A fuzzy logic based MPPT controller for wind-driven three-phase self-excited induction generators supplying DC microgrid

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Abstract

In this paper, a straightforward strategy for tracking the maximum power (MP) accessible in the wind energy conversion system (WECS) for DC microgrid is proposed. A three-phase diode bridge rectifier alongside a dc-dc converter has been utilized between the terminals of wind-driven induction generator and dc microgrid. Induction generator is being worked in self-energized mode with excitation capacitor at stator. The output current i.e. DC grid current act as a control variable to track the MP in the proposed WECS. In this manner, the proposed calculation for maximum power point tracking (MPPT) is autonomous of the machine and wind-turbine parameters. Further, a technique has been created for deciding the obligation proportion of the dc-dc converter for working the proposed system in MPPT condition utilizing wind turbine qualities, relentless state proportionate circuit of prompting generator and power balance in power converters. Circuit straightforwardness and basic control calculation are the significant points of interest of the proposed setup for supplying energy to the DC microgrid from WECS. The fruitful working of the proposed calculation for fuzzy logic based MPPT has been shown with broad exploratory results alongside the simulated values.

Keywords: DC microgrid; induction generators; maximum power point tracking (MPPT); Fuzzy Logic controller; wind power generation

Introduction

With a perspective to meet out the continuous and expanding energy demand, numerous nations have begun the procedure of liberalization of their electric systems, opening access to transmission and conveyance networks for associating little or medium scale generators. These distributed generated systems reduce the energy misfortune and base expense for transmission systems, since DGs are associated near the load focuses. Moreover, renewable energy sources, for example, wind and sunlight based are broadly conveyed in distributed generated systems, which further helps for the contamination free environment. It is realized that the electrical output from DGs utilizing renewable energy sources is of variable voltage dc or ac amounts. In the present day situation most of loads, for example, LED lighting, PC burdens and variable rate drives request dc as the source. Nonappearance of reactive power, no
symphonic issues, less power change stages and simple to interface vitality stockpiling gadgets, specifically, battery, module electric vehicles and super capacitors are alluring alternatives for dc microgrid with DGs. Lasting Magnet Alternators (PMAs) and Self-Excited Induction Generators (SEIGs) are the reasonable decisions for such little scale wind generators utilized in dc microgrids. Tough rotor development, nonattendance of slip rings, brushes and a different dc sources for excitation and simplicity of support are the fundamental explanations behind inclining toward actuation machines, with renewable vitality frameworks For separating maximum power (MP) accessible from the wind, the wind turbine (WT) must be worked to convey the greatest mechanical output power for a given wind speed as appeared in figure 1. The numerical demonstrating of WT attributes given in Fig.1From this figure, it could be watched that the rotor speed of the wind-generator system must be permitted to differ generally to extract the most extreme conceivable power accessible in the wind. Different power electronic topologies have been proposed in the writing for this motivation behind supplying energy to the AC network. In this way, the greater part of the examination directed so far has focused on ac network operations. With respect to network, just not very many articles are in the current writing.

Proposed system for wind-driven seig supplying DC microgrid

In this paper, induction generator is proposed to work in self-energized mode so that the WT system can be worked over a wide speed range for extricating MP accessible in the wind. The reactive power necessity of the generator is supplied locally through capacitor banks. Utilizing DBR at the generator terminals, helps in diminishing the responsive force load on the excitation capacitor banks following the removal element at the uncontrolled rectifier is solidarity. In perspective of these, DBR has been decided for making the proposed system basic in both setup and control. Further, to have the basic control procedure for MPPT in the proposed dc microgrid application, a DC-DC converter is proposed to be utilized at the matrix side. The general schematic of the proposed WECS supplying the DC microgrid is appeared in figure 2.

Fig. 1. Wind turbine output power curve for various wind velocities

A couple of analysts have depicted the execution of the DC microgrid system with various voltage levels and reasonable force electronic interface, taking into account proficiency, voltage drop, warm breaking point, expense and wellbeing issues. Consequently, in this paper 120V DC has been considered at the grid side of the proposed system. Further, financially accessible inverters of (10-20) kVA appraisals work with 120 V DC. Subsequently, this voltage level is most appropriate for such industrially accessible inverters alongside energy stockpiling systems in particular, battery banks.
In this way, the controller detects this DC system current through a present sensor and contrasts it and the past worth. The outcome chooses the change (increase or decrement) in the obligation proportion of the DC-DC converter. It is to be noticed that the rotor speed of the WT system is changed for separating MP accessible in the wind according to the qualities given in figure 1 for a given wind speed by conforming the obligation proportion of the DC-DC converter and ceaselessly observing the DC lattice current alone.

Analysis of the proposed system

To show the efficiency of the proposed MPPT control technique, the system appeared in figure 2 has been broke down both in unfaltering state and element conditions.

A) Steady-State analysis

For the system comprising of the SEIG supplying energy to the DC microgrid through power converters, the unfaltering state examination has been separated into two sections. Firstly, the execution of the generator has been gotten for working the wind-generator system at MPPT condition for a given wind speed according to figure 1. At that point, utilizing these execution amounts, to be specific, voltage and electrical power output at the generator terminal, the execution of the power electronic converter supplying energy to the DC microgrid has been acquired.

Analysis of WT-SEIG: For doing the consistent state investigation of SEIG, ordinary identical circuit of the induction machine is adjusted to incorporate the variable nature of the working frequency. For doing the consistent state examination of WT-SEIG, the heap should be fittingly reflected over the generator terminals. In this way, by expecting a consistent dc current at DBR, the proportional burden at the generator terminals can be spoken to as an immaculate resistive load and its quality is given by,

\[
R = \frac{3V_p^2}{P_g} \tag{1}
\]

Along these lines, the resultant comparable circuit utilized for the consistent state examination of the WT - SEIG framework proposed in this work. In this figure, \(a = \text{p.u. recurrence} = f/f_r\) and \(b = \text{p.u. speed} = N_r/N_s\). At that point, the working slip of the machine is \(s = (a - b)/a\). It is to be noticed that as the wind speed changes, the impelled emf (E) in the SEIG and consequently the charging reactance (Xm)
change with the level of immersion. Further, for this consistent state examination, all the machine parameters are thought to be known, aside from Xm and center misfortune in machine is ignored. For the circuit, circle condition can be composed as, $IZ = 0$ (2). All reactance correspond to rated frequency. Where,

$$Z = \left[ \frac{R}{a} \right]^2 \left[ \frac{jX}{a^2} \right] + \left[ \frac{R_k}{a} + jX_k \right]^2 \left[ \frac{Z_{m}}{a-b} \right]^2$$

Since under consistent state condition I not equal to zero, it takes after from (2) that $Z = 0$. For getting the working point, in particular, a and Xm for the predefined estimation of b to fulfill the above condition, some improvement method has been utilized. In this way, in the proposed plan, to get obscure parameters, to be specific, a and Xm for the predefined estimation of b, the goal capacity, $f(a, Xm) = |Z|$ is minimized to zero utilizing GA strategy. After touching base at the working point, for every estimation of Xm, the comparing affected emf, $E$ is resolved from an information of the charge normal for the machine. At that point, the execution of the SEIG is processed from the expressions got from the identical circuit appeared and they are condensed as takes after

$$V_P = \left[ \frac{R_k^2 + X_k^2}{j(R_k/a) + R_L Y} + (X_k - X_L)^2 \right]^{1/2}$$

$$I_{e} = \frac{V_P}{R} \quad \text{and} \quad P_e = 3V_P I_{R}$$

Where, $R_L = \frac{RX_L^2}{\alpha^2 R^2 + X_L^2}$ and

$$X_L = \frac{RX_L^2}{\alpha^2 R^2 + X_L^2}$$

The mechanical info energy to the rotor of the generator can be composed as,

$$P_m = -3I_2^2 R_2 \left[ \frac{b}{a-b} \right]$$

Where, $I_2 = \frac{E}{[(R_2/a-b)^2 + X_L^2]^{1/2}}$

It can be seen from (1), that the estimations of $V_P$ and $P_e$ are required for the count of $R$ for any given working conditions. For showing the viability of the proposed strategy for dissecting WT-SEIG system utilizing the stream graph of figure 4, a 3-phase, 4-post, 230 V, 50 Hz (1 p.u. frequency), 3.7 kW, delta-associated squirrel-confine prompting machine has been considered. The deliberate parameters of the generator are $R_1 = 1.30 \Omega$, $R_2 = 1.75 \Omega$, $X_1 = X_2 = 2.6 \Omega$. The ($E/a$) versus Xm trademark acquired tentatively at the appraised frequency of 50 Hz for this generator is communicated as takes after:

$$E/a = -296.35 \times 10^{-10} X_m^6 + 759.97 \times 10^{-3} X_m^5 + 784.84 \times 10^{-5} X_m^4 + 40.75 \times 10^{-3} X_m^3 - 111.07 \times 10^{-2} X_m^2 + 12.94 X_m + 245.92$$

To suit the rating of 3.7 kW actuation generator considered in this study, different parameters of WT model have been picked. The resultant power bend of the WT with the picked parameters, for this study is given in figure 1. At that point, utilizing the methodology for this wind speed, relentless state execution of the WT-SEIG system has been foreordained.

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2) Analysis of power converter: Having assessed the voltage furthermore, electrical power output at the generator terminals for working the WT-SEIG at MPPT condition by receiving the system created in the before sub-segment, it is of interest to build up the system for anticipating the execution of the power electronic controller interfaced with the proposed system.

\[ V_{\text{DBR}} = \frac{3\sqrt{2}V_s}{\pi} - 2V_{\text{D}(\text{ON})} \]  
\[ (9) \]

For the known estimation of dc matrix voltage, \( V_{\text{dc}} \) and inductor resistance (\( R_{\text{ind}} \)), the voltage over the freewheeling diode, \( V_{\text{FD}} \) is given by

\[ V_{\text{FD}} = V_{\text{dc}} + R_{\text{ind}} P_{\text{dc}} \]  
\[ (10) \]

Where, the DC grid current

\[ I_{\text{dc}} = \frac{P_{\text{dc}}}{V_{\text{dc}}} \]  
\[ (11) \]

At that point, the obligation proportion of the buck converter, \( \delta \) can be figured utilizing

\[ \delta = \frac{V_{\text{FD}}}{V_{\text{DBR}} - V_{\text{C}(\text{ON})}} \]  
\[ (12) \]

Where, \( V_{\text{C(ON)}} \) is the on-state voltage over the IGBT. At that point, the electrical power yield of the generator, \( P_e \), DC network force, \( P_{\text{dc}} \) and aggregate power misfortune in the converter, \( P_{\text{TL}} \) can be connected as,

\[ P_e = P_{\text{dc}} + P_{\text{TL}} \]  
\[ (13) \]

From (9-13), it can be seen that the estimation of \( I_a, P_{\text{dc}} \) and \( P_{\text{TL}} \) are required for the figuring of obligation proportion. Nonetheless, in the start of the fate procedure, these qualities are obscure. Subsequently, a strategy has been produced taking into account the power balance condition given in (13) and other known parameters.

B. Simulation study

The proposed arrangement of figure 2 has additionally been recreated utilizing Sim Power Systems tool stash as a part of MATLAB programming. The same machine considered in the before area alongside different parameters has been utilized for the recreation. Tentatively acquired polarization trademark (current versus voltage) of the affectionation machine at appraised recurrence of 50 Hz with a steady speed of 1500 rpm has been utilized as a part of the non-concurrent machine model accessible in the MATLAB and these qualities are given in Appendix C. A 3-stage DBR alongside the dc-dc converter has been assembled utilizing the segments accessible as a part of the MATLAB and this has been associated in the middle of the generator yield terminals and DC framework of 120 V. A WT model accessible in the MATLAB has been utilized to drive the affectionation generator. WT model gives the mechanical torque as yield for a given wind speed.
Using Incremental Conductance method

Fig. 3. Dynamic response of the proposed WECS for step change in wind velocity

To suit the rating of 3.7 kW impelling generator considered in this study, different parameters of WT model have been picked. The resultant force bend of the WT with the picked parameters, for this study is given in figure 1. The calculation for MPPT depicted in the past area has been composed utilizing the installed MATLAB capacity. This capacity consistently faculties the DC framework current and properly conforms the obligation proportion of the DC-DC converter for any given wind speed to concentrate MP accessible in the wind according to the attributes given in figure 1.

Steady-state execution: To learn the fruitful working of the proposed MPPT controller, reproduction has been done for the given wind speed and the unaltering state execution is given in table 1 alongside the anticipated qualities. It can be seen from this table the controller modifies the obligation proportion of the DC-DC converter for following the MP accessible in the wind according to the rationale depicted in Section II. For instance, alluding to figure 1, for separating most extreme conceivable estimation of mechanical force yield of 4.19 kW at 12 m/s wind speed, WT ought to be made to pivot at a rotor pace of 1500 rpm. For accomplishing this, shut circle controller constantly screens the dc grid present according to the rationale depicted in Section II and changes the obligation proportion to 41% for this 12 m/s wind speed.
Dynamic performance: To approve the agreeable element execution of the proposed system with the MPPT controller, reproduction has additionally been done for step change in wind speed. In this reproduction, wind speed has been changed from 8 m/s to 10 m/s and back. Every interim was kept up for 0.4 s. The reenacted waveforms of rotor pace (Nr), mechanical torque of the WT (Tm), electromagnetic torque (Te) of generator, stator output power (Pe), stator voltage (vS), stator current (iS), capacitor current (iC) and rectifier input current (iR) alongside the dc grid current (Idc) and DC system power (Pdc) have been watched for the progression change in wind speed (Vw) and they are displayed in matlab/simulink. The Dynamic response of the proposed WECS for step change in wind velocity by using fuzzy logic controller and its change in waveforms are shown below:

Using Fuzzy Logic Controller

From figures 3 and 4, we can observe Variation in Total Hormonic Distortion only in the sense of Rectifier input Current and Capacitor Current. Hence, their variation in THD are shown with their respective values as shown in the figure 5,
IR THD Under Incremental Conductance = 29.56% 

IR THD Under Fuzzy Controller = 11.40%

Ic THD Under Incremental Conductance = 22.72% 

Ic THD Under Fuzzy Controller = 10.32%

Fig. 5. Variation in THD regarding Incremental conductance and Fuzzy controller of Ir and Ic

Conclusion
As of late, numerous nations energize the customers for creating electrical power from exchange energy sources, which prompts the arrangement of microgrids. In such manner, 120 V DC microgrid systems draw substantially more consideration for low power applications supplied from renewable vitality sources. Especially, this voltage reach is most appropriate for family unit machines, home inverters and capacity frameworks. A straightforward circuit setup and control calculation is crucial for simple operation and upkeep of such DC microgrid frameworks by buyers. Subsequently, this paper has displayed a straightforward MPPT calculation and circuit topology for dc microgrid applications supplied from a little scale WECS. The rationale for diminishing the obligation proportion with expanding estimation of dc network current for the MPPT has been appeared with illustration. Without the requirement for the estimation of wind speed or turbine rotor speed i.e., with no mechanical sensors, the MPPT calculation proposed in this paper is easy to actualize. Further, the whole system has been created utilizing MATLAB/Simulink environment along with the WT model for surveying unfaltering state and dynamic execution of proposed WECS. Different foreordained and reenacted results outfitted in this paper exhibit best possible following of the MP point utilizing proposed single variable detecting calculation.

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