Research Article

Effect of Osmotic Pressure on Migration Behavior of nZnO in GCLs

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1.Introduction

Zinc oxide nanoparticles (nZnO) are a high-performance inorganic product and are currently one of the most widely used engineered nanoparticles (ENPs) in the world [1, 2]. However, Collins [3] reported that nZnO can affect the survival of organisms in the soil and can even change their community structure. At concentrations of 50 and 100 mg/L, nZnO exhibited cytotoxicity in Neuro-2A cells [4]. Moreover, nZnO can reach the membranes of human aortic endothelial cells (HAECs) and can be absorbed. At a concentration of 10 mg/L, nZnO induced a conspicuous inflammatory response in HAECs. At higher concentrations, nZnO could lead to HAEC necrosis [5]. The toxic effects of nZnO on human lung adenocarcinoma cells (A549) were concentration-dependent and time-dependent [6]. Deng [7] held that the cytotoxicity of nZnO was mainly caused by the dissolved zinc ions.

Solid waste landfill leaking is a key path for nanoparticles to enter the natural environment [8]. With increasing application of nano materials, large amounts of nanoparticles have entered landfills as three types of waste [9]. Nanoparticles in liquid waste can easily enter the leachate of landfill. Boilyard et al. [10] and Khan et al. [11] have found that nanoparticles suspended in leachate can migrate successfully through garbage soil. Current studies have mostly adopted column elution tests to simulate nanoparticle migration in the soil. The testing systems mainly consisted of a suspension of nZnO particles (nZnO suspension) and a porous medium [12]. The porous medium was typically composed of quartz sand, silica sand, and glass beads, which serve as a simplified replacement of natural soil. The physical and chemical properties of the porous medium are distinctly different from those of natural soil. Research results showed that the migration of carbon nanotubes was weaker in quartz sand than in glass beads [13]. The smaller the particle size of quartz sand is, the weaker the migration of nanoparticles is. When the particle size of quartz sand decreased from 0.106 mm to 0.043 mm, the concentration of nanoparticles in the effluent declined by 60% [14]. Similar patterns have also been observed in nTiO2 and nAg in subsequent studies [15]. The interception ratio of nC60 in

The migration of zinc oxide nanoparticles (nZnO) in geosynthetic clay liners (GCLs) under different osmotic pressures was conducted using a self-developed geosynthetic clay liner osmometer. The effects of the osmotic pressure on the migration behavior of nZnO in GCLs were analyzed. The results showed that, with an increase of osmotic pressure, the retention rate of nZnO increased greatly, the particle size increased, the stability of the soliquoid declined, GCLs pores were compressed, the infiltration coefficient of GCLs reduced, and the interception effect of GCLs on nZnO particles strengthened. The two-site model can simulate the migration behavior of nZnO in GCLs very well. The correlativity between the maximum migration distance ($L_{\text{max}}$) of nZnO in GCLs and the osmotic pressure was negative.
clay-containing soil specimens was far higher than that in quartz sand and glass beads. The interception in soil specimens was irreversible [16]. The findings indicated that soil properties exert significant influence on nanoparticle migration in soil. In addition, specific chemical properties of the suspension (e.g., ionic strength, organic matter content, surface active agents, and pH values) can indirectly affect the migration behavior of nanoparticles in a porous medium by influencing nanoparticle scattering and suspension stability [17, 18, 19, 20].

Aforementioned research on the migration of nanoparticles in ideal porous media (e.g., glass beads and quartz sand) or sand obtained preliminary results [21, 22]. The NPs migration and sorption processes are related to the soil properties differentiation [23]. Until now, no published studies have considered the influence of osmotic pressure on the migration properties of nanoparticles in a porous medium. A previous test conducted at landfill sites indicated that the water level of leachate inside landfills could be as high as 20 m–30 m [24]. Geosynthetic clay liner (GCL) was used as the last barrier preventing garbage leachate to enter the natural environment [25]. Whether can GCLs effectively intercept nanoparticles under high osmotic pressure? Therefore, it is an important issue that how osmotic pressure in landfill leachate impacts on migration behaviors of nZnO particles from GCLs to the groundwater.

2. Experimental Materials and Methods

2.1. Material

2.1.1. Geosynthetic Clay Liner. The GCL was prepared by stitching sodium bentonite particles between two layers of geotextiles. According to the data provided by the GCL manufacturer, the bottom layer was woven geotextile with a unit mass of 221 g/m², the top layer was nonwoven geotextile with a unit mass of 112 g/m², and the middle layer was bentonite. The performance of GCL and properties of bentonite are shown in Tables 1 and 2, respectively. The structural representation of the GCL is shown in Figure 1.

2.1.2. Preparation of the nZnO Suspension. nZnO particles were synthesized by a solid reaction process in this experiment. The specific processes are as follows:

1. After a specific amount of nZnO had been scattered in an adequate amount of deionized water, the mixture was subjected to an ultrasonic crusher. The nZnO suspension achieved optimal scattering when the frequency, temperature, and time of the ultrasonic crusher were set at 28 kHz, 50°C, and 25 min, respectively [26].

2. The experiment employed inductively coupled plasma mass spectrometry (ICP) to measure the concentrations of nZnO suspensions. When the concentrations of elements differed, the suspensions emitted characteristic lights of varying intensity. Quantitative analysis was conducted using this property. The measuring process included the following steps: (i) tetraacetic acid digestion to process the dispersion (the acid converted nZnO to zinc ions; the acid also dissolved soil and other impurities); (ii) ICP to measure the concentration of zinc ions and to calculate the concentration of nZnO suspension; and (iii) ZetaPALS to measure the zeta potential of the solution. The zeta potential represents the stability of colloidal dispersion. Table 3 shows the dispersion properties of nZnO suspension which is gotten as described above.

2.2. Experimental Setup. The osmometer self-developed comprised a pressure control system (composed of a pressure controller, an air pressure pump, and a pressure gauge), a temperature control system (a constant temperature sink), an infiltration chamber, and an automatic collector. The various parts of the system were connected by plexiglass hollow tubes to form a closed system (Figure 2). Osmotic pressure could be adjusted from 0.1 MPa to 0.5 MPa using a pneumatic pump.

| Parameters                        | 5.56 | 6.78 | 11.85 | 10.28 | 19.50 | 10.67 | 2.69 × 10⁻⁹ | 5.32 |
|----------------------------------|------|------|-------|-------|-------|-------|-------------|-----|
| Mass per unit area (kg/m²)       | 5.56 | 6.78 | 11.85 | 10.28 | 19.50 | 10.67 | 2.69 × 10⁻⁹ | 5.32 |
| Thickness (mm)                   | 6.78 | 6.78 | 6.78  | 6.78  | 6.78  | 6.78  | 6.78        | 6.78 |
| Longitudinal breaking strength (kN/m) | 5.56 | 6.78 | 11.85 | 10.28 | 19.50 | 10.67 | 2.69 × 10⁻⁹ | 5.32 |
| Transverse breaking strength (kN/m) | 5.56 | 6.78 | 11.85 | 10.28 | 19.50 | 10.67 | 2.69 × 10⁻⁹ | 5.32 |
| Longitudinal breaking elongation (%) | 5.56 | 6.78 | 11.85 | 10.28 | 19.50 | 10.67 | 2.69 × 10⁻⁹ | 5.32 |
| Transverse breaking elongation (%) | 5.56 | 6.78 | 11.85 | 10.28 | 19.50 | 10.67 | 2.69 × 10⁻⁹ | 5.32 |
| Vertical permeability coefficient (m/s) | 5.56 | 6.78 | 11.85 | 10.28 | 19.50 | 10.67 | 2.69 × 10⁻⁹ | 5.32 |
| Sodium bentonite content (kg/m²) | 5.56 | 6.78 | 11.85 | 10.28 | 19.50 | 10.67 | 2.69 × 10⁻⁹ | 5.32 |

Table 2: Basic properties of bentonite.

| Mineral composition (%) | Montmorillonite | Kaolinite | Illite | Orthoclase | Quartz |
|------------------------|-----------------|-----------|--------|------------|--------|
| SiO₂                   | 57.2            |           |        |            |        |
| Al₂O₃                  | 16.5            |           |        |            |        |
| CaO                    | 3.4             |           |        |            |        |
| TiO₂                   | 0.8             |           |        |            |        |
| Fe₂O₃                  | 5.7             |           |        |            |        |
| Na₂O                   | 3.3             |           |        |            |        |
| K₂O                    | 0.7             |           |        |            |        |
| MgO                    | 3.7             |           |        |            |        |

| Chemical composition (%) | Na⁺ 0.445 | K⁺ 0.010 | Ca²⁺ 0.159 | Mg²⁺ 0.017 |
|--------------------------|-----------|----------|------------|------------|

| Ion exchange capacity (mmol/g) | Na⁺ 0.445 | K⁺ 0.010 | Ca²⁺ 0.159 | Mg²⁺ 0.017 |
|--------------------------------|-----------|----------|------------|------------|

| Initial water content (%)     | 17.0      |
|--------------------------------|-----------|
| Initial thickness (mm)         | 6.65      |
| pH                             | 9.89-10.67 |
2.3. Experimental Methods. To investigate the effects of varying osmotic pressure on the migration of nZnO particles in GCLs, five osmotic pressure levels were set according to the water level of landfill leachate. Table 4 shows the experimental parameters.

The experiment steps were as follows:

(1) Inject 20 pore volumes (PV, obtained by dividing exudate volume by GCLs pore volume) of deionized water into the infiltration chamber and infiltrate GCLs under a specific pressure.

(2) Mix nZnO granule stock solution with a suitable amount of background solution at a specific proportion and use a magnetic stirrer to stir for 3 h to ensure complete mixing.

(3) Inject uniformly mixed nZnO granule suspension into the infiltration chamber and set a corresponding osmotic pressure using the control system.

(4) Collect exudate every 1/3 PV.

(5) When 15 PV of exudate have been collected, elute nZnO particles that have been intercepted in the GCLs using 5 PV of deionized water.

(6) Collect the exudate at the bottom of the infiltration chamber by using an automatic collector and centrifuge tubes. All exudate samples obtained through infiltration and elution were collected in 5 mL centrifuge tubes.

(7) Measure nZnO particle concentration using ICP.

Table 3: The basic properties of nZnO suspensions.

| Component | State                  | Particle distribution range | Dispersive medium | pH | Zeta potential | Concentration |
|-----------|------------------------|----------------------------|-------------------|----|----------------|---------------|
| nZnO      | Pure white uniform colloid | 2~40 nm                    | Deionized water   | 10~11 | 37 mV          | 50 mg/L       |

Table 4: The parameters of experiment.

| Experimental condition | Osmotic pressure  |
|------------------------|-------------------|
| Initial concentration 50 mg/L | From 0.1 to 0.5 MPa |
| Ionic strength 1 mmol/L  |                   |
| Organic content 1 mg/L   |                   |
| Temperature 30°C         |                   |

Note. °C = degrees centigrade.
Mark the concentration of nZnO particles before infiltrating GCLs as $C_0$ and that in the exudate collected after infiltrating GCLs as $C$. After the experiment has been completed, adopt the PV number as the abscissa and $C/C_0$ as the ordinate to plot a breakthrough curve (BTC) of nZnO particles. The maximum $C/C_0$ indicates maximum breakthrough equilibrium concentration ($C_{\text{max}}$). When at least three consecutive $C/C_0$ values are $\geq 95$ percent of the $C_{\text{max}}$, it is defined as equilibrium in the breakthrough curve. The smallest PV value corresponding to $C_{\text{max}}$ is defined as the equilibrium critical PV.

The compression test and infiltration test of GCLs were conducted with Chinese standard for soil test method (GB/T 50123-1999).

2.4. Theoretical Model. This study adopted a two-site kinetic attachment model in porous media proposed by van Genuchten and Wagenet [27] to analyze the migration of nanoparticles in porous media. The dimensionless form of the two-site kinetic attachment model can be expressed as:

$$\frac{\partial C_1}{\partial t} + (\beta R - 1) \frac{\partial C_1}{\partial t} + (1 - \beta) R \frac{\partial S}{\partial t} = \frac{1}{Pe} \frac{\partial C_1}{\partial X} \frac{\partial C_1}{\partial X},$$

where $C_1$ is the relative concentration $C/C_0$; $\beta$ is the fraction of instantaneous retardation, denoting the distribution of instantaneous equilibrium and rate-limited site types; $\omega$ is the Damköhler number, which is the ratio between the retention time and the characteristic absorption time in hydrodynamics; $T$ is the number of pore volumes; $S$ is the total adsorption; $Pe$ is the Péclet number, which is a dimensionless number designating the ratio between the convection rate and the diffusion rate; and $R$ is the retardation factor, reflecting the characteristics of retardation nanoparticles exhibit in migrating through the porous medium.

3. Analysis of Experimental Results

3.1. BTC of nZnO Particles under Varying Osmotic Pressures. Figure 3 shows the breakthrough curve of nZnO particles at varying pressures. The parameters of the BTC are shown in Table 5.

When the pressure rises from 0.1 MPa to 0.5 MPa, the critical PV rises from 7.5 to 9.8. As pressure increases, the maximum equilibrium concentration $C_{\text{max}}$ declines, and the interception ratio increases. When the osmotic pressure rises from 0.1 MPa to 0.5 MPa, the maximum equilibrium concentration $C_{\text{max}}$ drops from 40.04 mg/L to 20.145 mg/L. At the same time, the total rejection rate of nZnO particles in GCLs increases from 48.21% to 82.04%. In the experiments, the interception ratio was 82.04% under an osmotic pressure of 0.5 MPa, meaning that a substantial quantity of nZnO particles deposited in GCLs, with only 17.96% of the particles migrating from GCLs and only 0.18% of the particles migrating out of the GCLs. Both the maximum equilibrium concentration $C_{\text{max}}$ and interception ratio of nZnO particles under varying osmotic pressures indicated that the migration properties of nZnO particles in GCLs weakened when osmotic pressure increased.

3.2. Effect of Varying Osmotic Pressure on Transportation Parameters

3.2.1. Effect of Osmotic Pressure on the Stability of nZnO Suspension. The test results of the particles size and zeta potential of the nZnO particle suspensions under different osmotic pressures are shown in Figure 4. The results indicated that pressure can cause nZnO particles to grow in size and agglomerate and reduce the scattering stability of the nZnO suspension. The test results revealed that when the osmotic pressure rose from 0.1 MPa to 0.5 MPa, the zeta potential of the nZnO suspension rose from $-38.6 \text{ mV}$ to $-34.2 \text{ mV}$ and the size of nZnO particles increased by 5.8% from 317.1 nm to 335.5 nm.

3.2.2. Effect of Osmotic Pressure on the Microstructure and Infiltration Properties of GCLs. Under pressure changes, the porosity ratios of GCLs change accordingly. This study performed a compression test on the GCLs to obtain a compression curve (Figure 5). When the pressure rose from 0.1 MPa to 0.5 MPa, the GCLs porosity ratio decreased from 7.9 to 2.1. Specifically, at the initial stage of pressure application (0.05–0.20 MPa), the extent of change in the porosity ratio was relatively small because the pressure exerted relatively little force on the internal structure of GCLs. When the pressure increased from 0.2 MPa to 0.35 MPa, relatively high pressure accelerated the GCLs porosity change rate, causing the porosity ratio to decrease by 62.5% (i.e., from 6.4 to 2.4), the pressure had a relatively
large effect on the internal structure of GCLs. Finally, because the consolidation effect in the preceding stages had fully compressed the GCLs, changes in the GCLs porosity ratio were inconspicuous in the last stage of compression (0.35–0.5 MPa), and the porosity ratio remained between 2.0 and 2.4. Therefore, osmotic pressure exerted notable effects on GCLs microstructure.

The GCLs infiltration coefficients under varying pressures were tested using the infiltration test (Figure 6). The test results indicated that, with continual increases in osmotic pressure, GCLs infiltration coefficients continually decreased. When the osmotic pressure reached 0.35 MPa, the extent of change in infiltration coefficients was reduced.

The effect of pressure on the migration performance of nZnO particles in GCLs has a certain effect. The migration performance of nZnO particles deteriorates as the pressure increases. This is mainly due to the fact that nZnO particles tend to agglomerate in suspension as the pressure increases, and the nZnO particle size becomes larger, which is not conducive to its migration in porous media. In addition, pressure affects the microstructure of GCLs. Pressure causes the GCLs pores to decrease and the permeability to decrease. The retention of nZnO particles by GCLs is enhanced.

### 3.3. Mechanism of Effect of Osmotic Pressure on nZnO Particle Migration in GCLs

The two-site model was used to fit the breakthrough curves of nZnO particles in GCLs under different osmotic pressures. The results of the simulation are shown in Figure 7. The coincidence between the fitting curve and the measured data is good. When the pressure was lower

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| Osmotic pressure (MPa) | Critical PV | $C_{\text{max}}$ (mg/L) | Total rejection rate (%) | Desorption rate/reversible rejection rate (%) |
|------------------------|-------------|------------------------|-------------------------|-----------------------------------------------|
| 0.1                    | 7.5         | 40.04                  | 48.21                   | 3.91                                          |
| 0.2                    | 7.8         | 40.515                 | 57.00                   | 2.78                                          |
| 0.3                    | 8.3         | 30.095                 | 65.48                   | 1.89                                          |
| 0.4                    | 8.4         | 30.54                  | 75.38                   | 0.84                                          |
| 0.5                    | 9.8         | 20.145                 | 82.04                   | 0.18                                          |

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**Figure 4:** (a) Zeta potential of nZnO suspension and (b) particle size of nZnO particles under different osmotic pressures.

**Figure 5:** GCLs compression curve.
Figure 6: GCLs permeability coefficient under different osmotic pressures.

Figure 7: Continued.
than 0.3 MPa, the infiltration coefficients and void ratio of GCLs decrease quickly with increase of pressure. So, in the first 5 PV, the coincidence between the fitting curve and the measured data is relatively low. This indicates that the two-site model can describe the migration process very well. In addition, the coefficient of correlation ($R^2$) also notes that the two-site model has a better fitting effectiveness for the migration process, as shown in Table 6, $R^2$ are all above 0.945. Of the four dimensionless parameters, pressure had relatively large influences on the $P_e$, $R$, and $\omega$. Specifically, $P_e$ dropped when pressure rose, which indicated that the convection effect of nZnO particles weakened in the GCLs. $R$ was positively correlated with pressure. Greater values of $R$ indicated that the nanoparticles encountered greater retardation when nanoparticles migrated in the porous medium. Therefore, the retardation effect of GCLs on nZnO particles became increasingly conspicuous as pressure increased.

3.4. Maximum Migration Distance of Nanoparticles. The maximum migration distance ($L_{\text{max}}$) of nanoparticles in porous media is defined as the migration distance when 99% of nanoparticles (i.e., $C/C_0 = 0.01$) are trapped. The two-site model can accurately describe the migration process of nZnO particles in GCLs. Therefore, we adopted the two-site model to simulate the relationship between $C/C_0$ of nZnO particles and the migration distance ($z$) in GCLs under different experimental conditions by the CXTFIT module of the STANMOD software and to acquire the $L_{\text{max}}$. The results of the simulation are shown in Figure 8. From the simulation results, the correlativity between $L_{\text{max}}$ and osmotic pressure is negative. It is also proved that the migration properties of nZnO particles in GCLs drop down with the osmotic pressure increasing.

| Osmotic pressure (MPa) | $P_e$   | $R$    | $\beta$ | $\omega$ | $R^2$ |
|------------------------|--------|--------|--------|--------|-------|
| 0.1                    | 251.2448 | 61.9311 | 0.4014 | 0.0632 | 0.988 |
| 0.2                    | 229.2961 | 128.8189 | 0.3910 | 0.0981 | 0.988 |
| 0.3                    | 69.3585 | 170.7667 | 0.3244 | 0.5214 | 0.979 |
| 0.4                    | 62.3821 | 385.2743 | 0.3065 | 1.1122 | 0.977 |
| 0.5                    | 36.7632 | 501.5935 | 0.3874 | 2.3723 | 0.945 |

![Figure 8: Migration distance simulation results.](image)

4. Conclusion

Along with increasing pressure, the zeta potential among nZnO particles decreased, the maximum energy barrier...
(Φ_{\text{max}}) reduced gradually, the agglomeration properties of nZnO strengthened, and the tension-induced interception of nZnO particles in GCLs increased.

Along with increasing pressure, GCLs pores were compressed, the infiltration coefficient of GCLs reduced, and the interception effect of GCLs on nZnO particles strengthened.

The two-site model can accurately describe the migration process of nZnO particles in GCLs. The migration properties of nZnO particles in GCLs drop down with the osmotic pressure increasing.

The correlation between \( L_{\text{max}} \) and osmotic pressure is negative. It is also proved that the migration properties of nZnO particles in GCLs drop down with the osmotic pressure increasing.

Because of the complex environmental conditions of landfills, the actual conditions of such sites could not be accurately simulated in this study. However, the aforementioned results can serve as a reference for future research on the migration behaviors and mechanisms of nanoparticles in landfills.

**Data Availability**

The data used to support the findings of this study are included within the article.

**Conflicts of Interest**

The authors declare that they have no conflicts of interest.

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**References**

[1] M. F. Peterson, “Progress in preparation and application of one-dimensional nano zinc oxide,” *Journal of Materials Engineering*, vol. 43, no. 2, pp. 103–112, 2013.

[2] P. Sun, A. Shijirbaatar, J. Fang, G. Owens, D. Lin, and K. Zhang, “Distinguishable transport behavior of zinc oxide nanoparticles in silica sand and soil columns,” *Science of the Total Environment*, vol. 505, pp. 189–198, 2015.

[3] D. Collins, T. Luxton, N. Kumar, S. Shah, V. K. Walker, and V. Shah, “Assessing the impact of copper and zinc oxide nanoparticles on soil: a field study,” *Plos One*, vol. 7, no. 8, p. e42663, 2012.

[4] H. A. Jeng and J. Swanson, “Toxicity of metal oxide nanoparticles in mammalian cells,” *Journal of Environmental Science and Health Part A Toxic/hazardous Substances and Environmental Engineering*, vol. 41, no. 12, pp. 2699–2711, 2006.

[5] A. Gojova, B. Guo, R. S. Kota, J. C. Rutledge, I. M. Kennedy, and A. I. Barakat, “Induction of inflammation in vascular endothelial cells by metal oxide nanoparticles: effect of particle composition,” *Environmental Health Perspectives*, vol. 115, no. 3, pp. 403–409, 2007.

[6] W. Lin, Y. Xu, C.-C. Huang et al., “Toxicity of nano- and micro-sized ZnO particles in human lung epithelial cells,” *Journal of Nanoparticle Research*, vol. 11, no. 1, pp. 25–39, 2009.

[7] X. Deng, Q. Luan, W. Chen et al., “Nanosized zinc oxide particles induce neural stem cell apoptosis,” *Nanotechnology*, vol. 20, no. 11, article 115101, 2009.

[8] D. Wang, M. Paradela, S. A. Bradford et al., “Facilitated transport of Cu with hydroxyapatite nanoparticles in saturated sand: effects of solution ionic strength and composition,” *Water Research*, vol. 45, no. 18, pp. 5905–5915, 2011.

[9] G. S. Yazici, B. Alan, E. Adar, and M. S. Bilgili, “The impact of nanoparticles on aerobic degradation of municipal solid waste,” *Waste Management and Research*, vol. 35, no. 4, pp. 426–436, 2017.

[10] S. C. Bolyard, D. R. Reinhart, and S. Santra, “Behavior of engineered nanoparticles in landfill leachate,” *Environmental Science and Technology*, vol. 47, no. 15, pp. 8114, 2013.

[11] I. A. Khan, N. D. Berge, T. Sabo-Attwood, P. Lee Ferguson, and N. B. Saleh, “Single-walled carbon nanotube transport in representative municipal solid waste landfill conditions,” *Environmental Science and Technology*, vol. 47, no. 15, pp. 8425–433, 2013.

[12] Y. Zhang, P. Yang, and S. Xue, “Researching advances in transportation of nanomaterial contaminants in soil,” *Environmental Engineering*, vol. 3, pp. 88–91, 2015, in Chinese.

[13] X. Liu, D. M. O’Carroll, E. J. Petersen, Q. Huang, and C. L. Anderson, “Mobility of multiwalled carbon nanotubes in porous media,” *Environmental Science & Technology*, vol. 43, no. 21, pp. 8153–8158, 2009.

[14] N. T. Mattison, D. M. O’Carroll, R. K. Rowe, and E. J. Petersen, “Impact of porous media grain size on the transport of multi-walled carbon nanotubes,” *Environmental Science and Technology*, vol. 45, no. 22, pp. 9765–9775, 2011.

[15] Y. Liang, S. A. Bradford, J. Simunek, H. Vereecken, and N. B. Saleh, “Single-walled carbon nanotube transport in representative municipal solid waste landfill conditions,” *Environmental Science and Technology*, vol. 47, no. 15, pp. 8425–433, 2013.

[16] K. Wang, J. Liu, L. Liu, and D. Sun, “Biocompatibility of graphene oxide,” *Nanoscale Research Letters*, vol. 6, no. 1, pp. 1–8, 2011.

[17] D. Bouchard, W. Zhang, and X. Chang, “A rapid screening technique for estimating nanoparticle transport in porous media,” *Water Research*, vol. 47, no. 12, p. 4086, 2013.

[18] I. G. Godinez and C. J. Darnault, “Aggregation and transport of nano-TiO2 in saturated porous media: effects of pH, surfactants and flow velocity,” *Environmental Science & Technology*, vol. 45, no. 2, pp. 839–851, 2011.

[19] D. H. Lin, X. Tian, F. Wu, and B. Xing, “Fate and transport of nanomaterial contaminants in saturated porous media,” *Water Research*, vol. 47, no. 7, pp. 2572–2582, 2013.

[20] A. Braun, E. Klumpp, R. Azzam, and C. Neukum, “Transport and deposition of stabilized engineered silver nanoparticles in water saturated loamy sand and silty loam,” *Science of the Total Environment*, vol. 535, p. 102, 2015.
[22] D. Wang, C. Su, W. Zhang et al., "Laboratory assessment of the mobility of water-dispersed engineered nanoparticles in a red soil (Ultisol)," *Journal of Hydrology*, vol. 519, pp. 1677–1687, 2014.

[23] S. P. Kulizhskiy, S. V. Loiko, Y. N. Morgalev, G. I. Istigechev, A. V. Rodikova, and T. A. Maron, "Investigation of platinum and nickel nanoparticles migration and accumulation in soils within the South eastern part of West Siberia," *Nano Hybrids and Composites*, vol. 13, pp. 115–122, 2017.

[24] W. Zhang. *Experimental and Numerical Study on Water/Leachate Transport in Landfill of Municipal Solid Waste*. D., Zhejiang University, Hangzhou, China, 2007, in Chinese.

[25] J. Liu and X. J. Kong, "Seismic stability and permanent displacement analysis of a solid waste landfill slope containing geomembrane," *Rock and Soil Mechanics*, vol. 25, no. 5, pp. 778–782, 2004.

[26] G. K. Wang and Y. X. Yang, "Infection of different ultra audible frequency and temperature to dispersive property of ZnO nanometre granule," *Sichuan Textile Technology*, 2005, in Chinese.

[27] M. Th. van Genuchten and R. J. Wagenet, "Two-site/two-region models for pesticide transport and degradation: theoretical development and analytical solutions," *Soil Science Society of America Journal*, vol. 53, no. 5, pp. 1303–1310, 1989.
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