Biological hydrogen production from synthetic wastewater by an anaerobic migrating blanket reactor: Artificial neural network (ANN) modeling

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Abstract

Background: This study aimed to evaluate an anaerobic migrating blanket reactor (AMBR) for biological hydrogen production, and also to investigate its capability to treat synthetic wastewater.

Methods: A five-compartment AMBR (9 L effective volume) was made by Plexiglas and seeded with thermal pretreated anaerobic sludge at 100°C for 30 minutes. The AMBR was operated at mesophilic temperature (37 ± 1°C) with continuous fed of synthetic wastewater at five organic loading rates (OLRs) of 0.5 to 8 g COD/L.d.

Results: It was revealed that as the OLR increased from 0.5 to 8 g COD/L.d, the hydrogen production and also volumetric hydrogen production rate (VHPR) improved. Increasing the OLR over this range, led to a decrease in the average hydrogen yield from 1.58 ± 0.34 to 0.97 ± 0.45 mol H2/mol glucose. The concentration of both volatile fatty acids (VFAs) and solvents kept increasing with OLR. During the AMBR operation, the dominant soluble end products (SEPs) were acetic and butyric acids in all of the OLRs studied.

Conclusion: Based on the results, the hydrogen yield was related to the acetate/butyrate fermentation. The artificial neural network (ANN) model was well-fitted to the experimental obtained data from the AMBR, and was able to simulate the chemical oxygen demand (COD) removal and hydrogen production.

Keywords: AMB reactor, Fatty acids, Fermentation, Hydrogen, Wastewater treatment

Introduction

Hydrogen (H2) as an environmentally friendly gas is an energy carrier that could play a significant role in the reduction of greenhouse gases (1,2). Due to water production during combustion process, H2 is considered as a clean fuel. Hydrogen is regarded as an ideal energy with a high energy yield of 122 kJ/g, which is 2.75 folds greater than that of hydrocarbon fuels (3).

In comparison with conventional anaerobic process (fermentative methane production), due to some inconsistency and drawbacks, the H2 production processes by dark fermentation are less well developed than the methane (CH4) production. During anaerobic digestion of organic wastes, such as solid waste and wastewater, CH4 is produced and its production processes have been well established commercially. Hydrogen is a more valuable energy carrier and chemical feedstock compared with CH4 (4,5).

Apart from the difficulties in the stabilization of process, the low yield of H2 on sugars was reported. Based on the glucose stoichiometry, the oxidation of 1 mol of glucose can produce 12 mol H2. In dark fermentation process, the maximum yield of H2 is 4 mol per mol of glucose, which is only 33% of the theoretically stoichiometric and linked to microbial metabolism. In the H2 production by dark fermentation process at present, during carbon conversion to various organic acids and alcohols, H2 is not produced from the simple oxidation reactions of glucose to CO2 and water (4,6).

The maximum H2 production via dark fermentation is
related to the operational pH, substrate concentration (various carbohydrates), influent nutrients (N and P), hydraulic retention time (HRT), partial pressure of H₂, stirring rate, sludge pretreatment methods (e.g., thermal or acid or alkaline pretreatment), and the absence or activity inhibition of hydrogenotrophic methanogens (7-10). Previous studies on the H₂ bioreactors shows that the important design parameter is organic loading rate (OLR) (11).

Due to metabolites (volatile fatty acids [VFAs] and solvents) accumulation during fermentation, the solution pH drops and buffering capacity (BC) reduces, and as a result, leads to the inhibition of biological H₂ production (12). Furthermore, the acid-base condition of treatment system was expressed with VFAs concentration and solution pH. In addition, with increasing the BC, the redox condition of treatment system can be controlled. Furthermore, with increasing BC, the treatment system can be operated in a stable solution pH. The buffer supplementation at various solution pHs increased the H₂ production time by maintaining the optimum solution pH. In order to increase the treatment system BC, CO₂ was introduced to the bioreactor and lead to an increase in the H₂ production (13). The pretreatment of biocatalyst and also acidophilic conditions will facilitate the effective biological H₂ production during various wastewater treatment processes (14).

Different batch and continuous technologies, such as anaerobic sequencing batch reactor (ASBR) (15-17), up-flow anaerobic packed bed reactor, anaerobic digester sludge, and membrane bioreactor have been used for the biological H₂ production (15). The anaerobic migrating blanket reactor (AMBR) is a high rate anaerobic treatment system that is operated independent of an up-flow hydraulic pattern for mixing. The required contact between the substrate and biomass, was supplied using mechanical mixing. The biomass migration occurs in the horizontal flow in this system. To avoid solid-liquid phase separation and also, the sludge agglomeration in the bottom part of the reactor, the periodical flow reversal pattern is used in this mechanism. This system is a continuous flow by a short HRT, which is designed simply and does not need effluent recycling and gas-liquid separation system (18,19).

The artificial neural network (ANN) is a good tool working according to human nerve systems and brain that is broadly used to examine relationships in complex non-linear data due to the ANN ability to data classification and learning. During the last decade, the ANN models have been used for the environmental engineering fields, such as biological treatment of wastewater, membrane filtration, pollution adsorption, and electrodialysis of saline water (20-23).

The ANNs always consist of three layers including (i) input, (ii) hidden, and (iii) output layers. The outputs of a neuron are calculated using Eq. (1):

\[ o = f \left( \sum_{j=0}^{N} \omega_j x_j \right) \]  

(1)

where \( n \) is the input number, \( x_j \) is the \( j \)th input to the neuron, \( \omega_j \) is the \( j \)th synaptic weight, and \( f \) is a non-linear function.

For converting output data between -1 and +1, the hyperbolic tangent formula was applied as Eq. (2):

\[ \tanh(x) = \frac{2}{1 + e^{-2x}} - 1 \]  

(2)

During training process of input and output data set, the network weights are adjusted to achieve the similar outputs as seen in the training data set. For this purpose, the data were divided into two subsets for training model and validation purposes.

The Pearson correlation coefficient (\( r^2 \)) and mean standard error (MSE) were computed to evaluate the performance of the developed models according to the following formulas (24).

\[ r^2 = 1 - \frac{\sum_{i=1}^{N} \left( y_{\text{pre},i} - y_{\text{exp},i} \right)^2}{\sum_{i=1}^{N} \left( y_{\text{pre},i} - y_{\text{ave}} \right)^2} \]  

(3)

\[ MSE = \frac{1}{N} \sum_{i=1}^{N} \left( y_{\text{pre},i} - y_{\text{exp},i} \right)^2 \]  

(4)

In order to avoid numerical overflows related to very large or small weights, all of the data were converted to normalized values using Eq. (5):

\[ x_{\text{norm}} = 0.8 \times \left( \frac{x_i - x_{\text{min}}}{x_{\text{max}} - x_{\text{min}}} \right) + 0.1 \]  

(5)

Due to lack of related studies, the performance and efficiency of AMBR for biological hydrogen production and wastewater treatment in different initial OLR values were evaluated in the present study. In addition, the ANN model was developed to predict the performance of the AMBR for wastewater treatment and hydrogen production.

**Materials and Methods**

**AMBR set up and operation**

A 9-L continuous AMBR was made by Plexiglas with dimensions of 9 \( \times \) 10 \( \times \) 20 cm (L\( \times \)W\( \times \)H). The AMBR contained five compartments with the same size and total volume of 10 L and a 1 L headspace for the collection of biogas and foam. The flow regimes in the compartments were constituted with an up-flow and down-flow zone. The schematic diagram of the AMBR is shown in Figure 1. The gas collection systems consisted of gas sampling ports, gas pipes, and wet gasmeter. For biological solids trapping and also water level control, the last compartment was attached to a sedimentation tank (1.5 L volume).
The influent wastewater was introduced to the AMBR with an electrical pump (hose pump) and the trapped solids were discharged periodically from the sedimentation tank. The liquid and gas samples and also biological solids were extracted from each compartment via sampling ports. The sampling ports were installed at two heights (10 and 15 cm from floor). A mechanical mixer was employed for the sufficient contact between biomass and influent substrate. The mixers were attached with paddles with 1.5 cm in height and 5 cm in width in 12.5 and 2.5 minutes for idle and mixing time at 80 rpm, respectively. In order to separate the AMBR headspace of the outside compartment from the air, an effluent baffle was equipped and led to flow out of the AMBR via gravity without biogas losing from the headspace. The AMBR was operated at 37 ± 1°C by a thermostatically regulated recirculating hot water bath. The AMBR was operated at five OLRs (0.5, 1, 2, 4, and 8 g COD/L.d) and equal to 1.25, 2.5, 5, 10, and 20 g/L with HRT equal to 2.5 d. A wet gasmeter (ELSTER-AMCO, Germany) was applied for monitoring the overall biogas production.

Inoculum and medium composition
The anaerobic sludge was taken from the South Municipal Wastewater Treatment Plant (Tehran, Iran). In order to eliminate particulate materials, it was screened with sieve No. 16. The characteristics of anaerobic sludge including average pH, soluble chemical oxygen demand (COD), total COD, total suspended solids, and volatile suspended solids concentrations were obtained to be 7.75 ± 0.1, 2.5 ± 0.4 g/L, 12.6 ± 2.2 g/L, 32.56 ± 6.58 g/L, and 16.84 ± 3.4 g/L, respectively. The physically sludge pretreatment was done at 100°C for 30 minutes in order to selectively enrich spore-forming hydrogen producing microflora according to our previous work (25).

The sole carbon source used for hydrogen fermentation with the pretreated anaerobic sludge was glucose. As a function of influent COD, the inorganic nutrients (KH₂PO₄: 10.00 mg/g COD and NH₄Cl: 76.45 mg/g COD), trace elements as mg/g COD (FeCl₃: 1.021, K₂HPO₄: 25.32, CaCl₂ • 2H₂O: 2.06, MnCl₂ • 2H₂O: 0.34, MgSO₄ • 7H₂O: 2.14, NiSO₄ • 6H₂O: 0.0763, CoCl₂ • 6H₂O: 0.092, ZnSO₄ • 0.0592, H₃BO₃: 0.020, Na₂MoO₄ • 2H₂O: 0.0822, and CuCl₂ • 2H₂O: 0.016), as well as yeast extract: 36 mg/L and peptone: 36 mg/L were added (26). In addition, to provide the initial BC, 1.87 g/L of NaHCO₃ (NaHCO₃/COD ratio: 0.25) was added.

Data analysis
In the both influent and effluent wastewater, the solution pH, oxidation–reduction potential (ORP), alkalinity, tCOD, and sCOD were measured using a glass body pH probe (CG 824 SCHOTT), multi parameter device (WA 2017 SD, Lutron Electronic Enterprise Co. LTD), and titration and colorimetric methods (27). Using GC-FID, VFAs (acetate, propionate, lactate, and butyrate) were analyzed after liquid-liquid extraction and solvents (methanol, ethanol, and acetone) were measured using automatic headspace injections (28). The purity of biogas in respect of hydrogen was evaluated with a hydrogen analyzer (COSMOS-XP-3140 model, Japan).

Results
Biohydrogen production
The variations of biological hydrogen productions and volumetric hydrogen production rate (VHPR) in the AMBR are shown in Figure 2 for all OLRs studied. As shown in this figure, with increasing the OLR from 0.5 to 8 g COD/L.d, the biogas (H₂) production and also VHPR improved. The daily hydrogen gas production enhanced from 0.41 to 4.47 L/d, when the ORLs increased from 0.5 to 8 g COD/L.d. At this stage, the hydrogen content of biogas declined from 48 to 37%. The steepness of the hydrogen yield in respect of OLR is shown in Figure 3. As the OLR increased from 0.5 to 8 g COD/L.d, the average hydrogen yield rate declined from 1.58 ± 0.34 to 0.97 ± 0.45 mol H₂/mol glucose. Thus, the increase of OLR up to 8 g COD/L.d is negatively affected the hydrogen yield.

COD removal efficiency
Figure 4a presents the COD removal efficiency and the amount of removed COD as a function of the OLR during the AMBR operation. As seen in Figure 4a, during the initial stages of the AMBR operation, the COD removal
efficiency of 9% (OLR 0.5 g COD/L.d) was observed. Furthermore, at the end of the cycle period, the AMBR operation with an OLR of 0.5 g COD/L.d, registered a COD removal efficiency of 28%. Afterwards, with increasing the OLR (1 g COD/L.d), first, the COD removal efficiency promptly increased to 40%, but then due to dilution effect, reduced to 20%.

The removal of COD increased greatly with increasing the OLR of AMBR fermentation (Figure 4a). The higher removal of COD is related to the higher influent loading.

### Soluble End Products

As previously mentioned, the distribution and fraction of microbial soluble metabolites including VFAs and alcohols were used as monitoring indicators of anaerobic hydrogen production system (29). Figure 5 illustrates the results of soluble end products (SEPs) production during AMBR operation as a function of the OLR. As obvious in Figure 5, the SEPs production and their characteristics were significantly related to the applied OLR.

### Alkalinity, pH, and ORP of the effluent

The variations of the effluent alkalinity, pH, and ORP during the AMBR operation are shown in Figure 6. Before reaching stable AMBR performance, fluctuation was observed in the effluent solution pH. As shown in Figure 6, pH drop showed a distinct trend towards acidification.

### Discussion

The amount of hydrogen production per volume of AMBR should be taken into account as an indicator for the comparison of the obtained results. In this study, as seen in Figure 2, at OLR of 0.5 g COD/L.d, the average of VHPR was 0.04 ± 0.02 L H₂/L.d and improved to 0.53 ± 0.29 L H₂/L.d by applying 8 g COD/L.d. In a study performed by Guo et al, the operation of the expanded granular sludge bed (EGSB) reactor showed that the highest HPR of 0.71 L H₂/L.d was achieved at OLR of 120 g COD/L.d (21). Fues et al investigated biohydrogen production using continuous acidogenic packed-bed reactor and found that the VHPR was fluctuated from 0.4 to 0.8 L H₂/L.d (30). The calculated VHPR in this study is slightly lower than that obtained in the previous study and could be attributed to the reactor configuration, initial
inoculum, OLR, and HRT of the reactor, as well as the influent substrate concentration. The increase of OLR up to 8 g COD/L.d has negative effect on the biological hydrogen yield. This situation may be due to VFAs accumulation at higher OLRs, in addition, the supersaturation of hydrogen in liquid phase may be related to the lower biogas production and relieving inhibition due to hydrogen (31). In a study by Van Ginkel et al, the average hydrogen yield increased from 1.8 to 2.6 mol H₂/mol glucose as the glucose concentration reduced from 10 to 2.5 g COD/L (31). Nasr et al used an up-flow anaerobic staged reactor for biohydrogen production from starch wastewater and demonstrated that as OLR increased from 18 to 108 g COD/L.d, the hydrogen yield decreased (32). Kongjan et al reported that with increasing hydrogen production, OLR increased, but the increase of OLR to 120 g/L, resulted in light and sharp decrease in the hydrogen production rate and yield, respectively (33). A similar trend was reported by Buitrón et al (34). In case of other studied OLR, the same trend was observed. Overall, the variation of COD removal ranged between 9 and 42% in the OLR studied. Searmsirimongkol et al studied the hydrogen production from alcohol distillery wastewater using an ASBR and reported that the COD removal efficiency was 15%-28% by applying the OLR of 15-37.5 kg/m³.d (35).

The average COD removal efficiency in the studied OLR is illustrated in Figure 4b. As shown in Figure 4b, the COD removal efficiency was declined with increasing the OLR, which is consistent with the results of other studies (36-38). As previously stated, the biological hydrogen production during anaerobic degradation of organic matters is related to the COD removal (39). In biological hydrogen production process, the COD removal occurred via the release of cytogenesis and biogas (mainly CO₂ and H₂), while a significant fraction of COD was converted to SEPs and remained in the system (40). This manner leads to the lower COD removal efficiency during acidogenic phase compared to methanogenic phase. Due to conversion nature of biohydrogen production process (conversion of influent substrate to VFAs and solvents), the COD removal efficiency is not a good indicator for the evaluation of the process efficiency.

The concentration of both VFAs and solvents kept increasing with OLR. The dominant SEPs during AMBR operation were acetic and butyric acids in the all of OLRs. The high acetic and butyrate concentrations showed that the biological reaction was followed by acetic/butyrate fermentation. At this situation, Clostridium sp. are registries as dominant microorganisms in the anaerobic reactor due to their ability to ferment acetic/butyrate (36,41,42).

The results demonstrated that the sum of VFAs concentrations distinctly affects the AMBR performance, in respect of both biological hydrogen yield and COD removal. The VFA production is influenced by the metabolic pathway used by bacteria and the rate of mass transfer. In addition, the accumulation of the undissociated VFA forms leads to the shift of hydrogen production to solvent production (34). Methanol and ethanol were detected for higher studied OLRs with significantly lower concentrations than VFAs. The lower solvents production indicated that the fermentations occurred in the AMBR were acidogenic rather than solventogenic, which is consistent with the results of the previous study (31). The hydrogen fermentation changed to a solvent forming reaction at higher OLRs presumably is related to a decrease in the glucose flux through glycolysis by tying up the CoA and PO4 pools by the uptake of acids (43). The acetone was not detected during the AMBR operation.

Previous studies reported that to monitoring the anaerobic hydrogen production process, the solution pH, alkalinity, and ORP are the important factors. Variation of the above-mentioned parameters is affected not only by the anaerobic hydrogen production ability, but also by the microbial community and fermentation types (40).

During the AMBR operation, acid production during biological process lead to VFAs accumulation in the AMBR and a gradual reduction in BC (total alkalinity), which resulted in a simultaneous drop in the solution pH. The pH variation during stabilization phase of AMBR operation was 6.31 ± 0.29, 6.39 ± 0.41, 5.89 ± 0.34, 5.55 ± 0.4, and 5 ± 0.1 at different operating OLR. The pH variation in a narrow range showed a stable system. The previous research reported that the effluent pH ranged between 4.5 and 7.5 (37,38,44,45). Clostridium sp. are usually the dominant producers of hydrogen in acetate/butyrate fermentation with the optimal pH ranging between 5 and 6 (31,46,47).

In the case of ORP values, the ORP decreased from -47 mV at the beginning of the AMBR operation to ~130 mV at the end of the operation period. As seen in Figure 6, in the AMBR process, the values of ORP were mainly attributed to pH. In the previous study, the ORP value in the effluent of hydrogen production processes was reported to be -5 to -600 mV (29,40,44), which is consistent with the results of the present study. In contrast, Venkata Mohan et al studied the application of biofilm configured reactor for the biohydrogen production and reported that the effluent ORP ranged 82 to 145 mV (37).

For understanding the buffering activity of the AMBR, the alkalinity of the effluent was monitored and shown in Figure 6. The ascending trend of the effluent alkalinity was observed during the AMBR operation. As previously stated, due to the balance of pH level ([CO₃]⁻ and [HCO₃⁻]) within the reactor, the effluent alkalinity plays a critical role in the inhibition of VFAs accumulation and leading to substrate removal and biological hydrogen production (38,40).

**Artificial neural network (ANN)**

In order to generate neural network model, the MATLAB...
software (The Mathworks Inc., 2012) was used. To ensure more efficient training of the ANN, the targets and inputs were preprocessed by normalizing them (ranging 0 to 1) using ‘PREMNMX’ function. For mapping the input to hidden layer, the sigmoid transfer function, ‘TANSIG’ (hyperbolic tangent), was selected and also for mapping the hidden layer to output layer, ‘PURELIN’ (pure linear transfer function) was chosen. To construct the ANN model, the inputs and their corresponding outputs data were randomly segregated into three data sets including 70% for training (new model development), 15% for validation, and 15% for model reliability testing. In this study, the multilayer perceptron with back-propagation algorithm was trained in order to report the ability of feed-forward architecture of the ANN.

In this study, the optimum number of neurons (N) in the hidden layer was determined according to a trial and error approach. Therefore, different numbers of neurons in the range of 1-15 were tested in the hidden layer and the optimum hidden layer size was determined according to the minimum value of MSE and $R^2$ of the prediction data set. As seen in Figure 7, with increasing the number of neurons in the hidden layer, the value of MSE decreased promptly, and then increased.

As shown in Figure 7, three-layer feed forward back propagation neural network including 3:5:1, 3:9:1, and 3:6:1 were respectively used for modeling the effluent COD concentration hydrogen production.

Figure 8 shows a comparison between experimental values of sCOD and hydrogen production and the predicted ANN values. As shown in this figure, the value of $R^2$ for the ANN model was found to be up to 0.92. The ANN was an excellent model because of the lowest error and the highest coefficient values. The obtained results indicated that the simulation model based on the ANN is practical.

**Conclusion**

According to the obtained results, the following point can be concluded.

- The AMBR could simultaneously be used for the wastewater treatment and hydrogen production.
- With increasing the OLR value from 0.5 to 8 g COD/L.d, the hydrogen production and also VHPR improved.
- Hydrogen yields decreased from 1.58 to 0.97 mol H2/mol glucose as the OLR increased from 0.5 to 8 g COD/L.d
- The concentration of both VFAs and solvents kept increasing with OLR. During the AMBR operation, the dominant SEPs during the AMBR operation were acetic and butyric acids in the all OLRs.
- The ANN model was well fitted to the experimental obtained data from the AMBR, and was able to simulate the COD removal and hydrogen production.

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Ethical issues
The authors certify that this manuscript is the original work of the authors, and all data collected during the study are presented in this manuscript, and no data from the study has been or will be published separately elsewhere.

Competing interests
The authors declare that they have no conflict of interests.

Authors’ contributions
Mohammad Mehdi Amin supervised the study, Mohammad Ghasemian and Ali Fatehizadeh was the main investigators, and Mohammad Ghasemian, Ensieyh Taheri, and Ali Fatehizadeh drafted the manuscript. All authors read and approved the final manuscript.

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