Abstract

This study characterized the topography osseointegrated implants (cp-Ti) with machined surface (MS), laser beam surface (LS) and laser beam surface followed by deposition of sodium silicate (SS) by means SEM-EDX, roughness measurements, cross-sectional roughness, contact angle, X-ray diffraction (XRD) and laser confocal optical profilometry. The SEM of MS showed smooth surface, contaminated with machining residues, while LS and SS rough...
surfaces with a more regular and homogeneous morphological pattern. The EDX showed Ti peaks for MS and Ti and oxygen for LS and SS. The mean roughness values of LS and SS were statistically higher (p <0.05) than MS. The contact angle of LS and SS was 0°. The XRD of MS showed only Ti peaks, while LS and SS showed the presence of oxides and nitrides and presence of sodium silicate. The surface treatment performed in the LS and SS promoted important modifications in the topography and physical-chemical properties.

**Keywords:** Microscopy electron scanning; Dental implants; Topography; Laser beam.

**Resumen**

Este estudio caracterizó a topografía de implantes osseointegrados (Ti-cp) con superficie usinada (MS), superficie de feixe de laser (LS) y superficie de feixe de laser seguida de deposición de silicato de sódio (SS) por medio MEV-EDX, medidas de rugosidad, corte transversal rugosidad, ángulo de contacto, difracción de rayos X (DRX) y perfilometría óptica confocal a laser. El MEV de MS mostró superficie lisa, contaminada con residuos de usinaje, mientras que LS y SS superficies rugosas con patrón morfológico más regular y homogéneo. El EDX mostró picos de Ti para MS y Ti y oxigeno para LS y SS. Los valores medios de rugosidad de LS y SS fueron estadísticamente mayores (p <0.05) que MS. El ángulo de contacto de LS y SS era de 0°. El DRX de MS mostró apenas picos de Ti, mientras LS y SS mostraron la presencia de óxidos y nitritos y presencia de silicato de sodio. El tratamiento superficial realizado en LS y SS promovió modificaciones importantes en la topografía y las propiedades físico-químicas.

**Palabras clave:** Microscopía Electrónica de varredura; Implantes dentarios; Topografía; Feixe de laser.

**1. Introduction**

The concept of osseointegration was defined as the structural, direct and functional connection between the organized and healthy bone and the implant surface at an optical microscopic level, capable of withstanding masticatory forces (Bräimemark, et al., 1983). In order to provide better repair around osseointegrated implants, several measures have been suggested over the past few years. These measurements have almost always been related to the surface characteristics (Shibli, et al., 2007), more precisely in the topographic properties of the material (Albrektsson & Wennerberg, 2004). Previous studies have demonstrated that the surface treatment has allowed higher removal values by reverse torque (Carlsson, et al., 1988; Kesser-Liechti, et al., 2008; Faeda, et al., 2009) and bone / implant contact (Thomas & Cook, 1992; Xavier, et al., 2003; Qahash, et al., 2007), when compared to machined surface implants.

New methods of surface modification have been studied with promising results. Among these, the surface modification by laser beam stands out, which has the advantage of clean processing with a high degree of purity, in addition to being executed in a controlled and reproducible way (Carlsson, et al., 1988; Gaggl, et al., 2000; Cho & Jung, 2003; Braga, et al., 2007; Faeda, et al., 2009; Faeda, et al., 2009; Queiroz, et al., 2013; Sisti, et al., 2013; Souza, et al., 2013). The most common types of lasers used in material studies are those generated by a mixture of gases containing carbon dioxide (CO2) and the Yb: YAG laser (ytterbium laser). Currently, there is a trend towards the use of the ytterbium laser due to the advantage of being transported by flexible optical fibers, the absorption of the larger laser by the metal, wavelength and power of 20W (Gaggl, et al., 2000). This type of laser has sufficient and adequate energy to modify the implant surface (Carlsson, et al., 1988; Gaggl, et al., 2000; Queiroz, et al., 2013; Sisti, et al., 2013; Souza, et al., 2013), and higher values for removal by reverse torque (Cho & Jung, 2003; Faeda, et al., 2009; Sisti, et al., 2013). Previous published studies have shown that the modification
of the ytterbium laser surface provides greater bone / implant contact (Cho & Jung, 2003; Faeda, et al., 2009; Sisti, et al., 2013) when compared to the machined surface.

The deposition of biomaterials on a previously modified surface has been the subject of recent researches. The objective is to make the surface bioactive and osteocondutor. The surface modification technique by laser beam associated with sodium silicate deposition showed promising results in a previous published study (Souza, et al., 2013; Souza, et al., 2014). Sodium silicate is similar to silica oxide, found in the composition of bioactive ceramics. This compound acts as an osteocondutor by stimulating the differentiation of undifferentiated mesenchymal cells in osteoblasts, thus favoring the migration of osteogenic cells to the fibrin network promoted by the blood clot (Souza, et al., 2014).

In view of the above, the objective of this study was to characterize the topography of osseointegrated implants (cp-Ti) with machined surface (MS), laser modified surface (LS) and laser modified surface followed by deposition of sodium silicate (SS), using scanning electron microscopy (SEM-EDX), mean roughness measurements, cross-section roughness measurements, contact angle, X-ray diffraction (XRD) and confocal laser optical profilometry.

2. Methodology

The methodology applied in this study followed the guidelines described in Pereira (2018).

Surfaces

In this study, implants of commercially pure titanium (cp-Ti), grade IV with external hexagon connection, and dimensions of 3.75x10mm (Conexão Sistemas de Prótese, São Paulo, Brazil) were used with 3 different types of surfaces. Titanium disks with dimensions of 14 mm in diameter and 3 mm in thickness were also manufactured by the same company that supplied the implants. The analyzed surfaces were the machined and 2 experimental surfaces that were modified by the Biomaterials Group of the São Paulo State University (UNESP), Institute of Chemistry, Araraquara. The analyzed surfaces were:

(MS) - Machined surface;
(LS) - Surface modified by laser beam;
(SS) - Surface modified by laser beam followed by deposition of sodium silicate.

Preparation of experimental surfaces

Surface modified by laser beam (LS)

The cp-Ti implants with machined surface were fixed in a rotary lathe under the pulsed Yb: 20W laser equipment (Pulsed Ytterbium Fiber Laser, OmniMark System 20F, Ominitek Tecnologia Ltda, São Paulo, Brazil), with parameters of 140mJ nominal power supply and pulse frequency of 20 KHz. The laser beam was designed over the entire surface of the spiral implants at room temperature.

Surface modified by laser beam followed by deposition of sodium silicate (SS)

After irradiation of the surface by laser beam, the samples were immersed in 50 mL of NaOH solution (5.0 Mol.L-1) in the greenhouse for a period of 24 hours at 60°C, for the activation of the surface, forming a layer of sodium titanate. After immersion in alkaline solution, the samples were kept in the oven for 3 hours. The samples were then immersed in 70 ml of a sodium silicate solution, pH 7.25 and kept in the oven for 24 hours at 37°C (Souza, et al., 2013).
Topography characterization of surfaces

Scanning electron microscopy analysis coupled to the X-ray dispersive energy spectrometry system - SEM-EDX

The topography of the surface of the samples was analyzed using a scanning electron microscope (SEME ZEISS, model EVO LS15, equipped with an EDX microanalysis detector of the Inca X-act model, Oxford), coupled with the dispersive energy spectrometry X-ray (EDX), for semi-quantitative analysis of the chemical composition of surfaces (Queiroz, et al., 2013; Souza, et al., 2013; Souza, et al., 2014; Queiroz, et al., 2017).

Average rugosimetry

The average roughness (Ra) was analyzed in previously prepared discs of each surface by means of a rugosimeter (Mitutoyo SJ-400, Mitutoyo Sul Americana Ltda, São Paulo, Brazil). The results were submitted to statistical analysis of variance and Tukey's t-test (p <0.05) (Queiroz, et al., 2013; Souza, et al., 2013; Souza, et al., 2014; Queiroz, et al., 2017).

Roughness in cross section

Cp-Ti discs were analyzed in cross-section by SEM to determine the roughness thickness. Ten cross-sectional measurements of the experimental surfaces were performed. The values were annotated and tabulated. The average roughness of each surface was obtained. For the machined surface it was not possible to do this analysis, because there is no topographic modification of the surface (Queiroz, et al., 2013; Souza, et al., 2013; Souza, et al., 2014).

Contact angle measurements

The wettability of the samples (disks) was measured at room temperature with 75% relative humidity, using a Contact Angle System (video-based Dataphysics, model OCA-15) for contact angle analysis. The measurement of each sample was repeated 3 times to obtain the mean value of the contact angle (θ) of the different surfaces (Queiroz, et al., 2013).

X-ray diffractometry - XRD

The crystalline composition, as well as the types and phases of oxides formed for the modified surfaces, were analyzed by X-ray diffractometry (XRD) using an X-ray diffractometer (SIEMENS D5000 with angular sweep between 4 and 70°) (Queiroz, et al., 2013).

Laser confocal optical perfilometry

The roughness pattern of the samples was also analyzed by a confocal microscope, in which the light source consists of several laser beams that act as a scanner, focusing the sample line by line. The sample was then read by other detectors at a different wavelength, obtaining the peer-to-peer image through software. In addition, this microscope was able to form three-dimensional images through the union of two-dimensional images obtained by optical sectioning.

3. Results

Scanning electron microscopy analysis coupled to the X-ray dispersive energy spectrometry system – SEM/EDX

Scanning electron microscopy of the surfaces analyzed showed topographic differences between them. The MS presented a smooth surface topography, contaminated with machining debris (Fig.1a, b, c), while LS (Fig. 2a, b, c), and SS (Fig.3a, b, c) produced rough surfaces with a more regular and homogeneous morphological pattern.
EDX analysis revealed no contamination of the surfaces analyzed, and showed peaks of titanium for MS (Fig. 1d). For the LS, titanium and oxygen peaks were observed (Fig. 2d). However, SS revealed the presence of titanium, oxygen, silica, chlorine and sodium peaks (Fig. 3d).

**Figure 1.** (a, b, c) SEM: MS (500X, 1000X and 5000X), (d) MS EDX.

![Figure 1](image1)

Source: Authors.

**Figure 2.** (a, b, c) SEM: LS (1000X, 5000X and 10000X), (d) LS EDX.

![Figure 2](image2)

Fonte: Autores.
Figure 3. (a, b, c) SEM: SS (1000X, 5000X and 10000X), (d) SS EDX.

Source: Authors.

Average rugosimetry

The average roughness MS was 0.4±0.06μm, while LS was 4.73±0.48μm and SS 5.12±0.32μm (Table 1). The microtopographic analysis revealed a statistically significant difference (p <0.05) between the analyzed surfaces. The surface roughness of SS and LS were statistically superior when compared to the MS.

Table 1. Mean and standard deviation of different surfaces.

|   | MS           | LS           | SS           |
|---|--------------|--------------|--------------|
|   | 0.4 ± 0.06 μm (a) | 4.73 ± 0.48 μm (b) | 5.12 ± 0.32 μm (b) |

Different letters indicate statistical difference between the roughness surfaces. Source: Authors.

Roughness measures in cross section

SEM in cross section made on MS surface showed smooth surface due to absence of surface treatment (Fig.4a). The cross section of the discs showed a mean thickness of 0.84 ± 0.3 μm for MS (Fig.4a), 21.76 ± 9.05 μm for LS (Fig.4b) and 28.75 ± 10.12 μm for SS (Fig.4c). SEM in cross-section of the surface (SS) showed the presence of a "hybrid" layer, composed by irradiation with laser beam followed by deposition of sodium silicate, it being impossible to distinguish the laser beam modification of the silicate deposit sodium.
**Figure 4.** Mean Disk Thickness (a) MS (0.84 ± 0.3 μm), (b) LS (21.76 ± 9.05 μm), (c) SS (28.75 ± 10.12 μm).

Source: Authors.

**Contact angle measurements**

The contact angles obtained for the analyzed surfaces are shown in Table 2. It was found that the MS surface did not show adequate wetting, considering that the average contact angle of the surface was high (74.3º).

Table 2. Contact Angle Obtained for Different Surfaces.

| Surface/Angle | 1st evaluation | 2nd evaluation | 3rd evaluation | Mean |
|---------------|----------------|----------------|----------------|------|
| LS            | 0              | 0              | 0              | 0    |
| SS            | 0              | 0              | 0              | 0    |
| MS            | 68.9º          | 81.2º          | 72.9º          | 74.3º|

Source: Authors.

**X-ray diffractometry – XRD**

The XRD of MS showed only titanium peaks (Fig.5a), while LS showed the presence of oxides and nitrides (TiN) (Fig.5b) from the interaction between the surface and the air during the laser ablation process on the surface of the implant. XRD of SS revealed silica peaks (Fig.5c), characteristic of crystallinity, probably obtained during the deposition of sodium silicate.
**Laser confocal optical profilometry**

The confocal microscopy of MS showed a smoother surface with typical machining signals (Fig.6b, c) and it was observed in the 3D image (Fig.6a) that there were no peaks or valleys, being a smooth surface with "grooves" caused by the machining process. In the LS analysis, a homogeneous rough surface was evidenced with greater thickness when compared to the MS surface (Fig.7b, c). The 3D image of LS shows the peaks and valleys with a well-defined similar to honeycombs and homogeneous morphological pattern (Fig.7a). In the SS analysis confocal microscopy showed a rough surface, similar to the LS surface, with homogeneous pattern and greater thickness (Fig.8b, c) and in the 3D image it can be noticed that there were peaks and valleys similar to honeycombs, but some areas showed higher peaks due to the deposition of the sodium silicate (Fig.8a). The mean roughness values obtained in the profile analysis were 0.5247 μm, 8.2754 μm and 5.7120 μm for MS, LS and SS respectively.
Figure 6. (a b c) Confocal Optical Perfilometry Laser MS - 20x.

Source: Authors.

Figure 7. (a b c) Confocal Optical Perfilometry Laser LS-20x.

Source: Authors.
4. Discussion

In the beginnings of implantology, a period in which Branemark developed the first titanium implants, the surfaces were smooth, machined, without any type of surface treatment (Bränemark, et al., 1983). This type of surface used for decades has been the subject of several experimental (Souza, et al., 2013; Souza, et al., 2014) and clinical studies (Adell, et al., 1981). In a longitudinal study previously published (Adell, et al., 1981), the machined surface showed a success rate of 91% in implants installed in the mandible. However, in implants installed in the jaw, the success rate dropped to 81%, which leads to the conclusion that the machined surface, in addition to being time dependent, has a low success rate in low-density bone. For this reason, the modification of the surface of dental implants has assumed great relevance in recent years.

Surface modification by laser beam was shown to be a promising method for treatment of implant surfaces because it is clean, reproducible and economically viable (Cho & Jung, 2003; Sisti, et al., 2013). It is considered clean because it does not interact with external materials during the surface characterization process has a high degree of purity and roughness capable of promoting good osseointegration, and, furthermore there is no contamination of the oxide layer of titanium, since the technique does not use chemical elements (Filho, et al., 2011). The laser applied is of high intensity carried by optical fibers, which results in a greater homogeneity of this intensity on the surface of the implant. Between the lens system (focusing the laser beam on the sample diameter) and the sample, there is a device that has the function of protecting the lenses and preventing oxidation of the sample surface by creating an inert gas armature (Cho & Jung, 2003). The laser presents the physicochemical properties of the formation of an oxygen-rich layer and the incorporation of nitrogen during the rapid melting and solidification of titanium (Gaggl, et al., 2000; Braga, et al., 2007; Faeda, et al., 2009; Queiroz, et al., 2013; Sisti, et al., 2013). The modification of the surface by laser beam leads to the formation of erosions on this surface, making it rough (Filho, et al., 2011). Cho and Jung (2003) compared machined implants with a laser-modified surface by means of topographic analysis (SEM) and reported that the laser-modified surface had regular cavities similar to those of a honeycomb, while the machined surface was relatively smooth and with typical machining signals.

Previous published studies employing these surfaces evaluated in this present work (machined surface, laser surface and laser surface with deposition of sodium silicate) evaluated their potential for new bone formation in implants placed in
rabbit tibia and found higher removal torque values (Souza, et al., 2013) and bone implant contact, as well as neoformed bone area (Souza, et al., 2014) when compared to machined and acid-modified surfaces. Thus, the physico-chemical and morphological properties of the implant surface have a direct function in the osteogenesis, favoring the stages of the repair process in the interface formed between the bone and the implant (Queiroz, et al., 2017). In this present study when the surfaces were evaluated by SEM-EDX, LS and SS surfaces showed a complex morphology, and the presence of oxygen peaks, suggesting a physical-chemical modification of the surface. These physico-chemical modifications that the laser beam modification provides seem to favor the deposition of bone tissue.

The degree of bone implant contact seems to be influenced by the surface roughness of the implant (Gaggl, et al., 2000; Coelho, et al., 2009; Wennerberg & Albrektsson, 2009). From the results obtained in the rugosimetry analysis, it was observed that the LS and SS groups had statistically larger mean roughness values (p <0.05) when compared to the MS Group. Previous published studies has related to the correlation of roughness values with removal torque values (Queiroz, et al., 2013; Souza, et al., 2013; Vercaigne, et al., 1998), bone implant contact and neoformed bone area (Souza, et al., 2014; Queiroz, et al., 2017).

The measurement of the contact angle of the drop of a liquid of interest on a given surface has been used to characterize its wettability (Queiroz, et al., 2013). The surface is considered hydrophobic when the contact angle is greater than 90° and hydrophilic when the values are less than 90°. Hydrophilic surfaces allow a larger clot / implant contact due to their greater wettability (Elias, et al., 2008). In this present study it was observed that, although the mean value of the contact angle of the MS Group was less than 90°, that is, 74.3°, even though it was a high value when compared to the values found in LS and SS (0°). This fact indicates that MS does not present adequate wetting when compared to LS and SS that presents a wettability significantly superior to the MS. This greater wettability allows a better and more stable adhesion of the clot to the surface of the implant, favoring the deposition of bone tissue (Queiroz, et al., 2013).

Previous published study (Filho, et al., 2011) evaluated the titanium oxide formed compounds on laser-modified surfaces. The results obtained by the XRD suggested that the fusion and rapid solidification provoked by the irradiation of the laser (in normal atmosphere), induced the formation of titanium oxides, showing that the laser favored the propagation of oxygen atoms. One can also find the presence of nitrogen, according to the atmosphere. In this present study, it was verified that the machined surface showed only titanium peaks in the XRD analysis. In this present study the presence of oxides and nitrides was observed on the LS surface, due to the interaction with the air in the laser application process on the surface of the implant, and on the SS surface, silicate peaks were observed from the deposition of sodium silicate after modification by laser.

The surface-modifying laser beam's mechanism of action is based on the creation of a population of electrons encouraged to leave their natural state and enter a higher energy state. The electron population is created through the process of rapid fusion and solidification, which leads to a state of unbalance. When these electrons return to their natural state, the photons are emitted with an energy corresponding to the transition energy of the electron, leading to a physicochemical change on the surface (Gaggl, et al., 2000). The electron population may change due to creep. In other words, the electron population depends on creep, which is the relationship between density and area of energy (Silva, et al., 2016). The objective is create a homogeneous and controlled surface modification process, a fact observed in this present study at the SEM-EDX and XRD analysis. Also noteworthy is the high degree of wettability of the laser modified surface with or without sodium silicate coating as observed in the contact angle analysis.

Previous study published (Braga, et al., 2007) evaluated 9 parameters of the Nd: YV04 pulsed laser, analyzing the distribution of oxides and other compounds formed by cp-Ti surface irradiation through accumulated creep, pulse energy, repetition rate, and sweep rate. The results showed that the higher the creep, the higher the oxidation state of the titanium, that is, if the oxygen diffusion is high, the surface will retain a larger amount of oxygen, also showed that the creep of 280J / cm²
was not able. However another published study (del Pino, et al., 2002) demonstrated that fluencies above 294J / cm² favor the formation of TiO and Ti3O phases. The protocol applied in this present study was the pulsed Yb: 20W, with nominal power parameters of 140mJ and pulse frequency of 20 KHz, in order to obtain rougher surfaces and formation of relevant oxidation phases as observed in SEM-EDX and XRD analyses.

Perfilometry analysis has been used to evaluate surface morphology, mean roughness values (Faverani, et al., 2014). It has the advantage of providing a three-dimensional reconstruction of the analyzed surface, enabling greater visibility of the analyzed surfaces. In this present study, the profile analysis showed that the LS and SS groups presented rough surfaces, with homogeneous pattern throughout the sample, when compared to the MS group, which presented smooth surface, presenting only grooves caused by the machining process.

The goal of sodium silicate incorporation was to make the laser-modified surface more bioactive. Previous published study (Souza, et al., 2013) showned that the presence of sodium silicate favors osseointegration by stabilizing the blood clot, attracting bone cells (osteoblasts) by chemotaxis, allowing bone neoformation, by osteoconduction. It is noteworthy that osseointegration is favored by the presence of titanium oxides and titanium nitrides, leading to a lower risk of implant loss. In this sense, the material properties, such as oxides and nitrites formed by laser irradiation, can promote increased corrosion resistance, surface wettability and greater hardness, favoring osseointegration (Filho, et al., 2011).

Currently, several methodologies have been studied related to different types of surface treatment, which, as well as in the present study, have obtained relevant success rates. Thus, it is considered extremely important to carry out in vitro and in vivo studies of modifications of implant surfaces in order to seek viable means that can accelerate the osseointegration process, increase the bone / implant interface and guarantee the initial stability of the implant. implant even in low quality bone, promoting a higher rate of success and longevity of the treatment.

5. Conclusion

In view of the results obtained, it was concluded that the surface texturizations performed in the LS and SS implants promoted important modifications in the topography and physical-chemical properties of the analyzed surfaces.

Taking into account the results obtained with this research, it is necessary to carry out an clinical study in humans to evaluate the biological responses to the surface changes used.

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