Integrating giant microwave absorption with magnetic refrigeration in one multifunctional intermetallic compound of LaFe$_{11.6}$Si$_{1.4}$C$_{0.2}$H$_{1.7}$

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Both microwave absorption and magnetocaloric effect (MCE) are two essential performances of magnetic materials. We observe that LaFe$_{11.6}$Si$_{1.4}$C$_{0.2}$H$_{1.7}$ intermetallic compound exhibits the advantages of both giant microwave absorption exceeding $\sim 42$ dB and magnetic entropy change of $\sim 20$ J kg$^{-1}$ K$^{-1}$. The excellent electromagnetic wave absorption results from the large magnetic loss and dielectric loss as well as the efficient complementarity between relative permittivity and permeability. The giant MCE effect in this material provides an ideal technique for cooling the MAMs to avoid temperature increase and infrared radiation during microwave absorption. Our finding suggests that we can integrate the giant microwave absorption with magnetic refrigeration in one multifunctional material. This integration not only advances our understanding of the correlation between microwave absorption and MCE, but also can open a new avenue to exploit microwave devices and electromagnetic stealth.

The extensive development and use of the electronic devices have created a new kind of problem called electromagnetic interference (EMI). To suppress the serious EMI problem, it is becoming very urgent to design and fabricate the electromagnetic compatibility (EMC) devices, which can ensure that equipment items will not interfere with or prevent each other’s correct operation through spurious emission. For achieving sufficient EMC, researchers have long been involved in exploiting microwave absorbing materials (MAMs) due to their prospective applications in electronic devices, military affairs such as airplanes, steamboats, tanks, microwave darkrooms, and even broadband electromagnetic cloaking. Up to date, various MAMs composed of magnetic loss powders such as ferrite, nickel, cobalt, and dielectric loss materials such as carbon nanotubes (CNTs) and conducting polymers have been fabricated. Two approaches, either making electromagnetic wave disappearance by interference (Figure 1(a)), or absorbing electromagnetic wave effectively and converting electromagnetic energy into heat, are generally adopted for microwave loss. Unfortunately, the temperature increment and infrared radiation of MAMs due to the conversion of electromagnetic energy into heat will seriously hamper the application of microwave devices and electromagnetic stealth (Figure 1(b)). Therefore, it is interesting to explore whether MAMs can be refrigerated during microwave absorption (Figure 1(c)).

Compared with traditional gas-compression/expansion refrigeration, magnetic refrigeration exhibits the advantages of high energy efficiency and environment friendliness. The discovery of a giant magnetic entropy change in La(Fe$_{1-x}$Si$_{x}$)$_{13}$ intermetallic compounds gives rise to interest in searching for novel magnetic refrigerants. Both microwave absorption and magnetocaloric effect (MCE) are two essential performances of magnetic materials. Meanwhile, to our knowledge, microwave properties of these novel magnetic refrigerants have never been reported. According to the Snoek limit, the product of the high frequency susceptibility, $\chi = \mu - 1$, and the resonance frequency, $f_r$, is proportional to the saturation magnetization, $(\mu - 1) f_r \propto M_s$, where $\mu$ is permeability. In addition, the upper limit of magnetic entropy change is determined by the relation of $\Delta S_{\text{Max}} = R \ln (2J_f + 1)$, where $R$ is the gas constant and $J_f$ is the total angular momentum of the magnetic ion. The high saturation magnetization is thus one of prerequisites for achieving both high frequency permeability and giant magnetic entropy change. Among the rare-earth-Fe intermetallic compounds, LaFe$_{13.2}$Si$_{6.0}$ intermetallics have the most abundant Fe concentration, and consequently possesses high saturation magnetization.
Here, we present the microwave absorption and magnetic entropy change of LaFe$_{11.6}$Si$_{1.4}$C$_{0.2}$H$_{1.7}$ intermetallic compound. LaFe$_{11.6}$Si$_{1.4}$C$_{0.2}$H$_{1.7}$ intermetallic compound shows a metallic behavior with resistivity value of 3.8 $\Omega \cdot \text{m}$ at room temperature. The MAM must contain a sufficient quantity of free charge carriers in order to interact with microwave radiation. In order to reduce the eddy current loss induced by electromagnetic wave, the MAM sample was mixed with insulating paraffin wax. To satisfy the microwave devices application above room temperature, the Curie temperature up to 330 K is achieved by the addition of interstitial atoms C and H. In the case of LaFe$_{11.6}$Si$_{1.4}$C$_{0.2}$H$_{1.7}$ intermetallic compound, Fe atoms occupy two sites, 8b and 96i, the Curie temperature is determined by the overall exchange interaction between Fe(8b)-Fe(8b), Fe(8b)-Fe(96i) and Fe(96i)-Fe(96i) atoms. Our previous neutron diffraction work demonstrated that the bond-length of Fe(8b)-Fe(96i) is very short, resulting a negative exchange interaction between Fe(8b) and Fe(96i), and consequently weakens the overall exchange interaction. The addition of interstitial atoms C and H leads to an expansion of the bond-length of Fe(8b)-Fe(96i) and a change in sign of Fe(8b)-Fe(96i) exchange interaction from negative to positive$^{15}$. Therefore, the overall exchange interaction between Fe atoms and the Curie temperature are significantly enhanced by the introduction of interstitial atoms C and H. We observe that this intermetallic compound exhibits the advantages of both giant microwave absorption exceeding $-42$ dB and magnetic entropy change of $-20$ J kg$^{-1}$ K$^{-1}$. The value of $RL$ for LaFe$_{11.6}$Si$_{1.4}$C$_{0.2}$H$_{1.7}$/paraffin wax is comparable with that of the most common used microwave absorber, carbonyl iron (35 dB) and conventional ferrite MAMs (30 dB)$^{16,19}$. Our finding suggests that we can integrate the microwave absorption with magnetic refrigeration in one multifunctional material. This integration not only gives us a deeper insight into the effect of intrinsic magnetic properties on the performances of microwave absorption and MCE, but also provides a new possibility for solving the bottleneck of microwave devices and electromagnetic stealth.

**Results**

Figures 2(a) and 2(b) illustrates the frequency dependence of relative complex permeability $\mu_r = \mu' - j\mu''$ magnetic loss tangent $\tan \delta_r = \mu''/\mu'$ of the LaFe$_{11.6}$Si$_{1.4}$C$_{0.2}$H$_{1.7}$/paraffin wax.

*Figure 2* (a) Frequency dependence of relative complex permeability $\mu_r = \mu' - j\mu''$; and (b) magnetic loss tangent $\tan \delta_r = \mu''/\mu'$ of the LaFe$_{11.6}$Si$_{1.4}$C$_{0.2}$H$_{1.7}$/paraffin wax.

It is known that the real permittivity ($\varepsilon'$) is an expression of polarization ability of a material which mainly arises from dipolar polarization and interfacial polarization at microwave frequency$^{22}$. The imaginary permittivity ($\varepsilon''$) follows the relation $\varepsilon'' = 1/2\pi\alpha\rho f$ according to free-electron theory, where $\rho$ is the resistivity$^{22}$. Both the real
part \(\varepsilon'\) and the imaginary part \(\varepsilon''\) of relative complex permittivity \((\varepsilon_r = \varepsilon' - j\varepsilon'')\) for the sample of \(\text{LaFe}_{11.6}\text{Si}_{1.4}\text{C}_{0.2}\text{H}_{1.7}/\text{paraffin wax}\) are expected to decrease with increasing frequency (Figure 3(a)). The dielectric loss tangent \(\tan \delta_r\) keeps almost constant of 0.35 in the frequency range of 0.1–5.0 GHz, and reaches a maximum value of 0.46 around 8.2 GHz (Figure 3(b)). For comparison, the data of paraffin wax were also plotted in Figures 3(a) and 3(b). The dielectric loss for paraffin wax is about at least one order of magnitude smaller and can be ignored. Although the fundamental understanding of what determines the dielectric loss tangent has still not been established, we can conclude the displacement current by free carriers in highly conductive \(\text{LaFe}_{11.6}\text{Si}_{1.4}\text{C}_{0.2}\text{H}_{5}\) is a main source of dielectric loss in this composite compound. The large values of the dielectric loss owing to highly conductive \(\text{LaFe}_{11.6}\text{Si}_{1.4}\text{C}_{0.2}\text{H}_{5}\) are favorable for improving the microwave absorption properties. By comparing the frequency-dependence of dielectric loss with magnetic loss, the peak of \(\tan \delta_r\) occurs usually in higher frequency range.

To further confirm the magnetic loss and dielectric loss, the reflected loss (RL) of the sample was investigated. According to the transmission line theory, for a single layer absorber with a backed metal plate, the RL were simulated from the electromagnetic parameters at various sample thicknesses by means of the following expressions\(^{23,24}\):

\[
Z_{in} = Z_0\left(\frac{\mu_r}{\varepsilon_r}\right)^{1/2}\tanh\left[j2\pi f d/\varepsilon_r\right]\left(\frac{\mu_r}{\varepsilon_r}\right)^{1/2}\tag{1}
\]
\[
RL = 20\log\left|\frac{Z_{in} - Z_0}{Z_{in} + Z_0}\right|	ag{2}
\]

where \(f\) is the frequency of the electromagnetic wave, \(d\) is the thickness of the sample, \(c\) is the velocity of light, \(Z_0\) is the impedance of air, and \(Z_{in}\) is the input impedance of the sample. The RL curves are governed by the contribution of electromagnetic wave interference from interface and by the microwave absorption. Considering the incident electromagnetic wave reflected by both the upper and lower boundaries of a thin film, the path difference of the reflected waves must be calculated in order to determine the condition for interference (figure 1(a)). According to the quarter-wave length matching model, the reflected wave and the incident wave will be out of phase by 180° at a certain frequency point, and cancel each other for the thickness of the sample satisfying the quarter-wavelength thickness relation\(^{25}\):

\[
t_m = \frac{n}{4} = \frac{nc}{4f_m\sqrt{\varepsilon_{nr}\mu_r}} (n = 1, 3, 5, \ldots)\tag{3}
\]

where \(f_m\) is the peak frequency of RL, \(t_m\) is the thickness of the sample. When the sample thickness satisfies the quarter or three-quarter of wave-length criteria, a peak or two peaks of RL appear (Figure 4). The optimal reflectivity loss of RL = \(-42.5\) dB is reached at 2.7 GHz for 7.00 mm thickness. Since the RL is mainly determined by the incident electromagnetic wave reflected by both the upper and lower boundaries of a thin film, its peak is sharper than that of magnetic loss as shown in Figure 2(c).

In addition, as shown in the projection of RL in the basal plane, the peaks of RL obviously shift to lower frequencies with increasing the sample thickness. The RL value of \(-20\) dB is comparable to the 99% of electromagnetic wave absorption according to Eqs. (1) and (2), and thus “RL < \(-20\) dB” is considered as an adequate electromagnetic absorption at a microwave frequency. For our samples, the RL < \(-20\) dB can be obtained in the 2.0–12.0 GHz range for the absorber thickness of 2.5–8.3 mm. Moreover, owing to the large magnetic loss tangent and dielectric loss tangent, a considerably large RL = \(-10\) dB can be obtained in whole frequency range of 0.1–15 GHz and thickness of 1.0–8.3 mm, suggesting that this compound is an excellent candidate for MAMs. An effective MAMs need to satisfy the impedance matching condition, \(\mu_r/\varepsilon_r = 1\).

The large magnetic loss and dielectric loss are favorable for excellent broadband EMC application. Unfortunately, the conversion of electromagnetic energy into heat will increase the MAMs temperature, which restricts the miniaturization and rapid increase in frequencies of electric devices. Moreover, the increase in MAMs temperature leads to infrared radiation since infrared light includes most of the thermal radiation emitted by objects near room temperature. The infrared radiation of MAMs will seriously hamper their application for electromagnetic stealth. Magnetic refrigeration based on MCE is a promising technique for cooling the MAMs during microwave absorption. To understand the MCE, we measured the isothermal magnetization curves of \(\text{LaFe}_{11.6}\text{Si}_{1.4}\text{C}_{0.2}\text{H}_{1.7}\) in the temperature range of 300–350 K with an interval of 2 K. Owing to the low anisotropy field, the magnetization curve at room temperature

![Figure 3](image-url) | (a) Frequency dependence of relative complex permittivity \(\varepsilon_r = \varepsilon' - j\varepsilon''\), and (b) dielectric loss tangent \(\tan \delta_r = \varepsilon''/\varepsilon'\) of the \(\text{LaFe}_{11.6}\text{Si}_{1.4}\text{C}_{0.2}\text{H}_{1.7}/\text{paraffin wax}\). For comparison, the data of paraffin wax were also plotted.

![Figure 4](image-url) | Frequency- and thickness- dependence of reflection loss (RL) for the \(\text{LaFe}_{11.6}\text{Si}_{1.4}\text{C}_{0.2}\text{H}_{1.7}/\text{paraffin wax}\) samples with different thickness.
increases sharply with applied field (Figure 5). Moreover, we also observed that almost no hysteresis loops can be discerned from the magnetization curves measured either during heating and cooling processes or during increasing and decreasing magnetic field processes. No hysteresis loops is advantageous for the application of magnetic refrigeration10.

At temperature $T$, the magnetic entropy change due to applied field $H$ can be calculated from the isothermal curves by the Maxwell relation

$$\Delta S_M(T,H) = \int_0^H \frac{\partial M}{\partial T} \, dH$$

Figure 6 displays magnetic entropy change $\Delta S_M$ as a function of $T$ and $H$ of LaFe$_{11.6}$Si$_{1.4}$C$_{0.2}$H$_{1.7}$. From the calculated $\Delta S_M$ as a function of $T$ and $H$, a giant magnetic entropy change of $-20 \text{ J kg}^{-1} \text{ K}^{-1}$ can be achieved at temperature around 330 K and applied field of 70 kOe. It is noteworthy that the MCE is not only governed by the magnetic entropy change, but also the refrigeration capacity (RC). The RC can be calculated by integrating the area under $-\Delta S_M$ vs $T$ curves within the temperature range at half-maximum of the peak. The RC was observed to increase with applied field (Figure 7).

Discussion

In order to demonstrate the useful cooling power above room temperature, Zimm et al. constructed a rotary magnetic refrigerator through a 15 kOe Nd$_2$Fe$_{14}$B permanent magnet. They found that the peak cooling capacity of LaFeSiH compares favorably with that of Gd26. Although the value of $-\Delta S_M = 7.5 \text{ J kg}^{-1} \text{ K}^{-1}$ at 20 kOe is smaller than that of La(Fe$_{1-x}$Si$_x$)H$_y$ reported by Fujita et al.27, the value of $RC = 158 \text{ J kg}^{-1}$ owing the broad peak of magnetic entropy change of our sample suggests that LaFe$_{11.6}$Si$_{1.4}$C$_{0.2}$H$_{1.7}$ compound is also a promising magnetic refrigerant.

One may further concern whether the reflection loss is reduced by the applied field during magnetic refrigeration process. Figure 8 illustrates the reflection loss for the sample with thickness of 2.0 mm measured in the applied field ranging from 0 to 1900 Oe. Since the applied magnetic field may decrease magnetic permeability at low frequency range, the reflection loss is slightly reduced with increasing applied field. However, a slight enhancement of the reflection loss with increasing applied field was observed for the frequency range of 3.0–10 GHz. Therefore, for our sample, the applied field for magnetic refrigeration does not reduce the reflection loss seriously in the frequency range of 3.0–15.0 GHz.

In conclusion, we have demonstrated that LaFe$_{11.6}$Si$_{1.4}$C$_{0.2}$H$_{1.7}$ has both excellent microwave absorption and giant magnetic entropy change around ambient temperature. The excellent electromagnetic wave absorption results from the large magnetic loss and dielectric loss as well as the efficient complementarity between relative permittivity and permeability. The giant MCE effect in this material provides an ideal technique for cooling the MAMs to avoid temperature increase and infrared radiation during microwave absorption. A prototype of magnetic cooling MAMs during microwave absorption is illustrated in Figure 1(c). To our knowledge, the results of giant microwave absorption of $-42 \text{ dB}$ and magnetic entropy change of $-20 \text{ J kg}^{-1} \text{ K}^{-1}$ in one multifunctional material have never been reported. Our finding suggests that we can integrate the microwave
absorption with magnetic refrigeration in one multifunctional material. This integration not only advances our understanding of the correlation between microwave loss and MCE, but also can open a new avenue to exploit microwave devices and electromagnetic stealth.

**Methods**

The LaFe\(_{11.6}\)Si\(_{1.4}\)C\(_{0.2}\) samples were prepared by arc-melting by appropriate proportions of Fe–C alloy, La, Fe, and Si with the purity better than 99.9 wt.%. The heat treatment was carried out in a quartz tube of high vacuum at 1373 K for 7 days. The bulk LaFe\(_{11.6}\)Si\(_{1.4}\)C\(_{0.2}\) sample was crushed into small particles (<1.5 mm), and then hydrogenated at 523 K in a hydrogen atmosphere of ~0.6 MPa for a long time until saturation. Then, extraction of hydrogen to some extent from the saturated hydride was performed under a vacuum better than \(5 \times 10^{-4}\) Pa at 250°C for different lengths of time. The hydrogen content was calculated from the variation of the sample weight before/after hydrogen absorption (desorption) and the weight was measured by an electronic analytical balance (AND GR-202) with a readability of 0.01 mg and a repeatability of 0.002 mg in the range 0–42 g. The weight of absorbed hydrogen was about 0.21 wt.% by weighing the mass before and after hydrogenation, and then the hydrogen content x was estimated to be 1.7. The method of hot extraction was generally used to determine the hydrogen content. Powder x-ray diffraction data were obtained using Cu Ka radiation at room temperature. The lattice expansion as compared to the LaFe\(_{11}\)Si\(_{1}\)C\(_{0}\) compound is \(\Delta d/d = 1.1\%\), which is corresponding to \(x = 1.7\) as previous report. The hydrogen content obtained by weighing the mass before and after hydrogenation is consistent with the result estimated from lattice expansion. All magnetic measurements were performed on a commercial MPM-7 type superconducting quantum interference device magnetometer.

The measurement scheme of magnetic and dielectric spectra is shown in Figure 9. For magnetic and dielectric spectra measurements, the LaFe\(_{11.6}\)Si\(_{1.4}\)C\(_{0.2}\)H\(_{1.7}\) was ground to powders with grain size of 30-50 μm, then mixed homogenously with paraffin wax at the mass ratio of 4:1. The LaFe\(_{11.6}\)Si\(_{1.4}\)C\(_{0.2}\)H\(_{1.7}\)/paraffin wax samples were finely pressed into the toroidal-shaped samples of 7.00 mm outer diameter and 3.04 mm inner diameter with the thickness from 2.0 to 8.3 mm. The scattering parameters of the toroidal samples that correspond to the reflection (\(S_1\) and \(S_2\)) and transmission (\(S_3\) and \(S_4\)) were measured by a vector network analyzer (Agilent N5224A) using a coaxial transmission–reflection method in the frequency range of 0.1–15.0 GHz. The toroids tightly fit into the coaxial measurement cell. Full two-port S\(_{11}\) and S\(_{22}\) parameters of the toroidal samples that correspond to the reflection (\(S_1\) and \(S_2\)) and transmission (\(S_3\) and \(S_4\)) were measured by a vector network analyzer (Agilent N5224A) using a coaxial transmission–reflection method in the frequency range of 0.1–15.0 GHz.

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**Author contributions**

Z.H.C. planned the experiments. N.N.S. and Y.J.K. carried out the microwave and magnetic entropy changes experiments. H.Z. prepared the sample. H.T.Y. and X.Q.Z. setup the microwave measurements. B.G.S. performed the microwave measurements. All the co-authors contributed to the analysis and discussion for the results. Z.H.C. wrote the paper with the input from all the co-authors.

**Additional information**

Competing financial interests: The authors declare no competing financial interests.

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