A MONOLITHIC DIVERGENCE-CONFORMING HDG SCHEME FOR A LINEAR FLUID-STRUCTURE INTERACTION MODEL

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ABSTRACT. We present a novel monolithic divergence-conforming HDG scheme for a linear fluid-structure interaction (FSI) problem with a thick structure. A pressure-robust optimal energy-norm estimate is obtained for the semidiscrete scheme. When combined with a Crank-Nicolson time discretization, our fully discrete scheme is energy stable and produces an exactly divergence-free fluid velocity approximation. The resulting linear system, which is symmetric and indefinite, is solved using a preconditioned MinRes method with a robust block algebraic multigrid (AMG) preconditioner.

1. Introduction

Fluid-structure interaction (FSI) describes a multi-physics phenomenon that involves the highly non-linear coupling between a deformable or moving structure and a surrounding or internal fluid. There has been intensive interest in solving FSI problems due to its wide applications in biomedical, engineering and architecture fields, such as the simulation of blood-cell interactions, the study of wing fluttering in aerodynamics and the design of dams with reservoirs. However, it is generally difficult to achieve analytical solution to FSI problem with its nonlinear and multi-physics nature. Instead, there have been extensive studies in its numerical solutions and an increasing demand for more efficient and accurate numerical schemes [8, 12, 14, 26, 38].

Numerical methodologies for solving FSI problems can be roughly categorized into partitioned and monolithic schemes. Distinct mechanisms in fluid and structure domains naturally suggest solvers using partitioned schemes [17, 36]. This numerical procedure treats each physical phenomenon separately and allows the use of existing software frameworks that are well-established for each subproblem. However, the design of efficient partitioned schemes that produce stable and accurate results remains a challenge, especially when the density of fluid is comparable to that of structure due to numerical instabilities known as added mass effect [10]. The design and analysis of partitioned schemes to circumvent such problems has been an active research area in the past decade [3, 6, 10, 18, 32]. An alternative to partitioned strategy is the monolithic approach, which solves the fluid flow and structure dynamics simultaneously using one unified fully-coupled formulation [27, 39, 43]. The boundary conditions on the fluid-structure interface will be automatically satisfied in the procedure. Monolithic schemes are usually more robust than partitioned schemes and allow more rigorous analysis of discretization and solution techniques [29, 38]. However, monolithic schemes have been criticized for requiring well-designed preconditioners [2, 23, 35], more memory and computation time since the whole system is solved in one formulation.

In this paper, we present a novel monolithic divergence-conforming HDG scheme for a linear FSI problem with a thick structure. The fluid Stokes problem is discretized using the divergence-free HDG scheme of Lehrenfeld and Schöberl [30, 31], and the structure linear elasticity problem is discretized using the divergence-conforming HDG scheme of Fu et al. [22]. We approximate the fluid and structure velocities together using a single $H(\text{div})$-conforming finite element space, and we also

2020 Mathematics Subject Classification. 65N30, 65N12, 76S05, 76D07.

Key words and phrases. Divergence-conforming HDG, FSI, thick structure, block preconditioner.

G. Fu gratefully acknowledges the partial support of this work from U.S. National Science Foundation through grant DMS-2012031.
introduce a global (hybrid) unknown that approximate the tangential component of the velocities on the mesh skeleton for the purpose of efficient implementation. A pressure-robust optimal energy-norm estimate is obtained for the resulting semidiscrete scheme. We then use a Crank-Nicolson time discretization, and the fluid-structure interface conditions are naturally treated monolithically. Our fully discrete scheme produces an exactly divergence-free fluid velocity approximation and is energy stable.

When polynomials of degree $k \geq 1$ is used in the scheme, the global linear system, which is symmetric and indefinite, consists of degrees of freedom (DOFs) for the normal component of velocity (of polynomial degree $k$) on the mesh skeleton (facets), the tangential hybrid velocity (of polynomial degree $k - 1$) on the mesh skeleton, and one pressure DOF per element on the mesh. The linear system problem is then solved via a preconditioned MinRes method [41] with a block diagonal preconditioner which is of similar form as the uniform preconditioner studied in Olshanskii et al. [37] for a generalized Stokes interface problem. We further use an auxiliary space preconditioner of Xu [44] with algebraic multigrid (AMG) for the velocity block and a hypre AMG preconditioner for the pressure block to arrive at the final block AMG preconditioner. This preconditioner is numerically verified to be robust with respect to mesh size, time step size, and material parameters.

The rest of the paper is organized as follows. In Section 2, we introduce the spatial and temporal discretization of the divergence-conforming HDG scheme for a linear FSI problem with a thick structure. We then present the block AMG preconditioner in Section 3. The a priori error analysis of the semidiscrete scheme is performed in Section 4. Numerical results are presented in Section 5. We conclude in Section 6.

2. The monolithic divergence-conforming HDG scheme for a linear FSI model

2.1. The model FSI problem. We consider the interaction between an incompressible, viscous fluid and an elastic structure. We denote by $\Omega_f(t) \subset \mathbb{R}^d$ the domain occupied by the fluid and $\Omega_s(t) \subset \mathbb{R}^d$, $d = 2, 3$ by the solid at the time $t \in [0, T]$. Let $\Gamma(t) = \overline{\Omega_f(t) \cap \partial \Omega_s(t)}$ be the part of the boundary where the elastic solid interacts with the fluid; see Fig. 1. For the purpose of this paper, we assume that the nonlinear convection term in the fluid is negligible and the solid is linearly elastic and the deformation is small. Hence, the domain $\Omega_f^t$ does not change over time, and the fluid flow is modeled using the time dependent Stokes equations while the structure is modeled

![Figure 1. Sketch of a domain for FSI.](image)
using the linear elastodynamics equations:

\begin{align}
\rho^f \partial_t u^f - \nabla \cdot \sigma^f (u^f, p^f) &= f^f \quad \text{in } \Omega^f \times [0,T], \\
\nabla \cdot u^f &= 0
\end{align}

\begin{align}
\rho^s \partial_t u^s - \nabla \cdot \sigma^s (u^s) &= f^s \quad \text{in } \Omega^s \times [0,T], \\
\partial_s \eta^s - u^s &= 0
\end{align}

where $\rho^f$ is the fluid density, $u^f$ is the fluid velocity, $p^f$ is the fluid pressure, $f^f$ is the fluid source term, and $\sigma^f$ is the fluid stress tensor given as follows:

$$
\sigma^f (u^f, p^f) := -p^f I + 2\mu^f D(u^f),
$$

where $I$ is the identity tensor, $\mu^f$ is the fluid viscosity, and $D(u^f) := \frac{1}{2}(\nabla u^f + (\nabla u^f)^T)$ is the fluid strain rate tensor, while $\rho^s$ is the structure density, $\eta^s$ is the structure displacement, $u^s$ is the structure velocity, $f^s$ is the structure source term, and $\sigma^s$ is the structure Cauchy stress tensor given as follows:

$$
\sigma^s (\eta^s) := \lambda^s (\nabla \cdot \eta^s) I + 2\mu^s D(\eta^s),
$$

where $\mu^s$ and $\lambda^s$ are the Lamé constants.

The fluid and structure sub-problems are coupled with the following kinematic and dynamic coupling conditions \cite{38} on the interface $\Gamma$:

\begin{align}
\sigma^f n^f + \sigma^s n^s &= 0 \quad \text{on } \Gamma \times [0,T],
\end{align}

where $n^f$ and $n^s$ are the normal directions on the fluid-structure interface $\Gamma$ pointing from the fluid and structure domains, respectively.

To close the system, we need proper initial and boundary conditions. For simplicity, in our analysis we consider a homogeneous Dirichlet boundary conditions on the exterior boundaries:

\begin{align}
\left. u^f \right|_{\Gamma^f} &= 0 \quad \text{on } \Gamma^f := \partial \Omega^f \setminus \Gamma, \\
\left. \eta^f \right|_{\Gamma^f} &= 0 \\
\left. u^s \right|_{\Gamma^s} &= 0 \quad \text{on } \Gamma^s := \partial \Omega^s \setminus \Gamma.
\end{align}

We mention that other standard boundary conditions on the exterior boundaries can also be used, see e.g. the numerical results in Section \cite{5}. Finally, the initial condition is given as follows:

\begin{align}
\left. u^f \right|_{(x, 0)} &= u^f_0 (x) \quad \text{on } \Omega^f, \\
\left. u^s \right|_{(x, 0)} &= u^s_0 (x), \\
\left. \eta^f \right|_{(x, 0)} &= \eta^s_0 (x),
\end{align}

where $u^f_0, u^s_0, \text{ and } \eta^s_0$, respectively, are the initial fluid velocity, initial structure velocity, and initial structure displacement, respectively.

2.2. Preliminaries and finite element spaces. We assume the domains $\Omega^f, \Omega^s$, as well as the interface $\Gamma$ are polypope. Let $\Omega$ be the union of the fluid and structure domains, i.e., $\Omega = \Omega^f \cup \Omega^s$. Let $\mathcal{T}_h$ be an interface-fitted conforming simplicial triangulation of the domain $\Omega$ such that the interface $\Gamma$ is the union of element facets. For any element $K \in \mathcal{T}_h$, we denote by $h_K$ its diameter and we denote by $h$ the maximum diameter over all mesh elements. Denote by $\mathcal{E}_h^f$ the set of mesh elements that belong to $\Omega^f$ and by $\mathcal{E}_h^s$ those belong to $\Omega^s$. Denote by $\mathcal{E}_h$ the set of facets of $\mathcal{T}_h$, by $\mathcal{E}_h^f$ the set of facets that are interior to $\Omega^f$, and by $\mathcal{E}_h^s$ the set of facets that are interior to $\Omega^s$. We also denote by $\Gamma_h, \Gamma_h^f, \Gamma_h^s$ the set of facets that lie on the interface $\Gamma$, the fluid exterior boundary $\Gamma^f$, and the solid exterior boundary $\Gamma^s$, respectively. We have $\Gamma_h = \mathcal{E}_h^f \cap \mathcal{E}_h^s$. Given a simplex $S \subset \mathbb{R}^d, d = 1, 2, 3$, we denote $\mathcal{P}^m (S)$, $m \geq 0$, as the space of polynomials of degree at most $m$. Given a facet $F \in \mathcal{E}_h$ with normal direction $n$, we denote $\text{tang}(w) := w - (w \cdot n)n$ as the tangential component of a vector field $w$. 

\[DIV-HDG\]
The following finite element spaces will be used in our scheme:

(2a) \[ V^r_h := \{ v \in H(\text{div}; \Omega) : v|_K \in \mathcal{P}^r(K)^d, \forall K \in \mathcal{T}_h \}, \]

(2b) \[ V^r_{h,0} := \{ v \in V^r_h : v \cdot n|_F = 0, \forall F \in \Gamma^f_h \cup \Gamma^s_h \}, \]

(2c) \[ \tilde{V}^r_h := \{ \tilde{v} \in L^2(\mathcal{E}_h)^d : \tilde{v}|_F \in \mathcal{P}^r(F)^d, \tilde{v} \cdot n|_F = 0, \forall F \in \mathcal{E}_h \}, \]

(2d) \[ \tilde{V}^r_{h,0} := \{ \tilde{v} \in \tilde{V}^r_h : \text{tang}(\tilde{v})|_F = 0, \forall F \in \Gamma^f_h \cup \Gamma^s_h \}, \]

(2e) \[ Q^r_h := \{ q \in L^2(\Omega) : q|_K \in \mathcal{P}^r(K), \forall K \in \mathcal{T}_h \}, \]

where \( r \geq 0 \) is the polynomial degree. We further use a superscript \( f/s \) to indicate the restriction of these spaces on the fluid/structure domain, that is,

\[ V^{r,f}_{h,0} := \{ v|_{\Gamma^f_h} : v \in V^{r}_{h,0} \}, \quad V^{r,s}_{h,0} := \{ v|_{\Gamma^s_h} : v \in V^{r}_{h,0} \}, \]

\[ \tilde{V}^{r,f}_{h,0} := \{ \tilde{v}|_{\Gamma^f_h} : \tilde{v} \in \tilde{V}^{r}_{h,0} \}, \quad \tilde{V}^{r,s}_{h,0} := \{ \tilde{v}|_{\Gamma^s_h} : \tilde{v} \in \tilde{V}^{r}_{h,0} \}, \]

\[ Q^{r,f}_{h} := \{ q|_{\Gamma^f_h} : q \in Q^r_h \}, \quad Q^{r,s}_{h} := \{ q|_{\Gamma^s_h} : q \in Q^r_h \}. \]

2.3. Semi-discrete divergence-conforming HDG scheme. In this subsection, we present the divergence-conforming HDG spatial discretization \cite{22,30,31} of the linear FSI system \cite{1}.

We use the globally divergence-conforming finite element space \( V^r_h \) in (2b) to approximate the global velocity

\[ u = \begin{cases} u^f & \text{on } \Omega^f, \\ u^s & \text{on } \Omega^s, \end{cases} \tag{3} \]

and the global tangential facet finite element space \( \tilde{V}^r_h \) in (2d) to approximate the tangential component of the global velocity \( u \) on the mesh skeleton.

The weak formulation of the divergence-conforming HDG scheme with polynomial degree \( k \geq 1 \) for \cite{1} is given as follows: Find \( (u_h, \tilde{u}_h, p^f_h, \eta^s_h, \tilde{\eta}^s_h) \in V_h^k \times \tilde{V}_h^{k-1} \times Q_h^{k-1,f} \times V_h^{k,s} \times \tilde{V}_h^{k-1,s} \) such that

\[ (\rho \partial_t u_h, v_h) + 2 \mu^f A^f_h((u_h, \tilde{u}_h), (v_h, \tilde{v}_h)) - (p^f_h, \nabla \cdot v_h)_f - (\nabla \cdot u_h, q^f_h)_f + 2 \mu^s A^s_h((\eta^s_h, \tilde{\eta}^s_h), (v_h, \tilde{v}_h)) + \lambda^s (\nabla \cdot \eta^s_h, \nabla \cdot v_h)_s = (f, v_h), \]

\[ (\partial_t \eta^s_h - u_h, \xi^s_h)_s = 0, \]

\[ \langle \partial_t \tilde{\eta}^s_h - \tilde{u}_h, \tilde{\xi}^s_h \rangle_s = 0, \tag{4c} \]

for all \( (v_h, \tilde{v}_h, q^f_h, \xi^s_h, \tilde{\xi}^s_h) \in V_h^k \times \tilde{V}_h^{k-1} \times Q_h^{k-1,f} \times V_h^{k,s} \times \tilde{V}_h^{k-1,s} \), where \( (\cdot, \cdot) \) denotes the \( L^2 \)-inner product on the domain \( \Omega \), \( (\cdot, \cdot)_f \) denotes the \( L^2 \)-inner product on the fluid domain \( \Omega^f \), \( (\cdot, \cdot)_s \) denotes the \( L^2 \)-inner product on the structure domain \( \Omega^s \), and \( \langle \cdot, \cdot \rangle_s \) denotes the \( L^2(\mathcal{E}_h^s) \)-inner product on the structure mesh skeleton \( \mathcal{E}_h^s \); moreover, \( \rho = \begin{cases} \rho^f & \text{on } \Omega^f \\ \rho^s & \text{on } \Omega^s \end{cases} \) is the global density and \( f = \begin{cases} f^f & \text{on } \Omega^f \\ f^s & \text{on } \Omega^s \end{cases} \) is the global source term on \( \Omega \). Here the operators \( A^f_h \) and \( A^s_h \) are the following symmetric interior penalty HDG diffusion operators with a projected jumps formulation:
for $i \in \{f, s\}$,

(5) $$A_h^i((v_h, \tilde{v}_h), (w_h, \tilde{w}_h)) = \sum_{K \in T_h^f} \int_K D(v_h) : D(w_h) \, dx - \int_{\partial K} D(v_h) n \cdot \text{tang}(w_h - \tilde{w}_h) \, ds$$

$$- \int_{\partial K} D(w_h) n \cdot \text{tang}(v_h - \tilde{v}_h) \, ds + \int_{\partial K} \frac{\alpha h^2}{k} \Pi_h(\text{tang}(v_h - \tilde{v}_h)) \cdot \Pi_h(\text{tang}(w_h - \tilde{w}_h)) \, ds,$$

where $\Pi_h$ denotes the $L^2(\mathcal{E}_h)$-projection onto the tangential facet finite element space $V_h^{k-1}$. Efficient implementation of this local projector $\Pi_h$ was discussed in [31, Section 2.2]. Here $\alpha > 0$ is a sufficiently large stabilization parameter that ensures the following coercivity result:

(6) $$A_h^i((v_h, \tilde{v}_h), (v_h, \tilde{v}_h)) \geq \frac{1}{2} \sum_{K \in T_h^f} \left( \|D(v_h)\|_K^2 + \frac{\alpha h^2}{k} \|\Pi_h(\text{tang}(v_h - \tilde{v}_h))\|_{\partial K}^2 \right),$$

where $\| \cdot \|_S$ indicates the $L^2$-norm on the domain $S$. A sufficient condition on $\alpha$ that guarantees the above coercivity result was presented in [1, Lemma 1]. We take $\alpha = 8$ in our numerical experiments in Section 5.

The following two results show consistency and stability of the semi-discrete scheme [4].

**Lemma 2.1** (Galerkin-orthogonality for the semi-discrete scheme). Let $(u, p^f, \eta^s) \in H^2(\Omega) \times H^1(\Omega)^f \times H^2(\Omega)^s$ be the solution to the model problem [1]. Then, the equations [1] holds true with $(u_h, \tilde{u}_h, p_h^f, \eta_h^s, \tilde{\eta}_h^s)$ replaced by $(u, u|_{\mathcal{E}_h}, p^f, \eta^s, \eta^s|_{\mathcal{E}_h}|_{\mathcal{E}_h})$. That is, we have

(7a) $$(\rho \partial_t u, v_h) + 2\mu^f A^f_h((u, \tilde{u}), (v_h, \tilde{v}_h)) - (p^f, \nabla \cdot v_h)_f - (\nabla \cdot u, q^f_h)_f + 2\mu^s A^s_h((\eta^s, \tilde{\eta}^s), (v_h, \tilde{v}_h)) + \lambda^s (\nabla \cdot \eta^s, \nabla \cdot v_h)_s = (f, v_h),$$

(7b) $$(\partial_t \eta^s - u, \xi^s_h)_s = 0,$$

(7c) $$\langle \partial_t \tilde{\eta}^s - \tilde{u}, \xi^s_h \rangle_s = 0,$$

for all $(v_h, \tilde{v}_h, q^f_h, \xi^s_h, \tilde{\xi}^s_h) \in V_{h,0}^1 \times V_{h,0}^{k-1} \times Q_{h,0}^{k-1} \times V_{h,0}^s \times V_{h,0}^{k-1}$. Here $\tilde{u} = u|_{\mathcal{E}_h}$ and $\tilde{\eta}^s = \eta^s|_{\mathcal{E}_h}$.

**Proof.** The equations (7b) and (7c) follows from the second equation in (1b). We are left to prove the equation (7a). Since $\text{tang}(u - \tilde{u}) = 0$, we have, for any function $(v_h, \tilde{v}_h) \in V_{h,0}^1 \times \hat{V}_{h,0}^{k-1}$,

$$A_h^f((u, \tilde{u}), (v_h, \tilde{v}_h)) = \sum_{K \in T_h^f} \int_K D(u) : D(v_h) \, dx - \int_{\partial K} D(u) n \cdot \text{tang}(v_h - \tilde{v}_h) \, ds$$

$$= - (\nabla \cdot D(u), v_h)_f + \sum_{K \in T_h^f} \int_{\partial K} D(u) n \cdot ((v_h \cdot n) + \text{tang}(\tilde{v}_h)) \, ds$$

$$= - (\nabla \cdot D(u), v_h)_f + \int_{\Gamma_h} D(u) n^f \cdot ((v_h \cdot n) + \text{tang}(\tilde{v}_h)) \, ds.$$
Combining these equations, we get

\[
(\rho \partial_t \mathbf{u}, \mathbf{v}_h) + 2\mu^f A^f_{h}((\mathbf{u}, \tilde{\mathbf{u}}), (\mathbf{v}_h, \tilde{\mathbf{v}}_h)) - (\rho^f, \nabla \cdot \mathbf{v}_h)_f - (\nabla \cdot \mathbf{u}, q^f_h)_f \\
+ 2\mu^s A^s_{h}((\eta^s, \tilde{\eta}^s), (\mathbf{v}_h, \tilde{\mathbf{v}}_h)) + \lambda^s(\nabla \cdot \eta^s, \nabla \cdot \mathbf{v}_h)_s - (f, \mathbf{v}_h) \\
= (\rho^f \partial_t \mathbf{u} - \nabla \cdot \mathbf{s}^f - f^f, \mathbf{v}_h)_f + (\rho^s \partial_t \mathbf{s}^s - \nabla \cdot \mathbf{s}^s, \mathbf{v}_h)_s \\
+ \int_{\Gamma_h} (\sigma^f \mathbf{n}^f + \sigma^s \mathbf{n}^s)((\mathbf{v}_h \cdot \mathbf{n}) \cdot \mathbf{n} + \tan(\tilde{\mathbf{v}}_h)) ds \\
= 0,
\]

where we used the PDE (1a), (1b), and the dynamic interface condition in (1c). This completes the proof of the equation (7a). \( \square \)

**Lemma 2.2** (Stability for the semi-discrete scheme). Let \((\mathbf{u}_h, \tilde{\mathbf{u}}_h, p^f_{h, \eta^s_h, \tilde{\eta}^s_h}) \in V^k \times \tilde{V}^k \times Q^k \) be the numerical solution to the semi-discrete scheme (4). Then, the velocity approximation on the fluid domain is exactly divergence free:

\[
(8) \quad \nabla \cdot \mathbf{u}_h|_{\Gamma_h^f} = 0,
\]

and the following energy identity holds:

\[
(9) \quad \frac{1}{2} \frac{d}{dt} E_h = -2\mu^f A^f_{h}((\mathbf{u}_h, \tilde{\mathbf{u}}_h), (\mathbf{u}_h, \tilde{\mathbf{u}}_h)) + (f, \mathbf{u}_h),
\]

where \( E_h := (\rho \mathbf{u}_h, \mathbf{u}_h) + \lambda^s(\nabla \cdot \eta^s_h, \nabla \cdot \mathbf{u}_h) + 2\mu^s A^s_{h}((\eta^s_h, \tilde{\eta}^s_h), (\eta^s_h, \tilde{\eta}^s_h)) \) is the total energy.

**Proof.** Let us first prove the divergence-free property (8). By the choice of the velocity finite element space \( V^k \) and fluid pressure finite element space \( Q_h \), we have \( \nabla \cdot \mathbf{u}_h|_{\Gamma_h^f} \in Q^k_{h-f} \). Now taking \( q^f_h = \nabla \cdot \mathbf{u}_h|_{\Gamma_h^f} \) in equation (4a), we get

\[
(\nabla \cdot \mathbf{u}_h, \nabla \cdot \mathbf{u}_h)_f = 0.
\]

Hence the divergence-free property (8) holds true.

Next, let us prove the energy identity (9). Taking test function \((\mathbf{v}_h, \tilde{\mathbf{v}}_h) = (\mathbf{u}_h, \tilde{\mathbf{u}}_h)\) in equation (4a), and using the divergence-free property (8), we get

\[
(\rho \partial_t \mathbf{u}_h, \mathbf{u}_h) + 2\mu^f A^f_{h}((\mathbf{u}_h, \tilde{\mathbf{u}}_h), (\mathbf{u}_h, \tilde{\mathbf{u}}_h)) + 2\mu^s A^s_{h}((\eta^s_h, \tilde{\eta}^s_h), (\eta^s_h, \tilde{\eta}^s_h)) + \lambda^s(\nabla \cdot \eta^s_h, \nabla \cdot \mathbf{u}_h)_s = (f, \mathbf{v}_h).
\]

Since \( \mathbf{u}_h|_{\Gamma_h^s} \in V^k, \tilde{\mathbf{u}}_h|_{\tilde{\Gamma}_h^s} \in \tilde{V}^k, \) equations (4b)–(4c) implies that

\[
\mathbf{u}_h|_{\Gamma_h^s} = \partial_t \eta^s_h, \text{ and } \tilde{\mathbf{u}}_h|_{\tilde{\Gamma}_h^s} = \partial_t \tilde{\eta}^s_h.
\]

Hence,

\[
2\mu^s A^s_{h}((\eta^s_h, \tilde{\eta}^s_h), (\mathbf{u}_h, \tilde{\mathbf{u}}_h)) = 2\mu^s A^s_{h}((\eta^s_h, \tilde{\eta}^s_h), (\partial_t \eta^s_h, \partial_t \tilde{\eta}^s_h)) = \frac{1}{2} \frac{d}{dt} (2\mu^s A^s_{h}((\eta^s_h, \tilde{\eta}^s_h), (\eta^s_h, \tilde{\eta}^s_h))),
\]

and

\[
\lambda^s(\nabla \cdot \eta^s_h, \nabla \cdot \mathbf{u}_h)_s = \frac{1}{2} \frac{d}{dt} (\lambda^s(\nabla \cdot \eta^s_h, \nabla \cdot \eta^s_h)_s).
\]

Combining the above equations, we arrive at the energy identity (9). This completes the proof. \( \square \)
2.4. Monolithic fully discrete divergence-conforming HDG scheme. In this subsection, we consider the temporal discretization of the semi-discrete scheme [11]. We propose to use the second-order Crank-Nicolson scheme. For any positive integer \( j \in \mathbb{Z}_+ \), let \((u_h^{j-1}, \eta_h^{s,j-1}, \hat{\eta}_h^{s,j-1}) \in V_{h,0}^k \times V_{h,0}^{s,k} \times \hat{V}_{h,0}^{k,s} \) be the numerical solution at time \( t_{j-1} \). Give the time step size \( \delta t_{j-1} > 0 \), we proceed to find the solution \((u_h^{j}, \eta_h^{s,j}, \hat{\eta}_h^{s,j}) \in V_{h,0}^k \times V_{h,0}^{s,k} \times \hat{V}_{h,0}^{k,s} \) at time \( t_j = t_{j-1} + \delta t_{j-1} \) along with the solution \((\hat{u}_h^{j-1/2}, \hat{p}_h^{j-1/2}) \in \hat{V}_{h,0}^{k-1,f} \times Q_{h,0}^{k-1,f} \) at time \( t_{j-1/2} = t_{j-1} + \frac{1}{2} \delta t_{j-1} \) such that the following equations hold:

\[
(10a) \quad (\rho \frac{u_h^{j} - u_h^{j-1}}{\delta t_{j-1}}, v_h) + 2 \mu_f A_h((u_h^{j-1/2}, \tilde{u}_h^{j-1/2}, (v_h, \tilde{v}_h)) - (p_h^{j-1/2}, \nabla \cdot v_h)_f
\]

\[
- (\nabla \cdot u_h^{j-1/2}, q_h^{f})_f + 2 \mu_s A_h((\eta_h^{s,j-1/2}, \tilde{\eta}_h^{s,j-1}), (v_h, \tilde{v}_h)) + \lambda_s (\nabla \cdot \eta_h^{s,j-1}, \nabla \cdot v_h)_s = (f^{j-1/2}, v_h),
\]

\[
(10b) \quad \frac{\eta_h^{s,j} - \eta_h^{s,j-1}}{\delta t_{j-1}} - u_h^{j-1/2}, \xi_h^{s,j}_s = 0,
\]

\[
(10c) \quad \frac{\eta_h^{s,j} - \eta_h^{s,j-1}}{\delta t_{j-1}} - \hat{u}_h^{j-1/2}, \xi_h^{s,j}_h = 0,
\]

for all \((v_h, \tilde{v}_h, \eta_h^{s,j}, \xi_h^{s,j}, \hat{\xi}_h^{s,j}) \in V_{h,0}^k \times \hat{V}_{h,0}^{k-1,f} \times V_{h,0}^{s,k} \times \hat{V}_{h,0}^{k,s} \), where

\[
u_h^{j-1/2} := \frac{1}{2}(u_h^{j} + u_h^{j-1}), \quad \eta_h^{s,j-1/2} := \frac{1}{2}(\eta_h^{s,j} + \eta_h^{s,j-1}), \quad \hat{\eta}_h^{s,j-1/2} := \frac{1}{2}(\hat{\eta}_h^{s,j} + \hat{\eta}_h^{s,j-1}),
\]

We have the following result on the energy stability of the fully discrete scheme \(10\).

**Lemma 2.3** (Stability for the fully discrete scheme). Let \((u_h^{0}, \eta_h^{s,0}, \hat{\eta}_h^{s,0}) \in V_{h,0}^k \times V_{h,0}^{s,k} \times \hat{V}_{h,0}^{k,s} \) be a proper projection of the initial data in \([11]\) such that \( \nabla \cdot u_h^{0} |_{\tau_h} = 0 \). For any positive integer \( j \in \mathbb{Z}_+ \), let \((u_h^{j}, \hat{u}_h^{j-1/2}, \hat{p}_h^{j-1/2}, \eta_h^{s,j}, \hat{\eta}_h^{s,j}) \in V_{h,0}^k \times \hat{V}_{h,0}^{k-1,f} \times V_{h,0}^{s,k} \times \hat{V}_{h,0}^{k,s} \) be the numerical solution to the fully discrete scheme \(10\). Then, the velocity approximation on the fluid domain is exactly divergence free:

\[
(11) \quad \nabla \cdot u_h^{j} |_{\tau_h} = 0,
\]

and the following energy identity holds true:

\[
(12) \quad \frac{1}{2} E_h^{j} - E_h^{j-1} = -2 \mu_f A_h ((u_h^{j-1/2}, \tilde{u}_h^{j-1/2}, (v_h, \tilde{v}_h), (u_h^{j-1/2}, \tilde{u}_h^{j-1/2})), (f^{j-1/2}, u_h),
\]

where \( E_h^{j} := (\rho u_h^{j}, u_h^{j}) + \lambda_s (\nabla \cdot \eta_h^{s,j}, \nabla \cdot \eta_h^{s,j}) + 2 \mu_s A_h ((\eta_h^{s,j}, \xi_h^{s,j}), (\eta_h^{s,j}, \xi_h^{s,j})) \) is the total energy at time \( t_j \).

**Proof.** The proof follows the same line as those for the semi-discrete case in Lemma 2.2, which we omit for simplicity. \( \square \)

2.4.1. Efficient implementation of the fully discrete scheme \([10]\). We now present an efficient implementation of the scheme \([10]\) whose globally coupled linear system consists of DOFs for the normal component of the velocity approximation, the tangential component of the hybrid velocity approximation on the mesh skeleton, and one pressure DOF per element on the mesh.

We need the following result on the characterization of the fully discrete solution.

**Lemma 2.4** (Characterization of the fully discrete solution). For any positive integer \( j \in \mathbb{Z}_+ \), let \((u_h^{j}, \hat{u}_h^{j-1/2}, \hat{p}_h^{j-1/2}, \eta_h^{s,j}, \hat{\eta}_h^{s,j}) \in V_{h,0}^k \times \hat{V}_{h,0}^{k-1,f} \times V_{h,0}^{s,k} \times \hat{V}_{h,0}^{k,s} \) be the numerical solution
to the fully discrete scheme \((10)\). Then, \((u_j^{j-1/2}, \tilde{u}_j^{j-1/2}, p_j^{f,j-1/2}) \in V_{h,0}^k \times \hat{V}_{h,0}^{k-1} \times Q_h^{k-1,f}\) is the unique solution to the following equations:

\((13a)\)

\[
\begin{align*}
(2\rho \frac{u_j^{j-1/2}}{\delta t_j^{-1}}, v_h) + 2\mu f ((u_j^{j-1/2}, \tilde{u}_j^{j-1/2}), (v_h, \tilde{v}_h)) & \\
- (p_j^{f,j-1/2}, \nabla \cdot v_h) - (\nabla \cdot u_j^{j-1/2}, q_h)_f & \\
+ \frac{1}{2}\delta t_j^{-1} \left( 2\mu^s A_h^s(\eta^{s,j-1}, \tilde{\eta}_h^{s,j-1}), (v_h, \tilde{v}_h) \right) + \lambda^s (\nabla \cdot \eta^{s,j-1}, \nabla \cdot v_h) & = F_j^{1/2}((v_h, \tilde{v}_h))
\end{align*}
\]

for all \((v_h, \tilde{v}_h, q_h)^f \in V_{h,0}^k \times \hat{V}_{h,0}^{k-1} \times Q_h^{k-1,f}\), where the right hand side

\((13b)\)

\[
F_j^{1/2}((v_h, \tilde{v}_h)) = (2\rho \frac{u_j^{j-1}}{\delta t_j^{-1}}, v_h) + (f_j^{1/2}, v_h)
\]

\[- (2\mu^s A_h^s(\eta^{s,j-1}, \tilde{\eta}_h^{s,j-1}), (v_h, \tilde{v}_h)) + \lambda^s (\nabla \cdot \eta^{s,j-1}, \nabla \cdot v_h) \],

where \(f_j^{1/2}\) is the source term evaluated at time \(t_j^{-1/2}\). Moreover, the velocity and displacement approximations at time \(t_j\) satisfy the following relations:

\((13c)\)

\[
\begin{align*}
u_j^{j} = 2u_j^{j-1/2} - u_j^{-1}, \quad \eta_j^{s,j} = \eta_j^{s,j-1} + \delta t_j^{-1} u_j^{j-1/2}|_{\tau_h}, \quad \tilde{\eta}_h^{s,j} = \tilde{\eta}_h^{s,j-1} + \delta t_j^{-1} \tilde{u}_h^{j-1/2}|_{\tau_h}.
\end{align*}
\]

**Proof.** The relations \((13c)\) are direct consequences of the definition of \(u_j^{j-1/2}\), the same choice of the finite element spaces for velocity and displacement, and the equations \((10b)-(10c)\). Plugging in these relations back to the equations \((10a)\), and reordering the terms, we recover the equations \((13a)\). This completes the proof. \(\square\)

**Remark 2.1 (Connection with the coupled momentum method).** The idea of using the same finite element space for displacement and velocity approximations to eliminate the displacement unknowns in the global linear system was originated in the coupled momentum method of Figueroa et al. \((19)\), where they considered an FSI problem with thin structure. See also related work in \((36)\).

With the help of Lemma \((2.4)\) we proceed to implement the fully discrete scheme \((10)\) as follows: Let \((u_h^0, \eta_h^0, \tilde{\eta}_h^0) \in V_{h,0}^k \times V_{h,0}^{k,s} \times \hat{V}_{h,0}^{k-1,s}\) be a proper projection of the initial data in \((1e)\). For \(j = 1, 2, \cdots\), we proceed the following three steps to advance solution from time level \(t_{j-1}\) to time level \(t_j = t_{j-1} + \delta t_{j-1}:\)

1. Determine the time step size \(\delta t_{j-1}\) and compute the right hand side \(F_j^{1/2}\) in \((13b)\).
2. Solve for \((u_j^{j-1/2}, \tilde{u}_j^{j-1/2}, p_j^{f,j-1/2}) \in V_{h,0}^k \times \hat{V}_{h,0}^{k-1} \times Q_h^{k-1,f}\) using equations \((13a)\).
3. Recover velocity and displacement approximations at time \(t_j\) using the relations \((13c)\).

The major computational cost of the above implementation lies in the global linear system solver in step (2). To make the linear system problem easier to solve, we introduce an equivalent characterization of the solution to the equations \((13a)\) in Lemma \((2.5)\) below. In the actual implementation, we solve the equivalent linear system problem \((14)\) in step (2) instead of \((13a)\). In the next section, we will design an efficient block AMG preconditioner for this system.
Lemma 2.5 (A modified implementation of the scheme (13a)). For any positive integer $j \in \mathbb{Z}_+$, let $(u_h^{j-1/2}, v_h^{j-1/2}, p_h^{j-1/2}) \in \mathbf{V}^k_{h,0} \times \hat{\mathbf{V}}^{k-1}_{h,0} \times Q^{k-1}_h$ be the unique solution to the following equations:

\[(14) \quad (2\rho \frac{u_h^{j-1/2}}{\delta t_{j-1}}, v_h) + 2\mu f A_h^f((u_h^{j-1/2}, v_h^{j-1/2}), (v_h, \hat{v}_h)) + \delta t_{j-1} \mu s A_h^s(u_h^{j-1/2}, (v_h, \hat{v}_h)) \]

\[-(p_h^{j-1/2}, \nabla \cdot v_h) - (\nabla \cdot u_h^{j-1/2}, q_h) - (\frac{2}{\delta t_j - 1}) \rho_s p_h^{j-1/2}, q_h)_s = F^{j-1/2}((v_h, \hat{v}_h))
\]

for all $(v_h, \hat{v}_h, q_h) \in \mathbf{V}^k_{h,0} \times \hat{\mathbf{V}}^{k-1}_{h,0} \times Q^{k-1}_h$, where the right hand side $F^{j-1/2}$ is defined in (13b). Then $(u_h^{j-1/2}, v_h^{j-1/2}, p_h^{j-1/2}) \in \mathbf{V}^k_{h,0} \times \hat{\mathbf{V}}^{k-1}_{h,0} \times Q^{k-1}_h$ is the unique solution to the equations (13a).

Proof. Taking test function $q_h \in Q^{k-1,s}_h$ in equations (14), we get

\[\nabla \cdot u_h^{j-1/2} + \frac{2}{\delta t_{j-1}} \lambda^s p_h^{j-1/2}, q_h)_s = 0 \quad \forall q_h \in Q^{k-1,s}_h.
\]

Since $\nabla \cdot u_h^{j-1/2}|_{T_h} \in Q^{k-1,s}_h$, the above equation implies that

\[p_h|_{T_h} = -\frac{\delta t_{j-1} \lambda^s}{2} \nabla \cdot u_h^{j-1/2}|_{T_h}.
\]

Hence,

\[-(p_h^{j-1/2}, \nabla \cdot v_h) = -(p_h^{j-1/2}, \nabla \cdot v_h)_f + \frac{\delta t_{j-1} \lambda^s}{2} \nabla \cdot u_h^{j-1/2}, \nabla \cdot v_h)_s.
\]

Plugging this expression back to the equations (14), we recover the equations in (13a) for all $(v_h, \hat{v}_h, q_h) \in \mathbf{V}^k_{h,0} \times \hat{\mathbf{V}}^{k-1}_{h,0} \times Q^{k-1}_h$. This completes the proof. \qed

Remark 2.2 (Other high-order implicit time stepping strategies). We concentrated on the discretization and implementation of the Crank-Nicolson time stepping (10) in this subsection. Alternatively, one can use any other high-order implicit time stepping strategies, like the backward difference formula (BDF) or the diagonally implicit Runge-Kutta methods [24]. The third-order BDF3 scheme reads as follows (assuming uniform time step size $\delta t > 0$): For $j \geq 3$, given approximations $(u_h^{j-1}, \eta_h^{j-1}, \hat{\eta}_h^{j-1}, \hat{\xi}_h^{j-1}) \in \mathbf{V}^k_{h,0} \times \mathbf{V}^k_{h,0} \times \hat{\mathbf{V}}^{k-1}_{h,0} \times \hat{\mathbf{V}}^{k-1}_{h,0}$ at time $t_{j-1} = (j - m) \delta t$ for $m = 1, 2, 3$, we proceed to find the solution $(u_h^j, \hat{u}_h^j, q_h^j, \eta_h^j, \hat{\eta}_h^j, \hat{\xi}_h^j) \in \mathbf{V}^k_{h,0} \times \hat{\mathbf{V}}^{k-1}_{h,0} \times Q^f \times \mathbf{V}^k_{h,0} \times \hat{\mathbf{V}}^{k-1}_{h,0}$ at time $t_j = j \delta t$ such that the following equations hold:

\[(15a) \quad (\rho \partial_t u_h^j, v_h) + 2\mu f A_h^f((u_h^j, \hat{u}_h^j), (v_h, \hat{v}_h)) - (p_h^j, \nabla \cdot v_h)_f
\]

\[-(\nabla \cdot u_h^j, q_h^j)_f + 2\mu s A_h^s((\eta_h^j, \hat{\eta}_h^j), (v_h, \hat{v}_h)) + \lambda^s(\nabla \cdot \eta_h^j, \nabla \cdot v_h)_s = (f^j, v_h),
\]

\[(15b) \quad (\partial_t \eta_h^j - u_h^{j-1/2}, \xi_h^j)_s = 0,
\]

\[(15c) \quad (\partial_t \hat{\eta}_h^j - \hat{\xi}_h^{j-1/2}, \hat{\xi}_h^j)_s = 0,
\]

for all $(u_h, \hat{v}_h, q_h, \hat{\xi}_h, \hat{\xi}_h) \in \mathbf{V}^k_{h,0} \times \hat{\mathbf{V}}^{k-1}_{h,0} \times Q^{k-1,f} \times \mathbf{V}^k_{h,0} \times \hat{\mathbf{V}}^{k-1}_{h,0}$, where

\[\partial_t \phi^j := \frac{1}{\delta t} \left( \frac{11}{6} \phi^j - 3 \phi^{j-1} + \frac{3}{2} \phi^{j-2} - \frac{1}{3} \phi^{j-3} \right)
\]
3. Preliminaries

In this section, we concentrate ourselves to the efficient solver for the linear system problem \( [14] \). The same technique can be used to solve the related linear system for the scheme based on BDF3 time stepping \( [15] \). To simplify notation, we remove all temporal indices in this section. Hence the linear system problem we are interested in have the following specific form: Find \( (\mathbf{u}_h, \mathbf{u}_h, p_h) \in \mathbf{V}_{h,0}^k \times \mathbf{V}_{h,0}^{k-1} \times Q_h^{k-1} \) such that

\[
(2\rho \frac{\partial \mathbf{u}_h}{\partial t}, \mathbf{v}_h) + 2\mu f A^f_h((\mathbf{u}_h, \mathbf{u}_h), (\mathbf{v}_h, \mathbf{v}_h)) + \delta t \mu \gamma A_h^s((\mathbf{u}_h, \mathbf{u}_h), (\mathbf{v}_h, \mathbf{v}_h)) - (p_h, \nabla \cdot \mathbf{v}_h) - (\nabla \cdot \mathbf{u}_h, q_h) - \frac{2}{\delta t \lambda} (p_h, q_h) = F((\mathbf{v}_h, \mathbf{v}_h))
\]

for all \( (\mathbf{v}_h, \mathbf{v}_h, q_h) \in \mathbf{V}_{h,0}^k \times \mathbf{V}_{h,0}^{k-1} \times Q_h^{k-1} \). Note that all the finite element spaces are defined on the whole domain \( \Omega \). To further simplify notation, we denote

\[
\mu := \left\{ \begin{array}{ll} \mu_f & \text{on } \Omega_f \\ 0.5\delta t \mu_g & \text{on } \Omega_g \end{array} \right., 
\gamma := \left\{ \begin{array}{ll} 0 & \text{on } \Omega_f \\ 2/\delta t / \lambda & \text{on } \Omega_g . \end{array} \right.
\]

We also denote

\[
A^f_h((\mathbf{u}_h, \mathbf{u}_h), (\mathbf{v}_h, \mathbf{v}_h)) := 2\mu f A^f_h((\mathbf{u}_h, \mathbf{u}_h), (\mathbf{v}_h, \mathbf{v}_h)) + \delta t \mu \gamma A_h^s((\mathbf{u}_h, \mathbf{u}_h), (\mathbf{v}_h, \mathbf{v}_h))
\]

which is an HDG discretization of the variable coefficient diffusion operator \( -\nabla \cdot (\mu D(\mathbf{u})) \) on the whole domain \( \Omega \). Hence, the formulation \((16)\) simplifies to

\[
(17) \quad \frac{2}{\delta t}(\rho \mathbf{u}_h, \mathbf{v}_h) + A^f_h((\mathbf{u}_h, \mathbf{u}_h), (\mathbf{v}_h, \mathbf{v}_h)) - (p_h, \nabla \cdot \mathbf{v}_h) - (\nabla \cdot \mathbf{u}_h, q_h) - (\gamma p_h, q_h) = F((\mathbf{v}_h, \mathbf{v}_h)).
\]

The problem \((17)\) can be rewritten in a matrix-vector formulation: Find \( [\mathbf{u}_h; p_h] \in \mathbb{R}^{N_u+N_p} \) such that

\[
(18) \quad \begin{bmatrix} A^f_h + \frac{2}{\delta t} M^\rho_h & B_h \\ B^T_h & -M^\gamma_h \end{bmatrix} \begin{bmatrix} \mathbf{u}_h \\ p_h \end{bmatrix} = \begin{bmatrix} F \\ 0 \end{bmatrix},
\]

where \( \mathbf{u}_h \in \mathbb{R}^{N_u} \) is the coefficient vector for the compound velocity approximation \( \mathbf{u}_h := (\mathbf{u}_h, \mathbf{u}_h) \in \mathbf{V}_{h,0}^k \times \mathbf{V}_{h,0}^{k-1} \) with \( N_u \) being the dimension of the compound finite element space \( \mathbf{V}_{h,0}^k \times \mathbf{V}_{h,0}^{k-1} \). \( p_h \in \mathbb{R}^{N_p} \) is the coefficient vector for the pressure approximation \( p_h \in Q_h^{k-1} \) with \( N_p \) being the dimension of the finite element space \( Q_h^{k-1} \). Moreover, the matrix \( A^f_h \in \mathbb{R}^{N_u \times N_u} \) is associated with the bilinear form \( A^f_h(\mathbf{u}_h, \mathbf{v}_h) \), the matrix \( M^\rho_h \in \mathbb{R}^{N_u \times N_u} \) is associated with the bilinear form \( (\rho \mathbf{u}_h, \mathbf{v}_h) \), the matrix \( B_h \in \mathbb{R}^{N_u \times N_u} \) is associated with the bilinear form \( -(p_h, \nabla \cdot \mathbf{v}_h) \), the matrix \( M^\gamma_h \in \mathbb{R}^{N_p \times N_p} \) is associated with the bilinear form \( (\gamma p_h, q_h) \), and the vector \( F \in \mathbb{R}^{N_u} \) is associated with the linear form \( F(\mathbf{v}_h) \). The big matrix in the linear system \((18)\) has a block structure and is symmetric and indefinite, with the 1-1 block \( A^f_h + \frac{2}{\delta t} M^\rho_h \) being symmetric positive definite (SPD), and the 2-2 block \( -M^\gamma_h \) being symmetric and negative semi-definite.

A popular method to solve the symmetric saddle point problem \((18)\), which we adopt in this work, is to use a preconditioned MinRes solver \([41]\) with the following block diagonal preconditioner \([28,34]\):

\[
(19) \quad P = \begin{bmatrix} \hat{A} & 0 \\ 0 & \hat{S} \end{bmatrix}
\]

where \( \hat{A} \) is an appropriate preconditioner of the SPD matrix \( A := A^f_h + \frac{2}{\delta t} M^\rho_h \), and \( \hat{S} \) is an appropriate preconditioner of the (dense) Schur complement SPD matrix \( S := B^T_h(A^f_h + \frac{2}{\delta t} M^\rho_h)^{-1}B_h + M^\gamma_h \). The detailed construction of the preconditioner for the Schur complement (pressure) matrix \( S \) is discussed in Subsection \(3.2\) where we borrow ideas in the literature on preconditioning the closely
related, generalized Stokes problem [9, 15, 37]. The detailed construction of the preconditioner for the SPD velocity matrix $A$ is discussed in Subsection 3.3 where we use an auxiliary space preconditioner [44] along with algebraic multigrid. We mention that for polynomial degree $k \geq 2$, the preconditioned MinRes solver is applied to the static condensed subsystem of (18), see the discussion in Remark 3.2.

**Remark 3.1** (Connection with a generalized Stokes interface problem). The discretization [17], or the form [18], is closely related to a divergence-conforming HDG discretization of a generalized Stokes interface problem (with a fixed interface) with variable density $\rho$ and variable viscosity $\mu$, c.f. [21]. The only difference between the divergence-conforming HDG linear system for the generalized Stokes interface problem and the current FSI problem is that the pressure block is zero for the former, while it is $-M_h^\gamma$ for the latter, which is a symmetric negative semi-definite matrix and represents the compressibility of the structure. A non-zero pressure block also appears in the finite element discretization of the Stokes problem using pressure-stabilized methods, or the linear elasticity problem with a displacement-pressure formulation.

**Remark 3.2** (Static condensation for $k \geq 2$). When polynomial degree $k \geq 2$, we shall solve the linear system problem (18) using static condensation to locally eliminate interior velocity DOFs and high-order pressure DOFs [31]. The resulting global linear system after static condensation consists of DOFs for the normal component of velocity approximation (of degree $k$) in $V_{h,0}^k$ and the tangential (hybrid) velocity approximation (of degree $k-1$) in $\hat{V}_{h,0}^{k-1}$ on the mesh skeleton (facets), and cell-average of pressure approximations (of degree 0) on the mesh. We denote the compound velocity space corresponding to the DOFs on mesh skeleton by $V_{h,0}^k$, and is given as follows:

$$V_{h,0}^k = \bigcup_{iS} V_{h,0}^k,$$

where $M_{h,0}^{\mu,\gamma}$ is the weighted mass matrix associated with the bilinear form $((\mu^{-1} + \gamma)p, q)$ on the piecewise constant global pressure space $Q_{h,0}^0$, and $N_{h,0}^{\mu,\gamma}$ is the matrix associated with the bilinear form

$$\int_F \rho^{-1} h [p_h] [q_h] \, ds, \quad \forall p_h, q_h \in Q_{h,0}^0,$$

where $\{\rho\} := \frac{\phi^+ + \phi^-}{2}$ is the geometric average of $\rho$, and $[\phi] = \phi^+ - \phi^-$ is the jump of $\phi$ on an interior facet $F$. Note that the mass matrix $M_{h,0}^{\mu,\gamma}$ is diagonal and its inversion is trivial. Also, note that the bilinear form [21] corresponds to the interior penalty discretization of the operator $\gamma p - \frac{\delta t}{2} \nabla \cdot (\rho^{-1} \nabla p)$ with a homogeneous Neumann boundary condition using the piecewise constant constant global pressure space $Q_{h,0}^0$. The jump term in [21] was shown in [40] to be spectrally equivalent to the operator $\frac{\delta t}{2} B_h^T (M_{h,0}^\mu)^{-1} B_h$ when the density $\rho$ is uniformly bounded from above and below. Hence, $(N_{h,0}^{\mu,\gamma})^{-1}$ serves as a robust preconditioner for the (dense) Schur complement matrix $\frac{\delta t}{2} B_h^T (M_{h,0}^\mu)^{-1} B_h + M_{h,0}^\gamma$. In the actual numerical realization of $(N_{h,0}^{\mu,\gamma})^{-1}$, we use the hypre’s BoomerAMG preconditioner [16, 25] for the matrix $N_{h,0}^{\mu,\gamma}$.
We note that the pressure Schur complement preconditioner \( [20] \) was initially introduced for the generalized Stokes problem \((\text{constant density, constant viscosity, and } \gamma = 0) \) by Cahouet and Chabard [0]. Robustness of this Cahouet-Chabard preconditioner for the generalized Stokes problem with respect to variations in the mesh size \( h \) and time step size \( \delta t \) was proven in \([5,33,37]\). It was then generalized by Olshanskii et al. \([37]\) to the generalized Stokes interface problem \((\text{variable density, variable viscosity, and } \gamma = 0) \). While a theoretical proof of the robustness of the preconditioner in \([37]\) for the variable density and viscosity case was lacking due to the lack of regularity results for the stationary Stokes interface problem, numerical results performed in \([37]\) seems to indicate that the preconditioner is robust also with respect to the jumps in viscosity and density in large parameter ranges. Hence, our preconditioner \((20)\) can be considered as a generalization of the one in \([37]\) to take into account the structure compressibility \((\gamma > 0)\) on \( \Omega_s \) in the pressure block.

3.3. Preconditioning the velocity stiffness matrix \( A \). The matrix \( A \) corresponds to the divergence-conforming HDG discretization of the elliptic operator \( \frac{2}{\rho} \mu u - 2 \nabla \cdot (\mu D(u)) \). Here we propose to use the auxiliary space preconditioner \([44]\) developed in \([20]\). The auxiliary space is the continuous linear Lagrange finite elements:

\[ V_{h,0}^{c^g} := \{ v \in H_0^1(\Omega) : v|_K \in [P^1(K)]^d, \forall K \in T_h \}. \]

The auxiliary space preconditioner for \( A \) is of the following form:

\[
\widetilde{A} = R + P A^{-1} P^T,
\]

where \( R \in \mathbb{R}^{N_{c} \times N_{c}} \) is the (point) Gauss-Seidel smoother for the matrix \( A \), with \( N_{\text{gl}}^u \) being the dimension of the reduced compound space \( V_{h,0}^{c^g} \), the matrix \( \mathcal{A} \in \mathbb{R}^{N_c \times N_c} \) is the matrix associated with the following bilinear form on the auxiliary space \( V_{h,0}^{c^g} \):

\[
\left( \begin{array}{c}
\frac{2}{\delta t} u_h, v_h \\
2(\mu D(u_h), D(v_h))
\end{array} \right), \quad \forall u_h, v_h \in V_{h,0}^{c^g},
\]

where \( N_c \) is the dimension of \( V_{h,0}^{c^g} \), and the matrix \( P \in \mathbb{R}^{N_c \times N_c} \) is associated with the projector \( \Pi : V_{h,0}^{c^g} \to V_{h,0}^{k,\text{gl}} \), which is defined as follows: for any function \( u_h \in V_{h,0}^{c^g} \), find \( \Pi u_h = (\Pi u_h, \tilde{\Pi} u_h) \in V_{h,0}^{k,\text{gl}} \) such that

\[
\sum_{F \in \xi_h} \int_F (\Pi u_h \cdot n)(v_h \cdot n) ds = \sum_{F \in \xi_h} \int_F (u_h \cdot n)(v_h \cdot n) ds,
\]

\[
\sum_{F \in \xi_h} \int_F \nabla(\Pi u_h) \cdot \nabla(\tilde{v}_h) ds = \sum_{F \in \xi_h} \int_F \nabla(u_h) \cdot \nabla(\tilde{v}_h) ds,
\]

for all \( (u_h, \tilde{v}_h) \in V_{h,0}^{k,\text{gl}} \). Note that the projector is locally facet-by-facet defined, and the transformation matrix \( P \) is sparse. For the numerical realization \( A^{-1} \), we again use hypre’s BoomerAMG.

4. Semidiscrete a priori error analysis

In this section, we present an a priori error analysis for the semidiscrete scheme \([4]\). To simplify notation, we write

\[ A \lesssim B \]

to indicate that there exists a constant \( C \), independent of mesh size \( h \), material parameters \( \rho^{f/s} \), \( \mu^{f/s} \), \( \lambda^s \), and the numerical solution, such that \( A \leq CB \).
We denote the following (semi)norms:

\[(24a) \quad \|(v, \hat{v})\|_{i,h} := \sum_{K \in \mathcal{T}_h} \left( \|D(v_h)\|_{h,K}^2 + \frac{\alpha k^2}{h} \|\Pi_h(tang(v_h - \hat{v}_h))\|_{h,K}^2 \right), \]

\[(24b) \quad \|(v, \hat{v})\|_{i,s,h} := \left( \|(v, \hat{v})\|_{i,h}^2 + \sum_{K \in \mathcal{T}_h} h \|D(v_h)\|_{h,K}^2 \right)^{1/2}, \]

\[(24c) \quad \|\{v, \xi^s, \hat{\xi}^s\}\|_h := \left( \|\rho \|^{1/2} + 2 \mu \|\xi^s, \hat{\xi}^s\|_{s,h}^2 + \lambda \|\nabla \cdot \xi^s\|_{s,h}^2 \right)^{1/2}, \]

for \(i \in \{f, s\}\) and \((v, \hat{v}, \xi^s, \hat{\xi}^s) \in V_{h,0}^k \times \hat{V}_{h,0}^{k-1} \times V_{h,0}^{k,s} \times \hat{V}_{h,0}^{k-1,s}\), where we denote \(\| \cdot \|\) as the \(L^2\)-norm on \(\Omega\), \(\| \cdot \|_i\) as the \(L^2\)-norm on \(\Omega^i\). The inequality \((23)\) implies the coercivity of the bilinear form \(A_h^i\) with respect to the norm \(\| \cdot \|_{i,h}\). We also have the following boundedness of the operator \(A_h^i\):

\[(25) \quad A_h^i((v, \hat{v}), (w_h, \hat{w}_h)) \leq \|(v, \hat{v})\|_{i,s,h} \|(w_h, \hat{w}_h)\|_{i,h}, \]

for all \((v, \hat{v}) \in V^i + \left( V_{h,0}^k \times \hat{V}_{h,0}^{k-1,i} \right)\) and \((w_h, \hat{w}_h) \in V_{h,0}^{k,i} \times \hat{V}_{h,0}^{k-1,i}\), where

\[V^i := \{(v, v_{|\xi_h^i}) : v_{|K} \in H^2(K), \forall K \in \mathcal{T}_h\}. \]

We use the classical Brezzi-Douglas-Marini (BDM) interpolator \(\Pi_{BDM}\) [4] Proposition 2.3.2] to project \(u\) and \(\eta^s\) onto the finite element spaces \(V_{h,0}^k\) and \(V_{h,0}^{k,s}\). We denote \(\Pi_Q\) as the \(L^2\)-projection onto the finite element space \(Q_{h}^{k-1}\). Note that due to the commuting projection property, we have:

\[(26a) \quad (\nabla \cdot BDM_\psi, q_h^s) = (\nabla \cdot \psi, q_h^s), \quad \forall q_h^s \in Q_{h}^{k-1,s}, \]

\[(26b) \quad \nabla \cdot BDM_\psi(u_h|_{\xi_h^i} - \Pi_h u)|_{\Omega_f} = 0. \]

The following standard approximation property of the BDM projector \(\Pi_{BDM}\) and the \(L^2\)-projector \(\Pi_h\) onto \(V_{h,0}^{k-1}\) is well-known; see [30] Proposition 2.3.8].

**Lemma 4.1.** Let \(u \in [H^1(\Omega)]^d \cap [H^{k+1}(\mathcal{T}_h)]^d\). Then the following estimates hold:

\[(27) \quad \|\{(u - BDM_\psi u, u|_{\xi_h^i} - \Pi_h u)\|_{i,s,h}^2 \lesssim h^{2k} \sum_{K \in \mathcal{T}_h} \|u\|_{H^{k+1}(K)}^2, \]

for \(i \in \{f, s\}\).

To further simplify notation, we denote:

\[
\delta u := (\delta u, \delta u) := (u - BDM_\psi u, u|_{\xi_h^i} - \Pi_h u),
\]

\[
\delta \eta^s := (\delta \eta^s, \delta \eta^s) := (\eta^s - BDM_\psi \eta^s, \eta^s|_{\xi_h^i} - \Pi_h \eta^s),
\]

\[
\delta p_f := p_f - \Pi_Q p_f,
\]

\[
\varepsilon u := (\varepsilon u, \varepsilon u) := (u_h - BDM_\psi u, u_h - \Pi_h u),
\]

\[
\varepsilon \eta^s := (\varepsilon \eta^s, \varepsilon \eta^s) := (\eta_h^s - BDM_\psi \eta^s, \eta_h^s - \Pi_h \eta^s),
\]

\[
\varepsilon p_f := p_h - \Pi_Q p_f.
\]

where \((u_h, p_f, \eta_h^s) \in V_{h,0}^k \times \hat{V}_{h,0}^{k-1,f} \times V_{h,0}^{k,s}\) is the solution to the semi-discrete scheme [4], with the component spaces denoted as

\[
V_{h,0}^k := V_{h,0}^k \times \hat{V}_{h,0}^{k-1} , \quad V_{h,0}^{k,s} := V_{h,0}^{k,s} \times \hat{V}_{h,0}^{k-1,s}. \]
Lemma 4.2 (Error equations of the semi-discrete scheme [4]). We have the following error equations for the semi-discrete scheme [4]:

\begin{align}
(28a) \quad & (\rho \partial_t \varepsilon u, v_h) + 2\mu^f A_h^f (\varepsilon u, v_h) = (\varepsilon_{p^f}, \nabla \cdot v_h) + 2\mu^s A_h^s (\varepsilon \eta^s, v_h) + \lambda^s (\nabla \cdot \varepsilon \eta^s, \nabla \cdot v_h), \\
& \quad \quad = (\rho \partial_t \delta u, v_h) + 2\mu^f A_h^f (\delta u, v_h) + 2\mu^s A_h^s (\delta \eta^s, v_h), \\
(28b) \quad & (\partial_t \varepsilon \eta^s, \xi^h) = (\varepsilon u^s, \xi^h), \\
(28c) \quad & (\partial_t \varepsilon \eta^s, \Xi^h) = \langle \varepsilon u^s, \Xi^h \rangle.
\end{align}

for all $(v_h, q^f, \xi^h) \in V_{h,0}^k \times Q_{h,0}^{k-1,f} \times V_{h,0}^{k,s}$.

Proof. By subtracting the semi-discrete scheme (7a) from the consistency result (4a), then adding and subtracting the above projectors, we can get the error equation (28a), where the commutative property of BDM interpolation (26) is used. Then (28b) and (28c) can be easily derived since we have $\partial_t \Pi_{BDM} u^s = \partial_t \Pi_{BDM} \eta^s$, $\partial_t \Pi_{h} u^s = \partial_t \Pi_{h} \eta^s$. \hfill \square

Note that due to the same finite elements space of velocity and displacement approximation in $\Omega^s$, the error equations (28b) and (28c) actually imply that $\varepsilon u^s = \partial_t \varepsilon \eta^s, \varepsilon u^s = \partial_t \varepsilon \eta^s$. Now we are ready to present the main result in this section.

Theorem 4.1. Let $(u_k^f, p^f, \eta^h_k)$ be the solution to semi-discrete scheme [4] with initial data such that $(\varepsilon u(0), \varepsilon_{p^f}(0), \varepsilon \eta^s(0)) = (0, 0, 0)$. Assume the solution $(u, \eta^s)$ to the model problem [1] is smooth. Then the following estimation holds for all $T > 0$:

\begin{align}
\| \{ & \varepsilon u(T), \varepsilon \eta^s(T) \} \|_h^2 + \mu^f \int_0^T \| \varepsilon u \|_{f,h}^2 \, dt \lesssim h^{2k} (\Xi_1 + \Xi_2 + \Xi_3),
\end{align}

where

\begin{align}
\Xi_1 & := T \int_0^T \left( \| \rho^{1/2} \partial_t u \|_{H^k(\Omega)}^2 + \mu^s \| \partial_t \eta^s \|_{H^{k+1}(\Omega^s)} \right) \, dt, \\
\Xi_2 & := \mu^f \int_0^T \| u \|_{H^{k+1}(\Omega)}^2 \, dt, \\
\Xi_3 & := \mu^s \| \eta^s \|_{L^\infty(H^{k+1}(\Omega^s))}.
\end{align}

Proof. Here we use the standard energy argument. Take $(v_h, q^f) = (\varepsilon u, \varepsilon p^f)$ in error equation (28a) and plug in $\varepsilon u^s = \partial_t \varepsilon \eta^s, \varepsilon u^s = \partial_t \varepsilon \eta^s$, we get:

\begin{align}
& \frac{1}{2} \frac{d}{dt} \left( \| \rho^{1/2} \partial_t u \| + 2\mu^s A_h^s (\varepsilon \eta^s, \varepsilon \eta^s) + \lambda^s (\nabla \cdot \varepsilon \eta^s) \right) + 2\mu^f A_h^f (\varepsilon u, \varepsilon u) \\
& \quad = (\rho \partial_t \delta u, \varepsilon u) + 2\mu^f A_h^f (\delta u, \varepsilon u) + 2\mu^s A_h^s (\delta \eta^s, \partial_t \varepsilon \eta^s),
\end{align}

where we used the exactly divergence-free property of $u^f$ and $\Pi_{BDM} u^f$. By plugging in the right-hand side the chain rule for the time derivative

\[ \frac{d}{dt} A_h^s (\delta \eta^s, \varepsilon \eta^s) = A_h^s (\partial_t \delta \eta^s, \varepsilon \eta^s) + A_h^s (\delta \eta^s, \partial_t \varepsilon \eta^s), \]
and then applying the Cauchy-Schwarz inequality and boundedness of $A_h^i$ \cite{25}, we get:
\[
\frac{1}{2} \frac{\partial}{\partial t} \mathcal{H}(t) + 2\mu^f A_h^f (\epsilon u, \epsilon u) \lesssim \|\rho^{1/2} \partial_t \delta u\|_h \|\partial_t \epsilon u\|_h + 2\mu^f \|\delta_{u}^{f, s, h}\|_h \|\epsilon u\|_h
\]
\[
+ 2\mu^s \|\partial_t \delta \eta\|_{s, s, h} \|\epsilon \eta\|_{s, s, h} + 2\mu^s \frac{d}{dt} A_h^s (\delta \eta, \epsilon \eta)
\]
\[
\lesssim \Theta^{1/2} \|\epsilon u, \epsilon \eta\|_h + 2\mu^f \|\delta_{u}^{f, s, h}\|_h \|\epsilon u\|_h + 2\mu^s \frac{d}{dt} A_h^s (\delta \eta, \epsilon \eta),
\]
where $\Theta := \left(\|\rho^{1/2} \partial_t \delta u\|^2 + 2\mu^s \|\partial_t \delta \eta\|^2_{s, s, h}\right)$. Integrate both sides over time from $t = 0$ to $t = T$, combined with $(\epsilon u(0), \epsilon \eta(0), \epsilon \eta^*(0)) = (0, 0, 0)$, we get:
\[
\mathcal{H}(T) + \mu^f \int_0^T A_h^f (\epsilon u, \epsilon u) \, dt \lesssim \int_0^T \Theta^{1/2} \|\epsilon u, \epsilon \eta\|_h \, dt + \mu^f \int_0^T \|\delta_{u}^{f, s, h}\|_h \|\epsilon u\|_h \, dt
\]
\[
+ \mu^s A_h^s (\delta \eta^*(T), \epsilon \eta^*(T)).
\]
Applying the coercivity and boundedness of $A_h^i$, and Young’s inequality, we get:
\[
\|\{\epsilon u(T), \epsilon \eta^*(T)\}\|_h^2 + \mu^f \int_0^T \|\epsilon u\|^2_{f, h} \, dt \lesssim \int_0^T \Theta^{1/2} \|\{\epsilon u, \epsilon \eta\}\|_h \, dt
\]
\[
+ \mu^f \gamma_1 \int_0^T \|\delta_{u}^{f, s, h}\|^2 \, dt + \mu^s \gamma_2 \|\epsilon \eta^*(T)\|^2_{s, s, h}
\]
\[
+ \frac{\mu^f}{\gamma_1} \int_0^T \|\epsilon u\|^2_{f, h} \, dt + \frac{\mu^s}{\gamma_2} \|\epsilon \eta^*(T)\|^2_{s, s, h},
\]
for all $\gamma_1, \gamma_2 > 0$. The last two terms would be absorbed by the left-hand side when $\gamma_1$ and $\gamma_2$ are big enough. Then we have:
\[
\|\{\epsilon u(T), \epsilon \eta^*(T)\}\|_h^2 + \mu^f \int_0^T \|\epsilon u\|^2_{f, h} \, dt \lesssim \int_0^T \Theta^{1/2} \|\{\epsilon u, \epsilon \eta\}\|_h \, dt
\]
\[
+ \mu^f \int_0^T \|\delta_{u}^{f, s, h}\|^2 \, dt + \mu^s \|\epsilon \eta^*(T)\|^2_{s, s, h}.
\]
By applying the Gronwall-type inequality \cite{11} Proposition 3.1 and the Cauchy-Schwarz inequality, we get:
\[
\|\{\epsilon u(T), \epsilon \eta^*(T)\}\|_h^2 + \mu^f \int_0^T \|\epsilon u\|^2_{f, h} \, dt
\]
\[
\leq \left(\frac{1}{2} \int_0^T \Theta^{1/2} \, dt + \max_{0 \leq t \leq T} \left(\mu^f \int_0^t \|\delta_{u}^{f, s, h}\|^2 \, dt + \mu^s \|\epsilon \eta^*(T)\|^2_{s, s, h}\right)\right)^{1/2}
\]
\[
\lesssim T \int_0^T \Theta \, dt + \mu^f \int_0^T \|\delta_{u}^{f, s, h}\|_{s, s, h} \, dt + \mu^s \max_{0 \leq t \leq T} \|\epsilon \eta^*(T)\|^2_{s, s, h}.
\]
Finally, the estimate \cite{29} is obtained by the above inequality and the approximation properties of the projectors in Lemma 4.1. \qed

**Remark 4.1 (Robust velocity/displacement estimates).** It is clear that the velocity and displacement error estimate \cite{29} is independent of the pressure approximation $p_h^f$ and the lame parameter $\lambda^s$. Moreover, the error estimate \cite{29} is optimal in the energy norm $\|\cdot\|_h$, which contains a discrete $H^1$-norm on $\Omega^h$. On the other hand, we can only obtain a suboptimal convergence of order $O(h^k)$ for the $L^2$-norm of the velocity approximation from \cite{29}. However, our numerical results in the
next section indicate that the velocity $L^2$-norm seems to be optimal. The proof of the optimality of the velocity $L^2$-norm is our future work.

5. Numerical results

In this section, we present three numerical examples for the model problem (1) in two and three dimensions. The first example uses a manufactured solution to verify the accuracy of the proposed monolithic divergence-conforming HDG schemes (10) and (15) and the robustness of the preconditioner (19) with respect to mesh size, time step size, and material parameters. The second example is a classical benchmark problem typically used to validate FSI solvers [7, 35]. The third example is a 3D test case simulating the propagation of pressure pulse through a straight cylinder pipe. The NGSolve software [42] is used for the simulations.

5.1. Example 1: The method of manufactured solutions. We consider a rectangular fluid domain, $\Omega^f = (0, 1) \times (-1, 0)$, and a rectangular solid domain, $\Omega^s = (0, 1) \times (0, 0.5)$, connected by an interface, $\Gamma = \{(x, y) : x \in (0, 1), y = 0\}$. We choose the volume and interface source terms such that the exact solutions are given as follows:

$$\begin{align*}
\mathbf{u}^f &= \mathbf{u}^* = \left( \sin(2\pi x)^2 \sin\left(\frac{8}{3}\pi (y + 1)\right) \sin(2t), -1.5 \sin(4\pi x) \sin\left(\frac{4}{3}\pi (y + 1)\right)^2 \sin(2t) \right), \\
p^f &= \sin(2\pi x) \sin(2\pi y) \sin(t), \\
\mathbf{\eta}^s &= \left( \sin(2\pi x)^2 \sin\left(\frac{8}{3}\pi (y + 1)\right) \sin(t)^2, -1.5 \sin(4\pi x) \sin\left(\frac{4}{3}\pi (y + 1)\right)^2 \sin(t)^2 \right).
\end{align*}$$

We use a homogeneous Dirichlet boundary conditions (16) on the exterior boundaries. For the material parameters, we take the fluid density and viscosity to be one ($\rho^f = \mu^f = 1$), and vary the structure density and Lamé parameters in large parameter ranges:

$$\rho^s \in \{10^{-3}, 1, 10^3\}, \mu^s = \delta_1 \rho^s, \text{with } \delta_1 \in \{0.1, 1, 10\}, \text{and } \lambda^s = \delta_2 \mu^s, \text{with } \delta_2 \in \{1, 10^4\}.$$ 

Here $\delta_2 = 1$ corresponds to a compressible structure, while $\delta_2 = 10^4$ corresponds to a nearly incompressible structure.

We run simulations on a sequence of uniform unstructured triangular meshes with mesh size $h = \frac{1}{10 	imes 2^j}$ for $j = 0, 1, 2, 3$. We take the polynomial degree to be either $k = 1$ or $k = 2$. We use the (second-order) Crank-Nicolson temporal discretization (10) for $k = 1$, and the (third-order) BDF3 temporal discretization (15), and take a uniform time step size $\delta t = h$. To start the BDF3 scheme, we compute ($\mathbf{u}^m_h, \eta_h^m, \eta_h^m$) by interpolating the exact solution at time $t_m = m \delta t, m = 0, 1, 2$. The preconditioned MinRes solver with the preconditioner (19) with AMG blocks (20) and (22) is used to solve the linear system in each time step, for which we start with zero initial guess and stop until the residual norm is decreased by a factor of $10^{-8}$.

The $L^2$-errors in the velocity approximation $\| \mathbf{u} - \mathbf{u}_h \|_Q$ at the final time $T = 0.3$ are documented in Table 1 for various parameter choices. It is clear to observe that our fully discrete scheme provide an optimal velocity approximation of order 2 for polynomial degree $k = 1$ with Crank-Nicolson time stepping, and of order 3 for $k = 2$ with BDF3 time stepping. Moreover, we observe that our fully discrete scheme is robust with respect to large density variations and large Lamé parameter variations since the errors for different parameters in each row of Table 1 are similar.

The average numbers of iterations needed for the convergence of the preconditioned MinRes solver are recorded in Table 2. We observe for polynomial degree $k = 1$, we roughly need about 150 iterations to converge for the compressible structure case in Table 3 and about 116 iterations for the nearly incompressible structure case in Table 4. Also, the preconditioner is fairly robust with respect to the mesh size (and time step size), and parameter variations in $\rho^s$ and $\mu^s$. Similar results are observed for the $k = 2$ case, which needs roughly about 285 iterations to converge for the compressible case in Table 3 and about 210 iterations for the nearly incompressible case.
However, it is also clear that the preconditioner is not robust with respect to polynomial degree $k$. We finally point out that the $k$-dependency on the iteration counts is due to the auxiliary space velocity preconditioner \cite{22}, since if we replace $iA$ by the exact inverse $A^{-1}$, the iteration counts are then observed to be quite insensitive to the polynomial degree: about $30–40$ iterations are needed in the compressible cases, and about $20–30$ iterations in the nearly incompressible cases for polynomial degree $k = 1, 2, 3, 4$. This is expected as the polynomial degree in the pressure block is kept to be 0 regardless of the velocity polynomial degree $k$ in the global linear system due to static condensation; see Remark \ref{remark:1}.

|       | $\delta_1 = 0.1$ | $\rho^s = 10^{-3}$ | $\delta_1 = 1$ | $\rho^s = 1$ | $\delta_1 = 10$ | $\rho^s = 10^3$ |
|-------|------------------|---------------------|----------------|--------------|----------------|--------------|
| $k$   | $1/h$            | error               | error          | error        | error          | error        |
| 1     | 10               | 3.492e-02           | 3.420e-02      | 5.624e-02    | 3.498e-02      | 5.350e-02    |
|       | 20               | 8.499e-03           | 8.346e-03      | 1.145e-02    | 8.495e-03      | 1.085e-02    |
|       | 40               | 2.052e-03           | 2.074e-03      | 3.021e-03    | 2.051e-03      | 2.777e-03    |
|       | 80               | 5.063e-04           | 5.125e-04      | 9.015e-04    | 5.059e-04      | 8.126e-04    |
| rate  | 2.04             | 2.02                | 1.98           | 2.04         | 2.02           | 2.01         |
| 2     | 10               | 4.124e-03           | 4.273e-03      | 4.331e-03    | 4.120e-03      | 4.260e-03    |
|       | 20               | 5.151e-04           | 5.289e-04      | 5.262e-04    | 5.148e-04      | 5.283e-04    |
|       | 40               | 6.267e-05           | 6.549e-05      | 6.476e-05    | 6.265e-05      | 6.548e-05    |
|       | 80               | 7.733e-06           | 8.028e-06      | 7.712e-06    | 7.732e-06      | 8.039e-06    |
| rate  | 3.02             | 3.02                | 3.04           | 3.02         | 3.02           | 3.03         |

**Table 1. Example 1: History of convergence of the $L^2$-velocity errors. Compressible structure ($\delta_2 = 1$).**

|       | $\delta_1 = 0.1$ | $\rho^s = 10^{-3}$ | $\delta_1 = 1$ | $\rho^s = 1$ | $\delta_1 = 10$ | $\rho^s = 10^3$ |
|-------|------------------|---------------------|----------------|--------------|----------------|--------------|
| $k$   | $1/h$            | error               | error          | error        | error          | error        |
| 1     | 10               | 3.388e-02           | 3.304e-02      | 5.068e-02    | 3.351e-02      | 4.935e-02    |
|       | 20               | 8.211e-03           | 8.094e-03      | 1.066e-03    | 8.201e-03      | 9.373e-03    |
|       | 40               | 2.004e-03           | 1.998e-03      | 2.136e-03    | 2.002e-03      | 2.053e-03    |
|       | 80               | 4.919e-04           | 4.942e-04      | 8.038e-04    | 4.913e-04      | 7.295e-04    |
| rate  | 2.03             | 2.02                | 2.02           | 2.03         | 2.02           | 2.05         |
| 2     | 10               | 4.195e-03           | 4.354e-03      | 4.406e-03    | 4.164e-03      | 4.307e-03    |
|       | 20               | 5.200e-04           | 5.296e-04      | 5.221e-04    | 5.181e-04      | 5.237e-04    |
|       | 40               | 6.258e-05           | 6.421e-05      | 6.430e-05    | 6.245e-05      | 6.548e-05    |
|       | 80               | 7.697e-06           | 7.854e-06      | 7.708e-06    | 7.691e-06      | 7.860e-06    |
| rate  | 3.03             | 3.04                | 3.05           | 3.03         | 3.03           | 3.03         |

**Table 2. Example 1: History of convergence of the $L^2$-velocity errors. Nearly incompressible structure ($\delta_2 = 10^4$).**

### 5.2. Example 2: a linear two-dimensional test case

We consider a simplified linear version of the numerical experiment reported in \cite{35}. We use the similar set-up as in \cite{7}. We consider a fluid domain, $\Omega^f = (0.6) \times (0.5)\text{cm}^2$, and a structure domain, $\Omega^s = (0.6) \times (0.5, 0.6)\text{cm}^2$, ...
connected by an interface $\Gamma = \{(x, y) : x \in (0, 6), y = 0.5\}$. We consider the FSI problem (1a)–(1c) with $f^t = f^s = 0$, where we add a linear spring term, $\beta^s \eta^s$ to the first equation in (1b):

$$
\rho^s \partial_t u^s + \beta^s \eta^s - \nabla \cdot \sigma^s(\eta^s) = 0.
$$

The material parameters are given as follows: $\rho^s = 1.1 [\text{g/cm}^3]$, $\mu^s = 0.575 \times 10^6 [\text{dye/cm}^2]$, $\beta^s = 4 \times 10^6 [\text{dye/cm}^4]$, $\lambda^s = 1.7 \times 10^6 [\text{dye/cm}^2]$, $\rho^f = 1 [\text{g/cm}^3]$, $\mu^f = 0.035 [\text{g/(cm \cdot s)}]$, which are within physiologically realistic values of blood flow in compliant arteries. The flow is initially at rest, and we take the following boundary conditions which model a pressure driven flow:

$$
\begin{align*}
(\sigma^f) \cdot n &= -p_{in}(t), & \text{tang}(u^f) &= 0 & \text{on } \Gamma^f_{in} := \{(x, y) : x = 0, y \in (0, 0.5)\}, \\
(\sigma^f) \cdot n &= 0, & \text{tang}(u^f) &= 0 & \text{on } \Gamma^f_{out} := \{(x, y) : x = 6, y \in (0, 0.5)\}, \\
\text{tang}(\sigma^f) \cdot n &= 0, & u^f \cdot n &= 0 & \text{on } \Gamma^f_{bot} := \{(x, y) : x \in (0, 6), y = 0\}, \\
\eta^s \cdot n &= 0, & \text{tang}(\eta^s) &= 0 & \text{on } \Gamma^s_{in/out} := \{(x, y) : x \in (0, 6), y \in (0.5, 0.6)\}, \\
(\sigma^s) \cdot n &= 0, & \text{tang}(\eta^s) &= 0 & \text{on } \Gamma^s_{top} := \{(x, y) : x \in (0, 6), y = 0.6\}.
\end{align*}
$$

**Table 3. Example 1:** Average iteration counts for the preconditioned MinRes solver. Compressible structure $(\delta_2 = 1)$.

| $k$ | $1/h$ | $\delta_1 = 0.1$ | $\delta_1 = 1$ | $\delta_1 = 10$ | $\rho^s = 10^{-3}$ | $\rho^s = 1$ | $\rho^s = 10^3$ |
|-----|-------|-----------------|----------------|-----------------|----------------|----------------|----------------|
| 1   | 10    | 136             | 142            | 122             | 137            | 141            | 122            |
|     | 20    | 135             | 146            | 131             | 136            | 148            | 132            |
|     | 40    | 148             | 158            | 152             | 145            | 160            | 153            |
|     | 80    | 161             | 174            | 177             | 159            | 180            | 181            |
| 2   | 10    | 281             | 290            | 250             | 283            | 291            | 243            |
|     | 20    | 283             | 302            | 269             | 284            | 302            | 263            |
|     | 40    | 294             | 313            | 297             | 293            | 313            | 291            |
|     | 80    | 291             | 310            | 307             | 288            | 307            | 303            |

**Table 4. Example 1:** Average iteration counts for the preconditioned MinRes solver. Nearly incompressible structure $(\delta_2 = 10^4)$.
where the time-dependent pressure boundary source term at the inlet $\Gamma^f_{in}$ is given as follows:

\[
p_{in}(t) = \begin{cases} 
\frac{p_{\text{max}}}{2} \left( 1 - \cos\left(\frac{2\pi t}{t_{\text{max}}}\right) \right), & \text{if } t \leq t_{\text{max}}, \\
0, & \text{if } t > t_{\text{max}}, 
\end{cases}
\]

where $t_{\text{max}} = 0.03$[s] and $p_{\text{max}} = 1.333 \times 10^4$[dyne/cm$^2$]. The final time of the simulation is $T = 1.2 \times 10^{-2}$[s].

In this example, we use the divergence-conforming HDG scheme with Crank-Nicolson time stepping (10). The additional spring term $\beta^s \eta^s$ in the structure equation does not alter the form of the resulting global linear system. Hence we still apply the preconditioned MinRes solver using the preconditioner (19) with AMG blocks (22) and (20). Due to different boundary conditions, we shall add the boundary contribution

\[
\sum_{F \in \Gamma^f_{in} \cup \Gamma^f_{out} \cup \Gamma^{s}_{top}} \int_{F} \frac{1}{\rho h} p_h q_h \, ds
\]

to the bilinear form (21) associated with the matrix $N_{h}^{\rho,\gamma}$ in the pressure block (20), and take the following continuous linear velocity auxiliary finite element space with the modified boundary conditions

\[
V^{cg}_{h} := \{ v \in H^1(\Omega) : v|_{K} \in [P^1(K)]^d, \forall K \in T_h, v|_{\Gamma^f_{in/out}} = 0, v \cdot n|_{\Gamma^f_{bot}} = 0, \text{tang}(v)|_{\Gamma^f_{in/out} \cup \Gamma^{s}_{top}} = 0 \}
\]

in the velocity block (22).

For the discretization parameters, we consider polynomial degree $k \in \{1, 2, 4\}$, a uniform unstructured triangular mesh with mesh size $h \in \{0.1, 0.05, 0.025\}$, and a uniform time step size $\delta t \in \{10^{-4}, 0.25 \times 10^{-4}\}$. For all the numerical simulations, we stop the MinRes iteration when residual norm is decreased by a factor of $tol = 10^{-6}$. The average number of MinRes iterations for different discretization parameters are documented in Table 5. From Table 5 we observe that

(a) for the same polynomial degree $k$ and mesh size $h$, a smaller time step size $\delta t$ leads to a smaller number of MinRes iterations.

(b) for the same mesh size $h$ and time step size $\delta t$, a larger polynomial degree $k$ leads to a larger number of MinRes iterations, with the number of iterations roughly doubled from $k = 1$ to $k = 4$.

(c) for the same time step size $\delta t$ and polynomial degree $k$, the number of MinRes iterations roughly stays in the same level as mesh size $h$ decreases.

We also mention that the MinRes iterations in Table 5 are smaller than those in Table 3–4 in Example 1, which is partially due to the fact that we used a larger stopping tolerance $tol = 10^{-6}$ here.

| $\delta t = 10^{-4}$ | $\delta t = 0.25 \times 10^{-4}$ |
|---------------------|---------------------|
| \begin{tabular}{c|c|c|c|c|c|c|c|c|c}
  $k$ & 1 & 2 & 4 & 1 & 2 & 4 & 1 & 2 & 4 \\
  \hline
  $1/h$ & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} \\
  10 & 76 & 133 & 213 & 59 & 79 & 143 & 59 & 79 & 143 \\
  20 & 89 & 106 & 158 & 60 & 83 & 134 & 60 & 83 & 134 \\
  40 & 89 & 115 & 167 & 72 & 98 & 150 & 72 & 98 & 150 \\
\end{tabular} | \begin{tabular}{c|c|c|c|c|c|c|c|c|c}
  $k$ & 1 & 2 & 4 & 1 & 2 & 4 & 1 & 2 & 4 \\
  \hline
  $1/h$ & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} & \multirow{2}{*}{iter} \\
  10 & 76 & 133 & 213 & 59 & 79 & 143 & 59 & 79 & 143 \\
  20 & 89 & 106 & 158 & 60 & 83 & 134 & 60 & 83 & 134 \\
  40 & 89 & 115 & 167 & 72 & 98 & 150 & 72 & 98 & 150 \\
\end{tabular} |

Table 5. Example 2: Average iteration counts for the preconditioned MinRes solver.

Finally, we plot in Figure 2 the flow rate, which is calculated as two thirds of the horizontal velocity, and pressure at the bottom boundary $\Gamma^f_{bot}$, and the vertical displacement on the interface
at final time \( t = 1.2 \times 10^{-2} \) for \( k = 1 \) with mesh size \( h \in \{0.05, 0.025\} \) and time step size \( \delta t = 10^{-4} \), \( k = 2 \) with mesh size \( h \in \{0.1, 0.05\} \) and time step size \( \delta t = 10^{-4} \), along with reference data for \( k = 4 \) with mesh size \( h = 0.025 \) and time step size \( \delta t = 0.25 \times 10^{-4} \). We observe that both the results for \( k = 1 \) and \( k = 2 \) agrees well with the reference data. We also observe that the result for \( k = 2 \) on the coarse mesh with mesh size \( h = 0.1 \) is more accurate that that for \( k = 1 \) on the medium mesh with mesh size \( h = 0.05 \), which indicates the benefits of using a scheme with a higher order spatial discretization.

5.3. Example 3: a linear three-dimensional test case on a straight cylindrical pipe. Now we consider a 3D example that simulates the propagation of the pressure pulse on a straight cylinder (see [13]). The fluid domain is a straight cylinder of radius 0.5 cm and length 5 cm, \( \Omega_f = \{(x, y, z) : x \in (0, 5), y^2 + z^2 < (0.5)^2\} \), the structure domain has a thickness of 0.1 cm, \( \Omega_s = \{(x, y, z) : x \in (0, 5), (0.5)^2 < y^2 + z^2 < (0.6)^2\} \), and the interface \( \Gamma = \{(x, y, z) : x \in (0, 5), y^2 + z^2 = (0.5)^2\} \). We use the same material parameters as in Example 2. The flow is initially at rest, and we take the same boundary conditions as in Example 2 with the exception that a pure Neumann boundary condition \( \sigma^s n = 0 \) is applied on the exterior structure boundary \( \Gamma_{ext}^s = \{(x, y, z) : x \in (0, 5), y^2 + z^2 = 0.6^2\} \).

We apply the scheme (10) with time step size \( \delta t = 10^{-4} \). For the spatial discretization parameters, we consider two cases: \( k = 1 \) on a fine mesh with mesh size \( h = 0.05 \) (264,288 tetrahedra), and \( k = 2 \) on a coarse mesh with mesh size \( h = 0.1 \) (33,036 tetrahedra). The fine mesh is illustrated in Figure 3. For the preconditioned MinRes linear system solver, we replace the point Gauss-Seidel smoother \( R \) in the velocity preconditioner (22) by a block Gauss-Seidel smoother \( R^e \) based on edge blocks to further improve its efficiency. We stop the MinRes iteration when residual norm is decreased by a factor of \( 10^{-6} \). The average number of iterations for convergence for \( k = 1 \) with \( h = 0.05 \) is 60 and that for \( k = 2 \) with \( h = 0.1 \) is 52 when the edge-block Gauss-Seidel smoother \( R^e \) is used in the velocity preconditioner (22). If we instead use the point Gauss-Seidel smoother, the numbers would be 360 for \( k = 1 \) and 246 for \( k = 2 \).

Similar to Example 2, we plot in Figure 4 the flow rate, which is calculated as two thirds of the horizontal velocity, and pressure at the center line \( \{(x, 0, 0) : x \in (0, 5)\} \), and the \( y \)-component of the displacement on the interface line \( \{(x, 0.5, 0) : x \in (0, 5)\} \) at final time \( t = 1.2 \times 10^{-2} \). We find that the results for \( k = 1 \) and \( k = 2 \) agrees well with each other.

Finally, we plot the structure deformation along with the fluid pressure for \( k = 2 \) with \( h = 0.1 \) in Figure 5 for \( t \in \{4, 8, 12\} \times 10^{-3} \). We clearly observe the propagation of a pressure pulse as time evolves.

6. Conclusion

We have present a novel monolithic divergence-conforming HDG scheme for a linear FSI problem with a thick structure. The fully discrete scheme produces an exactly divergence-free fluid velocity approximation and is energy-stable. Furthermore, we design an efficient block AMG preconditioner and use it with a preconditioned MinRes solver for the resulting symmetric and indefinite global linear system. This preconditioner is numerically observed to be robust with respect to the mesh size, time step size and material parameters in large parameter ranges. A theoretical analysis of this preconditioner is our future work.

The extension of our scheme to other FSI models including thin structure and/or moving interfaces consists of our ongoing work.

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**Example 2:** Numerical solutions of the scheme (10) with different discretization parameters at final time $t = 1.2 \times 10^{-2}$ [s]. Top: flow rate $\frac{2}{3}v_h[0]$ along bottom line $\Gamma_{bot}^f$. Middle: pressure along bottom line $\Gamma_{bot}^f$; Bottom: vertical displacement $\eta_s[h][1]$ along the interface $\Gamma$. Reference data is obtained with the HDG scheme (10) using polynomial degree $k = 4$, mesh size $h = 0.025$, and time step size $\delta t = 0.25 \times 10^{-4}$. All the other methods use the time step size $\delta t = 10^{-4}$. 

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**Figure 2.** Diagrams showing the flow rate, pressure, and vertical displacement for different discretization parameters.
Figure 3. Example 3: the fine mesh with mesh size $h = 0.05$. The red region is the fluid domain, and the gray region is the structure domain.

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Flow Rate

Pressure

Vertical Displacement

**Figure 4. Example 3:** Numerical solutions of the scheme \((10)\) with different discretization parameters along cut lines at final time \(t = 1.2 \times 10^{-2}[s]\). Top: flow rate \(\frac{k}{2}v_{h}[0]\) along center line \(\{(x,0,0) : x \in (0,5)\}\); Middle: pressure along center line \(\{(x,0,0) : x \in (0,5)\}\); Bottom: y-component of displacement \(\eta_{h}[1]\) along the interface line \(\{(x,0.5,0) : x \in (0,5)\}\).

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Figure 5. Example 3: The structure deformation and pressure approximation at different time. The structure deformation is enlarged by a factor of 8 and is only shown on half of the structure domain with $y < 0$. The pressure approximation is only shown on half of the fluid domain with $z < 0$. From top to bottom, $t = 0.004, 0.008, 0.012$. ($k = 2, h = 0.1$).
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