1. Introduction

Methanol steam reforming (MSR) remains one of the most important reactions in hydrogen economy to access large amounts of hydrogen that can subsequently be used as a renewable energy carrier [1]. The most crucial parameter steering the reaction to high H₂ yields is efficient water activation, which is a prerequisite for high CO₂ selectivities [2]. Among many materials that can be used to selectively catalyze this reaction in the desired direction [3], intermetallic compounds have arisen as a promising material class [4–10]. Pd-based intermetallic compounds have been particularly scrutinized in this respect [11–14], but Cu-Zr materials have also been a focus of research [2,15,16]. As the common denominator to explain the catalytic selectivity patterns, a bifunctional synergistic action of intermetallic compound and supporting oxide, sharing the sites of methanol and water activation, respectively, has been proposed [11,17]. Different synthesis pathways have been reported to gain access to these materials, including reactive metal-support interaction starting from
small metal particles on oxide supports (i.e. reduction in hydrogen), yielding intermetallic compound particles distributed on the oxide support and a defined interface between them [5]. ZnPd-ZnO [12], Ga2Pd-Ga2O3 [13] and InPd-In2O3 [11] are prime examples of such systems. A second pathway is related to the in situ decomposition of nanosized or bulk intermetallic compounds in the MSR mixture, yielding both bifunctionally operating interfaces. In this respect, oxidative segregation effects either yield small patches of oxide on the intermetallic compound surface (as observed, for example, for ZnPd/ZnO) [17, 18] or a complete corrosive decomposition of the structure into a dispersed metal/oxide system (as prevalent, for example, for Cu2/Zr14) [15, 16].

Explaining the catalytic action of such systems necessarily involves a deep understanding of the individual constituents of the material and, in particular, the oxide phase. Depending on the intrinsic catalytic properties, the oxide could beneficially or detrimentally contribute to the catalytic properties of the entire system. As far as the latter, selectivity-spoiling effects by the (inverse) water-gas shift equilibrium (e.g. for Ga2O3) could be observed [11]. However, In2O3 is the archetypical beneficially acting oxide entity, as it is not only a highly CO2-selective (yet comparably inactive) catalytic material in MSR by itself [19] but has recently also been reported to act as a superior catalyst for the methanol synthesis by CO2 hydrogenation [20].

As copper is a recurrent metal constituent of many prospective MSR catalysts (despite the ongoing discussion about the nature of the active site, if either strain phenomena or ionic copper species are responsible for the catalytic action) [3], it is straightforward to combine Cu and In2O3 to potentially create a new MSR catalyst with superior activity and selectivity. Our interest in the system Cu-In2O3 is also fueled by recent reports on the beneficial influence of Cu on In2O3 in the formation of methanol by hydrogen/water reduction of CO2 [21]. Whether In2O3 is able to stabilize the potentially active and selective copper species (thereby suppressing the notorious sintering of Cu particles, for example, deactivating Cu particles on ZnO and significantly decreasing the lifetime of these catalysts) or rather leads to specific intermetallic Cu-In particles supported on In2O3 is in the focus of this article. The Cu-In phase diagram is well known and features a variety of different intermetallic compounds with variable stoichiometries [22]. As the region around 30 at% In exhibits compounds with high melting points, chances are high that single-phase oxide-supported intermetallic compounds can be accessed by reactive metal-support interaction. Additionally, a high temperature Cu-In phase, which undergoes eutectoid decomposition upon cooling, was reported to catalyze the oxidative dehydrogenation of methanol to formaldehyde. This proves that the obtained eutectic cast with the overall stoichiometry Cu3In is able to activate methanol, even though the resulting phases are not identified by the authors in [23].

This article focuses on two selected research areas, whose comprehension is necessary to develop a knowledge-driven synthesis routine and enable a full understanding of the operation of the Cu-In2O3 system in MSR. First, the reactive metal-support interaction between Cu and In2O3, that is, the reduction in hydrogen and the corresponding intermetallic compound formation, will be assessed. As the removal of reaction-induced water is a key parameter in the efficient formation of intermetallic compounds, we will perform experiments under recirculating batch and quasi-flowing conditions. This potentially enables us to access different oxide-supported single-phase intermetallic Cu-In compounds, whose catalytic properties can then be assessed. In the second part, we test the properties of these oxide-supported intermetallic Cu-In compounds in MSR and relate the results to previously tested intermetallic materials, especially systems based on Pd. An integral part of the characterization will be devoted to synchrotron-based in situ X-ray diffraction (XRD) measurements to follow the structural transitions in the course of reactive metal-support interaction.

2. Experimental details
2.1. Preparation of the Cu/c-In2O3 catalyst
Bixbyite-type cubic indium oxide (c-In2O3, space group Ia3, a = 10.118 Å [24]; Alfa Aesar, 99.99% metals basis) was suspended in deionized water and an aqueous solution of Cu(II) acetate (Cu(OOCCH3)2 ·H2O; Merck) was added dropwise under stirring. The solvent was subsequently removed under vacuum at 60 °C and the resulting turquoise powder calcined in air at 400 °C for 2 h, yielding the gray CuO/c-In2O3 catalyst with a nominal loading of 8.0 wt% CuO in the calcined state (corresponding to 6.5 wt% metallic Cu after pre-reduction).

2.2. Catalytic measurements
Catalytic testing was performed in a recirculating batch reactor connected to a quadrupole mass spectrometer (QMS) arranged in cross-beam geometry, equipped with a secondary electron multiplier (Balzers QMG 311). This setup is specialized for the measurement of small sample amounts (approximately 100 mg) and conversions (reactor volume = 13.8 mL). The reactor and the sample holder are made of quartz glass and can be heated up to 1100 °C in a Linn High Term furnace. The temperature is monitored with a K-type thermocouple (NiCr-Ni).

For the MSR measurements, ~28 mbar of a mixture with a ratio of methanol:water = 1.2 (v/v) in the gas phase is prepared to avoid water depletion during the reaction. One MSR cycle consists of three steps: (1) pre-oxidation
at 400 °C in 1 bar pure O\textsubscript{2} for 1 h (termed O400), (2) pre-reduction at 300 °C in 1 bar pure H\textsubscript{2} for 1 h (termed H300) and (3) MSR reaction. The latter is carried out by the addition of Ar to the MSR mixture (for correction of the signals considering the thermal expansion and the capillary leak to the QMS) and balancing the pressure to 1 bar with He (for improvement of the recirculation efficiency and the thermal conductivity) at 100 °C. Starting from this temperature, a heating ramp with 5 °C min\textsuperscript{-1} is applied, and the gas phase composition is continuously monitored by the QMS.

The formation rates are obtained by differentiation of the partial pressure versus reaction time graphs, which is acquired by the application of the calibration. Then, the conversion to μmol using the ideal gas law and normalization to the total copper mass determined by differential pulse voltammetry (DPP; see sections 2.4 and 3.1) yields the formation rates in μmol gCu\textsuperscript{-1} s\textsuperscript{-1}.

The apparent activation energy for the CO\textsubscript{2} evolution \((E_a)\) was calculated by Arrhenius fitting of the formation rate versus the temperature plot at the beginning of the rate increase, thus, excluding influences of the reaction products on the equilibrium. To enhance the comparability of the apparent activation energy between different catalytic materials, the pre-exponential factor \(A\) is fixed to a value of \(10^{8} \) μmol gCu\textsuperscript{-1} s\textsuperscript{-1} to avoid any influence of statistical fluctuations on the fitting procedure. These values are in good agreement with pre-exponential factors reported by Baetzold and Somorjai for diffusion-controlled surface reactions [25].

2.3. Structural characterization

The \textit{ex situ} XRD measurements were performed in the transmission mode utilizing a Stadi P diffractometer (STOE & Cie GmbH, Darmstadt, Germany). This setup is equipped with a MYTHEN2 DC54 detector (DECTRIS Ltd., Switzerland) and a Mo X-ray tube (GE Sensing & Inspection Technologies GmbH, Ahrensburg, Germany) with a heating current of 40 mA and an acceleration voltage of 50 kV. A curved Ge(111) crystal selects the Mo K\textsubscript{al} radiation with a wavelength of 0.7093 Å. The analysis of the diffractograms was carried out with the software WinXPOW using reference data from the ICDD database [26,27].

The \textit{in situ} high-temperature synchrotron XRD experiments in H\textsubscript{2} were performed at the beamline 12.2.2, Advanced Light Source (ALS), Lawrence Berkeley National Lab, CA, USA. The \textit{in situ} diffraction patterns were collected in the angle-dispersive transmission mode with a focused 25-keV monochromatic beam (\(λ = 0.4984 \) Å, 30 μm spot size). The sample powder was heated in a 0.7-mm quartz capillary under a continuous gas flow (10 ml min\textsuperscript{-1} pure H\textsubscript{2}) injected through a 0.5-mm tungsten tube. The capillary is heated at 10 °C min\textsuperscript{-1} to 500 °C in an infrared-heated SiC tube furnace as described in [28,29]. Diffraction patterns were recorded by a PerkinElmer flat panel detector (XRD 1621, dark image and strain correction) every 35 s during the heating cycle.

Transmission electron microscopy (TEM) measurements were carried out using a FEI Tecnai F20 2-TWIN analytical (high-resolution) transmission electron microscope (200 kV), equipped with an Apollo XLTW SDD X-ray detector (for collecting energy-dispersive X-ray (EDX) data).

2.4. DPP

The total copper content of the CuO/c-In\textsubscript{2}O\textsubscript{3} catalyst was determined by DPP) in 0.05 M sodium acetate as supporting electrolyte. Measurements were performed on a CV 50 W potentiostat (BAS) controlled by the software CV 50 (BAS) in combination with an EG&G 303a electrode stand and a classical three-electrode configuration with a hanging mercury drop electrode (HMDE; drop size M) as working electrode, a platinum wire auxiliary electrode and a Ag/AgCl/3 M KCl reference electrode. A pulse amplitude of 50 mV with a duration of 50 ms, a sampling time of 20 ms, a pulse period of 200 ms and a scan rate of 10 mV s\textsuperscript{-1} was applied during each voltammetric scan. The Cu\textsuperscript{2+}/Cu reduction peak occurs at 0.050 V versus Ag/AgCl/KCl (3 M) under these measurement conditions. Removal of oxygen from the solution is essential and was achieved by purging at least for 10 min with nitrogen 5.0 before the first recording of the voltammogram of the pure supporting electrolyte and at least 2 min after each sample or standard addition.

3. Results and discussion

3.1 Determination of the copper content of Cu/c-In\textsubscript{2}O\textsubscript{3} by DPP

Two different sample solutions containing nominal concentrations of 61 ppm Cu and 5.8 ppm Cu were analyzed. Quantification of the total copper amount was performed by standard addition and external calibration using freshly prepared 100 and 10 ppm Cu standard solutions. The more concentrated sample contained 49.7 mg CuO/c-In\textsubscript{2}O\textsubscript{3} with about 6.4 wt% copper dissolved in 50 ml of about 7% HNO\textsubscript{3}. For this sample, an average total amount of 48 ppm Cu was obtained by DPP. For the diluted sample of 9.4 mg CuO/c-In\textsubscript{2}O\textsubscript{3} with the same nominal copper content dissolved in 100 ml 7% HNO\textsubscript{3}, an average amount of 4.65 ppm Cu was found by DPP. Since both samples contain the same Cu/c-In\textsubscript{2}O\textsubscript{3} catalyst, an average copper loading of 6.4 wt% CuO and 5.1 wt% Cu in the calcined state can be deduced.
3.2 Reactive metal-support interaction between Cu and In$_2$O$_3$: monitoring the intermetallic compound formation between Cu and In during reduction in hydrogen

The formation of intermetallic Cu-In compounds was investigated at first by ex situ powder XRD after different pre-reduction temperatures in the recirculating batch reactor to directly relate the structural consequences during pre-reduction to the subsequent catalytic measurements in MSR. A measure of 1 bar of pure H$_2$ for pre-reduction was used for 1 h, whereby the temperature was increased stepwise from 100 °C to 500 °C. Higher reduction temperatures were not used, since at 500 °C, the In$_2$O$_3$ support already starts to be reduced to metallic In. A fresh calcined sample was used for each treatment. The label indicating the last treatment performed on a sample consists of a letter for the respective gas (A for air, O for O$_2$, H for H$_2$, MSR for the MSR mixture) and a value for the temperature (i.e. H100 denotes pre-reduction in pure H$_2$ at 100 °C for 1 h).

The ex situ collected XRD patterns of the pre-reduction series at five temperatures from 100 °C to 500 °C are displayed in Figure 1. Starting at 100 °C, Cu remains fully oxidized (as CuO), whereas reduction at 200 °C already yields metallic Cu on the yet unchanged c-In$_2$O$_3$ support. The H300 sample appears structurally very similar to the one treated at 200 °C, but a further increase to 400 °C leads to the formation of intermetallic Cu-In compounds. According to the Cu-In phase diagram, Cu$_2$In is the intermetallic phase with the highest melting point. The most prominent reflections in the H400 XRD pattern can be assigned to such a hexagonal Cu$_2$In structure with the space group P6$_3$/mmc ($a = 4.2943$ Å and $c = 5.2328$ Å) [30]. Cu$_2$In could also be present, as it also displays its most intense reflection in the same 20 region. However, the other reflections do not clearly match Cu$_4$In. Metallic copper vanishes completely, which further corroborates the formation of intermetallic Cu-In compounds. Most of the Cu-In intermetallic reflections are somewhat shifted from their ideal position, which can be explained by the still ongoing phase formation and the homogeneity range, allowing for the incorporation of some amounts of Cu/In into the parent intermetallic compound lattice resulting in deviations from the ideal lattice parameters. After pre-reduction at 500 °C, c-In$_2$O$_3$ starts to become partially reduced to metallic In, and the reflections of the intermetallic compounds change significantly in their position, as well as in their relative intensity. The shift in the diffraction angle could once more be the result of a phase width of a distinct intermetallic Cu-In compound with a concomitant change of the lattice parameters. In summary, we can conclude that after a reduction treatment at 300 °C, metallic Cu, but no bulk intermetallic Cu-In compound is present, whereas after reduction at 400 °C, the metallic Cu state disappears and is replaced by Cu$_2$In.

We mention already at this stage that a pre-reduction at 300 °C and 400 °C conveniently allows to assess the potential influence of intermetallic compound formation on the catalytic behavior in MSR as a test reaction. Two states can, hence, directly be accessed: Cu/c-In$_2$O$_3$ (300 °C) and Cu$_2$In/c-In$_2$O$_3$ (400 °C). An obvious prerequisite, however, is the bulk structural stability of the phases during the catalytic reaction. This has been assessed by ex situ XRD and is shown accordingly in Figure 2. Starting from the calcined state (A400, with an additional O400 treatment prior to MSR, ensuring that the sample is completely oxidized and removing residual surface impurities), the catalyst is reduced to a mixture of Cu$_2$O and Cu by the MSR mixture in the course of reaction (diffractograms after two MSR cycles each consisting of O400 and MSR up to 350 °C (termed MSR350) are being depicted in Panel A of Figure 2). Introducing an additional pre-reduction step at 300 °C in H$_2$ before MSR changes the initial state to fully reduced Cu on c-In$_2$O$_3$ and no significant changes in the diffractogram are visible after two complete MSR cycles (each consisting of O400, H300 and MSR350, see

Figure 1. Ex situ XRD diffraction patterns collected on the Cu/c-In$_2$O$_3$ catalyst after pre-reduction in 1 bar pure H$_2$ for 1 h at different temperatures from 100 °C (bottom) to 500 °C (top). The most intense reflections have been cut to enhance the visibility of the other peaks. Reference diffractograms (color-coded bars with respective legend on top) have been considered and taken from the ICDD database [27] (PDF files: c-In$_2$O$_3$ 00-006-0416 [24]; Cu 00-004-0836 [34]; CuO 01-071-3645 [31] (not observed here); CuO 01-080-1916 [32]; In 03-065-9292 [33]; Cu$_2$In 00-042-1475 [30]; Cu$_4$In 00-042-1477 [30]).
The thermodynamic driving force for intermetallic compound formation is, thus, the efficient removal of reaction-formed water, which shifts the equilibrium toward the products. Thus, it can be expected that a treatment in the recirculating batch reactor, where the water basically is not removed, merely causes a minor reduction of In$_2$O$_3$. Hence, also the intermetallic compound formation is apparently less efficient compared to treatments, where water is constantly removed. To assess the influence of water removal, in situ XRD measurements have been performed. In this capillary setup, quasi-flowing
conditions can be realized as discussed in the experimental section. These are collectively shown in Figure 4.

In the course of the experiment, qualitatively the same sequence of phase transformations can be observed, corroborating the data shown in Figure 1. Starting from oxidized Cu particles on c-In$_2$O$_3$, formation of metallic Cu sets in at around 240 °C, before reduction of In$_2$O$_3$ and intermixing of Cu and In is observed roughly between 370 °C and 450 °C. In this temperature region, a complex phase mixture of several intermetallic Cu-In compounds is observed, before finally at 460 °C, Cu$_2$In prevails as the sole intermetallic compound. The 2θ shift in the reflections of Cu$_2$In and Cu in the temperature range of Cu$_2$In formation suggests that the intermetallic compound is formed by interdiffusion of Cu and In. This finding directly corroborates the phase assignment in the ex situ XRD measurements, where around 400 °C also Cu$_2$In prevails as the main phase.

3.3 Influence of the intermetallic compound formation on the CO$_2$ selectivity and performance in MSR

The influence of intermetallic compound formation starting from CuO on c-In$_2$O$_3$ on the performance in MSR was investigated by starting the reaction from different initial states. The most important catalytic parameters of relevant cycles of the three initial states are summarized in Table 1. In Figure 5, the MSR reaction was conducted after calcination with an additional oxidation step at 400 °C for 1 h in pure O$_2$ (O400). The formation of hydrogen and carbon dioxide starts at approximately 180 °C, but no CO and only traces of CH$_4$ (below 0.05 mbar in total) are produced. As expected, hydrogen evolving in the beginning is almost entirely consumed again, reducing the initially present CuO to Cu$_2$O and Cu (see also Figure 2, Panel A). The methanol conversion reaches a maximum of 90%, and the CO$_2$ selectivity amounts to 100% at any time because of the absence of CO formation. The decrease in the
formation rates in all catalytic profiles is caused by the depletion of the reaction mixture, which is inherent to a batch reactor. The second cycle on this system was omitted, because it exhibits an almost identical behavior.

Starting MSR after pre-reduction in 1 bar pure H₂ for 1 h at 300 °C yields the catalytic profiles depicted in Panels A and B of Figure 6, which represent two full catalytic cycles (O400, H300, MSR350) on the same sample without exposure to air. In contrast to the measurements without pre-reduction, hydrogen is formed as the main product of the reforming reaction with a rate that is three times as high at its maximum as the corresponding value for CO₂ at the same time, representing the ideal stoichiometry of MSR. Only traces of CO and CH₄ are being formed with their maximum rates amounting to approximately 1.5% (1.8% CO and 1.0% CH₄ in the second cycle) compared to H₂. This is also reflected in the CO₂

Table 1. Summary of key catalytic parameters of the methanol steam reforming reaction starting from pre-oxidized CuO (O400), from metallic Cu (H300) and from Cu₂In (H400) on c-In₂O₃.

| Light-off T(H₂) (°C) | O400 CuO/c-In₂O₃ | H300 Cu/c-In₂O₃ | H400 (cycle 1) Cu₂In/c-In₂O₃ | H400 (cycle 4) Cu₂In/c-In₂O₃ |
|---------------------|-----------------|-----------------|-----------------------------|-----------------------------|
| Light-off T(CO) (°C) | 180             | 200             | 230                         | 230                         |
| Light-off T(CO₂) (°C) | –               | 290             | 300                         | 300                         |
| Light-off T(CH₄) (°C) | 180             | 200             | 320                         | 300                         |
| Maximum rate H₂ (µmol g⁻¹ s⁻¹) | 1.2             | 1.3             | 1.8                         | 3.8                         |
| Maximum rate CO (µmol g⁻¹ s⁻¹) | –               | 0.02            | 0.02                        | 0.07                        |
| Maximum rate CO₂ (µmol g⁻¹ s⁻¹) | 2.9             | 0.45            | 0.69                        | 1.3                         |
| Maximum rate CH₄ (µmol g⁻¹ s⁻¹) | 0.11            | 0.02            | 0.02                        | 0.01                        |
| Methanol conversion (%) | 90              | 56              | 62                          | 84                          |
| Minimum CO₂ selectivity (%) | 100             | 93              | 94                          | 92                          |
| Eₘ(CO₂) (kJ mol⁻¹) | –               | 101             | 99                          | 97                          |
selectivity, which exceeds 93% over the course of the entire measurement in both cycles. The methanol conversion, however, only reaches a final value of 56% (51% in the second cycle), suggesting a rather low activity of the catalyst.

Increasing the pre-reduction temperature to 400 °C, that is, starting from Cu\textsubscript{2}In/c-In\textsubscript{2}O\textsubscript{3}, leads to the catalytic patterns of four complete MSR cycles (O400, H400, MSR350) depicted in Panels C–F of Figure 6, which look similar to the ones...
obtained by pre-reduction at 300 °C (see Figure 6, Panels A and B). The differences are the absence of the noncatalytic H₂ consumption and the overall higher formation rates. Additionally, the activity increases with increasing number of catalytic cycles. Starting from H₄₀₀ instead of H₃₀₀ increases the H₂ formation rate by a factor of 1.5 in the first cycle and more than 3 times in the fourth cycle. Conducting four catalytic cycles on the same catalyst, thus, doubles the H₂ formation rate, while the initial final methanol conversion of 62% is enhanced to 84% during the fourth cycle. However, the CO formation rate also slightly increases, which leads to a decrease in the minimum CO₂ selectivity from 94% to 92%, whereas the CH₄ formation rate is lowered despite the increase in total activity.

Putting these results into perspective of the performance of previous intermetallic compounds in MSR especially on Pd basis, we note several similarities and differences. Speaking of reactive metal-support interaction, intermetallic compound formation in the Pd-In system, starting from Pd-In₂O₃, is much more efficient and occurs at much lower temperatures than on Cu-In₂O₃ [11,38]. InPd is formed already after reduction at 300 °C, followed by even In-richer intermetallic compounds at higher temperatures. The most intriguing difference between the two systems is the formation of thin TEM-detectable In₂O₃ layers around the InPd particles after contact to the MSR reaction mixture in batch reactor experiments, thus deactivating the catalyst after use due to the removal of active intermetallic surface/intermetallic compound-supporting oxide interfacial area. Apparently, this does not happen to this extent for the Cu-In₂O₃ material, which further activates after several catalytic cycles in the batch reactor. The immediate reason for this behavior in a very simplified picture might be found in the general lower indium content in the formed intermetallic Cu-In compounds, rendering the decomposition of the latter into a thin oxide layer surrounding the particles less likely. Note that the principal simple formation of a thinner, possibly also amorphous oxide layer, being invisible in XRD or TEM is excluded, as the catalytic profiles are very sensitive to changes in the surface composition. An immediate loss of Cu-In intermetallic surface area would, thus, be catalytically recognized. Comparing the catalytic key parameters between In-Pd and In-Cu catalysts reveals lower activation energies for the former (64 kJ mol⁻¹ on InPd/In₂O₃ [39] vs. around 96 kJ mol⁻¹ for Cu₂In/c-In₂O₃, see Table 1) but similar CO₂ selectivities (>95% for InPd/In₂O₃ [39] vs. >92% for Cu₂In/c-In₂O₃, see Table 1). CO₂ light-off temperatures are also comparable at around 230–250 °C for both. In combination with the obvious structurally favorable stability of the Cu₂In/c-In₂O₃ interface, it renders the latter a more attractive choice as a CO₂-selective MSR catalyst.

4. Conclusions

In conclusion, we have shown that reactive metal-support interaction in the Cu-In₂O₃ system leads to the formation of an intermetallic Cu₂In compound after reduction in hydrogen at 400 °C. Higher reduction temperatures lead to complex phase mixtures and eventually to the reduction of In₂O₃ to In metal. Cu₂In itself is structurally stable during MSR. Clearly, different catalytic profiles between a Cu/c-In₂O₃ and a Cu₂In/c-In₂O₃ interface in MSR with respect to self-activation and general activity have been observed. Therefore, Cu₂In/c-In₂O₃ is found to be superior to Cu/c-In₂O₃ in terms of activation at a comparable CO₂ selectivity, with a doubling of activity from the first run to the fourth run (accompanied by a 20% increase in the methanol conversion) at a constantly high CO₂ selectivity between 92% and 94%. This article, hence, features a new prospective class of intermetallic compound-based highly CO₂-selective MSR catalysts using c-In₂O₃ as starting support material before exploiting reactive metal-support interaction to access the intermetallic compounds. As especially in the in situ XRD measurements plenty of different intermetallic Cu-In phases have been observed after reduction in a temperature segment close to where Cu₂In has been obtained, future studies must be directed at the deliberate synthesis of intermetallic Cu-In compounds with controlled and defined stoichiometry to enable the knowledge-driven assessment of the ideal Cu-In ratio and the corresponding oxidative segregation/formation tendency of a potentially CO₂-selective intermetallic Cu-In compound/c-In₂O₃ interface. In particular, it needs to be assessed whether this segregation occurs at all (i.e. to answer the question if the interface is actually required) or whether the intermetallic compound itself is able to activate both methanol and water. If such an interface is indeed necessary for a high CO₂ selectivity, the Cu/c-In₂O₃ system can be incorporated into the large group of oxide-supported intermetallic compound catalysts (e.g. Cu₃Zr₁/Zr₂O₃, ZnPd/ZnO, Ga₃Pd/Ga₃O₃ or InPd/In₂O₃), where such a bifunctional synergism of oxide (water activation) and intermetallic compound (methanol activation) is prevalent. The presented results strongly suggest that this is indeed the case.

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**Disclosure statement**

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