Design and analysis of compact dual resonance patch antenna

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Abstract
In this work a high gain dual resonance patch antenna is designed and simulated. Analysis is done while changing geometry and dielectric thickness. Main advantage of this type of antenna is its compact structure. Due to its dual characteristics it is very demanding in the communication industry which makes designing and analyzing of this type of antenna more alluring. Values for S11 parameters are: -10.97dB and -30dB for 4.94GHz and 7.38GHz, respectively. Gain exceeds 8.85dB and 6.59dB for 4.94GHz and 7.38GHz, respectively. Characteristic impedance of the feed line is 50Ω.

Keywords: Microstrip patch antenna, Microstrip feed line, Radiation pattern, Via fed

1. Introduction
Antenna is an important part of the communication system. The performance of the communication link depends upon the performance of the antenna. Microstrip patch antenna is compact, low-cost and usually excels has high efficiency.

Its geometry consists of the ground plane and radiating patch with dielectric substrate between them. Designed antenna shown in figure 1 has high gain and low input impedance which makes it efficient and profitable.

These advantages make them outstanding when it comes to the communication industry, as part of satellites, remote sensing systems and radars [1].

The modern research on this type of the antennas is used to assist the curing of breast cancer. Different approaches such as arrays of the microstrip patch antennas are used to improve efficiency of the device. Mostly arrays are used to perform the functions which one single element can’t do and to increase the directivity and return loss [2].

The size of the antenna which is analyzed and designed in this paper together with other characteristics is given as follows:
- a) box size: 500mm x 500mm;
- b) cell size: 0.8mm;
- c) frequency range: 4GHz to 9 GHz.

Design and analysis are obtained by using sonnet software [3].
2. **Design methodology**

Dual characteristic is obtained by compilation of rectangular slits as can be seen from figure 1. While the main role in improving the performance of the antenna had a gap with cross at the center which also can be seen in figure 1. Dimensions of the antenna represented in figure 1 show the compactness of it and note that all of the dimensions are given in mm. Via feeding method is used in order to increase overall performance of the antenna and to simplify manufacturing of the antenna. Output signals are shown in figure 2 (S11) and figure 3 (gain). While designing we aim for the high absolute value of the input match (s11) since it represents the measure of the power absorbed by load.

![Figure 2. Input match response of dual resonance patch antenna](image)
Gain is the representation of the power density concentrated in a particular direction [4]. It is alluded to the isotropic reference antenna which radiates equally to all directions. Further, gain is given in the dB.

![Figure 3. Gain response of dual resonance patch antenna](image)

3. Parameters variations

In order to find optimum design adjustments that includes geometry dielectric thickness are done. Analysis on the dual resonance patch antenna includes changing the width of the gap with cross inside (Table 1), slit’s length changes (Table 2), dielectric thickness (Table 3 and 4) and port location (Table 5).

We observed the frequency at which S11 magnitude and gain occurs. From Table 1 we can conclude that the best performance is for a gap width of 10.4mm.

| WIDTH (mm) | Frequency (GHz) | S11(dB) | Gain(dB) |
|-----------|----------------|---------|----------|
| 7.2       | 5.04           | -16.47  | 8.88     |
|           | 7.42           | -19.32  | 5.71     |
| 8.8       | 4.98           | -15.48  | 8.82     |
|           | 7.42           | -22.01  | 5.92     |
| 10.4      | 4.94           | -10.97  | 8.85     |
|           | 7.38           | -30.33  | 6.59     |
| 12        | 4.8            | -10.73  | 8.56     |
|           | 7.32           | -24.07  | 7.08     |
| 13.6      | 4.74           | -8.71   | 8.39     |
|           | 7.12           | -17.26  | 6.13     |

Table 2 shows the changes of the slits length. They are located at the right and left upper corner of the antenna. Slits on both sides are perfectly symmetrical and work as a pair which means that changes in one slit reproduce change on another slit. Slit width of 1.6mm gives the best performance.
Table 2. Slit length changes

| LENGTH (mm) | Frequency (GHz) | S11 (dB) | Gain(dB) |
|-------------|-----------------|----------|----------|
| 0.8         | 4.88            | -10.99   | 8.76     |
|             | 7.48            | -23.25   | 7.28     |
| 1.6         | 4.94            | -10.97   | 8.85     |
|             | 7.38            | -30.33   | 6.59     |
| 2.4         | 4.96            | -13.35   | 8.81     |
|             | 7.24            | -23.50   | 5.25     |
| 3.2         | 4.98            | -13.77   | 8.77     |
|             | 7.06            | -18.41   | 3.15     |
| 4           | 5.02            | -14.86   | 8.81     |
|             | 6.82            | -13.94   | 2.19     |

Changing of the dielectric thickness is shown in Table 3. Dielectric thickness of 20 produces best performance but it is too thick for microstrip antennas. With all trade off we concluded that the best dielectric thickness for this design is 10mm.

Table 3. Changing dielectric thickness 1

| Dielectric thickness (mm) | Frequency (GHz) | S11 (dB) | Gain(dB) |
|--------------------------|-----------------|----------|----------|
| 5                        | 4.92            | -20.45   | 6.45     |
|                          | 7.28            | -15.26   | 5.30     |
| 10                       | 4.94            | -10.97   | 8.85     |
|                          | 7.38            | -30.33   | 6.59     |
| 15                       | 4.92            | -10.00   | 9.55     |
|                          | 7.38            | -24.32   | 7.04     |
| 20                       | 4.92            | -9.54    | 10.44    |
|                          | 7.38            | -19.88   | 7.48     |

However, in order to have a practical microstrip antenna we changed the dielectric thickness of the antenna in the range of 1mm to 3mm. Results are given in Table 4. We also achieved triple response in these simulations.

Table 4. Changing dielectric thickness 2

| Dielectric thickness (mm) | Frequency (GHz) | S11 (dB) | Gain(dB) |
|--------------------------|-----------------|----------|----------|
| 0.5                      | 4.92            | -42.49   | 6.25     |
|                          | 7.88            | -3.55    | 0.15     |
|                          | 9.0             | -8.14    | 4.59     |
| 1                        | 4.94            | -10.97   | 8.85     |
|                          | 7.38            | -30.34   | 6.59     |
|                          | 9.99            | -6.20    | 6.93     |
| 1.5                      | 4.84            | -10.89   | 9.37     |
|                          | 8.38            | -4.60    | 29.04    |
Port location is very important to achieve good directivity of the antenna. Further, it shows the best position of the port for fabrications. Up, left and right port locations represent middle positions in the antenna upper rectangle while bottom is shown in figure 1.

From Table 5 we can conclude that port location at bottom gives best performance regarding both S11 and gain.

Table 5. Changing port location

| Port Location | Frequency (GHz) | S11 (dB) | Gain(dB) |
|---------------|----------------|----------|----------|
| UP            | 6.62           | -5.11    | 6.52     |
|               | 7.88           | -7.51    | 11.47    |
| LEFT          | 6.66           | -16.68   | 7.30     |
|               | 7.42           | -15.23   | 9.99     |
| RIGHT         | 6.66           | -16.45   | 7.29     |
|               | 7.42           | -16.91   | 9.94     |
| BOTTOM        | 4.94           | -10.97   | 8.85     |
|               | 7.38           | -30.33   | 6.59     |

Before we reached results shown in Tables 1, 2, 3 and 4 design changes have been done. They are mostly based on changing the shape of the slit and obtained results are given in Table 6. However, we did not expect to have dual resonance so we did analysis in frequency range 1 to 5.

Table 6. Design changes on frequency range 1 to 5

| Changing the slit shape | Frequency (GHz) | S11 (dB) | Gain(dB) |
|-------------------------|-----------------|----------|----------|
| RECTANGULAR             | 5.04            | -14.75   | 6.40     |
| RECTANGULAR WITH TWO GAPS | 5.10           | -17.31   | 6.40     |
| STAR                    | 4.82            | -9.35    | 5.36     |
| STAR WITH ADDITIONAL GAP | 4.84           | -10.05   | 5.39     |
| SQUARE                  | 4.86            | -10.27   | 5.46     |
After finding which shape gives best results, we have analyzed how the cell size affects the antenna performance. Results of this analysis are given in Table 7.

**Table 7. Changing the cell size**

| Cell size | Frequency (GHz) | S11 (dB) | Gain (dB) |
|-----------|-----------------|----------|-----------|
| 0.6       | 5.24            | -13.24   | 6.98      |
| 0.7       | 5.08            | -21.25   | 6.65      |
| 0.8       | 4.96            | -12.25   | 5.96      |
| 0.9       | 4.86            | -11.61   | 5.9       |
|           | 7.38            | -30.33   | 6.59      |

In order to achieve the best antenna performance and do other analysis on specific types we chose to change the width of the port/via carrier. It is included as one part of design changes. Theory says that the wider it gets the better performance we achieve. In Table 8 are shown results we obtained.

**Table 8. Port/via carrier width**

| Width carrier | Frequency (GHz) | S11 (dB) | Gain (dB) |
|---------------|-----------------|----------|-----------|
| 1.6           | 4.68            | -13.54   | 6.12      |
| 1.7           | 4.94            | -12.62   | 6.04      |
| 1.8           | 5.08            | -15.11   | 6.47      |
| 1.9           | 4.96            | -9.08    | 8.88      |
| 2.0           | 4.86            | -16.96   | 8.36      |

We also performed analysis on changing the dielectric thickness from 1mm to 3mm on different designs. The one with best performance in that range is selected to be represented in Table 3 and 4. Designs are the same as one given in Table 5. We also increased the frequency range to be from 4GHz to 9GHz. Results obtained are shown in Table 9.

**Table 9. Changing dielectric thickness on different shapes**

| Changing the slit shape | Frequency (GHz) | S11 (dB) | Gain (dB) |
|-------------------------|-----------------|----------|-----------|
| RECTANGULAR             | 4.84            | -10.89   | 9.37      |
|                         | 9.0             | -7.46    | 29.04     |
| RECTANGULAR WITH 4.83   | 8.51            | -6.54    | 6.34      |
| TWO GAPS                | 4.92            | -12.11   | 4.87      |
|                         | 7.89            | -9.72    | 11.24     |
| STAR                    | 8.14            | -3.12    | 16.38     |
| STAR WITH 5.14          | 9.1             | -19.76   | 2.34      |
| ADDITIONAL GAP          | 4.58            | -8.19    | 8.13      |
|                         | 8.68            | -19.94   | 3.82      |
4. Numerical analysis and equivalent circuit

In order to predict and produce valuable results numerical analysis should be done. Behind the design of the antenna there are equations which explain how the antenna operates. Radiation is represented by the E field [5]. Radiating plane is composed of electrical and magnetic waves. There are various types of polarization as follows: linear, circular and elliptical. From names we can conclude that it depends upon the shape of radiation waves radiating from the antenna. Equations for the E-field for linear, circular and elliptical are given in equation 1, 2 and 3 respectively.

\[ E = \cos(2\pi f(t - \frac{z}{c})) (\hat{x} + \hat{y}) \]  
(1)

\[ E = \cos(2\pi f(t - \frac{z}{c})) \hat{x} + \sin(2\pi f(t - \frac{z}{c})) \hat{y} \]  
(2)

\[ E = \cos(2\pi f(t - \frac{z}{c})) \hat{x} + 0.3 \sin(2\pi f(t - \frac{z}{c})) \hat{y} \]  
(3)

In equations vector values represent direction of the E field. In linear polarization propagation of the E field stays at one single line. Field can be either horizontally or vertically propagated depending upon the x axis position to the ground. However, there are cases where radiation is in one positioned at one single line but the E field is not propagating either x or y axis. Those cases still represent linear radiation. As can be seen in equation 1 x and y components are in phase and have the same magnitude. Equation 2 represents the value of the magnetic field for circular radiation. Components x and y are 90 degrees out of phase and the E field rotates in a cycle so it gets name circular. Further, components must have the same magnitude and be orthogonal to each other. The direction depends on the direction of rotation of the E-field. It can be clockwise or counter clockwise. For elliptical polarization components don’t have equal magnitude and are out of phase for 90 degrees. Waves in this type of polarization are defined by a major axis. Axial ratio, the ratio between major and minor axis amplitudes, is one of the ways to represent the polarization [6]. If the axial ratio is 1 it is a circularly polarized wave while infinite axial ratio represents a linearly polarized wave. Any value between it two gives an elliptical wave. Due to the reciprocity theorem antennas transmit and receive in the same manner [7]. If the vertically polarized antenna transmits the signal, the vertically polarized antenna will receive signal. Any communication between opposite polarized antennas will not be successful. When two antennas are positioned from each other with angle \( \theta \), the power loss factor is given in equation 4.

\[ PLF = \cos^2\theta \]  
(4)

For equation 4, if the angle \( \theta \) is 0 it means that there is no power loss. However, if the antennas are opposite positioned (horizontally and vertically) the angle \( \theta \) is 90 and there is no power transmitted. Power density needed to transmit the signal properly is defined in equation 5.

\[ P_d = \frac{1}{2} R_e(E \times H^*) = \frac{E^2}{2\eta_0} \]  
(5)

where, \( \eta_0 \) is the intrinsic impedance of the free space [8]. It represents the density in the wave needed to transmit signal from the antenna. In order to transmit the signal, there must be a reference antenna which is usually an isotropic antenna. It is the type of antenna which transmits equally to all directions [9]. Power density at any distance from the reference antenna is power radiated from the transmitter divided by the spherical surface area which is given in equation 6 [10].

\[ P_d = \frac{P_r}{4\pi R^2} \]  
(6)

Further, one of the main parameters in tracking the performance of the antenna is antenna gain. It represents the directivity of the radiation of the antenna. Gain is given in equation 7.
Far field is a region of radiation of electromagnetic fields around the object which consists of the magnetic and electric field. Electric and magnetic field strength decreases as distance of the object increases [11].

5. Conclusion

Design demonstrated in this paper represents a simple, affordable and compact device. It is an important part of the communication wireless technology. However, excitation of surface waves which occur in the substrate layer is a disadvantage of patch antenna [12]. Further, it is the main reason why choosing proper design and dielectric thickness is important. Simulations are done in one minute which manifests high speed response. Values for S11 parameters are: -10.97dB and -30dB for 4.94GHz and 7.38GHz, respectively. Gain exceeds 8.85dB and 6.59dB for 4.94GHz and 7.38GHz, respectively.

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