Research on the reinforcement measures of close-parallel tunnels

Li Meng¹, Hu Ping¹, and Ma Liang¹

¹School of Civil Engineering and Architecture, University of Jinan, Jinan 250022, China

Abstract. Based on shallow parallel underground tunnel and double-line shield tunnel of Jinan Rail Transit Line R3, this paper proposes two reinforcement measures including bored piles and curtain grouting in the middle of the tunnel, making a numerical analysis and comparison of the reinforcement effect. The results show that the influence of later tunnel construction on the deformation of earlier tunnel can be effectively reduced after taking two reinforcement measures respectively and the reinforcement effect of the bored piles is better.

1 Introduction

With the increase in parallel construction of small-pitch tunnels⁴, the resulting engineering risks and construction difficulties are also increasing⁴⁻⁶. For small-pitch tunnels, especially small-pitch tunnel groups constructed by different construction methods (such as shield tunnels and shallow buried tunnels), the squeezing and unloading effect of the later tunnel on the earlier tunnel will cause great disturbance to the earlier tunnel structure and surrounding rock and soil bodies, thus affecting the stability and safety of the tunnel. When the clear distance of the tunnel is too small, certain reinforcement measures should be taken to increase the stability of the surrounding rock, so as to reduce the deformation of the surrounding rock of the tunnel and reduce the risk of the tunnel. Therefore, it is of great engineering significance to study the reinforcement measures of tunnels under the condition of small clear distance parallel construction.

Based on shallow parallel underground tunnel and double-line shield tunnel of Jinan Rail Transit Line R3, this paper proposes two methods for the construction and reinforcement of small-pitch tunnels suitable for this project, namely curtain grouting method and drilling bored pile method. MIDAS/GTS software is used to numerically simulate the two reinforcement methods and analyze the reinforcement effects. It will provide technical support and reference for similar projects in the future.

2 Project Overview

The section between Longdongzhuang Station and Mengjiazhuang Station of Jinan Rail Transit Line R3 consists of three parallel tunnels. The tunnel in the middle adopts shallow burying method (CD construction method), which is divided into two guide tunnels A and B to be constructed first. After that, the tunnels on both sides are constructed by shield method. The left line goes first, and the right line follows. During excavation, the two lines are bilaterally symmetrical and are at the same level as the previous shallow buried tunnel. And the horizontal clear distance gradually decreases. The minimum horizontal clear distance is only 2.55m, which is much smaller than the tunnel diameter. The tunnel section layout is shown in Figure 1.

The structure of the shallow buried tunnel is a single-hole, two-line horseshoe tunnel with a cross-section clearance of 11.7×8.59m (width×height). The tunnel section is divided into two small guide tunnels and excavated successively with CD construction method. And the tunnel shall be supported in advance before it is excavated. Two shield machines are selected in the shield tunnel section, where the left line goes first and the right line is behind, starting from the long-mile end of Longdong Station. The diameter of the shield tunnel is 6.4m and the thickness of the segment is 0.3m. Cement mortar is used as the synchronous grouting material in the shield tunnel.

3 Reinforcement measures and effect analysis

3.1 Reinforcement measures

For the three-hole small-pitch tunnels in this project,
when the shields on both sides of the tunnel are under construction, it can no longer meet the safety requirements that only supporting the intermediate tunnel or adjusting and optimizing the shield construction parameters through monitoring data. Certain reinforcement measures should be taken in the middle stratum of the tunnel, more importantly. On the basis of summarizing the existing reinforcement measures, the actual engineering conditions and the feasibility of construction, two types of reinforcement measures are proposed: (1) Curtain grouting reinforcement in the middle stratum; (2) Drilling and pouring piles are reinforced in the middle stratum.

### 3.2 Model establishment and parameter selection

MIDAS/GTS software is used for numerical simulation. The equivalent parameters of the rock-soil body and supporting structure before reinforcement are shown in Table 1, and the Mohr-Coulomb elastoplastic model is used for the soil constitutive model. The properties of the reinforced soil are obtained by adjusting the physical and mechanical parameters of the soil. And the parameters of the intermediate stratum after reinforcement are shown in Table 2. The model size is selected to be 100m×60m (width×height). And the clear distance between tunnels is 0.8D. The models of curtain grouting and cast-in-place bored piles are established as shown in Figure 2 and Figure 3 respectively.

#### Table 1. Equivalent parameters of soils and supporting structure before reinforcement

| Material layer                                      | Mass density (kN/m³) | Internal friction angle(°) | Cohesion (kPa) | Lateral pressure coefficient | Thickness (m) | Elastic Modulus (MPa) | Poisson's ratio |
|-----------------------------------------------------|----------------------|----------------------------|----------------|----------------------------|----------------|-----------------------|---------------|
| plain fill                                          | 18.90                | 15.00                      | 20.00          | 0.38                       | 0.80           | 47.48                 | 0.40          |
| silty clay                                          | 18.90                | 13.10                      | 20.30          | 0.41                       | 8.60           | 45.46                 | 0.29          |
| gravel soil                                         | 21.00                | 38.00                      | 10.00          | 0.25                       | 7.60           | 73.63                 | 0.20          |
| medium-weathered limestone                          | 26.90                | 39.00                      | 700.00         | 0.18                       | 43.00          | 3.23×10⁴               | 0.18          |
| Advanced small catheter reinforcement area          | 21.00                | 38.00                      | 100.00         | 0.28                       | 0.80           | 100.00                | 0.22          |
| shield segment                                      | 25.00                | /                          | /              | /                          | 0.30           | 2.23×10⁴               | 0.20          |
| equivalent layer                                    | 25.00                | /                          | /              | /                          | 0.15           | 1.20                  | 0.20          |
| initial support                                     | 22.00                | /                          | /              | /                          | 0.35           | 1.5×10⁴               | 0.20          |
| initial support hardening                           | 22.00                | /                          | /              | /                          | 0.35           | 3.0×10⁴               | 0.40          |

#### Table 2. Equivalent parameters of reinforced soil

| Material layer                                      | Mass density (kN/m³) | Internal friction angle(°) | Cohesion (kPa) | Lateral pressure coefficient | Thickness (m) | Elastic Modulus (MPa) | Poisson's ratio |
|-----------------------------------------------------|----------------------|----------------------------|----------------|----------------------------|----------------|-----------------------|---------------|
| the section of curtain grouting reinforcement        | 21.00                | 38.00                      | 100.00         |                            |                |                       |               |
| The section of bored cast-in-place piles reinforcement| 22.00                | 36.00                      | 100.00         |                            |                |                       |               |

| Material layer                                      | Lateral pressure coefficient | Thickness (m) | Elastic Modulus (MPa) | Poisson's ratio |
|-----------------------------------------------------|------------------------------|----------------|-----------------------|---------------|
| the section of curtain grouting reinforcement        | 0.28                         | 6.40           | 100.00                | 0.22          |

#### The section of bored cast-in-place piles reinforcement 0.28 1.00 100.00 0.22

Fig.2. reinforced model of curtain grouting
3.3 Effect analysis of different reinforcement schemes

3.3.1 Horizontal displacement

Table 3 shows the headroom convergence values of the middle leading tunnel under different reinforcement conditions during tunnel excavation on both sides. It can be seen from Table 3 that the headroom convergence values of the A and B holes of the intermediate tunnel will change greatly after the construction of the shield tunnels on the left and right sides is completed, if no reinforcement measures are taken before. However, the clearance of the intermediate tunnels A and B will not change much compared with the initial support if curtain grouting and bored piles are used for reinforcement. It shows that both of two schemes can effectively reduce the influence of the horizontal deformation of the preceding tunnel during the construction of the following tunnel.

![Fig. 3. Reinforced model of bored cast-in-place piles](image)

Table 3. Clearance Convergence of the shallow buried tunnel

| Working condition          | Position | Clearance convergence (mm) | Unreinforced | Curtain grouting | Bored cast-in-place piles |
|---------------------------|----------|----------------------------|--------------|------------------|--------------------------|
| Excavation of the middle tunnel | Hole A   | 6.46                        | \             | \                | \                        |
|                           | Hole B   | -5.27                       | \            | \                | \                        |
| Reinforcement measures construction | Hole A   | -7.05                       | 6.51         | \                | \                        |
|                           | Hole B   | \                          | -5.66        | -5.30            |                          |
| Excavation of the left tunnel | Hole A   | 4.97                        | 6.74         | 6.32             |                          |
|                           | Hole B   | -5.12                       | -5.65        | -5.31            |                          |
| Excavation of the right tunnel | Hole A   | 4.80                        | 6.72         | 6.33             |                          |
|                           | Hole B   | -4.03                       | -5.33        | -5.17            |                          |

It can also be found from Table 3 that the clearance of holes A and B of the middle tunnel has increased compared with the horizontal displacement during construction when curtain grouting is applied to the middle stratum. This shows that curtain grouting in the middle stratum will cause the tunnel surrounding rock to move into the tunnel. And the reason is that the pressure of the initial support of the soil around the intermediate tunnel increases due to the vibration of the machine and the pressure of grouting when drilling. As a result, the horizontal displacement of the soil increases and the surrounding rock moves inward. However, the deformation of the intermediate tunnel is relatively small when using bored piles for reinforcement, because the influence range of the slurry pressure is small and the distance between the pile and the tunnel is large.

![Fig. 4. Vertical displacement cloud image of the middle tunnel under the curtain grouting scheme](image)

![Fig. 5. Vertical displacement cloud image of the middle tunnel under the bored pile scheme](image)

3.3.2 Vertical displacement

Figure 4 and Figure 5 are the vertical displacement clouds of the three-hole tunnel under different reinforcement conditions. It can be seen that the vault settlement of the vault of the three-hole tunnel will still overlap with that of the upward arch uplift if curtain grouting is used to reinforce the middle stratum at the same level in the three-hole tunnel. And this means that the excavation of the back shield tunnel at this time will still affect the vertical deformation of the previous tunnel. However, the vault settlement map is shown as three unrelated parts due to the splitting effect of the piles when bored piles are installed in the middle stratum. At this time, the impact of the excavation of the later shield tunnel on the vertical displacement of the earlier tunnel will be greatly reduced.

Table 4 shows the vault settlement and invert arch uplifting values of the middle tunnel under different reinforcement conditions during the excavation of the tunnels on both sides. It can be seen from Table 4 that the settlement and vaulting of the vault of the first shallow buried tunnel are greatly reduced compared with the case without reinforcement when curtain grouting and bored cast-in-place piles are used for reinforcement. And it means that both of two kinds of reinforcement...
measures can effectively reduce the influence of the vertical deformation of the first shallow buried tunnel when the subsequent shield tunneling. In comparison, the numerical value of the measures for drilling bored piles is greater, which means that the reinforcement of the measures for drilling bored piles can better control the vertical displacement of the first shallow buried tunnel.

### Table. 4. Vertical displacement of the early shallow buried tunnel

| Working condition         | Vault settlement (mm) | Uplift (mm) |
|---------------------------|-----------------------|-------------|
|                           | Unreinforced | Curtain grouting | Bored cast-in-place piles |
| Excavation of the middle tunnel | -6.17        | \             | \                        |
| Reinforcement measures construction | \             | -6.34        | -6.18                    |
| Excavation of the left tunnel    | -7.67        | -6.92        | -6.32                    |
| Excavation of the right tunnel    | -9.12        | -7.42        | -6.41                    |

From the above analysis, it can be seen that curtain grouting in the middle of the stratum and the construction of bored piles both can effectively reduce the impact of the deformation of the first shallow buried tunnel when the subsequent shield tunneling. However, the surrounding rock moves into the middle tunnel because of the curtain grouting scheme. At the same time, the vertical displacement of the three-hole tunnel still overlaps. And the horizontal displacement, vault settlement and uplift of the leading tunnel in the middle of the shield tunnel excavation on both sides are bigger than those under the measures of drilling and pouring piles. It is proved that the use of drilling bored piles can better control the deformation effect of the subsequent shield excavation on the first shallow buried tunnel.

### 4 Conclusions

Based on the analysis of deformation control measures of small spacing tunnel, two reinforcement measures, namely curtain grouting method and bored pile method, which are suitable for the project, are put forward. Through the analysis of the two reinforcement methods by the use of MIDAS/GTS software, it can be seen that curtain grouting in the middle of the stratum and the construction of bored piles both can effectively reduce the impact of the deformation of the first shallow buried tunnel when the subsequent shield tunneling. In comparison, the use of bored piles can better control the deformation and displacement of the first shallow buried tunnel. Although the tunnel clearance decreases, the deformation of the first shallow buried tunnel is still slightly increased when the next shield tunnel is excavated after the bored piles are installed. But the change is not significant and is far less than its deformation control value. And the plastic zone no longer overlaps, which makes the construction of ultra-small clearance safe.

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