On the linear coupling between fast and slow MHD waves due to line-tying effects

J., Terradas¹, J., Andries²,³, E., Verwichte⁴

¹Département de Física, Universitat de les Illes Balears, E-07122, Spain, e-mail: jaume.terradas@uib.es
²Centre Plasma Astrophysics and Leuven Mathematical Modeling and Computational Science Centre, Katholieke Universiteit Leuven, Leuven, B-3001, Belgium, e-mail: jesse.andries@wis.kuleuven.be
³Centre for Stellar and Planetary Astrophysics, Monash University, Victoria, 3800, Australia
⁴Centre for Fusion, Space and Astrophysics, Department of Physics, University of Warwick, Coventry CV4 7AL, UK, e-mail: Erwin.Verwichte@warwick.ac.uk

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ABSTRACT

Context. Oscillations in coronal loops are usually interpreted in terms of uncoupled magnetohydrodynamic (MHD) waves. Examples of these waves are standing transverse motions, interpreted as the kink MHD modes, and propagating slow modes, commonly reported at the loop footpoints.

Aims. Here we study a simple system in which fast and slow MHD waves are coupled. The goal is to understand the fingerprints of the coupling when boundary conditions are imposed in the model.

Methods. The reflection problem of a fast and slow MHD wave interacting with a rigid boundary, representing the line-tying effect of the photosphere, is analytically investigated. Both propagating and standing waves are analysed and the time-dependent problem of the excitation of these waves is considered.

Results. An obliquely incident fast MHD wave on the photosphere inevitably generates a slow mode. The frequency of the generated slow mode at the photosphere is exactly the same as the frequency of the incident fast MHD mode, but its wavelength is much smaller, assuming that the sound speed is smaller than the Alfvén speed.

Conclusions. The main signatures of the generated slow wave are density fluctuations at the loop footpoints. We have derived a simple formula that relates the velocity amplitude of the transverse standing mode with the density enhancements at the footpoints due to the driven slow modes. Using these results it is shown that there are possible evidences in the observations of the coupling between these two modes.

Key words. Magnetohydrodynamics (MHD) — Waves — Magnetic fields — Sun: atmosphere—Sun: oscillations

1. Introduction

In coronal loops there is evidence of the presence of fast standing magnetohydrodynamic (MHD) modes and slow (propagating and standing) MHD modes. Standing kink oscillations were first reported using TRACE by [Aschwanden et al. (1999)] and Nakariakov et al. (1999). Later, similar observations were analysed by, e.g., Schrijver & Brown (2000); Aschwanden et al. (2002); Schrijver et al. (2002). There is also clear evidence of the presence of propagating slow waves at loop footpoints (see De Moortel, 2009, for a review). These slow waves are most likely due to coupling between the underlying atmospheric layers since the dominant periods tend to be around 5 min, suggesting a possible link with solar p-modes. Furthermore, observations of standing slow modes in coronal loops, with periods largely above 5 min, have been also reported by a number of authors, using different instruments such as SOHO/SUMER (e.g., Wang et al. 2003a,b, 2007), Yohkoh/BCS (e.g., Mariska 2005, 2006) and more recently, Hinode/EIS (e.g., Erdelyi & Taroyan, 2008).

The theoretical interpretation of such a variety of oscillations is done, in most of the cases, in terms of uncoupled MHD waves. On one hand, transverse oscillations are identified as fast kink modes in the zero-β approximation, meaning that in the linear regime there is no longitudinal velocity along the magnetic tube. On the other hand, the reported slow modes are associated to acoustic modes, ignoring the coupling with the transverse motions. Although these identifications are useful and simple, we have to bear in mind that under realistic conditions MHD modes may couple. In general, the effect of gas pressure, inhomogeneities or boundary conditions lead to the coupling between fast and slow modes. As we shall see, a clear example of coupling comes from the line-tying condition, which amounts to considering the photosphere as providing a complete reflection of any coronal disturbance impinging from above. This is justified in most of the cases due to the large difference in densities between the photosphere and corona but it obviously neglects the important role of the transition region.

In this paper we study the simplest configuration in which fast and slow modes are mixed to understand the basics of mode coupling. We use the simple idea that a fast wave that is obliquely incident on a boundary will generate a slow wave. As far as we know, this issue has been addressed in slightly different contexts by, e.g., Stein (1971); Vasquez (1990); Oliver et al. (1992). A remarkable work about magnetohydrodynamic waves in coronal flux tubes including the line-tying effect was carried out by Goedbloed & Halberstadt (1994). In that work, it was clearly stated that pure fast or pure slow modes do not exist in
a line-tied coronal loop. Here we follow a different approach to analyse this problem. Our interest is in the effects of the application of line-tying conditions on fast and slow modes and in the possible observational fingerprints of this coupling.

2. Model and Dispersion relation

We consider first the simplest magnetic configuration where the magnetic field points in the $z$-direction, the plasma density and pressure are constant, and $v_A > c_s$ ($v_A$ is the Alfvén speed and $c_s$ the sound speed). Since the medium is homogeneous, we consider perturbations that are proportional to $e^{i(k_x x + k_z z)}$, meaning that waves propagate in the negative $x$ and $z$-directions. In this configuration, the linearised MHD equations (see Appendix A) lead to the well known dispersion relation for fast and slow MHD waves,

$$\omega^4 - \left(k_z^2 + k_x^2\right)\left(c_s^2 + \omega^2 + k_x^2\left(k_z^2 + k_x^2\right)c_s^2 v_A^2\right) = 0. \quad (1)$$

In our problem it is more convenient to assume that $\omega$ and $k_z$ are known and solve for $k_x$. The reason is that the frequency of an incoming wave remains constant in the reflection problem while the longitudinal wavenumber can change. The dispersion relation written as a biquadratic equation for $k_x$ is,

$$c_s^2 k_x^4 - \left[c_s^2 + v_A^2\right] \omega^2 - c_s^2 v_A^2 k_x^2 + \omega^2 \left[\omega^2 - k_z^2 \left(c_s^2 + v_A^2\right)\right] = 0. \quad (2)$$

We denote by $k_F$ and $k_S$ the fast and the slow longitudinal wavenumbers that are solutions to the previous biquadratic equation, i.e.,

$$k_F^2 = \frac{-B + \sqrt{B^2 - 4AC}}{2A}, \quad (3)$$

$$k_S^2 = \frac{-B - \sqrt{B^2 - 4AC}}{2A}, \quad (4)$$

where

$$A = c_s^2 v_A^2, \quad B = -\left[c_s^2 + v_A^2\right] \omega^2 - c_s^2 v_A^2 k_x^2, \quad C = \omega^2 \left[\omega^2 - k_z^2 \left(c_s^2 + v_A^2\right)\right]. \quad (5)$$

These wavenumbers are associated to the same frequency $\omega$ and same $k_z$, and can be approximated, using the small plasma-\(\beta\) assumption, by (e.g. Oliver et al. 1992)

$$k_F^2 \approx \frac{\omega^2}{v_A^2} - k_z^2 \left(c_s^2 + \frac{1}{v_A^2}\right), \quad (8)$$

$$k_S^2 \approx \frac{\omega^2}{c_s^2}. \quad (9)$$

These approximations will turn out to be useful in the following sections. According to Eq. (8) the fast wavenumber may become purely imaginary for a certain choice of the parameters, indicating that the wave is evanescent. Hereafter, we will restrict our analysis to propagating waves.

It can be seen from the linearised MHD equations that the velocity polarisation for fast and slow modes is given by the following expression

$$v_z = \frac{c_s^2 k_F k_x}{\omega^2 - k_x^2 c_s^2} v_s. \quad (10)$$

where $k_z$ is either $k_F$ or $k_S$. Note that if we change the direction of propagation along the field, $k_z$ changes to $-k_z$ and the polarisation also changes sign. In our configuration and in the regime that we are interested ($v_A > c_s$), since $k_F < k_S$, fast modes are characterised by long wavelengths and by $v_A > v_s$, while slow modes have short wavelengths and $v_s < v_A$. The slow modes have a larger compression since the wavelength is small in comparison with the fast modes.

3. Propagating waves: the reflection problem

3.1. Fast MHD wave reflection

We consider the most elementary problem to show the process of mode coupling due to boundary conditions. A fast MHD wave travels downwards (in the negative $z$-direction) and represents an incoming wave. This wave interacts with the photosphere (located at $z = 0$, where line-tying conditions are applied) and reflects (now travelling upwards). The amplitude of the fast incoming wave is $F_1$, while the amplitude of the reflected fast wave is $F_R$. To satisfy the boundary conditions a slow MHD wave, also moving upwards, must be generated at $z = 0$. The excited slow mode has an amplitude $S_G$. It is easy to write the velocity components using the polarisation of fast and slow waves, given by Eq. (10), and the proper sign of the longitudinal wavenumber,

$$V_z = F_1 e^{i(\omega t + k_z x + k_x z)} + F_R e^{i(\omega t + k_z x - k_x z)}$$

$$V_z = F_1 \frac{c_s^2 k_F k_x}{\omega^2 - k_x^2 c_s^2} e^{i(\omega t + k_z x + k_x z)} - F_R \frac{c_s^2 k_F k_x}{\omega^2 - k_x^2 c_s^2} e^{i(\omega t + k_z x - k_x z)}.$$ 

Now boundary conditions are imposed at $z = 0$, representing the location of the photosphere. We use line-tying conditions, i.e., $V_z(z = 0) = V_s(z = 0) = 0$. According to Eqs. (11) and (12) the following conditions must be satisfied,

$$F_1 + F_R - S_G \frac{\omega^2 - k_x^2 c_s^2}{c_s^2 k_F k_x} = 0,$$

$$F_1 - F_R + S_G \frac{\omega^2 - k_x^2 c_s^2}{c_s^2 k_F k_x} = 0.$$ 

The solution in terms of the amplitude of the incoming wave (which is an arbitrary parameter) is

$$F_R = \frac{F_1}{S_G} \frac{(\omega^2 - k_x^2 c_s^2) k_F + (\omega^2 - k_x^2 c_s^2) k_S}{(\omega^2 - k_x^2 c_s^2) k_F - (\omega^2 - k_x^2 c_s^2) k_S},$$

$$S_G = \frac{F_1}{F_1} \frac{2 c_s^2 k_F k_S}{(\omega^2 - k_x^2 c_s^2) k_F - (\omega^2 - k_x^2 c_s^2) k_S}.$$ 

The coefficients depend on $\omega$, $k_z$ (same for the three waves) and on longitudinal wavenumbers, $k_F$ and $k_S$, which can also be expressed in terms of $\omega$, $k_z$ by using Eqs. (3) and (4).

When there is no coupling between fast and slow modes (i.e., $k_z = 0$) we have that $|F_R/F_1| = 1$ because $\omega^2 = k_x^2 c_s^2$, while $S_G/F_1 = 0$. Hence, there is a complete reflection of the incoming fast mode while the slow mode is absent. When there is coupling, the reflection coefficient for the slow mode is always different from zero, meaning that the incoming fast MHD wave
according to Eqs. (19) and (20). The sound speed is given by Eq. (18) while the dotted line shows the position of the maximum. The dashed line represents the approximation given as a function of the horizontal wavenumber for three different values of the sound speed.

Fig. 1. Amplitude of reflected fast mode given by Eq. (14) as a function of the horizontal wavenumber for three different values of the sound speed.

invariably generates a slow mode at the boundary. In Figure 1, the reflection coefficient of the fast wave, i.e., \( F_R/F_I \), is plotted as a function of \( k_x \) for different values of the sound speed. The coefficient is close to unity for values of sound speed low in comparison with the Alfvén speed, meaning that reflection is almost total. However, for relatively large values of \( c_s/\nu_A \) the curves clearly show a minimum indicating that the reflection of the fast wave is less efficient.

Fig. 2. Amplitude of the generated slow mode given by Eq. (15) as a function of the horizontal wavenumber for three different values of the sound speed. The dashed line represents the approximation given by Eq. (15) while the dotted line shows the position of the maxima according to Eqs. (19) and (20).

In Figure 2, the reflection coefficient of the slow wave, i.e., \( S_G/F_I \), is plotted. The behaviour of the reflected slow mode amplitude is basically opposite of the reflected fast wave. The curves show a maximum at the locations where the generation of the slow mode is more efficient. Again the value at the maximum strongly depends on the ratio of the sound speed to the Alfvén speed, and corresponds to a \( k_x \) which is very similar to \( k_F \). The location of the maximum can be analytically determined from Eq. (15) and using the approximation of the slow mode frequency, \( \omega^2 \approx k_S^2 c_s^2 \).

\[
S_G \approx \frac{2k_F V_F}{k_F^2 - k_S^2}
\]  

(16)

Since the frequency is fixed, we have from the approximate expressions (8)-(9) for \( k_S^2 \) and \( k_F^2 \) the following relation

\[
k_F^2 \approx k_S^2 \left(1 + \frac{\nu^2}{c_s^2}\right) + k_F^2 \frac{\nu^2}{c_s^2}
\]

(17)

Inserting this expression in Eq. (16) we find that

\[
S_G \approx \frac{2c_F^3 k_F}{k_F^2 \left(c_s^2 - \nu^2\right) - k_S^2 \left(c_s^2 + \nu^2\right)}.
\]

(18)

This is a good approximation to the slow mode reflection coefficient (see dashed line in Figure 2), at least for the case \( c_s \ll \nu_A \). It is used to determine the location of the maxima of the curves in Figure 2. Imposing that the derivative of Eq. (18) is equal to zero it is found that the maximum corresponds to

\[
k_{x,\text{max}} \approx k_F \sqrt{\frac{\nu^2 - c_s^2}{\nu^2 + c_s^2}}
\]

(19)

and the value of the reflection coefficient for this horizontal wavenumber is

\[
\left| \frac{S_G}{F_I}\right|_{\text{max}} \approx \frac{c_s^2}{\sqrt{\nu^2 - c_s^2}}
\]

In Figure 2, the location and value of the maximum is represented by a dotted line. There is excellent agreement between the approximation and the location of the maximum calculated using the original expression for the reflection coefficient of the slow mode (Eq. (15)). From Eq. (20) we see that the maximum amplitude of the generated slow wave depends only on the \( \beta \) of the plasma.

Once we know the coefficients it is straightforward to calculate magnitudes of interest such as the density perturbation of the slow reflected wave as a function of amplitude of the incoming fast wave. As we will discuss later, these magnitudes can be directly related to real observations. From the continuity equation (see Appendix A) the density perturbation for the slow mode is

\[
|\rho_1/\rho| = \frac{1}{\omega} \left(k_x V_x + k_z V_z\right) = \frac{k_S}{\omega} \left(1 - \frac{\omega^2 - k_S^2 c_s^2}{k_F^2 - k_S^2 c_s^2}\right) S_G.
\]

(21)

Using again the fact that \( \omega^2 \approx k_S^2 c_s^2 \) and Eq. (20) we find

\[
|\rho_1/\rho|_{\text{max}} \approx \frac{c_s F_I}{\sqrt{\nu^2 - c_s^2}}
\]

(22)

This equation relates the maximum density perturbation associated to the generated slow mode with the velocity amplitude of the incident fast wave.

3.2. The time-dependent problem

The time-dependent problem is numerically solved to demonstrate the mode coupling described in the previous section. The temporal evolution of the waves and specially their interaction with the boundaries provides a clear picture of the coupling and complements the analytical results.
In this numerical experiment a pulse in the \( v_x \) component is generated at \( t = 0 \). This pulse has the following form

\[
v_x(z, t = 0) = v_0 \cos(kz) e^{-(t/t_0)^2}, \quad (23)
\]

\[
v_c(z, t = 0) = 0, \quad (24)
\]

and the rest of the perturbed variables are set to zero. This particular profile has the property that represents a localised wave packet but with a rather well defined wavelength (basically given by \( \lambda = 2\pi/k \)). To show the interaction of the fast mode with a single boundary, rigid conditions are applied at \( z = 0 \) \( (v_x(z = 0) = v_c(z = 0) = 0) \) while open conditions are imposed at \( z = L \). The linearised time-dependent MHD equations (see Appendix A) are numerically solved using standard finite differences techniques.

The temporal evolution of the two velocity components is plotted in Figure 3. The initial disturbance excites the fast mode but also the slow mode since the initial perturbation does not satisfy the velocity polarisation relation, given by Eq. (10). The excited fast and slow modes split in two identical modes propagating in opposite directions (top panel). The fast and slow waves travelling to the left are denoted as \( F_L \) and \( S_L \), respectively, while \( F_R \) and \( S_R \) move to the right. Once the \( F_L \) mode reaches the rigid boundary \( (z = 0) \), it gets reflected (see middle panel) with an amplitude \( F_R \) and a slow mode is generated (see dotted line), i.e., the \( S_G \) mode according to the notation introduced above. The slow wave packet has a typical wavelength much smaller than the fast wavelength \( (k_F \ll k_S) \). At the other boundary \( (z = L) \) the fast mode \( F_R \) leaves the system due to the transparent boundary conditions. At later times (bottom panel) the \( S_G \) and \( S_I \) modes, moving in opposite directions, start to superpose, while the \( F_R \) and \( S_I \), travelling in the same direction also interfere.

The amplitudes of reflected fast and slow waves estimated from the time-dependent problem agree quite well with the calculations based on the analytical reflection coefficients given by Eqs. (14)–(15). Note that these equations were derived for purely sinusoidal and monochromatic waves but the initial packet is well represented by a dominant frequency (wavelength), and this is the reason of the agreement with the analytical results.

### 3.3. Slow MHD wave reflection

Although we are mainly interested in the fast reflection problem, for completeness the slow mode reflection problem is also studied. The difference with respect to the fast MHD reflection problem is that reflection of the slow MHD mode at the boundary generates a fast MHD mode. The velocity components for this problem are

\[
V_x = \bar{S}_1 \frac{\omega^2 - k_F^2 \epsilon_x^2}{c_I^2 k_F k_S} e^{i(\omega t + k_F x - k_S z)} - \bar{S}_R \frac{\omega^2 - k_S^2 \epsilon_x^2}{c_I^2 k_F k_S} e^{i(\omega t + k_F x - k_S z)} - \bar{F}_G e^{i(\omega t + k_F x - k_S z)},
\]

\[
V_c = \bar{S}_1 \frac{\epsilon_x}{c_I^2} e^{i(\omega t + k_F x - k_S z)} + \bar{S}_R \frac{\epsilon_x}{c_I^2} e^{i(\omega t + k_F x - k_S z)} - \bar{F}_G \frac{c_I^2 k_F k_F}{\omega^2 - k_F^2 \epsilon_x^2} e^{i(\omega t + k_F x - k_S z)}. \quad (26)
\]

Applying rigid boundary conditions the following coefficients for the reflected slow mode and the generated fast mode are found

\[
\bar{S}_R = \frac{\omega^2 - k_S^2 \epsilon_x^2}{c_I^2} k_F + \left( \frac{\omega^2 - k_F^2 \epsilon_x^2}{c_I^2} k_S \right) \bar{S}_1 \frac{\omega^2 - k_F^2 \epsilon_x^2}{c_I^2} k_F + \left( \frac{\omega^2 - k_F^2 \epsilon_x^2}{c_I^2} k_S \right)
\]

\[
\bar{F}_G = \frac{2}{c_I^2} \frac{\omega^2 - k_S^2 \epsilon_x^2}{c_I^2} \frac{\omega^2 - k_S^2 \epsilon_x^2}{c_I^2} k_F + \left( \frac{\omega^2 - k_F^2 \epsilon_x^2}{c_I^2} k_S \right) k_S.
\]

It is worth noting that the reflection coefficient of the slow mode is exactly the same as the reflection coefficient of the fast mode given by Eq. (14).

### 4. Standing waves

Once we understand the reflection of a propagating fast and a propagating slow wave at a rigid boundary we extend our anal-
These very simple expressions give the order of the maximum reflected mode as a function of the transverse velocity amplitude at while the density perturbation is.

Another way to analyze this problem is to solve the full standing problem. This was already done by Oliver et al. (1992) and Goedbloed & Halberstadt (1994) and it is based on the superposition of the fast reflection problem plus the slow reflection problem. The perturbation scheme and the full eigenmode problem give similar results, except where the solutions are completely mixed, i.e., when the slow mode component is not small in comparison with the fast component. This takes place around the “avoided crossings” in the dispersion diagram (see Oliver et al. (1992) for further details).

The advantage of the perturbation scheme is that we can still obtain simple approximations for the velocity and density changes around the footpoints. Let us assume that an initial disturbance mostly excites the standing pattern in the \( v_x \) component. This standing wave is composed by the superposition of two identical propagating waves travelling in opposite directions. We concentrate on the fundamental mode, having a maximum at \( z = L/2 \) and a node of the velocity at the boundaries. A propagating slow wave is induced by the reflection at the boundaries of the incident propagating fast wave that forms part of the standing fast pattern. Hence, if the transverse velocity amplitude of the standing fast wave at the loop apex is \( V_0 \) the amplitude of the incoming fast wave is \( V_0/2 \) (the reflected fast wave will also have an amplitude of \( V_0/2 \) in our approximation). Once we know this amplitude it is easy to estimate the velocity or density fluctuations associated to the slow mode using the results of the propagation problem. According to the analysis performed in the previous section (see Eqs. (29) and (30))

\[
|v_x|_{\text{max}} \approx \frac{c_s^2}{\sqrt{v_A^4 - c_s^4}} \frac{V_0}{2},
\]

and

\[
\left| \frac{\rho}{\rho_{\text{max}}} \right| \approx \frac{c_s}{\sqrt{v_A^4 - c_s^4}} \frac{V_0}{2}.
\]

These very simple expressions give the order of the maximum velocity and density perturbations associated to the slow reflected mode as a function of the transverse velocity amplitude at the loop apex and the characteristic speeds of the configuration. When \( c_s \ll v_A \) the velocity perturbation reduces to

\[
|v_x|_{\text{max}} \approx \frac{c_s^2}{v_A^2} \frac{V_0}{2} = \frac{1}{4} y\beta V_0,
\]

while the density perturbation is

\[
\left| \frac{\rho}{\rho_{\text{max}}} \right| \approx \frac{c_s}{v_A^2} \frac{V_0}{2} = \frac{1}{4} y\beta \frac{V_0}{c_s}.
\]

It is worth to calculate the order of magnitude of velocity and density fluctuations around the footpoint. Let us take typical values: \( v_A = 800 \text{ km s}^{-1}, c_s = 200 \text{ km s}^{-1} \), \( V_0 = 80 \text{ km s}^{-1} \). Thus, the velocity perturbation according to Eq. (29) is \( |v_x|_{\text{max}} \approx 2.5 \text{ km s}^{-1} \). Using Eq. (30) we find that the density fluctuation associated to the slow mode is \( |\rho/\rho_{\text{max}}| \approx 1.25\% \). These density perturbations, although small, should be detectable with the current instruments. Obviously, larger sound speeds and or small Alfvén velocities would result in an increase of velocity and density fluctuations.

The previous estimations are based on the assumption that the excited slow modes do not have time to reach the opposite footpoint and reflect. If this is the case, the problem is more difficult since the slow modes interfere and the velocity and density changes can be larger than those given by Eqs. (29)-(30). It is also important to remark that the density perturbation associated to the fast standing mode has the same profile as the velocity (the \( v_x \) component), therefore the fast density perturbation is zero at the footpoints (and maximum at the apex), this explains why it is enough to consider only the density changes associated to the excited slow modes around the footpoints.

### 4.1. The time-dependent problem

Now the time-dependent problem is solved. The initial perturbation, representing the excitation of a mainly fast standing wave, has the following profile,

\[
v_x(z, t = 0) = v_0 \sin (kz),
\]

(33)

\[
v_x(z, t = 0) = 0.
\]

(34)

### 4.1.1. Rigid boundary conditions

Line-tying conditions are applied at the two loop footpoints. We choose the longitudinal wavenumber that excites the fundamental standing fast MHD mode, i.e., \( k = \pi/L \). The results, represented in Figure 4, manifest the generation of slow modes at the footpoints (top panel). The fast mode drives slow modes which move in the direction of the loop apex, located at \( z = L/2 \) (see middle panel). At a certain time (when \( z = L/2 \)=) the interference between the opposite propagating slow waves is produced. Since the two slow waves are identical but travelling in opposite directions a quasi-standing pattern is visible (see the profile of \( v_x \) around \( z = 5a \) in the bottom panel). Eventually, slow modes reach the opposite footpoint and get reflected. Under such conditions the inverted process takes place, i.e., the slow mode generates a fast mode. Nevertheless, this problem would take us too far and it is out of the scope of this work. However, it is worth to note that depending on the equilibrium and wave parameters the generated slow modes might match the frequency of a standing slow eigenmode of the loop. This means that since the slow mode is driven by the fast standing mode, the frequencies of the slow standing and fast standing waves will be basically the same and the modes will have a highly mixed nature. This takes place around the “avoided crossings” in the dispersion diagram.

### 4.1.2. Sharp photosphere-corona transition

From the previous results we might think that the generation of slow modes takes place only when rigid boundary conditions are imposed. In order to address this question, instead of line-tying conditions, a density transition between the corona and the photosphere is considered. As density profile we use the following
Fig. 4. Time evolution of the standing fast excitation given by Eqs. (33)-(34). The continuous line represents the $v_x$ component while the $v_z$ component is plotted with a dotted line (its amplitude has been multiplied by a factor 10 for visualisation purposes). For this simulation $ka = \pi/10$, $v_0/v_A = 1$, $k_xa = 1.5$ and $c_s/v_A = 0.2$.

The parameter $w$ measures the width of the transition between the photosphere, with density $\rho_{ph}$, and corona, with density $\rho_c$. The density contrast is set to $\rho_{ph}/\rho_c = 10^8$. Non-reflecting conditions are imposed at the boundaries, now placed below the photosphere. The details of the model used to represent the transition photosphere-corona are not important since our focus is on the generated slow modes. The equilibrium gas pressure is set to the same constant value in the corona and photosphere to have magnetohydrostatic equilibrium.

The results of the time-dependent simulation are plotted in Figure 5. There are some differences with respect to the behaviour found for the perfectly reflecting boundaries. For example, the system now allows the energy to escape through the photosphere, i.e., there is a transmitted fast (and slow wave). This means that the energy can leak through the photosphere but this is not visible in Figure 5 because the amplitude is very small.

Nevertheless, the primary result here is that a similar slow mode generation in comparison with the case of reflecting boundaries is produced in the coronal part (compare Figures 4 and 5). The results are qualitatively similar, thus, the overall conclusion is that nonuniformity causes the coupling between fast and slow modes in a similar way as line-tying conditions.

5. Link with observations

It is interesting to look for signatures of the mode coupling studied in this work in the observations. Recently, Verwichte et al. (2010), have reported, using combined observations from TRACE and EIT/SoHO, intensity fluctuations at one loop footpoint with basically the same period, around 40 min, as the fast transverse oscillation of the loop. This long periodicity indicates that the origin of these density oscillations is most probably not photospheric. Verwichte et al. (2010) suggest that the intensity

\[ \rho = (\rho_{ph} - \rho_c) e^{-\frac{z}{w}} + (\rho_{ph} - \rho_c) e^{-\frac{z-L_w}{w}} + \rho_c. \]
oscillations are due to variations in the line of sight column depth produced by the changes in the loop inclination as it oscillates with the transverse kink mode. This would explain the coincidence in periods, and also in the damping times.

According to our study an alternative explanation for the intensity variations reported by [Verwichte et al. 2010] is done in terms of the coupling between fast and slow waves due to the line-tying conditions. The similarity of the periods of the transverse mode and the intensity fluctuations is explained by our model where the excited slow wave, and the corresponding intensity oscillation, has the same periodicity as the transverse loop motion. [Verwichte et al. 2010] show intensity variations associated with a transverse oscillation in a large loop of 690±60 Mm length. The oscillation, which is a horizontally polarised fundamental kink mode, has a period of $P=2418±5$ s. Therefore, the phase speed is equal to $v_p=580±50$ km s$^{-1}$. For a thin loop in the long wavelength limit, this phase speed tends to the kink speed, $c_k$, of a cylindrical tube. If the intensity oscillation is associated with a slow magnetosonic mode with the same periodicity as the kink mode, then its wavelength is equal to $\lambda_s=c_kP=(c_p/v_p)2L$. For a temperature between 0.9 and 1.8 MK, the coronal sound speed is in the range 144-198 km s$^{-1}$. Hence, $\lambda_s=(0.30±0.07)2L$. For a standing mode, this translates into a wavenumber $n=\sqrt{vp/\lambda_s}=3.3±1.0$. The EIT observations suggest that the intensity variations at the two footpoints of the loop oscillate in anti-phase. Hence, the mode, if standing, should be an odd harmonic. Figure 6 shows the relative profile of intensity variations as a function of loop distance. The relative intensity has an amplitude of approximately 13%, which translates into a density perturbation with an amplitude, $\Delta \rho/\rho = \pm 6.5\%$. This is consistent with the observed density amplitude (around 6.5%).

In another work, [Verwichte et al. 2005] also reported intensity oscillations associated with a kink mode seen by EUV on board of STEREO and interpreted these as resulting from variations in the line-of-sight column depth due to the loop showing a varying aspect to the observer. The measured relative density amplitude is 2.5%, and located around to loop top. Can this observation be explained by a slow mode instead? In that observation, the key parameters that were measured are $L=340±15$ Mm, $v_p=1100±100$ km s$^{-1}$, $v_\lambda=35±9$ km s$^{-1}$ and $v_\lambda=800±100$ km s$^{-1}$. For the peak temperature of the EUV 171Å bandpass of 0.9 MK, $c_s=144$ km s$^{-1}$. The slow mode would have a wavenumber $n=7±1$ (in the case of a standing mode), corresponding to a wavelength of about $\lambda_s=90±10$ Mm. Again, using Eq. (30), we calculate $|\rho_1/\rho_{\text{max}}|=0.4\%$, which is negligibly small. Therefore, for this observation, the slow mode is not able to explain the observed intensity variations. The main difference with respect to the case studied by [Verwichte et al. 2010] is that the density perturbations are located around the loop top instead of the loop footpoints.

6. Discussion and conclusions

In this work we have investigated the possible effects of linear coupling between fast and slow modes that takes place due to the reflection at the photosphere. We have shown, by solving the reflection problem, that the transverse motion of the loop produces slow MHD waves as long as the fast wave is obliquely incident on the boundary. These slow waves are manifested as propagating density fluctuations with the same frequency as the standing transverse mode and are generated at the loop footpoints. The wavelength of these slow modes is basically given by $k_s = \omega/\gamma$, and since $v_\lambda > c_s$ their wavelength is smaller than that of the corresponding fast standing transverse mode. Moreover, we have derived using the reflection coefficient of the slow mode, simple analytical expressions that relate the transverse displacement at the loop top with the amplitude of the density fluctuations produced at the footpoints. The coupling between fast and slow is proportional to the plasma-$\beta$, indicating that under coronal conditions it will be weak in general. However, it is proportional to the amplitude of oscillation of the fast mode, which can be large in some cases, and close to the footpoints, i.e., close to the photosphere, the ratio between the sound and Alfvén speeds can increase. Ideally, from the properties of the reflected slow modes, we could have indirect information about the real line-tying conditions in coronal loops and realistic values of the sound speed near the footpoints.

The generated slow waves can eventually form a standing pattern along the loop. Thus, mode coupling might provide an excitation mechanism of standing slow modes, different from the driven photospheric origin usually emphasised in the literature. However, since the sound speed is assumed to be smaller than the Alfvén speed, the time required for the slow mode to travel along the loop and reflect at the footpoint is much larger than that of the fast MHD mode. This means that slow standing modes will need much more time than fast standing modes to build up.

![Fig. 6. Relative profile of intensity variations seen in a transversely oscillating loop studied by Verwichte et al. (2010) using TRACE as a function of distance along the loop. The solid circle is the measurement of the intensity variation at the footpoint. The long-dashed and dashed curves are functions -0.13sin(3\pi/\lambda) and -0.13sin(5\pi/\lambda), respectively, representing a possible third or fifth standing harmonic of the slow mode.](image-url)
Nevertheless, if the wavelength of the slow modes is very short they might be damped by thermal conduction before the standing wave is formed.

It has been shown that in the observations analysed by Verwichte et al. (2010) there are possible fingerprints of the coupling between fast and slow modes due to line-tying, providing an alternative explanation to the effects of integration along the line of sight proposed by these authors. However, in the observations studied by Verwichte et al. (2009) the mechanism is unable to explain the intensity oscillations. One of the reasons might be that the density changes observed in this event are reported around the loop apex, while the estimations are based on propagating waves around the footpoints. In the case of the standing pattern the density fluctuations can be much larger. Further analysis of other observations will help to test the linear coupling as an operative mechanism in coronal loops.

It is worth to mention that the mode coupling discussed in this work is a purely linear effect. It is unrelated to the nonlinear coupling between fast and slow modes due to the ponderomotive force (see Hollweg, 1971; Rankin et al., 1994 or the parametric coupling studied by Zaqarashvili & Ofman, 2002 or 2003). It is also different from mode conversion that takes place when \( c_s = v_A \). Line-tying boundary conditions are the responsible ingredients of the coupling, but we have shown that they are not the only way in which fast and slow waves may couple. A sharp transition between the corona and the photosphere produces the generation of slow modes, i.e., a change in the properties of the medium, for example the transition region, leads inevitably to the coupling.

Our theoretical model is based on a Cartesian geometry without a density enhancement representing a loop. For this reason, it is necessary to improve the model by including a slab or a cylinder that mimics the effect of a dense magnetic tube. This will complicate the mathematical problem of the reflection at the boundary, and it might be difficult to derive simple analytical expressions. For example, in a cylindrical model, the eigenfunctions of the slow and fast MHD waves have different radial dependences and might share the same azimuthal wavenumber (playing basically the role of \( k_r \) in the present work). This issue will be addressed in a future study.

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Appendix A:

We use the linearised MHD equations of the momentum, induction, energy and continuity equation. Assuming Fourier analysis in the \( x \)- direction we have:

\[
\frac{\partial v_x}{\partial t} = \frac{1}{\rho} \left( -\frac{ik_z p_1 - ik_x B_0}{\mu} b_x + \frac{B_0}{\mu} \frac{\partial b_x}{\partial z} \right),
\]

(A.1)

\[
\frac{\partial v_z}{\partial t} = \frac{1}{\rho} \frac{\partial p_1}{\partial z},
\]

(A.2)

\[
\frac{\partial b_x}{\partial t} = B_0 \frac{\partial v_x}{\partial z},
\]

(A.3)

\[
\frac{\partial b_z}{\partial t} = -B_0 ik_x v_x,
\]

(A.4)

\[
\frac{\partial p_1}{\partial t} = -\gamma p \left( ik_x v_x + \frac{\partial v_x}{\partial z} \right),
\]

(A.5)

\[
\frac{\partial p_1}{\partial t} = -\rho \left( ik_x v_x + \frac{\partial v_x}{\partial z} \right).
\]

(A.6)

In these equations \( B_0 \) is the equilibrium magnetic field and \( \rho \) and \( p \) the equilibrium density and gas pressure, respectively. The rest of the variables correspond to the perturbed magnitudes. To eliminate the imaginary complex numbers we simply define

\[
v_x^* = i v_x,
\]

(A.7)

\[
b_x^* = i b_x.
\]

(A.8)

With this transformation the time-dependent equations are solved using standard numerical techniques.

The dispersion relation, given by Eq. (\ref{eq:dr}), is easily derived assuming in the previous equations a temporal dependence of the form \( e^{\omega t} \) and a spatial dependence with the \( z \)-coordinate of the form \( e^{ik_z z} \). We have used the following standard definitions for the Alfvén and sound speeds:

\[
v_A = \frac{B_0}{\sqrt{\mu \rho}},
\]

(A.9)

\[
c_s = \sqrt{\gamma \rho}
\]

(A.10)