Data Article

Data showing the effects of temperature and time variances on nano-additives treatment of mild steel during machining

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ABSTRACT

The effects of temperature and time variances on nano-additives treatment of mild steel during machining was presented in this study. Mild steel of 150 kg mass containing 0.56% carbon was charged into the furnace at melting and pouring temperature of 1539 and 1545 °C respectively. Also charged into the furnace with the mild steel were 0.05% max phosphorous and a bit of sulphur. Thereafter, the sample was cooled and annealed at a temperature of 900 °C for 9 h and then cooled to 300 °C of hardening, normalizing and tempering respectively. The treated samples were then soaked with pulverized in palm kernel shell and barium carbonate (20%) energizer at respective temperatures (800, 850, 900 and 950 °C) and time variances (60, 90 and 120 min) in a muffle furnace. The developed tool was tested on a lathe machine to evaluate its performance. The surface and core hardness, wear resistance and toughness were carried out using the hardness tester, Roto-pol–V and impact tester respectively. This is essential for predicting the useful life of the tool in service.

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Specifications Table

| Subject area               | Mechanical Engineering and Materials Engineering. |
|----------------------------|--------------------------------------------------|
| More specific subject area | Metallurgical Engineering, Production Engineering and Surface Engineering. |
| Type of data               | Table, text and graph.                           |
| How data was acquired      | Wear and hardness tests were measured using Rotopol –V and Impact tester respectively. The samples were weighed before and after to get the initial weight and grit was fixed at a point for the sample to revolve at a specific time 600 s/10 min. The maximum energy of the machine used was 300 J of Charpy impact and length of the sample = 55 mm, V-Knut was used at point 22.5 mm. The data was taken at particular interval of machining. |
| Data format                | Raw and analyzed.                                |
| Experimental factors       | Metallographic preparation was conducted. It involved the grinding and polishing of each sample on emery papers with grit size of 30, 160, 300, 600, 1000 and 1200. Other factors are the melting and pouring temperature, the quenching medium, normalizing and normalizing operations and the time (duration) of each operation. |
| Experimental features      | The casting was carried out at melting and pouring temperature of about 1539 and 1645 °C respectively. Heat treatments (annealing, hardening, normalizing and tempering) were conducted on the samples at respective temperatures of 900 and 400 °C for 90 °C per hour then hold for 2 h with natural cooling. The samples were further soaked at respective temperatures and time variances of 800, 850, 900 and 950 °C for 60, 90 and 120 min in a muffle furnance. Test was carried out to check the effects on the samples. |
| Data source location       | Federal University of Agriculture, Abeokuta, Ogun-State, Nigeria. |
| Data accessibility         | Data are available within this article           |

Value of the data

- The data for the hardness and toughness of the developed samples can be used to determine the optimum efficiency of case-hardened cutting tools.
- Wear rate and machining test data could be used to predict the performance of any carburized tool during the machining operation.
- The data on the use of nano-additive concentration can be used to determine the accuracy level of the carburization at each temperature and time.
- Also, the dataset could be used to predict the most significant heat treatment parameters.
- The data obtained could be used in investigating the trend in surface and micro hardness profile of carburized cutting tool.

1. Data

The study utilized scrap (steel) for casting using Palm Kernel Shell (PKS) as a nano-additives carbon to develop several cutting tool. Compositional analyses before and after the casting was done with melt correction of carbon increase from 0.560 to 0.65 during melting as shown in Table 1. Data of the micro-hardness values in Table 2 present the core of the carburized samples, while the surface hardness values depict the case of the carburized samples. Tests carried out on the treated cutting tool measured its weight loss, wear volume, wear rate, wear resistance and impact/toughness as shown in Tables 3 and 4.
2. Experimental design, materials and methods

The pulverized carbon additive was prepared from palm kernel shell by drying, grinding, milling and sieving. The casting process was carried out with an induction furnace having a maximum temperature capacity of 3000 °C [1–6]. The furnace was used to melt 150 kg mass of carbon steel at melting temperature of approximately 1539 °C and a pouring temperature of 1545 °C [6–8]. The samples were annealed at 900 °C at a rate of 90 °C per hour then, it was held for 2 h to cool. Hardening took place at 900 °C a rate of 100 °C/h for 9 h and then it was followed by force-cooling from 900 °C in an oil quenching medium. Thereafter, normalization was conducted at 900 °C at a rate of 100 °C/h for 9 h. Finally, the sample was tempered by heat treatment of 400 °C at a rate of 100 °C/h for 4 h with natural cooling [8–12]. The treated carbon steel was machined into 24 pieces each of 200 mm × 10 mm × 10 mm and 20 mm × 10 mm × 10 mm respectively. Thereafter, they were charged into furnace at temperatures of 800, 850, 900 and 950 °C and duration of 60, 90, 120, 180 min for each stage [12–14]. In order to evaluate the performance of the developed tool machining tests were carried out on the lathe machine [14–16]. Furthermore, the hardness tester, Rotopol-V and impact tester were used to conduct surface and core hardness, wear resistance and energy absorbed tests as shown in Figs. 1 and 2 on the developed sample tool [16–18].
Table 3
Summary of weight loss, wear volume and wear resistance results.

| Sample | Weight loss (g) | Wear volume (cm³) | Wear resistance (× 10 exp-7) |
|--------|-----------------|-------------------|-----------------------------|
| A      | 18.0            | 203.0             | 4.57                        |
| B      | 20.0            | 358.0             | 1.83                        |
| C      | 77.0            | 998.0             | 4.74                        |
| D      | 14.0            | 281.0             | 2.61                        |
| E      | 20.0            | 360.0             | 1.83                        |
| F      | 18.0            | 332.0             | 2.03                        |
| G      | 38.0            | 590.0             | 9.62                        |
| H      | 24.0            | 410.0             | 1.52                        |
| I      | 39.0            | 603.0             | 9.37                        |
| J      | 87.0            | 212.0             | 4.20                        |
| K      | 47.0            | 706.0             | 7.77                        |
| L      | 40.0            | 616.0             | 9.13                        |
| Control| 75.0            | 968.0             | 2.05                        |

Table 4
Energy absorbed test.

| S/N | Sample (S) | Energy absorbed (J) |
|-----|------------|---------------------|
| 1   | A          | 23.0                |
| 2   | B          | 22.0                |
| 3   | C          | 32.0                |
| 4   | D          | 71.0                |
| 5   | E          | 30.0                |
| 6   | F          | 50.0                |
| 7   | G          | 75.0                |
| 8   | H          | 36.0                |
| 9   | I          | 20.0                |
| 10  | J          | 16.0                |
| 11  | K          | 16.0                |
| 12  | L          | 24.0                |
| 13  | Control    | 17.0                |

Fig. 1. Wear resistance against carburizing temperature.
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Transparency document. Supporting information

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