Effect of Hip Prosthesis on Photon Beam Characteristics in Radiological Physics

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Abstract

Introduction: Aim of study is to investigate the effect of hip prosthesis on 6 and 15 MV photon beam energies.

Materials and Methods: Prosthesis was kept at the level of tray position. The measurements were done on Varian Clinac-iX linac. Customized prosthesis, termed as Prosthetic Metal Implant (PMI) was made up of wrought austenitic stainless steel rod and covered with paraffin-wax. ‘Standard prosthesis’ was made up of wrought titanium alloy. The dose profiles were measured for three field sizes i.e. 5, 10 and 20 cm at 100 cm SSD for 6 and 15 MV energies. The perturbation index (PI) was also calculated. Results: Perturbation caused by standard prosthesis was approximately 50% higher than that of PMI. This result may be due to difference in dimension and not because of material composition. Variation of central axis dose might be due to the dimensions of PMI used for experiment which gave intermediate response (e.g. 102.1%, 141.0% and 117.7% for Open, Standard and PMI respectively for 10x10 cm² field size, 10 cm depth and 15MV photon beam setup as compared to the ‘open’ and ‘standard’ prosthesis. Percentage dose at 10 cm field was increased rapidly with field-size for PMI. But, for 15MV photon, difference was not significant. Surface dose remains significantly higher for smaller field. Conclusion: The perturbation index varied from 0.05 to 0.22 for the measured energies and gave an idea to the planner to assess the behavior of the prosthesis. This range is applicable for both type of implants and for all clinical field-sizes. The attenuation caused by the prosthesis was significant and this effect should be considered in the treatment planning calculations.

Keywords: Prosthesis- photon- PDD- surface dose- perturbation index

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Introduction

Treatment planning of pelvic tumors (like bladder, rectum, anal canal, cervix and prostate) in radiotherapy with high density metallic prosthesis is always a challenging task. The composition of material as well as its form and location needs to be considered by the planner before radiotherapy planning. Behavioral study of high density materials have always been an area of interest in the field of clinical radiation physics. Wieslander and Knoos (2003) investigated the behavior of these materials which may be useful for accurate dose estimation in radiotherapy planning. The numbers of patients with hip prosthesis are increasing day by day in radiotherapy practice. The position of prosthesis (far or near to the target) alters the dose and creates dose inhomogeneity for the target. Ding and Yu (2001); Tang et al., (2013) reported that in order to avoid this situation, planner should try to avoid the beam entry through prosthesis, but if it is necessary to place the beam in such places, proper estimation of dose is required. The planning Computed Tomographic (CT) images of patient having high density prosthetic material creates metallic artifacts and hence under- or over-estimation of the radiotherapy dose. The treatment planning systems do not predict the dose accurately for such cases. Monte Carlo simulation is the only way to calculate the dose precisely. The AAPM task group has looked into such scenarios and published a report for understanding the issue scientifically and dosimetrically. Baxter et al., (2005) concluded that the risk of hip fractures increased substantially in elderly women who had received pelvic irradiation in the past. In case of pelvic fractures and re-irradiation, one should be aware of the nature and behavior of hip prosthesis for proper estimation of the dose. Although the advancement of treatment planning and delivery techniques like intensity modulated radiotherapy (IMRT) has some advantage of static beam angles hereby avoiding metal prosthesis, yet the beam characteristics should be known in presence of...
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a high density material (Peter et al., 2013).

Large number of published literature describe the
effect of radiation on pacemakers (Adamec et al., 1982;
Katzenberg et al., 1982) and teeth fillings in head and
neck cancer patients (Thambi et al. 1979); however not
much work has been done to establish the effect of hip
prostheses on photon energies.

Hudson et al., (1984) proposed an assumption of
average effective density for the whole prosthesis for
calculating distortion in the dose distribution in treatment
planning systems. Similarly, Hazuka et al., (1989) noted
the dose deviation due to different types of prosthesis
in the photon beams and tried to find out the necessary
corrections for the same.

In the present study, we investigated the dose distortion
caused by the titanium prosthesis and wrought stainless
steel prosthesis with different photon beam energies in
the water phantom.

Materials and Methods

The prosthesis was kept at the level of tray position
in the collimator of linac head which is the recommended
position for the measurements. The experiments were done
on Varian Clinac-iX linear accelerator (Varian Medical
Systems). This linac is equipped with dual photon energies
i.e. 6 MV and 15 MV with additional electron energies
(6, 9, 12, 15 MeV). This equipment facilitates the planner
to conform the tumour target with Multi-leaf collimator
with 120 leaves (characterized by special resolution of
0.5 cm at isocentre for the central 20 cm and of 1.0 cm
in the outer 2x10 cm, with a maximum leaf speed of 2.5
cm/sec and a leaf transmission of approximately 1.4%) (Sharma et al., 2014).

Customized prosthesis, termed as ‘Prosthesis Metal
Implant (PMI)’ made up of wrought austenitic stainless
steel rod which was then further covered with paraffin-wax
to compensate for the tissue effect. Second prosthesis
was made up of wrought titanium alloy and was termed as
the ‘standard prosthesis’. Dimensions of prosthesis and their
experimental setup are mentioned below. As per literature
of Mears (1979), the composition of materials in alloy and their
densities are mentioned in Table 1.

The dose profiles across the beam were measured in the
3-Dimensional water phantom [Radiation Field Analyser
(RFA-300; Blue Phantom, IBA)] using cylindrical
chamber CC-13 (IBA) at two depths i.e. dmax and 10 cm
in the central axis of beam under the prosthesis. The profiles
were measured for three field sizes i.e. 5 x 5 cm², 10 x 10
cm² and 20 x 20 cm² at 100 cm source-to- surface-distance
(SSD) for both the energies i.e. 6 MV and 15 MV. The
cross-line and in-line profiles were taken and their profile
characteristics studied.

In order to report the surface dose, the depth dose curve
was plotted using the above experimental setup. Parallel
plate chamber PPC40 (IBA Dosimetry, Germany) was
kept in the water phantom with source-to-surface-distance
(SSD) 100 cm in the central axis and exposure was given
for a pre-set number of monitor units i.e. 100 MU. 6 MV
and 15 MV beams were used as they are the most usable
photon energies in pelvic irradiation. Software ‘OmiPro
Accept v7.2 (IBA Dosimetry, Germany)” was used for
the analysis of scanned curves. Depth dose curves were
measured upto the depth of 31 cm in water.

The percentage attenuation was calculated using
following formula and the perturbation index (PI) was
defined as (Sibata et al., 1990):

\[ \text{PI} = \frac{(A_2 - A_1)}{A_2} \]

Where, \(A_1\) = Area of dose profile under prosthesis
\(A_2\) = Area of dose profile without prosthesis

Results

Perturbation Index (PI)
The area of dose profile under prosthesis i.e. A1, was
calculated using integration of data, acquired under the
prosthesis Figure 1. The results were analyzed and are
tabulated in Table 2.

Central Axis Dose Variation (Ddev%)
The measured data is tabulated in Tables 3 and 4. The
beam in open medium delivers a particular dose to a fixed
point. But due to the introduction of high density metallic
implants, the dose deviates from the above reference
point. Central axis dose for standard prosthesis deviates
more for 10 x 10 cm² field size for both 6 MV and 15
MV energies in the cross-line profile, in comparison to
the PMI and open medium which was also reported by
Jia et al., (2015). In-line profile was also measured and
the results are tabulated in Table 4. It is clear that there
is no significant variation in the central axis dose in this

| Table 1. Composition of Prosthetic material. British Standard 3531 (1981) Approved Alloys for Surgical Implants |
|---------------------------------------------------------------|
| **(a) Composition of prosthesis alloys**                      |
| Principal constituents | Wrought austenitic stainless steel (%) | Wrought Ti alloy (%) |
|-----------------------|--------------------------------------|----------------------|
| Cr                    | 24.0-26.0                            | -                    |
| Ni                    | 19.0-22.0                            | -                    |
| C                     | 0.08 max                              | 0.08 max             |
| Si                    | 0.75 max                              | -                    |
| Mn                    | 2.0 max                               | -                    |
| P                     | 0.045 max                             | -                    |
| S                     | 0.03 max                              | -                    |
| Mo                    | 0.75 max                              | -                    |
| Cu                    | 0.50 max                              | -                    |
| Fe                    | Balance                               | 0.25 max             |
| V                     | 3.5-4.5                               | -                    |
| O                     | 0.13 max                              | -                    |
| Al                    | 5.6-6.5                               | -                    |
| Ti                    | Balance                               | Balance              |

| (b) Relative density to water|
|-----------------------------|
| Relative density           | 7.9 | 4.4 |
| Relative electron density  | 6.6 | 3.7 |
Effect of Hip Prosthesis on Photon Beam Characteristics

The x-ray photon beam attenuates and scatters as per inverse-square law after entering into the patient surface or water medium (Kaushik et al., 2017). The presence of metallic implant in the beam path hardens the beam and thereby increases the mean energy of the beam as evident from the plotted data Figure 2.

**Surface Dose (Ds)**

Study of ‘surface dose’ parameter is an important aspect in the study of behavior of implant material. In

**Percentage Depth Dose (PDDs)**

| Energy | Point of Measurement (cm) | Field Size (cm²) | Perturbation Index (PI) |
|--------|-------------------------|-----------------|------------------------|
|        | Dmax                    | 5 x 5           | 0.211                  |
| 6 MV   | 10 cm                   | 0.182           | 0.083                  |
|        | Dmax                    | 10 x 10         | 0.195                  |
|        | 10 cm                   | 0.178           | 0.074                  |
|        | Dmax                    | 20 x 20         | 0.215                  |
|        | 10 cm                   | 0.172           | 0.075                  |
| 15 MV  | Dmax                    | 5 x 5           | 0.178                  |
|        | 10 cm                   | 0.178           | 0.076                  |
|        | Dmax                    | 10 x 10         | 0.16                   |
|        | 10 cm                   | 0.153           | 0.071                  |
|        | Dmax                    | 20 x 20         | 0.178                  |
|        | 10 cm                   | 0.111           | 0.05                   |

Table 2. Measured Perturbation

Figure 1. Profile with Perturbation Showing A₁ and A₂

Perturbation Index (PI) = (A₂ - A₁)/A₂
order to find out the changes in surface dose, the PDDs were measured. The data acquired from these profiles was plotted in the form of curve Figure 3.

Discussion

Conformity of dose is essential part for any clinically deliverable plan. Dose conformity assures the planner for better clinical outcomes. But, the introduction of any metallic object in the path of the beam has chances to deviate the doses from its original dosimetric values which was also reported by Mohammadi et al., (2017). The effectiveness of treatment depends on the plan made by the planner (medical physicist) and evaluated by radiation oncologist, for delivering optimum treatment to the patient. But the metallic high-Z implants create artifacts in the computed tomographic images and alter the dose distribution. It is necessary for any planner to know the beam characteristics in the presence of such objects for better assessment of the treatment plans.

Perturbation Index (PI)

It is evident that the perturbation caused by prosthesis made up of titanium alloy was approximately 50% higher than that made up of wrought austenitic stainless steel. This was due to the difference in dimensions of

| Beam Energy (MV) | Field Size (cm²) | Depth of Measurement (cm) | Prosthesis Setup | Flatness (%) | Symmetry (%) | Field Width (cm) | Penumbra (cm) | Central Axis Dose Deviation (Ddev%) |
|-----------------|-----------------|--------------------------|------------------|--------------|--------------|-----------------|--------------|-----------------------------------|
| 6               | 5               | 1.5                      | Open (O)         | 3.8          | 0.1          | 5.04            | 0.53-0.53    | 101.1                |
|                 |                 |                          | Standard (S)     | 19.8         | 4.3          | 5.32            | 0.39-0.44    | 146.9                |
|                 |                 |                          | PMI (P)          | 9.9          | 0.8          | 5.22            | 0.45-0.46    | 122                  |
|                 |                 |                          | Open (O)         | 4.5          | 0            | 5.47            | 0.61-0.61    | 100.3                |
|                 |                 |                          | Standard (S)     | 17           | 4.4          | 5.74            | 0.48-0.52    | 139                  |
|                 |                 |                          | PMI (P)          | 8.6          | 1.2          | 5.66            | 0.53-0.53    | 118.4                |
| 10              | 1.5             |                           | Open (O)         | 1.9          | 0.1          | 10.18           | 0.58-0.57    | 100.7                |
|                 |                 |                          | Standard (S)     | 22.6         | 1.5          | 10.43           | 0.43-0.45    | 156.7                |
|                 |                 |                          | PMI (P)          | 2.3          | 0.3          | 10.36           | 0.64-0.63    | 103.3                |
| 20              | 1.5             |                           | Open (O)         | 1.8          | 0.1          | 20.34           | 0.60-0.60    | 100.9                |
|                 |                 |                          | Standard (S)     | 22.1         | 0.6          | 20.75           | 0.55-0.55    | 154.4                |
|                 |                 |                          | PMI (P)          | 10.2         | 0.1          | 20.58           | 0.54-0.53    | 122.6                |
|                 |                 |                          | Open (O)         | 4.1          | 0.2          | 22.01           | 0.89-0.85    | 100.6                |
|                 |                 |                          | Standard (S)     | 18.1         | 0.8          | 22.46           | 1.14-1.14    | 142.8                |
|                 |                 |                          | PMI (P)          | 8.2          | 0.1          | 22.27           | 0.86-0.87    | 117.8                |
| 15              | 5               | 3                        | Open (O)         | 4.8          | 0.4          | 5.15            | 0.60-0.59    | 100.7                |
|                 |                 |                          | Standard (S)     | 13.4         | 3.7          | 5.37            | 0.50-0.54    | 130.3                |
|                 |                 |                          | PMI (P)          | 7.3          | 0.2          | 5.29            | 0.55-0.55    | 115.6                |
|                 |                 |                          | Open (O)         | 5.4          | 0.7          | 5.5             | 0.66-0.66    | 100.8                |
|                 |                 |                          | Standard (S)     | 12.7         | 4            | 5.73            | 0.57-0.59    | 126.6                |
|                 |                 |                          | PMI (P)          | 6.2          | 1.2          | 5.64            | 0.62-0.60    | 113                  |
| 10              | 3               | 3                        | Open (O)         | 2.3          | 0.3          | 10.36           | 0.64-0.63    | 103.3                |
|                 |                 |                          | Standard (S)     | 19.1         | 1.4          | 10.59           | 0.55-0.56    | 146.5                |
|                 |                 |                          | PMI (P)          | 9.2          | 0.1          | 10.48           | 0.57-0.56    | 120.1                |
|                 |                 |                          | Open (O)         | 2.9          | 0.1          | 11.06           | 0.73-0.71    | 102.1                |
|                 |                 |                          | Standard (S)     | 17.5         | 1.3          | 11.29           | 0.67-0.67    | 141                  |
|                 |                 |                          | PMI (P)          | 8.3          | 0.5          | 11.18           | 0.67-0.65    | 117.7                |
| 20              | 3               | 3                        | Open (O)         | 2.7          | 0.1          | 20.22           | 0.65-0.64    | 105.1                |
|                 |                 |                          | Standard (S)     | 19.5         | 0.5          | 21.07           | 0.64-0.63    | 147.1                |
|                 |                 |                          | PMI (P)          | 9.6          | 0            | 20.91           | 0.64-0.62    | 121.2                |
|                 |                 |                          | Open (O)         | 2.2          | 0            | 20.22           | 0.86-0.86    | 104.1                |
|                 |                 |                          | Standard (S)     | 17.9         | 0.5          | 22.48           | 0.84-0.84    | 142.5                |
|                 |                 |                          | PMI (P)          | 8.6          | 0            | 22.31           | 0.78-0.78    | 118.7                |
the prosthesis. It may be noted that the composition of the implant was not accurately determined. Although, it may be possible to measure it inside the laboratory, yet the prosthetic implant inside the patient body cannot be measured accurately by any means. Mahuvava et al., (2018) also found that the absorbed dose dropped significantly due to beam attenuation. For bilateral prosthesis, the target dose was reduced upto 23% and 17% for stainless steel and titanium prosthesis. Also, for unilateral hip prosthesis, the dose reductions were 19% and 12% respectively.

Central Axis Dose Variation (Ddev%)  
The measured data showed that variation of central axis dose was approximately 20% for PMI material, whereas the standard implant created a 50% variation in central axis...
dose in comparison to the open field. The reason behind this might be the dimension of PMI used for experiment, which gave intermediate response (mentioned in Tables 3 and 4) as compared to the ‘open’ and ‘standard’ prosthesis. Shimozato et al., (2010) examined the parameter for skull fixation and found the differences between simulation and the planned results on the entrance and exit sides of the plate as 23.1% and 12.7% respectively.

### Percentage Depth Dose (PDDs)

Percentage dose at 10 cm depth for 6 MV photon increased rapidly with field-size. The metallic implant PMI also showed a similar pattern. But, for 15 MV photon beam, the difference among all the three setups was not significant. This might be possible due to the high linear energy transfer and lesser attenuation in the medium Figure 4. Lesser attenuation of higher photon beam energies deposit maximum dose to any reference point in the medium. The similar pattern was followed in the present study also. Carolan et al., (2000) studied the effect of hip prosthesis and showed a dose reduction of 52% in the shadow of the prosthesis. A Monte Carlo simulation confirmed an increase in dose to the distal surface of the prosthesis by approximately 35%.
Figure 4. Variation of Surface Dose ($D_s$)

**Surface Dose ($D_s$)**

The curve showed that the surface dose ($D_s$) for PMI remained moderately higher for smaller fields and showed a gradual decrease and further increase in pattern. This might be possible due to the scatter contribution in the dose output with increasing field size. But, for the standard prosthesis, the curve increased linearly with field size. For open setup, the curve follows a similar pattern, but remains at lower side. Catli (2015) also has demonstrated that the dose increases in the tissue at a distance of 2 mm in front of the implant due to backscatter.

**Limitations**

This study highlights the beam characteristics in the presence of high density metallic implant in the water medium. But the limitation of the present study is its lack of correlation with the clinical data. Hip prosthesis will always be implanted within the body; hence more studies are needed for better understanding of the treatment planning parameters related to the actual patient data.

In conclusion, our study elaborates the available information in the literature regarding different prosthetic materials in different photon energies. The attenuation caused by the prosthesis was significant and this effect should be considered in the treatment planning calculations. The surface dose changed significantly especially for the smaller field sizes and hence was more significant for the intensity modulation. The perturbation index varied from 0.05 to 0.22 for the measured energies which are in contrast with observations made by Sibata CH et al., (1990) and gave an idea to the planner to assess the behavior of prosthetic material used.

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