Bond strength between acrylic resin and maxillofacial silicone

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ABSTRACT

The development of implant dentistry improved the possibilities of rehabilitation with maxillofacial prosthesis. However, clinically it is difficult to bond the silicone to the attachment system. Objectives: This study aimed to evaluate the effect of an adhesive system on the bond strength between acrylic resin and maxillofacial silicone. Material and Methods: A total of 120 samples were fabricated with auto-polymerized acrylic resin and MDX 4-4210 facial silicone. Both materials were bonded through mechanical retainments and/or application of primers (DC 1205 primer and Sofreliner primer S) and adhesive (Silastic Medical Adhesive Type A) or not (control group). Samples were divided into 12 groups according to the method used to attach the silicone to the acrylic resin. All samples were subjected to a T-peel test in a universal testing machine. Failures were classified as adhesive, cohesive or mixed. The data were evaluated by the analysis of variance (ANOVA) and the Tukey’s HSD test (α= .05). Results: The highest bond strength values (5.95 N/mm; 3.07 N/mm; 4.75 N/mm) were recorded for the samples that received a Sofreliner primer application. These values were significantly higher when the samples had no scratches and did not receive the application of Silastic Medical Adhesive Type A. Conclusions: The most common type of failure was adhesive. The use of Sofreliner primer increased the bond strength between the auto-polymerized acrylic resin and the Silastic MDX 4-4210 facial silicone.

Key words: Silicone elastomers. Acrylic resins. Polymethyl methacrylate. Dental implantation.

INTRODUCTION

Maxillofacial prosthesis has been used to rehabilitate mutilated patients by repairing extensive bone and soft tissues losses6,9,11,13,20,21. The aesthetic appearance, comfort, self-esteem as well as the quality of life of these patients have been improved with the use of facial prosthesis6,9,11-12,14,21.

The development of implant dentistry improved the possibilities of rehabilitation with maxillofacial prosthesis. Nowadays, the use of implants5,8,10,16,18,19 to retain maxillofacial6,8,10,16,19, thumb3 and digital10 prosthesis provides excellent clinical outcomes. However, clinically it is difficult to bond the silicone to the attachment system, and de-attachments have been observed4,7,8,16,19,25,27,30.

In order to overcome such a limitation, the association of acrylic resin and facial silicone has been proposed5,8,10,16,19. In this technique, the retention device of the implant is embedded in acrylic resin and then covered with silicone. Nevertheless, the resin/silicone bond is not safe, and the silicone may tear or separate from the resin when patients remove their prosthesis7,8,25,27,30.

Clinical studies have indicated the application of primers and adhesives on the resin/silicone interface to enhance the bonding between these materials. The association of polyurethane5 and acrylic resin7,10,16,25,27,30 with the facial silicone has been proposed. However, to the authors’ best
knowledge there is no study investigating the effect of the simultaneous application of primers and adhesives on the bond strength between auto-polymerized acrylic resin and facial silicone.

Therefore, the current study aimed to investigate the bond strength between auto-polymerized acrylic resin and facial silicone as a function of mechanical retention, primers and adhesives presence. The null hypothesis is that the application of an adhesive system (primer and adhesive) on the acrylic resin with mechanical retention would increase the bond strength between the acrylic resin and facial silicone.

**MATERIAL AND METHODS**

**Specimen fabrication**

Each sample consisted of two bars of auto-polymerized acrylic resin (Orto cor, VIPI, Pirassununga, SP, Brazil) and facial silicone (Silastic MDX 4-4210, Dow Corning Corporation, Midland, MI, USA). A metallic matrix with ten rectangular spaces with 75-mm length, 10-mm width and 3-mm thickness was used to fabricate the acrylic resin bars.

The auto-polymerized acrylic resin was manipulated according to the manufacturer’s instructions and was poured into the metallic matrix. The matrix was closed and 1.25 tons of pressure was applied for 10 minutes with a hydraulic press (Midas Dental Products Ltd, Araraquara, SP, Brazil). Afterwards, the matrix was placed in a curing resin device (Metalvander, Piracicaba, SP, Brazil) for 20 minutes under a hydrostatic pressure of 20 pounds. The matrix was opened and the acrylic resin bars were removed. P220 sandpaper (Tigre, Rio Claro, SP, Brazil) was used as a finishing procedure.

A total of 120 acrylic resin bars were obtained, and 60 bars did not receive any mechanical retention (scratches), and the remaining bars were scratched with a number 2135 diamond bur (KG Sorensen, Barueri, SP, Brazil). The bur was placed in a high-speed hand piece, and the long axis of the bur was parallel to the bar and tilted 45 degrees in relation to the horizontal axis during the scratches fabrication. Each scratch presented the same diameter of the bur and it was performed 25 mm in length of the bar in the bond area between the acrylic resin and silicone. The distance of each scratch had the same diameter of the bur.

Another metallic matrix was used to fabricate the facial silicone bar and to bond the acrylic resin bar to the facial silicone bar. This matrix had ten rectangular spaces with 75 mm in length, 10 mm in width and 6 mm in thickness.

Initially, the acrylic resin bars were cleaned with gauze and acetone and then placed into the matrix. An adhesive tape was positioned covering 50 mm in length of the acrylic resin bar (unbonded portion), and the remaining 25 mm length was used to bond the silicone to the acrylic resin. The bars were divided into 12 groups according to the adhesive system used and the presence of surface scratches (Table 1).

The application of primer on the acrylic resin surface was used to enhance the adhesive penetration. Therefore, a 30-minute period was allowed after the Dow Corning 1205 Primer (Dow Corning Corporation, Midland, MI, USA) or Sofreliner Primer S (Tokuyama Corp., Taitou-ku, Tokyo, Japan) application so that the primer could react with the resin surface. Afterwards, the MDX 4-4210 facial silicone was weighed on a digital precision scale (BEL Equipamentos Analíticos, Piracicaba, SP, Brazil) and manipulated according to the manufacturer’s instructions under a controlled temperature (23±2°C) and humidity (50±10%), in

| Group | Specimens | Scratch | Primer | Adhesive |
|-------|-----------|---------|--------|----------|
| 1 (control) | 10 | No | No | No |
| 2 | 10 | No | DC 1205 | No |
| 3 | 10 | No | Sofreliner | No |
| 4 | 10 | No | No | Yes |
| 5 | 10 | No | DC 1205 | Yes |
| 6 | 10 | No | Sofreliner | Yes |
| 7 | 10 | Yes | No | No |
| 8 | 10 | Yes | DC 1205 | No |
| 9 | 10 | Yes | Sofreliner | No |
| 10 | 10 | Yes | No | Yes |
| 11 | 10 | Yes | DC11205 | Yes |
| 12 | 10 | Yes | Sofreliner | Yes |
order to obtain a homogeneous mixture\textsuperscript{15}.

Before placing the silicone mixture into the matrix, some groups (Table 1) received a thin layer of Silastic Medical Adhesive Type A (Dow Corning Corporation, Midland, MI, USA) applied directly on the primed acrylic resin surface. The silicone mixture was then used to overfill the matrix and its surface was flattened with a steeling steel spatula and its thickness was standardized. The matrix was placed in a curing resin device with 20 pounds of pressure to avoid a bubble formation in the silicone. A total of 72 hours under room temperature was allowed so the silicone polymerizes and the formaldehyde releases, following the manufacturer’s instructions. After the silicone polymerization, the specimens were separated from the matrix and the adhesive tape, used to create the unbonded area of 50 mm in length and to allow the placement of the specimens in the universal testing machine, was removed\textsuperscript{5,7,25,27,30}.

A total of 120 specimens were obtained and they were divided into 12 groups (n=10) according to the function of scratches presence on the acrylic resin surface and adhesive system (primer and/or adhesive) type used (Table 1). The specimens were dry stored at room temperature (23±1°C) for 24 hours\textsuperscript{17} and then subjected to the bond strength test.

**Bond strength test (T-peel test)**

An universal testing machine (Emic DL-3000, EMIC, São José dos Pinhais, PR, Brazil) was used to conduct the bond strength test at a crosshead speed of 10 mm/min (Figure 1)\textsuperscript{5,7,16,25,27,29,30}.

The applied load and the limit load were recorded for each specimen. The T-peel strength for each specimen was determined using the average load divided by the specimen width, presented in the following formula: \[ F = \frac{W}{\lambda + 1} \]

where, \( F \) is the maximum force recorded (N), \( W \) is the width of the specimens (mm), and \( \lambda \) is the extension ratio of the silicone elastomer (the ratio of stretched to unstretched length)\textsuperscript{16}.

The acrylic resin/silicone interface was visually analyzed\textsuperscript{17}, and the failures were characterized as adhesive, cohesive, or mixed. Adhesive failure was defined when a complete separation of the resin and silicone occurs. Cohesive failure was characterized by the failure (i.e., tearing) occurring entirely within the silicone material. Mixed failure was characterized when both adhesive and cohesive failures are present\textsuperscript{5}.

**Statistical analysis**

The T-peel strength data was recorded. The effects of scratch, adhesive and primer on the bond strength (interactions among these factors) were

| Source of variation       | df | SS    | MS    | F     | P       |
|---------------------------|----|-------|-------|-------|---------|
| Scratch                   | 1  | 4.008 | 4.008 | 10.630| 0.001*  |
| Adhesive                  | 1  | 6.929 | 6.929 | 18.375| <0.0001*|
| Primer                    | 2  | 309.533| 154.767| 410.426| <0.0001*|
| Scratch x Adhesive        | 1  | 44.243| 44.243| 117.328| <0.0001*|
| Scratch x Primer          | 2  | 0.596 | 0.298 | 0.79  | 0.456   |
| Adhesive x Primer         | 2  | 24.706| 12.353| 32.759| <0.0001*|
| Scratch x Adhesive x Primer| 2  | 72.387| 36.194| 95.982| <0.0001*|
| Error                     | 108 | 40.725| 0.377 |       |         |
| Total                     | 119 | 503.128|       |       |         |

*(P=.05) indicates statistically significant difference
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analyzed by 3-way repeated-measures analysis of variance (ANOVA). The means were compared by the Tukey’s HSD test ($\alpha=.05$).

RESULTS

Data are summarized in Tables 2 and 3

The ANOVA results revealed a statistically significant difference on the T-peel strength of the specimens for all factors, except for the interaction scratch x primer (Table 2).

The T-peel strength data from group 3 only exhibited a statistically-significant highest bond value in comparison to all groups (Table 3). While groups 3, 9 and 12 displayed the highest T-peel strength values, group 1 exhibited the lowest (Table 3). Most of the specimens exhibited adhesive failure and some displayed mixed failures (Figure 2).

DISCUSSION

The null hypothesis was rejected since the greatest T-peel strength values were not observed in the groups with surface scratches, and primer and adhesive applications. Three mechanisms are involved in the bond between two materials: mechanical, micromechanical and molecular adhesion. The mechanical bond occurs when the materials are joined by small irregularities on their surface. The micromechanical bond is observed when a bonding agent is applied on the irregular surface of the material and an efficient micromechanical link is formed with adequate tensile strength. Finally, the combination of physical and chemical forces between the molecules of two different materials characterizes the molecular adhesion bond.

In the current study, different mechanisms to bond the facial silicone to the acrylic resin were used. It was possible to observe that all variables (scratches, primers and adhesives) statistically affected the T-peel strength values of the specimens, except for the scratch and primer interaction (Table 2). Such results were expected since several clinical studies observed bonding problems between the acrylic resin and silicone, and several mechanisms were developed to overcome these drawbacks.

Table 3 shows that groups that received the Sofreliner primer application (Groups 3, 9 and 12) displayed a statistically higher T-peel strength value when compared to the others. Therefore, it is possible to infer that the presence of scratches did not enhance the bond strength between the silicone and acrylic resin. This may be justified by the incomplete polymerization of the silicone into the scratched area.

Furthermore, the bonding between the silicone and acrylic resin may be affected by the chemical affinity between the silicone and primers. The chemical affinity is related to the composition of the materials used. According to the manufacturer, the auto-polymerized acrylic resin (OrtoCor) is composed by powder (polymethylmethacrylate and benzoyl peroxide) and liquid (methylmethacrylate, EDMA/Crosslink/ and an inhibitor). The MDX4-4210 is a two-component material. The elastomer component consists of a dimethylsiloxane polymer, reinforcing silica, and a platinum catalyst. The curing component consists of a dimethylsiloxane polymer, an inhibitor, and a siloxane crosslinking agent.

The results obtained herein are in accordance with those from Chang, et al. (2009), that investigated the bond strength between the polyurethane and facial silicone and observed a greater bond strength when the Sofreliner primer was applied on the polyurethane surface. Authors stated that
this primer has solvent in its composition, and the precise mechanism of its action remains unknown. Silastic Medical A adhesive has no solvent in its composition. Therefore, it is possible to speculate that the solvent has an effect in increasing the bond strength between the acrylic resin and facial silicone. According to the manufacturer, the DC 1205 primer is a liquid, solvent-based, film-forming primer applied to plastics, painted surfaces, plywood, masonry, metal and other construction materials to promote adhesion of one-component silicone sealants.

Furthermore, it was observed that group 3 exhibited the greatest value of bond strength even if it had no scratches and adhesive application on the acrylic resin surface, but presented a thin layer of Sofreliner primer (Table 3). The adhesive had no complete polymerization since its surface was not exposed to the room temperature necessary to release the byproducts from the polymerization reaction as recommended by the manufacturer. This situation might explain the results obtained herein.

Concerning the failure modes, most of the specimens exhibited adhesive failure, which characterizes a complete de-bonding between the two materials tested herein. These results are not in accordance with those from Hatamleh and Watts\textsuperscript{16} (2010) that noted greater cohesive failures. However, the authors used different silicone, acrylic resin and adhesives.

The high incidence of adhesive failures may be explained by the lack of affinity between the facial silicone and acrylic resin used herein, which characterizes a weak bonding when no primer or adhesive are applied.

Additionally, during the T-peel test, incomplete polymerization of the silicone and adhesive into the scratched areas of the acrylic resin bar was noted. The adhesive applied on the non-scratched resin bars was also not completely polymerized, maybe due to the fact that its surface was not exposed to the environment.

Groups 3 and 12 exhibited pure cohesive failure, while group 9 displayed mixed failures (Figure 2). These groups had the greatest values of bond strength (5.95, 4.73 and 3.07 N/mm, respectively), and received a Sofreliner primer application. Chang, et al.\textsuperscript{2} (2009) had similar results. They observed pure adhesive failure when DC 1205 primer was applied and pure cohesive failures when Sofreliner primer was used instead.

The Sofreliner primer is used to enhance the adhesion between the denture base acrylic resin and soft lining materials. Its composition and mechanism of action are unknown, but it is possible to speculate that some components of its composition are able to provide molecular adhesion between the acrylic resin and the facial silicone used herein. This may be proved since in most of the groups that had the Sofreliner primer application, the silicone was torn. In other words, the force necessary to break the resin/silicone bonding interface was higher than the tear resistance of the silicone.

Based on these in vitro results and our clinical experience, it is possible to assume that the application of Sofreliner primer on the acrylic resin devices used with maxillofacial prosthesis retained by implants can promote a safe bonding condition between the acrylic resin and facial silicone. But further laboratory studies and clinical trials are indicated. Further studies investigating the effect of the coloring agent used to tint the facial prosthesis as a function of different primers and adhesives application are warranted.

**CONCLUSION**

Considering the limitations of this in vitro study, it was possible to infer that the greatest bond strength between the auto-polymerized acrylic resin and the MDX 4-4210 facial silicone was observed for the groups that had no scratches on the acrylic resin bar and received the Sofreliner primer application. The adhesive failure was the most common bonding problem.

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