A Probabilistic Assessment of Tephra-Fall Hazards at Hanford, Washington, from a Future Eruption of Mount St. Helens
Cover. The Hanford pre-treatment facility, under construction, November 2016. USGS photo by Larry G. Mastin.
A Probabilistic Assessment of Tephra-Fall Hazards at Hanford, Washington, from a Future Eruption of Mount St. Helens

By Larry G. Mastin, Alexa Van Eaton, and Hans F. Schwaiger

Prepared in cooperation with the U.S. Department of Energy, Office of River Protection

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# Conversion Factors

International System of Units to U.S. customary units

| Multiply       | By             | To obtain                |
|----------------|----------------|--------------------------|
| **Length**     |                |                          |
| centimeter (cm)| 0.3937         | inch (in.)               |
| millimeter (mm)| 0.03937        | inch (in.)               |
| meter (m)      | 3.281          | foot (ft)                |
| kilometer (km) | 0.6214         | mile (mi)                |
| kilometer (km) | 0.5400         | mile, nautical (nmi)     |
| meter (m)      | 1.094          | yard (yd)                |
| **Area**       |                |                          |
| square meter (m²)| 0.0002471    | acre                     |
| hectare (ha)   | 2.471          | acre                     |
| square hectometer (hm²)| 2.471 | acre                     |
| square kilometer (km²)| 247.1 | acre                     |
| square centimeter (cm²)| 0.001076 | square foot (ft²)        |
| square meter (m²)| 10.76      | square foot (ft²)        |
| square centimeter (cm²)| 0.1550 | square inch (in²)        |
| square hectometer (hm²)| 0.003861 | section (640 acres or 1 square mile) |
| hectare (ha)   | 0.003861       | square mile (mi²)        |
| square kilometer (km²)| 0.3861 | square mile (mi²)        |
| **Volume**     |                |                          |
| cubic meter (m³)| 6.290        | barrel (petroleum, 1 barrel = 42 gal) |
| cubic meter (m³)| 264.2        | gallon (gal)             |
| cubic decimeter (dm³)| 0.2642 | gallon (gal)             |
| cubic meter (m³)| 0.0002642    | million gallons (Mgal)   |
| cubic centimeter (cm³)| 0.06102 | cubic inch (in³)        |
| cubic decimeter (dm³)| 61.02      | cubic inch (in³)        |
| liter (L)      | 61.02          | cubic inch (in³)        |
| cubic decimeter (dm³)| 0.03531 | cubic foot (ft³)        |
| cubic meter (m³)| 35.31         | cubic foot (ft³)        |
| cubic meter (m³)| 1.308         | cubic yard (yd³)        |
| cubic kilometer (km³)| 0.2399 | cubic mile (mi³)        |
| cubic meter (m³)| 0.0008107     | acre-foot (acre-ft)     |
| cubic hectometer (hm³)| 810.7      | acre-foot (acre-ft)     |
### Conversion Factors—Continued

| Multiply          | By           | To obtain                                      |
|-------------------|--------------|------------------------------------------------|
| gram (g)          | 0.03527      | ounce, avoirdupois (oz)                        |
| kilogram (kg)     | 2.205        | pound avoirdupois (lb)                        |
| metric ton (t)    | 1.102        | ton, short [2,000 lb]                         |
| metric ton (t)    | 0.9842       | ton, long [2,240 lb]                          |

| Density           |              |                                                |
|-------------------|--------------|------------------------------------------------|
| kilogram per cubic meter (kg/m³) | 0.06242 | pound per cubic foot (lb/ft³) |
| gram per cubic centimeter (g/cm³) | 62.4220 | pound per cubic foot (lb/ft³) |

Temperature in degrees Celsius (°C) may be converted to degrees Fahrenheit (°F) as follows:

\[ °F = (1.8 \times °C) + 32. \]

Temperature in degrees Fahrenheit (°F) may be converted to degrees Celsius (°C) as follows:

\[ °C = (°F - 32) / 1.8. \]

### Abbreviations

- **DOE/ORP**: U.S. Department of Energy, Office of River Protection
- **DRE**: Dense-rock equivalent
- **ECMWF**: European Centre for Medium-Range Weather Forecasts
- **ERA**: European Centre for Medium-Range Weather Forecasts reanalysis
- **GSD**: grain-size distribution
- **GVP**: Global Volcanism Program
- **HVAC**: heating, ventilation, and air conditioning
- **MSH**: Mount St. Helens
- **pdf**: probability density function
- **PM**: particulate matter
- **SEM**: scanning electron microscope
- **TSP**: total suspended particulates
- **USGS**: U.S. Geological Survey
- **VEI**: Volcanic Explosivity Index
- **VTTS**: Valley of Ten Thousand Smokes
- **WTP**: Waste Treatment and Immobilization Plant
A Probabilistic Assessment of Tephra-Fall Hazards at Hanford, Washington, from a Future Eruption of Mount St. Helens

By Larry G. Mastin, Alexa Van Eaton, and Hans F. Schwaiger

Abstract

Hanford, Washington (USA) is the construction site of a multi-billion-dollar high-level nuclear waste treatment facility. This site lies 200 kilometers (km) east of Mount St. Helens (MSH), the most active volcano in the contiguous United States. Tephra from a future MSH eruption could pose a hazard to the air intake and filtration systems at this plant. In this report, we present a probabilistic estimate of the amount of tephra that could fall, and the concentrations of airborne ash that could occur at the Hanford Site during a future eruption. Mount St. Helens has produced four large explosive eruptions in approximately the past 500 years, suggesting that its annual probability of eruption \((P_e)\) is roughly \(4/500 = 0.008\). Assuming that a large eruption occurs, we calculate the probability \((P_{d|e})\) of a given fall deposit thickness or airborne concentration at Hanford by running about 10,000 simulations of ash-producing eruptions using the atmospheric transport model Ash3d. In each simulation, we calculate the pattern of tephra dispersal, deposit thickness at Hanford, and airborne ash concentration at ground level. As input for each simulation, we choose meteorological conditions from a randomly chosen time in the historical record between 1980 and 2010, using data from the European Centre for Medium-Range Weather Forecasting (ECMWF) Reanalysis (ERA) Interim model. The volume (dense-rock equivalent) of each simulated eruption is randomly chosen from a uniform probability distribution on a log scale from the range of magma volumes \((0.008–2.3 \text{ cubic kilometers} [\text{km}^3])\) estimated for late Holocene eruptions at MSH. Plume heights and durations of each eruption are chosen using empirical correlations between volume, height, and eruption rate, which account for the fact that larger eruptions have higher plumes and last longer. We construct summary tables of final deposit thickness \((T)\), maximum ground-level airborne concentration \((C_{\text{max}})\), and average ground-level airborne concentration \((C_{\text{avg}})\) during tephra-fall for each run. Each table is sorted and ranked by decreasing value of \(T\), \(C_{\text{max}}\), or \(C_{\text{avg}}\); Conditional probabilities \((P_{d|e})\) are derived by dividing rank by \(n+1\), where \(n\) is the total number of successful runs. For example, a deposit thickness of 5.10 centimeters \((\text{cm})\) from run 446 is ranked 123 of 9,785 successful runs, yielding \(P_{d|e} = 123/9,786 = 0.01257\). Its annual probability is \(P = P_{d|e} \cdot P_e = 0.008 \times 0.01257 = 0.000101\). By interpolation, the deposit thickness \((T_{10k})\) having an annual probability of 1 in 10,000 \((P = 0.0001)\) is 5.11 cm. Analogous concentration values are \(C_{\text{max,10k}} = 3.819\) and \(C_{\text{avg,10k}} = 1.513\) milligrams per cubic meter \((\text{mg}/\text{m}^3)\), respectively. Independent calculations using the known mass accumulation rate of the deposit \((M = 0.001–0.006 \text{ kilograms per square meter per second} [\text{kg}/\text{m}^2/\text{s}])\), aggregate fall velocities \((u = 0.3–0.8 \text{ meters per second} [\text{m}/\text{s}])\), and the simple formula \(C = M/u\), yield similar results, although highly variable fall velocities add significant uncertainty. This formula implies that deposit accumulation rates of millimeters \((\text{mm})\) to greater than 1 cm per hour, which are not uncommon during heavy ash fall, are associated with airborne concentrations of \(10^2–10^3\) milligrams per cubic meter \((\text{mg}/\text{m}^3)\). These concentrations are much higher than published measurements \((10^3–10^4\text{ mg}/\text{m}^3)\), which record only suspended particles sampled in sheltered areas. During heavy ashfall, most fine ash falls as aggregates. Whether such aggregates will be ingested into air ducts will depend on the aggregate size and fall rate, the fragility of the aggregates, the air duct geometry, intake velocity, and other factors.

Introduction

Radioactive waste generated during World War II and the Cold War were originally contained in 177 underground tanks at the Hanford Site near Richland, Washington. In support of its nationwide environmental cleanup of nuclear facilities, the U.S. Department of Energy (DOE), Office of River Protection (ORP) is constructing a facility and supporting infrastructure (the Waste Treatment and immobilization Plant [WTP]) to retrieve, process and vitrify this waste for permanent storage. An explosive eruption from Mount St. Helens (MSH) could potentially deposit enough ash at Hanford to temporarily disrupt site operations (for example, WTP). DOE Standards that provide criteria and guidance for natural phenomena hazards analysis (for example DOE-STD-1020, Section 8) require that this be stated in probabilistic terms. For this project, it is interpreted to mean, “What deposit thickness and airborne ash concentration could be expected at Hanford given a Mount St. Helens eruption with an annual exceedance probability of 1 in 10,000?” We notate the thickness and concentration values at this threshold as \(T_{10k}\) and \(C_{10k}\), respectively (see table 1 for a list of variables). This report provides a methodology to quantify these values.
In 2011, Hoblitt and Scott (2011) found that ashfall at the Hanford site would most likely come from MSH, rather than Mount Rainier, Hood, Adams, or other regional volcanoes. Hoblitt and Scott (2011) also estimated $T_{10K}$ empirically from volcanological and meteorological data, by breaking the problem into three components:

1. What is the annual probability of a large ash-producing eruption ($P_{1|2}$) from MSH? Hoblitt and Scott noted that four large eruptions had occurred at MSH in approximately the past 500 years, suggesting that $P_{1|2} \approx 4/500 = 0.008$.

2. Given a large eruption, what is the probability that wind will be blowing toward Hanford ($P_{1|2}$)? From historical records they concluded that $P_{1|2} \approx 0.18$.

3. Given an eruption with wind blowing toward Hanford, what is the exceedance probability of a given amount of ash fall (for example, 1, 5, or 10 centimeters [cm]) at Hanford ($P_{1|2}$)? To address this question, they examined the thickness of 14 large eruptions whose deposits could be tracked 200 kilometers (km). The thickest deposited 10 cm, suggesting $P_{3|2} = 1/(14+1) = 0.067$ of greater than 10 cm thickness. The product $P_{3|2} \cdot P_{1|2} \cdot P_{1|2} = 0.008 \cdot 0.18 \cdot 0.067$ is about 1 in 10,000, implying that $T_{10K} \approx 10$ cm.

Snow and Nelson (2012) used this result, and an assumed deposit density of 1,125 kilograms per cubic meter (kg/m$^3$), to calculate an approximate mass load ($M$) of 112 kilograms per square meter (kg/m$^2$). Assuming a settling rate of $u = 1.7$ meters per second (m/s) and an ashfall duration of $D_s = 12$ hours (hrs, 43,200 seconds [s]), they calculated an airborne tephra concentration at ground level of $C = M/D_s u = 1,500$ milligrams per cubic meter (mg/m$^3$). Airborne concentrations this high could be economically challenging to filter.

A more sophisticated analysis could provide a more robust result. The erupted magma volume, plume height, eruption duration, and size distribution resulting from the next large eruption are uncertain; but a reasonable range of estimates can be made from past eruptions at Mount St. Helens and from eruptions of similar size around the world. Given specified inputs, the tephra-fall thickness at Hanford can be calculated using transport models such as the U.S. Geological Survey (USGS) Ash3d model (Schwaiger and others, 2012).

The purpose of this study is to use a Monte Carlo procedure and approximately 10,000 model simulations to calculate probabilities of exceedance of specified levels of ashfall or airborne concentration ($P_{3|2}$), given an eruption whose size and other characteristics range within likely bounds for Mount St. Helens. The probability $P_{3|2}$ replaces the product $P_{1|2} \cdot P_{1|2}$ from Hoblitt and Scott (2011). Combined with $P_{3|2}$, our results yield new values of tephra-fall thickness ($T_{10K}$) and maximum ($C_{max,10K}$) or average ($C_{avg,10K}$) airborne ash concentration having an annual probability of occurrence of 1 in 10,000. Key inputs for each simulation are assigned following Monte Carlo procedures, using methods similar to other studies (Stirling and Wilson, 2002; Hurst and Smith, 2004; Mastrolorenzo and others, 2008; Amigo, 2013; Bear-Crozier and others, 2016).

### Table 1. List of variables.

| Variable       | Description                                           | Units     |
|----------------|-------------------------------------------------------|-----------|
| $A$            | Area on ground surface                                | m$^2$     |
| $a, b, c$      | Ellipsoid semi-axes                                   | m         |
| $C$            | Airborne ash concentration                            | mg/m$^3$  |
| $C_{max}$      | Maximum airborne concentration during the period of Tephra-fall | mg/m$^3$  |
| $C_{avg}$      | Average airborne concentration during the period of Tephra-fall (dosage divided by fall duration) | mg/m$^3$  |
| $C_{max,10K}$  | Value of the maximum airborne ash concentration at Hanford having a recurrence interval of 10,000 yrs | mg/m$^3$  |
| $C_{avg,10K}$  | Value of the average airborne ash concentration at Hanford having a recurrence interval of 10,000 yrs | mg/m$^3$  |
| $C_{max,2K}$   | Value of the maximum airborne ash concentration at Hanford having a recurrence interval of 2,000 yrs | mg/m$^3$  |
| $C_{avg,2K}$   | Value of the average airborne ash concentration at Hanford having a recurrence interval of 2,000 yrs | mg/m$^3$  |
| $C_{max,1K}$   | Value of the maximum airborne ash concentration at Hanford having a recurrence interval of 1,000 yrs | mg/m$^3$  |
| $C_{avg,1K}$   | Value of the average airborne ash concentration at Hanford having a recurrence interval of 1,000 yrs | mg/m$^3$  |
| $D_s$          | Eruption duration                                     | hrs       |
| $D_f$          | Duration of ash fall                                  | hrs       |
| $d$            | Particle diameter                                     | mm        |

[Abbreviations: DRE, dense-rock equivalent; hr, hour; kg, kilogram; kg/m$^3$, kilogram per square meter; kg/m$^2$, kilogram per cubic meter; kg/m$^3$/s, kilogram per square meter per second; kg/s, kilogram per second; km, kilometer; km$^2$, square kilometer; km$^3$, cubic kilometer; m, meter; m/s, meter per second; m$^2$/s, square meter per second; mm, millimeter; mg/m$^3$, milligram per cubic meter; mg-s/m, milligram-seconds per cubic meter; yr, year]
| Variable | Description | Units |
|----------|-------------|-------|
| $d_e$ | Eruption dosage (airborne concentration times time) | mg·s/m³ |
| $dz$ | Vertical nodal spacing | km |
| $F$ | Particle shape factor $= (b+c)/2a$ | |
| $H$ | Plume height above sea level | km |
| $H_{bestfit}$ | Plume height above the vent calculated by equation 3 | km |
| $H_v$ | Plume height above the vent | km |
| $K_x$ | Diffusion coefficient in the horizontal direction | m²/s |
| $k$ | Suzuki constant | |
| $k_1,k_2,k_3$ | Slopes of lines on plots of log thickness versus square root of area covered | km⁻¹ |
| $M$ | Mass load of tephra deposit | kg/m² |
| $M_d$ | Mass accumulation rate of deposit | kg/m²/s |
| $m$ | Deposit mass | kg |
| $m_{<0.063}$ | Mass fraction ash in the deposit <0.063 mm | |
| $m_{size}$ | Mass fraction of a deposit moved into the aggregate size classes | |
| $m_{size}$ | Mass fraction of non-aggregating particles of size class i | |
| $n$ | Number of successful runs | |
| $P$ | Annual exceedance probability of a given tephra-fall thickness $T$ or airborne ash concentration $C$. $P=P_1P_2P_3$ (Hoblitt and Scott, 2011), or $P=P_1P_3$ (this study) | |
| $P_1$ | Annual probability of eruption, from (Hoblitt and Scott, 2011) (=0.008) | |
| $P_2$ | Probability of wind blowing toward Hanford given that an eruption has occurred, from Hoblitt and Scott (2011) | |
| $P_3$ | Probability of exceedance of a given tephra thickness given that an eruption has occurred, and that the wind is blowing toward Hanford. From Hoblitt and Scott | |
| $P_{3|1}$ | Probability of exceedance of a given tephra thickness or ash concentration given that an eruption has occurred | |
| $Q_m$ | Mass eruption rate | kg/s |
| $T$ | Tephra-fall thickness | mm |
| $T_{10K}$ | Tephra-fall thickness at Hanford having an annual probability of $P=0.0001$ (the “1-in-10,000-year event”) | mm |
| $T_{2K}$ | Tephra-fall thickness at Hanford having an annual probability of $P=0.0005$ (the “1-in-2,000-year event”) | mm |
| $T_{1K}$ | Tephra-fall thickness at Hanford having an annual probability of $P=0.001$ (the “1-in-1,000-year event”) | mm |
| $t_d$ | Arrival time of ashfall, in hours after the start of the eruption | hrs |
| $u$ | Settling velocity | m/s |
| $V$ | Erupted volume (DRE) | km³ |
| $V_{min}$ | Minimum erupted volume used in model simulations, (volume in DRE) | km³ |
| $V_{max}$ | Maximum erupted volume (DRE) used in model simulations. Equal to the volume of largest eruption likely to occur for the purposes of this study | km³ |
| $z_v$ | Elevation above the vent | m |
| $\phi$ | Particle size, $\phi=-\log_{2}(d)$, where $d$ is particle diameter in millimeters | |
| $\phi_{p,i}$ | Size of non-aggregating particle of class i | $\phi$ |
| $\mu_{agg}$ | Median aggregate size | $\phi$ |
| $\rho_{p}$ | Density of particle | kg/m³ |
| $\rho_{agg}$ | Density of aggregate | kg/m³ |
| $\rho_d$ | Density of deposit | kg/m³ |
| $\rho_m$ | Density of magma | kg/m³ |
| $\sigma_{agg}$ | Standard deviation in aggregate size | $\phi$ |
An accompanying study, appendix 1, characterizes the size and shape of tephra particles that have been tested for resuspension properties as part of this Department of Energy Ashfall Project (Etyemezian and others, 2019). The appendix was added as a means of publishing results that were contracted by DOE. A second appendix (appendix 2) describes a follow-up study that examines the effect that rare, very large events might have on our estimates of $T_{10k}$, $C_{max,10k}$, and $C_{avg,10k}$. This follow-up study was taken in response to concerns expressed by the Defense Nuclear Facilities Safety Board that our original study, which did not consider such events, could underestimate the hazard.

The Explosive History of Mount St. Helens

Mount St. Helens is the most active and among the most explosive volcanoes in the Cascade Range of North America. The Cascade Range extends along the west coast from Lassen Peak (California) in the south to Mount Garibaldi (British Columbia) in the north, roughly the same range of latitude where the Juan de Fuca Plate subducts beneath the North American Plate at a rate of about 40 millimeters per year (mm/yr) (Coltice and others, 2017). Globally, volcanic arcs with the highest rate of volcanism are those whose subduction rates are high. The subduction rate of the Juan de Fuca Plate beneath North America is in the middle of the range of subduction rates observed worldwide (as much as 80 mm/yr). Magma production rates along the Cascade arc are modest in comparison with, for example, those volcanic arcs of Indonesia or the southern Andes.

Volcanism along the Cascade arc has persisted for tens of millions of years, but most individual volcanoes, like Mount St. Helens or Mount Rainier, are only hundreds of thousands of years old. Mounts Rainier, St. Helens, and other Cascade volcanoes are built on eroded volcanic centers from past geologic periods. Mount St. Helens, for example, sits atop igneous rocks with an age of 28–23 mega-annum (Ma) (Evarts and others, 1987). Mount Rainier overlies rocks of age 36–14 Ma (Vance and others, 2001). All Mount St. Helens rocks are younger than about 300 ka (Clynne and others, 2008), and all of the Mount St. Helens edifice is younger than 4 ka—younger than the pyramids of Egypt.

Stratovolcanoes, such as the main Cascade Range peaks, primarily erupt during stages lasting centuries to millennia. At Mount St. Helens, the current, highly active stage (the Spirit Lake stage) has continued since 3.9 ka; earlier stages extended from 16–10 ka (Swift Creek), and 28–18 ka (Cougar stage; Pallister and others, 2017). Brief periods of quiescence are between these stages of activity.

In the past 4,000 years, MSH has produced nine mapped tephra deposits that can be traced tens, hundreds, or even greater than 1,000 kilometers from the volcano (Westgate, 1977; Zoltai, 1989; Carey and others, 1995; Mullineaux, 1996). By comparison, ash-producing eruptions from the neighboring volcanoes of Mounts Adams, Hood, and Rainier have been few and small during this period. At 8 kilometers from the vent, for example, the thickest post-4 ka tephra deposit from MSH (Yn of table 2) is about 2 meters (m) thick (Mullineaux, 1986; Carey and others, 1995). For comparison, at 7 km distance from Rainier, the thickest post-4 ka Rainier deposit (the C tephra) is about 30 centimeters (cm) (Mullineaux, 1974); and at 6 km from Mount Adams, the thickest layer (layer 23 of Hildreth and Fierstein [1997]) is less than 10 cm. At Mount Hood, the only post-4 ka tephra deposits were produced when domes growing south of the summit collapsed and avalanched down the steep south flank, releasing clouds of debris. Such deposits are decimeters thick near Timberline Lodge, 5 km south of the vent (Scott and Gardner, 2017). Thus, we infer that the tephra hazard to Hanford is primarily from eruptions of Mount St. Helens.

What We Learned from the Eruption of 1980

The May 18, 1980, eruption gave us vivid images of the hazard ash poses in central Washington. It also demonstrated some key processes that have influenced how we have set up this modeling study.

The May 18, 1980, eruption followed 2 months of precursory activity; seismicity started on March 20 and included many earthquakes of magnitude 3, 4, and even 5. Dramatic deformation of the volcano’s north flank (growth of the “bulge”) was underway within a few days of the onset of seismicity. Phreatic (steam) eruptions from the summit started March 27 and continued through early May. The climactic eruption on May 18, however, was not preceded by any uptick in seismicity or deformation rate in the hours or days preceding the event.

The May 18 eruption started with gravitational collapse of the north flank of the volcano, which had been destabilized by intrusion of a magma body into the upper edifice. At 8:32 a.m. local time, the north flank abruptly slid outward, uncorking the magma body whose gases expanded northward as a pyroclastic density current that destroyed about 600 square kilometers of forest. As the pyroclastic current rode over the ground surface, it entrained air and became buoyant, lifted off the ground from an area about 10 km north of the summit, rose to about 32 km in the atmosphere, and expanded as an umbrella cloud to about 150 km in diameter (Sparks and others, 1986; Holasek and Self, 1995) (fig. 1B).

Within a few tens of minutes after the flank collapse (Christiansen and Peterson, 1981), a vertical Plinian column began rising from the volcano’s decapitated summit, reached about 15 km above sea level, and fluctuated between 13 and 17 km for the next 9 hours (Harris and others, 1981). In the first few hours, airborne ash moved downwind from both the Plinian column and the umbrella cloud. In the afternoon, ash injected by the Plinian column was supplemented by fine ash rising buoyantly from pyroclastic flows that avalanched down the volcano’s north flank (fig. 1D).

The resulting ash cloud moved eastward at an average speed of 100 kilometers per hour (km/hr), reaching Yakima, Washington around 9:45 a.m. Pacific Time; Pasco, Washington
Figure 1. Maps and images from the May 18, 1980, eruption at Mount St. Helens. A, Mass load map of the May 18, 1980, Mount St. Helens tephra deposit, digitized from figure 338 of Sarna-Wojcicki and others (1981). B, Composite photograph of the growing umbrella cloud, taken from Toledo, Washington around 8:45 a.m. Wikimedia Commons photo by Rocky Koberg. C, Scanning electron microscope (SEM) image of ash collected in Yakima, Washington, 144 kilometers (km) downwind. D, Plume and pyroclastic flow activity at the vent around 1:50 p.m. USGS photograph by Joe Rosenbaum. E, Image of Washington Street, Yakima, taken around noon on May 18, 1980. U.S. Forest Service photograph. F, Tephra-fall thickness at Moses Lake, 250 km downwind. USGS photo by Daniel Dzurisin. G, Isopach map of the deposit, digitized from figure 336 of Sarna-Wojcicki and others (1981). km$^3$, cubic kilometers; mm, millimeter; USGS, U.S. Geological Survey; μm, micrometer.
around 10:45; Spokane around noon; and Missoula, Montana at about 3:00 p.m. (Sarna-Wojcicki and others, 1981). Although the plume reached heights of 32 km (15 ±2 km for the Plinian phase), the cloud’s leading edge that passed over central Washington was around 10–12 km elevation, where wind speeds were highest.

The tephra-fall deposit from this eruption (fig. 1A) is one of the world’s most thoroughly studied. Within days, field crews drove north-south transects across Washington State, stopping regularly (red dots, fig. 1A) to measure the thickness (T) of the deposit, and collect ash from measured areas (A) on the ground or on flat surfaces such as the roofs of cars, stairs (fig. 1F), or sidewalks. The fresh deposit had not yet been altered by wind or by rain, allowing scientists to sample to distances of more than 600 km, where thicknesses were a fraction of a millimeter. The samples were dried and weighed to obtain a mass (m), and to calculate a mass per unit area (M = m/A) and a deposit density (ρg = M/T) at each location. Maps of both thickness (fig. 1G) and mass load (fig. 1A) were created by contouring these data.

Like new-fallen snow, these deposits were light and fluffy. Bulk deposit densities in central Washington and beyond averaged 450 kg/m³ and decreased to less than 100 kg/m³ beyond 500 km distance (Sarna-Wojcicki and others, 1981). Rainfall rapidly compacted the ash, as observed when sampling deposits from May 25 and June 12 eruptions, which were accompanied or shortly followed by rain and had densities of 1,000 to 1,250 kg/m³ (Sarna-Wojcicki and others, 1981). Grain-size distributions were also analyzed from many samples, and then combined in a weighted sum to estimate the grain-size distribution of the entire erupted mass (Carey and Sigurdsson, 1982; Durant and others, 2009).

Several key findings were noted:

1. The overall grain-size distribution (fig. 2G) was exceedingly fine, with more than 60 percent of the erupted mass consisting of particles finer than 0.06 mm diameter. Beyond about 200 km distance, greater than 75 percent of ash was less than 0.06 mm diameter (Durant and others, 2009). Much of the fine ash consists of the walls of burst pumice bubbles. The fine grain size has been linked to both the bubble sizes in the magma (dominantly 0.01–0.022 millimeters [mm] (Genareau and others, 2012)) and the milling of ash within pyroclastic flows (Dartevelle and others, 2002).

2. The median grain size of the ash decreased downwind to about 300 km distance, then remained constant at greater distance (Carey and Sigurdsson, 1982; Durant and others, 2009).

3. The grain-size distribution (GSD) at about 25–200 km distance was bimodal (fig. 2A–C). A coarse mode of particles a few tenths of a millimeter in diameter dominated at proximal distances (fig. 2A, B), but they decreased in both median size and in mass fraction with distance and disappeared from the size distribution beyond about 200 km (fig. 2D). A fine mode of particles with a median size of 8–16 micrometers did not change significantly in median size but increased in abundance with distance.

4. Isopach maps showed that both deposit thickness and mass load decreased with distance, but they then increased again to form an intriguing secondary maximum about 290 km downwind (fig. 1G), near the town of Ritzville, Washington (Sarna-Wojcicki and others, 1981). At this distance, about 93 percent of the tephra is smaller than 0.06 mm. Particles of this size, falling from a 15-km-high plume, would not have deposited at this distance under these wind conditions if they were falling individually.

5. These observations indicate that the fine ash modes in figure 2A–F fell as clusters, so that their fall velocity was independent of the size of individual particles. The increased ashfall near Ritzville suggests either that the clusters had a narrow range of fall velocities (0.66–0.78 m/s; (Mastin and others, 2016)), causing them to land at a similar location, or that there was a change in the ash cloud that led to rapid sedimentation once the plume reached Ritzville. These ash clusters could be observed during active fallout. In Pullman, Washington for example (390 km downwind), aggregates were captured on wet, painted cardboard and described as delicate clusters 0.25–0.5 mm in diameter, composed of particles from less than 0.001 to 0.04 mm in size (Sorem, 1982). Nearly all aggregates disintegrated on landing and left little evidence of their existence in the deposit.

The bulk volume of the May 18, 1980, deposit, was estimated at 1.1 km³ and was calculated by determining the area within each isopach line, multiplying each isopach area by the isopach thickness, and then summing (Sarna-Wojcicki and others, 1981). Using the measured average deposit density and assuming a magma density of 2,000–2,600 kg/m³, Sarna-Wojcicki and others (1981) estimated the bulk tephra volume to be equivalent to about 0.20 to 0.25 cubic kilometers (km³) of dense-rock-equivalent (DRE) magma. Later, the estimate was revised to 0.33 km³ (Criswell, 1987; Pallister and others, 1992).

Older Tephra Deposits

Field geologists, in the past five decades, have identified and named at least a dozen sets of tephra beds at Mount St.
Figure 2. Graphs showing particle-size distributions of tephra-fall from the May 18, 1980, eruption at Mount St. Helens. A–F, Particle-size distributions of the deposit at different distances from the source, based on grain-size analyses published in Durant and others (2009). Names of samples analyzed are listed on the figure. Locations of these samples are shown in figure 1A. G, Total grain-size distribution (TGSD) for combined deposit. Blue bars give the mass fraction in a given bin. Blue lines with dots give the cumulative mass fraction coarser than the given size. Black dashed line is 0.063 millimeters (mm). km, kilometer.
Table 2. Tephra deposits from large Plinian eruptions of Holocene age at Mount St. Helens, Washington.

[For prehistoric eruptions, ages (column 2) are taken from Nathenson (2017). Columns 3–6 give approximate volumes of the deposits, as bulk tephra (columns 3 and 4), and dense-rock equivalent magma (DRE, columns 5 and 6). Volumes in columns 3 and 5 are from Carey and others (1995); those in 4 and 6 are revisions by Nathenson (2017). For the 1980 eruption, the erupted volume (DRE) of 0.3 km³ for the Plinian fall deposit is from Pallister and others (1992) Abbreviations: cal yrs B.P., calendar years before present (where present is 1950 C.E.); C.E., common era; DRE, dense-rock equivalent; km³, cubic kilometer; yr, year]

| Deposit name | Age       | Bulk volume, in km³ | DRE Volume, in km³ |
|--------------|-----------|---------------------|-------------------|
|              |           | Carey   | Nathenson | Carey   | Nathenson |
| 1980         | 1980 C.E. | 1.1     | 1.1       | 0.3     | 0.3       |
| T            | 1800 C.E. | 1.5     | 0.12–0.34 | 0.4     | 0.031–0.089 |
| We           | 1482 C.E. | 1.5     | 0.15–0.80 | 0.4     | 0.039–0.21 |
| Wn           | 1479 C.E. | 7.7     | 0.71–1.4  | 2.0     | 0.19–0.37 |
| Pu           | 2500–2900 cal. yrs B.P. | 0.8 | 0.030–0.18 | 0.2 | 0.008–0.047 |
| Ps           | 2550–2900 cal. yrs B.P. | 0.4 | 0.031–0.18 | 0.1 | 0.008–0.047 |
| Ye           | 3300–3500 cal. yrs B.P. | 3.5 | 0.5–1.5  | 0.9     | 0.13–0.39 |
| Yn           | 3500 cal. yrs B.P. | 15.3 | 1.6–8.8  | 4.0     | 0.78–2.3  |
| Yb           | 3850–3900 cal. yrs B.P. | 1.2 | 0.044–0.26 | 0.3 | 0.011–0.068 |
Figure 3. Map and graphs showing thickness of the Yn and 1980 deposits at Mount St. Helens. A, Measured thicknesses of the Yn deposit at Mount St. Helens and isopach contours of the thickness distribution, digitized from figure 3A of Carey and others (1995). B, Plot of log thickness (T) versus square root (sqrt) of the area encompassed within each isopach line for the May 18, 1980, deposit (fig. 1G). C, Plot of log thickness versus square root of area within each isopach for the Yn deposit (fig. 3A). Blue dots are the area within isopach lines (the lines had to be extrapolated to form closed polygons to derive these data points). Red line is the best-fit line through these points. Blue dashed line is the distal line inferred by Carey and others (1995) to derive a bulk tephra volume of 15.3 cubic kilometers (km³). Black lines were distal lines inferred by Nathenson (2017) to derive his estimated tephra volumes. km, kilometer.
Methods

To simulate tephra transport and deposition, we use the model Ash3d, developed by the U.S. Geological Survey (Schwaiger and others, 2012). Ash3d is an Eulerian, finite-volume, advection-diffusion model that divides the atmosphere into a three-dimentional grid of cells (fig. 4). In each cell, at each time step, atmospheric properties such as wind vectors, temperature and pressure are linearly interpolated from the nearest cells in a numerical weather prediction model.

The column of cells above the volcano (fig. 4B) act as source nodes, meaning that at each time step, a mass of ash is added to each node and distributed vertically using the following equation (Suzuki, 1983), with an adjustable constant $k$ that modulates the degree to which mass is concentrated near the top of the column:

$$\frac{dQ_m}{dz_v} = \frac{Q_m}{H_v} \frac{k^2 (1 - z / H_v) \exp(k(z_v / H_v - 1))}{1 - (1 + k) \exp(-k)}$$

where

- $Q_m$ is the mass eruption rate (kilograms per second [kg/s]),
- $H_v$ is plume height above the vent; and
- $z_v$ is elevation (above the vent) within the plume.

Within each cell, at a given time step, Ash3d calculates the flux through cell walls as tephra is: (1) advected by wind, (2) settles by gravity, and (3) spreads by turbulent diffusion. Advection and settling are calculated through the Donor-Cell Upwind method using a Lax-Wendroff scheme (LeVeque, 2002, Chapter 6) in which flux in each direction is calculated sequentially (dimension splitting). Diffusion is calculated using an implicit Crank-Nicolson method in each coordinate to keep time steps reasonable (Schwaiger and others, 2012). Diffusion rates are calculated using a specified diffusion constant $K_x$. The calculations are done sequentially for each of a series of grain-size classes. These size classes represent individual particle sizes, or aggregates of particles. Particles or aggregates are assumed to be ellipsoidal in shape, with a specified diameter $d$, density $\rho$, and shape factor $F \equiv (b + c) / 2a$, where $a$, $b$, and $c$ are the semi-major, intermediate, and semi-minor axes of an ellipsoid, respectively. The diameter $d$ is assumed to equal $(a + b + c) / 3$, and the volume is assumed to equal $\pi d^3 / 6$. The settling rate of particles or aggregates is calculated using relations of Wilson and Huang (1979).

Inputs

We define four categories of model inputs. The first category consists of eruption source parameters as conventionally defined in Mastin and others (2009), such as, erupted volume ($V$), plume height ($H$), duration ($D_e$), and a GSD characterized by parameters defined later. The source parameters differ from one simulation to the next, using...

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Figure 4. Model grid used by the Ash3d model for simulations. A, Full view of the model grid. B, Close-up of the grid in southern Washington State, highlighting the source nodes above Mount St. Helens, and the Hanford, Washington site. Grid spacing is 0.1° latitude and longitude.
procedures described below and summarized in table 3. Many of the parameter assignments involve randomly selecting the value of a variable from within a probability density function (pdf). The types of pdfs we use are uniform (fig. 5A) in which the probability of a given value is equal within a min–max range; and Gaussian (fig. 5B), in which the probability is highest at a mean value and decreases at a rate defined by the standard deviation.

The second category includes secondary physical parameters such as the Suzuki constant $k$; particle shape factor $F$; densities of particles ($\rho_p$), the deposit ($\rho_d$), and magma ($\rho_m$); and the diffusion coefficient $K_x$. These parameters do not vary between simulations. Rather, we use values that have been found to accurately reproduce mapped deposits in other studies (table 4). The third category consists of meteorological parameters: the wind field, atmospheric pressure, and temperature, which are used to calculate particle advection and fall velocities. These values are obtained from the output of an external meteorological model. The fourth category includes model settings such as vertical and horizontal cell spacing, which have been adjusted to give an acceptable balance between model accuracy and speed.

Table 3. Summary of procedures used to assign eruption source parameters in each simulation.

| Parameter                     | Method of assignment                                                                 |
|-------------------------------|--------------------------------------------------------------------------------------|
| Erupted volume ($V^*$)        | We choose randomly from a uniform pdf on a log scale, extending from $V_{\text{min}}=0.008$ to $V_{\text{max}}=2.3$ km$^3$ DRE. |
| Plume height ($H_v^*$)        | We calculate $H_v$ from $V^*$ using equation 3, and then add a random value, sampling from a Gaussian pdf with a mean of zero and a standard deviation of 2.9 km. |
| Eruption Duration ($D_e$)     | We calculate the eruption rate from the plume height using equation 2, and then calculate the duration by converting erupted volume to mass (assuming $\rho_m=2,500$ kg/m$^3$) and dividing by the rate $Q_m$. |
| Grain-size distribution       | We assume that all fine ash aggregates and characterize the fine ash fraction using two adjustable parameters, its fraction of the erupted mass ($m_{\text{fines}}$) and the size of aggregates ($\mu_{\text{agg}}$). We choose $m_{\text{fines}}$ from a Gaussian pdf that has a mean of 0.5 and standard deviation of 0.15, based on considerations explained in the text. We choose $\mu_{\text{agg}}$ from a Gaussian pdf having a median of $\phi=2.4$ (0.189mm) and a standard deviation of $\phi=0.1$ ($\pm7\%$). The aggregates are divided into five bins with mass fractions as shown in table 6 for median aggregate size $\sigma_{\text{agg}}=0.1$. For particles that do not aggregate, we use sizes and mass fractions derived from the May 18, 1980, deposit (Durant and others, 2009), with two modifications: (1) we consolidate particles greater than 2mm, which generally deposit at less than 100km distance, into a single $d=2$mm size bin; and (2) we adjust the mass fraction in each bin equally so that the sum in all these bins, plus $m_{\text{fines}}$, equals 1. |
| Eruption start time           | We randomly choose a start time within the period January 1, 1980, to January 1, 2010. |

Table 4. Values of secondary physical parameters and model settings used in each simulation.

| Physical Parameter or setting                      | Value                       |
|----------------------------------------------------|-----------------------------|
| Model domain                                       | 45–49°N                     |
|                                                   | 123–113°W                   |
|                                                   | 0–35 km asl (30 percent higher than plume) |
| Vent location                                      | 122.18°W                    |
|                                                   | 46.2°N                      |
| Vent elevation                                     | 2.00 (km)                   |
| Nodal spacing                                      | 0.1° horizontal             |
|                                                   | 2.0 km vertical             |
| Diffusion coefficient ($K_x$)                      | 0                           |
| Suzuki constant ($k$)                              | 8                           |
| Particle shape factor ($F$)                         | 0.44                        |
| Deposit density ($\rho_d$)                         | 1,000 kg/m$^3$              |
| Magma density ($\rho_m$)                           | 2,500 kg/m$^3$              |
| Aggregate shape factor ($F$)                        | 1.00                        |

Figure 5. Illustration of the two types of probability density functions (pdf’s) used to assign parameter values in this study: uniform (A) and Gaussian (B).
Eruption Source Parameters

We ran approximately 10,000 Ash3d simulations using a modified Monte Carlo approach. We did not use a straight Markov Chain Monte Carlo method, in which all key inputs are randomly assigned, independently of the others, because some inputs were correlated. For example, larger-volume eruptions tend to have higher plumes, and longer durations. Below, we explain how these relations are considered.

Erupted Volume

We choose volume \( V \) from a uniform pdf on a log scale ranging from 0.008–2.3 km\(^3\) DRE—the range estimated by Nathenson (2017); table 2) for Holocene Mount St. Helens eruptions. Eruptions smaller than 0.008 km\(^3\) are unlikely to impact the Hanford site. Our choice of a log scale implies that 0.1 km\(^3\) eruptions are about 10 times as likely as 1 km\(^3\) eruptions and reflects the greater frequency of small eruptions in the Holocene record.

Plume Height

Larger-volume eruptions produce higher plumes. On May 18, 1980, for example, Mount St. Helens erupted ash for about 9 hours at an average rate of \( 2 \times 10^7 \) kg/s (Carey and Sigurdsson, 1985). The Plinian phase (after 9:00 a.m.) produced a plume that fluctuated around 14 km above the vent (Harris and others, 1981). The much larger June 15, 1991, eruption of Mount Pinatubo in the Philippines expelled close to \( 1 \times 10^9 \) kg/s of magma for several hours (Koyaguchi and Tokuno, 1993), producing a maximum height of 34–39 km above the vent (Holasek and others, 1996). The smaller Eyjafjallajökull eruption in Iceland on April 14–18, 2010, emitted an average mass rate of \( 5 \times 10^5 \) kg/s (Gudmundsson and others, 2012) and produced plume heights about 4–8 km above the vent (Arason and others, 2011).

Historical eruption data illustrate this relationship. Because big eruptions produce higher plumes than small ones, the plume height for each simulation cannot be chosen independently from erupted volume. Data have been published for a few dozen recent eruptions for which average plume height, erupted mass, and duration have been recorded (Wilson and others, 1978, table 3; Sparks and others, 1997, table 5.1; Mastin and others, 2009, table 1). The correlation observed in equation 2 is based on a few dozen examples (fig. 64; (Mastin and others, 2009):

\[
H_v = 0.3Q_m^{0.241},
\]

where \( H_v \) is the plume height in kilometers above the vent; and \( Q_m \) is the mass eruption rate, in kg/s.

The best-fit exponent of 0.241 is similar to a theoretical prediction of 0.25 (Morton and others, 1956) and to previous empirical relations (Wilson and others, 1978, eq. 2; Sparks and others, 1997, eq. 5.1).

Table 5. Total grain-size distribution from the 1980 deposit (column 3) and used in this study (column 4).

[Mass fractions in column 3 are estimated by Durant and others (2009, supplementary file number 3 of their paper) by integrating the deposit to a distance of about 670 kilometers. Column 4 gives formulas used to calculate \( m_{p,i} \) if \( m_{fines} \) is known. Density values are calculated as described in the text. Size of particles (\( \phi \)) is \(-\log_2(d)\), where \( d \) is particle diameter in millimeters. Abbreviations: kg/m\(^3\), kilogram per cubic meter; mm millimeter; \( m_{p,i} \), mass fraction of non-aggregating particles of size class i]

| Size of particles, in \( \phi \) | Diameter, in mm | 1980 Mass Fractions | \( m_{fines} \) (this study) | Density of particles, in kg/m\(^3\) |
|---|---|---|---|---|
| \( \leq -4.0 \) | 16.0000 | | | 490 |
| -3.5 | 11.3137 | 0.0007 | | 490 |
| -3.0 | 8.0000 | 0.0019 | | 490 |
| -2.5 | 5.6569 | 0.0021 | | 490 |
| -2.0 | 4.0000 | 0.0047 | | 665 |
| -1.5 | 2.8284 | 0.0058 | | 1,292 |
| -1.0 | 2.0000 | 0.0056 | 0.0727(1-\(m_{fines}\)) | 2,003 |
| -0.5 | 1.4142 | 0.0084 | 0.0294(1-\(m_{fines}\)) | 2,350 |
| 0.0 | 1.0000 | 0.0141 | 0.0493(1-\(m_{fines}\)) | 2,005 |
| 0.5 | 0.7071 | 0.0214 | 0.0748(1-\(m_{fines}\)) | 2,248 |
| 1.0 | 0.5000 | 0.0459 | 0.1605(1-\(m_{fines}\)) | 2,624 |
| 1.5 | 0.3536 | 0.0723 | 0.2528(1-\(m_{fines}\)) | 2,644 |
| 2.0 | 0.2500 | 0.0532 | 0.1860(1-\(m_{fines}\)) | 2,639 |
| 2.5 | 0.1768 | 0.0292 | 0.0766(1-\(m_{fines}\)) | 2,706 |
Table 5. Total grain-size distribution from the 1980 deposit (column 3) and used in this study (column 4).—Continued

| Size of particles, in $\phi$ | Diameter, in mm | Mass Fractions | Density of particles, in kg/m$^3$ |
|-----------------------------|----------------|----------------|----------------------------------|
|                             |                | 1980 m$_{p,i}$ | $m_p (this\ study)$            |
| 3.0                         | 0.1250         | 0.0330         | 0.0577(1-m$_{fines}$)       | 2,691  |
| 3.5                         | 0.0884         | 0.0460         | 0.0402(1-m$_{fines}$)       | 2,730  |
| 4.0                         | 0.0625         | 0.0602         |                                | 2,698  |
| 4.5                         | 0.0442         | 0.0700         |                                | 2,640  |
| 5.0                         | 0.0313         | 0.0799         |                                | 2,581  |
| 5.5                         | 0.0221         | 0.0829         |                                | 2,570  |
| 6.0                         | 0.0156         | 0.0790         |                                | 2,670  |
| 6.5                         | 0.0110         | 0.07174        |                                | 2,670  |
| 7.0                         | 0.0078         | 0.0575         |                                | 2,670  |
| 7.5                         | 0.0055         | 0.0429         |                                | 2,670  |
| 8.0                         | 0.0039         | 0.0327         |                                | 2,670  |
| 8.5                         | 0.0028         | 0.0261         |                                | 2,670  |
| 9.0                         | 0.0020         | 0.0207         |                                | 2,670  |
| 9.5                         | 0.0014         | 0.0138         |                                | 2,670  |
| 10.0                        | 0.0010         | 0.0094         |                                | 2,670  |
| 10.5                        | 0.0007         | 0.0063         |                                | 2,670  |
| $\geq$11.0                 | 0.0005         | 0.0029         |                                | 2,670  |

EXPLANATION

Figure 6. Correlations between plume height and eruption rate or erupted volume. A, Plume height above the vent (kilometers) versus log of eruption rate (kilograms per second) using historical data tabulated in Mastin and others (2009) (blue diamonds). The red solid line is a best-fit curve through these data, and the dashed lines give the ±1σ standard error in prediction. B, Plume height above the vent versus total erupted volume (cubic kilometers [km$^3$] dense rock equivalent [DRE]) for the same historical eruptions.
Total erupted volume also correlates with plume height (Carey and Sigurdsson, 1989; Mastin and others, 2009, Table 1). A best-fit curve through historical data (fig. 6B) gives:

$$H_{\text{bestfit}} = 25.9 + 6.64 \cdot \log_{10}(V)$$

where

- $H_{\text{bestfit}}$ is plume height above the vent; and
- $V$ is erupted volume in km$^3$ DRE. The standard error in prediction ($1\sigma$) based on this correlation is about 5.8 km.

We assign plume height using relationship (3), but then add a random number using a Gaussian pdf with a mean of zero and standard deviation of 2.9 km—half the standard error in the regression. We arbitrarily reduced the standard deviation of the Gaussian adjustment from 5.8 to 2.9 km to avoid having negative plume heights near the low end, and unrealistically high plumes (higher than 45 km) at the high end.

### Grain-Size Distribution

The grain-size distribution (GSD) is challenging to parameterize because several processes can accelerate the fallout of fine ash; including particle aggregation, scavenging by rainfall, and bulk instabilities in the cloud (fig. 7). The Ash3d model does not explicitly account for these processes. Rather, we empirically adjust the input GSD, so fine ash is represented as aggregates of given size, shape, and density.

Our method to characterize distribution of both particles and aggregates in each simulation involves three groups of parameters: (1) one-dimensional arrays of the mass fractions ($\phi_{p,i}$) of particles too large to aggregate, along with their size ($\phi_{p,i}$) and density ($\rho_{p,i}$); and single parameters defining (2) the median aggregate diameter ($\mu_{\text{agg}}$), and (3) the mass fraction of fine, aggregating ash erupted ($m_{\text{fines}}$).

**Non-Aggregating Particles**

To assign $\phi_{p,i}$, we start with mass fractions of each size from the 1980 deposit (table 5, column 3). We assign densities ($\rho_{p,i}$) to each size fraction using measured proportions of mafic crystals, feldspar, lithics, pumice, and glass fragments (Carey and Sigurdsson, 1982), assuming a density of 3,200 kg/m$^3$ for mafic crystals, 2,600 kg/m$^3$ for feldspars, 2,900 kg/m$^3$ for lithics, 490 kg/m$^3$ for large pumice ($\phi \leq 1$) (Klug and Cashman, 1994), and 2,670 kg/m$^3$ for small glass fragments ($\phi \geq 4.5$). For intermediate-sized pumice or glass ($1 < \phi < 4.5$), the density was interpolated linearly between 490 and 2,670 kg/m$^3$.

Next, we consolidate all particles larger than 2 mm in diameter into a single 2 mm bin, dramatically speeding computation time. Particles larger than 2 mm diameter will almost certainly fall out upwind of Hanford. Under the wind and plume conditions of 1980, for example, nearly all particles larger than 0.25 mm diameter would have fallen out upwind (fig. 8A).

**Mean Aggregate Size ($\mu_{\text{agg}}$)**

Third, we divide $m_{\text{fines}}$ into five aggregate classes having a narrow Gaussian size distribution with a standard deviation $\sigma_{\text{agg}} = 0.1\phi$ (table 6). The narrow $\sigma_{\text{agg}}$ is justified by recent Ash3d modeling (Mastin and others, 2016) that optimally fits deposits of four well-documented eruptions with nearly the identical aggregate-size distributions (mean $\mu_{\text{agg}} = 2.4 \pm 0.1\phi$, standard deviation $\sigma_{\text{agg}} \leq 0.1\phi$). These eruptions—Mount St. Helens (May, 18, 1980); Crater Peak, Mt. Spurr, Alaska (September, 16–17, 1992); Ruapehu, New Zealand (June, 17, 1996); and Redoubt, Alaska (March, 23, 2009)—ranged widely in magma type, plume height, eruptive volume, mass fraction fine ash, and atmospheric temperature and water content, suggesting that these parameters are robust.

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**Figure 7.** Diagram showing processes that influence the distribution of fine, distal ash. These include development of gravitational instability and overturn within the downwind cloud (Carazzo and Jellinek, 2012), and the development of hydrometeors as descending ash approaches the freezing elevation (Durant and others, 2009).
Although $\mu_{agg}$ is tightly constrained, we vary it slightly between simulations by sampling from a pdf having a mean of 2.4$\phi$ and standard deviation of 0.1$\phi$.

**Mass Fraction Aggregating Ash**

The mass fraction of aggregating ash ($m_{agg}$) was very high in the 1980 deposit, altering the pattern of fallout and contributing to the secondary maximum in thickness near Ritzville (Carey and Sigurdsson, 1982). But $m_{agg}$ almost certainly will vary in future MSH eruptions. If we define $m_{fines}$ to contain all ash of $\phi \geq 4$ ($d \leq 0.063$ mm), and 75 percent, 50 percent, and 25 percent, respectively, of size bins $\phi = 3.5$, 3, and 2.5 (following Mastin and others (2016)), then $m_{fines}$ in the 1980 deposit is about 0.7 (table 5, column 3). The fraction smaller than 0.063 mm ($m_{fines}$) in the 1980 deposit is about 0.6.

Recent research suggests that $m_{agg}$ may increase in future events with eruption size, magma silica content, and the size and abundance of pyroclastic flows (Rose and Durant, 2009; Mastin and others, 2009). However, these relations are hard to document in historical events. Consider silica content for example. Rose and Durant (2009) found $m_{agg}$ (a proxy for $m_{fines}$) to be at least 0.3 in several silicic deposits, but $m_{agg}$ was only 0.08–0.12 in the silicic 2011 Cordon Caulle eruption (Bonadonna and others, 2015a). Another consideration is eruption size. Among the eruptions in table 7, $m_{agg}$ in the two largest ranges widely from 0.08–0.12 (Cordon Caulle) to 0.6 (MSH).

Entries in table 7 support the notion that pyroclastic flows (pf) generate fine ash, with $m_{agg} \geq 0.4$ among the three pf-producing eruptions at MSH and Spurr. Still, the small dataset prevents us from extracting robust relationships.

In the absence of better data, we still lean toward the notion that future MSH eruptions will produce substantial quantities of fine ash. MSH eruptions tend to be large, silicic, and in the past have involved much pyroclastic-flow activity. If $m_{agg}$ in 1980 was 0.7, we doubt it will be 0.1 in the next eruption. But the uncertainty is large, and the high $m_{agg}$ content in 1980 (relative to other eruptions) suggests $m_{agg}$ may be lower in the future. Thus, for model simulations, we assign $m_{agg}$ using a Gaussian pdf with a mean of 0.5 and a standard deviation of 0.15.

**Table 6.** Mass fraction of fine ash assigned to different size bins for aggregates.

[Abbreviations: $\mu_{agg}$ median aggregate size; $m_{fines}$ mass fraction of a deposit moved into the aggregate size classes]

| $\mu_{agg}$ | Fraction |
|-------------|----------|
| $0.2\phi$   | 0.06$m_{fines}$ |
| $0.1\phi$   | 0.24$m_{fines}$ |
| $0.4\phi$   | 0.40$m_{fines}$ |
| $0.1\phi$   | 0.24$m_{fines}$ |
| $0.2\phi$   | 0.06$m_{fines}$ |

**Table 7.** Mass fraction ($m_{agg}$) of fine (smaller than 0.063 mm) ash in selected recent eruption deposits.

[Entries are in order of decreasing erupted volume ($V$, in dense-rock equivalent). SiO$_2$ refers to the weight percent SiO$_2$ in the melt, a proxy for magma viscosity. “V” refers to the erupted volume, in cubic kilometers (km$^3$) dense-rock equivalent (DRE). Pf? indicates whether pyroclastic flows occurred during this eruption which could have milled fine ash. Max. dist. is maximum distance in kilometers (km) from the vent of the most distal sample used to calculate the total grain-size distribution]

| Deposit                  | SiO$_2$ wt% | V km$^3$ | Pf?     | $m_{agg}$ | Max. dist. km |
|--------------------------|-------------|----------|---------|-----------|--------------|
| Cordon Caulle, 2011      | 72          | 0.24     | x       | 0.08–0.12 | 100          |
| Mount St. Helens, 1980   | 70          | 0.2      | x       | 0.6       | 630          |
| Fuego, 1974              | 54          | 0.02     | x       | 0.03      | 150          |
| Spurr, August 18,1992    | 60–75       | 0.015    | x       | 0.4       | 370          |
| Spurr, September 17–18, 1992 | 60–75      | 0.015    | x       | 0.4       | 385          |
| Redoubt, March 23, 2009  | 68          | 0.0016   |         | 0.27      | 300          |
| Ruapehu, 1996           | 62–65       | 0.001    |         | 0.03      | 180          |

1Bonadonna and others (2015b)
2Castro and others (2013)
3supplemental file number 3 in Durant and others (2009)
4Rutherford and others (1985)
5Rose and others (2008)
6Ruggensack (2001)
7Durant and Rose (2009)
8Nye and others (1995)
9Mastin and others (2013)
10Coombs and others (2013)
11Bonadonna and Houghton (2005)
12Nakagawa and others (1999).
Secondary Physical Parameters

The following physical parameters are assigned non-changing values that have been found to optimally fit mapped deposits:

- **Suzuki constant** ($k$). This parameter, which is used in equation 1, controls the vertical distribution of mass in the source nodes (fig. 4B). Higher values of $k$ (for example $k \gtrsim 8$) concentrate most of the mass in the upper 20 percent or so of the column. A top-heavy column produces a prominent, realistic secondary thickening of the deposit but also produces an unrealistic decrease in the proximal deposit thickness (fig. 8 of Mastin and others [2016]). We chose a value of $k = 8$ to balance these two features.

- **Particle shape**. We use the drag coefficient formula of Wilson and Huang (1979) to calculate settling velocity, assuming particles settle at their terminal velocity. Wilson and Huang (1979) approximate particles as ellipsoids with a shape factor $F = (b + c) / 2a$, where $a$, $b$, and $c$ are the semi-major, intermediate, and semi-minor axes of the ellipsoids, respectively. Wilson and Huang (1979) measured these axes dimensions for a collection of volcanic ash particles. We use a shape factor of 0.44, which corresponds to the average of their measured values. We assume aggregates are round, consistent with previous work (Mastin and others, 2016). Aggregate shape strongly influences the depositional pattern, especially at distances of greater than 100 km (fig. 6 of Mastin and others [2016]).

![Figure 8](image_url)

**Figure 8.** Graphs showing settling velocity versus transport distance and diameter for particulate matter falling at Hanford, Washington. **A**, Transport distance versus average fall velocity, assuming a 15.1 meters per second (m/s) wind speed, equal to the average wind speed at Mount St. Helens between 0 and 15 kilometer (km) elevation on May 18, 1980, and a fall distance of 15 km. The vertical shaded bar represents the distance of the Hanford site. Horizontal shaded bar is the fall velocity at which objects falling from 15 km elevation would land at Hanford. Labels on dots give the average diameter (millimeters [mm]) of a round aggregate having a density of 600 kilograms per cubic meter (kg/m$^3$) and the given fall velocity, as calculated by Wilson and Huang (1979). **B**, Fall velocity at pressure=1 atmosphere (atm), Temperature=298.15 Kelvin (K), versus diameter, for round falling objects. Red lines represent aggregates (densities less than or equal to 800 kg/m$^3$). Black lines represent particles (densities greater than or equal to 1,000 kg/m$^3$). Objects falling at faster than about 1.2 m/s from 15 km under these wind conditions would land upwind from Hanford. All particles having densities greater than or equal to 1,000 kg/m$^3$ and diameters greater than 0.25 mm would fall faster than about 1.2 m/s and would therefore land upwind of Hanford.
• Density of individual particles ($\rho_{p,i}$). The density of individual particle classes (table 5) is calculated according to its componentry as explained in the mean aggregate size section of this report.

• Deposit density ($\rho_d$). Ash3d calculates mass per unit area ($M$) and converts ($M$) to deposit thickness ($T$) assuming a density ($\rho_d$) of 1,000 kg/m$^3$. This value of ($\rho_d$) is intermediate between new-fallen densities, which ranged from less than 100 to more than 1,000 kg/m$^3$ at Mount St. Helens in 1980 (Sarna-Wojcicki and others, 1981), and higher densities that follow rain or compaction. Densities of 400–2,000; 1,150–1,350; 200–800; and 1,200–1,300 kg/m$^3$ have been measured at Pinatubo (Paladio-Melosantos and others, 1996); Eyjafljallajökull (Bonadonna and others, 2011); Redoubt Volcano (Scott and McGregor, 1996); and Chaitén (Alfano and others, 2011) respectively.

Using a value of $\rho_d = 1,000$ kg/m$^3$ also conveniently implies that $T = 1$ mm when $M = 1$ kg/m$^2$. Changing the deposit density from 1,000 kg/m$^2$ would change $T$, but not $M$. The relationship is linear; in other words, using a value of 500 kg/m$^2$ would double the value of $T$; using 2,000 kg/m$^2$ would reduce $T$ by half.

• Magma density ($\rho_m$). Ash3d converts the input value of erupted volume, km$^3$ DRE, into mass, in kg, assuming a magma density of 2,500 kg/m$^3$. Like deposit density, the magma density is hard-coded into Ash3d and is a round number that lies within the range of observed densities. Magma contains melt, whose density ranges from about 2,200 to 2,600 kg/m$^3$ depending on composition, temperature and dissolved volatile content (Lange, 1994; Ghiorsso and Sack, 1995). It also contains crystals whose densities range from about 2,500 to 3,200 kg/m$^3$ depending on crystal type, composition, and temperature (Berman, 1988). The percentage of crystals in magma ranges from 0 percent to greater than 60 percent, and in MSH magmas from above 30 to 50 percent by volume (Gardner and others, 1995). Erupted masses calculated using our assumed magma density of 2,500 kg/m$^3$ are about 8 percent greater than those using 2,300 kg/m$^3$ as reported by Carey and others (1995) for MSH magmas, but this difference is well within the uncertainty in deposit volumes.

• Diffusion Coefficient ($K$). Mastin and others (2016) systematically varied $K$ from 0 to 3,000 square meters per second (m$^2$/s) in MSH test simulations and found that non-zero values of $K$ did not measurably improve the agreement compared to $K = 0$. However, setting $K > 0$ increased runtime by a factor of three. Thus, we set $K = 0$ for these simulations.

• Aggregate size bins. We use five aggregate size bins with the mass fractions of each bin assigned as shown in table 6 and as described in the mean aggregate size section of this report.

Meteorological Inputs

The wind and other meteorological conditions are varied in each simulation by randomly picking a start time between January 1, 1980, and January 1, 2010. For meteorology we use data from the ERA Interim model (Dee and others, 2011), published by the ECMWF. It has a roughly 79 km horizontal spacing between model nodes, 3-hour time intervals, and 60 pressure levels in the atmosphere extending to 0.1 hectopascal (greater than about 60 km). The data extend back to January 1, 1979.

The Interim-ERA data had to be reformatted to be read by Ash3d, which took about a month of processing time. A small percentage of the 65,700 files did not reformat successfully, resulting in failure of 2.1 percent of the simulations.

Model settings

We chose a horizontal nodal spacing of 0.1 degree (table 4), 8 x 11 km at this latitude, which tested well in earlier work (Mastin and others, 2016). Meteorological features smaller than a few times the 79 km nodal spacing of the ERA Interim model were not captured.

We chose a small model domain to maximize efficiency of calculations under the assumption that ash would be transported primarily to the east, toward Hanford from Mount St. Helens. The small domain may miss instances, however, in which ash takes a roundabout route outside the domain before arriving at Hanford. To evaluate this effect, we also ran 1,000 simulations using a larger model domain (125–111°W, 43–51°N). A small number of runs produced slightly higher values of $T$ or airborne ash concentration ($C$), increasing $T_{10k}$ by 6 percent and $C_{max,10k}$ by 3.5 percent. This inaccuracy is small relative to other uncertainties.

During test runs we found a surprising relation between model resolution and $T$ or $C$. For a thousand test runs, increasing horizontal resolution from 0.2 to 0.1 to 0.05 degrees, increases $T$ on average by about 10–20 percent and $C$ by about 20–40 percent, although results differ widely from run to run. With increasing resolution, the solution does not converge on a single, more accurate result as Eulerian model tests normally predict (LeVeque, 2002; Schwaiger and others, 2012). We think this relation results from the fact that ash is released in a single column of source nodes (fig. 4B) having a footprint (nodal area on the ground surface) determined by the nodal spacing. In higher-resolution runs, the same mass of ash occupies a smaller footprint, hence its airborne concentration is greater and, as it falls out, the deposit is thicker. This greater concentration is advected downwind. At nodal spacings smaller than the source region, model accuracy does not improve because the model is unable to capture the physics of the rising and spreading ash column. An optimal spacing would be roughly equal to the horizontal dimension of the volcanic plume at the neutral buoyancy elevation. This dimension increases with eruption size, from tens to hundreds of kilometers, for the range of eruption sizes considered here. We conclude that choosing a constant nodal spacing may introduce an uncertainty of tens of percent in the result.
Model testing found that varying vertical cell spacing \((dz)\) between 0.5 and 2 km has less than 10 percent effect on deposit thickness but as much as 30 percent on airborne concentration. The insensitivity in \(T\) seems to imply that most tephra is falling vertically. Halving vertical spacing quadruples run time; hence we chose \(dz = 2\) km for speed. Ash3d interpolates linearly between the nearest nodes in the ERA Interim model (in which spacing is tens of meters at ground level) to obtain pressure, temperature, and wind vectors at each height.

Ash3d does not calculate wet deposition, which would require difficult assumptions of the size and density of falling ashy raindrops. Ash3d can incorporate topography, but the implementation uses a crude cut-cell method, which creates a brickwork pattern of topography, sometimes creating deposit artifacts on the upwind sides of mountain ranges. Topography around Hanford is fairly subdued, and test runs with and without topography produced nearly identical values of \(T\) and \(C\). Thus, we did not include topography.

**Modeling Methodology**

We attempted a total of 10,000 simulations using these inputs. Table S1 of the accompanying Data Release (Mastin and others, 2020) lists the inputs for each run. Histograms (fig. 9) illustrate that the input distributions resemble the pdfs specified.
Two hundred fifteen simulations (2.1 percent) failed because of corrupt wind files, but the remaining runs are enough for the analysis. Table S2 (Mastin and others, 2020) gives tephra thickness, arrival time, fall duration, and grain-size distribution at the Hanford site (46.5507° N., 119.489° W.) for each run.

In each simulation, the total $C$ in the ground-level node at Hanford was recorded at each time step (roughly every minute or so) as long as ash was in the air. The maximum value of $C$ in each simulation was taken as $C_{\text{max}}$. The dosage (product of concentration times time) was calculated as $d_i = \sum C_i \Delta t_i$, where $C_i$ is the airborne concentration at each time step and $\Delta t_i$ is time-step duration. This dosage was divided by the time over which ash was falling ($D_i$) to obtain an average concentration $C_{\text{avg},i}$. For both the maximum and average airborne concentrations, about 56 percent of simulations gave less than 1 mg/m$^2$, and 60 percent gave less than 2 mg/m$^2$. Dosage is used to define aircraft engine tolerance (Clarkson and others, 2016), and may be relevant when considering the amount of ash required to clog air filters.

For each run, documented in Mastin and others (2020), we tabulated inputs (table S1 of Mastin and others (2020)), thickness and fall duration (table S2), maximum airborne concentration, and dosage (table S3). Thickness was ranked in decreasing order (table S4) and each thickness value was assigned a probability $P_3|1$ equal to its rank divided by (n+1), where n is the number of successful runs. In the notation of Hoblitt and Scott (2011) $P_{3|1}=P_{3|2}=P_{3|10}$, tables S5 and S6 are analogous to table S4, but they list maximum and average airborne ash concentration respectively rather than thickness. Plots of $P_{3|1}$ versus thickness and concentration are given in figure 10. About 60 percent of the simulations deposited no tephra at Hanford. Sixty-one percent deposited less than 0.1 mm, 88 percent less than 3.5 mm, and 94 percent 15 mm or less.

**Results**

Following the methodology above, the ranked values of thickness and concentration were interpolated to give $T$, $C_{\text{max}}$, and $C_{\text{avg}}$ at specified exceedance probabilities (table 8 and fig. 10). For the 10,000-year recurrence interval, $T_{10k}=51.1$, $C_{\text{max},10k}=3,819$ and $C_{\text{avg},10k}=1,513$ mg/m$^3$.

The values of $T_{10k}$ and $C_{\text{max},10k}$ were also calculated as a function of the number of runs completed ($n$; fig. 11). Changes in $T_{10k}$ or $C_{\text{max},10k}$ with $n$ result from changes to the statistical distribution as $n$ changes. Ideally, $T_{10k}$ and $C_{\text{max},10k}$ should converge on a stable value with increasing $n$. After about 5,000 runs, $T_{10k}$ is within about 5 percent of its final value, whereas more than 6,000 are required to bring $C_{\text{max},10k}$ within 5 percent of its final value.
Table 8. Threshold values of tephra-fall thickness in millimeters (which is equal to mass load in kilograms per square meter) and airborne concentration at different exceedance probabilities ($P_{st}$).

[Abbreviations: $C_{\text{max}}$, maximum airborne concentration during the period of tephra fall; $C_{\text{ave}}$, average airborne concentration during the period of tephra fall; mg/m$^3$, milligram per cubic meter; mm, millimeter; $T$, tephra-fall thickness]

| Probability $P_{st}$ | Recurrence years | $T$, in mm | $C_{\text{max}}$, in mg/m$^3$ | $C_{\text{ave}}$, in mg/m$^3$ |
|----------------------|------------------|------------|-----------------------------|-----------------------------|
| 0.0125               | 10,000           | 51.1       | 3819                        | 1513                        |
| 0.050                | 2,500            | 16.3       | 1350                        | 574                         |
| 0.0625               | 2,000            | 12.2       | 1090                        | 457                         |
| 0.125                | 1,000            | 2.9        | 372                         | 164                         |

Figure 11. Calculated values of tephra-fall thickness in a “1-in-10,000-year event” ($T_{10k}$; A) and maximum airborne ash concentration ($C_{\text{max,10k}}$; B) as a function of the number of runs. Horizontal dashed lines give the final value; dotted lines give the final value plus or minus 5%. kg/m$^2$, kilogram per square meter; $M$, mass load of tephra deposit; mm, millimeter; mg/m$^3$, milligram per cubic meter; $P_{3\text{r}}$, probability of exceedance of a given tephra thickness or ash concentration given that an eruption has occurred; %, percent.

Deposit Thickness and Mass Load

Among four simulated deposits where $T \geq T_{10k}$ (fig. 12), deposition patterns range widely, but in each case the dominant wind was blowing toward Hanford. Among ten runs with $T \geq T_{10k}$ (table 9), Erupted volumes are in the upper half of the input range (0.62–2.01 km$^3$). Average accumulation rates ($T/D_d$) ranged widely, from 3.6 to 23.2 millimeters per hour (mm/hr; 1 to 6 grams per square meter per second [g/m$^2$/s]).

Previous estimates of airborne concentration have assumed that $D_d$ are comparable to $D_e$, but a plot of these two parameters for all runs (fig. 13) shows surprisingly little correlation. When $D_d > D_e$, about two thirds (66 percent) of the time, with a difference ($D_d - D_e$) of about 2.6±2.5 hours (mean ± standard deviation). Greater fall duration may result when slower, low-elevation winds cause ashfall to linger. Shorter fall duration may result when Hanford lies near the edge of a deposit and catches a brief, passing cloud.
Figure 12. Maps of tephra deposition for four runs whose deposit thickness at Hanford is closest to $T_{10k}$ ASL, above sea level; cm, centimeter; DRE, dense-rock equivalent; ECMWF Interim ERA, European Centre for Medium-Range Weather Forecasts Interim Reanalysis; km, kilometer; km$^3$, cubic kilometer; mm, millimeter; UTC, coordinated universal time.

Table 9. Table of runs yielding deposit thicknesses close to $T_{10k}$

| Rank | $P_{is}$ | Run number | $T_i$ in mm | $t_d$ in hrs | $D_d$ in hrs | $V_i$ in km$^3$ DRE | $H_i$ in km asl | $D_e$ in hrs | $m_{max}$ |
|------|---------|------------|-------------|--------------|--------------|-------------------|---------------|--------------|----------|
| 118  | 0.0121  | 2305       | 51.85       | 2.8          | 15.5         | 0.98              | 30.8          | 4.28         | 0.41     |
| 119  | 0.0122  | 5896       | 51.7        | 3.3          | 10.5         | 0.38              | 28.9          | 2.23         | 0.55     |
| 120  | 0.0123  | 4473       | 51.38       | 3.5          | 13.3         | 2.02              | 31.1          | 8.36         | 0.48     |
| 121  | 0.0124  | 1453       | 51.26       | 2.5          | 7.2          | 2.01              | 31.4          | 7.99         | 0.61     |
| 122  | 0.0125  | 4788       | 51.2        | 5.4          | 16.4         | 1.42              | 28.9          | 8.09         | 0.71     |
| 123  | 0.0126  | 446        | 50.97       | 2.2          | 9.3          | 2.05              | 27.8          | 14.14        | 0.56     |
| 124  | 0.0127  | 695        | 50.79       | 1.4          | 6.4          | 0.62              | 28.5          | 3.84         | 0.55     |
| 125  | 0.0128  | 743        | 50.71       | 2.6          | 5.8          | 1.82              | 34.8          | 4.59         | 0.51     |
| 126  | 0.0129  | 6274       | 50.62       | 2.1          | 14.3         | 1.88              | 28            | 12.51        | 0.70     |
| 127  | 0.013   | 6124       | 50.62       | 8.8          | 12.1         | 0.99              | 29.8          | 4.93         | 0.53     |
Airborne Concentration

For runs where \( C_{\text{max}} \approx C_{\text{max,10k}} \), key inputs are summarized in table 10; similar lists for \( C_{\text{max}} \approx C_{\text{max,2k}} \), \( C_{\text{max}} \approx C_{\text{max,1k}} \) and \( C_{\text{avg}} \approx C_{\text{max,10k}} \) are given in tables 11–13. When \( C_{\text{max}} \approx C_{\text{max,10k}} \), erupted volumes for runs in table 10 are 0.4–1.8 km\(^2\) DRE. For the same runs, tephra starts falling at Hanford 2.2–14.7 hours after the eruption starts and falls for 4.5–18.4 hours. Deposits are 9–96 mm thick, and average accumulation rates are 2.3–19.1 mm/hr. Concentration versus time (fig. 14A) is mostly Gaussian in shape with peak values that last only a few hours before dropping to less than 80 percent of the peak value. Dosages (fig. 14D, table 10) range from 3.5\times10^7 to 6.1\times10^7 milligram-seconds per cubic meter (mg-s/m\(^3\)), reflecting the range of time over which these concentrations persisted.

Grain-Size Distribution

Tephra fall deposits at Hanford have coarser grain-size distributions in simulations where \( T \approx T_{10k} \) (table 14, fig. 15A)
Table 11. Table of runs producing ash concentrations close to $C_{max,h}$.  

[Abbreviations: asl, above sea level; DRE, dense-rock equivalent; hr, hour; km, kilometer; km$^3$, cubic kilometer; mg/m$^3$, milligram per cubic meter; mg-s/m$^3$, milligram-seconds per cubic meter; mm, millimeter]

| Rank | $P_{qq}$ | Run Number | $C_{max}$ in mg/m$^3$ | $t_p$ in hrs | $D_p$ in hrs | Dosage, in mg-s/m$^3$ | $T$ in mm | $V_i$ in km$^3$ DRE | $H_i$ in km asl | $D_p$ in hrs |
|------|---------|------------|-----------------------|--------------|--------------|----------------------|----------|------------------|----------------|------------|
| 607  | 0.062  | 6,851      | 1,100                 | 7.7          | 7            | 1.10E+07            | 6.8      | 0.4              | 23.6           | 6.14       |
| 608  | 0.0621 | 5,580      | 1,100                 | 5.1          | 4.9          | 8.11E+06            | 7.1      | 0.2              | 27.3           | 1.83       |
| 609  | 0.0622 | 3,228      | 1,100                 | 3.1          | 4.7          | 1.28E+07            | 13.9     | 0.3              | 23.5           | 4.28       |
| 610  | 0.0623 | 7,841      | 1,090                 | 8.7          | 5.3          | 8.78E+06            | 5.7      | 0.1              | 22.3           | 1.79       |
| 611  | 0.0624 | 7,368      | 1,090                 | 1.9          | 12.2         | 3.41E+07            | 73.4     | 2.3              | 29.6           | 11.62      |
| 612  | 0.0625 | 5,594      | 1,090                 | 5.4          | 10.4         | 2.02E+07            | 11.5     | 0.3              | 26.4           | 2.86       |
| 613  | 0.0626 | 5,453      | 1,090                 | 3.6          | 7            | 5.64E+06            | 3.7      | 0.7              | 27.8           | 4.53       |
| 614  | 0.0627 | 1,670      | 1,090                 | 1.7          | 3.7          | 8.16E+06            | 15.2     | 0.2              | 22.6           | 2.92       |
| 615  | 0.0629 | 534        | 1,090                 | 1.9          | 6.4          | 1.73E+07            | 34.5     | 0.6              | 25.5           | 5.9        |
| 616  | 0.0630 | 8,916      | 1,080                 | 5.3          | 19.8         | 3.42E+07            | 23.1     | 1.2              | 26.8           | 9.62       |

Table 12. Table of runs producing ash concentrations close to $C_{max,h}$.  

[Abbreviations: asl, above sea level; DRE, dense-rock equivalent; hr, hour; km, kilometer; km$^3$, cubic kilometer; mg/m$^3$, milligram per cubic meter; mg-s/m$^3$, milligram-seconds per cubic meter; mm, millimeter]

| Rank | $P_{qq}$ | Run Number | $C_{max}$ in mg/m$^3$ | $t_p$ in hrs | $D_p$ in hrs | Dosage, in mg-s/m$^3$ | $T$ in mm | $V_i$ in km$^3$ DRE | $H_i$ in km asl | $D_p$ in hrs |
|------|---------|------------|-----------------------|--------------|--------------|----------------------|----------|------------------|----------------|------------|
| 1219 | 0.1246 | 9,484      | 374                   | 13.5         | 6.5          | 1.99E+06            | 3.7      | 1.27             | 24.6           | 14.99      |
| 1220 | 0.1247 | 8,694      | 374                   | 3.9          | 3.2          | 2.70E+06            | 1.5      | 0.02             | 15.2           | 2.1        |
| 1221 | 0.1248 | 73         | 374                   | 7.4          | 9.8          | 4.48E+06            | 8.0      | 1.26             | 27.1           | 9.69       |
| 1222 | 0.1249 | 8,777      | 373                   | 2.4          | 10.2         | 5.43E+06            | 7.3      | 0.33             | 20.8           | 8.38       |
| 1223 | 0.125  | 7,033      | 373                   | 3.0          | 6.6          | 4.76E+06            | 4.4      | 0.22             | 21.8           | 4.46       |
| 1224 | 0.1251 | 5,875      | 372                   | 4.0          | 4.1          | 2.74E+06            | 1.5      | 0.02             | 14.3           | 2.45       |
| 1225 | 0.1252 | 5,098      | 372                   | 4.1          | 4.3          | 2.58E+06            | 1.8      | 0.04             | 16.2           | 3.25       |
| 1226 | 0.1253 | 4,692      | 372                   | 8.2          | 15.2         | 8.07E+06            | 4.5      | 0.56             | 24.2           | 7.14       |
| 1227 | 0.1254 | 2,510      | 372                   | 4.3          | 4.2          | 2.74E+06            | 1.7      | 0.02             | 14.9           | 2.66       |
| 1228 | 0.1255 | 1,149      | 372                   | 4.9          | 8.2          | 4.60E+06            | 2.6      | 0.04             | 15.0           | 4.6        |

Table 13. Run numbers producing ash concentrations at Hanford, Washington, close to $C_{avg,100}$.  

[Abbreviations: asl, above sea level; DRE, dense-rock equivalent; hr, hour; km, kilometer; km$^3$, cubic kilometer; mg/m$^3$, milligram per cubic meter; mg-s/m$^3$, milligram-seconds per cubic meter; mm, millimeter]

| Rank | $P_{qq}$ | Run Number | $C_{max}$ in mg/m$^3$ | $t_p$ in hrs | $D_p$ in hrs | Dosage, in mg-s/m$^3$ | $T$ in mm | $V_i$ in km$^3$ DRE | $H_i$ in km asl | $D_p$ in hrs |
|------|---------|------------|-----------------------|--------------|--------------|----------------------|----------|------------------|----------------|------------|
| 118  | 0.01206 | 5,175      | 1,555                 | 2.2          | 11           | 6.14E+07            | 96.6     | 1.5              | 32.8           | 5.08       |
| 119  | 0.01216 | 8,332      | 1,554                 | 4.5          | 19.9         | 1.12E+07            | 66       | 1.7              | 28.9           | 9.58       |
| 120  | 0.01226 | 9,899      | 1,546                 | 5.1          | 5.9          | 3.27E+07            | 23.1     | 1.2              | 28.7           | 7.12       |
| 121  | 0.01237 | 5,945      | 1,542                 | 5.1          | 11.4         | 6.35E+07            | 43.2     | 1.1              | 25.7           | 10.67      |
| 122  | 0.01247 | 1,320      | 1,515                 | 10           | 8.8          | 4.77E+07            | 30.9     | 1.6              | 28.3           | 9.85       |
| 123  | 0.01257 | 2,129      | 1,510                 | 5.2          | 9.1          | 4.95E+07            | 38.2     | 1.1              | 28.9           | 6.57       |
Table 13. Run numbers producing ash concentrations at Hanford, Washington, close to $C_{avg,10K}$—Continued

| Rank | $P_{str}$ | Run Number | $C_{avg}$ in mg/m$^3$ | $t_e$ in hrs | $D_e$ in hrs | Dosage, in mg-s/m$^3$ | $T_e$ in mm | $V_e$ in km$^3$ DRE | $H_e$ in km asl | $D_e$ in hrs |
|-------|-----------|-------------|----------------------|--------------|--------------|-----------------------|-------------|-------------------|----------------|-------------|
| 124   | 0.01267   | 167         | 1,506                | 4.6          | 6.3          | 3.42E+07              | 23.2        | 0.2               | 20.7           | 4.84        |
| 125   | 0.01277   | 9,642       | 1,497                | 1.8          | 8.6          | 4.66E+07              | 94.2        | 1.1               | 28.7           | 6.65        |
| 126   | 0.01288   | 8,701       | 1,494                | 4.7          | 9.8          | 5.28E+07              | 32.1        | 0.5               | 22.8           | 8.57        |
| 127   | 0.01298   | 530         | 1,490                | 9.7          | 8.7          | 4.64E+07              | 22.2        | 1                 | 24.1           | 12.41       |

Figure 14. Graphs showing airborne ash concentration versus time for eruption simulations shown in tables 10 (A), 11 (B), and 12 (C). Airborne ash dosage versus time (D) is also shown for eruptions listed in table 10. Numbers in the legends refer to the run numbers. mg/m$^3$, milligrams per cubic meter; mg−s/m$^3$, milligram-seconds per cubic meter.
than those where $C_{\text{max}} \cong C_{\text{max},10k}$ (table 15) or $C_{\text{avg}} \cong C_{\text{avg},10k}$ (table 16), as observed in the $m_{63}$ column of these tables. The $m_{63}$ for the $T \cong T_{10k}$ runs correlates poorly with $m_{\text{fines}}$ in the input (table 9), and plume heights for runs with a coarse grain-size are also not especially high, suggesting that wind speed plays a strong role in determining grain-size distribution.

Table 14. Grain-size distribution at Hanford, Washington for runs where $T \cong T_{10k}$.

| Run Number | Aggregate diameter, in mm |
|------------|---------------------------|
|            | 1.000 | 0.707 | 0.500 | 0.354 | 0.250 | 0.177 | 0.125 | 0.088 | ≤0.063 |
| 6,775      | 0.0000 | 0.0000 | 0.0000 | 0.0001 | 0.0435 | 0.1749 | 0.0318 | 0.0001 | 0.7497 |
| 7,132      | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0076 | 0.1147 | 0.0036 | 0.0000 | 0.8742 |
| 7,943      | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.2648 | 0.7061 | 0.0010 | 0.0006 | 0.0274 |
| 5,355      | 0.0000 | 0.0000 | 0.0043 | 0.5912 | 0.3632 | 0.0064 | 0.0014 | 0.0004 | 0.0331 |
| 3,330      | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0001 | 0.0443 | 0.0206 | 0.0016 | 0.9334 |
| 5,551      | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0428 | 0.8582 | 0.0662 | 0.0017 | 0.0308 |
| 3,046      | 0.0003 | 0.0162 | 0.2174 | 0.7216 | 0.0415 | 0.0001 | 0.0001 | 0.0001 | 0.0328 |
| 8,227      | 0.0000 | 0.0000 | 0.0000 | 0.0338 | 0.8840 | 0.0712 | 0.0004 | 0.0000 | 0.1004 |
| 7,921      | 0.0001 | 0.0036 | 0.0651 | 0.5708 | 0.3468 | 0.0028 | 0.0002 | 0.0001 | 0.0105 |
| 5,175      | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0515 | 0.0138 | 0.0026 |

Figure 15 (pages 25–26). Graphs showing grain-size distributions at Hanford, Washington, for several model runs at varying conditions. A. Grain-size distributions at Hanford for model runs in table 9, where tephra fall thickness ($T$) is close to the 1-in-10,000-year event thickness ($T_{10k}$). B. Grain-size distributions for model run numbers in table 10, where the maximum airborne concentration during the period of tephra fall ($C_{\text{max}}$) is close to the value of the maximum airborne ash concentration at Hanford having a recurrence interval of 10,000 yrs ($C_{\text{max},10k}$). C. Grain-size distributions at Hanford for model runs in table 13, where the average airborne concentration during the period of tephra fall ($C_{\text{avg}}$) is close to $C_{\text{avg},10k}$. Numbers in the explanation refer to the run numbers. $p$, particle diameter in millimeters (mm).
Table 15. Grain-size distribution at Hanford for runs producing ash concentrations close to $C_{\text{max,10k}}$.

[Rows 3–12, columns 2–10, give the mass fractions of the particle size indicated in row 2. Falling aggregates are included in the ≤ 0.063 millimeter (mm) size class. No size classes larger than 1 mm were present in these results]
Table 16. Grain-size distribution at Hanford for runs producing ash concentrations close to $C_{\text{avg,10k}}$.

[Rows 3–12, columns 2–10, give the mass fractions of the particle size indicated in row 2. Falling aggregates are included in the ≤ 0.063 millimeter (mm) size class. No size classes larger than 1 mm were present in these results]

| Run Number | 1.000 | 0.707 | 0.500 | 0.354 | 0.250 | 0.177 | 0.125 | 0.088 | ≤0.063 |
|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 5,175      | 0.0000| 0.0000| 0.0000| 0.1277| 0.8491| 0.0185| 0.0005| 0.0002| 0.0040 |
| 8,332      | 0.0000| 0.0000| 0.0000| 0.0000| 0.0246| 0.0218| 0.0007| 0.9529|        |
| 9,899      | 0.0000| 0.0000| 0.0000| 0.0000| 0.0217| 0.3946| 0.0523| 0.0014| 0.5300 |
| 5,945      | 0.0000| 0.0000| 0.0000| 0.0000| 0.0016| 0.1338| 0.0438| 0.0014| 0.8194 |
| 1,320      | 0.0000| 0.0000| 0.0000| 0.0000| 0.0000| 0.0017| 0.0508| 0.0031| 0.9444 |
| 2,129      | 0.0000| 0.0000| 0.0000| 0.0000| 0.0001| 0.0597| 0.0504| 0.0032| 0.8867 |
| 167        | 0.0000| 0.0000| 0.0000| 0.0000| 0.0222| 0.2246| 0.0001| 0.9531|        |
| 9,642      | 0.0000| 0.0000| 0.0022| 0.6295| 0.3366| 0.0046| 0.0013| 0.0002| 0.0256 |
| 8,701      | 0.0000| 0.0000| 0.0000| 0.0000| 0.0001| 0.0184| 0.0293| 0.0008| 0.9515 |
| 530        | 0.0000| 0.0000| 0.0000| 0.0000| 0.0001| 0.0761| 0.0552| 0.0015| 0.8671 |

Discussion

In this section we consider these results in the context of their inputs, and the implications of the results for hazards at Hanford.

Results in the Context of Inputs

Our $T_{10k}$ value of 51 mm is about half the 10 cm estimated by Hoblitt and Scott (2011); but our estimate of $C_{\text{avg,10k}}$ (1,513 mg/m$^2$) is nearly identical to the estimate of Snow and Nelson (2012) (1,500 mg/m$^2$). These results bear some scrutiny in the context of our inputs.

In choosing inputs, we used best estimates with no intent to add conservatism. Minimum and maximum erupted volumes ($V_{\text{min}}$ and $V_{\text{max}}$, respectively) for example, were chosen on the basis of Nathenson’s (2017) estimated range for Holocene MSH eruptions rather than those of Carey and others (1995), because the former are better documented and reproducible. However, Nathenson’s volume estimates are lower by at least a factor of two than those of Carey and others (1995). Our estimate of $T_{10k}$, half of Hoblitt and Scott (2011), is consistent with this. Our choice of a logarithmic probability distribution for $V$ was based on the abundance of small eruptions rather than large ones in the geologic record. The paucity of observations precludes a more specific size-frequency relationship, but a different one could alter the frequency of the largest eruptions, which strongly control $T_{10k}$ and $C_{10k}$.

Our choices of plume height and duration are also important. $H$ and $D$ are derived by correlation from $V$, with uncertainties indicated by the scatter of data in figure 6. Eruption rate is proportional to roughly the fourth power of plume height in kilometers above the vent (equation 2); thus, overestimating plume height by 20 percent would double the eruption rate and reduce eruption duration by half, essentially doubling the average airborne concentrations during the fall period. We consider it unlikely however that durations were systematically over- or underestimated by a factor of two; eruption durations in table 9, for example (2–14 hrs for volumes of 0.6–2.0 km$^3$), do not appear out of line with observed durations for similar-sized eruptions (see table 1, Mastin and others (2009)).

Other parameters such as $k$, $F$, and $\rho$, have uncertainties whose possible effects are listed in table 17. Most of these effects have never been explored.

Our results may be conservative in one respect. Eruptions larger than about 1 km$^3$ DRE produce umbrella clouds that drive ash radially outward, a process not included in this version of Ash3d. Umbrella spreading produces clouds that are circular (fig. 16B) in contrast to the fan shape of clouds of smaller eruptions (fig. 16A). Umbrella clouds spread ash over a wider area, reducing the maximum deposit thickness immediately downwind (Mastin and others, 2014), and making the statistical worst-case (thickest) scenario not so bad. In 1991, Pinatubo produced the biggest umbrella cloud in recent decades (fig. 16B), and erupted about three times more magma (6–10 km$^3$ DRE (Koyaguchi, 1996)) than the largest of our simulations (2.3 km$^3$ DRE).

The dispersal of ash can be quantified by contouring the thickness distribution of an ash deposit as shown in figure 1G for the 1980 deposit, and then constructing plots of log thickness versus sqrt(A) as in figure 3B. Data can be fit with a best-fit line of slope $k_0$ (fig. 3B), although well-mapped deposits like MSH 1980 are better fit with two lines, of slopes $k_1$ and $k_2$ (fig. 3B). Lower absolute slope values reflect broader dispersal. Fierstein and Nathenson (1992) compiled slopes for 27 published deposits. Plotted as a function of the bulk deposit
Table 17. Estimated range of uncertainty in secondary physical parameters and their possible effects on results.

[The range of uncertainty in these parameters are estimates. Abbreviations: cm, centimeter; DRE, dense-rock equivalent; m²/s, square meter per second; kg/m³, kilogram per cubic meter]

| Parameter(s)                           | Value used                  | Uncertainty       | Estimated effect                                                                 |
|----------------------------------------|-----------------------------|-------------------|----------------------------------------------------------------------------------|
| Diffusion coefficient $K_x$            | 0 m²/s or 1,000 m²/s?      |                   | Increasing $K_x$ could decrease max. thickness values in the deposit, and increase the deposit footprint area, by tens of percent. It would likely decrease $T_{10k}$ by a small fraction, though this is unverified. Effect on airborne concentration is unknown. |
| Suzuki constant $k$                    | 8                           | about 4–12        | In a given simulation, changing $k$ could increase or decrease thickness values at Hanford by tens of percent depending on winds and plume height. Effect on $T_{10k}$ or $C_{10k}$ is not known. |
| Particle shape factor $F$              | 0.44                        | about 0.3–1       | This parameter affects the settling velocity of larger particles that do not aggregate. The effect would vary from one simulation to another. How much it would affect $T_{10k}$ or other key outputs is not clear. |
| Deposit density $\rho_d$               | 1,000 kg/m³                 | about 500–1,400 kg/m³ | Varying $\rho_d$ would have no effect on mass load at Hanford (M). But because $T=M/\rho_d$, it would directly affect $T_{10k}$. Changing $\rho_d$ to 1,125 kg/m³ from 1,000 for example would change the value of $T_{10k}$ from 5.11 to 4.54 cm. |
| Magma density $\rho_m$                | 2,500 kg/m³                 | about 2,200–2,800 kg/m³ | Erupted volumes (DRE) are converted to erupted mass by multiplying by magma density. Increasing or decreasing $\rho_m$ by 10–20 percent would increase or decrease erupted mass, deposit mass load at Hanford, and $T_{10k}$ and $C_{10k}$ by the same amount. |

Figure 16. Contrasting ash-cloud shapes from small and large eruptions. A. The National Aeronautics and Space Administration Earth Observatory image of the shape of the cloud from the eruption of Eyjafjallajökull (Eyja), Iceland, on May 7, 2010. Under a modest mass eruption rate of 5–10 x 10⁶ kilograms per second (kg/s), the cloud emanates from a point source, advects downwind in the ambient wind field, and widens into a fan-like shape because of turbulent diffusion. B. Japanese geostationary meteorological satellite (GMS) visible image of the shape of cloud from the 1991 Pinatubo eruption, which produced one of the highest mass eruption rates in the past century, 4–20 x 10⁶ kg/s (Koyaguchi, 1996). The massive eruption formed a large, circular umbrella with radial winds that drove ash hundreds of kilometers upwind. C. Height and lateral extent in kilometers (km), of some plumes produced by recent eruptions: Etna in 2001 (Scollo and others, 2007), Eyjafjallajökull in 2010 (Arason and others, 2011), Mount St. Helens (MSH) in 1980, both the initial phase (8:30–9:00 a.m. Pacific Daylight Time [PDT]) and later (9:00 a.m.–5:00 p.m. [PDT]), and Pinatubo in 1991 (Holasek and others, 1996).
volume (fig. 17), the absolute values of these slopes generally decrease with increasing erupted volume. The upward-decreasing trend starts when bulk (not DRE) volumes exceed a few cubic kilometers—near the top of the range of volumes we are modeling. The decreasing trend likely reflects the increasing dominance of umbrella-cloud dispersal for larger eruptions.

Comparison with Measured Airborne Concentrations

Our estimates of airborne ash concentration for $C_{av,10k}$ (1,519 mg/m$^3$) are orders of magnitude higher than any that have been measured. At Soufrière Hills, Montserrat (Searl and others, 2002), Eyjafjallajökull, Iceland (Thorsteinsson and others, 2012), and Mount Spurr, Alaska (Gordian and others, 1996) for example, measured concentrations did not exceed several milligrams per cubic meter (table 18). On May 18, 1980, measurements in central Washington ranged as much as 33 mg/m$^3$ (Bernstein and others, 1986). However, a review of methods reveals why these values differ from ours.

Measurements like the one that recorded 33 mg/m$^3$ in Yakima in 1980 were taken from a device that resembled a small weather station with a birdhouse roof (fig. 18.4). Beneath that roof, air was drawn into a funnel-shaped intake and through a filter (Doug Jager, U.S. Environmental Protection Agency, Seattle, written commun., 2017). The filters were weighed every 24 hours, yielding an average value for total suspended particulates. Unpublished worksheets of the Yakima measurement from the Washington State Department of Ecology (unpublished data, 1980) indicate that, on May 18, 1980, the filter was withdrawn before 24 hours. In Colville, Wenatchee, and elsewhere, filters clogged before the end of the 24-hour period and concentrations could not be reported.

Measurements near Yakima provide evidence for how much total ash could have been airborne. Wanapum Dam lies 51 km northeast of Yakima, directly down the 1980 dispersal axis. As at Yakima, about 10 mm (8 kg/m$^3$) of ash fell at Wanapum Dam on May 18, 1980; but at Wanapum, workers laid out trays and recorded mass accumulation rates (Scheidegger and others, 1982), which averaged about $2.5 \times 10^4$ kg/m$^2$/s for a 9-hour period. Assuming a fall rate of $u=1.5$ m/s (Durant and others, 2009; Snow and Nelson, 2012), total airborne concentration during the fall period would have been about $=160$ mg/m$^3$—several times the suspended concentrations measured at Yakima.

During large eruptions, it is not uncommon for downwind areas to receive centimeters of ash in a few hours. For example, the Volcanic Explosivity Index (VEI) 6, 1912 Novarupta-Katmai eruption deposited greater than 30 cm (consolidated) of ash on Kodiak Island, about 170 km downwind from the

Figure 17. Graph of slopes of lines on plots of log thickness versus square root of area covered ($k_0$ and $k_1$) compiled from mapped deposits in table 6 of Fierstein and Nathenson (1992), as a function of bulk deposit volume. Red box represents the range of bulk volumes used in this study. One cubic kilometer (km$^3$) bulk equals about 0.4 km$^2$ DRE, using the values for magma density (2,500 kg/m$^3$) and deposit density (1,000 kg/m$^3$) in our study. km$^{-1}$, reciprocal kilometer.
Table 18. Measurements of suspended particle concentrations made during volcanic eruptions.

Abbreviations: mg/m$^3$, milligram per cubic meter; km, kilometer; PM10, particulate matter smaller than 10 micrometers in diameter; PM2.5, particulate matter smaller than 2.5 micrometers in diameter.

| Eruption                  | Concentration | Reference                              | Comments                                                                                                                                                                                                 |
|---------------------------|---------------|----------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Mount St. Helens,         | As much as    | (Bernstein and others, 1986)           | Measured in Yakima, Washington from filter measurements of a cyclone-type instrument. Concentration represents total suspended particles. (Bernstein and others, 1986). Unpublished measurements included 17.3 mg/m$^3$ in Spokane, and 15.3 mg/m$^3$ in Coeur d’Alene (Center for Disease Control, 1980). In Colville, Wenatchee, and elsewhere, filters clogged before the end of the 24-hour period and concentrations could not be reported. |
| May 18, 1980              | 33.4 mg/m$^3$ |                                        |                                                                                                                                             |
| Mount Spurr,              | 3 mg/m$^3$ PM10| (Gordian and others, 1996)             | Measured in Anchorage, 100 km downwind from the source. 80 percent was between PM2.5 and PM10. Values are 24-hour averages using an Anderson and Head sampler.                                                   |
| August 18, 1992           |               |                                        |                                                                                                                                             |
| Soufrière Hills,          | “up to several| (Searl and others, 2002)               | Respirable dust concentrations measured with cyclone filters and DustTrak instruments in Plymouth, Cork Hill, Salem, and North, Montserrat, between September 1996 and June 1997.                                                   |
| 1996–2000                 | mg/m$^3$”     |                                        |                                                                                                                                             |
| Eyjafjallajökull,         | > 13 mg/m$^3$ | (Thorsteinsson and others, 2012)       | 10-minute average PM10 concentration measured in Vik, Iceland, May 7, 2010, 40 km southeast of Eyjafjallajökull Volcano.                                                                                   |
| 2010                      |               |                                        |                                                                                                                                             |

Figure 18. Sketches showing airborne particle sampling tools. A, Sketch showing the approximate design of airborne particle samplers of the type used in Yakima, Washington, in May, 1980. Sketch downloaded from appendix B of 40 CFR Part 50, 2017. B, Illustration of falling ash and suspended ash, showing how falling ash may fail to be drawn into the sheltered intake because of its fall velocity.
volcano (Fierstein and Hildreth, 1992). In 1932, Malargüe, Argentina received about 10 cm of ash from the 18-hour-long VEI 6 eruption of Cerro Azul (Quizapu), Chile, 106 km upwind (Hildreth and Drake, 1992). Assuming \( u = 1.5 \) m/s, a fall rate of 1 centimeter per hour (cm/hr; \( \approx 0.003 \) kg/m\(^2\)/s) translates to \( C \cong 1,800 \) mg/m\(^3\). Average accumulation rates for runs in tables 10 and 13 are in this range.

Estimates using assume a control volume (fig. 19; Snow and Nelson, 2012) in which all mass enters from above, and no mass leaves. We think this method is robust and that \( C > 1,000 \) mg/m\(^3\) is reasonable given known accumulation rates, but fall velocity adds a level of uncertainty.

### The Implications of Uncertain Fall Velocity

Aggregates used in our study have a settling velocity of about 0.35–0.85 m/s (tables 11 and 16) and are assumed not to change as they move downwind. But real aggregates may form as the cloud descends and fall faster late in transport (fig. 7). For example, Durant and others’ (2009) estimates of 1.5 m/s were based on rate of 1980 cloud descent. If the 0.25–0.50-mm-diameter aggregates described by Sorem (1982) had a density similar to the deposit density at this location (about 500 kg/m\(^3\)), their fall velocity would have been 0.85 to 1.9 m/s (fig. 8B). Measurements of \( u \) in other studies range from about 0.05 to 4 m/s (table 19).

This wide range adds uncertainty to \( C \). Both Ash3d and the control-volume method calculate airborne concentration as downward flux through a control volume. Lower fall velocities imply higher airborne concentrations. If aggregate fall velocities are 0.4–4 m/s (Taddeucci and others, 2011), rather than 0.3–0.8 m/s, then airborne concentrations could be several times lower than we estimate.

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**Figure 19.** Diagram showing control volume into which ash is falling at the mass accumulation rate \( M_d \). The average fall velocity is \( u \). Dimension of the grid cells are shown in meters (m).

**Table 19.** Tabulated fall velocities of ash aggregates from different sources.

| Value  | Explanation |
|--------|-------------|
| 1.5 m/s | Estimated by Durant and others (2009) at MSH 1980 as an average between the cloud (11.5 km) and ground level, based on a 1 hour 46 minute time delay in Spokane between arrival of the cloud overhead and the first tephra-fall. |
| 0.4–4 m/s | Velocities of hundreds of falling dry aggregates measured 7 km downwind of Eyjafallajökull in high-speed video by Taddeucci and others (2011). Aggregates were mostly \( \pm 0.5 \) mm diameter and had densities of \(< 100 \) to \( > 1,000 \) kg/m\(^3\). |
| 0.05–0.5 m/s | Measured by James and others (2002) on loose, dry aggregates created in the laboratory by electrostatically charging pumice particles. |
Conclusions

One the basis of about 10,000 model simulations, we estimate maximum and average airborne ash concentrations for the “1 in 10,000-year” event at Hanford, Washington, of about 3,800 and 1,500 mg/m³, respectively. These are order-of-magnitude estimates with large uncertainties, but we are confident that airborne concentrations of about 10⁴ mg/m³ are possible, given known deposit accumulation rates elsewhere. We emphasize that these estimates are of total airborne ash; both falling, and in suspension. They are not comparable to most air quality measurements, which measure only suspended ash.

Falling particles differ from suspended ones in that their movement is no longer well coupled to the air. Air moving toward an HVAC air intake (fig. 20) may not draw them in. The fraction of falling ash ingested depends on the nearby flow field as well as the size, shape, and density of falling material. Some aggregates may disintegrate upon impact (fig. 20), locally increasing the suspended concentration. Assessing the ash ingestion rate into a Hanford HVAC system is beyond the scope of this project. It may involve uncertainties as great as those in this study.

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Appendix 1: Particle Characterization

Introduction

The purpose of this appendix is to characterize the size and shape of volcanic ash particles that could affect Hanford from a future eruption, and to provide supporting data for related modeling and experimental studies on ashfall and resuspension. A careful analysis of particle size and shape would not be necessary if volcanic ash were composed of smooth, uniform spheres akin to beach sand. But the reality is somewhat more complex. For example, ash from explosive eruptions like the May 18th, 1980 eruption of Mount St. Helens (MSH) consists of fragments of silicate glass, denser mineral crystals, and pieces of host rock blown out by the eruption. These components are present in varying proportions depending on the eruption dynamics and transport history, leading to a complex distribution of sizes and shapes at any given site (fig. 1.1). Here, we characterize some of the key physical properties that influence the aerodynamic properties of volcanic ash, and their entrapment by air intake filters, focusing on particle size and shape. We have analyzed samples of volcanic ash sourced from three primary locations: (1) the proximal MSH 1980 deposit, (2) distal MSH 1980 deposit,
Methods and Data

To address the issues described above, particle size distributions were analyzed for 10 samples of volcanic ash, 3 of which were selected for additional shape analysis (table 1.1, fig. 1.2). All analyses were completed at the U.S. Geological Survey Cascades Volcano Observatory in Vancouver, Wash., by Alexa Van Eaton (laser diffraction, shape analysis) and Katherine Norton (sieve, sedigraph).

Table 1.1. Volcanic ash samples used in particle characterization.

[Collection locations give latitude and longitude in decimal degrees. Abbreviations: DRI, Desert Research Institute; km, kilometer]

| Sample ID            | Analyses       | Collection location                  | Description                                                                 |
|----------------------|----------------|--------------------------------------|-----------------------------------------------------------------------------|
| MSH-B1sub            | sieve, sedigraph, laser, shape | Mount St. Helens, Wash., 46.26957, −122.18092 | Field sample from the “ramp” 8 km north of Mount St. Helens, derived from pyroclastic flows on the afternoon of May 18, 1980 |
| SUBVTTS1a            | sieve, sedigraph, laser | Katmai, Alaska, 58.40150, −155.38569  | Field sample of 1912 Plinian fall deposits from the Valley of Ten Thousand Smokes, 25 km from Novarupta |
| SUBVTTS2a            | sieve, sedigraph, laser, shape | Katmai, Alaska, 58.40150, −155.38569 | —as above                                                                       |
| SUBVTTS3a            | sieve, sedigraph, laser | Katmai, Alaska, 58.29762, −155.23869  | —as above, 10 km from Novarupta                                               |
| SUBVTTS4a            | sieve, sedigraph, laser | Katmai, Alaska, 58.29762, −155.23869  | —as above, 10 km from Novarupta                                               |
| SUBVTTS5a            | sieve, sedigraph, laser | Katmai, Alaska, 58.35327, −155.30924  | —as above, 18 km from Novarupta                                               |
| SUBVTTS6a            | sieve, sedigraph, laser | Katmai, Alaska, 58.35327, −155.30924  | —as above, 18 km from Novarupta                                               |
| MSH-Hop_3.17.2017    | laser           | DRI lab                              | Lab sample of ash resuspended during experiments on MSH material             |
| VTTS_Hop_3.21.2017   | laser           | DRI lab                              | Lab sample of ash resuspended during experiments on VTTS1, VTTS2, and VTTS5 material |
| MSH1980-C.RUSSELL    | laser, shape    | Yakima, WA, 46.60202, −120.41813     | Field sample of ashfall collected on May 18, 1980, during the first few hours of ashfall, 144 km from Mount St. Helens |

Figure 1.1 (page 39). Example of scanning electron microscope (SEM) images of volcanic ash used in this study. Arrows point to particle morphologies discussed in the text. Note scale bar on each image; magnification ranges from 270x to 370x. A–C, Images of proximal Mount St. Helens (MSH) ash deposit derived from pyroclastic flows on the afternoon of May 18, 1980, (sample MSHb1sub). Note the variety of grains present, from vesicular glass (containing abundant bubbles), to poorly vesicular or dense glass, and a smaller proportion of irregular, mossy grains. D–F, Images of distal MSH ashfall from May 18, 1980, collected from Yakima, Washington, roughly 78 kilometers west of Hanford, Washington (sample MSH1980-C.RUSSELL). This material contains less vesicular glass overall. G–I, Volcanic ash from the Valley of Ten Thousand Smokes, Alaska, derived from tephra-fall deposits of the 1912 Novarupta-Katmai eruption (sample subVTTS2a). Note the abundance of vesicular glass and bubble wall shards. μm, micrometer.
Size Analysis of Volcanic Ash

In conventional methods of particle size analysis, the coarser material is assessed by sieving, which involves passing the sample through progressively smaller meshes and weighing the fractions retained. This approach becomes unreliable for particles much smaller than about 63 micrometers (μm), so more sophisticated methods are required for the fine-grained material. In this study we have used a combination of laser diffraction and sedigraph to analyze the finer particles and merge results with sieve data where appropriate. Both laser diffraction and sedigraph have strengths and weaknesses. One benefit of the sedigraph is that it measures settling velocities of particles (in water), which may provide useful information for calculating settling velocities in air. Key benefits of laser diffraction are that it can cover a wider range of sizes (0.4 μm to 2 millimeters [mm]) and analyze very small amounts of sample (typically less than 0.2 grams [g]). Results from these two methods would be identical if the particles were perfect spheres with uniform densities and optical properties. But the natural complexity of volcanic ash means that sieving, laser diffraction, and sedigraph techniques each provide slightly different measurements of “diameter”, despite being robust and established methods that have been used in particle size analysis for decades.

Sieving

All samples containing particles larger than 1 mm were dry sieved (table 1.1) to obtain the distribution of sieve diameters from 31.5 mm to 63 μm. To prepare the sample, aggregates were lightly crushed with a mortar and rubber-tipped pestle. The material larger than 4 mm was hand-sieved at standard intervals of 8, 16, and 31.5 mm. Then the fraction finer than 4 mm was passed through a stack of sieves using an automated shaker for 10 ± 2 minutes, using sieve meshes of 2 mm, 1 mm, 500 μm, 250 μm, 125 μm, and 63 μm, plus a catch pan. Material retained on each sieve and pan was weighed to the nearest 0.1 gram. The cumulative particle size distribution was recorded as weight percent retained by each sieve and merged with fines analysis where appropriate (table 1.1), as described in the following sections.

Laser diffraction

Laser diffraction measures the optical diameters of particles less than 2 mm. For this study, the method was only applied to volcanic ash sieved below 1 mm, using a Beckman Coulter LS 13 320. The technique works by shining a 780 nm laser beam through a well-mixed dispersion of particles in water. The cross sectional areas of tumbling particles scatter the light into a diffraction pattern, which can be converted to a size distribution using Mie theory and some assumptions about the optical properties of the grains. With our instrument configuration, a sample mass of 0.1–0.2 g is typically enough for a standard analysis. This enabled analysis of the airborne material collected from resuspension experiments in the lab (table 1.1), which did not provide enough material for the sedigraph. To prepare the sample, a test portion of volcanic ash smaller than 1 mm was transferred to a plastic vial with 50–100 milliliters (ml) of Calgon solution and shaken by hand to disperse any aggregates. Using a plastic pipette, the dispersion was transferred to the instrument’s Aqueous Liquid Module and sonicated for 60 sec before analysis. The sample was analyzed 3 times for 60 seconds each, and an average of the three runs was used. A single optical model was applied to all volcanic ash samples used in this study (all are dacitic in composition), using values of 1.5 for the real refractive index and 0.0005 for the absorption coefficient based on comparison with published studies (Ball and others, 2015) and the International Organization for Standardization (ISO) lookup table (ISO, 2009). The results give volume percent finer for each size class. Note that laser diffraction measures volume rather than weight percent (like sieving and sedigraph), but results are comparable if a constant particle density is assumed. For samples that were sieved (table 1.1), the laser diffraction and sieve data were combined by scaling the laser diffraction results to the whole sample using the
known proportion of ash smaller than 1 mm determined from sieving. Data are provided in table 1.2. We have binned the laser data into half-phi intervals (see fig. 1.2) although higher-resolution bins are also available in the data archive. We included additional size classes at 2.5 and 10 micrometers (particulate matter [PM]2.5 and PM10, respectively) because of their relevance to resuspension and air filtration systems (highlighted rows in table 1.2).

Sedigraph

Sedigraph analysis was performed on all the sieved samples (table 1.1). This method determines the settling diameter of particles less than 63 \( \mu \text{m} \) by measuring their gravitational fall velocity in water and assuming perfectly spherical shapes. The Micromeritics Sedigraph III 5120 uses the relative absorption of a low-energy X-ray beam to estimate the concentration of particles in suspension at different heights, at known times during the analysis. Conversion to a particle-size distribution is performed through a combination of Beer’s Law and Stokes’ Law, assuming a constant particle density of 2.615 grams per cubic centimeter (g/cm\(^3\)) and water temperature of 35 °C (refer to ISO, 2001; Webb, 2004). The analysis requires 1.5 to 3 g of material for reliable results. To prepare the sample, a sufficient mass of the fraction finer than 63 \( \mu \text{m} \) fraction was placed in a cup, wetted with deionized water and dispersed using 1 milliliter (mL) of dispersing agent and a 30 second burst with an ultrasonic probe. Then the dispersion was

### Table 1.2. Particle-size distributions using combined sieve-laser diffraction analyses, shown as cumulative percent less than a given size fraction.

| Method | Diameter, in \( \mu \text{m} \) | MSH-B1sub | subVTT-S1a | subVTT-S2a | subVTT-S3a | subVTT-S4a | subVTT-S5a | subVTT-S6a | MSH_Hopper | VTTS_Hop_3 | MSH1980-C.RUSSELL |
|--------|-----------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|------------------|
| laser  | 1    | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
| laser  | 1.4  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 |
| laser  | 2    | 0.4 | 0.1 | 0.1 | 0.2 | 0.3 | 0.1 | 0.1 | 2.1 | 1.1 | 1.0 | 0.9 |
| laser  | 2.5  | 1.5 | 0.3 | 0.2 | 0.9 | 1.1 | 0.1 | 0.1 | 9.4 | 6.5 | 2.0 |
| laser  | 2.8  | 2.4 | 0.4 | 0.3 | 1.4 | 1.8 | 0.2 | 0.2 | 15.2 | 11.1 | 2.7 |
| laser  | 3.9  | 6.1 | 0.9 | 0.5 | 3.8 | 4.7 | 0.2 | 0.3 | 37.7 | 30.0 | 5.5 |
| laser  | 5.5  | 10.9 | 1.4 | 0.8 | 6.8 | 8.2 | 0.4 | 0.4 | 59.7 | 50.0 | 8.7 |
| laser  | 7.8  | 16.6 | 2.0 | 1.1 | 10.1 | 12.2 | 0.5 | 0.6 | 75.1 | 66.0 | 12.1 |
| laser  | 10   | 21.6 | 2.4 | 1.4 | 12.8 | 15.4 | 0.6 | 0.8 | 82.7 | 74.9 | 14.7 |
| laser  | 11   | 23.6 | 2.6 | 1.5 | 14.0 | 16.8 | 0.7 | 0.8 | 85.0 | 77.8 | 15.8 |
| laser  | 15.6 | 32.9 | 3.4 | 1.9 | 19.0 | 22.8 | 1.0 | 1.1 | 92.5 | 87.3 | 20.3 |
| laser  | 22.1 | 43.4 | 4.4 | 2.6 | 25.6 | 30.5 | 1.4 | 1.6 | 97.2 | 94.4 | 24.6 |
| laser  | 31.3 | 53.5 | 5.7 | 3.5 | 33.0 | 38.9 | 2.0 | 2.2 | 99.0 | 97.9 | 28.3 |
| laser  | 44.2 | 63.0 | 8.1 | 5.3 | 41.9 | 48.5 | 3.1 | 3.5 | 100.0 | 99.9 | 32.1 |
| laser  | 62.5 | 71.3 | 12.3 | 8.7 | 51.6 | 58.7 | 4.7 | 5.6 | 100.0 | 100.0 | 35.0 |
| laser  | 88.4 | 78.1 | 18.5 | 14.2 | 60.2 | 67.4 | 7.2 | 9.0 | 100.0 | 100.0 | 37.8 |
| laser  | 125 | 84.5 | 27.4 | 22.5 | 68.1 | 74.9 | 10.7 | 13.8 | 100.0 | 100.0 | 41.5 |
| laser  | 176.8 | 89.8 | 38.7 | 33.6 | 74.6 | 80.7 | 15.7 | 20.6 | 100.0 | 100.0 | 51.9 |
| laser  | 250 | 93.8 | 52.3 | 47.6 | 80.2 | 85.0 | 23.9 | 30.6 | 100.0 | 100.0 | 74.2 |
| laser  | 353.6 | 96.6 | 66.1 | 62.1 | 84.9 | 88.6 | 36.8 | 44.7 | 100.0 | 100.0 | 90.9 |
| laser  | 500 | 97.7 | 76.7 | 74.0 | 89.2 | 92.0 | 54.4 | 61.4 | 100.0 | 100.0 | 97.3 |
| laser  | 707.1 | 98.3 | 84.1 | 82.4 | 93.4 | 95.5 | 72.3 | 76.9 | 100.0 | 100.0 | 99.8 |
| sieve  | 1,000 | 98.9 | 90.4 | 89.8 | 95.7 | 97.4 | 89.4 | 90.3 | 100.0 | 100.0 | 100.0 |
| sieve  | 2,000 | 99.6 | 95.4 | 96.0 | 99.4 | 99.2 | 94.1 | 95.4 | 100.0 | 100.0 | 100.0 |
| sieve  | 4,000 | 100.0 | 97.9 | 98.8 | 99.9 | 100.0 | 96.6 | 97.3 | 100.0 | 100.0 | 100.0 |
| sieve  | 8,000 | 100.0 | 99.2 | 99.9 | 100.0 | 100.0 | 98.3 | 97.9 | 100.0 | 100.0 | 100.0 |
| sieve  | 16,000 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 |
introduced to the sedigraph for analysis. Recorded values for the mass of each size class were scaled to the whole sample using the known proportion of ash smaller than 63 µm determined from sieving (table 1.3).

Shape Analysis of Volcanic Ash

Particle morphology exerts a first-order control on the aerodynamic behavior of volcanic ash (Wilson and Huang, 1979). The particle sizes most likely to clog HVAC filters are in the range of 10 micrometers diameter and smaller (For example, Azimi and others, 2014). Particles in this size range are challenging to isolate and work with in the lab owing to the effects of electrostatic attraction in low-humidity environments (Miura and others, 2002; James and others, 2003). In our analysis, the 32–63 µm fraction was chosen as a reasonable compromise between imaging the finest particles and ensuring reliable results by minimizing electrostatic aggregation and touching grains during sample preparation.

Some of the useful ways to categorize particle shape include measurements of form (elongate versus equant) and roughness (jagged versus smooth) (Liu and others, 2015). To quantify the relevant parameters (table 1.4), we examined two-dimensional projected areas of unpolished grains using images from a scanning electron microscope. The areas are projected because they are based on two-dimensional images of complex three-dimensional objects, rather than flat thin sections or polished surfaces (fig. 1.3). This approach was chosen because it allows examination of the surface features and a better intuition for the overall appearance of volcanic ash in its natural state.

Bulk ash samples were sieved between 32–63 µm, sonicated in deionized water for 2–3 minutes to remove adhering fines, and oven dried. Particles were dusted onto pin-type scanning electron microscope (SEM) stubs and carbon coated using a Denton Vacuum Desk Sputter Coater. Typical SEM operating conditions used a working distance of 15–17 mm and accelerating voltage of 20 kilovolts (kV) in backscatter mode. Images were collected at a magnification of 55x or more and saved as 1024 x 1024 TIFF files, providing about 20–40 grains per image and a resolution of at least 0.63 pixels per µm. Then images were processed using digital thresholding to distinguish the particles from background. Where necessary, a line was manually drawn (2 pixels wide) to separate touching grains and those touching the edge of the image but still greater than 98 percent within the field of view. Next, the image was converted to binary (black and white) and used as input for ImageJ (software version 1.50c4). Within ImageJ, the scale was specified according to the pixel resolution of the image, and the following measurement routines enabled: (1) area, (2) shape descriptors, (3) perimeter, (4) fit ellipse, and (5) feret diameter (table 1.4). Particles were excluded from analysis if they were less than 200 square micrometers (µm²) area or touching the edges of the processed image. Resulting outlines were numbered and saved. More than 1,000 particles were analyzed from each of the three samples. The number of pixels per particle (pixel density) is an important factor in data quality, with previous studies showing consistent results with at least 750 pixels per particle (Liu and others, 2015). Therefore, we only include results from the particles defined by 750 pixels or more (table 1.5).

Table 1.3. Sieve-sedigraph particle-size distributions, shown as cumulative weight percent less than a given size fraction.

| Method   | Diameter, in µm | MSH-B1sub | subVTTS1a | subVTTS2a | subVTTS3a | subVTTS4a | subVTTS5a | subVTTS6a |
|----------|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| sedigraph| 1               | 0.9       | 0.1       | –         | 4.0       | 5.4       | –         | 0.1       |
| sedigraph| 2               | 4.9       | 0.3       | 0.4       | 6.3       | 7.6       | 0.3       | 0.3       |
| sedigraph| 3.9             | 10.0      | 0.5       | 0.5       | 8.3       | 10.3      | 0.4       | 0.4       |
| sedigraph| 7.8             | 21.8      | 1.1       | 1.2       | 11.8      | 15.0      | 0.9       | 0.9       |
| sedigraph| 15.6            | 41.3      | 2.4       | 2.1       | 17.5      | 23.5      | 1.7       | 1.6       |
| sedigraph| 31.3            | 57.9      | 6.8       | 5.7       | 27.0      | 36.6      | 4.3       | 3.9       |
| sieve    | 62.5            | 67.7      | 13.7      | 11.7      | 33.0      | 43.6      | 8.5       | 8.0       |
| sieve    | 125             | 85.0      | 32.8      | 31.1      | 48.4      | 59.8      | 19.5      | 18.9      |
| sieve    | 250             | 94.7      | 6.1       | 60.8      | 62.2      | 72.6      | 40.3      | 39.3      |
| sieve    | 500             | 98.1      | 81.7      | 82.2      | 81.9      | 87.2      | 72.9      | 71.6      |
| sieve    | 1,000           | 98.9      | 90.4      | 89.8      | 95.7      | 97.4      | 89.4      | 90.3      |
| sieve    | 2,000           | 99.6      | 95.4      | 96.0      | 99.4      | 99.1      | 94.1      | 95.4      |
| sieve    | 4,000           | 100.0     | 97.9      | 98.8      | 100.0     | 96.6      | 97.2      |           |
| sieve    | 8,000           | 100.0     | 99.2      | 99.9      | 100.0     | 98.3      | 97.9      |           |
| sieve    | 16,000          | 100.0     | 100.0     | 100.0     | 100.0     | 100.0     | 100.0     | 100.0     |
**Results and Discussion**

**Particle-Size Distributions**

Full results of the measured size distributions are tabulated in spreadsheet A1 in the accompanying data repository (Mastin and others, 2020). Size distributions of the volcanic ash from Mount St. Helens and Valley of Ten Thousand Smokes samples show several key features (fig. 1.4). First, the 10 samples of primary volcanic ash show marked variations in the content of particles less than or equal to 10 µm (PM10), from less than one percent in the coarsest samples from the Valley of Ten Thousand Smokes, to 22 percent in the proximal MSH sample. Particles smaller than 2.5 µm (PM2.5) range from 0.2–2 percent (fig. 1.4, table 1.2). In contrast, the airborne ash collected during resuspension...
Figure 1.4. Histograms showing particle-size distributions from sieve-laser diffraction analysis of each volcanic ash sample collected in the field. Note values are reported as percent within each size class, rather than cumulative percent as shown in table 1.2. Size bins are in half-\( \phi \) increments from 1 micrometer to 1 millimeter (mm), and whole-\( \phi \) increments from 1–16 mm. %, percent.
experiments (fig. 1.5) is almost entirely less than 32 µm and contains significantly more PM10 (75–83 percent) and PM2.5 (7–10 percent). These numbers vastly underestimate the PM2.5 fraction because particles smaller than 2.5 µm were removed during the lab’s collection process. The implication is that primary ashfall from an explosive eruption could transport significant quantities of extremely fine ash to Hanford, but resuspension by the wind would concentrate and re-entrain the sizes most relevant to air filtration systems.

Another observation is that the proximal sample of MSH 1980, collected 8 km from the volcano, contains substantially more fine ash than the distal fall deposit that landed in eastern Washington (fig. 1.4). Table 1.2 shows that the proximal sample is 71 percent finer than 63 µm compared to 35 percent at Yakima. The difference in PM10 content is somewhat less marked (22 percent versus 15 percent). The finer-grained nature of the proximal ash is clearly seen in figure 1.6A, which includes two additional ashfall samples that landed within 80 km of Hanford (reported by Durant and others, 2009). The contrast between proximal and distal samples mainly reflects their transport histories during different phases of the eruption. In this case, the proximal sample was sourced from the outer edges of pyroclastic flows on the afternoon of May 18. These ground-hugging currents simply did not travel as far as the higher-altitude vertical plumes, so all their mass—even the finest particles—deposited closer to the volcano. The key message is that both samples are useful for evaluating the range of possible size distributions transported by a Mount St. Helens eruption. To demonstrate this, figure 1.6B shows the proximal sample alongside the total grain-size distribution of the entire May 18, 1980, fall deposit from Durant and others (2009), which integrates several ashfall samples at different sites to reconstruct the original size population as it exited the volcano. The two plots show roughly comparable amounts of PM10, suggesting that the proximal sample is well within the expected range of size distributions produced by the May 18, 1980, eruption.

**Figure 1.5.** Comparison of parent versus resuspended ash from Portable In Situ Wind ERosion Lab (PI-SWERL) laboratory experiments, using material from Mount St. Helens, Washington, and the Valley of Ten Thousand Smokes, Alaska. Grain-size distributions are from sieve-laser diffraction data in table 1.2. The size distributions of resuspended ash from the two locations are nearly identical, despite very different parent material. The PI-SWERL laboratory instrument is designed to sample only the particles coarser than 2.5 micrometer (µm) “aerodynamic” diameter from the resuspended ash (labeled cutoff in this plot), although laser diffraction does show a small amount of material less than 2.5 µm “optical” diameter. %, percent.
Morphology of the Volcanic Ash Particles

Results of shape analyses are tabulated in spreadsheet A2 of the data repository (Mastin and others, 2020). The aerodynamic properties of volcanic ash and entrapment by filters are both influenced by the shape of the particles (Wilson and Huang, 1979). Figure 1.7 shows distribution of long axes in each of the three samples, based on feret diameter. Although these particles were sieved between 32–63 µm, their long axes are generally much larger, in the range of 60–100 µm, owing to the presence of elongate particles, particularly in the sample from the Valley of Ten Thousand Smokes (sub-VTTS2a). Figure 1.8A illustrates this particle elongation with a plot of axial ratios, which is the ratio of intermediate to long axes. The VTTS sample contains higher proportions of elongate grains compared to the proximal and distal MSH ash, perhaps reflecting differences in the style of magma fragmentation. For example, magma breakage may have occurred along bubble walls that were more elongate than in the Mount St. Helens 1980 magma. Elongate bubbles are visibly more common in scanning electron microscope (SEM) images of the VTTS ash (fig. 1.1H).

Another important observation is particle roughness, which is strongly affected by the presence of vesicular glass. The distal MSH sample from Yakima is an outlier in this regard. Both in terms of solidity (fig. 1.8b) and form factor (fig. 1.8c), it contains significantly more particles with smooth outlines, indicating less vesicular glass. Lower vesicularity is linked to the magma ascent and fragmentation processes associated with the earliest phase of the May 18th eruption. The sample was collected during the first few hours of ashfall in Yakima, at a time when the eruption was expelling a less vesicular batch of magma known as the cryptodome. The cryptodome magma rose slowly in the volcanic edifice and had time to partially degas before generating the lateral blast and its associated far-traveled ash plume (Hoblitt and Harmon,
Results and Discussion

Figure 1.7. Histogram of feret diameters (in micrometers [µm]) from each of the samples analyzed for shape, where n gives the number of grains used for each sample (meeting or exceeding the threshold of 750 pixels per particle). The green bar is from Yakima, Washington, sample MSH1980-C.RUSSELL; the yellow bar is from Mount Saint Helens (MSH), sample MSHb1sub; and the dashed black line is from the Valley of Ten Thousand Smokes (VTTS), sample subVTTS2a. The particles were sieved between 32–63 micrometers for analysis, but their feret diameters (long axes) are mainly in the range of 60–90 µm owing to the presence of elongate grains. Note that the Valley of Ten Thousand Smokes sample contains the longest feret diameters for the same sieve fraction, indicating a greater proportion of elongate grains. %, percent.

Figure 1.8. Plots showing the results of particle-shape analysis on the three samples of volcanic ash. A, axial ratio, or ratio of intermediate to long axes. B, Solidity which is a measure of particle roughness. C, Form factor, which is sensitive to both form and roughness. The green bar is from Yakima, Washington, sample MSH1980-C.RUSSELL; the yellow bar is from Mount St. Helens (MSH), sample MSHb1sub; and the dashed black line is from the Valley of Ten Thousand Smokes (VTTS), sample subVTTS2a. Note that the Valley of Ten Thousand Smokes (VTTS) sample has the lowest axial ratios because of elongate particles, and distal Mount St. Helens (MSH) (Yakima) has the highest values of solidity and form factor owing to poorly vesicular particles.
This is quite a different scenario from the later phases of the May 18th eruption (and the 1912 eruption Novarupta) which involved actively vesiculating magma that rose quickly to the surface and erupted as vertical Plinian columns (Gonnermann and Houghton, 2012). The key message here is that different magma fragmentation processes can produce far-traveled volcanic ash in the Cascades, leading to deposition of different particle shapes. And yet, despite the clear differences among samples in terms of eruption dynamics and particle morphologies, they do plot in a relatively consistent range, with most axial ratios in the range of 0.4–0.8, solidity 0.85–0.90, and form factor 0.45–0.75 (fig. 1.8).

Conclusions

An analysis of particle size and shape distributions of volcanic ash from the May 18, 1980, eruption of Mount St. Helens and 1912 eruption of Novarupta, Alaska (Valley of Ten Thousand Smokes), reveals several observations relevant to the hazards of ashfall impacting Hanford from a future eruption in the Cascades.

1. Particle-size distributions transported to the Hanford area by a Mount St. Helens eruption will vary greatly depending on the dynamics of eruption and transport, but a reasonable expectation is that the content of PM10 (particles smaller than 10 µm) could be less than 1 percent to greater than 20 percent, with PM2.5 comprising as much as 2 percent of the ashfall deposit by mass.

2. Resuspension of the ashfall deposit by wind will preferentially loft the material less than 32 µm, leading to a substantially greater proportion of PM10 in the airborne population (much greater than 70 percent by mass).

There are distinct differences in particle morphologies of the three ash samples analyzed in this study, related primarily to magma fragmentation processes. But overall, they show a relatively consistent range of shape parameters, with most axial ratios in the range of 0.4–0.8, solidity 0.85–0.90, and form factor 0.45–0.75.
Appendix 2: Effect of Extremely Large Eruptions of Mount St. Helens on Tephra-Fall Thickness and Airborne Ash Concentration at the Hanford Site, Washington

by Larry G. Mastin, Michael Clynne, Manuel Nathenson, John Pallister, and Alexa Van Eaton

Introduction

In December 2018, the U.S. Geological Survey’s Cascades Volcano Observatory submitted the main body of this report to the U.S. Department of Energy’s Office of River Protection (DOE-ORP), estimating the thickness and airborne ash concentration that could occur at the Hanford, Washington, facility with an annual probability of 1 in 10,000 during a future eruption of Mount St. Helens (MSH). To make this estimate, we ran approximately 10,000 model simulations of a hypothetical MSH eruption, randomly sampling erupted volumes within the range that are recorded in the Holocene stratigraphic record at MSH. The largest Holocene tephra deposit at MSH, the Yn, has a dense-rock-equivalent (DRE) volume between 0.8 and 2.3 cubic kilometers (km$^3$; Nathenson, 2017). The maximum volume we used for our modeling, 2.3 km$^3$ DRE, was a key input.

In July 2019, DOE-ORP forwarded us the Staff Factual Accuracy Check and Staff Review of our analysis, written by the Defense Nuclear Facilities Safety Board (DNFSB) staff. The Accuracy Check noted some key concerns, specifically:

1. The maximum eruption volume used in our analysis was “non-conservative”. The DNFSB staff cited an International Atomic Energy Agency document, IAEA-TEC-DOC-1795, Volcanic Hazards Assessments for Nuclear Installations, 2016 (International Atomic Energy Agency, 2016), which recommends that volcanic hazard assessments for nuclear facilities consider volcanic activity extending back 10 million years. “Including data from 10,000 years to 10 million years ago would have resulted in a larger estimated maximum erupted volume ($V_{\text{max}}$) and would therefore increase anticipated ashfall thickness and concentration values.” The DNFSB staff was not persuaded by previous assessment and appraisal from the U.S. Geological Survey (USGS) that the magma system for Mount St. Helens was different during pre-Holocene time, and that larger pre-Holocene eruptions did not reflect the current composition and (or) size of the magma system.

2. The maximum estimated volume for the Yn, 2.3 km$^3$, was used as an absolute upper bound and we did not consider aleatoric variability and epistemic uncertainty.

The USGS provides this report to address those concerns. In our modeling, we chose the Yn as the upper endmember because it was the largest Holocene eruption, and because it occurred in a magma system that in some way resembles the current one. We did not examine older eruptions because the lack of adequate geological and physical evidence makes estimates of their size impractical; however, we should at least consider the probability of eruptions bigger than the Yn. In this report, we examine evidence of larger eruptions, run additional models, and reach three conclusions: (1) that the Yn eruption is likely the largest at Mount St. Helens over at least the past 50,000 years; (2) that the annual probability of larger eruptions is likely about $10^{-5}$ or less, and (3) that including eruptions larger than the Yn in our analysis, weighted by their probability, does not change our estimates of thickness or airborne concentration by more than a few tens of percent, for the 1-in-10,000 year event. These variations are within the range of other uncertainties in our analysis.

Size of the Largest Eruptions at Mount St. Helens

The oldest rocks that make up Mount St. Helens are a few hundred thousand years old (Clynne and others, 2008). The area around the volcano was glaciated several times before about 10 kilo-annum (ka) and older tephras were mostly removed; thus, older tephras are known primarily from distal locations. The biggest late-Pleistocene tephras known from MSH are the C-set tephras (Mullineaux, 1996), at least four of which are exposed in the eastern Washington Palouse (Busacca and others, 1992). The younger two correlate with Cw and Cy (Busacca and others, 1992), with ages in the 45–50,000-year range. One of the two older C tephras was dated at 83±8.3 ka by thermoluminescence (Berger and Busacca, 1995), and it is not a C tephra recognized proximally. The age of the fourth Set C tephra was estimated by deposition rate to be as old as about 120 ka and is also probably not preserved proximally.

We have no estimates of the volume of these older eruptions, but in the most comprehensive study of MSH tephras, Mullineaux (1996) implies that they were big. In his abstract, and his summary of Ape Canyon Stage volcanism, Mullineaux (1996) describes a late Set C tephra (probably Cy) as the largest known Mount St. Helens tephra of Pleistocene age. “One of them erupted near the end of Ape Canyon time, records one of the largest [italics ours] volume tephra eruptions known for MSH and has been recognized as far away as Nevada.”. Also, in the abstract and discussion of Spirit Lake Stage volcanism (Mullineaux, 1996, abstract))
states: “One of the coarse layers, layer Yn, is the largest volume Holocene tephra known from Mount St. Helens.” Carey and others (1995) echo that statement: “Layer Yn (3,510 years before present.) represents the highest intensity and largest magnitude eruption at Mount St. Helens in post-glacial times.”

The best available indicator of the size of late-Pleistocene tephras, relative to the Yn, is their thickness at comparable distances along their dispersal axes (table 2.1). The Cb tephra is about 100 centimeters (cm) thick at 8–11 kilometers (km) downwind (Mullineaux, 1996, Fig. 11). At the same distance downwind, Cw is 40 cm and Cy is 60 cm, and the other Set C tephras are thinner. Yn is about 200 cm thick, and 120–180 cm at 18 km (Carey and others, 1995, Fig. 3c; Mullineaux, 1996, Fig. 40B). Also at 8–10 km distance, the Wn, the second largest Holocene tephra, is 180 cm thick (Carey and others, 1995, Fig. 7a; Mullineaux, 1996, Fig. 61E). In these proximal locations, the Yn is the thickest known MSH tephra. Studies of distal Cascade tephras from the American West or Canada (Jensen and others, 2019) also recognize the Yn as being the most widespread Mount St. Helens tephra.

There are caveats with this conclusion of course. Exposures of the Pleistocene tephra set C-set are sparser than of Holocene tephras; and for this reason, we are less confident that the C-set thicknesses observed at 8–11 km distance are along the dispersal axis. Moreover, because exposures degrade with time, the older tephras at distal sites will be less prominent. Despite those caveats, we have found no evidence of any MSH tephras thicker than the Yn.

Table 2.1. Thickness of the largest tephra layers at Mount St. Helens, at 8–11 kilometers from the vent.

| Unit | Thickness at 8–11 km distance (cm) |
|------|-----------------------------------|
| Wn   | 180                               |
| Yn   | 200                               |
| Cy   | 60                                |
| Cw   | 40                                |
| Cb   | 100                               |

Table 2.2. Number of eruptions in the Smithsonian Institution’s Global Volcanism Program (GVP) Volcanoes of the World Database, listed by size (VEI) (Global Volcanism Program, 2013). Eruptions with no size assignment are listed under “??”.

| VEI | Volume (km$^3$) | All GVP | Stratovolcanoes |
|-----|-----------------|---------|-----------------|
|     | Bulk            | Count   | Percent         | Count | Percent |
| ??  | 2,251           | 23      | 1,318           | 22    |
| 0   | $1 \times 10^5$–$1 \times 10^4$ | 804 | 8 | 174 | 3 |
| 1   | 0.0001–0.001    | 1,208   | 12 | 772 | 13 |
| 2   | 0.001–0.01      | 3,741   | 38 | 2,481 | 41 |
| 3   | 0.01–0.1        | 1,127   | 11 | 808 | 13 |
| 4   | 0.1–1           | 504     | 5 | 342 | 6 |
| 5   | 1–10            | 177     | 2 | 127 | 2 |
| 6   | 10–100          | 52      | 0.5 | 24 | 0.4 |
| 7   | 100–1,000       | 8       | 0.1 | 3 | 0.0 |

Probability of an Eruption Larger than the Yn

Even if the Yn were the biggest of the MSH tephra eruptions, the probability of a larger eruption must be greater than zero. In order to assign the size and probability of this larger eruption, we must consider a larger dataset.

The world’s volcanic activity is chronicled by the Smithsonian Institution. Their Global Volcanism Program Volcanoes of the World (GVP) Database (https://volcano.si.edu/) lists all known historical eruptions worldwide, plus all older Holocene eruptions that are known from deposits rather than direct observations. Where possible, the size of each eruption is assigned using the Volcanic Explosivity Index (VEI); a complicated ranking that uses both plume height and tephra volume to derive a number from 0 to 8. Considering only tephra volume, eruptions of VEI 3, 4, 5, 6, and 7 have bulk volumes exceeding 0.01, 0.1, 1, 10, and 100 km$^3$ respectively. Nathenson (2017) estimates the bulk volumes of the 1980, the Wn, and the Yn tephra deposits as 1.1, 0.7–4, and 2–9 km$^3$ respectively, ranking them all as VEI 5 on this scale. Nathenson’s (2017) 9 km$^3$ maximum tephra volume for the Yn converts to our modeled maximum dense-rock-equivalent (DRE) volume of 2.3 km$^3$, using Nathenson’s densities of 600 kilograms per cubic meter (kg/m$^3$) and 2,300 kg/m$^3$ for the deposit and the magma, respectively.

Nathenson’s (2017) volume estimate for the Yn ranks it as a large VEI 5 eruption. Among all eruptions in the GVP database, eruptions of size VEI 6 and larger (roughly, those bigger than the Yn) are about three times less common than VEI 5 (table 2.2, columns 2 and 3). However, some types of volcanoes are more capable of large eruptions than others. The GVP data indicate for example that of 6,049 eruptions from stratovolcanoes (of which MSH is one) 127 are VEI 5 (column 4), and 24 are VEI 6 or greater. Thus VEI 6 or greater eruptions compose less than 0.5 percent of all eruptions, and about 2 percent of VEI 3 or greater eruptions.

Within the Cascade Range, scattered layers record the infrequent occurrence of very large tephra eruptions. Nathenson (2012, Table 4) has tabulated about 20 Cascade tephras with deposit volumes ($V$) greater than 5 km$^3$, and 12 with ($V$) greater than 10 km$^3$, since 1.2 Ma. The volumes that form
this tally are mostly educated guesses using thicknesses extrapolated from a few outcrops or inferred from the size of a caldera. Some volumes have since been revised downward (Nathenson, 2017). But if we take these numbers at face value and plot them as a function of age (fig. 2.1), we can assess the eruptive frequency from the steepness of the curves. The frequency of eruptions with bulk volumes greater than 5 km$^3$ (the blue curve of fig.2.1) appears dramatically greater in the past few tens of thousands of years than at earlier times. We do not think that this indicates an increasing rate of activity; more likely, it is an artifact of preservation. Tephra deposits get buried or eroded with time, and the smaller deposits disappear. The magenta curve of figure 2.1 represents the larger eruptions and shows a more constant rate since about 600 ka—a trend that suggests the record may be more complete over this time. The last 300 ky shows a rate somewhat higher—perhaps twice as high as the overall average since 600 ka. Ten eruptions with $V > 10$ km$^3$ since 600 ka implies a Cascade-wide annual probability of $1.6 \times 10^{-5}$. The somewhat higher rate in the past 300 ky suggests an annual probability of about $3 \times 10^{-5}$. Whether this probability is evenly distributed among all 18 volcanoes of the Cascade Range is debatable. MSH is currently the most explosive volcano, but geodetic, seismic, and petrologic data make it uncertain whether its magma body is large enough to feed such an event. If evenly distributed so that the annual probability of a VEI 6 or greater eruption is the same at all volcanoes, the annual probability of a larger than 10 km$^3$ (bulk) eruption at MSH would be roughly $3 \times 10^{-5}/18 \approx 2 \times 10^{-6}$. If concentrated at MSH, the annual probability of a VEI 6 or greater there could be an order of magnitude higher. Corresponding recurrence intervals ($R_{VEI6+}$) of a larger than 10 km$^3$ (bulk) eruption at MSH would be about 50,000 to 500,000 years. At this rate, we would expect at least a few such eruptions in the more than 300,000-year history of MSH. In the geologic record, we see no evidence for any such eruptions.

**Effect of Large Eruptions on our Model Results**

Our analysis and that of Hoblitt and Scott (2011), noted that MSH produced 4 large explosive eruptions in roughly the last 500 years. Nathenson’s (2017) volume estimates suggest that these were VEI 3 or larger. To first order, the recurrence interval $R$ of these events is about one per century. If the recurrence interval ($R_{VEI6+}$) for VEI 6 or greater eruptions is between 50,000 and 500,000 years, then the conditional probability of a VEI 6 or greater eruption, given the occurrence of an eruption, would be roughly $R/R_{VEI6+} = 0.0002$ to 0.002. That is, for every VEI 6 or greater eruption, we would expect between 500 and 5,000 smaller (VEI 4–5) eruptions.

Including these larger eruptions with their appropriate conditional probability would require that we add between 2 and 20 larger eruptions to the roughly 10,000 we have run already. We have actually run 1,000 additional simulations with volumes of 2.3–40 km$^3$ DRE. In table 2.3, we examine the effect on the thickness ($T_{10k}$), maximum ($C_{max,10k}$), and average ($C_{avg,10k}$) airborne ash concentrations of adding 1, 10, 100, 1,000, and 10,000 eruptions.
or all 1,000 to the simulations already run. Our objective is to examine the sensitivity of model results to different probabilities of high-volume eruptions. Volumes of these additional runs were assigned randomly using a uniform cumulative distribution on a log scale (fig. 2.24). Model inputs and outputs from these runs is added in tables BS1–BS3 of Mastin and others (2020). New values of the $T_{10k}$, $C_{max,10k}$, and $C_{ave,10k}$ airborne ash concentrations at Hanford, having an annual probability of 1 in 10,000, were calculated using the same methodology as in our main report.

Table 2.3 shows that changes to $T_{10k}$, $C_{max,10k}$, and $C_{ave,10k}$ from the addition of these runs are less than 40 percent, even when all 1,000 of the large-volume runs are added. The small effect is due in part to the fact that most simulations produced no deposit at Hanford (red dots, fig. 2.2b).

A second reason for the small effect is that we left most of the volume distribution intact, changing only the upper (high-volume) tail. Here, we also consider the effects of entirely different volume distributions. Figure 2.3A shows the cumulative distribution function for our standard uniform distribution ($V = 0.008 – 2.3 \text{ km}^3 \text{ DRE}$), compared with four others: our standard with 100 (“hi-V”) high-volume runs added; our standard with 1,000 (“hi-V 10 percent”) high-volume runs added; a uniform distribution from 0.1 – 4 km$^3$ based on MSH tephra volume estimates in Carey and others (1995) and used in an analysis reported to DOE in 2017 (“Carey”); and a new, hypothetical distribution (“Hypo”). The hypothetical distribution was constructed by starting with the

Table 2.3. Effect of the addition of a small number of high-volume simulations on the tephra-fall thickness ($T_{10k}$), maximum airborne ash concentration ($C_{max,10k}$) and average airborne ash concentration ($C_{ave,10k}$) at Hanford, Washington, having an annual probability of one in 10,000.

| Number (%) of runs added | $R_{EFEV}$ yrs | $T_{10k}$, mm | $C_{max,10k}$ mg/m$^2$ | $C_{ave,10k}$ mg/m$^2$ |
|--------------------------|----------------|---------------|-------------------------|-------------------------|
| 0 (0%)                   | $\infty$       | 51.1          | 3819                    | 1513                    |
| 1 (0.01%)                | $1 \times 10^3$ | 51.1          | 3819                    | 1513                    |
| 10 (0.1%)                | $1 \times 10^5$ | 51.1          | 3856                    | 1529                    |
| 100 (1%)                 | $1 \times 10^8$ | 51.8          | 3849                    | 1568                    |
| 1,000 (9.3%)             | $1 \times 10^{-1}$ | 62.6          | 4071                    | 2083                    |

[Abbreviations: mg/m$^2$, milligram per cubic meter; mm, millimeter; yr, year; \%, percent; $\infty$, infinity]

Figure 2.2. Graphs showing volume and thickness of tephra deposits indicated by model runs. A. Cumulative volume distribution of the 1,000 large-volume model simulations. Blue dashed line depicts a volume of 2.3 cubic kilometers (km$^3$) dense-rock equivalent (DRE). Black dashed lines separate Volcanic Explosivity Index (VEI) 5, 6, and 7 eruption sizes, using bulk tephra volume as the defining quantity for these VEI ranges and assuming tephra and DRE densities of 1,000 and 2,500 kilograms per cubic meter (kg/m$^3$) respectively. The volumes are sampled from a distribution that is uniform on a log scale from 2.3 to 40 km$^3$ DRE. B. Tephra deposit thickness at Hanford, Washington, as a function of the run number, for the first 100 model runs. Model runs with exactly zero thickness ($T$) at Hanford are represented by red dots, while those with $T > 0.000$ millimeters (mm) are blue.
standard distribution but increasing the frequency of larger eruptions under the assumption that the volumes of older deposits are toward the larger end of the uncertainty range. In particular, we assumed: (1) that most (about 95 percent) Holocene eruptions in the stratigraphy are at least VEI 4 in size; (2) that about 1 percent of eruptions in this record are VEI 6 or greater; and (3) that among eruptions in the VEI 4–5 range, about two thirds will be VEI 4, based on global trends (table 2.2). The percentage of VEI 6 or greater eruptions in this distribution (1 percent) is 5 to 50 times greater than the percentage we estimated earlier, based on Cascade Range-wide large eruption frequencies. The hypothetical distribution includes volumes extending to 40 km$^3$ DRE. The probability density functions for these distributions are in figure 2.3 B–D.

For each of these distributions, we calculated values of $T_{10k}$, $C_{max,10k}$, and $C_{avg,10k}$ (table 2.4). Values based on the

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**Figure 2.3.** Graphs showing the cumulative distribution function and the probability distribution functions as a function of dense-rock equivalent (DRE) volume in cubic kilometers (km$^3$). A, Example cumulative distributions of DRE volume. Std (black line) is the standard distribution used in our analysis; hi-V (high volume, dashed red line) is the modification to the standard distribution, with 100 (1 percent) high-DRE-volume eruptions added (barely distinguishable from the Std curve); hi-V (10 percent; dotted red line) is the modification to the standard distribution, with 1,000 (10 percent) high-volume eruptions added; Carey (dashed magenta line) is the volume range of Holocene eruptions used in an earlier version of our analysis, based on Mount St. Helens Holocene volume estimates of Carey and others (1995); and Hypo (solid green line) is a hypothetical distribution as explained in the text. Alternating gray and white zones show the regions where erupted volumes match the ranges for Volcanic Explosivity Index (VEI) 3, 4, 5, and 6, when calculated by converting dense-rock equivalent volume to bulk volume using assumed densities of 1,000 kilograms per cubic meter (kg/m$^3$) for the deposit and 2,500 kg/m$^3$ for the magma. B–D Probability density function (pdf) versus DRE volume showing: B, this study’s standard distribution (with 1 percent and 10 percent hi-volume additions shown as a red dashed and red dotted lines, respectively); C, the volume distribution of Carey and others (1995); and D the hypothetical distribution illustrated in A.
Table 2.4. Values of tephra-fall thickness ($T_{10k}$), maximum airborne ash concentration ($C_{\text{max,10k}}$) and average airborne ash concentration ($C_{\text{avg,10k}}$) at Hanford, Washington, based on the distributions of eruptive volume given in figure 2.3.

[Abbreviations: mg/m$^3$, milligram per cubic meter; mm, millimeter]

| Distribution         | $T_{10k}$ mm | $C_{\text{max,10k}}$ mg/m$^3$ | $C_{\text{avg,10k}}$ mg/m$^3$ |
|----------------------|--------------|-------------------------------|-------------------------------|
| Standard             | 51.1         | 3,819                         | 1,513                         |
| Standard+100 large runs | 51.8         | 3,849                         | 1,568                         |
| Carey                | 105          | 7,387                         | 3,018                         |
| hypothetical         | 55.1         | 4,410                         | 2,148                         |

Carey and others (1995) DRE volume distributions were presented in a DOE meeting on October 2, 2017, and were based on about 10,000 additional simulations. Those for the hypothetical distribution were calculated by taking 3,000 of the about 11,000 runs (the original about 10,000 plus the 1,000 high-volume runs), to produce a population with the volume distribution shown.

The hypothetical distribution increases $T_{10k}$ about 8 percent relative to the standard distribution. $C_{\text{max,10k}}$ and $C_{\text{avg,10k}}$ are 15 percent and 42 percent higher, respectively, than the standard distribution. In summary, these new values are within a few tens of percent of the ones we reported. The Carey and others (1995) DRE volume distributions, which we think overestimates volumes, gives $T_{10k}$ roughly equal to the 100 mm value estimated by Hoblitt and Scott (2011), and concentration values about two times greater than our results using the standard distribution.

Conclusions

In the conclusions section of our original report, we characterized our results as order-of-magnitude estimates with large uncertainties. We also noted in the discussion section that these were “best estimates”, made with no intent to add conservatism. We have taken seriously the concern that our modeling did not consider a finite probability of an eruption larger than 2.3 km$^3$ DRE. In addressing this issue, we have shown (1) that there are no known eruptions from Mount St. Helens that are larger than 2.3 km$^3$ DRE; (2) that Cascades eruptive history suggests an annual probability of a larger eruption to be on the order of $10^{-5}$ or less; and (3) that when one adds larger eruptions to our dataset, using appropriate conditional probabilities, the calculated thickness and concentration at Hanford are still within a few tens of percent of our original calculations.
