Scanning Electron Microscopy Investigation of Surface Acoustic Wave Propagation in a 41° YX-Cut of a LiNbO₃ Crystal/Si Layered Structure

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Abstract: The propagation process of the surface acoustic waves (SAW) and the pseudo-surface acoustic waves (PSAW) in a bonded layered structure of a 41° YX-cut of a LiNbO₃ crystal/Si(100) crystal was investigated. The scanning electron microscopy (SEM) method, in the low-energy secondary electrons registration mode, made it possible to visualize the SAW and PSAW in the LiNbO₃/Si layered structure. The process of the SAW and PSAW propagation in a LiNbO₃/Si layered structure and in a bulk 41° YX-cut of a LiNbO₃ crystal were compared. It was demonstrated that the SAW velocities in the layered LiNbO₃/Si structure exceed the typical SAW velocities for LiNbO₃ and Si single crystals. In the layered structure, the SAW and PSAW velocities were 4062 m/s, 4731 m/s, and 5871 m/s. It was also demonstrated that the PSAW velocities are the same in the LiNbO₃/Si layered structure and in the bulk 41° YX-cut of a LiNbO₃ crystal.

Keywords: LiNbO₃ crystal; Si crystal; surface acoustic wave; X-ray diffraction; scanning electron microscopy; LiNbO₃/Si layered structure

1. Introduction

Ferroelectric LiNbO₃ and LiTaO₃ crystals are widely used in acoustoelectronics, acousto-optics, and optoelectronics as materials with excellent piezoelectric, acoustic, and optical properties [1–3]. In recent years, much attention has been paid to the possibility of creating layered structures using ferroelectric LiNbO₃ and LiTaO₃ crystals and semiconductor Si crystals [4–6]. The layered structure is formed by bonding two wafers of LiNbO₃ (or LiTaO₃) and Si, followed by the thinning of the ferroelectric wafer to a thickness of a few micrometers, using grinding and polishing methods. This makes it possible to solve a whole range of problems in acoustoelectronics. First, is the reduction in the temperature coefficient of the frequency in acoustoelectronics [7–9]. In acousto-optics and optoelectronics, layered structures allow for the creation of planar optical waveguides and optical resonators in a thin layer of ferroelectric crystal [10–14]. The presence of a thin layer of ferroelectric crystal greatly simplifies the process of creating waveguide structures by Ti implantation or proton exchange methods. Moreover, the thin crystal layers of LiNbO₃ and LiTaO₃ ferroelectric crystals allow for the formation of nanoscale domain structures [15–17].

In recent years, the 3D integration of chips and processors in microelectronics has been implemented and interposers have been fabricated [18,19]. In the near future, there lies the possibility of integrating semiconductor, acoustoelectronic, and optoelectronic devices into a single 3D chip. In this case, the creation of layered LiNbO₃/Si structures is of fundamental importance for the integration of acoustoelectronic, sensor, and optoelectronic devices into semiconductor processors.

This work investigates the propagation process of the surface acoustic wave in the LiNbO₃/Si layered structure. Usually, to study the acoustic properties of materials, the
amplitude–frequency response is measured, which is based on measuring the conversion of
the input high-frequency electrical signal into acoustic vibrations of the crystal lattice [1,2].
However, this method does not provide direct information about the process of SAW
excitation and propagation in solids. X-ray diffraction [20–24], topography [25–29], and the
scanning electron microscopy method [30–32] can be used to study the process of acoustic
wave propagation in solids. The X-ray diffraction method is based on the process of X-ray
diffraction on the crystal lattice modulated by SAW. SAW propagation in crystals leads to
a sinusoidal modulation of the crystal lattice, which, in turn, leads to the appearance of
the diffraction satellites on the rocking curve on both sides of the Bragg peak [24]. If the
angular divergence between the diffraction satellites on the rocking curve is determined by
the SAW wavelength, then the number of diffraction satellites and their intensity depend
on the SAW amplitude. Thus, this method allows one to determine the amplitudes and
wavelengths of the SAW. Moreover, the X-ray diffraction method makes it possible to study
the SAW propagation process in layered structures as well. Thus, [23] the SAW propagation
process was investigated in a ZnO/Si structure, which demonstrated the difference in the
SAW propagation (difference in SAW velocities) in silicon, in silicon covered by ZnO film,
and at the ZnO/Si interface.

The X-ray topography method allows for the visualization of the SAW propagation
process on the crystal surface in real-time mode at synchrotron radiation sources. There are
two approaches to visualize the acoustic wave fields on the crystal surface. The first one is
based on the implementation of the stroboscopic X-ray topography method, when a pulsed
modulation of synchrotron radiation with the frequency of the SAW excitation is carried
out. In this case, the SAW and synchrotron radiation are synchronized with each other and
in the Fresnel diffraction region, one can observe the SAW image at a distance determined
by the wavelength and amplitude of the SAW [25,27]. The second approach is simpler
and allows for the use of the Talbot effect for the SAW imaging on the third-generation
synchrotron radiation sources. Third generation and higher synchrotron radiation sources
possess radiation with space–time coherence, which allows for the Talbot effect to be used
for visualization of the periodic structures [28,29]. A SAW is a strictly periodic structure
with a period equal to the SAW wavelength. The SAW image can be observed at a Talbot
distance determined by the X-ray wavelength and the SAW wavelength. This method also
makes it possible to determine the SAW wavelengths and amplitudes, to study the SAW
interaction with the crystal structure defects, and to visualize the diffraction phenomena in
acoustic beams and acoustic energy flow drift.

The simplest and most effective method for studying the SAW propagation process
is the scanning electron microscopy method, which allows one to visualize the SAW
propagation in piezoelectric and ferroelectric crystals [30–32]. The SEM method is based
on the sensitivity of the low-energy secondary electrons to electric fields between the
SAW minima and maxima on the surface of piezoelectric and ferroelectric crystals. This
method, as well as the method of X-ray topography, allows one to determine the SAW
wavelength, to study the diffraction phenomena of acoustic beams, and to visualize the
acoustic energy flow.

In this work, the scanning electron microscopy method was used to study the process
of the SAW excitation and propagation in a bonded LiNbO$_3$/Si layered structure.

2. Fabrication of the LiNbO$_3$/Si Layered Structure and Electrical Characterization

The LiNbO$_3$/Si layered structure was formed by bonding two wafers (a 41° YX-cut of
a LiNbO$_3$ crystal and a Si(100) crystal) 100 mm in diameter and 250 µm thick at 600 °C. The
wafers were aligned so that the base cuts were parallel. Then, the wafer of the 41° YX-cut
of a LiNbO$_3$ crystal was thinned by grinding and subsequent polishing. Figure 1 shows
the SEM microphotograph of a cross-section view of the LiNbO$_3$/Si layered structure. A
good-quality interface between the LiNbO$_3$ and Si crystals can be observed at the figure.
The layer thickness of the LiNbO$_3$ crystal is near 8 µm.
During cooling, the materials have different coefficients of thermal expansion, which leads to the appearance of deformations in the crystal lattices. In this case, the deformations occur at the LiNbO$_3$ crystal and the Si crystal. The use of intense synchrotron radiation made it possible to measure the rocking curves of the layered structure for the LiNbO$_3$ crystal layer and the underlying Si crystal layer. Figure 2 shows the measured rocking curves of the 41° YX-cut of a LiNbO$_3$ crystal (a) and the Si(100) crystal (b). In the 41° YX-cut of a LiNbO$_3$ crystal, planes (012) and (024) were parallel to the crystal surface. The rocking curve of the LiNbO$_3$ crystal was measured for the reflection from the planes (024). The value of the Bragg angle was $\Theta_{(024)} = 24.511^\circ$, and the full width at half maximum of the rocking curve was $FWHM_{(024)} = 0.006^\circ$. In the case of the Si crystal, the rocking curve was measured for reflection from the planes (400). In this case, the value of the Bragg angle was $\Theta_{(400)} = 49.034^\circ$, and the full width at half maximum of the rocking curve was $FWHM_{(400)} = 0.010^\circ$. The calculated values of the full width at half maximum of the rocking curve were $FWHM_{(024)} = 0.0022^\circ$ for the 41° YX-cut of a LiNbO$_3$ crystal and $FWHM_{(400)} = 0.0011^\circ$ for the Si(100) crystal. The difference between the experimental and calculated values of the full widths at half maximum of the rocking curves of the LiNbO$_3$ and Si crystals indicates the distortion of the crystal lattices during bonding. In this case, the deformations occur at the LiNbO$_3$/Si interface because the materials are bonded at high temperatures of ~600 °C. The materials have different coefficients of thermal expansion, which leads to the appearance of deformations in the crystal lattices during cooling.

To study the SAW propagation in the LiNbO$_3$/Si layered structure, the structures of the interdigital transducers (IDT) were fabricated on the LiNbO$_3$ crystal surface by photolithography method to excite the SAW with a wavelength of $\Lambda = 30 \mu m$. The IDT consists of 26 pairs of aluminum electrodes, and the IDT aperture is equal to 60 SAW wavelengths (1.8 mm). The width and thickness of the Al-electrode is 7.5 $\mu m$ and 100 nm, respectively. The velocities of the SAW and PSAW propagation in the 41° YX-cuts of a LiNbO$_3$ crystal are $V_{SAW} = 3641 \text{ m/s}$ and $V_{PSAW} = 4749 \text{ m/s}$, respectively [33]. The presence of a thin crystal LiNbO$_3$ layer allows the excitation of the SAW with higher velocity in the LiNbO$_3$/Si layered structure, which should propagate along the [110] direction. The SAW velocity in the Si(100) along direction [110] did not exceed 5080 m/s [34,35]. A number of

![Figure 1. Cross-section view of the LiNbO$_3$/Si layered structure.](image-url)
papers [6,36] have demonstrated that the SAW and PSAW velocities in layered structures can exceed the velocities of their respective bulk crystals. In comparison, a similar IDT structure was also fabricated on the surface of a bulk 41° YX-cut of a LiNbO₃ crystal.

![Figure 2](image_url)

**Figure 2.** Rocking curves of the LiNbO₃/Si layered structure: (a) LiNbO₃, reflection (024); (b) Si, reflection (400).

Figure 3 shows the electrical characterization S11 of the LiNbO₃/Si layered structure (red line) and the 41° YX-cut of a LiNbO₃ crystal (blue line) under the SAW and PSAW excitation at a wavelength of Λ = 30 μm. The three resonances can be observed in the figure for the LiNbO₃/Si layered structure. The first resonance is observable at a frequency of f = 135.4 MHz and corresponds to the SAW excitation in a thin crystal layer of the 41° YX-cut of a LiNbO₃ crystal. In this case, the SAW propagation velocity is $V_{SAW} = f \times Λ = 135.4 \times 30 = 4062$ m/s, which exceeds the value of the SAW velocity on the surface of the 41° YX-cut of a thick LiNbO₃ crystal ($V_{SAW} = 3641$ m/s) [33]. The second resonance at the frequency of $f = 157.7$ MHz corresponds to the PSAW excitation in a thin crystal layer of the 41° YX-cut of a LiNbO₃ crystal. This resonance is very intense because of the high value of the electromechanical coupling coefficient for the PSAW in the 41° YX-cut of a LiNbO₃ crystal $K_{PSAW}^2 = 15.56\%$, while the electromechanical coupling coefficient for the SAW is only $K_{SAW}^2 = 0.22\%$ [33]. The PSAW propagation velocity is $V_{PSAW} = 157.7 \times 30 = 4731$ m/s, which corresponds to the value of the known PSAW velocity in the 41° YX-cut of a LiNbO₃ crystal ($V_{PSAW} = 4749$ m/s) [33]. The third resonance at $f = 195.7$ MHz corresponds to the SAW excitation in the LiNbO₃/Si layered structure. In this case, the velocity of the SAW propagation is $V_{SAW} = 195.7 \times 30 = 5871$ m/s, which exceeds the value of the SAW and PSAW velocities in the Si(100) along the [110] direction ($V_{SAW} = 5080$ m/s, $V_{PSAW} = 5570$ m/s) [35–38].

Only two resonances can be observed for the 41° YX-cut of a LiNbO₃ crystal on Figure 3. The first resonance at $f = 123.1$ MHz corresponds to the SAW with a velocity of $V_{SAW} = 3639$ m/s, which correlates with the known velocity value for the 41° YX-cut of a LiNbO₃ crystal [33]. The second resonance corresponds to the PSAW excitation at $f = 157.7$ MHz. Thus, the SAW velocity in the LiNbO₃/Si layered structure is higher than that of the bulk 41° YX-cut of a LiNbO₃ crystal, while the PSAW velocities coincide.
Thus, the SAW velocity in the LiNbO$_3$/Si layered structure is higher than in the YX-cut LiNbO$_3$ crystal (blue line) and 41° YX-cut of a LiNbO$_3$ crystal (red line).

3. Scanning Electron Microscopy Set-Up for Investigation of SAW and PSAW Propagation

The scanning electron microscopy method allows one to visualize the surface, pseudo-surface, bulk, and the propagation of standing and traveling acoustic waves in the real-time mode [30–32,37,38]. SEM, when set to register the secondary electron emission from the crystal surface, allows us to visualize the distribution of the electric potential on the crystal surface, since the low-energy secondary electrons with an energy of $1 \div 3$ eV are sensitive to the electric field that accompanies the propagation of acoustic waves in piezoelectric and ferroelectric crystals. To study the propagation process of the surface acoustic wave using the SEM method, it is necessary to use the accelerating voltage of $E = 1$ keV and an electron beam current of $I = 1$ nA. The use of a higher accelerating voltage is not possible, since, in this case, the piezoelectric substrate is strongly charged, which leads to the deflection of the primary electron beam and changes in the secondary electron emission from the crystal surface. Two methods can be used for visualization of the acoustic waves.

The first method is the stroboscopic scanning electron microscopy method, when the primary electron beam is modulated with the SAW frequency [39,40]. In this case, the electron beam is in a phase synchronization with the acoustic wave and remains in the same position at all times, since the secondary electron emission from the crystal surface is determined by the electric field that accompanies the SAW propagation in piezoelectric and ferroelectric crystals. This method requires a special upgrade to the scanning electron microscope (a stroboscopic system that deflects an electron beam with the frequency of an acoustic wave).

In the second method, which is more convenient (because it is not necessary to use the special stroboscopic technique), the high-frequency modulation of the low energy secondary electrons is defined by the electric field of the SAW (the minima and maxima of the SAW have different potentials and different coefficients of secondary electron emission from the crystal surface, respectively) and by the component, normal to the surface, of the electromagnetic radiation field of the IDT. The positive half-wave of the electromagnetic field accelerates the low-energy secondary electrons from the crystal surface to the secondary electron detector, while the negative half-wave prohibits the secondary electrons from reaching the detector. The electromagnetic and acoustic waves are mutually coherent,
since they are excited by the same source (IDT) and with the same frequency. In this case, an image of the acoustic wave field on the crystal surface is observed only at the moment of the positive half-wave of the electromagnetic radiation field of the IDT and the SAW is observed always in the same position [31,32].

SEM methods make it possible to determine the acoustic wavelengths, to measure the power flow angles, to visualize the diffraction phenomena in acoustic beams, and to study the process of acoustic wave interaction with the crystal structure defects. The second method was used to visualize the SAW and PSAW propagation process in a bonded LiNbO$_3$/Si layered structure.

4. SEM Imaging of the SAW and PSAW Propagation in a LiNbO$_3$/Si Layered Structure

Figure 4 shows the SEM photomicrographs of the SAW and PSAW propagation in a bonded LiNbO$_3$/Si layered structure. Microphotograph 4(a) displays an image of the traveling SAW with a wavelength of $\Lambda = 30$ $\mu$m, excited at the resonance frequency of $f = 135.4$ MHz. Both the IDT and acoustic wave field with a periodic SAW structure can be observed in the microphotograph. The dark lines of the SAW image correspond to the positive potential, which leads to a decrease in emission of the low-energy secondary electrons from the crystal surface. The bright lines, on the contrary, correspond to a negative potential and lead to an increase in the emission of the low-energy secondary electrons from the crystal surface. In this case, there is an even distribution of SAW. There are no diffraction phenomena in the acoustic beam; there is no distortion of the wave front. The SAW autocollimation can be observed. The SAW velocity in a bonded LiNbO$_3$/Si layered structure is $V_{SAW} = 4062$ m/s, which significantly exceeds the velocity of the bulk 41$^\circ$ YX-cut of a LiNbO$_3$ crystal.

Figure 4b shows a PSAW image with a wavelength of $\Lambda = 30$ $\mu$m in a LiNbO$_3$/Si layered structure. The resonance excitation frequency of PSAW is $f = 155.7$ MHz, and the PSAW velocity is $V_{PSAW} = 4731$ m/s. This PSAW velocity value is almost the same as the known PSAW velocity value $V_{PSAW} = 4749$ m/s for the 41$^\circ$ YX-cut of a LiNbO$_3$ crystal [33]. In this case, there is also no diffraction phenomena in the acoustic beam.

Figure 4c shows the microphotograph of the SAW with a wavelength of $\Lambda = 30$ $\mu$m, excited at the resonance frequency of $f = 195.7$ MHz and propagating with a velocity of $V_{SAW} = 5871$ m/s in a LiNbO$_3$/Si layered structure, which strongly exceeds the SAW velocity in the silicon crystal. The SAW image can be observed only in piezoelectric and ferroelectric crystals, where the SAW propagation causes a change in potential with a period corresponding to the SAW wavelength. In this case, the SAW propagates in a LiNbO$_3$/Si layered structure. The SAW propagates in a LiNbO$_3$/Si layered structure and causes a uniform sinusoidal deformation of a crystal lattice in the layer of the 41$^\circ$ YX-cut of a LiNbO$_3$ crystal, which leads to a periodic distribution of the electric potential corresponding to the SAW period. Thus, it is possible to visualize the high-velocity traveling SAW in a LiNbO$_3$/Si layered structure. In the figure on both sides of the IDT, the SAW wave field can be observed, in which there are no diffraction phenomena and no distortion of the SAW wave front.

The brighter contrast at Figure 4 corresponds to the highest value of the SAW amplitude. Usually, this is observable near the IDT. This effect can especially be observed at Figure 4b for the PSAW, because of the high value of the electromechanical coupling coefficient for the PSAW excitation in the 41$^\circ$ YX-cut of a LiNbO$_3$ crystal. The PSAW flows deep into the crystal and at a small distance from the IDT the wave contrast is decreased.
Figure 4. SEM microphotographs of the SAW and PSAW in a LiNbO$_3$/Si layered structure: (a) SAW, $f = 135.4$ MHz; (b) PSAW, $f = 155.7$ MHz; (c) SAW, $f = 195.7$ MHz. $\Lambda = 30$ $\mu$m.

Figure 5 presents the SEM microphotographs of the SAW (a) and PSAW (b) excitation in a bulk 41° YX-cut of a LiNbO$_3$ crystal. The SAW with a wavelength of $\Lambda = 30$ $\mu$m was excited at $f = 121.3$ and propagates with a velocity of $V_{SAW} = 3639$ m/s, while the PSAW was excited at $f = 155.7$ MHz and propagates with a velocity of $V_{PSAW} = 4731$ m/s.

In the case of the bulk 41° YX-cut of a LiNbO$_3$ crystal there is also no diffraction phenomena in the acoustic beam and a uniform distribution of the amplitude along the wave front. However, it is very often possible to observe the diffraction phenomena in the acoustic beam. For example, in Figure 6 under the condition of acoustic beam autocollimation one can observe the strong Fresnel diffraction pattern in the acoustic beam. In this case, the SAW with a wavelength of $\Lambda = 30$ $\mu$m was excited in the YZ-cut of a LiNbO$_3$ crystal by the IDT at a resonance excitation frequency of $f = 116.27$ MHz ($V_{SAW} \approx 3488$ m/s).
Figure 5. SEM microphotographs of the SAW (a) and PSAW (b) in a bulk 41° YX-cut of a LiNbO₃ crystal excited at \( f = 121.3 \) and \( f = 155.7 \) MHz, respectively. \( \Lambda = 30 \) μm.

Figure 6. SEM microphotograph of the traveling SAW propagation in the YZ-cut of a LiNbO₃ crystal. \( f = 116.27 \) MHz, \( \Lambda = 30 \) μm.

5. Conclusions

The excitation and propagation processes of the SAW and PSAW in the bonded LiNbO₃/Si layered structure and in the bulk 41° YX-cut of a LiNbO₃ crystal were investigated using the scanning electron microscopy method. The layer thickness of the 41° YX-cut of a LiNbO₃ crystal in the bonded LiNbO₃/Si layered structure was 8 μm. The SEM method allowed for the visualization of the SAW and PSAW propagation in a LiNbO₃/Si layered structure. The studies have shown that the SAW propagation in layered structures differs from the acoustic wave propagation in bulk crystals. Thus, the SAW propagation velocity in the bonded LiNbO₃/Si layered structure was \( V_{\text{SAW}} = 4062 \) m/s, which is significantly higher than that of the bulk substrate of the 41° YX-cut of a LiNbO₃ crystal \( V_{\text{SAW}} = 3642 \) m/s. At the same time, the PSAW propagation velocity is \( V_{\text{PSAW}} = 4731 \) m/s and practically corresponds to the SAW velocity in the bulk substrate of the 41° YX-cut of a LiNbO₃ crystal \( (V_{\text{PSAW}} = 4749 \) m/s) [33]. The scanning electron microscope also made it possible to observe the SAW at a velocity of \( V_{\text{SAW}} = 5871 \) m/s in the bonded LiNbO₃/Si...
layered structure, which exceeds the value of the SAW and PSAW velocities in the Si(100) along the [110] direction \((V_{\text{SAW}} = 5080 \text{ m/s}, V_{\text{PSAW}} = 5570 \text{ m/s})\).

It should be noted that the application of the SEM method allowed for not only the determination of the acoustic wave velocities, but also the visualization of the acoustic wave field in the bonded layered structure. It is necessary to note the absence of diffraction phenomena and divergence of the acoustic beam, and the absence of wave front distortion in the layered structure based on the 41° YX-cut of a LiNbO₃ crystal and Si(100) crystal.

Thus, the scanning electron microscopy method made it possible to study the excitation and propagation of the SAW and PSAW in the bonded LiNbO₃/Si layered structure and to observe the acoustic wave fields.

In the future, it is advisable to study the propagation of acoustic waves in such layered structures on synchrotron radiation sources by the X-ray diffraction and topography methods. X-ray methods will make it possible to study the propagation of traveling SAW both in the LiNbO₃ crystal layer and in the Si crystal. Of particular interest is the study of the SAW propagation in the Si crystal at high velocity when, at one Bragg angle (the Bragg angle for reflection (400) in Si crystal), the process of SAW propagation in silicon crystal is investigated, and at another value of Bragg angle (the Bragg angle for reflection (012) or (024) in LiNbO₃ crystal), the SAW propagation is studied in a thin layer of LiNbO₃ crystal. Application of the X-ray diffraction method will allow for the comparison of the SAW amplitudes in the LiNbO₃ and Si crystals. Unfortunately, due to the COVID-19 pandemic, it is unlikely that these experimental studies at a synchrotron radiation source can be realized in the near future.

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