Effects of Shrinkage Reducing Agent and Expansive Additive on Plastic Shrinkage of Mortar at Different Temperatures

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Abstract. In the construction, it is inevitable to perform plaster work in hot weather which causes the dehydration and rapid shrinkage on the paste during the early age. This research shows the studies of reducing the plastic shrinkage of mortar during the early age with such additives as the Shrinkage Reducing Agent (SRA), the Expansive Additive (EX), and the Fly Ash (FA) in controlled temperatures at 30 °C and 40 °C, with relative humidity between 60% and 70% according to the ASTM C1579-06 standard, with the strain gauge installed at 0.5 cm from the surface. The shrinkage rate was measured starting from the Initial Setting Time and every 10 minutes afterwards for 24 hours. The results show that high temperature effects the cracking and how to use different formulas of additive under different circumstances is considerably important. To use only one additive is not sufficient in high temperature. To use the SRA in addition to the EX enhances better expansion than to use only the EX. Moreover, it is recommended to pay close attention in adding large amount of the FA into mortar with the EX and SRA added which extremely enhances the expansion and potential cracking.

1 Introduction

There are several methods in reducing the shrinkage of mortar. One of the methods is to use such inorganic materials and additives as the Shrinkage Reducing Agent (SRA) and the Expansive Additive (EX) which can be added during the mixing process[1-4]. Different types of additive to be added with the cement give different results depending on such factors as the property and quantity of the cement used, the mixing ratio, and the curing method. Therefore, thorough study on each type of additives and on the manufacturer's instructions is highly recommended because these additives are beneficial when used appropriately. However, the recommended amount may not always suitable for all operations under different circumstances. Hence, tests is needed to be conducted and the amount used should be controlled. The plaster work is commonly done during the day when the temperature is ordinarily high especially for a tropical country where the average temperature is 30°C and, in summer, possibly 40°C while most tests are conducted at 25°C, which hardly is in accordance with real construction. The high temperature is one of several important factors that affects the plastic shrinkage which usually occurs during the early age, i.e., within the first 24 hours [5-6], by effecting the cracking on the surface which not only is difficult to repair but also acts upon the long-term durability of the building structure system. According to the standards from the American Concrete Institute (ACI), the Expansive Additives are divided into 3 types: (1) K-type, with anhydrous hauyne (CaO *Al₂O₃*CaSO₄) as its basis; (2) M-type, with gypsum (CaSO₄) as its basis; and (3) S-type, with tricalcium aluminate (C₃A) and gypsum (CaSO₄) as its bases, while, according to the Japanese Standards, the Expansive Additives are divided into 2 types: (1) C-S-A type, which approximates to the K-type according to the ACI standards, producing the ettringite; and (2) CaO type, with Calcium Oxide (CaO) as its basis, producing Calcium Hydroxide(Ca(OH)₂). In this experiment, the EX with Calcium Oxide (CaO) was used as the main additive. The EX helps reduce the shrinkage due to such factors as the expansion from water absorption and the forming of pores and crystals during the hydration reaction process[7]. The Shrinkage Reducing Agent (SRA) is a chemical substance that lowers the surface tension by decreasing the capillary stress on the surface of the paste and reserves the inner moisture which helps to reduce the evaporation on the surface, thus, reducing the shrinkage of the paste on the chemical and environmental aspects[8 9]. The fly ash is the residual material from coal combustion during the electricity generation. It is round, smaller than 1 micrometre to 150 micrometres in size, generally in finer powder form than the cement, with specific gravity between 2.00 and 2.60. It possesses cementitious property that is called pozzolanic material while other pozzolanic materials generally possesses little
or no cementitious value but will, in finely divided form and in the presence of sufficient moisture, chemically react with calcium hydroxide at ordinary temperatures to form compounds having cementitious properties. The fly ash is therefore considered beneficial as an additive to be added to the cement mixture [10]. Experiments on the plastic shrinkage during the early age and studies on the 3 types of additive are rare. This research thus focuses on the influence of the plastic shrinkage reduction during the early age, i.e., within the first 24 hours, of mortar added with the fly ash, the shrinkage reducing agent (SRA), and the expansive additive (EX) at 30°C and 40°C. The analysis was conducted conforming to the ASTM C1579-06 standard, using the strain gauge to measure the shrinkage near the surface.

2 Materials and experiments

2.1 Materials

Table 1. shows the materials used in the experiment and Table 2. shows the chemical composition. The ordinary Portland cement (C), the fly ash (FA) Class C – according to the ASTM C618 standard, the expansive additive (EX) CaO type of chemical used for shrinkage reduction and the shrinkage reducing agent (SRA) Polyoxyalkylene alkyl ether type– Tetraguard® AS20 were used in this experiment along with fine sand prepared in surface-dry, saturated condition with fineness modulus (F.M.) of 3.05, 0.54% of absorption, and bulk specific gravity of 2.60.

2.2 Experiments

Table 3. shows the mortar mixing ratio. The water to binder(W/B) ratios were 0.7, the shrinkage reducing agent was used to replace the water at 0 and 2% for binder. To replace the cement with the EX and FA, the EX was determined to stay unchanged at 15% which is the recommended maximum amount, while the amount of FA was adjusted in accordance with the amount of the binder left in the composition. The Hobart mixer was used to mix the mortar by mixing the water and admixtures at low speed for 30 seconds before adding the binder using medium speed and adding the sand in 30 seconds before using high speed. The entire mixing duration was determined for 3 minutes. The setting time was determined following the ASTM C807 standard at 30°C and the plastic shrinkage was measured following the ASTM C1579-06 standard. The relative humidity was controlled in the range of 60-70%. The shrinkage was measured at 30°C and 40°C by controlling the heat from the heat lamps with the waterproof strain gauge for cement work applicable for the range of temperatures between -10 °C and 70 °C installed in the middle of the mold above the crack riser at 0.5 centimetre from the surface. The plastic shrinkage was measured and recorded once every 10 minutes for 24 hours starting from the initial setting time. Figure 1 and Figure 2 show the plastic shrinkage measurement.

| Kind | Symbol | Specific gravity | Blaine (cm²/g) |
|------|--------|-----------------|---------------|
| Cement | Ordinary Portland Cement | C | 3.15 | 3,400 |
| Fly ash | FA | 2.23 | 3,800 |
| Expansive additive | EX | 3.16 | 3,450 |
| Shrinkage reducing agent | SRA | 0.99 | - |

| Kind | SiO₂( %) | Al₂O₃(%) | Fe₂O₃(%) | CaO(%) | MgO(%) | Na₂O(%) | K₂O(%) | SO₃(%) |
|------|---------|---------|---------|--------|--------|---------|--------|--------|
| C | 21.45 | 4.64 | 3.05 | 64.99 | 0.88 | 0.09 | 0.59 | 2.47 |
| FA | 24 | 10 | 21.2 | 32.6 | 2.08 | 0.1 | 3.57 | 1.1 |
| EX | 4.2 | 1.1 | 1 | 74 | 0.51 | - | - | 16.5 |

| W/B ratio | FA Replacement ratio(Bx%) | EX Replacement ratio(Bx%) | SRA Dosage (Bx%) |
|-----------|--------------------------|--------------------------|-----------------|
| 0.7 | 0,20,40 | 0,15 | 0,2 |
3 Results and discussions

Figure 3, 4 and 5 show the results of plastic shrinkage during the early age of mortar added with the EX, SRA and FA at 30°C and 40°C in comparison with that of the control mortar (C 100%) 24 hours after molding in accordance with the ASTM C1579-06 standard. The result shows that the shrinkage and expansion rate highly occurs since the initial setting time and the rate decreases after approximately 10 hours after molding. It is obviously seen that, as the temperature rises, the shrinkage rate tends to increase for all formulas of mixture, especially for the control mortar (C=100%) at 40°C, the risk of cracking is highest in this regard. Mortar with 15% of EX added expands extremely during the early age at ordinary temperatures. The mortar added with 2% of SRA extremely reduced the plastic shrinkage both at 30°C and at 40°C by 24.4% and 57.6% respectively after being compared to the control mortar at the same temperature. However, at 40°C, though the SRA extremely reduced the shrinkage, the measurable plastic shrinkage result was higher than 1000 µƐ. Therefore, there is still a high risk of the cracking on the surface to use only the SRA at high temperature. To add the FA helps to reduce the shrinkage during the early age. The mortar’s shrinkage rate decreases in accordance with the increasing ratio of the FA added. This decreasing shrinkage may be the result of the roundness of FA which lessens the water requirement of mortar, causing the excess water on the surface[11-12], resulting the extension of the evaporation period. Moreover, the cement replacement reduces the hydration reaction between the cement and the water which is a cause of the shrinkage[13]. The expansion rate shall increase when the EX+SRA are added. This increasing expansion may be the result of the CaO crystal forming of the EX which normally creates the calcium hydroxide in the form of Hexagonal plate but to add the SRA changes the crystal forming to be in the form of Prismatic needle which is longer in shape[14]. To replace the cement with 15% of EX +2% of SRA and 20% of the FA does not clearly result in the expansion compared to adding 15% of EX + 2% of SRA but, when 40% of the FA was replaced, the expansion rate increases for more than 50% compared to adding 15% of EX + 2% of SRA at 25 °C and at 40 °C respectively. Nevertheless, care should be taken in terms of compressive strength because the large amount of FA added can reduce the strength during the early age.
Figure 4. Early age plastic shrinkage results for SRA and SRA + FA at 30°C and 40°C

Figure 5. Early age plastic shrinkage results for EX+SRA and EX+SRA + FA at 30°C and 40°C

Figure 6. To compare Early-age plastic shrinkage of mortar mixed with FA, EX and SRA at 30°C and 40°C at 24 hrs. after casting

4 Conclusion

From the experiment, summaries can be stated as follow.

1) To replace the water with 2% of SRA helps to reduce the plastic shrinkage in all ranges of temperature but may not be sufficient when the temperature is up to 40 °C and it helps reducing the shrinkage to add the SRA+FA in accordance with higher amount of the FA added.

2) To add 15% of the EX increases the plastic expansion rate of mortar during the early age, i.e., the expansion rate increases when the ratio of replacing the cement with FA is raised.

3) To add 15% of EX + 2% of SRA increases the plastic expansion rate of mortar during the early age more than to add only the EX or SRA. The expansion rate extremely rises when the ratio of replacing the cement with FA especially for 40% is raised.

4) In all formulas of mixture, the plastic shrinkage rate during the early age rises as the temperature changes from 25 °C to 40 °C.

5) It is recommended to adjust the amount of EX, SRA and FA used in different circumstances to meet the appropriateness as each environmental circumstance differently affects the plastic shrinkage during the early age.

More research is required in different conditions such as steam curing and other properties such as strength and crystalline structure.
References

1. Palacios M and Puertas F, Y 2005, Cement and Concrete Research 37 pp 691-702
2. Saliba J, Rozière E, Grondin F and Loukili A, Y 2011, Cement and Concrete Composite 33 pp 209-217
3. Carballosa P, García JL, Revuelta D, Sánchez JJ and Gutiérrez JP, Y 2015, Construction and Building Materials 93 pp 223-229
4. Choi H, Lim M, Kitagaki R, Noguchi T and Kim G, Y 2015, Construction and Building Materials 84 pp 468-476
5. Uno P J, Y 1998 ACI Materials Journal, July-August pp 365-375
6. Holt E and Leivo M, Y 2004 Cement & Concrete Composites 26 pp 521-530
7. Nagataki S and Gomi H, Y 1998 Cement and Concrete Composite 20 pp 163-170
8. Wyrzykowski M, Trtik P, Müncha B, Weiss J, Vontobel P and Lura P, Y 2015 Cement and Concrete Research 73 pp 238-245
9. Bentz D P, Geiker M R and Hansen K K, Y 2001, Cement and Concrete Research 31 pp 1075-1085
10. Chindaprasirt P, Jaturapitakkul C and Sinsiri T, Y 2005 Cement & Concrete Composite 27 pp 425-428
11. Termkhajornkit P, Nawa T, Nakai M, and Saito T, Y 2005, Cement and Concrete Research 36 pp 473-482
12. Nawaz A, Julnipitawong P, Krammart P, Tangtermsirikul S, Y 2016, Construction and Building Materials 102 pp 515-530
13. Treesuwan S and Maleesee K, Y 2017, Advances in Materials Science and Engineering vol 2017 pp 1-11
14. Maltese C, Pistolesi C, Lolli A, Bravo A, Cerulli T and Salvioni D, Y 2005, Cement and Concrete Research 35 pp 2244-2251