Focusing and sorting of ellipsoidal magnetic particles in microchannels

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(Dated: October 2, 2017)

We present a simple method to control the position of ellipsoidal magnetic particles in microchannel Poiseuille flow at low Reynolds number using a static uniform magnetic field. The magnetic field is utilized to pin the particle orientation, and the hydrodynamic interactions between ellipsoids and channel walls allow control of the transverse position of the particles. We employ a far-field hydrodynamic theory and simulations using the boundary element method and Brownian dynamics to show how magnetic particles can be focussed and segregated by size and shape. This is of importance for particle manipulation in lab-on-a-chip devices.

Nowadays microscopic lab-on-a-chip devices have become powerful tools to analyse, manipulate and control droplets [1–5], biological particles [6–8] and active colloids [9–11]. Different particle types can be separated in microfluidic channels where a steady Poiseuille flow is imposed [12, 13]. In particular, positional control along the transverse direction of the channel is desirable in order to transport particles to outlets at different target positions. Under high Reynolds number flow, inertial forces lead to a migration of particles towards stable positions [14, 15] which can be manipulated by feedback-control [16]. In contrast, at low Reynolds number, which is the usual regime at the micron scale, spherical and elongated particles cannot achieve net transverse motion in the absence of external forces [17–20]. In this work, we focus on this low Reynolds number regime.

In lab-on-a-chip devices, magnetic forces are commonly used to manipulate the position of microscopic particles [21–23] or artificial microswimmers [24, 25]. For example, the segregation of different particle types can be realized by applying an external magnetic field gradient, which essentially acts as a body force [22]. Although this method can be used to segregate different types of particles, it can not be used to focus particles to a specific transverse target position. When a uniform magnetic field is applied instead of a gradient field, the particle will only experience a torque but no force, i.e. a uniform field is useful to preserve simplicity. It has one semi-axis of length \( b_1 = a \alpha^{2/3} \) and two of length \( b_2 = a \alpha^{-1/3} \), where \( \alpha \) is the particle’s aspect ratio \( \alpha = b_1/b_2 > 1 \). The particle has a magnetic moment \( \mathbf{m} = (m \cos \phi_p, m \sin \phi_p, 0) \), where \( m = 4 \pi a^3 M/3 \) is the magnetic moment parallel to the particle’s major axis and \( \phi_p \) is the particle orientation angle [Fig. 1(a)-(b)]. The particle is initially placed a distance \( y_0 \) away from an infinite plane wall located at \( y = 0 \), and it experiences a magnetic torque \( \mathbf{T}_m = \mathbf{m} \times \mathbf{B} \) due to a uniform external field \( \mathbf{B} \) applied to the whole domain. We assume that \( \mathbf{B} \) is oriented in \((x, y)\)-plane, \( \mathbf{B} = (B \cos \phi_B, B \sin \phi_B, 0) \), where \( B \) is the strength and \( \phi_B \) the orientation of the field which are both kept constant [Fig. 1(a)]. Note that we only consider in-plane motion of the particle in this paper, because a strong magnetic field will orient the major axis of the particle in-plane [28]. We introduce a non-dimensional parameter \( \beta \) that describes the strength of the magnetic torque compared to the hydrodynamic torque as

\[
\beta(y) = \frac{mB}{\eta a^3 \dot{\gamma}(y)} = \frac{4\pi MB}{3\eta \dot{\gamma}(y)} \quad (1)
\]

where \( \dot{\gamma}(y) \) is the local shear rate of the flow around the particle. For example, when we assume that the particle magnetization \( \mu_0 M = 10^{-3} \) T where \( \mu_0 = 4\pi \times 10^{-7} \) N/A² is the permeability of free space, particle size \( a = 10^{-5} \) m, water viscosity \( \eta = 10^{-3} \) Pa·s, water density \( \rho = 10^3 \) kg/m³, shear rate \( \dot{\gamma} = 10^2 \) s⁻¹ and magnetic field \( B = 1.0 \times 10^2 \) T, the particle Reynolds number is \( Re \approx 10^{-2} \) and \( \beta \approx 10^{-4} \).

We use the boundary element method [29–31] to solve for particle trajectory. When inertial effects are negligible, the flow field \( \mathbf{v} \) of a given point \( \mathbf{x} \) under Stokes flow can be described using a boundary integral formulation [29]:

\[
v_i(x) = v_i^S(x) - \frac{1}{8\pi \eta} \int_A G_{ij}(x, y) q_j(y) dA
\]
where $G$ is the Green’s function, $v^\infty$ is the background flow, and $q$ is the viscous traction acting at a point $y$ on the particle surface. The Blake tensor [32] is used for the Green’s function $G_{ij}$ to account for the walls. Integrating the traction force $q$ on the surface of ellipsoid $A$ gives the hydrodynamic force $F_h$ and torque $T_h$ acting on the particle. As the system is force- and torque-free, these satisfy $F_h = \int_A q \, dA = 0$, $T_h = \int_A q \times (x - x_0) \, dA + m \times B = 0$, where $x_0$ is the hydrodynamic centre of the particle [33]. A given surface material point $x_0$ on the ellipsoid moves with a velocity $v(x_0) = U + \Omega \times (x_0 - x_0)$, where $U$, $\Omega$ are the translational and rotational velocity of the particle, respectively. The surface of the ellipsoid is divided into $N_B = 512$ triangular elements and $N_N = 258$ nodes. The velocities are obtained by solving the dense matrix $Ax = b$ with a known vector $b = (v^\infty, F_h, T_h)$ and an unknown vector $x = (q, U, \Omega)$, and $A$ is a matrix with size $(3N_N + 6)$ based on equations above [30]. The particle position is updated using the first-order Euler method with a time step $\Delta t = 0.01$. The software is written in CUDA and all processes are parallelized [34].

First, we show that transverse motion can be manipulated by pinning the rotational motion of the particle in shear flow, $\varepsilon^\infty = \gamma_0 (y^\infty (y) = \text{const})$. The rotational motion of an ellipsoidal particle subjected to shear and a magnetic field was discussed in Ref. [28], in the absence of a wall. The authors showed that the particle moves in the shear plane for sufficiently large $\beta$ and reaches a stable angle $\phi_p^*$ where it is pinned by the magnetic field. The general expression for the in-plane rotational velocity is

$$\frac{1}{\gamma_0(y)} \dot{\phi}_p = \frac{\beta(y)}{8\pi} F(\alpha) \sin(\phi_B - \phi_p) - \frac{1}{2} (1 - J(\alpha) \cos 2\phi_p),$$

and $\phi_p^*$ is obtained by solving $\dot{\phi}_p = 0$. Note that the first term of Eq. (2) is due to the magnetic torque aligning the particle towards the field orientation $\phi_B$, and the second term is simply Jeffrey’s rotation of an ellipsoid in flow [35] with $J(\alpha) = (\alpha^2 - 1)/(\alpha^2 + 1)$ and $F(\alpha) = 3/(2(\alpha^2 - \alpha - 1) \ln(\alpha + \sqrt{\alpha^2 - 1}) - 1)$ [36].

Figure 1(c) is a schematic of the motion of an ellipsoid in shear flow at different $\beta$, now in the presence of a surface. In the absence of a magnetic field ($\beta = 0$) the particle rotates and oscillates along the $y$-direction, but has no net displacement along $y$ [19]. However, when the magnetic field is strong enough to pin the orientation, the ellipsoid either continuously travels upwards or downwards. The transverse motion can be explained by hydrodynamic interactions between the pinned ellipsoid and the wall. The wall can be considered to act as an image stresslet [37–39], and the leading order contribution to the lift velocity $U_l$ arises from the stresslet component $S_{yy}$ [32] evaluated for the stable angle $\phi_p^*$:

$$U_l(y, \phi_p^*) = -\frac{9}{64\pi \eta} P(y) S_{yy}(\phi_p^*)$$

where $P(y) = 1/y^2$, and to leading order it is sufficient to approximate $S_{yy}(\phi_p^*)$ by $S_{yy}(\phi_p^*)$, which is its value in free space $y \to \infty$ [33], given by

$$\frac{S_{yy}(\phi_p^*)}{\eta a^{3/2}} = A(\alpha) \sin 2\phi_p^* + B(\alpha) \sin 4\phi_p^*$$

where $A(\alpha) = \pi \alpha^2 (5X^M - 5Z^M + 12Y^H)/6$, $B(\alpha) = -5\pi \alpha^2 (3X^M - 4Y^M + 12Z^H)/12$ and $X^M, Y^M, Z^M, Y^H$ are shape functions [33, 40] that are only a function of the eccentricity $e = \sqrt{1 - \alpha^{-2}}$. Since $|A(\alpha)| \gg |B(\alpha)|$ [see inset of Fig. 1(d)], the stresslet changes its sign only for $\sin 2\phi_p^* = 0$ as shown in Fig. 1(d). Therefore, the particle moves away from the wall $U_l > 0$ for $\sin 2\phi_p^* > 0$, while it moves towards the wall $U_l < 0$ for $\sin 2\phi_p^* < 0$. Figure 1(e) shows simulation and theoretical results for the lift velocity under strong orientational pinning $\beta = 100$ for different distances of the particle from the surface. Very good agreement is obtained for $y/a \gtrsim 4$. Deviations occur close to the wall where higher order terms in Eq. (3) play a role. We also ignored the fact that the stresslet $S_{yy}$ itself is modified due to the presence of the wall.

Next we show that the magnetic particle can be focused to an arbitrary transverse position under Poiseuille flow between two walls. This geometry is an approximation for high aspect ratio rectangular channels away from side walls. The background velocity profile is

\begin{align*}
(a) &\text{ simple shear } + 1 \text{ wall} \\
(b) &\text{ Poiseuille } + 2 \text{ walls}
\end{align*}
FIG. 2. Focusing under Poiseuille flow: (a)-(c) Stable angle $\phi_0^*$ and transverse velocity $U_y$ as a function of the particle (a = 3) position $y$ for a magnetic field $\beta_w = 60$ and $\phi_p = (a) \pi/2$, (b) 0 and (c) $-0.4 \pi$ and channel width $H/a = 20$. Lines: prediction from far-field theory; dots in (c): results from boundary element simulations. (d) Time history of particle position $y(t)$ from boundary element simulations under the conditions of (c). The gray dotted curves show trajectories in a rectangular channel of aspect ratio $H_x/H_y = 4$ for different initial conditions $z_0 = \{0.5H_x, 0.8H_x\}$. The inset shows stable fixed point $y^*/H$ for ellipsoids (a = 3) as a function of the magnetic field $\beta_w$ and $\phi_B$ obtained by far-field theory. White lines are isolines for every 0.1. (e) Distribution of focussed particles under Poiseuille flow with $\gamma_w = 100 \text{ s}^{-1}$ and channel width $H/a = 20$ after 10s, from Brownian dynamics simulations with particle size $a = 10 \text{ \mu m}$. Inset: theoretical predictions (lines) and Brownian dynamics simulation (dots) for the standard deviation of the distribution $\sigma/a$. Dotted horizontal line indicates separations $a > 2 \text{ \mu m}$.
solving $\dot{\phi}_p = 0$ [Eq. (2)] for $\phi_p^* = \pm \pi/2$ as
\[
y^* (\alpha, \beta_w, \phi_B) = \frac{1}{2} \pm \frac{\beta_w F(\alpha)}{8\pi (1 + J(\alpha))} \cos \phi_B
\] (5)
where $J(\alpha)$ and $F(\alpha)$ are defined after Eq.(2). For example, when a field is applied in direction $\phi_B = -0.4\pi$ with $\beta_w = 60$ [Fig. 2(c)], the stable fixed point of an ellipsoid ($\alpha = 3$) is $y^*/H \approx 0.32$ and the particles are focused to this position. This we also confirm by performing boundary element simulations with different initial positions, shown in Fig. 2(d), and we observe that $U_y(y)$ and $\phi_p^*(y)$ obtained from simulations qualitatively agree with the far-field results. Note that the hydrodynamic contributions from the two walls are calculated considering the images of both walls [32] in the simulation, which is enough for relatively large channels $H/a = 20$, while higher order reflections are required for a much narrower channel [40, 41]. Inset of Fig. 2(d) describes the stable fixed point $y^*/H$ [Eq. (5)] for ellipsoids ($\alpha = 3$) with $-\pi/2 < \phi_B < 0$. The figure shows $y^*$ shifts toward the bottom wall with increasing $\beta_w$ or $\phi_B$, and the particles can be focused to arbitrary positions in the lower half of the channel ($y/H < 0.5$). By symmetry, the particles would be focused to the upper half of the channel for $0 < \phi_B < \pi/2$. Although the far-field theory predicts that the particles cannot cross the center line because $U_y(H/2) = 0$, in reality they can do so because of their finite size, as confirmed by boundary element simulations [Fig. 2(d)].

To see the effect of side walls, at $z = 0$ and $z = H_z$, on the motion of the particles, we extended our simulation scheme to a rectangular channel geometry by using a triangular mesh both for the particles and the walls [40, 42–44]. When the particles are not too close to the walls we observe very similar trajectories, focusing points and traveling distances as without side walls [40] [Fig. 2(d)]. Moreover migration in $z$ direction is negligible.

Finally we show how a static magnetic field can be used to separate particles of different aspect ratio $\alpha$ even in the presence of thermal fluctuations. The particles are initially uniformly distributed in the lower half of the channel [13], and we consider the same magnetic field and channel height as discussed above ($\beta_w = 60$, $\phi_B = -0.4\pi$, $H/a = 20$), wall-shear rate $\dot{\gamma}_w = 100$ s$^{-1}$, and viscosity of water ($\eta = 10^{-3}$ Pa·s). We use Brownian Dynamics simulations at room temperature, solving the equations
\[
\dot{\mathbf{r}} = \mathbf{U}_p + H \cdot \mathbf{B}_p,
\]
\[
\dot{\mathbf{n}} = \left( \Omega_p + \sqrt{2D_T} \mathbf{z} \times \mathbf{n} \right)
\] (7)
for different particle size $a$ and aspect ratio $\alpha$. Here $\mathbf{U}_p = v_z \mathbf{z} + U_y \mathbf{y}$, and $\Omega_p = \Omega_0 \hat{\mathbf{\phi}} + \Omega_\mathbf{\theta}$ is the full 3D particle reorientation rate for the particle orientation $\mathbf{n} = (\sin \theta_p \cos \phi_p, \sin \theta_p \sin \phi_p, \cos \theta_p)$ with $\Omega_\phi = \gamma_w \{ \beta(y) F(\alpha) \sin (\phi_B - \phi_p) / (8\pi \sin \theta_p) - (1 - J \cos 2\phi_p) / 2 \}$, $\Omega_\theta = \gamma_w \{ \beta(y) F(\alpha) \cos \theta_p \cos (\phi_B - \phi_p) / (8\pi) + J \sin 2\theta_p \sin 2\phi_p / 4 \}$ [28]. $H$ is calculated from the translational diffusion tensor $\mathbf{D}(\phi_p, \theta_p) = D_1 + (1/2) D_2$ $\mathbf{M}(\phi_p, \theta_p) = (1/2) H \cdot \mathbf{H}$ where $\mathbf{M}(\phi_p, \theta_p)$ is a symmetric 3x3 matrix [40] and $D = (D_1 + D_2)/2$, $\Delta D = D_1 - D_2$ where $D_1 = k_B T a^{-1} n^{-1} K_1(\alpha)$ and $D_2 = k_B T a^{-1} n^{-1} K_2(\alpha)$ are the respective longitudinal and transverse diffusion coefficients of an ellipsoid of aspect ratio $\alpha$ with shape functions $K_1(\alpha) > K_2(\alpha)$ [33, 40, 45–47]. The rotational diffusion constant $D_2 = k_B T a^{-3} n^{-1} K_2(\alpha)$ with the shape function $K_2(\alpha)$ [33, 36, 40]. The random numbers $\xi_i$ and $\xi_i'$ model Gaussian white noise with zero mean and $(\xi_i, \xi_i') = \delta_{ij}$ ($i = x, y, z$).

Distributions for 1000 particles of size $a = 10$ μm for $\alpha = \{2, 3, 4\}$ after $t = 10$ s are shown in Fig. 2(e). Our results clearly show that particles of different shape can be separated to different target positions $y^*(\alpha)$, given by Eq. (5), by applying a static magnetic field. 50% of the particles reach the target region $y^*(\alpha) \pm a$ in experimentally feasible times [7s ($\alpha = 4$) to 20s ($\alpha = 2$)] and traveling distances (< 30 mm). Note, the focusing times are even smaller for higher confinement [40]. Efficient separation is only possible for particles of size $a \gtrsim 2$ μm, where the width of the steady state distribution $\sigma$ [48] is smaller than the distance between two peaks [see inset of Fig. 2(e)]. We find an approximate analytic expression for $\sigma$ by linearizing the drift velocity around the fixed point $y^*$, $U_y = -k(y - y^*)$ where $k$ only depends on the system parameters [40]. We solve for the steady state distribution $p(y) \sim \exp[-V/k_B T]$ where we introduced a potential $V = \gamma_1 k(y - y^*)^2/2$ with $\gamma_1 = k_B T / D_1$ which keeps the particle near its target position $y^*$. Since $k \sim s^{-1}$ and $\gamma_1 \sim n a$ we obtain $\sigma / a \sim a^{-3/2} / (k_B T)^{1/2}$.

We have shown that the transverse position of magnetic ellipsoidal particles in microchannel Poiseuille flow can be controlled by a static magnetic field. This is due to the hydrodynamic interactions of the ellipsoids with the channel walls. Our method can be used to focus and segregate magnetic particles which is of importance for particle manipulation in lab-on-a-chip devices.

This project has received funding from the European Union’s Horizon 2020 research and innovation programme under grant agreement No. 665440 and under the Marie Skłodowska-Curie grant agreement No 653284.

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