Lie Symmetry Group for Unsteady Free Convection Boundary-Layer Flow over a Vertical Surface

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Abstract: The Lie symmetry group transformation method was used to investigate the partial differential equations that model the motion of a natural convective unsteady flow past a non-isothermal vertical flat surface. The one-parameter Lie group transformation was applied twice consecutively to convert the motion governing equations into a system of ordinary differential equations. The obtained system of ordinary differential equations was solved numerically using the Lobatto IIIA formula (implicit Runge–Kutta method). The effect of the Prandtl number on the temperature and velocity profiles is illustrated graphically.

Keywords: lie symmetry group transform; unsteady flow; free convection; boundary-layer flow; vertical surface

1. Introduction

Ludwig Prandtl (1875–1953) presented the boundary-layer theory for the first time in 1904 [1]. He obtained the boundary layer for 2D flow equations neglecting the viscosity effect up to the outer edge of the boundary layer to simplify the Navier–Stokes equations [2]. A boundary layer is the thin region of flow relative to the body surface, where the viscosity effect is dominant and the velocity of the flow changes with vertical distance. The fluid relative to a vertical heated surface gradually increases because of the difference in density distribution resulting from a temperature difference or non-uniform distribution of concentration difference without using any external forces. This process is known as the natural convective flow. Properties of free-convective laminar boundary-layer flow are widely involved in several studies due to their ever-increasing engineering and industrial applications such as metal coating, cooling processes, waste disposal, crystal industry, heat removal in nuclear recovery, oil recovery, building construction, and so on. The difficulty in boundary-layer problems is the rapid change in the fluid properties over the thin boundary-layer regions, aside from a host of different parameters that control the basic governing boundary-layer equations.

Recently, several methods have been developed to find the most efficient strategy for solving the complicated non-linear partial differential governing equations system. Lie symmetry transform is an effective technique to deal with non-linear partial differential equations by applying simple assumptions and steps [3–8]. It is used widely in the non-linear problems that appear in fluid mechanics studies. For instance, Boutros et al. [9] obtained similarity reductions of the boundary-layer equations governing the incompressible viscous fluid flow on a heated stretching sheet placed in a porous medium. Salem and Fathy [10] used the previous work to study the effect of the mass transfer on a boundary-layer magneto-hydro-dynamic (MHD) flow considering the temperature-dependent viscosity, the thermal conductivity, and the radiation effect. Abd-el-Malek and Amin [11] applied the Lie group method to the non-linear inviscid fluid flow considering a free surface under gravity. Sivasankaran et al. [12] applied the Lie group method to the heat and mass transfer
equations of the flow over an inclined surface and investigated changes in temperature, velocity, and concentration of the fluid with Prandtl number. Nanofluids have been the topic of numerous investigations because of their greatly enhanced thermal properties. Lie group analysis was used to study the free-convective flow of the nanofluids over a porous stretching vertical sheet by Rosmila et al. [13] and Hamad and Ferdows [14], past a vertical flat plate by Hamad et al. [15], and on a horizontal plate by Rashidi et al. [16].

This paper aims to analyze the unsteady free convective boundary-layer flow over a vertical surface using the one-parameter Lie group transformation. Abd-el-Malek [17] analyzed the governing equations of boundary-layer flow over a vertical surface by applying the two-parameter group transformation and they used some suitable assumptions in their study. In this analysis, the one-parameter Lie group transformation was professionally applied to the governing equations of conservation of mass, momentum, and energy and introduced advanced generators that could be useful for future research under appropriate initial and boundary conditions. In the boundary conditions of this study, the relation between the wall temperature with the vertical distance and the time was considered, unlike in Hamad et al. [15], who dealt with wall temperature as a constant value. The accepted generators in light of the boundary conditions were re-analyzed using the Lie group transformation to obtain the final system of ordinary differential equations, which is solved numerically with the Runge–Kutta scheme. The accepted generators lead to defining a specific formula of the horizontal and vertical velocities, the temperature, and the wall temperature in terms of the vertical distance “x” and the time “t”. The present work illustrated the effect of the Prandtl number on both temperature and velocity distributions and explained how its value controls the behavior of the thermal boundary layer, which is the main problem in high-performance designs such as “gliders” and airplane airfoils to avoid the increased drag.

2. Mathematical Formulation

Consider the laminar natural-convection fluid flow adjacent to a vertical heated surface. According to the Boussinesq approximation introduced by Abd-el-Malek [18], the basic governing equations of the conservation of mass, momentum, and energy in non-dimensional form are represented by the following system of equations:

\[
\begin{align*}
u_x + \nu_y &= 0 \quad (1) \\
u_t + \nu \nu_x + \nu \nu_y &= \frac{T}{Pr} + u_{yy} \quad (2) \\
T_t + \nu T_x + \nu T_y &= \frac{1}{Pr} T_{yy} \quad (3)
\end{align*}
\]

where \( u(x, y, t) \) and \( \nu(x, y, t) \) are velocity components in the \( x \) and \( y \) directions, respectively, and \( T(x, y, t) \) represents the temperature.

For the vertical surface in Figure 1, the temperature of the fluid starts with the wall temperature \( T_\omega \), and then gradually decreases. This difference in temperature, aside from the external body force such as gravitational force, leads to density changes. The flow velocity starts from zero at the wall and varies due to buoyancy force generated from density difference inside the boundary layer until reaching zero at its outer edge. Then, the appropriate boundary conditions are given by:

\[
\begin{align*}
(i) \quad \nu &= 0, \quad u = 0, T = T_\omega(x, t) \quad \text{at } y = 0, \\
(ii) \quad u &= 0, T = 0 \quad \text{as } y \to +\infty
\end{align*}
\]

(4)
Equations (1)–(3) are invariant under the scaling transformation generated by 
\( T_\varepsilon = \exp (\varepsilon X) \), where \( \varepsilon \) is the infinitesimal parameter and \( X \) is the infinitesimal generator defined as

\[
X \equiv \xi \frac{\partial}{\partial x} + \eta \frac{\partial}{\partial y} + \tau \frac{\partial}{\partial t} + \nu \frac{\partial}{\partial u} + \lambda \frac{\partial}{\partial v} + \psi \frac{\partial}{\partial T}.
\]  

The one-parameter Lie group infinitesimal transformations of \((x, y, t; u, v, T)\) under the invariant condition after applying Taylor series in \( \varepsilon \) (neighborhood of \( \varepsilon = 0 \)) are given by:

\[
\begin{align*}
\tilde{x} &= x + \varepsilon \xi(x, y, t; u, v, T) + O(\varepsilon^2), \\
\tilde{y} &= y + \varepsilon \eta(x, y, t; u, v, T) + O(\varepsilon^2), \\
\tilde{t} &= t + \varepsilon \tau(x, y, t; u, v, T) + O(\varepsilon^2), \\
\tilde{u} &= u + \varepsilon \nu(x, y, t; u, v, T) + O(\varepsilon^2), \\
\tilde{v} &= v + \varepsilon \lambda(x, y, t; u, v, T) + O(\varepsilon^2), \\
\tilde{T} &= T + \varepsilon \psi(x, y, t; u, v, T) + O(\varepsilon^2). 
\end{align*}
\]  

Equations (1)–(3) can be written as follows:

\[
\begin{align*}
\Delta_1 \equiv u_x + v_y \\
\Delta_2 \equiv u_t + u u_x + v u_y - T - u_{yy} \\
\Delta_3 \equiv T_t + u T_x + v T_y - \frac{1}{Pr} T_{yy}
\end{align*}
\]  

The infinitesimal generator \( X \) is said to be a Lie point symmetry generator for the system of Equations (1)–(3) if

\[
X^{[i]} \left|_{\Delta \equiv 0} \right. \equiv 0, \ i = 1, 2, 3
\]  

and \( n \) represents the prolongation order for each equation according to the highest derivative. Since the system of Equations (1)–(3) has at most second-order derivatives, then the prolonged generator takes the form,

\[
\begin{align*}
X^{[1]} &\equiv X + \eta^x \frac{\partial}{\partial u_x} + \eta^y \frac{\partial}{\partial u_y} + \eta^t \frac{\partial}{\partial u_t} + \lambda \frac{\partial}{\partial u_x} + \nu \frac{\partial}{\partial u_y} + \psi \frac{\partial}{\partial u_T} + \psi^t \frac{\partial}{\partial u_T} + \ldots, \\
X^{[2]} &\equiv X^{[1]} + \eta^{xy} \frac{\partial}{\partial u_{xy}} + \psi^{xy} \frac{\partial}{\partial u_{xy}} + \ldots
\end{align*}
\]  

Figure 1. Physical model of the boundary layer flow over a vertical surface.
According to Equation (10), applying Equation (11) to Equations (7)–(9) gives the following system of differential equations:

\[
\begin{align*}
\eta^x + \lambda^y &= 0, \\
\eta^y + \eta u_x + u \eta^x + \lambda u_y + v \eta^y &= \psi + \eta^y, \\
\psi^y + \eta T_x + u \psi^x + \lambda T_y + v \psi^y &= \frac{\partial}{\partial T} \psi^y,
\end{align*}
\]

\begin{equation}
(12)
\end{equation}

where

\[
\begin{align*}
\eta^k &= D_k \eta - u_x D_k \xi - u_y D_k \phi - u_t D_k \tau, \\
\lambda^k &= D_k (\lambda) - v_x D_k \xi - v_y D_k \phi - v_t D_k \tau, \\
\psi^k &= D_k (\psi) - T_x D_k \xi - T_y D_k \phi - T_t D_k \tau,
\end{align*}
\]

\begin{equation}
(13)
\end{equation}

and \(k\) stands for \(x, y, t\). In addition,

\[
\begin{align*}
\eta^{y y} &= D_y \eta^y - u_{y x} D_y \xi - u_{y y} D_y \phi - u_{y t} D_y \tau, \\
\psi^{y y} &= D_y \psi^y - T_{y x} D_y \xi - T_{y y} D_y \phi - T_{y t} D_y \tau.
\end{align*}
\]

\begin{equation}
(14)
\end{equation}

The total derivatives with respect to \(x, y\) and \(t\) should be defined as:

\[
\begin{align*}
D_x &\equiv \frac{\partial}{\partial x} + u \frac{\partial}{\partial t} + v \frac{\partial}{\partial y} + T \frac{\partial}{\partial T} + \ldots, \\
D_t &\equiv \frac{\partial}{\partial t} + u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} + T \frac{\partial}{\partial T} + \ldots, \\
D_y &\equiv \frac{\partial}{\partial y} + u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} + T \frac{\partial}{\partial T} + \ldots,
\end{align*}
\]

Substitution from (13) and (14) into (12) gives three large expressions, which leads to the following system of determining equations:

\[
\begin{align*}
\xi_{tt} - \xi_y &= 0, \\
\phi_{tt} - \phi &= 0, \\
\tau_t &= 0.
\end{align*}
\]

\begin{equation}
(15)
\end{equation}

Solving the system of determining Equation (15) gives,

\[
\begin{align*}
\tau &= 2 c_1 t + c_2, \\
\phi &= c_1 y + F(x, t), \\
\lambda &= f_t + u F_x - c_1 v, \\
\xi &= c_3 x + c_4 t^2 + c_5 t + c_6, \\
\eta &= 2 c_4 t + c_5 + (c_3 - 2 c_1) u, \\
\psi &= 2 c_4 + (c_3 - 4 c_1) T.
\end{align*}
\]

\begin{equation}
(16)
\end{equation}

In light of the boundary conditions (4), we have \(F(x, t) = 0\). Therefore, a symmetry generator represented by (5) is a linear combination of

\[
\begin{align*}
X_1 &\equiv \frac{\partial}{\partial y} + 2 T \frac{\partial}{\partial t} - 2 u \frac{\partial}{\partial u} - v \frac{\partial}{\partial v} - 4 T \frac{\partial}{\partial T}, \\
X_2 &\equiv \frac{\partial}{\partial x}, \\
X_3 &\equiv \frac{\partial}{\partial x} + u \frac{\partial}{\partial u} + T \frac{\partial}{\partial T}, \\
X_4 &\equiv \frac{\partial^2}{\partial x^2} + 2 \frac{\partial}{\partial u} + 2 \frac{\partial}{\partial T}, \\
X_5 &\equiv t \frac{\partial}{\partial x} + \frac{\partial}{\partial u}, \\
X_6 &\equiv \frac{\partial}{\partial T}.
\end{align*}
\]

\begin{equation}
(17)
\end{equation}
3. Invariant Solution Generated by $X_1$

Under the invariant condition of the Lie group method, the characteristic equations are

$$\frac{dx}{0} = \frac{dy}{y} = \frac{dt}{2t} = \frac{du}{-2u} = \frac{dv}{-4v} = \frac{dT}{-4T}$$

(18)

Hence, the general solutions are

$$u = \frac{g(x, \theta)}{t}, \quad v = \frac{f(x, \theta)}{\sqrt{t}}, \quad T = \frac{h(x, \theta)}{t^2}.$$  (19)

where $\theta = \frac{\psi}{\sqrt{t}}$. Substitution of (19) into (1)–(3) gives the following system

$$g_x + f_\theta = 0,$$  (20)

$$-\frac{\theta}{2} g_\theta - g + g g_x + f g_\theta = h + g_{\theta\theta}$$  (21)

$$-\frac{\theta}{2} h_\theta - 2h + g h_x + f h_\theta = \frac{1}{Pr} h_{\theta\theta}$$  (22)

with boundary conditions:

$$\begin{align*}
(i) \quad &g(x, \theta) = 0, f(x, \theta) = 0, T_\omega(x, t) = \frac{h(x, \theta)}{t^2} \text{ at } \theta = 0, \\
(ii) \quad &g(x, \theta) = 0, h(x, \theta) = 0 \text{ as } \theta \to +\infty
\end{align*}$$

(23)

The one-parameter Lie group infinitesimal transformations of $(x, \theta; g, f, h)$ under the invariant condition can be given by:

$$\begin{align*}
\bar{x} = x + \epsilon \xi_1 (x, \theta; g, f, h) + O(\epsilon^2), \\
\bar{\theta} = \theta + \epsilon \phi_1 (x, \theta; g, f, h) + O(\epsilon^2), \\
\bar{g} = g + \epsilon \lambda_1 (x, \theta; g, f, h) + O(\epsilon^2), \\
\bar{f} = f + \epsilon \eta_1 (x, \theta; g, f, h) + O(\epsilon^2), \\
\bar{h} = h + \epsilon \psi_1 (x, \theta; g, f, h) + O(\epsilon^2).
\end{align*}$$

(24)

The given system of equations has the following infinitesimal generator:

$$Y = \xi_1 \frac{\partial}{\partial x} + \phi_1 \frac{\partial}{\partial \theta} + \lambda_1 \frac{\partial}{\partial g} + \eta_1 \frac{\partial}{\partial f} + \psi_1 \frac{\partial}{\partial h}$$

(25)

According to the system of Equations (20)–(22), the generator (25) prolonged the second-order generator in the form,

$$Y^{[2]} = Y + \lambda_1 k \frac{\partial}{\partial g_x} + \lambda_1 \frac{\partial}{\partial g_\theta} + \eta_1 k \frac{\partial}{\partial f_x} + \eta_1 \frac{\partial}{\partial f_\theta} + \psi_1 k \frac{\partial}{\partial h_x} + \psi_1 \frac{\partial}{\partial h_\theta} + \lambda_1 \phi_1 \frac{\partial}{\partial g_\theta} + \psi_1 \frac{\partial}{\partial h_\theta} + \ldots$$

(26)

where,

$$\begin{align*}
\lambda_1^k &= D_k \lambda_1 - g_x D_k \xi_1 - g_\theta D_k \phi_1, \\
\eta_1^k &= D_k \eta_1 - f_x D_k \xi_1 - f_\theta D_k \phi_1, \\
\psi_1^k &= D_k \psi_1 - h_x D_k \xi_1 - h_\theta D_k \phi_1.
\end{align*}$$

(27)

and $k$ stands for $x$ and $\theta$. In addition,

$$\begin{align*}
\lambda_1^{\theta\theta} &= D_\theta \lambda_1 \theta - g_\theta \theta D_\theta \xi_1 - g_\theta \theta D_\theta \phi_1, \\
\psi_1^{\theta\theta} &= D_\theta \psi_1 \theta - h_\theta \theta D_\theta \xi_1 - h_\theta \theta D_\theta \phi_1.
\end{align*}$$

(28)

The total derivatives with respect to $x$ and $\theta$ should be defined as:

$$\begin{align*}
D_x &\equiv \frac{\partial}{\partial x} + g_x \frac{\partial}{\partial g} + f_x \frac{\partial}{\partial f} + h_x \frac{\partial}{\partial h} + \ldots, \\
D_\theta &\equiv \frac{\partial}{\partial \theta} + g_\theta \frac{\partial}{\partial g} + f_\theta \frac{\partial}{\partial f} + h_\theta \frac{\partial}{\partial h} + g_{\theta\theta} \frac{\partial}{\partial g_\theta} + g_{\theta \theta} \frac{\partial}{\partial g_{\theta \theta}} + f_{\theta \theta} \frac{\partial}{\partial f_{\theta \theta}} + f_{\theta \theta} \frac{\partial}{\partial f_{\theta \theta}} + h_{\theta \theta} \frac{\partial}{\partial h_{\theta \theta}} + h_{\theta \theta} \frac{\partial}{\partial h_{\theta \theta}} + \ldots,
\end{align*}$$

(29)
Following the same technique from the previous section leads to the following system of determining the equation:

\[
\begin{align*}
\zeta_1 g &= \zeta_1 f = \zeta_1 h = \zeta_1 \theta = 0, \\
\phi_1 g &= \phi_1 f = \phi_1 h = \phi_1 \theta = 0, \\
\lambda_1 f &= \lambda_1 h = \lambda_1 x = \lambda_1 \theta = 0, \\
\psi_1 g &= \psi_1 x = \psi_1 \theta = \psi_1 hh = 0, \\
\eta_1 g &= \eta_1 f = \eta_1 h = \eta_1 \theta = 0, \\
\eta_1 &= \phi_1 x + \frac{1}{2} \phi_1, \\
\psi_1 &= \lambda_1 g h.
\end{align*}
\] (29)

Solving the system of determining Equation (29) gives

\[
\begin{align*}
\phi_1 &= v(x), \\
\lambda_1 &= c_1 g, \\
\zeta_1 &= c_1 x + c_2, \\
\eta_1 &= g \phi_1(x) + v(x), \\
\psi_1 &= c_1 h.
\end{align*}
\] (30)

According to boundary conditions (23), \(v(x) = 0\), a symmetry generator represented by (25) is a linear combination of

\[
Y_1 \equiv x \frac{\partial}{\partial x} + g \frac{\partial}{\partial g} + h \frac{\partial}{\partial h}, \\
Y_2 \equiv \frac{\partial}{\partial x}.
\] (31)

The generated solution from \(Y_2\) contradicts the boundary conditions but for \(Y_1\), the characteristic equations are

\[
\frac{dx}{x} = \frac{d\theta}{0} = \frac{dg}{g} = \frac{df}{0} = \frac{dh}{h}.
\] (32)

Hence, the general solutions are

\[
g = x R_1(\theta), \quad f = R_2(\theta), \quad h = x R_3(\theta)
\] (33)

This gives the following solutions for the original governing system:

\[
u = \frac{x R_1(\theta)}{t}, \quad v = \frac{R_2(\theta)}{\sqrt{t}}, \quad T = \frac{x R_3(\theta)}{t^2}, \quad T_\omega = \frac{x}{t^2}
\] (34)

Substitution with (34) into (20)–(22) gives the following ordinary differential equations:

\[
R_1 + R_2' = 0
\] (35)

\[
-\frac{\theta}{2} R_1' - R_1 + R_1^2 + R_2 R_1' - R_1'' - R_3 = 0
\] (36)

\[
-\frac{\theta}{2} R_3' - 2 R_3 + R_1 R_2 + R_2 R_3' - \frac{1}{Pr} R_3'' = 0
\] (37)

The initial and boundary conditions take the form

\[
(i) \quad R_1(\theta) = 0, \quad R_2(\theta) = 0, \quad R_3(\theta) = 1 \text{ at } \theta = 0, \\
(ii) \quad R_1(\theta) = 0, \quad R_3(\theta) = 0 \text{ as } \theta \to \infty^+
\] (38)

4. Invariant Solution Generated by \(X_3\)

According to \(X_3\), the auxiliary equations take the form

\[
\frac{dx}{0} = \frac{dy}{0} = \frac{dt}{0} = \frac{du}{u} = \frac{dv}{0} = \frac{dT}{T}
\] (39)
Hence, the general solutions are

\[ u = \lambda (y, t), \quad v = m(y, t), \quad T = x n(y, t). \]  \hfill (40)

Substitution of (40) into (1)–(3) gives the following system:

\[
\begin{align*}
1 + m_q &= 0 \quad \hfill (41) \\
l_i + l^2 + m l_y &= n + l_{yy} \quad \hfill (42) \\
n_t + l n + m n_q &= \frac{1}{Pr} n_{yy} \quad \hfill (43)
\end{align*}
\]

The one-parameter Lie group infinitesimal transformations of \((y, t; l, m, n)\) under the invariant condition can be given by:

\[
\begin{align*}
\bar{y} &= y + \varepsilon \phi_3(y, t; l, m, n) + O(\varepsilon^2), \\
\bar{t} &= t + \varepsilon \tau_3(y, t; l, m, n) + O(\varepsilon^2), \\
\bar{l} &= l + \varepsilon \eta_3(y, t; l, m, n) + O(\varepsilon^2), \\
\bar{m} &= m + \varepsilon \lambda_3(y, t; l, m, n) + O(\varepsilon^2), \\
\bar{n} &= n + \varepsilon \psi_3(y, t; l, m, n) + O(\varepsilon^2).
\end{align*}
\]

Following the same process introduced in Section 3 yields

\[
\begin{align*}
\phi_3 &= c_1 y + B(t), \\
\tau_3 &= 2c_1 t + c_2, \\
\eta_3 &= -2c_1 l \\
\lambda_3 &= -c_1 m + B'(t), \\
\psi_3 &= -4c_1 n.
\end{align*}
\]

The auxiliary equation can be expressed as

\[
\frac{dt}{2c_1 t + c_2} = \frac{dy}{c_1 y + B(t)} = \frac{dl}{-2c_1 l} = \frac{dm}{-c_1 m + B'(t)} = \frac{dn}{-4c_1 n} \hfill (46)
\]

According to the initial and boundary conditions, both \(B(t)\) and \(c_2\) becomes zero. Then,

\[
\frac{dt}{2c_1 t} = \frac{dy}{c_1 y} = \frac{dl}{-2c_1 l} = \frac{dm}{-c_1 m} = \frac{dn}{-4c_1 n} \hfill (47)
\]

Hence, \(l, m, n\) take the form

\[
l = P_1 \left( \frac{y}{\sqrt{t}} \right), \quad m = P_2 \left( \frac{y}{\sqrt{t}} \right), \quad n = P_3 \left( \frac{y}{\sqrt{t}} \right) \hfill (48)
\]

From (48), the forms of \(u, v\) and \(T\) from (40) are similar to (34), thus the invariant solution generated by \(X_3\) will lead to the same reduced system of ordinary differential equations from \(X_1\).

5. Invariant Solution Generated by \(X_2\) and \(X_6\)

It is found that \(X_2, X_4, X_5\) and \(X_6\) contradict the initial and boundary conditions of the system (4). Here, we try to combine \(X_2\) with \(X_6\) to find out if it generates a new possible solution. Under the invariant condition of the Lie group method, the characteristic equations are:

\[
\frac{dx}{c_6} = \frac{dy}{0} = \frac{dl}{c_2} = \frac{du}{0} = \frac{dv}{0} = \frac{dT}{0} \hfill (49)
\]
Hence, the general solutions are:

\[ u = q(y, \pi), \quad v = r(y, \pi), \quad T = s(y, \pi) \]  

(50)

where \( \pi = ax + bt \) and \( c_2 = a, c_6 = b \). Substitution of (50) into (1)–(3) gives the following system:

\[ a \, q_\pi + r_y = 0 \]  

(51)

\[ b \, q_\pi + a \, q_\pi + r \, q_y = s + q_{yy} \]  

(52)

\[ b \, s_\pi + a \, q_\pi + r \, s_y = \frac{1}{Pr^2} q_{yy} \]  

(53)

The one-parameter Lie group infinitesimal transformations of \((\pi, y; q, r, s)\), under the invariant condition, are given by:

\[
\begin{align*}
\dot{\pi} &= \pi + \varepsilon \, a \, (x, y, q, r, s) + O(\varepsilon^2), \\
\dot{y} &= y + \varepsilon \, b \, (x, y, q, r, s) + O(\varepsilon^2), \\
\dot{q} &= q + \varepsilon \, c \, (x, y, q, r, s) + O(\varepsilon^2), \\
\dot{r} &= r + \varepsilon \, \gamma' \ (x, y, q, r, s) + O(\varepsilon^2), \\
\dot{s} &= s + \varepsilon \, \delta \ (x, y, q, r, s) + O(\varepsilon^2).
\end{align*}
\]

(54)

The given system of equations has the following infinitesimal generator:

\[ Z \equiv a \frac{\partial}{\partial \pi} + b \frac{\partial}{\partial y} + \gamma' \frac{\partial}{\partial q} + \gamma \frac{\partial}{\partial r} + \delta \frac{\partial}{\partial s}, \]

(55)

The second prolongation takes the form:

\[
\begin{align*}
Z^{[1]} &= Z + \gamma'' \frac{\partial}{\partial \pi} + \gamma'' \frac{\partial}{\partial y} + \gamma' \frac{\partial}{\partial q} + \gamma \frac{\partial}{\partial r} + \delta \frac{\partial}{\partial s} + \ldots, \\
Z^{[2]} &= Z^{[1]} + \gamma''' \frac{\partial}{\partial \pi} + \gamma''' \frac{\partial}{\partial y} + \gamma'' \frac{\partial}{\partial q} + \gamma' \frac{\partial}{\partial r} + \delta \frac{\partial}{\partial s} + \ldots.
\end{align*}
\]

(56)

The steps of the one-parameter Lie group leads to the following system of determining equations:

\[
\begin{align*}
\alpha_q &= \alpha_r = \alpha_s = \alpha_y = 0, \\
\beta_q &= \beta_r = \beta_s = \beta_y = 0, \\
\gamma''_q &= \gamma''_r = \gamma''_s = \gamma''_y = \gamma''_w = 0, \\
\gamma'_{q} &= \gamma'_{r} = \gamma'_{s} = \gamma'_{y} = \gamma'_{w} = \gamma'_{h} = \gamma'_s = \gamma'_r = 0, \\
\gamma'_q &= a_\pi - \gamma'_r + \beta_y = 0, \\
\eta_{2q} - a \, \beta = 0, \\
\gamma'' &= q \, (a_\pi - 2 \beta_y) + \frac{\partial}{\partial q} (a_\pi - 2 \beta_y), \\
\gamma' &= (a + b) \, \beta - r \, \beta_y, \\
\gamma &= s \, (a_2 - 2 \beta_y).
\end{align*}
\]

(57)

Solving the system of determining Equation (57) yields

\[
\begin{align*}
\beta &= c_1 y + w (\pi), \\
\alpha &= c_2 \pi + c_3, \\
\gamma'' &= (c_2 - 2c_1) \, q + \frac{1}{2} \, (c_2 - 2c_1), \\
\gamma' &= (a + b) \, w (\pi) - c_1 r, \\
\gamma &= (c_2 - 4c_1) \, s.
\end{align*}
\]

(58)

In light of the original system, the boundary condition is \( w (\pi) = 0 \). Therefore, a symmetry generator represented by (55) is a linear combination of

\[
\begin{align*}
Z_1 &= y \frac{\partial}{\partial q} - r \frac{\partial}{\partial q} - 2 (q + \frac{b}{a} \, \frac{\partial}{\partial q} - 4s \, \frac{\partial}{\partial s}, \\
Z_2 &= \pi \frac{\partial}{\partial q} + (q + b) \, \frac{\partial}{\partial q} + s \, \frac{\partial}{\partial s}, \\
Z_3 &= \frac{\partial}{\partial \pi}.
\end{align*}
\]

(59)
It was found that all the previous generators contradict the boundary conditions. Therefore, no ordinary differential equations could be obtained for the system of Equations (51)–(53) except considering that \( b = 0 \), which contradicts the assumption from the beginning.

6. Graphical Results and Discussion

The reduced ordinary differential system of equations from the generator \( X_1 \) is equivalent to the system obtained from \( X_3 \) thus analyzing both systems leads to the same results. Ordinary differential Equations (35)–(37) with the boundary conditions (38) were solved numerically using the Lobatto IIIA formula (implicit Runge–Kutta). The impact of Prandtl number on temperature and velocity has been highlighted through graphs.

Figures 2a and 3a present the relation between the velocity and Prandtl number. The velocity magnitude decreases with rising values of Prandtl number due to the higher viscosity and small thermal conductivity, which increases the thickness of the fluid and hence decreases its velocity. Both figures show that the velocity is the maximum near the surface, then it approaches the zero far away from the surface.

![Graph](image)

**Figure 2.** (a) Dimensionless velocity \( R_1(\theta) \) as a function of \( \theta \) and (b) dimensionless temperature \( R_3(\theta) \) as a function of \( \theta \) for values of the Prandtl number <1.

The temperature distribution for different Prandtl numbers is plotted in Figures 2b and 3b. It is noticeable that the fluid temperature decreases faster with higher values of Prandtl number because of the low heat transfer of the high viscous fluids with a large Prandtl number. The plots represent the relation between the Prandtl number and the thickness of the thermal boundary layer. \( Pr < 1 \) yields a thick thermal boundary layer due to the higher thermal diffusion, but this situation reverses for \( Pr > 1 \). The presented velocity and temperature graphs found good agreement with the related physical fact in addition to the mathematical results obtained by applying the two-parameter group transformation to the governing equations introduced in [17].
Figure 3. (a) Dimensionless velocity $R_1(\theta)$ as a function of $\theta$ and (b) dimensionless temperature $R_3(\theta)$ as a function of $\theta$ for values of the Prandtl number $>1$.

Figure 3a,b documents the phenomenon of flow reverse and temperature defect. Figure 3a indicates the relationship between the flow reversal and the higher Prandtl number. Due to the smaller values of buoyancy, a reverse flow takes place away from the surface. Figure 2b depicts the overshoot in the temperature distribution near the surface with a noticeable drop for higher Pr number ($Pr > 1$) due to the smaller thermal conductivity and diffusivity. Physically, the temperature reversal occurs when the cool flow that comes from below hits the high ambient temperature, and thus the temperature undershoots. The increment of Prandtl number leads to significant temperature undershoots and a weak flow reversal. The presented attitude of velocity and temperature agrees with the physical results that emerged in [19].

7. Conclusions

In this paper, the unsteady free convective boundary-layer flow over a vertical surface was analyzed using the one-parameter Lie group transformation. Applying the Lie group transformation to the main governing motion equations introduces accurate infinitesimal generators that could be useful in future studies under different study conditions. In light of the appropriate initial and boundary conditions, the Lie group symmetry solutions for the introduced system developed suitable formulas of the velocity components, the temperature, and the wall temperature in terms of the vertical distance “$x$” and the time “$t$”. The introduced symmetry solutions can be investigated with different physical parameters for characterizing the velocity and the thermal boundary layer. The present work concentrated on studying the Prandtl number effect on the temperature and velocity profiles, in addition to the thickness of the thermal boundary layer, which were analyzed. Based on the graphical results, the velocity and the temperature distributions decreased by increasing the Prandtl number, and hence the thickness of the thermal boundary layer also decreased. The present work showed the effect of the Prandtl number on the reversal of flow and temperature due to the difference in temperature between the high ambient temperature and the lower temperature flow.
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