Production, Characterization and Surface Properties of Sr Doped Hydroxyapatite Coating on Magnesium Alloy by Hydrothermal Method

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Abstract
In this study, the surface of AZ91D magnesium alloy was coated with undoped and at different ratios strontium doped hydroxyapatite. Coatings were carried out at 180 °C in 3 hours. The surface roughness of the coated samples was determined and the microstructure of the phases forming on the coated surfaces were examined by scanning electron microscopy (SEM). The chemical composition of the phases formed on the coated surfaces was determined by energy dispersed X-ray spectroscopy (EDS). The phases formed on the surfaces were characterized by X-Ray diffraction (XRD) and Fourier transform infrared spectrometry (FT-IR). The AZ91D magnesium alloy was coated successfully with undoped and strontium doped hydroxyapatite by hydrothermal method. The highest surface roughness value was measured as $R_a = 8.255$ µm in 15% strontium doped sample. It was determined that the (Ca + Sr) / P ratios of the coatings were higher than the stoichiometric ratio of hydroxyapatite, 1.67. It was determined that the closest coating to the stoichiometric ratio was 10% Sr doped coating.

Keywords: Hydroxyapatite coating, Magnesium alloy, Hydrothermal method, Surface roughness, Biomaterial.

1. INTRODUCTION
Repairing damaged bone tissue one of the important topics in tissue engineering. Implant materials used in tissue engineering should be biocompatible and biodegradable in the human body during the repair of bone tissues [1]. In recent years, magnesium (Mg) alloys have become very interesting among metallic implants due to their important advantages especially in orthopedic applications. These advantages include its extremely lightweight, limited biological reactions, biodegradability, outstanding mechanical properties close to natural bone, and excellent biocompatibility. In addition, the presence of Mg$^{2+}$ ions in apatite crystals can increase osteoblast adhesion rate and increase bone formation [2-4]. Besides these advantages, low wear-resistance and weak corrosion resistance especially in physiological solution are the most important disadvantages of Mg implants. In the implants exposed to corrosion and wear, the mechanical properties deteriorate before sufficient bone healing and limits their usage by preventing the use of implants as a load-bearing material [2, 3]. The most effective and efficient way to avoid these disadvantages of Mg implants is to increase their corrosion resistance, wear-resistance and biocompatibility by modification their surfaces with a biocompatible protective coating [2, 5]. Synthetic hydroxyapatite is one of the most preferred among biocompatible coatings ($Ca_{10}(PO_4)_6(OH)_2$, HA). This is because hydroxyapatite has the most similarity to the mineral part of the bone, excellent biocompatibility, good biodegradability and high osteogenic potential [6, 7].

The most commonly used techniques for coating the surfaces of Mg alloys with HA are sol-gel, electrodeposition, biomimetic method, atmospheric plasma spraying and hydrothermal method. Among these methods, hydrothermal method has advantages such as being simple, cost effective and needing low temperatures [8].

Strontium (Sr) is an element in the human body that is usually found in the body skeleton and has bone targeting properties. Sr has some positive properties like playing an important role in bone formation, the presence of Sr ions in biological environments, greatly increasing osteoblast differentiation, antimicrobial effect, inhibiting osteoclast activity, increasing preosteoblastic cell proliferation and bone matrix synthesis. Due to such positive properties, Sr has been doped to HA in recent years for improving the biological
production of HAs [9, 10].

Zhang et al. coated the surface of AZ31 magnesium alloy with hydroxyapatite by hydrothermal method at different temperatures and times [11]. Sun et al. investigated the coating surface properties and corrosion resistance of the AZ91D magnesium alloy, which they coated with fluorinated hydroxyapatite by hydrothermal method [8]. Yang et al. coated the surface of the ZK60 magnesium alloy with hydroxyapatite by hydrothermal method at different times [12]. In another study, Mg-2.9Gd-1.5Nd-0.3Zn-0.3Zr magnesium alloy was coated with hydroxyapatite by hydrothermal method [13]. Li et al. coated the surface of pure magnesium with calcium phosphate by hydrothermal method [14]. Asl et al. coated the surface of the AZ31 magnesium alloy with calcium phosphate by hydrothermal method at different temperatures [15]. Wang et al. coated the ZK60 magnesium alloy with Sr doped hydroxyapatite at different doping ratios (3%, 5% and 10%) by hydrothermal method [16].

As a result of the literature studies, not many studies have been encountered regarding the coating of AZ91D magnesium alloy with Sr doped hydroxyapatite by hydrothermal method and it has been decided to carry out this study. In this study, the surface of AZ91D magnesium alloy was coated with Sr doped hydroxyapatite in different doping ratios by hydrothermal method in constant process parameters. Surface roughness of coated surfaces was determined and microstructural properties of coated surfaces were analyzed by FT-IR, SEM, EDS and XRD.

2. EXPERIMENTAL DETAILS

In present study, AZ91D magnesium alloy with a diameter of 20 mm and a thickness of 10 mm, whose chemical composition is given in Table 1, was used as the substrate material. The substrate material was polished with 1200 mesh SiC sandpaper and then cleaned with ultrasonic bath for 15 min. with acetone and then dried with hot air. For HA coating, firstly 0.1 M Merck brand Ca(NO$_3$)$_2$·4H$_2$O was added to 30 ml of pure water in the beaker and stirred for 30 min. at room temperature in a magnetic stirrer. The pH of the mixture was adjusted to 4 with HNO$_3$ while stirring was continued. Finally, after stirring this mixture for another 10 min. in a magnetic stirrer, it was ultrasonicated for 30 min. and the final mixture was obtained. After the substrate material was placed on the bottom of the autoclave, the final solution was poured into the autoclave and placed in the hydrothermal reactor. Hydrothermal treatment was carried out at 180 °C for 3 hours and when the reactor temperature reached room temperature, the sample was removed and washed several times with pure water and then dried at 60 °C for 1 hour. Production methods of Sr doped samples are the same as HA coating. Only for the production of Sr additive samples, Acros organic brand Sr(NO$_3$)$_2$ was added in different [Sr] / [Sr + Ca] molar ratios (5%, 10%, 15% and 20%), keeping the molarity constant for the first solution containing Ca(NO$_3$)$_2$·4H$_2$O. Pure hydroxyapatite coated sample was named HA and 5%, 10%, 15% and 20% Sr doped samples were named Sr5HA, Sr10HA, Sr15HA and Sr20HA, respectively.

The surface roughness of the produced samples was determined using the Mitutoyo SJ-201 profilometer. Measurements were carried out from 10 different points of the coating surfaces and the surface roughness values were calculated by calculating the average. Microstructures of sample surfaces were examined with ZEISS EVO-MA10 brand SEM device in different magnifications. The chemical compositions of the coated surfaces were measured using the Bruker brand EDS detector connected to the ZEISS EVO-MA10 brand SEM device. The phases formed on coated surfaces were determined by XRD. XRD analyzes were performed on the Malvern Panalytical brand device at CuKa ($\lambda = 1.5406\text{Å}$) radiation, $2\theta = 20 - 90^\circ$ scanning range at 40 mA and 45 kV. FT-IR analysis was carried out on Thermo Scientific Nicolet IS 5 brand FT-IR spectrometer device with a scanning range of 4000 - 550 cm$^{-1}$.

3. RESULTS AND DISCUSSION

Figure 1 shows the coating surface images of samples coated with hydrothermal method. As can be seen, AZ91D magnesium alloy was successfully coated with undoped and Sr doped hydroxyapatite by hydrothermal method. No visible cracks or porosity were found on the coating surfaces. In addition, the coating layer is combined with the substrate surface well.

![Figure 1. Macro surface images of coated samples.](image_url)
The surface roughness values of the coated samples are seen in Figure 2. Surface roughness value of the sample coated with HA is lower than the Sr doped samples. Surface roughness increased with increasing Sr doping ratio up to 15%. Then, when the Sr doping ratio reaches to 20%, the surface roughness value decreased. This change in surface roughness is thought to occur due to the change in the shape and size of the crystals formed on the coated surface due to different doping ratios [15, 17]. In implants generally rough surfaces are preferred compared to a smooth surface. This is because of the surface roughness is an important factor for better osseointegration and biomechanical bonding. Thanks to the surface roughness, a better adhesion can be achieved between the implant surface and the bone [17]. The SEM photos are shown in Figure 3 also confirm the different microstructures formed on the coating surfaces. Similar shaped structures have also been seen in previous researches on hydroxyapatite coating of magnesium alloys by hydrothermal method [12, 15]. The coating surfaces of HA coated samples consisted of fine-grained triclinic and hexagonal structures compared to Sr-doped samples (Figure 3a and b). In Sr doped samples, these structures are more coarse and there are some spherical shaped particles in between these structures (Figure 3c-i). EDS analysis results obtained from coating surfaces at low magnification are given in Table 2. The (Ca + Sr) / P ratio of all samples is higher than 1.67, which is the stoichiometric ratio of HA, and the sample with the closest value to this ratio is 10% Sr doped sample [18]. As expected, as the Sr doping rate increased, the Sr composition in the coating layer increased. The (Ca + Sr) / P ratio of the flower-shaped structure at point-1 in Figure 3b is 1.88 and the crystal at point-2 is 2.01. In the Sr5HA sample, the crystalline (Figure 3d-point-3) (Ca + Sr) / P ratio is 1.46 and the spherical particle’s (Ca + Sr) / P ratio is 1.98 (Figure 3d-point-4). The crystalline (Ca + Sr) / P ratio at point-5 in Figure 3f is 1.8 and the particle at point 6 is 1.85. The crystalline (Figure 3h-point-7) and particle’s (Figure 3h-point 8) (Ca + Sr) / P ratios of 15% Sr doped sample are 1.56 and 1.70, respectively. The crystalline (Ca + Sr) / P ratio at point-9 in Figure 3i is 1.52 and the particle at point 10 is 1.93. As can be seen from the EDS analysis results, with the change of the Sr doping ratio, the (Ca + Sr) / P values of the structures in the coating layers changed. It has been seen also in the previous studies that the rates of doping elements change the (Ca + M) / P (M = doping element) ratios differ [19, 20]. In addition, the spherical shaped particles in the Sr doped samples are richer by Sr element and the (Ca + Sr) / P ratio of these particles are higher than the crystal structures.

When XRD diffraction patterns of pure HA and Sr doped HA coated samples are examined, sharp HA peaks are observed alongside Mg peaks (Figure 4). The absence of sharp peaks of other structures other than these sharp peaks indicates that the coatings are highly crystalline and that HA coating is successfully performed on Mg by hydrothermal method [9, 17]. The peak intensities of Sr doped samples in the (002) planes are higher than the undoped sample and other HA peaks. This shows that the crystal plane HA (002) is directed to AZ91D in the same manner as pure Mg [18]. Again, XRD results are generally in agreement with previous researches [18, 21].

| Sample | Ca   | P   | O    | Mg  | Zn  | Sr  | (Ca + Sr) / P |
|--------|------|-----|------|-----|-----|-----|--------------|
| HA     | 33.18| 12.33| 53.18| 0.72| 0.58| 0.00| 2.69         |
| Sr5HA  | 29.53| 12.26| 57.32| 0.70| 0.00| 0.19| 2.42         |
| Sr10HA | 25.62| 15.09| 58.88| 0.00| 0.05| 0.36| 1.72         |
| Sr15HA | 25.51| 13.21| 59.34| 0.44| 0.55| 0.94| 2.00         |
| Sr20HA | 25.11| 15.03| 58.68| 0.00| 0.00| 0.99| 1.74         |

FT-IR analysis results of samples are shown in Figure 5. The peak at about 601 cm⁻¹ correspond to vibration of PO₄³⁻ [15, 17]. The bands at about 1022 cm⁻¹ and 980 cm⁻¹ in HA and 1018 cm⁻¹ in Sr5HA, 1017 cm⁻¹ in Sr10HA, 1011 cm⁻¹ in Sr-
Figure 3. The coating surface SEM photographs of the samples a) HA x100, b) HA x2000, c) Sr5HA x100, d) Sr5HA x2000, e) Sr10HA x100, f) Sr10HA x2000, g) Sr15HA x100, h) Sr15HA x2000, i) Sr20HA x100 and j) Sr20HA x2000.
15HA and 1015 cm\(^{-1}\) in Sr20HA are ascribed to stretching modes of PO\(_4\)\(^{3-}\) [13]. The bands observed at 1651 cm\(^{-1}\) in Sr-10HA, 1726 cm\(^{-1}\) in Sr15HA and 1731 cm\(^{-1}\) in other samples correspond to H\(_2\)O [14]. The peaks observed at about 2362 cm\(^{-1}\) originate from CO\(_2\) in the air [14]. The wideband centered at approximately 3360 cm\(^{-1}\) is ascribed to adsorbed/lattice water [13, 17]. The FT-IR analysis results support to XRD analysis and are generally in agreement with the previous researches [13-15, 17].

**Figure 5.** FT-IR analysis results.

### 4. CONCLUSIONS

- The surface of the AZ91D magnesium alloy was successfully coated with HA and Sr doped HA.
- The surface roughness value of coated surfaces increased with increasing Sr doping ratio. The coating surfaces of HA coated samples consisted of finer grained structures than Sr doped samples. The coating layers are generally consisted of HA and Mg.
- The \((\text{Ca} + \text{Sr}) / \text{P}\) ratios of the undoped and Sr doped samples are higher than the stoichiometric ratio (1.67) of HA. The closest \((\text{Ca} + \text{Sr}) / \text{P}\) ratio to the stoichiometric ratio of HA was 1.72 in the sample with 10% Sr doped.
- It is thought that 10% Sr doped HA coating can be used as an implant material since the surface roughness value is high and \((\text{Ca} + \text{Sr}) / \text{P}\) ratio is closest to stoichiometric ratio.

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