Titanium dioxide-based picoseconds pulsed fiber laser performances comparison in the 1.5-micron region

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Abstract. We demonstrated and compared picoseconds pulsed fiber lasers based on Titanium dioxide based saturable absorbers (SAs); 20 cm long Titanium dioxide-doped fiber (TiO2:DF) and Titanium dioxide PVA film (TiO2:PF) in the 1.5-micron region. The laser cavity utilized 2.4 m long Erbium-doped fiber (EDF) as the gain medium. A self-starting pulsed laser with a consistent repetition rate of ~1 MHz emerged stably with the incorporation of TiO2 based SAs. The TiO2:DF SA produced 9.74 ps pulsed laser at a central wavelength of 1553 nm within a pump power range of 106-142 mW. The fiber SA promoted slightly higher slope efficiency and maximum pulse energy of 13.17% and 8.56 nJ, respectively in comparison with the film SA. On the other hand, the TiO2:PF SA generated stable 3.89 ps pulsed laser at an operating wavelength of 1560 nm within 86-142 mW pump power range. The film SA also produced slightly greater maximum output power of 12.17 mW and maximum peak power of 3.43 kW, respectively at the maximum pump power. The results confirmed that both TiO2 SAs can be good alternative pulse modulator in the 1.5-micron region.

Keywords. Optical fiber laser, fiber saturable absorber, Titanium dioxide, thin film

1. Introduction

Passive pulsed fiber lasers have several advantages in comparison with the active one, which includes, simplicity, flexibility and compactness. They also have significant potentials for use in many applications, such as telecommunication, biomedical and material engraving. Numerous methods have been claimed able to facilitate passively pulsed fiber lasers such as nonlinear polarization rotation [1], semiconductor saturable mirror (SESAMs) [2], carbon nanotubes (CNT) [3], graphene [4, 5], transition metal dichalcogenides (TMD) [6] and several others [7-26] including those which have been reported by our research group lately.

Although SESAMs have been successfully developed for commercial use in the last past two decades, they suffer from a relatively narrowband operation and has to be designed for explicit
wavelength. In addition to that, they are also quite bulky for fiber lasers and have a complex fabrication. NPR based lasers are environmentally unstable and have to be securely located in limited movements surroundings. On the other hand, CNT requires quite a complex bandgap engineering or diameter control for obtaining broader operation bandwidth. Additionally, graphene has a small absorption of 2.3% at 1550 nm. Thus, in this regard, new SA material that is small, easy to integrate, possessing quite a fast recovery time and can perform well in a robust environment is highly desirable.

Titanium dioxide (TiO$_2$), that belongs to transition metal oxides (TMO) have seized attention in recent years as alternative SAs in several regions; 1 [27], 1.55- [28, 29] and 2-micron [30]. It has a recovery time of $\sim$1.5 ps at room temperature [31], while Z scanning performed on anatase and rutile TiO$_2$ proved that it has saturable absorption feature. The modulation depth (35.41%) and the saturation intensity (0.013%) of TiO$_2$ [29] also are comparable to the others SAs [6]. Although it has a bandgap of $\sim$3.2 eV ($\sim$387 nm), it was claimed able to operate in the visible [32] and infrared [33] regions.

In this report, we demonstrated and compared TiO$_2$DF SA and TiO$_2$PF SA based picoseconds lasers performances in the EDFL cavity. The TiO$_2$PF was fabricated in-house, using polyvinyl alcohol (PVA) as the polymer film. On the other hand, the TiO$_2$DF was fabricated by doping TiO$_2$ element into silicate glass fiber core. Experimentally, we obtained about the same value of pulse repetition rates ($\sim$1 MHz) for both TiO$_2$ based SAs. The fiber laser performances of these TiO$_2$ based SAs are summarized and elaborated in the following topics to come.

2. Fabrication and Characterization of the Titanium dioxide-based SA

2.1. TiO$_2$DF SA (fiber) fabrication

The TiO$_2$DF was fabricated by doping TiO$_2$ element into silica glass matrix via a conventional modified chemical vapor deposition (MCVD) through bubbling of Helium (He) and Oxygen (O$_2$) gases into Titanium tetrachloride (TiCl$_4$) and Silicon tetrachloride (SiCl$_4$) containing bubbles. The developed TiO$_2$DF has core diameter and numerical aperture (NA) of $\sim$40 $\mu$m and 0.21, respectively. The fabricated fiber also contains 4.0 mol % doping levels of TiO$_2$. To effectively works as fiber SA, the TiO$_2$DF was cut into 20 cm length. Both of its arms were then fusion spliced with 10 cm long single-mode fiber (SMF28), to form 10 cm SMF28 – 20 cm TiO$_2$DF – 10 cm SMF28. However, in this report, the whole piece is regarded as TiO$_2$DF SA only. The TiO$_2$DF fabrication process in details, along with its important fiber characteristics can be found in [13].

2.2. TiO$_2$PF SA (film) fabrication

The TiO$_2$ powder used in the film SA was purchased from Sigma Aldrich. The powder is 99 % pure and has a diameter of lower than 45 $\mu$m. First, the host solution was prepared by dissolving 1 g of polyvinyl alcohol (PVA) into 120 ml of deionized (DI) water. Then, the host mixture was stirred using a magnetic stirrer at 90°C temperature, until the PVA powder fully dispersed. The mixture was then removed from the heating device and cooled down to room temperature. Additionally, TiO$_2$ solution was prepared by dissolving TiO$_2$ powder into DI water with the help of 1% sodium dodecyl sulphate (SDS) solvent. The mixture was stirred for 5 minutes and centrifuged at 3000 rpm for $\sim$15 minutes, to yield supernatant containing TiO$_2$ suspension. The TiO$_2$ suspension was collected and then poured onto the prepared PVA host solution. Next, the mixed solution was centrifuged to yield a composite precursor solution. The precursor solution was then transferred onto a flat and clean petri dish and left for two days at room temperature, to form TiO$_2$ composite film SA with a thickness of $\sim$30 $\mu$m. The TiO$_2$ film fabrication details and its important characteristics are explained in [30, 34]. To be effectively served as an effective SA, the composite film (TiO$_2$PF SA) was cut into a square shape of 1 mm x 1 mm and sandwiched between two clean fiber ferrules with the aid of an index matching gel. Then, a clean fiber adapter was carefully fixed at the coupling spot. The whole piece was then inserted into the EDFL cavity.

2.3. Linear absorption profile of the TiO$_2$ based SAs.

Figure 1 depicts linear absorption profiles of the TiO$_2$PF SA and the TiO$_2$DF SA taken at their respective mode-locked operating regime. The measurements were conducted by coupling the SA between a broadband white light source (WLS) and an optical spectrum analyzer (OSA). The net reduction of the injected WLS intensity is regarded as the linear absorption of the tested SA. As shown, the TiO$_2$PF SA shows relatively more consistent absorption profile than the TiO$_2$DF SA, due to the highly uniform
structure obtained in the thin film. The TiO$_2$PF SA has slightly lower absorption of 1.55 dB at 1560 nm wavelength as compared to the TiO$_2$DF SA (that has an absorption of 2.95 dB at 1553 nm wavelength).

![Figure 1. Linear absorption profile of TiO$_2$ based SAs.](image)

### 3. Picoseconds pulsed fiber laser cavity design

The proposed design of the mode-locked based TiO$_2$ element is shown in Figure 2. The laser cavity is driven by a 980 nm laser diode pump. The light enters into a wavelength division multiplexer (WDM) and then into 2.4 meters long Erbium-doped fiber (EDF) gain medium. An isolator ensures unidirectional light propagation in the cavity. The EDF is a commercial glass fiber (IsoGain, I-25) from Fibercore and has core diameter and NA of 4 µm and 0.23, respectively. In addition to that, the EDF has core concentricity of less than 0.5 µm and absorption of 23-27 dB/m at 980 nm wavelength. As shown, 3 dB coupler 1 is used to separate the laser output into equal halves. Half of the laser output is then channeled into 3 dB coupler 2, while the remaining half, is left to be looped inside in the cavity. The 3 dB coupler 2 divides the light into further halves, providing real-time light measurements at two different ports. The TiO$_2$ based SAs, acts as mode-lockers; exploiting its linear and non-linear absorption characteristic to generate stable picoseconds pulsed lasers. A commercial single-mode fiber (SMF28) with a length of 195 nm, is appended before the SA to provide sufficient intracavity nonlinear and dispersion in the cavity. At the same time, it also reduces the pulse repetition rate and improves the pulse energy. This improved pulse energy would be sufficient enough to saturate the SA for a reliable self-starting mode-locked operation. A digital oscilloscope (OSC) and a radio frequency spectrum analyzer (RFSA) with a pre-connected photo-detector were employed to measure the pulse in the time and frequency domain, respectively, while an OSA records the output laser spectrum. The output power is measured via an optical power meter.
4. Picosecond pulsed fiber laser performances

The mode-locked EDFL based on TiO$_2$DF SA self-started at 106 mW threshold pump power and destructed into continuous laser (CW) laser when the pump power goes beyond 142 mW. Figure 3(a) depicts the mode-locked laser optical spectrum with a central wavelength of 1553 nm. The 3 dB spectral bandwidth (3 dB SB) is found to be 0.269 nm (33.58 GHz). The pulsed laser has a pulse repetition rate of 0.984 MHz. The autocorrelator trace as depicted in Figure 3(b), shows a single enveloped pulse with a pulse duration of ~9.74 ps (using sech$^2$ fitting analysis). Based on the obtained 3 dB SB of 33.58 GHz, the time-bandwidth product (TBP) is measured to be 0.33 which is slightly higher than the transform limit value of 0.315. This phenomenon indicates that the pulse is marginally chirped.

Figure 2. Mode-locked EDFL based on TiO$_2$ based SA cavity design.

Figure 3. Mode-locked EDFL based on TiO$_2$DF SA (a) optical spectrum (b) autocorrelator trace
Figure 4. Mode-locked EDFL based on TiO$_2$PF SA (a) optical spectrum (b) autocorrelator trace

On the other hand, mode-locked EDFL based on TiO$_2$PF SA self-emerged at a threshold pump power of 86 mW and remained stable until 142 mW. Figure 4(a) illustrates the generated pulsed laser output spectrum, indicating a central wavelength of 1560 nm. As seen, the 3 dB SB is measured as 0.75 nm (72.57 GHz). The pulsed laser has a pulse repetition rate of 1.01 MHz. The autocorrelator trace as provided in Figure 4(b), depicts a pulse duration of ~3.89 ps (based on the sech$^2$ fitting analysis). By considering the 3 dB SB as 72.57 GHz, the time-bandwidth product (TBP) is calculated to be 0.36, slightly greater than the transform limit of 0.315, which also indicates that the pulse is chirped.

The TiO$_2$DF SA based pulsed laser performances as a function of pump power (106-142 mW) is demonstrated in Figure 5(a). As depicted, the output power increases linearly within a range of 3.73-8.42 mW. The pulse energy and the peak power also ascend with the increase of pump power. The maximum pulse energy and peak power are measured to be 8.56 nJ and 0.88 kW, respectively. The calculated slope efficiency is found to be 13.17%.

On the other hand, the TiO$_2$PF SA based pulsed laser performances against increasing pump power (86-142 mW) is demonstrated in Figure 5(b). As illustrated, the output power ascends linearly from 7.58 mW to 12.17 mW. The pulse energy and the peak power also increases almost linearly with the rise of pump power. The maximum pulse energy and peak power are found to be 4.21 nJ and 3.43 kW, respectively. The obtained slope efficiency is measured to be 8.17%.

Table 1 summarizes and compares the TiO$_2$DF SA and TiO$_2$PF SA based pulsed laser performances and characteristics. Both TiO$_2$ based SAs, have about the same repetition rate of ~1 MHz, due to the same cavity length (~204 m) used in the design. The generated pulse repetition rates via these TiO$_2$ SAs are examined to be associated with a single cavity round trip period, suggesting that the generated pulsed lasers are mode-locked lasers. As demonstrated, the TiO$_2$PF SA generates higher output power and peak power as compared to the TiO$_2$DF SA. Conversely, the TiO$_2$DF SA generates better slope efficiency and higher pulse energy. Higher pulse energy generated via the film SA is attributed to a slightly broader
pulse width obtained in the optical spectrum. In summary, both SAs produce almost comparable laser performances. However, in the aspect of durability, the TiO$_2$DF was observed to have better pulse stability when tested under several hours of laser operation at the maximum pump power operation [13].

5. Conclusion
We have demonstrated and compared picoseconds pulsed fiber laser at 1.5-micron by utilizing TiO$_2$ based SAs; fiber and film. Both pulsed fiber lasers have almost the same repetition rate of ~1MHz. The TiO$_2$DF SA generated 9.74 ps pulsed laser at 1553 nm wavelength. In addition, it generated higher slope efficiency and maximum pulse energy of 13.15% and 8.56 nJ, respectively, in comparison to the TiO$_2$PF SA. On the other hand, the TiO$_2$PF SA produced 3.89 ps pulsed laser at 1560 wavelength. The TiO$_2$ film based pulsed laser had relatively higher maximum output power and maximum peak power of 12.17 mW and 3.43 kW, respectively. In overall, the TiO$_2$DF provides advantages in terms of thermal damage threshold, flexibility and durability. These features are important for a portable laser source design.

Acknowledgement
The authors would like to acknowledge Universiti Teknikal Malaysia Melaka (JURNAL/2019/FTKEE/Q00029) for the financial support.

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Table 1. Mode-locked EDFL performances comparison between TiO$_2$DF SA (fiber) and TiO$_2$PF SA (film).

| Optical quantity     | Unit | TiO$_2$DF SA (fiber) | TiO$_2$PF SA (film) |
|----------------------|------|----------------------|----------------------|
| Central wavelength   | nm   | 1553                 | 1560                 |
| Pump power           | mW   | 106-142              | 86-142               |
| Output power         | mW   | 3.73-8.42            | 7.58-12.17           |
| Peak power           | kW   | 0.39-0.88            | 2.14-3.43            |
| Slope efficiency     | %    | 13.17                | 8.17                 |
| Pulse energy         | nJ   | 3.79-8.56            | 1.98-4.21            |
| Repetition rate      | MHz  | 0.984                | 1.01                 |
| Pulse width          | ps   | 9.74                 | 3.89                 |
| SNR (FF)             | dB   | 54                   | 67                   |
| Linear absorption    | dB   | 1.55                 | 2.95                 |


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