Study of Effect of Lateral Connection in Moment Carrying Capacity of Frame in Multi Storey Structure

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Abstract – Now a days in Reinforced Concrete “Specific Moment Resisting Frames” are used as a part of seismic force resisting methods in buildings which are created to resist earthquakes. Beam-column joints, columns, and beams in moment frames are proportioned as well as detailed to resist shearing, axial, and flexural measures which result as a construction sways via many displacement cycles in intense earthquake ground shaking. Exclusive proportioning & detailing requirements lead to a frame capable of resisting strong earthquake shaking with no substantial loss of strength or stiffness. These moment resisting frames are called "Special Moment Resisting Frames" due to these extra needs, which help the seismic resistance in comparison with much less stringently detailed Ordinary and intermediate Moment Resisting Frames. The design criteria for SMRF buildings are provided in IS 13920 (2002). In this particular study, the buildings are intended both as OMRF and SMRF, and the performance of theirs is compared. Because of this, the structures are modelled and pushover analysis is performed in SAP2000. The pushover curves are plotted out of the analysis results and also the behaviour of structures is analyzed for different assistance conditions as well as infill conditions. The behaviour variables are additionally discovered for every construction while using values from pushover curve and it is investigated.

Keywords - Static Nonlinear analysis, earthquake engineering, ductility factor, Moment resisting frames, SMRF, OMRF, Pushover analysis, SAP2000, plastic hinges, response reduction factor.

I. INTRODUCTION

Earthquake is a worldwide phenomenon. Because of regular occurrence of earthquakes it is no more considered as being an act of God quite a systematic developing that has be investigated. Throughout earthquake, ground motions happen both vertically and horizontally in arbitrary fashions that cause structures to vibrate as well as induce inertia forces in them. Analysis of destroys incurred in moment resisting RC framed constructions put through previous earthquake show which disappointment could be because of utilization of concrete not having sufficient resistance, soft storey, beam column joint disaster for improper anchorage or weak reinforcements, column failure causing storey mechanism. Beam-column connection is regarded as among the potentially weaker parts whenever a system is put through seismic loading. Figures of several of the beam Column joint column and failure collapses in previous earthquakes are revealed with

Fig. 1.1. Thus this kind of column as well as joint disaster needs to be provided particular attention.
IS 13920(2002), specific moment frames are permitted to be designed for a force reduction factor of $R=\frac{1}{5}$. That's, they're allowed to be made for a base shear equal to one fifth of the worth obtained from an elastic effect evaluation. Moment frames are versatile lateral systems; thus, strength needs might be managed by the minimum base shear equations of the code.

II. PROBLEM STATEMENT

Present study focus on different aspects associated with the functionality of SMRF buildings. The primary goal of current study will be the analysis of relative functionality of OMRF and SMRF frames, designed as per IS Codes, utilizing nonlinear analysis. The greater realistic performance of the SMRF and OMRF building necessitates modelling the stiffness along with strength of the infill walls. The variations in the kind of the infill walls utilizing in Indian constructions are considerable. Based on the modulus of elasticity and also the strength, it could be classified as weak or strong. The 2 extreme cases of infill walls, weak and strong are thought by modelling the stiffness as well as power of infill wall space as accurately as you possibly can in the current study. The behaviour of structures depends on the kind of soils. Determined by the foundations resting on medium soils, the displacement boundary conditions in the bottom part of foundations may be looked at as hinged or maybe fixed. As the modelling of soils isn't in the range of the research, 2 boundary conditions, fixed and hinged, which symbolize 2 extreme conditions, are considered.

III. METHODOLOGY

Building Configurations and Design Details

A maximum of 12 frames are selected by different amount of stories quantity of bays, infill wall configurations, and style strategy with regard to effect reduction factors as well as confinement detailing. A comprehensive explanation of all of the frames considered is provided in Table (A). The storey height is 3.5m and bay width is 3m, that is exact same for those frames. Each and every frame was created as SMRF and OMRF considering response reduction things including 3 and 5. IS code suggests a response reduction factor of 3 for OMRF plus 5 for SMRF. The style of the frames is performed by conducting linear static analysis of bare frames as well as accounting for all of the load combinations recommended by IS 1893(2002). Two serious conditions like fixed and hinged support conditions are mirrored in the research. For convenient presentation of results, a good naming convention is followed. 4S7B-SMRF-B-F presents a bare frame, designed as SMRF with fixed support conditions. 4S7B-SMRF-I-H is an infill walled frame, designed as SMRF with hinged support conditions. A building may be treated as being a bare frame in case the infill frames are constructed with a definite gap between the wall space & columns therefore the infill walls don't engage in lateral loads. The structure frame with infill walls offered in all of stories is viewed as a completely infill frame.

| Sr No | Frame Name | Frame type | No. of storey | No. of bays | R | Frame type | Support conditions |
|-------|------------|------------|---------------|-------------|---|------------|-------------------|
| 1     | 4S7B-SMRF-B-F | Bare       | 4             | 7           | 5 | SMRF       | Fixed             |
| 2     | 8S7B-SMRF-B-F | Bare       | 8             | 7           | 5 | SMRF       | Fixed             |
| 3     | 10S7B-SMRF-B-F | Bare      | 10            | 7           | 5 | SMRF       | Fixed             |
| 4     | 6S2B-SMRF-B-F | Bare       | 6             | 2           | 5 | SMRF       | Fixed             |
| 5     | 6S4B-SMRF-B-F | Bare       | 6             | 4           | 5 | SMRF       | Fixed             |
| 6     | 6S6B-SMRF-B-F | Bare       | 6             | 6           | 5 | SMRF       | Fixed             |
| 7     | 4S7B-OMRF-B-F | Bare       | 4             | 7           | 3 | OMRF       | Fixed             |
| 8     | 8S7B-OMRF-B-F | Bare       | 8             | 7           | 3 | OMRF       | Fixed             |
| 9     | 10S7B-OMRF-B-F | Bare      | 10            | 7           | 3 | OMRF       | Fixed             |
| 10    | 6S2B-OMRF-B-F | Bare       | 6             | 2           | 3 | OMRF       | Fixed             |
| 11    | 6S4B-OMRF-B-F | Bare       | 6             | 4           | 3 | OMRF       | Fixed             |
| 12    | 6S6B-OMRF-B-F | Bare       | 6             | 6           | 3 | OMRF       | Fixed             |

Table (A) Details of all the frames

Material properties and Geometric parameters assumed

| Sr No | Design Parameter | Value |
|-------|------------------|-------|
| 1     | Unit weight of concrete | 25 KN/m³ |
| 2     | Unit weight of infill walls | 18 KN/m³ |
| 3     | Characteristic Strength of concrete | 25 MPa |
| 4     | Characteristic Strength of concrete | 415 MPa |
| 5     | Compressive strength of strong masonry ($f_{cm}$) | 5000 MPa |
| 6     | Compressive strength of weak masonry ($f_{cm}$) | 350 MPa |
| 7     | Damping ratio | 5% |
| 8     | Modulus of elasticity of steel | 2e5 MPa |
| 9     | Slab thickness | 150 mm |
| 10    | Wall thickness | 230 mm |
| 11    | Beam | 230mm x 350mm |
| 12    | Column | 300mm x 300mm |

Seismic Design Data assumed for Special and Ordinary Moment Resisting Frames

| Sr No | Design Parameter | Value |
|-------|------------------|-------|
| 1     | Seismic Zone | V |
| 2     | Zone factor (Z) | 0.36 |
| 3     | Response reduction factor (R) | 5 |
| 4     | Response reduction factor (R) | 3 |
| 5     | Importance factor (I) | 1 |
| 6     | Soil type | Medium soil |
| 7     | Damping ratio | 5% |

Pushover Analysis

Performance examination of the designed frames is performed using nonlinear static pushover analysis. The modelling of the created frames for nonlinear examination
is performed inside the Program SAP2000 Nonlinear. Pushover examination is a fixed, nonlinear procedure to analysis a construction where loading is incrementally enhanced by using a particular predefined pattern (i.e., inverted triangular or maybe uniform). Local nonlinear effects are modelled and the system is pushed until a collapse mechanism is created. With the increased the magnitude of a lot, weak back links and failure modes of the structure are located. At every step, system is pushed until sufficient hinges form to get a curve between base shear of the structure and their corresponding this curve and roof displacement widely known as pushover curve. At every phase, the entire base shear as well as the best displacement are plotted to have this particular pushover curve at different phases. It provides a concept of the maximum base shear which the system is effective at resisting and also the corresponding inelastic drift. For frequent buildings, it also provides an estimation of the global strength and stiffness in terminology of displacement and force of the structure. A common design frame & a regular pushover curve diagram is shown in fig below -

**Modelling Of Structural Elements**

Beams and columns have been modelled as frame components readily available in SAP 2000, with the central lines joined at nodes. Beam column joints are viewed as rigid beam-column joints and these're modelled giving end offsets in the joints. A rigid zone factor of 1.0 is assumed to replicate the rigidity at the joints. The floor slabs are assumed acting as diaphragms, and that ensure important activity of the entire vertical lateral load resisting elements. The weight of the slab was sent out as trapezoidal and triangular ton on the surrounding beams as per IS 456:2000.

IV. RESULT

A. COMPARISON OF SMRF AND OMRF: BARE FRAME, FIXED SUPPORT

In this specific comparison, the functionality of ordinary moment resisting special moment and frames resisting frames with fixed support circumstances are deemed. The base shear compared to roof displacement at every analysis step is obtained. The pushover curves are provided in every case. Figure 4.1 shows pushover curves of 4S7B bare frames designed as both SMRF and OMRF, with fixed support conditions. In Fig 4.1, the starting shear capacity of 4S7B OMRF is approximately 40 % much more than that of a 4S7B SMRF building. But the displacement capacity of 4S7B SMRF is approximately 3.5 times than that of a 4S7B OMRF.
Fig 4.5 Shows The Pushover Curves Of 8S7B OMRF And 8S7B SMRF With Fixed Support Condition And No Infill.

Fig 4.6 Shows The Pushover Curves Of 10S7B OMRF And 10S7B SMRF With Fixed Support Condition And No Infill.

Table 4.1 shows performance comparison about the ability of SMRF and OMRF frames to resist base shear and furthermore, the maximum amount of displacement it is able to undergo. It's found that ductility is much more for SMRF configuration, in all of instances, while OMRF works much better in its ability to withstand base shear.

Table 4.1 Performance comparison of OMRF and SMRF buildings with Fixed Support

| Building Configuration | BASE SHEAR (KN) | % Increase in Base Shear for OMRF | ROOF DISPLACEMENT (mm) | % Increase in Displacement for SMRF |
|------------------------|----------------|----------------------------------|------------------------|-----------------------------------|
| 4S7B                   | 425            | 300                              | 14                     | 60                                | 328%                              |
| 6S2B                   | 140            | 115                              | 120                    | 220                               | 83.3%                             |
| 6S4B                   | 350            | 250                              | 100                    | 175                               | 75%                               |
| 6S6B                   | 375            | 360                              | 110                    | 320                               | 199%                              |
| 8S7B                   | 520            | 420                              | 175                    | 375                               | 114%                              |
| 10S7B                  | 580            | 470                              | 320                    | 625                               | 96%                               |

It may be observed from Table 4.1 that OMRF buildings has approximately 20-40 % additional capability to withstand base shear, while SMRF buildings has approximately 75-200 % additional deflection than OMRF buildings.

B. COMPARISON OF SMRF AND OMRF: BARE FRAME, HINGED SUPPORT

In this specific comparison, the performance of ordinary moment resisting special moment and frames resisting frames with hinged support situations are deemed. The pushover curves for different configurations of structures are plotted and the construction response is observed.
C. COMPARISON OF SPECIAL MOMENT RESISTING FRAMES (SMRF) WITH FIXED AND HINGED SUPPORTS.

The pushover curve of SMRF frames with fixed and hinged support condition is plotted and the outcomes are seen. The pushover curve of 6S4B SMRF-B-F and 6S4B OMRF-B-F is plotted in Fig 4.13.

D. STOREY WISE COMPARISON OF SMRF BUILDINGS

The buildings with the exact same number of bays are viewed in this specific comparative study. The buildings considered are 4S7B SMRF, 8S7B SMRF And 10S7B SMRF, all having seven bays.

E. BAY WISE COMPARISON OF SMRF BUILDINGS

The buildings with the exact same number of stories are viewed in this specific comparative study. The buildings considered are 6S2B SMRF, 6S4B SMRF And 6S6B SMRF, all having six stories.

F. COMPARISON OF SMRF BUILDINGS WITH STRONG AND WEAK INFILL: FIXED SUPPORT CONDITION.

In this particular study, the performance of SMRF buildings with weak and strong infill is compared. For strong infill condition the importance of modulus of suppleness of brick
is had as 5000 MPa whereas for weak infill it’s taken as 350 MPa. In Fig 4.16, the static pushover curve of 6S4B SMRF building with strong and weak infill is shown.

2. The behaviour of SMRF building and also OMRF building without any infill and also hinged support conditions are compared. It’s discovered that the structures designed as SMRF perform far better when compared with the OMRF building. The ductility of SMRF is much more in most instances and that has gone approximately 75-200 % than that of OMRF buildings. But OMRF buildings resist 20-40 % additional base shear than that be opposed by SMRF buildings

3. The SMRF buildings with exact same number of different number and bays of stories are compared. The pushover curve is plotted and also it's discovered that the magnitude and the ductility of base shear which may be resisted, increases with rise in the quantity of stories. It’s found that all of the SMRF buildings considered has practically similar value of first slope in the thrust over curve.

4. The SMRF buildings with exact same amount of different number and stories of bays are compared. The pushover curve is plotted and also it’s found that the magnitude of base shear which may be resisted increases with rise in the number of bays. As the number of bays increases from two to four, the base shear capacity increases by two times. When it improves from two bays to six bays, the magnitude of the base shear the structure is able to withstand increase by three times it may be suggested that the number of bays have a significant part in the stability of the buildings considered for the current study.

5. The SMRF buildings with weak and strong infill are compared and also it’s discovered that the structures with strong infill is able to tolerate a better magnitude of base shear when than all those with weak infill. It may be realized that the SMRF buildings with much stronger infill have base shear capacity of approximately 1.5 to 2.5 times over that of SMRF buildings with weak infill. Although, a highly accurate conclusion can't be pulled away for ductility, it could be recommended that weak infill isn’t better due to the linear nature of theirs within the pushover curve.

V. CONCLUSION

The efficiency evaluation of buildings designed as Special Moment Resisting Frame (SMRF) and Ordinary Moment Resisting Frame (OMRF) is examined for various building configurations, infill conditions as well as help conditions. The buildings are intended and also modelled utilizing computational software. Several comparative scientific studies are performed to learn the behaviour of OMRF and SMRF.-

1. The behaviour of SMRF building and also OMRF building without any infill plus fixed support conditions are compared. It’s found that the structures designed as SMRF perform much better when compared with the OMRF building. The ductility of SMRF buildings is nearly 75 % - 200 % more than the OMRF structures in all of instances, why simply being the large confinement of concrete on account of usage and splicing of even more number of stirrups as ductile reinforcement. It’s likewise discovered that the base shear electrical capacity of OMRF buildings is 20 to 40 % much more than that of SMRF buildings.

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