THD Reduction Using Shunt Active Power Filter: A Real Case Study

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Abstract Harmonic pollution in the industrial field causes extra heat dissipation and increased rms (root mean square) values of both voltage and current waveforms, which hence increase losses, decrease the overall efficiency, and increase the energy cost in power plants. Moreover, harmonic pollution results in a decline in industrial investment. A solution to mitigate harmonic pollution is proposed using an active power filter by identifying both the phase current and the voltage and then providing a compensation current the same in magnitude and negative in direction to the distorted current. In this paper, a three-phase active power filter for current harmonic compensation in power distribution lines is adopted. Practical measurements performed on the United Iron and Steel Manufacturing Company bus bar for different factory and Jordanian national power system grid loads demonstrate the validity of the proposed approach using a shunt active power filter (SAPF). Using p-q theory, the results show that the proposed SAPF is convenient for suppressing harmonic current. Hence, the overall power quality of the grid is improved, and the reliability is enhanced. Finally, this work is implemented using simulink/Matlab.

Keywords Energy consumption; Power harmonic filters; Power quality.

1 Introduction

The behavior of nonlinear loads has many undesirable effects on the quality of power systems. Harmonic contamination is a consequence of this behavior, which results in increased reactive power consumption, induces voltage fluctuations in the power line system, and creates additional problems such as electrical machine vibration, overheating in cables and transformers, and malfunction in power system components [1]. Many harmonic limitation standards such as IEEE519-1992, IEEE1459-2000, IEC1000-3-2, IEC1000-3-4 have been recommended to investigate the harmonic contamination problem effectively. Some of the available solutions (harmonic mitigation techniques) are summarized in [3][4], including reactors [5] (AC line reactors that provide better input protection, DC link reactors that provide better output voltage regulation and swinging choke design that provides enhanced light load harmonic performance), drive isolation transformers [6], passive filters [3], high-pulse-count rectification (12, 18, 24, 36 pulses), active methods [3] such as drive active front ends (AFEs; ULH or regen), and stand alone and shunt active power harmonic filters (SAPFs) [7]. Some of these harmonic mitigation techniques used in the market are shown in Fig. 1.

In the real world, the grid may black out due to devices that produce nonlinear loads, such as power supplies, computers, telecommunication equipment, battery chargers, electronics, and solid-state variable speed drives. Nonlinear loads cause stress in power system components. This excessive current is primarily thermal in nature, and the overall energy of a linear load is much less than that of a nonlinear load. A power system carrying a nonlinear load is less efficient. Therefore, it is important identify nonlinear loads and take correct action to reduce a negative impact on the power grid. Nonlinear loads distort sinusoidal wave currents in the power grid. Such distorted current waveforms become a problem, increasing line losses.
2 Shunt Active Power Filter

The nonsinusoidal currents or voltages that are present in a normally sinusoidal network are called harmonics. They are associated with nonlinear loads that draw nonsinusoidal currents from an essentially sinusoidal voltage source. Odd harmonics that are multiples of three in a three-phase power system are called triplen harmonics, which are theoretically absent in a balanced three-phase system. The concept of harmonics is helpful in using mathematics to quantify and systematically analyze complex distorted waveforms [8].

Harmonic currents interact with the impedance of a system at their respective frequencies and produce voltage distortion at those frequencies. Drawing distorted current can result in a reduction of productivity, which can shorten the life of all equipment on the grid and increase the neutral current. Moreover, it can cause malfunction operation of many types of electrical equipment [9]. To reduce the level of distorted voltage, it is important to limit the flow of distorted current. Thus, there is a need to remedy distorted waveforms in a power grid by defining and quantifying inconsistencies in the power grid. Resolving a nonlinear waveform into its components is called harmonic analysis.

Many theories have been considered to analyze a power system network under nonsinusoidal cases such as magnetic compensation [10], thyristor-based switching filters [11], an adaptive digital-control scheme [12] and instantaneous active and reactive power theory, or “p-q theory” [13].

In this work the p-q theory is implemented in the SAPF circuit that consists of three phase voltage source converter (VSC) [7][8]. P-q theory is defined in the time domain and valid both in transient and steady states, and it can be relevant to both three-phase power system or four wire (neutral) power systems as shown in Fig.2 and Fig. 3. It is based on an instantaneous power Clarke transformation from abc phases to three orthogonal axes αβ0 as shown in Equation (1) and Equation (2).

\[
\begin{bmatrix}
v_\alpha \\
v_\beta \\
v_\gamma \\
\end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix}
1 & \frac{1}{2} & \frac{1}{2} \\
0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \\
0 & -\frac{\sqrt{3}}{2} & \frac{\sqrt{3}}{2}
\end{bmatrix} \begin{bmatrix}
v_\alpha \\
v_\beta \\
v_\gamma \\
\end{bmatrix}
\]

(1)

\[
\begin{bmatrix}
i_\alpha \\
i_\beta \\
i_\gamma \\
\end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix}
1 & \frac{1}{2} & \frac{1}{2} \\
0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \\
0 & -\frac{\sqrt{3}}{2} & \frac{\sqrt{3}}{2}
\end{bmatrix} \begin{bmatrix}
i_\alpha \\
i_\beta \\
i_\gamma \\
\end{bmatrix}
\]

(2)

The instantaneous power \( S \) is given in Equation (3).

\[
S = v \star i^* = (v_\alpha + jv_\beta)(i_\alpha - ji_\beta)
\]

\[
= (v_\alpha i_\alpha + v_\beta i_\beta) + j(v_\beta i_\alpha - v_\alpha i_\beta)
\]

Hence, \( i_\alpha, i_\beta \) can be expressed as function of p-q as shown in Equation (4).

\[
\begin{bmatrix}
i_\alpha \\
i_\beta \\
\end{bmatrix} = \frac{1}{v_\alpha^2 + v_\beta^2} \begin{bmatrix}
v_\alpha & v_\beta \\
v_\beta & -v_\alpha \\
\end{bmatrix} \begin{bmatrix}
p \\
q \\
\end{bmatrix}
\]

(4)

The extra amount of real power is presented by \( \widetilde{p}_{loss} \) that has been regulated with the \( V_{dc} \). The capacitor is used to store the additional energy that flow. The compensated power \( \widetilde{p}_{loss} \) and the compensated imaginary power \( \widetilde{q} \) are added then passed as \( \alpha, \beta \) current reference calculation as shown in Equation (5). The compensated currents \( i_{ca}, i_{cb} \) and \( i_{cq} \) are obtained using inverse Clarke transformation as shown in Equation (6).

\[
\begin{bmatrix}
i_{ca} \\
i_{cb} \\
i_{cq} \\
\end{bmatrix} = \frac{1}{v_\alpha^2 + v_\beta^2} \begin{bmatrix}
v_\alpha & v_\beta \\
v_\beta & -v_\alpha \\
\end{bmatrix} \begin{bmatrix}
\widetilde{p} + \widetilde{p}_{loss} \\
\widetilde{q} \\
\end{bmatrix}
\]

(5)

\[
\begin{bmatrix}
i_{ca} \\
i_{cb} \\
i_{cq} \\
\end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix}
1 & -\frac{1}{2} & \frac{1}{2} \\
0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \\
0 & -\frac{\sqrt{3}}{2} & \frac{\sqrt{3}}{2}
\end{bmatrix} \begin{bmatrix}
i_{ca} \\
i_{cb} \\
i_{cq} \\
\end{bmatrix}
\]

(6)

The most general harmonic indices are as follows:

1. Total harmonic distortion (THD) is the root mean square (rms) value of the harmonic content expressed as a percentage of the fundamental component. THD is given by (7).

\[
THD = \sqrt{\sum_{n=2}^{N} \frac{X_n^2}{X_1}}
\]

(7)

where \( X_n \) is the rms of a certain waveform at harmonic order \( n \), \( N \) is the supreme harmonic order and \( X_1 \) is the fundamental rms value of the same waveform.
2. Total demand distortion (TDD) is very similar to THD but is expressed as a percentage of the rated waveform magnitude. TDD is given by Equation (8).

\[
TDD = \sqrt{\frac{\sum_{n=2}^{N} X_n^2}{X_R}}
\]

where \(X_R\) is the maximum rms value demand for the waveform at the fundamental frequency.

![Figure 2](image2.png)

**Figure 2.** The proposed active power filter system [7].

![Figure 3](image3.png)

**Figure 3.** Control scheme for the SAPF [8].

### 3 UISM Case Study

The United Iron and Steel Manufacturing (UISM) Company, Amman, Jordan, has a 33 kV bus bar in Queen Alia International Airport (QAIA) substations. The Jordanian national electric power grid faces problems associated with harmonics. Any component failure at UISM leads to a catastrophic consequence, and this may cause a loss of operation capability, a loss of production, critical safety concerns and poor power quality. When components under operation run at higher temperatures than designed, the operation of the power plant can be less than optimistic. In this case, insulation can melt, and shutdown is usually the result. At UISM, this can create a source of ignition with potentially tragic damage.

UISM operates a 40 MT (metric tonne) electric arc furnace (EAF) rated at 15 MVA, a 40 MT ladle furnace (LF) rated at 6 MVA, a casting machine and rolling mills that are supplied via a grid connection from the Queen Alia International Airport bulk supply point. This type of electrical load behaves as a highly nonlinear load, which produces a large harmonic distortion in the power line system. The main harmonic sources at UISM are arcing devices such as welders, arc furnaces, fluorescent lights and variable frequency drives. The electrical demand of the arc furnace is characterized by rapidly fluctuating active and reactive power, which put excessive mechanical and electrical stresses on the power plant, reduce the economic life of the power plant and result in high maintenance requirements and a loss of production due to a lack of spare capacity. To overcome these difficulties, UISM installed a SAPF. The collected data form the UISM power system showed high noise in the current waveform, with high levels up to 13th harmonics. This type of current is very harmful for an electrical system.

![Figure 4](image4.png)

**Figure 4.** Three-phase voltage source.

### 4 Results and Discussion

In this work, the computations were focused on THD, the phases of the harmonic voltage and current, and the overall system losses due to the harmonics. A significant increase in cost due to harmonics can be classified into three categories: harmonic energy losses, the lifespan of electrical equipment and the de-rating of electrical equipment. Utilities and the end users are adversely affected by the poor power quality and low power factor, and a penalty may therefore force polluted customers to take action using harmonic mitigation equipment. The steel plant substation is switched by disconnecting the electrical load, which consists of furnaces and general services.
The steel plant is simulated. First, the current THD created by the plant is calculated.

The different operational states of the UISM factory are investigated, which provide valuable information in evaluating the plant is calculated. The different operational states of the UISM factory are investigated, which provide valuable information in evaluating the plant.

The portable fault recorder was triggered carefully through different day periods, taking into account the change in the daily loads, making sure that the measured data cover all the factory situations: heavy, normal, and light loads and sudden load changes. A heavy case is investigated, where the voltage and current for each phase are recorded by the PFR. A
15 MVA, 33 kV three-phase source 50 Hz block feeds the load. The load voltages and currents waveforms are shown in Figs. 4, 5, 6, 7, 11, 12 & 13 and are highly nonlinear. The voltages of arc ignition decrease as a consequence of the short-circuit current, which is limited by the power system impedance of 5Ω. Figs. 14, 15 & 16 show that the distortion levels are unacceptable, and the need for a SAPF becomes evident. As a consequence, the THD current levels decreased by 63.86%, 69.73% and 42.69%. The system was upgraded by connecting a SAPF. The THD levels for the three-phase currents are enhanced to 19.01%, 16.2% and 16.4%.

Table 1. THD with and without the SAPF.

| THD % |  $I_{\phi,a}$ |  $I_{\phi,b}$ |  $I_{\phi,c}$ |
|-------|--------------|--------------|--------------|
| Without SAPF | 89.43 | 61.21 | 71.42 |
| With SAPF | 32.32 | 18.5 | 40.93 |

Table 2. Comparison between with and without SAPF

| Phase |  $I_{rms}$ (A) |  $V_{rms}$ (V) |  $\Phi$ (deg) |  $I_{rms}$ (A) |  $V_{rms}$ (V) |  $\Phi$ (deg) |
|-------|----------------|----------------|--------------|----------------|----------------|--------------|
| Without SAPF | 377.47 | 1.943 x 10^4 | 3.8 | 416.56 | 1.953 x 10^4 | 3.02 |
| With SAPF | 345.44 | 1.9% x 10^4 | 4.01 | 399.97 | 1.98% x 10^4 | 3.05 |
| Phase b | 358.68 | 1.9% x 10^4 | 4.30 | 408.47 | 1.9% x 10^4 | 3.28 |

5 Conclusions

The presence of harmonics can cause a wide range of failures and malfunctions in a power system grid. Hence, harmonics are not to be ignored. A certain level of harmonics is acceptable, especially in power plants with high nonlinearities. However, action should be taken to guarantee that this limited is not exceeded to avoid utility penalties and misoperation.

In this paper, a three-phase SAPF for current harmonic compensation is proposed based on the principle of inserting negative harmonics into the network, thus eliminating the undesirable harmonics. Practical measurements performed on the UISM factory bus bar for different factory and national power system grid loads are used to validate the proposed active power filter, showing that the intended SAPF has adequate effectiveness in terminating harmonic current.

In future work, more research should focus on issues such as harmonic measurement devices and malfunction of electrical components due to harmonics, including noise in transformers and rotating electrical machines. In addition to the potential economical impacts, the sizing and rating of components, utility penalties, power factor correction and capacitor resonances due to harmonics and harmonic measurement devices are also important factors.

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