Air–sea gas exchange in the North Atlantic: 
$^3$He/SF$_6$ experiment during GasEx-98

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ABSTRACT

GasEx-98 was the first open-ocean process study where gas transfer velocity measurements were made with several robust techniques, including airlside eddy covariance of CO$_2$ and deliberate injection of $^3$He and SF$_6$. While the CO$_2$ eddy covariance results have been fully analysed and publicised, leading to a boom in the use of this technique in the marine environment, the $^3$He/SF$_6$ results have not received the same level of analysis. Here, based on new approaches that we have developed to analyse $^3$He/SF$_6$ data in the subsequent years, we revisit the $^3$He/SF$_6$ dual tracer results from GasEx-98 and show that they are consistent with the results from other parts of the coastal and open ocean, and that they are in agreement with current parameterisations between wind speed and gas exchange for slightly soluble gases over the ocean at intermediate wind speeds.

Keywords: air–sea gas exchange, $^3$He/SF$_6$ dual tracer technique, North Atlantic

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1. Introduction

Air–sea gas exchange plays a major role in the cycling of biogeochemically important trace gases, such as CO$_2$ and DMS, between the atmosphere and the ocean, and in turn affects the climate of our planet. As such, great efforts have been made to study the factors that influence air–sea gas exchange and relate the rate of gas exchange to environmental processes that can be easily observed. Research so far has shown wind speed to be the best correlate for gas exchange, as wind produces near surface turbulence and bubbles, two of the main mechanisms responsible for regulating air–sea gas exchange. Until about 25 years ago, our understanding of the relationship between wind speed and air–sea gas exchange relied on studies that used the mass balance of opportunistic tracers such as $^{222}$Rn (Peng et al., 1979) and thermonuclear bomb produced $^{14}$C (Broecker et al., 1985). Since then, $^3$He/SF$_6$ dual tracer experiments have emerged as a robust way to obtain integrated measurements of air–sea gas exchange based on water column measurements in the ocean on short time scales. A series of these experiments have been conducted in both the coastal and open oceans (Watson et al., 1991; Wanninkhof et al., 1993, 1997, 2004; Nightingale et al., 2000a, 2000b; Ho et al., 2006, 2011b; Salter et al., 2011).

The results of these experiments reinforce the view that wind is the dominant process driving air–sea exchange of slightly soluble gases in most environments. Other processes and mechanisms (e.g. rain, convection, bubbles and surfactants) might be of importance under certain circumstances, but these processes are either affected by wind or are not dominant on regional to global scales (Ho et al., 2011b). $^3$He/SF$_6$ data from coastal ocean experiments in the North Sea (Nightingale et al., 2000b) and an open ocean in the Southern Ocean (Ho et al., 2006) have also been used to derive two wind speed/gas exchange parameterisations that are very similar (see below). These parameterisations show that wind can account for more than 80% of the variance in all the $^3$He/SF$_6$ data (Ho et al., 2011b), demonstrating that wind speed/gas exchange parameterisations obtained in one ocean location can be applied to another and implying that under most circumstances, a universal relationship between

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wind speed and gas exchange of slightly soluble gases (i.e. those with Ostwald solubility coefficients less than 1, including N₂, O₂, N₂O, CH₄ and CO₂) over the ocean can be used. Thus, with knowledge of wind speeds, measurements of air–water concentration differences can provide robust air–sea flux estimates.

GasEx-98 was the first ³He/SF₆ dual tracer experiment conducted in the open ocean and the first successful deployment of micrometeorological techniques, including CO₂ eddy covariance and gradient methods, for measurement of air–sea gas fluxes in the open ocean. While the CO₂ eddy covariance results have been fully analysed and publicised (Wanninkhof and McGillis, 1999; McGillis et al., 2001a, 2001b), the ³He/SF₆ results have not been analysed at daily resolution. This is partly due to the challenging nature of the results, characterised by occasional rapid changes in ³He/SF₆ ratios and fluctuating mixed layer depths as defined by temperature profiles.

Most of the ³He/SF₆ data for the open ocean are from the Southern Ocean (SOFeX (Wanninkhof et al., 2004), SAGE (Ho et al., 2006), SO GasEx (Ho et al., 2011b)), with only four data points from Northern Hemisphere; all from the North Atlantic, with one from GasEx-98 (McGillis et al., 2001b) and three from DOGEE II (Salter et al., 2011). In the following, based on novel approaches to interpret the data refined over the last 15 years, we revisited and analysed the ³He/SF₆ experiment from GasEx-98, which has been described briefly in McGillis et al. (2001b) and where a 2-week averaged gas transfer velocity based on ³He/SF₆ was presented (see Fig. 3).

2. Methods

2.1. GasEx-98

GasEx-98 took place in the North Atlantic in the boreal spring/summer of 1998 (Fig. 1). The experiment consisted of three separate cruises on the NOAA Ship Ronald H. Brown, with the middle leg being a process study in a warm-core ring in the North Atlantic near 46°N and 21.5°W. This leg of the cruise left Lisbon, Portugal on 25 May 1998 (year-day 145) and arrived in Ponta Delgada, Portugal on 26 June 1998 (year-day 177). This portion of the cruise is discussed here and is referred to as GasEx-98. The experiment represents the beginning of the successful GasEx franchise and was followed by GasEx-2001 in the Equatorial Pacific and SO GasEx in the Atlantic sector of the Southern Ocean (McGillis et al., 2001b, 2004; Ho et al., 2011a).

2.2. Tracer injection and sampling

On 28 May 1998 (year-day 149), a gaseous mixture of ca. 20 mol of SF₆ and 0.06 mol of ³He was injected as a 5-km streak into the surface mixed layer of a warm core eddy at 15 m depth by bubbling through some diffusion stones. After injection, 614 SF₆ samples and 97 ³He samples were taken from the Niskin bottles over the course of 17 days (from year-days 151 to 167). SF₆ was sampled in 550-ml borosilicate glass bottles with ground glass stoppers, and ³He was sampled in copper tubes mounted in aluminium channels with stainless steel pinch-off clamps. The SF₆ samples were
analysed on board the ship using a purge and trap gas chromatographic system equipped with an electron capture detector (Law et al., 1994), while the \(^3\)He samples were shipped back to the laboratory, extracted from the copper tubes and analysed on a helium isotope mass spectrometer (Ludin et al., 1998).

In addition to discrete sampling, the surface concentrations of SF\(_6\) were mapped with an underway SF\(_6\) analysis system that measured samples at 2-min intervals. This provided information on the spatial extent and movement of the tracer patch. The discrete samples used in this analysis were those well within the tracer patch to avoid possible biases in the technique caused by secondary dispersion effects.

\section{2.3. Wind speed measurements}

Wind speed and direction, along with other meteorological measurements such as air temperature, relative humidity, solar and long-wave radiation, were made at 18 m above sea level using a sonic anemometer on the forward jackstaff of the ship. The high-quality wind speed data were corrected for ship motion and scaled to neutral boundary conditions at 10 m height utilising the measured drag coefficients and taking into account the atmospheric boundary layer stability (Fairall et al., 1996). These robust normalisations to 10 m height and neutral boundary layer conditions removed an often overlooked ambiguity in wind speed measurements that can impact wind speed/gas exchange relationships. Details of the measurement and corrections are given in McGillis et al. (2001a).

\section{2.4. \(^3\)He/SF\(_6\) dual tracer technique}

With the \(^3\)He/SF\(_6\) dual tracer technique, the gas transfer velocity for \(^3\)He \(k_{3He}\) can be determined by the change in the \(^3\)He/SF\(_6\) ratio with time (Watson et al., 1991; Wanninkhof et al., 1993):

\[ k_{3He} = -h \frac{d}{dt} \left( \ln \left( \frac{3He_{exc}/SF6}{Sc_{3He}SF6} \right) / 1 - \left( Sc_{3He}/Sc_{3He} \right)^{-1/2} \right). \]  

where \(h\) is the depth over which \(^3\)He and SF\(_6\) are exchanging with the atmosphere (referred to here as the mixed layer), corresponding to the depth at which the SF\(_6\) reaches 70\% of its averaged concentration in the top 12 m. This threshold was chosen based on the depth where SF\(_6\) concentration changes dramatically from the mixed layer value. A comparison of how using a temperature-based mixed layer depth would affect the calculated \(k\) is shown in Supplementary File. \(^3\)He\(_{exc}\) and SF\(_6\) are the excess \(^3\)He concentration (i.e. \(^3\)He above solubility equilibrium; use interchangeably here with \(^3\)He) and SF\(_6\) concentration in the mixed layer, respectively. The ratios are determined for each depth and then averaged to obtain the profile average. \(Sc_{exc}\) and \(Sc_{3He}\) are the Schmidt numbers (i.e. kinematic viscosity of water, divided by diffusion of gas in water) for SF\(_6\) and \(^3\)He, respectively (Wanninkhof, 2014). The gas transfer velocity is then normalised to a Sc of 600, corresponding to that of CO\(_2\) at 20 °C in freshwater:

\[ k(600) = k_{3He}(600/Sc_{3He})^{-1/2} \]  

Equation (1) can be solved analytically to yield \(^3\)He/SF\(_6\) ratio with time, if the initial \(^3\)He/SF\(_6\) ratio and the time evolution of \(h\) and \(k(600)\) are known:

\[ \frac{\left( \frac{3He}{SF6} \right)}{\left( \frac{3He}{SF6} \right)_{t=0}} = e^{\frac{k_{3He}(600/Sc_{3He})^{-1/2}}{h} \left( 1 - \left( Sc_{SF6}/Sc_{3He} \right)^{-1/2} \right)}. \]  

\section{3. Results and discussion}

\subsection{3.1. \(^3\)He and SF\(_6\)}

After injection, initial excess \(^3\)He reached as high as ca. 7000 × 10\(^{-16}\) ccSTP g\(^{-1}\), from a background level of 2–6 × 10\(^{-16}\) ccSTP g\(^{-1}\) in the mixed layer, while SF\(_6\) was as high as 180000 fmol L\(^{-1}\), from a background of ca. 0.6 fmol L\(^{-1}\). Over the course of the experiment, both \(^3\)He and SF\(_6\) decreased towards background levels. At the end of the experiment, 18 days after injection, the tracer patch size was estimated to be 15 km in diameter based on the continuous surface SF\(_6\) surveys, and the SF\(_6\) concentrations were still easily detectable at 50 times above background levels. The \(^3\)He had decreased to ca. 5–10 × 10\(^{-16}\) ccSTP g\(^{-1}\) such that the background level correction was important for the measurements towards the end of the experiment.

As with other \(^3\)He/SF\(_6\) experiments, the \(^3\)He/SF\(_6\) ratios from GasEx-98 do not exhibit a monotonic decrease with time due to differences in fluxes arising from changes in wind speeds. However, there are periods when the ratio decreased more rapidly than can be explained by gas exchange and there are periods when the ratios increased. These rapid changes were most likely due to mixing and mixed layer dynamics as discussed in Ho et al. (2011b). In particular, some of the tracer mixture appeared to have been trapped below the mixed layer during shallowing and isolated from the atmosphere. During intensification of the wind and associated mixed layer deepening, the tracers got re-entrained into the mixed layer. The deepening of the mixed layer and associated mixing of the subsurface chlorophyll maximum and entrainment of nitrate from JD 159–160 when an increase in \(^3\)He/SF\(_6\) is observed (Fig. 4) is presented in Hood et al. (2001). Below, we divide our analysis of the \(^3\)He/SF\(_6\) time series into six segments, demarcated by station where unrealistic rapid changes in \(^3\)He/SF\(_6\) ratios occurred.
3.2. Wind speeds

During the period of the $^3$He/SF$_6$ tracer release experiment, wind speeds ranged from 0.8 to 18.3 m s$^{-1}$, with a mean of 7.1 m s$^{-1}$ (Fig. 2). The data show that during the experiment, storms moved through the study area in the North Atlantic with a periodicity of roughly 4 days. The wind speed distributions for the six segments differed greatly, with means of ca. 5–11 m s$^{-1}$ and standard deviations from the mean that varied from 21 to 48% (Table 1).

3.3. Choice of mixed layer depths

Mixed layer depth has a first order influence on the calculation of $k$ [see eq. (1)]. Different definitions of mixed layer based on temperature or density gradients are available. For purposes of determining $k$, it is the depth of water exchanging gases with the atmosphere and here we use the depth at which the SF$_6$ reaches 70% of its averaged concentration in the top 12 m and call this the tracer mixed layer. This depth is generally less variable than the thermal mixed layer depth (Kim et al., 2005, Fig. 7). The Supplementary File provides an overview of the thermal mixed layer and the tracer mixed layer for each station, and the impact of using the tracer derived mixed layer on determination of $k$. Internal waves within the eddy caused changes in mixed layer depth up to 5 m over periods of hours that made using thermal mixed layers less reliable.

![Wind speed graph](image)

Fig. 2. Wind speeds measured and adjusted to $u_{10}$ on the NOAA Ship Ronald H. Brown during GasEx-98. The shaded areas mark the six segments that were used to evaluate the $^3$He/SF$_6$ data.

| Segments | Stations | Date range | $h$ (m) | $u_{10}$ (m s$^{-1}$) | Temp$^b$ ($^\circ$C) | Sal$^b$ | $^3$He | SF$_6$ | $k$(600) (cm h$^{-1}$) | Mean ± error | Schmidt numbers$^a$ | Gas transfer velocities$^b$ |
|----------|----------|------------|---------|---------------------|-------------------|------|-------|-------|-----------------|---------------|----------------------|--------------------|
| 1        | 152, 154, 157 | 152.57–154.36 | 18.3 | 4.6 | 1.9–8.6 | 1.5 | 1.11 | 226 | 15.11 | 35.668 | 175.3 | 1370.7 | 7.6 ± 2.7 |
| 2        | 161, 163 | 155.74–156.53 | 15.3 | 7.9 | 2.9–14.1 | 2.5 | 1.10 | 114 | 15.41 | 35.663 | 173.2 | 1349.3 | 18.8 ± 2.8 |
| 3        | 165, 167, 169, 157.36–159.68 | 28.6 | 8.8 | 0.9–18.3 | 4.2 | 1.23 | 322 | 15.54 | 35.657 | 172.1 | 1338.5 | 18.7 ± 3.2 |
| 4        | 171, 172 | 160.35–161.40 | 21.7 | 10.7 | 1.1–14.9 | 2.3 | 1.04 | 138 | 15.10 | 35.657 | 175.9 | 1376.5 | 30.4 ± 4.6 |
| 5        | 178, 179, 180 | 162.37–163.35 | 30.8 | 8.3 | 2.3–12.8 | 2.7 | 1.10 | 136 | 15.40 | 35.670 | 173.6 | 1353.8 | 18.6 ± 8.5 |
| 6        | 184, 190 | 164.36–166.35 | 30.0 | 5.0 | 0.8–9.3 | 2.3 | 1.20 | 270 | 15.50 | 35.679 | 172.5 | 1342.8 | 10.7 ± 1.6 |

$^a$Averaged Schmidt numbers of all stations in each segment.

$^b$Enhancement-corrected $k$(600) for each segment (i.e. $k$(600)/$e$, where $e = u_{10}^2/u_{10}^2$; error in $k$(600) is determined from the least-squares fit to the $^3$He/SF$_6$ decrease for each segment, and the uncertainties in the mixed layer depth.

$^c$Stations in each segment.

$^d$Averaged mixed layer depth determined from SF$_6$ profiles.

$^e$Standard deviation.

$^f$Number of 10-minute averaged wind speed measurements in each segment.

$^g$Averaged temperature and salinity from the surface of all stations in each segment.
One disadvantage of using the SF$_6$ profiles is that the sampling for SF$_6$ was coarse (usually 2–5 m) compared to the CTD (conductivity, temperature, and depth sonde) temperature profile (1 m). The variability in mixed layer depth is a major contributor to the uncertainty in $k$.

3.4. Gas transfer velocities

Gas transfer velocities were calculated using eq. (1) on the six segments of the $^3$He/SF$_6$ time series using the average tracer mixed layer depth between subsequent measurements. Furthermore, these $k(600)$ values [eq. (2)] were corrected for enhancement $\varepsilon$ due to variability in $u_{10}$ over each time interval (Wanninkhof et al., 2004) by dividing the resulting $k(600)$ by $\varepsilon$, assuming that the relationship between $u_{10}$ and $k(600)$ has the functional form of a quadratic (i.e. $\varepsilon = \frac{u_{10}^2}{u_{10}^2}$). This yields a value of $k(600)$ for instantaneous or steady wind. $k(600)$ varied between 7.6 and 30.4 cm h$^{-1}$ and is correlated with wind speed (Fig. 3). The $k(600)$ as a function of wind speed for GasEx-98 was similar to other experiments in both the coastal and open oceans referenced above and is in agreement with the 2-week average determined previously from $^3$He/SF$_6$ for this study (McGillis et al., 2001b) (Fig. 3).

3.5. Modelling $^3$He/SF$_6$ decrease with different parameterisations

The decrease in $^3$He/SF$_6$ ratio during GasEx-98 was modelled using eq. (3). The approach follows the approach first described in Kuss et al. (2004). In short, the time evolution is modelled following a decrease in $^3$He/SF$_6$ ratios using one of six commonly used wind speed/gas exchange parameterisations (Liss and Merlivat, 1986; Wanninkhof, 1992; Wanninkhof and McGillis, 1999; Nightingale et al., 2000b; Ho et al., 2006; Wanninkhof et al., 2009) (Fig. 4). The gas exchange/wind speed parameterisations that can represent the decrease best are considered the optimal ones. Each of the six segments was evaluated separately. For each segment, the average tracer mixed layer depth $h$ was determined using the depth profile of SF$_6$ as described above and detailed in the Supplementary File. The goodness of fit between model and observations were evaluated in terms of relative root mean squared error (rRMSE):

$$rRMSE = \sqrt{\frac{\sum_{n=1}^{N} \left( \frac{R_{n,mod} - R_{n,obs}}{R_{n,obs}} \right)^2}{N}}.$$ (4)

Fig. 3. Gas transfer velocities for GasEx-98 (filled red circles), corrected to a Schmidt number of 600, plotted along with all published $^3$He/SF$_6$ derived $k(600)$ values from the coastal and open oceans against wind speed $u_{10}$. The 2-week averaged $k(600)$ presented in McGillis et al. (2001a) is also shown (filled red square). The points for GasEx-98 were determined using a least-squares fit to the $^3$He/SF$_6$ ratios from each of the six segments to determine $\frac{d}{dt} \frac{^3\text{He}}{\text{SF}_6}$, and then using eqs. (1 and 2) to calculate $k(600)$. The error estimation for the GasEx-98 data is described in the footnotes to Table 1.
where $R_{\text{obs}}$ and $R_{\text{mod}}$ are the observed and modelled $^3$He/SF$_6$ ratio, respectively, $N$ is the total number of stations in the segment. Table 2 summarises the rRMSE for all six segments. However, we focus our analysis on segments 1 and 3 (Fig. 5). Segments 2, 4 and 6 contain data from only two stations and the fits match one point and therefore have no independent constraint to determine the RMSE [eq. (4)]. Segment 5 contains three stations, but they span less than 1 day. Moreover, for segments 5 and 6, the $^3$He concentrations were close to background values, increasing the uncertainty in the $^3$He/SF$_6$ ratio and therefore the estimation of $k(600)$. However, the results for these segments are not used in the analysis, either because they occurred at the beginning of the experiment before the patch has mixed sufficiently (i.e. the first two stations), or because they were deemed to be outside of the tracer patch based on the surface SF$_6$ concentrations.

Table 2. Relative root mean square errors of the model/data comparison for each segment of the $^3$He/SF$_6$ data for each of the parameterizations listed.

| Parameterisations                  | Segment 1 (%) | Segment 2 (%) | Segment 3 (%) | Segment 4 (%) | Segment 5 (%) | Segment 6 (%) |
|-----------------------------------|---------------|---------------|---------------|---------------|---------------|---------------|
| Liss and Merlivat (1986)          | 7.8           | 14.3          | 11.9          | 17.3          | 4.1           | 15.4          |
| Wanninkhof (1992)                 | 2.5           | 1.3           | 9.8           | 6.7           | 4.6           | 6.9           |
| Wanninkhof and McGillis (1999)    | 8.7           | 5.5           | 9.4           | 10.4          | 2.7           | 14.7          |
| Nightingale et al. (2000b)        | 0.7           | 7.3           | 2.1           | 4.7           | 2.9           | 9.8           |
| Ho et al. (2006)                  | 1.8           | 6.7           | 2.4           | 2.3           | 2.9           | 10.5          |
| Wanninkhof et al. (2009)          | 2.2           | 9.9           | 1.7           | 6.9           | 3.0           | 10.3          |

The italicised values are segments 2, 4 and 6 that only contain two stations each, and segment 5, which occurs over the course of less than a day, and have greater measurement uncertainty. The bold values in each segment denote the top 4 parameterisations in terms of having low rRMSE.
As with data from SO GasEx (Ho et al., 2011b), the parameterisations of Nightingale et al. (2000b), Ho et al. (2006) and Wanninkhof et al. (2009) are most able to model the data from GasEx-98. Wanninkhof (1992) is able to accurately represent the results for segment 1, but not for segment 3. This can be explained by the difference in wind speed distributions between the two segments (Fig. 6).

Segment 1 covers a narrow range of wind speeds, from 1.9 to 8.6 m s\(^{-1}\), with a mean (± standard deviation) of 4.6±1.5 m s\(^{-1}\). Segment 3 covers a large range of wind speeds, from 0.9 to 18.3 m s\(^{-1}\) with a mean (± standard deviation) of 8.8±4.2 m s\(^{-1}\) and can be used effectively to distinguish the differences in the various wind speed/gas exchange parameterisations. This result shows one of the advantages of this approach, in that it can distinguish between differences in wind speed/gas exchange relationships.

**Fig. 5.** Model and data comparison of \(^3\)He/\(^6\)SF\(_6\) ratios for segments 1 and 3 of GasEx-98. For both segments, the parameterisations of Nightingale et al. (2000b), Ho et al. (2006) and Wanninkhof et al. (2009) are most able to model the data.
due to the differences in distributions of the wind speeds, while other approaches are limited to simply evaluating mean $k$ from mean wind speeds and over fixed time intervals.

Segment 1 covers a period with decreasing winds, while segment 3 covers a period with increasing winds. One could expect a period with increasing winds to have younger and steeper waves, and greater wave breaking and bubble mediated gas transfer (Kleiss and Melville, 2010). However, the $k(600)$ as a function of wind speed is similar from these two periods, indicating that for these intervals there were no difference between increasing and decreasing winds.

Of note is that over the last week of the study, $\text{He}/\text{SF}_6$ ratio changes were very small while winds were in the intermediate range $3\text{–}10 \text{ m s}^{-1}$ (Fig. 2). This appears in part due to significant mixed layer deepening from 20 to 30 m during this period and diurnal stratification during periods of low winds (Zhang et al., 2001). This observation also suggests that for GasEx-98, residual turbulence due to thermal gradients in the mixed layer and surface shear had little impact on $k$, in contrast to GasEx-2001 in the equatorial Pacific where $\text{CO}_2$ eddy covariance measurements suggested a significant enhancement (McGillis et al., 2004).

### 3.6. Similarity between different ocean basins

The results from GasEx-98 show that the relationship between wind speed and gas exchange in the North Atlantic is similar to that of the Southern Ocean. Ho et al. (2011b) showed that in the open ocean, for slightly soluble gases such as $\text{CO}_2$, there appears to be a universal relationship between wind speed and gas exchange as the very similar parameterisations of Nightingale et al. (2000b), Ho et al. (2006) and Wanninkhof et al. (2009) derived from different

| Citation                  | Approach | Region               | Parameterisations$^a$ |
|---------------------------|----------|----------------------|-----------------------|
| Nightingale et al. (2000b)| $^3\text{He}/\text{SF}_6$ | North Sea and Georges Bank | $k(600) = 0.333\mu_10 + 0.222\mu_10$ $^b$ |
| Ho et al. (2006)           | $^3\text{He}/\text{SF}_6$ | Southern Ocean        | $k(600) = (0.266 \pm 0.019)\mu_10$ |
| Sweeney et al. (2007)      | $^{14}\text{C}$ | Global               | $k(600) = 0.27\mu_10 (\pm 30\%)$ $^c$ |
| Wanninkhof et al. (2009)   | Synthesis | Global               | $k(660) = 3 + 0.1\mu_10 + 0.64\mu_10 + 0.011\mu_10$ |
| Wanninkhof (2014)          | $^{14}\text{C}$ | Global               | $k(660) = 0.251\mu_10 (\pm 30\%)$ $^f$ |

$^a$For all parameterisations, $\mu_{10}$ is in m s$^{-1}$ while the resulting $k$ is in cm h$^{-1}$.

$^b$In the literature, investigators have chosen to express wind speed/gas exchange parameterisations as either $k(600)$ or $k(660)$, corresponding to Schmidt numbers of 600 ($\text{CO}_2$ in freshwater at 20 °C) or 660 (close to 666, which is $\text{CO}_2$ in seawater at 20 °C), respectively. This choice is arbitrary. The conversion from $k(600)$ to $k(660)$ requires a multiplication of 0.953 assuming the dependence of gas exchange on Schmidt number scales to $\text{Sc}^{-1/2}$; for example, for Ho et al. (2006), $k(600) = 0.266\mu_10$ is equivalent to $k(660) = 0.254\mu_10$.

$^c$The uncertainty in the global $^{14}\text{C}$ relationships includes both the uncertainty in wind speeds and global bomb $^{14}\text{C}$ inventory.
datasets and assumptions (Fig. 3) are able to account for 82, 83 and 80% of the variance, respectively, in the $^{3}$He/SF$_6$ dual tracer data collected in open and coastal oceans. With the addition of data from GasEx-98, these statistics have not changed significantly, and Nightingale et al. (2000b), Ho et al. (2006) and Wanninkhof et al. (2009) are able to account for 83, 83 and 81% of the variance in all the $^{3}$He/SF$_6$ data, respectively.

3.7. Global constraints

The parameterisations that can explain most of the variance in the $^{3}$He/SF$_6$ during GasEx-98 also match the global constraints based on bomb $^{14}$C. Sweeney et al. (2007) used an ocean general circulation model to reproduce the global bomb $^{14}$C ocean inventory, based on a quadratic dependence between wind speed and gas exchange that has a coefficient very similar to that of Ho et al. (2006) (Table 3). Wanninkhof (2014) revised the analysis performed in Wanninkhof (1992), with updated global wind speed and bomb $^{14}$C inventories, and obtained a relationship that is 30% lower than in the original analysis, is nearly identical to that of Ho et al. (2006), and falls well within the uncertainty of the other parameterisations (Table 3).

4. Conclusions

Reanalysis of the GasEx-98 data show that the relationship between wind speed and gas exchange is similar between the North Atlantic and the Southern Ocean. Furthermore, the results are in agreement with wind speed/gas exchange parameterisations that have previously been deemed to be the most appropriate to use for predicting gas exchange of slightly soluble gases in the ocean.

With our current knowledge, we are able to predict the rate of gas exchange in the open ocean for slightly soluble gases such as CO$_2$. The agreement between $^{3}$He/SF$_6$ dual tracer studies in different parts of the ocean and agreement with parameterisations that meet the global $^{14}$C constraint suggest that these relationships can be used for estimating fluxes from air–sea concentration differences if no direct flux estimates are available. There are environments such as those affected with strong shear, thermal induced turbulence, partial ice coverage or extreme turbulence (McGillis et al., 2004; McNeil and D’Asaro, 2007; Loose et al., 2014) where the current wind speed/gas exchange parameterisations have limited capabilities and should be investigated. Other topics that remain to be investigated include the influence of surfactant on gas exchange in upwelling areas or in inland seas, and air–sea exchange of soluble gases, such as DMS and CH$_3$Br, that might not be as heavily influenced by bubbles.

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