Resolving velocity ambiguity of two coded pulse in broad-band acoustic Doppler current profiler

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Abstract. Broad-band Acoustic Doppler Current Profiler (BBADCP) adopts short-sequence coded pulse to measure high velocity. Short-sequence coded pulse has large measurable velocity, so it is not easy to have velocity ambiguity. But short coded pulse deteriorates the accuracy of the velocity. To obtain more accurate velocity, we adopt two coded pulse with a time lag. This paper analyzes the ambiguity velocity and velocity standard deviation of two coded pulse and single coded pulse, and gives a solution to resolve velocity ambiguity: single coded pulse which has a large ambiguity velocity due to the short time lag is used to establish a coarse estimate of the velocity, two coded pulse which has a long time lag is used to have a high accuracy velocity, then we combine the two velocities in a way to provide an accurate velocity. It has been demonstrated that the two coded pulse can reduce variance of velocity through analyzing numerous experimental data of pool. Meanwhile, the efficiency of method to solve ambiguity has been proved in accordance with multiple sets of data. Compared with the traditional methods, this method has good anti-noise performance and high single measurement accuracy.

1 Introduction

Acoustic Doppler Current Profiler is currently the most important velocity measuring device in the world. It is widely used in marine and river engineering. The ADCPs can be divided into three types: incoherent, pulse-to-pulse coherent, and broad-band ADCP. Broad-band ADCP transmits repeat-sequence coded signals\cite{1-4}, which have a large time bandwidth product that satisfies the requirements of high resolution, high accuracy, and large measurement velocity. After transmitting, it receives echoes formed by the scattering of the scatterers. Due to the Doppler shift caused by the relative motion between the transducer and the scatterers, the velocity can be estimated by detecting the change of the correlated pulse-pairs. The commonly used estimation method is complex autocorrelation method\cite{5,6}. It estimates the phase change according to the autocorrelation property of the echoes. For the phase change is limited to \([-\pi,\pi]\), it will have velocity ambiguity at high velocity. The length of the subsequence of the repeat-sequence coded signal affects the velocity ambiguity and measurement accuracy\cite{7,8}, which makes a contradiction between the measurable velocity and velocity accuracy.

People have been paying attention to solving velocity ambiguity for many years. The simplest and most straightforward ambiguity resolution scheme used a short-lag long-lag approach\cite{9}: the short-lag pulse-pair is used to establish a coarse estimate of the velocity, the short-lag pulse-pair provides more precise phase shift information. In 2008, A. E. Hay and L. Zedel proposed a method to extend the velocity ambiguity by transmitting multi-frequency signals, which was possible to extend the maximum measurable velocity, and analyzed the performance of the method\cite{10,11}. In 2014, P. Liu and N. Kouguichi proposed a combined method of incoherent and coherent Doppler sonar to avoid velocity ambiguity\cite{12}. The incoherent method can completely eliminate the velocity ambiguity, but it is necessary to perform multiple measurements and average to obtain satisfactory measurement results.

To this end, this paper proposes a combination method to provide accurate and precise velocity of two coded pulses with a time lag. Compared with the traditional method, this method has good anti-noise performance and high single measurement accuracy. It can obtain good velocity result without multiple measurements.

2 Velocity ambiguity of BBADCP

2.1 Repeat-sequence coded signal

BBADCP adopts repeat-sequence coded pulse. The subsequence is selected to have a small autocorrelation when the lag time is not zero. Commonly used codes are Barker codes and M-sequence codes. They have been shown to have small autocorrelation values when the codes are not completely aligned. Fig.1 shows the autocorrelation function of the 7-bit and 31-bit M-sequence codes, respectively. The number of repetition is 2.

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\begin{figure}[h]
\centering
\includegraphics[width=\textwidth]{figure1.png}
\caption{Autocorrelation function of 7-bit and 31-bit M-sequence codes.}
\end{figure}
The M-sequence codes have small and stable correlations when the measurement lag is not a subsequence multiple. When the subsequence is determined, increasing the number of sequence repetitions can increase the signal-to-noise ratio and the autocorrelation property of the echo. Fig. 2 shows the autocorrelation function of the 31-bit M-sequence with repetitions of 2 and 6, respectively. The theoretical autocorrelation value of the repetition of 2 is 0.50, and the repetition of 6 is 0.83. However, increasing the repetitions leads to correlation peaks at the multiples of the subsequence, which reduces the statistical independence of the individual echo samples, and provides some undesired correlation of self-noise.

Different subsequence length has different effect on the system measurement variance. When the length of subsequences is shorter, the phase variance is smaller due to the shorter time lag of the sample pair. But phase noise will have a larger influence on the final velocity measurement, so the larger the subsequence length, the higher the velocity accuracy. However, longer subsequence decreases the measurement range. It’s easy to have velocity ambiguity.

2.2 Pulse-pair method and velocity ambiguity

The pulse-pair method estimates the Doppler shift by comparing the phase of the echo. The change in phase is proportional to the velocity. The code bit of a repeat-sequence encoded pulse is given by

\[
f(t) = a(t)e^{j2\pi f_0 t}
\]

where \(a(t)\) represents the code bit of the baseband coded signal, \(f_0\) is the carrier frequency. The repeat-sequence coded pulse can be expressed as

\[
s_o(t) = \sum_{n=1}^{M_L} [a(t-mT)]e^{j2\pi f_0 t}
\]

where \(L\) is the number of code bits in a subsequence, \(M\) represents the repetitions of the subsequence, and \(T\) is the length of bit. The two coded pulse of a time lag can be written as

\[
s(t) = \sum_{n=1}^{M_L} a(t-mT) + \sum_{n=M+1}^{2M_L} a(t-nT-\Delta T)]e^{j2\pi f_0 t}
\]

where \(\Delta T\) is the time interval between two coded pulse. The received echo signal is superimposed by a large number of scattered signals. Assuming that the relative velocity between the transducer and the scatter is \(v\), and the scattered signals are independent of each other. For \(v \ll c\), the Doppler shift of the echo can be expressed as

\[
f_d \approx 2vf_0/c, \text{ where } c \text{ is the sound speed in seawater.}
\]

The received echo can be expressed as

\[
r(t) = \sum_i b_is(t-\tau_i)e^{j2\pi(f_0+\Delta f(t-\tau_i))}
\]

where \(b_i\) is the amplitude of the \(i\)th scattered signal and \(\tau_i\) represents time delay. The influence of external noise is not considered here. The echo signal which is demodulated and filtered can be given as

\[
r(t) = \sum_i b_i \sum_{n=1}^{M_L} a(t-mT-\tau_i)e^{j2\pi f_0(t-\tau_i)}
\]

\[
\quad+ \sum_i b_i \sum_{n=M+1}^{2M_L} a(t-nT-\Delta T-\tau_i)e^{j2\pi f_0(t-\tau_i)}
\]

Doppler shift can be estimated by complex autocorrelation method

\[
f_d = \frac{1}{2\pi T_L} \arctan \left( \frac{\text{Im}(R_u(T_L))}{\text{Re}(R_u(T_L))} \right)
\]

where \(T_L = MLT + \Delta T\), \(R_u(T_L)\) is the autocorrelation function of the echo signal with the measurement lag \(T_L\). Fig. 4 shows the autocorrelation process of the two coded pulse.

Since the phase change is limited to \([-\pi, \pi]\), when the velocity is estimated by the phase method, the velocity range is limited to \([-V_m, V_m]\), where \(V_m\) is the ambiguity velocity.
\[ V_e = \frac{c}{4f_j \tau_L} \]  

When the true velocity exceeds the range \([-V_m, V_m]\), velocity ambiguity occurs.

### 3 Measurement deviation analysis

Regardless of the influence of the environmental noise, the main source of the standard deviation is the self-noise of the signal itself. The self-noise is the non-overlapping part of the echo. As shown in Figure 4, the signal of the dotted line frame is not used in estimating the Doppler shift, which is equivalent to noise introduced by the signal. So it is called self-noise. But it does not ultimately have effect on the overlap of the signal.

When the interval between the two coded pulses is very small, it can be regarded as a repeat-sequence coded pulse signal, and the repetition \( M=2M \). The received echo is sampled at a sampling interval of \( T \), assuming that the sampling rate is equal to the system bandwidth, so that each sample is independent. At time \( t_0 \), the received echo is

\[ A_e = e^{j2\pi f_j t_0 \sum_{m=1}^{M_L} a(t-mT)b_{n_m}} \]

The received echo at time \( t_0 (t_0=t_0+nt) \) can be expressed as

\[ A_e = e^{j2\pi f_j (t_0+nt) \sum_{m=1}^{M_L} a(t-mT)b_{n_m}} \]

the autocorrelation function of the \( k \)th sample at measurement lag \( \tau \) can be given as

\[ R_k(\tau) = A_k^* A_{k+\tau} \]

\[ R_k(\tau) = e^{j2\pi f_j \sum_{m=1}^{M_L} \sum_{m=1}^{M_L} a^*(t-mT)a(t-nT)b_{n_m}^* b_{n_{m+\tau}}} \]  

Assuming that the scatters in the water are uniformly distributed, the echo strength of different bits is the same, and the samples of the received echo are sufficient. For ideal coded signal, the expected value of the autocorrelation can be expressed as (the time lag is \( T_L \))

\[ E(R_k) = B e^{j2\pi f_j \sum_{m=1}^{M_L} \sum_{m=1}^{M_L} A_{m}^* A_{m} B \frac{ML}{2} e^{j2\pi f_j \tau}} \]

where \( B=\langle b_{m}\rangle^2 \) is the expected intensity of each cell and \( |a|^2 \equiv 1 \). The main cause of the velocity estimation error is the phase error of the autocorrelation function. To facilitate the analysis, the Doppler shift is set to 0, that is, the error introduced by the self-noise in the static condition is considered. The phase error term can be represented by the imaginary part of the signal autocorrelation function

\[ \langle E^2 \rangle = \frac{1}{4} \left\langle \left| R_{\tau} - R_{\tau}^* \right|^2 \right\rangle \]

\[ \approx \frac{1}{2} \left\langle \left| R_{\tau} \right|^2 - \left\langle R_{\tau} R_{\tau}^* \right\rangle - \operatorname{Re} \left\langle R_{\tau} R_{\tau}^* \right\rangle \right\rangle \]

\[ \approx \frac{3}{8} B^2 L^2 M^2 \]

which \(<\cdot><\cdot>\) represent time average. Then we should consider averaging samples in a period of time or range, and obtain small velocity variance. When the samples are completely independent, the phase error can be reduced to \( 1/NL \), where \( NL \) is the number of samples in the range averaging. But the correlation peaks are introduced at the multiple of the subsequence, so the self-noise will reduce the statistical independence of the samples in range averaging. For ideal coded pulse, the correlation is 0, when the lag time is not multiples of the subsequence. The phase error after range averaging is

\[ \langle E^2 \rangle = (NL)^{-1} \sum_{n=1}^{NL} \left\{ \text{Im}(R_{ML}(n)) \text{Im}(R_{ML}(m)) \right\} \]

\[ \approx (NL)^{-1} \left( E^2 + \frac{2}{NL} \left( N+1 \right) N \left( 2N+1 \right) L^2 \left( \frac{1}{2} B^2 L^2 \right) \right) \]  

The phase variance \( \sigma^2 \) is the ratio of \( E^2 \) to the expected autocorrelation

\[ \sigma^2 = \frac{E^2}{\left\langle R_{\tau} \right\rangle^2} \approx \frac{3}{2} \frac{M^2 + \frac{2}{3} (N+1)(2N+1)}{LM^2} \]

\[ \sigma^2 \approx \frac{3}{2} \frac{M^2 + \frac{2}{3} (N+1)(2N+1)}{LM^2} \]  

\[ \left( \frac{c}{4\pi f_j \tau_L} \right)^2 \]  

\[ \left( \frac{c}{4\pi f_j \tau_L} \right)^2 \]

The interval between the two coded pulse can increase the length of the time lag and does not introduce self-noise, so the final velocity variance can be reduced. But too long a time lag will decrease the echo correlation, increasing the velocity variance. Since the scatters are constantly moving, after a certain time interval, some of the scatters will leave the area ensonified by the acoustic beam, and some of new scatters will enter. The scatters in the ensonified area change more as the interval increases, so the residence time becomes shorter and the correlation of the pulse pairs decreases. The residence time is proportional to the velocity. When the measure velocity is low, the decorrelation caused by the scatters change is small, and the pulse interval can be appropriately increased to improve the accuracy. However, when higher velocity is measured, a shorter time lag is advisable.

### 4 Amendment of velocity ambiguity
4.1 Method

To obtain more precise velocity information and avoid velocity ambiguity, this paper proposes a method to realize ambiguity interval determination of the two coded pulse. The basic method is: the single coded pulse which has a large ambiguity velocity due to the short time lag is used to establish a coarse estimate of the velocity, and the two coded pulse which has a long time lag is used to have a high accuracy velocity, then we combine the two velocities in a way to provide an accurate and precise velocity.

According to equation (7), the ambiguity velocity is inversely proportional to the measurement lag. The single coded pulse has a large measurable velocity range $[-V_M, V_M]$ due to the short time lag, which is the $T_{11}/T_{12}$ Times of the range of the two coded signal ($T_{11}/T_{12}$ is an integer). The velocity range of the single coded signal is equally divided into $T_{11}/T_{12}$ cells, as shown in Fig.5. First, the average velocity ($\bar{v}$) of the single coded pulse signals is estimated by the complex autocorrelation function method, the velocity standard deviation $\sigma_v$ is calculated, so the true velocity range $[\bar{v} - 3\sigma_v, \bar{v} + 3\sigma_v]$ is determined. Second, the more accurate velocity $v_2$ is obtained by the two coded pulse. Since the velocity of the two coded pulse may be limited to the range $[-V_M/V_M]$, the real velocity should be $v_2 + 2n \times V_m$, where $n$ is 0, ±1, ±2, … ± $T_{11}/T_{12}$. And it is in the true velocity range $[\bar{v} - 3\sigma_v, \bar{v} + 3\sigma_v]$. That is

$$-v_1 - 3\sigma_v \leq v_2 + 2n \times V_m \leq v_1 + 3\sigma_v$$ (16)

Finally, the integer factor $n$ can be determined by (16), so the accurate and precise velocity is calculated.

$$v_a = v_2 + 2n \times V_m$$ (17)

4.2 Boundary

When $v_2$ is close to the ambiguity boundary $\pm V_M$, the true velocity range $[\bar{v} - 3\sigma_v, \bar{v} + 3\sigma_v]$ is related to two ambiguity intervals, but $n$ is unique. It should be determined by the symbol of $v_2$. When $v_2$ is considered to be close to the boundary of the ambiguity velocity. If $v_2 \leq 0$, the true velocity $v_a$ is in the left half of a certain interval, $n = \frac{\sqrt{v^2 - 3\sigma_v v_2}}{2V_m}$; if $v_2 > 0$, the true velocity $v_a$ is in the right half of a certain interval, $n = \frac{\sqrt{v^2 + 3\sigma_v v_2}}{2V_m}$.

\begin{figure}[h]
\centering
\includegraphics[width=0.5\textwidth]{fig5.png}
\caption{Ambiguity velocity interval.}
\end{figure}

4.3 Conditions

In order to prevent the interval misjudgment, the condition must be satisfied: $V_m > 3\sigma_v$, otherwise the factor $n$ is not unique. This method uses single coded pulse to establish a coarse estimate of the velocity. To ensure a large ambiguity velocity, the measurement lag should be short, so a short-sequence coded signal is advisable.

5 Experimental results

To verify the feasibility of the algorithm, we carried out the pool test. The pool test site is shown in Fig.6. The depth of water is 1.8 meters.

\begin{figure}[h]
\centering
\includegraphics[width=0.5\textwidth]{fig6.png}
\caption{The pool test site.}
\end{figure}

Loading an ADCP onto the driving vehicle, the transducer is heading vertically to the bottom of the water. When the vehicle is driving at a constant speed, the ADCP transmits two coded pulse and receives echo signals.

\begin{figure}[h]
\centering
\includegraphics[width=0.5\textwidth]{fig7.png}
\caption{Velocities of single coded pulse and two coded pulse.}
\end{figure}

The velocity is estimated by the complex autocorrelation function, and the ambiguity velocity is corrected by the combined method. Among them, the length of the two coded pulse is 1.3584ms, the carrier frequency is 600kHz, the code length is 7, the repetition is 4, the interval between the two coded pulse is 1ms, and the average velocity of the vehicle is about 180.8cm/s. The single beam ambiguity velocity of the two coded pulse calculated by the actual parameters is 145.93cm/s. The actual velocity exceeds the ambiguity...
velocity. The measurement velocities of the single coded pulse and the two coded pulse are shown in Fig. 7.

![Fig. 8. Amendment of velocity ambiguity.](image)

The variance of the velocity measured by two coded pulse is significantly smaller than single coded pulse. But the two coded pulse has velocity ambiguity. The method of resolving velocity ambiguity is used to correct the velocity. The result is shown in Fig. 8. The accuracy of the algorithm can be verified by observing the velocity results. The correct rate of the velocity is so high that no misjudgments occur. Fig. 9 shows the velocity at the boundary of the ambiguity velocity. It can be seen that the correct rate of the algorithm is very high at the ambiguity boundary from Fig. 10. The length of the two coded pulse in Fig. 9 and Fig. 10 is 1.4728ms, the carrier frequency is 600kHz, the code length is 19, the repetition is 2, the interval between the two coded pulse is 0.5ms. The average velocity of the vehicle is about 181cm/s.

6 Conclusions

To avoid velocity ambiguity, this paper proposes a combination method to obtain accurate and precise velocity. Experiments are carried out to verify the accuracy of the method. Compared with the traditional methods, this method has good anti-noise performance and high single measurement accuracy. It can obtain good velocity results without multiple measurements. It does not change the original signal coded mechanism and system structure, having good applicability.

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