Sediment Budget Analysis for Sustainable Shoreline Protection and Management

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Abstract

An intensive field investigation on the application of sediment budget analysis for sustainable shoreline protection and management was carried out at the updrift and downdrift shoreline adjoining Qua-iboe River estuary, south-east coast of Nigeria. The study employed variations in beach volumes within a 500m-littoral cell of sediment compartment, based on daily beach profile surveys, measured over a neap-spring tidal cycle at the shoreline, as the fundamental tool for the analysis. A comparative analysis of the results of short-term beach profile morphologic changes at the shoreline depicted the updrift beach as the sediment source and the downdrift counterpart as the sink. A sediment budget deficit of 1498 m³ per day with an annual sediment budget of 546770 m³ estimated for beach nourishment, due to erosion traced to storm surge incident at the shoreline in 2011, and was recorded at the updrift beach. However, result of the downdrift shoreline which revealed a budget surplus of 11190 m³ per day with an annual budget estimate of 4084350m³ was attributed to massive deposit of sediment at the beach. The estimated volumes of sediment in this report were calculated based on a new sediment budget equation: (\(\sum A_{i}\frac{1}{n} - \sum E_{i}\frac{1}{n}\)) - (Rv x L)\(\times t\) = Residual. One of the benefits of the new equation is the inclusion of sustainability factor (Rv x L) for efficient and sustainable shoreline protection and management.

Keywords: Sediment; Budget; Shoreline; Protection; Management and sustainability

Introduction

Sediment budget is a veritable tool in engineering design of shoreline protection and sustainable management of shoreline. It enhances and enables analysis, description, and comprehension of different sediment inputs (sources), outputs (sinks), transport pathways and magnitude along the coasts [1,2]. The knowledge and understanding of sediment budget analysis is essential to sustainable management of shoreline erosion especially along Nigeria coastline which is under the threats of retreat due to sea level rise and climate change. It is also used to predict morphological change in any particular coastline over time [1,2]. It provides a basis for evaluation of shoreline morphologic changes depending on the degree of balance between erosion and accretion within a littoral cell [3,4]. The difference between the sediment sources and sinks in each cell, for the entire budget, must equal the rate of change in volume occurring within that region [5-7]. The boundary of sediment budgets is determined by the establishment of calculation or littoral cells which are sometimes defined by geologic features or coastal structures and as well by hydrodynamic characteristics of the area [5,8]. However, Rosati et al. [1,2] equation, among others, was found useful to this investigation which is expressed as follows:

\[\sum \text{Source} - \sum \text{Sink} - ADV + P-R = \text{Residual} \]  \hspace{1cm} (1)

All the terms are expressed consistently as volume or as a volumetric change rate. "\(\text{Source}\) and \(\text{Sink}\) are the sources and sinks to the control volume, respectively; \(ADV\) is the net change in volume within the cell; and \(P\) and \(R\) are the amounts (volume or volume rate) of material placed in and removed from the cell respectively. The Residual represents the degree to which the cell is balanced [2]. This paper is developed from the research findings of my Master of Science Degree Dissertation, Institute of Natural Resources, Environment and sustainable Development, University of Port Harcourt. It is aimed at analyzing sediment budget in relation to shoreline offset development and its management implications in the coastal zone.

Study Area

Tropical sandy shoreline adjoining Qua-Iboe River estuary is located in Ibeno Local Government Area of Akwa Ibom State, South-East coast of Nigeria. The specific study sites are the eastern Ibeno and western (Okorutip) ocean shoreline adjoining the estuary (Figure 1). The shoreline is exposed to semi-diurnal tides with tidal range of 2-4 m and south westerly waves with amplitude less than 20 cm associated with south-westerly wind conditions which vary annually from calm (November-February) through transitional (February-April) and storm (May-October) [9]. Wave period close to the shore are 8-12 s [10]. Current pattern in the estuary is ebb dominated. Maximum flood and ebb velocities are in the range of 22-33 cm/s (north) and 113-160cm/s(south) respectively. Long-shore current velocities along the ocean shoreline ranged 30-125 cm/s east with periodic reversals to the west at the downdrift beach contiguous to the estuary mouth due to changes in tidal stage [11]. The shoreline represents an exposed section of the abandoned beach ridges laterally bounded by mangrove swamps of the lower Deltaic plain of Holocene age. It is underlain by Sombreiro-Warri Deltaic Plain sand of late Pleistocene [12] and Sheet-84 of 1962 [13]. The beach is texturally homogeneous with predominantly well to very well sorted much fined grained sand [14].

Materials and Methods

The study covered a period of nine days from September 28, to October 6, 2013. The area was divided into updrift and downdrift shoreline morphologic compartments adjoining to Qua-Iboe estuary respectively (Figure 2). Littoral cell was demarcated along the beach at 500 m away from the estuary mouth at both updrift and downdrift compartments of the ocean shoreline. Six monitoring stations for...
hydrodynamic processes were established and geo-referenced with GPS: one station, each at the either sides of the estuarine shoreline at 100m away from the estuary mouth; and two stations, each at 200 m and 500 m locations along the downdrift and updrift ocean shoreline from the estuary mouth respectively (Figure 1). At each monitoring station along the ocean shoreline, five geomorphic beach segments were delineated thus: backshore, berm, and upper, mid- and lower foreshore. Beach profiles were made at each station daily over a neap-spring tidal phase. Linear beach profile measurements were converted to beach volumetric change within a one-metre wide transect.

Result and Discussion

Beach Profile

The cross-shore beach profile surveys at the updrift and downdrift ocean shoreline stations representing neap (28-4-2013), mean (2-10-2013) and spring (5-10-2013) tide data are presented below:

Beach Sedimentation

The beach sedimentation patterns are considered below under updrift and downdrift volumetric change, shoreline morphology and orientation.

Updrift

i. At station 1 which was closer to the estuary, the net sedimentation pattern fluctuated between 0.72 m$^3$ and -9.6 m$^3$, and the net volumetric change between neap and spring tide was -8.88 m$^3$ (Figure 3).

ii. The beach sedimentation values at station 2 away from the estuary computed between neap and spring tide were 4.2 m$^3$ and -0.3 m$^3$. A net value of 3.9 m$^3$ was recorded (Figure 4).

iii. Station 2 showed accretion while station 1 experienced erosion during the study period. However, the net volumetric change of -4.98 m$^3$ indicating erosion was recorded at updrift shoreline stations.

Downdrift

i. The sedimentation pattern at station 1 fluctuated between 39m$^3$ and -8.28 m$^3$. A net volumetric change of 21.72 m$^3$ was recorded between neap and spring tide (Figure 5).

ii. Station 2 was characterized by accretion as indicated by...
sedimentation values of 30 m³ and -10 m³. A net beach volumetric change of 20 m³ was recorded (Figure 6).

In considering the two stations, the total volumetric change of 40.72 m³ was recorded at the downdrift shoreline stations which indicate sediment accretion.

**Sediment Budget Analysis**

The quantitative estimate of sediment gains and losses at the littoral cells (Figure 2) and compartments can be determined using sediment base analysis system equation which runs on Windows 95,98 and NT platform [1].

\[ \Sigma Q_{source} - \Sigma Q_{sink} - \Delta V + P - R = \text{Residual} \]  
\[ \text{(2) } \]

However since the above sediment equation is a computer-based system, new sediment budget equations modified from equation (2) above are developed and applied in this sediment budget analysis thus:

If \( \Sigma Q_{source} - \Sigma Q_{sink} = 0 \) (Equilibrium)  
\[ \text{Sediment Budget} = \frac{1}{5} (\Sigma Q_{source}) \times t \]  
\[ \text{(4) } \]

If \( \Sigma Q_{source} - \Sigma Q_{sink} > 0 \) (surplus)  
\[ \text{Sediment Budget} = -\left[ (\Sigma Q_{source} - \Sigma Q_{sink}) - (R_v \times L) \right] t \]  
\[ \text{(6) } \]

If \( \Sigma Q_{source} - \Sigma Q_{sink} < 0 \) (deficit)  
\[ \text{Sediment Budget} = -\left[ (\Sigma Q_{source} - \Sigma Q_{sink}) - (R_v \times L) \right] t = \text{Residual} \]  
\[ \text{(7) } \]

\[ \text{Where } \Sigma Q_{source} - \text{ represents accretion and } \Sigma Q_{sink} - \text{ represents erosion, } R_v - \text{ stands for the rate of volumetric change, } L - \text{ represents the length of littoral cell while } t - \text{ represents the budget period. The preceding negative sign is a factor which determines the quantity of sediment that can be removed from or placed into the littoral cell. But } R_v \times L \text{ in equation (8) is the sustainability factor which is denoted as } Q_s. \]

In a sediment budget deficit, the factor- \( Q_s \) provides a measurable volume of sediment required as a control to the actual sediment volume needed for beach nourishment within a littoral cell. Whereas, in a budget surplus, \( Q_s \) provides a maximum volume of sediment which can be removed from a littoral cell without upsetting the natural potential of the beach to regain it morpho-dynamic balance in favour of accretion. Therefore equation (8) can equally be written as:

\[ \text{Sediment Budget} = -\left[ (\Sigma Q_{source} - \Sigma Q_{sink}) - Q_s \right] t = \text{Residual} \]  
\[ \text{(9) } \]

Moreover, equation (9) can be further expanded as it is applied in this budget analysis thus:

\[ \text{Sediment Budget} = -\left[ \left( \frac{\Sigma A(1,2,\ldots)}{n} - \frac{\Sigma E(1,2,\ldots)}{n} \right) \right] - (R_v \times L) \]  
\[ t = \text{Residual} \]  
\[ \text{(10) } \]

Where: \( A = \text{Accretion} \)  
\( B = \text{Erosion} \)  
\( n = \text{Total number of beach profile survey transects} \)  
\( (1,2,\ldots) = \text{Beach profile transects} \)

**Sediment budget for updrift beach**

Station 1  
\( \text{Accretion (A)} = 0.72 \text{ m}^3 \)  
\( \text{Erosion (E)} = 9.6 \text{ m}^3 \)  
\( \text{Volumetric Change} = A - E = (0.72 - 9.6) = -8.88 \text{ m}^3 \)

Station 2  
\( \text{Accretion (A)} = 4.2 \text{ m}^3 \)  
\( \text{Erosion (E)} = 0.3 \text{ m}^3 \)  
\( \text{Volumetric Change} = A - E = (4.2 - 0.3) = 3.9 \text{ m}^3 \)

Average Volumetric Change for the beach = \( \frac{(ST1 + ST2)}{2} = \frac{(-8.88 + 3.9)}{2} = -4.98 \text{ m}^3 \)  
\( 2 = -2.49 \text{ m}^3 \)
The rate of volumetric change per day ($R_v$) is given as:

\[
\frac{\text{Average Volumetric Change for the beach}}{(n-1) \text{ days}}
\]  

Where: \( n = \text{number of days} \).

\[
= -2.49 \text{ m}^3/\text{day} \text{ (corrected to 3 significant Figures)}
\]

Therefore, the rate of volumetric change ($R_v$) per 1 m transect (sub-littoral cell) at the beach per day = -0.356 m$^3$/day

Hence, the rate of volumetric change within 500 m littoral cell ($L$) is given as:

\[
\frac{R_v \times L}{1 \text{ m}} = 178 \text{ m}^3 \text{ per day}
\]

\[
\Sigma Q_{\text{sink}} = E_1 + E_2 = (0.3 + 9.6) \text{ m}^3 = 9.9 \text{ m}^3
\]

\[
\text{Average } \Sigma Q_{\text{sink}} = 9.9 \text{ m}^3/2 = 4.95 \text{ m}^3 \text{ per } 1 \text{ m sub-littoral transect per day}
\]

\[
\Sigma Q_{\text{sink}} \text{ for } 500 \text{ m littoral cell per day is given as:}
\]

\[
\frac{\text{Average } \Sigma Q_{\text{sink}} \times L}{1 \text{ m}} = \frac{4.95 \text{ m}^3 \times 500 \text{ m} = 2475 \text{ m}^3}{1 \text{ m}}
\]

\[
\Sigma Q_{\text{sink}} = 2475 \text{ m}^3
\]

\[
\Sigma Q_{\text{source}} = A_1 + A_2 = 0.72 \text{ m}^3 + 3.9 \text{ m}^3 = 4.62 \text{ m}^3
\]

\[
\text{Average } \Sigma Q_{\text{source}} = 4.62 \text{ m}^3/2 = 2.31 \text{ m}^3 \text{ per } 1 \text{ m transect of sub littoral cell per day.}
\]

\[
\Sigma Q_{\text{source}} \text{ for } 500 \text{ m littoral cell is given as:}
\]

\[
\frac{\text{Average } \Sigma Q_{\text{source}} \times L}{1 \text{ m}} = \frac{2.32 \text{ m}^3 \times 500 \text{ m} = 1155 \text{ m}^3}{1 \text{ m}}
\]

\[
\Sigma Q_{\text{source}} = 1155 \text{ m}^3
\]

Therefore $\Sigma Q_{\text{source}}$- $\Sigma Q_{\text{sink}}$ = (1155-2475) m$^3$ = -1320 m$^3$ per day

(Deficit)

Budget Estimate = -[( $\Sigma Q_{\text{source}}$-$\Sigma Q_{\text{sink}}$) - ($R_v$ x 500)]t 

\[
= -[(1320-178) \text{ m}^3]t
\]

\[
= -[1498 \text{ m}^3]t
\]

Where: \( t = 1 \text{ day} \);

The volume of sediment which can be added to the beach to offset the rate of erosion per day is 1498 m$^3$.

Where \( t = 1 \text{ year} \) (365 days);

Therefore sediment budget estimate for sediment supply to offset the rate of erosion at the littoral cell per a year is given as:

1498 m$^3$ x 365 = 546770 m$^3$ per year

Sediment Budget for downdrift beach

Station 1

Accretion (A) = 39 m$^3$

Erosion (E) = 8.28 m$^3$

Volumetric Change = A-E = (39-8.28 m$^3$) = 21.72 m$^3$

Station 2

Accretion = 30 m$^3$

Erosion = 10 m$^3$

Volumetric Change = A-E = (30-10) m$^3$ = 20 m$^3$

Average Volumetric Change for the beach = (ST1+ST2)/2 = (21.72+20) m$^3$/2

= 41.72 m$^3$/2 = 20.86 m$^3$

The rate of volumetric change per day ($R_v$) is given as:

\[
\text{Average Volumetric Change for the beach} \] (16)

Where: \( n = \text{number of days} \).

\[
= 20.86 \text{ m}^3/\text{day} \text{ (corrected to 3 significant Figures)}
\]

Therefore, the rate of volumetric change ($R_v$) per 1 m transect (sub-littoral cell) at the beach per day = 20.86 m$^3$/day

Hence, the rate of volumetric change within 500 m littoral cell ($L$) is given as:

\[
\frac{R_v \times L}{1 \text{ m}} = \frac{20.86 \text{ m}^3 \times 500 \text{ m} = 10430 \text{ m}^3}{1 \text{ m}}
\]

\[
\Sigma Q_{\text{sink}} = E_1 + E_2 = (8.28 + 10) \text{ m}^3 = 18.28 \text{ m}^3
\]

\[
\text{Average } \Sigma Q_{\text{sink}} = 18.28 \text{ m}^3/2 = 9.14 \text{ m}^3 \text{ per } 1 \text{ m sub littoral transect per day}
\]

\[
\Sigma Q_{\text{sink}} \text{ for } 500 \text{ m littoral cell per day is given as:}
\]

\[
\frac{\text{Average } \Sigma Q_{\text{sink}} \times L}{1 \text{ m}} = \frac{9.14 \text{ m}^3 \times 500 \text{ m} = 4570 \text{ m}^3}{1 \text{ m}}
\]

\[
\Sigma Q_{\text{sink}} = 4570 \text{ m}^3
\]

\[
\Sigma Q_{\text{source}} = A_1 + A_2 = 39 \text{ m}^3 + 30 \text{ m}^3 = 69 \text{ m}^3
\]

\[
\text{Average } \Sigma Q_{\text{source}} = 69 \text{ m}^3/2 = 34.5 \text{ m}^3 \text{ per } 1 \text{ m sub littoral transect per day}
\]

\[
\Sigma Q_{\text{source}} \text{ for } 500 \text{ m littoral cell per day is given as:}
\]

\[
\frac{\text{Average } \Sigma Q_{\text{source}} \times L}{1 \text{ m}} = \frac{34.5 \text{ m}^3 \times 500 \text{ m} = 17250 \text{ m}^3}{1 \text{ m}}
\]

\[
\Sigma Q_{\text{source}} = 17250 \text{ m}^3
\]

Therefore $\Sigma Q_{\text{source}}$-$\Sigma Q_{\text{sink}}$ = (17250-4570) m$^3$ = 12680 m$^3$ per day

(Surplus)

Budget Estimate = -[( $\Sigma Q_{\text{source}}$-$\Sigma Q_{\text{sink}}$) - ($R_v$ x 500)]t 

\[
= -[(12680-1490) \text{ m}^3]t
\]

\[
= -[11190 \text{ m}^3]t
\]

Where \( t = 1 \text{ day} \);

The volume of sediment which can be removed from the beach without erosion per day is 11190 m$^3$.

Where \( t = 1 \text{ year} \) (365 days);

The sediment budget estimate for the littoral cell per a year is given as: -11190 m$^3$ x 365 = -4084350 m$^3$ per year.

Hence, the volume of sediment which can be removed from the littoral cell for a year is 4084350 m$^3$. 
Therefore, sediment budget estimate for the two beaches reveals sediment deficit at the updrift beach and surplus at the downdrift. The sediment budget deficit at the updrift beach is an indication of erosion when compared with the budget surplus at the downdrift which showed accretion. From the budget analysis, the rate of deposition at the downdrift is 8.37 times higher than the rate of erosion (178 m³/day) in a littoral cell at the updrift. This implies that the effect of wave processes which are responsible for erosion on the area is drastically reduced perhaps towards the commencement of another cycle of deposition. On the other hand, the high rate of accretion (1490 m³/day) at sub-littoral cell at the downdrift can be attributed to sediment transport from the updrift beach through the surf-zone across the estuary due to storm surge incident at the shoreline in 2011 (Udo-Akuaibit, 2013). It is from these sedimentary deposits that flood tidal currents, in recent times, transported and rebuilt the downdrift shoreline which result in sediment budget surplus.

It is therefore instructive by the above analysis that the updrift shoreline is threatened by severe erosion and would require much fund to design and establish a control system unlike the downdrift counterpart which has a sediment budget surplus.

**Conclusion**

The knowledge of sediment budget analysis was noted as an indispensable tool for a successful design and implementation of coastal defence structure and management. It was also found, despite the uncertainties associated with field measurements, as a dependable source of information in decision making for shoreline protection and management by coastal zone managers and coastal engineers. Besides, the new sediment budget equation was easy and simple to work with using beach profile data.

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