Front speed enhancement in cellular flows

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The problem of front propagation in a stirred medium is addressed in the case of cellular flows in three different regimes: slow reaction, fast reaction and geometrical optics limit. It is well known that a consequence of stirring is the enhancement of front speed with respect to the non-stirred case. By means of numerical simulations and theoretical arguments we describe the behavior of front speed as a function of the stirring intensity, $U$. For slow reaction, the front propagates with a speed proportional to $U^{1/4}$, conversely for fast reaction the front speed is proportional to $U^{3/4}$. In the geometrical optics limit, the front speed asymptotically behaves as $U/\ln U$.

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Front propagation in a stirred medium is an important problem in a number of fields ranging from combustion to plankton dynamics. For a realistic study of such a class of problems one has to take into account the modification of the advecting flow induced by the reaction, e.g. in combustion. However, many features can be understood by neglecting the back-reaction on the velocity field. The problem addressed here is the enhancement of the front speed induced by a certain class of flows. In particular, we consider front propagation in a two dimensional laminar flow with a stationary vortical structure in different regimes, namely slow reaction, fast reaction and geometrical optics limit. This last limit corresponds to a very sharp front propagating as an optical front, i.e., according to the Huygens principle. We provide predictions on the dependence of the front speed on the flow intensity, which are confirmed by numerical simulations.

1. INTRODUCTION

The study of front propagation of a stable phase into an unstable one encompasses several issues of great interest: flame propagation in gases, population dynamics of biological communities (plankton in oceans) and chemical reactions in liquids. A common feature of all these phenomena is that they take place in a strongly deformable medium such as a fluid. The interplay among transport, diffusion and reaction is therefore a crucial problem with several open issues (e.g. for questions concerning combustion see Ref. [3]).

In the most compact model of front propagation the state of the system is described by a single scalar field $\theta(x,t)$, that represents the concentration of products. The field $\theta$ vanishes in the regions filled with fresh material (the unstable phase), equals unity where only inert products are left (the stable phase) and takes intermediate values wherever reactants and products coexist, i.e., in the region where production takes place. Here we assume that the concentration of chemicals does not modify the underlying flow. Therefore, in the following, we consider the velocity field as given. This approximation, hardly tenable in the context of flame propagation in gases, is rather appropriate for chemical front propagation in some liquid solutions [2,5–7]. Under these simplifying assumptions, the evolution of $\theta$ is described by

$$\partial_t \theta + u \cdot \nabla \theta = D \Delta \theta + \frac{1}{\tau} f(\theta), \quad (1)$$

where the second term on the l.h.s. accounts for the transport by an incompressible velocity field. On the r.h.s the first term describes molecular diffusion and the second one describes the production process with time scale $\tau$. We will first consider a production term of Fischer-Kolmogorov-Petrovski-Piskunov (FKPP) type, i.e., a function $f(\theta)$ convex ($f''(\theta) < 0$) and positive in the interval $(0,1)$, vanishing at its extremes, and $f'(0) = 1$. Here we take $f(\theta) = \theta(1-\theta)$. It is also of interest to consider a production term in the form of the Arrhenius law, $f(\theta) = (1-\theta) \cdot \exp(-\theta_c/\theta)$, where $\theta_c$ is the activation concentration. The latter choice is more pertinent to the study of flames and/or chemical reactions.

Until now we did not specify any details of the velocity field. In many engineering applications $u$ is turbulent. In this paper we investigate front propagation in laminar flows, which, albeit simpler than turbulent ones, show remarkable qualitative similarities with more complex flows [3]. Specifically, we consider a two dimensional stationary incompressible flow with cellular structure (see also [10,12]) $u = (-\partial_y \psi, \partial_x \psi)$ with the streamfunction [3]

$$\psi(x,y) = \frac{UL}{2\pi} \sin\left(\frac{2\pi x}{L}\right) \sin\left(\frac{2\pi y}{L}\right), \quad (2)$$

We considered $L$-periodic boundary conditions in $y$ and an infinite extent along the $x$-axis. This kind of flow is interesting because, in contrast to shear flows, all the streamlines are closed and, therefore, the front propagation is determined by the mechanisms of contamination
of one cell to the other \[ \Box \Box \Box . \] Since we are interested in the propagation in the \( x \)-direction, the boundary conditions are set to \( \theta(-\infty, y; t) = 1 \) and \( \theta(+\infty, y; t) = 0 \). The maximum principle ensures that at later times the field still takes values in the range \( 0 \leq \theta \leq 1 \) \[ \Box \Box \Box \]. The instantaneous front speed is defined as

\[
v_t(t) = \frac{1}{L} \int_0^L dy \int_{-\infty}^{\infty} dx \partial_t \theta(x, y; t). \tag{3}
\]

This expression defines the so-called bulk burning rate \[ \Box \Box \Box \] which coincides with the front speed when the latter exists, but it is also a well defined quantity even when the front itself is not well defined. The asymptotic (average) front speed, \( v_\ell \), is determined by \( v_\ell = \lim_{T \to \infty} 1/T \int dt v_t(t) \).

In a medium at rest, it is known that Eq. \[ \Box \Box \Box \], for FKPP nonlinearity, generates a front propagating, e.g., from left to right with an asymptotic speed \( v_0 = 2\sqrt{D/\tau} \) and a reaction region of thickness \( \xi = 8\sqrt{D\tau} \). In the more interesting case of a moving medium, the front will propagate with an average speed \( v_t \) greater than \( v_0 \) \[ \Box \Box \Box \Box \Box \]. The front velocity \( v_t \) is the result of the interplay among the flow characteristics (i.e., intensity \( U \) and length-scale \( L \)), the diffusivity \( D \) and the production time scale \( \tau \). The goal of our analysis is to determine the dependence of \( v_t \) on such quantities. In particular, introducing the Damköhler number \( Da = L/(U\tau) \) (the ratio of advective to reactive time scales) and the Pécellet number \( Pe = UL/D \) (the ratio of diffusive to advective time scales), we seek for an expression of the front speed as an adimensional function \( v_t/v_0 = \phi(Da, Pe) \geq 1 \). We will see that a crucial role in determining such a function is played by the renormalization of the diffusion constant and chemical time scale induced by the advection \[ \Box \Box \Box \Box \Box \Box \].

Moreover, we consider an important limit case, i.e., the so called geometrical optics limit, which is realized for \( (Da, \tau) \to 0 \) maintaining \( D/\tau \) constant \[ \Box \Box \Box \Box \Box \Box \]. In this limit one has a non zero bare front speed, \( v_0 \), while the front thickness \( \xi \) goes to zero, i.e., the front is sharp. In this regime the front dynamics is well described by the so-called \( G \)-equation \[ \Box \Box \Box \Box \Box \Box \Box \]

\[
\frac{\partial G}{\partial t} + u \cdot \nabla G = v_0|\nabla G|. \tag{4}
\]

The front is defined by a constant level surface of the scalar function \( G(r, t) \). Physically speaking, this limit corresponds to situations in which \( \xi \) is very small compared with the other length scales of the problem. Also in this case we provide a simple prediction for the front speed, which turns out to be expressible as an adimensional function \( v_t/v_0 = \psi(U/v_0) \).

The paper is organized as follows. In Sect. \[ \Box \Box \Box \] we discuss a theoretical upper bound for the front speed which becomes an equality in the limit of (very) slow reaction. In Sect. \[ \Box \Box \Box \Box \] we present a numerical study for slow and fast reaction, comparing the results with a phenomenological model. In Sect. \[ \Box \Box \Box \Box \] we consider the geometrical optics limit. Sect. \[ \Box \Box \Box \Box \] is devoted to some concluding remarks. The Appendix contains the details of the numerical method used in the simulations.

## II. UPPER BOUND FOR THE FRONT SPEED

For a generic incompressible flow and a generic production term which has a bounded growth rate, \( c(\theta) \), i.e.,

\[
c_{\text{max}} = \sup_\theta c(\theta) = \sup_\theta \frac{1}{\tau} \frac{f(\theta)}{\theta} < \infty, \tag{5}
\]

it is possible to establish an upper bound for the speed of front propagation. Explicitly, we have

\[
v_t \leq 2\sqrt{D_{\text{eff}} c_{\text{max}}} \tag{6}
\]

where \( D_{\text{eff}} \) is the effective diffusion coefficient in the \( x \)-direction, which can be derived from Eq. \[ \Box \Box \Box \Box \] by switching off the production term. This bound is the consequence of the deeply rooted link existing between front propagation and advective transport.

We start the derivation of Eq. \[ \Box \Box \Box \Box \] by recalling the fundamental relation among the solution of the PDE \[ \Box \Box \Box \Box \Box \Box \] and the trajectories of particles advected by a velocity field \( u(r, t) \) and subject to molecular diffusion \[ \Box \Box \Box \Box \Box \Box \Box \Box \Box \Box \]

\[
\theta(x, t) = \left( \theta(r(0), 0) e^{\int_0^t c(\theta(r(s), s))ds} \right)_\eta. \tag{7}
\]

The average is performed over the trajectories evolving according to the Langevin equation

\[
\frac{dr(t)}{dt} = u(r(t), t) + \sqrt{2D} \eta(t) \tag{8}
\]

with ending point \( r(t) = x \). The white noise term \( \sqrt{2D}\eta(t) \) accounts for molecular diffusion.

Since the growth rate is bounded, \[ \Box \Box \Box \Box \Box \Box \] yields the inequality

\[
\theta(t, x) \leq \langle \theta(r(0), 0) \rangle_\eta \exp(c_{\text{max}} t). \tag{9}
\]

In the previous inequality, the term in angular brackets denotes the probability that the trajectory ending at \( x \) was initially located at the left of the front interface. For FKPP production term the maximum occurs for \( \theta = 0 \), i.e., \( c(\theta) \leq c_{\text{max}} = c(0) = 1/\tau \). Under very broad conditions, i.e., nonzero molecular diffusivity and finite variance of the velocity vector potential \[ \Box \Box \Box \Box \Box \Box \Box \Box \Box \Box \Box \Box \], it is possible to show that asymptotically the particles undergo a standard diffusion process with an effective diffusion coefficient \( D_{\text{eff}} \), always larger than the molecular value \( D \). The issue of single particle diffusion, and the problem of finding the effective diffusivity has been the subject matter of a huge amount of
work (see e.g. [22] for a recent review). In the presence of an asymptotic standard diffusion, we can substitute the term \((\theta(r(0),0))_i \delta_{ij}\) with the Gaussian result
\[
1 - \frac{1}{2} \text{erfc}(-x/\sqrt{2D_{\text{eff}}t}) \simeq \exp[-x^2/(4D_{\text{eff}}t)]/\sqrt{2\pi D_{\text{eff}}t}
\]
with exponential accuracy. We thus obtain \(\theta(x,t) \leq \exp[\varepsilon_{\text{max}}t - x^2/(4D_{\text{eff}}t)]/\sqrt{2\pi D_{\text{eff}}t}\). It is thus clear that at the point \(x\) the field \(\theta\) is exponentially small until a time \(t\) of the order of \(x/\sqrt{4D_{\text{eff}}\varepsilon_{\text{max}}}\). We finally obtain the upper bound for the front velocity \(v_f \leq \sqrt{4D_{\text{eff}}\varepsilon_{\text{max}}\tau}\), which is Eq. (6).

The bound (1) becomes an equality in the limit of very slow reaction. If \(\tau\) is the slowest time scale under consideration, advection and molecular diffusion act jointly to build an effective diffusion process, essentially unaffected by the reaction. In this case the front width is large enough and the reaction takes place in a region of effective diffusivity. Therefore, it is allowed to substitute Eq. (1) with an effective reaction-diffusion equation
\[
\partial_t \theta = \sum_{i,j} D_{ij}^\text{eff} \partial_j \theta + \frac{1}{2} f(\theta),
\]
where \(D_{ij}^\text{eff}\) is the eddy-diffusivity tensor [24]. For the FKPP nonlinearity, this last equation gives rise to \(u \simeq 2 D_{\text{eff}}/\tau\), where \(D_{\text{eff}} = D_{ij}^\text{eff} \frac{\partial}{\partial x} \frac{\partial}{\partial y} [11]\). One can find a detailed derivation of this formula in Ref. [4].

For cellular flows, it is known that \(D_{\text{eff}} \sim \sqrt{ULD}\) [23] [24]. Inserting this expression in Eq. (1) one obtains \(v_f \propto U^{1/2}\) [10], remarkably close to the observed ones for \(Da \ll 1\) (see next Section).

III. FRONT SPEED IN THE REACTION ADVECTION DIFFUSION EQUATION

The bound (1) is very general and holds for generic incompressible flows and production terms. Here, by means of numerical simulations, we consider the front propagation problem arising in the reaction advection diffusion equation [1] for the particular case of the cellular flow [2] of stirring intensity \(U\) and FKPP nonlinearity (with characteristic time, \(\tau\)). In our discussion, we always suppose that the diffusion time scale is the slowest occurring one, i.e., \(L^2/D \ll L/U, \tau\) and thus \(Pe \gg 1\) and \(Da, Pe \ll 1\).

Now before presenting the numerical results it is helpful to introduce a macroscopic description of the problem which will reduce it to an effective reaction-diffusion process with renormalized coefficients.

The basic observation is that the dynamics of \(\theta\) in cellular flows is characterized by the cell-size \(L\), so that we can perform a space discretization that reduces each cell, \(C_i\), to a point, \(i\), mapping the domain – a two-dimensional infinite strip – onto a one-dimensional lattice. The field \(\theta\) becomes a function defined on the lattice \(\Theta_i = L^{-2} \int_{C_i} \theta \, dx \, dy\). Integrating Eq. (1) over the cell \(C_i\), we obtain \(\dot{\Theta}_i = J_{i+1} - J_i + \chi_i\) where \(J_i = L^{-2} \int_{C_i} \partial_t D_{\text{eff}} \theta dx dy\) is the flux of matter through the left boundary of the \(i\)-th cell, and \(\chi_i = L^{-2} \int_{C_i} \tau^{-1} f(\theta) \, dx \, dy\)
is the rate of change of \(\Theta_i\) due to reaction taking place within the cell. On the basis of the numerical results (see below), we will show that the space-discretized macroscopic reaction-diffusion equation
\[
\frac{d}{dt} \Theta_i = D_{\text{eff}} \left( \frac{1}{2} \Theta_{i+1} - \Theta_i + \frac{1}{2} \Theta_{i-1} \right) + \frac{1}{\tau_{\text{eff}}} F(\Theta_i) \tag{10}
\]
is a pretty good model for the front dynamics. The effect of the advective field is to renormalize the values of the diffusivity, \(D \rightarrow D_{\text{eff}}(U,L)\), and the reaction time scale, \(\tau \rightarrow \tau_{\text{eff}}(U,L)\). This is why the velocity does not appear any more in the effective dynamics, described by Eq. (10) [14]. The renormalized diffusivity \(D_{\text{eff}}\) accounts for the process of diffusion from cell to cell as a result of the nontrivial interaction of advection and molecular diffusion [23] [24]. The renormalized reaction time \(\tau_{\text{eff}}\) amounts to the time that it takes for a single cell to be filled by inert material, and depends on the interaction of advection and production. Of course, also the production term will be affected, i.e. \(f \rightarrow F\), but, as we will see, such a modification is not dramatic. Indeed, the modified production term turns always to be in the FKPP universality class.

The limiting speed of the front in the moving medium turns out to be \(v_f \sim \sqrt{D_{\text{eff}}/\tau_{\text{eff}}}\), similar to Eq. (1) [4]. The problem is now reduced to derive the expressions for the renormalized parameters by means of physical considerations.

In the following sections, using as an interpretative framework the above described macroscopic model, we will present the results of detailed numerical simulations for slow \((Da \ll 1)\) and fast \((Da \gg 1)\) reaction.

A. Slow reaction regime

At small \(Da\), the reaction is significantly slower than the advection, and consequently the region where the reaction takes place extends over several cells, i.e., the front is distributed. To obtain the expression of \(D_{\text{eff}}\) we neglect the reaction term in Eq. (1), which reduces to the equation for a passive scalar in a cellular flow. This is a well studied problem, the solution of which is [23] [24]:
\[
D_{\text{eff}}/D \sim Pe^{1/2} \quad Pe \gg 1. \tag{11}
\]
For large \(Pe\) \((D\) small\) the cell-to-cell diffusion mechanism can be qualitatively understood in the following way. The probability, \(p\), for a particle to jump across the boundary of the cell, within a circulation time \(L/U\), by virtue of molecular diffusion can be estimated as the ratio of the diffusive motion across streamlines, \(O(\sqrt{DL}/U)\), to advective motion along streamlines, \(O(L)\). As a result \(p \sim (D/(UL))^{1/2}\), hence the effective diffusivity \(D_{\text{eff}} \sim pUL \sim DPc^{1/2}\).

To obtain the expression of the typical time it takes for a whole cell to react, let us concentrate on the reaction in a single cell: it is first invaded by a mixture
of reactants and products (with a low content of products, $\Theta_i \ll 1$) on the fast advective time scale; subsequently complete reaction ($\Theta_i \approx 1$) is achieved on the slower time scale $\tau_{eff} \approx \tau$ (see Fig. 1). In this regime, the front speed is well approximated the homogenization result $v_f = 2\sqrt{D_{eff}}$, discussed in the previous section.

To check these ideas, we performed numerical simulations of Eq. (1), with a FKPP production term (see appendix for details on the numerical technique). In Fig. 2, we show the result of the calculations for the front speed $v_f$ in dependence on $Da$, the slow reaction corresponds to the plateau at $Da \ll 1$.

We have now to repeat the estimation of $D_{eff}$ and $\tau_{eff}$ for the fast reaction regime, i.e., for large $Da$. Since we work always in the regime of large Peclet numbers, all the above arguments for the effective diffusion still hold, while the effective time scale is different. At large $Da$, the ratio of time scales reverses, and in a (now short) time $\tau$ two sharply separated phases emerge inside the cell. In this regime indeed, the interface is thin compared to the cell size. The cell filling process is characterized by an inward spiral motion of the outer, stable phase (see Fig. 3), at a speed proportional to $U$, as it usually happens for a front in a shear flow at large $Da$. Therefore, the $\theta = 1$ phase fills the whole cell on the advective time scale, giving $\tau_{eff} \approx L/U$.

With respect to the upper bound we observe for fast reaction a significative slowing-down of the front speed signaled by a different scaling dependence on the parameters $U, D, L, \tau$ (see Fig. 4).

**B. Fast reaction regime**

We have now to look at the shape of the effective reaction term $\tau_{eff} F(\Theta)$ for three different parameter: $Da \approx 4$ ($\square$), $Da \approx 2$ ($\circ$) and $Da \approx 0.4$ ($\times$). The continuous line shows $f(\theta)$. The dotted and dash-dotted lines are the slopes (0.2 and 0.4) proportional to $Da^{-1}$ in the region of slow advection.

We have now to look at the shape of the effective reaction term $\tau_{eff}^{-1} F(\Theta)$ appearing in the renormalized equa-
As shown in Fig. 4, for small $Da$, the effective production term is indistinguishable from the “bare” one. Increasing $Da$, the reaction rate tends to reduce, inducing the slowing-down of the front speed. For $\Theta \approx 0$, the effective production term essentially coincides with the microscopic one. However, there is an intermediate regime characterized by a linear dependence on the cell-averaged concentration, with a slope proportional to $Da^{-1}$. This is in agreement with a typical effective reaction time $\tau_{\text{eff}} \sim \tau Da$ (see below Eq. (12)). To measure the macroscopic quantities $F(\Theta)$ and $\Theta$, one simply integrates numerically both $\theta$ and $f(\theta)$ at a fixed time over a cell volume.

It is worth to remark that, notwithstanding the change of shape of the effective chemical potential, the production term remains in the FKPP universality class.

Let us stress that what we call fast reaction regime is still not in the geometrical optics limit. Indeed, to obtain this limit it is not sufficient to take $\tau$ small, but one has to take also $D$ small in such a way that $v_0 \sim 2\sqrt{D/\tau}$ is constant when $(D, \tau)$ goes to zero and the front thickness $\xi \propto \sqrt{D\tau}$ is negligible with respect to the cell size. In the fast reaction regime studied here the condition on the front thickness holds.

Collecting the information about fast and slow reaction

$$\frac{\tau_{\text{eff}}}{\tau} \sim \begin{cases} 1 & Da \ll 1 \\ Da & Da \gg 1. \end{cases}$$  \hspace{1cm} (12)$$

and $D_{\text{eff}} \sim DPe^{1/2}$, we can derive the scaling of the effective speed of front propagation for a cellular flow. Indeed, recalling that $v_1 \sim \sqrt{D_{\text{eff}}/\tau_{\text{eff}}}$, we have the final result

$$\frac{v_1}{v_0} \sim \begin{cases} Pe^{1/4} & Da \ll 1, Pe \gg 1 \\ Pe^{1/4}Da^{-1/2} & Da \gg 1, Pe \gg 1 \end{cases}$$  \hspace{1cm} (13)$$

The case of $Pe \ll 1$ is less interesting because the dynamics is dominated by diffusion.

At small $Da$ the front propagates with an effective velocity scaling as the upper bound derived above, that is as $Pe^{1/4}$. At large $Da$, the front speed enhanced is less effective than at small $Da$: according to Eq. (12), we have $v_1/v_0 \sim Da^{-1/2}$ for $Da \gg 1$. In terms of the typical velocity of the cellular flow, we have $v_1 \propto U^{1/4}$ for slow reaction ($U \gg L/\tau$, or equivalently $Da \ll 1$) whereas $v_1 \propto U^{3/4}$ for fast reaction ($U \ll L/\tau$, or $Da \gg 1$). The scaling $v_1 \propto U^{1/4}$ for slow reaction (i.e., fast advection) is a consequence of the well known result $D_{\text{eff}} \propto DPe^{1/2}$ in the homogenization limit [11,14], it has been obtained in [17]. The numerical results are summarized in Fig. 4.

As a remark we mention that, for the class of boundary conditions investigated here, where the region of initially burnt material extends to infinity, no quenching [28] takes place no matter of the used production term. Indeed, Arrhenius-type nonlinearity substantially gives the same results as those of FKPP-type reaction presented above, i.e., one has the two scaling laws $v_1 \propto U^{1/4}$ and $v_1 \propto U^{3/4}$ at fast and slow advection respectively (see [44]).

**IV. FRONT SPEED IN THE GEOMETRICAL OPTICS REGIME**

When the front thickness and the reaction time are much smaller than the length and time scales of the velocity field fluctuations one has the geometrical optics regime [44,27]. In this case the front is a sharp interface separating the reactants from the products, and can be modeled in the framework of the $G$-equation [11,14,16]. Physically speaking, one uses the $G$-equation when the front thickness is very thin and it is hard to resolve the diffusive scale.

As far as the cellular flow is concerned, the front border is wrinkled by the velocity field during propagation and its length increases until pockets of fresh material develop [28,30]. After this, the front propagates periodically in space and time with an average speed $v_1$, which is enhanced with respect to the propagation speed $v_0$ of the fluid at rest [31] (see Ref. 29 for some pictorial views).

The problem addressed here is the dependence of the effective speed $v_1$ on the flow intensity, $U$, and the bare velocity, $v_0$, that is expected of the form [11]:

$$\frac{v_1}{v_0} = \psi \left( \frac{U}{v_0} \right),$$  \hspace{1cm} (14)$$

where $\psi(U)$ is a function which depends on the flow details.

As far as we know, apart from very simple shear flows (for which $\psi(U) = 1 + U$ [10,16]), there are no methods...
to compute $\psi(U)$ from first principles. Mainly one has
to resort to numerical simulations and phenomenological
arguments.

For turbulent flows, by means of dynamical renormal-
ization group techniques, Yakhot \cite{32} proposed
\begin{equation}
\frac{v_1}{v_0} = e^{(U/v_0)\alpha} \tag{15}
\end{equation}
with $\alpha = 2$. Now $U$ indicates the root mean squared
average velocity (see also \cite{14,15}). Therefore, from \cite{14}
one has that $v_1 \to U/\sqrt{\ln(U)}$ for $U \to \infty$.

For the cellular flow under investigation, albeit the ex-
act form of the function $\psi(U)$ is not known, a simple
argument can be given for an upper and a lower bound
by mapping the front dynamics onto a one-dimensional
problem. The starting point is the following observa-
tion. In the optical regime, since the interface is sharp,
i.e., $\theta(x,y)$ is a two-valued function ($\theta = 1$ and $\theta = 0$),
we can track the farther edge of the interface between
product and material $(x_M(t), y_M(t))$, which is defined
as the rightmost point (in the $x$-direction) for which
$\theta(x_M, y_M; t) = 1$. Then we can define a velocity
\begin{equation}
\hat{v}_f = \lim_{t \to \infty} \frac{x_M(t)}{t}, \tag{16}
\end{equation}
which gives an equivalent value of the standard definition
within less than 2\% (see Fig. 6).

\begin{figure}[h]
\centering
\includegraphics[width=0.5\textwidth]{fig6}
\caption{Front velocity as a function of time, $v_1(t)$ mea-
sured in the standard way \cite{13} (C), and as in Eq. \cite{14} (o).
The straight lines represents the average (over a period) of
the measured value, and the lower and upper bounds. The
simulation parameters are $U = 4$, $v_0 = 1$ and $L = 2\pi$.
}
\end{figure}

In Fig. 6 we show the time evolution of the point
$(x_M(t), y_M(t))$. After a transient, in the unit cell $[0, 2\pi]$.
we describe the case $L = 2\pi$, i.e., the one adopted here)
the point $(x_M(t), y_M(t))$ moves to the right along the
separatrices of the streamfunction \cite{13}, so that $y_M(t)$ is
essentially close to the values 0 or $\pi$. Along this path one
can reduce the edge dynamics to the 1d-problem
\begin{equation}
\frac{dx_M}{dt} = v_0 + U\beta |\sin(x_M(t))| \tag{17}
\end{equation}
where the second term of the r.h.s. is the horizontal
component of the velocity field. We have neglected the
$y$-dependence, replacing it with a constant $\beta$ which takes
into account the average effect of the vertical component
of the velocity field along the path followed by $(x_M, y_M)$.
By solving \cite{17} in the interval $x_M \in (0, 2\pi)$ one obtains
the time, $T$, needed for $x_M$ to reach the end of the cell.
The front speed, as the speed of the edge particle, is then
given by $v_1 = 2\pi/T$. The final result is
\begin{equation}
\psi_{\beta}(U) = \pi \sqrt{(U\beta)^2 - 1} \ln^{-1} \left( \frac{U + \sqrt{(U\beta)^2 - 1}}{U - \sqrt{(U\beta)^2 - 1}} \right) \tag{18}
\end{equation}
Note that (18) is valid only for $U\beta \geq 1$.

\begin{figure}[h]
\centering
\includegraphics[width=0.5\textwidth]{fig7}
\caption{Time evolution of the edge point: $x_M(t)$ (solid line)
and $y_M(t)$ (dashed line). The simulation parameters are the
ones of Fig. 6}
\end{figure}

We have taken $\beta = 1$ for the upper bound and $\beta = 1/2$
(which is the average of $|\cos(y)|$ between 0 and $\pi$) for
the lower bound. We have also computed the average
of $|\cos(y_M(t))|$ in a period of its evolution (see Fig. 7)
getting $\beta \approx 0.89$ which gives indeed a very good ap-
proximation of the measured curve (see Fig. 8). We stress
that the theoretical curve is not a fit, but it just involves
the measured parameter $\beta$.

This agreement is an indication that the average of
$|\cos(y_M(t))|$ depends on $U$ and $v_0$ very weakly (as we
checked numerically). Previous studies \cite{33} reported an
essentially linear dependence of the front speed on the
flow intensity, i.e., $v_1 \propto U$ for large $U$ which is not too
far but different from our result. A rigorous bound has
been obtained in Ref \cite{34} by using the G-equation:
\begin{equation}
v_1 \geq U/\ln(1 + U/v_0) \tag{19}
\end{equation}
As one can see from Fig. 8, the lower bound \cite{19} seems
to be closer to the numerical data than the one obtained
with $\beta = 1/2$ in \cite{18}. From Eq. \cite{18}, asymptotically (i.e.
for $U \gg v_0$) one has: $v_1 \sim U/\ln(U)$ which corresponds
to \cite{13} for $\alpha = 1$. 


the Yakhot formula (15) with 

A definite answer to this question is beyond the scope of this paper, however it could be an interesting point for future investigations.

V. CONCLUSIONS

We addressed the problem of front speed enhancement induced by stirring due to a cellular flow in different regimes. In the slow reaction case a rather general result (based on homogenization techniques) gives \( v_f \sim U^{1/4} \); for the fast reaction case, physical arguments give \( v_f \sim U^{3/4} \). In the geometrical optics limit one finds that \( v_f \) is a linear function of \( U \), apart from logarithmic corrections. All these results has been confirmed by numerical simulations.

The steady cellular flow treated here, albeit its simplicity, provides a paradigm that can be insightful for the study of front propagation in more general flows. For instance, in the geometrical optics limit the asymptotical behavior \( v_f \sim U / \ln(U) \) is rather similar to the one found by Yakhot \( (v_f \sim U / \sqrt{\ln(U)}) \) for turbulent velocity fields.

One could conjecture that there are nontrivial reasons for this similarity: the front propagation principally involves the largest scales. In this context, it is not surprising that a multiscale process (as turbulence) or a single scale process can yield similar results.

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APPENDIX A: NUMERICAL METHOD

We introduce a lattice of mesh size \( \Delta x \) and \( \Delta y \) (for the sake of simplicity we assume \( \Delta x = \Delta y \)) so that the scalar field is defined on the points \( x_{n,m} = (n \Delta x, m \Delta y) \):

\[ \theta_{n,m}(t) = \theta(n \Delta x, m \Delta y, t) \]

Giving the field at time \( t \), the algorithm computes the field at time \( t + \Delta t \), and the integration method depends on which kind of physical regime we are interest in: reaction-advection-diffusion equation (1) or optical limit (4).

1. Reaction Diffusion Equation

In numerical approaches one is forced to discretize the dynamics, so let us consider the case of a velocity field which is always zero apart from \( \delta \)-impulses at times \( t = 0, \pm \Delta t, \pm 2 \Delta t, \pm 3 \Delta t, \ldots \)

\[ u(x, t) = \sum_{n=-\infty}^{\infty} u(x) \delta(t - n \Delta t) . \tag{A1} \]

In such a case the Lagrangian evolution is given by a conservative map (in 2d the map is symplectic due to incompressibility)

\[ x(t + \Delta t) = F^{\Delta t}(x(t)) . \tag{A2} \]

If also the production term is zero apart from \( \delta \)-impulses

\[ f(\theta) = \sum_{n=-\infty}^{\infty} g(\theta) \delta(t - n \Delta t) , \tag{A3} \]

one can introduce a reaction map

\[ \theta(t + \Delta t) = G_{\Delta t}(\theta(t)) . \tag{A4} \]

Let us remark that choosing a \( \delta \)-impulsed production term can be particularly relevant in some experimental settings, i.e., when one considers periodic illumination in light-sensitive chemical reactions as in Ref. [37].
The concentration field $\theta(x, t + \Delta t) - 0$ is obtained from $\theta(x, t+0) = G_{\Delta t}(\theta(x, t))$ solving the bare diffusion equation $\partial_t \theta = D \nabla^2 \theta$:

$$\theta(x, t + \Delta t) = \frac{1}{(2\pi)^{d/2}} \int e^{-\frac{1}{2} \theta(x - \sqrt{2D \Delta t} \eta, t + 0)} \, d\eta,$$  \hspace{1cm} (A5)

or, in other terms:

$$\theta(x, t + \Delta t) = \left\langle G_{\Delta t}(\theta(F^{-\Delta t}(x - \sqrt{2D \Delta t} \eta), t), t) \right\rangle_\eta$$ \hspace{1cm} (A6)

which is equivalent to Eq. (A4). Let us remark that Eq. (A6) is exact if both the velocity field and the reaction are $\delta$-impulsed processes. However one can also use the formula (A6) as a practical method for the numerical integration of Eq. (A4) if one assumes small enough $\Delta t$, so that the Lagrangian and reaction maps are given at the lowest order by

$$F^{\Delta t}(x) \simeq x + u(x) \Delta t, \hspace{1cm} G_{\Delta t} \simeq \theta + \frac{\Delta t}{\tau_r} f(\theta).$$

From an algorithmic point of view the whole process between $t$ and $t + \Delta t$, Eq. (A6), can be divided into three steps: (1) diffusive, (2) advective and (3) reactive. The first two steps determine the origin of the Lagrangian trajectory evolving with a given noise realization $\eta$ and ending in $x$. In the third step, the reaction at point $x$ for the advected/diffused passive scalar $\theta$ is computed:

1) backward diffusion: $x \rightarrow x - \sqrt{2D \Delta t} \eta$

2) backward advection by the Lagrangian map:
$$x - \sqrt{2D \Delta t} \eta \rightarrow F^{-\Delta t}(x - \sqrt{2D \Delta t} \eta)$$

3) forward reaction:
$$\theta(t + \Delta t) = G_{\Delta t}(\theta(t)).$$

This three steps can be numerically implemented as follows. For each grid point $x_{n,m}$, one uses $N$ independent Gaussian processes $W^\alpha$, $\alpha = 1, \ldots, N$, $N \gg 1$, and computes $\tilde{x}_{n,m}^\alpha = x_{n,m} - \sqrt{2D \Delta t} W^\alpha$. Then, using the Lagrangian backward propagator, $r_{n,m}^\alpha = F^{-\Delta t}(\tilde{x}_{n,m}^\alpha)$. For $\theta_{n,m}(t + \Delta t)$ one needs the values of $\theta$ at time $t$ in the positions $r_{n,m}^\alpha$. Typically the $r_{n,m}^\alpha$ are not on the grid points $(n \Delta x, m \Delta y)$, nevertheless we can compute the value $\theta(r_{n,m}^\alpha, t)$ using simple linear interpolation from $\theta_{n,m}(t)$. Therefore we have

$$\theta_{n,m}(t + \Delta t) = \frac{1}{N} \sum_{\alpha=1}^{N} G[\theta(r_{n,m}^\alpha, t)].$$

2. Geometrical optics limit

Similar to the previous case, one can integrate the dynamics of the optical front using a two step discrete-time process.

![Pictorial scheme of the numerical algorithm for RAD systems.](image)

To correctly simulate the diffusion process we have to impose a relation between $D$, $\Delta x$ and $\Delta t$ to assure that diffusion transports a particle over distances $\sim \sqrt{2D \Delta t}$ much larger than the grid size $\Delta x$ (see Fig. 9).

![Pictorial scheme of the numerical algorithm for the geometrical optics limit.](image)

Starting from the field $\theta_{n,m}$ at time $t$, one can obtain the field at time $t + \Delta t$ with the following algorithm

1) using the Lagrangian propagator one evolves the interface between burned and unburned region;

2) at each point of the evolved interface one constructs a circle of radius $v_0 \Delta t$, burning the points within the circles.
To numerically implement such an algorithm one can proceed as follows: starting in a grid point, \( x_{n,m} \), of the scalar field at time \( t + \Delta t \) one applies the backward evolution arriving at the point \( y = F^{-\Delta}x_{n,m} \) at the time \( t \). In this point we construct the circle of radius \( v_0 \Delta t \). If in this circle there is at least one burned point of the scalar field at time \( t \), we fix \( \theta(x_{n,m}; t + \Delta t) = 1 \) otherwise \( \theta(x_{n,m}; t + \Delta t) = 0 \).

Also in this case we have to care about the radius of circle \( v_0 \Delta t \) has to be much larger than the grid size \( \Delta x \).

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