Enhancement of the Corrosion Resistance of 304 Stainless Steel by Cr–N and Cr(N,O) Coatings

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Abstract: Chromium nitride and oxynitride coatings were deposited as monolayers ((Cr–N), Cr(N,O)) and bilayers (Cr–N/Cr(N,O), Cr(N,O)/Cr–N) on 304 steel substrates by reactive cathodic arc method. The coatings were characterised by X-ray diffraction (XRD), scanning electron microscopy (SEM), energy dispersive X-ray spectrometry (EDS), surface profilometry, and scratch tester. The anticorrosive properties of the coatings were assessed by electrochemical tests in 0.1 M NaCl + 1.96 M H₂O₂, carried out at 24 °C. Cr₂N, CrN, and Cr(N,O) phases were identified in the coatings by grazing incidence X-ray diffraction (GI-XRD) measurements. The measured adhesion values ranged from 19 N to 35 N, the highest value being obtained for the bilayer with Cr(N,O) on top. Electrochemical tests showed that Cr(N,O) presence in both mono- and bilayered coatings determined the lowest damage in corrosive solution, as compared to the Cr–N coatings. This improvement was ascribed to the more compact structure, lower coatings porosity, and smoother surface.

Keywords: chromium nitride; chromium oxynitride; multilayer; cathodic arc deposition; corrosion resistance; coating adhesion

1. Introduction

For the past decades, material science has emerged as one of the major scientific fields aiming at the improvement of the physical and chemical properties of materials, taking their projected purpose into consideration. The stainless steel (SS) family represents one of the most utilized alloys, being used in a wide range of applications, such as cutting tools, convenient support in biomedicine, rotor blades of gas turbines, aircraft parts, automobiles, pipelines, and naval vessels [1–20]. The selection of the specific SS to be used in a certain application is done considering the economic aspects as well as its physical and chemical properties. An excessive amount of transition metals (TMs) such as Cr and Fe in SS alloys may influence the chemical stability. The abundance of Cr in SS alloy may largely contribute to the formation of a passive Cr₂O₃ layer, acting as a corrosion-protective layer. However, an excessive amount of Fe in SS alloy may induce its oxidation to FeO, which accelerates SS rusting [21]. More often, the chemical stability of alloys is either temperature- or pH-dependent [20,22,23]. The exposure of SS to such harsh environments may result in corrosion that further limits its performance and durability [6,20,24]. Even though various approaches to corrosion prevention have been proposed in the literature [16], they might be costly.
The use of coatings containing carbon, oxygen, or nitrogen (e.g., carbides, nitrides, carbonitrides, or oxynitrides) has become a practical method used to improve the performance of SS [15,17–20,24]. Coatings designed to withstand corrosion are already in use in various fields, such as orthopaedics, dentistry, tribology, and photocatalysis. In order to enhance the performance of SS, numerous anticorrosion solutions have been developed based on coating application by the pulse laser deposition (PLD) or cathodic arc deposition (CAE) [14]. While large area coatings are still difficult to produce economically by PLD, CAE is a high-productivity method, producing an intense plasma flux at the cathode spots generated by the electric arc. The arc plasma comprises an important fraction of single or multiple ionized atoms. This peculiarity is of great importance, since the bombardment of the growing film by energetic ions and neutrals creates a highly adhesive coating, which can ensure the integrity of the coated structure in the long term [25,26]. Another particularity of the CAE method consists of the significant roughness of the coated surfaces, resulting from droplets ejected by the cathode due to its local melting. Considering this issue, different techniques have been developed, including venetian blinds, magnetic shielding, increased deposition pressure, as well as the development of more sophisticated methods consisting mainly of short-pulsed voltage applied on the substrate [27–31].

Therefore, understanding the corrosion behaviour of coated materials is an important step in achieving the maximum protection of coated materials and hence boosting their life service in chemically aggressive environments [12–14,16,32]. Based on the reported results, various corrosion-resistant coatings have been developed to improve the corrosion resistance of SS. Different TM nitride coatings have been synthesised and investigated due to their high hardness, good oxidation resistance, and low wear rate in dry atmosphere, as well as their phase stability in corrosive environments [10,15,33–37]. Oxynitride coatings have also been studied due to their plasmic properties, relatively low electrical resistivity, good biocompatibility, and high oxidation resistance [25,38–46].

The aim of the present study was to develop rough, large surface area, corrosion- and erosion-resistant coatings for 304 stainless steel mesh, used as support for powder photocatalysts, utilised in water remediation technologies [47]. The first step was to ascertain the corrosion behaviour of such coatings deposited on solid pieces of 304 stainless steel in relation to other properties, such as crystalline structure, mechanical properties, and surface roughness.

In the current study, we report on the electrochemical behaviour of Cr nitride and oxynitride coatings deposited on 304 SS substrates by CAE technique, as there is abundant scientific literature about the use of Cr-based coatings in severe environments, due to their superior corrosion resistance [45,48–54]. The corrosion tests of the plain and coated SS were carried out in saline solution by potentiodynamic polarization technique. The corrosion performance of the coatings was examined in relation to the coatings features, such as elemental and phase composition, surface morphology, hardness, reduced elastic modulus, and adhesion to SS substrate.

2. Materials and Methods

The Cr-based coatings (nitride and oxynitride) were prepared on 304 SS discs (Φ = 20 mm) and Si pieces (20 × 20) mm² by the reactive CAE, using a Cr cathode (99.5% purity, Cathay Advanced Materials Ltd., Guangdong, China).

The chemical composition of the 304 SS, as given by the manufacturer in wt.% and at.%, is presented in Table 1.

Each 304 SS substrate was sanded using a SiC abrasive paper (grit 800), polished (Rₐ = 60 nm), ultrasonically washed in isopropyl alcohol and water for 10 min, then dried at 120 °C for 1 h.

For controlling the coating uniformity, the samples were placed on a rotating sample holder. Moreover, before deposition, the substrates were sputter etched with Ar⁺ for 5 min to remove any contaminant layer. The residual pressure in the system was 2 × 10⁻³ Pa. The total gas pressure during the deposition was 8 × 10⁻² Pa. For the nitride coatings, nitrogen was introduced in the chamber at a mass flow rate of 60 sccm, while for the oxynitrides, the same value of the nitrogen mass flow rate was used, and 17 sccm of the oxygen was added. The arc current applied on the Cr cathode was
90 A, and the substrates were biased at −200 V. This value was selected based on our previous studies [55], aiming for the enhancement of coatings’ corrosion resistance. As previously reported, by selecting the appropriate value for the bias voltage, the coatings’ properties can be tuned, mainly related to their crystallinity and surface roughness [56]. For the bilayer coatings, the same deposition parameters were used. However, the deposition time of each individual layer was modified in order to obtain almost the same thickness for all the coatings, around 1 µm.

The thickness and the surface roughness of the coatings were investigated using a Dektak 150 surface profilometer (Bruker, Billerica, MA, USA) equipped with a 2.5 µm radius stylus. The thickness of the coatings was measured by surface profilometry according to the standard DD ENV1071-1:1994 [57], as follows. Part of a Si substrate was masked, such that an edge was formed during the deposition. Ten lines transverse to this edge were scanned at a scan rate of 20 µm/s, resulting in different heights; the averaged value was considered as the mean thickness of the film. The roughness of each SS sample was determined before and after the corrosion testing using the same 2.5 µm radius stylus, moving over a length of 10 mm at a scan rate of 50 µm/s. The roughness of all the investigated specimens (substrate and coatings) was evaluated based on two roughness parameters: the arithmetic average deviation from the mean line (Rq) and the root mean square average of the profile heights over the evaluation length (Ra). Moreover, the asymmetry of the profile about the mean line was also considered by calculating the skewness parameter (Sr). The presented roughness values represent the average data obtained from 5 measurements (10 mm length), performed on different areas of each specimen. After the corrosion tests, the profilometry measurements were also carried out on the substrate and all the coatings for visualisation of the significant profiles of the resulted pits.

The phase composition of the samples was investigated by X-ray diffraction (XRD) using a SmartLab diffractometer (Rigaku, Tokyo, Japan), with a Cu Kα radiation (λ = 0.15405 nm). Grazing incidence scans in the range 30°–70° at 2θ incidence, with a step size of 0.02° were obtained for the coatings deposited on Si and SS substrates.

A Hysitron TI Premier nanoindenter, equipped with a Berkovich diamond tip (100 nm radius), was used for the nanoindentation measurements, for obtaining the hardness (H) and the reduced modulus (Er) values. The normal force used was 5 mN to obtain individual indents for penetration depths in the 50–80 nm range. In order to take the possible imperfections of the indenter into account, the system was calibrated before indentation measurements using a standard fused quartz piece. Five indentations were done at the same force for each measurement, which were positioned at least 12 µm apart in order to prevent the effects of any possible interference between the indentation points. The Oliver–Pharr method was used to extract hardness (H) and reduced elastic modulus (Er) values from the load–displacement curves [58].

The corrosion resistance was evaluated by the potentiodynamic techniques in 0.1 M NaCl + H2O2 (pH = 4), at room temperature (24 °C), using a VersaStat 3 Potentiostat/Galvanostat (Princeton

Table 1. Chemical composition of 304 L stainless steel (wt.% and at.%).

| Composition | Element | Fe | C | Mn | Si | Cr | Ni | P | S | Co | Mo | Cu |
|-------------|---------|----|---|----|----|----|----|---|---|----|----|----|
| wt.%        |         | 70.976 | 0.004 | 1.220 | 0.208 | 17.746 | 8.524 | 0.020 | 0.14 | 0.160 | 0.589 | 0.539 |
| at.%        |         | 70.380 | 0.020 | 1.230 | 0.410 | 18.900 | 8.040 | 0.036 | 0.024 | 0.150 | 0.350 | 0.470 |
Applied Research, Oak Ridge, TN, USA). A typical three-electrode cell was used, with a Pt counter-electrode and an Ag/AgCl reference electrode. The coated and uncoated (used as control) stainless steels were used as working electrode, being placed in a Teflon holder with a working area of 1 cm². Firstly, the open circuit potential (Eoc) was monitored for 15 h after immersion. To identify the polarisation resistance (Rp), a linear polarisation technique was used by applying a perturbation potential of −0.01 to 0.01 V vs. Eoc at a scanning rate of 1 mV/s. Rp parameter was determined as the slope of the linear region of the ΔE−Δi curve at corrosion potential (Ecorr). Further, Tafel plots were recorded from −0.25 V to 0.25 V vs. Eoc at a scanning rate of 1 mV/s. The Ecorr parameter, anodic (βa) and cathodic (βc) slopes, and corrosion current density (icorr) were extracted from Tafel plots. The porosity (P) was estimated from Elsener’s empirical equation (Equation (1)) based on the polarisation resistance of the uncoated (Rpo) and coated (Rpc) SS specimen, the difference between the corrosion potentials of the coated and uncoated SS specimen (ΔEcorr) and corresponding anodic slope (βa).

\[
P = \left( \frac{R_{pc}}{R_{po}} \right) \times 10^{-\frac{-\Delta E_{corr}}{\beta_a}}
\] (1)

The protective efficiency (Pe) was also calculated (Equation (2)) based on the corrosion current densities of the coatings (icorr,c) and the SS specimen (icorr,s):

\[
Pe = \left( 1 - \frac{icorr,c}{icorr,s} \right) \times 100
\] (2)

Scratch tests under standard conditions (indenter—0.2 mm radius diamond tip, load—continuous increase from 0 to 100 N, scratching speed—10 mm/min, scratching distance—10 mm) were undertaken to determine the coating adhesion, using a laboratory system. The critical loads values at which the film flaking starts (Ls) and at which the delamination is completed (Ld) were determined by optical microscopy.

The coatings were labelled considering the left written coating, being near the substrate, such as in Cr–N/Cr(N,O) bilayer, the top layer being Cr(N,O).

3. Results and Discussion

3.1. Surface Morphology and Elemental Composition before Corrosion Measurements

Representative SEM micrographs of Cr–N and Cr(N,O) coatings are presented in Figure 1. As expected in CAE deposition, microdroplets can be noticed over the surface of all the investigated specimens—more evident in the Cr–N coating, while the Cr(N,O) coating presents a smoother surface, as seen in the magnified images. The same results were reported by Li Ming-sheng on the reactive CAE deposition of chromium in nitrogen and oxygen atmosphere [59]. It was documented by Munz that a cathode material with low melting temperature (Tm) generates an increased number of droplets with larger size [60]. The observed differences in roughness may be explained by the difference between the Tm of Cr and its compounds: TmCrN (1923 K) < TmCrN (2043 K) < TmCr (2143 K) < TmCrO3 (2708 K), as documented by the binary phase diagrams of Cr–N and Cr–O [61]. The process is related to the temporary formation of small islands of the reactive compounds on the cathode surface due to the dense plasma arc condition. The islands are melted by the steering arc, such that the resulting microdroplets are propelled to the substrate. In a nitrogen atmosphere, the surface of the metallic Cr cathode is covered with CrN and CrN, and mainly with CrN or even CrO3 if the deposition atmosphere consists of a mixture of oxygen and nitrogen, as a direct result of the higher reactivity of oxygen compared to the nitrogen molecule. It is reasonable to believe that the observed difference in surface roughness of Cr–N and Cr(N,O) coatings is related to the different Tm of the reactive compounds formed on the cathode as a result of metal target poisoning in reactive CAE.

Despite this peculiarity, the surface of both coatings was uniform, without major morphological defects such as pores, pinholes, and voids, proven as deleterious for corrosion protection of the steel substrate.
Figure 1. SEM micrographs of the investigated monolayers before the corrosion tests: (a) Cr–N; (b) Cr(N,O).

For each type of coating, the averaged values of the atomic concentrations, together with O/N, O/Cr, and (O + N)/Cr concentration ratios, are presented in Table 2. As standard samples were not available, the accepted precision in EDS measurement was defined as the relative standard deviation: 
\[
RDS(\%) = \left( \frac{\delta_{at}}{C_{am}} \right) \times 100
\]
where \(\delta_{at}\) represents the calculated SD (%) of 10 measurements, and \(C_{am}\) represents the arithmetic mean concentration of the constituent element. In order to improve the accuracy of the results, long counting (acquisition) times were used [46,47]. To improve the accuracy of the light elements concentration, the low-energy domain of each spectrum was deconvoluted, considering the constituent elements of the substrate and of the coatings. The calculated RDS values are presented in Table 2. One can notice the presence of oxygen and nitrogen in the coatings, as well as a small amount of carbon, probably due to the external handling of samples. A high oxygen content was measured on Cr(N,O) coatings. The low oxygen concentration found in the Cr–N coatings should be treated as contamination, as already reported [62].

Chromium oxynitride coating has a complex structure, its composition and properties being controlled by the deposition parameters, which should ensure the reproducibility of each deposition run. The deposition of chromium oxynitride coating, performed in a mixture of two reactive gases such as O\(_2\) and N\(_2\), is a complex process due to the different reactivity of the Cr with nitrogen and the more reactive oxygen atoms and ions. The observed increase of O/N ratio—about five-fold—demonstrates the successful deposition of chromium oxynitride coating. The observed significant increase can be ascribed to the higher affinity of Cr for oxygen compared to nitrogen [63].

Table 2. The elemental composition of the monolayered coatings deposited on Si substrates.

| Coating   | Elemental Composition (at.%) | O/N | O/Cr | (O + N)/Cr |
|-----------|-------------------------------|-----|------|------------|
| Cr–N      | 30.5 ± 1.2 2.6 ± 0.2 63.4 ± 2.5 3.5 ± 0.2 | 0.085 | 0.041 | 0.522      |
| Cr(N,O)   | 35.6 ± 1.7 14.9 ± 0.8 46.8 ± 2.2 2.6 ± 0.1 | 0.419 | 0.318 | 1.079      |

3.2. Phase Composition

Due to the significant overlapping of 304 SS peaks and those of the deposited coatings (Figure 2a), Figure 2b shows the XRD patterns of the coatings deposited on silicon wafers, discussed as follows. The diffractogram of the Si/Cr–N monolayer presents a shallow peak at 37.7° corresponding to (111) cubic CrN phase (JCPDS 11-0065, at 37.57°) or to the hexagonal (110) Cr:Cr phase (JCPDS 35-0803, at 37.35°). Additionally, a second small peak situated at 43.38° was attributed more probably to the (200) plane of hexagonal Cr:Cr phase (JCPDS 35-0803, at 43.40°) than to (200) plane in B1 phase (JCPDS 11-0065, at 43.77°). The high-intensity peak observed at 67.6° was ascribed to the hexagonal Cr:Cr phase (JCPDS 35-0803, at 67.3°), suggesting that the deposition conditions favour the formation of a highly-stressed Cr:Cr coating. Our results are in good agreement with those reported by Rebholz et al., who showed that in chromium nitride with nitrogen content of about
30 at.%, only Cr$_2$N phase is present [64], similar to our result (30.5 at.% N). They also showed that both Cr$_2$N and CrN phases coexist in coatings if the nitrogen content is raised to about 40 at.% [64]. This result is also consistent with the phase diagram of the Cr–N system [65]. Considering the XRD pattern of the coating deposited on SS, one can observe a first broad peak, most probably representing the superposition of the (111) cubic CrN phase and (110) hexagonal Cr$_2$N phase. The second peak is also broad, higher than the one observed on Si substrate. As such, the presence of (200) planes of the hexagonal Cr$_2$N and cubic CrN phases is evident from the peak asymmetry. A distinctive feature of the coatings grown on SS is the presence of a third broad peak at about 63°, indicating the overlap of the (211) plane of Cr$_2$N (JCPDS 35-0803, at 62.44°) and the (220) plane of CrN (JCPDS 11-0065, at 63.60°). Note also that the (300) Cr:N maximum observed on the Si deposited coating is no longer visible.

In the Cr(N,O) coating deposited on Si, three peaks were observed at 37.9°, 44.2°, and 63.6°, shifted to higher 2θ angles compared to the cubic CrN phase (JCPDS 11-0065, at 37.60°, 43.77°, and 63.60°). The observed shift is due to oxygen incorporation, as also reported by Suzuki et al. for PLD grown Cr(N,O) with different oxygen contents [66]. The observed decrease in the lattice constant and peak shift to higher angles suggests the formation of a solid solution which stabilises the single-phase cubic solid solution of Cr(N,O) [67]. This conclusion is supported by the almost unity value of (N + O)/Cr ratio obtained by EDS. The diffractogram of this coating deposited SS substrate shows the clear signatures of the (200) and (220) planes of Cr(N,O), while the peak ascribed to the (111) plane is not visible. As previously reported, the overall energy contains surface energy and strain energy, and the main coating orientation is correlated with the lower overall energy direction of the films. The presence of only (200) and (220) maxima might be an indication of the surface energy minimisation in Cr(N,O) coating deposited on SS when compared to the one deposited on Si, in which the plane (111) was also present [68,69].

Considering the bilayer coatings, one may observe that the peaks’ location was shifted in between the positions observed in Cr–N and Cr(N,O) monolayers, indicating the overlapping of the peaks specific for each monolayer. On the Si/Cr–N/Cr(N,O) diffractogram, one can observe the (111) preferred orientation, as well as the presence of the (300) Cr:N peak. As the Cr–N layer is located closest to the substrate the peak has a lower intensity, especially in grazing incidence measurement set-up. The diffractogram of SS/Cr–N/Cr(N,O) presents the same peaks as the Si/Cr–N/Cr(N,O), except for the Cr:N peak (300), which was also missing from that of the SS/Cr–N monolayer.

As expected, in Si/Cr(N,O)/Cr–N bilayer, the Cr:N peak is more intense, and a (111) significant orientation is present. Moreover, in this bilayer, two diffraction lines were found at 43.3° and 44.3°, ascribed to Cr:N and Cr(N,O), respectively. As expected, the diffractogram of the SS/Cr(N,O)/Cr–N presents all peaks observed on both SS/Cr–N and SS/Cr(N,O) diffractograms. Summarising the crystalline structures observed in Cr–N/Cr(N,O) coatings deposited on both Si and SS substrates, they are accurately depicting the two composing monolayers. However, the crystalline structures of Si/Cr(N,O)/Cr–N and SS/Cr(N,O)/Cr–N are more complex, as the crystalline Cr(N,O) layer underneath seems to promote the growth of CrN and Cr$_2$N crystallites in the Cr–N top layer, as it results from the better separated maxima of the two types on chromium nitride.
3.3. Coating Thickness and Roughness

Figure 3 presents, as an example, a profile line of the edge measured on Cr(N,O) coating deposited on the masked Si piece. Additionally, the thickness values of all the investigated coatings are shown.

The values of the roughness parameters, $R_s$ and $Rq$, determined for the SS substrate and all deposited coatings, are presented in Figure 4a,b, respectively. One may notice an increase of coating roughness (by a factor of up to approximately 8.5) compared to the bare substrate ($R_s = 48$ nm, $Rq = 60$ nm). In accordance with SEM images, the highest values were obtained for the Cr–N coating: $R_s = 281.2$ nm, $Rq = 470.6$ nm. This result is due to the observed microdroplets generated from the
target material during the reactive cathodic arc deposition, determining the presence of the most numerous peaks. The oxygen addition in the deposition atmosphere slightly decreased the surface roughness, as observed in Cr(N,O) monolayers. In the case of bilayers, considering the errors, the surface roughness is in the same range as that of the oxynitride coating. The observed decrease of the roughness for both bilayers, as compared to the nitride coating, may be ascribed to the lower roughness of Cr(N,O) layer in the bilayer, and to the thinner dimensions of the composing individual layers in the bilayers compared to the monolayer. The trend evidenced for the $R_a$ parameter (Figure 4a) was also preserved for the $R_q$ parameter (Figure 4b).

![Image of roughness parameters](image)

**Figure 4.** The roughness of Cr-based coatings before the corrosion test: (a) $R_a$ parameter; (b) $R_q$ parameter; (c) $S_k$ parameter.

Since $R_a$ and $R_q$ parameters are not sufficient to evaluate the surface quality, the skewness parameter ($S_k$) values are presented in Figure 4c. Near the value close to 0 for the SS substrate, indicating a relatively uniform distribution of the peaks and valleys on the surface. The $S_k$ values corresponding to the coatings are in the 2–3 range, indicating the presence of high peaks, since a positive number relates to a higher percentage of profiles situated above the mean line. The presence of these peaks on the surface of coatings is the result of the droplets, as observed by SEM. As mentioned above, this is a characteristic topography of the coatings obtained by the CAE deposition method. It was also reported that other hard coatings (CrN [70], TiN/CrN [71]) deposited by CAE present structural defects on the surface in the form of overgrown droplets, leading to an increased surface roughness, which can affect the corrosion behaviour.

3.4. Coating Mechanical Properties

A coating’s functionality is dependent on its superior mechanical properties, which might be the warrant of a prolonged lifetime.

The SEM micrographs of the scratch traces are illustrated in Figure 5. The first sign of coating delamination ($L_1$) was measured around 10 N loads on the coatings. The highest value, 11.2 N, was obtained for the Cr–N/Cr(N,O) coating.

The Cr(N,O) monolayer was completely delaminated for a load $L_2$ higher than 19.1 N, while Cr–N coating withstood the gradual increasing loading force up to 23.7 N, denoting an excellent adhesion to the metallic substrate.
Considering the two bilayered coatings, the one containing Cr(N,O) layer at the metal interface presented lower values for both loads \((L_1 \text{ and } L_2)\), but notably higher than the ones corresponding to Cr(N,O) monolayer. As expected, the presence of Cr–N layer at the metal interface determined the highest values for both \(L_1\) and \(L_2\) (35 N). The best adhesion was measured for the coating Cr–N/Cr(N,O), as a result of the good adhesion of the Cr–N monolayer to the substrate \((L_2 = 23.7)\), in comparison with the one exhibited by the Cr(N,O) monolayer \((L_2 = 19.1 \text{ N})\).

To sum up, both types of bilayer exceed the delamination load values obtained for monolayers: \(L_{1,2}^{\text{Cr(N,O)}} < L_{1,2}^{\text{Cr–N}} < L_{1,2}^{\text{Cr(N,O)/Cr–N}} < L_{1,2}^{\text{Cr–N/Cr(N,O)}}\). The higher adhesion of the two bilayers may be ascribed to the lower internal stress in the bi- and multi-layers, as a reduced intrinsic stress is commonly associated with an enhanced adhesion. Additionally, the presence of a supplementary interface between the two monolayers hinders the crack propagation, determining a better adhesion of the coating to the substrate.

The hardness and reduced elastic modulus of the coatings as determined by nanoindentation are presented in Table 3, and a typical force–displacement curve, with an indentation depth of 67.9 nm—less than 10% of the coating thickness—is presented in Figure 6. As expected, the highest hardness values were obtained for the Cr–N monolayer and for the SS/Cr(N,O)/Cr–N double layer, due to the superior mechanical characteristics of nitrides compared with oxynitrides. However, the aim of the study was to develop corrosion-resistant coatings working under soft erosive conditions. As such, we also looked for superior mechanical properties of the coating, which are related to the various ratios of hardness to reduced elastic modulus \([72–74]\). It has been reported that \(H/E_r\) is related to wear resistance, \(H/E_r\) to the coating’s resilience, and \(H/E_r^2\) to plastic deformation resistance, thus it can also predict erosion resistance. As can be observed in Table 3, all these ratios present the same trend as critical load \(L_2\). The obtained values for \(H\), \(E_r\), and \(H/E_r\) for Cr–N coating are in agreement with the data previously reported in the literature \([75–77]\).

**Table 3.** Hardness \((H)\), reduced elastic modulus \((E_r)\), \(H/E_r\), \(H/E_r^2\), \(H/E_r\) ratios, and the critical loads \(L_2\) as determined for the Cr-based coatings deposited on 304 SS substrate.

| Coating                  | \(H\) (GPa) | \(\Delta H\) (GPa) | \(E_r\) (GPa) | \(\Delta E_r\) (GPa) | \(H/E_r\) | \(H/E_r^2\) | \(H/E_r\) | \(L_2\) (N) |
|--------------------------|-------------|--------------------|---------------|----------------------|-----------|-------------|-----------|-------------|
| SS/Cr–N                  | 24.53       | ±1.17              | 227.12        | ±6.71                | 0.1080    | 0.286       | 2.649     | 23.7        |
| SS/Cr(N,O)               | 21.43       | ±1.70              | 203.34        | ±7.95                | 0.1054    | 0.238       | 2.259     | 19.1        |
| SS/Cr(N,O)/Cr–N          | 25.28       | ±1.56              | 233.57        | ±8.26                | 0.1082    | 0.296       | 2.736     | 24.1        |
| SS/Cr–N/Cr(N,O)          | 22.75       | ±1.03              | 175.45        | ±5.31                | 0.1296    | 0.382       | 2.949     | 35          |

Figure 5. Scratch traces of Cr-based coatings deposited on 304 SS substrate.
3.5. Corrosion Measurements

The open circuit potential evolution during 15 h immersion in 0.10 M NaCl + 1.96 M H₂O₂ is presented in Figure 7. In the first hours of immersion, a slight decrease of potential was observed for all analysed specimens, more pronounced for 304 SS. However, all the coated specimens reached a steady state, the corresponding E_{OC} being in the range 0.02–0.3 V. The stable E_{OC} of the coated specimens is a sign of the probable formation of a stable passivation layer. The slow decrease of the potential corresponding to 304 SS indicates the instability of the passive layer. For the Cr(N,O)/Cr–N bilayer, the initial rapid decrease of the E_{OC} value was followed by a steady increase, such that after 15 h of immersion the value exceeded the one obtained for 304 SS, displaying an increasing tendency up to 117 mV, proving the protective nature of this coating. The most passive layers were formed on the surfaces of the Cr–N/Cr(N,O) and Cr(N,O) coatings, both presenting almost the same variation tendency for E_{OC}, leading to the conclusion that the presence of Cr(N,O) at the point of contact with the corrosive environment has a beneficial effect on the corrosion resistance. In contrast with the above result, the Cr–N monolayer exhibited a better passivation of its surface compared to the Cr(N,O)/Cr–N bilayer, showing an E_{OC} value as low as 0.1 V. This result may be ascribed to the poorer adhesion measured for the Cr(N,O)/Cr–N bilayer. Han and coworkers also studied the corrosion resistance of chromium nitride deposited on low alloy steel (AISI 4140) in an aerated 3% NaCl solution, and reported small negative E_{OC} values (~−0.7 V), which might be ascribed mainly to the different corrosive environment [78].

![Figure 6. Typical force–displacement curves of Cr(N,O) coating.](image)

![Figure 7. Open circuit potential evolution of Cr-based coatings deposited on 304 SS.](image)
the Cr(N,O) crystallites diffuse outwards, forming Cr:O$_3$ layers which surround the crystallites and slow down the oxidation speed, such that the oxidation resistivity of Cr(N,O) is increased [67]. No significant differences were found between the Cr–N monolayer and Cr(N,O)/Cr–N bilayer.

Furthermore, $E_{corr}$ and corrosion current density ($i_{corr}$) were extracted from Tafel plots, as frequently reported (e.g., [79]). Figure 8 shows the Tafel plots for the plain SS substrate and all the coatings deposited on SS. The inset presents the fitting lines for the Cr(N,O) coating. It can be stated that the behaviour of a material is nobler in a corrosive solution, when the corrosion potential ($E_{corr}$) value is more electropositive. According to Table 4, all coatings were nobler compared to the uncoated substrate. When the Cr(N,O) is used as top layer, the sample has a more electropositive corrosion potential, indicating that the corrosive solution had less influence on these surfaces. Comparing the coating with Cr–N in top, the most noble corrosion potential was measured for Cr–N monolayer, suggesting a good corrosion resistance.

$R_p$ was determined at the open-circuit potential by linear polarisation tests performed by applying a small perturbation (±10 mV vs. E$.oc$). The $R_p$ values were determined as the slope of the linear region of the $\Delta E - \Delta i$ curve near $E_{corr}$. The $i_{corr}$ was extracted based on Tafel plots which were recorded from ±0.25 V vs. E$.oc$, using the corrosion test software (VersaStudio) and performing a numerical fit to the Butler–Volmer equation, as we considered that both a cathodic and an anodic reaction occur on the same electrode. As also indicated by the current density parameter, the coated surfaces are less inclined to allow current to flow, as the $i_{corr}$ parameter was two orders of magnitude lower in value than the SS substrate. Considering this parameter, the Cr(N,O) monolayer showed the lowest $i_{corr}$, followed by Cr–N/Cr(N,O), Cr(O,N)/Cr–N, and Cr–N coatings. The corrosion rate is proportionally related to the $i_{corr}$. Thus, we can conclude that the Cr(N,O) monolayer has the lowest corrosion rate. It is interesting to note that the presented Cr–N-based coatings exhibited $i_{corr}$ values lower than the multilayered NbN/CrN coatings with 2 to 10 bilayers, immersed in 0.5 M NaCl solution, deposited by the magnetron sputter deposition, as reported by Aperador and Delgado [80].

![Figure 8. Tafel plots of Cr-based coatings deposited on 304 SS steel; the inset presents the fitting lines in the Tafel plot of Cr(N,O) coating.](image)

Both porosity and protection efficiency of the investigated coatings were calculated based on Equations (2) and (3). By comparing the porosity values, one can conclude that the addition of oxygen leads to a porosity decrease in Cr-based coatings. When the Cr(N,O) layer is on top, it can be seen that the porosity is lower. The Cr(N,O)/Cr–N system shows higher porosity than that Cr–N/Cr(N,O) or Cr(N,O) coatings, its properties being more akin to that of Cr–N.

Regarding the protection efficiency, the best value was found for the Cr(N,O) monolayer, indicating better corrosion resistance. This result is in good agreement with the above-mentioned findings. We note that the Cr(N,O) coating exhibited the best protection efficiency. Moreover, its presence on the top of a bilayer also produced a high protection efficiency, superior to that observed in Cr(N,O)/Cr–N bilayer, probably as a direct result of the beneficial effect of the oxide layers surrounding the crystallites, preventing further oxidation.
Table 4. Corrosion parameters of Cr-based coatings.

| Sample                  | Eoc (mV) | Rp (kΩ) | Ecorr (mV) | icorr (µA/cm²) | P  | Pe (%) |
|-------------------------|----------|---------|------------|----------------|----|--------|
| 304 SS                  | 18       | 2.109   | 34         | 14.689         | –  | –      |
| Cr–N                   | 263      | 86.136  | 236        | 0.492          | 0.016 | 96.7   |
| Cr(N,O)                 | 277      | 187.75  | 250        | 0.137          | 0.007 | 99.1   |
| Cr(N,O)/Cr–N           | 117      | 85.599  | 143        | 0.336          | 0.020 | 97.7   |
| Cr–N/Cr(N,O)           | 276      | 223.047 | 250        | 0.168          | 0.006 | 98.9   |

Figure 9a presents the evolution of corrosion current density (icorr) versus the coatings’ thickness. One may observe that the increase of coating thickness was accompanied, as expected, by the decrease of icorr and the increase of the protection efficiency, as shown in Figure 9b. The comparison of Cr–N and Cr(N,O)/Cr–N coatings provides evidence that the superior corrosion resistance of the bilayer might be related to its higher adhesion to the substrate and with the presence at the substrate interface of the Cr oxynitride layer, conferring a higher protection efficiency to the bilayer. For the Cr–N/Cr(N,O) bilayer, a small decrease of the protection efficiency and icorr values compared to Cr(N,O) monolayer was evident, despite the modest adhesion performance of the monolayer on SS. Probably the superior corrosion resistance of the Cr(N,O) monolayer might be related to the low roughness, low porosity, and low quantity of microdroplets.

3.6. Characterisation of the Coatings after the Corrosion Tests

3.6.1. Coating Roughness

The roughness of the Cr-based coatings after corrosion tests is presented in Figure 10. The most significant result is related to the roughness increase for all investigated surfaces as a result of corrosive attack, thus we could conclude that all surfaces were affected by the corrosive environment to various extents, as presented in Figure 10 and detailed below.

The roughness parameter Ra of the 304 SS substrate increased from 50 µm before corrosive attack to about 1300 µm (Figure 10a), demonstrating that a significant corrosion process affected the bare substrate. The Cr–N monolayer was also considerably affected by corrosion, the Ra increasing from 281 nm (Figure 8a) before corrosion to 549 nm (Figure 10a). This outcome is in good agreement with the electrochemical results, as the Ra value after corrosion increased from 200 nm to 316 nm. On the contrary, the bilayer with Cr(N,O) on top exhibited an almost similar Ra value before and after the corrosive attack, indicating that the roughness was not the main factor influencing the corrosion behaviour. We should underlie that within the limit of experimental error, the protection efficiency Pe and the roughness parameters Ra and Rp exhibited the same trend. Moreover, the lower roughness measured on the bilayered coatings compared to the monolayered ones might be explained by the cracks and dislocation blocking at layer interfaces.
After the corrosion tests, all of the coated surfaces show negative values of $S_k$ compared to the surfaces before corrosion (Figure 10c), pointing to the formation of more valleys on the corroded surfaces as a consequence of significant corrosive processes taking place locally, where the electric field is more intense due to specific surface morphology. The Cr–N monolayer may well illustrate this conclusion, since compared to all the other coatings, it presented the most negative $S_k$ value and also had the lowest corrosion resistance, as presented in Table 4.

3.6.2. Surface Morphology and Elemental Composition

In order to gain a deeper insight into the corrosion mechanism in relation to the alteration of the roughness parameters after the corrosion tests, we investigated the surface morphology of corroded surfaces. SEM images of the Cr-based coatings after the corrosion test are presented in Figure 11. As can be seen, the uncoated 304 SS substrate was significantly affected by corrosion, the result being in good agreement with the electrochemical tests. Additionally, the surface of the Cr–N monolayer was deteriorated by the corrosive attack, with numerous damaged zones being observed where the coating was cracked. Some corrosion products were also found on coated surfaces. The poor corrosion resistance of Cr–N monolayer was probably due to the high density of microdroplets and high porosity, confirmed by both SEM images and electrochemical tests, allowing easy chloride penetration and reaching the coating–substrate interface, accelerating the corrosion processes.

According to the electrochemical parameters, the following evolution of corrosion resistance can be stated: Cr(N,O) $>$ Cr–N/(Cr(N,O)) $>$ Cr(N,O)/Cr–N $>$ Cr–N $>$ SS. By comparing the profilometry lines on selected pits (Figure 11c), it can be seen that the pits found on uncoated 304 SS substrate were deeper and larger than those found on coated surfaces. The Cr(N,O) coating exhibited the best corrosion behaviour, which also showed the small dimensions of pits that appeared during the corrosion tests. This result supports the electrochemical results.

Figure 12 shows the EDS mapping of the damaged zone found on each investigated coating after the corrosion tests. The elemental compositions of the coatings on SS substrates before and after the corrosion tests are presented in Table 5. A low content of the substrate’s elements was found in coatings with high corrosion resistance, such as Cr(N,O) monolayer and Cr–N/Cr(N,O) bilayer. The
The highest amount of Fe originating from the substrate was detected on the Cr–N monolayer surface, confirming that this coating was significantly affected by the corrosion. In conclusion, the results obtained from SEM and EDS analyses carried out on corroded surfaces sustain the electrochemical results.

**Figure 11.** Investigation of the Cr-based coatings surfaces after the corrosion tests: micrographs of: (a) SEM micrographs at 30× magnification; (b) SEM micrographs at 100× magnification; (c) profilometry lines on selected pits.
Figure 12. Energy dispersive X-ray spectrometry (EDS) mapping micrographs of the Cr-based coatings after the corrosion test.

Table 5. The elemental composition of the investigated specimens before (B) and after (A) the corrosion test in the areas shown in Figure 11a.

| Substrate/Coating (Image Zone) | Elemental Composition (at.%)|  |
|-------------------------------|-----------------------------|--|
| N                             | O                           | Cr | C | Fe               |
| 304 SS (A)                    | –                           | 41.0 ± 2.8  | 9.5 ± 0.1 | –               | 49.5 ± 3.2 |
| Cr–N (B)                      | 30.5 ± 1.2                  | 2.6 ± 0.2  | 63.4 ± 2.5 | 3.5 ± 0.2 | –               |
| Cr–N (A)                      | 22.7 ± 0.8                  | 17.5 ± 0.1 | 56.8 ± 1.8 | –           | 3.0 ± 0.1     |
| Cr(N,O) (B)                   | 35.6 ± 1.7                  | 14.9 ± 0.8 | 46.8 ± 2.2 | 2.6 ± 0.1 | –               |
| Cr(N,O) (A)                   | 32.4 ± 1.5                  | 20.2 ± 0.3 | 46.2 ± 2.1 | –           | 1.2 ± 0.1     |
| Cr–N/ Cr(N,O) (B)             | 36.9 ± 1.7                  | 13.5 ± 0.7 | 49.3 ± 2.2 | 2.2 ± 0.1 | –               |
| Cr–N/ Cr(N,O) (A)             | 35.8 ± 1.5                  | 17.4 ± 0.8 | 46.6 ± 1.8 | –           | 0.5 ± 0.1     |
| Cr(N,O)/Cr–N (B)              | 31.5 ± 1.3                  | 2.8 ± 0.2  | 61.5 ± 2.5 | 4.2 ± 0.2 | –               |
| Cr(N,O)/Cr–N (A)              | 31.1 ± 1.3                  | 22.9 ± 1.3 | 44.1 ± 2.1 | –           | 1.9 ± 0.1     |

4. Conclusions

Cr-based coatings in monolayered (Cr–N and Cr(N,O)) and bilayered structures (Cr–N/Cr(N,O) and Cr(N,O)/Cr–N) were prepared by the cathodic arc method. The presence of Cr2N, CrN, and Cr(N,O), as well as mixtures of these phases were identified and related to the composition of coatings. The oxynitrides were smooth, compact, and homogenously deposited on 304 SS, with few microdroplets. The corrosion protection performance of the developed mono- and bilayered Cr-based coatings was evaluated in 0.10 M NaCl + 1.96 M H2O2.

- The corrosion current densities of the coatings decreased by more than 30 times compared to the bare substrate.
- The Cr–N coating, as mono- or bilayer, had high porosity and lower protective performance.
The protective efficiency of Cr(N,O) coating (99.1%) and porosity (0.007) were excellent when compared to other coatings, because this coating is denser, less porous, and more adherent to the substrate.

Both bilayer coatings substantially improved the corrosion protection of 304 SS.

The bilayer with Cr(N,O) on top possessed the best corrosion resistance behaviour, having the lowest current density corrosion and consequently the highest protective efficiency and the lowest porosity.

The corrosion resistance can be ranked in the following order: Cr(N,O) > Cr–N/Cr(N,O) > Cr(N,O)/Cr–N > Cr–N.

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