Uncertain Systems Order Reduction by Aggregation Method

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ABSTRACT
In the field of control engineering, approximating the higher-order system with its reduced model copes with more intricate problems. These complex problems are addressed due to the usage of computing technologies and advanced algorithms. Reduction techniques enable the system from higher-order to lower-order form retaining the properties of former even after reduction. This document renders a method for demotion of uncertain systems based on State Space Analysis. Numerical examples are illustrated to show the accuracy of the proposed method.

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1. INTRODUCTION
In present time engineers and scientists are often with the analysis, design and synthesis of real time problems. The primary step to be followed is to develop a mathematical model which is an equivalent representation for the real problem.

In general, these mathematical models possessed with large dimensions and are named as large-scale systems. On the other hand, a highly detailed model would lead to a great deal of unnecessary complications. Hence forth a mechanism being applied to bring a compromise between the reduced model and original system so as to preserve the properties of the original system in its reduced model. The large-scale systems model reduction has two approaches like Time domain and Frequency domain. In frequency domain, continued fraction expansion method has lower computational efforts and is applicable to multivariable systems, but the major drawback in this method is it does not preserve the stability after reduction [1]. Similarly in Time domain approach using root approximation method, the steady state condition of the system is preserved, but it does not preserve the transient state of system [2].

Reduction of continuous interval systems by root approximation [3], and discrete interval systems by retention of dominant poles and direct series expansion method [4]. Based on study of stability and transient analysis of interval systems many methods have been proposed by the researchers on interval systems [5-9]. In this note the author extends the paper by reduction of interval systems into state space form of realization using ‘Aggregation method’.

The outline of this note consists of four sections. In Section 2, Problem Statement will be discussed. In Section 3, Procedural Steps for the proposed technique is explained. In Section 4, Error Analysis is done. In Section 5, the performance of the proposed method is shown by a numerical example. In

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Section 6, comparisons between the proposed and other methods are illustrated. At last, a conclusion is stated in Section 7.

2. PROBLEM STATEMENT
Consider an original linear time invariant uncertain system in Controllable Canonical Form:

\[
\Sigma : \begin{cases}
\dot{x}(t) = A_{nxn}x(t) + B_{nxm}u(t) \\
y(t) = C_{qxn}x(t) + D_{qxm}u(t)
\end{cases} \Leftrightarrow \Sigma : \begin{bmatrix}
A_{nxn} & B_{nxm} \\
\vdots & \vdots \\
C_{qxn} & D_{qxm}
\end{bmatrix}
\]

(1)

where

\[
A_{nxn} = \begin{bmatrix}
0 & 1 & \cdots & 0 \\
\vdots & \vdots & \ddots & \vdots \\
0 & 0 & \cdots & 1 \\
-\langle w_{0}^-, w_{0}^+ \rangle & -\langle w_{1}^-, w_{1}^+ \rangle & \cdots & -\langle w_{n}^-, w_{n}^+ \rangle
\end{bmatrix}
\]

\[
B_{nxm} = \begin{bmatrix}
0 \\
\vdots \\
0 \\
1
\end{bmatrix}
\]

\[
C_{qxn} = \begin{bmatrix}
\langle z_{0}^-, z_{0}^+ \rangle & \cdots & \langle z_{n}^-, z_{n}^+ \rangle
\end{bmatrix}
\]

The corresponding demoted order model of an uncertain system is represented in Controllable Canonical Form (CCF) as follows:

\[
\Sigma _{r} : \begin{cases}
\dot{x}_r(t) = A_{r}x_r(t) + B_{r}u(t) \\
y_r(t) = C_{r}x_r(t) + D_{r}u(t)
\end{cases} \Leftrightarrow \Sigma : \begin{bmatrix}
A_{r} & B_{r} \\
\vdots & \vdots \\
C_{r} & D_{r}
\end{bmatrix}
\]

(2)

where

\[
A_{r} = \begin{bmatrix}
0 & 1 & \cdots & 0 \\
\vdots & \vdots & \ddots & \vdots \\
0 & 0 & \cdots & 1 \\
-\langle x_{0}^-, x_{0}^+ \rangle & -\langle x_{1}^-, x_{1}^+ \rangle & \cdots & -\langle x_{r}^-, x_{r}^+ \rangle
\end{bmatrix}
\]

\[
B_{r} = \begin{bmatrix}
0 \\
\vdots \\
0 \\
1
\end{bmatrix}
\]

\[
C_{r} = \begin{bmatrix}
\langle y_{0}^-, y_{0}^+ \rangle & \cdots & \langle y_{r}^-, y_{r}^+ \rangle
\end{bmatrix}
\]

r=reduced order

Hansen. E [10] explained the fundamental arithmetic rules for an interval plant as follows: Addition:

\[
[i, j] + [o, v] = [i+o, j+v]
\]

(3)
Subtraction:

\[ [i, j] - [o, v] = [i-o, j-v] \]  \hspace{1cm} (4)

Multiplication:

\[ [i,j] \times [o,v] = [\min(io,iv,jo,jv), \max(io,iv,jo,jv)] \]  \hspace{1cm} (5)

Division:

\[ \frac{[i,j]}{[o,v]} = [i,j] \times \left[ \frac{1}{o}, \frac{1}{v} \right] \]  \hspace{1cm} (6)

3. PROCEDURAL STEPS

Step 1: The equivalent transfer function for the original uncertain plant expressed in Equation 1 is:

\[ Q(s) = \frac{N(s)}{D(s)} \]  \hspace{1cm} (7)

where

\[ D(s) = s^n + \sum_{k=1}^{n-1} w_k \cdot s^k, \quad w_k = [w_k^-, w_k^+] \]

\[ N(s) = \sum_{k=0}^{n-1} z_k \cdot s^k, \quad z_k = [z_k^-, z_k^+] \]

Step 2: The above uncertain system is converted to four fixed transfer functions which carries the coefficients of Equation 7 this can be represented in its general form using Kharitonov’s theorem [3]

\[ E_p(s) = \frac{\sum_{e=f}^{e=n} N_{pe} s^e}{\sum_{p=0}^{p=n} D_{pe} s^p} \]  \hspace{1cm} (8)

where

\[ e \leq n-1; \quad f \leq n; \quad p=1, 2, 3, 4 \]

Step 3: The above four transfer functions are transformed into four fixed state models:

\[ \Sigma_{p/n!/i} = \begin{bmatrix} A_{p/n \times n} & B_{p/n \times m} \\ \ldots & \ldots & \ldots \\ C_{p/q \times n} & D_{p/q \times m} \end{bmatrix} \]  \hspace{1cm} (9)

\[ p=1, 2, 3, 4 \]

Step 4: Evaluate the Eigen values for the obtained four fixed state models represented in Equation 9 individually

Step 5: Calculate the modal matrix \( M_p \) is calculated for each individual state model:

\[ M_p = \begin{bmatrix} M_{p1} & M_{p2} \\ M_{p3} & M_{p4} \end{bmatrix} \]  \hspace{1cm} (10)

where

\[ p=1, 2, 3, 4 \quad : M_{p1} = (r \times r) \text{ and } M_{p4} = (n-r \times n-r) \]

Step 6: Now the inverse of modal matrix\( \tilde{M}_p \) is to be evaluated from
\[
\overline{M}_p = \begin{bmatrix}
\overline{M}_{p1} & \overline{M}_{p2} \\
\overline{M}_{p3} & \overline{M}_{p4}
\end{bmatrix}
\] (11)

where
\[p=1, 2, 3, 4; \quad \overline{M}_{p1} = (r \times r) \quad \text{and} \quad \overline{M}_{p4} = (n - r \times n - r)\]

**Step 7:** Obtain the arbitrary matrix \((M_{pu})\) followed by the Equation below:
\[
M_{pu} = \begin{bmatrix} I_r & 0_{r \times (n-r)} \end{bmatrix}
\] (12)

**Step 8:** Determine the aggregation matrix ‘\(K_p\)’ using the Equation
\[K_p = M_{p1}M_{pu}\overline{M}_p\] (13)

**Step 9:** Using the aggregation matrix the four reduced state models are obtained and are represented in generalized form as
\[
\sum_{p/r} = \begin{bmatrix}
A_{p/r \times r} & \vdots & B_{p/r \times m} \\
\vdots & \ddots & \vdots \\
C_{p/q \times r} & \vdots & D_{p/q \times m}
\end{bmatrix}
\] (14)

where
\[
A_{p/r \times r} = K_pA_{p/n \times n}K_p^T[K_pK_p^T]^{-1} \\
B_{p/r \times m} = K_pB_{p/n \times m} \\
C_{p/q \times r} = C_{p/q \times n}K_p^T[K_pK_p^T]^{-1}
\]
\[p=1, 2, 3, 4; \quad r = \text{order of reduced system}\]

**Step 10:** The corresponding four reduced \(r\)th order transfer functions for the above obtained four reduced \(r\)th order state model expressed in Equation 14 in its general form:
\[
R_p(s) = \sum_{s = g+1}^{s = +\infty} \frac{y_{p_{g}}}{s^{g}}
\] (15)

where
\[g \leq r-1; \quad h \leq r; \quad p=1, 2, 3, 4; \quad r = \text{order of reduced system}\]

**Step 11:** Now the equivalent transfer function for reduced interval system is equated below:
\[
R(s) = \frac{[y_{\alpha} \gamma_{\alpha}][y_{\beta} \gamma_{\beta}]^{* \infty} + \cdots + [y_{r-1} \gamma_{r-1}][s^{r-1}]}{[x_{\alpha} x_{\alpha}^{T}][x_{\beta} x_{\beta}^{T}]^{* \infty} + \cdots + [x_{r} x_{r}^{T}]^{* \infty}}
\] (16)

**Step 12:** Finally the demoted model of the interval system is expressed in Controllable Canonical Form (CCF):
\[
\sum_{t} \begin{cases}
0 & 1 & \cdots & 0 \\
\vdots & \ddots & \vdots & \vdots \\
0 & 0 & \cdots & 1 \\
-x_{\alpha^2} \quad -x_{\beta^2} & \cdots & -x_{r \times r}
\end{cases}
+ \begin{bmatrix} 0 \\
\vdots \\
0 \\
1 \end{bmatrix} u(t)
\]
\[
y_{\alpha}(t) = [[y_{\alpha} \gamma_{\alpha}][y_{\beta} \gamma_{\beta}]^{* \infty} + \cdots + [y_{r-1} \gamma_{r-1}][s^{r-1}]]x_r(t)
\] (17)
4. INTEGRAL AND RELATIVE INTEGRAL SQUARE ERROR

The integral and relative integral square error between transient responses of original and reduced systems is also determined as formulated below:

\[ \text{Relative ISE} = \int_{0}^{\infty} \frac{(q(t) - r(t))^2}{q(t) - r(t)} \, dt \]

\[ \text{ISE} = \int_{0}^{\infty} (q(t) - r(t))^2 \, dt \]

where \( q(t) \) and \( r(t) \) are the unit step responses of original \( Q(s) \) and reduced \( R(s) \) systems, \( r(\infty) \) final value of original system.

5. NUMERICAL ILLUSTRATION

5.1. Example 1

Let us consider an interval system having state model as followed below:

\[
\dot{x}(t) = \begin{bmatrix}
\dot{x}_1(t) \\
\dot{x}_2(t) \\
\dot{x}_3(t)
\end{bmatrix} = \begin{bmatrix}
0 & 1 & 0 \\
0 & 0 & 1 \\
-6.833,10.75 & 11.667,18 & -5.667,9
\end{bmatrix} \begin{bmatrix}
x_1(t) \\
x_2(t) \\
x_3(t)
\end{bmatrix} + \begin{bmatrix}
0 \\
0 \\
1
\end{bmatrix} u(t)
\]

Subject to:

\[
y(t) = \begin{bmatrix}
-5,8 & -5.8333,9.25 & -0.667, 1.5
\end{bmatrix} \begin{bmatrix}
x_1(t) \\
x_2(t) \\
x_3(t)
\end{bmatrix}
\]

1. The equivalent transfer function of an uncertain is as follows:

\[ Q(s) = \frac{[0.6667,1.5]s^3 + [5.8333,9.25]s + [5,8]}{[1,1]s^3 + [5.667,9]s^2 + [11.667,18]s + [6.8333,10.75]} \] (20)

2. Evaluate the four 3rd order transfer functions by using Kharitonov’s theorem as expressed in Equation (8)

3. The above four transfer functions are converted into four state models by using Equation 9 are:

\[
\Sigma_1/3 = \begin{bmatrix}
-9 & -11.667 & -6.833 \\
1 & 0 & 0 \\
0 & 1 & 0
\end{bmatrix} : \begin{bmatrix}
1 \\
0 \\
0
\end{bmatrix}
\]

\[
\Sigma_2/3 = \begin{bmatrix}
-9 & -18 & -6.833 \\
1 & 0 & 0 \\
0 & 1 & 0
\end{bmatrix} : \begin{bmatrix}
1 \\
0 \\
0
\end{bmatrix}
\]

\[
\Sigma_3/3 = \begin{bmatrix}
-5.667 & -11.667 & -10.75 \\
1 & 0 & 0 \\
0 & 1 & 0
\end{bmatrix} : \begin{bmatrix}
1 \\
0 \\
0
\end{bmatrix}
\]

\[
\Sigma_4/3 = \begin{bmatrix}
-5.667 & -18 & -10.75 \\
1 & 0 & 0 \\
0 & 1 & 0
\end{bmatrix} : \begin{bmatrix}
1 \\
0 \\
0
\end{bmatrix}
\]

4. Next Eigen values are to be determined individually for the above four state models

5. Then modal matrix, inverse of modal matrix and \( M_{po}K_p \) matrices are obtained for the four state models individually by using Equations 10 to 13.
6. Four reduced order state models are obtained from Equation 14 as given below:

\[
\Sigma_{1/2} := \begin{bmatrix} -8.314 & -7.197 \\ 1.0001 & 0.0002 \\ 0.945 & 8.145 \end{bmatrix} \begin{bmatrix} 1.104 \\ 0.109 \end{bmatrix} = \begin{bmatrix} 1 \end{bmatrix}
\]

\[ (25) \]

\[
\Sigma_{2/2} := \begin{bmatrix} -8.504 & -13.784 \\ 0.999 & 0.0002 \\ 1.0333 & 6.8325 \end{bmatrix} \begin{bmatrix} 0.9749 \\ 0.0505 \end{bmatrix} = \begin{bmatrix} 0 \end{bmatrix}
\]

\[ (26) \]

\[
\Sigma_{3/2} := \begin{bmatrix} -4.510 & -5.627 \\ 1.0002 & 0.0006 \\ 1.1394 & 2.498 \end{bmatrix} \begin{bmatrix} 1.5635 \\ 0.3435 \end{bmatrix} = \begin{bmatrix} 0 \end{bmatrix}
\]

\[ (27) \]

\[
\Sigma_{4/2} := \begin{bmatrix} -4.9159 & -14.3097 \\ 0.9999 & 0.0003 \\ 0.2666 & 7.3319 \end{bmatrix} \begin{bmatrix} 0.9495 \\ 0.0672 \end{bmatrix} = \begin{bmatrix} 0 \end{bmatrix}
\]

\[ (28) \]

5. The corresponding demoted order transfer functions are obtained as expressed in Equation 15 using four reduced state models from Equations 25 to 28.

6. Then the equivalent reduced order transfer function for interval system is obtained as expressed in Equation 16:

\[
R(s) = \frac{0.2392.2165s + [4.2659.639]}{[1.1]s^2 + [4.5098.504]s + [5.62614.31]}
\]

\[ (29) \]

Under steady state condition \( s \to 0 \)

\[
R(s) = \frac{0.23062.3923s + [4.115710.6511]}{[1.1]s^2 + [4.5098.504]s + [5.62614.31]}
\]

\[ (30) \]

7. The CCF of the reduced order interval system

\[
\Sigma_r: \begin{bmatrix} \dot{x}_r(t) \\ y_r(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -[5.626,14.31] & -[4.5098.504] \end{bmatrix} \begin{bmatrix} x_r(t) \\ u(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)
\]

\[ (31) \]

Step responses of both original and reduced 3rd order systems are shown in Figure 1 below.

Figure 1. Step Response of Original and Reduced 3rd Order System using Proposed Method
6. COMPARISON OF METHODS

The demoted order models of proposed method are compared with other methods are shown in Figure 2, 3 and 4.

Figure 2. Step Response of Original and Reduced 3rd Order System using Mihailov and Cauer Second Form

Figure 3. Step Response of Original and REDuced 3rd Order System using Routh and Factor Division Method

Figure 4. Step Response of Original and Reduced 3rd Order System using Mihailov and Factor Division Method
Table 1 shows Comparison of Reduced Order Models for 3rd order system.

| S.no. | Methods | Reduced Order Systems | Step Response of Lower Limit | Step Response of Higher Limit |
|-------|---------|-----------------------|------------------------------|------------------------------|
|       |         |                       | ISE Values                  | Relative ISE Values          |
| 1.    | Proposed Method | \( R(s) = \frac{[0.2306,2.3923]s + [4.1157,10.6511]}{1.1s^2 + [4.509,8.504]s + [5.626,14.31]} \) | 0.012 | 0.070 |
| 2.    | Mihailov and cauer second form | \( R(s) = \frac{[11.19,20.37]s + [14.16,16.94]}{[17.1,18.1]s^2 + [31.382,33.6]s + [20.31,21.2]} \) | 0.014 | 0.086 |
| 3.    | Routh and Factor Division Method | \( R(s) = \frac{[8.8417,47.0513]s + [14.3023,16.7005]}{[17,18]s^2 + [29.4722,35.7059]s + [20.5,21.5]} \) | 0.344 | 2.152 |
| 4.    | Mihailov and Factor Division Method | \( R(s) = \frac{[35.6065,49.4454]s + [14.0331,17.1024]}{[17.0011,18.0007]s^2 + [31.3826,33.6111]s + [20.3001,21.7052]} \) | 0.457 | 2.833 |

7. CONCLUSION

To decrease the complexity of the system order reduction is done. In this note the order reduction by proposed method is numerically solved. The proposed method implemented for order reduction represented the uncertain systems in state model. The demoted model obtained by proposed method is compared with other methods, and the ISE & Relative ISE values of step response are also compared. Hence the proposed method maintains stability with low ISE values compared to other existing methods.

REFERENCES
[1] L. S. Shieh and M. J. Goldman, “Continued Fraction Expansion and Inversion of cauer third Form,” IEEE Trans. On Circuits and systems, vol/issue: CAS-21(3), pp. 341-345, 1974.
[2] M. Chand, “Reducing Model Ordering using Routh Approximation Method,” International Journal of Emerging Technology and Advanced Engineering, vol/issue: 4(8), 2014.
[3] Bandyopadhyay B., et al., “Routh pade approximation for interval systems,” IEEE Trans Autom Control, vol. 39, pp. 2454–2456, 1994.
[4] C. Younseok, “A note on discrete interval system reduction via retention of dominant poles,” Int J Control Autom Syst, vol/issue: 5(2), pp. 208–211, 2007.
[5] Saraswathi G., “A mixed method for order reduction of interval systems,” Int Conf IntelAdv. Syst, pp. 1042–1046, 2007.
[6] Ismail O. and Bandyopadhyay B., “Model order reduction of linear interval systems using pade approximation,” IEEE Int Symc. Syst, 1995.
[7] Singh V. P. and Chandra D., “Routh approximation based model reduction using series expansion of interval systems,” IEEE Int Conf Power Control Embedded Syst (ICPCES), vol. 1, pp. 1–4, 2010.
[8] Singh V. P. and Chandra D., “Model reduction of discrete interval system using dominant poles retention and direct series expansion method,” in Proceedings of the IEEE 5th International power engineering and optimization conference (PEOCO), vol. 1, pp. 27–30, 2011.
[9] K. Kumar D. et al., “Model order reduction of interval systems using modified routh approximation and factor division method,” in Proceedings of 35th national system conference (NSC), IIT Bhubaneswar, India, 2011.
[10] Hansen E., “Interval arithmetic in matrix computations,” Part I Siam J Numer Anal, pp. 308–320, 1965.
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