of the four architectures are shown in Figure 1b,c, respectively. The spread in stabilized efficiencies can be attributed to both batch-to-batch variations, as a result of the deposition optimization process, and also to variations in the quality of the spin coated ETLs and HTLs. Further details of the comparison between the SPO of regular and inverted devices are provided in Figure S2 (Supporting Information), and evidence that the HTL, Spiro-OMeTAD, does not contribute to the drop in the SPO is also presented in Figure S2 (Supporting Information). Thus by assessing such a large number of devices, we can confidently attribute the discrepancy that arise between the PCE and SPO in MAPbI$_3$ planar heterojunction solar cells to the choice of the ETL.

Having established that device SPO is affected by the ETL and its charge extraction efficiency, we now discuss the origins of the hysteresis effect. To achieve this, we investigated a set of devices with different ETLs in which the MAPbI$_3$ layer was deposited in the same deposition run. This enables us to study the interface and its effect on the perovskite independent of the perovskite composition or batch variations. Figure 2 presents a single batch of devices with identical perovskite layers and with differing ETLs, enabling us directly to compare the effect of different charge extraction layers. The specific ETL for each device was, c-TiO$_2$ for type A; both c-TiO$_2$ and a 50 nm layer of PCBM for type C$_{50 \text{ nm}}$; both c-TiO$_2$ and a 100 nm layer of PCBM for type C$_{100 \text{ nm}}$; and only a 50 nm layer of PCBM for type E. Figure 2a shows a cross-sectional scanning electron microscopy (SEM) micrograph of a type A device, where only c-TiO$_2$ is employed as an ETL. It reveals that the interface between c-TiO$_2$ and MAPbI$_3$ is poor with substantial low electron density (dark) regions. As will be discussed later, these low electron density regions are in fact regions of amorphous MAPbI$_3$ that result from a lattice mismatch between perovskite MAPbI$_3$ and FTO/c-TiO$_2$ layers. The amorphous MAPbI$_3$ at the interface leads to poor charge
collection efficiency, extensive charge recombination, and is likely to result in device hysteresis via an electrical capacitive effect across the amorphous region.\cite{32,33}

In contrast, with the introduction of a 50 nm layer of PCBM in between the c-TiO$_2$ and MAPbI$_3$ (type C$_{50}$ nm), as has been previously employed in solution-processed perovskite solar cells,\cite{34,35} there is a considerably improved interface between the MAPbI$_3$ and PCBM as shown in Figure 2b. However, the coverage of PCBM over the rough c-TiO$_2$ surface is not complete, hence regions of direct contact between the c-TiO$_2$ and MAPbI$_3$ exist. Consequently, the $J$–$V$ characteristics show some hysteresis even though the SPO is representative of the PCE. As shown before in Figure 2a, c-TiO$_2$/MAPbI$_3$ is not an ideal ETL for the MAPbI$_3$.

Doubling the thickness of the PCBM layer to 100 nm creates a pinhole-free layer which eliminates any regions of amorphous MAPbI$_3$ resulting from direct contact between MAPbI$_3$ and TiO$_2$. Hence an excellent interface is created for efficient electron extraction, and thus negligible hysteresis is observed (Figure 2c). Since the PCBM is deposited before the MAPbI$_3$, and there was no post-deposition annealing of these devices, it is unlikely that PCBM infiltrates between the grains. This indicates that the reduction in hysteresis, caused by PCBM, is a result of modifying the interface, rather than passivation of grain boundaries throughout the bulk. Therefore, to suppress hysteresis the ETL/MAPbI$_3$ interface incorporates an efficient electron extraction material that is free of pinholes. The features are exemplified in the type C$_{100}$ nm devices, while the 100 nm PCBM film is uniform and pinhole free, it is too thick to enable efficient device operation. This is evident by its considerably lower $J_{sc}$. As shown in type E devices, where there is only a thin layer of PCBM, there are areas at the interface where the perovskite makes direct contact with the FTO (Figure 2d). This is not ideal, as shown earlier with C$_{60}$, and causes $J$–$V$ hysteresis. Other studies have shown that the optimum PCBM thickness is around 10 nm.\cite{19}

The reason why PCBM needs to be so thin is not clear, since its electron mobility is at least as high as the hole mobility in Spiro-OMeTAD. It is likely however that it requires n-type doping in order to operate efficiently at thicknesses $>$10 nm.

Markedly, while the reverse sweep $J$–$V$ characteristics may not always represent the performance of the device under load, it always shows the potential of the device PCE and more specifically the MAPbI$_3$ thin film. Simply inserting a PCBM layer in the type A device to create a type C$_{50}$ nm device is a clear example of this. The type A devices show a reverse scan PCE of 10% and SPO of 2.7% (Table S2, Supporting Information). On the other hand, type C$_{50}$ nm shows an improved SPO of 12.4%, which closely represents the reverse sweep of the type A device. This is essential for troubleshooting the cause of low SPO and hysteresis observed in many perovskite devices. Modification of the interface rather than the perovskite itself should achieve a hysteresis-free device with an SPO representative of the PCE.

To gain a better understanding of the effect of the ETL on the morphology, composition, and crystal structure of the MAPbI$_3$ layer we performed TEM, high angle annular dark field (HAADF) imaging in STEM mode, and energy dispersive X-ray spectroscopy (EDX) on the type A and type C$_{100}$ nm devices. HAADF imaging is especially sensitive to atomic number (Z) contrast because heavier elements will scatter electrons at the high angles subtended by the HAADF detector. Consequently, bright regions will result from higher Z elements and in addition to denser regions while dark regions correspond to light elements and low density regions. The cross-sectional view of these devices reveals clear differences in the ETL/MAPbI$_3$ interface and the crystallinity of the perovskite layer. Figure 3a,e shows HAADF images of the type A and C$_{100}$ nm, devices, respectively. The main difference between the two is a dark contrast region between the MAPbI$_3$ and the FTO/c-TiO$_2$ layers in the C$_{100}$ nm EDX maps of the corresponding HAADF regions are shown in Figure 3b,f with a composite false color image of the elements Pb (green), C (red), and Sn (blue). The presence of Ti from the thin layer of c-TiO$_2$ is shown in Figure S3 (Supporting Information). In the case of the type C$_{100}$ nm (Figure 3e), the darker contrast observed in the HAADF image at the interface between the FTO and MAPbI$_3$ layers corresponds to a C rich layer, observed in the EDX map, which represents the continuous conformal PCBM layer (Figure 3f). TEM analysis of the whole sample reveals that in the case of the type A devices, there was variability in the crystallinity of the perovskite layer. Electron diffraction analysis of the perovskite layers shows diffuse ring patterns of the perovskite grain that clearly illustrates the presence of amorphous regions of MAPbI$_3$ within the perovskite layer (Figure 3d). This is further supported by the high-resolution transmission electron microscopy (HRTEM) image of the type A interface which shows some amorphous MAPbI$_3$ regions (Figure 3c, light contrast). In this HRTEM image the amorphous MAPbI$_3$ can also be seen to propagate away from the TiO$_2$ interface, deeper into the perovskite thin film. Conversely, the type C$_{100}$ nm devices show a more homogeneous nucleation (Figure 3g). Electron diffraction of the perovskite layers is consistent with a higher crystallinity as shown by the selected area diffraction patterns in Figure 3h. Furthermore, the HRTEM image of the interface (Figure 3g) clearly shows the high crystallinity of the perovskite layer and the FTO/c-TiO$_2$ layer interlaced with amorphous regions of the PCBM. Overall, the observation of amorphous MAPbI$_3$ when in contact with FTO/c-TiO$_2$ provides strong evidence for the origin of hysteresis and poor SPO observed in type A devices. It is also clear that with the presence of a conformal PCBM layer with good electrical contact to a high quality perovskite layer, there is little to no hysteresis with a high SPO, as shown by the type C$_{100}$ nm, devices. Furthermore, measurements from thermal admittance spectroscopy, suggest that the introduction of amorphous MAPbI$_3$ in combination of using TiO$_2$ as an ETL lead to an increase in trap density of states (Figure S4, Supporting Information). While hysteresis observed in perovskites based devices has been previously shown to be a combination of ion migration and the presence of interfacial trap states,\cite{16,6,8,16,17} it is clear from this particular study that interface morphology of the perovskite plays a significant role in $J$–$V$ hysteresis.

In conclusion, we have used an important advantage of the vapor deposition technique, whereupon a single batch of perovskite thin films have the same stoichiometry and thickness, to probe which particular interface is the cause of the hysteresis and deficient SPO. The results show that the quality of the interface between ETL and MAPbI$_3$, and the choice of ETL, is critical in suppressing hysteresis and reduced SPO. We observe amorphous regions of MAPbI$_3$ near the ETL.
interfaces of hysteretic devices with low SPO. We hypothesize that the poor electrical properties of the corresponding interface are a significant contributing factor affecting the device hysteresis. Therefore, the key to eliminating hysteresis from MAPbI$_3$ planar heterojunction solar cells is to develop a well-engineered interface between the perovskite layer and the (n-type) ETL. Ideally, the ETL should be an efficient electron extraction material with no pinholes, while the MAPbI$_3$ at the interface should be both homogenous and crystalline, such hysteresis-free devices have stabilized power outputs matching the power conversion efficiencies from single sweep $J$–$V$ measurements, and are promising for large-area renewable energy generation.

**Experimental Section**

*Device Fabrication:* Fluorine doped tin oxide coated glass substrates were first cleaned with Hellmanex, acetone, isopropanol, and ozone treatment. Different transport layers were then spin coated on to substrates. This was followed by coevaporation of PbI$_2$ and CH$_3$NH$_3$I under high vacuum ($1 \times 10^{-6}$ mbar). Post-deposition annealing times varied with different devices types except for the batch studies, where there was no post-deposition annealing. Transport materials were then spin coated on top of the CH$_3$NH$_3$PbI$_3$ (MAPbI$_3$) thin film. Silver electrodes were then thermally evaporated at ($1 \times 10^{-6}$ mbar) with a mask to create a device with a total active area of 0.0919 cm$^2$. Full details of techniques and materials used to create the different device architectures are provided in the Supporting Information.

*Current–Voltage Characterization:* The solar cells were measured under simulated AM1.5, 100 mW cm$^{-2}$ sunlight (1 sun), using an ABET Technologies Sun 2000 and a Keithley 2400 Sourcemeter in ambient conditions. The active area of each device was defined by a mask which exposed a 0.0919 cm$^2$ active area for testing of both the current voltage characteristics and stabilized power output. The devices were prebiased at 1.4 V for 5 s before initiating the reverse and forward scans. The scan rate was 0.38 V s$^{-1}$. Immediately after the $J$–$V$ measurements, the SPO was measured without prebiasing. The devices were kept at the voltage defined at maximum power, which was determined from the $J$–$V$ scans, for 50 s to measure the stabilized PCE and current density.

*Scanning Electron Microscopy:* Devices were sputter coated with a 3 nm conductive layer of Pt. Images were taken using a Hitachi S-4300 microscope.

*Transmission Electron Microscopy:* TEM samples devices were sub-100 nm thick lamella prepared by focused ion beam (FIB) using a Ga beam in an FEI Helios 600 NanoLab instrument. These samples were transferred onto a TEM carbon grid. TEM analysis was carried out in a JEOL2100F instrument operated at 200 keV and equipped with STEM capabilities and a silicon drift detector for EDX analysis.

**Supporting Information**

Supporting Information is available from the Wiley Online Library or from the author.

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