Growth and remodeling play opposing roles during postnatal human heart valve development

Pim J. A. Oomen1,2,3, Maria A. Holland3,4, Carlijn V. C. Bouten1,2, Ellen Kuhl3,5 & Sandra Loerakker1,2,3

Tissue growth and remodeling are known to govern mechanical homeostasis in biological tissue, but their relative contributions to homeostasis remain unclear. Here, we use mechanical models, fueled by experimental findings, to demonstrate that growth and remodeling have different effects on heart valve stretch homeostasis during physiological postnatal development. Two developmental stages were considered: early-stage (from infant to adolescent) and late-stage (from adolescent to adult) development. Our models indicated that growth and remodeling play opposing roles in preserving tissue stretch and with time. During early-stage development, excessive tissue stretch was decreased by tissue growth and increased by remodeling. In contrast, during late-stage development tissue stretch was decreased by remodeling and increased by growth. Our findings contribute to an improved understanding of native heart valve adaptation throughout life, and are highly relevant for the development of tissue-engineered heart valves.

Scientists have been intrigued for many centuries by the intrinsic capability of biological tissues to actively change their form and properties. While these changes are most prominent during embryonic development, most living tissues are in a continuous state of adaptation. Since the time of Galileo Galilei, it has been believed that these changes are strongly influenced by mechanical factors. Now, almost four centuries later, functional tissue adaptation, and its relation with mechanics, is still only partially understood. From a biomechanical perspective, it is well accepted that growth (here defined as mass or volume change), and remodeling (here defined as property change) occur at least partly in response to changes in the tissue's mechanical environment, in order to maintain a homeostasis. Different mechanical constituents have been proposed to determine mechanical homeostasis across different tissue types, including stress, strain, and strain energy density.

By investigating the postnatal development of native heart valves, we can increase our understanding of how growth and remodeling maintain mechanical homeostasis in heart valves throughout life. During physiological development, the environment of the aortic and pulmonary heart valves, i.e. the annulus radius and blood pressure, changes significantly. As a response to these changes, tissue growth and remodeling are believed to occur to maintain mechanical homeostasis. Tissue growth occurs through production of new extra-cellular matrix (ECM), which leads to changes in leaflet length, area, and thickness. Tissue remodeling, on the other hand, has been observed through a change in ECM structure and composition. The most interesting changes in the ECM properties, from a biomechanical perspective, occur in the leaflets' collagen architecture, which is the main determinant of the mechanical behavior of heart valves. The collagen network matures with age, represented by thicker collagen fiber bundles and increasing cross-link density. As a result of the remodeling of the collagen network, the stiffness of the leaflets generally increases with age.

Recent research from our group on postnatal human native heart valves has shown relatively small differences in tissue stretch during development, and between aortic and pulmonary valves, thereby suggesting that tissue adaptation in this particular tissue occurs to maintain a stretch-driven homeostasis. However, the relative roles of growth and remodeling in maintaining stretch homeostasis are still unclear. An improved knowledge of these...
roles is pivotal to understand the functioning of heart valves during health and disease, as adverse growth and remodeling can lead to valvular pathologies\cite{11,12,29,30}. Moreover, growth and remodeling are of key importance for the emerging field of heart valve tissue engineering, which aims to create living heart valves that have the capability to grow and remodel after implantation\cite{31–36}.

During postnatal valvular development, growth and remodeling occur simultaneously\cite{18}, which makes it challenging to experimentally deduce their relative contributions to maintaining mechanical stretch homeostasis. Therefore, numerical models can be particularly useful to study their relative roles. The past two decades, two major approaches have been used to model growth and remodeling in collagenous tissues: constrained mixture models\cite{37} and kinematic growth models\cite{5,38,39}. Constrained mixture models may provide the more physiological representation of growth and remodeling. However, their parameters are hard to derive from experimental data, as they are based on the turnover of ECM components. Kinematic growth models, on the other hand, consider growth as isotropic or anisotropic volumetric changes, typically driven by a certain mechanical stimulus to reach a homeostatic target. In addition, when experimental data is available, kinematic growth could be defined in terms of known geometrical changes, rather than being driven by a mechanical stimulus. This approach only allows for prescribing homogeneous growth, as it is based on the overall geometrical changes, and is therefore not capable of releasing local stress concentrations.

The goal of the current study was to use a numerical model fueled by experimental data to elucidate the relative roles of tissue growth and remodeling in preserving the mechanical stretch homeostasis during physiological valvular development. In these mechanical models, growth was implemented via changes in leaflet area and thickness according to finite growth theory, and microstructural remodeling via prescribing changes in the material properties. Our mechanical model was informed by hemodynamic, geometric, mechanical, and structural data of paired aortic and pulmonary human native heart valves from infant to adult origin\cite{14,18–21}. We used a generic approach to divide age-dependent hemodynamic, geometric and structural data for aortic and pulmonary valves to three groups: infant, adolescent and adult (Fig. 1a). Between these three groups, two developmental stages were addressed: early-stage development, from infant to adolescent, and late-stage development, from adolescent to adult. During these stages, the independent influences of growth and remodeling on leaflet stretch and valve function were studied. Moreover, we systematically studied the effects of growth and remodeling on the temporal evolution of the elastic stretches during development. To this end, we varied the initial rates of growth and remodeling relative to the environmental changes and each other, and studied their influences on the temporal evolution of the elastic stretch. With this framework we show that growth and remodeling appear to play opposing roles in terms of preserving stretch homeostasis during the development of heart valves.

**Results**

**Temporal changes occur in and around the human native heart valve during development.** The hemodynamic, geometric and structural properties of 24 previously analyzed paired aortic (n = 12) and pulmonary (n = 12) human native heart valves\cite{14,18} were assigned to three age groups: infant (n = 6, average age 0.9 ± 0.6 yr), adolescent (n = 8, average age 19.5 ± 1.4 yr) and adult (n = 10, average age 46 ± 3.0 yr) (Fig. 1a). Several changes were considered between the age groups. In the valves’ environment, the aortic diastolic pressure increased with age (Fig. 1b), and the annulus radius increased significantly during early development (p < 0.01 within each age group (Fig. 1c)).

**Age-dependent changes in human heart valves.** (a) A timeline of experimental data of 24 paired human aortic and pulmonary heart valves (where each horizontal bar represents the age of one pair) were assigned to three age groups: infant, adolescent and adult (where the red dashed bars indicate the average age of each group). The age-dependent data informed the generation of a finite element model for each group. Temporal changes were considered in diastolic blood pressure\cite{19–21} (b), annulus radius (c), leaflet thickness (d), circumferential (e) and radial (f) leaflet length, and aspect ratio between the circumferential and radial length (g)\cite{14,18}. Significant differences (p < 0.05) of geometrical measurements (c–g) between groups are indicated by paired symbols.
for aortic and \( p < 0.05 \) for pulmonary) and only slightly during late development (Fig. 1c). Within the valves themselves, aortic leaflet thickness increased significantly \( (p < 0.01) \) during early-stage development, followed by a significant \( (p < 0.05) \) decrease during late-stage development (Fig. 1d). The adolescent \( (p < 0.001) \) and adult \( (p < 0.01) \) aortic valves were thicker than their pulmonary counterparts. The circumferential and radial leaflet length increased with age (Fig. 1e,f), while no significant differences were found between the aortic and pulmonary leaflet lengths. Finally, no significant differences were found in the circumferential-radial length ratio with age and between the two valve types (Fig. 1g).

To estimate the mechanical behavior of the different age groups, a set of material parameters was determined for each age group by fitting a fiber-reinforced hyperelastic constitutive model to the group’s individual stress-stretch responses (Fig. 2). According to the stress-stretch curves, aortic leaflet stiffness decreased during early development (Fig. 3a), followed by an increase during late development (Fig. 3b). The pulmonary leaflets were more compliant than their aortic counterparts, but featured the same temporal evolution (Fig. 3c,d).

The mechanical properties, alongside the other age-dependent data (Fig. 1), were used to generate a finite element model of each valve group in order to simulate the average mechanical state of heart valves at valve closure during diastole. The elastic stretch in the center of the belly region in the circumferential direction, which coincides with the main collagen orientation, was similar between the aortic and pulmonary valves for all age groups, and between infant and adult valves (Fig. 4a). Of note, stretch in the adolescent valves was slightly higher than in the other age groups. In contrast, the circumferential Cauchy stress in the belly region was considerably higher in the aortic valves than in the pulmonary valves, and continuously increased with age (Fig. 4b). These findings comply with our previous observations in individual valves.

**During early-stage development growth reduces stretch, whereas remodeling increases stretch.** Physiological valve development from the infant to the adolescent, and from the adolescent to the adult valve, was simulated by applying environmental changes (annulus radius and diastolic blood pressure) to the infant and adolescent models. With these simulations, the combined and individual influences of growth (change in leaflet length and thickness according to Fig. 1d–f) and microstructural remodeling (change in mechanical properties according to Fig. 3) after development on leaflet stretch were estimated.

Growth and/or remodeling during early-stage development had a similar effect on tissue stretch in both the aortic and pulmonary valve, despite their different mechanical, geometric and environmental properties (Figs 5a and 6). Tissue growth alone reduced circumferential stretch after early-stage development towards homeostatic values. In contrast, with remodeling alone, or without growth and remodeling altogether, the stretches after early-stage development were extremely high. Interestingly, the combination of growth and remodeling also prevented excessive stretches, although the stretches were larger compared to applying growth alone, and to the initial state. The latter result coincides with the elevated stretch that we found in the adolescent valve (Fig. 4a). Incomplete valve closure was observed without leaflet growth, while remodeling was not observed to significantly influence valve closure (Fig. 5a).

**During late-stage development remodeling reduces stretch, whereas growth increases stretch.** Similar to early-stage development, growth and/or remodeling during late-stage development had comparable effects on leaflet stretch between the aortic and pulmonary valve (Figs 5b and 6). Interestingly, during
this stage the effects of growth and remodeling on tissue stretch were opposite compared to early development: remodeling alone reduced the circumferential stretch, while growth alone increased tissue stretch. When growth and remodeling were combined, the stretch was reduced compared to the initial state, which coincides with the lower stretch that we found in the adult valve compared to the adolescent valve (Fig. 4a). Incomplete valve closure was only observed in this stage in the pulmonary valve when no growth was applied (Fig. 5b).

Leaflet volume changes primarily during early development. During both early and late-stage development, leaflet area was found to increase with age, while thickness increased during early-stage development and decreased during late development (Fig. 1d–f). As a consequence, the total leaflet volume of the models increased dramatically during early-stage development for both valves (Fig. 7), whereas stabilization of leaflet volume was observed during late-stage development. This suggests that the changes in leaflet geometry during late-stage development are rather due to tissue dilation than to growth.

Importance of growth and remodeling kinetics. The model was used to systematically study the effects of growth and remodeling on the temporal evolution of the elastic stretches during development. To this end, we varied the initial rates of growth and remodeling relative to the environmental changes and each other, and studied their influences on the temporal evolution of the elastic stretch. Rate change parameters were introduced for both growth ($k_g$) and remodeling ($k_r$), which governed their initial rate change relative to the environmental changes. Overall, the aortic and pulmonary valves showed similar temporal trends in terms of stretch, so for the sake of brevity only the results for the aortic valve are shown (Fig. 8).

During early development, the stretch increased more or less linearly when growth and remodeling occurred at the same rate as the environmental changes (Fig. 8a–c). The changes in growth rate affected leaflet stretch most at the beginning of the developmental time, with a slower relative growth rate ($k_g > 0$) leading to increased intermediate stretches, observed at the halfway point of early development (Fig. 8b). In contrast, the changes in remodeling rate had the largest effect at the end of the development, with a faster rate ($k_r < 0$) leading to higher intermediate stretches (Fig. 8c). Accordingly, when both rates were changed simultaneously, growth was most influential at the beginning, and remodeling at the end of development (Fig. 8d), with a transition taking place halfway. When growth initially occurred slower than the environmental changes, no full valve closure was observed halfway the developmental time.

Interestingly, during late-stage development, the stretch decreased in an exponential decay fashion when growth and remodeling occurred with the same rate as the environmental changes (Fig. 8d–f). The effect of
Figure 4. Evolution of stretch and stress with age. Age-dependent simulations indicated that the circumferential (circ.) stretch was similar with age and between the aortic and pulmonary valves (a), whereas the circumferential Cauchy stress was higher in the aortic valve than in the pulmonary valve and increased continuously with age (b).

Figure 5. The influence of growth and/or remodeling on circumferential leaflet stretch and valve closure. Valve closure during diastole was simulated for early-stage (a) and late-stage (b) development of aortic and pulmonary heart valves and tissue stretch was assessed after applying growth and remodeling either combined or alone. Circumferential elastic leaflet stretches after growth and/or remodeling were similar in the aortic and pulmonary valves, with stretches in the early-stage valves without growth higher than 1.6. Insufficient valve closure was observed without growth after early-stage development of the aortic and pulmonary valves, and pulmonary late-stage development.
different growth rates on the temporal change in stretch was negligible (Fig. 8d–e), while a relatively fast remodeling rate ($k_r < 0$) led to a fast decrease in intermediate stretches (Fig. 8d,f). Full valve closure was observed at all times.

Discussion
Growth and remodeling are widely believed to occur to maintain a certain mechanical homeostasis\textsuperscript{2–6}, with recent evidence indicating that in native heart valves this homeostasis is determined by tissue stretch\textsuperscript{14}. In this study, we used mechanical models that were informed by experimental data to elucidate the relative roles of growth and remodeling on the preservation of tissue stretch in aortic and pulmonary human native heart valves during physiological development.

Growth and remodeling have opposing effects on valve tissue stretch and with age. Our results indicate that growth and remodeling play opposing roles in preserving tissue stretch and with time. During early-stage development, growth preserved tissue stretch, whereas remodeling led to an increase in stretch (Figs 5a and 6). These effects occurred more rapidly when the initial growth and remodeling rates were increased (Fig. 8a,b). The decrease in tissue stretch via growth can be explained by the increase in both leaflet area and thickness (Fig. 1e,f). The increase in stretch via remodeling can be explained by the tissue softening that occurred during early-stage development (Fig. 3a,c). Changes in the material stiffness of heart valves by remodeling have previously been correlated with collagen cross-link formation\textsuperscript{18,27}. Collagen cross-link formation is a much slower process than tissue growth, and cannot occur while ECM is being produced\textsuperscript{27}. Therefore, we hypothesize that the tissue softening that was observed during early-stage development is a repercussion of growth, as an increase in tissue stiffness via remodeling may be impossible while ECM is still being produced.
In contrast to early-stage development, the influences of growth and remodeling on stretch appeared to be reversed during late-stage development. Our results indicate that during late-stage development, leaflet stretch is decreased by remodeling, and increased via geometrical changes (Figs 5b and 6). Interestingly, the geometrical changes that occurred during this stage (Fig. 1d–f) did not result in a clear change in volume. Therefore, it can be concluded that valvular tissue growth, which we defined as change in volume, primarily occurs during early-stage development, with tissue dilation, rather than growth, occurring during late-stage development. Leaflet thinning due to dilation appears to be mostly responsible for the large deformations that were observed after late-stage development with only growth, in both the aortic and pulmonary valve. These deformations cannot be solely caused by the increase in pressure, since the diastolic pressure only increases for aortic valve, whereas it remains constant for the pulmonary valve throughout development.

Since no active growth took place during late-stage development, tissue remodeling is more likely to occur via cross-link formation. This could be responsible for tissue stiffening (Fig. 3b,d) and thus counteracts the increase in leaflet stretch that occurs via dilation, associated with the decrease in leaflet thickness. Aside from cross-link formation, leaflet calcification and collagen fiber alignment could have contributed to leaflet stiffening with aging. Calcification occurs gradually with age in most valves, and increases local stiffness during late-stage development40. Collagen fiber alignment was previously found to increase during late development14 for both aortic and pulmonary valves, which coincides with the increased circumferential stiffness that was found in the same valves.

Volumetric changes with age can be explained by mechanical stimuli. The presence of active growth during early-stage development, and its absence during late-stage development, can be explained by the influence of mechanical stimuli on valvular interstitial cells, which are responsible for leaflet growth and remodeling. In previous in vitro studies, it was shown that valvular interstitial cells become activated upon mechanical stimulation41,42, resulting in a myofibroblast-like phenotype that is associated with ECM production22,43. Clearly, larger overall changes in mechanical stimuli are provided via environmental changes during early-stage in comparison with late-stage development (Fig. 1b,c). These changes in mechanical stimuli activate the valvular cells and thus explains why in our study leaflet growth was only observed during early development. Leaflet dilation during late-stage development would then be a passive process. During the latter stage, the cells remain quiescent due to less prominent changes in mechanical stimuli, since the environmental changes are much smaller compared to early development.

In a physiological situation, changes in mechanical stimuli are primarily present during early-stage development. At an older age, cells can still become activated when mechanically stimulated by pathologies, as observed in dilated cardiomyopathy, where the ventricle and mitral valve annular radius are enlarged and cause increased...
leaflet stretch. It has been demonstrated in adult human patients and animal models that this pathology results in significantly enlarged mitral leaflets, and that interstitial cells are activated, which is in a physiological situation only the case during early development. The occurrence of leaflet growth during cardiomyopathy suggests that growth can occur regardless of age, provided that the valvular interstitial cells are presented with changes in mechanical stimuli.

**Growth and remodeling feature similar temporal trends but different magnitudes in the aortic and pulmonary valves.** It is interesting to note that the aortic and pulmonary valve operate under completely different mechanical circumstances, since the aortic diastolic pressure, leaflet thickness, and leaflet stiffness are much higher than the pulmonary pressure. Still, the same homeostatic stretches (Fig. 4) and temporal effects of growth and remodeling on preserving stretch (Figs 5 and 6) were found for both valve types. Growth and remodeling appeared to occur proportionally to the environmental changes, with higher magnitudes in the aortic than in the pulmonary valves. More growth occurred in the aortic valve (Fig. 7), mainly characterized by a larger increase in thickness (Fig. 1d). The stiffness, modulated by remodeling, of the aortic valves was also higher than in their pulmonary counterparts (Fig. 3). This further supports the hypothesis that growth and remodeling occur to maintain a stretch homeostasis, for more growth and remodeling are required in the aortic valve to counteract the increasing aortic diastolic pressure, and thus to establish the same stretches as in the pulmonary valve.

**Limitations of the mechanical model.** The current model features three main limitations. First, although the experimental foundation of the model is a great advantage, we were limited by data availability. We could now only consider developmental stages of rather large time spans of at least 18 years. Particularly, the temporal step between the infant and adolescent groups was relatively large, since extensive somatic changes take place during this transition. An intermediate group of around 12 years old would have been desirable, but no experimental data were available around this age.

Second, we did not implement prestretch, which is known to significantly influence tissue mechanics. To the best of our knowledge, the only data on aortic and pulmonary valve prestretch has recently been obtained from valves of elderly patients (average age 63 yr) who underwent heart transplantation. We used these novel findings in the generation of the leaflet geometry to ensure an appropriate circumferential-radial leaflet length ratio of 2 according to Fig. 1g. Yet, since it is still unknown if and how prestretch evolves with age, no actual tissue prestretch was implemented in the age-dependent growth and remodeling simulations.

Third, the growth and remodeling that we applied in the numerical model was different to traditional approaches, where tissue growth not only occurs to reach a mechanical homeostasis, but also to release any local stress and/or strain concentrations. Due to the global manner in which growth and remodeling were applied in our model, local artifacts in the stress and strain fields may have arisen.

**Conclusion.** Our mechanical model, that was informed by experimental data, indicates that growth and remodeling play opposing roles in preserving tissue stretch and with time. During early-stage development, growth preserves tissue stretch, while remodeling leads to an increase in stretch, which we hypothesize is caused by tissue softening as a repercussion of growth. In contrast, the influences of growth and remodeling on stretch appeared to be reversed during late-stage development. During this stage, leaflet stretch was decreased by remodeling, and increased by volume changes that we now identified as dilation, rather than growth. The obtained understanding of the distinct roles of valvular growth and remodeling is pivotal for improving the knowledge of the functioning of native heart valves during health and disease. This is highly relevant for understanding pathologies like valvular stenosis and dilated cardiomyopathy, but also for heart valve tissue engineering, which aims to create heart valves that have the capability to grow and remodel after implantation.

**Methods**

**Age-dependent data from human native heart valves.** The mechanical models were informed by age-related properties that were obtained from healthy paired aortic and pulmonary native human heart valves (n = 24) that we analyzed previously. The valves were obtained from postmortem donors from mixed gender, whose cause of death was not related to valvular disease or conditions known to precede valvular disease. These valves were mechanically and structurally uneffected, but were deemed unfit for implantations due to findings that contra-indicated implantation, for instance: positive bacteriological sampling, serological findings in the generation of the leaflet geometry to ensure an appropriate circumferential-radial leaflet length ratio of 2 according to Fig. 1g. Yet, since it is still unknown if and how prestretch evolves with age, no actual tissue prestretch was implemented in the age-dependent growth and remodeling simulations.

To accommodate the biological variability between individual valves, the valves were assigned to three generic age groups: infant (n = 6, average age 0.9 ± 0.6 yr), adolescent (n = 8, average age 19.5 ± 1.4 yr) and adult (n = 10, average age 46 ± 3.0 yr). In between these groups two developmental stages were considered for both the aortic and pulmonary valve: early-stage development, from infant to adolescent, and late-stage development, from adolescent to adult (Fig. 1a). For each group, the average and standard deviation of the circumferential leaflet length L_c, radial leaflet length L_r, leaflet thickness t, and diastolic blood pressure (obtained from the literature) were determined.

The data are presented as mean ± the standard error of the mean. Statistical differences between age groups and aortic and pulmonary valves were tested with two-way ANOVA, followed by Bonferroni post-hoc testing. GraphPad Prism (GraphPad Software, Inc., USA) was used for the analysis.

**Mechanical model of physiological heart valve development.** Finite element models were generated for each age group and valve type based on the age-dependent leaflet dimensions in Abaqus FEA (Dassault Systèmes, Simulia Corp., Providence, RI). Only one leaflet was modeled due to symmetry. The contact between the leaflets was modeled by adding two contact surfaces directly adjacent to the ventricular side of the leaflet,
parallel to the two free edges (Fig. 8). As all leaflets were assumed to deform similarly, there cannot be any slip between adjacent leaflets. Therefore, the contact was set to be frictionless.

Although we previously generated leaflet geometries based on the lower half of a spherical surface\textsuperscript{49}, in the current study a spheroid surface with age-dependent thickness $t$ was used to ensure an appropriate circumferential-radial length ratio $L_c/L_r$. The ratio $L_c/L_r \approx 2.0$ that we found for all valves (Fig. 1e–g) was measured \textit{ex vivo} in excised leaflets, while it has recently been found in elderly patients who underwent heart transplantation that aortic heart valve leaflets are radially prestretched by 1.31 \textit{in vivo}, with no evidence of circumferential prestretch\textsuperscript{48}. Therefore, the \textit{in vivo} leaflet length ratio should be $L_c/L_r \approx 2.0/1.31 \approx 1.53$. To ensure this, the major axis of the spheroid coincided with the annular radius and was equal to half the leaflet circumferential length, and the minor principal axis length was set such that the resulting radial leaflet length (equal to a quarter of the ellipsoid minor circumference) was 1/1.53 times the circumferential length (Fig. 9).

Valvular development was simulated by first of all changing the environmental properties, i.e. annular radius and diastolic blood pressure. The former was implemented via displacement boundary conditions on the leaflet nodes at the annulus, and the latter via a change in the hydrostatic pressure that was applied to the arterial side of the leaflets (Fig. 9). Growth and remodeling were implemented and applied either combined or separately during the developmental changes, in order to assess their relative effects on preserving the leaflet stretch.

**Growth via geometrical changes.** Growth was modeled as a change in volume. This was achieved kinematically according to the theory of finite growth, where the total deformation gradient tensor $F$ was decomposed into an elastic contribution $F_e$ and a growth contribution $F_g$.

$$ F = F_e \cdot F_g $$

Similarly, the overall volume change $J = \det(F) = J_e J_g$ was decomposed into a growth $J_g = \det(F_g)$ and elastic change $J_e = \det(F_e)$. The so-called growth tensor $F_g$ was defined in terms of changes in circumferential leaflet length $L_c$, radial leaflet length $L_r$, and leaflet thickness $t$. Since the ratio between \textit{ex vivo} circumferential and radial leaflet length remained constant during development (Fig. 1g), the relative change in circumferential $(L_c + \Delta L_c)/L_c$ and radial leaflet length $(L_r + \Delta L_r)/L_r$ were similar, thus defining an isotropic leaflet area change$^{46}$ $\vartheta = (L_c + \Delta L_c) (L_r + \Delta L_r)/(L_c L_r)$. Additionally, a relative thickness change $\eta = (t + \Delta t)/t$ was prescribed as a uniaxial change in the direction of plane normal $n_0$, in the reference configuration$^{10}$. Thus we arrive at the definition of a transversely isotropic growth tensor that describes growth-induced volumetric changes in terms of area change $\vartheta$ and thickness change $\eta$.  

---

**Figure 9.** Mechanical model of heart valve development. A finite element model of a heart valve was generated for every age group based on the lower half of a spheroid. Due to symmetry, only one leaflet was modeled, and frictionless contact was modeled by adding a contact surface with friction coefficient 0 between adjacent leaflets, parallel to the free edges (blue lines). Somatic changes were applied by adjusting the diastolic blood pressure and prescribing displacement boundary conditions on the annular nodes (red lines). Leaflet stretch and stress were investigated in the highlighted element in the center of the belly region. Volumetric growth was applied in the plane spanned by the circumferential and radial direction, and in the thickness direction, given by plane normal $n_0$. A collagen fiber network was implemented in the model which was mainly oriented in the circumferential direction.
Remodeling via changes of material properties. Remodeling, e.g. stiffening due to cross-link formation, or different degrees of anisotropy due to collagen fiber reorientation leads to changes in the microstructure of valvular tissue. These microstructural changes lead to a different material response. In our model, we phenomenologically implemented microstructural remodeling by this change in material response. The (change in) material response was governed by (changes in) the material parameters of the constitutive model. These material parameters were interpolated between two developmental stages, by parameterizing them as a function of a weight factor \( w \) using polynomials (Fig. 10). The polynomials were fitted on the linear transition of the circumferential (\( d = \text{circ.} \)) and radial (\( d = \text{rad.} \)) Cauchy stress response:

\[
\sigma_d(w) = (1 - w) \sigma_d^0 + w \sigma_d^\text{end}\quad (0 \leq w \leq 1)
\]

such that when \( w = 0 \) the Cauchy stress before remodeling \( \sigma_d^0 \) was obtained, and when \( w = 1 \) the stress-stretch response after remodeling \( \sigma_d^\text{end} \) was obtained (Fig. 3).

The material behavior of the individual valves was previously estimated using micro-indentation testing on a confocal microscope, in combination with inverse finite element modeling, as described before. This method allowed for anisotropic mechanical characterization in a strain range that is physiological for heart valve leaflets. For each age group (for both aortic and pulmonary valves) the average stress-stretch response in the circumferential (\( d = \text{circ.} \)) and radial (\( d = \text{rad.} \)) direction was determined. The material parameters for each group were then fitted to these average stress-stretch responses (Fig. 2).

The material behavior was modeled by a hyperelastic constitutive model, where the Cauchy stress \( \sigma \) was obtained from a strain energy density function \( \Psi \). Since growth occurs stress-free, the strain energy density function is only dependent on elastic deformation \( \Psi = \Psi(F_e)^{16} \), and is therefore defined per amount of grown volume,

\[
\sigma = \frac{2}{J_e} E_e \frac{\partial \Psi}{\partial F_e^T} F_e^T
\]
with \( C_\varepsilon = F^T \cdot F \) the elastic right Cauchy-Green deformation tensor. A fiber-reinforced material was used to model the valvular constitutive behavior, where the strain energy density function consists of an isotropic matrix part \( m \) and anisotropic fibrous part \( f \) with fiber volume fraction \( \Phi_f \), arbitrarily chosen to be 0.553.

\[
\Psi = (1 - \Phi_f)\Psi_m + \Phi_f\Psi_i
\]  

The constitutive behavior of the isotropic matrix part was described by a Neo-Hookean constitutive model,

\[
\Psi_m = \frac{k}{2} \ln(2\mathbf{I}) + \frac{\mu}{2} (\mathbf{I}_1 - 3 - 2 \ln(\mathbf{I}))
\]

where \( k = \frac{2\mu(1 + \nu)}{\nu(1 - 2\nu)} \) is the bulk modulus, \( \mu \) the shear modulus, and \( \mathbf{I}_1 \) the first invariant of the elastic right Cauchy-Green deformation tensor. Quasi-incompressibility was enforced by setting the Poisson's ratio at \( \nu = 0.498 \). The fibrous part was modeled by an angular fiber distribution given by a periodic version of the normal probability distribution function \( ^54,55 \), with a main circumferential orientation \( ^56 \) and age-dependent dispersity \( \beta \) (Fig. 9). The direction of each fiber \( i \) was given by the unit vector \( e_i^0 \) in the reference configuration and \( e_i^g \) in the configuration after growth. Each fiber additively contributed to the total fiber strain energy density function \( ^53 \), where the strain energy density function \( \Psi_i^f \) for each individual fiber \( i \) was given by an exponential model \( ^14,49,53,56 \),

\[
\Psi_i^f = k_1 \left[ \exp\left( \frac{k_2}{2} (\lambda_i^f)^2 - 1 \right) \right] - k_2 (\lambda_i^f)^2 - 1 - 1
\]

with \( k_1 \) and \( k_2 \) material parameters, \( (\lambda_i^f)^2 = C_{\varepsilon} \cdot \left( e_i^g \otimes e_i^g \right) \) the squared elastic fiber stretch, and \( (\cdot)^\diamond \) the Macaulay brackets to enforce that the fibers only resist tension.

**Kinetics of growth and remodeling.** The environmental changes were applied as a linear function of developmental time \( \tau (0 \leq \tau \leq 1) \). The importance of the kinetics of growth and remodeling were investigated by defining the growth (\( \vartheta \) and \( \eta \)) and remodeling (\( w \)) parameters as a function of \( \tau \) and adjusting their rate change in an exponential fashion relative to the environmental changes, governed by rate change parameters \( k_g \) (growth rate) and \( k_r \) (remodeling rate),

\[
\vartheta(\tau) = (\vartheta_{\text{end}} - 1) e^{k_g \tau} - 1 \left( e^{k_g \tau} - 1 + 1 \right)
\]

\[
\eta(\tau) = (\eta_{\text{end}} - 1) e^{k_r \tau} - 1 \left( e^{k_r \tau} - 1 + 1 \right)
\]

\[
w(\tau) = w_{\text{end}} e^{k_r \tau} - 1 \left( e^{k_r \tau} - 1 \right)
\]

where \( \vartheta_{\text{end}}, \eta_{\text{end}} \) and \( w_{\text{end}} \) were the parameter values at the end of the developmental stage. Note that if \( k_g \to 0 \) and \( k_r \to 0 \) growth and remodeling occur linearly with time (and at an equal rate to the environmental changes), if \( k_g < 0 \) and \( k_r < 0 \) growth and remodeling initially occur faster, and if \( k_g > 0 \) and \( k_r > 0 \) growth and remodeling initially occur slower compared to the environmental changes (Fig. 11).
The relative influences of growth and remodeling. A total of six models (aortic and pulmonary infant, adolescent and adult) were prepared to study the homeostatic stretches and stress. Subsequently, early development was simulated by applying environmental changes to the aortic and pulmonary infant valves, whereas for late development these changes were applied to the adult valves. The relative influence of growth and remodeling on leaflet stretch was investigated by applying growth and remodeling combined, only growth, only remodeling, and no growth and remodeling. For all simulations, leaflet stretch in the middle of the belly region (Fig. 9) was investigated. The importance of the kinetics of growth and remodeling relative to the environmental changes were investigated by applying combined growth and remodeling with different rates, using three cases: changing only the growth rate ($k_g = \pm 1, \pm 2, \pm 3$ while $k_r = 0$), changing only the remodeling rate ($k_r = \pm 1, \pm 2, \pm 3$ while $k_g = 0$), and changing both rates simultaneously ($k_g = k_r = \pm 1, \pm 2, \pm 3$). For all cases, the temporal changes in valve coaptation and leaflet stretch were investigated.

Data availability. The datasets generated during and/or analyzed during the current study are available from the corresponding author on reasonable request.

References
1. Ascenzi, P. Biomechanics and Galileo Galilei. Journal of Biomechanics 26, 95–100 (1993).
2. Fung, Y. C. Biomechanical Aspects of Growth and Tissue Engineering. In Biomechanics, 499–546 (Springer, New York, NY, New York, NY, 1990).
3. Humphrey, J. D. Vascular adaptation and mechanical homeostasis at tissue, cellular, and sub-cellular levels. Cell biochemistry and biophysics 50, 53–78 (2008).
4. Hoffmann, B. D., Grashoff, C. & Schwartz, M. A. Dynamic molecular processes mediate cellular mechanotransduction. Nature 475, 316–323 (2011).
5. Ambrosi, D. et al. Perspectives on biological growth and remodeling. Journal of the Mechanics and Physics of Solids 59, 863–883 (2011).
6. Humphrey, J. D., Dufresne, E. R. & Schwartz, M. A. Mechanotransduction and extracellular matrix homeostasis. Nat Rev Mol Cell Biol 15, 802–812 (2014).
7. Taber, L. A. & Humphrey, J. D. Stress-modulated growth, residual stress, and vascular heterogeneity. J Biomech Eng 123, 528–535 (2001).
8. Humphrey, J. D., Eberth, J. F., Dye, W. W. & Gleason, R. L. Fundamental role of axial stress in compensatory adaptations by arteries. Journal of Biomechanics 42, 1–8 (2009).
9. Valentin, A., Cardamone, L., Baek, S. & Humphrey, J. D. Complementary vasoactivity and matrix remodeling in arterial adaptations to altered flow and pressure. J R Soc Interface 6, 293–306 (2009).
10. Goktepe, S., Ablee, O. J., Parker, K. K. & Kuhl, E. A multiscale model for eccentric and concentric cardiac growth through sarcomerogenesis. Journal of theoretical biology 265, 433–442 (2010).
11. Chapat, M. et al. Mitral leaflet adaptation to ventricular remodeling: occurrence and adequacy in patients with mitral mitral regurgitation. Circulation 118, 845–852 (2008).
12. Rauch, M. K., Tibayan, F. A., Miller, D. C. & Kuhl, E. Evidence of adaptive mitral leaflet growth. Journal of the Mechanical Behavior of Biomedical Materials 15, 208–217 (2012).
13. Obbink-Huizer, C. et al. Computational model predicts cell orientation in response to a range of mechanical stimuli. Biomech Model Mechanobiol 13, 227–236 (2013).
14. Oomen, P. J. A. et al. Age-dependent changes of stress and strain in the human heart valve and their relation with collagen remodeling. Acta Biomater 29, 161–169 (2016).
15. Kroon, W., Delhaas, T., Arts, T. & Bovendeerd, P. Computational modeling of volumetric soft tissue growth: application to the cardiac left ventricle. Biomech Model Mechanobiol 8, 301–309 (2009).
16. Cyron, C. J. & Humphrey, J. I. D. Vascular homeostasis and the concept of mechanobiological stability. Int J Eng Sci 85, 203–223 (2014).
17. Van Geemen, D. et al. Age-Dependent Changes in Geometry, Tissue Composition and Mechanical Properties of Fetal to Adult Cryopreserved Human Heart Valves. PloS one 11, e0149020 (2016).
18. NIH. The fourth report on diagnosis, evaluation, and treatment of high blood pressure in children and adolescents. Tech. Rep., U.S. Department of Health and Human Services (2005).
19. Silverthorn, D. & Johnson, B. HumanPhysiology: An Integrated Approach. 5th edition. (Pearson/Benjamin Cummings, 2010).
20. Wright, J. D., Hughes, J. P., Ostchega, Y., Yoon, S. S. & Nwankwo, T. Mean systolic and diastolic blood pressure in adults aged 18 and over in the United States, 2001–2008. Natl Health Stat Report 22, 1–9 (2009).
21. Wright, J. D., Hughes, J. P., Ostchega, Y., Yoon, S. S. & Nwankwo, T. Mean systolic and diastolic blood pressure in adults aged 18 and over in the United States, 2001–2008. Natl Health Stat Report 22, 1–9 (2009).
22. Ackerman, M. J. & Kuhl, E. Computational model predicts cell orientation in response to a range of mechanical stimuli. Biomech Model Mechanobiol 13, 227–236 (2014).
23. Oomen, P. J. A. et al. Age-dependent changes of stress and strain in the human heart valve and their relation with collagen remodeling. Acta Biomater 29, 161–169 (2016).
24. Kroon, W., Delhaas, T., Arts, T. & Bovendeerd, P. Computational modeling of volumetric soft tissue growth: application to the cardiac left ventricle. Biomech Model Mechanobiol 8, 301–309 (2009).
25. Cyron, C. J. & Humphrey, J. I. D. Vascular homeostasis and the concept of mechanobiological stability. Int J Eng Sci 85, 203–223 (2014).
26. van Geemen, D. et al. Age-Dependent Changes in Geometry, Tissue Composition and Mechanical Properties of Fetal to Adult Cryopreserved Human Heart Valves. PloS one 11, e0149020 (2016).
27. NIH. The fourth report on diagnosis, evaluation, and treatment of high blood pressure in children and adolescents. Tech. Rep., U.S. Department of Health and Human Services (2005).
28. Silverthorn, D. & Johnson, B. HumanPhysiology: An Integrated Approach. 5th edition. (Pearson/Benjamin Cummings, 2010).
29. Wright, J. D., Hughes, J. P., Ostchega, Y., Yoon, S. S. & Nwankwo, T. Mean systolic and diastolic blood pressure in adults aged 18 and over in the United States, 2001–2008. Natl Health Stat Report 1, 22–24 (2011).
30. Aikawa, E. et al. Human semilunar cardiac valve remodeling by activated cells from fetus to adult: implications for postnatal adaptation, pathology, and tissue engineering. Circulation 113, 1344–1352 (2006).
31. McDonald, P. C. et al. The challenge of defining normality for human mitral and aortic valves: geometrical and compositional analysis. Cardiovasc. Pathol. 11, 193–209 (2002).
32. Bashey, R. I., Torii, S. & Angrist, A. Age-Related Collagen and Elastic Content of Human Heart Valves. Journal of gerontology 22, 203 (1967).
33. Stephens, E. H., de Jonge, N., McNeill, M. P., Durst, C. A. & Grande-Allen, K. J. Age-related changes in material behavior of porcine mitral and aortic valves and correlation to matrix composition. Tissue Engineering Part A 16, 867–878 (2010).
34. Kasyonov, V. et al. Age-related analysis of structural, biochemical and mechanical properties of the porcine mitral heart valve leaflets. Connect Tissue Res 54, 394–402 (2013).
35. Balguid, A. et al. The role of collagen cross-links in biomechanical behavior of human aortic heart valve leaflets - Relevance for tissue engineering. Tissue Eng. Part C, 1501–1511 (2007).
36. Stradins, P. et al. Comparison of biomechanical and structural properties between human aortic and pulmonary valve. Eur J Cardiothoracic Surg 26, 634–639 (2004).
37. Grande-Allen, K. J. et al. Apparently normal mitral valves in patients with heart failure demonstrate biochemical and structural derangements - An extracellular matrix and echocardiographic study. J Am. Coll. Cardiol. 45, 54–61 (2005).
38. Chapat, M. et al. Mitral leaflet adaptation to ventricular remodeling: prospective changes in a model of ischemic mitral regurgitation. Circulation 120, 599–103 (2009).
39. Hoerstrup, S. P. et al. Functional growth in tissue-engineered living, vascular grafts: follow-up at 100 weeks in a large animal model. Circulation 114, 1159–66 (2006).
40. Flanagan, T. C. et al. In Vivo Remodeling and Structural Characterization of Fibrin-Based Tissue-Engineered Heart Valves in the Adult Sheep Model. Tissue Engineering Part A 15, 2965–2976 (2009).
41. Gottlieb, D. et al. In vivo monitoring of function of autologous engineered pulmonary valve. The Journal of Thoracic and Cardiovascular Surgery 139, 723–731 (2010).
34. Driessen-Mol, A. et al. Transcatheter implantation of homologous "off-the-shelf" tissue-engineered heart valves with self-repair capacity: long-term functionality and rapid in vivo remodeling in sheep. J. Am. Coll. Cardiol. 63, 1320–1329 (2014).
35. Syedain, Z. et al. Tissue engineering of acellular vascular grafts capable of somatic growth in young lambs. Nat Commun 7, 12951 (2016).
36. Kuhn, J. et al. In situ heart valve tissue engineering using a bioreabsorbable elastomeric implant - From material design to 12 months follow-up in sheep. Biomaterials 125, 101–117 (2017).
37. Humphrey, J. D. & Razjagopal, K. R. A constrained mixture model for growth and remodeling of soft tissues. Mathematical Models & Methods in Applied Sciences 12, 407–430 (2002).
38. Rodriguez, E. K., Hoger, A. & McCulloch, A. D. Stress-dependent finite growth in soft elastic tissues. Journal of Biomechanics 27, 455–467 (1994).
39. Kuhl, E. Growing matter: a review of growth in living systems. Journal of the Mechanical Behavior of Biomedical Materials 29, 529–543 (2014).
40. Schoen, F. J. Mechanics of function and disease of natural and replacement heart valves. Annu Rev Pathol 7, 161–183 (2012).
41. Gould, R. A. et al. Cyclic strain anisotropy regulates valvular interstitial cell phenotype and tissue remodeling in three-dimensional culture. Acta Biomater 8, 1710–1719 (2012).
42. Kural, M. H. & Billiar, K. L. Mechanoregulation of valvular interstitial cell phenotype in the third dimension. Biomaterials 35, 1128–1137 (2014).
43. Rabkin-Aikawa, E., Farber, M., Aikawa, M. & Schoen, F. J. Dynamic and reversible changes of interstitial cell phenotype during remodeling of cardiac valves. Journal of Heart Valve Disease 13, 841–847 (2004).
44. Komeda, M. et al. Papillary muscle-left ventricular wall "complex". J. Thorac. Cardiovasc. Surg. 113, 292–300 (1997).
45. Otsui, Y. et al. Insights from three-dimensional echocardiography into the mechanism of functional mitral regurgitation - Direct in vivo demonstration of altered leaflet tethering geometry. Circulation 96, 1999–2008 (1997).
46. Dal-Bianco, J. P. et al. Active adaptation of the tethered mitral valve: insights into a compensatory mechanism for functional mitral regurgitation. Circulation 120, 334–342 (2009).
47. Rausch, M. K. & Kuhl, E. On the effect of prestrain and residual stress in thin biological membranes. Journal of the Mechanics and Physics of Solids 61, 1955–1969 (2013).
48. Aggarwal, A. et al. In-vivo heterogeneous functional and residual strains in human aortic valve leaflets. Journal of Biomechanics 49, 2481–2490 (2016).
49. Loerakker, S., Ristori, T. & Baaijens, F. P. T. A computational analysis of cell-mediated compaction and collagen remodeling in tissue-engineered heart valves. Journal of the Mechanical Behavior of Biomedical Materials 58, 173–187 (2015).
50. Buganza Tepole, A., Floch, C. J., Wong, J., Gossain, A. K. & Kuhl, E. Growing skin: A computational model for skin expansion in reconstructive surgery. Journal of the Mechanics and Physics of Solids 59, 2177–2190 (2011).
51. Cox, M. A. J., Driessen, N. J. B., Bouten, C. V. C. & Baaijens, F. P. T. Mechanical characterization of anisotropic planar biological soft tissues using large indentation: a computational feasibility study. J. Biomech Eng 128, 428–436 (2006).
52. Cox, M. A. J., Driessen, N. J. B., Boerboom, R. A., Bouten, C. V. C. & Baaijens, F. P. T. Mechanical characterization of anisotropic planar biological soft tissues using finite indentation: experimental feasibility. Journal of Biomechanics 41, 422–429 (2008).
53. Driessen, N. J. B., Mol, A., Bouten, C. V. C. & Baaijens, F. P. T. Modeling the mechanics of tissue-engineered human heart valve leaflets. Journal of Biomechanics 40, 325–334 (2007).
54. Gasser, T. C., Ogden, R. W. & Holzapfel, G. A. Hyperelastic modelling of arterial layers with distributed collagen fibre orientations. J R Soc Interface 3, 15–35 (2006).
55. Driessen, N. J. B., Cox, M. A. J., Bouten, C. V. C. & Baaijens, F. P. T. Remodelling of the angular collagen fiber distribution in cardiovascular tissues. Biomech Model Mechanobiol 7, 93–103 (2008).
56. Loerakker, S., Argento, G., Oomens, C. W. J. & Baaijens, F. P. T. Effects of valve geometry and tissue anisotropy on the radial stretch and coaptation area of tissue-engineered heart valves. Journal of Biomechanics 46, 1792–1800 (2013).

Acknowledgements
This work has received funding from the European Union’s Horizon 2020 programme under the Marie Skłodowska-Curie grant agreement no. 654513, and the European Union’s Seventh Framework Programme for research, technological development and demonstration under grant agreement no. 604514 (ImaValve) and the NIH grant U01-HL-119578. We further acknowledge the support from the Netherlands Cardiovascular Research Initiative (CVON 2012-01): The Dutch Heart Foundation, Dutch Federation of University Medical Centers, the Netherlands Organization for Health Research and Development and the Royal Netherlands Academy of Sciences.

Author Contributions
P.J.A.O., E.K. and S.L. designed the research; P.J.A.O., M.H., E.K. and S.L. designed computational tools; P.J.A.O. performed simulations; P.J.A.O., C.V.C.B., E.K. and S.L. analyzed the results. All authors reviewed the manuscript.

Additional Information
Competing Interests: The authors declare that they have no competing interests.

Publisher's note: Springer Nature remains neutral with regard to jurisdictional claims in published maps and institutional affiliations.

Open Access
This article is licensed under a Creative Commons Attribution 4.0 International License, which permits use, sharing, adaptation, distribution and reproduction in any medium or format, as long as you give appropriate credit to the original author(s) and the source, provide a link to the Creative Commons license, and indicate if changes were made. The images or other third party material in this article are included in the article’s Creative Commons license, unless indicated otherwise in a credit line to the material. If material is not included in the article’s Creative Commons license and your intended use is not permitted by statutory regulation or exceeds the permitted use, you will need to obtain permission directly from the copyright holder. To view a copy of this license, visit http://creativecommons.org/licenses/by/4.0/.

© The Author(s) 2018