Beamforming Design for Intelligent Reflecting Surface-Enhanced Symbiotic Radio Systems

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Abstract—This paper investigates multiuser multi-input single-output downlink symbiotic radio communication systems assisted by an intelligent reflecting surface (IRS). Different from existing methods ideally assuming the secondary user (SU) can jointly decode information symbols from both the access point (AP) and the IRS via multiuser detection, we consider a more practical SU that only non-coherent detection is available. To characterize the non-coherent decoding performance, a practical upper bound of the average symbol error rate (SER) is derived. Subsequently, we jointly optimize the beamformer at the AP and the phase shifts at the IRS to maximize the average sum-rate of the primary system taking into account the maximum tolerable SER constraint for the SU. To circumvent the couplings of variables, we exploit the Schur complement that facilitates the design of a suboptimal beamforming algorithm based on successive convex approximation. Our simulation results show that compared with various benchmark algorithms, the proposed scheme significantly improves the average sum-rate of the primary system, while guaranteeing the decoding performance of the secondary system.

1. INTRODUCTION

Recently, intelligent reflecting surface (IRS)-assisted symbiotic radio (SR) systems [1] have been proposed as one of the promising technologies to achieve spectrally and energy-efficient transmission towards the sixth-generation (6G) communications. By exploiting the IRS, SR systems not only enhance the quality of the primary transmission from the access point (AP) to its primary users (PUs), but also allow the IRS to be served as a secondary transmitter to convey its information to the desired secondary users (SUs). Conventionally, an IRS consists of a large number of low-cost passive reflection elements (REs) and the phase shift of each element can reflect/redirect the incident signals to the desired users in a nearly-passive manner. Thus, the introduction of an IRS can further enhance the quality of primary transmission by providing a controllable additional signal propagation path for dedicated energy-focusing and energy-nulling [2]. On the other hand, in an SR system, an environment sensor serving as an information source can be connected to the IRS [3] for collecting the environmental information such as light intensity, temperature, and humidity. Thus, the IRS has its need to transmit the sensed information to a low data-rate SU. In these scenarios, the IRS can embed its information to the reflected radio frequency signals originating from the AP. As such, a mutualistic SR system can be established by intelligent synergistic resources exchanges. Specifically, the SU shares the same frequency spectrum, energy, and infrastructure with PUs, which results in more spectrally and energy-efficient communications compared with conventional networks [4], [5].

To realize practical IRS-assisted SR systems, various schemes have been proposed. For instance, in [6], [7], the IRS is able to transmit information to the SU by adopting binary phase shift keying modulation to modulate its information over the incident signals from the AP. Yet, having the off state of all IRS elements concurrently reflects the purpose of deploying an IRS as it leads to a low spectral efficiency in end-to-end information transmission in the primary system. To further improve the spectral efficiency of IRS-assisted systems, [3] and [8] adopted a higher order IRS modulation by exploiting spatial modulation over IRS elements. However, the problem formulations in [3] and [8] did not take into account the quality-of-service (QoS) requirement of decoding IRS symbols at the SU. As such, the performance of the SU cannot be guaranteed. Moreover, all the aforementioned papers, i.e., [3], [6–8], ideally assumed that the SU is capable to perform sophisticated multiuser detection or successive interference cancellation for decoding the information symbols of the AP and the IRS jointly, which is generally impossible for a low-cost SU. Besides, without knowing the symbols transmitted by the AP, the effective channel state information (CSI) is generally unknown at the desired SU as it is a product of instantaneous CSI and AP symbols. As a result, it is challenging, if not impossible, for the implementation of the coherent detection proposed in [6], [7]. Thus, a more practical resource allocation design for non-coherent detection in SR systems is desired.

In this paper, we consider an IRS-assisted multiuser multiinput single-output (MISO) downlink multiuser SR system, where the IRS can transmit its information to the SU while assisting the primary transmission between the AP and PUs. In particular, the IRS can modulate its information by applying an on/off multi-level amplitude modulation to the index of the IRS elements. In contrast to existing methods, e.g. [3], [6–8], we investigate a practical SR system which is able to acquire modulated IRS symbols at the SU without decoding AP symbols. In particular, non-coherent detection is adopted at the SU for decoding the IRS symbols. To quantify the decoding performance of the SU, we first derive an upper bound of the average symbol error rate (SER). Furthermore, by jointly designing the precoding vector at the AP and the phase shift matrix at the IRS, the average sum-rate of the primary system is maximized subject to an SER-based constraint for the SU. Due to the coupling among the optimization variables and the explicit expression of the derived SER upper bound, the formulated problem is non-convex such that obtaining an optimal solution in polynomial time is generally intractable. As a compromise, we exploit the Schur complement and adopt...
successive convex approximation (SCA) to obtain a suboptimal solution of the beamforming design problem. Simulation results show that the proposed scheme not only guarantees the decoding performance of the secondary system, but also significantly improves the average sum-rate of the primary system compared with various benchmarks.

Notations: Scalars, vectors, and matrices are represented by lowercase letter $x$, boldface lowercase letter $\mathbf{x}$, and boldface uppercase letter $\mathbf{X}$, respectively. $\mathbb{B}^{N \times M}$ and $\mathbb{C}^{N \times M}$ denote the spaces of $N \times M$ matrices with binary and complex entries, respectively. $\mathbf{X}(n, m)$ denotes the element at the $n$-th row and the $m$-column of the matrix. The Euclidean norm, Frobenius norm of a vector/matrix are denoted by $\| \cdot \|$ and $\| \cdot \|_F$, respectively. The absolute value of a complex-valued scalar is denoted by $| \cdot |$. The occurrence probability of an event is denoted by $\Pr \{ \cdot \}$. The conditional probability density function of $x$ on event $\mathcal{H}$ is denoted by $p(x | \mathcal{H})$. The transpose, conjugate transpose, conjugate, expectation, and trace of a matrix/vector are denoted by $(\cdot)^T$, $(\cdot)^H$, $(\cdot)^*$, $E[\cdot]$, and $\text{Tr}(\cdot)$, respectively. $\mathbf{X} \succeq 0$ and $\mathbf{X} \preceq 0$ mean that matrix $\mathbf{X}$ is positive semi-definite and negative semi-definite, respectively. $\text{diag}(\mathbf{x})$ denotes a diagonal matrix with its diagonal elements given by vector $\mathbf{x}$. $j$ denotes the imaginary unit. The distribution $\mathcal{CN}(\mu, \sigma^2)$ of a circularly symmetric complex Gaussian (CSCG) random variable with mean $\mu$ and variance $\sigma^2$ is denoted by $\mathcal{CN}(\mu, \sigma^2)$ and $\sim$ stands for “distributed as”. The distribution of an Erlang random variable with scale parameter $\alpha$ and shape parameter $n$. $\mathbf{I}_N$ denotes an $N \times N$ identity matrix.

II. SYSTEM MODEL

As shown in Fig. 1, we consider an IRS-assisted SR system, which includes an AP equipped with $N_t > 1$ antennas, an IRS with $M > 1$ elements, $K > 1$ single-antenna PUs, and a single-antenna SU. \footnote{The extension to the case of multiple SUs will be considered in our future work.} In particular, the AP transmits $K$ independent data streams to $K$ PUs simultaneously with the assistance from the IRS. The precoding vector for the $k$-th PU $(\mathbf{P}_{k,l})$ adopted at the AP is defined as $\mathbf{w}_k \in \mathbb{C}^{N_t \times 1}$, $\forall k \in \mathcal{K} = \{1, \ldots, K\}$. Meanwhile, the IRS passively transmits the sensed environmental information of the connected sensor to the SU by altering the IRS reflection patterns via index modulation, which will be detailed in Sections II-B and II-C. The IRS reflection matrix is defined as $\Phi = \text{diag}(e^{j\theta_1}, \ldots, e^{j\theta_M}) \in \mathbb{C}^{M \times M}$ with $\theta_m \in [0, 2\pi)$, $\forall m \in \mathcal{M} = \{1, \ldots, M\}$, denoting the phase shift at the $m$-th IRS element. For the ease of practical implementation of the IRS, the amplitude coefficients of all the elements are fixed to be unity in this paper. Besides, as depicted in Fig. 1, the direct links of AP-to-PUs and AP-to-SU are blocked due to heavy shadowing. The aforementioned assumptions are commonly adopted in the literature [2], [4], [5]. On the other hand, this paper considers a quasi-static flat fading channel model. We assume that handshaking has been performed between the AP, PUs, and the SU at the beginning of transmission. As such, the channel coefficients of the AP-to-IRS link, the IRS-to-PU link, and the IRS-to-SU link can be acquired by exploiting some existing advanced channel estimation methods, e.g. [9], which are denoted by $\mathbf{G} \in \mathbb{C}^{M \times N_t}$, $\mathbf{h}_{P,k} \in \mathbb{C}^{M \times 1}$, and $\mathbf{h}_S \in \mathbb{C}^{M \times 1}$, respectively.

A. Transmission Framework

Fig. 2 shows the transmission frame structure of the considered IRS-assisted SR network, where the AP and the IRS simultaneously transmit their information symbols. In particular, $s_q \in \mathbb{B}^{M \times 1}$ denotes the IRS symbol to be transmitted in each IRS transmission frame, which spans over a pilot sequence and $L$ AP symbols, $c_k(l) \sim \mathcal{CN}(0, 1)$, $\forall k, l \in \mathcal{L} = \{1, \ldots, L\}$.

Although $s_q$ is unknown at the PUs, at the beginning of each IRS transmission frame, the AP emits some pilot symbols that allows the PUs to obtain the effective CSI at the receiver (CSR) of the cascaded AP-to-IRS-to-PU link with existing techniques, e.g. [9]. As such, the PUs are able to apply coherent detection to decode their information symbols. On the other hand, in contrast to the existing works, e.g. [3], [6]–[8], the SU is assumed to be a practical receiver which does not equip with powerful computational capability to perform joint decoding of $c_k(l)$ and $s_q$. Without knowing AP symbols $c_k(l)$, the phase of the instantaneous CSI of the cascaded AP-to-IRS-to-SU link cannot be obtained for performing conventional coherent detection. In this case, a non-coherent detection \footnote{The extension to the case of multiple SUs will be considered in our future work.} is adopted at the SU for decoding $s_q$.

B. Signal Model

1) Transmitted Signal at the AP: For each AP transmission frame, the transmitted signal at the AP is given by

$$c(l) = \sum_{k \in \mathcal{K}} \mathbf{w}_k c_k(l), \forall l \in \mathcal{L}. \quad (1)$$

2) Reflected Signal at the IRS: As only non-coherent detection can be performed at the SU, we introduce a multi-level amplitude modulation. In particular, the IRS consists of $Q > 1$ information-carrying elements (ICEs) and $M - Q$ REs. With the similar idea as in [11], switching on/off among the ICEs can modulate the information into the signal swing of reflected
Table I: A truth table of the proposed multilevel amplitude modulation scheme at the IRS with $Q=3$ ICES and $M-Q$ REs.

| ICE 1 | ICE 2 | ICE 3 | All REs |
|-------|-------|-------|---------|
| Level 1 | 0 | 0 | 0 | X |
| Level 2 | 0 | 0 | 1 | X |
| Level 3 | 0 | 1 | 1 | X |
| Level 4 | 1 | 1 | 1 | X |

$X = \text{Don't care}$

...signals from the IRS, by creating the required multiple power level signals. The remaining REs is in the “on” state at each IRS symbol duration to reflect the impinging signals. Note that ICES in the “on” state reflect impinging signals as well but with its index modulated. Based on this, the transmitted IRS symbol is denoted by $s_q = [s_{1q}, \ldots, s_{mq}, \ldots, s_{Mq}]^T$, $\forall q \in Q = \{1, \ldots, Q + 1\}$, $s_{mq} \in \{0, 1\}$ denotes the on/off state of the $m$-th IRS element when IRS transmitting symbol $s_q$, i.e., $s_{mq} = 0$ and $s_{mq} = 1$ denote that the $m$-th IRS elements is turned “off” and “on”, respectively. The truth table in Table I shows an example of the proposed modulation scheme. In this case, there are $Q + 1$ possible on/off patterns. Without loss of generality, we assume that $(Q + 1)$ is a power of 2. Hence, each IRS symbol contains $\log_2(Q + 1)$ IRS information bits. Since all IRS reflection patterns are assumed to be transmitted equiprobably. We have $\mathbb{P}(\hat{H}_q) = \frac{1}{2^{Q+1}}$, where $\hat{H}_q$ is the hypothesis of the IRS sending symbol $s_q$.

3) Received Signal at PUs: For each AP transmission frame, the received signal at PU_k is given by

$$y_{p,k}(l) = h_{p,k}^H S_q \Phi \Phi c(l) + n_k(l), \forall k, l,$$  \tag{2}

where $S_q = \text{diag}(s_q)$ and $n_k(l) \sim \mathcal{CN}(0, \sigma_n^2)$ denotes the background noise at PU_k with power $\sigma_n^2$. Since $s_q$ remains unchanged during the $L$ AP symbol durations, the achievable rate for PU_k to decode $c_k(l)$ is given by

$$R_{k,q}^\text{PU} = \log_2 \left( 1 + \frac{|h_{p,k}^H S_q \Phi \Phi c(l)|^2}{\sum_{j \neq k} |h_{p,k}^H S_q \Phi \Phi c(l)|^2 + \sigma_n^2} \right),$$  \tag{3}

where $h_{p,k} = \text{diag}(h_{p,k}^H)$. Although the CSIR of the cascaded AP-IRS-PU_k link, i.e., $h_{p,k}^H S_q \Phi \Phi$, is known at the PU_k, the AP has no prior knowledge of $s_q$ while optimizing $w_k$ and $\Phi$. Hence, to facilitate the precoding and IRS reflection coefficients design, the average achievable rate of PU_k is adopted. To this end, the expectation of $R_{k,q}^\text{PU}$ is taken over $s_q$ as

$$\overline{R}_{k,q}^\text{PU} = \mathbb{E}_{s_q}[R_{k,q}^\text{PU}],$$  \tag{4}

4) Received Signal at SU: Since each IRS transmission frame spans $L$ AP symbol durations, the received signal at the SU for each IRS transmission frame is given by

$$y_{s} = [y_{s}(1), \ldots, y_{s}(l), \ldots, y_{s}(L)]^T,$$  \tag{5}

where

$$y_{s}(l) = h_{q}^H S_q \Phi \Phi c_l + n_q(l) = s_l^Q H_{q} \Phi \Phi c_l + n_q(l), \forall l,$$

being the received signal of the SU at the $l$-th observation, where $H_q = \text{diag}(h_{q}^H)$ and $n_q(l) \sim \mathcal{CN}(0, \sigma_q^2)$ denotes the noise at the SU with power $\sigma_q^2$. As the SU does not have the prior knowledge of $c_k(l)$, the effective CSIR of the cascaded AP-IRS-SU link, $\Phi H_{q} \Phi \Phi$, is not available at the SU. Fortunately, the distribution of the AP symbols is $c_k(l) \sim \mathcal{CN}(0, 1)$ such that the distribution of $y_{s}(l)$ is available at the SU, i.e., $y_{s}(l) \sim \mathcal{CN}(0, P_{s} + \sigma_q^2)$, where $P_{s} = \sum_{k=1}^{K} \text{Tr}(s_{k}^Q H_{q} \Phi \Phi c_l H_{q} \Phi \Phi s_{k})$. As a result, the distribution of the received signal power at the SU is $\sum_{l=0}^{L} y_{s}^2(l) \sim \text{Erlang}(\frac{1}{\lambda_q}, L)$ with $\lambda_q = (P_{s} + \sigma_q^2)^{-1}$, $\forall q \in Q$. Therefore, we adopt the non-coherent detection method to detect the modulated IRS symbols at the SU via

$$[i] = \arg \max_{q \in \mathcal{Q}} p\left( \sum_{l \in \mathcal{L}} y_{s}^2(l) | \mathcal{H}_q \right) \Pr(\mathcal{H}_q),$$  \tag{6}

where

$$p\left( \sum_{l \in \mathcal{L}} y_{s}^2(l) | \mathcal{H}_q \right) = \frac{\lambda_q^L \left( \sum_{l \in \mathcal{L}} y_{s}^2(l) \right)^{L-1} e^{-\lambda_q \sum_{l \in \mathcal{L}} y_{s}^2(l)}}{(L-1)!}.$$  \tag{7}

It can be observed from (6) that the non-coherent detection performance can be improved by exploiting $\lambda_q$ and $y_{s}$ in (7), which can be achieved by optimizing the precoder at the AP and IRS phase shifts.

To characterize the detection performance of the SU, we first derive an SER upper bound $P_{s}^{\text{upper}}$, by adopting the well-known union bounding technique, whose tightness has been verified in [12], that yields

$$P_{s}^{\text{upper}} = \sum_{q=1}^{Q+1} \sum_{l=1,q=1} \Pr \{ s_q \rightarrow s_i | \mathcal{H}_q \} \Pr(\mathcal{H}_q),$$  \tag{10}

where $\Pr \{ s_q \rightarrow s_i | \mathcal{H}_q \}$ is the pairwise error probability in deciding $s_q$ to $s_i$, $\forall i \neq q$, under the hypothesis $\mathcal{H}_q$. According (6), the total error probability of the hypothesis $\mathcal{H}_q$ is

$$P_{s}^{\text{upper}} = \sum_{q=1}^{Q+1} \Pr \{ s_q \rightarrow s_i | \mathcal{H}_q \},$$  \tag{11}

where

$$P_{s}^{\text{upper}} = \sum_{q=1}^{Q+1} \gamma(L, L \lambda_q d_q),$$  \tag{10}

where $\gamma(L, L \lambda_q d_q)$ is the incomplete Gamma function and the upper incomplete Gamma function, respectively.

III. PROBLEM FORMULATION

We aim to maximize the average achievable sum-rate of the primary system while guaranteeing the power budget at the AP and the QoS requirements of the SU by jointly designing the precoding vectors $w_k$, $\forall k$, and the phase shifts $\theta_m, \forall m$. The joint design can be formulated as the following:

$$\text{maximize} \sum_{k \in \mathcal{K}} \overline{R}_{k,q}^\text{PU} \text{subject to} \sum_{k \in \mathcal{K}} \|w_k\|_2^2 \leq P_{\text{max}}, \forall k \in \mathcal{K},$$  \tag{11}

s.t. C1: $P_{s}^{\text{upper}} \leq P_{s}^{\text{max}}$, C3: $0 < \theta_m \leq 2\pi, \forall m \in \mathcal{M}$. Constraint C1 ensures that the transmit power consumption of the precoder at the AP is less than the maximum available power budget $P_{s}^{\text{max}}$. Constraint C2 is imposed to restrict the upper bound of the SER for decoding the modulated
In particular, the couplings among optimization variables $C_2c_3$ and $C_2c_4$ are convex w.r.t.

Also, and $\lambda$ in the next section. prohibited even for a moderate system size. As an alternative, application of a brute-force search is required for obtaining their equivalent forms, such that they are convex with respect to the highly coupled variables. We first in-

transformed optimization problem. $w$ can only vary from 0 to $2\pi$. The formulated problem is non-convex due to the non-convexities in both the upper and lower incomplete Gamma functions in constraint C2 and the couplings among optimization variables $w_k$ and $\theta_m$ in both the objective function and constraint C2. In general, the application of a brute-force search is required for obtaining the globally optimal solution of (13), which is computationally prohibited even for a moderate system size. As an alternative, a computationally efficient suboptimal algorithm is proposed in the next section.

IV. SOLUTION OF THE OPTIMIZATION PROBLEM

To address the proposed optimization problem in (11), we first transform the objective function and constraint C2 into their equivalent forms, such that they are convex with respect to (w.r.t.) $\Phi_{H_P,G_{w_k}}$, $\forall k,j$, and $\Phi_{H_P,G_{w_k}}$, $\forall k,j$, respectively. Then, we decouple the coupling between optimization variables $w_k$ and $\theta_m$ by utilizing the Schur complement. Finally, SCA is applied to address the non-convex constraints in the transformed optimization problem.

As shown in (5) and (11), constraint C2 in (11) is non-convex due to the highly coupled variables. We first introducing auxiliary optimization variables $\gamma_q$, $\Gamma_q$, $\xi_q^1$, $\xi_q^2$, $\xi_q^3$, $\tau^1_q$, and $\tau^2_q$, $\forall q,j$, for decoupling. Then, by exploiting the properties of logarithm and quadratic equation, constraint C2 can be equivalently transformed as:

$$C2a: \sum_{q=2}^{Q+1} \gamma_q + \sum_{q=1}^{Q} \Gamma_q \leq (Q + 1)P^\text{max},$$

$$C2b1: -Le_\gamma^1 + \ln \xi_q^1 \geq \ln(1-\gamma_q), C2b2: \xi_q^1 \leq \sum_{l=0}^{L} \left( \frac{Le_\gamma^2 l!}{l!} \right), \forall q,j,$$

$$C2b3: P_{\sigma_q} - \sum_{l=0}^{L} \left( \frac{Le_\gamma^2 l!}{l!} \right), \forall q,j,$$

$$C2b4: \rho_q - \sum_{l=0}^{L} \left( \frac{Le_\gamma^2 l!}{l!} \right), \forall q,j,$$

$$C2c1: \gamma_q + \ln \xi_q^1 \geq \ln \Gamma_q, C2c2: \xi_q^1 \leq \sum_{l=0}^{L} \left( \frac{Le_\gamma^2 l!}{l!} \right), \forall q,j,$$

$$C2c3: \rho_q - \sum_{l=0}^{L} \left( \frac{Le_\gamma^2 l!}{l!} \right), \forall q,j,$$

$$C2c4: \rho_q - \sum_{l=0}^{L} \left( \frac{Le_\gamma^2 l!}{l!} \right), \forall q,j,$$

In particular, $\gamma_q$, $\Gamma_q$, $\xi_q^1$, and $\xi_q^3$ replace $\gamma(L, L\lambda d_q^{-1}), \Gamma(L, L\lambda d_q^{-1}), \sum_{l=0}^{L} \left( \frac{Le_\gamma^1 l!}{l!} \right)$, and $\sum_{l=0}^{L} \left( \frac{Le_\gamma^1 l!}{l!} \right)$ in constraint C2, respectively. Besides, $\xi_q^1$ and $\xi_q^3$ replace $\lambda d_q^{-1}$ and $\lambda d_q^{-1}$ in $e^{-L\lambda d_q^{-1}}$ and $e^{-L\lambda d_q^{-1}}$ of constraint C2, respectively. Also, $\xi_q^2$ and $\xi_q^2$ replace $\lambda d_q^{-1}$ and $\lambda d_q^{-1}$ in $e^{-L\lambda d_q^{-1}}$ and $e^{-L\lambda d_q^{-1}}$ of constraint C2, respectively. It can be verified that constraints C2b3, C2b4, C2c3, and C2c4 are convex w.r.t. $\Phi_{H_P,G_{w_k}}$ that paves the way for further simplification in the sequel.

On the other hand, since $s_p$ has a finite number of choices, i.e., $Q + 1$, the average achievable capacity in (4) can be directly expressed as $R_k = \sum_{q=1}^{Q+1} \frac{H_{SU}}{Q+1} P_k \{ H_q \}$. Thus, the objective function in (11) can be equivalently transformed to a new objective function as

$$f_0 = \frac{1}{Q+1} \sum_{q=1}^{Q+1} \left( \log_2 \left( \sum_{j=1}^{K} P_{k,j}^\text{PU} + \gamma_q \right) - \log_2 \left( \sum_{j=1}^{K} P_{k,j}^\text{PU} + \sigma_q^2 \right) \right),$$

where $P_{k,j}^\text{PU} = \text{Tr}(s_j^T \Phi_{H_P,G_{w_k}} w_h^H G_{H_P,K}^H \Phi_{H_P,K} s_j), \forall k,j, q$. Next, we decouple the coupled variables $\{ w_k, \Phi \}$ in the objective function in (13) via utilizing the Schur complement. We first introduce auxiliary optimization variables $\Phi_{H_P,G_{w_k}} \in C^{M \times 1}, \text{U}_{k,j} \in C^{M \times M}, c_{k,j}, \forall k,j$, and $A \in C^{M \times M}$. Then, by substituting $\Phi_{H_P,G_{w_k}} w_h^H G_{H_P,K}^H \Phi_{H_P,K} = \text{U}_{k,j}^\text{PU}$ into (13), the objective function in (13) and constraint C3 in (11) can be equivalently transformed as

$$f_0 = \frac{1}{Q+1} \sum_{q=1}^{Q+1} \left( \log_2 \left( \sum_{j=1}^{K} P_{k,j}^\text{PU} + \gamma_q \right) - \log_2 \left( \sum_{j=1}^{K} P_{k,j}^\text{PU} + \sigma_q^2 \right) \right),$$

where $P_{k,j}^\text{PU} = \text{Tr}(s_j^T \Phi_{H_P,G_{w_k}} w_h^H G_{H_P,K}^H \Phi_{H_P,K} s_j), \forall k,j, q$.
maximize \( \frac{1}{Q+1} \sum_{q=0}^{Q} \sum_{r=1}^{K} \left( \log_2 \left( \sum_{j=1}^{K} P^{PU}_{q,k,j} + \gamma_q \sigma^2 \right) \right) - \log_2 \left( \sum_{j=1}^{K} P^{PU}_{q,k,j} \right) - \sum_{j=1}^{K} \left( P^{PU}_{q,k,j} - P^{PU}_{q,k,j} / (\ln(2)) \right) \left( \sum_{j=1}^{K} P^{PU}_{q,k,j} + \gamma_q \sigma^2 \right) \)

s.t. C1, C2a, C2b1, C2c2, C2d1, C2d3, C3a, C3b, C4a, C4c,

C2b1: \( x_q^q = 0 \sum_{l=0}^{L/2} \left( L_{2q}^{(r)} / 2 \right) + \sum_{l=0}^{L/2} \left( L_{2q}^{(r)} / 2 \right) \left( \gamma_q^r - \gamma_q^r \right) \), \( \forall q \).

C2b2: \( \tilde{P}_{q,k} - \tilde{P}_{q,k} - \left( \gamma_q^r + \gamma_q^r \right)^2 - (\gamma_q^r - \gamma_q^r)^2 - (\gamma_q^r - \gamma_q^r)^2 - 2(\gamma_q^r + \gamma_q^r)^2 - 2(\gamma_q^r + \gamma_q^r)^2 \), \( \forall q \).

C2c1: \( -L_{q}^{(r)} + \ln(\gamma_q^r) + (\gamma_q^r - \gamma_q^r) \ln(\gamma_q^r) \leq 0, \forall q \).

C2c2: \( \tilde{P}_{q,k} - \tilde{P}_{q,k} - \left( \gamma_q^r + \gamma_q^r \right)^2 - (\gamma_q^r - \gamma_q^r)^2 - 2(\gamma_q^r + \gamma_q^r)^2 - 2(\gamma_q^r + \gamma_q^r)^2 \), \( \forall q \).

C2c3: \( \tilde{P}_{q,k} - \tilde{P}_{q,k} - \left( \gamma_q^r - \gamma_q^r \right)^2 - (\gamma_q^r - \gamma_q^r)^2 - 2(\gamma_q^r + \gamma_q^r)^2 - 2(\gamma_q^r + \gamma_q^r)^2 \), \( \forall q \).

C2d1: \( \text{Tr}(U_{SU}) \leq -\|E_{SU}(r)\|_2^2 + 2\text{Tr} \left( (E_{SU}(r))^H E_{SU}(r) \right) \).

C2d2: \( \text{Tr}(D_{SU}) \leq -\|E_{SU}(r)\|_2^2 + 2\text{Tr} \left( (E_{SU}(r))^H E_{SU}(r) \right) \).

Since constraints C2b1, C2b2, C2b3, C2b6, C2c1, C2c3, C2c4, C2c6, C2d2, C2d4, C4b, C4d and the objective function in problem (16) are in the difference of convex (D.C.) functions form and differentialable, we apply an iterative method based on SCA to obtain a suboptimal solution. Taking constraint C2b1 as an example, for any feasible point \( \gamma_q^r \), an upper bound of \( \ln(1 - \gamma_q^r) \) can be construct by deriving its first-order Taylor expansions:

\[ \ln(1 - \gamma_q^r) \leq 1 - (1 - \gamma_q^r) + (\gamma_q^r - \gamma_q^r) / (\gamma_q^r - 1), \]

where \( \gamma_q^r \) denotes the iteration index for the proposed algorithm summarized in Algorithm 1 (to be discussed in detail later). By applying SCA, a subset of constraint C2b1 can be obtained, which is given by

C2b1: \(-L_{q}^{(r)} + \ln(\gamma_q^r) - T_q^r \geq 0, \forall q \).

As C2b1 implies C2b1, replacing C2b1 with C2b1 can ensure that the former is satisfied when the proposed algorithm converges. Similarly, by applying SCA to the rest of D.C. functions in problem (16), a lower bound of (16) can be obtained via solving the optimization problem in (19) at the top of this page. To tighten the obtained performance lower bound, we iteratively update the feasible solution by solving the optimization problem in (19) in the \( (r) \)-th iteration. The proposed SCA-based algorithm is shown in Algorithm 1 and the proof of its convergence to a suboptimal solution can be found in (15) which is omitted here for brevity. Note that the proposed algorithm has a polynomial time complexity.

V. NUMERICAL RESULTS

This section evaluates the system performance of the proposed scheme via simulation. We set \( K = 2, Q = 3, N_t = 4, \)

\( M = 30, L = 30 \). The location of AP, IRS, SU, and PUs are set in a Cartesian coordinate system, i.e., \((0,0), (15,10), (20,2), \) and \((65, 2), (65, -2) \) in meters (m), respectively. The distance-dependent path loss model in (2) is adopted with a reference distance of 1 m. Other important parameters are summarized as follows unless specified otherwise. The centre carrier frequency is set as 2.4 GHz. The path loss exponents of AP-IRS, IRS-SU, and IRS-PU links are identical for simplicity, i.e., \( \alpha_{AI} = \alpha_{AI} = \alpha_{IP,K} = 2.2 \). Rician factors of AP-IRS, IRS-SU, and IRS-PU links are \( \beta_{AI} = \beta_{IS} = \beta_{IP,K} = 3 \). The maximum power budget at the AP is \( P_{max} = 30 \) dBm. Noise power at the SU and PUs are \( \sigma_q^2 = \sigma_q^2 = -100 \) dBm.

For comparison, we also evaluate the system performance of three other schemes: 1) Baseline scheme 1 is identical to the proposed scheme except that the QoS of the SU constraints is not considered; 2) Baseline scheme 2 is the same as the proposed scheme except that the phase shifts of the reflect elements are randomly set; 3) A performance upper bound approach to meet QoS requirements of constraint C2 in (11), we set the system sum-rate for that channel realization as zero to account the penalty for the corresponding failure.
The average system sum-rate of the primary system is given by $P_{\text{max}}$, which is not suitable for most practical applications. By comparing the average sum-rate of the proposed scheme and the upper bound, it can be observed that there is a performance gap between the proposed scheme and the upper bound when $P_{\text{max}}$ is small. This is mainly because the IRS phase shifts are forced to align to the channels of the SU for satisfying the more stringent SER constraint. This leads to a weakened signal received at the PU. However, unlike the proposed scheme, the upper bound cannot serve the primary and secondary system concurrently to realize a mutualistic SR system. Once constraint $C2$ becomes less stringent, the performance degradation of the proposed scheme is negligible compared with the upper bound, even though the proposed scheme turns off some of the IRS elements to convey IRS modulated information. On the other hand, as $P_{\text{max}}$ increases, the performance of all the schemes approaches a constant. This is because the limited transmit power budget $P_{\text{max}}$ becomes the bottleneck of system performance, instead of $P_{\text{max}}$. In Fig. 4, by further increasing the maximum transmit power budget at the AP, the system sum-rate increases monotonically. Indeed, by applying the proposed scheme, the AP and the IRS can effectively exploit the additional transmit power to create more powerful beamforming for improving the system sum-rate of the primary system. Moreover, the average sum-rates for both the proposed scheme and baseline scheme 2 grow as the number of the antennas at the AP increases due to an increasing beamforming gain. However, diminishing return appears when $N_t$ is large as the result of channel hardening.

VI. CONCLUSION

In this paper, we proposed a MISO downlink SR communication system assisted by an IRS, which facilitates the primary transmission and mutualistic information transmission to the SU simultaneously. Different from existing works, we considered a more practical secondary system adopted a non-coherent detection at the SU. We derived an SER upper bound to characterize the non-coherent decoding performance. The joint design of the beamformer at the AP and the phase shifts at the IRS was formulated as a non-convex optimization problem to maximize the average system sum-rate taking into account the QoS requirement of decoding IRS symbols at the SU. Simulation results showed that the proposed scheme greatly enhances the performance of both the primary system and the secondary system significantly compared with some existing schemes.

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