Description of bandgaps opening in chiral phononic crystals by analogy with Thomson scattering

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Abstract
Chiral phononic crystals (PnCs) provide unique properties not offered by conventional metamaterial based on classic Bragg scattering and local resonance. However, it is insufficient to only consider the inertial amplification effect to describe its bandgap mechanism due to the absence of the bandgap caused by the chirality in some specific chiral structures. Here, we theoretically and experimentally introduce an analogy with Thomson scattering in electromagnetic waves to characterize the bandgap phenomena in chiral PnCs with translation–rotation coupling. Another phononic structures with translation–translation coupling are proposed to illustrate the universality of the analogy. We evidence that the coupling motion in chiral unit cells is similar to the result of Thomson scattering, which quantitatively formulizing as inertial amplification in theory and, twice elastic Thomson scattering allows the waves in the same polarization mode to superpose in antiphase, which is essence of the bandgap formation. This finding sheds a new light on the physics of the elastodynamic wave manipulation in chiral PnCs, thus opening a definite route for the pragmatic exploitation of chiral PnCs as well as other structures with motion coupling in achieving low-frequency and broad bandgaps.

1. Introduction
Phononic crystals (PnCs), one artificial periodical structure with the capability of flexible manipulation of acoustic and elastic waves, have received much attention [1–3]. The remarkable feature, i.e. the bandgap, provides a powerful ability to control the wave propagation, such as the design of the non-reciprocal device [4–6] and the recent valley state formation with Dirac points degeneracy operation in its bandgap [7, 8].

Local resonance [9] and Bragg scattering [10] are regarded as the mainstream bandgap mechanisms. In essence, both mechanisms mean two methods of realizing destructive interference. For the distinction, the destructive interference of the former features by the opposite movements between the main structure and resonant subsystem [11–14]. Therefore, we can observe the negative mass or the negative stiffness from a macro perspective. For the latter, in classical Bragg scattering, the destructive interferences are caused by the distance difference that satisfies $\lambda/2$ ($\lambda$ is one wavelength) [15, 16]. Distinguished from electromagnetic Bragg scattering, elastic waves are matter waves and their propagation relies on the vibration of the matter. Therefore, for elastic Bragg scattering, the tailored matrix can constrain the wave-propagation path. As a
result, the bandgaps do not meet the principle of the classical Bragg scattering as shown in equation (1) [17–19], called deep sub-wavelength bandgaps. In other words, as long as realizing the destructive interferences in the propagation path, a bandgap would be available,

\[ 2a \sin \theta = \lambda . \]  

(1)

Independent of local resonance and Bragg scattering gap, there is a design method called inertial amplification [20]. Ideally, its dynamic inertia can be amplified to infinity [20, 21]. Therefore, the disadvantages of local resonance and Bragg scattering, i.e. low frequency and broad band are incompatible with high stiffness and lightweight, can be overcome by this bandgap [20, 22–25]. Although some remarkable advances have been achieved [26–30], the structure configurations with inertial amplification effect always originate from the classic geometric model to extend their versatility and applicability [26–28, 31], rather than for further progress in amplifying dynamic inertia. Eventually, the breakthrough in low-frequency bandgaps is stalled, which can be attributed to the lack of diverse structures superficially. Actually, the ultimate reason is the obscureness in the underlying physics of the bandgap. In detail, despite the existence of the inertial amplification (see supplementary S1 and S2 or the [25]) in the system, the bandgap formation cannot be ensured in different geometrical configurations [24, 25, 32, 33]. Therefore, it deserves to study the essence of the inertial amplification and the underlying physics of this bandgap, to guide the advances of geometric diversification and thus provide more possible in lower-frequency bandgaps [26, 29, 31, 34].

In this work, we theoretically and experimentally investigate the wave phenomena and bandgap generation in the compression-torsion coupled PnCs to concretize the bandgap mechanism. An incident wave polarizing in one mode passing the chiral subunit cells will be decomposed into the outgoing waves with two polarizations, the one in translation and the other in rotation. The decomposition of the polarization can be considered as a splitting process of the incident waves, which can be an analogy to the result of Thomson scattering in electromagnetic waves [35] to be distinct from Bragg scattering [36]. It demonstrates that a minimum of twice Thomson scattering and the outgoing waves vibrating in identical mode have opposite phases after the second Thomson scattering are required to generate a bandgap. The findings are verified in a kind of chiral PnCs with translation–rotation coupling. For the universality of the underlying physics, another non-chiral lattice with the translation–translation coupling is proposed to demonstrate that this bandgap is not unique to chiral lattices but available in other lattices with Thomson scattering effects.

2. Structure and results

Figure 1 shows the schematics of the unit cells and calculated band structures. The lattices in figures 1(a) and (b) are unit cells with translation–rotation coupling, and in figures 1(c) and (d) are unit cells with translation–translation coupling. Each type of lattice consists of two subunit cells. As depicted in figures 1(a) and (b), the arrayed translation–rotation coupling unit cell named ATR consists of two subunit cells I. The mirrored translation–rotation coupling unit cell called MTR consists of subunit cells I and II. The right panels in figures 1(a) and (b) represent the corresponding band structure calculated by utilizing finite-element method-based software COMSOL Multiphysics. In terms of the bandgap, there is an extensive bandgap in MTR but not available in ATR.

In fact, the study on such bandgaps in MTR can be traced back to Bergamini’s work in 2019 [25], where the bandgap mechanism is attributed to inertial amplification and the nature of the coupling between the spins of the atoms which is provided by the relative orientation of adjacent chiral centers. As revealed by equations (S58) and (S63) in supplementary S2, the inertial matrixes of MTR and ATR have the inertial amplification effect, but the bandgap only exists in MTR. In other words, the current definition of inertial amplification lacks the universality principle of one mechanism like Bragg scattering and local resonance, even though inertial amplification has been studied for almost two decades. Therefore, this study aims to elucidate the underlying physics of inertial amplification and the coupling between the spins of the atoms.

As illustrated in the analysis of the subunit cell I (more details in supplementary S1), the chiral effect essentially achieves the motion coupling and thus exhibits the function of the inertial amplification, but this is not sufficient to form a bandgap. Due to the ambiguous contribution of chirality to the bandgap generation, one may easily attribute the underlying physics of the bandgap in figure 1(b) to the chirality. For instance, in some specific functional structures, chirality can indeed bring novel phenomena [37], such as negative Poisson’s ratio [38], high structural damping [39], and spin mechanical metastructures [40]. Some of these aforementioned properties have been realized in other non-chiral structures [17, 41, 42]. Therefore, chirality is one of the effective ways but not the exclusive way to achieve the desired function.
Figure 1. The lattices and the band structures. (a) Arrayed translation–rotation coupling unit cell (ATR); (b) mirrored translation–rotation coupling unit cell (MTR); (c) arrayed translation–translation coupling unit cell (ATT); (d) mirrored translation–translation coupling unit cell (MTT). As denoted in (a), each disk represents an individual lumped mass $m_i$. The symbols 'I' and 'II' represent two different subunit cells of translation–rotation coupling lattices (More details of the geometry can refer to figure S1). The symbol 'I' is left-handed, and the symbol 'II' is right-handed. The symbol ‘$\alpha$’ is the subunit cell of translation–rotation coupling lattices, and its geometry is illustrated in figure S7. The right panels in (a)–(d) represent the corresponding band structure with the bandgaps highlighted by gray areas.

The designed non-chiral unit cells with translation–translation coupling consist of two subunit cells $\alpha$ are demonstrated in figures 1(c) and (d). The arrayed and mirrored translation–translation coupling unit cell with central and rotational symmetry in $\alpha$ is named ATT and MTT. The right panels in figures 1(c) and (d) represent the calculated band structure. From the perspective of the bandgap, there is a phenomenon similar to that between MTR and ATR in figures 1(a) and (b), i.e. MTT has a bandgap that is not in ATT, which is an encouraging result as it confirms that the bandgap possessed in MTR is not exclusive to chiral lattices.

3. Mechanism analysis

To elucidate the mechanism of the bandgap generation, figure 2 shows the initial polarization orientations of the oscillators when the wave propagates in four types of unit cells shown in figure 1. For the sake of simplicity, two assumptions are made during the analysis. The z-axis rotational freedom of $m_1$ is restricted; the incident wave vibrates sinusoidally in translational form, and the initial direction of vibration is along $+z$ axis with an initial phase of zero (refer to the coordinate system shown in figure 1). As shown in figures 2(a) or (b), when the incident wave passes through the first subunit cell, the translation $u_1$ will split into the translation $u_2$ and rotation $\phi_2$.

Actually, the splitting process of the polarization is similar to the Thomson scattering. As illustrated in figure 3(a), in classical Thomson scattering, the plane electromagnetic wave forces the electron to vibrate; the vibration of electrons will create a harmonic electric field, thus resulting in two electromagnetic waves with the same frequency as the incident wave, which propagate in two directions [35]. For simplicity, we defined the torsional harmonic as rotational polarization. In our analogue, the subunit cell is regarded as the electron; as shown in figure 3(b) (Please refer to the results of the time domain simulation in supplementary S7 for more details), if the input is translational polarization, the subunit cell will vibrate in linear polarization but radiate another component wave which vibrates in rotational polarization; conversely, when the input is the rotational polarization, the radiative wave will vibrate in translational polarization.

One can see some similarities between the process of the classical Thomson scattering (figure 3(a)) and the wave propagation in the models (figures 3(b) and (c)). In terms of the function, the compression-torsion feature of the subunit cell is similar to the charged property of the electron in Thomson scattering. In terms of the scattering process, the forced vibration of the electrons driven by the incident electromagnetic wave is
Figure 2. The decomposition of the movement for (a) ATR, (b) MTR, (c) ATT, and (d) MTT. $u_i$ and $\varphi_i$ is the corresponds to the $i$th lumped mass, as denoted in figure 1(a). The abbreviation 'Scat' refers to scattering.

Figure 3. (a) Diagram of the classical electromagnetic Thomson scattering. (b) The scattering diagram of the translational polarization in chiral sub-unit cells when the input is rotational polarization. (c) The scattering diagram of the rotational polarization in chiral sub-unit cells when the input is translational polarization. The translational polarization in (b) and (c) strictly is longitudinal. For clarity, we use the shear linear polarization to replace it. (Refer to supplementary S7 for more details on the numerical data).
multiple directions \([43, 44]\). However, limited by the layout of the chiral subunit cell, the scattered waves cannot diverge to infinite space like the classical Thomson scattering but can only propagate in the direction of the periodical structure. These similarities enable us to draw an analogy with Thomson scattering to clarify the process of wave propagation in chiral subunit cells. Therefore, for simplicity, we name the wave propagation process in the chiral subunit cell as Thomson scattering.

Furthermore, the process that these scattered waves \((u_2, \varphi_2)\) pass through the second subunit cell is equivalent to undergoing a second Thomson scattering. The distinction from the first is that the second scattering has two incident waves \((u_2, \varphi_2)\). Consequently, after the second scattering, it will produce four scattered waves, i.e. \(u_{31}, u_{32}, \varphi_{31},\) and \(\varphi_{32}\). Among them, \(u_{31}\) and \(u_{32}\) vibrate in translation, but \(\varphi_{31}\) and \(\varphi_{32}\) vibrate in rotation.

In ATR, by the first scattering, the initial direction of the scattered waves \(u_2\) and \(\varphi_2\) are \(+z\) and clockwise around the \(+z\)-axis (from the \(+z\)-axis perspective), respectively. After the second scattering, regarding \(u_2\) as the incident wave, the initial direction of the scattered wave \(u_{31}\) is \(+z\), and the initial direction of the scattered wave \(\varphi_{31}\) is in the clockwise direction. Meanwhile, regarding \(\varphi_2\) as the incident wave, the initial direction of \(u_{32}\) is \(+z\), and the initial direction of \(\varphi_{32}\) is also in the clockwise direction. Since the two translations \(u_{31}\) and \(u_{32}\), and the two rotations \(\varphi_{31}\) and \(\varphi_{32}\) have the same direction, \(u_3\) and \(\varphi_3\) of \(m_3\) in ATR can be written as equations (2) and (3),

\[
\begin{align*}
u_3 &= u_{31} + u_{32}. \\
\varphi_3 &= \varphi_{31} + \varphi_{32}.
\end{align*}
\]

Eventually, the absolute angle \(\varphi_3\) of \(m_3\) in ATR can be determined as

\[
\varphi_3 = q(u_1 - u_3),
\]

where \(q\) is the rotational angle of translation per unit (see supplementary S2 for details).

Conversely, in MTR, the initial direction of the scattered wave \(u_2\) is \(+z\), and the initial direction of the scattered wave \(\varphi_{31}\) is in the clockwise direction; nevertheless, the initial direction of \(u_{32}\) is \(-z\), and the initial direction of \(\varphi_{32}\) is in the counterclockwise direction. The \(u_3\) and \(\varphi_3\) of \(m_3\) in MTR can be written as

\[
\begin{align*}
u_3 &= u_{31} - u_{32} \\
\varphi_3 &= \varphi_{31} - \varphi_{32}.
\end{align*}
\]

Then, in MTR, the absolute angle \(\varphi_3\) can be determined as

\[
\varphi_3 = q(u_1 + u_3 - 2u_2).
\]

\[
M\ddot{u}_n + Ku_n = M'\ddot{u}_1 + K'u_1.
\]

Although the governing equation can be generalized to an identical form, as illustrated in equation (8), the difference in the absolute angle for \(m_3\) in ATR and MTR leads to the immense variability of the elements in inertial matrices \(M\) and \(M'\). Detailly, for instance, for the inertial matrix for ATR containing \(n\) sub unit cells, \(M_{ATR}\) is written as

\[
M_{ATR} = \begin{bmatrix}
m_{11} & 0 & 0 & \ldots & 0 \\
0 & m_{22} & 0 & \ldots & 0 \\
0 & 0 & m_{33} & \ldots & 0 \\
\vdots & \vdots & \vdots & \ddots & \vdots \\
0 & 0 & 0 & \ldots & m_{nn}
\end{bmatrix}.
\]

Please refer to equation (S63) for the principle of the non-zero elements in \(M_{ATR}\).
\[ M'_{\text{ATR}} \]

\[
M'_{\text{ATR}} = \begin{bmatrix} m_{11}' & m_{12}' & \cdots & m_{1n}' \\ m_{21} & m_{22} & \cdots & m_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ m_{n1} & m_{n2} & \cdots & m_{nn} \end{bmatrix}.
\] (10)

Please see equation (S64) for the detailed expression of \( m_{ij}' \) in \( M'_{\text{ATR}} \).

However, for MTR containing \( n \) unit cells, inertial matrix \( M_{\text{MTR}} \) has the form denoted as equation (10),

\[
M_{\text{MTR}} = \begin{bmatrix} m_{11} & m_{12} & \cdots & m_{1n} \\ m_{21} & m_{22} & \cdots & m_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ m_{n1} & m_{n2} & \cdots & m_{nn} \end{bmatrix}.
\] (11)

Please refer to equation (S58) for the principle of \( m_{ij} \) in \( M_{\text{MTR}} \).

\[ M'_{\text{MTR}} \]

\[
M'_{\text{MTR}} = \begin{bmatrix} m_{11}' & m_{12}' & \cdots & m_{1n}' \\ m_{21}' & m_{22} & \cdots & m_{2n}' \\ \vdots & \vdots & \ddots & \vdots \\ m_{n1}' & m_{n2}' & \cdots & m_{nn}' \end{bmatrix}.
\] (12)

Please see equation (S60) for the details of \( m_{ij}' \) in \( M'_{\text{MTR}} \).

In brief, after twice Thomson scattering, the property that the scattered waves vibrating in the same modes have opposite initial vibration directions similar in MTR determines the feature that whether the inertial matrix has non-zero elements, thus plays a decisive role presence of the bandgap.

The splitting process and wave propagating in the translation–translation coupling (ATT and MTT) PnCs can also be an analogy to Thomson scattering, as shown in figures 2(c) and (d). In ATT, by the first scattering, the initial directions of the scattered waves \( u_2 \) and \( v_2 \) point in \(+z\) and \(+x\) axis. \( u_{31}, u_{32} \) and \( v_{31}, v_{32} \) point to \(+z\) and \(+x\) directions after the second scattering when \( u_2, v_2 \) are considered as the incident wave. However, in MTT, \( u_{31} \) and \( u_{32} \) point to \(+z\) and \(-z\), \( v_{31} \) and \( v_{32} \) point to \(-x\) and \(+x\) directions, respectively. The superposition of these waves in MTT with opposite vibrating directions enables the capability of energy cancellation and generating bandgap, coinciding with the findings in MTR. Therefore, the analogy results confirm the universality of the mechanism proposed in this work.

4. Theoretical, numerical, and experimental verification

To verify the reasonability of the wave phenomena and bandgap feature described by using the analogy of Thomson scattering in figure 2, we have built the movement relationship in formulas according to the scattering process (more details of the theory in supplementary S2). Meanwhile, the theoretical frequency response functions (FRFs) of the two unit cells in figure 4(b) are carried out, as displayed by the red solid lines in figures 4(c) and (d). From the theoretical results, at high frequencies, the FRFs of MTR and ATR are constant, but only the MTR exhibits significant attenuation, which allows the excellent potential for generating an ultra-broad bandgap in this lattice. Figure 4(d) shows two anti-resonant notches, which facilitate enhancing the attenuation of bandgaps. Meanwhile, compared with the FRF in figure S2, the theoretical result in figure 4(d) shows one more anti-resonance peak when the finite structure has two unit cells, which means that the number of the anti-resonance notches can be increased with the increase of the number of the unit cell. This property will be further discussed in section 5.

To demonstrate the correction of the theory, the finite-period structures containing two unit cells of ATR and MTR are numerically calculated in COMSOL solid mechanics module. The material is one kind of Nylon with the elastic modular \( E = 1.6 \times 10^9 \) Pa, the Poisson’s ratio \( v = 0.4 \), and the density \( \rho = 1000 \) kg m\(^{-3}\). In the simulation, only the \( z \)-axis translational freedom of the disk at the input end is reserved to match the boundary conditions of the theory. The surface displacement load is applied at the
Figure 4. (a) The schematic of the experimental configuration. The insert in the upper right corner is the detail of the connection between the sample and the plexiglass. (b) Photograph of the investigated samples. ATR sample on the left, and MTR sample on the right. (c) Experimental (green solid with stars), numerical (blue dotted), and analytical (red solid) frequency response functions (FRFs) of ATR. (d) Experimental (green solid with stars), numerical (blue dotted), and analytical (red solid) FRFs of MTR.

input end disk rather than a force load to ensure consistency with the analysis and experiment. The domain point probes record the acceleration signals $a_i$ at the center of the input end lumped mass and $a_o$ at the output end. The FRF can be calculated by taking $a_i$ as the reference and the numerical results are presented as blue dotted lines in figures 4(c) and (d).

Figure 4(a) shows the details of the experimental configuration, and figure 4(b) shows the fabricated ATR and MTR samples through photopolymerization-based 3D printing technology. The sample input disk is bolted to a plexiglass with a thickness of 10 mm. Notably, the plexiglass has approximately ten times weight than the two unit cells, to limit the freedom of rotation of the disk around the $z$-axis as much as possible. The plexiglass is supported using elastic supports to avoid exceeding the allowable amplitude range to protect the shaker. Three foam pieces are used instead of the ideal elastic support to level the plexiglass easily. The shaker is excited directly on the plexiglass through the top bar to simulate the input of displacement load input in simulation and analysis. Two sensors (PCB 353B15) are attached to the top and the bottom of the sample to pick up the output acceleration $a_o$ and the input acceleration $a_i$, respectively. The experimental results obtained by the accelerometers are recorded in real-time using M + P Vibpilot. The frequency range of the sine sweep is 100–1500 Hz with a frequency resolution of 2 Hz and the sweeping speed is 400 Hz min$^{-1}$, to guarantee the precision of experimental data. The experimental FRFs are marked by the green line with stars.

As illustrated in figures 4(c) and (d), a significant attenuation occurs from 450 Hz to 1280 Hz in the FRF of MTR, and it does not exist in that of ATR. In a nutshell, the bandgap does only exist in MTR, not in ATR. Significantly, the consistency of experimental, numerical, and theoretical results demonstrates the correctness of the analysis. Also, it verifies the validity of the analogy that the bandgap generation mechanism of this PnC is similar to Thomson scattering. Limited by the insufficient degrees of the freedom in the lumped mass method, the theoretical FRF at high frequency has a large discrepancy with numerical and experimental results, such as over 500 Hz for ATR and over 1000 Hz for MTR. Nevertheless, the intuitive nature of this method in bandgap-mechanism explanation is irreplaceable than other precise methods, such as spectral element method [45].
5. Discussion

5.1. Anti-resonant notches

Previous studies [20, 30] mentioned that when the inertia is amplified, there will be an anti-resonant notch in FRF, and the anti-resonant notch can be observed in complex band structures [7, 34]. Although the inertial amplification is involved in the Thomson scattering-induced bandgap, the anti-resonant notch is unessential for forming the Thomson scattering-induced bandgap.

Figure 5 shows the band structures of the MTRs with \( a = 60 \) mm and \( a = 35 \) mm. When the lattice constant is 60 mm, the bandgap is 480–1250 Hz; when \( a = 35 \) mm, it is 960–1940 Hz. Figures 5(c) and (d) show the analytical FRFs of MTR with different numbers of the unit cell when the lattice \( a = 35 \) mm (blue line) and \( a = 60 \) mm (red line). Because the lattice constant varies from 60 mm to 35 mm, the stiffness increases from 256060 N m\(^{-1}\) to 377630 N m\(^{-1}\), and the amplified inertia decreases from 0.0432 to 0.0062 (both variables are obtained theoretically). One can observe from figure 5(c) that the anti-resonant frequency disappears when \( a = 35 \) mm. As shown in figure 5(d), despite the anti-resonant frequency appears again when the number of the unit cell is 4, the reduction of the amplified inertia leads to the shift of the anti-resonant frequencies toward higher frequency and even beyond the range of the bandgap.

To accurately catch the effect of the anti-resonant notches on the FRF, figure 5(e) shows the numerical FRFs of the finite structures with four unit cells. For comparison purposes, we consider the influence of the geometric configurations of the lattice constant and equivalent physical parameters on the FRF [22, 46], so we use equation (13) to normalize the frequency in FRFs,

\[
f_n = \frac{f_n}{f_a}.
\]

The filling ratio can be determined as

\[
\rho_e = \frac{M}{V},
\]

where the parameter \( V \) can be calculated by

\[
V = \frac{D^2 \pi a}{4}.
\]

The equivalent stiffness \( k_{\text{eff}} \) can be determined by equation (S15).
Figure 6. (a) Schematics of the finite structure with different numbers of the MTR unit cells. (b) Theoretical and (c) numerical discussion about the variation of the anti-resonant notch with the number of the MTR unit cells.

According to the analysis, the filling ratio is 586 kg m\(^{-3}\) for \(a = 35\) mm, and it is 346.9 kg m\(^{-3}\) for \(a = 60\) mm; the equivalent stiffness is equal to 377 630 N m\(^{-1}\) for \(a = 35\) mm, and that is equal to 256 060 N m\(^{-1}\) for \(a = 60\) mm. The normalized FRFs are shown in figure 5(e).

It can be observed from figure 5(e) that the depth of \(a = 35\) mm is significantly weaker than that of \(a = 60\) mm when the anti-resonant notches disappear. When the number of periods is up to 4, the attenuation difference is even by more than two orders of magnitude. Most importantly, influenced by the resonant frequency at the upper boundary, the theoretical anti-resonant frequency is not reflected in the FRFs. Despite the disappearance of the anti-resonant notches, the bandgap is still reserved in the band structure.

Undeniably, the existence of anti-resonant notches has significant implications. Figure 6(a) gives the pattern of variation in the number of MTRs. As shown in figure 6(b), as the number of the unit cells increases, the converged value at high frequency will decrease, and the number of the anti-resonant notch will increase (These properties do not exist in ATR, please see supplementary S4 for more details). The increase in anti-resonant gaps can accelerate bandgap formation. Notably, the anti-resonant notches are located mainly at the lower boundary of the bandgap and are spread, which enhances the modulation capacity of low-frequency and broad elastic waves.

In fact, as shown in figure 6(b), the infinite extension of the attenuation will be cut off due to the higher-frequency resonance modes. These resonant modes will suppress the anti-resonant notches close to it. Therefore, the anti-resonant notches at high frequency will be covered with the number of periods increases, thus weakening the attenuation, as illustrated by the green plot in figures 6(a) and (b).

To sum up, the bandgap formation does not depend on the anti-resonant notch. The anti-resonance frequency just has the function of enhancing the manipulation of low-frequency. Determining the type of the bandgap by the shape of the attenuation is inaccurate \([16, 47–49]\), especially for Bragg scattering-induced and Thomson scattering-induced bandgaps.

5.2. Thomson scattering-induced and Bragg scattering-induced bandgaps
Figures 7(a) and (b) exhibit a Thomson scattering unit cell and a Bragg scattering unit cell to find the intrinsic distinction between the Bragg scattering and Thomson scattering bandgaps. The parameter \(\theta\) of the MTR is set as 90\(^\circ\) to invalidate the coupled motion and reserve the translation alone, thus allowing a Bragg
scattering unit cell to be obtained, as shown in figure 7(b). Consequently, there is a Bragg scattering bandgap due to the impedance mismatch between the lumped masses and the ligaments [10, 50].

For a fair comparison, all physical parameters are the same except that the elasticity modulus of the ligaments in the Bragg scattering unit cell is determined to be $1.05 \times 10^8$ Pa to maintain the same stiffness between both unit cells in figure 7. Consequently, the equivalent stiffness and lattice constants of the cells are identical. There is a slight variation in the equivalent density of the unit cells because of the variation in ligament length. The total mass of the six ligaments in the MTR unit cell is 2.3 g, while the one in the Bragg scattering unit cell is 1.9 g (the total mass of the MTR unit cell is 58.86 g). Therefore, we named the condition quasi-equal density.

Under the condition of the same lattice constant, stiffness, and quasi-equal density, the Thomson scattering bandgap extends from 400 Hz to 1200 Hz with a relative width of 100% (as illustrated in figure 7(a)), while a Bragg scattering bandgap at 930–2610 Hz with a relative width of 95% can be observed in figure 7(b). A shift in the starting frequency to a lower frequency is evident, reaching 57% with 930 Hz as a reference.

From figures 7(c) and (d), significant variances in energy distributions of both types of bandgaps can be observed. In classical Thomson scattering, the forced vibration of the electron is the key to scattering. In the bandgap induced by the analogous Thomson scattering, it requires that the scattered waves undergone the first scattering needs to undergo the Thomson scattering again. In addition, the second-round scattered waves polarized in the same mode must have opposite phases to achieve destructive interference. It can be determined from this process that the involvement of the lumped masses is crucial for achieving attenuation. Since the first lumped mass is the vibration source and the waves have destructive interference in the process of the second scattering, the energy within the bandgap should be mainly concentrated in the second lumped mass. Indeed, figure 7(c) verifies this reasoning.

However, in classical Bragg scattering, the interaction between the incident wave and the scatterer is for reflecting incident waves. In Bragg scattering PnCs, the function of the scatterers is to reflect the incident wave and thus produce destructive interference. Correspondingly, the energy of the Bragg scattering bandgap is mainly localized in the matrix medium. For the unit cell of figure 7(b), the lumped masses act as the scatterers and the ligaments act as the matrix. Therefore, the energy of the bandgap should be mainly localized to the ligaments as the matrix medium, as can be observed in figure 7(d).

The analogy of Thomson scattering can reasonably explain several phenomena from the perspective of underlying physics. It is well known that Bragg scattering is the elastic collision between the waves and the atoms. The scattered waves in Bragg scattering rely on the heavy atoms to reflect the incident waves and thus
to destructive interferences [51]. Thomson scattering depends on the polarization of electrons to generate divergent outgoing waves in different polarizations [36]. In the Bragg scattering lattice, the propagation of the scattered wave does not depend on the vibration of the scatterers represented by the lumped masses, and thus the scattered waves propagate mainly as reflections [51] with the vibration concentrated on the ligaments [15, 47]. In Thomson scattering, however, the propagation of the scattered waves depends on the polarization of the electrons represented by the entire subunit cell. The orientation of the scattered waves is primarily in the forward direction of the incident wave. As a result, the attenuation in the bandgap is gradient rather than localized on ligaments (please refer to figure S8). Because the electrons are much lighter in mass than the atoms, the Thomson scattering will produce a more lightweight unit cell than a Bragg scattering unit cell for the same lattice, stiffness, and bandgap starting frequency [52, 53], which can also be drawn from figure 7. In addition, Thomson scattering allows a smaller number of the periods to reflect the significant attenuation of the bandgap (please refer to figure 6).

6. Conclusion

In conclusion, we have theoretically and experimentally demonstrated the wave propagation and the formation mechanism of bandgaps in compression-rotation coupling PnCs. The coupling motion and wave propagation profile present an analogy to Thomson scattering. The results revealed that several conditions need to be met in the analogue Thomson scattering-based PnCs to generate a bandgap. First, the orthogonal coupling motions are essential for producing the Thomson scattering, which is quantitatively characterized as inertial amplification in equations. Second, these initial scattered waves must undergo a minimum of twice Thomson scattering. Third, the secondary scattered waves vibrating in the same mode should have the opposite initial direction of the vibration, which is the cause of the superimposable attenuation, and thus generates the bandgap. Remarkably, the third condition is the nature of that the inertial coupling phenomena (i.e. a non-diagonal inertial matrix as mentioned in [26, 30, 31] and equation (S58)) occurs in theory. Although the quantitative characterizations demonstrate the anti-resonant frequencies in FRFs, the anti-resonant frequency is not essential for the bandgap generation. This work revealed that PnCs with inertial amplification only cannot ensure an extensive bandgap similar to MTR and MTT. Chirality is a virtual design element and one of the methods in realizing the Thomson scattering but not an indispensable condition for achieving such a bandgap.

It should be emphasized, the analogue to classic Thomson scattering of electromagnetic waves was proposed to help us to understand the underlying physics of the bandgap. Indeed, the underlying physics of the bandgap in our work cannot be considered to be completely identical to the general mechanism (classic Thomson scattering). Both have some significant differences and are not limited by the fact that the extremely important aspect of the Thomson scattering is for the long-wavelength limit which is not considered in this analogue. Despite these, the materialization of the inertial amplification and bandgap generation carried out in this work enables to couple of any two or more orthogonal modes to generate a substantial inertial amplification (instead of by the law of leverage [26, 54]), and thus generate an ultra-low-frequency bandgap. The works could shed new light on the physics of the elastodynamic wave manipulation in inertial amplification-induced PnCs, and offer an entirely exotic avenue for the diverse design and investigation of PnCs with remarkable properties, such as the bandgap with lower starting frequency, broadband, and extensive attenuation.

Data availability statement

All data that support the findings of this study are included within the article (and any supplementary files).

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