Sustainability of biodiesel production in Malaysia by production of bio-oil from crude glycerol using microwave pyrolysis: a review

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ABSTRACT

Biodiesel being one of the most promising renewable biofuels has seen rapid increase in production capacity due to high demand for diesel replacement; along with oversupply of its by-product, crude glycerol. Developing new industrial usage for glycerol is essential to defray the cost and sustainability of biodiesel industry and to promote the biodiesel industrialization. One of the approaches is by the transformation of glycerol into a liquid, referred as bio-oil through pyrolysis technology. Bio-oils produced by pyrolysis processes can be upgraded to produce transportation fuels or for power generation. However, current state of pyrolysis technologies are still major hurdles their development with respect to its commercial applications. Recently, microwave technology has attracted considerable attention as effective method for significantly reducing reaction time, improving the yields and selectivity of target products. Hence, this review strives extensively towards addressing the application of microwave-assisted technology applied to the pyrolysis process as a way of cost-effective and operationally feasible processes to directly utilize crude glycerol. The present review will focus on the pyrolyzed liquid product (bio-oil) derived by employing the microwave-assisted pyrolysis method. This review concludes that microwave-assisted glycerol conversion technology is a promising option as an alternative method to conventional glycerol conversion technology.

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1. Introduction

Every aspect of modern society runs on energy. The conventional oil and natural gas resources are a valuable supply of energy; however, they are finite resources that contribute to greenhouse gas emissions as well as air pollution. Carbon dioxide (CO2) is the primary greenhouse gas emitted through human activities. Between 1990 and 2015, there has been an increase in CO2 emissions corresponding with increased energy use by an expanding economy and population, an overall growth in emissions from electricity generation, and increased demand for travel (1). Energy efficiency and conservation, as well as decarbonizing the energy sources, are a prerequisite for sustainable development. Reducing carbon emissions is very crucial to mitigate the significant climate-change risks posed by greenhouse gas emissions. The most effective way to reduce CO2 emissions is to reduce fossil fuel consumption. The first years of the twenty-first century have witnessed remarkably rapid growth in the production and consumption of renewable energy. Despite the significant growth in the...
use of renewable energy, reducing carbon emissions on the timescale is necessary to mitigate the significant climate-change risks (2). In developed societies, energy demands are however so high that renewables with limited supply potential such as geothermal or hydro will be able to meet only a small proportion of future global energy demands. The largest contribution will have to come from wind, ocean, and solar sources. However, wind, ocean, and solar projects have limited lifetimes and if applied globally, they might consume a remarkable share of construction materials. Although such renewables may reduce CO2 emissions’ footprint of the energy sector, on the other hand they may increase the CO2 footprint of the industrial sector, where the production of these construction materials creates additional CO2 emissions (3). In addition, nuclear is also a proven technology and can play an important role in a low-carbon strategy. Although the nuclear power plants do not release CO2 emissions, they generate highly radioactive spent nuclear fuel. The disposal of the generated radioactive waste, especially high-level ones, remains a major concern for society around the world (4). To overcome these challenges, a viable option is biofuels, which have been receiving increasing attention because of being a neutral carbon source (5). Biofuels have the ability to reduce about 41% CO2 emissions, have better engine performance due to complete combustion, require no modifications to diesel engine usage, and low price, which make them an environmentally friendly diesel replacement (6). Biodiesel is outstanding among the biofuels, and has become widely acceptable in the energy market owing to its unique features including higher cetane number, lack of sulfur, inherent lubricity, positive energy balance, higher flash point, non-toxicity, and high biodegradability (7,8).

In Malaysia, to date, all of the established biodiesel production chains are using palm oil as primary feedstock. As a second largest producer and exporter of palm oil in the world, Malaysia accounts for 40% of total global palm oil produced annually. Palm oil has high potential because of its high yield per hectare and high oil content over other oils crops (9). Considering the comparative yields of various oil bearing crops, oil palm is clearly the most efficiently produced oil in the world today. When the world is looking at vegetable oils as renewable fuel, palm oil will undoubtedly stand out among other vegetable oils. In 2011, the total biodiesel production in Malaysia was 170,000 tons, which constitutes only 6% of the total capacity of 2.7 million tons from 23 biodiesel plants (10). Several issues in the Malaysian biodiesel industry have led to its underperformance such as lack of processing facilities. New facilities need to be installed in order to further develop biodiesel capacity and at present, the government is providing subsidies for the construction of additional facilities in existing refineries. The major hindrance to propping up the biodiesel production in Malaysia is the fuel subsidies given by the government for fossil fuels, which hamper the technology development and the market competitiveness of biodiesel. However, since 2012 the subsidies on petroleum fuel were gradually removed under the subsidy rationalization policy. This had somewhat created better price competitiveness for biodiesel. The Government’s latest commitment in its biodiesel mandates can be seen as an attractive investment venture for oil palm planters, which already have the main feedstock for the production of biodiesel. It may not be surprising to see a trend among cash-rich plantation companies lately to acquire “idle” biodiesel plants in Malaysia. These acquisitions will take place as plantation companies are beginning to realize that biodiesel can provide a safe avenue and act as a good buffer to support the crude palm oil price in case of oversupply. In spite of the attractiveness, the Malaysian palm oil biodiesel industry faces disadvantages regarding duties. Malaysian biodiesel and palm oil are subject to 30% export duties, whereas Indonesia imposes only a 2% export duty on biodiesel and 16.5% export duty on palm oil (10). This (export duty) disadvantage has contributed to Malaysia’s drop in ranking among other palm oil producers, such as Indonesia, Thailand, and Colombia, which are more competitive biodiesel producers. Other challenges include problems faced during pre-processes, and during post-processes (waste problem). Problems will arise when the feedstock is too expensive compared to the processing cost itself. As high as 75–90% of the total biodiesel production cost is actually used for purchasing the required raw materials alone. There will be significant challenges to the biodiesel industry when the demand for feedstock fluctuates and destabilizes the market. Another arising issue is the waste glycerol problem. It is estimated that approximately for every 100 kg of biodiesel produced, 10 kg of glycerol is generated as a by-product (11,12). The abundance of waste glycerol generated from the biodiesel industry not only affects the cost of the biodiesel production but it also severely creates an environmental issue (13). A more sustainable biodiesel production can be achieved if the waste glycerol could be utilized in a more effective way such as conversion to a value-added product. The world scenario of biodiesel production as shown in Figure 1 predicts that by 2020 the global production of glycerol will reach 4.0 billion liters. Thus, crude glycerol disposal and its utilization have become a serious issue and a financial and environmental liability for the
biodiesel industry (14). Thus, waste glycerol abundance is a problematic issue in biodiesel production at present. The market value of pure glycerol was US cent 19.4–20.1 per liter in 2014 (15) and almost close to US cent 12.01–15.03 per liter of crude glycerol. The current and the projected market values of glycerol up to 2020 are expected to remain within this range (16). A marginal (2–5%) increase in the price in 2020 may be expected if there are new demands for vegetable oil-based glycerol as continuous research is being carried out to find new applications for crude glycerol. New applications for glycerol must be found to avoid the continuous fall of glycerol prices. Added to that is the fact that crude glycerol generated from biodiesel production is impure; purification of crude glycerol is needed to remove impurities in order to meet the requirements of the existing and emerging usage. The conventional techniques for purification of crude glycerol for reuse are cumbersome and too costly (17).

Over the past few years, the development of products from biomass through the pyrolysis technique has been intensively investigated. Pyrolysis technology has attracted more interest in producing liquid fuel product, known as bio-oils, because of its considerable advantages of being storable, transportable, and versatile in applications such as combustion engines, boilers, and turbines. However, it is still at an early stage of development and needs to overcome a number of technical and economic barriers to compete with traditional fossil fuel (18). The development of more advanced technologies is the next challenge for pyrolysis researchers to achieve this target. The ultimate goal of this technology is to produce high-quality bio-oil, which is able to compete with and eventually partially replace the non-renewable fossil fuels for direct use in micro gas turbines for power generation, and other sustainable products such as bioplastics and platform chemicals. Many researches are interested in the application of microwave irradiation, not only due to its ability to enhance the reaction rates and rapid heating, but also for its ability to revolutionize the chemical reactions bringing about products and reactions’ performance with unexpected results (19–21). Among the important benefits of microwave-assisted reactions are rapid heating, lower relative energy consumption, environmental friendliness, higher production yield, controllable processing, shorter processing time, and quality and properties’ improvement. Hence, the production of bio-oil is another promising use of glycerol since waste glycerol is difficult and costly to manage which also gives impetus to pyrolysis research. The aim of this review paper is to emphasize the principles of microwave-assisted pyrolysis and to show recent research on the application of this technology for waste glycerol.

2. New opportunity for the usage of crude glycerol

Crude glycerol from biodiesel plants has low economic value and is not pure enough for direct use in many applications, due to the presence of various impurities. The problem with crude glycerol from biodiesel production is that it has heavy contamination from toxic methanol and has a high salt and free fatty acids (FFA) content and a substantial color (yellow to dark brown). The impurities present in crude glycerol significantly affect its properties and thus its conversion to value-added products. Another major challenge for the utilization of crude glycerol is the inconsistency in its composition since it varies with the feedstock and production procedures (22). This makes crude glycerol unsuitable for most traditional glycerol markets. Many studies have reported various methods to purify crude glycerol; among them are vacuum distillation, ion exchange, membrane separation, and activated carbon adsorption whereby each of the purification techniques uses different properties of crude glycerol. The conventional techniques for purification of crude glycerol are energy extensive, too costly, cumbersome, and economically unavailable for the biodiesel producers (23–27). The crude glycerol must be purified before it can be used in food and pharmaceutical applications. Traditional Oleochemicals refiners cannot use the crude glycerol from the biodiesel industry, even at 80% purity, because it would damage expensive pipes and storage equipment. Prior to use, it must be refined to an acceptable purity level at dedicated refineries and then sold at low price as “technical-grade” refined glycerol [Technical grade – used as a building block in chemicals, not for food or
Glycerol has a large number of applications in varied fields; however, the current market cannot accommodate this large volume of crude glycerol coming from biodiesel industry. In the last 10 years, the world has seen a rise in usage of bio-glycerol as chemical ingenuity was rapidly opening the route to glycerol derivatives for use in fields as diverse as fuels, chemicals, pharmaceuticals, detergents, and the automotive and building industries. Table 1 presents a summary of the main applications of crude glycerol.

### 3. Utilization of biodiesel derived from waste glycerol for value-added products

Glycerol has a large number of applications in varied fields; however, the current market cannot accommodate this large volume of crude glycerol coming from biodiesel production, which needs further costly purification steps. For these commercial applications, the quality of glycerol must be improved until it has an acceptable purity (>98%) (38). The other viable solution for the residual glycerol from biodiesel production is for the synthesis of value-added chemicals or materials of industrial importance. From a technical standpoint, the multifunctional structure and properties of glycerol allow for its utilization by several different reaction pathways. Driven by the motivation to search for alternative and sustainable ways of utilizing crude glycerol, many researchers are looking at the production of valuable end products or intermediate feedstock for the production of new classes of renewable biofuels and important platform chemicals. The production of sustainable products, which can replace petroleum-based products, will ultimately extend the utilization of renewable resources for a sustainable environment. Generally, biomass can be transformed into many useful forms by thermochemical and biochemical conversion. In thermochemical conversion pathways, heat and chemical catalysts are used for the production of energy from biomass, while biochemical conversion pathways use biological organisms and biological catalysts for the transforming of biomass into energy and value-added products (24). For instance, combustion, gasification,
and pyrolysis are known as the main thermochemical conversion pathways, while fermentation and anaerobic digestion are the most common biochemical conversion pathways. The crude glycerol utilization in microbial fermentation has been studied extensively and many excellent reviews have been published in the last 15 years, and can be referred to for further information (25–27,60,61).

3.1. Thermochemical conversion of crude glycerol: gasification and pyrolysis

Waste glycerol is abundantly available and can be utilized effectively by using appropriate technologies, for use as a renewable resource for energy and other chemicals’ production. Three different thermochemical conversion routes are found according to the oxygen content in the process: combustion (complete oxidation), gasification, (partial oxidation), and pyrolysis (thermal degradation without oxygen). Among them, combustion (also called incineration) is the most established route in industry but this is also associated with the generation of carbon oxides, sulfur, nitrogen, chlorine products (dioxins and furans), volatile organic compounds, polycyclic aromatic hydrocarbons, and dust. On the contrary, gasification and pyrolysis offer the potential for greater efficiencies in energy production and less pollution. Although pyrolysis is still under development in the waste industry, this process has received special attention, as not only a primary process of combustion and gasification, but also as an independent process leading to the production of energy-dense products with numerous uses.

Gasification refers to the thermochemical decomposition of organic material under high temperatures (>800°C) to produce a mixture of hydrogen, carbon dioxide, carbon monoxide, methane, and light hydrocarbon gases, termed as syngas, or producer gas. Crude glycerol has been frequently used as an additive in the gasification of biomass to improve gas yields and the hydrogen fraction of the produced gas. In a recent review, different biomass co-gasification processes were performed using crude glycerol with lignocellulosic biomass (62). Some of the studies done in the last 8 years on gasification of crude glycerol are summarized in Table 2. In this proven option for glycerol disposal and utilization, co-gasification of glycerol and other feedstock was able to improve the yield of syngas or hydrogen considerably.

Pyrolysis is another thermochemical conversion process similar to gasification. It generates gas, bio-oil, and char, three product streams, through the decomposition of biomass at high temperatures (>350°C) in the absence of oxygen. The difference between the two methods is that in gasification, higher temperatures are used, so the char produced in the pyrolysis stage is further converted to syngas. There are three basic categories of pyrolysis (slow pyrolysis, fast pyrolysis, and

| Table 2. Studies on the gasification of crude glycerol to produce syngas. |
|-----------------|-----------------|-----------------|-----------------|-----------------|
| Method          | Crude glycerol  | Conditions       | Production/yield | References      |
| Air gasification with olive kernel | 85.4% glycerol, 8.4% water, 6% other | Co-gasified glycerol with olive kernel in a fixed bed reactor at 750–850°C. | Syngas production increased from 0.4 to 1.2 N m⁻³/kg. 19% to 33% (v/v) H₂ increase and tar decrease from 19.5% to 2.4% | (50) |
| Hydrothermal continuous gasification by supercritical water | 68.53–71.18% glycerol, 2.62–4.19% methanol, 25.91–29.71% MONG, 1.49–2.51% ash, 0.01–0.04% water | 650°C, 5% glycerol, continuous tubular reactor | Syngas 26.44–35.85 mmol/g produced. LHV: 8–10 MJ/m³ | (63) |
| Gasification by supercritical water | – | 500°C, 7% glycerol, 45 MPa and 2.39 mol/L KOH | H₂ mole fraction yield 27.9 mol%, most significant | (64) |
| Gasification with hardwood chips | – | Co-gasification of hardwood chips and crude glycerol | Up to 20% glycerol produce syngas within ICE standards, having higher heating values (HHV) of 18.71 MJ/kg | (65) |
| Steam gasification | 60% glycerol, 31% methanol, 7.5% water, 1.05% KOH | Liquid hourly space velocity of 0.77/h, 800°C, Ni/Al₂O₃ catalyst, 1:3 steam to glycerol | 69.4% yield of syngas | (60) |
| Hydrothermal gasification in supercritical water | – | The impact of acid and base catalyst on the yield of syngas. Effectiveness of catalyst on gasification | K₃PO₄ > K₂HPO₄ > H₃PO₄ > KH₂PO₄ for crude glycerol gasification, K₂HPO₄ and K₃PO₄ gave max H₂, H₃PO₄ and KH₂PO₄ gave max CH₄ | (67) |
| Air/O₂ Gasification | 60% glycerol, 20% MONG, 15% methanol, 5% ash | Entrained flow gasifier, excess air ratio 0.35–0.4, Temperature of 950–1500°C | Syngas HV of Syngas about 2500 kcal/N m⁻³ | (68, 69) |

The fraction of syngas decreased as the oxygen-to-fuel ratio increased and atomization of glycerol using a nozzle improved the efficiency of the gasification process.
Solid char from pyrolysis is a carbonaceous residue. It can be used as a solid fuel for the production of heat and electricity; feedstock for gasification processes; feedstock for activated carbon production, and feedstock for carbon nano filaments’ production, among other uses.

Syngas from pyrolysis: the gas produced during the pyrolysis process (light molecular weight gases) is another valuable by-product. A vast diversity of biomass materials can be converted to combustible gases (H₂, CO, C₂H₂, CH₄, and C₂H₄). These combustible gases can be used as the direct firing in boilers for heat production or in gas turbines or engines for electricity production.

Pyrolysis studies have been performed using crude glycerol as an auxiliary compound to pyrolyze different types of feedstock. The improvement in the bio-oil quality and quantity was observed in co-pyrolysis of glycerol with lignocellulosic biomass and manure in these studies as summarized in Table 4. Co-pyrolysis is undoubtedly a promising option; however, more research and detailed analysis are necessary to identify the mechanism for energy production enhancement. Researches have reported that water and methanol existing in crude glycerol acted as the catalysts in pyrolysis and decreased the activation energy of the decomposition of glycerol, demonstrating crude glycerol to be a very promising additive (71). Approximately, each 450 g of glycerol feedstock produce about 270 g of bio-oil, 90 g of char, and 90 g of gas when paralyzed. According to the literature, most of the pyrolysis processes have been conducted using several types of equipment heated by a conventional heating source (e.g. an electrical gas heater), namely melting vessels, blast furnaces, tubular or fixed bed reactors; these types of pyrolysis processes are termed generally as “conventional pyrolysis.” These types of equipment were used in a manner where the thermal energy is externally applied to the reactor and heats all the substances in the reactor including the evolved pyrolysis-volatiles, the surrounding gases, and the reactor chamber itself. In this case, energy is not fully targeted at the material being heated and this results in significant energy losses in terms of the energy efficiency of the whole process. Nevertheless, several of these processes have been developed into a pilot plant scale despite their limited energy efficiency (72,73).

4. Microwave technology

In the pyrolysis process, the three components, which is solid (char), liquid (bio-oil), and syngas (gaseous), are produced and the yield would vary with the changing operational parameters. Generally, the bio-oil may be considered as the more valuable and useful. The bio-oil (also known as pyrolysis oil) can be upgraded into biofuel which can be readily stored and transported as a promising candidate to replace petroleum fuels for power generation, heat, or for extraction of valuable chemicals (79). Flash pyrolysis processes are so far the common technology for the production of a high liquid yield. It is achieved through rapid heating rates of 10 to >1000°C/s, short residence times of <2 s, temperatures of 400–650°C, and rapid quenching of the vapors in the absence of oxygen (80). However, the product is not readily available for consumption. Many issues negatively affect the ability of raw bio-oil’s usage as a source of fuel or for the usage in value-added chemical production. Its complex chemical composition is one of the main reasons it cannot be utilized directly in combustion systems. Bio-oil has a low heating value of 16–18 MJ/kg because of a 15–30 wt% of water and 35–50 wt% of oxygen; its high acidity of pH 2–3 also contributes to its undesirable qualities (81). There is a need for upgrading to improve the chemical and physical

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### Table 3. The three different types of pyrolysis processes.

| Type            | Operating parameters                          | Yield                                      |
|-----------------|-----------------------------------------------|--------------------------------------------|
| Slow pyrolysis  | Temperature of 400°C. Residence time of more than 30 min and a heating rate of 0.1–1°C/s | 35% bio-char (solid), 30% bio-oil (liquid) and 35% syngas (gas) |
| Fast pyrolysis  | Temperature of 500°C. Residence time of 10–20 seconds and a heating rate of 1–200°C/s | 20% bio-char (solid), 50% bio-oil (liquid) and 30% syngas (gas) |
| Flash pyrolysis | Temperature of 400°C. Residence time of about 1 second and a heating rate greater than 1000°C/s | 2% bio-char (solid), 75% bio-oil (liquid) and 13% syngas (gas). Efficient decomposition of the feedstock components strongly influenced by the process parameters such as reaction temperature, pressure, residence time, reactor configuration, and catalyst |
One of the main difficulties that occur during biomass pyrolysis is the selectivity of the desired compounds in the bio-oil. Different feedstock sources lead to different ratios in the chemical composition of the bio-oil/pyrolysis oil. Currently, many investigations are geared toward improving the bio-oil yield during the pyrolysis process as well as improving the selectivity of the desired compounds in the pyrolysis oil.

In the early 1980s, it was reported that microwave irradiation could promote organic chemical reactions and this has led to the surge in research involving microwave irradiation in various chemical reactions. The application of microwave technology for the thermal treatment of biomass saw a major increase around the mid-nineties. This technique not only reduces the energy consumption and processing time, but also enables the use of a unique internal heating phenomenon. It can also enhance the overall production quality. Microwave irradiation is an electromagnetic irradiation in the range of wavelengths from 0.01 to 1 m with the corresponding frequency range of 0.3–300 GHz.

Most microwave reactors for chemical synthesis operate at 2.45 GHz frequency, which corresponds to a wavelength of 12.25 cm. Microwave technology can be very useful in chemical processing because products can be heated volumetrically instead of surface heating via convection and conduction. Microwaves cause molecular motion by migration of ionic species or rotation of dipolar species or both to generate heat because of the friction among molecules. Materials that absorb microwave irradiation are called microwave diellectrics. Microwave heating also called as dielectric heating transfers electromagnetic energy to thermal energy. Microwave energy can be delivered directly to the reacting or processing species by using their dielectric properties or by adding absorbers to materials, which allows more volumetric heating of materials. Researchers have reported two possible ways by which reactions are enhanced using the microwave irradiation technique.

Table 4. Studies on the co-pyrolysis of crude glycerol with other biomass to produce bio-oil.

| Method | Crude glycerol properties | Conditions | Char | Bio-oil | Gas | References |
|--------|---------------------------|------------|------|---------|-----|------------|
| Pyrolysis of corn straw with crude glycerol | 56.2% glycerol, 7.3% methanol, 2.4–4.3% water, 3.5–7.2% ash | 30°C/min to 550°C, use helium to remove air, 1:1 ratio of corn to glycerol | Low amount LHV: 24.84 MJ/kg | High yield LHV: 30.52 MJ/kg | High yield LHV: 28.65 MJ/kg | (74) |
| Pyrolysis of Greek lignite with 20% crude glycerol | 85.4% glycerol, 8.4% water, <6% methanol, <51.5% MONG, 0.2% FFA | 850°C, 20% glycerol | - | - | 71% conversion to volatiles. 65.44 v/v% hydrogen yield | (75) |
| Pyrolysis of olive kernel with crude glycerol | 85.4% glycerol, 8.4% water, 6% other | 720°C, 25% glycerol | - | - | Increase in H₂ production by 11.6% (v/v) | (76) |
| Pyrolysis of swine manure with crude glycerol | 55.09% glycerol/methanol/water, 31.09% FFA, 13.81% salts | 1:3 manure: glycerol, 7°C/min, 340°C, 0.65 MPa | - | - | 68% yield. FFA was the key beneficial to oil yield. Yield enhanced 1.83 times. Lowers viscosity and density | (77) |
| Pyrolysis of olive kernel with crude glycerol | 85.4% glycerol, 8.4% water, 6% other | Microwave pre-treatment of substrate (25% crude glycerol +75% olive kernel), followed by pyrolysis at 720°C | Bio-oil 59.53% v/v; Enriched syngas (H₂+CO₂) concentration (84.9% v/v) | - | - | (78) |
found in a recent review article (93). In terms of the characteristics of microwave heating and conventional heating, Table 5 provides a summary of the features of both heating methods.

### 4.1. Microwave-assisted pyrolysis process

A variety of conventional pyrolysis systems used have been covered in many research works. To date, however, only a few researches have investigated the microwave irradiation-induced pyrolysis process. Microwave pyrolysis technology has gained momentous attraction, which offers a number of merits over conventional pyrolysis. The main advantage is that microwave pyrolysis can be performed for large-sized particle feedstocks as the polar molecules that oscillate under the influence of an oscillating electric and magnetic field agitate the heating. Compared to fast pyrolysis like fluidized bed, pre-dried biomass is not required in microwave pyrolysis. The moisture in biomass needs to be removed for obtaining high heating rate in conventional fast pyrolysis. However, in microwave pyrolysis the moisture is a good adsorption material for irradiation that induces the pyrolysis. Microwave pyrolysis also produces clean products like bio-oil because of an increasing secondary reaction. In addition, higher heating rates favor the production of liquid and gaseous fractions (99). Many efforts have been made to estimate the energy recovery in microwave pyrolysis of waste materials. Studies have shown that the microwave pyrolysis process is capable of recovering pyrolysis products (e.g. hydrocarbon oils) whose calorific values are many times greater than the amount of electrical energy used in the operation of the process, showing both a positive energy ratio (energy content of hydrocarbon products/electrical energy supplied for microwave heating) and a high energy output (94).

In conventional pyrolysis, energy is transferred to the biomass sample through the processes of convection or conduction. There must be physical contact between the heating source and the biomass sample. This has proven to be very inefficient because of a large amount of energy that is needed to increase the temperature of
the feedstock. The use of microwaves in pyrolysis has been proven to be more efficient because of the heating pattern; in conventional pyrolysis, heat is transferred from the outer layers of the sample to the interior. This results in uneven heating and the quantity and quality of the bio-oil produced is degraded. In microwave heating, the interior of the sample is heated first and it gradually spreads to the outer most regions of the sample. As a result, the heating is more uniform and this allows for greater yields of bio-oil. Table 6 gives an extensive overview of microwave-assisted pyrolysis that has been applied to various lignocellulosic feedstocks. The relationships among heating, bio-oil yield, and feedstock particle size, moisture content, inorganics, and organics in microwave-assisted pyrolysis are given in detail in Table 7 (100). An up-to-date summary of recent studies on advances on the microwave-assisted pyrolysis methods have been reviewed extensively (100). The review provides information that will aid in the development of a newer microwave-assisted pyrolysis system.

### 4.2. Microwave-assisted pyrolysis of crude glycerol as sole biomass

There are already some studies on co-pyrolysis of crude glycerol with other biomass to produce bio-oil as shown previously in Table 2. However, research related to pyrolysis of waste glycerol (derived from biodiesel transesterification) as sole or major biomass with minimal or no co-substrate (5–20% of other biomass) addition to producing bio-oil is limited. In fact, studies on microwave-assisted pyrolysis of waste glycerol to produce bio-oil are even scarcer. Previous investigations of glycerol pyrolysis have mostly focused on the production of synthesis gas (syngas) (132,133). In the work reported in 2008, 72 mol% of gaseous yield was obtained from glycerol at 800°C, in which the syngas contained 93.5 mol% of H₂ and CO (133). Conventional furnace heating was used as the heat source (133). By varying the carrier gas flow rate and temperature, different gas yields and compositions can be achieved. Gas production was favored at a lower particle size of the packing materials. In another study, syngas was produced by pyrolysis of glycerol using the microwave-induced pyrolysis technique and high gas yield of 81 vol.%, consisting of 34.6 vol.% of H₂ and 45.9 vol.% of CO were reported (134). Although microwave pyrolysis can provide various advantages over conventional pyrolysis, it still faces several challenges. The bio-oil yield (up to approximately 40 wt%) of microwave pyrolysis is much lower than that from fluidized bed pyrolysis, which indicates that the high bio-oil yield production remains a large challenge for microwave pyrolysis. The microwave pyrolysis method has shown to yield a higher conversion rate of glycerol into gaseous products compared to conventional heating processes in all cases, but the effects on solid and liquid products were not investigated (135). In a related study reported in 2015, the results obtained showed that microwave-assisted pyrolysis can be used to convert waste glycerol into hydrogen. In addition to hydrogen, there were also liquid products, such as methanol, allyl alcohol, acrolein, and some products that are not identified (136). The report also showed that activated carbon catalyst can produce more hydrogen than Ni/HZSM-5 catalyst (136). It is noteworthy that most waste glycerol to energy processing techniques focused on optimizing operating conditions (including effect of catalyst) to obtain synthesis gases with no or very minimal emphasizing on the solid and liquid products.

In a recent study, it was reported that generally the presence of the catalyst during the microwave-assisted pyrolysis of crude glycerol resulted in an increase in liquid product and a decrease in gaseous product at both the temperatures of 300°C and 400°C (137). At 300°C, the use of the catalyst decreased the gaseous product by 4.2%, but increased the liquid product by 9.2%. The

### Table 6. Product yields of lignocellulosic biomass using microwave pyrolysis.

| Biomass          | Conditions used for the experiment | Yield (wt %) | References |
|------------------|------------------------------------|--------------|------------|
|                  |                                     | Gas          | Liquid     | Solid     |           |
| Larch            | Sample: 191 g; microwave power: 1.5 kW; reaction time: 18 min | 60.8         | 18.1       | 21.1      | (101)     |
| Pine wood        | Sample: 15 g; microwave power: 0.3–1 kW; reaction temperature: 470°C; reaction time: 12 min | 60.0         | 22.7       | 17.3      | (102)     |
| sawdust          |                                     |              |            |           |           |
| Peanut shell     | Sample feeding rate: 2 kg/h; reaction temperature: 500°C; particle size: 0.5–1.0 mm | 17.1         | 52.4       | 30.5      | (103)     |
| Rice straw       | Sample: 3–5 g; microwave power: 300 W; reaction temperature: 400°C; reaction time: 30 min; particle size: <0.425 mm | 49.4         | 22.6       | 28.1      | (104)     |
| Corn stover      | Sample: 100 g; microwave power: 875 W; reaction temperature: 450–550°C; reaction time: 20 min; particle size: 6.2 mm in diameter and 10–20 mm in length | 34.4         | 37.0       | 28.6      | (96)      |
| Wheat straw      | Sample: 100–150 g; microwave power: 1.2 kW (max); reaction temperature: 180°C (max); reaction time: 10 min | 14           | 57         | 29        | (105)     |
| Oil palm shell   | Microwave power: 450 W; reaction time: 25 min; particle size: 1–100 mm | 19           | 13         | 68        | (106)     |
| Oil palm fiber   | Microwave power: 450 W; reaction time: 25 min; particle size: 0.3–0.6 mm | 12           | 8          | 80        | (106)     |
Table 7. Biomass feedstock properties and microwave-assisted pyrolysis (100).

| Biomass feedstock property | Remarks | References |
|---------------------------|---------|------------|
| Particle size             | • Smaller feedstock particle size – generally improves the microwave-assisted pyrolysis process (higher heating rates).  
  • Very small particles lead to very high external surface area and give complete pyrolysis, whereas too large particles may result in incomplete pyrolysis. Each of these would result in a low bio-oil yield for the microwave-assisted pyrolysis of biomass.  
  • The biomass particle sizes of 2–4 mm are better for microwave-assisted pyrolysis. However, the optimal particles sizes for the conventional heating pyrolysis are between 0.85 and 2 mm. | (107, 108, 109) |
| Moisture content          | • Water has a very good microwave absorbability (because of its high tangent lost – tan δ) and renders the feedstock a high temperature during the process.  
  • With increasing temperature, the moisture evaporates, the biomass becomes less microwave absorptive, and the temperature rising rate slows down.  
  • Reaction temperatures of the process also affect the tangent loss value of a biomass feedstock.  
  • When tangent loss value decreases, the microwave absorbability of the biomass becomes lower and lower. This makes the achievable temperature of the pyrolysis process low (e.g. less than 200°C) even if the microwave power is increased.  
  • Microwave absorbers which can absorb microwave energy (those with high tangent lost) are used to enhance heating and make the process more efficiently. | (111) |
| Inorganics                | • Ash is another main inorganic matter in a biomass. The ash components in biomass feedstock vary significantly, e.g. rice straw and wood sawdust have high contents of SiO₂ (52.66–69.52%) and K₂O (10.30–40.13%) while sewage sludge have low contents of SiO₂ (1.62–26.40%) and K₂O (0.05–1.62%).  
  • Generally, some ashes are good microwave absorbers and some are not. For example, Fe₂O₃ and TiO₂ have higher tan δ values (0.001–0.05) whereas MgO and SiO₂ have lower tan δ values (0.0002–0.0005).  
  • The ash components themselves do not convert to bio-oil. The high ash content would therefore reduce the bio-oil yields. Studies on microwave-assisted heating have shown that the high ash content (60.5–70.9%) will give low bio-oil yields (0–0.24 wt%). | (105, 116–118, 117) |
| Organics                  | • Lignocellulosic biomass is mainly composed of cellulose (23–60%), hemicellulose (25–44%), and lignin (12–49%). Generally, cellulose and hemicellulose result in more bio-oil than lignin.  
  • With conventional heating, the decomposition temperature ranges are cellulose (315–390°C), hemicellulose (250–350°C), and lignin (200–550°C). However, with microwave-assisted pyrolysis, the lignocellulose components decomposed at lower temperature (around 100–150°C lower).  
  • Generally, the lignocellulosic biomass components under microwave-assisted pyrolysis would produce more bio-oil than conventional heating pyrolysis.  
  • Algae biomass is rich in protein (9–30%), lipids (30–62%), and some carbohydrates (2–18%). Algae biomass is usually not a good microwave absorber, even if it has high lipid content (among carbohydrate, protein, and lipid, the good microwave absorber is lipid).  
  • Microwave absorbers are generally required to obtain high temperatures for microwave-assisted pyrolysis of an algal biomass. The bio-oil yield from the microwave-assisted pyrolysis algal is lower. However, algal biomass produces bio-oil that has much better quality by having higher H/C and H/O ratios and thereby showing higher HHVs.  
  • Plastics and rubbers (high hydrocarbon) are also widely used as absorbers in microwave pyrolysis for bio-oil production. Compared with the plastic, rubber is a better microwave absorber. Rubber can achieve a high temperature of 500°C and give high bio-oil yields during microwave pyrolysis.  
  • Due to the low microwave absorbability of the plastic components (e.g. polypropylene, polystyrene, polyethylene), the plastic cannot achieve a high temperature (lower than 180°C) if no microwave absorber is added but can increase significantly when microwave absorbers are added.  
  • Due to the high hydrocarbon content of plastics, the microwave-assisted pyrolysis of plastics would result in high bio-oil yields. | (120, 111, 121, 122, 123, 124, 125, 126–131) |
difference was more significant when the heating temperature was raised to 400°C and the gaseous product was reduced by 19%, while the liquid product increased by 22% (137). The same authors reported that the highest liquid (bio-oil) product yield was obtained at the heating temperature of 400°C. A further increase in the pyrolysis temperature resulted in a decrease of bio-oil product. At 700°C, the bio-oil product yield was 15.7%, while the gaseous product yield was 83%. The function of a catalyst is to increase heat transfer and assist in the thermal cracking process. Hence, a more complete cracking of the molecules with fewer solid products can be achieved. Studies have shown that adding a catalyst can increase the liquid yield and improve the quality of the liquid product (138,139). The pyrolysis temperature is one of the main parameters that can affect product yields. Liquid bio-oil shows a maximum yield at an intermediate temperature but it decreases at higher temperatures, due to the thermal cracking of heavy compounds into small-chain products. Varying the carrier gas flow rate changes the residence time of the products during the pyrolysis process, as the nitrogen (N₂) flow rate changes the distribution of carbon inside the reactor. A lower flow rate of carrier gases provides ample residence time for the product to undergo the chain-cracking process that leads to secondary reaction (134,140). Furthermore, the higher N₂ flow rate reduces the time available for gaseous products to undergo the condensation process. As a result, the pyrolysis product remains largely as gaseous product (approximately >80%). From the study published in 2017, researches have noted that during microwave-assisted pyrolysis of glycerol, the proportion of products’ phases is mainly dependent on the residence time inside the reactor, followed by the reaction temperature (141).

Generally, production of liquid product is more favored at lower pyrolysis temperature as more vapor is able to condense. At higher pyrolysis temperature (>600°C), more energy is available for the cracking of vapor, resulting in less liquid product (141). Not only is the quantity but also the quality of the pyrolysed liquid product is affected by pyrolysis temperature. When reaction temperature decreases, there is a tendency for the higher proportion of liquid product to form. However, for solid products, it is dependent on both decreasing temperature and carrier gas flow rate. In the same study, the authors have reported that for microwave pyrolysis of glycerol, the operating conditions of 400°C, 1000 mL/min of N₂ gas flow rate, and residence time of around 30–50 seconds is the optimal setting where the liquid product exceeds that of the gaseous products (141). The report further mentions a third factor that affects the gaseous product portion. The activated carbon-based catalyst is a good microwave absorber. The porous structure of the activated carbon also prolongs the resistance time of volatiles. These factors allow the catalyst-assisted microwave pyrolysis to gain sufficient thermal energy to achieve temperatures exceeding 400°C. The higher selectivity of carbonaceous catalysts toward hydrogen gas formation will lead to greater H₂/CO ratio. As the volume of H₂ increases by proportion when a catalyst is used, the proportion of the overall gaseous product weight will decrease, as H₂ has a lower molar mass (141). The activation energy and pre-exponential factor of microwave pyrolysis are much lower than conventional methods. Thus, the mechanism and kinetic of the reaction for the microwave pyrolysis are different from the conventional pyrolysis process (142). Finally, it can be envisaged that the conversion of waste into portable energy products through microwave pyrolysis makes crude glycerol a potential candidate for bioenergy production of bio-oil and syngas.

4.2.1. Properties of bio-oil obtained by microwave-assisted pyrolysis

The liquid or oil fraction of the biomass pyrolysis can be a promising alternative energy source for biofuel or a platform molecule for production of other products such as organic acids. Microwave pyrolysis offers the potential for greater efficiencies and less pollution for the production of reactive intermediate products from biomass in comparison with other techniques. The bio-oil or pyrolysis oil is usually a dark-brown organic liquid with the heating value of approximately half that of conventional fuel oil (due to the relatively high oxygen and water contents of bio-oil). Thus, further upgrading and refining processes are needed to increase its heating value. There have been intensive studies on bio-oil upgrading and various technologies have been developed for bio-oil upgrading, including hydro-treating, hydrocracking, supercritical fluids extraction, solvent addition/esterification, emulsification, steam reforming, and chemical extraction. Solvent addition (esterification) appears to be the most practical approach due to its simplicity, low cost of some solvents, and their beneficial effects on the oil properties. However, none of these bio-oil upgrading techniques has been commercialized due to low biofuel efficiency and their limitations and high up-grading cost of the overall pre-treatment process (79). It was reported that the properties of microwave pyrolysis bio-oil were slightly different from those of conventional pyrolysis bio-oil. The quality of the oil produced is also better because more of the chemical components in the feedstock sample are broken down into liquid products (143,144). Hence, different feedstock sources lead to different ratios in the chemical
composition of the bio-oil. The properties of bio-oils produced by microwave and conventional pyrolysis are listed in Table 8. The bio-oil from microwave pyrolysis have higher carbon content and higher heating value and lower oxygen content (139,145,146). Microwave pyrolysis of biomass has demonstrated the potential to produce a unique grade of products owing to the unique thermal gradients that exist during processing (123,126,147–151). A number of reviews and scientific articles have discussed the use of microwaves to induce the production of higher quality bio-oils, mostly from the perspective of optimizing the involved operational conditions (e.g. microwave power, temperature, residence time or concentration of different microwave susceptor additives). Furthermore, it was reported by a researcher in 2007 that the properties and stability of bio-oils can be improved by blending methanol or ethanol into the bio-oils (145).

4.2.2. Bio-oil derived from microwave pyrolysis as boiler fuel

The renewable liquid fuel, bio-oil derived from pyrolysis processes, has great potential to replace or substitute fossil fuel to generate heat, power, and/or chemicals. Boilers and furnaces (including power stations) can be fueled with bio-oil. Alternatively, the crude bio-oil could serve as a raw material for the production of adhesives and phenol-formaldehyde-type resins. Upgrading of the bio-oil to a transportation fuel is technically feasible but needs further development. Transportation fuels, such as methanol and Fischer-Tropsch liquids, can be derived from bio-oil as gasifier feedstock, instead of the solid biomass (can save transportation cost). Furthermore, there is a wide range of chemicals that can be derived from bio-oil. The quality of the combustion is directly comparable to the properties of the fuel. Pyrolysis bio-oil is completely different from fossil fuels oils; its properties can vary greatly depending on the feedstock and process used in production. When compared to fossil fuel oils, the differences in combustion properties are mainly due to the significant differences in chemical composition of these fuels. In combustion applications, the physical and chemical properties of the bio-oil are responsible for the negative impacts on atomization quality, ignition, droplet vaporization and burning rate, clogging, coking tendency, and emissions (152). The usage of bio-oil to completely replace fossil fuels has some limitations, since bio-oil has bad properties, such as high viscosity, water content, poor volatility, coking, and corrosiveness. These limitations cause the primary challenge in the combustion process and industrial applications (153).

The current method of utilizing bio-oils in the boiler requires preheating of the bio-oil prior to combustion and after use, the engine may need to be flushed by diesel or methanol to prevent corrosion and scale formation (146). In addition, modifications of the combustion boiler system and operating conditions are required in order to improve combustion of bio-oil with fossil fuels, since some problems might take place during the usage of standard equipment constructed for firing fossil fuels. For instance, the existing burner must be replaced with a modified oil burner or a newly designed bio-oil burner (such as a burner head configuration) for firing bio-oil. In addition, the pumping, piping, oil preheating, and valve systems must also be specially designed for bio-oil (153). The experiment conducted to investigate the spray combustion characteristics of bio-oil produced from rice husk found that after attaining steady-state combustion, the temperature in the center of the combustion chamber exceeded 1400°C (154). The carbon monoxide (CO) emission concentration dropped, indicating that complete combustion was improved under operating conditions with higher oxygen concentrations. Meanwhile, the NOx concentration was slightly increased due to the higher temperature and the increased O2 concentration. Furthermore,
the measured SOx concentration was very low (smaller than 30 ppm), since bio-oils contain insignificant amounts of sulfur (154).

One possible non-laborious option is modifying the bio-oil to accommodate the boiler requirements through blending with other biofuels/additives (155). Hence, a low blend ratio of bio-oil to petroleum-derived diesel (low bio-oil content) has advantages as it can be easily combusted in the existing industrial boilers without modification of the burner and boiler sections (153). Since the bio-oil from microwave pyrolysis has higher carbon content and higher heating value as well as lower oxygen content, the bio-oil produced from microwave pyrolysis is an attractive candidate for blending with different petroleum-based oils, which eventually will enhance the performance and emissions characteristics on the boiler application. Standard test methods have been used to evaluate the fuel properties and specification for selection of suitable fuels for boilers (156). Table 9 highlights the important pyrolysis oil properties required for boiler application (156). The specifications differentiate between two grades of pyrolysis oil, grade G and grade D. Grade G is intended for use in industrial burners and not suitable for residential heaters, small commercial boilers, engines, or marine applications. Grade D is for commercial/industrial burners requiring lower solids and ash content and only suitable in residential heaters, engines, or marine applications if they have been modified to handle these types of fuel. Based on the previous studies on microwave-derived pyrolysis oil properties, such as the one mentioned previously in Table 9, it is obvious that the bio-oil can be blended with diesel at a low percentage (up to 20%) for application as boiler oil.

5. Net energy analysis of the bio-oil produced from pyrolysis of glycerol

Acetaldehyde, acetone, methanol, ethanol, water, and acetic acid were the major liquid products obtained during the pyrolysis of glycerol as stated in Table 10. Acrolein and unreacted glycerol were also found in the liquid product for the pyrolysis runs at 400–500°C (157). Acetaldehyde, methanol, and acrolein could have been formed by the radical mechanism as reported by Büuhler et al. (157) and Antal et al. (158). Energy balance calculations for bio-oil production from the pyrolysis of glycerol are given as follows, which is based on the thermal cracking of glycerol reaction in the absence of water.

\[
6C_3H_8O_3 + 2H^+ \rightarrow CH_3CHO + CH_3COCH_3 + CH_3OH \\
+ 2C_2H_5OH + 7H_2O + CH_3COOH + CH_3CHCHO \\
+ C_3H_6O_3.
\]

Specific heat capacity, the heat of formation, and standard enthalpy of formation of components such as glycerol, water, and acetaldehyde and others were obtained from Chemical Properties Handbook (159). Feed at 25°C and Product at 400°C

Basis: 6 mol of glycerol in feed

Table 9. Standard test for pyrolysis oil for boiler fuel application by ASTM D 7544 (156).

| Property                      | Test method | Grade G | Grade D |
|-------------------------------|-------------|---------|---------|
| Gross heat of combustion, MJ/kg, min | D240        | 15      | 15      |
| Water content, wt%            | E203        | 30      | 30      |
| Pyrolysis solids content, wt% | D7579       | 2.5     | 0.25    |
| Kinematic viscosity at 40°C, mm²/s | D445       | 125     | 125     |
| Density at 20°C, kg/dm        | D4052       | 1.1–1.3 | 1.1–1.3 |
| Sulfur content, wt%           | D4294       | 0.05    | 0.05    |
| Ash content, wt%              | D482        | 0.25    | 0.15    |
| pH                            | E70         | Report  | Report  |
| Flash point, °C               | D93         | 45      | 45      |
| Pour point, °C                | D97         | –9      | –9      |

Table 10. Standard enthalpies of formation for major liquid components’ presence in the bio-oil during the pyrolysis of glycerol.

| Reactant/Product name       | Formula | Enthalpies of Formation \( \Delta H^\circ \) at 25°C (kJ/mol) | Energy required to raise the product temperature from 25°C to 400°C \( [E = C_p \Delta T] \) (kJ/mol) |
|-----------------------------|---------|--------------------------------------------------------------|--------------------------------------------------------------------------------|
| Glycerol liquid             | C₃H₈O₃  | –669.6                                                      | 84.71                                                                          |
| Acetaldehyde                | CH₃CHO  | –191.70                                                     | 33.40                                                                          |
| Acetone                     | CH₃COCH₃| –247.48                                                     | 47.06                                                                          |
| Methanol                    | CH₃OH   | –238.42                                                     | 29.81                                                                          |
| Ethanol                     | C₂H₅OH  | –277.05                                                     | 41.80                                                                          |
| Water                       | H₂O     | –241.8                                                      | 28.48                                                                          |
| Acetic acid                 | CH₃COOH | –484.93                                                     | 46.31                                                                          |
| Acrolein                    | CH₃CHCHO| –120.0                                                      | 26.73                                                                          |
Boiling temperature of glycerol is 290°C
The energy required to take liquid glycerol from 25°C boiling temperature (290°C):

\[ Q_1 = \int_{25}^{290} mC_p \, dt, \]

\[ Q_1 = 6 \times \int_{25}^{290} \left(132.145 + 8.6007 \times 10^{-1} T - 1.9745 \times 10^{-3} T^2 + 1.8068 \times 10^{-6} T^3 \right) dT, \]

\[ Q_1 = 642.81 \text{ kJ}. \]

Heat of vaporization \((H_{\text{vap}})\) of glycerol at 290°C is 66.13 kJ/mol

Energy required to vaporize the liquid glycerol at 290°C

\[ Q_2 = H_{\text{vap}} \times 6 \text{ mol} = 396.78 \text{ kJ}. \]

Energy required to take glycerol vapor from 290°C to 400°C

\[ Q_3 = 6 \times \int_{290}^{400} \left(9.656 + 4.2826 \times 10^{-1} T - 2.6797 \times 10^{-4} T^2 + 3.1794 \times 10^{-8} T^3 + 2.7745 \times 10^{-11} T^4 \right) dT, \]

\[ Q_3 = 171.25866 \text{ kJ}. \]

The total energy required for the feed at reaction temperature:

\[ Q_F = Q_1 + Q_2 + Q_3, \]

\[ Q_F = 1210.8486 \text{ kJ}. \]

Calculation for the enthalpies of formation of the reaction (details are given in Table 11)

\[ Q_R = \Delta H_R^0 = \sum np \Delta H_f \text{ (products)} - \sum nr \Delta H_f \text{ (reactants)}, \]

\[ \Delta H_R^0 = -4198.83 - (-4017.6), \]

\[ \Delta H_R^0 = -181.23 \text{ kJ}. \]

By assuming the heat capacity for each product is constant from 25°C to 400°C,

Energy required to raise the product temperature from 25°C to 400°C, \(Q_4 = 550.98 \text{ kJ (Table 11)}\)

Total energy required for the reaction:

\[ Q_{rxn} = Q_F + Q_R + Q_4, \]

\[ Q_{rxn} = 1210.8486 + (-181.23) + (550.98), \]

\[ Q_{rxn} = 1, 580.60 \text{ kJ}. \]

Energy output:

Taking the average heating value of bio-oil as 17 MJ/kg (142)

or \(17 \frac{\text{ MJ}}{\text{kg}} \times 1000 \frac{\text{kJ}}{\text{kJ}} = 17,000 \text{ kJ/kg}\)

The molar mass of the bio-oil is assumed to be 350 g/mol (adopted from Järvik and Oja (160))

17,000 kJ/kg \times 0.35 g/mol = 5950 kJ/mol
By assuming 100% selectivity for bio-oil production and that the bio-oil product is equal to 1 mole, the total heating value of bio-oil = 5950 kJ/mol \times 1 = 5950 kJ

The net energy gain is

5950 – 1580.60 = 4369.94 kJ/6 mol of glycerol reacted = 728.32 kJ/mol of glycerol reacted.

6. Glycerol prices and production cost of bioglycerol based polymer

Looking at the glycerol market worldwide, there has been a rapid increase in glycerol supply since 2003. The prices of both refined and crude glycerol have been on the decline due to a surplus of glycerol from biodiesel. The market surplus of glycerol from biodiesel is far from being tackled by new demand as platform chemical. Recent market analysis projects that demand glycerin by-product of oleochemicals and biodiesel production will expand at an annualized average rate of 7% during 2007–2021, with 6 million tons of overall production in 2025 (161). There are several studies on the techno-economic analysis of biomass fast pyrolysis for bio-oil production available in the literature. These studies have reported that bio-oil costs can range from US$0.62/gal to US$1.40/gal and the capital costs ranging from US$7.8 to US$143 million over a 240 MT/day to 1000 MT/day plant capacity (162). In terms of usage of glycerol for production of bio-based products, the versatile chemical acrolein is one of the most important. Acrolein is one of the very useful intermediates in the chemical industry due to its wide utilization of

Table 11. The details of calculation for enthalpy of formation for the reactants and products.

| Calculation | Total (kJ) |
|-------------|-----------|
| \(\sum nr \Delta H_f \text{ (reactants)}\) | 6^* – 669.6 |
| \(\sum np \Delta H_f \text{ (products)} \text{ at 25°C}\) | \(1^* - 191.70 + 1^* - 247.48 + 1^* - 238.42 + 2^* - 277.05 + 7^* - 241.8 + 1^* - 484.93 + 1^* - 120 + 1^* - 669.6\) |
| \(\sum np \Delta H_f \text{ (products)} \text{ from 25°C to 400°C}\) | \(1^* 33.40 + 1^* 47.06 + 1^* 29.81 + 2^* 41.80 + 7^* 28.48 + 1^* 46.31 + 1^* 26.73 + 1^* 84.71\) | 550.98 |
acrylic acid, superabsorbent polymer, 1,3-propanediol, and many more polymers or polyesters’ production (163). An analysis of the cost of production of acrolein from bio-glycerol (both pure and crude) will give a better understanding of the implication of utilization of waste glycerol for value-added products to the biodiesel industry. Table 12 shows the several major components in the cost that differ greatly between propylene-based and bio-based methods for a 10,000-ton acrolein production. The quantities for steam only refer to what is used in the reaction. In addition, the energy listed in the table only refers to the part of the energy required to heat up the reactant(s) and required for the reaction (assuming the energy consumption of all the other processes are the same for both production methods). The quantities of the feedstocks required for both processes are calculated based on the stoichiometric relation under the assumption of 80 mol% acrolein yield, and the quantity calculated for crude glycerol was based on the glycerol purity of 80%.

In terms of the last two variations in the cost in Table 12, the bio-based method of producing acrolein using pure glycerol costs around USD 12.11–12.73 million (per 10,000 ton per year), which is about 27% less than the cost of acrolein production using the propylene-based method. Meanwhile, the bio-based method using crude glycerol for the production of acrolein costs around USD 7.88–8.52 million (per 10,000 tons per year), which is 47.0–50.8% lesser than that of the propylene-based method. Based on the calculation made, at the current developmental stage of gas-phase glycerol dehydration, the acrolein production price provided by the bio-based route using pure glycerol as the feedstock is much lower and significantly reduced (47.0–50.8% reduction) if the production begins with crude glycerol. The comparison of the cost provided for acrolein synthesis suggests that usage of crude glycerol could also bring about cost reduction and reduction in usage of petroleum-based raw materials. Even the production from pure glycerol may be worthwhile, because it is renewable and sustainable, and yet it does not increase the price much. The comparative cost analysis presented here will definitely be very valuable and meaningful in directing the industrial processes and future research thrusts involving bio-based product utilizing crude glycerol.

7. The state of the art in microwave-assisted pyrolysis

The overall prospect of pyrolysis technology is promising because it is already a proven concept. Pyrolysis offers more scope for recovering products from agricultural waste or biodiesel production waste than

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### Table 12. Comparison of propylene-based and bio-based acrolein production (10,000 ton/year) regarding feedstock and energy consumption.

| Raw material       | Price       | Propylene process (ton) | Bio-based process (ton) |
|--------------------|-------------|-------------------------|-------------------------|
|                    | ($/ton)     |                        | From pure glycerol     | From crude glycerol |
| Propylene          | $1770.9/ton | 9375                    | –                       | –                      |
| Pure glycerol      | $350–380/ton| –                       | 20,536                  | –                      |
| Crude glycerol     | $275–300/ton| –                       | 25,669                  | –                      |
| Steam              | $0.07/kWh   | 20,089                  | 82,144                  | 82,144                  |
| Energy             | $0.07/kWh   | –                       | 2.67 x 10^6 kWh        | 2.67 x 10^6 kWh        |
| Total cost (Million)|            | $16.76                  | $12.11–12.73            | $7.88–8.52             |

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a: The price reported in January 2014 by ICIS (164).
b: Calculated based on the 10,000-ton annual acrolein production and 80 mol% acrolein yield: [10, 000 ton/(56 g/mol)=(42 g/mol)]=80% = 9375 ton.
c: The price of pure glycerol and crude glycerol reported in June 2017 by Oleo line (165).
d: Calculated based on the 10,000 ton annual acrolein production, 80 mol% acrolein yield, and the stoichiometry of glycerol dehydration to acrolein: [10, 000 ton/(56 g/mol)=(92 g/mol)]=20,536 ton.
e: Calculated based on the same assumptions as 6 and the assumption that the crude glycerol contains 80% glycerol: [10, 000 ton/(56 g/mol)=(92 g/mol)]=25,669 ton.
f: The cost of the steam per ton is reported for 2003 by U.S. Department of Energy (166).
g: Calculated based on the calculated feed molar ratio of propylene-air-steam as 1:10:5 and the calculated propylene requirement: 9375 ton/(42 g/mol) = 18 g/mol/5 = 20,089 ton.
h: Calculated based on the calculated requirement for glycerol and the assumption that the feed has a concentration of 25 wt% glycerol: 20,536 ton/25% = 82,144 ton.
i: The price of energy reported in 2017 by EIA (167).
j: Calculated based on the heat requirement (43 kJ/mol) for the endothermic dehydration reaction of glycerol to acrolein, from [168] and the annual working hours of 80 h/year: (10^5 ton/year)(10^6 g/1 ton)(56 g/mol)/80%=(43kJ/mol)/0.0000278 kWh/1 kJ = 2.6710^6 kWh/year.

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k: The total cost of acrolein production from Propylene-based process: ($1770.9/ton) (9375 ton) + ($7.7/ton) (20,089 ton) = $16.76 Million.
l: The total cost of acrolein production from pure glycerol-based process at low acrolein price value: ($550/ton) (20,536 ton) + ($7.7/ton) (20,089 ton) = $12.73 Million.
m: The total cost of acrolein production from crude glycerol-based process at high glycerol price value: ($280/ton) (20,536 ton) + ($7.7/ton) (20,089 ton) = $7.88 Million. The total cost of acrolein production from crude glycerol-based process at high glycerol price value: ($300/ton) (25,669 ton) + ($7.7/ton) (20,089 ton) + ($0.07/kWh) (2.67 x 10^6 kWh) = $8.52 Million.
simply burning it. When agricultural or waste glycerol residues are burnt directly in a furnace/boiler, the only practical product is heat; however, when they are pyrolyzed first, bio-oil, syn-gases, and bio-char are produced. These pyrolysis products not only can be used as a fuel but also can be purified and used as a feedstock for petrochemicals and other applications. A significant number of researches have directed increasing activities on the fixed bed production technology for bio-oil from biomass. However, these systems are unlikely to give high liquid yields but are likely to give phase separated liquids (70). Microwave pyrolysis, which is a much newer process, has gained plenty of attention and its prospects are very optimistic. Hence, microwave-assisted pyrolysis can offer both technical and financial benefits. A number of works have been performed for economic evaluation of microwave pyrolysis of biomass to determine its viability. A commercial size bioenergy production was recently suggested, whereby a distributed bioenergy production strategy was proposed for the implementation on average-size farms to pyrolyze crop residues by exploiting the scalable fast microwave pyrolysis technology (169). The energy balance involved in the microwave pyrolysis of biomass is also an important issue. There are several reasons for the application of the use of microwave pyrolysis; first is the only little amount of energy needed to generate a high amount of heat and second is the efficiency of microwave heating during pyrolysis (70). There is little energy wasted and the majority of the dipole effect generated by the microwave is concentrated directly into the sample. Nevertheless, very few reports regarding energy input and output from microwave pyrolysis

| Reactor type         | Advantages                                      | Disadvantages                                      | Bio-oil yield (%) |
|----------------------|-------------------------------------------------|----------------------------------------------------|-------------------|
| Fixed bed            | Simple design, Reliable, Biomass size independent | High carbon conservation, Long solid residence time, Low ash carry over | 35–50%            |
| Bubbling fluidized bed | Simple design, Easy operation, Good temperature control, Suitable for large scale | Small particle sizes are needed                  | 70–75%            |
| Circulating fluidized bed | Well-understood technology, Good thermal control, Large particle sizes can be used | Unlikely to be suitable for large scale, Complex hydrodynamics, Char is finer | 70–75%            |
| Rotating cone        | Centrifugal force moves heated sand and biomass, No carrier gas required, Less wear | Complex process, Small particle sizes needed, Not proven yet for large scale, Slow process | 65%               |
| Vacuum               | Produces clean oil, Can process larger particles of 3–5 cm, No carrier gas required, Lower temperature required, Easier liquid product condensation | Solid residence time is too high, Require large-scale equipment, Poor heat and mass transfer rate, Generates more water | 35–50%            |
| Ablative             | Inert gas is not required, Large particle sizes can be processed, System is more intensive, Moderate temperature required | Reactor is costly, Low reaction rate, Low reaction rate | 70%               |
| Auger                | Compact, No carrier gas required, Lower process temperature | Moving parts in hot zone, Heat transfer in large scale is not suitable | 30–50%            |
| PyRos                | Compact and low cost, High heat transfer, Short gas residence time | Complex design, Solids in the oil, Alkaline dissolved in the oil, High temperature required | 70–75%            |
| Plasma               | High energy density, High heat transfer, High temperature, Very good control | High electrical power consumption, High operating costs, Small particle sizes required | 30–40%            |
| Microwave            | Efficient heat transfer, Exponential control, Compact, High heating rate, Large size biomass can be processed, Uniform temperature distribution, Moderate temperature | Economics of the process scaling-up | 60–70%            |
| Solar                | Use renewable energy, High heating rate, High temperature | High costs, Weather dependant | 40–60%            |
of waste material have been reported. One paper discussed the benefits of microwaves on pyrolysis of straw feedstock (170). The minimum microwave power was found to be about 0.371 kW (per kg straw) and the ratio of heat loss and conversion loss of electricity to microwave energy occupied in the total input energy was 42% (balancing against the energy content of the char, bio-oil, and gases). From the results presented in such a study, it can be derived that the energy efficiency of microwave pyrolysis of wheat straw is 79.8% (ratio between biofuel energy and the sum of energy required for pyrolysis plus energy content of biomass). In another report, the energy recovery from the raw biomass resulted in 91%, which is much higher compared to the energy recovery from similar biomass feedstock by the means of conventional flash pyrolysis technologies (35–39%) (171). Similarly, in a pyrolysis study at 500°C, using coffee hull as feedstock, the energy recovery from conventional pyrolysis was 84%, whereas it increased up to 99% using microwave technology (139). Table 13 summarizes the state of the art in microwave-assisted pyrolysis in comparison with different reactor types.

So far, there have been lesser research reported on the microwave pyrolysis of waste materials compared to microwave pyrolysis of other non-waste feedstocks. It has been reported that current microwave pyrolysis techniques offer a number of advantages and show excellent potential for treating waste materials. However, the current review still shows that there are gaps to be filled in order to fully exploit the advantages of using the microwave pyrolysis process in the treatment of waste materials, especially waste glycerol. The focus of using microwave pyrolysis is to provide an alternative pyrolysis process by making use of the high temperatures that the carbonaceous material can achieve when subjected to a microwave field. This alternative way of heating is reported to have advantages over other conventional pyrolysis processes on account of better heat transfer to the waste materials, good control over the heating process, as well as offering a sustainable processing route. However, in view of mainly positive findings reported in the literature on the microwave pyrolysis studies, it would be worthwhile to carry on researching further aspects of microwave pyrolysis of waste materials, especially waste glycerol from the biodiesel process in order to explore its full potential. The optimization of this process and the subsequent scale-up to a commercial scale is the next level of progression, and hence better understanding of the microwave technology knowledge is crucial.

8. Conclusions
Pyrolysis of agricultural residues and waste glycerol from the biodiesel industry can help to meet renewable energy targets by displacing fossil fuels and, thereby, deal with concerns about global warming. Besides the use of bio-oil and syngases, the other pyrolysis product, which is bio-char, can also be used for soil amendment and as a carbon-sequestering agent. With the growing production of biodiesel in the coming years, managing crude glycerol produced will become an increasingly difficult task. Although the development of glycerol-free biodiesel production is making progress significantly, implementation of these processes at a large scale still faces a number of challenges such as high costs, low efficiency, and lack of relevant technologies. It is crucial to utilize this waste stream generated from biodiesel production efficiently. Most of the current methods of utilization of crude glycerol are only able to uptake small volumes of the waste glycerol. Furthermore, the real costs of its utilization are uncertain. Pyrolysis of glycerol is a viable process for clean energy production. Liquid bio-oils, produced from the pyrolysis process, are a promising route to utilize large quantities of the waste glycerol. However, several key technical barriers must be addressed – (a) optimization of process conditions and catalyst performance to maximize bio-oil yield and quality while reducing the impact of feedstock variability and impurities; (b) improving the thermal stability of bio-oil and impurities be removed to facilitate economical upgrading to biofuels, and (c) maximizing carbon efficiency during bio-oil deoxygenation. One of the promising technologies for enhancement of bio-oil quality and quantity is by using the microwave-assisted pyrolysis process. Only few literatures are available on the microwave-assisted pyrolysis of waste glycerol. A more detailed study on the production of bio-oil from waste glycerol by microwave-assisted pyrolysis is needed in order to have a better understanding of the process parameters. Further research and development on microwave-assisted pyrolysis should focus on: (i) the types of microwave absorbents since it is necessary to achieve desired temperatures, (ii) improving catalyst selectivity, (iii) optimizing reaction conditions such as flow rate of inert gas to improve yield, (iv) study of the reaction kinetics of the overall process, and (v) study on the mechanism for microwave-assisted crude glycerol pyrolysis. The raw glycerol may also present some difficulties in feeding since it is liquid. For this reason, further studies must be done to reduce the water content in order to obtain a smaller concentrated volume of waste glycerol. The concentrated waste could be blended with a small portion of sawdust or...
similar waste to make the glycerol into a semi-solid paste. Finally, it can be concluded that the utilization of waste glycerol into higher value products through pyrolysis can potentially improve the issue of excess glycerol within the biodiesel industry. More work is needed to extend the existing understanding of the microwave technology for pyrolysis in order to improve the process and ultimately to transform it into a commercially viable route to recover energy from waste materials.

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