Research Article

Improvement of Thermal and Mechanical Properties of Vietnam Deproteinized Natural Rubber via Graft Copolymerization with Methyl Methacrylate

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In this study, we investigated the improvement of the thermal and mechanical properties of Vietnam deproteinized natural rubber (DPNR) via graft copolymerization of methyl methacrylate (MMA). The graft copolymerization was achieved successfully in latex stage using tert-butyl hydroperoxide (TBHPO) and tetra-ethylenepentamine (TEPA) as radical initiators at 30°C. By grafting with various MMA feeds and initiator concentration of 6 × 10⁻⁵ mol/g-rubber, the highest grafting efficiency and conversion were achieved at MMA of 15 wt.% per kg of rubber, 68% and 90%, respectively. The structure of grafted copolymers was characterized by ¹H NMR, FTIR-ATR, and GPC, and thermal properties were investigated through DSC and TGA measurements. These showed that graft copolymers were more stable and rigid than DPNR. Storage modulus (G') of graft copolymer was found to double that of DPNR, which contributed to the formation of graft copolymer. After sulfur vulcanization, the mechanical properties of DPNR-graft-PMMA, such as tensile strength, tear strength, and hardness, were improved significantly. Curing behaviors of the graft copolymers were found to be remarkably better than virgin DPNR.

1. Introduction

In recent years, environmental issues have become more important. As a result, the use and development of renewable materials as natural polymers are becoming a new trend in society. Natural rubber (NR) obtained from the Hevea Brasiliensis tree is considered to be a renewable resource and an environmentally friendly material [1]. Vietnam ranked third as NR producer as well as exporter in the world in 2017 [2]. Therefore, NR is an abundant green material and also an important resource of Vietnam’s economy. Global demand for natural rubber has however increased rapidly in the past decade, driven particularly by China’s economic emergence [3]. Additionally, the price of NR has fluctuated for more than a year due to some factors including climate conditions, which can directly affect NR’s quality [1, 2, 4, 5]. The recent rise of the global NR consumption has encouraged Vietnam as the main NR producing country to expand its expertise with rubber trees into a multipurpose crop for the national economic development. This will improve the social conditions of rural areas and lead to regreening bare land towards environmental protection. Besides various excellent physical properties, including high elasticity and high tensile strength, NR also has some undesirable properties such as low heat resistance and poor aging properties, as well as low oil resistance due to the low saturation degree of the molecular chain [1, 6–8]. The quest for NR’s practical applications led to the investigation into the enhancement of NR’s properties. This also contributes to the sustainable management of natural resources by the development of highly functional polymers.
based on natural rubber and furthermore boots Vietnam’s rubber industry [2].

To limit NR’s drawbacks, many methods have been attempted from blending NR with other synthetic materials or adding fillers to chemical modification [9–13]. Efficient paths towards adding value to NR have been followed by incorporating new functional groups onto the natural polymer, chemical modification such as hydrogenation [14–17], epoxidation [18], and copolymerization with vinyl monomers over more than 50 years [3]. Among those, the graft copolymerization has received considerable interest from scientists, which is shown by the increasing number of studied monomers. In addition, different aspects of this modification have been examined recently. Some prominently used vinyl monomers are acrylonitrile (AN) [19], methyl methacrylate (MMA) [20–23], maleic anhydride (MA) [24], and styrene [2, 7, 8]. MMA and styrene are the most suitable for grafting with NR because of their high grafting efficiency. Due to the high polarity of MMA, the graft copolymer of NR will have outstanding prospects in the fields of adhesive and conducting polymer materials.

Thermal and mechanical properties of natural rubber are very important for its applications, since NR products are often exposed under real environmental conditions, including sunlight, UV irradiation, and high temperature. Therefore, it is necessary to improve NR properties as well as its thermal stability to widen its practical application. Among various monomers being grafted on NR, MMA is one of the precursors of thermoplastic polymer. Subsequently, the product, i.e., DPNR-graft-PMMA possesses good thermal stability and high resistance to heat and light. Hence, chemical modification of NR using MMA through graft copolymerization is promising for improving the mechanical and thermal properties of NR. However, in order to prolong the lifecycle for NR materials, vulcanization is necessary to be performed for NR. Thus, cure characteristics and properties of graft copolymer in vulcanized state are also an important aspect to apply the materials in human life.

In previous work, graft copolymerization of MMA onto NR’s backbone has been studied for several years and is conducted via radical emulsion polymerization using redox initiators [25–27]. Potassium persulfate (K₂S₂O₈)-sodium thiosulfate (Na₂S₂O₃) [27], cumene hydroperoxide CHPO-TEPA [25], and TBHPO-TEPA [2, 7, 21, 28] are examples. Among these, TBHPO-TEPA initiator is the dominant choice for many researchers due to possible reaction at ambient temperature. Besides this, the presence of protein in NR latex will adversely impact the grafting process. According to previous studies [4, 7], protein can be a free-radical scavenger and terminate the free-radical species of the graft copolymerization. Thus, protein should be removed before graft copolymerization to avoid undesired reactions.

In the present work, graft copolymerization of MMA onto Vietnam DPNR has been studied to obtain high conversion and high grafting efficiency using TBHPO-TEPA as radical initiators at room temperature. Nuclear magnetic resonance (¹H NMR) and attenuated total reflection/Fourier transform infrared spectroscopy (ATR/FTIR) were used to confirm the structure of the grafted copolymer. Gel permeation chromatography (GPC) measurements were conducted to determine the molecular weight and molecular weight distribution of DPNR and grafted copolymer samples. The thermal and dynamic mechanical properties of the graft copolymer have also been investigated. The grafted NR was afterward vulcanized with sulfur in order to examine the curing and mechanical properties of this copolymer as a commercial material.

2. Experimental

2.1. Chemicals

2.1.1. Chemicals for Copolymerization. High ammonium natural rubber latex (HANR, 60 wt.% of dry rubber content rubber) was supplied by Merufa Co., Ltd, Vietnam. Sodium dodecyl sulfate (SDS, 99 wt.%) and MMA (98 wt.%) were purchased from Tokyo Chemical Industry Co., Ltd, Japan. Urea (99 wt.%) was obtained from Nacalai Tesque, Inc (Kyoto, Japan). TEPA (95 wt.%), TBHPO (68 wt.%), and other chemical products for copolymerization preparation were purchased from Sigma-Aldrich.

2.1.2. Chemicals for Vulcanization. The sulfur, zinc oxide, stearic acid, accelerators including disulfua mercaptothiazole (DM), mercapthobenzothiazoyle (M), and antioxidant RD (TMQ, 2,2,4-Trimethyl-1,2-Dihydroquinoline) were purchased from Nacalai Tesque Inc.

2.2. Preparation of DPNR Latex and Graft Copolymer. DPNR latex was prepared by incubating diluted HANR 60% dry rubber content (DRC) with 0.1 wt.% urea in the presence of 1 wt.% SDS at 30°C for 1 hour and followed by centrifugation at 10,000 rpm for 30 minutes. After centrifugation, the cream fraction was separated and dispersed in 1 wt.% SDS solution to make 30% DRC latex. The latex was washed two more times by centrifugation before obtaining the final DPNR, which was dispersed and preserved, respectively, in a 0.9 and 0.8 wt.% SDS. This SDS concentration level in DPNR latex was used for graft copolymerization with MMA to avoid the coagulation of colloidal suspensions. The removal of proteins in HANR by incubation of the rubber latex with urea has been proved effective in laboratory and batch processing [4].

The DPNR was flushed with nitrogen gas for an hour at 30°C to remove any dissolved oxygen in the latex and then graft copolymerized with MMA using a redox initiator system comprising TBHPO and TEPA with mol ratio of 1:1. The reaction was kept for 2.5 hours at 400 rpm under N₂ atmosphere. Thereafter, the unreacted monomer was removed in a rotary evaporator under reduced pressure, and the obtained emulsion was dried under reduced pressure at 40°C for a week. Soxhlet extraction was performed to purify the product. Free-poly methyl methacrylate obtained after extraction with acetone in darkness for 24 hours and drying under reduced pressure for a week. The schematic to perform the graft copolymerization is indicated in Figure 1.
2.3. Preparation for Vulcanization of DPNR and DPNR-Graft-PMMA. The vulcanization was carried out using an internal mixer (Brabender, Germany). A typical vulcanization recipe can be seen in Table 1. In the process, we used a mixing chamber of 60 cm³ and the batch size was 50 ± 5 g.

The mixer was operated at a constant rotor speed at 50°C. The mixing for each batch took place for 13 minutes. Firstly, a rubber sample was added into the chamber and mixed for 6 minutes. Then, stearic acid, ZnO, and RD were added sequentially. The mixture was afterward mixed additionally for 4.5 minutes. Sulfur, DM, and M were then added into the system and mixed for 2.5 minutes. The mixture was immediately removed from the chamber and left at room temperature for 24 hours. The samples were kept at room temperature for 24 hours and then directly subjected to a rotorless rheometer for defining cure characteristics or cure time for the following pressing step. After that, the produced rubber was pressed in a hot press at 150°C and 10 MPa for about 5 minutes (for the DPNR-graft-PMMA samples) or 14 minutes (for the DPNR sample).

After pressing, the obtained rubber sheets were cooled down to room temperature and then cut into small samples with a size according to the ASTM D412-16 standard for each mechanical testing.

2.4. Characterization. Conversion and grafting efficiency (GE) of MMA were calculated by gravimetric method follows these equations [29]:

\[
\text{Conversion, } \% = \frac{m_1 - m_0}{m} \times 100
\]  

\[
\text{GE, } \% = \frac{PP_1 - EP_0}{PP_1} \times 100
\]

\( m_1 \): weight of product after grafting  
\( m_0 \): weight of DPNR before grafting  
\( m \): weight of MMA monomer  
\( PP_1 \): mass of produced polymer  
\( EP_0 \): mass of extracted polymer

Proton nuclear magnetic resonance (1H NMR) spectra were recorded on a JEOL JNM-ECA 400 MHz spectrometer; samples were swollen with deuterated chloroform. The spectrum was collected for 128 scans.

Attenuated total reflection/Fourier transform infrared spectroscopy (ATR/FTIR, Bruker TENSOR 27 FTIR) was used for the analysis of the NR samples. The frequency region between 4000 ÷ 400 cm⁻¹ was examined.

Molecular weight and molecular weight distribution of DPNR and DPNR-graft-PMMA samples were measured with a TOSOH GPC consisting of a TOSOH CCPD pump, RI-8012 differential refractometer, and UV-8011 UV detector. The measurement was made at room temperature with the flow rate of the mobile phase, i.e., THF, of 0.5 ml/min. Standard polystyrene, purchased from PSS Polymer Standards Service GmbH (Mainz, Germany), was used as a GPC standard material for calculating the molecular weight.

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**Table 1: Typical recipe used for the vulcanization of rubber samples.**

| Ingredients              | Compound (part per hundred of rubber) |
|--------------------------|---------------------------------------|
| Rubber*                  | 100                                   |
| Stearic acid             | 2.5                                   |
| ZnO                      | 5                                     |
| Antioxidant RD           | 1.5                                   |
| Sulfur                   | 1.7                                   |
| Disulphua mercaptothiazole (DM) | 0.8                                   |
| Mercaphtothiazole (M)    | 0.2                                   |

*Including DPNR and graft copolymers with different monomer concentrations.
The dynamic mechanical properties (DMA) were determined using an Anton Paar Physica MCR 302 analyzer. Measurements of the storage modulus, the loss modulus, and the damping factor \( \tan \delta \) were performed at 298 K and frequency range of 0.1 to 16 Hz. Parallel plate geometry of 12 mm diameter was used. The measurement was carried out within the range of linear viscoelasticity.

Differential scanning calorimetry (DSC) with a DSC 7020 Exstar analyzer was used to measure the glass transition temperature \( (T_g) \) of both DPNR and DPNR-graft-PMMA samples. The samples were cooled down to \(-90^\circ\text{C}\) using liquid nitrogen and heated up to 150\(^\circ\text{C}\) at a heating rate of 10\(^\circ\text{C}/\text{min}\).

Thermal gravimetric analysis (TGA) experiments were carried out using a Shimadzu DTG-60H analyzer under argon atmosphere. The temperature ranged from 30 to 600\(^\circ\text{C}\). The heating rate was 10\(^\circ\text{C}/\text{min}\).

The curing behaviors were assessed by using a Rotorless Rheometer RLR-4 (Japan), at 150 ± 1\(^\circ\text{C}\), according to ASTM D2084-95. The tensile tests dumbbell-shaped samples were cut from the molded rubber sheets according to ISO 37:2011. Both tensile strength and elongation at break are determined on an Instron 5582 Universal Testing Machine with a crosshead speed of 300 mm/min. The analysis here focused mainly on the presence of PMMA grafted onto DPNR in general. The bands at 1732 and 1148 cm\(^{-1}\), observed for the DPNR-graft-PMMA 15\% sample, are related to the carbonyl groups (C=O stretching) and C-O-C stretching when MMA was grafted on the natural rubber backbone [27]. This proves the presence of the PMMA segment in DPNR-graft-PMMA, and this is a strong evidence to confirm the occurrence of grafting reaction.

3. Results and Discussion

3.1. Graft Copolymerization of MMA. Figure 2 shows the effect of monomer concentrations, ranging from 5 to 20 wt.% per kg of dried rubber, on the conversion and grafting efficiency of MMA onto DPNR.

It can be seen that both the grafting efficiency and conversion increase with increasing content of MMA up to 15 wt.%. However, when the monomer content exceeds 15 wt.%, the GE decreases, while the conversion tends to rise continuously. This might be explained by MMA’s homopolymerization becoming dominant over the graft copolymerization of MMA onto the NR particles. At a high MMA concentration (20 wt.%), monomers are more likely to react with each other than with DPNR’s backbone [7, 30]. The highest grafting efficiency was about 68% at 15 wt.% of MMA, and it decreased to 62% at 20 wt.% MMA. Therefore, the optimum condition for graft copolymerization of MMA is determined to be 15 wt.% of MMA. This sample is purified with acetone extraction and subjected for characterization of graft copolymer in the next section.

3.2. Structural Characterization of the Graft Copolymer. Figure 3 exhibits the characteristic absorption bands of DPNR and DPNR-graft-PMMA 15\% MMA. There are three mentioned characteristic peaks attributed to isoprene: the C-H stretching vibration in aliphatic C-H bond at high frequency 2960 cm\(^{-1}\), C=C bending vibration at 840 cm\(^{-1}\), and C-H stretching vibration at 1443 cm\(^{-1}\). A similar type of observation in the IR spectra was already reported [31, 32]. The analysis here focused mainly on the presence of PMMA grafted onto DPNR in general. The bands at 1732 and 1148 cm\(^{-1}\), observed for the DPNR-graft-PMMA 15\% sample, are related to the carbonyl groups (C=O stretching) and C-O-C stretching when MMA was grafted on the natural rubber backbone [27]. This proves the presence of the PMMA segment in DPNR-graft-PMMA, and this is a strong evidence to confirm the occurrence of grafting reaction.

The presence of PMMA in natural rubber is also further proved by the \(^1\text{H}-\text{NMR}\) method using CDCl\(_3\) as a solvent of the measurement. In Figure 4, the characteristic signals of cis-1,4-isoprene units appeared at 1.67, 1.93, and 4.95 ppm.
These can be attributed to the methyl, methylene, and unsaturated methine protons of cis-1,4-isoprene units, respectively [33, 34]. On the other hand, an additional signal at about 3.58 ppm was assigned to the protons of O-CH$_3$ of the grafted PMMA [27]. This is in agreement with above FTIR assignments. Therefore, the combination of $^1$H NMR data and FTIR results surely confirms the occurrence of grafting polymerization of MMA onto DPNR.

3.3. Molecular Weight Distribution. Figure 5 shows the molecular weight distribution for DPNR and DPNR-graft-PMMA 15 wt.%. The appearance of a sharp peak at about
$3 \times 10^3$ Da implies that new particles were formed during the graft-copolymerization. This is evident from the formation of various components in the resulting materials, which are grafted PMMA and PMMA homopolymer. The Gaussian distribution is related to DPNR. After the graft-copolymerization of MMA, the particle size distribution became multimodal. Table 2 shows the weight averaged molecular weight ($M_w$), number averaged molecular weight ($M_n$), and polydispersity $PDI = M_w/M_n$ for the uncross-linked polymers in the sol fraction [35]. PDI was found to be $1.1789 \times 10^2$. It was too high for the obtained polymer. This may be purified by fractional precipitation to remove the low molar mass of residues [36, 37]. In the presence of TBHPO and TEPA initiators, chain session or chain degradation could possibly take place. The shoulder peak at about $10^5$ Da could indicate the formation of unstable molecules, which cannot polymerize. The uncross-linked polymers in the sol fraction gave lower $M_n$ and $M_w$ values than those before the graft copolymerization. This result may suggest that various molecules with different chain lengths of chain appeared in DPNR-graft-PMMA [27]. In terms of practical applications, it is vital to do the cure step for the graft copolymerization. It will be presented below.

### Table 2: $M_n$, $M_w$, and PDI for DPNR and DPNR-graft-PMMA 15 wt.%.

| Samples                  | $M_n$          | $M_w$          | PDI = $M_w/M_n$ |
|--------------------------|----------------|----------------|-----------------|
| DPNR                     | $7.4769 \times 10^3$ | $8.8145 \times 10^5$ | $1.1789 \times 10^2$ |
| DPNR-g-PMMA 15 wt.%      | $1.9238 \times 10^3$ | $5.4952 \times 10^5$ | $2.8565 \times 10^2$ |

#### 3.4. Thermal Properties

The glass transition temperatures ($T_g$) of the materials were investigated with differential scanning calorimetry (DSC). The curves for DPNR and DPNR-graft-PMMA with 15 wt.% MMA are shown in Figure 6. There was only one $T_g$ observed at $-62.5^\circ$C, which corresponds to the cis-1,4 polyisoprene structures of the DPNR, which has also been reported in Derouet’s study [23]. It can be seen that after graft copolymerization, the $T_g$ of graft copolymer slightly shifts to $-60.5^\circ$C due to the presence of grafted PMMA chain on the NR molecules. The appearance of PMMA chain may result in the stiffening or the increased interchain interaction between polar functional groups in the graft copolymer [30].

TGA curves of DPNR and the graft copolymer are shown in Figure 7. It can be seen that the degradation of DPNR occurs vastly at the decomposition temperature ($T_d$) of $365.36^\circ$C. However, DPNR-graft-PMMA showed a higher decomposition temperature at $373.77^\circ$C. This could be ascribed in terms of decreasing levels of reactive unsaturated backbone and therefore less susceptibility to degradation. Thus, it is clear that the MMA grafting improved the thermal stability of the DPNR. This observation is in agreement with the thermal degradation of modified natural rubber with other vinyl monomers [5, 32, 34, 38, 39].

#### 3.5. Dynamics Mechanical Properties of DPNR and DPNR-Graft-PMMA

Figure 8 illustrates the frequency dependence of storage modulus $G'$ at rubbery plateau region for DPNR.
and DPNR-graft-PMMA 15 wt.%. The value region of $G'$ for DPNR was about 0.1 MPa, similar to values reported in literature [28, 29]. By graft copolymerization of MMA onto DPNR, the value of $G'$ of DPNR-graft-PMMA 15 wt.% was increased double at high-frequency region. Hence, it is proved that graft copolymerization of MMA onto NR increases the ability of natural rubber to store deformation energy [29].

Figure 9 shows the loss modulus ($G''$) in the plateau region versus the frequency for DPNR and DPNR-graft-PMMA samples. The loss modulus value of DPNR was $10^4$ Pa. We can readily demonstrate that this value is typical for conventional uncross-linked rubber and is similar to the $G''$ of NR previously reported [29, 40]. In addition, the loss modulus decreases as the frequency increases [41]. In contrast, the loss modulus of DPNR-graft-MMA increases gradually with the frequency, indicating its different behavior compared to ordinary rubber. DPNR-graft-PMMA exhibits both entropic elasticity and energetic elasticity [29, 41].

Figure 10 plots the loss tangent (tan δ) versus the frequency in the plateau region for DPNR and DPNR-graft-PMMA 15 wt.%. The values of tan δ for DPNR decrease with increasing of frequency. Tan δ for the grafted DPNR is almost independent on the frequency in the low-frequency region.
region but decreases slightly in the high-frequency region. This observation agrees with the frequency dependency of the $G'$ and $G''$. The trend of tan δ with frequency also demonstrates that DPNR-graft-PMMA generates entropic elasticity [41] due to the behavior of DPNR, and energetic elasticity due to the grafting of MMA.

3.6. Cure Behaviors and Properties of Vulcanized DPNR-Graft-PMMA. The cure characteristics of DPNR-graft-PMMA were determined via values of the scorch time ($t_{s2}$), cure time ($t_{c90}$), minimum torque ($M_L$), maximum torque ($M_H$), torque difference ($M_H - M_L$), and cure rate index (CRI) according to ASTM D5289, as shown in Table 3. The CRI is related to the speed at which the cure reaction occurs and was calculated as follows [42]:

$$CRI = \frac{100}{t_{c90} - t_{s2}}$$

The effects of the initial amount of MMA on the curing characteristics of DPNR-graft-PMMA were examined separately using a moving die rheometer. The values of the scorch time ($t_{s2}$) and cure time ($t_{c90}$) of DPNR-graft-PMMA compounds were found to be much smaller than virgin DPNR, indicating that the presence of MMA in DPNR’s backbone could accelerate vulcanization during the induction period of curing and shorten the optimum cure time. This is confirmed by an increase in CRI for higher degree grafting. Higher degrees of grafting were caused by crosslinking reactions via the sulfidic linkages as well as reactions of carbonyl groups between MMA molecules [43].

Figure 11 shows the influence of the weight concentration of MMA used in the graft copolymerization on torques. Theoretically, the torque relates to the shear modulus or the stiffness of the rubber materials. As can be seen in Table 3, the minimum torque $M_L$ and maximum torque $M_H$ of all DPNR-graft-PMMA compounds have higher values than the virgin DPNR compounds. This might be caused by an increasing chemical interaction between the DPNR backbone and MMA, causing limited mobility for DPNR [44]. The maximum torque ($M_H$) and delta torque ($M_H - M_L$) are significantly related to the amount of crosslinking, crosslink density, and interactions in the rubber vulcanization. The DPNR-graft-PMMA 15 wt.% compound exhibited the highest $M_H$. The increase in ($M_H - M_L$) elucidated an increased crosslink density in compounds by crosslinking from sulfidic linkages and polar MMA as mentioned before.
The mechanical properties of copolymers and DPNR vulcanizates are illustrated in Table 4. The tensile strength and tear strength (at break) of DPNR vulcanizate increased significantly with the incorporation of MMA, in agreement with previous literature [45]. The hardness for DPNR-graft-PMMA was 1.5-2 times higher than for DPNR. Whereas in elongation at break, the values for DPNR-graft-PMMA compounds were much lower than those for DPNR. All those trends could be the result of interaction between DPNR and MMA, which may lead to improved physical entanglement and a stiffer structure [42, 45]. In addition, it can be seen that for MMA feeds of 15 wt.% MMA and higher, the tensile and tear strength rose negligibly, while the elongation at break decreased remarkably and the hardness value increased significantly.

In conclusion, by introducing MMA segment onto DPNR molecules, the material becomes harder after vulcanization, and the curing times are shorter. However, the small differences observed in cure characteristics for the studied vulcanized DPNR-graft-PMMA samples indicated that the difference in amount of MMA does not have a significant effect on the torque of sulfur vulcanized DPNR-graft-PMMA.

4. Conclusions

The graft copolymerization of MMA onto DPNR in latex stage with TBHPO/TEPA as radical initiators was performed successfully. This was confirmed by FTIR as well as by $^1$H NMR spectra, where the presence of MMA on the synthesized material was observed. The grafted DPNR proved to
have more stable thermal properties, demonstrated by increased values in both $T_g$ and $T_d$. It was revealed that the thermal properties and the rigidity of graft copolymer, DPNR-graft-PMMA, were improved after graft copolymerization. The DPNR-graft-PMMA with 15 wt.% MMA exhibited better mechanical properties in terms of practical application. By introducing PMMA into the NR molecule, the storage modulus of NR also increased remarkably. Natural rubber was vulcanized faster and more efficiently than DPNR due to the presence of polar functional groups. The sulfur-vulcanized DPNR-graft-PMMA exhibited better mechanical properties than cured DPNR.

**Data Availability**

The data used to support the findings of this study are included within the article.

**Conflicts of Interest**

The authors declare that they have no conflicts of interest.

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