Analysis of compressive strength of occlusal splints manufactured with three liquid resins at three angles of orientation on 3D printer

Análise de resistência a compressão de placas oclusais fabricadas por três resinas líquidas, confeccionadas em impressora 3D em três orientações de angulação

Análisis de resistencia a la compresión de férulas oclusales de tres resinas líquidas, realizadas en una impresora 3D en tres orientaciones de angulación

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Abstract

The aim of this study is to analyze the compressive strength of occlusal splints manufactured with three different liquid resins in a 3D printer and in three angles of orientation. The resins used here are (n=12): Resilab Clear (Wilcos do Brasil, Petrópolis, RJ, Brazil), Prizma Smart Print Bio (Makertech Labs, Tatuí, SP, Brazil), and Cosmos Splint (Yller Biomateriais, Pelotas, RS, Brazil); each resin group are divided into three subgroups according to orientation of manufacture: 0, 45 and 90 degrees. A dental manikin was scanned and the file was used to manufacture a steel hemiarch model. This model was used to design the occlusal splints and as a basis for the tests. The splints were designed with flat occlusal surface and minimum thickness of 2 mm. The compressive test was performed with constant force of 200N, velocity of 0.5 mm/min, along the entire occlusal surface until fracture. Results show no difference between the resins, regardless of orientation of manufacture. The orientation showed no intragroup effect for resins Prizma Smart Print Bio and Resilab Clear; the resin...
Cosmos showed larger compressive strength for the samples manufactured at 45 degrees than at 0 degree. The 90-degree samples were intermediary and showed no difference from other angles. This study shows that the three resins had similar behavior in terms of compressive strength, except for the intragroup effect of orientation of Cosmos Splint resin, where plates manufactured at 0 degree performed worse than those at 45 degrees.

Keywords: Occlusal splints; Three-dimensional printing; Computer aided design.

1. Introduction

The occlusal splint is a removable device used to improve the temporomandibular joint stability and enable a functional occlusion, which reorganizes the neuromuscular reflex activity (Maia, 2014). These devices are also used to protect the teeth of patients with bruxism from wear and excessive occlusal forces, and to minimize the symptoms of temporomandibular disorders. They can also be used to test a new occlusal dimension of patients in need of extensive prosthetic treatment. (Reymus & Stawarczyk, 2020)

Traditional manufacturing techniques of occlusal splints require several laboratory steps, which increases the odds of errors and distortions. In the last years, new technologies enabled the manufacturing of digitized occlusal splints that improve and simplify treatment (Vasques, 2018). This manufacturing process can either be subtractive, with the use of milling procedure, or additive, with the use of 3D printing. (Reymus et al., 2020).

The additive method of manufacturing was first described in 2013 and used stereolithography (SLA). Nowadays, SLA and DLP (Digital Light Processing) are commonly used technologies in the manufacturing of occlusal devices and both techniques use liquid resin immediately polymerized with laser (SLA) or light beam in wide areas (DLP) (Reymus & Stawarczyk, 2020).

In 3D printing, the angle of orientation may affect the reproducibility of the test specimens in terms of roughness and
strength (Unkovskiy et al., 2018).

Regardless of the manufacturing process, the material used in the occlusal device must meet the mechanical requirements to allow its clinical use and must be resistant to occlusal forces of up to 770 N and to the impact of clenching and grinding of teeth. This study aims to analyze, through compressive tests, the resistance of occlusal splints manufactured in a MoonRay 3D printer (SprintRay Inc. Los Angeles-CA, USA) with DLP technology, using three liquid resins: Resilab Clear (Wilcos do Brasil indústria e comércio LTDA Petrópolis-RJ, Brazil), Prizma Smart Print Bio (Makertech Labs- Resinas para impressora 3D BF Tecnologia 3D LTDA; Tatuí – SP, Brazil), Cosmos Splint (Yller Biomateriais; Pelotas- RS, Brazil) and three angle of orientations: 0, 45 and 90 degrees.

2. Methods

Samples calculation was run on G*Power 3.1.9.4. The groups were defined with 12 samples for each resin type and 4 samples for each angle. Therefore, each subgroup was composed of 4 test specimens for each angle, totaling 36 occlusal splints.

The test specimens were manufactured using DLP technology in a MoonRay 3D printer (SprintRay Inc. Los Angeles-CA, USA) with photopolymerized resins divided into three groups according to resin type: Resilab Clear (Wilcos do Brasil indústria e comércio LTDA Petrópolis-RJ, Brazil); Prizma Smart Print Bio (Makertech Labs- Resinas para impressora 3D BF Tecnologia 3D LTDA; Tatuí-SP, Brazil); and Cosmos Splint (Yller Biomateriais; Pelotas- RS, Brazil).

For the production of the test specimens, a dental manikin (DENT-ART Materiais Didáticos Odontológicos Ltda. São Paulo-SP, Brazil) was scanned on a bench scanner Ceramill MAP 400+ (Amann Girrbach Brasil LTDA, Curitiba-PR, Brazil) to generate an STL file. The file was used as the basis to produce a 2D model in steel (Figure 1), which was then machined on a DCM 620-5F (Indústrias ROMI S.A. Santa Bárbara do Oeste-SP, Brazil). The model was tempered with 46 HRC and scanned with the bench scanner Ceramill MAP 400+ (Amann Girrbach Brasil LTDA, Curitiba-PR, Brazil) to serve as the model for the design and manufacture of the occlusal splints and as a basis for the compressive test of the test specimens.

![Figure 1 - Steel model.](image)

Source: Authors.

The test specimens were designed as hemiarches; the splint’s occlusal surface is flat and encompasses the region from the upper right second molar to the upper right first premolar. The splints measure 35mm X 12mm X 5mm and have minimum thickness of 2 mm, considering the longest cuspid (Vasques, 2018).

The test specimens were manufactured in three different angles in the 3D printer; 0 degree (4 test specimens; Figure 2), 45 degrees (4 test specimens; Figure 3), and 90 degrees (4 test specimens; Figure 4).
After printing, the excess resin was removed with 2 isopropyl alcohol (Isopropanol, Votorantim, São Paulo - Brazil) baths (Berli et al., 2020): the first bath for 3 minutes, followed by a second bath for 2 minutes, replacing the alcohol between procedures. The splints were dried and taken to the light chamber, Photopolymerizer LabFlo UV (Labflo São Paulo-SP, Brazil) oven for 12 minutes according to the manufacturer’s recommendations. Supports were removed using an engine (straight part) and milling machine (Maxicut Black, series XXBL 105, Trihawk, Morrisburg, Ontario, Canada) (Vasques, 2018).

A compression bar was manufactured with the same dimensions of the occlusal splints (35mm x 12 mm x 5 mm) so that the compression was applied along the test specimen. The compressive strength of the materials used in the splints was analyzed by submitting all samples to constant strength until fracture (Figure 5) (Ribeiro et al., 2014). The test was performed on a universal testing machine EMIC DL 2000 (Instron Brasil Equipamentos científicos Ltda., São José dos Pinhais-PR, Brazil) (Wendler et al.,
2016), applying 200 N at 0.5mm/min, as per the protocol in De Carvalho et al. (2017).

**Figure 5** - Compressive test of occlusal splint over steel model.

The distribution of compressive strength values did not follow the normal distribution. Hence, data were compared using Kruskal-Wallis and Dunn’s non-parametric tests. All statistical calculations were run on SPSS 23 (SPSS Inc., Chicago, IL, USA), with 5% of significance.

3. Results

The Kruskal-Wallis’ test showed no significant difference between resins Resilab Clear (Wilcos), Prizma Smart Print Bio (Makertech Labs) and Cosmos Splint (Yller) used in the occlusal splints, regardless of angle of orientation, as seen in Table 1 and Graph 1.
Table 1 – Averages, standard deviations, medians and minimum and maximum values of compressive strength (N) of the resins used in the Michigan plates, according to angle of orientation.

| Angle of orientation | Resin used in the Michigan plates | p-value |
|----------------------|-----------------------------------|---------|
|                      | Prizma Smart Print Bio Markertch  |         |
| 0 degree             | 3772.51 $^a$ (3827.30)            | 0.105   |
|                      | Med: 2256.00                      |         |
|                      | Min: 1126.94                      |         |
|                      | Max: 9451.09                      |         |
| 45 degrees           | 3594.38 $^a$ (746.73)             | 0.116   |
|                      | Med: 3695.86                      |         |
|                      | Min: 2661.25                      |         |
|                      | Max: 4324.53                      |         |
| 90 degree            | 4416.50 $^A$ (1026.78)            | 0.174   |
|                      | Med: 4355.54                      |         |
|                      | Min: 3503.46                      |         |
|                      | Max: 5451.47                      |         |

| Angle of orientation | Resin used in the Michigan plates | p-value |
|----------------------|-----------------------------------|---------|
|                      | Resilab Clear Wilcos              |         |
| 0 degree             | 3744.32 $^a$ (3084.80)            |         |
|                      | Med: 2553.07                      |         |
|                      | Min: 1580.12                      |         |
|                      | Max: 8291.03                      |         |
| 45 degrees           | 6512.87 $^a$ (3472.21)            |         |
|                      | Med: 6877.24                      |         |
|                      | Min: 2553.42                      |         |
|                      | Max: 9743.58                      |         |
| 90 degree            | 3278.99 $^A$ (345.88)             |         |
|                      | Med: 3386.12                      |         |
|                      | Min: 2802.91                      |         |
|                      | Max: 3540.81                      |         |

| Angle of orientation | Resin used in the Michigan plates | p-value |
|----------------------|-----------------------------------|---------|
|                      | Cosmos Splint Yller               |         |
| 0 degree             | 1496.25 $^b$ (45.99)              |         |
|                      | Med: 1504.71                      |         |
|                      | Min: 1433.52                      |         |
|                      | Max: 1542.06                      |         |
| 45 degrees           | 6722.72 $^b$ (419.64)             |         |
|                      | Med: 6908.96                      |         |
|                      | Min: 6097.75                      |         |
|                      | Max: 6975.20                      |         |
| 90 degree            | 4781.05 $^{A_b}$ (1573.78)        |         |
|                      | Med: 4839.02                      |         |
|                      | Min: 6611.54                      |         |

Caption: Standard deviation in brackets. Med = median; Min = minimum value; Max = maximum value. Source: Authors.

Graph 1 – Bar chart of compressive strength (N) of the resins used in the manufacturing of the Michigan plates, according to angle of manufacture orientation.

Orientation of manufacture had no statistical effect on the compressive strength of resins Prizma Smart Print Bio (Makertech Labs) ($p = 0.292$) and Resilab Clear (Wilcos) ($p = 0.246$) (Table 1 and Graph 1). On the other hand, orientation affected resin Cosmos Splint (Yller), according to Kruskal-Wallis’ test ($p = 0.010$); according to Dunn’s test, the manufacture orientation of 45 degrees obtained larger compressive strength values in comparison with 0 degree and 90 degrees (Table 1 and Graph 1). The
manufacture orientation of 90 degrees obtained intermediary compressive strength, with no significant difference from other orientations.

4. Discussion

Studies show that 3D printed occlusal splints are a safe choice because, compared with conventional and milled splints (Prpic et al., 2019), they are more precise and present good compressive strength, and can be used in the clinical practice (Tahayeri et al., 2018). Other studies also show good precision and accuracy of the digital light processing (DLP) technique in the manufacture of occlusal splints (Brown et al., 2018; Kim et al., 2018; Sherman et al., 2020; Emir et al., 2021). Based on the mentioned results, the present study used the DLP technology as printing method.

Studies show that the orientation of printing influences strength and mechanical properties. Some of these studies show larger strength values for the vertical orientation (Väyrynen et al., 2016; Kebler et al., 2021; Nold et al., 2021). The present study showed that the orientation of 45 degrees of manufacture of occlusal splints with the Cosmos Splint resin increased the compressive strength in comparison with 0 degree; the splints manufactured at 90 degrees showed no significant difference from other orientations in terms of compressive strength. Splints manufactured with Resilab Clear and Prizma Smart Print Bio resins were not affected by angle of orientation in terms of compressive strength.

Studies show that test specimens printed vertically, with the layers positioned perpendicularly to the load vector present enhanced mechanical properties and compressive strength in comparison with those printed horizontally (Alharbi et al., 2016; Marcel et al., 2020). However, the methods used in the mentioned study are different from the methods used here.

The present study aimed to analyze the compressive strength of occlusal splints manufactured with three different resins in 3D printer in three different manufacture orientations: 0º, 45º and 90º degrees. Unkovskiy et al. (2018) used a similar method, but the test specimens were designed as bars and the compressive test was done in three points. In the present study, the test specimens were designed as plates on top of a dental model and the compressive test was done along the entire test specimens. Here, results show that the printing orientation can affect the structure of splints manufactured with Cosmos Splint resin; Unkovskiy et al. (2018) results also show that the angle of manufacture influences the strength of the 3D-printed material.

Regarding angle of manufacture, Shim et al. (2020) show that a 90-degree orientation produces the smallest error rates for length and the 45-degree orientation, the largest error rates for thickness; flexural strength increases according to 90<45<0. Unkovskiy et al. (2021) obtained better mechanical properties with 0 degree.

Rubayo et al. (2020) also obtained better results with 45 and 0 degree, corroborating the present study’s findings; however, the 90-degree test specimens required less support and used a smaller amount of material in the manufacturing. Studies that tested flexural strength obtained larger values for the orientation of 45 degrees (Hada et al., 2020; Gao et al., 2021; Grymak et al., 2020).

In the present study and on Hirai et al. (2017) and Vasques, 2018, the occlusal splints were designed with 2 mm of thickness from the longest cusp. Kurt et al. (2012) designed the occlusal splints with 3 mm of thickness to quantify the wearing on different plates.

5. Conclusion

The three resins showed the same behavior regarding compressive strength, except for the intragroup effect of orientation with the Cosmos resin, where splints manufactured at 0 degree performed worse than those manufactured at 45 degrees.

More studies using other methodologies, other resins and different angulation orientations are needed to prove the best effectiveness when making plates in 3D Printer.
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