Effect of Minor Co Substitution for Fe on the Formability and Magnetic and Magnetocaloric Properties of the Amorphous Fe$_{88}$Ce$_7$B$_5$ Alloy $^{†}$

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Abstract: A small amount of Co was added to the Fe$_{88}$Ce$_7$B$_5$ glass forming alloy for the possibility of improving its glass formability and magnetocaloric effect. The Curie temperature of the amorphous Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ ($x = 0, 1, 2, 3$) ribbons increases linearly with the Co content, while the maximum magnetic entropy change ($-\Delta S_m^{peak}$) increases to 3.89 J/(kg K) under 5 T at $x = 1$ and subsequently decreases with further Co addition. The mechanism for the influence of Co addition on magnetic properties and the magnetocaloric effect of the amorphous alloys was investigated. Furthermore, a flattened $-\Delta S_m$ profile was designed in the amorphous laminate composed of the amorphous Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ ($x = 0, 1, 2$) ribbons. The high average $-\Delta S_m$ from ~287 K to ~320 K indicates the potential application perspective of the amorphous hybrid as a magnetic refrigerant of a domestic refrigerator.

Keywords: amorphous alloy; glass formability; Curie temperature; magnetic entropy change

1. Introduction

With the increasing shortage of energy and the worsening environmental pollution, it is vitally urgent to develop new refrigeration technology to replace the vapor expansion/compression refrigerators because the traditional refrigeration technology is of low refrigeration efficiency and is not eco-friendly. The magnetic refrigerators based on the magnetocaloric effect (MCE) of magnetic materials are regarded as one of the potential alternatives to the traditional refrigerators because of their energy conservation (at least 30%), eco-friendliness due to their free of ozone-depleting gases, and compactness due to the use of solid refrigerants [1,2].

The MCE refers to the heating of a magnetic material upon magnetization under an adiabatic condition induced by the decrease of magnetic entropy due to the ordering of magnetic moment [3]. Materials exhibiting excellent MCE are considered to be suitable for application as magnetic refrigerants. The magnetic refrigerator generally undergoes an Ericsson cycle, and thus the magnetic refrigerant should better exhibit a table-like magnetic entropy change ($-\Delta S_m$) profile within the working temperature range of a magnetic refrigerator [4]. However, the table-like $-\Delta S_m$ profile can hardly be achieved in a single alloy or compound; instead, it is usually achieved in composites composed of several alloys or compounds with Curie temperatures ($T_c$) ranging from the cold end ($T_{cold}$) to the hot end ($T_{hot}$) of a magnetic refrigerator [5–9]. Obviously, the broad $-\Delta S_m$ hump of the alloys...
experiencing 2nd-order magnetic phase transition (MPT) behavior rather than the narrow $-\Delta S_m$ peak of 1st-order MPT alloys, and the tunable Curie temperature of the alloys, are essential for constructing the table-like $-\Delta S_m$ profile.

Amorphous alloys (AAs) can perfectly match the above requirements, not only because they experience a 2nd-order MPT and exhibit a broadened $-\Delta S_m$ hump but also due to their tailorable $T_c$ within a wide temperature range by compositional adjustment [10–22]. The major challenge for the AAs to be used as magnetic refrigerants is how to enhance the $-\Delta S_m$ as much as possible. The rare earth (RE)-based AAs, typically the Gd-based bulk metallic glasses, show outstanding glass formability as well as rather large peak value of magnetic entropy change ($-\Delta S_m^{peak}$) at low temperature [10–12]. However, the RE-based metallic glasses are expensive, and the alloys with $T_c$ near room temperature (RT) usually show poor glass formability and low $-\Delta S_m^{peak}$ [13]. The transition metal (TM)-based metallic glasses with $T_c$ near RT are less expensive and can be easily fabricated, but their $-\Delta S_m$ peak values are very low. For instance, the Fe-Zr-B-based AAs show better MCE in the iron-based metallic glasses near the ambient temperature, but most of their $-\Delta S_m^{peak}$ are not higher than 3.2 J/(kg × K) under 5 T [14–17]. The minor substitution of Co for Fe can obviously improve the $-\Delta S_m^{peak}$ of the Fe-Zr-B amorphous ribbons to above 3.2 J/(kg × K) under 5 T, or even to about 3.4 J/(kg × K) under 5 T at 2% (at.%) Co, but they simultaneously enhance their Curie temperature to above 330 K, which is well higher than RT [18,19].

More recently, we successfully fabricated the Fe-La/Ce-B metallic glasses and achieved better magnetocaloric properties with $-\Delta S_m^{peak}$ of at least 10% larger than those of the Fe-Zr-B-based AAs near the ambient temperature [20,21]. In this paper, we selected a Fe$_{88}$Ce$_7$B$_5$ AA with a $-\Delta S_m^{peak}$ of ~3.83 J/(kg × K) under 5 T at 287 K [22] as a basic alloy and prepared the Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ (x = 1, 2, 3) amorphous ribbons. The effect of minor Co replacement for Fe on the glass formability, magnetic properties and MCE of the ternary amorphous alloy, as well as the mechanisms involved, was studied.

2. Materials and Methods

The master ingots with nominal Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ (x = 1, 2, 3) compositions were prepared one by one by arc-melting the mixture of raw materials several times using a non-consumable electrode in a high vacuum furnace (Physicence Opto-electronics, Beijing, China) filled with high-purity Ar. The ingots were manufactured to be the shape of ~40-µm-thickness ribbons under a high-purity Ar atmosphere by a melt-spinning method at a wheel surface speed of 50 m/s. The amorphous features of the as-spun Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ (x = 1, 2, 3) ribbons were ascertained by their X-ray diffraction (XRD) patterns measured by a Rigaku D\(\max-rC\) diffractometer (Rigaku, Tokyo, Japan) with Cu K$_\alpha$ radiation [23]. The glass formability of the amorphous ribbons was evaluated from the thermal properties obtained from their differential scanning calorimetry (DSC) traces measured by a NETZSCH 404C calorimeter (Netzsch, Selb, Germany) [24] at a heating rate of 20 K/min. The temperature and field dependence of magnetization curves were measured by a vibrating sample magnetometer (VSM), which is a module of a Physical Property Measurement System (PPMS, model 6000, Quantum Design, San Diego, CA, USA) [25]. The Arrott plots were derived from the isothermal magnetization ($M$-$H$) curves to confirm the type of phase transition. The $-\Delta S_m$ vs. temperature curves were constructed from $M$-$H$ curves according to the Maxwell equation. The $-\Delta S_m$ of the amorphous hybrid was calculated as

$$-\Delta S_m^{(hybrid)} = \sum_{i=1, 2, \ldots, n} w_i \times (-\Delta S_m)_i$$

where $w_i$ is the weight fraction of an amorphous ribbon.
3. Results and Discussion

The X-ray diffraction results of the as-spun Fe\textsubscript{88-\textit{x}}Ce\textsubscript{7}B\textsubscript{5}Co\textsubscript{\textit{x}} (\textit{x} = 1, 2, 3) ribbons are displayed in Figure 1a. The ribbons show smooth and broad diffraction humps, indicating that all the as-spun Fe\textsubscript{88-\textit{x}}Ce\textsubscript{7}B\textsubscript{5}Co\textsubscript{\textit{x}} (\textit{x} = 1, 2, 3) ribbons are amorphous. From the DSC traces of the three samples, as shown in Figure 1b, the endothermic glass transition hump and the exothermic crystallization peaks also ascertain the amorphous characteristics of these samples. Simultaneously, the onset temperatures of glass transition (\(T_g\)) and primary crystallization (\(T_c\)), as well as the liquid temperature (\(T_l\)) of the Fe\textsubscript{88-\textit{x}}Ce\textsubscript{7}B\textsubscript{5}Co\textsubscript{\textit{x}} (\textit{x} = 1, 2, 3) ribbons, are listed in Table 1. Therefore, two commonly used criteria for evaluating the glass formability of amorphous alloys, namely, the reduced glass transition temperature (\(\Delta T_g\)), and the parameter \(\gamma\) (defined as the ratio of \(T_{g} - T_{x}\)), can be calculated accordingly to be 0.421 and 0.368 for Fe\textsubscript{87}Ce\textsubscript{7}B\textsubscript{5}Co\textsubscript{1}, 0.426 and 0.361 for Fe\textsubscript{86}Ce\textsubscript{7}B\textsubscript{5}Co\textsubscript{2}, 0.437 and 0.360 for Fe\textsubscript{85}Ce\textsubscript{7}B\textsubscript{5}Co\textsubscript{3}. Compared to the Fe\textsubscript{88}Ce\textsubscript{7}B\textsubscript{5} ribbon, the minor Co substitution for Fe dramatically decreases the \(\Delta T_g\) and reaches a minimum at \(x = 1\) but obviously enlarges the supercooled liquid region (\(\Delta T_l = T_x - T_g\)), which makes the \(\gamma\) value reach a maximum at \(x = 1\), as illustrated in Figure 1c. Overall, both the \(T_{g}\) and \(\gamma\) of the Fe\textsubscript{88-\textit{x}}Ce\textsubscript{7}B\textsubscript{5}Co\textsubscript{\textit{x}} (\textit{x} = 0, 1, 2, 3) ribbons are in accordance with their glass formability: they can be quenched into amorphous ribbons easily but are not able to be vitrified into bulk amorphous samples.

![Figure 1](image_url)

Figure 1. (a) XRD patterns and (b) DSC curves of the Fe\textsubscript{88-\textit{x}}Ce\textsubscript{7}B\textsubscript{5}Co\textsubscript{\textit{x}} (\textit{x} = 1, 2, 3) as-spun ribbons; the inset is the melting behaviors. (c) The compositional dependence of \(T_{g}\) and \(\gamma\) for these amorphous ribbons.
Table 1. The thermal properties of the Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ ($x = 0, 1, 2, 3$) amorphous ribbons.

| Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ | $T_g$ (K) | $T_r$ (K) | $T_l$ (K) | $\Delta T_g$ (K) | $T_T$ | $\gamma$ |
|---------------------------|-----------|-----------|-----------|-----------------|-------|--------|
| $x = 0$                   | 647       | 761       | 1442      | 114             | 0.449 | 0.364  |
| $x = 1$                   | 606       | 753       | 1441      | 147             | 0.421 | 0.368  |
| $x = 2$                   | 613       | 740       | 1438      | 127             | 0.426 | 0.361  |
| $x = 3$                   | 627       | 743       | 1436      | 116             | 0.437 | 0.360  |

Figure 2a shows the hysteresis loops under 5 Tesla of the Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ ($x = 1, 2, 3$) glassy samples measured at 180 K and 380 K, respectively. All these samples show soft magnetic at 180 K and almost paramagnetic at 380 K, indicating that the ferromagnetic-paramagnetic transition occurs within 180 K and 380 K. The saturation magnetization is approximately 144.4 Am$^2$/kg for $x = 1$, 145.0 Am$^2$/kg for $x = 2$, and 144.0 Am$^2$/kg for $x = 3$, which implies the slightly fluctuation of the magnetic moment with the Co addition. The temperature dependence of magnetization curves for the Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ ($x = 1, 2, 3$) ribbons was measured under 300 Oe after a zero-field-cooling operation, as shown in Figure 2b. The $T_c$, which is obtained at the minimum of $dM/dT$, can be found to be 305 K for Fe$_{87}$Ce$_7$B$_5$Co$_1$, 323 K for Fe$_{85}$Ce$_7$B$_5$Co$_2$, and 346 K for Fe$_{83}$Ce$_7$B$_5$Co$_3$. Similar to the situation in the Co substituted Fe$_{88}$Zr$_8$B$_4$ amorphous ribbons [19], $T_c$ of the Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ ($x = 0, 1, 2, 3$) amorphous ribbons increases linearly with the Co content, as shown in the inset of Figure 2b, which is attributed to the enhanced 3d-3d interaction between 3d atoms by the Co addition [29]. As shown in Figure 3a for $x = 1$, Figure 3b for $x = 2$, and Figure 3c for $x = 3$, the magnetic phase transition of the Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ ($x = 1, 2, 3$) amorphous samples was confirmed to be 2nd-order MPT by the Arrott plots at various temperatures derived from their isothermal magnetization ($M$-$H$) curves (illustrated in the inset of Figure 3a–c, respectively).

The magnetic phase transition from ferromagnetic to paramagnetic usually results in the reduction of magnetic entropy due to the ordering of magnetic moments. Figure 4 illustrates the relationship between $-\Delta S_m$ and temperature ($(-\Delta S_m)$-$T$ curve) under various fields of the Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ ($a$) for $x = 1$, ($b$) for $x = 2$, and ($c$) for $x = 3$) amorphous ribbons. The three AAs show typical broad $-\Delta S_m$ hump of 2nd-order MPT materials, and the $-\Delta S_m^{peak}$ were observed near $T_c$ on each $(-\Delta S_m)$-$T$ curve. The $-\Delta S_m^{peak}$ under different fields of the ribbons are summarized in Table 2, accompanied with that of the Fe$_{88}$Ce$_7$B$_5$ amorphous ribbon for comparison purposes. It was found that $-\Delta S_m^{peak}$ of Fe$_{88}$Ce$_7$B$_5$AA was improved by adding 1% (at. %) Co but was decreased by adding more Co. As the
average magnetic moment of Co atoms is lower than that of the Fe atoms, the $-\Delta S_m^\text{peak}$ of the Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ (x = 0, 1, 2, 3) AAs should be generally decreased with the Co addition. The slightly increased $-\Delta S_m^\text{peak}$ at $x = 1$ may be induced by the extra 3$d$-3$d$ interaction between Co and Fe atoms [30].

According to the Arrott–Noakes equation, the relationship between the $-\Delta S_m$ and the external magnetic fields ($H$) in an amorphous alloy undergoing a 2nd-order magnetic transition can be expressed as $-\Delta S_m = A \times H^n$, where $A$ is a constant [31]. Figure 4d shows exponent $n$ vs temperature curves of the Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ ($x = 1, 2, 3$) glassy ribbons by linearly fitting $\ln(-\Delta S_m)$-$\ln(H)$ plots at various temperatures. As predicted by V. Franco [31], $n$ exponent of all the three samples is about 1 at low temperatures well below $T_c$, subsequently decreases to a minimum (about 0.75) near $T_c$, and finally approaches to a value of 2 at temperatures much higher than $T_c$. The values of $n$ near $T_c$ of these three samples, seen in the inset of Figure 4d, are 0.763 for $x = 1$ at 305 K, 0.758 for $x = 2$ at 322.5 K, and 0.756 for $x = 3$ at 347.5 K, all of which agree well with the results of other alloys undergoing a 2nd-order MPT [11,15–21] and indicate the typical magnetocaloric effect of these AAs.

**Figure 3.** The Arrott plots of the Fe$_{88-x}$Ce$_7$B$_5$Co$_x$ amorphous ribbons: (a) $x = 1$, (b) $x = 2$, and (c) $x = 3$, the insets are the isothermal magnetization curves of these ribbons under 5 T.
Table 2. $-\Delta S_m^{\text{peak}}$ and $T_c$ of some Fe-based amorphous alloys near room temperature.

| Composition                  | $-\Delta S_m^{\text{peak}}$ (J/(kg \times K)) | $T_c$ (K) | Ref. |
|------------------------------|-----------------------------------------------|----------|------|
| Fe$_{86}$Ce$_7$B$_5$Co$_2$    | 1.12, 1.54, 1.91, 2.60, 3.83, 3.93           | 287      | [22] |
| Fe$_{87}$Zr$_5$Cu$_1$        | 0.94, 1.28, 1.59, 2.16, 3.17, 3.78           | 1.7     |      |
| Fe$_{88}$Zr$_5$B$_3$         | 0.99, 1.35, 1.67, 2.26, 3.29, 3.94           | 304      | [15] |
| Fe$_{86}$Zr$_5$B$_3$         | 1.02, 1.39, 1.72, 2.34, 3.34, 3.94           | 327      |      |
| Fe$_{88}$Zr$_5$B$_3$         | 0.88, 1.20, 1.50, 2.06, 3.04, 3.94           | 291      |      |
| Fe$_{87}$Zr$_5$B$_3$         | 0.94, 1.29, 1.61, 2.19, 3.25, 3.94           | 306      | [16] |
| Fe$_{88}$Zr$_5$B$_3$         | 1.01, 1.38, 1.72, 2.34, 3.42, 3.94           | 333      | [18] |
| Fe$_{88}$Zr$_5$B$_3$         | 0.93, 1.29, 1.61, 2.24, 3.24, 3.94           | 317      |      |
| Fe$_{88}$Zr$_5$B$_3$         | 0.98, 1.35, 1.69, 2.31, 3.34, 3.94           | 340      |      |
| Fe$_{89}$La$_7$Ce$_5$B$_5$   | -     1.45, -          -               3.34, 3.64, 3.94 | 313      | [20] |
| Fe$_{88}$Zr$_5$B$_3$         | -     -    1.78, -               -            3.54, 3.64, 3.94 | 284      |      |
| Fe$_{88}$Zr$_5$B$_3$         | -     -    1.91, -               -            3.81, 3.94, 3.96 | 291      | [32] |
| Fe$_{88}$Zr$_5$B$_3$         | -     -    1.96, -               -            3.90, 3.96, 3.99 | 297      |      |
| Fe$_{88}$Zr$_5$B$_3$         | 1.03, 1.41, 1.76, 2.41, 3.55, 3.95           | 336      | [33] |
| Fe$_{88}$Zr$_5$B$_3$         | 1.04, 1.41, 1.73, 2.32, 3.38, 3.94           | 325      | [34] |
| Fe$_{88}$Zr$_5$B$_3$         | 1.09, 1.47, 1.81, 2.44, 3.55, 3.94           | 333      |      |
| Fe$_{88}$Zr$_5$B$_3$         | 0.87, - 1.47, 2.00, 2.93, 3.83, 3.94          | 283      | [35] |
| Fe$_{88}$Zr$_5$B$_3$         | -     -    1.8, -                -            3.18, 3.34, 3.53 | 334      | [36] |
| Fe$_{88}$Zr$_5$B$_3$         | 1.12, 1.42, -               -            3.59, 3.55, 3.77 | 355      | [37] |
Figure 5a shows the $-\Delta S_m^{peak}$ under 5 T of various iron-based metallic glasses with $T_c$ ranging from 280 K to 360 K (also listed in Table 2). The $-\Delta S_m^{peak}$ of the Fe(Co)-Ce-B glassy alloys are comparable to or even larger than those of most iron-based metallic glasses around RT [9,14–16,18–20,32–37]. For example, the $-\Delta S_m^{peak}$ of the Fe87Ce5B3Co1 amorphous ribbon (3.89 J/(kg × K) under 5 T) is comparable to that of the Fe83Ce11B6 glassy alloy [32], which is the largest among those metallic glasses. The $-\Delta S_m^{peak}$ of the Fe88Ce5B3Co3 amorphous ribbon, which is the lowest $-\Delta S_m^{peak}$ value among the Fe86Ce5B4Co2 ribbons, is still higher than the $-\Delta S_m^{peak}$ of most of those iron-based metallic glasses. On the other hand, it should be noted that the $T_c$ of Fe88Ce5B4 (287 K) and Fe86Ce5B4Co2 (323 K) glassy alloys are close to the $T_{cold}$ and $T_{hot}$ of a domestic air conditioner. Therefore, high $-\Delta S_m^{peak}$ of the Fe88-x-Ce7-xB5-Co3 metallic glasses allows us to construct a specific table-like $-\Delta S_m$ profile within temperature interval from 280 K to 320 K in an amorphous hybrid composed of these amorphous ribbons. Figure 5b displays the table-like ($-\Delta S_m$)-T curves under 1.5 T and 5 T for an amorphous laminate composed of 49% (wt.%) Fe88Ce5B5 + 2% (wt.%) Fe87Ce5B3Co1 + 49% (wt.%) Fe87Ce5B3Co2 glassy ribbons. The average $-\Delta S_m$ value ($-\Delta S_m^{average}$) of the amorphous laminate is about 1.28 J/(kg × K) under 1.5 T from 280 K to 315 K, and approximately 3.48 J/(kg × K) under 5 T from 287 K to 320 K; these values are much higher than those of other Fe-Zr-B-based amorphous hybrids [19,34]. Furthermore, the compositions of the amorphous laminate do not contain any radioactive elements and will not bring about some health hazards. Therefore, the high $-\Delta S_m^{average}$ from the $T_{cold}$ to the $T_{hot}$ of the amorphous composite indicates the potential application perspective as magnetic refrigerant in a domestic air conditioner.

4. Conclusions

In this work, the Fe88-x-Ce7B5-Co3 (x = 1, 2, 3) alloys were successfully fabricated to be about 40-μm-thickness amorphous ribbons, and the magnetic properties, as well as MCE of these glassy samples, were investigated. All the samples are soft magnetic at 180 K and paramagnetic at 380 K. The $T_c$ of the Fe88-x-Ce7B5-Co3 amorphous ribbons increases linearly from 287 K when $x = 0$ to 305 K when $x = 1$, 323 K when $x = 2$, and 346 K when $x = 3$, which is probably due to the enhanced 3d-3d interaction by the Co addition. The Arrrott plots as well as the $-\Delta S_m = A \times H^2$ relationship of the amorphous Fe88-x-Ce7B5-Co3 ribbons confirm the typical magnetocaloric behaviors of 2nd-order MPT alloys. The $-\Delta S_m^{peak}$ of these amorphous samples increases to 3.89 J/(kg × K) at $x = 1$ and subsequently decreases with further Co addition, which may be attributed to the compromise of two factors: the decreasing $-\Delta S_m^{peak}$ with Co addition due to the lower average magnetic moment of Co, and the slightly enhanced $-\Delta S_m^{peak}$ due to the introduction of extra 3d-3d interaction.

Figure 5. (a) $-\Delta S_m^{peak}$ of various Fe-based metallic glasses with $T_c$ ranging from 280 K to 360 K under 5 T; (b) table-like ($-\Delta S_m$)-T plots of the amorphous composite composed of Fe(Co)-Ce-B amorphous ribbons under 1.5 T and 5 T.
between Co and Fe atoms by Co substitution. Based on these results, an amorphous laminate with a table-like $-\Delta S_m$ profile from ~280 K to ~320 K was achieved by mixing 49% (wt.%) Fe$_{50}$Co$_{2}$B$_{2}$ + 2% (wt.%) Fe$_{50}$Ce$_{2}$B$_{2}$Co$_{1}$ + 49% (wt.%) Fe$_{50}$Ce$_{2}$B$_{2}$Co$_{2}$ amorphous ribbons. The high $-\Delta S_m$ *average* of the amorphous hybrid makes it a better candidate for application as a magnetic refrigerant in a domestic air conditioner.

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