Indoor Tracking by Adding IMU and UWB using Unscented Kalman Filter

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Indoor Tracking by Adding IMU and UWB using Unscented Kalman Filter

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Abstract

In recent days Internet of Things (IoT) applications becoming prominent, like smart home, connected health, smart farming, smart retail and smart manufacturing, will lead to a challenging task in providing low cost, high precision localization and tracking in indoor environments. Positioning in indoor is yet an open issue mostly because of not receiving the signals of GPS in the context of indoor. Inertial Measurement Unit (IMU) can give an exact indoor tracking, however, they regularly experience the cumulated error as the speed and position are gotten by incorporating the increasing acceleration constantly as for time. At the same time Ultra Wideband (UWB) localization and tracking will be influenced by the real time indoor conditions. It is difficult to utilize an independent localization and tracking system to accomplish high precision in indoor conditions. In this paper, we come up with an incorporated positioning system in indoor by joining IMU and the UWB over the Unscented Kalman Filter (UKF) and the Extended Kalman Filter (EKF) to enhance the precision. All these algorithms are analyzed and assessed dependent on their exhibition.

Key Words Extended Kalman Filter, Indoor positioning, IoT, Ultra Wideband, IMU, Unscented Kalman Filter

1 Introduction

High-precision and low-cost localization and navigating systems for indoor portable devices have gotten basic in IoT applications, like smart home and smart manufacturing [1]. As of late, real-time location systems (RTLS) are being utilized for stock administration and security uphold in manufacturing plants and circulation focuses. It is vital in RTLS to appraise the position of moving articles, for example, forklifts and laborers along with the fixed bodies. To evaluate the position of movable items, an exceptionally fast and exact algorithm is needed.

The precise and strong indoor position is a major facilitator in forthcoming Internet applications. Inertial navigation is a technique utilizing the estimation from the IMU, primarily, gyroscopes and accelerometers for positioning and navigation. Utilizing the estimation given by the IMU, the Inertial Navigation System (INS) can enumerate the velocity, position and the direction of the system beginning from some known starting point. In any case, because of their drawn out floats, for example, accelerometer inclination and scale factor mistakes, from the calculated states of navigation (position, velocity, and attitude) will gain with time.

For indoor 3D human tracking, there are many technological hurdles to overcome because of the complexity of indoor conditions [2, 3]. The influence of obstacles like walls, equipment, furniture, the existence of people etc. leads to fading and multi path issues. There are individual technologies which are used in wireless network, for example, Bluetooth, Wi-Fi, UWB and ZigBee. The better appropriate innovation for large precision localization is UWB.

Ultra-Wideband is a radio innovation, which is essentially different in relation to the at present generally utilized conventional radio technologies. It transmits signals over various groups of frequencies (3.1 GHz to 10.6 GHz) all the while with hundreds MHz of transmission capacity (more prominent than 500 MHz). It is intended for Indoor Positioning Systems (IPSs) to conquer numerous difficulties, for example, signals because of extreme multi path reflect from furniture and wall, Non-Line-of-Sight (NLOS) signal because of blockages, and scattering of signal because of more prominent thickness of obstacles. With the known positions of reference nodes, by estimating the Time-of-Arrival (TOA) between the target node and each of the receivers, reference nodes, and their relating distances can be calculated. By using calculated distances, the location of the target can be estimated utilizing various methods of positioning [3-7]. Since 2010, localization devices based on UWB radio sensor, like Pozyx from Kickstarter and DWM1000 from DecaWave [8], have gotten industrially accessible. At present, a few IPSs like the Ubisense System and Zebra System, utilizing UWB radio sensor have been conveyed [9-10].
In spite of the fact that UWB has been recognized as perfect radio technology in indoor scenario for getting accurate data about the location, still there is a challenge for the IPS based on UWB technology to predict precise location data because of the multi path propagation of the direct LOS signal and propagation of the NLOS signal. To defeat the multi path impacts, a simple method is to eliminate the obstructions that may cause those inferences or to consider the open zone. This choice may not be conceivable in most indoor situations. IMU-based INSs are obtuse toward these interference but the errors resulted from the estimated position will increase over time. So these two technologies, IMU and UWB can be coupled for applications of IPS because these two technologies are corresponding to one another. IMU estimation is introduced. We will get high exactness with TDOA on account of the enormous transmission capacity of UWB signals, however, its application is compelled by the corresponded measurement noise because of TDOA values. A multi-sensor combination design is presented in [15] for the IPS. At the point when UWB is accessible and reliable, the long-term drift error of IMU is aligned by UWB. Something else, the system will change from UWB to IMU promptly to obtain the status of positioning and navigation. In [16], a combined localizing solution of UWB and IMU is presented, which can give continuous and reliable position, particularly on account of NLOS situations. But, in [16], regarding the time synchronization issue, all the UWB modules are associated with a central regulator through the fibre line. This will build the complexity of the deployment and the expense of the system.

TOA algorithm is used in both [15] and [16] and have not taken the clock drift impact into account. Besides, despite the fact that noise of acceleration from IMU is considered in the measurements of acceleration, the impact of acceleration noise on the displacement and velocity because of incorporation is not evaluated in [15, 16].

In [17], a tracking and positioning algorithm coupling IMU, UWB and sensors specific to an area is proposed. It is indicated that the combination algorithm can acquire more precise three-dimensional velocity and information of height by utilizing the lower body biomechanical model. Note that large portion of the current indoor navigation and positioning systems are depended on human lower body MOCAP frameworks [18], which expands the expense and difficulty in deployment. Hence, to accomplish less price and high precision of the indoor navigation and positioning system, this paper centers on the coupling of IMU and UWB dependent on Kalman Filter (KF) calculations. The information received by IMU is utilized for the equation of state, while the information received by UWB is utilized for the equation of observation in KF calculations. To improve further the accuracy of indoor positioning, the nonlinear kalman filter, namely, UKF algorithm is considered in this paper.

The main contributions of this paper can be summarized as follows:

Positioning with UWB using the Iterative method compared with linear least squares method using TOA values for two different configurations of reference node placement. An UKF fusion positioning algorithm introduced to decrease the computational complexity and to get better accuracy compared with EKF. From the results of simulation, we can conclude that the UKF fusion algorithm can obtain better accuracy of position compared to EKF fusion positioning algorithm in a three-dimensional area. The effect of the number of reference nodes or reference nodes density is also performed for all the algorithms.

In Section II, Indoor positioning System using IMU is explained first and then positioning using UWB, which uses TOA values as range measurements and Iterative Method for position estimation is explained. In Section III, the calculations dependent on coupling IMU and UWB positioning system is introduced in environment of 3D. In Section IV, simulation results are given and positioning performances of all algorithms are analyzed and explained. Conclusions are given in Section V.

2 Positioning and Tracking System Using the coupling of IMU and UWB

The proposed positioning and tracking system by coupling sensor based IMU and UWB localizing system in indoor environment of three dimension is given in Fig. 1. Here the three axis(x, y, and z) accelerometers, one UWB radio sensor (given as Target sensor) are placed on the body of a platform, and four UWB radio sensors (given as reference sensors) are placed inside the building with known locations.
2.1 Positioning algorithm using IMU

To change the coordinates from one set to another, we need a rotation matrix that reveals to us precisely how one frame is rotated with respect to the other. Rotations are especially precarious mathematical objects and they can be the source of significant bugs if not managed cautiously and determinedly. There is a wide range of approaches to represent rotations [19].

The best method of representing a rotation is utilizing the euler angles. These angles represent an arbitrary rotation as the creation of three separate rotations about different principal axes. Euler angles are attractive in part because they are a parsimonious representation, requiring only three parameters instead of nine for a full rotation matrix, and it is easier to understand than another way of quaternion method and no need to calculate quaternion multiplication.

C1, C2, and C3 are the Euler angles about x, y, and z axis respectively, given as shown below.

\[
C_1 = \begin{bmatrix}
1 & 0 & 0 \\
0 & \cos \theta_1 & \sin \theta_1 \\
0 & -\sin \theta_1 & \cos \theta_1
\end{bmatrix},
\]

\[
C_2 = \begin{bmatrix}
\cos \theta_2 & 0 & -\sin \theta_2 \\
0 & 1 & 0 \\
\sin \theta_2 & 0 & \cos \theta_2
\end{bmatrix},
\]

\[
C_3 = \begin{bmatrix}
\cos \theta_3 & \sin \theta_3 & 0 \\
-\sin \theta_3 & \cos \theta_3 & 0 \\
0 & 0 & 1
\end{bmatrix},
\]

And

\[
C = C_3 \times C_2 \times C_1
\]  

By considering rotations with infinite, then the functions of trigonometry approximate as \( \sin (\theta) \approx \theta \) and \( \cos (\theta) \approx 1 \). Using these approximations, C can be written in terms of angular velocity as shown in (2).

\[
C \approx \begin{bmatrix}
1 & 0 & 0 \\
0 & 1 - \theta_1 & -\theta_1 \theta_2 \\
0 & \theta_1 & 1 - \theta_3 \theta_2
\end{bmatrix} \begin{bmatrix}
1 & 0 & \theta_2 \\
0 & 1 & 0 \\
\theta_2 & 0 & 1
\end{bmatrix} \begin{bmatrix}
1 - \theta_3 & 0 \\
\theta_3 & 1 \\
0 & 0 & 1
\end{bmatrix}
\]

\[
a, \text{ the accelerometers of the three axis are used to calculate the acceleration in system A as follows}
\]
\[
\mathbf{a} = \begin{bmatrix} a_x & a_y & a_z \end{bmatrix}^T
\]

Then, the acceleration in system B, \( \mathbf{a}^b \), can be calculated using the rotation matrix as follows

\[
\mathbf{a}^b = \begin{bmatrix} a_x^b & a_y^b & a_z^b \end{bmatrix}^T = \mathbf{C} \times \mathbf{a}
\]

If we consider the acceleration gravity \( g \), then the acceleration in system B can be calculated by subtracting it from its value as follows

\[
\mathbf{a}^b = \begin{bmatrix} a_x^b \\ a_y^b \\ a_z^b \end{bmatrix} = \begin{bmatrix} a_x^b \\ a_y^b \\ a_z^b \end{bmatrix} - \begin{bmatrix} 0 \\ 0 \\ g \end{bmatrix}
\]

If we consider the sampling interval is short, then constant force is subjected to the carrier with a linear motion of uniform acceleration. Let the position of the system B be \( \mathbf{x}^b \), can be calculated as follows

\[
\begin{bmatrix}
x_x^{b(t+1)} \\
x_y^{b(t+1)} \\
x_z^{b(t+1)}
\end{bmatrix} = \begin{bmatrix}
x_x^{b(t)} \\
x_y^{b(t)} \\
x_z^{b(t)}
\end{bmatrix} + \begin{bmatrix}
v_x^{b(t)} \\
v_y^{b(t)} \\
v_z^{b(t)}
\end{bmatrix} (\Delta t) + \frac{1}{2} \begin{bmatrix}
a_x^{b(t)} \\
a_y^{b(t)} \\
a_z^{b(t)}
\end{bmatrix} (\Delta t)^2
\]

Where \( x^b(t) \), \( v^b(t) \), and \( a^b(t) \) be the position, velocity and the acceleration of the system at time \( t \), \( x^b(t+1) \) be the position of system B at time \( (t+1) \), \( (\Delta t) \) be the sampling interval.

### 2.2 Position processing algorithm using UWB

UWB positioning of an unknown target node can be made by using fixed known locations of reference nodes. For a 3D environment a minimum of four reference nodes will be enough for positioning. Positioning of the target node can be performed in two steps. First one is measuring the signal parameters either time difference of arrival (TDOA) or time of arrival (TOA) or direction of arrival (DOA) or received signal strength (RSS), of the transmitted signal from reference nodes utilized as range values for target positioning. Second step, using range values, the location of the target can be calculated. The most applicable one for the UWB system is TOA as this takes the advantage of a huge time resolution of UWB signals [20]

#### 2.2.1 TOA Estimation Algorithms

Measuring the TOA values is difficult due to the high dispersive nature of UWB channels. Always the first arrival path need not be the strongest path. Hence, there is a need for precise ranging and less complicated techniques at achievable sampling rates. The Fig.2 shows the method for the calculation of TOA values. Here the TOA estimation is done utilizing the samples \( z[n] \), which are taken after the square-law device.

![Fig. 2. Energy samples of the received signal](image)
Fig. 3. TOA estimation algorithms using the samples of energy

The algorithms for TOA calculation using the samples of energy received after a square law device, summarized in Fig.3. Maximum Energy Selection, where the sample output with maximum energy is selected as the first path. But in indoors due to multi path it is not necessary that the maximum energy sample is the direct path between the target and reference node. Next one is Threshold Comparison, where the sample first exceeds the threshold can be calculated as TOA value. This method performance is poor at lower SNR’s because there may be more threshold crossings due to the noise addition. The next suitable technique is Maximum energy Selection Search Back, where the window of search-back from a maximum energy selection sample given by $w$ assigned using the measurements of the channel. It performs best among the above mentioned techniques. The equation for calculating TOA value using Maximum energy Selection Search Back is given by

$$t_{MES-SB} = \left[ \min \{Z[n] > \xi\} - 0.5 + n_{max} - w_{sb}\right] T_b$$  \hfill (7)

where

$$Z[n] = \{z[n_{max} - w_{sb}], z[n_{max} - w_{sb} + 1], \ldots, z[n_{max}]\}$$

2.2.2 Position Estimation

Position of the target node can be calculated by using well known triangulation/trilateration (2D) or multilateration for higher dimensions by two ways. One is nonlinear equations obtained directly from the nonlinear relationships between target and the range measurement like maximum likelihood (ML) and nonlinear least squares (NLS) algorithms. Another way is converting these equations into linear like, weighted linear least squares (WLLS) and linear least squares (LLS) algorithms. But in triangulation/trilateration the three circles with radius as the measured distance between a reference sensor and the target sensor using TOA values may not converge to a single point thereby the performance of the system decreases. If we consider three dimensions where we require four reference nodes, this convergence issue still extends and degrades the performance. So another method called Iterative method with Hessain function is used.

The function for optimization method is

$$f(x) = \sum_{i=1}^{N} \left[ \left( (p - p_i)^2 + (q - q_i)^2 + (r - r_i)^2 \right)^{1/2} - c(t_i - t_m)^2 \right]^2$$  \hfill (8)

where,

$$x = [p, q, r, t_m]^T$$ be the position to calculate

$$t_i, t_m$$ be the $i^{th}$ reference sensor received time and target sensor transmitted time

To calculate the location of the target sensor the following iterative equation is used.

$$x_{k+1} = x_k - \delta B_k s_k$$  \hfill (9)

Where,

$$s_k$$ be the objective function

$$s_k = \Delta f(p, q, r, t_m) = \begin{bmatrix} \frac{\partial f}{\partial p} & \frac{\partial f}{\partial q} & \frac{\partial f}{\partial r} & \frac{\partial f}{\partial t_m} \end{bmatrix}_p = p_{nk}$$

$$B_k$$ is the Hessain function increased by utilizing below equation

$$B_{k+1} = B_k + \frac{h_k h_k^T}{\|h_k q_k\|^2} - \frac{B_k q_k q_k^T B_k}{q_k^T B_k q_k}$$  \hfill (10)

where, 

$$h_k$$ be the vector of partial derivatives

$$h_k^T$$ be the transpose of vector of partial derivatives

$$q_k$$ be the search-back sample

$$q_k^T$$ be the transpose of the search-back sample
The mean of known reference nodes is taken as the initial estimate and the Identity matrix (I) as the hessian grid beginning.

3. Algorithm based on IMU and UWB

To beat the individual deficiencies of the UWB and IMU, we execute an UKF that couple the two positioning systems so that the UWB sensor based result of position is used to change the IMU mistakes and the IMU sensor based result of position solution is used to distinguish and isolate the adjusted UWB sensor data to build the general precision of positioning performance. Here, we present the coupling algorithm using EKF first, then the coupling algorithm using UKF.

3.1 EKF algorithm

Here we are considering a plane of three -dimensions target moving with uniform acceleration. The vector of state at time $k$, is given by

$$
\mathbf{x}(k) = \begin{bmatrix} x_s(k) & x_v(k) & x_a(k) & v_s(k) & v_v(k) & v_a(k) & a_s(k) & a_v(k) \end{bmatrix}
$$

(11)

Here, $x_s$, $v_s$, and $a_s$ are the position, velocity, and acceleration respectively.

Let $(\Delta t)$ be the sample interval and $(\Delta t)w(k)$ is the process noise of acceleration. Then $\frac{(\Delta t)^2}{2}w(k)$ represents the process noise of velocity and $\frac{(\Delta t)^3}{6}w(k)$ represents the process noise of position, because of integrating acceleration two times. The velocity and acceleration values can be obtained from IMU.

The equation of state at time $(k+1)$ with uniform acceleration motion is given in (12)

$$
x_s(k+1) = x_s(k) + v_s(k)(\Delta t) + \frac{1}{2}a_s(k)(\Delta t)^2 + \frac{1}{6}w_s(k)
$$

$$
x_v(k+1) = x_v(k) + v_v(k)(\Delta t) + \frac{1}{2}a_v(k)(\Delta t)^2 + \frac{1}{6}w_v(k)
$$

$$
x_a(k+1) = x_a(k) + v_a(k)(\Delta t) + \frac{1}{2}a_a(k)(\Delta t)^2 + \frac{1}{6}w_a(k)
$$

$$
v_s(k+1) = v_s(k) + a_s(k)(\Delta t) + \frac{1}{2}w_s(k)
$$

$$
v_v(k+1) = v_v(k) + a_v(k)(\Delta t) + \frac{1}{2}w_v(k)
$$

$$
v_a(k+1) = v_a(k) + a_a(k)(\Delta t) + \frac{1}{2}w_a(k)
$$

$$
a_s(k+1) = a_s(k) + (\Delta t)w_s(k)
$$

$$
a_v(k+1) = a_v(k) + (\Delta t)w_v(k)
$$

$$
a_a(k+1) = a_a(k) + (\Delta t)w_a(k)
$$

(12)

The matrix form of the state equation written as

$$
\mathbf{x}(k+1) = F\mathbf{x}(k) + Gw(k)
$$

(13)

Where $F$ represents the transition matrix of state,

$G$ represents the driving matrix of noise.

The process noise vector with zero mean and covariance matrix $Q$ is given by

$$
w(k) = \begin{bmatrix} w_x(k) & w_y(k) & w_z(k) \end{bmatrix}^T
$$

And

$$
Q = diag\left(\sigma_{x}^2 \sigma_{y}^2 \sigma_{z}^2 \right)
$$
Let the observation vector be \( Z(k) \), including the correct distance from reference sensor to target sensor \( d_i(k) \) and the observation noise \( n_i(k) \).

The equation of observation matrix including the range between the target sensor, four reference sensors and the angle between target sensor to four reference sensors is expressed as

\[
F = \begin{bmatrix}
1 & 0 & 0 & (\Delta t) & 0 & 0 & \frac{(\Delta t)^2}{2} & 0 & 0 \\
0 & 1 & 0 & 0 & (\Delta t) & 0 & 0 & \frac{(\Delta t)^2}{2} & 0 \\
0 & 0 & 1 & 0 & 0 & (\Delta t) & 0 & 0 & \frac{(\Delta t)^2}{2} \\
0 & 0 & 0 & 1 & 0 & 0 & (\Delta t) & 0 & 0 \\
0 & 0 & 0 & 0 & 1 & 0 & 0 & (\Delta t) & 0 \\
0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & (\Delta t) \\
0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\
0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1
\end{bmatrix}
\]

And

\[
G = \begin{bmatrix}
\frac{(\Delta t)^3}{6} & 0 & 0 \\
0 & \frac{(\Delta t)^3}{6} & 0 \\
0 & 0 & \frac{(\Delta t)^3}{6} \\
\frac{(\Delta t)^2}{2} & 0 & 0 \\
0 & \frac{(\Delta t)^2}{2} & 0 \\
0 & 0 & \frac{(\Delta t)^2}{2} \\
(\Delta t) & 0 & 0 \\
0 & (\Delta t) & 0 \\
0 & 0 & (\Delta t)
\end{bmatrix}
\]

\[
z(k) = \begin{bmatrix}
d_1(k) + n_1(k) \\
d_2(k) + n_2(k) \\
d_3(k) + n_3(k) \\
d_4(k) + n_4(k) \\
\phi_1(k) + n_5(k) \\
\phi_2(k) + n_6(k) \\
\phi_3(k) + n_7(k) \\
\phi_4(k) + n_8(k)
\end{bmatrix} = H(k) x(k) + n(k)
\]

Here at time \( k' \), \( H(k) \) denotes the observation matrix

And \( n(k) \) represents the vector of noise having mean with zero and covariance of the matrix as

\[
R = diag\left(\sigma_1^2, \sigma_2^2, \sigma_3^2, \sigma_4^2, \sigma_5^2, \sigma_6^2, \sigma_7^2, \sigma_8^2\right)
\]

The equations of true distances are given as

\[
R = diag\left(\sigma_1^2, \sigma_2^2, \sigma_3^2, \sigma_4^2, \sigma_5^2, \sigma_6^2, \sigma_7^2, \sigma_8^2\right)
\]
And equations of true angle are given by

$$\phi_i(k) = \arccos \left( \frac{x(k) \cdot \overline{x}_i}{|x(k)| |\overline{x}_i|} \right) \text{ for } i = 1, 2, 3, 4$$

(16)

Where

$$\left( x(k) \cdot \overline{x}_i \right) = x_i^x x_k^x + x_i^y x_k^y + x_i^z x_k^z$$

be the dot product of two vectors namely the position of reference sensor and the position of target sensor for \( i = 1 \).

And

$$|x(k)| = \sqrt{x_k^x^2 + x_k^y^2 + x_k^z^2}$$

(17)

$$|\overline{x}_i| = \sqrt{x_i^x^2 + y_i^y^2 + z_i^z^2} \text{ for } i = 1, 2, 3, 4$$

(18)

The above nonlinear equations require linearization, so the EKF algorithm is used with Taylor expansion of first order.

\( H(k) \), the matrix of Jacobian is given as in (19).

Here in EKF we are calculating the matrix of Jacobian, which increases the algorithm’s complexity of computation. If the assumption of linearization is not correct, then algorithm of EKF performance will diverge and degrade. Algorithm 1 gives the EKF algorithm process step by step.

$$H(k) = \begin{bmatrix}
\frac{\partial d_1(k)}{\partial x_i(k)} & \frac{\partial d_1(k)}{\partial y_i(k)} & \frac{\partial d_1(k)}{\partial z_i(k)} \\
\frac{\partial d_2(k)}{\partial x_i(k)} & \frac{\partial d_2(k)}{\partial y_i(k)} & \frac{\partial d_2(k)}{\partial z_i(k)} \\
\frac{\partial d_3(k)}{\partial x_i(k)} & \frac{\partial d_3(k)}{\partial y_i(k)} & \frac{\partial d_3(k)}{\partial z_i(k)} \\
\frac{\partial d_4(k)}{\partial x_i(k)} & \frac{\partial d_4(k)}{\partial y_i(k)} & \frac{\partial d_4(k)}{\partial z_i(k)} \\
\frac{\partial \phi_1(k)}{\partial x_i(k)} & \frac{\partial \phi_1(k)}{\partial y_i(k)} & \frac{\partial \phi_1(k)}{\partial z_i(k)} \\
\frac{\partial \phi_2(k)}{\partial x_i(k)} & \frac{\partial \phi_2(k)}{\partial y_i(k)} & \frac{\partial \phi_2(k)}{\partial z_i(k)} \\
\frac{\partial \phi_3(k)}{\partial x_i(k)} & \frac{\partial \phi_3(k)}{\partial y_i(k)} & \frac{\partial \phi_3(k)}{\partial z_i(k)} \\
\frac{\partial \phi_4(k)}{\partial x_i(k)} & \frac{\partial \phi_4(k)}{\partial y_i(k)} & \frac{\partial \phi_4(k)}{\partial z_i(k)}
\end{bmatrix}$$

(19)

Where,

$$\frac{\partial d_1(k)}{\partial x_i(k)} = \frac{x_i(k) - x_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial d_1(k)}{\partial y_i(k)} = \frac{y_i(k) - y_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial d_1(k)}{\partial z_i(k)} = \frac{z_i(k) - z_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial d_2(k)}{\partial x_i(k)} = \frac{x_i(k) - x_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial d_2(k)}{\partial y_i(k)} = \frac{y_i(k) - y_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial d_2(k)}{\partial z_i(k)} = \frac{z_i(k) - z_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial d_3(k)}{\partial x_i(k)} = \frac{x_i(k) - x_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial d_3(k)}{\partial y_i(k)} = \frac{y_i(k) - y_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial d_3(k)}{\partial z_i(k)} = \frac{z_i(k) - z_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial \phi_1(k)}{\partial x_i(k)} = \frac{x_i(k) - x_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial \phi_1(k)}{\partial y_i(k)} = \frac{y_i(k) - y_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial \phi_1(k)}{\partial z_i(k)} = \frac{z_i(k) - z_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial \phi_2(k)}{\partial x_i(k)} = \frac{x_i(k) - x_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial \phi_2(k)}{\partial y_i(k)} = \frac{y_i(k) - y_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial \phi_2(k)}{\partial z_i(k)} = \frac{z_i(k) - z_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial \phi_3(k)}{\partial x_i(k)} = \frac{x_i(k) - x_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial \phi_3(k)}{\partial y_i(k)} = \frac{y_i(k) - y_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial \phi_3(k)}{\partial z_i(k)} = \frac{z_i(k) - z_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial \phi_4(k)}{\partial x_i(k)} = \frac{x_i(k) - x_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial \phi_4(k)}{\partial y_i(k)} = \frac{y_i(k) - y_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

$$\frac{\partial \phi_4(k)}{\partial z_i(k)} = \frac{z_i(k) - z_i}{\sqrt{(x_i(k) - x_i)^2 + (y_i(k) - y_i)^2 + (z_i(k) - z_i)^2}}$$

(20)
Algorithm of Extended Kalman Filter

Initialization: Mean $\mu(0) = E[x(0)]$
Covariance $P(0) = var(x(0))$

1: Prediction of state
$$\hat{x}_k = F \hat{x}_{k-1} + G w_{k-1}$$

2: Prediction of state covariance
$$\overline{P}_k = F_{k-1} \overline{P}_{k-1} F^T_{k-1} + G_{k-1} Q_{k-1} G^T_{k-1}$$

3: Gain calculation of Kalman filter
$$K_k = \overline{P}_k H^T_k \left[ H_k \overline{P}_k H^T_k + R_k \right]^{-1}$$

4: State correction
$$\hat{x}_k = \hat{x}_k + K_k (Z_k - H_k \hat{x}_k)$$

5: State co-variance correction
$$\overline{P}_k = \left( I - K_k H_k \right) \overline{P}_k$$

3.2 Unscented Kalman Filter

For the estimation of parameter EKF is the standard technique, but EKF is having some drawbacks. In EKF, the non-linear equations of the system are converted into linear equations. In this situation, the accuracy of EKF can attain up to first order of Taylor’s series and also, it needs to calculate the matrix of Jacobian. Because of the mentioned drawbacks and issues, UKF has been used to present better performance as compared to the EKF algorithm and especially for the non-linear systems. UKF is based on unscented transformation (UT), the approach used to estimate the statistics of the random variable. In UKF, some points are used to catch the actual covariance and mean of the random variables.

Dissimilar to EKF, UKF doesn’t have to calculate matrix of Jacobian at each time and embraces UT to make the measurements save reliable for the random variables which undergo transformation of nonlinear. For the random variable with distribution as Gaussian, by choosing the sample points cautiously, UT can catch the covariance and mean precisely to the Taylor series third order. So it can successfully conquer the low precision restriction of the EKF algorithm. So the algorithm of UKF is more advantageous and exact when contrasted with the algorithm of EKF.

In the 3D plane expecting that the target sensor is moving with uniform acceleration, the vector of state contains acceleration, velocity and position and the vector of measurement containing distances and angles from reference sensors to target sensors is the equivalent to that in the algorithm EKF.

Here the $2n+1$ sigma points can be calculated by using (21), these points are propagated through the nonlinearity and are used to calculate the covariance and mean of the variable after transformation.

$$X = [m \ldots m] + \sqrt{c}[0 \sqrt{P} - \sqrt{P}]$$

And calculate the weights using (22).

$$W_m^{(i)} = \frac{\lambda}{(n+\lambda)}$$
$$W_c^{(i)} = \frac{\lambda}{(n+\lambda)} + (1 - \alpha^2 + \beta)$$
$$W_m^{(i)} = \frac{\lambda}{2(n+\lambda)}$$
$$W_c^{(i)} = \frac{\lambda}{2(n+\lambda)}$$

$$i = 1, \ldots, 2n.$$  

here $\lambda$ is a scaling parameter to decrease the total error of prediction which is given by

$$\lambda = \alpha^2 (n+k) - n$$

$\alpha, \beta$ and $k$ are positive values

where $W_m^{(i)}$ is the sigma points mean weight and $W_c^{(i)}$ is the sigma points covariance weight, $i$ in the above weights is the sample point index.

Generally, $\alpha$ is normally taken as a small positive value to maintain the sigma points mean nearer to $x$, $\beta$ is a positive
coefficient to integrate the x prior distribution, and κ is taken as zero to make the matrix \((n + \lambda) P\) as a semi-positive definite matrix. The algorithm begins considering the initial mean as \(m_0\) and co-variance as \(P_0\).

The algorithm of Unscented Kalman Filter algorithm is given below

Algorithm 2 Unscented Kalman Filter Algorithm

**Initialization:**

\[
\begin{align*}
    m_0 &= E[x_0] \\
    P_0 &= E[(x_0 - m_0)(x_0 - m_0)^T]
\end{align*}
\]

**Step 1:** Calculate the predicted mean of state \(\mu_k\) and covariance \(P_k\) from transformed sigma points

\[
X_{k-1} = \begin{bmatrix} m_{k-1} \ldots m_{k-1} \end{bmatrix} + \sqrt{c}[0 \sqrt{P_{k-1}} - \sqrt{P_{k-1}}]
\]

\[
X\_k = f_k(X_{k-1}, k-1)
\]

\[
m_k = \sum X\_k w\_m
\]

\[
P_k = X\_k W[X\_k]^T + Q_{k-1}
\]

Here vector \(w_m\) and weighted matrix \(W\) are given as

\[
w\_m = \begin{bmatrix} W\_m^0 \ldots W\_m^2 \end{bmatrix}
\]

\[
W = (I - [w\_m \ldots w\_m]) \times \text{diag} \begin{bmatrix} W\_m^0 \ldots W\_m^2 \end{bmatrix}
\]

**Step 2:** Calculate the measurement predicted covariance \(S_k\) and mean \(\mu_k\), the measurement and state cross covariance \(C_k\) as

\[
X\_k = \begin{bmatrix} m\_k \ldots m\_k \end{bmatrix} + \sqrt{c}[0 \sqrt{S_k} - \sqrt{S_k}]
\]

\[
Y\_k = h_k(X\_k, k)
\]

\[
\mu_k = Y\_k w\_m
\]

\[
S_k = Y\_k W[Y\_k]^T + R_k
\]

\[
C_k = X\_k W[Y\_k]^T
\]

**Step 3:** Calculate the gain of the filter \(K_k\) and mean \(m_k\) and co-variance \(P_k\) of the state

\[
K_k = C_k S_k^{-1}
\]

\[
m_k = m\_k + K_k (y_k - \mu_k)
\]

\[
P_k = P\_k - K_k S_k K_k^T
\]

4. Results and Discussion

A number of Monte Carlo simulations were performed to estimate the performance of algorithms, in terms of precision for both the localization and tracking methods. We are considering two scenarios for placement of reference nodes. First one, at the top four corners of the building and second one Cuboid-Shape Configuration as shown below. For the given two scenarios the reference nodes are fixed accordingly and the unknown target position is randomly selected. The estimated position of the target using Iterative method (IM) is compared with the traditional linear least squares (LLS) method of UWB for two scenarios in Fig.4 and Fig.5.

The estimated target position for each run result is obtained and averaged over 1000 runs are presented. The result shows that the Iterative method gives better accuracy compared to the linear least squares method.
The variance of time of arrival error, $\sigma^2_{\text{TOA},i}$, is assigned proportional to the distance between reference node $i=1,2,3,4$ and the target node, $d^2_i$ with $\text{SNR} = d^2_i / \sigma^2_{\text{TOA},i}$.

Here the mean square position error MSPE of the linear least squares (LLS) method and iterative method (IM) for SNR belongs to $[-10, 60]$ dB are compared. The MSPE is given by $\text{MSPE} = E\{(\hat{x} - x)^2 + (\hat{y} - y)^2 + (\hat{z} - z)^2\}$. As expected, the iterative method is preferable to the LLS method and the MSPE is less for both scenarios as given in Fig.6 and Fig.7 for two scenarios respectively.

The comparison of two scenarios is given in Fig. 8. And among the scenarios, the second with Cuboid-Shape Configuration gives better performance compared to the first scenario with reference nodes at the top four corners of the building. The MSPE of iterative method, with reference nodes fixed as second scenario is smaller by around 1 dB at SNR $\in [-10, 60]$ dB compared to the first scenario. For the second scenario, the reference nodes occupy four corners including top and bottom of the area of localization. Hence, almost the total area of localization is covered. In the case of the scenario 1 reference sensors at top of the positioning area covered less area compared to previous one. So geometry of the reference nodes plays an important role in calculating positioning. The Cumulative distribution function of location errors for both scenarios are given in Fig.9. It can be observed that scenario 2 is the best precise technique with an error under 2 meters in 90% of situations, for scenario 1 a similar exactness is accomplished in just between 60% and 70% of situations.
Fig. 6. Comparison of mean square position error for linear least squares and iterative method for scenario 1

Fig. 7. Comparison of mean square position error for linear least squares and iterative method for scenario 2

Fig. 8. Comparison of mean square position error scenario 1 and scenario 2
A simulation to evaluate the performance of indoor tracking with UWB positioning and IMU tracking is compared with EKF and is compared with the true (ground truth) trajectory in Fig 10. EKF gives better performance compared to UWB with IMU. In this simulation, for the first time the estimated state vector is taken as Xest is Zero matrix, in which Xtrue = Xest. The parameters of UKF are taken as $\alpha = 0.001$, $k = 0$, and $\beta = 2$. The state vector size is $n = \text{length}\ (Xest)$. Where the process noise vector is taken as Gaussian white sequences noise with zero mean and covariance $R = I \sigma^2$, where, $\sigma = 0.01$. The covariance matrix of process noise is given by $Q = I \times 10^{-10}$, here $I$ is the identity matrix. The comparison of EKF and UKF tracking algorithms is shown in Fig 11. UKF still provides better estimation accuracy than EKF does. We can see that the tracking result is quite good with the estimated result from UKF.
The function of cumulative distribution of the tracking errors for all the algorithms are given in Fig.12. It is noticed that UKF tracking algorithm is the best precise technique with an error around 2 meters in 90% of situations, but for EKF a similar exactness is accomplished in 75% and only 60% in case of UWB.

![Cumulative distribution function of UWB, EKF and UKF Algorithms](image)

4.1 Density of the Reference Nodes

By expanding the number of the reference sensors may reduce the positioning errors. For four reference sensors, the position is similar to in Fig 4. The position of 8 reference sensors is acquired from that of 4 reference sensors by embedding an extra sensor halfway between each two neighbouring reference sensors. The position of 12 reference sensors relates to that of 8 reference sensors with 4 extra sensors set at the focal point of the rectangular zone. At last, the position of 16 reference sensors is acquired by embedding 4 new sensors halfway between the 4 past sensors.

The mean square error (MSE) for different numbers of reference nodes is summarized in table 1 for all algorithms. To sum up, we can say that expanding the quantity of reference sensors diminishes the positioning errors basically when utilizing techniques dependent on nonlinear Kalman filtering. However, no substantial improvement is achieved by expanding the quantity of reference nodes beyond some point. This must be evaded, since expanding this number increments mostly the complication.

| No.of Reference Sensors | 4    | 8    | 12   | 16   |
|-------------------------|------|------|------|------|
| UWB-IMU                 | 2.93 | 2.87 | 2.74 | 2.65 |
| UWB-EKF                 | 2.09 | 1.75 | 1.54 | 1.43 |
| UWB-UKF                 | 1.65 | 1.43 | 1.05 | 0.94 |

5. Conclusion

In this paper, we have proposed an effective approach for indoor tracking and positioning systems in 3D. The positioning is calculated using Ultra Wideband with the TOA values received from all four reference nodes. The TOA values are obtained using Maximum energy Selection Search Back algorithm. And the position is calculated using an iterative method by using those TOA values. The positioning using Iterative method is compared with the linear least squares algorithm and showed that Iterative method gives better performance compared with linear least square algorithm. The positioning performance is compared in two scenarios, reference nodes placed at top corners of the building and other as cuboid shape configuration. The latter gives better results compared to previous configuration. The position of reference nodes has a significant effect on the exactness of localization.

The tracking is done by integrating UWB with IMU. And the performance can still be increased by using the nonlinear Extended and Unscented kalman filters. The state equations of the Kalman filters are obtained from IMU data and the observation equation from UWB measurements. EKF is compared with UKF and showed that later can improve the performance.
The outcomes got shows that the proposed UKF technique have been contrasted with the EKF and have shown significant gain in tracking of moving objects. The UKF displays excellent performance when contrasted with regular EKF since the series approximations in the EKF calculation can lead to poor representations of the nonlinear functions and probability distributions of interest.

In this paper the impact of the quantity of reference sensors on the position exactness has also been analysed. Undoubtedly, as expected, normally, the position exactness increments when the quantity of reference sensors increments, however just up to a specific value. Anyway the cost to pay for this is an expansion in the computational load.

Declarations

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**Figures**

**Figure 1**
Proposed sensor based indoor positioning and tracking system by coupling IMU and UWB

**Figure 2**
Energy samples of the received signal

**Figure 3**
TOA estimation algorithms using the samples of energy

Figure 4

Comparison of linear least squares and Iterative method for scenario 1
Figure 5

Comparison of linear least squares and Iterative method for scenario 2
Figure 6

Comparison of mean square position error for linear least squares and iterative method for scenario 1

Figure 7

Comparison of mean square position error for linear least squares and iterative method for scenario 2
Figure 8

Comparison of mean square position error scenario 1 and scenario 2
Figure 9

Cumulative distribution function of scenario 1 and scenario 2

Figure 10

Performance comparison of UWB and EKF tracking algorithms with the actual ground truth trajectory
Figure 11

Performance comparison of UKF and EKF tracking algorithms with the actual ground truth trajectory
Figure 12

Cumulative distribution function of UWB, EKF and UKF Algorithms