Phase Diagram and Order Reconstruction Modeling for Nematics in Asymmetric π-Cells

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Abstract: Intense electric fields applied to an asymmetric π-cell containing a nematic liquid crystal subjected to strong mechanical stresses induce distortions that are relaxed through a fast-switching mechanism: the order reconstruction transition. Topologically different nematic textures are connected by such a mechanism that is spatially driven by the intensity of the applied electric fields and by the anchoring angles of the nematic molecules on the confining plates of the cell. Using the finite element method, we implemented the moving mesh partial differential equation numerical technique, and we simulated the nematic evolution inside the cell in the context of the Landau–de Gennes order tensor theory. The order dynamics have been well captured, putting in evidence the possible existence of a metastable biaxial state, and a phase diagram of the nematic texture has been built, therefore confirming the appropriateness of the used technique for the study of this type of problem.

Keywords: nematic asymmetric cell; nematic biaxiality; order reconstruction; nematic liquid crystals; MMPDE; FEM

1. Introduction

Bistable behaviors in nematic liquid crystals (NLCs) play a crucial role for their optical and switching properties. They can arise in the biaxial domains of such materials as a consequence of distortions of the nematic texture when the biaxial coherence length $\xi_b$ is comparable to the length scale of the nematic distortion [1]. In fact, thermotropic NLCs are rod-like molecules possessing cylindrical symmetry and exhibiting orientational order. For such reason, a dimensionless unit vector $n$, the director, is identified as suitable to describe the NLC long axis average orientation in most electro-optical phenomena, while the scalar order parameter $S$ accounts for the degree of order along the $n$ direction. Due to the cylindrical symmetry, NLCs are said to be uniaxial [2], as they possess a unique optical axis.

On the other hand, local and continuous changes of the director orientation inside uniaxial nematic textures can happen [3–10]. By applying a distortion capable to break the uniaxial symmetry, two distinct optical axes arise inside the NLCs, giving rise to bistable behaviors which lower the degree of order, and their description is made by coupling the $n$ and $S$ parameters in the frame of the Landau–de Gennes order tensor theory [2,11].

The optical and switching properties of NLCs are experimentally investigated using the π-cell, a device in which a thin nematic film is confined between two flat glass plates. In order to obtain on both surfaces a nematic alignment exhibiting strong anchoring energy and a given pre-tilt angle $\theta$, the internal surfaces are appropriately treated [12]. The generation of a splayed texture is ensured by an anti-parallel arrangement of the two plates [12] (Figure 1a). Such a configuration permits the existence of a second texture which is topologically distinct from the first one, where the nematic is π-twisted (or π-bent) (Figure 1c), while any spontaneous relaxation from each other is prevented by the energy barrier existing between them. The splayed texture can be transformed...
into the topologically different bent texture under the action of an electric field applied perpendicular to the boundary plates, a textural switch mediated by the biaxial order reconstruction (Figure 1b), a mechanism which connects two competing uniaxial textures through a wealth of transient biaxial states in the nanometric scale [12], and allowing for changing the local order of the nematic phase, avoiding any macroscopic rotation of the unit vector $n$. More generally, studies putting forth evidence of biaxial structural transitions induced by electric [13–16] or mechanical fields [17], growth of biaxial domains in the bulk and at the NLC interface [18–21], or surface effects [22,23] have been performed, while it is also found that further relaxation mechanisms become possible if strong anchoring asymmetries operate [22–24].

Figure 1. Geometry of the $\pi$-cell with nematic molecules in different states: (a) horizontal alignment with a slight splay; (b) intermediate state with a thin wall in the center; and (c) mostly vertical alignment ($\pi$-bent).

In a recent series of papers [24–27], we studied the order dynamics of a 5CB NLC confined inside a $\pi$-cell and solved the partial differential equation (PDE) system arising from the modeling, implementing the moving mesh PDE (MMPDE) numerical technique using the finite element method (FEM). Such an adaptive grid technique, which is of the r-type [28], relies on domain discretization typical of the FEM in which the number of mesh points is kept constant; the nodes instead move driven by a monitor function, a suitable functional of the order parameter (in our case of the order gradient $\nabla Q$) which causes the nodes to cluster toward regions with growing $\nabla Q$, where greater accuracy is required, and vice versa. This results in an efficient and effective numerical tool, which is appropriate to model the order dynamics of the liquid crystals confined between plates, allowing reliable results to be obtained, aside from resolution improvement [25]. Moreover, with respect to computational techniques based on uniform discretizations, the MMPDE method allows computational savings. In fact, the domain regions of growing $\nabla Q$ are a priori unknown, but the mesh points are moved from time to time toward regions of high variability, always keeping them constant in number. The order dynamics of a nematic confined in a $\pi$-cell with symmetric [26,27] or asymmetric [24] anchoring angles has been studied using the MMPDE technique. Denoting with $E_{th}$ a threshold level for applied electric field...
(AEF) amplitudes above which an order reconstruction transition occurs in the bulk of an NLC confined in a \( \pi \)-cell with symmetric anchoring conditions [12], applied fields with amplitudes not too far beyond \( E_{th} \) induce distortions in the cell center, which relax by means of an order reconstruction transition [26]. AEFs with higher amplitudes are instead capable of inducing other phenomena, such as delocalization of the order reconstruction transition, transient order lowering, and transitions of the nematic textures from splay to bend configuration (Figure 1), exhibiting first- and second-order features [27]. On the other hand, if asymmetric pre-tilt angles are imposed on the \( \pi \)-cell, the nematic distortion relaxes by means of a growing biaxiality propagating toward the boundary surface, identified by the smaller anchoring angle [23]. At this stage, depending on the choice of the amplitude of the applied electric pulse \( E \) and of the pre-tilt angle \( \theta_U \), the planar nematic texture imposed on the boundary surface can be connected to the nematic molecules aligned vertically along the field direction through either a bulk- or surface-order reconstruction transition [24]. Further, monitoring the order evolution as a function of the applied electric pulse amplitude \( E \) and the anchoring angle of the nematic on the upper boundary surface \( \theta_U \) allows one to clearly distinguish bulk- from surface-order reconstruction occurring in the cell and to compute a partial phase diagram in which the nematic texture is mapped according to its switching mechanism [24]. In particular, we obtained a partition of the \((E, \theta_U)\) plane in regions where the modeled nematic texture obeys mechanisms with bulk switching, surface switching, or no switching at all. Nevertheless, the mapped region is a limited part of the phase diagram whose extension requires the investigation of more and more \((E, \theta_U)\) pairs in order to predict the phase boundaries among all possible switching regimes. Since increasing amplitudes of the applied electric pulse, as well as the marked asymmetries, induce nano-confined strong distortions in the NLC [23,24,27], being the scale of the physical problem, instead, in the micrometer range, a sophisticated computational technique is needed to obtain more reliable results. Following such an idea, in this work, we simulated a 5CB NLC confined in an asymmetric \( \pi \)-cell and subjected it to AEFs with amplitudes extending far beyond \( E_{th} \). The time-dependent governing equations have been solved using the MMPDE numerical technique, and the biaxial order dynamics as well as the \( Q \)-eigenvalues have been monitored while imposing variable degrees of asymmetry. Moreover, being the order reconstruction transition confined within the duration of the applied electric pulse, material flow effects have been neglected [29].

The paper has the following organization. In Section 2, we introduce the order tensor model, while in Section 3, we describe the computational technique. In Section 4, the results are presented and discussed, and we conclude the paper in Section 5.

2. The Mathematical Model

Globally, the order and orientation of biaxial nematics are described by the second-rank tensor \( Q \), which is symmetric and traceless, according to the Landau–de Gennes theory [2,30]:

\[
Q = \sum_{i=1}^{3} s_i e_i \otimes e_i
\]  

(1)

Each \( e_i \) of the orthonormal basis of the \( Q \) eigenvectors \( \{e_1, e_2, e_3\} \) lies along the directions of the preferred molecular orientation, assumed to be pointing along the \( x, y, \) and \( z \) directions of the laboratory frame of reference, respectively, while the degree of order along such directions is represented by the eigenvalues \( s_i \). Nematics can be found in three different phases—isotropic, uniaxial, or biaxial—each associated to the \( s_i \) values. When they are in the isotropic phase, then each \( s_i = 0 \), and the optical behavior is an ordinary isotropic fluid. Uniaxial nematics have a unique optical axis, identified by the eigenvector \( e_j = n \), associated to the maximum eigenvalue \( s_{max} \) giving in turn the scalar order parameter \( S = (3/2) s_{max} \). Finally, biaxial nematics all have different eigenvalues.

Modeling the dynamical evolution of the \( Q \)-tensor encompasses the NLC free energy density \( F \) minimization [2]. Imposing fixed boundary conditions to the cell surfaces results
in infinite anchoring energy for the NLC molecules. For this reason, we assume that contributions to $F$ arise only from the bulk, thus neglecting surface terms, and the ion effects are neglected, considering the nematic as a purely dielectric material [12]. Hence, the following is true:

$$F = \int_V (F_l + F_d + F_e) dV$$  \hspace{1cm} (2)

where

$$F_l = a \text{tr} \left( \mathbf{Q}^2 \right) - \frac{2d}{3} \text{tr} \left( \mathbf{Q}^3 \right) + \frac{1}{2} \left[ \text{tr} \left( \mathbf{Q}^2 \right) \right]^2$$

$$F_d = L_1 \left( \frac{\partial Q_{ij}}{\partial x_k} \right)^2 + L_2 \frac{\partial Q_{ij}}{\partial x_k} \frac{\partial Q_{kl}}{\partial x_j} + L_3 Q_{kl} \frac{\partial Q_{ij}}{\partial x_k} \frac{\partial Q_{ij}}{\partial x_l}$$  \hspace{1cm} (3)

$$F_e = -C_0 \left( \varepsilon_i |\nabla U|^2 + \varepsilon_d \nabla \mathbf{Q} \cdot \nabla U \right) + \tau \nabla \mathbf{Q} \cdot \nabla U$$

are thermotropic, elastic, and electric contributions, respectively, expressed assuming small $Q$ distortions. In $F_l$, $a = 3.6 \times 10^{-12}$ J/m, $k_{22} = 2.4 \times 10^{-12}$ J/m, and $k_{33} = 4.3 \times 10^{-12}$ J/m are the Frank’s elastic constants, while $S_{eq}$ is the equilibrium order parameter for uniaxial systems:

$$S_{eq}(\Delta T) = \frac{b}{4c} \left[ 1 + \left( 1 - \frac{24ac}{b^2} \right)^{1/2} \right]$$  \hspace{1cm} (5)

Furthermore, in $F_e$, $\varepsilon_i$ and $\varepsilon_d$ refer to the isotropic and the anisotropic dielectric susceptibilities, and $U$ is the electric potential. The last term accounts for polarization effects, where $F_e = (\varepsilon_{11} + \varepsilon_{33})/2S_{eq}$, with $\varepsilon_{11}$ and $\varepsilon_{33}$ being the splay and bend flexo-electric coefficients, respectively. By introducing the five degrees of freedom of a nematic molecule, we express the order tensor in terms of the five independent parameters $q_i$, $i \in [1,5]$:

$$\mathbf{Q} = \begin{pmatrix}
q_1 & q_2 & q_3 \\
q_2 & q_4 & q_5 \\
q_3 & q_5 & -q_1 - q_4
\end{pmatrix}$$  \hspace{1cm} (6)

We introduce the Rayleigh dissipation function as

$$D = \int_V \mathbf{D} \, dV = \int_V \gamma \text{tr} \mathbf{Q}^2 \, dV$$  \hspace{1cm} (7)

in which $D$ is the dissipation function density and $\gamma$ is related to the rotational viscosity. The generalized Euler–Lagrange equation for the modeled system is obtained from the balance equation [31,32] $\delta D + \delta F = 0$, once expressing the variation of the dissipation function density as

$$\frac{\partial D}{\partial q_i} \delta q_i = 2\gamma \text{tr} \left( \mathbf{Q} \frac{\partial \mathbf{Q}}{\partial q_i} \right) \delta q_i$$  \hspace{1cm} (8)

This yields the following:

$$\frac{\partial D}{\partial q_i} + \frac{\partial D}{\partial q_j} + \frac{\partial E_l}{\partial q_i} + \frac{\partial E_d}{\partial q_i} + \frac{\partial E_e}{\partial q_i} = 0, i = 1 \ldots 5.$$  \hspace{1cm} (9)
In Equation (9), the subscript \( j \) denotes differentiation with respect to the spatial coordinates \( x_1, x_2, \) and \( x_3 \), assuming summation over repeated indices. More details on Equation (9) can be found in [16]. Furthermore, the governing equation for the electric potential is
\[
\nabla \cdot D = \nabla \cdot (-\varepsilon_0 \epsilon \nabla U + P_S) = 0
\]
(10)
in which \( D \) and \( \epsilon_0 \) are the displacement field and the vacuum dielectric permeability, respectively with the dielectric tensor expressed as \( \epsilon = \epsilon_i I + \epsilon_a Q \) [33], and \( P_S = \tau(\nabla Q) \) is the spontaneous polarization vector [34,35].

An invariant measure for the degree of biaxiality is given by [12]
\[
\beta^2 = 1 - 6 \frac{\text{tr}(Q^3)}{\text{tr}(Q^2)} \in [0, 1]
\]
(11)
This allows for identifying the uniaxial nematic textures when \( \beta^2 = 0 \), while for a biaxial nematic phase, we have \( \beta^2 = 1 \) (i.e., the maximum of biaxiality). Equations (9) and (10) constitute a system of six coupled PDEs whose solution gives the dynamical evolution of the system.

3. The Numerical Method

The solution of the PDE system governing the \( Q \)-tensor dynamics has been performed using the FEM [36] and implementing the MMPDE numerical technique, in which the discretization of the one-dimensional integration domain is based on the equidistribution principle [37–41]. The method is aimed at the quality control of the mesh mapping and relies on the choice of a functional, the monitor function, which can depend on the solution gradient [42,43], or on the solution error [44]. Then, the equidistribution of the monitor function in each subinterval of the integration domain results in an accurate representation of sharp solution features, such as shocks or defects. Let \( u(z,t) \) be a solution of a PDE system over a physical domain \( \Omega_p = [0, 1] \) with \( z \) as the physical coordinate, and let \( \xi \) be a computational coordinate of a fixed computational domain \( \Omega_c = [0, 1] \). Then, a one-to-one mapping from physical domain \( \Omega_p \times (0, T] \) to computational domain \( \Omega_c \times (0, T] \) is represented by
\[
\xi = \xi(z,t), z \in \Omega_p, t \in (0, T]
\]
(12)
The reverse of this also holds:
\[
z = z(\xi,t), \xi \in \Omega_c, t \in (0, T]
\]
(13)
This is true from computational domain \( \Omega_c \times (0, T] \) to physical domain \( \Omega_p \times (0, T] \). Hence, the equispaced grid \( \xi_i = i/N, i = 0, 1, \ldots N \) in the computational space corresponds to a set of nodes in the physical space \( 0 = z_0(t) < z_1(t) < \ldots z_N(t) = 1 \).

To determine the node coordinates \( z(\xi,t) \) on which to compute the solution, we equidistributed the monitor function \( M(u(z,t)) \) over the one-dimensional domain:
\[
\int_0^1 M(u(s,t))ds = \xi \int_0^1 M(u(s,t))ds.
\]
(14)
By differentiating Equation (14) with respect to \( \xi \), the following mesh equation is obtained:
\[
M(z(x,t)) \frac{\partial}{\partial \xi} z(x,t) = \int_0^1 M(u(s,t))ds = C(t).
\]
(15)
Thus, keeping constant the equidistribution of the monitor function over the integration domain at a larger monitor function value corresponds a denser mesh.
For our purposes, we have demonstrated [25] that the choice of the monitor function tested by Beckett et al. [37] and based on a method proposed by Huang et al. [45] ensures good quality control of the mesh and final convergence of the FEM solution [37, 42, 43]. Then by putting

$$M(u(z, t)) = \int_0^1 \left( \left| \frac{\partial u(z, t)}{\partial z} \right| \right)^{1/2} dz + \left( \left| \frac{\partial u(z, t)}{\partial z} \right| \right)^{1/2}$$

(16)

there is the advantage of having a naturally smoothed function which allows to avoid external interventions.

The initial discretization of our PDE system is performed via the method of lines according to the following iterative process: (1) a mesh is generated by the equidistribution of the monitor function at the current time step; and (2) the PDE system is solved on a new generated grid and updated in time. The appropriate selection of the updating time step $\Delta t$ at which Equations (9) and (10) are numerically solved ensures the stability of the iterative updating [46]. By using Galerkin’s method, associated with a weak formulation of the residual of the differential equations, we overcome non-linearity-related difficulties, and Ritz’s method, when applied to Equation (10), allows for calculating the potential distribution [36]. An implicit Euler method was used for the time discretization, while the variables’ local distribution in each element was interpolated by quadratic shape functions.

Since our problem is modeled by six coupled PDEs solved simultaneously, at each time step, we have six unknown exact solutions $u(z, t)$, and the used multi-pass Algorithm 1 is as follows.

**Algorithm 1.** Multi-pass algorithm description.

1. generate a uniform initial grid $z_j(0)$ and calculate the corresponding initial solution $u_j(0)$ using FEM;

   done a temporal loop in the time domain, update mesh and solution $u$, putting forward PDEs:

   while $t_n < T$

     redistribute the in a few steps $\nu \geq 0$:

     do

     2. evaluate the monitor function at the current time step, move the grid from $z_j(\nu)$ to $z_j(\nu + 1)$ equidistributing the monitor function in each subinterval and calculate a solution $z_j(\nu + 1)$ on the new mesh, for each of the six coupled Equations (9) and (10).

     until $\nu \leq \nu_{\text{max}}$

     3. put forward the PDE system on the new mesh $z_j(\nu + 1)$ to obtain a numerical approximation $u_j(\nu + 1)$ at the new time level $t_{n+1}$.

   end

To solve the PDE system of Equations (9) and (10), in Equation (16), we replaced the unknown $u(z, t)$ with $tr(Q^2)$, since it is a quantity strongly related to the varying degree of order, thus becoming suitable to monitor the order reconstruction phenomena. The interaction of nematics with the confining surfaces of the cell resulted in the orientation of the nematic molecules along a given direction, an effect referred to as anchoring. Therefore, the asymmetric $\pi$-cell was modeled in one dimension with a thickness of 1 $\mu$m and infinite anchoring energy on the boundary plates, imposing Dirichlet boundary conditions. The rectangular electric pulses were applied perpendicularly to the plates with a duration $\Delta t = 0.25$ ms and amplitudes $E$ in the [15 V/$\mu$m, 90 V/$\mu$m] interval, with variable steps from 1 V/$\mu$m to 5 V/$\mu$m. The asymmetric anchoring conditions were modeled by imposing appropriate pre-tilt angles, measured with respect to the plates ($\theta_L = 19^\circ$ on the lower boundary surface, while on the upper boundary plate, $\theta_U$ varied in the $[-19^\circ, 0^\circ]$ interval, with variable steps in the $[0.1^\circ, 1^\circ]$ range). The PDE system was integrated over a one-dimensional physical domain discretized with a mesh with 285 nodes, sampling
the Q tensor dynamics with a time step size $\delta t = 0.1$ ms using the physical parameters typical for 5CB nematic liquid crystals at $\Delta T = -1$ °C [47].
which bulk- and surface-order reconstruction coexist, while above $E = 70 \text{ V/\mu m}$, only the bulk transition is present for whatever $\theta_U$. The upper boundary delimiting BSS and BS switching exhibits a bi-lobed shape, suggesting that for points of the $(E, \theta_U)$ plane included under each lobed region, the corresponding textures may have behaved differently with regard to the relaxation of the nematic distortion along the cell thickness. In order to verify such an assumption, we identified in the $(E, \theta_U)$ plane the points marked by “x”. Since the electric field was applied along the $e_3$ direction, we monitored the dynamics of the $s_3$ eigenvalue, since it was sensitive to order variations along this direction [27] (see Figure 1). We also added $(E = 42.5 \text{ V/\mu m}, \theta_U = -14^\circ)$ and $(E = 62 \text{ V/\mu m}, \theta_U = -14^\circ)$, which were not drawn for plotting convenience. In Figures 4 and 5, we show the $s_3$ computations obtained for $\theta_U$ values of $-4^\circ$ (a), $-6^\circ$ (b), $-9.5^\circ$ (c), and $-14^\circ$ (d) for $E = 42.5 \text{ V/\mu m}$ and $E = 62 \text{ V/\mu m}$, respectively. In both figures, time is reported in a logarithmic scale on the horizontal axis.

Figure 2. Surface contour plots obtained at $\theta_L = 19^\circ$ and $\theta_U = -3^\circ$ for electric pulses with amplitudes of $15 \text{ V/\mu m}$ (a), $22 \text{ V/\mu m}$ (b), $25 \text{ V/\mu m}$ (c), $40 \text{ V/\mu m}$ (d), $60 \text{ V/\mu m}$ (e), and $90 \text{ V/\mu m}$ (f). The biaxiality is linearly mapped in a gray-level scale between black (zero biaxiality) and white (maximum biaxiality) colors. The cell thickness is represented on the vertical axis, while on the horizontal one, the solution’s evolution is reported in the $0 \text{ ms} \leq t \leq 0.1 \text{ ms}$ range in a logarithmic scale. In each panel, the inset shows the magnification not spatially scaled for the biaxiality within 15 nm under the upper boundary plate.
is linearly mapped in a gray-level scale between black (zero biaxiality) and white (maximum biaxiality) colors. The cell thickness is represented on the vertical axis, while on the horizontal one, the solution's evolution is reported in the $0 \leq t \leq 0.1$ ms range in a logarithmic scale. In each panel, the inset shows the magnification not spatially scaled for the biaxiality within 15 nm under the upper boundary plate.

In Figure 3, we show the phase diagram obtained from monitoring the biaxiality inside the simulated domain for several $(E, \theta_U)$ pairs. Circles and squares mark the boundaries among the four regions where each texture obeys the same switching mechanisms: bulk switching (BS), surface switching (SS), bulk plus surface switching (BSS), or no switching (NS). In particular, the points in Figure 3 are given from the biaxiality computation performed for each value of the $(E, \theta_U)$ pair imposing $\theta_L = 19^\circ$ and noting the resulting switching regime to which the texture was eventually attributed. The horizontal axis reports the amplitude of the electric pulse, while the vertical one represents the opposite of the anchoring angles $\theta_U$. The data presented in [24] are well reproduced and marked with squares. As can be seen in Figure 3, most of the diagram concerns the textures for which bulk- and surface-order reconstruction coexist, while above $E = 70 V/\mu m$, only the bulk transition is present for whatever $\theta_U$. The upper boundary delimiting BSS and BS switching exhibits a bi-lobed shape, suggesting that for points of the $(E, \theta_U)$ plane included under each lobed region, the corresponding textures may have behaved differently with regard to the relaxation of the nematic distortion along the cell thickness. In order to verify such an assumption, we identified in the $(E, \theta_U)$ plane the points marked by "x". Since the electric field was applied along the $e_3$ direction, we monitored the dynamics of the $s_3$ eigenvalue, since it was sensitive to order variations along this direction [27] (see Figure 1). We also added $(E = 42.5 V/\mu m, \theta_U = -14^\circ)$ and $(E = 62 V/\mu m, \theta_U = -14^\circ)$, which were not drawn for plotting convenience. In Figures 4 and 5, we show the $s_3$ computations obtained for $\theta_U$ values of $-4^\circ$ (a), $-6^\circ$ (b), $-9.5^\circ$ (c), and $-14^\circ$ (d) for $E = 42.5 V/\mu m$ and $E = 62 V/\mu m$, respectively. In both figures, time is reported in a logarithmic scale on the horizontal axis.

**Figure 3.** Phase diagram of the biaxial order reconstruction obtained from imposing $\theta_L = 19^\circ$. The horizontal axis shows the amplitude $E$ of the applied electric pulse, and the vertical one reports the opposite of the anchoring angle $\theta_U$.

**Figure 4.** Dynamical evolution of the $s_3$ eigenvalue computed with an applied pulse $E = 42.5 V/\mu m$. In each panel, the plots refer to the first five mesh points starting from the upper boundary plate (top curve) for $\theta_U$ values of $-4^\circ$ (a), $-6^\circ$ (b), $-9.5^\circ$ (c), and $-14^\circ$ (d). On the horizontal axis, time is reported in a logarithmic scale.
Figure 5. Dynamical evolution of the $s_3$ eigenvalue computed with an applied pulse $E = 62 \text{ V/µm}$. In each panel, the plots refer to the first five mesh points starting from the upper boundary plate (top curve) for $\theta_U$ values of $-4^\circ$ (a), $-6^\circ$ (b), $-9.5^\circ$ (c), and $-14^\circ$ (d). On the horizontal axis, time is reported in a logarithmic scale.

Once $E$ was fixed, for each $\theta_U$ value, the $s_3$ dynamics were computed on the first five grid points, beginning from the upper boundary plate. The first curve from the top in each panel refers to the grid point located on the upper boundary surface, and it represents a constant $s_3$ since along $e_3$, the nematic order did not change, being prescribed by the fixed anchoring conditions. Under the upper boundary surface, instead, the nematic molecules began to align along the field direction, and the nematic distortion grew together with the biaxiality. For $E = 42.5 \text{ V/µm}$ and $\theta_U = -4^\circ$ (Figure 4a), in the second and third curve under the top one, corresponding to the first two grid points under the upper plate, a smooth temporal evolution of $s_3$ can be observed, a behavior characterizing biaxial phenomena as second-order transitions, since the nematic distortion relaxes through a wealth of biaxial states without any director rotation [27]. The fourth curve is characterized by a discontinuity highlighting a first-order transition. In fact, under the effect of the applied electric pulse, the director $n$ reoriented along the $e_3$ direction, and a predominant uniaxial order settled down. When imposing $\theta_U = -6^\circ$ (Figure 4b), a sharp structure is visible during the dynamical evolution of $s_3$ on the second grid point below the surface, which is superimposed to the smooth evolution. We interpreted such behavior as an attempt of the nematic director to reorient itself along the field direction which was suddenly aborted, meaning that the dynamical evolution of the biaxiality was mediated by a metastable uniaxial state. On the remaining two grid points, the $s_3$ evolution shows a first-order transition superimposed to the smooth temporal evolution. For $\theta_U = -9.5^\circ$ and $-14^\circ$ (Figure 4c,d, respectively), nothing changed, except that all the features became sharper and faster, and the duration of the metastable state increased.

When increasing the pulse amplitude to $E = 62 \text{ V/µm}$, for all the investigated $\theta_U$ values (see Figure 5a–d), the $s_3$ temporal evolution was similar to the previous one at $E = 42.5 \text{ V/µm}$, except that the metastable state disappeared, thus indicating that both the
uniaxial and biaxial orders coexisted without the need for a metastable state to mediate the nematic order evolution.

The evolution of the $s_3$ eigenvalue in Figure 4 displays evidence of a metastable state inside the nematic texture, located in a thin region below the upper boundary plate, whose existence depended on both the cell asymmetry ($\theta_U$) and the AEF ($E$) but whose duration was determined by the $\theta_U$ value only. More generally, referring again to the phase diagram in Figure 3, it was possible to map nematic textures that, depending on the imposed electrical and mechanical stresses, relaxed the nematic distortion differently. In particular, two ranges of $(E,\theta_U)$ pairs were identified. There was a first one in which the nematic order showed a smooth and continuous biaxial evolution typical of a second-order transition, on which a first-order-like uniaxial transition was superimposed. Nematic textures falling in the second range of values at a lower electric distortion presented a qualitatively similar order evolution, but a nematic layer existed below the upper boundary surface, in which the superposition of the uniaxial transition was mediated by a uniaxial metastable state.

We believe such a result is worthy of further experimental investigations, as it might bring new and useful insights in the route of multi-stable device design [50,51].

Quite recent experiments have also been carried out to try to distinguish between surface- and bulk-order reconstruction phenomena [52,53]. One way was to investigate the electro-hydrodynamics of nematics and, in particular, the DSM1 and the DSM2 regimes. DSM1 and DSM2 behave very differently. DSM1 leaves the texture’s topology unchanged, while DSM2 generates textures that are topologically non-equivalent. Disclinations separate untwisted and $\pi$-twisted textures. Therefore, as in both cases, the initial state is quasi-planar and uniform, where DSM2 is characterized by irreversible order reconstruction phenomena, while DSM1 is only characterized by elastic reversible texture deformations. Unfortunately, as the surface extrapolation length and the biaxial coherence length in this system are comparable, the surface anchoring breaking is in the same order of the energy required for bulk-order reconstruction, and both surface and bulk phenomena can coexist for the transitions between untwisted and $\pi$-twisted textures. In DSM2, the static disclinations, separating the two topologically non-equivalent textures, are presumably formed by strong short-range fluctuations in the flow field due to the viscous coupling between the director and the flow field itself. In principle, it is possible to distinguish the anchoring breaking from the order reconstruction by spatially resolving the flow field at the scale of the biaxial coherence length and of the surface extrapolation length, which is 10 nm for both phenomena [53], but no decisive experiment has been performed up to now.

5. Conclusions

In this work, we presented a mathematical model with a numerical simulation to investigate the order tensor $Q$ dynamical evolution for an NLC confined in a $\pi$-cell with strong asymmetries as well as strong electric distortions. For this purpose, we implemented the MMPDE numerical method using the FEM. Our simulations were consistent with previous computations, thus also confirming the validity of our numerical method in simulating notable distorted physical systems, as in the present case. Moreover, the peculiarity of the used technique revealed high sensitivity to distinguishing tiny features during the order dynamics of the studied system, allowing for building a phase diagram mapping the nematic regarding its switching properties, with computational savings with respect to the simulations performed using numerical techniques based on uniform discretizations. We considered several $(E,\theta_U)$ pairs, imposing strong anchoring conditions for the nematic molecules on both confining plates (with a fixed $\theta_L = 19^\circ$ on the lower one), and then we carried out the simulations for several $(E,\theta_U)$ pairs, searching for the phase boundaries among nematic textures obeying different switching mechanisms. Textures undergoing the same switching mechanism were mapped in each of the four regions in which the $(E,\theta_U)$ plane was parted, while the phase diagram exhibits a bi-lobed region in which surface- and bulk-order reconstruction coexist. The $Q$-tensor dynamics show that the nematic textures mapped within the low-energy lobed region exhibited a switching
mechanism that could be mediated by a metastable uniaxial state, as deduced from studying the evolution of the $Q$-tensor $s_3$ eigenvalue. The study presented in this paper definitely indicates that strong distortions induced by electrical and mechanical stresses can be relaxed by order variations of the nematic texture up to admitting the coexistence of bulk- and surface-order reconstruction transitions.

The proposed problem involves characteristic lengths and times with large-scale differences, and although it is simplified and only in one dimension, it has almost all of the features of higher-dimensional real problems, making it a very useful model. Work is in progress to extend the computations in two-dimensional domains.

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