Optimization of Synthesis Conditions of Carbon Nanotubes via Ultrasonic-Assisted Floating Catalyst Deposition Using Response Surface Methodology

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Received: 20 March 2018; Accepted: 7 May 2018; Published: 9 May 2018

Abstract: The growing use of carbon nanotubes (CNTs) in a plethora of applications has provided to us a motivation to investigate CNT synthesis by new methods. In this study, ultrasonic-assisted chemical vapor deposition (CVD) method was employed to synthesize CNTs. The difficulty of controlling the size of clusters and achieving uniform distribution—the major problem in previous methods—was solved by using ultrasonic bath and dissolving ferrocene in xylene outside the reactor. The operating conditions were optimized using a rotatable central composite design (CCD), which helped optimize the operating conditions of the method. Response surface methodology (RSM) was utilized as the basis of designing experiments to optimize the operating conditions of the method, which was newly used to synthesize CNTs. According to the analysis results, hydrogen flow rate and temperature are more effective parameters than catalyst concentration in this method.

Keywords: floating catalyst deposition; carbon nanotubes; response surface methodology

Highlights:
• Floating catalyst (FC) chemical vapor deposition (CVD) method was used to synthesize carbon nanotubes.
• Ultrasonic bath was used in the FC method. It helped to control the cluster size, decrease the produced amorphous carbon, and improve the quality of produced carbon nanotubes (CNTs).
• Response surface methodology (RSM) was utilized as the basis of designing experiments to optimize the operating conditions of the method, which was newly used to synthesize CNTs.
• According to the analysis results, hydrogen flow rate and temperature are more effective parameters than catalyst concentration in this method.

1. Introduction
Nanotechnology is a multidisciplinary field dealing with a variety of materials produced at the nanometric scale through various physical, chemical, and biological procedures. The characteristics...
observed in nanomaterials are different from those of their bulk counterparts. Thus, they may overcome the limitations of existing products in terms of cost, functionality, fabrication strategies, and overall performance. Nanomaterials have been studied in depth as carriers in modern healthcare applications due to their tunable surface characteristics. Spherical nanoparticles are the most practical form of nanomaterials. This is due to the fact that they are easier to manufacture in comparison with nonspherical nanoparticles, such as nanowires, microtubes, and nanotubes. Particularly, carbon nanotubes (CNTs) have a large number of interesting characteristics in terms of structure, morphology, functionality, stability, ease of modification, and appropriateness in hybrid materials [1]. As such, CNTs are often a good candidate for the fabrication of devices with novel features.

CNTs are hollow cylindrical tubes consisting of carbon (graphite) with a high aspect ratio (B1000) and $sp^2$ hybridization. Considering the number of graphite layers, CNTs are classified as single-walled nanotubes (SWNTs), double-walled nanotubes (DWNTs), and multiwalled nanotubes (MWNTs) [2, 3]. These materials potentially have applications in many areas, such as electronic, mechanical, and gas storage fields [4], photonics, renewable energy, drug delivery, and the biomedical sector [5]. Consequently, CNTs potentially have various applications in several fields, such as effective hydrogen storage media, quantum wires, field emitters, field effect transistors, nanoreactors, field emission displays, adsorbents to control environmental pollution [6,7], and fillers in composites. Hence, CNT production has recently been on a huge increase.

Various techniques, including arc discharge, laser ablation, and chemical vapor deposition (CVD), can be used to synthesize CNTs. Considering the progress in the laser ablation and electrical arc discharge techniques, significant advancement has been made in large-scale production of CNTs. However, CNT synthesis via these methods cannot be carried out continuously. Thus, the production yield is limited. Furthermore, the products generally contain many impurities, which include amorphous carbon, carbon nanoparticles, $C_{60}$, and other fullerenes [8,9]. Furthermore, arc discharge and laser ablation techniques need high temperatures ($>1700 \, ^\circ C$) during synthesis. However, they have now been replaced with CVD, which can be conducted at lower temperatures ($<800 \, ^\circ C$). In addition to these techniques, some nonstandard techniques, such as pyrolysis and hydrothermal treatment, have also been used [2]. Major synthesis strategies for CNTs are briefly shown in Figure 1.

![Figure 1. Classification of synthesis methods employed for carbon nanotubes (CNTs).](image)

The synthesis strategy used in the present study is displayed in Figure 1 by the red path. The CVD method was introduced in 1993 for large-scale production of CNTs [10]. It requires the pyrolysis of
hydrocarbons (e.g., acetylene, ethylene, propylene, methane, benzene, and toluene) [11,12] or other carbon feedstock (e.g., polymers and carbon monoxide), which are carried in a stream of an inert gas into a chamber with metal catalysts (e.g., Ni, Fe, and Co). A vast variety of parameters (including hydrocarbon precursor composition, catalyst, temperature, pressure, gas flow rate, deposition time, and reactor geometry) play a role in controlling the growth mechanism of CNTs [13,14].

The temperature of the CVD-based CNT synthesis generally ranges from 500 to 1200 °C at atmospheric pressure. The basic structure of CNTs (e.g., diameter, length, and alignment) is highly dependent on and can be controlled by controlling the temperature. Moreover, adjusting the gas flow rate can control the pressure of the gaseous carbon precursor. In the case of utilizing a solid hydrocarbon precursor, the vapor pressure is optimized by controlling the hydrocarbon precursor mass, vaporizing temperature, and the carrier gas flow rate. Similarly, for a liquid hydrocarbon precursor, the vapor pressure is optimized by heating the precursor at a specific temperature before being pumped into the reactor. According to Figure 1, several CVD alternatives have been developed for synthesizing CNTs in a controlled way in order to help mass production: (1) fixed bed reactors; (2) fluidized bed reactors; (3) laser-assisted; (4) plasma-assisted (plasma sources including microwave discharge, hot filament, dc-glow discharges, radio frequency (RF) capacitive coupled plasmas and RF inductively coupled plasmas); (5) aerosol-assisted; and (6) floating catalysts [2,15,16]. Recently, the floating catalyst (FC) approach has been the focus of CNT synthesis by some researchers. This is due to its simple equipment, low reaction temperature, low cost, and its ability to produce highly pure CNTs continuously [8,9]. Considering that the FC method has the potential to act as an industrial process for high-yield production of pure CNTs, some investigations have been carried out to optimize the processing operating conditions. It has been found that the decrease in ferrocene/benzene mole ratio contributes to an increase in the diameter of CNTs [4].

Care should be taken for the removal of metal catalyst impurities for any method used to synthesize CNTs because metals may impact the electrocatalytic characteristics of CNTs. Despite the fact that several purification methods are considered to be acceptable, the purified amount of CNTs still varies for different techniques. Large-scale production of purified CNTs needs economic methods for isolating the purified product from metallic and amorphous impurities. It is anticipated that such approaches will decrease the market price of CNTs for application in diverse fields. Therefore, producing CNTs with economic feasibility is a challenge for researchers.

Li and coworkers [17] proposed a possible explanation of the difference in carbon vapor deposition products based on different pyrolytic behaviors of carbon precursors and formation mechanism. Yamada et al. [18] proved that the number of layers in the CNTs depends more on the catalyst size than on the diameter of CNTs. Less amorphous carbon and CNTs with smaller diameter are desired, considering their higher quality. Therefore, controlling the cluster size and consequently their uniform distribution are of high importance because they decrease the tendency of clusters to become agglomerated.

In this research, a modification was carried out in the synthesis process in order to overcome the shortcomings with respect to the control of cluster size and uniform distribution in the FC method. In this modification, the catalyst was dissolved in xylene outside the reactor, and ultrasonic bath was used to prevent the agglomeration of clusters. It is worth mentioning that using ultrasonic bath hinders the agglomeration. It has been used in different studies for different substances [19,20] and we used it for synthesizing CNTs. According to Beltowska-Lehman et al. agglomeration of nanoparticles can be prevented considerably by physical dispersion, including by ultrasound. The propagation of ultrasonic waves in the bath generates high pressure, inducing stress, which leads to less agglomeration of nanoparticles [21]. According to Versteeg et al. using an ultrasonic atomizing nozzle ensures that the liquid solution is broken up into a fine mist of tiny droplets, which hinders the agglomeration of particles [22]. In order to study the impact of main synthesis parameters and obtain optimized process variables, response surface methodology (RSM) under DESIGN EXPERT software was used. RSM is a collection of statistical and mathematical techniques used for modeling and analyzing engineering
problems [23]. In this methodology, the major goal is to optimize the response surface, which is affected by different process parameters at the same time, by considering any possible interactions between different parameters. Moreover, RSM quantifies the relationship between the controllable input parameters and the obtained response surfaces [24].

2. Experimental Procedures

2.1. Dispersing Catalyst in Carbon Precursor

The old FC method, which is based on dissolving the catalyst in carbon feedstock outside the reactor, exhibits some problems (e.g., difficulty in controlling the size of clusters and their agglomeration). Thus, ultrasonic-assisted CVD method was used in this study to keep the solution homogeneous outside the reactor. In the present work, an apparatus was designed aiming to better control experimental parameters and to obtain CNTs with more desirable properties. The schematic diagram of the apparatus is presented in Figure 2. The quartz tube was 1000 mm long and its diameter was 25 mm. The quartz tube was located in a cylindrical furnace (Carbolite, Watertown, MA, USA). Xylene, hydrogen, and ferrocene were used as the carbon source, the carrier gas, and the catalyst precursor, respectively. It is worth mentioning that the inert gas of argon, which is shown in the Figure 2, was used to remove the oxygen from the reactor.

![Figure 2. Diagram of the CNT synthesis apparatus.](image)

In order to keep the solution homogeneous, two methods were compared in this study: (1) using stirring heater; and (2) using ultrasonic bath. The obtained results of thermogravimetric analysis (TGA) showed that using ultrasonic bath was a more suitable technique. The ferrocene-xylene solution was preheated at 50 °C. Subsequently, hydrogen gas carried the solution into the reactor. Partial pressure of catalyst/carbon depended on hydrogen flow rate. Using ultrasonic bath (Bandelin Sonorex Super, Berlin, Germany) provided a homogeneous solution in which controlling the ferrocene/xylene proportion was possible. It is worth mentioning that ferrocene and xylene were both provided from Merck KGaA, Darmstadt, Germany. First, the metal-organic precursor was reduced by hydrogen to form atomic iron and agglomerated to iron clusters or iron particles to grow CNTs. After CNT synthesis, the carbon products were deposited on the cooler zone of reaction tube wall.

In order to characterize the morphology and microstructure of the synthesized products, some characterization techniques were applied, including: TGA, field-emission scanning electron microscopy (FESEM), transmission electron microscopy (TEM), and Raman spectroscopy.

2.2. Experimental Design and Data Analysis

RSM is an effective and flexible experimental design methodology for modeling and analyzing a problem in which the response is under the influence of several variables [25,26]. After performing
the designed experiments, the procedure of response analysis is carried out and the presented model is analyzed by general statistical tests, such as Fisher’s statistical test (F-test). The test determines the F-value, the p-value, and R² coefficient and the model can be analyzed by investigating these values. F-test can state the importance of any process parameter. The larger the F-value, the more valid the model [27]. For any parameter to be a significant, the p-value (probability value) must be less than 0.05. However, in RSM, a p-value of lack-of-fit >0.05 (not significant) means that the model fits well [28]. The coefficient of determination (R² value) certifies reasonable fitting of the model with experimental data. If R² is close to 1, it shows good fitness of the correlation between the predicted and experimental values [29].

In comparison with the conventional optimization method, RSM can provide more information from fewer experiments. Hence, it is time-saving and economic. [30]. RSM consists of a collection of empirical techniques, which are allotted to the evaluation of the relationship that exists between a cluster of controlled experimental factors and measured responses based on one or more chosen criteria. In RSM, central composite design (CCD) determined the optimum operating conditions for the synthesis of CNTs [31]. Optimization studies were performed by studying the impact of three variables: hydrogen flow, catalyst concentration, and synthesis temperature. The system behavior is explained by the following empirical second-order polynomial model (Equation (1)):

\[ Y = \beta_0 + \sum_{i=1}^{k} \beta_i x_i + \sum_{i=1}^{k} \beta_{ii} x_i^2 + \sum_{i<j}^{k} \beta_{ij} x_i x_j \]

where \( Y \) is the predicted response, and \( x_i, x_j, \ldots, x_k \) represent the input variables, which influence the response \( Y \). \( x_i^2, x_j^2, \ldots, x_k^2 \) are the square effects, \( x_i x_j \) and \( x_j x_i \) are also the interaction effects. \( \beta_0 \) is the intercept term, \( \beta_i \) (\( i = 1, 2, \ldots, k \)) is the linear effect, \( \beta_{ii} \) (\( i = 1, 2, \ldots, k \)) is the squared effect, and \( \beta_{ij} \) (\( i = 1, 2, \ldots, k; j = 1, 2, \ldots, k \)) is the interaction effect [32].

The DESIGN EXPERT software (Design Expert 6, Stat-Ease, Minneapolis, MN, USA) was used for regression and graphical analysis of the obtained data. In this research, CCD was utilized to probe the characterization of CNT synthesis by fitting a quadratic surface, which is the common tool for process optimization. By solving the regression equation at desired values of the process responses as the optimization criteria, the optimum values of the chosen variables were obtained. Each parameter was coded at five levels: \( -\alpha, -1, 0, +1, \) and \(+\alpha \) (\( \alpha = \pm 2 \)). The range and the level of the variable in coded units from RSM investigations are presented in Table 1.

| Variables                              | Range and Level |
|----------------------------------------|-----------------|
| Catalyst concentration (wt %) (\( x_1 \)) | 2 3 4 5 6       |
| Reaction temperature (°C) (\( x_2 \))   | 800 900 1000 1100 1200 |
| Hydrogen flow (cm³/min) (\( x_3 \))     | 120 100 200 240 280 |

3. Results and Discussion

3.1. Suitable Dispersion Method

In order to select the effective dispersion method (stirring heater or ultrasonic bath) to obtain a homogeneous ferrocene-xylene solution during the synthesis process, the same operating conditions (catalyst concentration = 4 wt %, hydrogen flow = 200 cm³/min, and temperature = 1000 °C) were applied for each dispersion method. In another investigation, Bai et al. [4] reported that the inner diameter of CNTs is controlled by the size of the catalyst particle during the growth process. Similarly, in this study, controlling the size of catalyst particles and having a homogeneous solution had strong
effect on the structure of synthesized CNTs. As displayed in Figure 3, the ultrasonic curve in contrast to stirring heater has a much sharper slope in the range of 400–700 °C, which corresponds to CNTs.

![Figure 3. TGA data for pristine CNTs by using ultrasonic bath and stirring heater as two dispersion methods (catalyst concentration = 4 wt %, hydrogen flow = 200 cm³/min, and temperature = 1000 °C).](image)

Table 2 shows the percentage of each carbon structure existing in the sample using Figure 3 and indicates higher productivity yield of CNTs using ultrasonic bath in comparison with a stirring heater. When the ultrasonic bath is used, there would be less agglomeration of catalyst particles, smaller ferrocene particles size, and hence higher quality nanotubes and less amorphous carbon.

| Methods          | Carbon Structure (wt %) |
|------------------|-------------------------|
|                  | Amorphous Carbon | SWNT | MWNT |
| Ultrasonic bath  | 7               | 30   | 45   |
| Stirring heater  | 65              | 7    | 8    |

This is a clear indication of higher CNT production rate via ultrasonic bath application in the CNT synthesis. Moreover, the SEM results shown in Figure 4 reveal that using ultrasonic bath provides nanotubes with smaller diameters, which we consider beneficial results. As illustrated in Figure 4, the ultrasonic-assisted technique seems to produce CNTs with smaller diameters and less amorphous carbon in comparison with those produced using stirring heater (27 nm in comparison with 121 nm, respectively).

3.2. Central Composite Design and Fitted Regression Model

In order to study the relationship between the experimental parameters and Raman spectroscopy analysis of CNTs, 20 experiments designed by CCD were performed. Determination of the error value was the reason for repeating the experiments. Moreover, when the average of the data is used to estimate the effect of each factor, repetition makes the effect more accurate. The number of these repetitions is based on statistical rules and the method we chose for experimental design (central composite design). To put it more simply, the software determined the number of repetitions.

In this study, the diameter of the quartz tube and the reaction time were kept constant (2.5 cm and 80 min, respectively). The operating conditions of synthesis experiments and \((I_C/I_D)\) ratio are given in Table 3.
Moreover, in Figure 5 the Raman spectroscopy results of CNT samples with run number of (a) 4 and (b) 16 are shown.

Figure 4. SEM image of pristine CNTs (a,b) using ultrasonic bath (the scale bars represent 1 µm and 500 nm, respectively) and (c,d) using stirring heater (the scale bars represent 1 µm and 500 nm, respectively) (catalyst concentration = 4 wt %, hydrogen flow = 200 cm³/min, and temperature = 1000 °C).

Table 3. Experimental runs based on central composite design (CCD) and Raman spectroscopy data at constant reaction time (80 min) and internal diameter (2.5 cm).

| Run No. | Catalyst Concentration (wt %) | Hydrogen Flow Rate (cm³/min) | Temperature (°C) | Raman (I₆/I₃) |
|---------|-------------------------------|-------------------------------|-----------------|-------------|
| 1       | 3                             | 160                           | 900             | 5.4         |
| 2       | 5                             | 160                           | 900             | 4.4         |
| 3       | 6                             | 200                           | 1000            | 2.83        |
| 4       | 5                             | 240                           | 1100            | 1.87        |
| 5       | 4                             | 200                           | 1000            | 6           |
| 6       | 4                             | 200                           | 1000            | 6.67        |
| 7       | 4                             | 200                           | 1200            | 0.96        |
| 8       | 4                             | 200                           | 1000            | 6.33        |
| 9       | 4                             | 120                           | 1000            | 3.7         |
| 10      | 3                             | 240                           | 900             | 3.2         |
| 11      | 4                             | 280                           | 1000            | 1.05        |
| 12      | 2                             | 200                           | 1000            | 3.8         |
| 13      | 4                             | 200                           | 1000            | 6.48        |
| 14      | 4                             | 200                           | 800             | 2.00        |
| 15      | 3                             | 160                           | 1100            | 3.26        |
| 16      | 5                             | 240                           | 900             | 2.5         |
| 17      | 4                             | 200                           | 1000            | 6.3         |
| 18      | 5                             | 160                           | 1100            | 2.92        |
| 19      | 3                             | 240                           | 1100            | 2.16        |
| 20      | 4                             | 200                           | 1000            | 5.88        |
Figure 5. Raman spectra of the products using: (a) catalyst concentration = 5 wt %, hydrogen flow rate = 240 cm$^3$/min, and temperature = 1100 °C, ($I_G/I_D$) = 1.87 and (b) catalyst concentration = 5 wt %, hydrogen flow rate = 240 cm$^3$/min, and temperature = 900 °C, ($I_G/I_D$) = 2.5.

Considering the operational conditions of these two samples, it is possible to find more insights on the temperature effect on the characteristics of synthesized nanotubes. Moreover, according to Figure 5, the value of ($I_G/I_D$) is higher at lower temperatures and decreases as the temperature increases.

The empirical relationship between $I_G/I_D$ ratio (Y), where ($I_G/I_D$) is the ratio of symmetry-allowed G-band to disorder-induced D-band, and the synthesis parameters, in coded units and obtained by RSM, are shown in Equation (2). A group of peaks around 1340 cm$^{-1}$, called the “D-band”, is attributed to disorder in graphitic materials. Another significant mode is the G mode (G from graphite), which is in the range of 1550–1600 cm$^{-1}$. G mode, which is present in most graphite-like materials, is associated with the planar vibrations of carbon atoms. The ($I_G/I_D$) ratio quantifies the structural quality of CNTs. Study of the D- and G-band modes by Raman spectroscopy gives information about the crystal structure of the product and about many of its interesting physical properties. A line is present around 2600 cm$^{-1}$; it is an overtone or second-order harmonic of the D mode. It is called G’ or D* or 2D. The G’-band indicates long range order in a sample and arises from a two-phonon, second-order scattering process, which creates an inelastic phonon [33]. Longer 2D peaks show better crystallinity and graphitization, which means CNTs of better quality.

Raman spectroscopy gives information about purity, tube alignments, crystalline size, clustering of the sp$^2$ phase within a given sample, the presence of sp$^3$ hybridization and chemical impurities, its mass density, optical energy gap, elastic constants, and doping and defects of CNTs [34].

Moreover, A, B, and C are the coded values for catalyst concentration, hydrogen flow rate, and reaction temperature, respectively.

$$Y = (I_G/I_D) = +6.25 - 0.27A - 0.72B - 0.46C - 0.75A^2 - 0.99B^2 - 1.21C^2 + 0.044AB + 0.13AC + 0.24BC$$

F- and p-values, which are shown in Table 4, determine the significance of each coefficient. The model F-value of 60.71 shows that the model is significant. The p-values less than 0.05 indicate that the model terms are significant. Furthermore, p-value of hydrogen flow is <0.0001, which reveals that this parameter has a more significant influence on the quality of CNTs. The lack-of-fit value in this model (0.2532) shows a good compatibility between the experimental and the predicted data.

In this design, the value of the correlation coefficient, $R^2 = 0.982$, and the value of the adjusted determination coefficient, $R^2 (Adj.) = 0.966$, certify a good correlation between the predicted and the observed values. In order to obtain a better view of the model significance, the actual and the predicted values are compared in Figure 6.
Table 4. Analysis of variance (ANOVA) for the response surface quadratic model.

| Source | Sum of Square | DF | Mean Square | F-Value | p-Value | Remarks |
|--------|--------------|----|-------------|---------|---------|---------|
| Model  | 68.11        | 9  | 7.57        | 60.71   | <0.0001 | significant |
| A      | 1.14         | 1  | 1.14        | 9.14    | 0.0128  |          |
| B      | 8.34         | 1  | 8.34        | 66.89   | <0.0001 |          |
| C      | 3.39         | 1  | 3.39        | 27.23   | 0.0004  |          |
| A2     | 14.29        | 1  | 14.29       | 114.63  | <0.0001 |          |
| B2     | 24.59        | 1  | 24.59       | 197.23  | <0.0001 |          |
| C2     | 36.97        | 1  | 36.97       | 296.59  | <0.0001 |          |
| AB     | 0.015        | 1  | 0.015       | 0.12    | 0.7332  |          |
| BC     | 0.48         | 1  | 0.48        | 3.81    | 0.0794  |          |
| AC     | 0.14         | 1  | 0.14        | 1.15    | 0.3091  |          |
| Residual | 1.25     | 10 | 0.12        |         |         |         |
| Lack of fit | 0.81 | 5  | 0.16        | 1.88    | 0.2532  | not significant |
| Pure error | 0.43 | 5  | 0.087       |         |         |         |
| Cor total | 69.36    | 19 |             |         |         |         |

CV: 9.09; SD: 0.35; R²: 0.982; R² (Adj.): 0.966.

Figure 6. Experimental and theoretically predicted values for Raman spectroscopy analysis.

3.3. Effect of Operating Conditions on CNTs

As shown in Figure 7, the effects of operating conditions (reaction temperature, hydrogen flow rate, and catalyst concentration) on CNT synthesis were investigated. The trend of hydrogen in the diagrams is very complicated. First, it acts as the carrier gas. The hydrogen flow carried xylene and catalyst precursors (ferrocene) into the reactor, and the hydrogen flow rate affects the partial pressure of xylene and ferrocene. Second, ferrocene is reduced and decomposed into iron atoms in the hydrogen, which further agglomerate into iron clusters or iron particles [18]. The results of Figure 7a show that by increasing the hydrogen flow rate, \((I_G/I_D)\) value increases with a low slope up to approximately 180 cm³/min of hydrogen flow in which the maximum quality of CNTs is produced. Subsequently, further increase in hydrogen flow contributes to a decrease in CNT quality. As illustrated in Figure 7b, the \((I_G/I_D)\) ratio improves slightly by increasing the catalyst concentration. However, this ratio decreases with a low slope after the optimum point (the maximum value of \((I_G/I_D)\)). As displayed in Figure 7c, the higher reaction temperature improves the quality of CNTs up to approximately 970 °C at which the highest quality of CNTs is observed, and increasing the temperature beyond that point decreases CNT quality. This phenomenon may be explained by considering that increasing the temperature with a constant catalyst concentration first enhances the solubility of carbon atoms into iron particles up to the optimum point (the maximum value of \((I_G/I_D)\)) [8]. Beyond this point, a decrease in CNT quality occurs, which is due to the increase in agglomeration of iron nanoparticles after melting.
Decreasing the concentration of iron particles in the reaction volume decreases the number of collisions among these species, hence, the resulting nuclei are relatively small and uniform. This phenomenon results in preferential formation of SWNTs. Increasing the concentration of Fe particle contributes to the formation of larger catalytic sites and products consisting primarily of MWNTs [9]. The effect of catalyst concentration on CNT synthesis was studied in the operating range of 3–5 wt %. The higher ferrocene concentrations enhance CNT quality up to approximately 4 wt % at which the best quality of CNTs is formed but, beyond that, a decrease in CNT quality ($I_G/I_D$) is observed. The observed trend may be explained by considering that a higher agglomeration tendency is expected at higher ferrocene concentrations. The explained trends (relative symmetry) are also noticeable via the circular contours in Figure 7. The higher observed symmetry in Figure 7c displays a more uniform behavior of catalyst concentration during the CNT synthesis compared with that of hydrogen flow rate and reaction temperature.

**Figure 7.** Three-dimensional surface graph to investigate the effect of (a) hydrogen flow rate (cm$^3$/min) and reaction temperature (°C); (b) catalyst concentration (wt %) and hydrogen flow rate; (c) catalyst concentration (wt %) and reaction temperature (°C).
TEM images from a number of as-prepared CNTs are shown in Figure 8. The results presented in Figure 8a–c are associated with the tests 10, 9, and 2, respectively. As it is observed in Figure 8, the diameter of nanotubes ranges between 10 and 25 nm and CNTs are uniform.

3.4. Optimization Using the Desirability Functions

The optimization was carried out by Design Expert aiming to find the best operating conditions that will lead to the best quality CNTs. We specified a limit for each factor. Desirability in the program is defined to be an objective function ranging from zero (outside the limits) to one (at the goal). The maximization of this function is the ultimate aim of this program. Since the response surfaces have a curvature format, more than one maximum point and their combination into the desirability function is expected. The standard routine of this computer software is to start from many points in the design space until the search ends up by finding the “best” local maximum. A multiple response method was used for optimizing any combination of four goals, namely, the catalyst concentration ratio, reaction temperature, hydrogen flow rate, and CNT quality ($I_C/I_D$). An optimum point which maximizes the desirability function was found by the numerical optimization. Figure 9 shows a ramp desirability generated from 10 optimum points via numerical optimization.
Based on the results from Figure 10, the best local maximum response surface \( (I_{C}/I_{D}) = 6.47 \) was predicted via RSM (Equation (2)) to be at the optimal operating conditions of catalyst concentration ratio of 3.8 wt %, hydrogen flow rate of 184 mL/min, reaction temperature of 976 °C, and desirability of 0.93. The triplicate experimental syntheses were carried out at the aforementioned optimum operating conditions in which a very close compatibility (CNTs production \( (I_{C}/I_{D}) = 6.4 \)) was observed. As shown in Figure 10, \( (I_{C}/I_{D}) \) is close to the predicted value.

![Raman spectra of the CNTs synthesizing in optimum conditions (catalyst concentration \( = 3.79 \) wt %, hydrogen flow = 185 cm\(^3\)/min, and temperature = 975 °C, \( (I_{C}/I_{D}) = 6.4 \)).](image)

According to Figure 10, higher quality CNTs are produced at optimal operating conditions. The radial breathing mode (RBM) Raman features are unique to CNTs and happen with frequencies between 120 cm\(^{-1}\) and 350 cm\(^{-1}\) for SWNTs [35]. The presence of this peak in most of the samples is due to the impact of ultrasonic bath and its prevention of the agglomeration of iron nanoparticles, which has increased the probability of producing CNTs with smaller diameters. Considering that in the sample produced under the optimum conditions we have the lowest D-band value in comparison with G-band value, it can be concluded that the highest number of few-walls were produced in the sample.

4. Conclusions

In the present study, in order to control the size of CNT clusters and distribute them uniformly, ultrasonic bath was used in the floating catalyst technique. The obtained results show the effectiveness of this method in controlling catalyst nanoparticle size, decreasing the produced amorphous carbon, and improving the quality of produced CNTs in comparison with the previous methods.

To this end, RSM was applied in characterizing the effects of this parameter and the three process variables in order to consider the interaction effects, too. Catalyst concentration, hydrogen flow rate, and synthesis temperature, which are the three effective parameters in CCD, were optimized in the present work. Analysis results showed that hydrogen flow rate and temperature are more effective than catalyst concentration. This might have been induced by the fact that the experiments were carried out at low catalyst concentration.

The quadratic model obtained by CCD and the lack-of-fit value in this model (0.2532) show a good compatibility between the experimental and the predicted data. In this design, analysis of variance displayed a coefficient of determination value (0.966–0.982) which ensures a good correlation between the predicted and the observed values. Furthermore, triplicate experimental synthesis at the optimum operating conditions resulted in a CNT production of 6.4, which confirms the modeling prediction.
Author Contributions: N.M. performed literature survey, built the experimental set up, performed the computations, planned the experiments, carried out the experiments and fabricated and characterized the samples, analyzed the data, drafted the manuscript, contributed in designing the figures and also in the final revision of the manuscript including revision of the figures. S.M.G. supervised the whole project, supported the preparation of the materials and instruments, supported the characteriztion of the samples and supervised drafting the manuscript. S.H. contributed in characterizing the samples, performed the English revision of the manuscript, contributed in the final revision of the manuscript including revision of the figures. S.S. contributed in supervision of the final manuscript and in designing the figures and also adding the main part of literature to the introduction, performed the revision of the figures and contributed in the final revision of the manuscript. D.D.D. supervised the final manuscript and contributed in the revision of the final manuscript.

Acknowledgments: The authors would like to express their genuine gratitude to Isfahan University of Technology (IUT), Department of Chemical Engineering and Iran Nanotechnology Initiative Council (INIC) for the financial support of the project. They are also very grateful for the precious guidance of Alimorad Rashidi, assistant professor of Research Institute of Petroleum Industry (RIPI).

Conflicts of Interest: The authors declare no conflicts of interest.

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