A Silicon Carbide photonic platform based on suspended subwavelength waveguides

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Silicon Carbide (SiC) displays a unique combination of optical and spin-related properties that make it interesting for photonics and quantum technologies. Among its many polytypes, 3C and 4H-SiC are hosts of a large variety of point defects emitting in the visible and in the near infrared (NIR) \[1\]–\[4\]; these defects can be used as single photon sources and their spin state can be addressed through radio frequency and optical electromagnetic fields, while the coherence time has been shown to exceed milliseconds \[5\]–\[7\].

Photonic structures can enhance the interaction between these colour centres and light, providing a path for the development of a scalable approach for quantum technologies. Moreover, SiC provides interesting optical properties. Being non-centrosymmetric crystals, both polytypes of SiC possess a strong static second-order nonlinearity \(\chi^{(2)} \approx 60 \text{ pm/V for } 3C\)-SiC \[8\] and \(\chi^{(2)} \approx 32.8 \text{ pm/V for } 4H\)-SiC \[9\]); they do not suffer from two-photon absorption at telecommunication wavelengths due to their large electronic bandgap \(2.4 \text{ eV for } 3C\) and \(2.9 \text{ eV for } 4H\) \[10\]); as well as diamond, SiC is one of the hardest known materials \[11\], providing the mechanical stability required to support complex nanostructures at small scale, along with excellent thermal conductivity. Finally, SiC is known to be an established platform for high power microelectronics, making promising the integration of photonic and electronic devices on the same platform.

The fabrication of SiC for photonic applications, however, can be problematic. For example, few hundred nanometers of 3C-SiC can be grown heteroepitaxially on silicon (Si), but this poses two issues: i) having a higher index of refraction, the substrate prevents the use of total internal reflection (TIR) to obtain light confinement in the vertical direction; ii) due to crystalline mismatch, the interface between 3C-SiC and Si grows with very low quality, increasing losses of light travelling in such region. These two problems can be addressed at once by adopting wafer-bonding techniques \[12\]. On the other hand, the homoepitaxial growth of 4H-SiC provides high quality films, but obtaining thin membranes is not straightforward. Smart-cut process \[13\] can be applied to obtain SiC on insulator, but the ion implantation step increases optical losses and produces lattice damages detrimental to color center properties. Wafer bonding and thin down has demonstrated excellent material properties and low losses in photonic crystal cavities \[14\] and ring resonators \[15\]. However, the uniformity of the thickness of the SiC layer over appreciable chip sizes is a limiting factor for the scalability of SiC photonics.

An alternative approach is to suspend membranes in air, either removing part of the Si substrate, or by electrochemical etching of doped SiC. This approach has been used to produce photonic crystal cavities \[16\]–\[17\] as well as optical waveguides using a two-step lithography technique \[15\]. In this case, the first etch defines the lateral confinement of the waveguides, while the second one opens holes to access the substrate that has to be removed.

Here we propose subwavelength geometries that allow the use of a single etch step to access the substrate, simplifying the fabrication, as it has already been demonstrated for other platforms \[19\]–\[22\]. Subwavelength structures can be defined as periodic dielectric structures whose periodicity is much smaller than the wavelength of light; more rigorously, they are periodic structures where the energy of the photonic bandgap lies above the energy of the photons propagating in the medium. As such, they behave as an effective homogeneous medium (EHM) and they prevent the scattering of light \[23\]. Subwavelength structures can be used easily to obtain a complete photonic platform in SiC, capable not only to guide light, but also to realize ring resonators, grating couplers and slow-light

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waveguides.

In Section II, the design of the most basic component of the platform, a straight subwavelength suspended waveguide, is presented, followed by a discussion on the results of the numerical simulations which led to the choice of the dimensions of the waveguide. Then, we consider the amount of losses expected from the waveguide design, and we give an estimate of the nonlinear waveguide parameter. In Section III we assess the tolerance of the design to fabrication imperfections, in terms of the variation of the modal refractive index resulting from variation in the geometry of the waveguide. Section IV briefly introduces the analysis of additional photonic components and presents detailed results of numerical simulations used to design a uniform grating coupler. Section V describes how the platform can be adapted easily to reach a slow-light regime by changing the periodicity of the lateral suspending structures. Section VI discusses the performances of a proposed design for an electro-optical modulator integrated alongside the suspended waveguides. Finally, in Section VII we give the conclusions and perspectives.

II. SUBWAVELENGTH WAVEGUIDE

When a dielectric medium is periodic in one direction, the light travelling inside it can be described in terms of the photonic band structure [24]. The periodicity will produce the emergence of the photonic bandgap, a range of frequencies at which light cannot propagate in the medium. If the energy of the light is lower than the photonic bandgap, radiation can propagate, ideally without scattering, and the periodic medium acts as an EHM [23].

In Figure 1(a) we show the design of a SiC waveguide that exploits this principle to guide light at 1550 nm wavelength. The design is based on previous works realized in silicon on insulator (SOI) [20, 22] and germanium [21]. Light is confined in the vertical direction by TIR. The lateral arms serve two functions: to mechanically suspend the waveguide and to introduce the periodic perturbation. The perturbation has a periodicity that is much smaller than the wavelength of light, hence, similarly to a multilayer, the arms act as a homogeneous medium with index of refraction \( n_e \) intermediate between the one of SiC and air. Thus, for the case of the straight waveguide presented here, the structure is akin to the one shown in Figure 1(b), where the yellow region highlights the EHM; in practice, this confines light by TIR on the horizontal direction, as well.

The bulk effective index \( n_e \) of the subwavelength region can be tuned changing the filling factor (FF) of the arms \( f_{wg} \) in the periodic cell, and can be estimated by calculating the effective index of the light travelling normal to a SiC-air multilayer with the same periodicity and FF of the lateral arms [25]. The minimum feature size given by the fabrication process sets the constraints for \( f_{wg} \) and hence to \( n_e \). For our SiC structure we believe the higher limit on \( f_{wg} \) will be set by the resolution of the lithographic process, while the lower limit will be determined by the mechanical strength of the material. For instance, other structures in SOI [20, 22] were fabricated with a minimum dimension of the arms equal to 100 nm. Since SiC is a very hard material [11], it is reasonable to assume that the minimum dimension of the arms could be smaller than this value, but a more detailed analysis is required that takes into account not only the mechanical stability of the material but also the inner stress.

| Dimension          | Length [nm] |
|-------------------|-------------|
| Film thickness \((h)\) | 300         |
| Waveguide width \((w)\) | 650         |
| Periodicity \((a_0)\)  | 300         |
| Arm width \((u = f_{wg} a_0)\) | 150         |
| Arm length \((v)\)    | 2000        |

TABLE I. Proposed dimensions for a single TE-TM subwavelength waveguide. We assume a value of 2.6 for the index of refraction of SiC, suspension in air and vertical walls.

Aiming at the use of the waveguide’s fundamental TE mode, the dimensions of the proposed structure are listed in Table I. We assumed a value of 2.6 for the refractive index of the SiC layer since it is close to the refractive indexes of both 3C and 4H-SiC. Then, the layer thickness \((h)\) of 300 nm was chosen in order to have the fundamental slab mode close to the cut-off condition. The periodicity of the structure \((a_0)\) is set by the subwavelength condition: the continuous lines of Figure 2 are the band structure of our subwavelength waveguides calculated using MPB - MIT Photonic Bands [26]; choosing a periodicity of 300 nm puts the TE bandgap well above the energy of 1550 nm radiation, ensuring the suppression of scattered light and the validity of the EHM approximation.

We have chosen \( f_{wg} \) equal to 0.5, which provides \( n_e \) equal to 2.144, a good compromise between a higher lateral confinement and a high mechanical strength; the lateral arms are thus 150 nm long \((u)\) in the propagation direction. The proposed waveguide’s width \((w)\) of 650 nm is the one that maximizes the confinement of the fundamental mode while maintaining the structure single-TE-mode. In fact, the structure sustains a single TM mode \((TM_{00})\) and two TE modes \((TE_{00} \ and \ TE_{01})\); the \( TE_{01} \) mode is very loosely bound and is likely to experience very high losses compared to the \( TE_{00} \) mode, since it would be easily coupled to radiative modes.

The mode profiles have been simulated both with the MPB simulation suite and with a numerical eigensolver (Lumerical MODE). In Figures 1(c), 1(d) and 1(e) we show the profiles of the TE and TM modes calculated with the eigensolver, under the EHM approximation for the lateral arms, which agree very well with the ones obtained from MPB. Although not perfectly, the dispersion of the three modes calculated from the eigensolver (the
FIG. 1. a) Scheme of the proposed design of a SiC suspended waveguide. The SiC film is 300 nm thick and sits on top of a Silicon substrate. The central branch (650 nm wide) is supported by the lateral arms, which have a longitudinal periodicity of 300 nm and dimensions of 2 µm × 150 nm. b) The arms act as an effective uniform medium (yellow) and contribute to guide light by total internal reflection. c-e) Electric field intensity profiles of the TE\textsubscript{00}, TE\textsubscript{01} and TM\textsubscript{00} modes.
roughness couples light from the guided modes to radiative modes \cite{27,28}. With respect to traditional ridge waveguides, we expect this effect to be slightly higher due to the presence of the additional material interfaces corresponding to the arms. Still, if needed, the effect of roughness can be counteracted by increasing the width of the central branch \((w)\), which increases confinement, at the expense of the introduction of additional guided modes. Disorder in the periodicity or in the position of the lateral arms also increases losses and has to be kept to low enough values. As shown in ref. \cite{29}, where these effects are studied on a similar structure to the one considered here, the jitter in the position and dimension of periodic structures should not exceed 5 nm to keep losses to a reasonable level. Choosing a working point far below the bandgap can decrease the effect of disorder.

We now consider the nonlinear optical properties of the system. In particular, we estimate the nonlinear waveguide parameter \(\gamma\) for the nominal waveguide design. For uniform waveguides, \(\gamma\) can be defined in terms of the nonlinear Kerr index \(n_2\) and of the Poynting vector \(\mathbf{P}\) \cite{30}, according to

\[
\gamma = \frac{k_0}{a_0} \int_{z}^{z+a_0} \gamma(z) \, dz = \frac{k_0}{a_0} \int_{z}^{z+a_0} \frac{n_2(x,y,z) P_z(x,y,z)^2 \, dx \, dy}{|\int P_z(x,y,z) \, dx \, dy|^2} \, dz
\]

where \(n_2(x,y,z)\) is assumed equal to \(5.31 \cdot 10^{-19} \text{ m}^2/\text{W}\) \cite{18} where \((x,y,z)\) is found within the SiC structure and zero otherwise. Using the Poynting field calculated from MPB, we find \(\gamma = 7.346 \text{ W}^{-1} \text{m}^{-1}\). The nonlinear waveguide parameter is calculated also using Lumerical and the EHM approximation, obtaining \(\gamma = 6.182 \text{ W}^{-1} \text{m}^{-1}\); in this case, the presence of the lateral arms is taken into account by assuming that the nonlinear index of the homogeneous medium is the average of the ones of SiC and air (i.e. equal to \(n_2/2 = 2.655 \cdot 10^{-19} \text{ m}^2/\text{W}\)). By comparison, in ref. \cite{18} the nonlinear waveguide parameter of slightly lesser confining SiC waveguides was measured to be \(\gamma = 3.86 \pm 0.03 \text{ W}^{-1} \text{m}^{-1}\), while the one of typical Silicon Nitride waveguides is close to \(2 \text{ W}^{-1} \text{m}^{-1}\) \cite{32}.

III. TOLERANCE

In order to determine the tolerance of the design to fabrication, we simulated the subwavelength waveguide varying its geometry; in particular, we considered variations in the cross-section and in the filling factor of the arms, and we monitored the change in the effective index along the propagation, we average the nonlinear waveguide parameter along a single periodic cell, following the approach described in ref. \cite{31}:

\[
\gamma = \langle \gamma(z) \rangle = \frac{1}{a_0} \int_{z}^{z+a_0} \gamma(z) \, dz = \frac{k_0}{a_0} \int_{z}^{z+a_0} \frac{n_2(x,y,z) P_z(x,y,z)^2 \, dx \, dy}{|\int P_z(x,y,z) \, dx \, dy|^2} \, dz
\]

where \(n_2(x,y,z)\) is assumed equal to \(5.31 \cdot 10^{-19} \text{ m}^2/\text{W}\) \cite{18} where \((x,y,z)\) is found within the SiC structure and zero otherwise. Using the Poynting field calculated from MPB, we find \(\gamma = 7.346 \text{ W}^{-1} \text{m}^{-1}\). The nonlinear waveguide parameter is calculated also using Lumerical and the EHM approximation, obtaining \(\gamma = 6.182 \text{ W}^{-1} \text{m}^{-1}\); in this case, the presence of the lateral arms is taken into account by assuming that the nonlinear index of the homogeneous medium is the average of the ones of SiC and air (i.e. equal to \(n_2/2 = 2.655 \cdot 10^{-19} \text{ m}^2/\text{W}\)). By comparison, in ref. \cite{18} the nonlinear waveguide parameter of slightly lesser confining SiC waveguides was measured to be \(\gamma = 3.86 \pm 0.03 \text{ W}^{-1} \text{m}^{-1}\), while the one of typical Silicon Nitride waveguides is close to \(2 \text{ W}^{-1} \text{m}^{-1}\) \cite{32}.

FIG. 2. Simulated band structure of the proposed suspended waveguide along the propagation direction. Assuming \(a = 300 \text{ nm}\), the horizontal black line corresponds to 1550 nm. Orange and light blue lines correspond to guided TE and TM modes respectively, calculated with the MIT MPB simulation suite \cite{26}; red and blue dots are the same modes calculated with a numerical eigensolver; dashed red and blue lines are effective horizontal TE and TM light-lines calculated from an effective index approach.
FIG. 3. Simulations of the effective index $n_{TE}$ of the waveguide’s fundamental TE$_{00}$ mode as a function of the cross-section of the central waveguide. a) Variation of $n_{TE}$ in terms of the waveguide width ($w$). b) Variation of $n_{TE}$ in terms of the waveguide height ($h$). Continuous lines: MPB - Dashed lines: Numerical.

dis this platform, once the difference in the effective index given by the two simulation methods is taken into account.

IV. PHOTONIC COMPONENTS

A whole range of additional structures can be easily realized under the EHM approximation for the lateral arms region. We can apply standard photonic design and simulation tools to obtain, for example, tapers and bends. In order to avoid losses introduced by periodicity mismatch, the arms in bent sections have to maintain their mutual spacing as close as possible to the nominal value of the straight waveguide. Again, simulations of the structures with FDTD methods confirmed the expected behaviour of the devices.

Efficient coupling of light into the suspended waveguide can be achieved using grating couplers. On this matter, different designs that exploit subwavelength structures have been proposed [33-35]. Briefly, the subwavelength arms, in this case, are used to define the effective index for the subwavelength grooves of the grating coupler and thus are oriented along the propagation direction, as shown schematically in Figure 4.

Table II lists the dimensions for a uniform grating coupler with simulated -3.8 dB maximum coupling efficiency, designed for TE radiation incoming at an $8^\circ$ angle to normal incidence. For the subwavelength grooves we chose a (transversal) periodicity $b_T$ and filling factor $f_{\text{grat,}T}$ of 300 nm and 0.5, respectively, which give an effective index $n'_e$ for the grooves equal to 1.110. At variance with the bulk effective index of the lateral arms, these values were obtained numerically, simulating the effective index of the mode travelling in the slab and applying periodic boundary conditions in the lateral direction. Thus the value of $n'_e$ for $f_{\text{grat,}T} = 1$ would correspond to the effective index of the fundamental mode of the SiC slab suspended in air (2.134).

| Film thickness | 300 nm |
|----------------|--------|
| Longit. period ($b_L$) | 1230 nm * |
| Longit. FF ($f_{\text{grat,L}}$) | 32.4% * |
| Number of periods | 13 |
| Transv. period ($b_T$) | 300 nm |
| Transv. FF ($f_{\text{grat,T}}$) | 50% |
| Transv. length | 12 µm |
| Max. transmission: | 41.8% (-3.8 dB) |
| 1 dB bandwidth: | 75 nm |

TABLE II. Proposed dimensions and properties for a TE SiC subwavelength grating coupler operating around 1550 nm. The index of SiC is assumed to be 2.6. The values marked with * are obtained by numerical optimization.

Following the design method described in ref. [33], the values marked with * in Table II are obtained by numerical 3D FDTD optimization (having maximum transmission at 1550 nm as target and exploiting periodic boundary conditions in the transverse direction); they are very close to the values obtained from the simplest analytic descriptions of the uniform grating coupler:

$$l_1 = \frac{\lambda_0}{2(n_1 - n_c \sin \alpha)}; \quad l_2 = \frac{\lambda_0}{2(n_2 - n_c \sin \alpha)},$$  

(4)
where \( l_1 \) and \( l_2 \) are the longitudinal dimensions of the low- and high-index sections of the grating (so that \( b_L = l_1 + l_2 \) is the grating period and \( f_{\text{grat},L} = l_2/(l_1 + l_2) \) is the grating longitudinal filling factor), \( \lambda_0 \) is the vacuum wavelength of light, \( \alpha \) is the angle to normal incidence, \( n_1 \) and \( n_2 \) are the low and high effective indexes of the light travelling in the grating, and \( n_c \) is the index of the surrounding material. In our case \( n_1 \) and \( n_2 \) are equal to 1.110 and 2.134, while \( n_c \) is the index of air (1.0). This gives \( b_L = 1187 \text{ nm} \) and \( f_{\text{grat},L} = 32.7\% \).

Figure 5 shows the transmission of the grating as a function of the wavelength, obtained from 3D FDTD simulations; The 1 dB bandwidth is 75 nm large, ranging between 1511 nm and 1586 nm. At the expense of the bandwidth, apodised designs can be employed to increase the maximum coupling efficiency.

\[
\text{PF} = \frac{3\pi c^3 a}{V_{\text{eff}} \omega_0 \epsilon^{3/2} \nu_g} \tag{5}
\]

where \( \omega_0 = 2\pi c/\lambda_0 \) is the frequency of light at the working point, \( \epsilon^{1/2} = n_{\text{SiC}} \) is the refractive index of SiC and \( v_g \) is the group velocity of light; the effective volume \( V_{\text{eff}} \) is given by

\[
V_{\text{eff}} = \frac{1}{\max(\epsilon(\mathbf{r}) |\mathbf{e}(\mathbf{r})|^2)} \tag{6}
\]

where \( \epsilon \) is the modal electric field traveling in the waveguide, \( \epsilon(\mathbf{r}) \) is the dielectric function that defines the periodic structure and where \( \mathbf{r} \) is allowed to vary on the periodic cell. Figure 6 also reports the enhancement of PF (i.e. \( \text{PF}(a)/\text{PF}(a_0) \)), where \( a \) is the increased periodicity compared to the nominal periodicity \( a_0 \), showing that it is mainly induced by the increase of group index.

A transition region between nominal and slow-light regimes can be realized easily by changing adiabatically the periodicity of the waveguide. Since the field profiles of the different regions are very similar, there is no need to modulate the waveguide width to spatially match the two modes, which has been shown to be a key aspect to obtain low insertion losses [36]. Yet, as discussed previously, the closeness of the photon energy to the photonic bandgap would make the system more sensitive to disorder and the fabrication more challenging, and will likely set the limitation of the slow-light operation.

The achievement of modest PF can benefit the field of quantum technologies based on color centres embedded in SiC. For example, the emission rate of the silicon vacancy (SiV) center is limited by the non-radiative decay from the excited state to a metastable state [39]. Moreover, the collection efficiency in confocal microscopy setups is hampered by the high refractive index due to TIR. A
moderate PF would increase the radiative rate to values sufficient to accomplish quantum non-demolition readout of the spin state.

VI. ELECTRO-OPTIC MODULATORS

Active modulation of light travelling inside SiC can be performed with electro-optic modulators that exploit the high $\chi^{(2)}$ nonlinearity of the material. Assuming that the bottom surface of the structure is not accessible, the modulator could be realized by patterning two metallic pads to the sides of the suspending arms’ region. In order to give an estimate of the performance of the device, we model the two pads as a parallel plate capacitor with 6 $\mu$m spacing and centered on the SiC waveguide [40], so that the overlap between the driving and optical fields is equal to unity. Since the index of refraction of the material $n = \sqrt{1 + \chi^{(1)}}$ is modified by an applied electric field $E$ according to

$$n(E) = \sqrt{1 + \chi^{(1)} + 2\chi^{(2)}E} \approx n + \chi^{(2)}E,$$

the standard voltage-length figure of merit for a $\pi$ phase shifter is given by

$$L_{\pi}V_{\pi} \approx \frac{\lambda l}{r n^3},$$

where $l$ is the distance between the capacitor plates and $r = 2\chi^{(2)}/n^4$ is the electro-optic coefficient of the waveguide material. Assuming $n = 2.6$, $\lambda_0 = 1550$ nm, $l = 6$ $\mu$m, $\chi^{(2)} = 32.8$ pm/V, then $r = 1.43$ pm/V and $L_{\pi}V_{\pi} \approx 36.9$ V $\cdot$ cm; this performance can be improved by a factor 2 by implementing an amplitude modulator based on a Mach-Zehnder interferometer driven by pads in the ground-signal-ground configuration, reducing $V_{\pi}L_{\pi}$ down to 18.4 V $\cdot$ cm. This value is about one order of magnitude higher than the one of state of the art electro-optic modulators based on Lithium Niobate [41] ($r_{33} \approx 30.8$ pm/V [25]) which use similar spacing between the pads [42]. As for other platforms, it is conceivable to improve the performance of electro-optic modulators using resonant structures like microring resonators [43]. We also confirmed that the pads induce negligible losses: a numerical simulation of the optical mode propagating alongside gold pads spaced by 6 $\mu$m and placed outside the arms’ region results in about 2 dB/m losses.

VII. CONCLUSIONS

In this work we proposed a scalable photonic platform based on SiC that allows coupling of electromagnetic radiation into and out of a SiC thin film, and that allows the manipulation of the electromagnetic field in the material. This platform, based on suspended subwavelength waveguides, is flexible enough to allow the realization of all the basic photonic components such as waveguides, bends, directional couplers, grating couplers and tapers. The proposed design requires a single etch step to access the substrate and to define the geometry of the devices, simplifying the fabrication process with respect to other previous SiC suspended platforms: despite this, the platform retains a powerful design flexibility, because the duty cycle of subwavelength sections can be different in different parts of the sample. As explained, an increase in the periodicity allows to reach a slow-light regime, which can be used to increase the linear and nonlinear interaction of light with SiC nonlinearities or color centers therein. For instance, this effect can be used to shorten the length of superconducting nanowires or electro-optical modulators integrated alongside the suspended waveguides.

Since SiC is very hard, compared to other subwavelength platforms realized in other materials such as Si and germanium, we believe that the lateral suspended structures can be very thin, hence allowing subwavelength regimes for shorter wavelengths than previously demonstrated. Reaching a periodicity shorter than 280 nm would allow the propagation of 1100 nm light, which in turn enables the interaction with NIR defects in SiC. Quantum optics applications would then become feasible. This, together with the increase of the $\beta$ factor given by slow-light could make this platform appealing for both 3C- and 4H-SiC. An even shorter periodicity of 200 nm would allow the guided propagation of 785 nm radiation, the second harmonic of 1550 nm; provided that the overall losses of the platform, given not only by the material but also by roughness and disorder, can be kept low enough, squeezing on an integrated, scalable platform would become a concrete and promising application.

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