Extreme Wave Runup on a Steep Coastal Profile

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It is shown that very steep coastal profiles can give rise to unexpectedly large wave events at the coast. We combine insight from exact solutions of a simplified mathematical model with photographs from observations at the Norwegian coast near the city of Haugesund. The results suggest that even under moderate wave conditions, very large run-up can occur at the shore.

I. INTRODUCTION

In the present work, we are interested in the interaction of ocean waves with steep offshore topography such as encountered in some areas at the Norwegian coast. If surface waves propagate on such a steep bottom slope, they experience only slight amplification until very close to shore. However, just before they reach the beach face, the waves receive a large boost in amplitude which can lead to an explosive run-up on the shore. As this large run-up may seem wholly unexpected to the casual observer, it may constitute a potentially hazardous situation.

It is well known that the Norwegian coast especially in the south and the west features a multitude of fjords. These rocky cliffs often continue past the waterline, and may drop to several hundred meters depth, cutting through the continental shelf as submarine valleys. This landscape was formed by glaciers during the last ice age. Indeed, it is well known that fjords developed due to glaciers’ capability of eroding below the sea level, leaving deep submerged valleys when the ice age came to a close and melting was completed.

In some cases, these valleys are offshore of the present shoreline, and there are some places today where coastal platforms give way to very steep seaward slopes carved by these thick glaciers. In fact it is not unusual to see 200 or 300 meter drops of the sea bed over a distance of a few hundred meters. These steeply sloping shores typically consist of bedrock which has been smoothed by the glacial ice and is rather immune to erosion and littoral processes. In fact, wide stretches of the coast have not been filled with mud and other sediments, and the rocks remain exposed. As a result, this coast is generally classified as primary coast, similar to coasts in other places around the word such as New Zealand and the northernmost part of the East Coast of the United States.

Further offshore, the Norwegian coast features very irregular bathymetry which dissipates much of the incoming wave energy through wave focusing, shoaling and local breaking. However, some long waves of moderate amplitude and steepness are able to pass the rugged offshore topography relatively unscathed and reach the coast. If these long waves hit an area with sharply sloping coastal profiles, even waves of relatively small amplitude can lead to large run-up. In what follows, in section II, we report observations of waves made at a site with a sharp, nearly 1:1 drop from the water line. In section III, we detail a mathematical model capable of predicting large run-up from a moderate-sized offshore wavefield in the case of bathymetry featuring a steep slope such as seen at the observation site. The results are discussed in section IV.

II. OBSERVATIONS

Observations were made at a site near the Norwegian city of Haugesund. As shown in Figure 1, the bathymetry near the coast features a steep drop to about 200m right from the waterline. Indeed, it can be seen in the schematic of a cross-section of the site in Figure 2 that the slope is very steep, about 1:1. Due to the very steep slope, it is common for waves to exhibit surging breaking, such as defined in [6–8]. However, as waves of slightly larger amplitude quickly shoal on the steep slope they

FIG. 1. Bathymetric chart of sea bed near Bleivika lighthouse. The depth contours run nearly parallel to the shore, and feature a steep drop from the shoreline to about 200m depth. © Kartverket. Used with permission from The Norwegian Mapping Authority.

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sometimes reach the point of plunging almost as soon as they can be made out as a large wave. One such example is shown in Figure 3. Under the rough conditions prevailing when the photos in Figure 2 were taken, energetic waves crash into the rocks, creating large areas of turbulent flow. The accompanying foam and spray immediately alert the observer to the fact that wave conditions are serious, and caution must be exercised. On the other hand, the conditions in Figure 4 were mostly calm with little visible swell, and only a small chop due to a moderate local wind. A few small patches of foam are visible which appear to be remnants of previous waves interacting with the jagged rocks, or white-capping due to local wind gusts. The smaller swell waves were just lapping the shore, and the limited foam and absence of spray do not signal any danger. As a slightly larger swell wave approaches and shoals, the subsequent wave run-up appears extreme against the backdrop of otherwise benign wave and weather conditions. An example of such explosive run-up is shown in Figure 4, and one may argue that the flooding of the rocks may happen unexpectedly to a non-initiated observer.

**A. Observations on January 16th, 2020**

Observations were made from a location near the lighthouse Bleivika indicated by a star on the map in Figure 1. We used an Olympus Mark III E camera to shoot 4K video clips. Individual frames from those clips are shown in the figures below. Wave conditions were monitored using operational wave forecasts from two sources. First, the NOAA site  was consulted. Near the coast, the waves had already encountered several shoals, and the waveheight and wave periods were somewhat smaller. The wind speed was above 9 m/s so there was a significant wind sea component in addition to swell. Most waves were surging breakers, but some waves were steep enough to break before reaching the shore. Figure 5 shows a wave developing along the steep sloping bottom. It can be seen that the waveheight develops quickly, and in this case the wave is large enough for the wave to plunge before it hits the rocky shore. This situation would not pose a danger to the casual observer since wave conditions were not calm.

**B. Observations on January 29th, 2020**

In this case, the wave forecasts from NOAA and BarentsWatch Centre estimated the local significant waveheight to be just above 1 m, with a maximum waveheight of about 2 m. Visually, conditions were rather calm, as also borne out from a study of Figure 2. However, there was swell from a distant storm, and the peak wave period was about 13 s (i.e. wavelength of ~ 260 m based on linear wave theory). The authors were at the site for about 90 minutes, and the visually measured wave period was on average about 9 – 13 s, though some waves were as short as 6 s, and some waves were longer than 13 s.

The rock which is in view in Figure 4 stayed dry for the most part, though in the 90 minutes we were present, it was flooded 3 times. In fact, as far as we can tell, what typically seemed to happen was that a group of waves arrived which had slightly higher than normal waveheight, and the rock was flooded not by the first, but by the second and/or third wave in the group. After such an incident, the conditions went back to normal. Indeed, it is well known that swell will organize into wave groups (see and references therein), so the situation above would have to be expected. As mentioned above, in the 90-minute observational period, there were three waves that flooded the rock, two of these in one wave group, and one in another wave group.

Figure 4 shows a wave crest at $t = 15$ s (relative time in the video), an approximately flat surface at $t = 18$ s, and the wave trough at $t = 21$ s. This was a relatively unspectacular wave with a small waveheight hitting the rock. The next wave (not shown) already has a larger amplitude, but stops short of the rock. Finally, 25 seconds later, at $t = 46$ s the third wave crest hits the rock, flooding the top of the rock almost entirely. Using tide tabulations, and a local elevation map, the run-up can be estimated to be about 3.8 m.

**III. MATHEMATICAL MODEL**

In the following, it will be shown that a comparatively simple mathematical model can be used to understand how relatively small waves can lead to significant and unexpected run-up if encountering a steep slope. For this purpose, we will use the shallow-water system

$$h_t + (uh)_x = 0, \quad (1)$$

$$u_t + uu_x + g(h + b)_x = 0, \quad (2)$$

where $h(x,t)$ is the total depth of the fluid, $u(x,t)$ is the average horizontal velocity, $g$ is the gravitational acceleration, and $b(x)$ is the bottom profile. In the present case, we define the
FIG. 3. This figure shows four snapshots of wave conditions at 59.48° N, 13.44° E on January 16th, 2020. Upper left: $t = 105s$, upper right: $t = 115s$, lower left: $t = 120s$, lower right: $t = 124s$.

bathymetry by $b(x) = \theta x$. The surface elevation is then given by $\eta(x,t) = h(x,t) + \theta x$.

This system is able to describe long waves in shallow water, and it is possible to find exact solutions in the presence of non-constant bathymetry which enable us to make predictions of the development of the waterline. Exact solutions of $2 \times 2$ systems of conservation laws are classically obtained using a hodograph transformation, where dependent and independent variables are interchanged\textsuperscript{14}. In the presence of bathymetry, it is somewhat more difficult to find the requisite change of variables than in the case of constant coefficients. Nevertheless, an appropriate hodograph transformation was found by Carrier and Greenspan\textsuperscript{15}, and there have been a number of works seeking to extend and generalize that idea (see\textsuperscript{16–21} and references therein).

In the present situation, it is important that the system be solved in dimensional coordinates in order to understand the influence of the steep bottom slope. For the convenience of the reader, the construction of the exact solutions is explained in the appendix. As demonstrated in the appendix, the independent variables $\lambda$ and $\sigma$ are introduced through a hodograph transformation. These variables do not have a clear physical meaning. However, using separation of variables, an exact solution can be specified with the help of a “potential” $\phi$ defined in terms of the velocity $u$ by the relation $u = \frac{1}{\sigma} \phi_\sigma$. In terms of the potential, the solution has the form

$$\phi(\sigma, \lambda) = \frac{A}{k} J_0(k\sigma) \cos(k\lambda).$$  \hspace{1cm} (3)

Here $J_0$ is the zeroth-order Bessel function of the first kind, and $A$ and $k$ are arbitrary constants. Using the potential $\phi$, an expression for $x(\sigma, \lambda)$ is found in the form

$$x = \frac{1}{2g\theta} \left( \frac{1}{2} \phi_\lambda - u^2 - \frac{\sigma^2}{8} \right),$$  \hspace{1cm} (4)

and $t(\sigma, \lambda)$ can be expressed as

$$t = \frac{1}{2g\theta} \left( \lambda - 2u \right).$$  \hspace{1cm} (5)

The surface elevation $\eta = h + \theta x$ is given by

$$\eta = \frac{1}{2g} \left( \frac{1}{2} \phi_\lambda - u^2 \right).$$  \hspace{1cm} (6)

Note that in contrast to the solution provided in\textsuperscript{15}, the slope $\theta$ appears explicitly in the final solution.

This solution can now be used to investigate the run-up for various wave conditions. In Figure\textsuperscript{5} an exact solution is plotted with a steep slope of $\theta = 1$. In the left panel, we choose $A = 100 \frac{m^2}{s^2}$ and $k = 0.04 \frac{m}{s}$ (we emphasize that even though $A$ and $k$ feature units, there is no clear physical meaning assigned to these constants) in the solution to obtain an offshore amplitude 0.459m, and run-up 2.548m. The steepness, defined as $2\pi A/L$ where $L$ is the wavelength is 0.0029. In the right panel, we chose $A = 200 \frac{m^2}{s^2}$ and $k = 0.04 \frac{m}{s}$ to plot an offshore amplitude 0.918m with a steepness of 0.0059 and run-up of 5.097m. In Table 1 the run-up for four different offshore
FIG. 4. This figure shows four snapshots of wave conditions at 59.48° N, 13.44° E on January 29th, 2020. Upper left: wave trough at $t = 15s$, upper right: mean water level at $t = 18s$, lower left: wave crest at $t = 21s$, lower right: wave crest at $t = 46s$.

FIG. 5. Offshore wavefield and run-up on a 1 : 1 slope for two different offshore wave conditions. In the left panel, we have offshore amplitude 0.459m and run-up 2.548m. In the right panel, we have offshore amplitude 0.918m and run-up 5.097m.

TABLE I. Run-up for four different offshore amplitudes for waves with period $T = 8s$ and varying steepness. The amplification factor between offshore amplitude and run-up is 5.5.

| Amplitude (offsh.) [m] | Steepness (offsh.) | Period [s] | Run-up [m] |
|-----------------------|--------------------|------------|------------|
| 0.229                 | 0.0015             | 8          | 1.274      |
| 0.459                 | 0.0029             | 8          | 2.548      |
| 0.918                 | 0.0059             | 8          | 5.097      |
| 1.377                 | 0.0088             | 8          | 7.645      |

amplitudes for waves with a period $T = 8s$ is recorded. The values of $A$ used in the table are $50 \text{m}^2$, $100 \text{m}^2$, $200 \text{m}^2$, $300 \text{m}^2$, $400 \text{m}^2$. The 8s period is found by choosing $k = 0.04 \frac{m}{s}$. The amplification factor between offshore amplitude and run-up is 5.5.

IV. DISCUSSION

In this work, the run-up of waves on a steep slope has been studied through field observations at the Norwegian coast and a mathematical model. The observations presented here point to the possibility that extreme wave run-up may occur during otherwise benign conditions. The effect of the large run-up is further enhanced by the more moderate slope of the coast above the waterline (see Figure 4), leading to a large area of flooding, such as shown in Figure 4.
The mathematical model used here also shows that unusually large run-up can be realized on a steep slope by small offshore amplitudes. Indeed, it is evident from Table 1 that a moderate rise in offshore amplitude from 0.459m to 0.918m may lead to a difference of more than 2.5m in the run-up height. A still moderate wave amplitude of 1.377m can lead to run-up height of 7.648m.

In summary, both observations and the shallow-water theory show that large run-up may occur under otherwise inconspicuous conditions. The two approaches do not give a perfect quantitative match because of the inherent quantitative uncertainty in the observations, and because some of the shorter waves observed are only shallow-water waves once they enter the coastal slope. Nevertheless both observation and mathematical theory clearly show large amplification of the waves as they approach the shore, and it is clear that an observer focusing on offshore conditions may be taken by surprise as moderate waves experience such strong amplification and subsequent explosive run-up on the shore.

In the present work we have focused on a very steep 1 : 1 slope where the bathymetry has a decisive effect on the wave evolution and the resulting run-up. It appears that in many previous works on extreme wave events in shallow water, a gently sloping bottom was assumed. This is the case in particular in studies on so-called sneaker waves, which are generally taken to be large run-up events on gentle beaches. On the other hand, there are some studies on unusually large waves, or freak waves in shallow water, but not near the shore. For example in 40, the authors describe freak waves occurrences in the nearshore zone, and in 28,29, the authors look at wave interaction phenomena as possible route to freak wave development. In 22, laboratory experiments and numerical simulations are used to explain the occurrence of freak waves. In the situation considered in these works, even though the waves are in shallow water, the bathymetry does not exert a major effect on the fashion in which large wave events develop.

In contrast, a strong influence of the bathymetry on the wave conditions was found in 33, where resonant behavior due to irregular underwater topography was considered and also in 29,30. However, the slopes considered in these works were still much more gentle than the steep 1 : 1 bathymetry considered in the present work. On the other hand, run-up on a vertical wall, such as a sea cliff were studied in 31. However with the conditions in this case such as the extreme slope, the slippery rocks and small tidal range, it appears challenging to obtain reliable measurements.

There is a large literature on rogue or freak waves (see 33,39 and the references therein). It is not clear whether the present phenomenon should be classified as a freak wave event since at least in theory it can be predicted if measurements of the offshore wavefield are available. Indeed it would be interesting to conduct field measurements at this or a similar site, such as reported on in the in-depth study 32. However with the conditions in this case such as the extreme slope, the slippery rocks and small tidal range, it appears challenging to obtain reliable measurements.

FIG. 6. Definition sketch for mathematical model, including the slope b(x) and the water depth h(x,t) = η(x,t) - b(x).

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Appendix: Exact solutions for the shallow-water equations

The shallow-water equations (1) and (2) are to be solved on a domain such as indicated in Figure 6. As suggested in (1), a gas dynamics analogy may be used to find the eigenvalues and the Riemann invariants for the shallow-water system. Using (1) to rewrite (2) as

\[(hu)_t + (hu^2 + p(h))_x = -gh\theta, \quad (A.1)\]

where \(p(h) = \frac{1}{2}gh^2\), a similarity to the gas-dynamic equations for a barotropic gas can be seen if we consider \(P(h)\) as the “pressure” and \(h\) as the “density”. For more details, the reader may consult (2). Indeed, with this analogy, the eigenvalues are \(\lambda_{1,2} = u \pm c\) and the Riemann invariants can be found to be

\[\alpha = u + \int \frac{c(h)}{h} dh + g\theta t, \quad (A.2)\]
\[\beta = u - \int \frac{c(h)}{h} dh + g\theta t, \quad (A.3)\]

where \(c\) is defined by \(c^2 = \frac{dP}{dh}\). The last term on the right hand side is due to the bathymetry. The system can then be written in terms of the characteristic variables \(\alpha = u + 2\sqrt{gh} + g\theta t\) and \(\beta = u - 2\sqrt{gh} + g\theta t\) as

\[\left\{ \frac{\partial}{\partial t} + \left(u + 2\sqrt{gh}\right) \frac{\partial}{\partial x} \right\} \left(u + 2\sqrt{gh} + g\theta t\right) = 0, \quad (A.4)\]
\[\left\{ \frac{\partial}{\partial t} + \left(u - 2\sqrt{gh}\right) \frac{\partial}{\partial x} \right\} \left(u - 2\sqrt{gh} + g\theta t\right) = 0. \quad (A.5)\]

The hodograph transform can be effected by implicit differentiation of the equations (A.4) and (A.5) and using the dependent variables \(x = x(\alpha, \beta)\) and \(t = t(\alpha, \beta)\) instead of
\[ \alpha = \alpha(x,t) \text{ and } \beta = \beta(x,t). \] Assuming a non-zero Jacobian \( \frac{\partial(x,t)}{\partial(\alpha,\beta)} \), the equations (A.4) and (A.5) become

\[ \begin{align*}
x\beta - \lambda t\beta &= 0, \\
x\alpha - \lambda t\alpha &= 0.
\end{align*} \tag{A.6} \tag{A.7}
\]

In order to obtain a linear set of equation, we define new independent variables \( \lambda = \alpha + \beta \) and \( \sigma = \alpha - \beta \). The systems then appears as

\[ \begin{align*}
x_\lambda - u_\lambda + \sqrt{gh} t_\sigma &= 0, \\
x_\sigma - u_\sigma + \sqrt{gh} t_\lambda &= 0.
\end{align*} \tag{A.8} \tag{A.9}
\]

Assuming that \( x_\sigma \lambda = x_\lambda \sigma \) and \( t_\sigma \lambda = t_\lambda \sigma \), the two equations reduce to

\[ \begin{align*}
u_\sigma t_\lambda - u_\lambda t_\sigma - \left( \sqrt{gh} \right)_\sigma t_\sigma + \left( \sqrt{gh} \right)_\lambda t_\lambda &= \sqrt{gh} \left( t_{\sigma \lambda} - t_{\lambda \sigma} \right). \tag{A.10}
\end{align*}
\]

Using the expressions for the new independent variables yields

\[ \begin{align*}
\lambda &= \frac{u + gh\theta t}{\sqrt{\sigma}}, \\
\sigma &= \sqrt{gh}.
\end{align*} \tag{A.11} \tag{A.12}
\]

By using (A.11) and (A.12), expressions for \( u_\sigma, u_\lambda, \sqrt{gh}_\sigma \) and \( \sqrt{gh}_\lambda \) can be found and (A.10) turns into the linear wave equation

\[ \sigma (t_{\lambda \lambda} - t_{\sigma \sigma}) - 3t_\sigma = 0. \tag{A.13}
\]

Using the expression (A.11) for \( \lambda \) together with an appropriate potential function \( u = \frac{\sigma}{\beta} \phi_\sigma \), the equation (A.13) can be rewritten as

\[ \left( \sigma \phi_\beta \right)_\sigma - \sigma \phi_\lambda = 0. \tag{A.14}
\]

Using separation of variables, we are able to find an exact solution which is bounded as \( \sigma \to 0 \). This solution can be written as

\[ \phi(\sigma, \lambda) = \frac{A}{\lambda} J_0(k\sigma) \cos(k\lambda), \tag{A.15}
\]

where \( J_0 \) are the Bessel function of first kind of order zero, and \( A \) and \( k \) are constants.

With this solution in hand, an expression for \( x(\sigma, \lambda) \) is found in the form

\[ x = \frac{1}{2\sqrt{\theta}} \left( \frac{1}{2} \phi_\lambda - u^2 - \sigma^2 \right), \tag{A.16}
\]

and \( t(\sigma, \lambda) \) can be expressed as \( t = \frac{1}{\sqrt{\theta}} (\lambda - 2u) \). The surface elevation \( \eta = h + \theta x \) is then given by \( \eta = \frac{1}{2\sqrt{\theta}} \left( \frac{1}{2} \phi_\lambda - u^2 \right) \).

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