Use of Polycarbonate Waste as Aggregate in Recycled Gypsum Plasters

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Abstract: The use of gypsum as an indoor coating material for buildings is very extensive. This means that huge amounts of gypsum waste are generated daily worldwide. Therefore, many researchers in the last years have been working on the generation of new gypsum-related materials and products that incorporate recycled gypsum waste as a replacement for the commercial one. On the other hand, trying to reduce the large amounts of plastic generated globally each year, several studies have used different types of plastic waste as aggregates for the development of new construction and building materials. However, up to now, no previous studies have been found in which any type of plastic waste has been used as an aggregate in a recycled gypsum matrix. This paper presents a study in which two different types of waste were mixed for the development of new gypsum plasters: unheated gypsum waste from industrial plasterboard production (GPW) and polycarbonate (PC) waste from rejected compact discs (CDs) and digital versatile discs (DVDs). In this sense, the mechanical and thermal performance of plasters was evaluated. Finally, in order to evaluate the changes in the microstructure of the composites, a scanning electron microscopy (SEM) analysis was conducted. The results showed a good performance of the new composites when both types of waste were combined in the mixes. New lightweight eco-efficient plasters, completely recycled, with enhanced flexural strength (by 14.8%), compressive strength (by 26.8%), and thermal conductivity (42.8% less), compared to the reference material, were achieved.

Keywords: recycled gypsum; gypsum plaster; plastic waste; mechanical properties; SEM

1. Introduction

The use of gypsum as an indoor coating material for buildings is very extensive. Its use in pastes, plastering mortars, or prefabricated elements (plasterboards, blocks) makes gypsum one of the most used materials on construction sites [1]. This means that huge amounts of gypsum waste are generated daily worldwide. According to Ahmed et al. [2], around 15 million tons of gypsum plasterboard waste end up in landfills each year worldwide.

Gypsum plaster for construction (CaSO₄·0.5H₂O, calcium sulfate hemihydrate/bassanite) is obtained by drying calcination of natural gypsum rock (CaSO₄·2H₂O, calcium sulfate dehydrate/gypsum) at 105 °C to 200 °C, as shown in Equation (1). After that, it must be mixed with water to be used, producing an exothermic reaction, described by Le Chatellier, in which the gypsum plaster rehydrates, becoming a hard material [3–5].

\[
\text{CaSO}_4 \cdot 2\text{H}_2\text{O} \rightarrow (105 \text{ to } 200 \, ^\circ\text{C}) \rightarrow \text{CaSO}_4 \cdot 0.5\text{H}_2\text{O} + 1.5\text{H}_2\text{O} \rightarrow \text{CaSO}_4 \cdot 2\text{H}_2\text{O} + \text{Heat} \tag{1}
\]
As can be seen, the material chemical composition does not change, making it a completely recyclable product [6]. Therefore, many researchers in the last years have been working on the generation of new gypsum materials and products that incorporate recycled gypsum waste as a replacement of the original commercial one [7–9].

In this regard, Jimenez-Rivero and Garcia Navarro [10–13] studied the environmental and economic cost of reusing gypsum plasterboard waste, concluding that more than 87% of that waste is sent to landfills in Europe. In a second stage, they developed new plasters and plasterboards using the gypsum waste as a partial substitute of a commercial one [14]. The results achieved by Camarini et al. were also very interesting. They analyzed the effects of recycling gypsum plasterboard waste from different points of view: influence of the heating time [15], thermal conductivity of the new composites [16], and the effects of citric acid as set retarder [17], among others.

The advantages of recycling that type of gypsum residue, in terms of waste reduction, energy consumption, and economics, have been analyzed by Fernandez-Casado [18]. Furthermore, the physicochemical and mechanical performance of gypsum plasters, with recycled gypsum waste, after multiple dehydration and hydration cycles, have been studied by Gerardo et al. [19], who did not observe an important loss in the mechanical properties of the new plasters after each cycle. In that sense, Erbs et al. [5] performed a similar study, in which they achieved 8.40 MPa of compressive strength of the plaster after three recycling cycles. This was well above the 2.00 MPa value established by the regulations as the minimum value for gypsum plasters.

As seen in Equation (1), recycled gypsums should be heated to be reused as a substitute of commercial gypsum. Therefore, Erbs et al. [8] evaluated various calcination temperatures (160 °C, 180 °C, and 200 °C) and times (1, 2, 4, 8, and 24 h) and concluded that the highest mechanical performance was achieved at 180 °C for 24 h. Later, fixing the calcination temperature (150 °C), Rosalì de Moraes Rossetto et al. [20] used different heating periods of the wastes (1, 2, 3, 4, 5, and 6 h) and found that when gypsum waste (from wall coverings, plasterboards and decorative ornaments) was used, the surface hardness and compressive strength of the plasters increased, while their workability worsened.

On the other hand, trying to reduce the large amounts of plastic generated each year worldwide, several studies have used different types of plastic waste as aggregates for the development of new construction and building materials [21–24]. Focusing on the investigations that used a gypsum matrix, one can differentiate the contributions that used foamed plastics (expanded polystyrene (EPS), extruded polystyrene (XPS), polyurethane (PUR), among others) from those that used more non-expanded ones (polyethylene terephthalate (PET), high-density polyethylene (HDPE), etc.).

The first group includes studies made by San-Antonio-González et al. [25,26], who used EPS and XPS as aggregates in the development of lightweight gypsum plasters with enhanced thermal properties. In this sense, González-Madariaga and Macia [27] also studied the influence of EPS waste in the generation of new gypsum panels for construction. Furthermore, PUR waste (up to 2 mm) was used as an aggregate in the gypsum matrix, obtaining composites and plasterboards with improved thermal behavior [28,29].

In 2006, Karaman et al. [30] obtained PET waste from recycled plastic bottles, using it as an aggregate in a gypsum matrix at weights of up to 20% of the added gypsum. Recently, Vidalès-Barriguete et al. [31] recovered pellet waste (heterogeneous mixture of thermoset and thermoplastic polymers), using them as aggregates in gypsum plaster with enhanced mechanical properties. Finally, other researchers have developed flame-retardant bio-composites, trying to improve their behavior in the case of fire [32].

As demonstrated above, several works have studied, separately, the influence of plastic and gypsum waste in plasters. However, up to now, no previous study has been found in which any type of plastic waste has been used as an aggregate in a recycled gypsum matrix.

This paper presents the third step of research in which two different types of waste were mixed for the development of new gypsum plasters: unheated gypsum waste from industrial plasterboard
In the first phase of the research, different percentages and sizes of polycarbonate waste were used as aggregates in a commercial gypsum matrix. New lightweight plasters with good mechanical performance and with improved thermal and environmental properties were obtained. The highest mechanical values were obtained in mixes with 10% (by weight of gypsum) of PC waste, while the best thermal and environmental performance was achieved for the plasters with 40% of plastic added [34];

- Second, a study in which gypsum waste was used as a partial substitute of commercial gypsum was conducted. Different heating temperatures and times were checked. It was concluded that it is possible to use unheated gypsum waste from plasterboards as a complete substitute of a traditional one, improving the environmental (77%), thermal (18.8%), and mechanical properties (17%) of the new plasters. However, the workability of the composites worsened [35,36].

Consequently, in this article, the effects of using both types of residues (GPW and PC), at different percentages, on the mechanical and thermal behavior of plasters was evaluated. Thus, the influence of a plastic aggregate (in this case, PC) in a recycled gypsum matrix was analyzed for the first time. Finally, in order to evaluate the changes in the microstructure of the composites, a SEM analysis was conducted.

2. Materials and Methods

2.1. Materials

For this study, the following materials were used for the development of the new gypsum plasters:

- **Commercial gypsum (CG):** traditional commercial gypsum for construction B1 [37], with controlled setting properties (Figure 1a);
- **Unheated gypsum waste from plasterboard production (GPW):** acquired at a plasterboard manufacturing plant based in Sines (Portugal). The recycled gypsum came from the panels' cutting process, using the pieces smaller than 1 mm (Figure 1b);
- **Polycarbonate waste (PC):** rejected CDs and DVDs obtained from all the recycling points located in the University of Seville (Spain). After that, the pieces were crushed, obtaining pieces smaller than 4 mm, as seen in Figure 1c.
- **Citric acid:** used as a set retarder in some composites to maintain the water/gypsum (w/g) ratio in all the plasters [17,35].

![Materials used to develop the new plasters: (a) commercial gypsum; (b) unheated gypsum waste from plasterboard production; (c) polycarbonate waste.](image-url)
The chemical composition of both types of gypsum used was obtained using the x-ray diffraction (XRD) technique. For this purpose, a XPERT-PRO PANALYTICAL diffractometer from the Laboratory of Mineralogy, Petrology, and Geochemistry of Instituto Superior Técnico (LAMPGIST) was used.

Figure 2 presents the diffractogram of both materials where it can be noticed that the commercial gypsum (from Escayescos production plant, located in Alcaudete, Spain) was mostly 100% hemihydrated gypsum (bassanite, CaSO$_4$·0.5H$_2$O) with a small amount of calcite (CaCO$_3$), while GWP is a mixture of dihydrate particles (gypsum, CaSO$_4$·2H$_2$O) and bassanite.

![Figure 2. X-ray diffraction (XRD) of both types of gypsum waste used.](image)

### 2.2. Plaster Preparation

Different gypsum plasters [37,38] were produced by mixing different contents of polycarbonate waste, commercial gypsum, and recycled gypsum. The composition of all the mixes under study is presented in Table 1.

| Sample | Commercial Gypsum [g] | Gypsum Waste [g] | Water [g] or [mL] | w/g Ratio | Citric Acid [g] | Polycarbonate Waste [g] |
|--------|-----------------------|------------------|-------------------|-----------|----------------|------------------------|
| Reference | 1000                 | -                | 550               | 0.55      | -              | -                      |
| P10     | 1000                 | -                | 550               | 0.55      | -              | 100                    |
| P20     | 1000                 | -                | 550               | 0.55      | -              | 200                    |
| P30     | 1000                 | -                | 550               | 0.55      | -              | 300                    |
| P40     | 1000                 | -                | 550               | 0.55      | -              | 400                    |
| GPW50   | 500                  | 500              | 550               | 0.55      | 0.5            | -                      |
| GPW50 P10 | 500                 | 500              | 550               | 0.55      | 0.5            | 100                    |
| GPW50 P20 | 500                 | 500              | 550               | 0.55      | 0.5            | 200                    |
| GPW50 P30 | 500                 | 500              | 550               | 0.55      | 0.5            | 300                    |
| GPW50 P40 | 500                 | 500              | 550               | 0.55      | 0.5            | 400                    |
| GPW100  | -                   | 1000             | 550               | 0.55      | 1              | -                      |
| GPW100 P10 | -                   | 1000             | 550               | 0.55      | 1              | 100                    |
| GPW100 P20 | -                   | 1000             | 550               | 0.55      | 1              | 200                    |
| GPW100 P30 | -                   | 1000             | 550               | 0.55      | 1              | 300                    |
| GPW100 P40 | -                   | 1000             | 550               | 0.55      | 1              | 400                    |

The w/g ratio of the plasters was obtained using the flow-table test, following the procedure defined in UNE-EN 13279-2 [38]. As noted in previous studies, the use of gypsum waste worsened the
workability of the new plasters, requiring more water to make the mixes [35]. Therefore, and in order to maintain the w/g ratio in all the plasters, citric acid was used as a set retarder of the composites. According to previous studies, it was used as 1% per weight of the recycled gypsum used in the mixes [19].

Following these proportions, three 40 × 40 × 160 mm³ prismatic samples per mix were produced for the physical and mechanical characterization of the new plasters [38]. In addition, 70 mm round samples, 20 mm thick, were prepared to test the thermal conductivity of the composites.

2.3. Test Methods

Following the procedure defined in UNE-EN 13279-2, the specimens were placed at 24 °C and 50 ± 1% of relative humidity for seven days. Then, they were put in an oven at 40 ± 2 °C to reach constant mass [38]. After that, the new plasters were characterized, analyzing the following properties:

- **Dry bulk density**: according to the method described in UNE-EN 13279-2 [38], density is defined as the ratio between the dry mass of the sample and its volume;
- **Flexural strength**: the three-point bending test was used to measure the flexural strength of the new plasters, as defined by the regulation [38] (Figure 3a);
- **Compressive strength**: after the three-point bending test pieces were broken, the resulting six halves were subjected to a progressive centered load test [38] until the compressive strength of the composites was determined (Figure 3b);
- **Thermal conductivity**: this was obtained by using the ISOMET-2114 device (located in Instituto Superior Técnico, Lisbon, Portugal) (Figure 3c), in accordance with the procedure described in ASTM D5930-09 [39];
- **Scanning electron microscopy (SEM)**: a FEI TENEO microscope (located in Universidad de Sevilla, Seville, Spain) was used to carry out the SEM analysis of the new plasters (Figure 3d).

![Figure 3. Test methods: (a) Flexural strength; (b) Compressive strength; (c) Thermal conductivity; (d) scanning electron microscopy (SEM).](image-url)
3. Results and Discussion

3.1. Dry Bulk Density

Figure 4 presents the dry bulk density results of the new gypsum mixes. It is concluded that when the percentage of PC waste added to the plasters increased, the density of the material decreased. Therefore, the highest decrease was obtained for the GPW100 P40 mix, in which the density of the plaster was 36.8% lower than the one obtained for the reference material. In addition, the differences between the density values achieved for the GPW100 and GPW50 plasters, with the same percentage of plastic waste added, was not very significant compared to the one obtained for the reference series (without recycled gypsum).

3.2. Flexural Strength

Figure 5 presents the flexural strength results with error bars (standard deviation). It shows that increasing the amount of polycarbonate waste added to the plasters resulted in a drop in flexural strength of the new plasters. In all of the mixes, and for the same waste content, plasters with complete substitution of the commercial gypsum with a recycled one (GPW100 series) showed the best mechanical behavior. On the other hand, GPW50 mixes presented the worst capacity. According to the results, the biggest rise in the strength performance of the plasters compared to the material without the plastic aggregate was achieved in samples with 10% PC waste, with the biggest growth (32.9%) found in the GPW50-P10 composite. Furthermore, all mixes with 50% of gypsum waste (GPW50 series) that contained a PC aggregate showed an improvement in their flexural strength capacity relative to the one without plastic waste (GWP50), which achieved the lowest value (1.58 MPa). Finally, all the newly developed composites achieved the minimum 1 MPa standard requirement for gypsum plasters, thus being fit to be used in any construction work [37].

3.3. Compressive Strength

The compressive strength results of the gypsum plasters are presented in Figure 6 with error bars (standard deviation). In general terms, the same behavior as in the bending test was detected. A slight improvement of the resistance values was obtained, in all cases, when 10 wt% PC was used as an aggregate in the mixes. Once again, the GPW100-P10 mix was the one with the best performance (9.30 MPa), with an improvement of 26.9% relative to the reference sample. On the other hand, the worst compressive strength result was obtained for the GPW50-P40 composite at 4.01 MPa. Furthermore, it is...
important to highlight again that, for all the developed plasters, the minimum 2 MPa value required by the standard for the compressive strength of gypsum plasters [37] was noticeably exceeded. Thus, all of these are ready for use as a construction material with a wide number of applications.

Figure 5. Flexural strength of the developed gypsum plasters with error bars.

Figure 6. Compressive strength values for the developed gypsum plasters with error bars.
3.4. Thermal Conductivity

According to the results obtained in this test (Figure 7), it can be said that a slight drop in thermal conductivity of the new gypsum composites was observed as the amount of both types of wastes added (GPW and PC) increased. Thus, the best values were achieved for GPW100-P40 (0.143 W/m°K), in which an enhancement of 42.8% was obtained relative to the reference plaster (0.250 W/m°K).

![Thermal conductivity graph]

Figure 7. Thermal conductivity of the developed gypsum plasters.

3.5. Scanning Electron Microscopy (SEM) Analysis

To clarify some of the values achieved in the mechanical performance tests, a SEM analysis was carried out for samples with 20% PC waste out of the entire series (P20, GPW50-P20, and GPW100-P20). Figure 8 shows some of the images taken in the analysis. First of all, it must be said that an important change in the gypsum matrix microstructure was detected when gypsum waste was used as a substitute for a commercial one and citric acid as the set retarder. The crystalline structure seen in the P20 images was completely different from the one obtained for the other plasters. In addition, the adherence on the interface between the gypsum matrix and the PC particles seemed to be excellent in the P20 and GPW100-P20 samples. However, a deterioration of the adherence was observed in the GPW50-P20 samples. This can justify the results obtained in the mechanical tests, where a drop in strength occurred in the GPW50 series. It could be said that the union of both types of gypsum residues generated an internal structure that worsened the mechanical capabilities of the new plasters [35,36], also decreasing the adhesion with the added PC. Finally, some glass fibers were seen in plasters with GPW, improving the bending properties of the plasters as it presented a good adherence to the gypsum matrix.
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Figure 8. Cont.
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Figure 8. SEM images of the gypsum plasters (300×): (a) P20; (b) GPW50-P20; (c) GPW100-P20.  
Highlights: crystalline gypsum structure (red); good adherence between the PC and the gypsum matrix  
(blue); glass fiber (green) and bad adherence between the matrix and the plastic aggregate (purple).  

4. Conclusions

In this paper, new gypsum plasters were produced using gypsum waste as the total or partial  
replacement of commercial gypsum and polycarbonate waste as the aggregate in the mixes. According  
to the results obtained during the experimental program, the following conclusions can be drawn:

• For all new composites, the increase in content of both types of residues added was linked to a  
decrease in dry bulk density of the plasters. In addition, that drop was more relevant in composites  
in which the amount of recycled gypsum used was higher. Consequently, the highest decrease  
was obtained for the GPW100 P40 mix, in which the density of the plaster was 36.8% lower than  
the one obtained for the reference plaster;

• According to the mechanical performance tests, it was noticed that some of the developed plasters  
exceeded the values of the reference composite. For both tests, flexural and compressive strength,  
the highest increase was obtained for the GPW100 P10 plaster (reaching 3.88 MPa and 9.30 MPa,  
respectively), so these plasters can have different applications; and

• The thermal conductivity test showed that all of the newly developed plasters presented a  
significant improvement in this property relative to the value of the reference plaster, and the  
GPW100 P40 composite was the one with the lowest coefficient (0.143 W/m°K).

Summing up, new lightweight eco-efficient plasters, completely recycled, with enhanced flexural  
strength (by up to 14.8%), compressive strength (by up to 26.8%), and thermal conductivity (up to 42.8%  
less), relative to the reference material, were developed. This means that the newly developed materials  
contribute to significantly reduce the amounts of this waste that ends up in landfills, contributing  
to a circular economy, while simultaneously achieving a notable enhancement in their physical and  
mechanical properties.

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