An analysis of the temperature dependence of force, during steady shortening at different velocities, in (mammalian) fast muscle fibres

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Abstract We examined, over a wide range of temperatures (10–35°C), the isometric tension and tension during ramp shortening at different velocities (0.2–4 L0/s) in tetanized intact fibre bundles from a rat fast (flexor hallucis brevis) muscle; fibre length (L0) was 2.2 mm and sarcomere length ~ 2.5 μm. During a ramp shortening, the tension change showed an initial inflection of small amplitude (P1), followed by a larger exponential decline towards an approximate steady level; the tension continued to decline slowly afterwards and the approximate steady tension at a given velocity was estimated as the tension (P2) at the point of intersection between two linear slopes, as previously described (Roots et al. 2007). At a given temperature, the tension P2 declined to a lower level and at a faster rate (from an exponential curve fit) as the shortening velocity was increased; the temperature sensitivity of the rate of tension decline during ramp shortening at different velocities was low (Q10 0.9–1.5). The isometric tension and the P2 tension at a given shortening velocity increased with warming so that the relation between tension and (reciprocal) temperature was sigmoidal in both. In isometric muscle, the temperature T0.5 for half-maximal tension was ~ 10°C, activation enthalpy change (ΔH) was ~ 100 kJ mol⁻¹ and entropy change (ΔS) ~ 350 J mol⁻¹ K⁻¹. In shortening, these were increased with increase of velocity so that at a shortening velocity (~4 L0/s) producing maximal power at 35°C, T0.5 was ~ 28°C, ΔH was ~ 200 kJ mol⁻¹ and ΔS ~ 700 J mol⁻¹ K⁻¹; the same trends were seen in the tension data from isotonic release experiments on intact muscle and in ramp shortening experiments on maximally Ca-activated skinned fibres. In general, our findings show that the sigmoidal relation between force and temperature can be extended from isometric to shortening muscle; the implications of the findings are discussed in relation to the crossbridge cycle. The data indicate that the endothermic, entropy driven process that underlies crossbridge force generation in isometric muscle (Zhao and Kawai 1994; Davis, 1998) is even more pronounced in shortening muscle, i.e. when doing external work.

Keywords Temperature effects · Force-velocity relation · Force generation · Enthalpy · Entropy · Thermodynamics

Introduction

The maximal isometric force of mammalian muscle increases in warming from low temperatures to physiological temperatures (>30°C; Hadju 1951; Ranatunga and Wylie 1983); the subsequent, more detailed, studies showed that the force versus reciprocal absolute temperature is sigmoidal with a half- maximal force occurring at 8–10°C (Ranatunga 1994, 1996; Coupland and Ranatunga 2003). Studies that used rapid temperature-jump (T-jump) and other techniques also showed that the muscle force generation is endothermic (Davis and Harrington 1987; Goldman et al. 1987; Bershitsky and Tsaturyan 1992; Zhao and Kawai 1994; Ranatunga 1996) so that the rate of force rise to a small T-jump increased with temperature (Q10 ~ 3–4). It may be argued that, if active isometric muscle in steady state can be simplified to and treated as a two state system—pre-force generating and force generating states, a sigmoidal temperature dependence of force is expected since increase of temperature favours force...
generation (Davis 1998). Additionally, this force generating transition in isometric muscle has been shown to be before the release of inorganic phosphate in the actomyosin crossbridge/ATPase cycle (Fortune et al. 1991; Kawai and Halvorson 1991; Dantzig et al. 1992; Ranatunga 1999; Sleep et al. 2005). Furthermore, when the crossbridge cycle was altered with added inorganic phosphate (Pi) or MgADP (products released from ATP hydrolysis by crossbridges), the sigmoidal relation between force and temperature was shifted to higher (with Pi; Coupland et al. 2001) or lower temperatures (with MgADP; Coupland et al. 2005).

Although the sigmoidal temperature dependence of force in isometric muscle has been well characterized and its significance discussed (see above), whether or not such a relation can define the temperature dependence of force in shortening muscle, doing external work, is not known. At a given temperature, the active muscle force decreases during steady shortening in a velocity dependent manner leading to the characteristic force–shortening velocity relation (Hill 1938) and this may be due to shortening-enhanced detachment, and cycling, of crossbridges (Huxley 1957), a change in the crossbridge cycle. Moreover, the force–shortening velocity relation in mammalian muscle is shown to be temperature sensitive (Ranatunga 1982, 1984) so that the maximal mechanical power output (force x velocity) at 10°C is only ~5% of that at the physiological temperatures (Ranatunga 1998); also, we reported recently that the force generation induced by a T-jump in muscle, although absent in lengthening, is pronounced during steady shortening (Ranatunga et al. 2007). Thus, it would be important to examine the temperature dependence of force in shortening muscle and this was the main aim of the present study. Experimental data for isometric force and force during ramp shortening at different velocities are examined at a range of temperatures in tetanized intact (rat fast) muscle fibres and in maximally Ca-activated skinned (rabbit psoas) fast muscle fibres; previous data from isotonic release experiments on intact rat fast muscle (Ranatunga 1984) are also re-analysed. Our results and analyses show that, for a given velocity, an approximate sigmoidal relation does exist between force and (reciprocal) temperature for shortening muscle but, compared to the isometric case, the relation is shifted to higher temperatures, its slope increased and more so at higher velocities.

Methods

Intact fibre experiments

Details of various methodologies and procedures used in intact fibre experiments have been reported previously (Coupland and Ranatunga 2003; Roots et al. 2007). The experiments used small bundles of 5–10 fibres isolated from a foot muscle (flexor hallucis brevis—FHB, containing ~90% type 2 (fast) muscle fibres Coupland and Ranatunga 2003) of adult male rats that were humanely killed with an intraperitoneal injection of an overdose (>200 mg kg⁻¹ body mass) of sodium pentobarbitone (Euthatal, Rhône Mérieux). By means of aluminium foil T-clips, attached within 0.2 mm of the fibre-end to each tendon, a preparation was made horizontally between a force transducer (AE 801 element; AME, Horten, Norway) and a servomotor, in a flow-through stainless steel chamber (volume ~2 ml). The chamber was perfused at 0.5 ml min⁻¹ with a physiological saline solution containing (mM): NaCl, 109; KCl, 5; MgCl₂, 1; CaCl₂, 4; NaHCO₃, 24; NaH₂PO₄, 1; sodium pyruvate, 10 and 200 mg l⁻¹ of bovine foetal serum; the solution was continuously bubbled with 95% O₂ and 5% CO₂.

Typically, a fibre bundle was first set-up for recording at 20°C and stimulated and the initial length (L₀) adjusted for maximal isometric tetanic tension; the sarcomere length for this setting was ~2.5 μm, as expected from the relationship between steady state tetanic tension and length for rat muscle fibres (Elmubarak and Ranatunga 1984; ter Keurs et al. 1984). Following an equilibration period of at least 30 min at 20°C, isometric tetanic contractions and tetanic contractions with ramp shortening of 20% L₀, applied on the tension plateau at five different velocities ranging from 0.2 to 4 L₀/s were recorded; the frequency and duration of tetanic stimulation was adjusted as appropriate for the recording (see Coupland and Ranatunga 2003). In each experiment similar recordings were then made at 5°C intervals during cooling to 10°C, warming from 10 to 35°C and cooling back to 20°C; solution temperature changes and control (±1°C) were achieved by a Peltier device fitted underneath the chamber and was monitored with a thermocouple inside the chamber. In a few experiments the change in the relative position of two markers, placed on the surface of the fibre bundle, was monitored using a position-sensitive detector (see Mutungi and Ranatunga 2001); the two small aluminium foil pieces were placed 0.5–0.7 mm apart, across the whole width of the bundle and at the force transducer end (excluding the tendon), so that the magnified images of their relative displacement provided a signal for the segment-length change (see Fig. 1c; Roots et al. 2007).

In six fibre bundle experiments in which a cooling-warming-cooling series was recorded, the mean (±s.e.m.) fibre length (L₀) and width of the fibre bundles were 2.17 (±0.11) mm and 148 (±2.5) μm, respectively. The mean (±s.e.m.) tetanic tension (P₀) was 237 (±29) kN m⁻² at 20°C; as a ratio of the P₀ recorded at the beginning, P₀ at the series end at 20°C was 0.88 (±0.02).
Skinned fibre experiments

As detailed in several previous papers (Ranatunga 1996; Coupland et al. 2001, 2007), these experiments used chemically skinned (using 0.5% Brij) single fibres from rabbit psoas muscle (fast). The buffer solutions contained 10 mM glycerol-2-phosphate (a temperature-insensitive pH buffer; pH = 7.1), 4.6 mM MgATP, 12 mM creatine phosphate, 15 mM EGTA (relaxing solution), CaEGTA (activating solution) or HDTA (pre-activating solution), 9 mM glutathione and ~50 mM potassium acetate. The solution compositions were calculated using a computer program for solving multi-equilibria, maintaining ionic strength of 200 mM, an excess free $[Mg^{2+}]$ of $\sim$1 mM and, in the activating solution, a free $[Ca^{2+}]$ of $\sim$0.032 mM. 1–2 mg ml$^{-1}$ creatine kinase ($\sim$300 units/mg, Sigma) was added to buffer solutions before use to decrease $[MgADP]$. All solutions also contained 4% Dextran (mol. mass $\sim$500 kDa) in order to compress the filament lattice spacing to normal dimensions.

The trough assembly was mounted on the stage of an optical microscope and the fibre could be moved and immersed in the different trough solutions (relaxing, pre-activating and activating solutions), by means of a lever mechanism. Using thermo-electric modules (Peltier units) fixed on the back wall, and with feedback from a small thermistor, the solution temperature in the front experimental trough could be changed and/or clamped at a desired pre-$T$-jump temperature and was monitored with a thermocouple. In order to maintain fibre stability, the temperature in the other troughs containing relaxing and pre-activating solutions was kept below $5^\circ$C by cooling fluid circulating through the trough assembly. The details of the technique of laser pulse induced $T$-jumps in muscle fibres have been described fully elsewhere (Ranatunga 1996, 1999). A $T$-jump was induced by a 0.2 ms laser pulse radiation ($\lambda = 1.32 \mu$m) from a Nd-YAG laser (Schwartz Electro-Optics) that entered the experimental trough through the front glass window. A laser pulse heated the buffer solution in the trough and the muscle fibre bathed in it; the heated fluid/fibre volume ratio was $>2500$. The elevated solution temperature remained constant for at least $\sim$500 ms and decreased only slowly (half-time longer than 5 s) afterwards (see Fig. 1, Ranatunga 1996).

A short fibre segment was attached using nitrocellulose glue between two metal hooks, one connected to the force transducer and the other to the motor. The sarcomere length was set to 2.5 $\mu$m using He–Ne laser diffraction and the fibre width and length were measured under light microscope; fibre length ($L_0$) was $\sim$2 mm in most experiments. In these experiments data were collected during warming from 8–9 to $\sim$30°C. The force responses to a standard $T$-jump of 3–4°C were also examined after a fibre was activated to steady isometric state and then exposed to steady shortening at a standard ramp velocity; one of two velocities were used in experiments, for convenience, referred to as low (0.05–0.09 $L_0$/s) and high (0.6–0.9 $L_0$/s).
velocities. Fibres were regularly examined under the microscope and an experiment was terminated when evidence of fibre damage was observed.

Data presented in the paper are from seven fibre experiments; their mean (± s.e.m.) maximum isometric (\(P_0\)) was 169 (±16) kN m\(^{-2}\) at 8–10°C.

Data recording and analysis

The outputs from the force transducer, the motor (fibre length) and the thermocouple (in skinned fibre experiments) were examined on digital cathode ray oscilloscopes and digital voltmeters and, using CED micro-1401 (Mk II) laboratory interface and Signal 3 software (Cambridge Electronic Design Ltd., Cambridge, UK), stored in a PC based computer. Various measurements were determined offline using Signal software and additional analysis, non-linear curve fitting etc were performed using Fig P (Biosoft, Durham, USA), Excel (Microsoft), and Mathcad 2000 professional (Mathsoft) software.

Distribution of tension data against temperature was approximately sigmoidal for isometric as well as for ramp shortening conditions and hence, for analytical and descriptive purposes, the multi-state crossbridge cycle in muscle was assumed reducible to be a two-step, two-state system, between no-force (pre-force generating) and force-bearing (generating) crossbridges, as indeed considered for isometric muscle force in previous studies (see Ranatunga 1984, 2001). In order to characterise the tension (\(P\))–temperature relation, the tension values from each preparation were normalised to its isometric force, at isometric muscle force in previous studies (see Ranatunga 1984, 2001) was extended to examine the temperature-dependence of steady force in shortening muscle. It consisted of three actomyosin/crossbridge states (1–3) in a linear scheme (Scheme 1) as:

\[
\text{States}
\]

\[
\begin{align*}
\text{Steps} & \quad \text{M/AM. ADP.Pi} & \quad \text{AM* ADP.Pi} & \quad \text{AM*. ADP + Pi} \\
\text{(I)} & \quad \text{(II)} & \quad \text{(III)} \\
\end{align*}
\]

Scheme 1 A minimal actomyosin/crossbridge cycle

According to the scheme, state 1 (M/AM, ADP, Pi) is a no force state (pooled pre-force generating and detached states) whereas states 2 and 3 (AM*, ADP, Pi and AM*ADP) are high (and equal) force generating states; the sum of the fractional occupancy of these two states was taken to represent isometric force and it was calculated as,

\[
\text{Force}_{(\text{isom})} = \text{Occ}(2 + 3) = (k_d k_a [\text{Pi}] + k_a k_c + k_a k_c) + k_d k_a [\text{Pi}] + k_a k_c + k_a k_c.
\]

where total is \((k_d k_a [\text{Pi}] + k_a k_c + k_a k_c) + k_d k_a [\text{Pi}] + k_a k_c + k_a k_c\).

The steady isometric tension behaviour at different Pi-levels and temperatures are predicted by changes in two *“equilibria”* (steady-states) in the cycle, step I \((k_d/k_a)\) and step II \((k_d/k_c)\), where step I is temperature-sensitive and step II the Pi-release/binding step. Essentially as in our previous studies (Coupland et al. 2001; Ranatunga et al. 2007), the forward rate constant \(k_a\) in step I was 20 s\(^{-1}\) at 10°C, and the temperature effects were simulated (for 5°C temperature intervals between 0 and 40°C) by changing \(k_a\) with a \(Q_{10}\) of 4; the reverse \(k_d\) was 120 s\(^{-1}\). In step II, \(k_c\) the Pi-release, was 10\(^3\) s\(^{-1}\), \(k_d\) for Pi-binding was 1.0 \(\times\) 10\(^{-5}\) m\(^{-1}\) s\(^{-1}\), and was changed to simulate Pi-effects. Step III \((k_c)\) was irreversible—representing all the steps (including detachment, hydrolysis and attachment) necessary to reprime the crossbridges for the next cycle and for isometric case \(k_c\) was 10 s\(^{-1}\).
Since an increased detachment rate is generally assumed for shortening muscle (Huxley 1957; He et al. 2000; Ranatunga et al. 2007), \( k_e \) was increased to values between 12.5 and 640 s\(^{-1} \) to simulate shortening and, assuming an exponential dependence of \( k_e \) on velocity, \( \ln(k_e/k_e^{(\text{isom})}) \) was taken as velocity in \( L_0/s \). In order to simulate the temperature-dependence of steady force during shortening at a given velocity, the occupancy estimates as above and representing isometric force, were further transformed in two ways. Firstly, since at a certain critical low temperature \( T_c \), a given velocity would represent the \( V_{\text{max}} \), where force is zero—due to negative and positive strained crossbridges being equal, the occupancy at \( T_c \) was subtracted from \( \text{Occ}(2 + 3) \) for that velocity at all the temperatures; from previous experiments \( T_c \) was known for some velocities and the \( \text{Occ}(2 + 3) \) at \( T_c \) was directly known from the calculations, for other velocities (e.g. low velocities) it was approximated. Secondly, since the crossbridges would be exposed to negative strain during shortening, the average force per crossbridge would be less than in isometric. Thus, the steady force during shortening at a given velocity at different temperatures was calculated as,

\[
\text{Force}_{\text{(short)}} = \left[ \text{Occ}(2 + 3) - \text{Occ}(2 + 3)_{T_c} \right] \times r,
\]

where \( r \) ranged from 1 (isometric) to 0.4 (high velocity); \( r \) decreased linearly with increase of velocity to approximately fit the experimental data. Although the kinetic scheme does not separately identify detached states, the two transformations above amount to a decrease of attached crossbridges, and of positive-strain in them, as compared with isometric case, broadly consistent with the experimental finding that stiffness is decreased with increase of shortening velocity (Julian and Morgan 1981; Ford et al. 1985).

**Results**

**Experiments on intact fibres**

**Tension response to ramp shortening and analyses**

The superimposed tension traces shown in Fig. 1a illustrate the general features of the tension response to a ramp shortening from an intact fibre bundle from the rat flexor hallucis brevis (FHB) muscle; the fibre bundle-ends were held isometric until the tetanic tension-plateau, \( P_0 \), and then a ramp shortening of 20% \( L_0 \) (lowermost trace) was applied. The change in length of a segment of the bundle near the force transducer end (middle trace) shows a basic similarity with the applied ramp shortening; the late increase of slope may be due to decrease of filament overlap after \( >12\% \) shortening (see Fig. 1 for details). During a ramp shortening, the tension (uppermost trace) falls rapidly initially (to an inflection) and then undergoes a gradual transition (referred to as \( P_2 \)—Roots et al. 2007) after which tension declines more slowly. The tension \( P_2 \) at a given velocity was estimated as the tension at the point of intersection between two linear slopes, as shown in the inset (Fig. 1c); the inset, on an expanded time scale, also shows the occurrence of the inflection at the beginning of the tension decline as reported in previous studies (Ford et al. 1977; Roots et al. 2007); this represents the force generating transition in the attached (pre-stroke) crossbridges on exposure to negative strain. The post-inflation tension decline during a ramp shortening was fitted with a double exponential function (see Fig. 1) to isolate the time course of the faster, major, component from the slower subsequent decay. Figure 1b shows the traces and component curves obtained from a preparation at three different temperatures using one velocity. With increase of temperature from 10 to 35 °C, the amplitude of the faster component shows temperature-sensitivity and the rate of the (faster) tension decline increases slightly. Both the isometric tension (before the ramp) and the “steady” shortening tension \( P_2 \), or the tension reached after the faster exponential component (\( \sim P_2 \)), increase markedly with temperature.

**Temperature dependence of force during ramp shortening**

In experiments on six fibre bundles, the tension during steady shortening at five different ramp velocities (0.25, 0.4, 0.8, 1.9 and 3.6 \( L_0/s \)) and the isometric tension \( P_0 \) were determined, and analysed as above, at six different temperatures (see “Methods”). Figure 2a shows isometric force (as stress) and stiffness data plotted against temperature; stiffness was estimated from the linear slope of initial tension decline at the onset of the highest ramp shortening velocity (3.6 \( L_0/s \), see Fig. 2). Assuming that there is no crossbridge detachment prior to \( P_1 \)-inflection (see above), the stiffness data shows that a two-fold increase of isometric tension between 10–35°C is not associated with an increase of number of crossbridge attachments. Examination of the force–shortening velocity per se was not the main concern of this study; nevertheless, when the \( P_2 \) tension data for the five standard velocities were examined to define the force–shortening velocity curve at each temperature (see Fig. 2b), the curves showed a higher \( V_{\text{max}} \) and a lower curvature at the higher temperatures. The \( V_{\text{max}} \) by extrapolation to zero force was \( \sim 2 \) \( L_0/s \) at 10°C and it increased to \( >10 \) \( L_0/s \) at 35°C. As shown in Fig. 2c, a velocity of \( \sim 3.6 \) \( L_0/s \) was within the range for producing the maximum power output at 35°C (physiological temperatures); the maximum power was
Fig. 2 Isometric force, stiffness and force–shortening velocity curves at different temperatures. (a) The mean isometric force per cross-sectional area (±s.e.m., filled squares) recorded from 6 fibre bundles at different temperatures (1/T); the errors in these absolute force values become reduced when force from different fibre bundles is normalized to a particular temperature, as in Fig. 3a. A sigmoidal curve is fitted as in Fig. 3. Mean (±s.e.m.) $P_0$ at 35°C was 282 ± 35 kN/m². Open symbols show the mean (s.e.m.) stiffness data ($n = 6–18$ per symbol); stiffness was determined as slope of the initial tension decline (before $P_1$ inflection—see Fig. 1c) divided by the velocity, from the highest velocity ($\sim 3.6 L_d/s$), and is given as $P_0(10°C)/L_0$. Note that an average force increase of two-fold in warming from 10 to 35°C is not associated with a stiffness change (slope of the fitted line is not significant). (b) The pooled $P_2$ force data in Fig. 3 (i.e. for five shortening velocities) are shown as force–velocity curves at the six different temperatures (different symbols; 10°C lower most curve and 35°C uppermost curve). The mean force values (in kN/m²) are plotted against the velocity (V) on a negative abscissa. From the fitted Hill curves (1938) the curvature is less and the $V_{\text{max}}$ (extrapolated to zero force) is higher at the higher temperatures, as reported previously (Ranatunga 1984). (c) The mechanical power (force $\times$ velocity, in kW/m³ = W/l) versus velocity curves from the same data. Note that the maximum power is $\sim 230$ kW/m³ at 35°C (V of $\sim 3.6 L_d/s$) and it is $\sim 13$ kW/m³ (V of 0.27 $L_d/s$) at 10°C.

$\sim 230$ kW m⁻³ (=230 W l⁻¹). At 10°C, the power is $\sim 13$ kW m⁻³ (velocity, $\sim 0.3 L_d/s$), i.e. reduced to 5–6% of that at 35°C. The above findings are basically similar to those reported for rat fast (e.d.l.) muscle in previous studies that used the isotonic release method in determining the force–shortening velocity curve for rat fast muscle (see Ranatunga 1984, 1998).

Figure 3a shows pooled (mean ± s.d.) data for the temperature dependence of tension during steady shortening ($P_2$) at the five velocities and of the isometric tension; for pooling the data from different experiments, tension ($P$) was normalised to the isometric tension at 35°C ($P_{0(35)}$) and are plotted against reciprocal absolute temperature (1/T). Each set of data is fitted with a sigmoidal curve (see “Methods”). The curve fit for isometric data gives a $T_{0.5}$ of $\sim 10$ °C, $\Delta H$ (activation enthalpy change) of $\sim 100$ kJ mol⁻¹ and $\Delta S$ (activation entropy change, as $\Delta H/ T_{0.5}$) of $\sim 360$ J mol⁻¹ K⁻¹; in shortening, these values are increased with velocity so that at 3.6 $L_d/s$ (open circles, bottom curve), $T_{0.5}$ is $\sim 28$ °C, $\Delta H \sim 200$ kJ mol⁻¹ and $\Delta S \sim 700$ J mol⁻¹ K⁻¹. Figure 3b illustrates the same mean data with the force normalised to the maximum ($P_{\text{max}}$) in each case; the shift of the curves to higher temperatures as the shortening velocity is increased is clearly seen. If the sigmoidal temperature dependence is due to the fact that a force generating muscle can be simplified to a two-step (force generation/force loss) system in equilibrium, a vant Hoff plot can be constructed for each set of data (see Brown 1957); Fig. 3c are vant Hoff plots using the mean data (see Methods), where $P/(P_{\text{max}} - P)$ is plotted on a logarithmic ordinate against 1/T. Despite the scatter in them, the data shows an approximate linear relation for each case; compared to the isometric case (filled squares), the slope ($\Delta H$) and the intercept at 1/$T_0 = \text{zero}$ ($\Delta S/R$) are increased with shortening velocity.

Temperature dependence of shortening force from isotonic release experiments

In a previous study (Ranatunga 1984), we examined the force–shortening velocity relation in rat fast (extensor digitorum longus) muscle using the isotonic release method, where the steady velocity was measured at
constant force levels and data defining the force–velocity curve were obtained at six different temperatures during warming and cooling (range 10–35°C, see “Methods”). (a) The tension during shortening at each velocity (i.e., tension at the P2 transition) was normalised to the isometric tension (P0) at 35°C and the mean (±s.d., n = 6–18 per symbol) values are plotted against reciprocal absolute temperature (10³/T); the velocities were 0.27, 0.4, 0.8, 1.9 and 3.6 L0/s. The filled squares represent mean isometric tension data (same data as in Fig. 3 but with ±s.d.) from the same experiments (n = 40–120 per symbol). Note that, in all cases, the tension increases with warming and a sigmoidal curve (see “Methods”) can approximately describe the distribution of each set of data. (b) The mean tension data are normalised to the maximum force (Pmax) from curve fit to each data set; note the temperature for half-tension is ~10°C for isometric tension (as found previously, Ranatunga and Wylie 1983; Coupland and Ranatunga 2003) but it is higher at higher velocities (curves shifted to the left, higher temperatures). (c) Linear van’t Hoff plots on the same data; force/(maximum force-force) ratio (see Brown 1957) is plotted. Each set of data is approximately linearly distributed and the slope of the linear regression increases with velocity from ΔH of ~110 kJ mol⁻¹ for isometric data to ~200 kJ mol⁻¹ for shortening at ~4 L0/s; ΔS (from the intercept) increases from ~400 to ~700 J mol⁻¹ K⁻¹.
the 5 shortening velocities and the isometric force (filled squares) are plotted, as a ratio of isometric force at 35°C, against reciprocal absolute temperature; a sigmoidal curve is fitted to the set of data for a given velocity. Note that, force increases with increase of temperature in all cases and, with increase of velocity (from right to left), the sigmoidal curves are shifted to higher temperatures - as obtained with ramp shortening (Fig. 3a). (b) The linear van’t Hoff plots made on the data; the slope of the linear regression increases with velocity so that $\Delta H$ increases from $\sim 125$ kJ mol$^{-1}$ for isometric to $\sim 220$ kJ mol$^{-1}$ for velocity of $\sim 5$ L/s; $\Delta S$ increases from $\sim 400$ J mol$^{-1}$ K$^{-1}$ to $\sim 750$ J mol$^{-1}$ K$^{-1}$, basically similar to the findings from ramp shortening (Fig. 3c).

(i.e. $T = 308$ K), $\Delta H$ and $T\Delta S$ are 100–110 kJ mol$^{-1}$ in isometric and they increase to 200–210 kJ mol$^{-1}$ for maximum power production.

It may be argued that the characteristic differences in the activation thermodynamic parameters ($\Delta H$ and $\Delta S$) seen between isometric and steady shortening, arise during the time course of tension decline from isometric to the steady shortening state. Figure 6 shows, as an Arrhenius plot, the temperature dependence of the apparent rate of tension decline (the reciprocal time constant, $\tau$, from the faster of the two exponential components in curve fit, Fig. 1) at the five ramp shortening velocities. There is much variability (error bars) at the low temperatures for high velocities, presumably due to force declining to zero. Nevertheless, the results show that at any given temperature the rate is higher at higher velocities but that, in general, the rate of shortening induced tension decline is not very temperature sensitive; the slopes of the fitted lines correspond to a $Q_{10}$ of $<1.5$ for 0.25 L/s (lowermost curve) and it decreases with increase of velocity to $Q_{10}$ of $<1$ for 3.6 L/s (top curve).

Experiments on skinned (rabbit psoas) muscle fibres

The significance of the sigmoidal temperature dependence of isometric tension in relation to the crossbridge cycle has been fully considered in relation to data from maximally Ca-activated skinned fibres (see Davis 1998; Coupland et al. 2001). Although our recent experiments (Ranatunga et al. 2007) showed that the endothermic ($T$-jump) force generation was evident during low velocity ramp shortening, (see “Introduction”), whether the sigmoidal relation is force dependent is not known. Since getting reliable and reproducible data from skinned fibres at high temperatures is difficult, the experimental protocol was different to that for intact fibres and limited to two velocities; a fibre is Ca-activated at low temperature ($<9^\circ$C) and rapidly warmed to obtain data at higher temperature (see “Methods” and also, Coupland et al. 2001). Figure 7a and b show tension traces (upper panels) from two experiments; in each case, a ramp shortening at a given velocity was applied at different temperatures; also, a small $T$-jump (see “Methods”) was induced during steady shortening to examine whether endothermic force is evident. $T$-jump induces a clear tension rise at both velocities, suggesting that tension decline during shortening contains a temperature-sensitive component.

Figure 7c shows the tension data for isometric (filled symbols) and shortening conditions at two different velocity ranges (see Fig. 7) collected from experiments on seven fibres; this includes previous data from Ranatunga et al. (2007) but they were re-analysed for comparison with intact fibre experiments (Fig. 3). The data show that a sigmoidal curve can describe the tension data not only for isometric (solid symbols) but also for shortening conditions (open symbols); from the curves, $T_{90.5}$ was $\sim 8^\circ$C for isometric (similar to Coupland et al. 2001) and it increased to...
For higher velocity (0.5–0.9 \(L_0/\text{s}\)), \(D_H\) was \(100 \text{ kJ mol}^{-1}\) for isometric and \(140 \text{ kJ mol}^{-1}\) for the same shortening velocity (see other details in Fig. 7). Thus, although the data are limited to two velocity ranges (low and high) and the temperature range is \(<30^\circ\text{C}\), the basic trends shown in intact fibre experiments are clear in these experiments.

Figure 8 illustrates, in the form of Arrhenius plots, the kinetic data obtained for the two shortening velocity ranges; the data distribution for each case appears linear within the temperature range. As found in intact fibre experiments in Fig. 6, the apparent rate of tension decline (open symbols) is higher for higher shortening velocity (B) than for low velocity (A) but their temperature sensitivities are low, \(Q_{10} 0.85–1.0\). T-jump tension rise (filled symbols) is faster with higher velocity, but both have higher temperature sensitivity \(Q_{10}\) of 1.7 (higher velocity) and 2.7 low (velocity) than for tension decline. Interestingly, with high velocity shortening, although the rate of T-jump tension rise is higher than in isometric fibres (Bershitsky and Tsaturyan 1990), it has a lower temperature sensitivity.

**Discussion**

The present study extends previous findings on the temperature dependence of force in isometric muscle to temperature dependence of force in shortening muscle, i.e. when muscle is performing external work. The main findings from the study are listed and briefly discussed below and some general aspects related to the findings considered later.

**Findings from the present study**

1. The sigmoidal curve for isometric tension versus temperature (1/\(T\)) has a half-maximal tension at a temperature
T0.5 of 8–10°C, as reported in previous studies (Coupland et al. 2001; Coupland and Ranatunga 2003); on average, the tension at ~10°C is ~150 kN m⁻² and it is increased to ~300 kN m⁻² at the physiological temperatures (~35°C). The stiffness remains unchanged at different temperatures (Fig. 2a) and hence, the temperature dependent change of force is due to a shift in the equilibrium between low-force and high-force attached states with little change in the total number of attachments; this is not inconsistent with the finding from single-molecule experiments of Kawai et al. (2006) at different temperatures have demonstrated that the force each crossbridge generates is independent of temperature. From different analyses, the activation enthalpy change ΔH is 103–110 kJ mol⁻¹ and entropy change ΔS is 364–391 J mol⁻¹ K⁻¹; these values are remarkably similar to those derived by Zhao and Kawai (1994) for the force generating equilibrium in the isometric crossbridge cycle (ΔH 103 kJ mol⁻¹ and ΔS 357 J mol⁻¹ K⁻¹, their Table 3), from sinusoidal perturbation experiments on skinned (rabbit psoas) fibres.

(2) The steady force during ramp shortening at a given velocity also increases on warming and, to a first approximation, the data can be described by a sigmoidal relation; the basic features and trends were clear in the data from isotonic release experiments and from Ca-activated skinned fibre experiments. In comparison to the isometric curve, the sigmoidal curve for force versus temperature in shortening muscle is shifted to higher temperatures, in a velocity dependent manner (Figs. 3, 4, 7); ΔH (and ΔS) determined from different analyses is increased, also in a velocity dependent manner (Fig. 5). It is noteworthy that, within the temperature range of 10–35°C, the vant Hoff’s plots (∼ln(K) vs. 1/T, Figs. 3c, 4b) were approximately linear for each velocity in shortening muscle and for isometric muscle; this indicates that ΔH is independent of temperature for each case (see Edsall and Gutfreund 1983). At 3–5 L0/s, a shortening velocity producing the maximum power at the physiological temperatures, T0.5 is ~28°C (Figs. 3, 4) and ΔH is ~200 kJ mol⁻¹, approximately twice that of isometric; TΔS at 35°C was ~210 kJ mol⁻¹. Thus, since ΔG (free energy change) = ΔH − TΔS, it seems that the temperature T0.5 for the minimum ΔG is increased in shortening muscle. The enthalpy changes of various molecular steps in the myosin ATPase reaction in solution also have been calorimetrically determined (see Kodama and Woldge 1979; Kodama 1985; Millar et al. 1987) and, to some extent, they can be correlated with the crossbridge cycle in isometric muscle (see Zhao and Kawai 1994; Coupland et al. 2001); such experiments indicate that the summed ΔH for the molecular steps Pi-release, ADP-release, ATP-binding and ATP-hydrolysis is ~18 kJ mol⁻¹ so that, in the actomyosin cycle in muscle, the net endothermic process may be the force generation step before Pi-release in isometric muscle.

In general terms, the results show that the “endothermic character” is enhanced, in a velocity dependent manner, in the shortening muscle; the findings are consistent with the well known principle regarding the energetics of a muscle’s physiological performance, “the Fenn effect”, that energy liberation is increased in shortening muscle doing external work (Fenn 1924).

(3) At a given ramp velocity, the observed rate of tension decline during shortening had low temperature-sensitivity in both intact and skinned fibres (Q10 < 1.5, Figs. 6, 8); this contrasts with high temperature sensitivity obtained in our previous studies for many other contraction parameters of mammalian muscle (Ranatunga 1982; Ranatunga and Wylie 1983). In terms of a crossbridge cycle, the tension decline during ramp shortening involves a combination of two processes, force loss due to detachment of originally attached force generating crossbridges and force generation by newly attached crossbridges (Roots et al. 2007). Since crossbridge force generation is an endothermic process (Bershitsky and Tsaturyan 1992; Davis and Harrington 1987; Goldman et al. 1987) with a high Q10 (Zhao and Kawai 1994; Ranatunga 1996), which is also evident with T-jumps in the present experiments (see Figs. 7, 8), the results suggest that crossbridge detachment process that drives the tension decline during ramp shortening may

![Image](54x528 to 287x732)

**Fig. 6** Temperature dependence of the apparent rate of tension decline during ramp shortening. Arrhenius plots of the rate of the tension decline (reciprocal of the time constant for the faster exponential component) at 5 different velocities of shortening (range 0.25–3.6 L0/s—different symbols from bottom to top); the tension decline is faster higher the velocity at any given temperature. Mean (±s.e.m.) are displayed and lines are the fitted regressions to the pooled data (n > 50); the slopes give ΔH/2.9 R (filled squares) to 0.89 at ~4 L0/s (filled diamonds and negative slope)
indeed be temperature-insensitive, or has a “negative” temperature sensitivity. Some effects of series compliance and sarcomere non-uniformity etc in our experiments can not of course be excluded, even though the tendon length was kept short in our preparations (see “Methods”); on the other hand, it may be argued that, series compliance would decrease the actual rate but not necessarily its temperature-sensitivity. Although our measurements relate to shortening muscle, the observations are consistent with the findings of Zhao and Kawai (1994) who found low temperature sensitivity ($Q_{10} \sim 1.1$) for the rate-limiting step of the crossbridge cycle in isometric muscle ($k_6$ in their model).

The sigmoidal temperature dependence of muscle force and a simulation

From several different studies of muscle proteins in solution, considerable body of knowledge is available on the thermodynamics of the myosin- and acto-myosin ATPase mechanisms. With respect to temperature-dependence, such studies have shown the need to identify two fundamental conformations of myosin, one (referred to in different studies as $M_{17}$- or $R$-state) favoured by low temperature and the other ($M_{18}$ or $T$-state) favoured by high temperature. Moreover, the relative populations of the two
states would not only be determined by temperature but also the nucleotide on the myosin binding site (see reviews Kodama 1985; Shriver 1984). Given that isometric tension, either in relaxed muscle fibres (i.e. stretched passive tension and no crossbridges attached) or in rigor fibres (no ATP; crossbridges attached), does not show a sigmoidal relation (see Ranatunga 1994), the sigmoidal temperature dependence of muscle force is associated with actively cycling of crossbridges. If the two acto-myosin conformations above can be linked with force generation mechanisms in muscle, in broad outline, the sigmoidal temperature dependence of active muscle force and its sensitivity P_i and ADP (see “Introduction”) would be explicable.

In an attempt to simulate the basic trends seen in our experimental data, we used a minimal three-step actomyosin ATPase/crossbridge cycle (see Scheme 1 in “Methods”) that qualitatively modelled the effects of increased P_i on the force versus temperature relation in isometric muscle (Coupland et al. 2001). Basically, the scheme contains a reversible endothermic force generation (step 1) coupled to reversible P_i-release (step 2) and an irreversible step (step 3) completing the cycle; the temperature-sensitivity of force was due to increase of forward rate constant in step 1 and the isometric force was calculated as the sum of occupancy of states 2 and 3. Figure 9a shows the tensions calculated for different temperatures in control (filled squares, assumed to contain 0.5 mM P_i) and with increased P_i (to 1 mM and 25 mM—open circles) and each data set is fitted with a sigmoidal curve; as found in experiments (Coupland et al. 2001), the curve is shifted to higher temperatures with increased P_i. Figure 9b shows that similar shifts of the curve, showing increase of T_{0.5}, are obtained by increasing the rate constant of the irreversible step (decreasing this would shift the curve to lower temperature - as found experimentally with increased MgADP, Coupland et al. 2005). In either case, however, the ΔH and ΔS were not much altered by such changes in the rate constants of the kinetic scheme (see Fig. 9 for details).

In order to obtain, the temperature dependent behaviour of shortening muscle force—when the irreversible step is made faster, the occupancy data that represent force needed to be transformed, based on two established principles on the mechanics of crossbridge cycle (see “Methods” for details). Firstly, since at a certain critical low temperature (T_c), a given velocity would represent the V_{max}, where force is zero, the occupancy at T_c was subtracted from Occ(2+3) for that velocity at all the temperatures. Secondly, the average positive force exerted by a crossbridge would be less during shortening, being exposed to negative strain. Figure 10a shows the data transformed in this manner for a number of shortening velocities (taken as 0.2 to 4–5 L_0/s—see “Methods”), Fig. 10b shows vant Hoff’s plots and Fig. 10c shows the force–velocity curves for three temperatures. The data from this simulation do illustrate the basic features of the experimental findings, particularly, the increase with shortening velocity of T_{0.5}, ΔH and ΔS (see Fig. 11); also, the simulated force–velocity curves (Fig. 10c) show qualitatively the basic characteristics seen in the experimental force–velocity curves (Fig. 2a), namely, increased V_{max} and decreased curvature at the higher temperature.
Some features and assumptions in the model

A few of the features and assumptions intrinsic to the minimal three-step cycle that qualitatively simulated the basic trends in the experimental data are worthy of note (see also “Methods”).

1. The model assumed that, except for the (single) force generation step (endothermic, $k_a$ in step I), all other (forward and backward) steps in the cycle as insensitive to temperature; indeed, the tension decline during ramp shortening (crossbridge detachment) was found to have a low temperature-sensitivity (see above).

2. An increase of $k_e$, (rate of irreversible step) to simulate crossbridge operation in shortening muscle (higher cycling rate, Huxley 1957) resulted in a shift of the sigmoidal curve to higher temperatures (an increase of $T_{0.5}$) as in the experiments, but it failed to simulate the marked increase of $\Delta H$ and $\Delta S$ in the experiments. The two further transformations that had to be done, in principle, amount to a decrease of the number of attached crossbridges and their contribution to force in shortening muscle (see Methods). From X-ray interference and mechanical measurements, Piazzesi et al. (2007) concluded that the force–shortening velocity relation of muscle is primarily a result of a reduction in the number of attached crossbridges, rather than the crossbridge force or stroke size; in our modelling, however, a decrease with shortening velocity of the average force per crossbridge was necessary to account for our findings, as generally considered (see “Methods”; Huxley et al. 2006) and also suggested from other recent studies in literature (e.g. Bagni et al. 2005).

3. The temperature-dependent increase of force in isometric case is attributed conversion of low-force to high-force attached states with little change in the total number of attachments (see above). In the model, the number of attached crossbridges during shortening was lower than in isometric (see above), but remained unchanged at the different temperatures, so that the increase of force was still due to conversion of low-force to high-force attached states. This seems a remarkable simplification that requires experimental scrutiny in the future. Exactly why the number of attached crossbridges in maximally activated muscle is not much altered by temperature changes, even in isometric muscle (Fig. 2a), remains unclear; a more complex mechano-kinetic model, incorporating strain-sensitivity to the force generation step, would be required to achieve accurate simulation of both the steady state data and the tension transients.

Endothermic nature of muscle force generation

Following the original experiments and formulations by Huxley and Simmons (1971), quick tension recovery induced by a small length-release step is thought to represent crossbridge power stroke or force generation in muscle; Gilbert and Ford (1988) showed experimentally
that there is heat absorption during quick tension recovery and concluded that force generation would be entropy driven. Also, a rapid T-jump increases isometric force without appreciable delay showing that force rises on absorption of heat (endothermic—see “Introduction”). Additionally, exposure to high hydrostatic pressure reduces force in isometric muscle fibres and force quickly recovers on rapid pressure release; thus, force generation at constant temperature may be accompanied by a volume increase (Fortune et al. 1991; Vawda et al. 1999). Therefore, the endothermic nature of muscle (crosbridge) force generation, and increase of entropy associated with it, have been well recognised from studies on isometric muscle and the present study shows that these features are enhanced in shortening muscle performing external work.

A conformational change of the acto-myosin crossbridge, resulting in lever arm tilting, is thought to be the molecular-structural mechanism of force muscle generation (see review Geeves and Holmes 1999); how this is associated with increased entropy (disorder) remains unclear. Two different molecular-structural mechanisms have been proposed to account for the increase of entropy during force generation by an acto-myosin crossbridge. Firstly, Zhao and Kawai (1994) suggested and favoured a mechanism involving altered hydrophobic interaction between actin and myosin (S1) for the large increase of entropy (see also, Kodama 1985); in principle, the transition of non-stereo-specifically attached to stereo-specifically attached crosbridge states would represent such an event, since stereo-specific interaction may be hydrophobic. From examination of X-ray diffraction pattern of muscle fibres during force rise induced by rapid T-jumps, Bershitsky et al. (1997) proposed such a mechanism as a force generating step that is additional to the lever arm

Fig. 10 Simulations of steady force during shortening. The occupancy of [AM*ADP Pi + AM*ADP], i.e. force-holding attached crossbridges, was transformed on the basis of two established principles. (1) Compared to isometric, the average force per crossbridge would be less during shortening at V, due to negative strain on them. (2) Depending on V, the force will be zero at a certain low temperature (Tc) at which the number of crossbridges with negative strain = the number with positive strain; hence, the occupancy at Tc (e.g. ~10°C for V of ~2 L0/s) was subtracted from the occupancy at all other temperatures. Thus, occupancy data (Occ) at different temperatures for a given V were transformed as, Force(short) = [Occ(isom) - Occ(Tc)] × r, where r decreased from 1 for isometric to 0.4 for ~4 L0/s; since Tc was known for some velocities from experiment, Occ(Tc) could be easily obtained from the model but for others, it was estimated (see “Methods” for details). (a) Filled squares are isometric force data and others are transformed occupancy data representing force during shortening at different velocities (range 0.2–4 L0/s); a sigmoidal curve is fitted to each data set as in Fig. 8. (b) vant Hoff’s plot of the data; note the increase of slope (DH) and increase of intercept at 1/T of zero (DS) with increase of velocity (from right to left), as found in the experimental data. (c) Force–velocity curves for ~10, ~20 and ~30°C from the above simulations; although the data transformation was not exact, an increase of Vmax and a decrease of curvature are seen with warming, as in the experiments (see Fig. 3)
tilting step in the crossbridge cycle (see Ferenczi et al. 2005). A contribution of such a mechanism to an entropy increase cannot be excluded, although whether it is intrinsic to crossbridge force generation alone remains to be established.

Secondly, Davis and Epstein (2007) proposed an alternative mechanism, namely, a local unfolding within the crossbridge secondary/tertiary structure and suggested that this might cause the lever arm tilting movement and force generation. From analyses of the rate of tension rise induced by T-jumps at different temperatures as Arrhenius plots, they showed that the observed rate could be resolved into the forward and reverse rate constants for force generation \(k_a/k_b\) of step-I in our Scheme) with clearly different temperature-sensitivities; in particular, the reverse rate constant showed anti-Arrhenius behaviour (negative temperature-sensitivity) characteristic for protein folding. Our results show that the increase of entropy becomes even larger in shortening muscle, i.e. when the attached crossbridges are exposed to continuous negative strain by filament sliding, the number of attachments is reduced and the crossbridge cycle is operating faster. Arrhenius plots for the observed rate of T-jump-induced tension rise, during shortening at two velocities (Fig. 8a, b filled symbols), show no obvious evidence of a non-linearity as expected; however, this might be due to scatter in the pooled data. Also, our findings suggest that another step in the cycle may also have negative temperature-sensitivity, although this is not shown conclusively.

As stated by Gilbert and Ford (1988), since the energy transduction by the actomyosin ATPase in muscle is a cyclic process, an increase in the entropy of the system in one part of the cycle requires a decrease in entropy in another part. It is possible that, whereas the entropy increase is associated with force generation, the entropy decrease may not be restricted to a single step in the cycle, at least in shortening muscle performing external work; further experiments to gather data amenable to more quantitative and detailed analyses would be required to resolve these uncertainties.

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