Adsorption, Kinetic and Thermodynamic Study for Removal of Nickel Ions by Activated Carbon from Palm Kernel

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ABSTRACT

Palm kernel (PK) was activated by chemical activation ([HNO3 at 230-350°C]) to remove Ni(II) ions from aqueous solutions. Physicochemical properties of PK were reported. FT-IR analysis revealed changes in wave numbers and absorbance indicating Ni(II) adsorption onto activated carbon-PK surface. Energy dispersive X-ray fluorescence technique was used to determine the content of metals in activated carbon-PK and showed the metals found in activated carbon-PK were in recommended human usages. The maximum removal of Ni(II) ions was to be 49.7% at pH 4.6 and the equilibrium reached at 80 min. The removal efficiency of Ni(II) ions increased as the dosage of activated-PK increases and the optimum amount of activated carbon-PK dose was found to be 70 mg. The optimum pH was 4.6. The isotherms, kinetics and thermodynamics were studied. The Ni(II)-activated carbon-PK adsorption was found to follow the Freundlich isotherm based on correlation coefficient (R²) values and to be physical adsorption from the mean free energy found by Dubinin-Radushkevich, which confirmed by isothermal microcalorimetry data and the heat of sorption process using Temkin isotherm model to be 1.58 kJ/mol. The adsorption kinetic data were described well by a second order, with the kinetic constant rates in the range of 1.82-83.5 g/g.min and was not controlled by intra-particle diffusion model. The thermodynamic studies showed that the Ni(II)-ACPK adsorption process is exothermic due to the negative values of ΔH (-30.9 J/mol) and is physical nature process due to the negative values of ΔS (-14.9 J/mol). The magnitude of Ea is 15.04 kJ/mol, which is proven the physical adsorption in nature.

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INTRODUCTION

For the last decay, the level of toxic heavy metals in fresh and ground waters have been gradually increased due their release of untreated industrial efluents. Nickel is a heavy metal and has broad industrial applications such as in stainless steel for 11% total nickel processing like electroplating industries within the range of 20-200 mg/l. However, the acceptable nickel in drinking water is 0.01 mg/l. The wastewaters can contain certain amount of nickel from nickel processing. High exposure to nickel has been found to be linked to cancer, sink irritation, and asthma. Therefore, nickel should be removed from these processes before discharge to the environment.

The removal of different heavy metals from wastewater like nickel is a big matter for the governments, environmental agencies and researchers dealing with the production of water sources and ecosystems for more than a decay [1]. Among to several chemical and physical techniques have been used in the big scale to remove these heavy metals from wastewater, such as conventional technologies, separation methods, etc. Adsorption has been found to be one of the simplest, low cost and high efficiency techniques used for purification of waters in industries [2, 3]. This technique uses to immobilize ions from liquid phase onto solid phase by using different materials, such as activated carbon [2]. Almost, all carbon-rich materials from plants may be used to remove these heavy metals from an aqueous solution. Activated carbon form after either physical or chemical carbonization processes are found to be more useful products like activated carbon if carefully controlled processes of dehydration, carbonization, and physical and chemical activation [4, 5]. These agricultural wastes have been increasingly in demand for activated carbon in industrial processes due to their ability to absorb any organic solvent at low temperature and release it at high temperature [6]. The adsorption of heavy metals onto waste agricultural materials could be related to their lignin, cellulose and
hemicellulose with carboxylic, hydroxyl, sulphate, phosphate and amino groups that can bind to heavy metal ions [7].

Many studies have reported on the development of these activated carbon from low cost and readily available natural materials [7, 8]. One of widespread heavy metals use in many industrial applications is nickel (Ni) ions with small quantities (0.1-0.6 ppm) in natural ecosystems [9]. The non-degradable Ni metals present in the Eco environments from the large scale industrialization such as mining, electroplating, tanning, metallurgical operation and manufacturing leads to serious problems on aquatic life, animal, plant life and human health even at low concentrations [7].

The removal of heavy metals is a matter of great interest for researchers and environmental agencies because of their toxicity, reactivity and mobility in soil and waters [10]. The main objectives of this study were: to offer effective and economical adsorptive materials and to investigate its ability for the adsorption of Ni(II) ions from aqueous solution and to study the isotherm, kinetic and thermodynamic of Ni-activated carbon-PK adsorption processes.

MATERIALS AND METHODS

All chemicals used in this research were purchased from different companies, Scharlau, BDH chemicals Ltd and Surechem products Ltd, and were used without further purification. The Ni(II) stock solution was prepared by dissolving an accurately amount of nickel chloride (NiCl2.6H2O) from BDH chemicals Ltd in deionized water. The desired concentrations of Ni(II) were prepared by diluting the Ni (1000 mg/l) stock solution with deionized water. Nitric acid was used for the activation. pH of the solution was adjusted with Hydrochloric acid and sodium hydroxide, from Scharlau.

pH meter and conductivity meter were used for pH and conductivity measurements. These instruments were supplied from Thermo, Orion 4 star and conductivity meter from Philips, PW-9527.

Analyzer EA-1112 was used from thermo for CHNS analysis. Oxygen was used to combust activated carbon-PK and helium was used as carrier gas. The furnace was set to 950°C at the initial and gases were flowed. A few mg of PACK was put on the aluminum foil. Thermal conductivity detector was used for analyze CHNS.

Atomic absorption spectrophotometer from Thermo AA spectrometer S-series was used for Ni concentration before and after adsorption processes.

In this research, Fourier transform infrared (FT-IR) and spectrometer were used for characterization of the surface of PK and to identify chemical functional groups present on the surface of PK. Samples were scanned with an Burker instrument and resolution 2 cm-1 over spectral range extending from 4000 to 400 cm-1.

Surface area of activated carbon-PK was determined by BET method from nitrogen adsorption resulting isotherm at 77 K in an automatic analyzer (Micromeritics 2020 ASAP apparatus) after pre-treatment for 3 h at 473 K under vacuum.

Energy dispersive X-ray fluorescence, EDXRF, NEX QC+QuantEZ from Rigaku was used for the determination of elements present in activated carbon-PK. All measurements were carried out under helium and the tube voltage (kV) was High-Z 50.0, Mid-Z 30.0 and Low-Z Open 6.5. FP method was used for analysis. 4g was put it onto the EDXRF container. XRF thin film (TF-240, polypropylene) from premier lab supply was used.

Differential heat flow reaction calorimeter (TITRYS, from Setaram) equipped with a stirring system used for heat measurement.

Adsorbent collection and preparation was carried out according to previous method developed with slight modifications [11]. The PK as low-value or zero cost agricultural waste production especially in Libya was collected from Sirte region, north part of Libya. The collected PK samples were first washed with distilled water for several times in order to remove the dirt, dust and fine. Then, dried in an oven at 378 K for 24 h and later grounded to obtain a powder form and sieved to a 1.0 mm to 0.5 mm.

The chemical activation process for PK was carried out by following method with slight modifications [12]. 100 ml of HNO3 (65%, w/w) was mixed with 20 g of PK with ratio 1:5 (raw PK:HNO3). The suspension of PK-HNO3 was allowed to soak at 383 K for 3 hours and then left to cool for overnight at room temperature in closed container. The activated carbon palm kernel (ACPK) was washed with distilled water until the pH remained constant. Then, ACPK was dried at 378 K for 24 hours. Finally, ACPK samples were heated at 473 K, crushed, sieved at 125 μm and stored in desiccator.

The effect of time at which the equilibrium of Ni(II)-ACPK adsorption was investigated. 0.1 to 1.0 g of ACPK was added to 150 ml of 20.0 mg/l Ni(II) solution at 298 K. The suspension was placed on a stirring plate for 120 min. During the experimental time period, 5 ml aliquots of Ni(II)-ACPK suspensions were filtered at various time intervals (0 to 120 min). The percentage removal of Ni(II) was investigated by adding 50 mg of ACPK to different Ni(II) concentrations from 5 to 25 mg/l at a pH of 4.6, agitation speed 200 rpm, contact time 80 min and T=298, 308 and 318 K. The effect of ACPK dose on Ni(II)-ACPK adsorption was investigated by adding 0.1 to 1.0 g of ACPK to 20 mg/l Ni(II) ions, pH of 4.6, contact time 80 min and T=298, 308 and 318 K. In order to evaluate the effect of initial pH on Ni(II)-ACPK adsorption from aqueous solution, 50 mg of ACPK was added to 150 ml of 20 mg/l Ni(II) at different pH values.
agitation speed 200 rpm, contact time 80 min and T=298, 308 and 318 K. During the experimental time period, 5 ml aliquots of Ni(II)-ACPK suspensions were taken and filtered with 0.45µm filter paper. The filtrate was analyzed for Ni(II) concentration by AAS. All the experiments were carried out triplicate runs and the average values were taken. The amount of Ni(II) ions adsorbed onto ACPK surface per unit of mass (q_{max}, mg/g) was evaluated by the following equation:
\[
q_{max} = \frac{C_o - C_e}{W} \times V
\]
(1)
where: initial Ni(II) concentration (C_o, mg/l); final Ni(II) concentration at equilibrium (C_e, mg/l), volume of Ni(II) solution (V, ml); mass of ACPK sample (W, mg). The percent sorption of Ni(II) was also evaluated by the following equation:
\[
\%\text{Removal} = \frac{C_o - C_e}{C_o} \times 100
\]
(2)
In order to measure the heats of Ni(II)-ACPK adsorption, a calorimeter equipped with a stirring system and a system for the introduction of liquids (a programmable syringe pump PHD 2000, from Harvard Apparatus, linked to the calorimeter by capillary tubes), in aqueous phase was used. Successive pulse injections of 20 mg/l solution of Ni(II) ions in deionised water were sent to the sample maintained at 303 K at 2 hours time intervals. Water and the aqueous solution of Ni(II) used in this study were previously purged with flowing nitrogen to avoid formation of air bubbles in the capillary tubes. A preheating furnace was used to allow the injection of the probe solution at the same temperature of 303 K. The reference and measurement cells contained water (1.5 ml) and water with a weighted amount of the solid sample (cal. 100 mg), respectively. The samples were activated in situ by outgassing the powders at 323 K for 2 hours and then transferred into the calorimeter cell. The evolved heat from the adsorption processes was obtained by using the integration of the area under the calorimeter signal for each dose.

RESULTS AND DISCUSSION

The proximate composition of ACPK was carried according to previous methods [13, 14]. The ACPK characteristics, which are essential to understand the adsorptive behavior, are presented in Table 1.

The moisture content was found to be high, which might be due to its plant origin of PK. Ash content was high which might be related to acid and water wash might not have been able to reduce leachable ash or the presence of substantial amounts of water-soluble minerals remained in the ACPK sample. Conductivity and salinity of ACPK were used to indicate the quality of activated carbon and found to be slightly high comparing to those of other studies which might be due to the presence of soluble minerals in surface of ACPK after carbonization process [13]. The bulk density is important parameter for biosorption application because the higher bulk density is better the filterability of activated carbon. The bulk density of ACPK was found to be generally higher than lower limit of 0.25 g/cm³ for granular activated carbon. The pH of ACPK was acidic 4.8, which might be due to the acid wash was incomplete or the nature of PK. It was found that the suspension pH affects the rate of activated carbon adsorption, which is more effective at low pH than high pH [14]. Further, surface area is an important parameter to achieve the adsorption behavior of the biocarbon. It was found that the surface area of ACPK was 1.13 m²/g, using Brunauer, Emmet, and Teller (BET) method. These results are indicated the biocarbon with a good activity for adsorption with one exception.

The EDXRF results of the ACPK samples for contained oxide elements are shown in Figure 1 and additional data are listed in Table 2. The EDXRF results of the ACPK samples for contained elements as shown in Figure 1 and listed in Table 3. These results indicated that the ACPK can be used for water purification process.

Figure 2 shows the FT-IR spectrum of ACPK-Ni(II), 50 mg of ACPK was added to 150 ml of 20 mg/l Ni(II) at a pH of 4.6, agitation speed 200 rpm, contact time 80 min (time study) and T= 298 K. The spectrum revealed the presence of the following groups: a peak at 3361.05 cm⁻¹ assigned with –OH group belongs to cellulose or lignin [15]. After addition of Ni(II) ions, this peak was shifted from 3361.05 to 3363.44 cm⁻¹ and the percentage of peak transmittance was increased from 92.8 to 98.2%, which was probably due to complexation of Ni(II) with –OH group of hydroxyl group and bonded -OH bands of carboxylic acids in the inter- and intra-molecular hydrogen bonding of polymeric compound [15]. Furthermore, carbonyl group (–C=O stretch) peak at 1741.85 cm⁻¹ and the peak appeared at 1611.97 cm⁻¹ assigned with H-bend stretching from amide groups were observed and a change of these peaks was also

| TABLE 1. Physico-chemical characteristics of ACPK |
|-----------------------------------------------|
| Physico-chemical properties | Value | Physico-chemical properties | Value |
| Moisture content (%) | 7.28 | Matter soluble in water | 0.190 |
| Ash content (%) | 5.80 | N (%) | 6.94 |
| Bulk density (g/cm³) | 0.35 | C (%) | 24.5 |
| pH | 4.80 | H (%) | 2.65 |
| Conductivity (µS/cm) | 285 | S (%) | 8.13 |
| Salinity (mg/l) | 163 | net heat value (kcal/kg) | 3125 |
| S_{net} (m²/g) | 1.13 | gross heat value (kcal/kg) | 2989 |
Figure 1. EDXRF spectrum of ACPK for oxide element analysis method

noted after the addition of Ni(II). The peak at 1036.88 cm$^{-1}$ assigned to the surface -C-O bond stretching of phenolic groups. Therefore, FT-IR studied revealed that several functional groups present in ACPK are likely to bind the Ni(II) ions and to suggest considerable cation exchange capacity to adsorbent surface [16].

Figure 3 shows the effect of contact time on the removal of Ni(II) onto the surface of ACPK. 0.1 to 1.0 g of ACPK was added to 150 ml of 20 mg/l Ni(II) at a pH of 4.6, agitation speed 200 rpm and T=298K. The ACPK-Ni(II) adsorption was shown a similar trend with respect to time, but the extent of removal was differed. Generally, the trend was a rapid increase in Ni(II) ions removal after addition of ACPK, followed by leveling off towards the end of the experiment at certain time. The AAS data clearly shows that no significant additional adsorption of Ni(II) onto ACPK surface occurred after 40 min. Thus, 80 min was chosen as the time the equilibrium of ACPK-Ni(II) adsorption was attained.

Figure 4 shows the effect of initial Ni(II) concentration on the percentage removal of Ni(II) by ACPK. 50 mg of ACPK was added to 150 ml of different concentrations of Ni(II) (5 to 25 mg/l) at a pH of 4.6, agitation speed at 200 rpm, contact time at 80 min and T at 298 K. It was found that the percentage removal of Ni(II) by ACPK was decreased with increasing in

Figure 2. FT-IR spectrum of ACPK-Ni(II). 50 mg of ACPK was added to 150 ml of 20 mg/l Ni(II) at a pH of 4.6, agitation speed 200 rpm, contact time 80 min (time study) and T=298K

Figure 3. Effect of contact time on the removal of Ni(II) by ACPK. 0.1 to 1.0 g of ACPK was added to 150 ml of Ni(II) at a pH of 4.6, agitation speed 200 rpm and T=298K

Figure 4. Effect of initial Ni(II) concentration on the percentage removal of Ni(II) by ACPK. 50mg of ACPK was added to 150 ml of different concentrations of Ni(II) (5 to 25 mg/l) at a pH of 4.6, agitation speed 200 rpm, contact time 80 min and T=298K
### TABLE 2. The EDXRF results of ACPK for oxide metals

| No. | Component | Result | Unit | Stat.Err. | LLD | LLQ |
|-----|-----------|--------|------|-----------|-----|-----|
| 1   | K₂O       | 63.5   | mass%| 0.65      | 0.907 | 2.72 |
| 2   | P₂O₅      | 28.2   | mass%| 0.0522    | 0.0465 | 0.14 |
| 3   | CaO       | 19.1   | mass%| 0.793     | 1.73  | 5.2 |
| 4   | SO₃       | 15.4   | mass%| 0.0312    | 0.0384 | 0.115 |
| 5   | NiO       | 4.03   | mass%| 0.0517    | 0.0118 | 0.0353 |
| 6   | SiO₂      | 2.96   | mass%| 0.0356    | 0.0833 | 0.25 |
| 7   | Fe₂O₃     | 2.31   | mass%| 0.0616    | 0.0727 | 0.218 |
| 8   | MnO       | 1.75   | mass%| 0.0643    | 0.0385 | 0.116 |
| 9   | ZnO       | 1.65   | mass%| 0.0247    | 0.0079 | 0.0236 |
| 10  | CuO       | 1.37   | mass%| 0.0267    | 0.0282 | 0.0846 |
| 11  | Dy₂O₃     | 0.934  | mass%| 0.0999    | 0.279 | 0.837 |
| 12  | Ta₂O₅     | 0.423  | mass%| 0.0568    | 0.17  | 0.509 |
| 13  | CdO       | 0.36   | mass%| 0.0057    | 0.014 | 0.0419 |
| 14  | WO₃       | 0.336  | mass%| 0.0373    | 0.0947 | 0.284 |
| 15  | Rh₂O₃     | 0.297  | mass%| 0.0052    | 0.0107 | 0.0322 |
| 16  | Cd        | 0.294  | mass%| 0.0058    | 0.0112 | 0.0335 |
| 17  | Ag₂O      | 0.0575 | mass%| 0.0038    | 0.0105 | 0.0315 |
| 18  | SnO₂      | <0.0001| mass%| 0.007     | 0.0211 | 0.0633 |

### TABLE 3. The EDXRF results of ACPK for elements

| No. | Component | Result | Unit | Stat.Err. | LLD | LLQ |
|-----|-----------|--------|------|-----------|-----|-----|
| 1   | K         | 52.7   | mass%| 0.54      | 0.753 | 2.26 |
| 2   | Ca        | 13.6   | mass%| 0.567     | 1.24  | 3.72 |
| 3   | P         | 12.3   | mass%| 0.0228    | 0.0203 | 0.0609 |
| 4   | S         | 6.17   | mass%| 0.0125    | 0.0154 | 0.0462 |
| 5   | Ni        | 3.16   | mass%| 0.0406    | 0.0093 | 0.0278 |
| 6   | Cl        | 2.57   | mass%| 0.007     | 0.0127 | 0.0382 |
| 7   | Fe        | 1.62   | mass%| 0.0431    | 0.0508 | 0.153 |
| 8   | Si        | 1.38   | mass%| 0.0166    | 0.0389 | 0.117 |
| 9   | Mn        | 1.35   | mass%| 0.0498    | 0.0298 | 0.0895 |
| 10  | Zn        | 1.32   | mass%| 0.0199    | 0.0063 | 0.0189 |
| 11  | Cu        | 1.09   | mass%| 0.0213    | 0.0225 | 0.0676 |
| 12  | Dy        | 0.814  | mass%| 0.0871    | 0.243  | 0.729 |
| 13  | Br        | 0.398  | mass%| 0.0059    | 0.004  | 0.0119 |
| 14  | Ta        | 0.346  | mass%| 0.0466    | 0.139  | 0.417 |
| 15  | Cd        | 0.315  | mass%| 0.005     | 0.0122 | 0.0367 |
| 16  | Rb        | 0.269  | mass%| 0.0053    | 0.0102 | 0.0306 |
| 17  | W         | 0.267  | mass%| 0.0295    | 0.0751 | 0.225 |
| 18  | Rh        | 0.241  | mass%| 0.0042    | 0.0087 | 0.0261 |
| 19  | Ag        | 0.0535 | mass%| 0.0035    | 0.0098 | 0.0293 |
| 20  | Sn        | <0.0001| mass%| 0.0055    | 0.0166 | 0.0498 |
| 21  | O         | <0.0001| mass%|          |       |      |
initial Ni(II) concentrations. This may due to the ratio of available ACPK surface active sites to Ni(II) at low concentration is high and decreased with increasing Ni(II) concentration. Therefore, lower concentrations of Ni(II) were used to study the kinetic and isotherm models.

Figure 5 shows the effect of adsorbent dose on the removal of Ni(II) by ACPK. Different amounts of ACPK (0.1 to 1.0 g) were added to 150 ml of 20 mg/l Ni(II) at a pH of 4.6, agitation speed 200 rpm, contact time 80 min and T=298K. As expected, the removal efficiency of ACPK was significantly increased with increasing ACPK doses from 0.1 to 1.0 g. This may be due to availability of more surface area with the higher dose of ACPK in solution [17]. The maximum removal of Ni(II) by ACPK is 77.6% for adsorbent of 70mg per 150 ml of Ni(II) solution, while no significant additional Ni(II) adsorption onto ACPK occurred after 70mg of ACPK. This might due to aggregation/agglomeration of adsorbent particles at higher concentrations leading to decrease in the total ACPK surface active sites for adsorption or over crowding the adsorbent particles [18].

Figure 6 shows the effect of pH on the removal of Ni(II) ions by the surface of ACPK. 50 mg of ACPK was added to 150 ml of 20 mg/l Ni(II) at different pH, agitation speed 200 rpm, contact time 80 min and T=298K. The removal efficiency increases with increasing in solution pH from 3 to 4.6 and then decreases with increasing in solution pH. This could be due to the concentration of protons which are released from active sites of ACPK is high at low pH, so the Ni(II) ions and the protons compete for binding sites of the ACPK surface which decrease with increasing pH, namely electrostatic interaction mechanism. At high pH, the degree of protonation of ACPK functional groups decreased gradually and therefore the efficiency of Ni(II) removal decreased as well due to neutralization of the ACPK surface. The optimal Ni(II) removal efficiency was at pH 4.6 due to the negative charge density on the ACPK surface. Also, pH affects the solubility of Ni(II) in solution and ions on the functional groups of ACPK. Therefore, the uptake of Ni(II) by ACPK is pH-dependent. A similar result was obtained when other adsorbents were used [19-21].

Figure 7 shows equilibrium concentration of Ni(II) ions as function of solution temperature. 0.1 g of ACPK was added to 150 ml of 5 to 25 mg/l Ni(II) at a pH of 4.6, agitation speed at 200 rpm and T at 298, 308 and 318 K. It can be seen that the percentage removal of Ni(II) on ACPK decreases as the temperature increases. This result confirms that the adsorption process is exothermic. The decrease in Ni(II) adsorption on ACPK surface as temperature increases may be due to the relative increase in escaping tendency of Ni(II) ions from solid phase to solution phase. Also, this could be due to the weakness of adsorptive forces between Ni(II) and active sites on ACPK [22]. Therefore, the increasing in solution temperature may be used to recover the active sites on ACPK.
Adsorption isotherms

The Freundlich isotherm model is useful to identify sorption phenomena of ACPK-Ni(II) adsorption process and can be determined by following equation:

\[ q_e = K_F C_e^{1/n} \]  \hspace{1cm} (3)

where: adsorption equilibrium constant \((K_F, \text{mg/g})\); amount of Ni(II) per unit mass of adsorbate \((q_e, \text{mg/g})\); equilibrium concentration \((C_e, \text{mg/l})\) [23]. A straight line was obtained by plotting \(q_e\) versus \(C_e\) and the results are listed in Table 4. Based on Freundlich assumptions, a smaller value of \(1/n\) indicates that weak adsorptive forces are effective on the ACPK surface at all temperatures. Therefore, the process was favorable at higher Ni(II) concentrations and PK surface was a weak Van der Waals attraction due to high surface area, multilayer of Ni(II) adsorption onto the ACPK matrix with increasing solution temperature indicating that the adsorption process is exothermic [18].

Langmuir model assumes the monolayer sorption occupied onto the surface containing a finite number of identical sorption site and can be described by the following equation:

\[ q_e = \frac{b C_m q_m}{1 + b C_e} \]  \hspace{1cm} (4)

where: the maximum Ni(II) ions uptake per unit mass of ACPK \((q_m, \text{mg/g})\); Langmuir equilibrium constant \((b, \text{L/g})\). A plot of \(C_e/q_e\) versus \(C_e\) yields a straight line with its slope of \(1/b\) and intercept of \(1/q_m b\) and results are listed in Table 2. The experimental values of \(b\) were slightly increased with the increase of temperatures, indicating that a smaller heat of adsorption was liberated with increasing temperature. The \(q_e\) value was decreased with increasing solution temperature from 298 to 318K, indicating the weak adsorption interactions between Ni(II) and ACPK at high temperature, which support the physic-sorption. This may be due to the destruction of the active sites on ACPK matrix with increasing solution temperature [16]. This confirms that the ACPK-Ni(II) adsorption process is exothermic.

Also, the Langmuir model can be used to evaluate the constant separation factor, \(R_L\), as expressed by the following equation:

\[ R_L = \frac{1}{1+b C_e} \]  \hspace{1cm} (5)

The value of \(R_L\) indicates the isotherm shape to be unfavorable \((R_L>1)\), favorable \((0<R_L<1)\) and irreversible \((R_L=1)\) [19]. The magnitude of \(R_L\) was found to be less than unity showing that ACPK-Ni(II) adsorption was most favorable under different temperature studied under these conditions using Langmuir isotherm.

The D-R equation has the following form:

\[ q_e = q_{max} e^{-\beta \varepsilon} \]  \hspace{1cm} (6)

where \(q_{max}\): D-R monolayer capacity (mg/g); \(\beta\) is a constant related to sorption energy and \(\varepsilon\) is Polanyi potential. The DKR parameters are calculated from the slope of the plot of \(\ln q_e\) versus \(\varepsilon\) gives \(\beta\) (mol²/J²) and intercept gives \(q_m\) (mg/g). The \(\beta\) means free energy \((E)\) of sorption per molecule of the sorbate when it is transferred to the surface of the solid from infinity in the solution:

\[ E = \frac{1}{\sqrt{2\beta}} \]  \hspace{1cm} (7)

The magnitude of \(E\) is used to estimate the adsorption mechanism [15]. The value of \(E\) is \(<8\,\text{(1.58 kJ/mol)}\) that reveals the sorption process follows physical sorption. TABLE 4. This may be due to the surface area of ACPK was relatively low (\(S_{BET}=1.13\,\text{m}^2/\text{g}\) as comparing to other studies. Therefore, the attraction between the Ni(II) and PK surface was a weak Van der Waals attraction due ACPK-Ni(II) physisorption.

The linear form of Temkin isotherm taking into an account of adsorbent-adsorbate interactions is represented by the following equation:

\[ q_e = \frac{RT}{b} \ln A + \frac{RT}{b} \ln C_0 \]  \hspace{1cm} (8)

where: \(B = \frac{RT}{b}\) constant related to heat of sorption (J/mol) obtained From the Temkin plot (\(q_e \quad \text{versus} \quad \ln C_e\)) and listed in TABLE 4; A is Temkin isotherm equilibrium binding constant (l/g); \(b\) is Temkin isotherm constant; \(R\) is universal gas constant (8.314 J/mol/K) at different \(T=298, 308\) and 318 K [21]. The heat of sorption, \(B\), is lower than 8 kJ/mol, which indicating a physical adsorption process and decreased with increasing temperature suggesting the adsorption process is exothermic [12].

From \(R^2\) values given in Table 4, it can be clearly seen that the Freundlich model yields a better fit than other isotherm models used in this study. This trend probably due to high surface area, multilayer of Ni(II) adsorption onto ACPK surface and the adsorption on a surface was not containing a finite number of identical sites which is heterogeneous surface and the boundary layer thickness is also increased. Also, based on \(R^2\), it was noted that the adsorption process was followed Freundlich model at low temperature, while it was followed Langmuir model.

Figure 8 shows the results from microcalorimetric experiment for the adsorption of Ni(II) onto ACPK surface. Each pulse injection of dosed amount of 2mg/l Ni(II) in deionised water, 303 K. The heats of ACPK-Ni(II) interactions were very low nearly base line of calorimeter indicating that the Ni(II) adsorption onto ACPK surface was low. This is confirmed that the ACPK-Ni(II) adsorption was physical adsorption, which is consistent with the result obtained from Temkin isotherm.

Figure 9 shows the plots of (A) first-order, (B) second-order, (C) Elovich and (D) intra-particle diffusion and (E) Boyd model for ACPK-Ni(II) adsorption. Different ACPK doses (0.1, 0.3, 0.5, 0.7 and 1.0 g) was
TABLE 4. Freundlich, Langmuir, D-R and Temkin constants 50mg of ACPK was added to 25 ml of 5 to 25 mg/l of Ni(II) at a pH of 4.6, agitation speed 200 rpm, contact time 80 min and T=298, 308 and 318K

| T (K) | K_f (mg/g/L/g)^1/n | 1/n | R^2 | q_e-exp (mg/g) | b (L/g) | R_e | R^2 |
|-------|-------------------|-----|-----|---------------|---------|-----|-----|
| 298   | 0.783             | 0.491 | 0.9924 | 28.5 | 0.097 | 0.802-0.352 | 0.8543 |
| 308   | 0.584             | 0.463 | 0.9717 | 22.2 | 0.122 | 0.744-0.298 | 0.9201 |
| 318   | 0.047             | 0.406 | 0.8850 | 2.53 | 0.142 | 0.602-0.225 | 0.9234 |

| T (K) | q_m (mg/g) | b | E (kJ/mol) | R^2 | B (J/mg) | A (L/g) | B (J/mol) | R^2 |
|-------|-------------|---|-------------|-----|---------|--------|-----------|-----|
| 298   | 48.4        | 2.00 | 1.58      | 0.7756 | 0.419 | 1.07 | 5.91 | 0.8763 |
| 308   | 49.5        | 2.00 | 0.8835     | 0.523 | 1.19   | 4.89  | 0.1996  |
| 318   | 12.1        | 3.00 | 0.9192     | 4.53  | 1.25   | 0.584 | 0.8725  |

 added to 150 ml of 20 mg/l Ni(II) at a pH of 7.0, agitation speed 200 rpm and T=298 K. The sorption kinetics can be described by a first-order equation:

\[
\ln(q_e - q_t) = \ln q_e - k_1 t
\]

where: \(k_1\) is the adsorption rate (min\(^{-1}\)) and \(q_e\) (at equilibrium) and \(q_t\) (at time \(t\)) are the amount of Ni(II) adsorbed onto ACPK surface (mg/g) at time \(t\). A plot of \(\ln(q_e - q_t)\) versus \(t\) gives a straight line of slope and intercept as shown in Figure 9A and the results are summarized in Table 5.

The experimental data are not well fitted for pseudo-first-order equation. This was due to the correlation coefficients (\(R^2\)) were low. Also, the large differences between \(q_{e-exp}\) and \(q_{e-cal}\) values were observed.

The mechanisms of the ACPK-Ni(II) adsorption was tested by pseudo second-order model:

\[
\frac{t}{q_t} = \frac{1}{k_2q_e^2} + \frac{t}{q_e}
\]

where: \(k_2\) is the adsorption rate constant (g/mg.min). The plot of \(t/q_t\) versus \(t\) gives \(q_e=1/slop\) and \(k_2=slop^2/intercept\). Figure 9B shows the linearized pseudo-second order kinetic plot and the parameters were listed in Table 5. It can be seen from Table 5 that the \(R^2\) values for all different ACPK doses are extremely high coefficients (upto 1.000). In addition, the \(q_{e-cal}\) values agree with the experimental \(q_{e-exp}\) from Langmuir isotherm. The values of \(k_2\) increase with increasing ACPK concentrations. This may due to the increase in the surface active sites at high ACPK concentrations.

The mechanism of ACPK-Ni(II) adsorption was tested by Elovich model:

\[
q_t = \frac{1}{\beta} \ln(a\beta) + \frac{1}{\beta} \ln (t)
\]

where: \(a\) is the initial adsorption rate (mg/g.min) and \(\beta\) is the adsorption constant (g/mg). Figure 9C shows the plots of \(q_t\) versus \(\ln(t)\) give a linear relationship with a slope \((1/\beta)\) and intercept \((1/\beta)\ln(a\beta)\) and the parameters were summarized in Table 5. However, the correlation coefficients for Elovich model obtained at all the studies ACPK doses were low, suggesting that the adsorption process is not an acceptable for Elovich model system.

The Weber and Morris intra-particle diffusion model was used to analyze the experimental kinetic results.

\[
q_t = K_{ip}t^{0.5} + C
\]

where: \(K_{ip}\): the intra-particle diffusion rate constant and \(C\): the intercept which reflects the boundary layer effect. The intra-particle parameters were determined by a plot of \(q_t\) versus \(t^{0.5}\), shown in Figure 9D and summarized in Table 5. The \(K_{ip}\) values were decreased with increasing ACPK dosage. It is clear from Figure d that the linear plots at each ACPK concentration did not pass through the origin. This may due to the difference in the rate of
mass transfer in the initial and equilibrium steps of the sorption [22]. Therefore, the intra-particle diffusion Model was not the only rate-limiting step for adsorption process of ACPK-Ni(II).

The experimental data were tested by Boyd model to determine the actual process involved in the Ni(II)-ACPK adsorption using Equation (13).

\[
\log(q_m - q_t) = \log q_m - \left(\frac{R}{2.303} \right) \frac{t}{T}
\]

(13)

The Boyd plots as shown in Figure 9E was not linear with high correlation coefficients (R^2>0.8496), indicate that the film diffusion mainly governs the Ni(II) adsorption onto ACPK.

The Arrhenius equation is used to evaluate the activation energy (E_a, kJ/mol) by the following expression:

\[
b = A \exp(-\frac{E_a}{RT})
\]

(14)
TABLE 5. Parameters of First-order and Second-order Kinetics for Sorption of Ni(II) onto ACPK Different ACPK doses (0.1 to 1.0 g) was added to 150 ml of 20 mg/l Ni(II) at a pH of 4.6, agitation speed 200 rpm and T=298K

| Dose (g) | \( q_e \text{ exp (mg/g)} \) | \( q_e \text{ cal (mg/g)} \) | \( k_1 \times 10^2 \text{ min}^{-1} \) | \( R^2 \) | \( q_e \text{ exp (mg/g)} \) | \( q_e \text{ cal (mg/g)} \) | \( k_2 \times 10^2 \text{ g/mg/min} \) | \( R^2 \) | \( K_d \times 10^2 \) | \( C \) | \( R^2 \) |
|----------|----------------|----------------|-----------------|-----|----------------|----------------|-----------------|-----|-------------|-----|-----|
| 0.1      | 8.16           | 2.45           | 8.79            | 0.9852 | 10.1           | 1.28           | 0.9876          | 1.06 | 514         | 0.8070 | 3.16 | 0.725 | 0.8828 |
| 0.3      | 4.43           | 0.75           | 1.69            | 0.9927 | 3.72           | 2.15           | 0.9650          | 1.69 | 71.1        | 0.7717 | 2.03 | 0.365 | 0.8720 |
| 0.5      | 3.79           | 2.81           | 1.09            | 0.944  | 3.96           | 8.86           | 0.9997          | 3.05 | 978         | 0.8880 | 0.99  | 0.316 | 0.7789 |
| 0.7      | 3.07           | 0.612          | 4.38            | 0.9477 | 3.37           | 8.45           | 0.9992          | 4.39 | 7192        | 0.9593 | 0.73  | 0.271 | 0.9453 |
| 1.0      | 2.27           | 2.49           | 11.6            | 0.9426 | 2.29           | 83.5           | 1.000           | 18.8 | 2.23E+16    | 0.7585 | 0.15  | 0.225 | 0.6142 |

**TABLE 6.** Thermodynamic parameters of Ni(II) adsorption on ACPK

| T (K) | \( B \text{ (l/mg)} \) | \( \Delta G^0 \text{ (kJ/mol)} \) | \( \Delta H^0 \text{ (kJ/mol)} \) | \( \Delta S^0 \text{ (J/Kmol)} \) | \( E_a \text{ (kJ/mol)} \) |
|-------|----------------|----------------|----------------|----------------|-----|
| 298   | 0.0967        | 5.79           | -30.9          | -14.9          | 15.04 |
| 308   | 0.122         | 5.39           | -30.9          | -14.9          | 15.04 |
| 318   | 0.142         | 5.17           | -30.9          | -14.9          | 15.04 |

**Figure 10.** Arrhenius plot for adsorption of Ni(II) onto ACPK

\[
\ln b = -\frac{\Delta H^0}{R} + \frac{\Delta S^0}{R} + \frac{E_a}{R}
\]

where: \( A \) is the frequency factor. The \( E_a \) were calculated from the plot of \( \ln b \) versus \( 1/T \) (K\(^{-1}\)) which the slope is \( E_a/R \) obtained from Figure 10. The obtained \( E_a \) from slope was 15.04 kJ/mol. The magnitude of \( E_a \) value lies in the range of 0-40 J/mol for physical sorption process [22]. This confirms that the ACPK-Ni(II) adsorption is physisorption.

The adsorption thermodynamic parameters were calculated from the Equations (15) and (16):

\[
\Delta G^0 = -RT \ln b
\]

\[
\ln b = -\frac{\Delta H^0}{RT} + \frac{\Delta S^0}{R}
\]

where: \( \Delta G^0 \) is a standard free energy, \( \Delta S^0 \) is entropy, \( \Delta H^0 \) is enthalpy, \( b \) is the Langmuir equilibrium constants and \( R \) is gas constant (8.314 J/mol/K) [19]. Van’t Hoff plots (\( \ln b \) versus \( 1/T \)) of ACPK-Ni(II) adsorption at different initial concentrations of Ni(II) give slope (\( -\Delta H^0/R \)) and intercept (\( \Delta S^0/R \)), while \( \Delta G^0 \) is calculated from Equation (15) and listed in Table 6.

A negative value of \( \Delta H^0 \) indicates that the adsorption process takes place by an exothermic process and the magnitude value of \( \Delta H^0 \) (-0.0309 J/mol) was less than 2.1 J/mol and the negative values of both \( \Delta H^0 \) and \( \Delta S^0 \) suggesting the physisorption of Ni(II) onto ACPK in nature and involving weak forces of attraction [23]. This result confirms the previous result which was obtained in DKR, Temkin isotherms and calorimetry data. The positive value of \( \Delta G^0 \) suggests the non-spontaneous nature of adsorption ACPK-Ni(II). The decrease in \( \Delta G^0 \) value with increasing in temperature indicates that the reaction is more favorable at high temperature.

**CONCLUSION**

The finding in this study revealed that palm kernel, which is an agricultural wastes material, can be applied in water treatment systems to remove Ni(II) ions from aqueous solutions. The effect of several parameters such as; pH, initial concentration, contact time and dose was investigated. Results show that the study ACPK has a good adsorption capacity for nickel. The best condition for the removal of nickel was observed at pH 4.6, concentration 20 mg/l, dose 70mg with in 80 min. FT-IR analysis indicated the presence on ACPK surface of hydroxyl and carboxyl groups which reduced after the addition of Ni(II). The equilibrium was the best described by Freundlich isotherm based on correlation coefficient, while the kinetic of the process was the best described by using second order at different ACPK doses indicating heterogenic multilayer adsorption and followed by Langmuir, Temkin and D-R isotherms. From DKR and calorimetry results, the sorption energies were 1.58 kJ/mol and 0.2981 J/g, respectively, indicating the
The adsorption process could be described by a pseudo-second order model. The removal efficiency of Ni(II) ions by ACPK decreases as the temperature increases. The kinetic of the process was best described by pseudo-second order at different ACPK. The thermodynamic studies revealed that the ACPK-Ni(II) adsorption is exothermic and physical nature process.

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چکیده

هسته نخل (PK) با فعال سازی شیمیایی (PK-3HNO_{3} هیدروفورمال) فعال شد تا آب‌های نیکل (II) (Ni(II)) از محلول‌های آبی حذف شود. تجزیه و تحلیل FT-IR نشان داد که فعال PK در pH 4.6، در دما 230 درجه سانتی‌گراد، در مدت 80 دقیقه فعالیت پایداری داشت. این فعال PK نیز در pH 4.6 نیکل (II) (Ni(II)) را تجزیه کرد و تعادل 80 دقیقه برسد. برای تعیین محتوای فلزات در کربن فعال PK از روش فلورسانس اشعه ایکس استفاده شد. در pH 4.6 مقدار متوسط 74% حذف یون Ni(II) را نشان داد. برای تعیین مقدار متوسط میزان انرژی آزاد گی (Dubinin-Radushkevich) و میزان فیزیکی (Temkin Isotherm) فعال PK، از مدل فلوتانس اشعه ایکس بهره‌مند شد. برای محاسبه E\text{a} (15.04 kJ/mol) فلهای گرمایش و ترمودینامیک به استفاده از مدل Temkin Isotherm از داده‌های میکرو کالری متری ایزوترمال تأیید شد.