Curved digital X-ray detectors

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A curved image sensor on plastic foil has been developed for cone beam computed tomography (CBCT) X-ray imaging. The image sensor of about $6 \times 8 \text{ cm}^2$ size has been built on a thin polyimide foil with an indium gallium zinc oxide (IGZO) backplane and an organic photodetectors (OPD) frontplane. A flexible cesium iodide (CsI) scintillator has been attached to the optical sensor with 480 $\times$ 640 pixels of 126 $\mu\text{m}$ size. Dark current density of the OPD was low with less than $10^{-7} \text{ mA/cm}^2$ at $-2 \text{ V}$, while an external quantum efficiency (EQE) of about 50% was reached in the visible wavelength range matched to the scintillator output. The image quality of the digital X-ray detector allowed for 3D reconstruction images of a bone phantom on a rotating stage with a lab setup. The curved detector with 32 cm curvature radius opens up the path for very compact CBCT gantries with largely reduced footprint.

**RESULTS**

Figure 2a shows the cross section of the digital X-ray detector-on-foil. It consists of (1) an IGZO-based active-matrix TFT backplane fabricated on a polyimide foil, followed by (2) an inverted stack OPD frontplane that is formed by a ~300 nm thick photoactive organic layer sandwiched between bottom pixel electrode and non-patterned optically transparent top electrode, (3) an optically transparent thin-film barrier, and finished by (4) a bendable CsI scintillator, developed by Hamamatsu Photonics (Japan).

The IGZO TFT backplane is processed on a $\text{SiN}_x$ bottom encapsulation barrier on polyimide foil/glass carrier via a series of lithographic mask steps. The display-compatible TFT fabrication process is discussed in detail both previously\textsuperscript{11} and in the “Methods”. Transfer characteristics of 25 transistors with a channel length of 20 $\mu\text{m}$ and a channel width of 60 $\mu\text{m}$ equally distributed over the $320 \times 352 \text{ mm}$ substrate are presented in Fig. 3a. The TFTs show a typical mobility of $15.1 \pm 0.8 \text{ cm}^2/\text{Vs}$, onset voltage ($V_{\text{on}}$) of $0.4 \pm 0.3 \text{ V}$, ON/OFF-current ratio $\sim10^2$, and a subthreshold swing of $0.4 \pm 0.02 \text{ V/decade}$.

In the current digital detector, we employed a single pass transistor configuration per pixel, as used in most current X-ray imaging products. The TFT switch requires a high ON/OFF ratio, a reasonably sharp turn-ON region but particularly a low leakage.
The low OFF-current of substantially <1 pA compares favorably to amorphous and polycrystalline silicon transistors. This is inherent to IGZO as the low leakage current is related to the large bandgap of IGZO (~3 eV). The formation of the OPD on top of the IGZO transistor does not affect the IGZO TFT properties. This is also not expected as the OPD deposition occurs at much lower temperatures than the maximum process temperature during IGZO TFT fabrication.

The photodetector is based on a bulk heterojunction (BHJ) structure, with a donor polymer and an acceptor fullerene derivative. BHJ photodetectors show high photogeneration sensitivities, fast response times, and their absorption can be tuned from the ultraviolet to the near-infrared. Moreover, they can be solution-processed at low temperatures and on flexible substrates by roll-to-roll and sheet-to-sheet large-area processing techniques. In this work, we have used a 280 nm thick blend...
of poly[N-9′-heptadecanyl-2,7-carbazole-alt-5,5-(4′,7′-di-2-thienyl-2′,1′,3′-benzothiadiazole)], PCDTBTT, a p-type (donor) polymer and [6,6]-phenyl-C61-butyric acid methyl ester, PCBM, (acceptor) fullerene, followed by a thermally evaporated MoOx hole transport layer and a thin Ag semitransparent anode. Finally, a top transparent thin-film encapsulation barrier is processed (Fig. 2b). Figure 2c, d show photographs of curved image sensor and flexible scintillator, respectively. Details of the step by step fabrication can be found in the “Experimental” section.

OPD test devices having the same layer stack as the OPD frontplane and processed in the same way were also fabricated. These devices were used to measure the OPD performance and consisted of a series of 1 mm² pixels. Figure 3b shows the current density–voltage (J–V) characteristics of the OPDs in dark (Ud) and under illumination of low intensity, white light (Uphoto). The nonzero Jd at 0 V results from transient displacement currents that occur during a J–V sweep even at very low scan rates. We consider the static measurement to be a more reliable way of determining Jd. Figure 3c depicts a static measurement of Jd at −2 V over a time interval of 5 min. Typically, the OPDs have a leakage current density of 0.3−10−7 mA/cm² at −2 V (Supplementary Fig. 3). This value is lower than that of low-temperature a-Si p–i–n photodiodes. It compares favorably with other reported dark current densities for BHJ based OPDs with ~300 nm thick active layers. For an OPD pixel of 126 × 126 µm² with a fill factor of 50% this would translate to a leakage current of 8 × 10−15 A. The leakage current of the TFT is estimated from TFT measurements on devices with larger channel widths. It can be seen that Jphoto is orders of magnitude larger than Jd. We found Voc to decrease reciprocally with In(I) with the light intensity. The so-called ideality factor n was 1.6. Voc was determined to be 0.85 V under simulated solar light (AM1.5G, 100 mW/cm²).

The external quantum efficiency (EQE) and spectral responsivity (SR) vs. wavelength at a reverse bias of −2 V are depicted in Fig. 3d. Both metrics peak near the emission wavelength of the CsI:Tl scintillator at values of 48% and 0.21 A/W, respectively. Simulations show that a photodiode quantum efficiency of 48% with a dark current density lower than 10−6 mA/cm² image quality is determined by the random variations in the number of X-ray photons that are generated and absorbed by the scintillator. The noise current density, Jn, was measured at reverse bias between 1 and 50 Hz (Supplementary Fig. 4). Below ca. 10 Hz a 1/f behavior is observed. Above 10 Hz, the frequency response was flat, at ~8 fA Hz−1/2. Taking this value together with SR of 0.21 A/W, the specific detectivities D* = SR/√A/Jn (in Jones, where Jones = cmHz1/2/W and A is device area). At −2 V bias, the calculated maximum specific detectivity D* = 3 × 1012 Jones (at ~550 nm). With a dark current density as low as 3 × 10−8 mA/cm², sensitivity of 0.21 A/W, and specific detectivity of 3 × 1012 Jones in the green wavelength range, the performance of our solution-processed photodetector rank amongst the best so far for OPDs.

A sensor array of 480 × 640 pixels, 126 × 126 µm² in size, is built. The photodiodes are operated with a reverse bias voltage, of typically a few Volt. The positive electrodes of the photodiodes are
formed by the optically transparent common electrode (Fig. 2a). The negative, patterned, and bottom electrodes of the photodiodes of a column are connected to the data line via a TFT. The gates of the TFTs of a row are connected to a common gate line. The flat panel sensor is scanned one-row-at-a-time by a dedicated row driver, in a similar way as active-matrix displays. During one frame time all the rows are sequentially selected and TFTs switch from the non-conducting to the conducting ("ON") state. With the TFTs in the ON state charge sense amplifiers (CSAs) coupled to the data line detect the pixel current as the TFT transfers the charge from the photodiode capacitance to the data line until the voltage across the photodiode is back to its original value. Current levels are digitized using analog-to-digital converters (ADCs). More details can be found here in ref. 11.

In order to characterize the optical response, we illuminate the OPD arrays from the top, using a large-area homogenous LED light source. The mean wavelength of 540 nm is similar to the light produced by a typical CsI-Tl based X-ray scintillator. Figure 4a shows the spatially averaged image sensor signal of all pixels in the array as a function of light intensity for different reverse bias voltage over the photodiode and two image scan rates, 2 and 4 frames per second (fps). The applied photodiode bias voltage was varied. The measurement was done for 2 frames per second (fps), equivalent to 500 ms integration time and 4 fps, equivalent to 250 ms integration time. A log-log plot of (a) is shown in Supplementary Fig. 5. In Fig. 4b the EQE as calculated from the slope of the graphs from (a) vs. impinging light intensity. In Fig. 4c the temporal behavior of the image sensor. At \( t = 0 \) the light pulse is switched off, and the decay of photocurrent is monitored for different applied biases. d Optical image taken with the image sensor on foil.

The temporal response of the sensor array is measured by a sequence of illuminated images followed by images where the light source is switched off. As shown in Fig. 4c there is still some charge detected in the non-illuminated images, a phenomenon
known as residual signal or lag also from other noncrystalline photodiodes like a-Si25. The residual signal is attributed to charges in the photodiode, which are released from deep traps after a certain time26. The residual signal is in the order of a few tenths of a percent of the signal height during illumination at 1 s after end of the illumination. It is decreasing with increasing bias voltage due to faster removal of charge with higher bias field. After about 2 s the residual signal falls below our measurement limit of about 0.2%. The temporal response is comparable to standard a-Si X-ray digital detectors and thus good enough for the initial medical application. The impact of lag or "residual signal" depends not only on the frame rate, but also on the medical application. For long-term low dose X-ray video imaging (fluoroscopy) applications, a-Si-based X-ray detectors are frequently used without problems with 30–60 fps frame rate. For 3D imaging (cone beam CT) with C-arm systems they are used normally up to 30 fps, too. Here the residual signal can produce some artefacts (rings) after 3D image reconstruction, which have to be corrected by software.

An optical image is taken with a b/w photograph printed on a transparent slide on top of the sensor array (Fig. 4d). For this image a dark image is subtracted (offset correction) and a homogeneously illuminated image is used to correct for sensitivity differences between pixels (gain correction). Finally, single pixels and lines with too low or too high signal ("defects") are corrected by simple interpolation with the neighboring pixels.

The sensor array is produced while the polyimide foil is still attached to a glass carrier. To show that delamination of the foil does not influence the performance of the sensor array, the optical characterization has been done before and after the laser delamination process. The graphs of signal vs. light intensity at different bias voltages (Fig. 5a) show no difference between the two measurements. We conclude that the delamination process does not affect the sensitivity of the sensor array. In addition, no new defect single pixels, lines or areas with increased dark current were found comparing images before and after releasing the foil from the glass. To prove the long shelf-life, we repeated the same measurement 44 days after the delamination. In between the sensor array has been kept at ambient air and room temperature. Again, no signs of degradation were found as shown in Fig. 5b. Hence, the bottom and top encapsulation layers, with water vapor transmission rate WVTR of $10^{-6}$ g/m$^2$/day$^{19,27}$ serve as an excellent barrier for potential degradation by the ambient.

Subsequent to the optical characterization we tested the digital detector also with X-rays. Flexible cesium iodide (CsI) scintillator sheets of 400 and 700 µm, typical thicknesses in current state-of-the-art flat panel X-ray detectors exceeding the attenuation length of 99 µm at the X-ray energy used, were coupled to the sensor array by simply pressing them with the weight of 1 mm Al to achieve a good optical contact. X-ray images with 70 kV tube voltage and 350 mA tube current were acquired with 50 ms exposure time. No additional filtration other than the internal tube filtration (about 2.5 mm Al equivalent) has been used, i.e., X-ray beam quality is defined as RQR5 with about 40 keV average X-ray energy. With a source-image distance of about 1 m a dose of about 450 µGy air/frame was applied. Typical X-ray resolution test phantoms with thin lead lamella (Huettner, type 10) were put as contrast objects on top of the digital detector (Fig. 6). An optical image (Fig. 4d) an offset, gain, and defect correction were performed. The images show a good and homogeneous contrast over the entire area of the digital detector. It is clearly visible that the spatial resolution is higher with the thinner scintillator (Fig. 6a, 400 µm) layer because the lateral spread of optical photons is lower than in the thicker scintillator layer (Fig. 6b, 700 µm). The modulation transfer function (MTF), has been measured with a tungsten edge according to IEC standard IEC 62220-1 CDV. It is 31 and 37% at 1 lp/mm for the 700 and 400 µm thick scintillator. These values are in agreement with the expected MTF for an X-ray detector with a 40 µm thin-film barrier in between the image sensor and scintillator (Fig. 2a).

In case of a flat detector, oblique incident X-rays lead to a degradation of the MTF at the edges and corners, because the point of interaction in the layer determines the lateral displacement and leads to a blur. Following the analysis method of Hajdok & Cunningham28 a MTF degradation of 17% at 2 line pairs per mm is expected. More details can be found in (Fig. S1). By curving the detector with the right radius for a given source-detector distance, all X-rays are impinging perpendicular to the scintillator surface and no degradation due to oblique incident X-ray occurs. The test bench for 3-dimensional X-ray imaging (Fig. 7a) comprises a standard medical X-ray tube (Philips MRC200 0407 ROT-GS 1004), a rotational stage to place objects, and the foil-based digital detector in a curved holder with 32 cm curvature radius. The X-ray beam from the tube passes the object horizontally before hitting the detector. The tube and detector are fixed in their position. The object can be rotated in a controlled manner. This geometry is equivalent to medical CBCT, just in that case the object (patient) is in a fixed position while tube and detector are rotating.

X-ray images of a piece of bone are taken with a rate of 2 images per second while the object is rotating with 4° per second, thus 180 projection images are taken in a full 360° rotation. The steps of offset, gain, and defect correction mentioned earlier were also applied to the 2D projection images. With a standard 3D reconstruction algorithm (FDK filtered back-projection), which has been adapted for the curved geometry, a 3D volume image (Fig. 7b) of $256 \times 256 \times 256$ voxels with a voxel size of (0.234 mm$^3$) is created. Since 3D reconstruction is very sensitive to any nonideal
behavior of the digital X-ray detector, our result with the prototype detector is quite remarkable.

**DISCUSSION**

Today’s flat panel digital X-ray detectors are heavy, difficult to transport, and prone to breakages because they are made on glass substrates. When processed on plastic substrates, such detectors become less vulnerable. Moreover, detectors-on-film can be mechanically curved. Curving could create a digital X-ray detector that conforms to the specification of different patients. Here, we integrated a curved digital X-ray detector into a demonstration CBCT X-ray system. 3D images of biological objects were taken with a reconstruction algorithm adapted to the curved geometry. The curved digital X-ray detector consisted of solution-processed OPDs on top of an IGZO TFT backplane, on top of a flexible plastic substrate. The prototype digital detector array consists of 480 × 640 pixels with each a size of 126 × 126 µm², thus the X-ray imaging area was 6.10 × 8.13 cm². Stability of the digital detector performance could be shown at ambient air conditions for a long time even after delamination of the foil from the support glass substrate. Equipped with a bendable CsI scintillator, the curved digital detector delivered the same X-ray imaging performance as the flat, foil-based digital X-ray detectors. The advantage of this solution is that it can now be built into a much more compact 3D X-ray imaging system with much smaller footprint, as the area for the gantry can shrink by as much as 50%.

**METHODS**

**IGZO TFT array**

A bottom-gate top-contact TFT layout with an etch-stop layer for the image sensor backplane is used. First, a 150 nm-thick SiNx thin-film moisture barrier was deposited on the top of a 13 µm thick spin-on PI foil applied on a 320 × 352 mm glass plate. A MoCr gate metal was then sputtered and patterned using photolithography, followed by a 200 nm-thick plasma-enhanced chemical vapor deposited (PECVD) SiN gate dielectric layer deposited at 180°C. A gate dielectric breakdown field of >6 MV/cm was measured, which is sufficient for the typical voltages used in the TFTs. The semiconductor layer was a 24 nm-thick IGZO layer, deposited using dc sputtering from a target with an In:Ga:Zn atomic ratio of 1:1:1. IGZO layer thickness and O₂ flow (6%) in the sputter chamber were optimized in order to achieve good TFT performance at low temperature. A 100-nm-thick SiO₂ etch-stop layer was grown using PECVD at 200°C on top of the patterned IGZO semiconductor. A dry etching process was used to open the contact holes between the gate metal and semiconductor, and finally, source–drain layers, together with interconnect lines, were sputtered from a MoCr target. The TFT stack was encapsulated with a 2 µm-thick photopatternable SU8 resist interlayer. The TFT technology was originally developed to make flexible OLED displays.

**Organic photodetector**

A 100 nm of MoCr was sputtered and subsequently patterned using photolithography to form the reflective pixel electrode. Contact holes and the edges of the pixel electrodes were covered with a SU8 resist, preventing shorts between the bottom and the top electrode. The photoactive layer is a 300 nm-thick blend of a p-type polymer, PCDTBT (purchased from PCAS), and n-type small molecule, [6, 6]-phenyl-C61 butyric acid methyl ester (purchased from nano-c) in a 1:4 wt ratio. The bandgap of PCDTBT and PCBM are ~1.6 and 2.3 eV, respectively. HOMO ~5.1 eV, LUMO ~3.5 eV for PCDTBT, HOMO ~6.1 eV, and LUMO ~3.8 eV for...
PCBM. This leads to an optical absorption onset of \( \sim 700 \) nm. The photoactive blend was slot die coated from chlorobenzene on top of the TFT backplane. Prior to deposition of the top electrode, the photoactive layer was annealed at 60–90°C for 10 min in ambient. Thermally evaporated 60 nm MoO\(_x\), and 10 nm Ag are used as a semitransparent anode. The image sensor on foil was protected from oxygen and moisture by an optically transparent, multi-layer stack of two low-temperature plasma-deposited amorphous hydrogenated silicon nitride (a-SiN\(_x\):H) layers and an organic intermediate layer\(^{19}\). The total thickness of that encapsulation stack is 40 \( \mu \)m.

**Delamination**

In order to release the image sensor on foil from the temporary glass carrier, laser-assisted debonding is used. Three hundred fifty-five nanometers light from 3rd harmonic ND:YAG shines from the backside of the glass carrier onto the polyimide foil. The laser energy has to be able to reach the interface between glass and polyimide. The 3rd harmonic ND:YAG 355 nm is absorbed only slightly by the (Eagle XG) glass carrier, but extremely well by polyimide. In polyimide this laser has a penetration depth of around 50 nm. When the intense laser light is absorbed fully in this very thin polyimide layer, the polyimide foil almost instantaneously decomposes and gaseous compounds are formed. Heat further pressurizes the gaseous species and triggers delamination of the polyimide foil from the glass. Because of the high absorption of the polyimide, TFT and OPD are screened relatively well from the intense laser light, and therefore the laser does not damage the image sensor during release.

**Electronic drivers**

Each data line is connected to a channel of a charge sensitive amplifier (CSA; type Indigo ISC0701, FLIR systems) with subsequent digitization with 14-bit resolution. The charge of the CSA is sampled with 14 bit, but scaled to 16 bit inside the FPGA of the detector electronics, because all further image processing is done with 16 bit numbers. Gate line drivers from NEC (type uPD160702B) have been used. In the detector mode used, the capacitance of the feedback capacitor of the integrator \( C_{\text{int}} \) equals 4 pF. Additional image corrections such as subtraction of dark images, and correction of individual pixel gain, are done inside the PC, and the resulting image is displayed on the PC monitor.

TFT and OPD characterization: all TFT characteristics were measured in ambient using an Agilent 4155C semiconductor parameter analyzer connected to a semi-automatic prober. OPD test devices were characterized in a glovebox under a \( N_2 \) atmosphere and at ambient temperature.

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**Fig. 7 3D X-ray characterization.**

*a* Schematic of CBCT test bench used for characterization of the curved digital X-ray detector, showing X-ray source, bone phantom, and curved digital X-ray detector. 

*b* Reconstructed 3D images of the bone phantom.
Current versus voltage characteristics were measured using an Agilent 4155C semiconductor parameter analyzer connected to manual probes. The voltage was swept from $-2$ to $2 \text{V}$. Using the same equipment, EQE was also measured in a glovebox under a N$_2$ atmosphere and at ambient temperature. The system uses a solar simulator light source and a series of filters resulting in 20–50 nm steps. The devices are connected to a Keithley 2400 to apply the voltage to the devices. The MTF has been measured with a tungsten edge according to IEC standard IEC 62220-1 CDV.

**DATA AVAILABILITY**

The authors declare that the data supporting the findings of this study are available within the paper (and its Supplementary Information files).

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**AUTHOR CONTRIBUTIONS**

A.v.B., M.S., O.T., J.J., and G.H.G conceived the idea and designed the experiments. A.v.B., M.S., O.T., S.S., J.-L.v.d.S., H.A., A.K., W.R., R.R., L.A., P.E.M., and F.D.F. performed experiments and analyzed the data. A.v.B., M.S., and O.T. coordinated the experiments. J.J. and G.H.G. were project supervisors. A.v.B., M.S., and O.T. wrote the paper, with editing contributions from all the co-authors.

**COMPETING INTERESTS**

The authors declare no competing interests.

**ADDITIONAL INFORMATION**

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