Planetary Accretion Shocks with a Realistic Equation of State

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Abstract

The final stage of gas giant formation involves accreting gas from the parent protoplanetary disk. In general, the infalling gas likely approaches a freefall velocity, creating an accretion shock, leading to strong shock heating and radiation. We investigate the kinematics and energetics of such accretion shocks using 1D radiation hydrodynamic simulations. Our simulations feature the first self-consistent treatment of hydrogen dissociation and ionization, radiation transport, and realistic gray opacity. By exploring a broad range of giant-planet masses (0.1–3 M⊕) and accretion rates (10−3–10−2 M⊕ yr−1), we focus on global shock efficiency and the final entropy of the accreted gas. We find that radiation from the accretion shock can fully disassociate the molecular hydrogen of the incoming gas when the shock luminosity is above a critical luminosity. Meanwhile, the post-shock entropy generally falls into “cold” (≤12 k_B/m_H) and “hot” (≥16 k_B/m_H) groups depending on the extent of the endothermic process of H2 dissociation. While 2D or 3D simulations are needed for more realistic understandings of the accretion process, this distinction likely carries over and sheds light on the interpretation of young direct imaging planets.

Unified Astronomy Thesaurus concepts: Accretion (14); Hydrodynamical simulations (767); Planet formation (1241)

1. Introduction

A major paradigm shift in our understanding of protoplanetary disks (PPDs) over the past few years is the ubiquity of disk substructures found in high-resolution observations of protoplanetary disks (e.g., van der Marel et al. 2013; Dipierro et al. 2015; Pérez et al. 2016; Andrews et al. 2018; Avenhaus et al. 2018; Long et al. 2018). As a common interpretation, these substructures are considered to be the outcome of planetary-mass companions interacting with the disk, which generally requires the formation of giant planets which can naturally open gaps (e.g., Goldreich & Tremaine 1979; Lin & Papaloizou 1986; Goodman & Rafikov 2001; Dong et al. 2017), create asymmetries (e.g., de Val-Borro et al. 2007; Zhu & Stone 2014), or drive spiral patterns (e.g., Dong et al. 2015; Bae & Zhu 2018; Bae et al. 2021). Despite the expectation of multiple planets carving substructures in dozens of disks, including evidence from kinematic signatures in a few systems (e.g., Pinte et al. 2018, 2020; Teague et al. 2019), so far, the only bona fide detection has been the two giant planets in the central cavity of the PDS 70 disk (Kepler et al. 2018; Wagner et al. 2018; Haffert et al. 2019). The two planets are found to be accreting from the parent PPD as the pathway to building up their masses, showing Halpha emission characteristic of planetary accretion shocks (Aoyama et al. 2018; Aoyama & Ikoma 2019; Thanathibodee et al. 2019; Szułagyi & Ercolano 2020).

The ability to detect young giant planets and direct imaging of gas giants in general after disk dispersal crucially depends on the initial conditions, particularly the initial entropy that largely sets the subsequent evolution of its luminosity and temperature as main observables. The initial entropy is closely related to the amount of the specific energy (energy per unit mass) of the accreted gas. In general, the smaller the fraction of specific energy retained in the gas, the lower the initial entropy. Correspondingly, models of giant-planet evolution are classified into “cold,” “warm-,” and “hot-start” models that primarily differ in their initial entropy (Marley et al. 2007; Spiegel & Burrows 2012). The differences among these models are most pronounced over the first year to a few tens of Myr after giant-planet formation (Berardo et al. 2017), and hence crucially affect the inference of detection limits and estimation of planet masses.

In the standard theory of giant-planet formation by core accretion (Pollack et al. 1996), the bulk of giant-planet mass is built up by accreting gas from a PPD in a runaway manner. Upon becoming sufficiently massive, the planet opens a gap and becomes “detached” from the disk, forming a circumplanetary disk (CPD, e.g., Ayliffe & Bate 2009; Tanigawa et al. 2012; Gressel et al. 2013). How gas accretion proceeds through a CPD is unclear, but existing studies suggest that most gas falls into the circumanetary region from high latitudes from the meridional flow (e.g., Szułagyi et al. 2014; Szułagyi & Mordasini 2017; Fung et al. 2019). Planetary accretion may proceed through an accretion shock either from this infalling material or via magnetospheric accretion from the CPD. This accretion shock is also the source of the Halpha emission observed from the PDS 70 system.

Detailed models of planetary accretion shocks are of great significance to understand the initial conditions of giant planets. With the accreting material approaching at near-freefall velocity, such models are usually in 1D, focusing on energy transport through the shock and the accreting column (Marleau et al. 2017, 2019). In this Letter, we show that a realistic equation of state (EoS) that incorporates the dissociation of H2 plays a highly significant role in setting the post-shock entropy of the accreting gas that will further affect the initial conditions of giant-planet evolutionary models.

This Letter is organized as follows. Section 2 describes the setup and physical ingredients of our 1D radiation...
hydrodynamic simulations. Major results are presented in Section 3 and are summarized with further discussion in Section 4.

2. Physical Model

In this section, we describe the setup for our accreting gas giant simulations, highlighting the combination of radiation hydrodynamics with a general EoS that incorporates the dissociation of hydrogen molecules.

2.1. Governing Equations

We solve radiation hydrodynamic equations in 1D spherical geometry along the radial (r) direction with a general EoS for gas accretion toward a planet with mass $M_\ast$. The governing equations are

$$\frac{\partial \rho}{\partial t} + \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 \rho v) = 0, \quad \text{(1)}$$

$$\frac{\partial \rho u}{\partial t} + \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 \rho v^2) = -\frac{\partial p}{\partial r} - \frac{\rho G M_\ast}{r^2}, \quad \text{(2)}$$

$$\frac{\partial E}{\partial t} + \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 (E + p)v) = -\frac{\rho G M_\ast}{r^2}v, \quad \text{(3)}$$

$$\frac{\partial E_i}{\partial t} + \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 F_i) = -G, \quad \text{(4)}$$

where $\rho$, $v$, $p$, $E$, and $G$ are gas density, radial velocity, pressure, total energy density, and the gravitational constant, with

$$p = \sum_i n_i k_B, \quad \text{(5)}$$

$$E = \rho (\epsilon_{\text{kin}} + \epsilon) = \rho (v^2/2 + \epsilon), \quad \text{(6)}$$

where $n_i$ is the number density of the $i$th species (to be specified later), $k_B$, $T_g$, $\epsilon_{\text{kin}}$, and $\epsilon(p, T_g)$ are the Boltzmann constant, gas temperature, specific kinetic energy, and specific internal energy. Radiation energy density and energy flux are denoted by $E_{\text{rad}}$ and $F_r$, and $G$ is the rate of energy exchange between radiation and matter, given by

$$G = \kappa_T \rho c (E_r - a_R T_g^4), \quad \text{(7)}$$

where $\kappa_T$, $a_R$, and $c$ are Planck opacity, the radiation constant, and the speed of light. For future convenience, radiation temperature $T_{\text{rad}}$ is defined by $E_{\text{rad}} = a_R T_{\text{rad}}^4$.

The radiation subsystem is closed using the flux-limited diffusion (FLD) approximation, which relates $E_r$ and $F_r$ by

$$F_r = -\frac{c \lambda(R) \partial E_r}{\kappa_T \rho}, \quad \text{(8)}$$

$$R = \frac{[\partial E_r / \partial r]}{\kappa_T \rho E_r}, \quad \text{(9)}$$

where $\kappa_T$ is the Rosseland mean opacity. In this paper, we adopt the flux limiter $\lambda(R)$ described in Levermore & Pomraning (1981)

$$\lambda(R) = \frac{2 + R}{6 + 3R + R^2}. \quad \text{(10)}$$

2.2. Equation of State and Opacity

Our typical simulations encompass a temperature range between $\sim 10^2 - 4$ K, where $H_2$ can be dissociated and eventually ionized, and the standard ideal gas EoS becomes questionable. As a first study, we incorporate such physics but make a simplified assumption of chemical local thermal equilibrium of $H_2$, H, and $H^+$. The abundance of these species can be obtained analytically from the Saha equations at run time according to Appendix C of Chen et al. (2019). The EoS is given by $\epsilon = \epsilon(p, T_g)$ in an analytical form, which avoids the use of a tabulated EoS and improves the efficiency and accuracy of our simulations. In particular, we consider a hydrogen mass fraction of $X = 0.74$, assuming the remaining mass in helium.

One important quantity we compute in this work is the gas entropy. With the general EoS, it is given by

$$s = \sum_i k_B n_i \left( 1 + \frac{d \ln Z_i}{d \ln T} - \ln \frac{n_i}{Z_i} \right), \quad \text{(11)}$$

where $Z_i$ is the partition function for the $i$th species, given in Appendix A.

Opacity is a crucial physical component in our model. We adopt the same opacity tables as in Marleau et al. (2019), combining the gas opacity table of Malygin et al. (2014), which dominates over 1500 K, and the dust opacity table of Semenov et al. (2003) which dominates below 1100–1200 K, depending on the density. For temperatures in between, the maximum value of the two tables is taken.

Note that the opacity tables assume gas and radiation temperatures are the same. In reality, as we will see, $T_{\text{rad}}$ and $T_g$ can be different at the Zel’dovich spike and $H_2$ dissociation region. Here we use the radiation temperature to obtain opacity from lookup tables, bearing in mind the caveat that they can be improved in future works.

2.3. Simulation Setup

We solve the numerical problem with Guangqi (Z. Chen & X. Bai 2022, in preparation), a new 1D radiation hydrodynamic code with adaptive- and static-mesh-refinement (AMR/SMR). It employs the FLD approximation for gray radiative transfer, which is solved implicitly and is self-consistently coupled with a general EoS. In this problem, the shock and the planetary atmosphere require high resolution; they are located at the bottom of the computational domain and we employ SMR to properly resolve the Zel’dovich spike behind the shock (Section 3.3).

Our simulation domain spans between $[r_{\text{in}}, r_{\text{max}}]$, where $r_{\text{max}}$ is fixed to $20 R_j$ ($R_j$ is Jupiter radius), using a uniform grid with 256 cells at base level. We use 7 or 8 levels of mesh refinement with each level doubling the resolution of the parent level. Therefore, the finest cell has a length of approximately 43.6 km or 21.8 km ($r_{\text{in}}$ varies from 1 to 1.9$R_j$). In comparison, the finest cell in Marleau et al. (2019) is 35.7 km.

Gas is injected from the outer boundary assuming freefall velocity, and gas density at the outer boundary is parameterized by the accretion rate $M_\ast$, given by

$$v_{\text{inj}} = -\frac{2GM_\ast}{r_{\text{max}}}, \quad \text{(12)}$$

$$\rho_{\text{inj}} = -\frac{M_\ast}{4\pi f_r r_{\text{max}} v_{\text{inj}}}, \quad \text{(13)}$$
for spherical geometry, where $f_c$ is the covering fraction of the accretion flow over planetary surface, and we take $f_c = 1$ in this work. Gas temperature in the outer boundary is linearly extrapolated at run time, and radiation energy is set according to $\partial (\rho E_r)/\partial r = 0$.

For simplicity, we set the initial condition to be $\rho_{\text{init}} = \rho_{\text{inj}}$, $v_{\text{init}} = v_{\text{inj}}$, and $T_{g,\text{init}} = T_{\text{rad,init}} = 100$ K everywhere. The particular form of the initial condition does not affect the steady-state solution that we look for after running the simulations for many freefall timescales.

Setting inner boundary conditions requires some care. A straightforward reflecting boundary condition would gradually build up mass and pressure near the inner boundary, and the system hardly achieves a steady state. In reality (especially with $f_c < 1$), the post-shock gas flow likely spreads out, eventually maintaining equilibrium with atmospheric pressure. This motivates us to choose a fixed-state inner boundary condition set by $\rho_{\text{in}}, p_{\text{in}}, T_{g,\text{in}}$ in gas variables. However, $\rho_{\text{in}}, P_{\text{in}}$, and $T_{g,\text{in}}$ are unknown beforehand. In practice, we choose $p_{\text{in}}$ as the atmospheric pressure at the planet’s surface for each simulation (to be specified in the next subsection). We first set the inner hydro boundary condition to be nonpenetrating and the inner radiation boundary condition to be zero gradient. As the gas falls onto the planet, we keep monitoring the increase of gas pressure at the inner boundary. Once it reaches $p_{\text{in}}$, we record the $\rho$ and $T_g$ of the innermost cell as $\rho_{\text{in}}$ and $T_{g,\text{in}}$, and impose the aforementioned fixed-state inner boundary condition. The radiation boundary condition is still zero gradient.

### 2.4. Model Selection

To sample a broad range of parameter space, we choose $M_p = [0.1, 0.3, 1, 3]M_\odot$ to study the accretion of super Neptune, Saturn-mass, Jupiter-mass, and more massive planets. We choose $M_p = [10^{-3}, 10^{-2}]M_\odot$ yr$^{-1}$ to represent the low and high accretion rates.

Since we do not model the internal structure of the planet (e.g., Mordasini et al. 2012), which itself depends on the accretion history and shock properties, we cannot give a self-consistent prescription of $r_{\text{in}}$ and $p_{\text{in}}$ of the forming gas giants. Therefore, we treat $r_{\text{in}}$ as another parameter and adopt the results that newly formed gas giants with $M_p \geq M_\odot$ are expected to have radii of $\sim 1.4 - 4R_\oplus$ (Spiegel & Burrows 2012). In our simulations, the accretion shock (and the Zel’ dovich spike) forms at $r_p > r_{\text{in}}$, where the ram pressure ($\rho v^2$) of the infalling gas equals the pressure of the atmosphere. Note that the free energy available in the shock scales as $M_p/r_p$ and a larger $r_p$ would largely be equivalent to reducing planet mass (Section 3.3 for more discussion). Our choice of $p_{\text{in}}$ is also somewhat arbitrary, ranging from 2 to 10 bars as $M_p$ increases, but we have verified that the results are insensitive to this choice. Using a larger $p_{\text{in}}$ will lead to a larger $r_p$ as the planetary atmosphere becomes thicker.

We carry out a total of 12 runs, varying $M_p$, $M_p$, and $r_{\text{in}}$. The specific run parameters, as well as their major diagnostic properties, are listed in Table 1, and they are labeled as models 1–12.

### 3. Simulation Results

In this section, we choose two representative simulations, model 4 and 10, corresponding to accretion onto a Jupiter-mass planet with high and low accretion rates. Results from the steady-state solutions are shown and analyzed in detail, paying special attention to the post-shock entropy.

#### 3.1. Overview of Simulation Results

Figure 1 shows the steady-state solution of models the two models. In both models, the gas largely freefalls onto the planet as shown in the first panel. The infalling gas is stopped by the planetary atmosphere at $r_p$, forming the accretion shock. Gas can be substantially heated to high temperatures at $r_p$ by the shock, followed by a rapid fall-off in temperature, known as the Zel’ dovich spike. At the Zel’ dovich spike, $T_g > T_{\text{rad}}$ (see the zoom in the plot of the fourth panel), the gas internal energy is quickly converted to the radiation energy, which is then transported outward, seen as the emergence of high radiative energy flux in the second panel from top. The shock is resolved by 8 SMR levels around $r_p$ as shown in the third panel. We confirm that our solution is converged in the sense that the post-shock entropy $s_{\text{ps}}$ (to be defined later) does not differ by much if we use 7 SMR levels.

From large to small radii, we can approximately divide our simulation domain into three zones: the pre-shock upstream where gas freefalls, the Zel’ dovich spike where kinetic energy of the infalling gas is converted to heat and radiation, and a radiative zone in the downstream region considered to be a part of the giant-planet upper atmosphere. The three zones are separated by a pre-shock radius $r_{\text{pre}}$ and a post-shock radius $r_{\text{ps}}$. We define $r_{\text{ps}}$ as the radius with the maximum infalling speed and $r_{\text{ps}}$ as the radius where $T_g = T_{\text{rad}}$ in the downstream of the Zel’ dovich spike.

For future convenience, we define radiation mean-free path as

$$\lambda_{\text{mfp}} = (\kappa_R \rho)^{-1},$$

and we compare $\lambda_{\text{mfp}}$ to $r$ in the bottom panel of Figure 1. The interior of the planet is optically thick with $\lambda_{\text{mfp}}/r \ll 1$, while the pre-shock region is typically optically thin.\(^4\) We further define

$$f_t = F_t/(cE_r),$$

$$L_r = 4\pi r^2 F_r,$$

where $f_t$ is the reduced radiation flux that characterizes how close radiation transport is to the free-streaming limit, and $L_r$ is the outward radiation flux, i.e., luminosity.

Exterior to the planet, the infalling gas undergoes compression and hence, adiabatic heating. Additional heating results from the absorption of the outgoing radiation originating from the shock region, maintaining $T_{\text{rad}} \sim T_g$ (Marleau et al. 2019). When the infalling gas is heated to $T_{g,\text{dis}} \approx 2000$ K, $H_2$ starts to dissociate. Let us define the fraction of hydrogen species as,

$$\chi_H^+ = \frac{n_H^+ m_H}{\rho X},$$

$$\chi_{H_2} = \frac{2n_H^+ m_H}{\rho X},$$

$$\chi_H = \frac{n_H^+ m_H}{\rho X} = 1 - \chi_H^+ - \chi_{H_2}.$$ 

\(^3\) More rigorously speaking, we refer to “post-shock” as the immediate downstream of the Zel’ dovich spike.

\(^4\) More rigorously, one may use the $R$ factor (Equation (9)) to quantify how close the system is to the diffusive or free-streaming limit, and the result is qualitatively the same.
In the third panel, the red and blue lines show the profiles of $\chi_{\text{H}}$ and $\chi_{\text{H}^+}$, while $\chi_{\text{H}}$ can be easily deduced from Equation (17). The temperatures in these two cases are insufficient to ionize hydrogen. For the high-accretion model, H$_2$ is almost fully dissociated ahead of the shock. For the low-accretion model, in contrast, the infalling gas is almost molecular.

It is worth noting that hydrogen is not ionized at the shock in model 4 but is partially ionized in model 10. This is because the cooling strength in the shock zone is determined by $\kappa_p (\alpha R T_p^3 - E_r)$ and $\kappa_p$ is a strong function of both density and temperature. A high density (from a higher accretion rate) at the shock leads to a large $\kappa_p$ thus, a relatively low $T_p$ (at the Zel’’dovich spike) is sufficient. Conversely, a low density at the shock would result in a small $\kappa_p$, and hence, a higher gas temperature that may ionize the hydrogen.

### 3.1.1. H$_2$ Dissociation in the Pre-shock Region

By comparing the two models, we see that radiation temperature closely follows gas temperature in the pre-shock region in general, except when H$_2$ gets dissociated. In model 4, the endothermic process increases the gas’s heat capacity, leading to $T_{\text{rad}} > T_{\text{g}}$ in this region, and hence, more radiation is absorbed by the infalling gas. This is accompanied by a drop in $L_r$ between 2.5 and 4.7 $R_g$. In model 10, however, $L_r$ is largely flat in the pre-shock region.

The dissociation of H$_2$ and absorption of accretion luminosity in the pre-shock has important consequences. The black line in the fourth panel shows the entropy profile $s$. When $T_g < T_{\text{g,diss}}$ the gas radiates away energy as it is compressed, resulting in a slowly decreasing entropy profile as the gas falls inward. In model 4, upon $T_g$ reaching $T_{\text{g,diss}}$ the dissociation of H$_2$ and subsequent energy absorption drives the entropy to rapidly increase from 4.7$R_g$ to 2.5$R_g$ by almost 10$k_B/m_H$. This substantial increase in $s$ is not present in model 10 with only a small fraction of H$_2$ dissociated.

### 3.2. Global Shock Efficiency

Global shock efficiency quantifies the fractional energy that leaves the system, defined as (Marleau et al. 2019)

$$\eta_{\text{phy}} = \frac{E(r_{\text{max}}) - E(r_{\text{ps}})}{E(r_{\text{max}})}, \quad (18)$$

where $E(r) = -M_p(\epsilon + \epsilon_{\text{kin}} + p/\rho + \phi)$ is the total energy flux measured at $r$. A derivation of $\eta_{\text{phy}}$ can be found in Appendix B.

In long-term planetary evolution, shock efficiency largely determines the initial entropy of the planet and affects the mass–radius relation of the planet. Often, it was treated as a free parameter (Spiegel & Burrows 2012), and hence the outcome of the calculations somewhat hinges on this parameter. Recently, Marleau et al. (2017, 2019) studied global shock efficiencies with a perfect gas EoS, and concluded that $\eta_{\text{phy}} \geq 97\%$ in their models with $1.3M_J \leq M_p \leq 10M_J$. 

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**Table 1**

| ID | $M_p$ | $M_p$ (Ms) | $r_m$ | $p_m$ | $r_p$ | $\gamma_{\text{ps}}$ | $\gamma_{\text{ps}}^{15}$ | $\eta_{\text{phy}}$ | $\chi_{\text{H},\text{pre}}$ | $\chi_{\text{H},\text{ps}}$ | $M_{\text{ps}}$ | $T_{\text{g,pre}}$ | $T_{\text{g,ps}}$ | $p_{\text{ps}}$ | $M_p/M_{\text{ps}}$ |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| (1) | 0.1 | $10^{-2}$ | 1.0 | 2 | 1.284 | 11.42 | 11.42 | 82.23 | 16.67 | 5.18 | 5.24 | 1865 | 1920 | 2.850 | 0.56 |
| (2) | 0.3 | $10^{-2}$ | 1.1 | 2.5 | 1294 | 17.04 | 17.06 | 64.90 | 98.73 | 71.55 | 6.00 | 2458 | 2474 | 5.077 | 1.28 |
| (3) | 1 | $10^{-2}$ | 1.5 | 10 | 1.679 | 19.21 | 19.20 | 81.59 | 99.93 | 95.72 | 8.39 | 2685 | 2754 | 4.987 | 2.46 |
| (4) | 4 | $10^{-2}$ | 1.7 | 10 | 1.865 | 18.25 | 18.20 | 82.34 | 99.72 | 83.39 | 8.61 | 2495 | 2526 | 3.765 | 1.81 |
| (5) | 3 | $10^{-2}$ | 1.7 | 10 | 1.780 | 19.61 | 19.61 | 92.81 | 100 | 99.22 | 12.57 | 3358 | 3465 | 7.843 | 7.05 |
| (6) | 3 | $10^{-2}$ | 1.9 | 10 | 1.998 | 19.68 | 19.67 | 92.12 | 100 | 99.24 | 12.37 | 3092 | 3201 | 5.791 | 4.95 |
| (7) | 0.1 | $10^{-3}$ | 1.0 | 2 | 1.266 | 11.45 | 11.45 | 91.85 | 0 | 0 | 6.06 | 1290 | 1299 | 0.304 | 0.06 |
| (8) | 0.3 | $10^{-3}$ | 1.1 | 5 | 1.198 | 11.24 | 11.23 | 97.02 | 1.24 | 0.11 | 11.82 | 1456 | 1468 | 0.696 | 0.24 |
| (9) | 0.1 | $10^{-3}$ | 1.5 | 10 | 1.568 | 11.49 | 11.48 | 98.52 | 11.76 | 1.21 | 18.04 | 1612 | 1667 | 0.702 | 0.37 |
| (10) | 0.1 | $10^{-3}$ | 1.7 | 10 | 1.785 | 11.47 | 11.46 | 98.57 | 4.43 | 0.35 | 17.38 | 1511 | 1536 | 0.489 | 0.25 |
| (11) | 0.1 | $10^{-3}$ | 1.7 | 10 | 1.734 | 13.16 | 13.21 | 98.34 | 71.71 | 20.41 | 23.12 | 1831 | 1920 | 1.130 | 0.81 |
| (12) | 0.3 | $10^{-3}$ | 1.9 | 10 | 1.940 | 12.18 | 12.21 | 98.92 | 48.3 | 8.18 | 24.02 | 1740 | 1889 | 0.817 | 0.58 |

**Note.** From column 1 to column 16: (1) the model ID, (2) planet mass, (3) accretion rate, (4) inner boundary radius, (5) inner boundary pressure, (6) radius where $p_{\text{max}} = \rho v^2 = \rho$, (7) post-shock entropy with 8 SMR levels, (8) post-shock entropy with 7 SMR levels, (9) global shock efficiency, defined in Equation (18), (10) the number fraction of H at the pre-shock radius, (11) the number fraction of H at the post-shock radius, (12) pre-shock gas Mach number, (13) pre-shock gas temperature, (14) post-shock gas temperature, (15) post-shock pressure, (16) and the actual accretion rate divided by the critical accretion rate.

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3.1.2.

We note that at the shock, the gas internal energy is quickly converted to radiation energy, leading to a rapid decrease in entropy. The post-shock entropy keeps decreasing toward the planet’s interior, accompanied by an outgoing radiation flux. Since there is no radiation flux at the inner boundary, here we use the radiation flux at $r_{\text{ps}}$, the internal luminosity. The internal luminosity of the planets are marked with black circles in the second panel.

We have also examined the simulation results of other models. Generally, results from models 2, 3, 5, 6, 11, and 12 are similar to model 4 because a large fraction of H$_2$ dissociates before the infalling gas hits the planetary atmosphere. They differ in the radii where H$_2$ dissociation takes place. Results from models 1, 7, 8, and 9, however, are similar to model 10, as they all show zero to a very low degree of H$_2$ dissociation in the pre-shock region. They are also very similar to the solutions of a perfect gas EoS with $\gamma > 4/3$ (Marleau et al. 2017, 2019) as there is no dissociation/ionization except at the shock.
In Figure 2, we can see that 64.9% \( \lesssim \eta^{\text{phy}} \lesssim 98.92% \) in our simulations. In particular, models with high accretion rates yield relatively low efficiencies of 64.9% \( \lesssim \eta^{\text{phy}} \lesssim 92.81% \), because the hydrogen dissociation consumes a significant amount of energy and this latent heat is retained in the post-shock region by \( \text{H} \), lowering \( \eta^{\text{phy}} \). In contrast, the low-accretion rate models yield \( 91.85% \lesssim \eta^{\text{phy}} \lesssim 98.92% \), as molecular hydrogen is largely retained in the pre-shock region, behaving like a perfect gas. Without surprise, \( \eta^{\text{phy}} \) versus \( M_{\text{pre}} \) (the pre-shock gas Mach number) of the low-accretion models is largely consistent with Figure 4 of Marleau et al. (2019).

### 3.3. Post-shock Entropy

Incorporating all simulation results, we present \( s_{\text{ps}} \) versus \( M_{\text{ps}} \) in Figure 2. We find a clear dichotomy, characterized by a high-entropy “hot group” with \( s_{\text{ps}} \gtrsim 16k_B/m_H \) (marked in orange), and a low-entropy “cold group” with \( s_{\text{ps}} \lesssim 12k_B/m_H \) (marked in blue). By noting the fraction of \( \text{H} \) in the pre-shock and post-shock regions in Table 1, we clearly identify that the “hot group” is associated with models where most \( \text{H}_2 \) is dissociated before reaching the shock, whereas those without \( \text{H}_2 \) dissociation before the shock fall into the “cold group.” We should note that the post-shock gas will continue to cool in a radiative zone, further decreasing the entropy, and the general
zero-age entropy of planets (Spiegel & Burrows 2012) should be lower than $s_{ps}$.

A few comments are in order concerning the dichotomy. First, the post-shock entropy generally increases monotonically with increasing accretion rate and planet mass. When choosing intermediate accretion rates for low-mass planets $M_p = 0.3$–$1M_J$, one would fill the gap of $s_{ps}$ in Figure 2 between the two groups. This also applies to models 11 and 12 for massive planets with low accretion rates. However, the dichotomy remains a valid description as the “gap” region corresponds to $H_2$ being partially dissociated. Second, Marleau et al. (2019) varied $\gamma$ from 1.1 to 1.667 to mimic realistic gas. Their entropy profiles with low $\gamma$ are similar to our results when $H_2$ dissociates and their high $\gamma$ results are similar to our results when $H_2$ does not dissociate. Third, even though $s_{ps}$ of massive planets ($>3M_J$) can be low at low accretion rates ($<10^{-3}M_\odot$ yr$^{-1}$), we should still expect high initial planet entropy because they must build the bulk of their mass through phases of high accretion rates.

Finally, given its importance, we provide an approximate estimate of the condition for which $H_2$ gets fully dissociated. This can be obtained by equating radiation temperature from the accretion luminosity at the pre-shock region to $T_{g,\text{dis}}$. During dissociation, we have $f_e = c_f e_r = c_f d_R T_{rad}^4$ where $f_e \approx 1$. Assuming the shock luminosity is much larger than the internal luminosity, we obtain

$$
\eta^\text{phy} \frac{G M_p M_p}{r_p} \approx 4\pi f_e \frac{r_p^3}{R_1} c_f d_R T_{g,\text{dis}}^4,
$$

(19)

$$
\approx 6 \times 10^{-4} f_e \left( \frac{r_p}{R_1} \right)^2 L_\odot.
$$

(20)

We can see that the aforementioned $M_p/r_p$ is correlated to the dissociation of $H_2$. Equation (19) can be translated to a critical accretion rate for $H_2$ dissociation, given by

$$
\dot{M}_\text{crit} \approx 7 \times 10^{-4} f_e \left( \frac{r_p}{R_1} \right)^3 \left( \frac{M_p}{M_J} \right)^{-1} \frac{M_\odot}{\text{yr}}.
$$

(21)

We can calculate $\dot{M}_\text{crit}$ by plugging in our assumption of $f_e = 1$, and $f_e = 1$ with $\eta^\text{phy}$ from the simulation results. We present $M_p/\dot{M}_\text{crit}$ in Table 1. When $M_p/\dot{M}_\text{crit} > 1$, $H_2$ is indeed almost fully dissociated; when $M_p/\dot{M}_\text{crit} < 1$, $H_2$ is partially dissociated; when $M_p/\dot{M}_\text{crit} < 0.56$, $H_2$ largely remains in molecular form in the pre-shock region. In general, we find that this criterion well characterizes the chemical state of the hydrogen in the pre-shock region and separates the “cold group” and “hot group” in our simulations (see Figure 2).

4. Summary and Discussion

In this Letter, we carried out 12 radiation hydrodynamic simulations in 1D with a hydrogen EoS to study planetary accretion with a broad range of planet masses and accretion rates. The simulations suggest that hydrogen dissociation in the pre-shocked infalling gas plays an important role in setting the initial condition of giant planets. More specifically, we find

The post-shock entropy $s_{ps}$ of the 12 simulations generally fall into two groups (Figure 2): a “cold” group with a high degree of $H_2$ dissociation and a “hot” group with a high degree of $H_2$ dissociation.

The global shock efficiency $\eta^\text{phy}$—the fraction of the accretion energy that is radiated away—can be lowered by hydrogen dissociation.

There is a critical accretion rate $\dot{M}_\text{crit}$ above which $H_2$ gets largely dissociated in the infalling gas, which is given by Equation (21).

We note that the post-shock entropy (Figure 2) should be higher than the entropy of zero-age planets because the newly accreted gas can still radiate energy away. In addition, our simulations represent individual snapshots of planetary accretion shocks, while the final result should depend on the accretion history, especially over the period when giant planets build most of their masses. Our results of the global shock efficiencies and post-shock entropy can serve as more realistic inputs for more detailed modeling of the structure and evolution of accreting planets (Mordasini et al. 2012; Berardo et al. 2017), which eventually determines the initial conditions of gas giants.

As a first approximation, we have assumed that accretion is spherically symmetric. While we expect the actual accretion process could be more complex through a CPD (Takasao et al. 2021), we note that existing studies of CPDs have yet to self-consistently incorporate the major physical ingredients, including radiation with realistic EoS and magnetic fields. Despite the
major uncertainties in our ignorance of how gas giants accrete, our results also imply that whether the hydrogen is accreted in molecular or atomic form likely has a significant impact on setting the initial condition of gas giants.

Current imaging surveys may be approaching the limit to detect more young gas giants in PPDs, especially in systems setting the initial condition of gas giants. Various areas with predicted dynamical mass awaiting for direct imaging detection (e.g., Dong et al. 2015; Maire et al. 2017; Brown-Sevilla et al. 2021), which are ideal tools to test the evolution models of gas giants. The discovery space will be greatly enhanced with the upcoming James Webb Space Telescope (Carneri et al. 2021), the Extremely Large Telescope (Carlomagno et al. 2020), and the Chinese Space Station Telescope which, together with modeling effort, will likely yield a more decisive picture of gas giant formation.

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Software: Guangqi (Z. Chen & X. Bai 2022, in preparation), Matplotlib (Hunter 2007), Petsc (Balay et al. 1997, 2019).

Appendix A
Equation of State
The general EoS can be derived based on the partition functions of the underlying species. The partition functions of all the species used in this work are given by

\[ Z_{H_2} = \left( \frac{2 \pi m_{H_2} k_B T_e}{h^2} \right)^{3/2}, \]
\[ Z_H = \left( \frac{2 \pi m_H k_B T_e}{h^2} \right)^{3/2} \exp \left( -\frac{\phi_{\text{dis}}}{2 k_B T_e} \right), \]
\[ Z_{H^+} = \left( \frac{2 \pi m_{H^+} k_B T_e}{h^2} \right)^{3/2} \exp \left( -\frac{\phi_{\text{dis}} + 2 \phi_{\text{ion}}}{2 k_B T_e} \right), \]
\[ Z_e = \left( \frac{2 \pi m_e k_B T_e}{h^2} \right)^{3/2}, \]
\[ Z_{He} = \left( \frac{2 \pi m_{He} k_B T_e}{h^2} \right)^{3/2}, \]

where \( m_{H_2}, m_H, m_{H^+}, m_e, \) and \( m_{He} \) are the masses of the elements. \( \phi_{\text{dis}} = 7.17 \times 10^{-12} \text{ erg} \) and \( \phi_{\text{ion}} = 2.18 \times 10^{-11} \text{ erg} \) are the binding energy of H and H2.

In the above, we do not consider the spin and atomic structure of any species and have ignored the rotational and vibrational degrees of freedom of H2. Incorporating these degrees of freedom would lead to very complex partition functions, yet because the energy needed to excite these transitions is small compared to the binding energy, we expect the resulting impact to be relatively minor. Moreover, we would need to use a tabulated EoS if we were to include them in the partition function, which would make our calculations inefficient and less accurate.

In many of the simulations, H2 reforms in the post-shock region. We note that the underlying assumption with our treatment of the general EoS is chemical equilibrium, implying that H2 formation is instantaneous based on the Saha equation. In reality, given that the post-shock gas density is high \( (\rho_{ps} > 10^{-6} \text{ g cm}^{-3}) \), we anticipate that efficient H2 formation can be achieved through the three-body H2 formation channel on a timescale of less than one minute (Omomukai et al. 2005), which is much shorter than the freefall time.

Appendix B
Global Shock Efficiency
Global shock efficiency \( \eta_{\text{phy}} \) quantifies the fraction of the energy that leaves the system, in our case, the radiation energy. For steady-state solutions, Equations (3) and (4) become

\[ \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 (\epsilon_{\text{kin}} + \epsilon + p) v \right) = G - \rho v \nabla \phi, \]  
\[ \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 F_r) = -G, \]

where \( \phi = -GM_p/r \) is the gravitational potential energy. We can multiply by \( r^2 \) and add up the two equations above, recognizing that \( M_p = -4\pi \rho r^2 v \) is constant in steady-state and \( 4\pi r^2 F_r = L_r \) is the luminosity, to obtain

\[ M_p \frac{\partial}{\partial r} (\epsilon + \epsilon_{\text{kin}} + p/\rho + \phi) + \frac{\partial L_r}{\partial r} = 0. \]

Equation (B3) illustrates the balance of the radiative flux and the total energy flux \( E(r) = -M_p (\epsilon + \epsilon_{\text{kin}} + p/\rho + \phi) \) in steady state. Since radiation energy is the one that leaves the system, the fraction of accretion energy radiated away, which is defined as the shock efficiency \( \eta_{\text{phy}} \), is given by

\[ \eta_{\text{phy}} = \frac{L_r (r_{\text{max}}) - L_r (r_{ps})}{E (r_{\text{max}}) - E (r_{ps})} \leq 1. \]

Consequently, \( 1 - \eta_{\text{phy}} \) is the fraction of the energy retained after the shock.

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