Optimal Synergy between Photovoltaic Panels and Hydrogen Fuel Cells for Green Power Supply of a Green Building—A Case Study

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Abstract: Alternative energy resources have a significant function in the performance and decarbonization of power engendering schemes in the building application domain. Additionally, “green buildings” play a special role in reducing energy consumption and minimizing CO₂ emissions in the building sector. This research article analyzes the performance of alternative primary energy sources (sun and hydrogen) integrated into a hybrid photovoltaic panel/fuel cell system, and their optimal synergy to provide green energy for a green building. The study addresses the future hydrogen-based economy, which involves the supply of hydrogen as the fuel needed to provide fuel cell energy through a power distribution infrastructure. The objective of this research is to use fuel cells in this field and to investigate their use as a green building energy supply through a hybrid electricity generation system, which also uses photovoltaic panels to convert solar energy. The fuel cell hydrogen is supplied through a distribution network in which hydrogen production is outsourced and independent of the power generation system. The case study creates virtual operating conditions for this type of hybrid energy system and simulates its operation over a one-year period. The goal is to demonstrate the role and utility of fuel cells in virtual conditions by analyzing energy and economic performance indicators, as well as carbon dioxide emissions. The case study analyzes the optimal synergy between photovoltaic panels and fuel cells for the power supply of a green building. In the simulation, an optimally configured hybrid system supplies 100% of the energy to the green building while generating carbon dioxide emissions equal to 11.72% of the average value calculated for a conventional energy system providing similar energy to a standard residential building. Photovoltaic panels account for 32% of the required annual electricity production, and the fuel cells generate 68% of the total annual energy output of the system.

Keywords: fuel cell; green building; hybrid energy system; hydrogen energy; optimal synergy; photovoltaic panel; power supply; solar energy

1. Introduction

The implementation of energy efficiency sustainability elements in the construction domain is the goal of numerous international organizations engaged in this field. The use of alternative energy sources, alone or in hybrid configurations, to provide power to buildings is recommended more and more often, and will become mandatory in the near future. The implementation of hydrogen energy in various practical applications has
been a growing concern for the community of researchers in the field, and, during 2020, hydrogen energy was in the spotlight as a major part of the world’s energy strategies.

Chaouki Ghenai et al. [1] considered an off-grid system composed of photovoltaic panels (PV)/fuel cells (FCs), located in a desert region from the economic perspective. They described conditions in which the system was placed because of its extreme characteristics. Considering dust accumulation and the operating temperature of the panels, they built models and simulated the system to optimize its functionality and increase its performance. Hongbo Ren et al. [2], considering environmental and economic objectives, analyzed a system composed of a PV/FC/battery (B). They highlighted the performance, cost, and size of the equipment. This model was filtered and analyzed through numerical examples. The strategy for the application was selected from several perspectives to improve and demonstrate the environmental performance of the system. Ishaq and Dincer [3] presented a novel system in which hydrogen was added to natural gas for combustion. The hybrid system included wind and solar sources. In order to increase efficiency and decrease emissions, they added 0 to 20% hydrogen gas. They observed that carbon dioxide (CO₂) emissions decreased with inverse proportionality to hydrogen addition, and the combustion energy efficiency grew by 10%. In [4], Al-Hamed and Dincer envisioned a clean locomotive with an integrated solid oxide fuel cell (SOFC) system. To optimize the system they assessed its effectiveness, fuel costs, and carbon emissions. The results showed that compared to diesel, natural gas has a better impact on the environment, reducing costs and emissions.

Ishaq and Dincer [5] comprehensively considered hydrogen’s role in the transition to 100% renewable energy. They described the implementation of this process, highlighting three elements: hybrid hydrogen production, renewable energy sources, and applications and services that could use hydrogen. The paper presents classifications, methods, systems, and a case of study.

Jamshidi and Askarzadeh [6] studied a PV/FC/diesel generator system from a multi-objective optimization perspective, with the purpose of optimizing size, operating emissions, and investigating uncertainties and reservations. The Crow search algorithm was introduced to solve the sizing problem, and the system proved efficient. Bukar and Tan [7] described energy management strategies (EMS) for the system to find the most cost-effective one and analyzed and compared multiple cases from the literature.

Siddiquio and Dincer [8] proposed a multigeneration system with a novel recovery technique for waste heat. They conducted a dynamic investigation with analyses on exergetic and energetic efficiency to evaluate the system over the period of a full year. Several tests were conducted to prove the system’s efficiency. Luta and Raji [9] proposed an algorithm for energy management strategies to balance the load between supply and demand for a fuel cell system. This solution proved also to be effective in the reduction of power losses. Gharibi and Askarzadeh [10] discussed on-grid diesel/PV/FC system optimization. They introduced purchase and selling coefficients in the optimization of its size. Their multiple objectives were renewability, loss of power supply probability (LPSP), and leveled cost of energy.

In [11], Bizon proposed a 2D function to optimize fuel cell fuel consumption. Dynamic power was defined by power profiles and loads or energy sources. Variable mitigation in load and renewable energy was ensured and control of power flow ensured a charge sustaining mode. Therefore, fuel economy increased for this strategy. Krishan and Suhag [12] provided an assessment from technical and financial points of view for two hybrid energy storage systems with configurations technically compared using Mathlab/Simulink models. Configuration feasibility was checked with a real-time hardware in-loop simulator. Samy et al. [13] investigated the technical and financial aspects of a combined renewable energy system (CRES) using simulation, mathematical modeling, and optimization approaches. The project was located in Egypt and contained a small-scale PV/FC/wind turbine (WT). Multiple combinations were developed and presented for optimization. Temiz and Javeni [14] used hydrogen as a medium to store energy for a floating system formed of integrated photovoltaic cells and hydrogen. The main objective was to increase
efficiency and avoid occupying the land. This application provides the cost of electricity per unit. Kamel et al. [15] used the conventional proportional integrated (PI) control strategy as an energy management strategy in a PV/FC/batteries/supercapacitor (SC) system. This system was built to supply the demand power for a dump load. Using high-frequency decoupling and fuzzy logic, the system proved to be efficient as a microgrid system. To provide environmental protection, Ellahi et al. [16] built a database that addressed further hybrid systems and their applicability. They provided an analysis using forecasting techniques, predicted renewable energy sources (RES) availability, and extracted information. Rezk et al. [17] analyzed a hybrid PV/FC/B system built in Neom, Saudi Arabia, where the solar irradiance reaches high levels. The technical–financial and feasibility evaluation covered 500 kWh. To measure the size of the system, the net existing costs and energy costs were calculated. The system proved to be viable when compared to a diesel generation system. In [18], Bizon and Thounthong provided two hybrid power system topologies based on RESs and FC. RESs power flow consisted of modeled wind turbines and photovoltaic arrays. Efficiency in the fuel consumption was observed, as well as the total fuel consumption. Bizon, Stan, and Cormos [19] compared seven control topologies to obtain the optimal strategy in operational aspects such as fuel economy, best operating model for loading, or most appropriate strategy for switching. They found a strategy that ensured a reduction in fuel consumption by 15%.

Balencia, Benavides, and Cardenas [20] conducted an analysis in order to optimize the electricity production in a non-interconnected area in the Colombian Caribbean region. Using the meteorological history of the zone, they ran a comparative analysis on a WT/FC/electrolyzer/SP/regulator. The optimization through the Pareto diagram obtained minimization in CO₂ emissions and in energy costs. Kosmadakis et al. [21] assessed the economic feasibility of a system consisting of PV and lead–acid batteries. Calculations of costs per kWh were variable depending on the conditions. This system was optimized to reduce costs and improve functioning. Dawood, Shafiullah, and Anda [22] analyzed a stand-alone energy-based system installed in rural and urban locations. Multiple scenarios were simulated in order to identify the optimal one from the perspective of technical and financial feasibility. The study by Shakti et al. [23] provided an environmentally friendly and cost-effective system. This project was made to supply the demand in India, in a central community. The system used an electrolyzer, hydrogen storage tank, and fuel cell. Mathematical modeling and operational algorithm were used to optimize the costs. The Homer software proved the effectiveness of the system.

Cheng and Lin [24] aimed to enhance the performance of a green building with the purpose to improve its characteristics and optimize its processes. This building used wind turbines, solar cells, proton exchange membrane fuel cells (PEMFCs), batteries, power electronic devices, and electrolyzers. In conclusion, this system proved reliable, improving costs and performance. In [25], Jena and Kumar Kar projected a system that covers the demand for commercial, residential, and domestic sectors using noncarbonaceous resources. They used the approximation method to estimate the lifespan of the electrolyzer. This system was validated through modeling and simulation in MATLAB/Simulink. Arnaout et al. [26] found a new solution using building-integrated photovoltaics (BIPV) for the façade of the buildings. The value of this solution is its reliability and cleanliness of the solution. The location chosen for the system is in Malaysia, a tropical region, and on the roof surface, to provide the potential for maximum energy levels, and different functional scenarios were analyzed. The main purpose was to preserve energy, satisfy BIPV rules, and capitalize the space on the roof. Hosseini et al. [27] analyzed a system with PV and FC for a residential area, and they investigated the monthly performance of the building. They compared electricity unit cost considering the lifetime of the system through exergonic and financial analysis. The results have shown that the system is not rentable for the winter months due to its low efficiency and costs. In [28], Sedaghati and Shakarami proposed a multiple phase control strategy using fuel cell, battery systems, and photovoltaic panels to establish certain parameters and conditions. The control strategy shows lower steady-state error and faster
response. Alam et al. [29] designed a system of 110V DC for fuel cell and photovoltaic generators to operate on loads such as laptops, fans, mobile phones, and LED lights in a microgrid DC. The system proved to be applicable on stable applications, and it was used for railways. Amirkhalili and Zahedi [30] studied wind power with backup power from a storage system. The system contained a fuel cell, a hydrogen storage tank, an electrolyzer, and a wind turbine. Located in Kouhin, Qazvin, this system proved to be efficient when three wind turbines are used, and the fuel cell provides the energy. Yoichi and Masao [31] used PEMFCs to provide for household cogeneration. This system was chosen because of its high efficiency and to improve the performance of the system.

Ou et al. [32] built a hybrid system for household application with a battery/fuel cell and studied its efficiency and robustness. Using dynamic programming, fuzzy logic control, and state machine control, they simulated the system. This system proved to have a longer life and easier operability. Tai et al. [33] analyses aimed to improve the development of the fuel cells and to save time on the demand for manufacturability and flexibility. This article reviewed the applications and advantages of additive manufacturing in fuel cells. In [34], Doi et al. conceived a system using high purity hydrogen as fuel. They needed to obtain better power that was continuously generated and provided stability and reliability. The European Green Deal strongly recommends the widespread use of green energy, and clean hydrogen vector energy is gaining special importance in all energy strategies across the globe. Research articles, literature reviews, and scientific initiatives in the field of integrating hydrogen fuel cell technologies into practical applications [35] successfully demonstrate the sustainability of hydrogen energy in serving as power supplies for stationary applications, in general, and green buildings, in particular [36,37]. This study addresses the future of a hydrogen-based economy, which involves the supply of hydrogen as the fuel needed for fuel cells in the distribution infrastructure. The practical application of the system is in the “green building” sector, a concept that defines this type of construction as a building that supplies its energy directly from solar energy, with a low energy demand that can be satisfied exclusively by alternative resources [38,39]. This research paper shows the results of a case study on the analysis of the performance of alternative primary energy sources (solar and hydrogen), integrated into a hybrid photovoltaic panel/fuel cell system, and their optimal synergy to provide green energy for a green building. The highlights of this study can be summarized as follows:

- The optimal sizing of solar units implemented in the design, along with the optimal capacities of hydrogen technology, to fulfill the daily electricity demand of the green building in an uninterrupted manner;
- Assessing the feasibility of the proposed hybrid energy system pairing solar energy with hydrogen technologies to power a low-energy green residential building;
- Investigating the possibility of supplying 100% green energy to green residential buildings under conditions of constraints and limitations due to the stochastic nature of the building’s electricity consumption, volatile and intermittent nature of solar resources, local weather conditions specific to the building location, and space limitations for the positioning of the photovoltaic panels, as well as determining the amount of hydrogen fuel required for such a practical application as the one presented in the case study.

2. Materials and Methods

2.1. Framework

This case study is part of a complex project whose main objective was to investigate the ways of integrating fuel cells and the role of hydrogen energy in energy supply systems of energy-efficient buildings [40–44]. Within the project, different possible practical situations for the implementation of hydrogen energy in the domain of these types of buildings were subjected to the study. Fuel cells are suitable for the energy supply of individual residential consumers with low energy requirements, but such systems with small power capabilities have already been developed, and therefore, the new projects aimed at providing fuel cells for the energy supply of residential building complexes that
include more apartments [45,46]. The energy efficiency of fuel cells is higher than that of conventional power generation systems, which operate at an efficiency of over 45%, compared to traditional ones that offer maximum efficiencies of 25–35% [37,46]. This also leads to significant reductions in CO2 emissions [47–50].

This case study involved the supply of energy to an energy-efficient building by a hybrid energy system that used the sun as the primary renewable source of energy and hydrogen as an alternative resource, delivered through a centralized distribution network in the event of a future hydrogen-based economy, shown schematically in Figure 1.

![Figure 1. PV–FC hybrid energy system; principal scheme.](image_url)

The system used photovoltaic panels for the conversion of solar energy for electricity generation, and the hydrogen-powered fuel cell from the central grid supported the energy demands of consumers during periods when solar energy was not available or was inefficient in ensuring energy demand.

The case study concerned the optimal sizing of energy conversion equipment, determining the hydrogen demand as fuel for fuel cell consumption, analysis of the optimal synergy between the photovoltaic panels and the fuel cell for powering the green building, highlighting environmental performance compared to the traditional version of grid electricity and cost analysis.

2.2. Methodological Approach

The research methodology used in conducting the case study is schematically illustrated in Figure 2. Input data refers to the potential of renewable energies available at the studied location, the energy demands of the green building to be supplied with clean, sustainable energy, as well as the technical, environmental, and financial elements particular to the main energy conversion equipment: photovoltaic panels, the fuel cell, and the inverter.

The virtual simulation software of the energy system was Hybrid Optimization by Genetic Algorithms (iHOGA) PRO +2.5 version [51–55], and output data are presented in detail in Section 3, Results.

The power produced by the PV was computed using the following Equation (1):

\[ P_{PV} = G_i \cdot I_{SC} \cdot F_p \cdot U_{DC} \]  

where \( P_{PV} \) is power produced by the PV (kW), \( G_i \) is the hourly solar irradiation (kW/m²), \( I_{SC} \) is the short-circuit current (A), \( F_p \) is the factor of loss compensation by power due to shading, and \( U_{DC} \) is the DC voltage generated by the PV (V) [40,51–56].

The demand for hydrogen as fuel by FC is directly influenced by the nominal power and actual power generated in the system. The computation of fuel cell consumption using hydrogen as the fuel is based on the following equations [40,51–56]:

\[ G_{H2} = \frac{P_{FC} \cdot \eta_{FC}}{\Delta H_{H2}} \]

where \( G_{H2} \) is the hydrogen demand (kg/h), \( P_{FC} \) is the power consumption of the fuel cell (kW), \( \eta_{FC} \) is the efficiency of the fuel cell, and \( \Delta H_{H2} \) is the heat of reaction of hydrogen combustion.
When \( \frac{P_{FC}}{P_{N, FC}} \leq P_{\text{max, ef}} \), the fuel cell consumption is computed with the following math formula:

\[
C_{FC} = \beta_{FC} \cdot P_{N, FC} + \alpha_{FC} \cdot P_{FC}
\]  
(2)

and when \( \frac{P_{FC}}{P_{N, FC}} > P_{\text{max, ef}} \), the fuel cell consumption of fuel cell is computed with the following math formula:

\[
C_{FC} = \beta_{FC} \cdot P_{N, FC} + \alpha_{FC} \cdot P_{FC} \cdot \left[ 1 + F_{ef} \cdot \left( \frac{P_{FC}}{P_{N, FC}} - P_{\text{max, ef}} \right) \right]
\]  
(3)

where

- \( C_{FC} \) is the fuel cell hydrogen consumption (kg/h);
- \( P_{N, FC} \) is the fuel cell nominal power (kW);
- \( P_{FC} \) is the fuel cell real power produced by the energy system (kW);
- \( \alpha_{FC} \) and \( \beta_{FC} \) are coefficients of consumption and efficiency curve (kg/kWh);
- \( F_{ef} \) is consumer factor furthermore of the yield power at maximum efficiency;
- \( P_{\text{max, ef}} \) is the power generated for green building at the fuel cell maximum efficiency (kW).

![Figure 2. Methodological approach.](image)

### 2.2.1. Placement Specific Geo-Climatic Parameters

The geographical data of the location and the particularities of the external climatic parameters of the municipality of Cluj-Napoca, Romania, are summarized in Table 1, as follows:

**Table 1. Geographical and climatic particularities for Cluj-Napoca.**

| Particularities                        | Measure Unit   | Value  |
|----------------------------------------|----------------|--------|
| Latitude                               | °N             | 46.76  |
| Longitude                              | °E             | 23.6   |
| Altitude                               | m              | 523    |
| Daily average solar irradiation        | kWh/m²/zi      | 3.29   |
| Wind speed                             | m/s            | 3.4    |
| Relative humidity                      | %              | 71.2   |
| Atmospheric pressure                   | kPa            | 95.6   |
| Soil temperature                       | °C             | 9      |
| Outdoor temperature                    | °C             | −18    |
The values taken into account for determining the green building energy demand were in accordance with the reference documents recommended for average monthly temperatures, average daily temperatures for the months of a year, the intensity of solar irradiation, and the conventional wind calculation speed, depending on the wind area.

The conventional calculation of outdoor temperatures was considered in accordance with the climate zoning map of the Romanian territory for the winter period. Mc 001/2-2006 [57] includes this map, according to which the Romanian territory is divided into four climatic zones; the municipality of Cluj-Napoca is located in climatic zone III, with the conventional outdoor temperature of calculation \(\theta_{e} = -18 \, ^{\circ}C\).

The establishment of values of the necessary parameters for the calculation of the energy performance of the building was made based on the data measured according to the methodology established by the World Meteorological Organization and processed in accordance with the technical regulations in force [58,59].

For the geographical location of the studied climatic zone, in which the green building is located, the values of the solar irradiation are shown in Figure 3, and the values of the wind speed are presented in Figure 4. The solar energy resource has a total annual irradiation potential of 1297.6 kWh/m\(^2\)/year, with an average daily solar irradiation of 3.29 kWh/m\(^2\)/day [60].

### Average Values of Daily Solar Irradiation

![Average Values of Daily Solar Irradiation](image)

| Month   | Value |
|---------|-------|
| Jan.    | 1.35  |
| Febr.   | 2.16  |
| Mar.    | 3.18  |
| Apr.    | 4.02  |
| May     | 4.87  |
| June    | 5.32  |
| July    | 5.35  |
| Aug.    | 4.93  |
| Sep.    | 3.47  |
| Ocr.    | 2.37  |
| Nov.    | 1.42  |
| Dec.    | 1.08  |

### Wind Speed Average Values

![Wind Speed Average Values](image)

| Month | Value |
|-------|-------|
| Jan.  | 4.0   |
| Febr. | 3.8   |
| Mar.  | 3.3   |
| Apr.  | 3.2   |
| May   | 2.9   |
| June  | 3.2   |
| July  | 3.1   |
| Aug.  | 3.1   |
| Sep.  | 3.6   |
| Oct.  | 3.2   |
| Nov.  | 3.4   |
| Dec.  | 3.9   |

The wind speed has an average of 3.39 m/s and is important in computing the green building energy demand [60].

#### 2.2.2. Dimensional Characteristics of Green Building Envelope Elements

The building envelope consists of a series of surfaces through which heat transfer takes place. The area of the building envelope \((A)\, m^2\) representing the sum of all the
areas of the perimeter constructive elements of the building through which a thermal transfer takes place is calculated as

\[ A = \sum_{k} A_{k} \text{ (m}^2\text{)} \]

where \( A_{k} \) is the area of the building element that forms part of the building envelope.

The dimensional characteristics of the constructive elements for the studied building are presented in Table 2.

| Constructive Element        | Temperature Zone     | Aria (m\(^2\)) |
|-----------------------------|----------------------|----------------|
| Exterior walls              | outdoor environment  | 184.3          |
| Terrace–Roof                | outdoor environment  | 83.4           |
| Floor above the ground      | ground               | 80.9           |
| Windows and doors           | outdoor environment  | 43.5           |
| **TOTAL**                   |                      | **392.07**     |

The envelope area was calculated taking into account exclusively the interior surfaces of the perimeter construction elements, ignoring the existence of the interior construction elements (structural and nonstructural interior walls, as well as the intermediate floors).

The volume of the building ((V); m\(^3\)) represents the volume delimited by the perimeter surfaces that make up the building envelope, which is, in fact, the heated volume of the building, comprising both directly heated rooms (with heating elements) and indirectly heated rooms (without heating elements but ones in which heat penetrates through adjacent walls, devoid of significant thermal insulation). The volume of the studied building is equal to 400.00 (m\(^3\)).

As a general principle, the surfaces of the perimeter construction elements that together make up the building envelope are delimited from the external environments by the inner faces of the construction elements. In this sense, the following elements are involved in performing the calculations regarding the whole building; the free height of the rooms, which is equal to 2.50 (m), and the developed usable area, which is equal to 160.00 (m\(^2\)).

The lengths of the thermal bridges (l) are measured according to their actual lengths existing within the areas (A) determined above; consequently, they are delimited at the extremities by the contour of the respective surfaces. In terms of values, l—the lengths of the thermal bridges in contact with the external environment were equal to 116.86 (m), and the lengths of the thermal bridges in contact with the ground were equal to 11.35 (m).

2.2.3. Green Building—Energy Demands

The energy demand established by the computational and mathematical calculations in accordance with the design norms, standards, and the legislation in force [57] for the green building studied, along with the values of the main consumers, are illustrated in Figure 5, and the hourly distribution of the energy demand is shown in Figure 6.

It turned out that the energy demand of the studied building falls in the category of energy-efficient class A constructions. The energy required for heating was 2106 kWh/year, and in terms of the developed surface of the building of 160 m\(^2\), the value of 13.16 kWh/m\(^2\).year was obtained, a value that was lower than the maximum standardized value in the field of “passive houses,” which is, respectively, 15.00 kWh/m\(^2\).year. With reference to the total energy demands for the green building, it was also observed that the total value amounted to 6759 kWh/year, compared to the developed area of 160 m\(^2\), i.e., 42.24 kWh/m\(^2\).year; in the context initially established, all the demands supported by electricity fell within the standards of the “passive houses,” with the total demand for primary energy being \( \leq 120 \text{ kWh/m}^2\cdot\text{year} \), respectively.
Energy demand data referred to alternating current with a lower frequency of 50 Hz, voltage by 230 V, and power factor \( \cos \phi = 0.9 \) \cite{58, 59}.

The graph of hourly energy demand, shown in Figure 6, highlights the waveforms specific to energy consumption. The most adverse case can be noticed during December, when the hourly maximum active load was 1695 W, occurring between 9 and 11 p.m., and the hourly minimum active load was 360 W, obtained between 4 and 6 a.m.

The most advantageous case may be achieved during June when the hourly maximum active load was 920 W, occurring between 10 and 11 p.m., and the hourly minimum active load was 310 W, achieved between 4 and 6 a.m. Other months registered intermediate values to those presented as limits.
2.2.4. The Hybrid Energy System Proposed for Analysis in the Case Study

The energy conversion equipment units that were the main components in the analyzed hybrid energy system are presented in Table 3.

Table 3. Hybrid energy system equipment.

| Equipment Type | Number of Equipment Units | Nominal Capacity of the Equipment |
|----------------|---------------------------|----------------------------------|
| Photovoltaic panel | SiP12 A135P: 24 panels | 135 Wp; Ptotal = 3.24 kWp |
| Fuel cell | 1 | 3 kW |
| Inverter | S.Solarix 1200 × 2 | 1800 VA |

The constituent equipment units that composed the hybrid energy system were photovoltaic panels with a total installed nominal power of 3.24 kWp, a fuel cell with a nominal power of 3 kW, and an S.Solarix 1200 × 2 type inverter with a capacity of 1800 VA.

(a) Photovoltaic Panels

Photovoltaic panels with the following characteristics were used as technologies for the conversion of solar energy into electricity [52]: 12 V—nominal voltage; 8.23 A—short circuit current; 135 Wp—nominal power; 25 years lifespan; 800 kg CO₂ equiv./kWp; EUR 192—acquisition cost; 2 EUR/year—operation and maintenance cost. The azimuth of the photovoltaic panels was 0°, the ground reflectance had a value = 0.2, the compensation factor for the loss of power due to shading and dirt deposition was considered = 1.2, and the photovoltaic panels were not equipped with solar tracking systems.

(b) Fuel Cell

As a technology for the conversion of hydrogen for use as a vector or secondary energy carrier in the energy system, the iHOGA simulation program database [51–53] has a series of fuel cells of different rated powers, from 1 to 10 kW. This type of equipment considered for the present study has low nominal powers due to the influence of the low energy consumption specific to the building under study. The fuel cell taken into account for the configuration had a power of 3 kW; 50,000 h—lifetime; EUR 15,000—acquisition cost; 0.15 EUR/h—operation and maintenance cost; the consumption and efficiency diagram are shown in Figure 7.

Figure 7. Diagram of hydrogen consumption and efficiency for the 3 kW fuel cell.

(c) Inverter

For the green building consumer, the primary target of the present case study, an inverter with the following features was chosen: 1800 VA—rated power; 10 years—lifetime; EUR 1200—acquisition cost; the efficiency diagram in relation to the generated power is presented in Figure 8.
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Figure 8. Inverter efficiency diagram.

3. Results

3.1. Energy Analysis

The results obtained from the operation simulation are briefly illustrated numerically in Table 4 and represent annual average values of the parameters that characterize this type of system. From the provided data in the table, it is observed that during one year of operation, the photovoltaic panels generated 32% of the total energy production of the optimally configured system, which was directly influenced by the intermittent conditions of solar resource availability, and fuel cell provided the majority of energy in the system, with 68% of the total energy production. It should be noted that in the case of achieving an energy balance between the amount of energy generated by the system and the amount of energy consumed by the system, there was a maximum loss of 15.50% due to DC–AC and/or AC–DC conversion, depending on inverter efficiency.

Table 4. System performance indicators.

| Parameter Studied                              | Value  | Unit    |
|------------------------------------------------|--------|---------|
| Green building total energy demand             | 6759   | kWh/year|
| Energy generated by photovoltaic panels        | 2550   | kWh/year|
| Energy generated by the fuel cell              | 5413   | kWh/year|
| Hydrogen consumption for electricity generation| 403.5  | kg/year |
| Energy loss                                    | 1204   | kWh/year|
| Fuel cell operating time                       | 7720   | h/year  |
| Total carbon dioxide emissions                 | 613    | kg CO₂/year |

The monthly average values of the energy parameters (consumption and production) are summarized in Figure 9.

It is observed that the configured hybrid power generation system delivered an amount of electricity that fully covered the energy demand at the consumer level, and there were no periods with uncovered charges throughout the year. The advantage of combining the two types of alternative energies completely eliminated the deficiencies due to the intermittent availability of solar irradiation, especially that of alternating day/night, due to the fact that hydrogen is constantly delivered through the centralized network, and thus, the disadvantage of electricity production by RES disappeared, but the issue of the nonuniform nature of power generation for 24 h remains valid.

For the analyzed system, the most unfavorable situation was found during December, when it was observed that the energy demand had a maximum value and the level of solar irradiation was minimal; the most favorable situation, by contrast, occurred in June when the energy demand was minimal, and the availability of solar energy was maximum.

Table 5 shows the detailed results obtained for a day in December regarding the most unfavorable situation, and the values are graphically illustrated in Figure 10.
Energy generated by photovoltaic panels 2550 kWh/year
Energy generated by the fuel cell 5413 kWh/year
Hydrogen consumption for electricity generation 403.5 kg/year
Energy loss 1204 kWh/year
Fuel cell operating time 7720 h/year
Total carbon dioxide emissions 613 kg CO2/year

The monthly average values of the energy parameters (consumption and production) are summarized in Figure 9.

It is observed that the configured hybrid power generation system delivered an amount of electricity that fully covered the energy demand at the consumer level, and there were no periods with uncovered charges throughout the year. The advantage of combining the two types of alternative energies completely eliminated the deficiencies due to the intermittent availability of solar irradiation, especially that of alternating day/night, due to the fact that hydrogen is constantly delivered through the centralized network, and thus, the disadvantage of electricity production by RES disappeared, but the issue of the nonuniform nature of power generation for 24 h remains valid.

Figure 9. Monthly average energy performance.

Table 5. Hourly values of energy indicators recorded for one day in December.

| Hour | Energy Demand (Wh) | PV (Wh) | FC (Wh) | Hydrogen Consumption (kg) | Excess (Wh) |
|------|--------------------|--------|--------|----------------------------|-------------|
| 00:00 | 1005              | 0      | 1150   | 0.08                       | 0           |
| 01:00 | 650               | 0      | 727    | 0.05                       | 0           |
| 02:00 | 501               | 0      | 554    | 0.04                       | 0           |
| 03:00 | 375               | 0      | 408    | 0.032                      | 0           |
| 04:00 | 360               | 0      | 392    | 0.032                      | 0           |
| 05:00 | 360               | 0      | 392    | 0.032                      | 0           |
| 06:00 | 420               | 0      | 460    | 0.035                      | 0           |
| 07:00 | 570               | 0      | 635    | 0.044                      | 0           |
| 08:00 | 765               | 0      | 862    | 0.059                      | 0           |
| 09:00 | 810               | 232    | 673    | 0.046                      | 0           |
| 10:00 | 855               | 483    | 473    | 0.036                      | 0           |
| 11:00 | 900               | 693    | 320    | 0.028                      | 0           |
| 12:00 | 960               | 813    | 300    | 0.027                      | 1.25        |
| 13:00 | 980               | 813    | 300    | 0.027                      | 1.92        |
| 14:00 | 1100              | 693    | 554    | 0.04                       | 0           |
| 15:00 | 1230              | 483    | 920    | 0.063                      | 0           |
| 16:00 | 1200              | 232    | 1141   | 0.079                      | 0           |
| 17:00 | 1185              | 0      | 1371   | 0.098                      | 0           |
| 18:00 | 1260              | 0      | 1465   | 0.10                       | 0           |
| 19:00 | 1410              | 0      | 1656   | 0.124                      | 0           |
| 20:00 | 1575              | 0      | 1870   | 0.145                      | 0           |
| 21:00 | 1695              | 0      | 2028   | 0.162                      | 0           |
| 22:00 | 1650              | 0      | 1968   | 0.155                      | 0           |
| 23:00 | 1380              | 0      | 1617   | 0.12                       | 0           |
Table 5. Hourly values of energy indicators recorded for one day in December.

| Hour | Energy Demand (Wh) | PV (Wh) | FC (Wh) | Hydrogen Consumption (kg) | Excess (Wh) |
|------|--------------------|---------|---------|---------------------------|-------------|
| 00:00 | 1005               | 0       | 1150    | 0.08                      | 0           |
| 01:00 | 650                | 0       | 727     | 0.05                      | 0           |
| 02:00 | 501                | 0       | 554     | 0.04                      | 0           |
| 03:00 | 375                | 0       | 408     | 0.032                     | 0           |
| 04:00 | 360                | 0       | 392     | 0.032                     | 0           |
| 05:00 | 360                | 0       | 392     | 0.032                     | 0           |
| 06:00 | 420                | 0       | 460     | 0.035                     | 0           |
| 07:00 | 570                | 0       | 635     | 0.044                     | 0           |
| 08:00 | 765                | 0       | 862     | 0.059                     | 0           |
| 09:00 | 810                | 232     | 673     | 0.046                     | 0           |
| 10:00 | 855                | 483     | 473     | 0.036                     | 0           |
| 11:00 | 900                | 693     | 320     | 0.028                     | 0           |
| 12:00 | 960                | 813     | 300     | 0.027                     | 1.25        |
| 13:00 | 980                | 813     | 300     | 0.027                     | 1.92        |
| 14:00 | 1100               | 693     | 554     | 0.04                      | 0           |
| 15:00 | 1230               | 483     | 920     | 0.063                     | 0           |
| 16:00 | 1200               | 232     | 1141    | 0.079                     | 0           |
| 17:00 | 1185               | 0       | 1371    | 0.098                     | 0           |
| 18:00 | 1260               | 0       | 1465    | 0.10                      | 0           |
| 19:00 | 1410               | 0       | 1656    | 0.124                     | 0           |
| 20:00 | 1575               | 0       | 1870    | 0.145                     | 0           |
| 21:00 | 1695               | 0       | 2028    | 0.162                     | 0           |
| 22:00 | 1650               | 0       | 1968    | 0.155                     | 0           |
| 23:00 | 1380               | 0       | 1617    | 0.12                      | 0           |

Figure 10. Diagram of energy performance obtained for one day in December.

For this period, the solar irradiation was available between 9:00 a.m. and 5:00 p.m., during which PV manufactured electricity for the green building depending on the availability of the sun and the capacity of the equipment; from the data provided in the table, 16.65% of the demand was provided by these components, the remaining 83.35% being delivered by the fuel cell.

It was also observed that the fuel cell worked permanently throughout the day, ensuring the support of 100% energy demand, except for the time interval 9:00–17:00, described above.

At the same time, there was an extremely small amount of excess energy in the case of overlapping energy production from the two alternative sources, which can be exported to the electricity grid or used in other practical applications; the excess energy occurred between 12:00 and 2:00 p.m. when the maximum of the solar irradiation characteristic of the studied period was also registered.

Table 6 shows the detailed results obtained for one day in June regarding the most favorable situation.

In a summer month, solar irradiation was available between 6:00 a.m. and 9:00 p.m., with a maximum achieved during the time interval 11:00 a.m.–5:00 p.m. period in which the photovoltaic panels generated electricity for the green building consumer. It was also observed that the fuel cell did not work during this period. During 24 h, the fuel cell operated for 19 h in this case, providing 100% of the energy demand during the night and part of the energy in the time interval 6:00–11:00 and 17:00–21:00 when solar irradiation decreased in intensity. Additionally, an amount of excess energy was observed during the day when the maximum solar irradiation was recorded, as well as in the case of overlapping energy production from the two alternative sources, but in a smaller amount, for a relatively short time of 3 h.

For a better view of the data obtained and analyzed previously, they were graphically illustrated in Figure 11.
Table 6. Hourly values of energy indicators recorded for one day in June.

| Hour | Energy Demand (Wh) | PV (Wh) | FC (Wh) | Hydrogen Consumption (kg) | Excess (Wh) |
|------|--------------------|---------|---------|--------------------------|------------|
| 00:00| 520                | 0       | 576     | 0.04                     | 0          |
| 01:00| 510                | 0       | 565     | 0.04                     | 0          |
| 02:00| 120                | 0       | 460     | 0.035                    | 0          |
| 03:00| 300                | 0       | 325     | 0.028                    | 0          |
| 04:00| 310                | 0       | 336     | 0.028                    | 0          |
| 05:00| 310                | 0       | 336     | 0.028                    | 0          |
| 06:00| 408                | 17      | 445     | 0.035                    | 0          |
| 07:00| 423                | 100     | 360     | 0.03                     | 0          |
| 08:00| 520                | 195     | 375     | 0.03                     | 0          |
| 09:00| 610                | 400     | 300     | 0.027                    | 28.25      |
| 10:00| 660                | 622     | 300     | 0.027                    | 184.35     |
| 11:00| 680                | 830     | 0       | 0                        | 66.6       |
| 12:00| 700                | 990     | 0       | 0                        | 203.87     |
| 13:00| 760                | 1077    | 0       | 0                        | 221.15     |
| 14:00| 810                | 1077    | 0       | 0                        | 161.9      |
| 15:00| 740                | 990     | 0       | 0                        | 157        |
| 16:00| 710                | 830     | 0       | 0                        | 31.48      |
| 17:00| 690                | 622     | 300     | 0.027                    | 150.5      |
| 18:00| 660                | 400     | 330     | 0.028                    | 0          |
| 19:00| 711                | 195     | 595     | 0.042                    | 0          |
| 20:00| 730                | 100     | 715     | 0.05                     | 0          |
| 21:00| 820                | 17      | 925     | 0.063                    | 0          |
| 22:00| 920                | 0       | 1067    | 0.072                    | 0          |
| 23:00| 820                | 0       | 930     | 0.063                    | 0          |

Figure 11. Energy performance diagram obtained for one day in June.

It can be argued, in this case, that the values of energy performance indicators are directly influenced not by the degree of availability of solar irradiation during a year of operation, but by the fact that the fuel cell uses hydrogen, an alternative energy source,
constantly delivered by the centralized distribution network in a future hydrogen-based economy, thus obtaining a 100% autonomous system, compared to the national electricity network. The hourly hydrogen consumption within the analyzed energy system is presented in Figure 12.

![Hourly hydrogen consumption (kg)](image)

**Figure 12.** Hydrogen consumption schedule in June and December.

For one day in December, 1.654 kg of hydrogen was required to ensure the energy demand of the building. For one day in June, the building needed 58.10% less hydrogen and 0.693 kg of hydrogen, respectively.

3.2. **Environmental Analysis**

Taking into account the fact that for a residential building in Romania, an average carbon footprint of 5.23 tons CO$_2$/year resulting from household energy consumption was calculated [61,62], the analyzed green building supplied by the PV–FC hybrid energy system generated CO$_2$ emissions equal to 11.72% of the average value computed for a standard residential building supplied with power by traditional electricity from the grid (Figure 13).

![CO2 Emission](image)

**Figure 13.** CO$_2$ performance diagram.

3.3. **Economic Analysis**

Table 7 summarizes information on the financial aspects that characterize this type of energy system; the centralized data are as follows: initial investment, the total cost for a life of 25 years, cost of component equipment, the unit price of energy, other costs of generating the inflation rate, the discount rate, interest rates, etc. [63]. In addition, the description of this hypothesis includes the cost of purchasing hydrogen, the fuel for the fuel cell, which is delivered to the consumer through the distribution network supposed to exist within a hydrogen infrastructure in a future hydrogen-based economy, and the tariff of the purchase price was considered 3 EUR/kg H$_2$ purchased.
The costs of the component equipment of the system, along with the costs associated with the acquisition of hydrogen, are illustrated as percentages in Figure 14. At 25 years of operation, it was found that the largest share in the cost diagram was held by the fuel cell, the equipment for converting hydrogen into electricity, which was 67.20%. This share of total expenditures was followed by the costs of purchasing hydrogen fuel necessary for electricity generation, with a value of 22.87%.

A relatively small share of 4.39% was obtained for photovoltaic panels—the technology for converting solar energy into electricity.

Hydrogen-based electricity generation technology, as well as hydrogen production, storage, and distribution methods, are in continuous research and development, and since a number of pilot projects currently underway in this field will be validated, it is expected that in the near future, this equipment, and hydrogen fuel, in general, will decrease costs, gaining a competitive advantage against other technologies in the field of energy production and storage.

### 4. Conclusions

In the hypothesis studied in this case study, the optimally configured system energetically supported 100% of the green building consumer, the subject of the study, generating carbon dioxide emissions of 11.72% of the average value calculated for a conventional energy system in a standard residential building, photovoltaic panels achieving 32% of the annual electricity production, and the fuel cell generating the remaining 68% of the total annual energy production of the system with a hydrogen consumption of 403.5 kg/year, operating 7720 h/year.
Following the computational simulations and the analysis of the results on the energy and financial performance of the electricity generation system, the hypothesis of supplying energy to the green building through a hybrid system consisting of photovoltaic panels for the conversion of solar energy and the fuel cell that consumes the delivered hydrogen was validated. Using the distribution network for electricity generation, in which hydrogen production is outsourced and independent of the power generation system, leads to the conclusion that fuel cell technology is a promising solution for supporting the energy demands of green building consumers, with high efficiency and low carbon emissions, in a future hydrogen-based economy.

The implementation and public acceptance of hydrogen technology depend largely on the development of this technology and the infrastructure necessary for safe operation as well as on the reduction of global costs of this type of alternative energy.

Quantifying the main research findings of this study, the following future research directions will be considered as topics to be addressed in future dedicated works:

- Validation of the present research findings by comparison with results obtained from virtual simulations with OPAL-RT technology that works with PC/FPGA-based real-time simulators, hardware-in-the-loop (HIL) testing equipment, and rapid control prototyping (RCP) systems to design, test, and optimize control and protection systems used in power grids;
- Economical features are extremely important in the implementation of green energy systems. While photovoltaic panels are gaining extensive practical applicability, the prices of this technology are already decreasing, whereas hydrogen fuel cell technologies have still high prices. Green Deal European Strategies encourage and influence the development of renewable energies domain and their implementation in all sectors. In this sense, an interesting future research direction to address is the impact analysis of EU directives and government incentives in supporting the hydrogen and fuel cell industry players;
- The social component, as an essential pillar of sustainability, leads imperatively to the elaboration of some studies to outline the societal perception, viability, and public acceptance of the use of new technologies, especially of hydrogen, as an alternative energy resource in the regional transition to sustainable and ecological energy generation systems based on green energies.

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