Research Article

Fabrication and Characterization of In Situ Synthesized SiC/Al Composites by Combustion Synthesis and Hot Press Consolidation Method

Hongyu Yang,1 Erting Dong,2 Bingqi Zhang,3 Yanyan Yuan,1 and Shili Shu4

1National Demonstration Center for Experimental Materials Science and Engineering Education, Jiangsu University of Science and Technology, Zhenjiang 212003, China
2Department of Materials Engineering, Henan Institute of Technology, Xinxiang 453000, China
3Datang Northeast Electric Power Test And Research Institute, No.3195 Weishan Street, Changchun 130000, China
4State Key Laboratory of Luminescence and Applications, Changchun Institute of Optics, Fine Mechanics and Physics, Chinese Academy of Sciences, Changchun 130033, China

Correspondence should be addressed to Shili Shu; shushili@ciomp.ac.cn

Received 27 September 2017; Revised 8 November 2017; Accepted 20 November 2017; Published 11 December 2017

1. Introduction

The SiC reinforced aluminum matrix (SiC/Al) composites have become very promising materials in the fields of semiconductor packaging, automobile, and aeronautics industry due to their high thermal conductivity and low coefficient of thermal expansion, lightweight, high strength, and wear-resistance [1–5]. For example, the SiC/Al composites which we fabricated in this work can be used for engine piston and heat sink [6, 7]. Therefore, the SiC/Al composites are actively investigated in an effort to improve their comprehensive properties [8, 9].

In recent years, several methods have been applied to fabricate the SiC/Al composites, such as stir casting [10–12], hot pressing sintering [2, 13], powder metallurgy [8], liquid pressing process [14], high pressure solidification [15], and squeeze-cast [16]. Nevertheless, in these methods the reinforcing SiC particles are usually directly added to Al matrix to form ex situ SiC/Al composites. The ex situ SiC/Al composites have several inherent disadvantages [17–19]: (I) the reinforcing SiC particles is difficult to be uniformly dispersed into the Al matrix; (II) during the incorporation of particles, interfaces between SiC and Al matrix are easy to be contaminated. In addition, cracks could appear in the interfaces due to the formation of thin oxide layers on the surfaces of the particles. To overcome these drawbacks stated above, the research on Al matrix composites is moving in two directions: one is metallic glasses replaced by typical ceramic particles reinforcements [20–22]; the other is in situ methods replaced by traditional ex situ methods. Compared to the ex situ methods, in the in situ methods the reinforcement is synthesized through a chemical reaction among the pristine elemental materials themselves in the matrix [23, 24]. Therefore, the interfaces between...
reinforcement and matrix are very clean, and the bonding strength is strong. At the same time, the reinforcing particles formed by the in situ method are finer in size and uniformly distributed into the matrix [25, 26]. Nie et al. [27] fabricated the in situ SiC/Al composites by the structural evolution of TiC in Al-Si melt. They reported that the synthesis of the SiC particles occurred via the gradual reaction between the TiC and the Si atoms, and the needle-like TiAl₃Si₄ phase simultaneously is formed. The needle-like TiAl₃Si₄ phase plays a detrimental role in the mechanical properties of the composites. Du et al. fabricated the in situ SiC/Al composites by liquid-solid reaction [28] and master alloy casting method [6, 29], respectively. They reported that the formation of SiC particles was attributed to the reaction between dissolved Si atoms and Al₄C₃ intermediate phase, which indicates that the fabrication of in situ SiC/Al composites through gradual phase transformation mechanism was feasible. However, the formation process of the in situ SiC particles is reversible if the intermediate phase Al₄C₃ is as carbon source. Therefore, different reaction conditions will significantly impact on the synthesis reaction. Meanwhile, the effects of Si/C ratio and holding time on the fabrication of the in situ SiC/Al composites have not been involved in previous work. Besides, to our knowledge, the method of the combustion synthesis and hot press consolidation is another effective way for the fabrication of in situ SiC/Al composites [30–32]. This method takes advantage of low energy requirement, one step forming process, density, and high purity of the products. Thus, the objectives of the present work are to fabricate the in situ SiC/Al composites in an Al-C-Si system using the method of the combustion synthesis and hot press consolidation. Meanwhile, the effects of Si/C mass ratio and holding time on the phase constitution, microstructure, and hardness of the in situ SiC/Al composites were investigated.

### 2. Experiment

In this work, commercial Al powders, Si powders, and C-black powders were used for making the powder blends. The detailed information of the raw materials is given in Table 1. The SEM images and particle size distribution are shown in Figure 1.

The detailed fabrication process procedure is shown as follows: First, Al powders and carbon powders were mixed with different Si/C mass ratio (as shown in Table 2). The dispersion method was a dry process using ball milling. The mixtures of powders were sealed into a 500 mL volume zirconia jar together with ZrO₂ milling balls (ball to powder mass ratio of 10). The jar was aerated with argon gas to protect the powder from excessive oxidation. The milling was carried out on a roller ball milling machine at 35 rpm for 8 h. Second, the mixtures were cold pressed into cylindrical compacts with the diameter of 28 mm and height of 30 mm. Third, the powder compact was contained in a graphite mold. And the graphite mold with powder compact was put in a self-made vacuum thermal explosion furnace as illustrated in Figure 2, in which the combustion synthesis and hot press consolidation experiment was conducted. During this process, the temperature was monitored by W5-RE26 thermocouples and the heating rate was 20°C/min. The furnace temperature was set to 950°C, and after different holding time, the pressure of 30 MPa was applied. Finally, the compact was cooled inside the furnace to room temperature. Notice that the compact was heated and cooled in a vacuum environment (≤5 × 10⁻² Pa).

The phase constitution of the samples was investigated by X-ray diffraction (XRD, Model D/Max 2500PC, Rigaku, Tokyo, Japan) with Cu Kα (λ = 0.154 nm) radiation. The samples were firstly mechanical ground, then polished down to a diamond finish of 1.5 μm, and then etched in a hybrid solution of 5% HCl and 95% ethanol at room temperature for 5 s for the microstructural observations. The morphology was observed by scanning electron microscopy (SEM, Model Evo18 Carl Zeiss, Oberkochen, Germany). The size measurement and distribution statistics of SiC particle were performed with the Nano Measurer software. The hardness tests were conducted on a XHB-3000 digital Brinell hardness tester according to the ASTM E10-14 standard.

### 3. Results and Discussion

#### 3.1. Fabrication of In Situ SiC/Al Composites

The in situ SiC/Al composite was firstly fabricated in an Al-Si-C system with the Si/C mass ratio of 5:1 at 950°C and holding time for 15 min. Figure 3 shows the XRD pattern of the fabricated SiC/Al composite. It can be seen that the in situ SiC/Al composite was successfully fabricated and no Al₄C₃ phase existed in the composite. Figure 4(a) shows the SEM images of the etched surfaces of the fabricated SiC/Al composite. It can be observed that a large quantity of irregular blocky-shaped particles is distributed in the Al matrix. By the EDS

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**Table 1:** Characteristics of the raw materials used in experiment.

| Raw materials | Purity (wt.%) | Particle size | Morphology                | Production units                     |
|---------------|--------------|---------------|---------------------------|-------------------------------------|
| Al            | ≥99.7        | <48 μm mesh   | Spherical particles       | Shanghai ST-Nano Science and Technology Co., Ltd. |
| Si            | ≥99.9        | <48 μm mesh   | Irregularly shaped particles |                                      |
| C-black       | ≥99.9        | 100 ± 20 nm   | Spherical particles       |                                      |

**Table 2:** Weight of the raw materials with different Si/C mass ratio used in the fabrication procedure.

| Si/C mass ratio | Al  | Si  | C   |
|-----------------|-----|-----|-----|
| 4:1             | 75g | 20g | 5g  |
| 5:1             | 70g | 25g | 5g  |
| 6:1             | 65g | 30g | 5g  |
analysis of the content of Si and C elements in (Figure 4(b)), the irregular blocky-shaped particles are identified as SiC. According to Du et al. reports [28], it can be known that the formation of SiC is achieved via the replacement reaction of Si and Al₄C₃. Hence the obtained SiC particles are liable to inherit morphological characteristics of the reactant of Al₄C₃. Figures 4(c)–4(f) show the element mapping of the SiC/Al composite. It can be seen that there are bulk crystal Si and SiC particles, and they are nearly uniformly distributed in the Al matrix. Meanwhile, a little amount of oxygen can be found, because the raw materials contained trace amounts of oxygen. Finally, the above results indicate that the pure SiC/Al composites are synthesized by in situ method at 950°C and holding time for 15 min by combustion synthesis and hot press consolidation.

3.2. Effect of the Si/C Mass Ratio. In order to investigate the effect of Si/C mass ratio on the phase constitution and
microstructure of the in situ SiC/Al composites, the SiC/Al composites with different Si/C mass ratio were fabricated. Figure 5 shows the XRD patterns of the SiC/Al composites with different Si/C mass ratio (4:1, 5:1, and 6:1). It can be seen that the main phases are Al, Si, and SiC in these samples. The peak intensity of the SiC phase is enhanced with increasing of the Si/C mass ratio. Figure 6 shows the SEM images of etched surfaces of the SiC/Al composites with different Si/C mass ratios. It clearly reveals that the irregular blocky-shaped SiC particles are formed in these samples. Nevertheless, the amount of SiC particles increases and the size decreases with the increase of Si/C mass ratio.

Figure 7 shows the corresponding size distribution of the in situ synthesized SiC particles in the tested samples. As shown in Figure 7(a), the maximum and average value of the SiC particles size in the composites with the Si/C mass ratio of 4:1 are about 4.1 μm and 1.6 μm, respectively, and the percentage of the submicroparticle is about 22% in total. As shown in Figure 7(b), when the Si/C mass ratio is 5:1, the maximum and average value of the SiC particles size are reduced to be 2.0 μm and 1 μm, respectively. Meanwhile, the percentage of submicroparticles increases to about 63%. As shown in Figure 7(c), when the Si/C mass ratio is 6:1, the maximum and average value of the SiC particle size are reduced to be 1.9 μm and 0.9 μm, respectively. The percentage of submicroparticles increases up to about 66%. The results indicate that the increase of the Si/C mass ratio can reduce the size of the SiC particles and lead to more uniform distribution of the particle size. Particularly, when the Si/C mass ratio increases from 4:1 to 5:1, the size of SiC particles is reduced significantly. The reason is that when the concentration of Si in the system increases, the contact opportunity between Al₁₄C₃ phase and Si atoms increases; consequently SiC nucleation rate increases. The average hardness value of the SiC/Al composites with different Si/C mass ratio (4:1, 5:1, 6:1) is 65.3 HB, 73.8 HB, and 75.6 HB, respectively. It can be found that when the percentage of the SiC submicroparticle in the composites increases from 22% to 63%, the hardness is increased by 13%.

The above results indicate that the increase of the Si/C mass ratio is helpful to synthesis of SiC particles. However, when the remaining Si in Al matrix is much more than the eutectic composition (12.6%) after in situ synthesized SiC, the additional Si leads to the rapid reduction of the compactness, strength, and ductility of the sample [33]. As a result, Si content is about 12% in research on most Al-Si alloy [34–36]. Therefore, the Si/C mass ratio of 5:1 is considered to be reasonable for the fabrication of the in situ SiC/Al composites.

3.3. Effect of the Holding Time. The holding time in the fabrication process of the in situ SiC/Al composites is the dynamic factor of direct impact on the reaction process; therefore the SiC/Al composites with the Si/C mass ratio of 5:1 under different holding time (0, 15, 30 min) were fabricated, respectively. Figure 8 shows the XRD patterns of the SiC/Al composites with different holding time (0, 15, and 30 min). It can be seen that the products in the sample with the holding time of 15 min are mainly Al, Si, and SiC phases, shown in Figure 8(b). Meanwhile, the Al₄C₃ phases appear in the sample without holding and with the holding time of 30 min as shown in Figure 8((a) and (c)).

In the Al-Si-C systems, the synthesis reaction of SiC is mainly limited by the diffusion of Si atoms. If without holding in the fabrication, the first generated Al₄C₃ phases have not enough time to react completely with Si atoms. Meanwhile, when the holding time is extended to 30 min, the Si concentration in the system is decreased with the continual reaction between Al₄C₃ and Si atoms. The above two factors will lead the remaining of Al₄C₃ phases to appear in composites.
Figure 9 shows the SEM images of etched surfaces of the SiC/Al composites with different holding time (0, 15, and 30 min). It can be seen that the in situ SiC particles with the irregular blocky-shape formed in the three samples. Nevertheless, SiC particles are few when the holding time is 0 min. With the holding time of 15 min, the amount of SiC particles is increased. Meanwhile, with further increase of the holding time (30 min), the amount of the SiC particles has no obvious changes. Figure 10 shows the corresponding size distribution of the in situ synthesized SiC particles in the tested samples under different holding times. It can be seen that holding times had no discernible effect on the SiC particles size. Nevertheless, the average hardness value of the SiC/Al composites with different holding time (0 min, 15 min, and 30 min) is measured to be 58.5 HB, 73.8 HB, and 71.6 HB, respectively. It can be found that when holding time is 15 min the composites have the largest hardness value. Particularly, if there is no holding time during fabrication process, the hardness value of the SiC/Al composites is decreased by 21% because the SiC particles are few in this sample.
Figure 5: XRD patterns of the SiC/Al composites with different Si/C mass ratio: (a) Si/C mass ratio = 4 : 1, (b) Si/C mass ratio = 5 : 1, and (c) Si/C mass ratio = 6 : 1.

Figure 6: SEM images of the etched surfaces of the SiC/Al composites with different Si/C mass ratios: (a) Si/C mass ratio = 4 : 1, (b) Si/C mass ratio = 5 : 1, and (c) Si/C mass ratio = 6 : 1.
In general, the Al₄C₃ phase plays a detrimental role in the mechanical properties of the composites [37]. Therefore, it is important to strictly control the residue of Al₄C₃ phase in the aluminum matrix composite. According to above results, the holding time should be chosen as 15 min for the fabrication of in situ SiC/Al composites.

4. Conclusions

In this study, the in situ SiC/Al composites are successfully fabricated by the method of combustion synthesis and hot press consolidation. With the increase of the Si/C mass ratio, the size distribution of SiC particles becomes more uniform. When the Si/C mass ratio increases from 4:1 to 5:1, the maximum size of SiC particles was reduced from 4.1 μm to 2.0 μm. Meanwhile, the percentage of the submicroparticles was increased from 22% to 63% and the hardness value was increased by 13%. In addition, without holding and with the holding time of 30 min in the fabrication process of the in situ SiC/Al composites, the transition phase Al₄C₃ was residue. Furthermore if there is no holding time the SiC particles were few in composites; as a result the average hardness value was decreased by 21%. When the holding time was set to be fifteen minutes, the Al₄C₃ phase totally reacts with Si atoms to form SiC particles, and the average hardness value was 73.8 HB.
Figure 8: XRD patterns of the SiC/Al composites with different holding times: (a) 0 min, (b) 15 min, and (c) 30 min.

Figure 9: SEM images of the etched surfaces of the SiC/Al composites with different holding times: (a) 0 min, (b) 15 min, and (c) 30 min.
Conflicts of Interest
The authors declare that they have no conflicts of interest.

Acknowledgments
This work was financially supported by the National Natural Science Foundation of China (nos. 51501176 and 51701086).

References
[1] N. Gangil, A. N. Siddiquee, and S. Maheshwari, "Aluminium based in-situ composite fabrication through friction stir processing: A review," Journal of Alloys & Compounds, vol. 715, pp. 91–104, 2017.
[2] L. Zhang, H. Xu, Z. Wang, Q. Li, and J. Wu, "Mechanical properties and corrosion behavior of Al/SiC composites," Journal of Alloys & Compounds, vol. 678, pp. 23–30, 2016.
[3] D. Yang, F. Qiu, W. Zhao, P. Shen, H. Wang, and Q. Jiang, "Effects of Ti-coating layer on the distribution of SiCP in the SiCP/2014Al composites," Materials and Corrosion, vol. 87, pp. 1100–1106, 2015.
[4] L.-J. Zhang, D.-L. Yang, F. Qiu, J.-G. Wang, and Q.-C. Jiang, "Effects of reinforcement surface modification on the microstructures and tensile properties of SiCp/Al2014 composites," Materials Science and Engineering: A Structural Materials: Properties, Microstructure and Processing, vol. 624, pp. 102–109, 2015.
[5] L. Wang, F. Qiu, Q. Zou et al., "Microstructures and tensile properties of nano-sized SiC p/Al-Cu composites fabricated
by semisolid stirring assisted with hot extrusion," Materials Characterization, vol. 131, pp. 195–200, 2017.

[6] X. Du, T. Gao, G. Liu, and X. Liu, “In situ synthesizing SiC particles and its strengthening effect on an Al–Si–Cu–Ni–Mg piston alloy,” Journal of Alloys & Compounds, vol. 695, pp. 1–8, 2017.

[7] M. Schöbel, W. Altendorfer, H. P. Degischer et al., “Internal stresses and voids in SiC particle reinforced aluminum composites for heat sink applications,” Composites Science and Technology, vol. 71, no. 5, pp. 724–733, 2011.

[8] H. M. Zakaria, “Microstructural and corrosion behavior of Al/SiC metal matrix composites,” Ain Shams Engineering Journal, vol. 5, no. 3, pp. 831–838, 2014.

[9] D.-L. Yang, F. Qiu, Z.-K. Lei, Q.-L. Zhao, and Q.-C. Jiang, “The interfacial structure and mechanical properties of Ti5Si3-coated SiCp/Al2014 composites fabricated by powder metallurgy with hot pressing,” Materials Science and Engineering: A: Structural Materials: Properties, Microstructure and Processing, vol. 661, pp. 217–221, 2016.

[10] L. J. Zhang, F. Qiu, J.-G. Wang, and Q.-C. Jiang, “High strength and good ductility at elevated temperature of nano-SiCp/Al2014 composites fabricated by semi-solid stir casting combined with hot extrusion,” Materials Science and Engineering: A: Structural Materials: Properties, Microstructure and Processing, vol. 626, pp. 338–341, 2015.

[11] I. Balasubramanian and R. Maheswaran, “Effect of inclusion of SiC particles on the mechanical resistance behaviour of stir-cast AA6063/SiC composites,” Materials and Corrosion, vol. 65, pp. 511–520, 2014.

[12] L.-J. Zhang, F. Qiu, J.-G. Wang, H.-Y. Wang, and Q.-C. Jiang, “Microstructures and mechanical properties of the Al2014 composites reinforced with bimodal sized SiC particles,” Materials Science and Engineering: A: Structural Materials: Properties, Microstructure and Processing, vol. 637, pp. 70–74, 2015.

[13] Z. Chen, Z. Tan, G. Ji et al., “Effect of Interface Evolution on Thermal Conductivity of Vacuum Hot Pressed SiC/Al Composites,” Advanced Engineering Materials, vol. 17, no. 7, pp. 1076–1084, 2015.

[14] H. Lee, S. S. Sohn, C. Jeon, I. Jo, S.-K. Lee, and S. Lee, “Dynamic compressive deformation behavior of SiC-particle-reinforced A356 Al alloy matrix composites fabricated by liquid pressing process,” Materials Science and Engineering: A: Structural Materials: Properties, Microstructure and Processing, vol. 680, pp. 368–377, 2017.

[15] Z. Wei, P. Ma, H. Wang et al., “The thermal expansion behaviour of SiCp/Al-20Si composites solidified under high pressures,” Materials and Corrosion, vol. 65, pp. 387–394, 2015.

[16] B.-K. Hwu, S.-J. Lin, and M.-T. Jahn, “Effects of process parameters on the properties of squeeze-cast SiCp-6061 Al metal-matrix composite,” Materials Science and Engineering: A: Structural Materials: Properties, Microstructure and Processing, vol. 207, no. 1, pp. 135–141, 1996.

[17] L. M. Tham, M. Gupta, and L. Cheng, “Effect of limited matrix-reinforcement interfacial reaction on enhancing the mechanical properties of aluminium-silicon carbide composites,” Acta Materialia, vol. 49, no. 16, pp. 3243–3253, 2001.

[18] I. A. Ibrahim, F. A. Mohamed, and E. J. Lavernia, “Particulate reinforced metal matrix composites—a review,” Journal of Materials Science, vol. 26, no. 5, pp. 1137–1156, 1991.

[19] L. Wang, F. Qiu, L. Ouyang et al., “A novel approach of using ground CNTs as the carbon source to fabricate uniformly distributed nano-sized TiCx/2009Al composites,” Materials, vol. 8, no. 12, pp. 8839–8849, 2015.

[20] Z. Wang, K. G. Prashanth, S. Scudino et al., “Tensile properties of Al matrix composites reinforced with in situ devitrified Al94Gd6Ni5Co2 glassy particles,” Journal of Alloys and Compounds, vol. 586, no. 1, pp. S419–S422, 2014.

[21] D. Markó, K. G. Prashanth, S. Scudino et al., “Al-based metal matrix composites reinforced with Fe49.9Co35.1Ni7.7B4.5Si2.8 glassy powder: Mechanical behavior under tensile loading,” Journal of Alloys and Compounds, vol. 615, no. 1, pp. S382–S385, 2015.

[22] Z. Wang, J. Tan, B. A. Sun et al., “Fabrication and mechanical properties of Al-based metal matrix composites reinforced with Mg96Cu4Zn10Y10 metallic glass particles,” Materials Science and Engineering: A: Structural Materials: Properties, Microstructure and Processing, vol. 600, pp. 53–58, 2014.

[23] S. C. Tjong and Z. Y. Ma, “Microstructural and mechanical characteristics of in situ metal matrix composites,” Materials Science and Engineering: R: Reports, vol. 29, no. 3, pp. 49–113, 2000.

[24] L. Wang, F. Qiu, J. Liu et al., “Microstructure and tensile properties of in situ synthesized nano-sized TiCx/2009Al composites,” Materials & Design, vol. 79, pp. 68–72, 2015.

[25] B. AlMangour, D. Grzesiak, and J.-M. Yang, “In-situ formation of novel TiC-particle-reinforced 316L stainless steel bulk-form composites by selective laser melting,” Journal of Alloys and Compounds, vol. 706, pp. 409–418, 2017.

[26] B. S. S. Daniel, V. S. R. Murthy, and G. S. Murthy, “Metal-ceramic composites via in-situ methods,” Journal of Materials Processing Technology, vol. 68, no. 2, pp. 132–153, 1997.

[27] J. Nie, D. Li, E. Wang, and X. Liu, “In-situ synthesis of SiC particles by the structural evolution of TiCx in AlSi melt,” Journal of Alloys & Compounds, vol. 613, no. 613, pp. 407–412, 2014.

[28] X. Du, T. Gao, D. K. Li, Y. Wu, and X. Liu, “A novel approach to synthesize SiC particles by in situ reaction in Al–Si–C alloys,” Journal of Alloys & Compounds, vol. 588, no. 10, pp. 374–377, 2014.

[29] T. Gao, D. Wang, X. Du, D. Li, and X. Liu, “Phase transformation mechanism of Al4C3bym the diffusion of Si and a novel method for in situ synthesis of SiC particles in Al melt,” Journal of Alloys and Compounds, vol. 685, pp. 91–96, 2016.

[30] L. Wang, F. Qiu, Q. Zhao, H. Wang, and Q. Jiang, “Simultaneously increasing the elevated-temperature tensile strength and plasticity of in situ nano-sized TiCx/Al-Cu-Mg composites,” Materials Characterization, vol. 125, pp. 7–12, 2017.

[31] L. Wang, F. Qiu, Q. Zhao, M. Zha, and Q. Jiang, “Superior high creep resistance of in situ nano-sized TiCx/Al-Ca-Mg composite,” Scientific Reports, vol. 7, no. 1, article 4540, 2017.

[32] Q. Zhao, Y. Liang, Z. Zhang, X. Li, and L. Ren, “Study on the impact resistance of bionical layered composite of TiC-TiB2/Al from Al-Ti-B4C system,” Materials, vol. 9, no. 8, article 7086, 2016.

[33] P. Ma, Y. Jia, K. G. Prashanth et al., “Effect of Si content on the microstructure and properties of Al-Si alloys fabricated using hot extrusion,” Journal of Materials Research, vol. 32, no. 11, pp. 2210–2217, 2017.

[34] Y. Birol, “Microstructural evolution during annealing of a rapidly solidified Al-12Si alloy,” Journal of Alloys and Compounds, vol. 439, no. 1-2, pp. 81–86, 2007.
[35] K. G. Prashanth, S. Scudino, H. J. Klauss et al., "Microstructure and mechanical properties of Al-12Si produced by selective laser melting: Effect of heat treatment," *Materials Science and Engineering: A Structural Materials: Properties, Microstructure and Processing*, vol. 590, pp. 153–160, 2014.

[36] K. G. Prashanth, S. Scudino, A. K. Chaubey et al., "Processing of Al-12Si-TNM composites by selective laser melting and evaluation of compressive and wear properties," *Journal of Materials Research*, vol. 31, no. 1, pp. 55–65, 2016.

[37] H. Li, J. Kang, C. He, N. Zhao, C. Liang, and B. Li, "Mechanical properties and interfacial analysis of aluminum matrix composites reinforced by carbon nanotubes with diverse structures," *Materials Science &amp; Engineering A*, vol. 577, no. 9, pp. 120–124, 2013.