Research Article

Effect of Limestone Powder on Thaumasite Form of Sulfate Attack (TSA) of Cement-Based Materials

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Received 28 May 2021; Accepted 29 July 2021; Published 6 August 2021

1. Introduction

In the natural environment, thaumasite is a rare six-sided crystalline mineral that mainly exists in metamorphic rocks and limestone [1, 2]. Thaumasite consists of silicate, carbonate, sulfate, and water. The thaumasite formation (TF) was first reported by Erlin and Stark in 1965 and was found in sewers, cement grouting layers, and road holes [3]. The formation of thaumasite is a complex process in multifactorial environments that includes temperature, humidity, the type of sulfate, the concentration of sulfate, the pH of the environment, the type of cementitious material, and the type of aggregates. The typical degradation caused by the formation of large amounts of thaumasite leads to the transformation of cement-based materials into grey pulp that loses its cementitious properties, known as the thaumasite form of sulfate attack (TSA) [4–6]. The TSA was found in a 30-year highway bridge in Gloucestershire, England, in the 1990s [7]; hence, thaumasite expert groups were established by the UK government [8]. After that, the research on thaumasite began to appear more frequently, and the first international conference on TSA was held in the UK in July 2002 [9].

Carbonate is a necessary ingredient of thaumasite. Thaumasite is generated and TSA is present when carbonate or bicarbonate is available, as well as when there is adequate moisture and a low temperature. The sources of carbonate are generally divided into internal and external sources, which generally come from cement itself, concrete aggregates, and additives, while external sources come from groundwater and CO₂ in the atmosphere [10]. A high content of limestone powder can greatly increase the risk of concrete corrosion from TSA [11–16], and carbonate and ettringite can obviously promote TSA [17]. At present, the limestone content of most cement is approximately 5%. Cement is clearly classified according to the content of limestone in the cement when the content of the limestone in the cement exceeds 5%. In Portland cement used throughout the world, the content of limestone is generally between 5% and 35%, while the most widely used Portland cement currently contains between 5% and 20% limestone, as defined in the adopted European standard CEM II/A [18]. The main purpose of adding limestone to cement is to reduce the amount of clinker in the cement, which can greatly reduce the energy and carbon emissions. Although the heavy use of
limestone reduces energy consumption, it also increases the risk of TSA in concrete, especially in large quantities [1–3].

The duration of TSA degradation is long, usually several years, which is not conducive to rapid development in the laboratory. Many studies by Luo et al. [19–21] and Zeng et al. [22] have indicated that an electrical field can accelerate the TSA of cement-based materials. Hence, the electrical field acceleration method can be utilized to study the effects of the limestone content on the TSA mechanism and process of cement-based materials within a short duration. The limestone powder will lead to TSA in sulfate attack environment, but the relationship between the content of limestone powder and the degree of TSA is unclear. Besides, the corrosion test is difficult to carry out in the laboratory due to the long time of TSA in the actual environment. Hence, the influence of six kinds of limestone powder content (0%, 5%, 10%, 15%, 30%, and 45%) on TSA of cement-based materials was studied by means of electric field acceleration method, and the influence degree and mechanism of limestone powder content on TSA were explored.

2. Materials and Methods

2.1. Preparation of the Basic Materials. The cement consists of 97% Portland cement clinker and 3% gypsum, and its specific surface area is 320 m²/kg. The limestone powder consists of more than 98% CaCO₃, and its specific surface area is 266 m²/kg. The chemical components of the clinker, gypsum, and limestone powder are shown in Table 1.

2.2. Experimental Methods. The cement pastes were made with different limestone powder contents of 0%, 5%, 10%, 15%, 30%, and 45%. The water/cementitious material ratio was 0.40 (shown in Table 2), and the size of the specimen was 40 mm × 40 mm × 40 mm. After 24 hours of moulding, the specimen was cured in a mould for 30 days and then placed in a low temperature environment with a temperature of 5 ± 2°C. The electrical voltages were 30 V, and the periods were 20 s. The mould and schematic diagram for electrification are shown in Figure 1. The cathode is a Na₂SO₄ solution, the anode is a MgSO₄ solution, and the concentrations of SO₄²⁻ are both 3.38 wt% [19–22].

The changes in the appearance of the specimen were observed, photographed, and recorded every 30 days, and the corrosion level was recorded according to Table 3 [20].

The microspecimens were created for XRD, FTIR, Raman, and chemical analyses. The specimens were sliced to the cathode surface and anode surface, and the thickness of the sliced specimen was 4 mm (shown in Figure 2).

The broken pieces were soaked and rinsed using anhydrous alcohol and dried at 50°C in the oven. The X-ray diffractometer was from Ricoh Company with D/MAX-III C and CoKα radiation (0.2 A). A Fourier transform infrared spectroscopy (FTIR) instrument with a resolution of 2.25px⁻¹ was adopted. Raman spectroscopic measurements were carried out using a HORIBA Jobin Yvon S.A.S spectrometer (product model: LabRAM HR Evolution; spectral resolution: visible spectrum ≤ 0.65 cm⁻¹; spectral region from 200 nm to 1050 nm).

The chemical analysis included the pH, content of SO₃, content of CaO. The content of sulfate in the powder specimens was expressed by the content of SO₃, which was based on the determination method of SO₃ in the Chinese standard method (GB/T 176-2017) [23], barium sulfate gravimetric method (reference method), expressed by %. The calcium content in the specimen was calculated by CaO, and the test was conducted in accordance with the EDTA titration method (reference method), the determination method of CaO in the Chinese standard method (GB/T 176-2017) [23], as %. The pH value of the specimens was determined by solid solution extraction.

3. Results and Discussion

3.1. Appearance of the Specimens. The apparent failure degree of the specimens at 120 days of degradation and the appearance of the specimens at 120 days of degradation were observed and recorded, as shown in Figures 3 and 4. The specimens were almost untouched by degradation within 120 days when the content of limestone was from 0% to 10%. The specimens began to show significant degradation when the content of the limestone powder was more than 10%, and the degradation degree was as follows: the content of 30% limestone powder > the content of 45% limestone powder > the content of 15% limestone powder. A small amount of grey pulp was found on the cathode edge of the 15% limestone powder specimen, the 30% limestone powder specimen was almost completely argillaceous, grey pulp was found only on the surface of the cathode of the 45% limestone powder specimen, and the appearance of the limestone powder specimen with less than 15% limestone powder hardly changed within 120 days, as shown in Figure 4.

3.2. Microstructure Analysis

3.2.1. The FTIR and Raman Spectroscopy. The author’s previous experiments [19–21] showed that TSA mainly occurs in the cathode region of the specimen; hence, the identification of thaumasite focuses on the cathode of samples. The microstructure specimens were obtained from the cathode surface of 6 groups and were tested by FTIR and Raman spectroscopy to identify the type of degradation products, as shown in Figure 5. The vibrational spectra and band assignment of thaumasite are shown in Table 4 [21].

The diffraction peak of thaumasite was the most significant when the content of limestone powder was 30%, followed by the 45% content of limestone powder. There was no obvious diffraction peak of thaumasite when the content of limestone powder was less than 15%. The degradation mechanism is herein analyzed by XRD and chemical analyses.

3.2.2. XRD Analysis. The XRD analysis of the 6 groups at 30 days is shown in Figure 6, in which specimens were cured for 30 days. The diffraction peak of ettringite is the highest when...
There were obvious diffraction peaks of ettringite and calcium hydroxide on the anode surface with 5% and 10% limestone powder, indicating that the degradation degree was low. The degradation products on the anode surface with 30% limestone powder content were still mainly thaumasite and gypsum. Almost no degradation products were found on the anode surface with 45% limestone powder content. The diffraction peaks of the main phases on the anode surface of the specimen were calcium carbonate.

To study the role of the limestone powder in cement-based material TSA, the XRD of the cathode surface and anode surface of 6 groups of specimens were tested, as shown in the following figures. The XRD pattern for the 0% content of limestone powder within 120 days is shown in Figure 8. The main phases of the cathode surface and anode surface of the specimen were ettringite, calcium hydroxide, and calcium carbonate. The diffraction peak of the ettringite had the highest diffraction intensity for the 0% limestone powder content. After being exposed to the electric field, the diffraction peak of ettringite gradually disappeared, and ettringite gradually began to form after 90 days of degradation. In addition, it can be observed that the diffraction peak of gypsum was obviously found within 30 to 90 days of degradation, while no diffraction peak of gypsum was found at 0 and 120 days. Meanwhile, the diffraction intensity of the diffraction peak of the calcium hydroxide was first weakened and then enhanced from 0 to 90 days. In the early stages of degradation, calcium hydroxide was consumed in large quantities to form gypsum, while ettringite decomposed, which also produced gypsum (reaction 1). Ettringite decomposition is caused by magnesium ions and hydrogen ions electrolyzed by the anode entering the specimen and lowering the pH value inside the specimen. A large amount of sulfates concentrated at the cathode of the specimen and began to regenerate ettringite with the development of degradation. In addition, diffraction peaks of calcium carbonate were found in the XRD patterns, indicating that the specimens were carbonized.

\[
3\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot 3\text{CaSO}_4 \cdot 32\text{H}_2\text{O} + 4\text{SO}_4^{2-} + 8\text{H}^+ \rightarrow 4\text{CaSO}_4 \cdot 2\text{H}_2\text{O} + 2\text{Al(OH)}_3 + 12\text{H}_2\text{O} \quad (1)
\]

Figure 9 shows the XRD pattern of the cathode surface and the anode surface of 5% limestone powder within 120 days. Combined with the above data, according to the FTIR and Raman results, ettringite and gypsum were the main degradation products with 5% limestone powder, and no thaumasite was found in the specimens. The diffraction intensity of ettringite hardly changed, while that of gypsum gradually increased with the development of the degradation age, and the diffraction intensity of the calcium hydroxide diffraction peak did not decrease significantly. The results showed that the degradation degree was still very low at 120 days. Compared with that of the 0% content of limestone powder, the ettringite did not decompose in the 5% content of limestone powder, indicating that the existence of

| Materials          | SiO₂ | Fe₂O₃ | Al₂O₃ | CaO  | MgO  | SO₃ | K₂O  | Na₂O | LOI  |
|--------------------|------|-------|-------|------|------|-----|------|------|------|
| Clinker            | 19.99| 2.98  | 4.80  | 61.22| 3.27 | 0.23| 0.88 | 0.18 | 3.52 |
| Gypsum             | 4.47 | 0.36  | 0.99  | 34.05| 1.84 | 40.61| 0.23 | 0.08 | 16.87|
| Limestone powder   | 0.23 | 0.21  | —     | 55.46| —    | —   | —    | 16.87| 41.75|

Table 1: Chemical components of the clinker, gypsum, and limestone powder (wt%).

| Cementitious materials (wt%) | Water/cementitious materials ratio |
|------------------------------|-----------------------------------|
| Cement                      | Limestone powder                 |
| 100                          | 0                                 | 0.40 |
| 95                           | 5                                 | 0.40 |
| 90                           | 10                                | 0.40 |
| 85                           | 15                                | 0.40 |
| 70                           | 30                                | 0.40 |
| 55                           | 45                                | 0.40 |

Table 2: Mixture proportions of the cement paste.
Table 3: Corrosion damage grade of TSA [20].

| Damage grades | Corrosion features                                      |
|---------------|----------------------------------------------------------|
| 1             | No visible deterioration                                  |
| 2             | Some deterioration at corners                            |
| 3             | Deterioration at the corners and edges                   |
| 4             | Deterioration at the corners and some cracking along the edges |
| 5             | Cracking and expansion along the edges                    |
| 6             | Serious cracking, expansion, or spalling                  |
| 7             | Serious spalling or expansion of surfaces                 |
| 8             | Grey pulp at the corners, edges, and surface             |
| 9             | Amount of grey pulp at the specimens                     |
| 10            | Complete damage                                          |

Figure 1: Mould and schematic diagram for electrification.

Figure 2: Sliced specimen.

Figure 3: Appearance change grade of different limestone powder contents within 120 days.
limestone powder can stabilize the ettringite because the nucleation effect of limestone powder can stabilize the formation of ettringite. It was difficult to find the presence of gypsum in the positive extreme of the specimen when the dosage of limestone was 5%.

Figure 10 shows the XRD of the cathode surface and the anode surface of specimens with 10% limestone powder within 120 days. Combined with the above data, according to the FTIR and Raman results, ettringite and gypsum were the main degradation products with 10% limestone powder, and no thaumasite was found in the specimens. The changes in ettringite and gypsum were not obvious within 120 days, and the changes in calcium hydroxide were also not obvious. After 120 days of electric field action, no serious sulfate attack occurred in the specimen. Limestone powder could promote the formation of ettringite, the limestone powder...
content reached 10%, and it could simultaneously promote the formation of ettringite and gypsum.

Figure 11 shows the XRD pattern of the cathode surface and the anode surface of 15% limestone powder within 120 days. Combined with the above data, according to the FTIR and Raman results, ettringite and gypsum were the main degradation products with 15% limestone powder, and no thaumasite was found in the specimens. However, as seen from the appearance of the specimen after 120 days of degradation, a small amount of grey pulp was found in the corner cracks of the specimen, indicating that it would be capable of producing thaumasite under a longer degradation period in the future. On the surface of the cathode of the specimen, with the development of the degradation age, the diffraction intensity of the ettringite and gypsum diffraction peaks increased in the specimen, especially between 90 days and 120 days, and the gypsum diffraction peak significantly increased, indicating that a large amount of gypsum was generated on the surface of the cathode of the specimen. In addition, it was observed that the diffraction intensity of the calcium hydroxide diffraction peak on the surface of the cathode decreased gradually with the increase in the degradation age, indicating that the degradation degree occurred deeper in the specimen as time continued. Ettringite and gypsum could still be found on the anode surface of the specimen, but their diffraction intensity was significantly lower than that of calcium hydroxide.

Figure 12 shows the XRD of the cathode surface and the anode surface of 30% limestone powder within 120 days. Combining the above FTIR and Raman data, there were very serious TSAs in the specimen. The limestone powder content reached 30%, and the specimen anode and the cathode surface had obvious diffraction peaks of thaumasite. Combined with the limestone powder content from 0% to 15% in this paper, according to the data on the limestone powder content, the higher the content is, the more accelerated the sulfate attack of the cement base material is; first, ettringite is stabilized, the formation of gypsum speeds second, and finally, the generation of thaumasite is accelerated.

Figure 13 shows the XRD of the cathode surface and the anode surface of 45% limestone powder within 120 days. Combining the above FTIR and Raman data, little thaumasite was found, and the degradation degree was not urgent for a limestone powder dosage of 30%. The diffraction peaks of ettringite and gypsum were found on the surface of the cathode after 60 days. In addition, the formation of new products, monocarboaluminate and tricarboaluminate, was found. The limestone powder could react with C3A to produce hydrated calcium carboaluminate. The monocarboaluminate was more stable than the other products, and the TSA was slow. The formation of ettringite and hydrated calcium carboaluminate both consumed C3A, ettringite and gypsum were hardly found on the cathode surface at 60 days, and little ettringite was found at 90 days, indicating that the formation of hydrated calcium carboaluminate delayed the ettringite and gypsum formation and that the formation of ettringite and gypsum was closely related to thaumasite; thus the generation of thaumasite was delayed. No degradation products were found on the anode surface, and the main products were calcium hydroxide and calcium carbonate.

3.2.3. Chemical Analysis. The changes in the pH value and the SO₃ and CaO contents on the cathode surface of the 6 groups were tested at 0 days and 120 days. The results are shown in the following figures. The change in the pH value is shown in Figure 14. The higher the content of limestone powder is, the lower the pH value of the cathode surface is. The decrease range is small, and the effect is not obvious when the dosage of limestone powder is less than 10%. However, when the content of limestone powder exceeds 15%, the pH value of the cathode surface begins to drop sharply. For the control group, due to the increase in the content of limestone powder, the cement content is relatively reduced, so the content of the hydration product calcium hydroxide is also reduced; hence, the pH value in the sample will gradually decrease, but the decrease range is smaller than that for the other groups. The pH value drops sharply when the dosage of limestone exceeds 15%, and the higher
the dosage of limestone, the greater the decline when the specimen is corroded. The more the pH value decreases, the more the degradation occurs. The pH value of the cathode surface of the limestone powder group containing 45% is reduced to approximately 10 at 120 days, and the formation of thaumasite is closely related to the pH value of the sulfate. In addition, a high concentration of sulfate and high alkalinity can accelerate TSA in concrete [11, 24, 25]. Gaze and Crammond [4] reported that thaumasite is not formed at a pH of less than 10.5, and when the pH is lower than 10.5, thaumasite is formed into calcite [26]. Hobbs and Taylor believed that a pH of 12.5 was a necessary condition for the formation of thaumasite [27]. Experiments in [27] have studied the chemical reactions of thaumasite with different solutions: the reactions of thaumasite with phosphate, carbonate, and bicarbonate decrease with increasing pH. When the pH value is greater than 12.45, thaumasite is more stable than when the pH value is less than 12.45. These studies show that the formation process and TSA cannot occur in an acidic environment, while gypsum is mainly formed in a low pH environment because gypsum is more stable in a low pH environment. Therefore, it can be seen from the results of the pH value of the cathode surface of the specimen that an excessively low pH value causes the thaumasite to decompose.

The change in the content of SO$_3$ is shown in Figure 5. There was no significant difference in the amount of sulfates transferred into the samples with limestone powder contents.
Figure 9: XRD pattern of 5% limestone powder content within 120 days. (a) Cathode surface and (b) anode surface.

Figure 10: XRD pattern of 10% limestone powder content within 120 days. (a) Cathode surface and (b) anode surface.

Figure 11: XRD pattern of 15% limestone powder content within 120 days. (a) Cathode surface and (b) anode surface.
of 0%, 5%, and 10%, and the amount transferred into the samples was also very small. However, the content of sulfate migrated into the cement sample increased sharply when the content of limestone powder exceeded 15%, and the higher the content of limestone powder was, the more the sulfate migrated into the sample. The increase in the content of limestone powder correspondingly reduced the content of cement, hydration products, and C-S-H gel, which reduced the compactness of the specimen, facilitating sulfate migration into the specimen. In addition, the nucleation effect of limestone powder participated in generating thaumasite and was advantageous to the cement base material of the sulfate attack, which resulted in cracking of the specimen for further expansion and loosening, resulting in a growing amount of sulfate into the specimen during the reaction; thus, the degradation of the sample was more severe.

The change in the content of CaO is shown in Figure 16. The CaO content and the change rule of the specimen were similar with pH and SO₃ content change, the same is within 10% limestone powder content, the inside of the specimen CaO content difference is small, and when the limestone powder content exceeds 15%, the decalcification of the cathode region becomes more pronounced, especially when limestone powder content is 45%.

The addition of limestone powder can promote the sulfate attack of cement-based materials due to the stabilization of the ettringite; it can also promote a very large formation of gypsum. The limestone powder content is 5%....
and 10%, compared with the 0% limestone powder content. The above XRD data show that the specimen generated a large amount of ettringite and gypsum. Combined with the above data, the limestone powder content is within 10%, and the pH change and SO$_3$ content of the cathode surface show little change. The dosages of 5% and 10% limestone powder do not accelerate more sulfate into the specimen, and the specimens still generate a large amount of gypsum and ettringite, indicating that the limestone powder has a promoting effect on sulfate attack. The sulfate attack of cement-based materials by limestone powder begins to change qualitatively when the content of limestone exceeds 10%. The chemical reaction is accelerated, and the replacement of limestone powder reduces the density and stability of the cement-based materials, which is mainly manifested in reducing the pH value of cement-based materials, speeding up the process of sulfate attack and experiencing severe TSA. The pH of cement-based materials is too low when the content of limestone powder is 45%, which leads to the degradation products being decomposed (except the gypsum). In addition, more limestone powder also reacts with C$_3$A to generate hydrated calcium carboaluminate, which can delay the TSA.

4. Conclusions

This paper studies the effects of different contents of limestone powder on the TSA in cement-based materials for studying the influence degree and mechanism of limestone powder content on TSA; the limestone powder contents are 0%, 5%, 10%, 15%, 30%, and 45%. The degradation process and mechanism were analyzed by appearance, FTIR, Raman, XRD analysis, and chemical analysis.

It can be clearly found that although limestone powder can lead to serious TSA of cement-based materials, the degree of corrosion is closely related to the content of limestone powder, and the degree of corrosion is not completely linear with the content of limestone powder. The effect of limestone powder on the sulfate attack of cement-based materials is low, and it will not cause obvious sulfate attack when the content of limestone powder is no more than 10%. Limestone powder can cause severe TSA when the content of limestone powder is 15%–30%. TSA actually decreased when the content of limestone powder is 45% because the more limestone powder also reacts with C$_3$A to generate hydrated calcium carboaluminate, which can delay the TSA. The details results are discussed as follows:

1. There was no obvious sulfate attack when the content of limestone powder was not more than 10%. However, the 5% content of limestone powder can stabilize the ettringite, and the 10% content of
limestone powder can promote the formation of gypsum.

(2) The sulfate attack was obviously accelerated when the content of limestone powder was more than 15%, especially when the TSA was obviously accelerated when the content of limestone powder was 30%.

(3) There were new products in which mono-carboaluminate and tricarboaluminate were found when the content of limestone powder was 45%, and the degradation of TSA was also delayed when compared with a limestone powder content of 30%.

(4) The limestone powder can lead to a rapid decrease in the pH and the content of CaO and a rapid increase in the content of SO₃ when the content of limestone powder is more than 10%, which accelerates the sulfate attack. The excessive limestone powder content, in which the content of limestone powder is 45%, leads to the pH being excessively low and is a disadvantage for the degradation products.

Data Availability

The data used to support the findings of this study are included within the article.

Conflicts of Interest

There are no conflicts of interest.

Acknowledgments

The authors want to acknowledge the financial support of the China West Construction Group Co., Ltd., Science and Technology Research and Development Foundation (nos. ZJXJ-2019-12 and ZJXJ-2019-13) and the National Natural Science Foundation of China (no. 51772033).

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