Comparative Studies of WC-Co and WC-Co-Ni Composites Obtained by Conventional Powder Metallurgy

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The present work reports a comparative study of cemented carbides of compositions WC-6Co, WC-10Co, WC-20Co, WC-6Co-6Ni and WC-12Ni-6Co. The purpose was to study the powder metallurgical production process of these compositions starting from a commercial WC-6Co powder, obtaining the desired compositions by mass balance with pure Co and pure Ni powders. During the process steps mixing, milling, compacting and sintering the powders were described by its apparent density, green density, shrinkage and sintered density. Lower densities were observed in composites with higher binder content. The process was monitored by scanning electron microscopy and EDS analysis to evaluate the homogeneity of the powders, to detect contaminations by the process and to characterize the microstructure of the sintered materials. A finer microstructure was found when the binder contained Ni. Potentiodynamic polarization tests in sulfuric acid revealed pseudo-passive behavior for all the tested hard metals.

Keywords: powder metallurgy, hard metal, WC-Co, WC-Co-Ni

1. Introduction

Hard metals are essentially composed of WC particles incorporated in a Co matrix. Their characteristics are high hardness and wear resistance, resistance to compression, tenacity and thermal stability. The properties are defined by the combination of the properties of the carbides and of the matrix. Other carbide forming elements, present in many hard metals, are Ti, Ta, V, Nb. The addition of small quantities of these elements has the function to inhibit WC grain growth during sintering. WC dissolves in the Co matrix during sintering and precipitates again at other carbide particles during cooling. In this way particle coarsening occurs since small carbides dissolve preferentially and reprecipitate at greater particles. Together with the grain growth the morphology of the carbides changes. The carbon content is another important aspect which modifies the properties of hard metals. The carbon content has to be between 6.15 and 6.20 wt. (%), in the matrix phase between 0.10 and 0.18 wt. (%). Higher carbon contents cause reprecipitation of carbon as free graphite.

The role of Co in hard metals is to form a ductile matrix for the carbide particles. During liquid phase sintering it permits to obtain material of high density. Commercial hard metals have a Co content between 3 and 25 wt. (%). Nickel, a ductile metal, is sometimes added to modify the binder composition. The most important aim of this modification with Ni is to improve the corrosion resistance of the hard metal.

In the present work the powder metallurgical production of WC-CoNi composites is documented, using as raw material a commercial WC-6Co powder. The influence of Ni on the different production steps is monitored by electron microscopy and EDS. The influence of Ni on the electrochemical behavior is examined by voltammetric curves.

2. Materials and Methods

Commercial WC-6%Co powder with purity of 99% and granulometry of -325 Mesh was delivered by Alfa Aesar. Powders of the pure metals, Co and Ni, (99% purity, ~-400 Mesh) were also delivered by Alfa Aesar.

Composites with the desired composition were obtained by mixing the commercial WC-6Co powder with the pure metal powders. Using mass balance calculations the necessary quantities of Co and Ni were determined, which have to be added to 100 g of WC-6Co in order to obtain the following materials: 90WC-10Co, 80WC-20Co, 94WC-6Co, 88WC-6Co-6Ni, 82WC-6Co-12Ni. The calculated quantities of Co and Ni are listed in Table 1.

The powder mixture was prepared in two steps: At first the powder components were put in an attritor mill and mixed one hour at 100 rpm in ethyllic alcohol under argon atmosphere. In the second step the powder mixture was homogenized during 30 minutes in a Y-mixer with the addition of 1.5 wt. (%) zinc stearate as lubricant.
3. Results and Discussion

3.1. Raw material

Figure 1 represents the commercial WC-6Co powder delivered by Alfa Aesar. It shows agglomeration of the powder particles. The particle size is clearly less than 10 μm as shown in Figure 1a. In Figure 1b the EDS analysis in the marked area of Figure 1a is shown. Only the elements Co and W are detected confirming the purity of the powder material.

The powders of the pure metals, Co and Ni, are shown in Figure 2a and b, respectively. Almost all particles seen in the micrographs have less than 10 μm.

The powders of WC-6Co, WC-10Co and WC-20Co were mixed in the quantities indicated in Table 1 as described in the Materials and Methods section.

3.2. Characterization of powder mixtures

The powder mixtures were analyzed by scanning electron microscopy in order to evaluate the degree of homogeneity obtained by the mixing procedure. Figure 3a and 3b show the mixtures of the WC-6Co and WC-20Co composites, respectively. In Figure 3a agglomerated WC-6Co particles of grey color can be distinguished from agglomerated Co particles which are darker. White particles of lubricant can also be identified. The powder mixture of the WC-20Co composite in Figure 3b shows a much more homogeneous distribution of the powders and the lubricant.

The powder mixture for WC-6Co-6Ni in Figure 4a shows good homogeneity, since none of the constituents can be identified separately. In the case of the WC-6Co-6Ni mixture (Figure 4b) agglomerated Ni as well as agglomerated and isolated WC-6Co particles are visible. Pure Co cannot be identified due to its low amount in the sample.

After the described mixing procedure the apparent density of the powder mixtures were determined. Table 2 shows that the commercial WC-6Co powder has the highest apparent density and the value diminishes with the growing quantity of binder phase.

3.3. Powder compacting

The powders were pressed in a cylindrical die with a compacting pressure of 200 MPa. The highest green density is obtained with the commercial WC-6Co powder. The green density is lowered as the binder content grows (Table 3).
Figure 2. a) Micrograph of pure Co-powder. b) Micrograph of pure Ni-powder.

Figure 3. a) Micrograph of WC-10Co. b) Micrograph of WC-20Co.

Figure 4. a) Micrograph of WC-6Co-6Ni. b) Micrograph of WC-6Co-12Ni.
3.4. Sintered hard metals

After the sintering treatment described above, the density of the sintered hard metals was determined by Arquimedes' principle, in accordance with the MPIF-95 norm (Table 4). With increasing binder phase contents lower relative densities were determined. Also, the comparison of WC-6Co-12Ni and WC-20Co indicates that Ni in the binder phase lowers the relative density.

Volumetric and linear contractions of the hard metal are compared in Table 5. Radial contraction was smaller than axial contraction, since the latter is more strongly influenced by variations of compacting pressure, temperature and duration of sintering.

Sintered alloys were studied by scanning electron microscopy, which revealed the microstructure better than light microscopy with Murakami attack. Electron microscopic studies showed that sintering of the WC-6Co and WC-10Co powders (Figure 5) led to a homogeneous distribution of the carbide particles and the Co binder phase. Diffusion between carbides and grain growth was observed. Small islands of Co are present in the WC-10Co material. EDS analysis showed only the presence of elements from the raw materials. No sign of contamination by the production process was detected (Figure 6). This applies to all compositions studied.

The microstructure of the Ni-containing samples differs from the Ni-free ones (Figure 7). A finer and more homogeneous distribution

| Table 2. Apparent density of the hard metals. |
| Composition of hard metal | Apparent density (g.cm\(^{-3}\)) |
|---------------------------|-------------------------------|
| WC-6%Co                  | 2.63 ± 0.02                  |
| WC-10%Co                 | 2.57 ± 0.04                  |
| WC-6%Co6Ni               | 2.55 ± 0.03                  |
| WC-6%Co12Ni              | 2.47 ± 0.03                  |
| WC-20%Co                 | 2.45 ± 0.02                  |

| Table 3. Green density of the compacted hard metals. |
| Composition | Green density (g.cm\(^{-3}\)) |
|-------------|-------------------------------|
| WC-6Co      | 8.02 ± 0.13                   |
| WC-10Co     | 7.80 ± 0.16                   |
| WC-6Co-6Ni  | 7.62 ± 0.19                   |
| WC-6Co-12Ni | 7.11 ± 0.18                   |
| WC-20%Co    | 7.03 ± 0.12                   |

| Table 4. Density of sintered hard metals. |
| Composition of hard metals | Density of sintered materials (g.cm\(^{-3}\)) | Theoretic density (g.cm\(^{-3}\)) | Relative density (%) |
|---------------------------|--------------------------------|------------------|-------------------|
| WC-6Co                    | 14.64 ± 0.06                  | 14.90            | 97.8 – 98.6       |
| WC-10Co                   | 14.19 ± 0.16                  | 14.60            | 96.1 – 98.3       |
| WC-6Co-6Ni                | 13.40 ± 0.21                  | 14.30            | 92.3 – 95.2       |
| WC-6Co-12Ni               | 13.05 ± 0.21                  | 13.76            | 93.3 – 96.4       |
| WC-20Co                   | 13.13 ± 0.14                  | 13.60            | 95.5 – 97.6       |

| Table 5. Volumetric and linear contraction of the hard metals. |
| Composition of hard metal | Volumetric contraction (\%) | Linear contraction (height) (%) | Linear contraction (diameter) (%) |
|---------------------------|---------------------------|-------------------------------|-------------------------------|
| WC-6Co                    | 43.6 – 48.6               | 17.2 – 19.3                   | 19.0 – 19.8                   |
| WC-10Co                   | 43.8 – 47.8               | 17.1 – 19.3                   | 19.0 – 19.8                   |
| WC-6Co-6Ni                | 43.6 – 48.7               | 17.3 – 19.5                   | 19.0 – 19.7                   |
| WC-6Co-12Ni               | 44.1 – 48.7               | 17.3 – 19.5                   | 18.9 – 19.8                   |
| WC-20Co                   | 43.8 – 48.5               | 17.3 – 19.4                   | 19.0 – 19.8                   |

Figure 5. a) WC-6Co, sintered at 1450 °C. b) WC-10Co sintered at 1420 °C.

Figure 6. EDS analysis of WC-10Co sintered at 1420 °C.
of carbides and of Ni and Co binder was found, especially in the WC-6Co-6Ni material (Figure 7a). No distinction between Co and Ni binder could be made, nor could be detected islands of Co or Ni, despite of a total binder content of 12%. Small islands of binder phase were found in WC-6Co-12Ni. Growth of carbide particle up to more than 10 μm can be observed in some parts of the specimen (Figure 7b).

The sintered WC-20Co shows islands of Co and growth of carbide particles, some of them reaching about 10 μm (Figure 8). Due to the higher binder content WC particles are completely surrounded by Co.

3.5. Electrochemical behavior

Potentiodynamic tests in H₂SO₄ were performed in order to get an overview of the electrochemical behavior of the sintered hard metals. Figure 9 compares the curves as a function of the Co-binder content. The cathodic curves are nearly identical for the three compositions studied. The same observation was made with respect to the anodic Tafel lines. Therefore the corrosion potentials of the three hard metals are similar. At higher anodic potentials WC20Co reaches a
current density plateau of about 10 mA.cm$^{-2}$. With lower Co content the current density in the anodic potential region becomes smaller. However, WC10Co showed a lower current density than WC6Co, which indicates that other parameter than the binder content might have an influence. This question is also controversially discussed in the literature. Some works report lower current densities with lower binder content$^{11}$, while others found that the binder content has no influence$^{15}$. Also, others report that the current density depends on the carbide grain size$^{15}$.

Figure 10 compares hard metals with different Ni contents. The anodic curves show a small influence of the Ni content. The anodic curves, however, are shifted to higher potentials with growing Ni content. Therefore, the corrosion potential is also shifted to higher potentials and the corrosion current density becomes smaller with growing Ni content. At higher anodic potentials current densities remain high in all examined materials. Transpassive behavior begins above approximately +1 V.

4. Conclusions

The powder metallurgical production route of WC-Co and WC-CoNi hard metals, starting from a commercial WC-6Co powder, gave satisfactory results for the analysed compositions: WC-10Co, WC-20Co, WC-6Co-6Ni and WC-6Co-12Ni. A homogeneous distribution of the added Co and Ni powders was found, showing that the mixing, milling, compacting and sintering procedures were performed with adequate parameters. No contamination with elements other than the constituents of the raw materials was detected by EDS analysis.

A comparison of sintered density and sintering temperature of the examined alloys shows that sintering temperature is the main factor which determines the density. The highest sintered density was obtained with the commercial WC-6Co powder which was sintered at the highest temperature. In the case of WC-6Co the different production process of the commercial material might also have an influence on the results. The comparison of WC-6Co-12Ni and WC-20Co indicates that Ni in the binder phase tends to lower the relative density.

Carbide grain growth was observed in all sintered materials, however, a finer distribution of the constituents, WC particles and Co-Ni binder phase, was found in the composition WC-6Co-6Ni.

In the potentiodynamic corrosion tests in sulfuric acid all materials showed a behavior described sometimes as “pseudo-passive”$^{16}$, which means that the current density in the passive range remains high due to non-adherent, non-protecting corrosion products. The Ni-containing hard metals showed a shift of the anodic curve of metal dissolution, indicating a decrease of the corrosion current density with growing Ni content in the binder.

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