A state-of-the-art review of the fabrication and characteristics of titanium and its alloys for biomedical applications

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Abstract
Commercially pure titanium and titanium alloys have been among the most commonly used materials for biomedical applications since the 1950s. Due to the excellent mechanical tribological properties, corrosion resistance, biocompatibility, and antibacterial properties of titanium, it is getting much attention as a biomaterial for implants. Furthermore, titanium promotes osseointegration without any additional adhesives by physically bonding with the living bone at the implant site. These properties are crucial for producing high-strength metallic alloys for biomedical applications. Titanium alloys are manufactured into the three types of α, β, and α + β. The scientific and clinical understanding of titanium and its potential applications, especially in the biomedical field, are still in the early stages. This review aims to establish a credible platform for the current and future roles of titanium in biomedicine. We first explore the developmental history of titanium. Then, we review the recent advancement of the utility of titanium in diverse biomedical areas, its functional properties, mechanisms of biocompatibility, host tissue responses, and various relevant antimicrobial strategies. Future research will be directed toward advanced manufacturing technologies, such as powder-based additive manufacturing, electron beam melting and laser melting deposition, as well as analyzing the effects of alloying elements on the biocompatibility, corrosion resistance, and mechanical properties of titanium. Moreover, the role of titania nanotubes in regenerative medicine and nanomedicine applications, such as localized drug delivery system, immunomodulatory agents, antibacterial agents, and hemocompatibility, is investigated, and the paper concludes with the future outlook of titanium alloys as biomaterials.

Graphic abstract

Keywords  Titanium and titanium alloys · Biomedical application · Functional properties · Biocompatibility · Antibacterial activity · Advanced manufacturing

Extended author information available on the last page of the article
Introduction

In recent years, the number of patients in need of replacing failed tissue with artificial alternatives or implants, such as arthroplasty, hip joints, craniofacial, maxillofacial, dental implants, prostheses, and surgical instrumental applications, has increased [1]. Researchers estimate that demand for the replacement of hip and knee arthroplasties could reach 3.48 billion operations (673%) in 2030 compared to 2005 in the USA [2]. Therefore, many endeavors have targeted recognizing appropriate biomaterials for the fabrication of durable medical implants [3]. Biomaterials are utilizable owing to their superior mechanical and thermal conductivity properties. The main essential factor for metals to be recognized as biomaterials should be that no adverse reaction occurs when used in the targeted biomedical application; that is, they act as biocompatible materials. Metallic biomaterials are generally utilized for load-bearing applications; thus, they should have adequate fatigue strength. In comparison with ceramics and polymeric materials, using metals as biomaterials and the relevant technologies are continually enhancing because their properties can be modified in the function of the manufacturing processes [4]. Among various types of materials, metallic biomaterials such as 316L stainless steels, Co–Cr-based alloys, titanium, and its alloys have desirable properties and hence remain the most adequate choice for replacing failed hard tissue [5].

Grade 316L stainless steels (18Cr–14Ni–2.5Mo wt%) have been used as implants since the 1920s. The “L” in 316L stainless steel denotes low carbon content, which can intercept the formation of chromium carbides and increase the corrosion resistance. However, stress corrosion cracking, which cannot be prevented in 316L stainless steel, can be triggered by the combined effect of tensile stress and a Cl-rich environment such as human body fluid, resulting in an undesirable sudden failure of the implant under stresses [6]. Moreover, although Co–Cr-based alloys have a higher corrosion resistance compared to 316L stainless steels in human body fluid, some undesirable ions such as Cr and Co are released due to wear and corrosion [7]. There have been reports of Co exhibiting carcinogenicity in many animal researches and cases of neurological symptoms in patients after implantation. The released Cr could affect the blood cells, kidney, and liver by oxidative reactions; therefore, Co–Cr-based alloys and 316L stainless steel have potential risks as implants [8]. Hence, these two alloys may not be the best alternative for orthopedic implants, making titanium (Ti) deserve more attention.

Titanium and its alloys have been used as medical implants due to their long fatigue life, corrosion resistance, high biocompatibility, and lower Young’s modulus compared to other implants [9]. Despite the advantages of Ti alloys, supplementary development and modification are essential to devise clinically useful applications. Owing to the inadequate biocompatibility of alloys in this category, which are used in medical implant manufacturing, the risk of implant failure may be enhanced. This may also cause the poisonous agglomeration of ion discharge and wear debris entering the human body. To overcome these drawbacks, different types of advanced manufacturing and surface modification have been proposed [10].

Consequently, it is necessary to conduct comprehensive research on suitable biomaterials like titanium for biomedical applications. The present review focuses on the development of titanium and its multiple biomedical applications, such as bone replacement, dental implants, craniofacial, maxillofacial, surgical instruments, and prostheses. Then, we explore its functional properties, such as biocompatibility, density, corrosion resistance in the biomedical environment, ductility, thermal expansion, yield strength, tensile strength, magnetism, toxicity, host tissue response, protein adsorption, and antibacterial activity. Moreover, we carefully examine the different surface modifications and advanced manufacturing technologies of titanium and its alloys to improve its biomaterial properties. Finally, the applications of Ti in nanomedicine are discussed along with the future directions of research.

History of development of titanium alloys

The first reported application of commercially pure titanium (CP-Ti) in medicine originated from 1940, when this metal was found to have excellent compatibility with bones based on results from testing the reaction of bone to multiple metallic implants on animals [11]. During the subsequent decade of the 1940s, achievements made in industrial-scale manufacturing processes for titanium paved the way for an increasing number of studies on the medical applications of titanium [12]. During the 1950s, discoveries were made regarding the compatibility of titanium with soft tissue and the bone of rabbits, as well as its non-cytotoxic properties due to its remarkable corrosion resistance in biological environments, where research on the surgical application of titanium in dogs showed its excellent biocompatibility [13]. Clinical evaluations further confirmed this advantageous characteristic of Ti in long-term animal testing [14]. Subsequently, the utility of CP-Ti was developed through additional clinical reviews of its biocompatibility.

Observations on the long-term medical application of CP-Ti in the human body established that it is prone to fracture in this type of biological environment. However, CP-Ti has currently many applications in the medical field,
such as an artificial tooth root, internal fixation plates, and mandibular reinforcement plates. Therefore, the safety of long-term applications prompts the appropriate design process for stress conditions [15–17]. Proposals were made to utilize Ti−6Al−4V, which is the most widely utilized titanium alloy in the aerospace industry and is an alternative biomaterial for artificial joints and bone fixators [18]. Subsequently, β-type and α+β-type titanium alloys possessing low Young’s modulus and free of vanadium (V) or aluminum (Al) compounds were developed [19]. A new α+β-type titanium alloy, Ti−6Al−7Nb, was created by replacing the vanadium (V) in Ti−6Al−4V titanium alloy with a safer element, niobium (Nb), to reduce the cytotoxicity of titanium and associated alloys [20]. The development of other types of α+β-type titanium alloys also began during the 1970s using iron (Fe), molybdenum (Mo), and tantalum (Ta), which included Ti−6Al−2Nb−1Ta−0.8Mo and Ti−6Al−2.5Fe [21–23].

The advancement of enhancing β-type titanium alloys for biomedical applications was prolific in the USA and Japan. Different β-type titanium alloys compounded with elements such as oxygen (O), silicon (Si), and zirconium (Zr) to produce Ti−13Zr−13Ta (a near β-type titanium alloy), Ti−12Mo−6Zr−2Fe, T−15Mo, and Ti−15Mo−2.8Nb−0.2Si−0.28O, were developed in the USA. On the Japanese front, β-type titanium alloys such as Ti−15Mo−5Zr−3Al, Ti−15Mo−5Zr, and Ti−15Zr−4Nb−4Ta were formulated [24–30].

The dentistry field has seen successful implementations of CP-Ti from 1965 with the introduction of cast titanium-base partial denture for use as dental implants, which was based on research establishing the excellent compatibility of titanium with hard tissue [31]. Further advances spurred the use of titanium in dentistry from 1982, when the argon-arc casting machine and magnesia-system investment material were developed following the establishment of multiple dental casting systems utilized in dental restoratives [32].

At the turn of the century, attempts were made to develop novel β-metastable titanium alloys by alloying titanium alloys through transformation-induced plasticity (TRIP) and twinning-induced plasticity (TWIP). The TRIP and TWIP concepts originated from application on steels, which consequently lead to their adaptation to titanium in the form of Ti−Ni shape memory alloy. This opened the future possibility for β-type titanium alloy with extremely high rates of strain-hardening to be utilized in biomedical applications. In addition to the development of TRIP and TWIP concepts for titanium alloy-based medical devices, extensive research is also being conducted on the design and development of new β-type titanium alloys as biomaterials for implants based upon the design theory of d-electron [33]. The history of development of titanium alloys for biomedical applications is summarized in Table 1.

### Biomedical applications of titanium alloys

Titanium and its alloys are widely used in various biomedical treatment scenarios, including arthroplasty and bone replacement, craniofacial, maxillofacial and dental implants, surgical instruments, healthcare goods, or external and internal prostheses. The utilization of titanium alloys in medical devices throughout the entire human body, as well as the specifications of titanium alloys used in medical devices, is shown in Fig. 1.

### Arthroplasty and bone replacement

Titanium is used extensively throughout the whole human musculoskeletal structure. The most prevalent biomedical application of titanium is currently for hip and knee replacements, with shoulder and elbow joint implants following closely. Titanium has also seen frequent utilization in the spinal area for spinal correction parts, spinal fixation devices, spinal fusion cages, and in recent years, replacements of spinal disks [45, 46]. Rib cages for children made of titanium allow the implant to expand as the body grows, thereby allowing young patients to grow with the rib cage [47]. Finger and toe implants, as well as tibial nails employed in the reinforcement of lower leg fractures, are also made of titanium [48]. Fixation and reconstructive devices that support broken bones, such as bone plates, mesh, pins, screws, and rods made of titanium, are frequently used nowadays [49]. To increase implant lifetime for younger patients, some of these applications utilize roughened bioactive surfaces to limit resorption and stimulate osseointegration.

### Craniofacial and maxillofacial applications

Neurosurgical and cranioplasty applications of titanium include cranial plates, mesh, and acrylic. The biocompatible properties of titanium facilitate faster recovery and reduce the chance of infection. Maxillofacial prosthetics made from titanium alloys with appropriate levels of biocompatibility, strength, and osseointegration are able to stabilize soft tissue prostheses [50]. The application of maxillofacial prosthetics after maxillofacial surgery may often be necessary to restore the patients’ cosmetic appearance, their ability to eat or speak and replace any missing facial features due to disease or accident damage [51]. A schematic briefly depicting the design and fabrication process of a patient-specific mandibular prosthetic implant for defects related to maxillofacial clinical applications is shown in Fig. 2.

### Dental implants

Titanium alloys are utilized in restorative dental practice as dental implants, functioning as artificial roots to provide
Table 1 History of development of titanium alloys for utilization in biomedical applications

| Year   | Material     | Application                                                                 | Type of alloy | Reference |
|--------|--------------|------------------------------------------------------------------------------|---------------|-----------|
| 1940   | CP-Ti        | Compatibility with bones as a metallic implant                               | α type        | [11]      |
| 1940   | Ductile Ti   | Launching industrial production and smelting by the Kroll process for medical applications | α type        | [12]      |
| 1950   | Ti           | Compatibility of titanium with soft tissue and the bone of rabbits as well as the non-cytotoxic properties of titanium | α type        | [13]      |
| 1957   | Ti           | Non-toxicity with long term implantation                                      | α type        | [14]      |
| 1959   | Ti–Ni        | Shape memory alloy                                                            | β type        | [34]      |
| 1960   | Ti           | Artificial joints                                                            | α type        | [35]      |
| 1970   | Ti–6Al–4V    | Orthopedic implants                                                           | β-type and α+β-type | [36]      |
| 1979   | Ti–6Al–2Nb–1Ta–0.8Mo | Surgical implants                                                                 | α+β-type     | [21]      |
| 1970s  | Ti–6Al–2.5Fe | Medical devices                                                               | α+β-type      | [37]      |
| 1985   | Ti–6Al–7Nb   | Joint replacement                                                             | α+β-type      | [38]      |
| 1996   | Ti–12Mo–6Zr–2Fe | Surgical implants                                                                | β-type        | [25]      |
| 1996   | Ti–15Mo–2.8Nb–0.2Si | Prosthetic implants                                                             | β-type        | [39]      |
| 1997   | Ti–15Mo–5Zr–3Al | Dental casting and surgical implants                                            | β-type        | [28, 30] |
| 1998   | Ti–15Sn–4Nb–2Ta–0.2Pd | Medical implants                                                                | α+β-type      | [40]      |
| After 2000 | Ti–13Zr–13Ta | Implant                                                                      | β-type        | [24]      |
| After 2000 | T–15Mo     | Biomedical                                                                    | β-type        | [26]      |
| After 2000 | Ti–15Mo–2.8Nb–0.2Si–0.28O | orthopedic                                                                     | β-type        | [27]      |
| After 2000 | Ti–15Zr–4Nb–4Ta | Implant                                                                      | β-type        | [29]      |
| After 2000 | Ti–35.3Nb–5.1Ta–7.1Zr | Biomedical                                                                    | β-type        | [41]      |
| After 2000 | Ti–29Nb–13Ta–4.6Zr | Biomedical                                                                    | β-type        | [42]      |
| After 2000 | Ti–15Zr–4Nb–4Ta–0.2Pd | Medical implants                                                                | α+β type      | [43]      |
| After 2000 | Ti–5Al–1.5B | Biomedical                                                                    | –             | [44]      |

Fig. 1 Titanium alloys used in medical devices throughout the entire human body
a secure base for a single tooth to a complete dental arch. The titanium dental root comprises biocompatible anchors surgically implanted into the jawbone where the natural tooth is missing to support the artificial crown once the osseointegration period has occurred over time. During this period, the bone grows into and surrounds the titanium implant to create a firm structural support. Thereafter, the higher assembly of tooth superstructure is attached onto the implant as a dental replacement using cementation or the screw-tightening retaining method. Orthodontic braces made of titanium alloys are lighter, stronger, and feature better biocompatibility than steel [52, 53]. In this regard, pure titanium, Ti–6Al–4V, and Ti–6Al–7Nb are the primary titanium alloys utilized in surgical and dental applications. The mechanical properties of the various titanium alloys used in dental applications are listed in Fig. 3 [54].

The casting process is instrumental for the dental applications of Ti, with an emphasis on low elongation and high strength [55]. Hydrogenation processing and dehydrogenation processing are efficient techniques to improve elongation without compromising the strength of cast titanium alloys. These include thermochemical processing by post-heat treatments such as broken-up structure or β and α-β solution treatment [56]. Titanium alloys have a higher melting point and are more reactive than other dental alloys, such as Ag- and Au-based alloys that are preferred for precision dental castings.

**External prostheses**

Owing to the inherent properties of titanium, such as corrosive resistance, low weight, and toughness, its alloys are used extensively for the fabrication of temporary or long-term external devices and fixations, including artificial limbs and orthopedic calipers [57–59].

**Internal prostheses**

Titanium alloy pegs are used to secure false ears and eyes, while pure titanium grid implants provide fixation for interorbital fractures. The aural applications of titanium include bone conduction hearing aids anchored with devices made of titanium that are connected to the middle ear [60].

The carrier structure for replacement heart valves, coronary angioplasty catheters, defibrillators, intravascular stents, pacemaker cases, and vascular access ports are also made of titanium alloys [61–66]. Infusion pumps utilize titanium–nickel shape memory alloys that flex when the applied electrical current enables the creation of a heating and cooling cycle that changes the shape of the chamber.
Urethral strictures are treated with urethral stents made from titanium [68].

**Surgical instruments**

An extensive range of surgical instruments, such as dental drills, forceps, and laser electrodes, often contain titanium due to its antibacterial properties, resistance to corrosion, compatibility with radiation, durability, and lightweight nature [69]. The low weight of titanium reduces the onset of fatigue for surgeons wielding the instrument for extended periods of time [70]. For microsurgical operations, such as ocular surgery, titanium surgical instruments are usually anodized to produce a non-reflecting surface essential for such operations [70, 71]. The non-magnetic property of titanium reduces the possibility for electromagnetic damage or interference to small and sensitive implants during surgery [72]. The durability of titanium surgical instruments enables them to withstand repeated sterilization cycles without compromising their corrosive resistance, strength, edge quality, and surface quality.

**Utilization in healthcare products**

The utilization of titanium alloys for the fabrication of healthcare goods is expanding. Such uses include external prostheses and wheelchairs, particularly those used for sporting purposes, due to their outstanding biocompatibility, low weight, and high-strength properties. The titanium alloys widely used in this aspect are TFCA (Ti–4.0Fe–6.7Cr–3.0Al) and TFC (Ti–4.2Fe–6.9Cr) due to their lower cost than pure titanium, as recycling titanium with iron (Fe) contents, or low-cost ferrochrome (FeCr) can be utilized for this purpose [73, 74].

Even though healthcare goods are not implanted into the patient’s body, biocompatibility issues such as allergic reactions still need to be addressed, especially for the elderly who have weaker immune systems and a higher propensity to use these healthcare devices. A study involving pure titanium, Ti–6Al–4V, TFC and TFCA, has shown that TFC and TFCA had greater cell viability among the groups. As such, there is a potential for TFC and TFCA to be used more widely in other types of healthcare goods [75].
Functional properties of titanium alloys used in biomedical applications

Commercially pure titanium possesses several functional properties that are particularly advantageous for various biomedical uses. Here, we explore the characteristics that make titanium a suitable option as a biomedical material for such applications. Table 2 presents the properties of titanium compared to other lightweight metals used in the biomedical field. It can be seen that titanium has a higher melting and boiling point compared to aluminum and magnesium. The demand for biomaterials is related to different parameters based on their applications, such as elasticity modulus; hence, alloys with higher strength have a broader usage in biomedicine [76].

Bio-inertness (inert to chemical reactions with human bodily fluids)

Decades of medical studies and evaluation performed on titanium as a biomaterial demonstrated its excellent resistance to chemical reactions in the biological environment of the human body under fatigue, stress, as well as in crevice conditions [77]. The bio-inertness property of titanium is the result of its ability to naturally form a protective oxide film under the presence of even trace amounts of oxygen. This protective film is chemically impermeable, highly adherent, insoluble, and prevents chemical reactions between human tissue and titanium under the biological environment of the human tissues [78].

Ductility and malleability

Pure titanium possesses a relatively high level of ductility and malleability, which allows the use of conventional metal processing techniques and tools to form, machine, and join the biomaterial into functional biomedical implants. Such level of workability enables sheet metal techniques, such as tungsten inert gas welding performed without vacuum, to fabricate biomedical implants with larger and more complex designs [79, 80].

Tensile strength

Titanium exhibits the highest strength ratio of any metal suitable for medical application as a biomaterial [81, 82]. Titanium is lighter than stainless steel by approximately 56% but possesses twice the yield strength and an ultimate tensile strength that is approximately greater by 25% [83, 84].

Magnetism

Titanium is not susceptible to magnetization. Due to its non-magnetic properties, the benefits for patients with titanium inserted into the human body include reducing complications when undergoing CT scan or X-ray, avoiding the magnetization of titanium insert or prosthetic when near an electromagnetic source (such as most modern electronics), and not triggering metal detectors at airports [85].

Density

Titanium possesses the lowest density among the metallic biomaterials. Matching the density of the biomaterial with that of the already low density of human bone also contributes to the reduction of the stress shielding phenomenon by maintaining the proper distribution of body weight throughout the skeletal structure. Moreover, these properties enhance the image quality produced by computed tomography, magnetic resonance imaging (MRI), and X-ray [86]. Typically, β-type titanium alloys that have niobium and zirconium elements are utilized in applications where a low modulus of elasticity is required, while α + β-type titanium alloys are employed in cases where a high modulus of elasticity is required, such as for bone plate.

Corrosion resistance

Titanium exhibits excellent resistance to corrosion due to the self-formation of a passive titanium dioxide film that protects the metal from further oxidation, thereby inducing low toxicity in comparison with most other biometals. However, the property of corrosion resistance alone is not a determinant of the excellent tissue compatibility of titanium [87, 88]. The electrical plating of titanium with platinum improves its corrosion resistance at the cost of depleting

Table 2 Physical properties of lightweight metals used as biomaterials

| Metallic element | Boiling point (°C) | Metal density (g·cm⁻³) | Melting point (°C) | Hardness (HBW) | Elastic modulus (GPa) | Tensile strength (MPa) | Thermal conductivity (W/m·K) |
|------------------|--------------------|-------------------------|--------------------|---------------|----------------------|------------------------|-----------------------------|
| Titanium         | 3289               | 4.512                   | 1678               | 716           | 120                  | 220                    | 26                          |
| Aluminum         | 2520               | 2.7                     | 660                | 160           | 70                   | 90                     | 238                         |
| Magnesium        | 1090               | 1.74                    | 650                | 44            | 45                   | 175                    | 156                         |
the bone formation capability due to the surface property of titanium being shielded [89, 90]. Several studies investigated the corrosion resistance of Ti–6Al–4V and Ti–6Al–7Nb in phosphate-buffered saline (PBS) solution. The corrosion potential and current density of Ti–6Al–4V are −0.143 V and 4.334 × 10−5 μA·cm−2, respectively, and their values are −0.217 V and 4.83 × 10−5 μA·cm−2 for Ti–6Al–7Nb, respectively, which demonstrated that the corrosion resistance of Ti–6Al–7Nb is better than that of Ti–6Al–4V for biomedical purpose. This also results from the fact that niobium has higher corrosion resistance compared to vanadium [88, 91].

Resemblance of thermal expansion and elasticity modulus of Ti to human bone

The coefficient of thermal expansion as well as the modulus of elasticity of titanium closely resembles those of human bone, which in turn significantly reduces the potential for the patient receiving titanium implants to experience stress shielding, as the loads will be comparatively well distributed across the skeletal structure [92, 93].

Rigidity of titanium alloys

Most titanium alloys are designed with low rigidity as the fundamental property for biomedical application as implants and prosthetics [94]. Taking the cortical bone as an example, it is important for the Young’s modulus of a biomaterial to be as close as possible to that of cortical bone, as resorption may occur if this value is higher [95]. The α + β-type titanium alloy Ti–6Al–4V is commonly utilized in biomedicine [96]. Its Young’s modulus is lower than that of cobalt-based alloys and stainless steel, but still much higher than that of cortical bone. The Young’s moduli of β-type titanium alloys have been established to be lower than those of α + β-type or α-type titanium alloys, thereby allowing β-type titanium alloys to feature the required property of low rigidity. Furthermore, these alloys display high strength and outstanding cold workability [97].

The mechanical biocompatibility of titanium alloys with low rigidity for biomedical use was established on rabbits. In the relevant model, an experimental tibial fracture was induced in the tibia beneath the tibial tuberosity through the utilization of an oscillating saw [98]. The fracture was treated with the insertion of an intramedullary rod into the intramedullary canal, which was fabricated from Ti–6Al–4V ELI, Ti–29Nb–13Ta–4.6Zr, or stainless-steel SUS 316L. Atrophy, bone healing, and remodeling were monitored via X-ray imagery every fortnight for a period of 24 weeks. The shape of the fracture callus for Ti–29Nb–13Ta–4.6Zr was discovered to be very smooth, gradually decreasing from week 6, and traces of fracture disappearing by week 10.

Some atrophy change at the posterior of the tibial bone was observed after week 20. Ti–6Al–4V ELI displayed similar results, albeit at a slower rate. For SUS 316L stainless steel, significant fracture calluses were detected that remained until the end of the subsequent period. Observations of the proximal tibial bone at week 10 showed bone atrophy at the posterior part, which became more apparent every fortnight. The posterior tibial bone at week 24 showed signs of the bone structure becoming severely weakened. The low-rigidity titanium alloy Ti–29Nb–13Ta–4.6Zr has therefore shown a potential to address the load transmission issue faced by current implants [99, 100].

Elasticity and shape memory of titanium alloys

Ti–Ni is a shape memory titanium alloy used extensively in the wider industry beyond the field of biomedicine. In fact, Ti–Ni has seen limited biomedical applications due to its significant Ni content, which causes high rates of allergy. However, Ti–Ni has the potential for applications as catheters or stents where shape memory and superelastic properties are desirable [101]. To address the issue of metallic allergy due to the high Ni content, ongoing research and development have been underway for non-toxic titanium alloys with shape memory as well as superelastic properties.

A β-type titanium alloy known as “Gum Metal” (also called TNTZ) has a similar chemical composition to Ti–Nb–Ta–Zr system titanium alloys utilized in biomedical applications and has been used as flexible glass frames. Modifications to the chemical composition of “Gum Metal” may enable its potential for biomedical use. The superelastic feature of Ti–29Nb–13Ta–4.6Zr has been established for biomedical application with reports describing the very low density of dislocations post-deformation [102]. Developments are ongoing for Ti–Nb–Sn system titanium alloys as shape memory Ni-free titanium alloys for biomedicine [103]. Research and development on various β-type system titanium alloys for biomedical use, such as Ti–Mo–Ga, Ti–Mo–Ge or Ti–Mo–Al, Ti–Ta, Ti–Ta–Zr, and Ti–Sc–Mo, have also been intensive [104–108].

Bioactive surface treatments

Titanium alloys are generally treated with bioactive surface modifications to enhance their biocompatibility. Despite demonstrating superior biocompatibility in comparison with their metallic counterparts for biomedical use, titanium alloys exhibit similar bio-inertness to ceramics such as alumina and zirconia. Therefore, bioactive materials including phosphate calcium (CaP), β-CPP (β-Ca2P2O7), and β-TCP (β-Ca3(PO4)2) coatings are applied on the titanium alloy surface to facilitate the
formation of hydroxyapatite (HAP). The various bioactive surface modification processes are categorized into dry or wet processes [109–111].

Dry processes consist of direct and indirect HAP forming methods. The former includes the ion beam dynamic mixing method, ion plating, the plasma spray method, the pulse laser deposition method, the superplastic joining method, and radio frequencies (RF) magnetron sputtering, whereby the formation of HAP occurs directly on the surface of the titanium alloy [112–116]. Indirect HAP forming methods include calcium ion implantation, in which calcium alloys are incorporated into titanium alloy, and the calcium ion mixing method where calcium is deposited on the surface of titanium alloy, followed by the implantation of argon ion. These treatments enhance the precipitation of phosphate calcium on biomedical titanium alloy surfaces [117]. In a similar manner, wet processes consist of direct and indirect HAP forming methods. Electrochemical treatment is a direct HAP forming method, while alkali treatment is an indirect HAP forming method that involves heating the titanium alloy during immersion in sodium hydroxide solution (NaOH), followed by immersion of the said titanium alloy in simulated body fluid (SBF) for various biomedical applications, as follows: NaOH and heat treatments; NaOH, CaCl₂, heat and water treatments; H₂SO₄/HCl and heat treatments; NaOH, and acid and heat treatments [120].

### Biocompatibility of and host tissue responses to titanium alloys

#### Host tissue response

Observations on the structural interface located between the titanium biomaterial and bone tissue both at the microscale and the nanoscale facilitate the understanding of the osseointegration mechanism. The titanium substrate is covered by several layers of materials in the following order: titanium oxide with a thickness of a few nanometers; an amorphous layer of proteoglycans with a thickness of 20–50 nm; a slim layer of cells; a region with mild calcification; and bone tissue. Researchers have recently investigated the reaction mechanisms contributing to the capability of titanium for osseointegration. The influencing factors found include effects of healing and immune modulation; hydrophilicity and wettability; increase in gene expression associated with angiogenesis, neurogenesis and osteogenesis; inflammation–immunological balance; interactions between platelets and red blood cells; and molecular signaling mechanisms related to immune osteocytes [121–123].

### Surface hydroxyl groups

The properties of the surface oxide film covering the titanium substrate govern reaction mechanisms at the interface located between the titanium biomaterial and living tissue. Hydroxyl groups are formed on the surface oxide film due to interactions with moisture from the air, which in turn form electric charges after dissociating in aqueous solutions, such as bodily fluids. The pH of the surrounding solution determines the value of the electric charge, which becomes zero at a certain pH value. This pH is also called point of zero charge (PZC) that is dependent on the oxide and is an indicator showing acid or base property. In the case of titanium oxide, the PZC of anatase is 6.2, while that of rutile is 5.3, which translates to an almost neutral property that is neither significantly acidic nor basic. The concentration of surface hydroxyl groups on titanium oxide, at 4.9–12.5 nm⁻², is relatively large [121, 124]. This large concentration or wettability increases post-immersion in an aqueous solution, which promotes the absorption of proteins such as cytokines and integrins.

### Protein adsorption

Since proteins carry charges depending on the pH environment, their conformation is altered via adsorption onto the biomaterial surface. The relative permittivity of the surface oxide film determines the electrostatic force between proteins and the metal surface; that is, a larger relative permittivity translates to a smaller electrostatic force. Titanium oxide has a relative permittivity of 82.1, which is similar to that of water at 80.0 and is significantly larger than that of other oxides. Thus, the conformational fluctuations of protein adsorbed on titanium oxide are comparatively small. The absorption layer for fibrinogen is thicker, though the absorption amount in aqueous solution is smaller on titanium, and proteins adsorbed on titanium are less susceptible to conformational changes compared with those adsorbed on gold [125, 126].

### Formation of calcium phosphate

While the surface oxide film is macroscopically stable, its chemical state and composition vary based on the surrounding conditions. The composition of surface oxide film continuously changes based on the environment; from a microscopic viewpoint, it participates in a constant cycle of partial dissolution and reprecipitation in the electrolyte. In a biological environment, calcium phosphates easily
form on the surface of titanium and titanium alloys, while under cell culture, they form sulfite and sulfide, respectively. The Ca/P atomic ratio to stimulate the generation of a bone-like apatite layer is considered as a key feature for rapid bone rehabilitation. Titanium is stabilized following calcium phosphate formation with a Ca/P atomic ratio of around 1.6 when soaked in Hank’s solution, which is close to the stoichiometric molar ratio of hydroxyapatite. Furthermore, phosphorous and calcium can be detected at the interface located between the titanium biomaterial and bone tissue. The capability of titanium to form calcium phosphate is one of the contributing factors to its outstanding hard-tissue compatibility [127, 128].

**Osseointegration**

For a patient’s body to successfully accept the biomedical implant, it is instrumental to establish safe implant placement and shorten the postoperative healing period, as the human body will begin to reject the implants after a response to osseointegration for a minimum period [129, 130].

Due to the high dielectric constant of its surface oxide, titanium possesses the capability to form a direct interface with and bond well to living bone tissue without intervening soft tissue. This high dielectric constant does not denature proteins when titanium biomedical implants are inserted into the body. Such functional ankylosis enhances the durability and mechanical stability of load-bearing titanium implants as compared to biomaterials that require the use of adhesives, as the amount of force required to break the physical bond formed between the human bone and titanium inset is considerable [129, 131]. However, according to other researches, in early implementations of implants into the human body made of CP-Ti, the surface of the biomaterial is unable to integrate with the patient’s bone due to the bioinert surface property of titanium [132, 133]. This leads to a longer healing duration and occasionally the surface encapsulation of the implant over time. The possible consequences are the loosening of the implant, the formation of wear debris or fibrous tissue developing at the implant site, micromotion, and the possibility of fracture or delamination at the implant–bone interface [134, 135].

The key factors that determine the successful osseointegration of implants include biological compatibility in that the implant is not toxic to the surrounding living tissues, mechanical compatibility in that the implant is able to transfer stress loads between the receiving living tissue and the root of the placed implant, and morphological compatibility in that the implant is able to promote bone cell growth at the implant location [136, 137].

**Strategies to enhance the antimicrobial properties of titanium alloys through ultraviolet (UV) irradiation**

The surface of pure titanium shows signs of decreased histocompatibility over time. The application of UV irradiation reverses the effects of the biological aging phenomenon through the physiochemical alteration of the titanium surface, a process known as photo-functionalization [138]. Titanium implants used in dental surgery are sterilized via UV irradiation [139]. In addition, there is potential in exploring the antibacterial effects of UV irradiation on orthopedic biomaterials typically comprised of titanium alloys, including Ti–6Al–4V. Accordingly, evaluations have been performed on the antimicrobial and bactericidal effects of UV irradiation, at a shorter and lower dosage than in prior applications, to treat Ti and titanium alloy Ti–6Al–4V for utilization in implant surgery [140, 141].

Postoperative infections involving the use of metallic biomaterials comprise a significant complication for patients. Thus, multiple studies have attempted to develop methodologies that can alter the surface of implants to prevent or reduce the initial bacterial adhesion. These alterations are based on the principle of hindering the ability of microorganisms to form biofilms by enabling the patient’s cells to attach to the implant surface first. Pure TiO₂ substrates with photocatalytic properties have been demonstrated as capable to function as disinfectants and eliminate organic compounds when exposed to UV irradiation [142, 143]. Prior studies have shown the bactericidal effect of Ti–6Al–4V alloy surface exposed to UV subtype UV-C light at 227 J/cm² dosages for 15 h. Studies have also indicated that exposing Ti–6Al–4V alloy to UV irradiation at lower duration and energy induces increased bioactivity and osteoconduction. However, the dimensions of the implant are typically determined perioperatively, which leads to challenges in preparing the implants by UV irradiation before surgery. The difficulties experienced in the perioperative replication of the aforementioned antimicrobial strategies in clinical practice involving total implant surgeries have led to the conclusion that it is necessary to evaluate the antimicrobial and bactericidal effects of exposing Ti and Ti–6Al–4V to UV irradiation of shorter durations and energy levels [140].

Based on previous knowledge, one study investigated how UV irradiation contributes to the antimicrobial effect, which involved seeding *Staphylococcus aureus* 834 bacterial suspensions onto Ti and Ti–6Al–4V disks that had been exposed to a 9 J/cm² dosage of UV light for a period of 15 min. The evaluation of the bactericidal effect of UV irradiation involved seeding the bacteria onto the disks at different time points after UV irradiation under the

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same conditions. The time periods were 0, 0.5, 1, 6, 24, and 48 h, followed by 3 and 7 days. After harvesting and culturing the bacteria, the colonies were counted in both groups. Findings showed the absence of colonies on the UV-irradiated disks after seeding the bacteria. After the addition of bacteria onto the UV-irradiated disks, the number of live bacteria initially decreased before showing a steady rise. However, the antimicrobial effect faded over time [140].

The conclusive results showed that UV-irradiated Ti and Ti-6Al-4V exhibited similar antimicrobial properties, the bactericidal effect was maintained for a week post-UV irradiation on both disks, and this effect was similar on both types of disk. In addition, low-energy and short-duration UV irradiation was determined to contribute to the bactericidal effect on both Ti and Ti-6Al-4V [140].

Surface modifications of titanium

The detailed description of the surface properties of the biomedical implant, such as its surface morphology, structure, and chemistry, is critical to determine the reactions between the biomaterial implanted into the body and the associated live tissues [144]. The biocompatibility of a biomaterial is typically improved via modifying its surface properties through a combination of biochemical coatings and morphological changes. The main aim of these surface modifications performed on implants is to avoid foreign body response, decrease bacterial adhesion and inflammatory reaction, as well as increase implant integration and tissue adhesion [145].

Biocompatibility has shown to be dependent on the interrelation of various factors influencing the bulk and surface properties of biomaterials, which include surface topography (e.g., surface roughness), surface chemistry (e.g., surface tension and purity for wetting), and nature of tissue integration (e.g., fibrous, osseous, or mixed) [146–148].

Roughness modifications commonly applied to titanium and titanium alloys can yield significant improvements in biomedical performance without compromising the bioinert nature of these materials. Furthermore, chemical modifications may be required to ensure rapid osseointegration. These include deposition methods, such as precipitating calcium phosphate through immersion into synthetic body fluid, electrodeposition, protein absorption, and plasma spray [149, 150]. Alternatives to chemical modification have also been developed, such as the biomolecular functionalization of implant surface with various biomolecules, including collagen, fibronectin, peptides, as well as bioengineered protein fragments. Regardless, the critical mechanism involved pertains to how the bioactive molecule binds to the surface of the implant, as well as the method of immobilization [151–153].

The host environment has been reported to have the most significant influence on the biomaterial-to-tissue interface zone, where the interaction occurs between the implanted biomaterial and recipient tissues. This interface zone, which involves the implant surface layer and several nanometers into the recipient tissues, determines the circumstances of healing, as well as the clinical longevity of the implant’s load-bearing function [121].

The mechanical methods generally used for titanium and titanium alloys to obtain rough surfaces are subtraction processes, such as blasting, grinding, machining, and polishing, while smoothing the surfaces requires attrition processes, such as milling. The objective of such mechanical modifications is to produce a surface with specific topographies for improved adhesion in bonding while cleaning or roughening the surface, since the increased surface roughness of the implant structure is deemed more conducive for biomineralization [154, 155].

Chemical methods, such as acid and alkaline etching, biochemical surface coating methods, chemical deposition, and electrochemical anodization, are generally utilized to provide titanium and titanium alloys with bioactive surface characteristics. The aim is to improve bioactivity, biocompatibility, corrosion resistance, and osteoconduction and remove any contaminations. Obtaining irregular morphologies for titanium implant surfaces on the nanoscale can be achieved through a multitude of chemical methods, while electrochemical anodization is generally used when the aim is to fabricate controlled nanostructures, such as nanodots, nanorods, and nanotubes [156–158]. The fabrication process of titanium dioxide nanotube (TNT) arrays by anodization is shown in Fig. 4.

Physical surface modification methods do not require chemical reactions to produce the desired engineered surface. Such methods include glow discharge plasma treatments, ion implantation, physical vapor deposition, and thermal spraying. The resulting layer of coating or film formation on the surface of titanium substrate is simply a product of transferring various types of energy, such as kinetic, electrical, or thermal, which is unique to each method [159–161].

Titanium/silver physical vapor deposition (PVD) coatings

The formation of biofilm and endoprosthesis infection are regular issues pertaining to complications of implant surgeries. Adjustments to the implant surface prior to implantation have been applied to overcome such postoperative infections. One of the techniques for surface modification to improve the biocompatibility and antimicrobial properties of titanium
is silver coating by PVD. Several researches have been conducted to develop antimicrobial coatings with titanium and silver using PVD [162, 163]. Some of the recent studies investigated the mixed system of anodization and PVD to improve the titanium/silver coating, and the results showed the deposition of Ag$_2$O on the edges of highly ordered TiO$_2$ nanotubular arrays (schematic shown in Fig. 5) [128].

Relevant techniques involve direct impregnation utilizing antibiotics before implantation, or polymer coatings doped with antibiotics or silver. The antimicrobial activity and non-toxic nature of active silver ions to human cells have been well established, as only a few bacteria are intrinsically resistant to silver via resistance mechanisms derived from plasmids [162, 164]. The incorporation of silver ions into polymeric materials has been extensively performed for some time [165]. Urinary and central venous catheters use silver coatings, while dialysis units or heart valves have silver dotted surfaces to reduce infection [166]. Unfortunately, the relevant techniques may not meet the mechanical requirements for load-bearing biomedical implants, particularly those implanted into bone, due to the high levels of abrasive and shear forces occurring at the implant-bone interface.

Moreover, the PVD process is commonly utilized in medical and technical applications due to the excellent adhesiveness and wear resistance of ceramic and metallic coatings. In one study, silver–titanium was applied to samples of titanium alloys by PVD and tested for bactericidal action, biocompatibility, and hardness. The objective of the study was to assess the antimicrobial capability of coatings with silver ion under an aqueous environment, without compromising the hardness and biocompatibility of titanium with soft and hard tissue, for utilization in biomedical implants with load-bearing requirements, such as knee joints or hip joints [167].

In one study, both titanium and silver were vaporized in an atmosphere filled with inert argon, and antimicrobial coatings with a thickness of about 2 µm were deposited on the titanium surface. Through X-ray analysis, the silver content of the coatings was determined to be about 0.7% to 9%. Subsequently, eukaryotic culture cells and microorganisms were grown on these surfaces. After immersion in phosphate-buffered saline (PBS), the coatings released adequate amounts silver ions (between 0.5 and 2.3 ppb) and displayed remarkable antimicrobial potency against Klebsiella pneumoniae and Staphylococcus epidermidis strains.
Furthermore, the coatings had no cytotoxic effects on the epithelial cells and osteoblasts [168].

Using commercial grade 2 pure titanium as control, the reaction of *Klebsiella pneumoniae* and *Staphylococcus epidermidis* bacterial strains on surfaces dotted with silver was observed. The datum for the adherence of bacteria to the control surface was defined as 100%, and bacterial contamination on the surfaces containing silver was subsequently recorded. *Klebsiella pneumoniae* displayed reduced adhesion ($p < 0.05$) on the surfaces with 0.7% silver to 4% silver in the range of 32–64%, respectively. Meanwhile, *Staphylococcus epidermidis* displayed reduced adhesion ($p < 0.01$) on the surfaces with 0.7–4% silver in the range of 43–52%, respectively. Due to their similar mechanical performance to pure titanium, titanium silver (Ti-Ag) coatings may be a viable antimicrobial strategy for load-bearing implant surfaces [168].

**Advanced manufacturing (AM) of titanium alloys for biomedical application**

The fabrication techniques of titanium alloys for biomedical application include casting and powder metallurgy, cold working and hot working, machining, and additive manufacturing. Titanium alloys are manufactured into three types, including $\alpha$, $\beta$, and $\alpha+\beta$. Some alloying elements are dissolved preferentially in $\alpha$ phase such as Zr, Al, Sn, O, and Si raising the $\alpha+\beta$-phase. The addition of these elements results in the modification of alloy properties, such as in hardening and tensile strength improvement. Oxygen plays a dominant role controlling the range of strength of several grades, which are collectively called CP-Ti. The $\beta$-phase transformation stabilizes titanium alloys and makes them suitable for biomedical application because of their subsequent low modulus (which is below that of the $\alpha$- and $\alpha+\beta$-phase and near that of the human femoral bone), and confers them high specific strength [76].

The CP-Ti and Ti-64 are manufactured via the traditional routes, such as strips, sheets, plates, bars, billets, forgings, and wires, specified according to the American Society for Testing and Materials (ASTM) as grades 1–5. Grades 1–4 comprise the unalloyed CP-Ti, and grade 5 is the alloyed Ti-64 [169]. One of the AM methods is the powder-based additive manufacturing technology of titanium and its alloys, with the advantages of low-cost, resource-saving, suitable time, and customized parameters for fabrication, and has received great attention for biomedical application [170]. The quality of additively manufactured implants highly depends on the selected additive manufacturing technique and the quality of titanium and its alloy powders. Additive manufacturing techniques employed to fabricate the biomaterials include directed energy deposition [171], laser-based powder bed fusion of metals (PBF-LB/M) [172], powder fed system of binder jetting [173], electron beam powder bed fusion of metals (PBF-EB/M) [174], plasma atomization [175], gas atomization [176], and plasma rotating electrode process [177].

Developments in porous titanium structures for biomaterial application have enabled design optimizations for
patient-tailored implants. The additive manufacturing techniques allow for the fabrication of porous surface structures with predetermined, predictable unit cells for a biomedical implant, which have the necessary capabilities such as promoting cell proliferation and osseointegration. Thus, biomedical implants can achieve mechanical properties similar to those of human bone, such as compressive strength and elastic modulus, thereby preventing post-implantation complications, like stress shielding effects [178, 179]. To achieve such desired traits, it is necessary for biomedical implants to have an accurate design of porosities and pores to replicate the various mechanical properties and characteristics of the two main categories of bones, namely cortical bone and trabecular bone [180]. Despite having a similar composition, these two bone types vary in the degree of porosity and the proportion of organic and inorganic materials. The combination and organization of these two categories of bone differ according to the applied mechanical loading, as well as the skeletal region. Cell differentiation and proliferation are also affected by the morphology of pores, which is related to the pore size, porosity, and pore quantity [181].

Cellular structures can be classified into two main types, namely stochastic and non-stochastic. The cells in stochastic structures vary randomly in shape and size, while non-stochastic structures can be defined by the periodic repetition of the lattice structure with a unique shape and size of cells. Due to the absence of random variations in their cell shapes and sizes, non-stochastic metal structures are considered superior to stochastic metal foams on the basis of fabrication via powder bed technologies, which leads to better mechanical properties and the ease of removal of unfused powder [182, 183].

Evaluations have been performed on how variances in non-stochastic structures, such as the shape and size of pores, permeability, and porosity, affect the in vitro biological outcomes, as well as the mechanical properties of Ti–6Al–4V scaffolds fabricated via selective laser melting (SLM). The different pore shapes had an effect on cell permeability and consequently the number of cells attached to the Ti–6Al–4V scaffold. Other studies also reported that the circular cell growth pattern was not dependent on the shape and size of pore, which was primarily attributed to the amount of pore occlusion being higher on hexagonal pores in comparison to rectangular or triangular pores [184].

Moreover, research has been carried out on titanium hip implants with the aim of reducing the stress shielding effects without compromising mechanical strength. This was achieved by applying finite element analysis (FEA) to the design process and utilizing electron beam melting (EBM) fabrication technologies. A periodic lattice structure was used to modify the solid stems to achieve the desired reduction in implant stiffness. The comparisons between the constructed model and the simulated model demonstrated the possibility of utilizing EBM to fabricate non-stochastic lattice structures. The orientation of lattice struts was also instrumental to the fabrication process. Due to differences among the surfaces of struts between the EBM-fabricated model and the FEA-simulated model, the design of implants had to incorporate safety factors. The FEA model featured a consistent cross-section with a smooth surface, whereas the fabricated struts exhibited cross sections with slight variances coupled with textured surfaces. The study involved three model configurations, namely complete solid, hole configuration, and mesh configuration. The mesh configuration incorporated into the Ti–6Al–4V stem was found to possess better stress distribution characteristics at the proximal portion of the femur [185–188].

Another study was conducted to determine the properties of porous structures in terms of internal geometry, pore size, and pore density in Ti–6Al–4V fabricated by continuous laser melting deposition (LMD) and pulsed LMD. Both fabrication methods were shown to produce different internal porous structures, while optimizing the parameters such as laser power and powder mass flow rate yielded different densities in both cases. Ti–6Al–4V powder was used as the deposition material on the substrate, and parameter optimization resulted in the fabrication of suitable pores for osseointegration. Analytical models of the processes built using Wolfram Mathematica software are also necessary to find interacting, transient heat, temperature, and mass flow models [189]. A more controlled porosity was obtainable by utilizing a pulsed beam fabrication methodology as compared to a continuous beam. A regular structure was instrumental to avoid premature failure [190].

### Effect of alloying elements on biocompatibility, corrosion resistance, and mechanical properties

In order to develop safer biological Ti alloys with high strength and ductility, biocompatible alloying elements were examined as alternatives to V and Al. The strength of the alloy was found to increase with the Zr and Sn content. In this regard, Sn is more effective than Zr, while Nb, Ta, and Pd are less potent; therefore, the tensile strength of Ti–15Sn–4Nb–2Ta–0.2Pd is higher than that of Ti–6Al–4V for medial implants [191, 192]. Elements such as Mo, Zr, Ta, Sn, and Nb are selected as the safest alloying metals to adjust the properties of the biomaterial and maintain its suitability for implantation [76]. The β alloying elements of titanium, including V, Mo, Nb, Ta, and Zr, improve its corrosion behavior. Accordingly, it has been proven that Ti–6Al–4V has higher corrosion resistance compared to titanium alloyed with elements such as Co and Cr alloys, while pure titanium has higher pitting corrosion resistance rate. The β-phase stabilizing elements, such as Mo and V,
improve the stress corrosion cracking of titanium owing to the increased heat treatment capability [193–195].

Titanium β-phase alloys, including Ta, Nb, Zr, and Sn, have excellent mechanical properties, such as low Young’s modulus, high strength, good cold workability, and good biocompatibility and, therefore, have been more commonly used in recent years [76, 196, 197]. Moreover, Mo in titanium is not suitable for biomaterial application in high amounts due to the increased possibility of ion releasing to the surrounding tissue, resulting in totally diminished cytoplasm content and reduced cell spreading. Therefore, this element must be used in small quantities, just as Ni, V, and Al [198]. Cell culture experiments on osteoblast cells with Ti–5Nb–xFe alloys showed that the rate of cell proliferation is related to the amount of Fe and the chemical bonding between Fe and cells and that Fe with specific ratio has good biocompatibility [199]. The ranking of elements added to Ti in bioimplants regarding their cell viability enhancing effect, from lowest to highest, is Cu < Al < Ag < V < Mn < Cr < Zr < Nb < Mo < Cp-Ti, and that regarding their cytotoxicity is Cp-Ti < Sn < Ta < Mo < Nb < Zr < Cr < Mn < V < Ag < Ni = Al < Cu [200–204].

Potential of titanium alloys for regenerative medicine and nanomedicine

Properties of titania nanotube arrays (TNA)

Nanomedicine aspires to supply a valuable set of research tools and clinically functional devices for different biomedical applications. Titania nanotube arrays (TNA), also known as titanium dioxide nanotube (TNT) arrays, are garnering significant prominence as nanomedicine technique thanks to improvements to orthopedic procedures due to its unique properties, including a high specific surface area and the capability to exhibit a positive cellular response. TNA can be fabricated by various chemical, electrochemical, and physical methods. Self-assembled nanotube arrays grown using anodic oxidation have been of particular interest due to the cost efficiency and ease of fabrication, combined with the exceptional electrical, optical, structural, and thermal properties exhibited by these nanotubes. The anodization layering process produces a continuous array of TiO2 nanotubes vertically aligned on the surface of titanium alloy [205–207].

Applications in localized drug delivery systems

TiO2 nanotubes (TNT) comprise a viable option for localized drug delivery systems to address shortfalls in conventional drug delivery. Several methodologies can be utilized to control extended drug release in small dosages for long-term therapies, such as adjustment of pore openings via biopolymer coatings, modification of internal chemical characteristics, regulation of TNT dimensions, and utilization of polymeric micelles as drug nanocarriers [208, 209]. Strategies to control drug delivery from TNTs are shown in Fig. 6. Emergency conditions, such as the sudden onset of inflammation, osteomyelitis, and unexpected viral attack, may arise with an imminent requirement for high concentrations of drugs [210]. Such critical situations can be addressed by employing stimuli-responsive drug delivery systems triggered by external conditions, such as magnetic, pH, radiofrequency (RF), temperature, ultrasound, ultraviolet (UV) light, or voltage-sensitive drug delivery systems. The concept of stimuli release is based on the application of magnetic field, RF signal, ultrasonic wave, UV light, or voltage field to induce the movement of related stimuli particles, and forcing the release of polymer micelles out from the TNT. External stimuli for on-demand and responsive drug delivery can also be triggered via changes in the pH and temperature of the surrounding bioenvironment. The internal volume of TNT may be filled with biomolecules and chemicals, such as proteins or enzymes. Extrapolating this approach, titania nanotube arrays (TNA) may be coated with drugs that reduce inflammation, an example being dexamethasone, by utilizing the physical adsorption or deposition of a drug via a drug delivery system that is stimuli responsive. This application can work in conjunction with post-remission therapies, such as stem cell transplant and radiation therapy [211, 212].

Some researchers have attempted to fabricate smart implants with an on–off drug release capability using temperature as the external stimulus. It is assumed that the formation of a thermosensitive polymer coating on the surface of TiO2 NTs endows a sustained release potential, resulting in lower required drug dosages and decreased systemic toxicity. The schematic of the drug encapsulation and release mechanisms is shown in Fig. 7. The polymer coating on top of the nanotubes undergoes a rapid transition from a hydrophilic state with coil-shaped polymer chains to hydrophobic globules at a specific temperature, which results in the release of the drugs in a specific area of the human body. This phenomenon leads to the partial removal of the protective shell from the surface of TiO2 NTs and the generation of preferred trajectories for drug diffusion within the surrounding environment [213, 214].

Applications as immunomodulatory agents

Recent advancements in nanomedicine have facilitated the development of new immunomodulatory agents that include immunosuppressive agents or immunologically active components. In conjunction with an immunosuppressive agent, the unique surface structure of TNA enables the effective reduction of compromising immune responses that would contribute to unsuccessful transplants as a result of
localized autoimmune or allergic reactions [205, 215]. Such applications have the potential to significantly enhance clinical outcomes for a range of infectious and non-infectious diseases.

**Applications as antibacterial agents**

Coating the TNA nanomatrix surface with drugs that reduce infections, including streptomycin and penicillin, can be utilized to mitigate the bacterial colonization of indwelling medical devices. The medical device surface is aligned with TNA to act as an antimicrobial chemotherapy agent. The internal cylindrical surface of the aligned TNA is then coated with bactericidal antibiotics such as streptomycin and penicillin. This antibacterial surface provided by the TNA coated with bactericidal antibiotics has proved to inhibit and mitigate bacterial growth, thereby reducing the risk of bacterial infection originating from the system [216, 217]. Nanomedicine approaches also provide an enhanced solution to limit bacterial infection by delivering traditional antibiotic treatments. Research has established the utilization of nanotubes with larger diameters (30 to 100 nm) as compared to nanotubes with smaller diameters (around 20 nm), which may potentially stunt the growth of bacteria such as *Staphylococcus epidermidis* or *Staphylococcus aureus* [218].

**Applications for hemocompatibility**

TNA is a viable option as a nano-blood-contacting agent; it has the ability to transform fibrinogen to fibrin, thereby increasing the formation of a dense fibrin network and subsequently reducing the clotting time. The topology of TNA is conducive to enhancing the activation and adhesion of platelets, protein absorption of the blood serum, and kinetics of blood coagulation. In addition, the surface of TNA has the potential to act as a link between biological substances for propitious implants that are blood related [219]. TNA also evokes low cytokine secretion and monocyte activation. The adsorption of blood on TNA enables further evaluation through the utilization of micro bicinchoninic acid (BCA) assay, as well as X-ray photoelectron spectroscopy [220–222].
Conclusions and future directions

Pure titanium (Ti) and its alloys have been used extensively as medical implants owing to their high biocompatibility, fatigue life, corrosion resistance, and lower Young’s modulus compared to other medical implants. With the development of AM technologies over recent years, the fabrication of medical devices has not only become cheaper and faster in comparison with conventional manufacturing techniques, but also these products have demonstrated superior mechanical properties with reduced tooling operations and material wastage. The biomedical application of AM technologies has garnered considerable popularity in recent years due to improved capabilities in the fabrication of implants specifically tailored to individual patients. AM technologies using biomaterials such as titanium can replicate patient organs and tissues with precision, which allows for the reproduction of complex porous structures that enable tailored cell morphologies, promote cell differentiation and proliferation, a requirement for bone in-growth, and act as an antimicrobial agent. These benefits consequently reduce the risk of implant rejection and accelerate the healing process.

Ongoing research is being conducted on orthopedic devices constructed from porous metal. Based on clinical studies using such porous metals like titanium foam, the formation of vascular systems in a porous area seems viable. The mechanisms of osseointegration in titanium foams share similarities with that in bone grafts, whereby the porous properties of the titanium foam facilitate considerable bone infiltration, allowing osteoblast activity to occur. Furthermore, the porous structure enhances vascularization and the adherence of soft tissue within the implant. Therefore, the utility of porous materials may see a future expansion in replacement arthroplasty and dental applications.

In the nanotechnology field, biomedical research and development primarily target improvements to current diagnostic and therapeutic methodologies. The ultimate goal is to reduce the overall medical cost by improving the efficiency and reusability of available practices. Thus far, titanium nanostructures have proved to be a viable option for advanced biomedical implants, as well as theragnostic applications; however, a more in-depth understanding of the biomolecular interactions involving titanium as a nanomaterial is necessary for further developments in this field.

Fig. 7 Proposed mechanism of thermal-triggered drug release from polymer-coated TiO₂ nanotubular structures before a and after b heating. At low temperatures, the polymer capping forms a uniform protective layer on the nanotubes, resulting in a negligible level of uncontrolled drug release. However, heating of the implant to a specific temperature leads to the coil-to-globule transition of the polymer shell and the provision of preferred routes for drug diffusion.
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Declarations

Conflict of interest The authors declare that they have no conflict of interest.

Ethical approval This study does not contain any studies with human or animal subjects performed by any of the authors.

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