Testing of a force sensor used to measure the briquetting process parameters of lignocellulosic materials

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Abstract. The study presents a control and measurement system for the drive parameters of screw compactor machine with open working chamber for shredded materials. The study demonstrates the construction and working principle of the force sensor for measuring the axial force at the compacting screw. The calibration method for the measuring system was presented together with example measurement results for compaction of broken up rye straw, oat straw and hay. The study results were analyzed for feasibility of use for the compaction of materials with specific thermomechanical properties. The conclusion presents the possible forms of application of the established solution in mass production.

Keywords: worm/screw-based compaction machine, force sensor

1 Introduction

Manufacturing of solid fuels from broken down lignocellulosic materials has been steadily growing in popularity in the last years. This is caused by overproduction of materials suitable as fuel. Such overproduction is also observed in Poland since many years. Table 1 presents the balance of the total production compared to the utilization together with the forecast for the years 2010-2030.

Table 1. The balance of the total production and utilization of straw in the years 2010-2030 [1-8]

| Year  | Production [million tons] | Utilization [million tons] |
|-------|---------------------------|----------------------------|
|       | 2010 | 2011 | 2012 | 2013 | 2014 | Forecast | 2020 | 2030 |
| Production | 29.753 | 28.89 | 30.793 | 29.343 | 35.608 | 30.533 | 30.862 |
| Utilization | | | | | | | |
| Mulch | 11.843 | 11.24 | 10.698 | 10.303 | 10.47 | 9.868 | 9.319 |
| Fodder | 3.923 | 3.914 | 3.898 | 3.763 | 3.806 | 3.527 | 3.221 |
| Green manure | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Bedding for mycelium | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Balance | 9.987 | 9.736 | 12.198 | 11.277 | 17.322 | 13.138 | 14.322 |
Compaction of materials enables the change of their mechanical and usable properties as well as transport and storage conditions [8-15]. The manufacturing of solid fuels calls for the utilization of proper compaction technique. The most popular are piston, roller and screw based solutions. The utilization of any of the above methods depends on proper preconditioning of the material to be compacted. Pelletization utilizing roller technology calls for a finer breakdown of straw material. Whereas worm/screw-based compaction allows to compact cut straw with length from several to several dozen millimeters [8-15]. Fig. 1 shows the diagram of a compacting machine utilizing the screw technique with open forming sleeve.

![Diagram of a compacting machine utilizing the screw technique with open forming sleeve.]

2 Process parameters for the compaction of lignocellulosic materials utilizing compacting screw technique

The working system of the machine utilizing the compacting screw consists of the two basic components: worm screw set in rotational motion via electrical drive together with the forming sleeve in which the worm performs the rotating motion. Fig. 2 presents the working system diagram of the machine utilizing compacting screw.

![Diagram of the working system of the compaction machine for broken down lignocellulosic materials (compacting screw technique).]

Fig. 2. Geometric properties of the working system of the compaction machine for broken down lignocellulosic materials (compacting screw technique): $D$ – diameter of the cylindrical part of the worm, $d_r$ – worm root diameter, $P$ – worm pitch, $F_{re}$ – resistance force, $F_a$ – axial force, $T_r$ – torque, $A$ – main compaction area of the material.
Analyzing the operating principle of such a working system, we can identify two basic functional parameters: the torque necessary to affect the rotating motion for compaction $T_r$, and resistance force $F_a$, which puts load on the worm during machine operation. The value of both parameters depend partially on the thermomechanical properties of the compacted materials. Therefore, during operation of the compacting screw mechanism, process temperature is another parameter to materially affect the entire process.

Identifying the torque and axial force values may be critical for machine control to facilitate efficient compaction process. Therefore, an attempt was made to suggest a construction solution for a specialized force gauge dedicated for this type of machine. The proposed solution is protected by a Polish patent no. 225645. Fig. 3 demonstrates the construction diagram of the force gauge.

![Hydraulic rotational force gauge](image)

**Fig. 3.** Hydraulic rotational force gauge: 1 – shaft, 2 – body, 3 – force gauge body 1, 4 – force gauge body 2, 5 – sealing ring, 6 – pressure chamber, 7 – threaded sleeve, 8, 9, 10 – bearing, 11 – chain wheels, 12 – slot for pressure gauge, 13 – slot with inlet groove for the installation of worm pin, $F_a$ – axial force [8, 16]

The operating principle of the presented force gauge is based on the direct measurement of the axial force based on the pressure change in the hydraulic chamber (between items no. 2, 3 and 4). After calibrating the force gauge using a durometer, it can be used to measure axial force for compacting selected materials. The calibration entails identifying the force-pressure characteristics allowing to use the pressure value within the hydraulic chamber to calculate the axial force accounting for resistances from construction.

### 3 Methodology and scope of test measurements

The examination was carried out on a compaction machine utilizing compaction worm screw. The compaction process was undertaken for oat straw, rye straw and hay (Fig. 4). The examination was carried out for three rotation speeds of the worm: 210, 280 and 350 rpm. Figs. 5-7 present example results of the examination. Table 2 presents a breakdown of collected results of the axial force examination for the three materials at three rotation speeds of the worm.
Fig. 4. Materials used for the examination: oat straw, rye straw, hay

Fig. 5. The change of axial force $F_a$ as a function of time; rye straw

Fig. 6. The change of axial force $F_a$ as a function of time; oat straw
The change of axial force $F_a$ as a function of time; hay

**Table 2. Breakdown of results of the examination of axial force values $F_a$**

| Material   | Axial force $F_a$ [kN] |
|------------|------------------------|
|           | $n_{1}$ | $n_{2}$ | $n_{3}$ |
| Rye straw  | 2.8-4.8 | 3.2-4.2 | 3.1-4.8 |
| Oat straw  | 2.3-3.4 | 2.7-3.9 | 3.4-4.7 |
| Hay        | 1.7-4.0 | 1.8-3.3 | 1.8-3.6 |

**4 Conclusion**

The proposed hydraulic force gauge intended for use in the compacting machine utilizing worm screw technique fulfills its purpose successfully. The variability of the compaction process of the broken down lignocellulosic materials prevent designing dedicated working systems for specific materials. It is therefore much more advantageous to utilize dedicated measurement systems allowing to monitor selected parameters during machine operation. This may be utilized to control the machine utilizing the known value of axial force load on the auger. Analyzing the results of the study, we can conclude that even within a single type of material, the variability of the axial force value is considerable. The value ranges of axial force for different materials overlap. This confirms the thesis regarding the suitability of designing dedicated, specialized measuring systems allowing constant control of the selected parameter during machine operation.

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