Tuning of Passivity-Based Controllers for Mechanical Systems

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Abstract—This article describes several approaches for tuning the parameters of a class of passivity-based controllers for standard nonlinear mechanical systems. In particular, we are interested in tuning controllers that preserve the mechanical system structure in the closed loop. To this end, first, we provide tuning rules for stabilization, i.e., the rate of convergence (exponential stability) and stability margin (input-to-state stability). Then, we provide guidelines to remove the overshoot. In addition, we propose a methodology to tune the gyroscopic-related parameters. We also provide remarks on the damping phenomenon to facilitate the practical implementation of our approaches. We conclude this article with experimental results obtained from applying our tuning rules to a fully actuated and an underactuated mechanical system.

Index Terms—Passivity-based control (PBC), robot control, performance, stability of nonlinear systems.

I. INTRODUCTION

THE modeling and control of mechanical systems have been widely studied and reported in the literature due to their fundamental role in industries such as aerospace, automotive, biomedics, semiconductors, or manufacturing.

For modeling, we find the port-Hamiltonian (pH) framework among the existing approaches. This framework is an energy-based modeling technique that represents a large class of nonlinear physical systems from different domains [1], [2]. Moreover, it highlights the physical properties of the system under study. In particular, for the mechanical domain, this modeling approach underscores the role of the interconnection structure, dissipation, potential, and kinetic energy play in the system behavior. Furthermore, the passivity property of the system can be verified by selecting the total energy of the system—i.e., the Hamiltonian—as the storage function.

On the other hand, amidst the existing control strategies to stabilize pH mechanical systems, we study the passivity-based control (PBC) methodologies, a set of well-established techniques that offer a constructive approach for stabilizing a large class of complex systems [3], [4]. In general, these techniques consist of two main steps: 1) the so-called energy shaping (resp. power shaping) process and 2) the damping injection. The former step modifies the total energy (resp. power) of the system to guarantee that the closed-loop system has a stable equilibrium at the desired point; in addition, the interconnection structure of the closed-loop system may be modified as a result of this step. Then, the second step ensures asymptotic stability properties for the desired equilibrium point. Some results of PBC approaches for stabilizing mechanical systems can be found in [5], [6], [7], [8], [9], and [10].

Customarily, the control parameters of PBC approaches are selected such that its closed-loop system exhibits a prescribed performance in terms of stability. For instance, in [4], [11], [12], and [13], we find results on $L_2$ stability, asymptotic stability, input-to-state (ISS) stability, and exponential stability (ES). However, sometimes, it is not sufficient to only prescribe a performance in terms of stability for several real applications [14], [15]. For instance, it is essential to ensure a prescribed performance in terms of other indices (e.g., oscillations and rate of convergence) to solve a task from applications involving mechanical systems that require high precision.

In contrast to the linear counterpart—where we can find a substantial amount of results on tuning the linear (PID) controller [16]—the literature on tuning the gains for any nonlinear controller (including PBC schemes) is relatively scarce as the characterization of the nonlinear phenomena is in several cases an open problem. Moreover, despite the well-known theoretical advantages (e.g., stability guarantees and improved performance despite the nonlinearities phenomena) of the nonlinear schemes compared with their linear counterpart, there is an evident gap between the practitioners and the theorists. This breach stems from the fact that implementing the nonlinear schemes is challenging and rarely seen in real-life applications as there are no guidelines to achieve a desirable performance. Moreover, an additional challenge in creating tuning methodologies in the nonlinear field is that there is no unified framework for characterizing the frequency domain for the nonlinear systems, although there are a few tuning methods for nonlinear approaches—e.g., neural networks [17], [18]—stability guarantees remain a challenge.

Amid the PBC schemes, we find the interconnection and damping assignment (IDA)-PBC methodology, which is a
universally stabilizing controller in the sense that it generates all asymptotically stabilizing controllers for systems that can be represented in the pH structure [19]. To tune this scheme, Kotyczka [20] proposed a methodology that consists of prescribing local dynamics to the closed-loop system via the eigenvalue assignment approach. However, the gain selection process from this methodology lacks physical intuition. Additional results for other PBC approaches can be found in [9], [21], [22], [23], [24], and [25], where they demonstrate that the parameters can be associated directly with the physical quantities of the closed-loop system—e.g., damping or energy. Ferguson et al. [21] and Chen-Zheng et al. [22] explored the relationship of the parameters with the decay ratio of the system trajectories via a particular choice of Lyapunov candidates; while in [9], [23], [24], and [25], we find the results for tuning the gains to remove the oscillations exhibited during the transient response. Moreover, in [10], we find the results on tuning the gyroscopic-related forces, where the authors demonstrate an improved performance in terms of oscillations; however, no theoretical background is provided. The inclusion of the gyroscopic forces is critical for stabilizing some underactuated mechanical applications (see [26], [27], [28], [29]).

Nonetheless, to the best of the authors’ knowledge, there is no comprehensive set of tuning methodologies in the literature for PBC approaches on standard mechanical systems that prescribe the performance of the closed-loop system in terms of other indices rather than the stability. In this article, we provide tuning methodologies for PBC approaches that in closed loop other indices rather than the stability. In this article, we provide the tuning rules to prescribe the behavior of the closed-loop system in the vicinity of the desired equilibrium. Section V, we provide some remarks on the practical implementation of the tuning rules. Then, we describe the experimental results obtained from two separate configurations: 1) a five-degree-of-freedom (DOF) robotic arm (a fully actuated mechanical system) and 2) a 2-DOF planar manipulator with flexible joints (an underactuated mechanical system), in Section VI. We conclude this article with some remarks and future work in Section VII.

Notation: We denote the $n \times n$ identity matrix as $I_n$, the $n \times m$ matrix of zeros as $0_{n\times m}$. For a given smooth function $f : \mathbb{R}^n \to \mathbb{R}$, we define the differential operator $\nabla_x f := (\partial f / \partial x)$, which is a column vector, and $\nabla_x^2 f := (\partial^2 f / \partial x^2)$. For a smooth mapping $F : \mathbb{R}^n \to \mathbb{R}^m$, we define the $ij$-element of its $n \times m$ Jacobian matrix as $(\nabla_x F)_{ij} := (\partial F_i / \partial x_j)$. When clear from the context, the subindex in $\nabla$ is omitted. For a given vector $x \in \mathbb{R}^n$, we say that $A$ is positive definite (semidefinite), denoted as $A > 0$ ($A \succeq 0$), if $A = A^\top$ and $x^\top A x > 0$ ($x^\top A x \geq 0$) for all $x \in \mathbb{R}^n - \{0\}$. For a given vector $x \in \mathbb{R}^n$, we denote the Euclidean norm as $\|x\|$ and the $L_2$-norm as $\|x\|_2$. For a given matrix $B \in \mathbb{R}^{n \times m}$, we denote its largest singular value as $\sigma_{\text{max}}(B)$. For $B = B^\top$, we denote by $\lambda_{\text{max}}(B)$ [resp. $\lambda_{\text{min}}(B)$] as the maximum (resp. minimum) eigenvalue of $B$. Given a distinguished element $x_0 \in \mathbb{R}^n$, we define the constant matrix $B_0 := B(x_0) \in \mathbb{R}^{n \times m}$. We denote $\mathbb{R}_+$ as the set of strictly positive real numbers and $\mathbb{R}_{\geq 0}$ as the set $\mathbb{R}_+ \cup \{0\}$. If $x, y \in \mathbb{R}^n$, we define $\text{col}(x, y) := [x^\top \ y^\top]^\top$. We denote $e_i$ as the $i$th element of the canonical basis of $\mathbb{R}^n$. All the functions considered in this article are assumed to be (at least) twice continuously differentiable.

Caveat: When possible, we omit the arguments to simplify the notation.

II. PRELIMINARIES AND PROBLEM FORMULATION

In this section, we provide the pH representation of standard mechanical systems considered throughout this article. Moreover, we present the target dynamics and provide a brief discussion on some PBC approaches that can achieve such dynamics. Then, we describe a particular pH structure, namely, the canonical Hamiltonian system. In addition, we discuss some stability properties and conclude this section with the problem formulation.

A. Description of Standard Mechanical Systems

Consider a standard mechanical system in the pH framework

$$
\begin{bmatrix}
\dot{q} \\
\dot{p}
\end{bmatrix} = \begin{bmatrix}
0_{n \times n} & I_n \\
-I_n & -D(q, p)
\end{bmatrix} \begin{bmatrix}
\nabla_q H(q, p) \\
\nabla_p H(q, p)
\end{bmatrix} + \begin{bmatrix} 0_{n \times m} \\
G(q)
\end{bmatrix} u
$$

$$
H(q, p) = \frac{1}{2} p^\top M^{-1}(q) p + U(q), \quad y = G(q)^\top M^{-1}(q) p
$$

where $q, p \in \mathbb{R}^n$ are the generalized positions and momenta vectors, respectively; $H : \mathbb{R}^n \times \mathbb{R}^n \to \mathbb{R}$ is the Hamiltonian.
of the system; the potential energy of the system is denoted with \( U : \mathbb{R}^n \to \mathbb{R} \); \( M : \mathbb{R}^n \to \mathbb{R}^{n \times n} \) corresponds to the mass inertia matrix, which is positive definite; \( D : \mathbb{R}^n \times \mathbb{R}^n \to \mathbb{R}^{n \times n} \) is positive semidefinite and represents the natural damping of the system; \( u, y \in \mathbb{R}^m \) are the control and passive output vectors, respectively; \( m \leq n \); and \( G(q) : \mathbb{R}^n \to \mathbb{R}^{n \times m} \) is the input vector with \( \text{rank}(G) = m \), which we define—to ease the presentation of the results—as

\[
G := \begin{bmatrix} 0_{\ell \times m} \\ I_m \end{bmatrix}
\]

with \( \ell := n - m \).

The set of assignable equilibria for (1) is defined by

\[
\mathcal{E} := \{ q, p \in \mathbb{R}^n \mid p = 0 \_n, \; G^\top \nabla U(q) = 0 \_\ell \}
\]

where \( G^\top := [I_\ell \ 0_{\ell \times m}] \).

Moreover, for all \( q \), \( M(q) \) is bounded, i.e.,

\[
\lambda_{\text{min}}(M(q)) I_n \leq M(q) \leq \lambda_{\text{max}}(M(q)) I_n. \tag{2}
\]

We refer the reader to [30] for a complete characterization of robot manipulators with bounded inertia matrix.

B. Target Dynamics

The stabilization of mechanical systems via PBC has been extensively studied (see, for instance, [3], [5], [6], [7], [8], [9], [10]). In addition, the energy shaping process is translated to find a Hamiltonian with an isolated minimum at \( (q_*, 0_n) \in \mathcal{E} \), where \( q_* \in \mathbb{R}^n \) is the desired configuration. Moreover, for some PBC approaches, shaping the kinetic energy results directly in modifying the interconnection structure (see, for instance, [8], [10], [31]). On the other hand, the damping injection process is performed by feeding back the passive output—customarily, it corresponds to the velocity—and ensures that the equilibrium is asymptotically stable.

Although the aforementioned references provide guidelines to guarantee stability, they lack tuning methodologies to ensure the performance in terms of other indices. Therefore, in this article, we focus on providing tuning rules for PBC methodologies that obtain the following target dynamics:

\[
\begin{bmatrix} \dot{q} \\ \dot{p} \end{bmatrix} = (J_d(q, p) - R_d(q, p)) \nabla H_d(q, p) \tag{3}
\]

with

\[
J_d(q, p) := \begin{bmatrix} 0_{n \times n} & M^{-1}(q) M_d(q) \\ -M_d(q) M^{-1}(q) & J_2(q, p) \end{bmatrix}
\]

\[
R_d(q, p) := \begin{bmatrix} 0_{n \times n} & 0_{n \times n} \\ 0_{n \times n} & D_d(q, p) \end{bmatrix}
\]

\[
H_d(q, p) := \frac{1}{2} p^\top M_d^{-1}(q) p + U_d(q) \tag{4}
\]

where \( H_d : \mathbb{R}^n \times \mathbb{R}^n \to \mathbb{R}_+ \) is the desired Hamiltonian, the desired inertia matrix \( M_d : \mathbb{R}^n \to \mathbb{R}^{n \times n} \) is positive definite, the desired potential energy \( U_d : \mathbb{R}^n \to \mathbb{R}_+ \) has a locally isolated minimum at \( q_* \), the desired damping matrix \( D_d : \mathbb{R}^n \times \mathbb{R}^n \to \mathbb{R}^{n \times n} \) is positive semidefinite, and \( J_2 : \mathbb{R}^n \times \mathbb{R}^n \to \mathbb{R}^{n \times n} \) is skew-symmetric.

Then, we consider the following assumption throughout this article to obtain the tuning guidelines.

**Assumption 1:** Given (1) and the desired equilibrium \( (q_*, 0_n) \in \mathcal{E} \), there exists a control approach \( u = \mathbb{R}^m \) such that the target dynamics takes the form (3) and (4). Moreover, the desired Hamiltonian \( H_d(q, p) \) has a local isolated minimum at \( (q_*, 0_n) \), that is, the closed-loop system (3) and (4) is stable.

In other words, we are interested in tuning PBC approaches such that the closed-loop system preserves the mechanical structure—in addition to the pH one—as in (3) and (4). We emphasize that preserving the structure is crucial for developing our tuning rules, whose main benefit is endowing with physical intuition the process of gain selection. Some PBC methodologies encountered in the literature that verify Assumption 1 are reported in [5], [10], and [11]. The stabilization of mechanical systems via IDA-PBC is described in [5], while in [10] and [11], works report PID-PBC approaches that do not require the solution of partial differential equations.

C. Canonical Hamiltonian System

A change of coordinates is a well-known tool for converting a particular system into another structure that may provide better insight into a particular feature of the system under study (see [22], [32], [33]). In this section, we describe a particular transformation for (3) and (4) whose resulting structure—namely, the canonical Hamiltonian system—may highlight the effects of the gyroscopic forces on the behavior of the closed-loop system. The transformed system is given by

\[
\begin{bmatrix} \dot{q} \\ \dot{p} \end{bmatrix} = (J_c - R_c) \begin{bmatrix} \nabla_q H_c(q, p) \\ \nabla_p H_c(q, p) \end{bmatrix} \tag{5}
\]

with

\[
J_c := \begin{bmatrix} 0_{n \times n} & I_n \\ -I_n & 0_{n \times n} \end{bmatrix}, \quad R_c := \begin{bmatrix} 0_{n \times n} & 0_{n \times n} \\ 0_{n \times n} & D_c(q, p) \end{bmatrix} \tag{6}
\]

where \( D_c : \mathbb{R}^n \times \mathbb{R}^n \to \mathbb{R}^{n \times n} \) is positive semidefinite, \( H_c : \mathbb{R}^n \times \mathbb{R}^n \to \mathbb{R}_+ \) is the canonical Hamiltonian, and \((q, p_c)\) are the canonical coordinates of (3) and (4).

The process to transform (3) and (4) into the canonical Hamiltonian system is reported by Blankenstein et al. [26], where they describe a particular choice for \( J_2(q, p) \). We summarize such process in the following proposition.

**Proposition 1:** Let

\[
p_c := M(q) M_d^{-1}(q) p + Q_d(q)
\]

with \( Q_d : \mathbb{R}^n \to \mathbb{R}^n \) being any smooth vector-valued function. Then, the closed-loop system (3) and (4) results in the canonical Hamiltonian system (5) and (6) if and only if

\[
J_2(q, p) := \hat{J}(q, p) + J_g(q) \tag{7}
\]

where

\[
\hat{J}(q, p) := M_d(q) M^{-1}(q) \left[ (\nabla_q M(q) M_d^{-1}(q) p)^\top - \nabla_q (M(q) M_d^{-1}(q) p) \right]
\]

\[
J_g(q) := M_d(q) M^{-1}(q) (\nabla_q Q_d(q))^\top - \nabla_q Q_d(q) \times M^{-1}(q) M_d(q).
\]
Moreover, the Hamiltonian of (5) and (6) takes the form
\[
H_c(q, p_c) := \frac{1}{2} (p_c - Q_d(q))^T M_c^{-1}(q)(p_c - Q_d(q)) + U_d(q)
\]
where
\[
M_c(q) := M(q)M_d^{-1}(q)M(q) \\
D_c(q, p) := M(q)M_d^{-1}(q)D_d(q, p)M_d^{-1}(q)M(q).
\]

Note that if \( J_\infty(q) \neq 0_{n \times n} \)—equivalently, \( \nabla_q Q_d(q) \neq 0_{n \times n} \) or \( \nabla_q Q_d(q) \neq \nabla_q Q_d(q)^T \)—introduces gyroscopic-related forces into the closed-loop system (5) and (6) via the term \( p_c^T M_c^{-1}(q)Q_d(q) \) from the canonical Hamiltonian (8). The introduction of gyroscopic-related forces has interesting positive effects on the performance in terms of stabilization and oscillations. For instance, Wesselink et al. [10] and Chan-Zheng et al. [34] demonstrated—via experiments—that the inclusion of \( J_\infty(q) \) reduces the oscillations in some coordinates for underactuated mechanical systems; moreover, the addition of this term is crucial for stabilizing underactuated mechanical applications such as spacecraft control and underwater vehicle control [26, 27, 29].

Furthermore, we can characterize the gyroscopic terms by dividing it into intrinsic or nonintrinsic of which we provide the definition as follows.

**Definition 1 (Intrinsic Gyroscopic Terms [26]):** The gyroscopic terms are called intrinsic if there does not exist a canonical transformation \( (q, p_c) \mapsto (\tilde{q}_c, \tilde{p}_c) \) such that the Hamiltonian in the new coordinates takes the form of the kinetic plus the potential energy, i.e.,
\[
\tilde{H}_c(\tilde{q}_c, \tilde{p}_c) := \frac{1}{2} \tilde{p}_c^T M_c^{-1}(\tilde{q}_c)\tilde{p}_c + \tilde{U}(\tilde{q}_c)
\]
for some \( \tilde{M} : \mathbb{R}^n \to \mathbb{R}^{n \times n} \) and \( \tilde{U} : \mathbb{R}^n \to \mathbb{R}_+ \).

Then, the following proposition verifies the intrinsic property.

**Proposition 2:** The gyroscopic terms are intrinsic to the closed-loop system (5) and (6) if and only if \( J_\infty \neq 0_{n \times n} \).

For further details on Proposition 2, see [26].

**D. Some Stability Properties**

Throughout this article, we consider two stability properties for systems (3) and (4): the ES and ISS. The former ensures that an exponential decay function bounds the closed-loop system trajectories, while the latter ensures that the system trajectories are bounded for any initial conditions as long as the input is also bounded. Although both properties reveal interesting behaviors of the closed-loop system, these are only qualitative attributes. Therefore, they may not provide explicit information for tuning purposes. In order to use these properties in a quantitative manner, we provide some concepts that allow us to exploit the stability properties for tuning purposes.

To this end, let us first introduce a definition related to the ES property.

**Definition 2 (Rate of Convergence [35]):** The rate of convergence of the closed-loop system (3) and (4) is the exponential decay value of the trajectories of the system approaching the equilibrium \((q_*, 0_n)\). We can characterize this value by defining some constants \(k_1, k_2, k_3 \in \mathbb{R}_+\) such that
\[
\|\text{col}(q, p)\| \leq \frac{k_2}{k_1} \|\text{col}(q_0, p_0)\| \exp \left\{ -\frac{k_3}{2k_2} (t - t_0) \right\}
\]
where \((k_3/2k_2)\) corresponds to the upper bound of the rate of convergence, \(t_0 \geq 0\) is the initial time, and \(q_0, p_0 \in \mathbb{R}^n\) are the initial conditions.

On the other hand, consider the closed-loop system (3) and (4) with a disturbance signal, i.e.,
\[
\begin{bmatrix}
\dot{q} \\
\dot{p}
\end{bmatrix} = (J_\infty(q, p) - R_d(q, p))\nabla H_d(q, p) + d(t, q, p)
\]
where \(d : \mathbb{R}_{\geq 0} \times \mathbb{R}^n \times \mathbb{R}^n \to \mathbb{R}^{2n}\) is a vector of disturbances, satisfying \(\|d(t, q, p)\| \leq \infty\). Then, we provide the following ISS-related definitions.

**Definition 3 (Comparison Functions [35]):** The following conditions hold.

1) A continuous function \(\alpha : [0, a) \to [0, \infty)\) is said to belong to class \(K\) if it is strictly increasing and \(\alpha(0) = 0\). Moreover, if \(\alpha \in K, a = \infty\) and \(\alpha(r) \to \infty\) as \(r \to \infty\), then it belongs to class \(K_\infty\).

2) A continuous function \(\beta : [0, a) \times [0, \infty) \mapsto [0, \infty)\) is said to belong to class \(KL\) if for each fixed \(s\), the mapping \(\alpha(r, s)\) belongs to class \(K\) with respect to \(r\), and for each fixed \(r\), the mapping \(\alpha(r, s)\) is decreasing with respect to \(s\) and \(\beta(r, s) \to 0\) as \(s \to \infty\).

**Definition 4 (Stability Margin [36]):** Consider system (9). Then, the nonlinear stability margin is any function \(\rho \in K_\infty\) that verifies
\[
\|d(t, q, p)\| \leq \rho(\|\text{col}(q, p)\|)
\]
and
\[
\|\text{col}(q, p)\| \leq \beta(\|\text{col}(q_0, p_0)\|, t) \quad \forall t \geq 0
\]
where \(\beta \in KL\).

Moreover, system (9) is said to be ISS if and only if (10) and (11) are satisfied.

**E. Problem Formulation**

Given \((q_*, 0_n) \in \mathcal{E}\), propose tuning methodologies to select the system matrices \(M_d(q, p), J_2(q, p), D_2(q, p),\) and Hamiltonian \(H_d(q, p)\) such that the closed-loop system (3) and (4) exhibits a prescribed behavior.

These values are referred as control parameters for the rest of this article.

**III. QUANTIFYING THE ES AND ISS PROPERTIES**

In this section, we exploit the ES and ISS properties in a quantitative manner by selecting an appropriate Lyapunov function candidate, of which we deduce the tuning rules for the upper bound of the rate of convergence, maximum permissible overshoot, and the stability margins of the system. Toward this
end, we split the section into two parts: 1) we describe rules for the nonperturbed system (3) and (4) and 2) we provide guidelines for the perturbed system (9).

A. Tuning Guidelines for the Nonperturbed System

Interesting properties for (3) and (4) are revealed through a convenient choice of a Lyapunov candidate. Chan-Zheng et al. [22] provided a tuning rule for the upper bound of the rate of convergence obtained from the Lyapunov stability analysis. In this article, we extend such an approach, where we exploit the Lyapunov candidate to deduce the upper bound of the rate of convergence for a broader class of mechanical systems stabilizable via a larger class of PBC techniques. We also provide a novel expression for tuning the upper bound of the maximum permissible overshoot. To this end, consider the following assumption.

Assumption 2: The control parameters from the closed-loop system (3) and (4) are chosen such that the following conditions hold.

C1: $U_d(q)$ is strongly convex.

C2: $\|M_d(q)\| < c$ for some positive constant satisfying $c < \infty$.

C3: $D_d(q, p) > 0$.

Then, we prove the ES stability of the equilibrium point for the closed-loop system (3) and (4) in the following theorem.

Theorem 1: Consider the closed-loop system (3) and (4), the desired equilibrium $x_\ast := (q_\ast, 0) \in \mathcal{E}$, and Assumption 2. Then, the following conditions hold:

1) $x_\ast$ is an exponentially stable equilibrium.

2) $x_\ast$ is globally exponentially stable if $U_d(q)$ is radially unbounded.

Proof: To prove 1), consider the matrix decomposition

$$M_d^{-1}(q) = T_d(q)T_d^T(q)$$

where $T_d : \mathbb{R}^n \to \mathbb{R}^n \times \mathbb{R}^n$ is a full-rank upper triangular matrix with strictly positive diagonal entries (see the Cholesky decomposition [37]). Furthermore, we introduce the change of coordinates (described first in [32])

$$\tilde{q} := q - q_\ast, \quad \tilde{p} := T_d(q)^T p.$$  \hspace{1cm} (12)

Then, define

$$\tilde{x} := \text{col}(\tilde{q}, \tilde{p})$$

and by transforming (3) and (4) with (12), we get the new pH system

$$\begin{bmatrix} \dot{\tilde{q}} \\ \dot{\tilde{p}} \end{bmatrix} = \begin{bmatrix} 0_{n \times n} & \tilde{A}(\tilde{q}) \\ -\tilde{A}^T(\tilde{q}) & \dot{\tilde{H}}(\tilde{x}) - \tilde{D}(\tilde{x}) \end{bmatrix} \begin{bmatrix} \tilde{V}_q \tilde{H}(\tilde{x}) \\ \tilde{V}_p \tilde{H}(\tilde{x}) \end{bmatrix}$$

$$\dot{\tilde{H}}(\tilde{x}) = \frac{1}{2} \tilde{p}^T \tilde{p} + \tilde{U}(\tilde{q})$$  \hspace{1cm} (13)

where

$$\tilde{U}(\tilde{q}) := U_d(q + q_\ast)$$

$$\tilde{T}_d(\tilde{q}) := T_d(q + q_\ast)$$

$$\tilde{A}(\tilde{q}) := M^{-1}(\tilde{q} + q_\ast)\tilde{T}_d^{-T}(\tilde{q})$$

$$\dot{\tilde{D}}(\tilde{x}) := \tilde{T}_d^T(\tilde{q})D_d(q + q_\ast, T_d^{-T} \tilde{p})\tilde{T}_d(\tilde{q})$$

$$\dot{\tilde{H}}(\tilde{x}) := \tilde{T}_d^T(\tilde{q})J_2(\tilde{q} + q_\ast, T_d^{-T} \tilde{p})\tilde{T}_d(\tilde{q})$$

$$+ \sum_{i=1}^n \left\{ \tilde{p}^T \tilde{T}_d^{-1}(\tilde{q}) \frac{\partial \tilde{T}_d^T(\tilde{q})}{\partial \tilde{q}_i} \right\}^T \left[ \tilde{A}^T(\tilde{q})e_i \right]^T$$

$$- \left[ \tilde{A}^T(\tilde{q})e_i \right] \left( \tilde{p}^T \tilde{T}_d^{-1}(\tilde{q}) \frac{\partial \tilde{T}_d^T(\tilde{q})}{\partial \tilde{q}_i} \right).$$

Note that by implementing the change of coordinates (12), it follows that the new equilibrium $\tilde{x}_\ast$ is the origin. Now, we prove the ES of the origin for (13) by considering the Lyapunov candidate

$$S(\tilde{x}) := \tilde{H}(\tilde{x}) + \epsilon \tilde{p}^T \tilde{A}^T(\tilde{q})\tilde{V}_q \tilde{U}(\tilde{q})$$  \hspace{1cm} (14)

with $\epsilon \in \mathbb{R}_+$. Thus, due to Assumption 2, note that $\tilde{H}(\tilde{x})$ satisfies the bounds

$$\beta_{\min} \leq \tilde{H}(\tilde{x}) \leq \beta_{\max}$$  \hspace{1cm} (15)

with

$$\beta_{\min} := \max \left\{ 1, \lambda_{\max} \left( \tilde{V}_q^2 \tilde{U}(\tilde{q}) \right) \right\}$$

$$\beta_{\max} := \min \left\{ 1, \lambda_{\min} \left( \tilde{V}_q^2 \tilde{U}(\tilde{q}) \right) \right\}.$$  \hspace{1cm} (16)

Furthermore, by applying Young’s inequality,\footnote{For $a, b \in \mathbb{R}$ and $\epsilon \gamma \in \mathbb{R}_+$, Young’s inequality is given by $ab \leq (a^2/2\epsilon \gamma) + (\epsilon \gamma b^2/2)$.} we have that

$$\| \epsilon \tilde{p}^T \tilde{A}^T(\tilde{q})\tilde{V}_q \tilde{U}(\tilde{q}) \| \leq \epsilon \beta_{\max} \beta_{\max}^2.$$  \hspace{1cm} (17)

Also, note that from Assumption 2, we get the following chain of implications:

$$\|M_d\| < \infty \implies \| \tilde{T}_d \| < \infty \implies \| \tilde{A} \| < \infty.$$  \hspace{1cm} (18)

Thus, from (15) and (17), we get

$$k_1 \| \tilde{x} \|^2 \leq S(\tilde{x}) \leq k_2 \| \tilde{x} \|^2$$  \hspace{1cm} (19)

with

$$k_1 := \beta_{\min} - \epsilon \sigma_{\max}(\tilde{A})\beta_{\max}^2, \quad k_2 := \beta_{\max} + \epsilon \sigma_{\max}(\tilde{A})\beta_{\max}^2.$$  \hspace{1cm} (19)

Note that there exists a sufficiently small $\epsilon$ such that $k_1 \in \mathbb{R}_+$. Hence, $S(\tilde{x}) \in \mathbb{R}_+$ for all $\tilde{x} \neq 0_n$.

Then, via some computations, it follows that the derivative of $S(\tilde{x})$ is given by:

$$\dot{S}(\tilde{x}) = -\tilde{V}^T \tilde{H}(\tilde{x}) \Gamma_{\text{sym}}(\tilde{x}) \tilde{V} \tilde{H}(\tilde{x})$$

where the matrix $\Gamma_{\text{sym}}(\tilde{x})$ is defined as

$$\Gamma_{\text{sym}}(\tilde{x}) := \begin{bmatrix} \tilde{\gamma}_{11} & \tilde{\gamma}_{12} \\ \tilde{\gamma}_{12} & \tilde{\gamma}_{22} \end{bmatrix}$$

$$\tilde{\gamma}_{11}(\tilde{x}) := \epsilon (\tilde{A}(\tilde{q}))^T(\tilde{q}) + \tilde{A}(\tilde{q})\tilde{A}(\tilde{q})$$

$$\tilde{\gamma}_{12}(\tilde{x}) := \frac{\epsilon}{2} [\tilde{A}(\tilde{q})[\tilde{D}(\tilde{x}) - \dot{\tilde{J}}(\tilde{x})] - \tilde{A}(\tilde{q})]$$

$$\tilde{\gamma}_{22}(\tilde{x}) := \tilde{D}(\tilde{x}) - \epsilon (\tilde{A}(\tilde{q})\tilde{V}_q \tilde{U}(\tilde{q})\tilde{A}(\tilde{q})).$$  \hspace{1cm} (20)

Then, note that $\Gamma_{\text{sym}}$ must be positive definite for $S(\tilde{x})$ qualifying as a suitable Lyapunov candidate. It follows that we can demonstrate that $\Gamma_{\text{sym}} > 0$ by applying the Schur
complement analysis, i.e., observe that \( \gamma_{11} > 0 \) and there always exists a sufficiently small \( \epsilon \) such that \( \gamma_{22} > 0 \) and the Schur complement of \( \gamma_{11} \) is also positive definite, i.e.,
\[
\gamma_{11} - \gamma_{12} \gamma_{22}^{-1} \gamma_{12}^T > 0
\]  
(21)
since \( \hat{D}(\hat{x}) > 0 \).

Subsequently, let \( \mu \in \mathbb{R}_{+} \) be the minimum eigenvalue of \( \gamma_{\text{sym}}(\hat{x}) \), and then, it follows that:
\[
\dot{\gamma}(\hat{x}) \leq -\mu \left\| \nabla \hat{H}(\hat{x}) \right\|^2 \leq -\mu \beta_{\max}^2 \left\| \hat{x} \right\|^2.
\]  
(22)

Therefore, from (18) and (22), \( \dot{x}_* \) is an exponentially stable equilibrium point for (13) (see [35, Th. 4.10]).

To prove 2), we have the following chain of implications:
\[
\dot{\hat{q}} \rightarrow \infty, \quad \dot{p} \rightarrow \infty \Rightarrow \dot{U}(\hat{q}) \rightarrow \infty \Rightarrow S(\hat{x}) \rightarrow \infty.
\]

Remark 1: The term \( \epsilon \) is used in: 1) ensuring that the Schur complement of \( \gamma_{11} \) is positive definite and 2) verifying that \( S(\hat{x}) \in \mathbb{R}_{+} \) for all \( \hat{x} \neq 0_n \), i.e., there always exists a sufficiently small \( \epsilon \) such that \( k_1 \) from (19) is positive.

Remark 2: We remark that the proof from Theorem 1 considers the closed-loop system (3) and (4), which can be obtained through different PBC approaches. Thus, it is more general than [22], where a standard mechanical system is in closed loop with a particular PBC approach (namely, PID-PBC).

Note that from (18) to (22), we get
\[
\dot{\gamma}(\hat{x}) \leq -\frac{2 \mu \beta_{\max}}{1 + \epsilon \sigma_{\max}(\hat{A}(\hat{q}))) \beta_{\max}} \gamma_{\text{sym}}(\hat{x}).
\]

Then, via the comparison lemma (see [35]), we have that the solution of (13) is bounded, i.e.,
\[
\left\| \hat{x} \right\| \leq \sqrt{\frac{k_2}{k_1}} \left\| \hat{x}_0 \right\| \exp\left\{ -\frac{\mu \beta_{\max}}{1 + \epsilon \sigma_{\max}(\hat{A}(\hat{q}))) \beta_{\max}} t \right\}
\]  
(23)

where \( \hat{x}_0 \in \mathbb{R}^{2n} \) are the initial conditions in the new coordinates.

It follows that we can exploit the inequality (23) and obtain two expressions: 1) an upper bound for the rate of convergence and 2) an upper bound for the maximum overshoot of output of the system.

For the latter, note that the transformed output—i.e., \( \hat{y} := G^T \hat{T}(\hat{q}) \hat{p} \)—verifies the following:
\[
\left\| \hat{y} \right\| \leq \left\| G^T \hat{T}(\hat{q}) \hat{p} \right\|
\leq \sigma_{\max}(G^T \hat{T}(\hat{q}))) \left\| \hat{p} \right\|
\leq \sigma_{\max}(G^T \hat{T}(\hat{q}))) \left\| \hat{x} \right\|.
\]

Then, from (23), it follows that:
\[
\left\| \hat{y} \right\| \leq \xi \exp\left\{ -\frac{\mu \beta_{\max}}{1 + \epsilon \sigma_{\max}(\hat{A}(\hat{q}))) \beta_{\max}} t \right\}
\]

with
\[
\xi := \sigma_{\max}(G^T \hat{T}(\hat{q}))) \sqrt{\frac{k_2}{k_1}} \left\| \hat{x}_0 \right\|
\]  
(24)

Fig. 1. Gershgorin circles for \( \gamma_{\text{sym}} \).

where \( k_1 \) and \( k_2 \) are defined in (19). Therefore, we have proven the following result.

Corollary 1: The convergence rates of the trajectories of (13) are upper bounded by
\[
\frac{\mu \beta_{\max}}{1 + \epsilon \sigma_{\max}(\hat{A}(\hat{q}))) \beta_{\max}}.
\]  
(25)

Moreover, the maximum overshoot of the system output \( \hat{y} \) is upper bounded by (24).

Note that (24) and (25) are expressed in terms of \( \beta_{\max}, \beta_{\min}, \sigma_{\max}(\hat{A}(\hat{q}))) \), \( \epsilon \), and \( \mu \). The parameters \( \beta_{\min} \) or \( \beta_{\min} \) can be computed easily from the potential energy, and \( \sigma_{\max}(\hat{A}(\hat{q}))) \) can be obtained directly from the kinetic energy. Conversely, the computation of \( \epsilon \) and \( \mu \) is a challenge; nonetheless, we can still employ other well-known tools to study the behavior of these parameters. For \( \mu \), we can employ the Gershgorin circle theorem (see [37] for further details), which defines circles containing the location of the spectrum of \( \gamma_{\text{sym}} \). Each circle is defined by the \( i \)th row elements (with \( i = 1, \ldots, n \)), with the center being the diagonal element and the radius being the sum of the absolute values of the nondiagonal entries. For example, in Fig. 1, we show the Gershgorin circles for some \( \gamma_{\text{sym}} \) (with \( n = 4 \)); note that by augmenting the diagonal elements of (20), the centers of the circles are shifted to the right; consequently, \( \mu \) may increase. As for \( \epsilon \), we can employ the Schur complement analysis tool. For instance, note that \( \gamma_{12} \) from (20) increases as \( \hat{D}(\hat{x}) \) increases. Thus, it follows that \( \epsilon \) must be adjusted to guarantee that condition (21) still holds.

Since \( \beta_{\max}, \beta_{\min}, \sigma_{\max}(\hat{A}(\hat{q}))) \), \( \epsilon \), and \( \mu \) are related to the control parameters of the closed-loop systems, we can employ (24) and (25) as guidelines to prescribe the maximum permissible overshoot of the closed-loop system and the desired upper bound for the decay ratio of the trajectories, respectively.

Remark 3: Note that (24) and (25) provide an upper bound of the overshoot and the rate of convergence, respectively. Thus, we can adjust the worst case scenarios for these two performance indices by reducing the mentioned bounds. However, reducing the bounds does not necessarily affect...
the behavior of the system, especially if the bounds are conservative. Nevertheless, in the proof of Theorem (1) and from the discussion above, note that the parameters from these indices are intimately related to the physical quantities of the system.

B. Tuning Guidelines for Perturbed Systems

The Lyapunov candidate (14) is conveniently chosen so that it reveals the effect of the control parameters on the rate of convergence and the maximum permissible overshoot of the closed-loop system. In this section, we further exploit this candidate selection by studying the effect of such parameters on the stability margin of the closed-loop system (see Definition 4). Hence, we consider the closed-loop system (9) with the change of coordinates (12), i.e.,

\[
\begin{bmatrix}
\begin{array}{l}
\dot{\hat{q}} \\
\dot{\hat{p}}
\end{array}
\end{bmatrix} =
\begin{bmatrix}
0_{n \times n} & \hat{A}(\hat{q}) \\
-\hat{A}^T(\hat{q}) & \hat{\dot{x}}(\hat{q}) - \hat{D}(\hat{q})
\end{bmatrix}
\begin{bmatrix}
\begin{array}{l}
\nabla \hat{y} \hat{H}(\hat{q}) \\
\nabla \hat{p} \hat{H}(\hat{q})
\end{array}
\end{bmatrix} + \hat{d}(t, \hat{q}, \hat{p})
\]

\[
\hat{H}(\hat{x}) = \frac{1}{2} \hat{b}^T \hat{p} + \hat{u}(\hat{q})
\]

where \( \hat{d} : \mathbb{R}_{>0} \times \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^{2n} \) is the time-dependent disturbance vector, satisfying \( \| \hat{d}(t, \hat{q}, \hat{p}) \| \leq \sigma \). Then, we state the following result.

Theorem 2: System (26) is ISS with nonlinear stability margin

\[
\rho(\|\hat{x}\|) := g_r \|\hat{x}\|(27)
\]

where

\[
g_r := \frac{\mu \beta_{\max}}{\varphi} \leq 0(28)
\]

is the gain margin of the closed-loop system (9) with \( 0 < \theta < 1 \), and some \( \varphi, \mu, \beta_{\max} \in \mathbb{R}_+ \).

Proof: Consider the Lyapunov candidate (14), the bounds (18), and

\[
\hat{d}(t, \hat{q}, \hat{p}) := \begin{bmatrix}
\hat{d}_1(t, \hat{q}, \hat{p}) \\
\hat{d}_2(t, \hat{q}, \hat{p})
\end{bmatrix}
\]

where \( \hat{d}_1, \hat{d}_2 : \mathbb{R}_{>0} \times \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^n \). Then, via some computations, it follows that:

\[
\begin{align*}
\hat{S} & = -\nabla^T \hat{H} \gamma_{\text{sym}} \nabla \hat{H} \\
& \quad + \epsilon \left( \nabla^T \hat{q} \nabla \hat{d}_1 + \hat{A}^T \nabla \hat{d}_1 \hat{U} + \hat{A}^T \nabla \hat{d}_2 \hat{U} \right) \\
& \quad \leq -\mu \beta_{\max}^2 \|\hat{x}\|^2 + \beta_{\max} \sigma_{\max}(\gamma_d) \|\nabla \hat{H}\| \|\hat{d}\|
\end{align*}
\]

Consider \( 0 < \theta < 1 \); then, by rewriting the previous expression, we get

\[
\hat{S} \leq -\mu \beta_{\max}^2 \|\hat{x}\|^2 (1 - \theta) + \beta_{\max} \sigma_{\max}(\gamma_d) \|\hat{x}\| \|\hat{d}\|
\]

Therefore,

\[
\hat{S} \leq -\mu \beta_{\max}^2 \|\hat{x}\|^2 (1 - \theta) \quad \forall \|\hat{x}\| \in \Omega \tag{29}
\]

where

\[
\Omega := \{ \hat{x} \in \mathbb{R}^{2n} \mid \|\hat{d}\| \leq \rho(\|\hat{x}\|) \}
\]

and \( \rho(\|\hat{x}\|) \) is defined as in (27) with \( \varphi := \sigma_{\max}(\gamma_d) \).

From (18) and (29), the closed-loop system (26) is ISS with nonlinear stability margin \( \rho(\|\hat{x}\|) \) (see [35, Th. 4.19] and [36]).

Remark 4: Note that via the nonlinear stability margin concept, we can define the gain margin (28) that corresponds to the maximum permissible growth of the norm of the disturbance with respect to the norm of the trajectories in which the closed-loop system remains ISS. In other words, we get better disturbance attenuation by increasing the gain margin.

Similar to Section III-A, we can provide a decay ratio bound and a maximum overshoot for the system output. Note that from (18) and (29), we get

\[
\hat{S}(\hat{x}) \leq -\frac{2 \mu \beta_{\max}(1 - \theta)}{1 + \epsilon \sigma_{\max}(\hat{A}) \beta_{\max}} \hat{S}(\hat{x})
\]

Then, via the comparison lemma (see [35]), we have that the solution of (26) is bounded, i.e.,

\[
\|\hat{x}\| \leq \sqrt{\frac{k_2}{k_1}} \|\hat{x}_0\| \exp \left\{ -\frac{\mu \beta_{\max}(1 - \theta)}{1 + \epsilon \sigma_{\max}(\hat{A}) \beta_{\max}} t \right\}
\]

on \( t \in [t_0, T] \) for some \( T > 0 \).

Thus, we have proven the following result.

Corollary 2: Let

\[
\Omega_\epsilon := \{ \hat{x} \in \mathbb{R}^{2n} \mid \|\hat{x}\| \leq \frac{1}{g_r} \|\hat{d}\| \}
\]

Then, for some initial conditions \( \|\hat{x}_0\| \in \Omega \) [see (30)], the trajectories approach exponentially to \( \Omega_\epsilon \) at a rate of convergence that is upper bounded by

\[
\frac{\mu \beta_{\max}(1 - \theta)}{1 + \epsilon \sigma_{\max}(\hat{A}) \beta_{\max}}
\]

as \( t \rightarrow T \) for some \( T > 0 \).

Furthermore, the maximum overshoot of the output of the system on \([t_0, T]\) is given by (24).

By using simultaneously the expressions (28), (31), and (24), we provide an insight into the relationship of the control parameters with three performance metrics—i.e., the gain margin, the upper bound of the rate of convergence, and the maximum overshoot—of the perturbed system [see (26)]. For instance, a tradeoff between these metrics is evident by
increasing $\beta_{\text{max}}$, the disturbance $\hat{d}$ is attenuated, and the stability margin increases. Simultaneously, the maximum overshoot is augmented.

**Remark 5:** Another approach for tuning the stability margin of general nonlinear systems can be found in [38], where the authors introduce an equivalent concept to ISS, namely, input-to-state dynamical stability (ISDS). However, this tuning methodology lacks physical intuition as there is no clear relation between the parameters associated with the stability margin with energy or damping.

**Remark 6:** By using the expression (29), we can calculate the $L_2$-norm for the signal $\tilde{x}$, i.e.,

$$
\|\tilde{x}\|_2 = \int_0^\infty \|\tilde{x}(\tau)\|^2 d\tau 
\leq -\frac{1}{\mu_\text{max}}(1-\theta) \int_0^\infty S(\tau)d\tau 
\leq \frac{1}{\mu_\text{max}}(1-\theta)(S(0) - S(\infty)) 
\leq \frac{1}{\mu_\text{max}}(1-\theta)S(0).
$$

In addition, consider (32), and since $\|\hat{d}\|_2 \leq g_r \|\hat{x}\|_2$, we have

$$
\|\hat{d}\|_2 \leq g_r \int_0^\infty \|\hat{x}\|^2 d\tau = g_r^2 \|\hat{x}\|^2_2 
\leq \frac{\mu_\text{th}^2}{\sigma_{\text{max}}(Y_d)2(1-\theta)S(0)}.
$$

Recall that the square of the $L_2$-norm of a signal corresponds to the energy contained in such signal. Therefore, (33) provides the upper bound of the energy of the disturbance in which the system remains stable. We remark the effect of the control parameters on such bound. Moreover, (33) can be rewritten as

$$
\|\hat{d}\|^2_2 \leq g_r^2 _2 \|\hat{x}\|^2_2
$$

and thus, we can see clearly from the previous expression that the maximum permissible growth of the energy of disturbance with respect to the energy of the trajectories—in which the system remains stable—is given by the square of the gain margin $g_r$.

IV. ON THE BEHAVIOR OF THE CLOSED-LOOP SYSTEM NEAR THE EQUILIBRIUM

In this section, we propose tuning rules to prescribe a desired performance in the transient response. To this end, we recur to the linearization of the closed-loop system (3) and (4), and later, we find a transformation such that the linearized system has a saddle point matrix structure (we refer the reader to [39] and [40] for further details of this class of matrices). This particular structure reveals interesting spectral properties for the linearized matrix, of which we deduce our tuning guidelines.

Let us first introduce the vectors $\bar{q} := q - q_s$ and $\bar{p} := p - p_s$ with $p_s := 0_n$. Then, it follows that the linearized system around the equilibrium point $(q_s, 0_n)$ corresponds to:

$$
\begin{bmatrix}
\bar{\dot{q}} \\
\bar{\dot{p}} \\
\end{bmatrix} = (J_{ds} - R_{ds})^{-1} H_{ds} \begin{bmatrix}
\bar{q} \\
\bar{p} \\
\end{bmatrix}.
$$

Subsequently, consider the following Cholesky decomposition (see [37]):

$$
M_{ds}^{-\frac{1}{2}} = \phi_T^\dagger \phi_M, \quad \nabla_2^2 U_{ds} = \phi_T^\dagger \phi_P
$$

where $\phi_M, \phi_P \in \mathbb{R}^{n \times n}$ are upper triangular matrices; then, consider the similarity transformation matrix $T \in \mathbb{R}^{2n \times 2n}$ and new coordinates $z \in \mathbb{R}^{2n}$

$$
T := \begin{bmatrix}
0_n & \phi_M \\
\phi_P & 0_n \\
\end{bmatrix}, \quad z = T \begin{bmatrix}
\bar{q} \\
\bar{p} \\
\end{bmatrix}.
$$

Thus, the linearized system in the newly introduced coordinates $z$ becomes

$$
\dot{z} = -Az,
$$

$$
A := \begin{bmatrix}
\phi_M(D_{ds} - J_{2s})\phi_T^\dagger & \phi_T^\dagger M_{ds}^{-1}\phi_P^\dagger \\
-\phi_P M_{ds}^{-1}\phi_T^\dagger & 0_n \\
\end{bmatrix}.
$$

Then, inspired by the results of Brayton and Moser [41], we provide a proposition on the location of the spectrum of $A$ from (34).

**Theorem 3:** Let $\lambda \in \mathbb{C}$ be an eigenvalue of $A$ and $\text{col}(v, w)$ its corresponding eigenvector with $v, w \in \mathbb{C}^n$. Then, $\lambda$ lies on a circle centered in the point $(p_r, p_i)$ of the complex plane where

$$
p_r := \frac{v^*(\phi_M D_{ds} \phi_T^\dagger) v}{\|v\|^2}, \quad p_i := \frac{i v^*(\phi_M J_{2s} \phi_T^\dagger) v}{\|v\|^2}.
$$

Moreover, the radius of such circle is defined as

$$
r_c := \sqrt{\left(\|\phi_T^\dagger M_{ds}^{-1}\phi_P^\dagger w\|^2 - \|\Psi v\|^2\right)\frac{\|v\|^2}{\|v\|^2} + p_r^2 + p_i^2}.
$$

where $\Psi := \phi_M(D_{ds} - J_{2s})\phi_T^\dagger$.

**Proof:** Consider the eigenvalue problem $A \begin{bmatrix} v \\ w \end{bmatrix} = \lambda \begin{bmatrix} v \\ w \end{bmatrix}$. Then, it follows that:

$$
\Psi v + (\phi_T^\dagger M_{ds}^{-1}\phi_P^\dagger) w = \lambda v
$$

$$
\Rightarrow \|v - \lambda I_n v\|^2 = \left\|\phi_T^\dagger M_{ds}^{-1}\phi_P^\dagger w\right\|^2
$$

$$
\Rightarrow |\lambda|^2 - \frac{v^*(\phi_T^\dagger M_{ds}^{-1}\phi_P^\dagger) v}{\|v\|^2} \Re(\lambda) - \frac{v^*(\Psi^\dagger \Psi) v}{\|v\|^2} \Im(\lambda)
$$

$$
\Rightarrow \Re(\lambda)^2 + \Im(\lambda)^2 + 2 \frac{v^*(\phi_M D_{ds} \phi_T^\dagger) v}{\|v\|^2} \Re(\lambda)
$$

$$
- 2i \frac{v^*(\phi_M J_{2s} \phi_T^\dagger) v}{\|v\|^2} \Im(\lambda)
$$

$$
\Rightarrow \left\|\phi_T^\dagger M_{ds}^{-1}\phi_P^\dagger w\right\|^2 - \|\Psi v\|^2.
$$

2 Brayton and Moser [41] considered $J_{2s} = 0_n \times n$. 

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Subsequently, by completing the squares in (37) with the expressions defined in (35), we get the circle centered in $(p_r, p_l)$ with radius $r_c$ as defined in (36) in the complex plane.\footnote{Note that $(\iota v^T (\phi M^T) v)/\|v\|^2 \in \mathbb{R}$.}

\textbf{Remark 7:} A similar analysis for the location of the eigenvalues can be performed using the Gersgorin circle theorem or Gershgorin-like theorems (see [37, 42]), where the radius of the circle (resp. the center of the circle) from these theorems is characterized by the sum of the nondiagonal elements (resp. by the diagonal element), whereas Theorem 3 characterizes the radius and the center of the circle by using the norms of the subblocks of $A$.

Theorem 3 claims that each eigenvector of $A$ defines a circle where its corresponding eigenvalue lies on. This theorem provides a quick and intuitive visual way of studying the effect of the parameters on the spectrum of $A$. Moreover, it aids in designing the controller gains without computing the eigenvectors, which may be cumbersome (especially when the matrix $A$ is large). In Fig. 2, we provide a visual example\footnote{Since the term $(\iota v^T (\phi M D^* M^T) v)/\|v\|^2$ is positive definite, every circle of $-A$ lies in the left-half-plane.} for particular choices of $J_2(q, p)$. Note that the inclusion $J_2(q, p)$ leads to a more unpredictable oscillatory behavior of the closed-loop system as the circle (37) loses its symmetry on the real axis. Therefore, the oscillations may be increased in some coordinates and they can be reduced in others. For example, if the particular eigenvalue is located in the red arc, the oscillations may be reduced. Conversely, if the eigenvalue is located in the blue arc, the oscillations may be augmented.

In general, the presence of $J_2(q, p)$ introduces a nonsymmetric component to the block (1, 1) from $A$. Therefore, in the sequel, we consider two scenarios for (34): 1) $A$ with symmetric block (1, 1) and 2) $A$ with nonsymmetric block (1, 1).

\subsection*{A. Particular Case: $A$ With Symmetric Block (1, 1)}

We recover a class of saddle point matrices whose block (1,1) is symmetric for some particular choices of $J_2(q, p)$; for simplicity of exposition and without loss of generality, in this section, we consider $J_2(q, p) = 0_{n \times n}$.\footnote{See [40] for a complete description of the spectrum of $A$ when $J_2(q, p) = 0_{n \times n}$.} The spectrum can be characterized by the norm of each of its submatrix blocks; thus, it simplifies the analysis (especially when $A$ is large).

Moreover, the linearization of closed-loop system with PID-PBC (see [11]) recovers this particular class of saddle point matrices, which is later exploited in [25] to provide tuning guidelines. Interestingly, the pioneering results of Brayton and Moser [41] also use this form to study stability properties of electrical networks near their equilibrium point.

Here, we extend the methodologies described in [25] for characterizing the spectrum to mechanical systems stabilizable by a broader class of PBC approaches that obtain the target dynamics as described in (3) and (4).

The following proposition provides a tuning rule that reduces the transient response oscillations to the minimum.

\textbf{Theorem 4:} Consider the system (34). If

$$\lambda_{\min}(D_{d*})^2 \geq 4 \lambda_{\max}(M_{d*} M_{d*}^{-1} V_{d*}^2 U_{d*} M_{d*}^{-1} M_{d*}) \lambda_{\max}(M_{d*})$$

holds, then the spectrum of $A$ is real and positive.

\textbf{Proof:} Consider the eigenvalue problem $A \begin{bmatrix} v \\ w \end{bmatrix} = \lambda \begin{bmatrix} v \\ w \end{bmatrix}$ with $\lambda \in \mathbb{C}$ and $v, w \in \mathbb{C}^{n \times 1}$. Some computations yield the quadratic equation

$$\lambda^2 - \frac{v^* (\phi_M D_{d*} \phi_M^T) v}{\|v\|^2} \lambda + \frac{v^* (\phi_M^T M_{d*}^{-1} V_{d*}^2 U_{d*} M_{d*}^{-1} \phi_M^T) v}{\|v\|^2} = 0$$

whose solution is given by

$$\lambda = \frac{1}{2} \left[ \frac{v^* (\phi_M D_{d*} \phi_M^T) v}{\|v\|^2} \pm \sqrt{\left(\frac{v^* (\phi_M D_{d*} \phi_M^T) v}{\|v\|^2}\right)^2 - 4 \frac{v^* (\phi_M^T M_{d*}^{-1} V_{d*}^2 U_{d*} M_{d*}^{-1} \phi_M^T) v}{\|v\|^2}} \right]$$

Note that $\lambda$ is real if and only if the discriminant of the previous solution is nonnegative, i.e.,

$$\frac{v^* (\phi_M D_{d*} \phi_M^T) v}{\|v\|^2} \geq 4 \frac{v^* (\phi_M^T M_{d*}^{-1} V_{d*}^2 U_{d*} M_{d*}^{-1} \phi_M^T) v}{\|v\|^2}$$

holds. In order to verify (39) for the entire spectrum of $A$, consider the change of coordinates $v_1 = \phi_M^T v$, then it follows that:

$$\left(\frac{v_1^* D_{d*} v_1}{\|v_1\|^2}\right)^2 \geq 4 \left(\frac{v_1^* M_{d*} M_{d*}^{-1} V_{d*}^2 U_{d*} M_{d*}^{-1} M_{d*}}{\|v_1\|^2}\right) \left(\frac{v_1^* M_{d*} v_1}{\|v_1\|^2}\right)$$

and by multiplying both sides with $(1/\|v_1\|^4)$, it follows that:

$$\left(\frac{v_1^* D_{d*} v_1}{\|v_1\|^2}\right)^2 \geq 4 \frac{v_1^* M_{d*} M_{d*}^{-1} V_{d*}^2 U_{d*} M_{d*}^{-1} M_{d*} v_1}{\|v_1\|^4} \left(\frac{v_1^* M_{d*} v_1}{\|v_1\|^2}\right)$$

(40)

Then, note that we have the following inequalities:

$$\left(\frac{v_1^* D_{d*} v_1}{\|v_1\|^2}\right)^2 \geq \lambda_{\min}(D_{d*})^2$$

and

$$\left(\frac{v_1^* M_{d*} M_{d*}^{-1} V_{d*}^2 U_{d*} M_{d*}^{-1} M_{d*} v_1}{\|v_1\|^2}\right) \left(\frac{v_1^* M_{d*} v_1}{\|v_1\|^2}\right).$$
trajectories—at 2% of its initial value, i.e., trajectories of the closed-loop reaching 98% of its steady-state.

Proposition 2—as there is a transformation such that the new Hamiltonian is of the form of the kinetic plus the potential energy. Therefore, we can find a transformation of its linearized system such that it has a saddle point form whose block (1, 1) is symmetric. We summarize this result in the following proposition.

Theorem 6: There exists a transformation such that the linearization of (3) and (4) around the equilibrium \((q_*, 0_n)\) has a saddle point form whose block (1, 1) is symmetric if and only if the gyroscopic terms are nonintrinsic.

Proof: Consider the closed-loop system in the canonical Hamiltonian system form (5) and (6) and define \(J_2(q, p)\) as in (7). Then, it follows that the linearization of the canonical Hamiltonian system around the equilibrium \((q_*, 0_n)\) corresponds to (recall that \(\bar{q} := q - q_*\) and \(\bar{p} := p - p_*\) with \(p_* = 0_n\))

\[
\begin{bmatrix}
\bar{q} \\
\bar{p}
\end{bmatrix} = \begin{bmatrix} 0_{n \times n} & I_n \\
-I_n & -D_{c*} \end{bmatrix} \nabla^2 H_c \begin{bmatrix}
\bar{q} \\
\bar{p}
\end{bmatrix}
\]

\[
\nabla^2 H_c = \begin{bmatrix}
\nabla^2 U_{d*} + B_{12} M_{c*} B_{12}^\top & B_{12} \\
B_{12}^\top & M_{c*}^{-1}
\end{bmatrix}
\]

with \(B_{12} := -\nabla Q_{d*)M_{c*}^{-1}}. \) Subsequently, let

\[
M_{c*}^{-1} = \phi_{Mc^\top} \phi_{Mc}, \quad \nabla^2 U_{d*} = \phi_{Pc} \phi_{Pc}
\]

where \(\phi_{Mc^\top}, \phi_{Pc} \in \mathbb{R}^{nxn}\) are upper triangular matrices obtained from the Cholesky decomposition, and consider the similarity transformation matrix \(T_c \in \mathbb{R}^{2n \times 2n}\) and new coordinates \(z_c \in \mathbb{R}^{2n}\)

\[
T_c := \begin{bmatrix}
\phi_{Pc} \\
-\phi_{Mc} \nabla Q_{d*) \phi_{Mc^\top}
\end{bmatrix} \begin{bmatrix} 0_{n \times n} \\
0_{n \times n}
\end{bmatrix}, \quad z_c = T_c \begin{bmatrix}
\bar{q} \\
\bar{p}
\end{bmatrix}
\]

The linearized system in the coordinates \(z_c\) becomes

\[
\dot{z}_c = -A_c z_c
\]

\[
A_c := \begin{bmatrix}
\nabla Q_{d*) \phi_{Mc^\top} \\
-\nabla Q_{d*) \phi_{Mc^\top} \phi_{Pc}
\end{bmatrix} \phi_{Mc}, \quad \phi_{Mc^\top} \phi_{Mc} \phi_{Pc} \phi_{Pc} \phi_{Pc^\top} \phi_{Pc} \phi_{Pc^\top}
\]

Thus, \(A_c\) is a saddle point matrix with symmetric block (1, 1) if and only if the gyroscopic terms are nonintrinsic, i.e.,

\[
\nabla Q_{d*)} = (\nabla Q_{d*)^\top}
\]

Therefore, Theorem 6 suggests that when \(J_2(q, p)\) is chosen as in (7) with nonintrinsic gyroscopic terms [i.e., \(Q_{d*(q)}\) satisfying (43)]; then, we can implement the tuning rules as described in Section IV-A.

Remark 9: We can also prescribe the oscillation behavior to the transient response of the linearized system (34) by employing the well-known eigenvalue assignment (or pole placement) methodology, which is also known as the inverse problem for damped (gyroscopic) systems, i.e., given the complete set of eigenvalues and eigenvectors, find \(M_{c*}, J_{d*}, D_{d*}, \) and \(\nabla^2 U_{d*}.\) However, we underscore that this tuning methodology lacks physical intuition.

Remark 10: The tuning rules described in this section require a proper characterization of \(M(q), U(q),\) and \(D(q, p).\)
Although the mass-inertia matrix and potential energy can be obtained relatively easily compared to $D(q, p)$, obtaining the natural damping can be challenging. Nonetheless, the tuning rules work even with a rough estimate as the closed-loop remains stable. However, we underscore that it may change the oscillatory behavior (the system may become overdamped or underdamped). Section V discusses some practical remarks on the damping treatment.

V. On Damping Treatment

The implementation of the tuning rules described in Section IV requires certain knowledge of the parameters of the open-loop system, i.e., the stiffness, mass inertia, and damping matrices. Albeit characterizing the former two parameters remain relatively easy, identifying the damping phenomenon is still an open question due to its complex nonlinear behavior. Hence, to ensure the accuracy of our tuning methodology, we describe some methodologies found in the literature to identify the damping matrix in this section.

Some detailed assessments for general damping identification methods can be found in [44] and [45]. Most of these damping identification techniques are based on the well-established modal analysis tool. The tool characterizes the dynamics of a physical structure—with the help of the acquired data—in terms of the modal parameters such as natural frequency, damping factor, eigenvalues, and eigenvectors (or mode shape). The main disadvantage of the modal analysis tool is that it requires different equipment types, e.g., tens of sensors, impact hammer, and data acquisition hardware. On the other hand, in [46], we find a simple damping identification method based on the energy of the system that simplifies the data recollection process. Such a methodology requires only one set of measurements—position, velocity, and acceleration data—but a larger set improves the identification accuracy. However, this damping identification methodology is restricted to constant and diagonal mass inertia and stiffness matrices. An extension of such results to a larger class of mechanical systems is the energy-based damping identification (EBDI) approach, which can be found in [34].

Nevertheless, the mentioned references only characterize linear damping (or viscous damping) matrices. Therefore, these identifications are only valid in a region near the equilibrium point. Thus, the accuracy of the tuning rules may decrease when the trajectories start far from the equilibrium point. Also, note that the damping inaccuracy characterization can be included as part of $\hat{d}(t, x)$ in (26). Then, it follows that due to this disturbance, the closed-loop system may not converge to the equilibrium point. To overcome this issue, Chen [47] proposed a nonlinear disturbance observer-based control (NDOBC). This dynamic extension approach is twofold: 1) estimating the disturbance and 2) compensating the estimated disturbance using proper feedback. Sandoval et al. [48] and Fu et al. [49] extended such an approach to pH systems.

Thus, we can ensure the accuracy of the tuning rules described in Section IV by selecting a proper damping identification methodology (the selection process may depend on the availability of the equipment). Moreover, if the damping matrix is highly nonlinear, we can implement the chosen identification methodology combined with the NDOBC approach.

VI. Case Studies

In this section, we illustrate the applicability of some of our tuning rules for fully actuated and underactuated mechanical systems. For the former, we employ the results from Sections III-A and IV-A. For the latter, we employ the tuning rules discussed in Sections III-B and IV. For both configurations, we employ a PBC approach with the form

$$u = -K_{es}G^\top(q - q_s) - K_{di}G^\top \dot{q} - K_{int}G^\top \dot{q} + \tilde{k}(q)$$

(44)

where $K_{es}$ and $K_{di}$ are positive definite matrices with appropriate dimensions, $K_{int}$ is a matrix with appropriate dimensions that modifies the interconnection of the system, and $\kappa : \mathbb{R}^n \to \mathbb{R}^m$ is a vector to be defined later. Moreover, we employ robot manipulators that verify (2).

A. Fully Actuated Mechanical System: A 5-DOF Robotic Arm

To demonstrate the effectiveness of the rules proposed in Sections III-A and IV-A, we use the Philips Experimental Robotic Arm (PERA), as shown in Fig. 3 (see [50]). For our experiments, we select the 5-DOF configuration with the following joints:

1) shoulder yaw with angle $q_1$;
2) shoulder pitch with angle $q_2$;

This controller structure can be found in PBC approaches such as in [10] or [5] and we refer the reader to these results for further details.
3) shoulder roll with angle $q_3$;
4) elbow pitch with angle $q_4$;
5) elbow roll with angle $q_5$.

The model is given by (1) with $n = m = 5$, $D(q, p) = 0_{5 \times 5}$, and $G = I_5$. Furthermore, the expressions for $M(q)$ and $U(q)$ are omitted due to space constraint; we refer the reader to [51] and [52] for further details. In addition, a MATLAB\textsuperscript{7} script to generate the latter expressions can be found in [53]. We stabilize the PERA at the desired configuration $q_\star = \text{col}(0.5, 0.6, -1.6, 1.3, 0.5)$ rad with the controller (44) with $K_{\text{int}} = 0_{5 \times 5}$ and $\tilde{k}(q) = \nabla U(q)$. Thus, the targets dynamics are described as in (3) and (4) with

$$
\begin{align*}
J_5(q, p) &= 0_{5 \times 5} \\
D_d(q, p) &= D(q, p) + GK_{d1}G^T \\
M_d(q) &= M(q) \\
U_d(q) &= \frac{1}{2}(q - q_\star)^T G K_{\text{es}} G^T (q - q_\star).
\end{align*}
$$

We consider a rough estimate of the damping for this experimental setup. As mentioned in Remark 10, the tuning rules require a proper characterization of the parameters of the mechanical system and obtaining them in practice may be challenging. However, we demonstrate that the guidelines work even with an approximation. The gains selection for this case study is shown in Table I.\textsuperscript{8}

First, the response for Case A corresponds to an arbitrary tuning for comparison purposes, where we can see the oscillations (and overshoot) for every joint in Fig. 4. Then, to remove the oscillations from the transient response, we employ (38) from Theorem 4 to select the parameters of the control law (44). Note that from (45), we get that $M_d = M_\star$, $D_d = K_{d1}$, and $\nabla_q^2 U_{d\star} = K_{\text{es}}$. Subsequently, to calculate $\lambda_{\min}(K_{d1})$, we fix $K_{\text{es}} = \text{diag}(200, 175, 200, 175, 200)$.\textsuperscript{9}

Therefore, we get that

$$
\lambda_{\min}(K_{d1}) = 19.8731.
$$

Next, for Case B, we have selected $K_{d1}$ according to the calculated above. Note that, in Fig. 4, the oscillations (and overshoot) from Case B are attenuated in comparison with Case A. Moreover, in Case B, the responses are slightly overdamped, suggesting that the calculated $K_{d1}$ is conservative and the natural damping is different than zero, i.e., $D(q) < 0$ (see Remark 10). Nonetheless, even with a rough estimate, this tuning approach ensures that the oscillations in the closed loop are removed.

\textsuperscript{7}Registered Trademark.

\textsuperscript{8}For simplicity, we have selected $K_{\text{es}}$ and $K_{d1}$ as diagonal matrices.

\textsuperscript{9}We have chosen this $K_{\text{es}}$ value since we obtain an acceptable response for any $\lambda_{\min}(K_{d1})$.

Then, to illustrate the applicability of (25) as a tuning rule, we use Case B as the new reference baseline and decrease the term $\beta_{\max}$ for Case C (recall from (16) that $\beta_{\max} := \nabla_q^2 U_{d\star}$). Since $\beta_{\max}$ is proportional to the upper bound of the rate of convergence, it is expected that the rate of convergence reduces in Case C with respect to Case B, which is verified in Fig. 5.

There is a small steady-state error in the joint positions, which may be due to nonmodeled physical phenomena such as
measurement noise, dry friction, or asymmetry of the motors. We underscore that the implemented PBC scheme is applied to the passive output signal, which corresponds to the actuated velocities for mechanical systems. Therefore, the integral action is applied on the actuated velocities and this scheme does not compensate for the error seen in the trajectories of the positions. For further details on compensating the position error, we refer the reader to [54], [55], and [56].

Remark 11: We omit the use of Theorem 5, i.e., the rise time tuning rule, as the results for this particular study case are highly conservative. However, it may be relevant for another set of mechanical system parameters, see the example in [25].

B. Underactuated Mechanical System: A 2-DOF Planar Manipulator With Flexible Joints

This section illustrates the guidelines described in Sections III-B and IV. To this end, we employ a 2-DOF planar manipulator with flexible joints, as shown in Fig. 6 (see [57] for the reference manual). The manipulator in closed loop with (44) is described in (9) with a disturbance given by $d = \text{col}(0, 0, 0.5, 0.5) \text{Nm}$, and we have the following.

1) $q_1$: Position of the link 1.
2) $q_2$: Position of the link 2.
3) $q_3$: Position of the motor of link 1.
4) $q_4$: Position of the motor of link 2.

Note that col($q_1, q_2$) corresponds to the unactuated coordinates. The rest of the parameters—obtained from [34]—are given as

$$G = \begin{bmatrix} 0_{2 \times 2} & G_1 \end{bmatrix}, \quad G_1 = \text{diag}[1, 1.67]$$

$$U(q) = \frac{1}{2} \|\text{col}(q_1, q_2) - \text{col}(q_3, q_4)\|_K^2,$$

$$K_s = \text{diag}[8.43, 16.86]$$

$$D = \text{diag}[D_u, D_a]$$

$$D_u = \text{diag}[0.0331, 0.0077]$$

$$D_a = \text{diag}[2.9758, 2.8064]$$

$$M(q) = \begin{bmatrix} M_1(q_2) & 0_{2 \times 2} \\ 0_{2 \times 2} & M_m \end{bmatrix}$$

$$M_m = \text{diag}[0.0628, 0.0026]$$

$$M_1(q_2) := \begin{bmatrix} a_1 + a_2 + 2b \cos(q_2) & a_2 + b \cos(q_2) \\ a_2 + b \cos(q_2) & a_2 \end{bmatrix}$$

where $a_1 = 0.1547$, $a_2 = 0.0111$, and $b = 0.0168$.

The manipulator is stabilized at the desired configuration $q_* = \text{col}(0.6, 0.8, 0.6, 0.8) \text{rad}$ by employing the controller (44) with $K(q) = 0.2$. The corresponding closed loop is described as in (3) and (4) with

$$J_2 = \begin{bmatrix} 0_{2 \times 2} & \frac{1}{2}(G_1K_{\text{int}})^\top \\ -\frac{1}{2}G_1K_{\text{int}} & 0_{2 \times 2} \end{bmatrix}$$

$$D_{d} = \begin{bmatrix} D_u & \frac{1}{2}(G_1K_{\text{int}})^\top \\ \frac{1}{2}G_1K_{\text{int}} & D_a + G_1K_{d_1}G_1^\top \end{bmatrix}$$

$$M_{d}(q) = M(q)$$

The open-loop model is described as in (1) with $n = 4$ and $m = 2$, which corresponds to an underactuated configuration since $m < n$.

### Table II

| Case | $K_{d_1}$ | $K_{s}$ | $K_{\text{int}}$ |
|------|-----------|---------|------------------|
| D    | diag[1.5, 1.5] | diag[3.5] | diag[0.0] |
| E    | diag[1.5, 1.5] | diag[12.15] | diag[0.0] |
| F    | diag[0.5, 1.5] | diag[12.15] | diag[0.0] |
| G    | diag[0.5, 1.5] | diag[12.15] | diag[1.0, 0.43] |

Now, we proceed to improve the performance of the closed loop. First, we tune the nonlinear stability margin (27) and the maximum overshoot (24) by modifying $\beta_{\text{max}}$.

Recall that $\beta_{\text{max}}$ is given by $K_{\text{es}}$, which shapes the potential energy of the manipulator [see (16)]. Note that $\beta_{\text{max}}$ is proportional to the gain margin and the maximum overshoot; therefore, the gain margin is expected to increase at the expense of a higher overshoot when $\beta_{\text{max}}$ is augmented. To highlight the mentioned, we have selected two sets of gains as shown in Cases D and E from Table II. We choose Case D as the baseline case and, then, we increment $\beta_{\text{max}}$ in Case E by augmenting $K_{\text{es}}$. The responses in Fig. 7 verify that we obtain a better attenuation of the disturbance—i.e., the steady-state error improves—at the expense of an increased overshoot.

Next, we proceed to reduce the overshoot. Toward this end, we select Case E as the new baseline and modify $K_{d_1}$ and $K_{\text{int}}$ in Cases F and G. The gains and responses for these cases are shown in Table II and Fig. 8, respectively.

The gain selection for Case F is based on the circle-like theorem described in Theorem 3, where we use Fig. 2(a) as a quick visual aid. Note that, by augmenting $K_{d_1}$, some of the circles shift to the left, leading to a faster convergence rate and, consequently, fewer oscillations. The latter is verified in Fig. 8, where the oscillations are reduced substantially in Case F with respect to Case E.

Then, to improve further the performance, we inject gyroscopic forces via $J_2(q, p)$ in Case G, which employ again Theorem 3 to tune $K_{\text{int}}$. Consider Fig. 2(b) and note that the inclusion of $J_2(q, p)$ (or equivalently, $K_{\text{int}}$) shifts some of the circles in the imaginary axis; therefore, the eigenvalue may be located anywhere in the red arc resulting in less damping ratio, and consequently, the response may exhibit fewer oscillations.
The oscillations are reduced slightly in Case G with respect to Case F, as verified in Fig. 8 and Table III, where it contains the values of the square of the $L_2$-norm.\textsuperscript{11} The improvement in oscillations when $K_{\text{int}}$ is introduced is slight for this particular case study since this gain is small. This behavior stems from a limitation with the controller, that is, $K_{\text{int}}$ is selected such that $D_a > 0$. To verify this condition, we employ the Schur complement analysis, i.e., $K_{\text{int}}$ is chosen such that

$$D_a + G_1 K_{\text{int}} G_1^T > \frac{1}{2} G_1 K_{\text{int}} D_a G_1^T - 1/2 G_1 K_{\text{int}} > 0.$$  

Therefore, the selection of $K_{\text{int}}$ cannot be incremented further as it is restricted to the previous condition. Nonetheless, the improvement is still evident.

A video of the experimental results can be found in https://youtu.be/yUGs44K77wE.

VII. CONCLUSION AND FUTURE WORK

We have provided a broad guide for tuning the control parameters of a class of PBC methodologies that preserve the mechanical structure and prescribe the desired behavior in terms of several attributes: upper bound of the rate of convergence, maximum permissible overshoot, gain margin and oscillations in the transient response. Moreover, we have associated the PBC parameters with the physical quantities of the closed-loop system (energy or damping). Therefore, we have endowed the parameter selection process of PBC approaches with more intuition.

Furthermore, we have shown how a class of gyroscopic forces affects the behavior of the closed loop near the equilibrium.

In addition, we have successfully implemented our tuning rules on two mechanical system setups: 1) the PERA system (fully actuated configuration using 5-DOF) and 2) a planar manipulator with flexible joints (underactuated configuration). In both cases, we have reduced the oscillations of the transient response.

Regarding future work, we aim to find tuning rules to prescribe the behavior in the vicinity of the equilibrium of the closed-loop system when intrinsic gyroscopic forces are introduced. Moreover, we aim to find methodologies to calculate the parameters $\mu$ and $\epsilon$.

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