Multiple Criteria Method for Designing Distillation Sequence for Sharp Separation

A.G. Kamel¹, M. Kaoud² and S.M. Aly³

¹,²,³ Department of Chemical and Refining Engineering, Suez University, Egypt.
ORCID: 0000-0002-4320-3778 (Kaoud)

Abstract
In almost every chemical process, distillation depending on sequences of separation. These systems of separation are utilized for preparation of feed, for the separation of products and finishing as well as for the waste treatment. This paper presents Multiple Criteria Approach for the synthesis of flow sheets with simple, sharp separator splitting. This approach based on quantification three heuristic rules will be used for selection of optimum separation sequence. The suggested procedure combines the values of the difference in normal boiling points of the components and the estimate separation mass load coefficients and relative volatility. The proposed method used to deal with previously reported literary problems produced optimal solutions which are better or at least similar to the optimum flow sheet with the indicated values, and overcame some obstacles of using the evolutionary, heuristic and mathematical programming. The proposed algorithm can be implemented by hand calculation and characterized by its simplicity.

Keywords: Process synthesis; sharp separation; multiple criteria separation.

1. INTRODUCTION
One of the most important subjects in process synthesis has been the synthesis of optimum sequences of separation. Separation processes represent a significant portion of the operating expenses and the chemical plant's total capital investment, and a great deal of interest has been generated in developing systematic approaches that will select optimum sequences of separation. The development of such systematic approaches has been developed in developing systematic approaches that will select optimum sequences of separation. In the chemical unit design of sharp separation sequence is considered one of the most examined problems.

For the synthesis of sharp separation sequence. Several of published works that have dealt with the synthesis, the main papers are reviewed in this area in Hendry et al. [1], Hlavacked [2], Westerberg [3], Stephanopoulos [4], Nishida et al. [5], Umeda [6], Westerberger [7] and Floquet et al. [8]. These authors proposed the following method, for resolving sharp separator sequence synthesis which could be categorized into (3) key categories:-

Algorithmic methods attempt to solve and optimize the problem through the use of algorithms developed in the field of discrete mathematical programming, the major procedures used in the literature are the following:-

1- Dynamic programming (Hendry and Hughes [9]).
2- Branch and bound type method (Westerberg and Stephanopoulos [10]; Rodrigo and Seader [11]).
3- Mixed integer linear programming methods (Andrecovich and Westerberg [12]; Floquet et al [13]).

Evolutionary strategies attempt to identify the better scheme of separation by a sequence of evolutionary enhancements. The evolutionary approach depends on both the initial flow sheet and the evolutionary strategies, which can be categorized into (2) key categories Heuristic strategy (Nath and Motard [14]; Lu and Motard [15]; Breadth first or depth first strategies (Stephanopoulos and Westerberg [16]; Seader and Westerberg [17]). Heuristic methods use rules of thumb resulting from long experience (Heaven [18]; Powers [19]; Nishimura et Hiraizumi [20]; Thompson and King [21]; Rudd et al. [22]; Nifda et al. [23]; Dougles [24]). In this paper a synthesis approach suggested for sharp separation sequences combining the quantification three rules, difference in normal boiling point of components and relative volatility and the values of estimate separation mass load coefficient in multiple criteria decision method. The effectiveness of this synthesis approach is illustrated using two problems.

2. PROBLEM STATEMENT
In the synthesis of chemical units. The design of sharp separation sequences is consider one of the most studied problems it could be stated as follows:

In the context a single multicomponent feed mixture with known conditions (i.e. flow rate, composition, pressure and temperature) synthesize a process which can separate the wanted products from the feed at minimum annual cost (including the sum of the plant's annual operating costs and investment costs).
3. SOLUTION METHOD

The suggested methods for resolving synthesis of sharp separator sequence can be categorized into (3) key categories:

- Evolutionary strategies, heuristic methods and Algorithmic methods
- The procedure described below is in the heuristic range and allows flow sheet structures to be easily found which are also nearly ideal solutions.

3.1 Quantification of the Rules

The synthesis algorithm is based on the application of expert rules, well suited for economical design problem. From an extensive complication of three rules of thumb have been retained:

I. If the difference \( \Delta T_b \) of the normal boiling point temperatures between two adjacent key components is big then split between these two components.

II. Favor the separation at the point where the relative volatility \( \alpha \), j of two adjacent key components is the most important.

III. When the value of the estimated mass load (EML) coefficient of the spilt is small, perform this spilt.

**Rule 1:**

\[
\mu^1 = \begin{cases} 
0 & \text{if } \Delta T_b \leq T_{\text{min}} \\
\frac{\Delta T_b - T_{\text{min}}}{T_{\text{max}} - T_{\text{min}}} & \text{if } T_{\text{min}} < \Delta T_b < T_{\text{max}} \\
1 & \text{if } \Delta T_b \geq T_{\text{max}} 
\end{cases}
\]

With \( T_{\text{min}} \) (\( \Delta T_b \) and \( T_{\text{max}} = \sum_{n=1}^{n-1} \Delta T_b / n-1 \))

**Rule 2:**

\[
\mu^2 = \begin{cases} 
0 & \text{if } \alpha_{i,j} \leq 1.1 \\
(\alpha_{i,j} - 1.1) / 0.9 & \text{if } 1.1 < \alpha_{i,j} \leq 2 \\
1 & \text{if } \alpha_{i,j} > 2 
\end{cases}
\]

**Rule 3:**

\[
\mu^3 = \begin{cases} 
0 & \text{if } \text{EML} < \text{EML}_{\text{min}} \\
\frac{\text{EML}_{\text{max}} - \text{EML}}{\text{EML}_{\text{max}} - \text{EML}_{\text{min}}} & \text{if } \text{EML}_{\text{min}} \leq \text{EML} \leq \text{EML}_{\text{max}} \\
1 & \text{if } \text{EML} < \text{EML}_{\text{max}} 
\end{cases}
\]

The value of EML coefficient for a spilt is bounded; Table 2 showing these two boundaries for some splits. \( \text{EML}_{\text{min}} \leq \text{EML} \leq \text{EML}_{\text{max}} \)

**Table 2:** Bounds on Estimated Mass Load (EML) coefficients for N=5 components

| Splits | EML | EML min | EML max |
|--------|-----|---------|---------|
| A/BCDE | O+11/6E+5/2Xc+5/2Xo+11/6Xe | 0 | 5/2 |
| AB/CDE | Xa+Xb+3/2Xc+2Xd+3/2Xe | 1 | 2 |
| ADC/DE | 3/2Xa+2Xb+5/2Xc+Xo+Xe | 1 | 2 |
| ABCD/E | 11/6Xa+5/2Xb+5/2Xc+11/6Xo+0 | 0 | 5/2 |
| A/BCD or B/CDE | O+3/2Xb+2Xc+3/2Xo | 0 | 2 |
| AB/CD or BC/DE | Xa+Xb+Xc+Xo | 1 | 1 |
| ABC/D or BCD/E | 3/2Xa+2Xb+3Xc+4 | 0 | 2 |
| A/BC | O+Xa+Xc | 0 | 1 |
| AB/C | Xa+Xb+4O | 0 | 1 |
| A/B or B/C or C/D or D/E | O | 0 | 0 |
3.2. Multiple criteria decision method

The multikriteria problem in its general form for a finite set A of n alternatives and certain system of m assessment criteria f_i, can be defined as following: (Diakoulaki, et.al. (26))

Max \{ f_j(a), f_2(a), ..., f_m(a) \} \ a \in A \quad (4)

We can define the membership function x_i. For each criterion f_j of this multikriteria problem by layout the values of f_j to the interval [0,1]. This conversion is based on the idea of the perfect point. Thus, the value x_{ij} below, expresses the degree to which the substitute is near to the ideal value f^*_j whenever the better performance in criterion j, and far from the ideal-value f^*_j, which is the worse performance in criterion j both f^*_j and f^*_j, are actualized by the least one of the substitutes under consideration.

x_{ij} = [f_j(a) - f^*_j] / [f^*_j - f^*_j] \quad (5)

In this way the initial evaluation matrix is transformed into a matrix of relative scores with generic dimension x_{ij}. By examining the jth criterion in isolation, we generate a vector x_j showing the scores of all n substitutes considered.

x_j = (x_j(1), x_j(2), ..., x_j(n)) \quad (6)

The standard deviation \sigma_j, which determines the contrast intensity of the corresponding criterion, is used for characterized each vector x_j. The standard deviation of x_j is also an indicator of its importance for decision-making. Instead of use of standard deviation it is apparent that any other of the divergency in scores could be used

\sigma x = \sqrt{\frac{n \sum_{i=1}^{n} (x_i - \bar{x})^2}{n-1}} \quad (7)

Where \bar{x} the mean variable of x and n is number of variable

The linear correlation coefficient R_{IK} between x_i and x_k is calculated

R_{IK} = \frac{n \sum x_i x_k - \sum x_i \sum x_k}{\sqrt{(n \sum x_i - (\sum x_i)^2)(n \sum x_k - (\sum x_k)^2)}} \quad (8)

The amount of C_j information emitted by the jth criterion can be identified by composing measures that quantify the two notions by using the following formula of multiplicative aggregation:

C_j = \sigma_j \sum_{k=1}^{m} (1 - r_{jk}) \quad (9)

As per to the former analysis the higher the C_j value, the greater the amount of information given by the corresponding criterion and its relative relevance to the decision-making process is increased. Objective weights result from the normalization of those values to the unit in accordance with the equation below.

W_j = C_j / \sum_{k=1}^{m} C_k \quad (10)

Construct a multi-criteria ranking of the firms examined according to the following aggregation formula:

D_i = \sum_{j=1}^{m} W_j \cdot x_{ij} \quad (11)

Where:

D_i = the multicriteria score of firm i,

x_{ij} = the score of firm i under criterion j,

w_j = the weight criterion j

The strategy suggested is based on an assessment of the validity of each rule for every possible split. After the quantification step, the values of \mu_1, \mu_2 and \mu_3 for each split I are calculated and then multiple criteria decision method are applied.

Summarized of The key steps in the strategy showing in the following Fig.1

![Fig.1 Main steps of the strategy](image)

Quantification of the 3 rules

Conjunction of the rules

Multiple criteria decision method

Choice of the split

For each split of the separation task
4. CASES STUDY

Example 1: Separation of a 4 component mixture

Consider the separation of the mixture of four light hydrocarbons into pure components by ordinary distillation Floudas And Anastasiadis [27] Studied this case the problem specification are given in Table 1

Table 3. Data of The problem specification

| Component | Mole fraction | Boiling point temperature (k) | Normal boiling point difference (k) | Relative Volatility (α) |
|-----------|---------------|-------------------------------|------------------------------------|-------------------------|
| A:1-Butane | 0.158         | 261.3                         | 11.4                               | 1.33                    |
| B:N-Butane | 0.263         | 272.7                         | 28.3                               | 2.40                    |
| C:I-Pentane | 0.210        | 300.8                         | 8.20                               | 1.52                    |
| D:N-Pentane | 0.369         | 309                           |                                     |                         |

The first step is to determine the boiling point difference and normalized and hence the corresponding estimated mass load values for every split by using equation 1, 2 and 3 Summarized of the calculations is showing in

Table 4. Summary of result by quantification of rules

| Split | Boiling point Difference (Δ T) | Relative volatility (α) | Estimated mass load (EML) | Normalize boiling point difference (µ1) | Normalize relative volatility (µ2) | Normalize Estimated mass load (µ3) |
|-------|--------------------------------|-------------------------|---------------------------|----------------------------------------|----------------------------------|-----------------------------------|
| A/BCD | 11.4                           | 1.33                    | 1.368                     | 0.159                                  | 0.178                            | 0.059395                          |
| AB/CD | 28.3                           | 2.4                     | 1                         | 1                                      | 1                                | 0.026755                          |
| ABC/D | 8.2                            | 1.52                    | 1.078                     | 0                                      | 0.178                            | 0.022197                          |

In the second step calculate the standard deviation for each parameter by using equation (7) is summary of the calculations is shown in table 3

Table 5. Summary of result for standard deviation

| Normalize boiling point difference (µ1) | A/BCD | AB/CD | ABC/D | Standard deviation (σ) |
|----------------------------------------|------|------|-------|------------------------|
| 0.159                                  | 0.53764 |
| Normalize relative volatility (µ2)     | 0    | 1    | 0.178 | 0.5334                 |
| Normalize Estimated mass load (µ3)     | 0.316| 1    | 0.461 | 0.360417               |

Then calculate the correlation $R_{ik}$ between each two normalization variables by using equation (8).The values of $R_{ik}$ are as follows: $R_{12}= 0.95$, $R_{13}= 0.939$ and $R_{23}= 0.999$.

Applying equation (9) to get the quantity of information $C_j$ emitted by the $j_n$ criterion

Table 6. Summary of the results for standard deviation and $C_j$

| split | Standard deviation (σ) | $C_j$ |
|-------|------------------------|-------|
| A/BCD | 0.53764                | 0.059395 |
| AB/CD | 0.5334                 | 0.026755 |
| ABC/D | 0.36041                | 0.022197 |
Applying equation (10) to obtain the object weight of each variable. The result as the following $W_1 = 0.548317$, $W_2 = 0.246866$ and $W_3 = 0.204817$.

For obtaining decision maker, $D$, (or the multicriteria-score of firm), the following table is constructed:

**Table 7. Evaluation of decision maker**

| Solution   | $W_1 \cdot \mu_1$ | $W_2 \cdot \mu_2$ | $W_3 \cdot \mu_3$ | multi-criteria-score (D) | Ranking of firm |
|------------|-------------------|-------------------|-------------------|--------------------------|-----------------|
| A/BCD      | 0.087182          | 0                 | 0.064722          | 0.151904                 | 2               |
| AB/CD      | 0.548317          | 0.246866          | 0.204817          | 1                        | 1               |
| ABC/D      | 0                 | 0.043942          | 0.09442           | 0.138363                 | 3               |

By comparing the values of multicriteria-score (D) for all the possible split, split AB/CD is chosen for it yield the highest $D$ value that is 1.

The resulting sequence is **AB/CD, A/B and C/D**.

The cost of all possible towers is calculated by shortcut method and is shown in the following table 8

**Table 8**

| Column | Cost*10^5($/yr.) | Column | Cost*10^5($/yr.) |
|--------|------------------|--------|------------------|
| A/BCD  | 7.200            | C/D    | 6.922            |
| AB/CD  | 5.869            | B/C    | 2.099            |
| ABC/D  | 10.801           | A/B    | 3.345            |
| B/CD   | 4.670            | A/BC   | 6.400            |
| BC/D   | 9.728            | AB/C   | 3.778            |

The total cost of the possible separation sequences schemes as shown in table is calculated by shortcut method, and it was found that the optimum sequence is consistent with the results of proposed method.

**Table 9. The total cost of possible separation sequences schemes.**

| NO. | Separation       | Cost*10^5($/yr.) |
|-----|------------------|------------------|
| 1   | AB/CD, A/B, C/D  | 1.548            |
| 2   | ABC/D, AB/C, A/B | 1.792            |
| 3   | A/BCD, B/CD, C/D | 1.879            |
| 4   | A/BCD, BC/D, B/C | 1.903            |
| 5   | ABC/D, A/BC, B/C | 1.931            |

![Optimum sequence for four-component mixture separation](image-url)
Example 2:
The problem data are shown in table studied by Heaven [28] for separation the mixture of five light hydrocarbons into pure components by ordinary distillation

### Table 10. Data for example 2:

| Component   | Mole fraction | Boiling point Temp (k) | Normal boiling Pt difference (k) | Relative volatility α |
|-------------|---------------|------------------------|----------------------------------|-----------------------|
| A: Propane  | 0.05          | 231.1                  | 30.2                             | 2.00                  |
| B: 1-Butane | 0.15          | 261.3                  | 11.4                             | 1.33                  |
| C: N-Butane | 0.25          | 272.7                  |                                  |                       |
| D: 1-Pentane| 0.2           | 300.8                  | 28.1                             | 2.40                  |
| E: N-Pentane| 0.35          | 309.0                  | 8.2                              | 1.52                  |

The Summary of quantification rule is shown in the Table 11:

| Split       | Boiling point Difference (Δ T<sub>b</sub>) | Relative volatility (α) | Estimated mass load (EML) | Normalize boiling point difference (µ<sub>1</sub>) | Normalize relative volatility (µ<sub>2</sub>) | Normalize Estimated mass load (µ<sub>3</sub>) |
|-------------|-------------------------------------------|-------------------------|---------------------------|--------------------------------------------------|------------------------------------------------|-----------------------------------------------|
| A/BCDE      | 30.2                                      | 2                       | 2.042                     | 1                                                | 1                                              | 0.1832                                        |
| AB/CD       | 11.4                                      | 1.33                    | 1.5                       | 0.145                                            | 0                                              | 0.5                                           |
| ABC/DE      | 28.1                                      | 2.40                    | 1.3                       | 0.904                                            | 1                                              | 0.7                                           |
| ABCD/E      | 8.2                                       | 1.52                    | 1.458                     | 0                                                | 0.178                                          | 0.416                                         |

The following table is summarized standard the calculation of standard deviation (σ) by equation (7) and amount of information (C<sub>j</sub>) as shown in table 12:

|                                  | A/BCDE | AB/CD | AB/CD | AB/CD | AB/CD |
|----------------------------------|--------|-------|-------|-------|-------|
| Normalize boiling point difference (µ<sub>1</sub>) | 1      | 0.145 | 0.904 | 0     | 0.512718 |
| Normalize relative volatility (µ<sub>2</sub>) | 1      | 0     | 1     | 0.178 | 0.530962 |
| Normalize Estimated mass load (µ<sub>3</sub>) | 0.1832 | 0.5   | 0.7   | 0.416 | 0.213961 |

The values of R<sub>ik</sub> are as follows: R<sub>12</sub>= 0.965, R<sub>13</sub>= -0.1007 and R<sub>23</sub>= -0.06577
And then C1 =0.582167, C2 = 0.584338 and C3 = 0.46354.
And then W1= 0.357148, W2 =0.35848 and W3= 0.284373

For obtain decision - maker, D, (or the multi-criteria-score of firm), the following table is constructed.

### Table 13: Evaluation of decision maker

| Solutions | W1, µ1 | W2, µ2 | W3, µ3 | multi-criteria-score (D) | ranking of firm |
|-----------|--------|--------|--------|--------------------------|-----------------|
| A/BCD     | 0.357148 | 0.35848 | 0.052097 | 0.767724 | 2 |
| AB/CD     | 0.051786 | 0      | 0.142186 | 0.193973 | 3 |
| ABC/DE    | 0.322861 | 0.35848 | 0.199061 | 0.880402 | 1 |
| ABCD/E    | 0      | 0.063809 | 0.118299 | 0.182108 | 4 |

By comparing the values of multicriteria-score (D) for all the possible split, split ABC/D is chosen for it yield the highest D value that is 1.
The resulting sequence is ABC/D

Summary of results in table 14:

| split   | Δ Tb | α  | EML | µ1 | µ2 | µ3 |
|---------|------|----|-----|----|----|----|
| A/BC    | 30.2 | 2  | 0.4 | 1  | 1  | 0.6 |
| AB/C    | 11.4 | 1.33| 0.2 | 0  | 0  | 0.8 |

Table 15 Summary of result for standard deviation

| Normalize boiling point difference (µ1) | A/BC | A/BC | Standard deviation (σ) |
|----------------------------------------|------|------|------------------------|
| Normalize relative volatility (µ2)      | 1    | 0    | 0.707107               |
| Normalize Estimated mass load (µ3)      | 0.6  | 0.8  | 0.141421               |

R12 = 1  R13 = -1  R23 = -1
and then
C1 = 1.414214,  C2 = 1.414214 and so  C3 = 0.565685
and then
W1 = 0.416667,  W2 = 0.416667 and  W3 = 0.204817

For obtaining decision - maker, D, (or the multi-criteria-score of firm), the following table is constructed:

Table 16: Evaluation of decision maker

| Solutions | W1.X1 | W2.X2 | W3.X3 | multi-criteria-score (D) | ranking of firm |
|-----------|-------|-------|-------|--------------------------|-----------------|
| A/BC      | 0.416667 | 0.416667 | 0.1 | 0.833333 | 1 |
| AB/C      | 0      | 0     | 0.133333 | 0.133333 | 2 |

Comparing the values of multicriteria score (D) for all the possible split, split A/BC is chosen for it yield the highest D value that is 1.

The resulting sequence is ABC/DE, A/BC, B/C and D/E

The total cost of possible separation sequence schemes in table 17

| NO. | Separation | Cost*10^6($/yr) |
|-----|------------|-----------------|
| 1   | ABC/DE,D/E,A/BC,BC | 2.087 |
| 2   | ABC/DE,D/E,AB/C,A/B | 2.329 |
| 3   | AB/CDE,A/B,C/DE,D/E | 2.432 |
| 4   | AB/CDE,A/B,CD,E/C/D | 2.758 |
| 5   | ABCD/E,A/BCD,B/C,D/C/E | 2.778 |
| 6   | ABCD/E,ABC,D/A/BC,B/C | 2.846 |
| 7   | ABCD/E,AB/CD,A/B,C/D | 2.956 |
| 8   | ABCD/E,A/BCD,B/CD,C/D | 3.056 |
| 9   | ABCD/E,ABC/CD,AB/C,A/B | 3.088 |
| 10  | A/BCDE,BC/DE,B/C,D/E | 5.393 |
| 11  | A/BCDE,BCD/E,B/C,D/C | 5.554 |
| 12  | A/BCDE,B/CD,E,CLDE,D/E | 5.692 |
| 13  | A/BCDE,B/CD,E,CD/E,C/D | 5.712 |
| 14  | A/BCDE,B/CD,E,B/CD,C/D | 5.910 |

Fig.3 Optimum sequence for five-component mixture separation

The consequence of our approach is comparison with the earlier technique depending on the number of sequences developed (Nsd) and the unique search factor (F), which is the ratio of the number of unique subproblems analyzed and the number of unique subproblems. The greater the F value, the lower efficient the search:

| Method                          | Nsd | F (%) |
|--------------------------------|-----|-------|
| HEAVEN(1969)                    | 14  | 100   |
| RATHORE et al.(1974a,b)         | 14  | 100   |
| RODRIGO and SEADER(1975)        | 11  | 100   |
| GOMEZ and SEADER (1981)         | 1   | 65    |
| NATH and MOTARD (1983)          | 1   | 20    |
| NADGIR and LIU (1985)           | 1   | 20    |
| GOMEZ and SEADER (1985)         | 1   | 20    |
| Y.Y. RAWASH (2002)              | 1   | 20    |

Where Nsd is the number of sequence developed
4. CONCLUSION

Multiple criteria decision method has been suggested for synthesis sharp separation sequences by quantification of the three rules. The proposed algorithm method is characterized by its simplicity and can be implemented by hand calculation when applied for problems which had been mentioned earlier in literature yielded optimum solutions which are consistent with the reported values and overcoming the barriers of using heuristic, evolutionary and mathematical programming.

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