Optomechanical tailoring of quantum fluctuations

S. Mancini

INFM and Dipartimento di Fisica, Università di Milano, Via Celoria 16, 20133, Italy

H. M. Wiseman

School of Science, Griffith University, Nathan, Brisbane, Queensland 4111 Australia

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We propose the use of feedback mechanism to control the level of quantum noise in a radiation field emerging from a pendular Fabry-Perot cavity. It is based on the possibility to perform quantum-nondemolition measurements by means of optomechanical coupling.

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I. INTRODUCTION

Optomechanical coupling between light and (movable) mirrors gives rise to a variety of intriguing effects. A wide class of quantum states coming from such coupling has been investigated in Ref. [1]. Furthermore, due to the recent technological developments in optomechanics, this area is now becoming experimentally accessible [2] and quite interesting. Usually in such a systems, a mirror moves in response to radiation pressure exerted by the light. This leads to an intensity-dependent phase shift for the light field equivalent to an optical Kerr effect [3]. Hence, among the others, this system shows bistable behaviour [4], and quantum noise reduction effects [5,6]; moreover, it can be used to realize quantum-nondemolition (QND) measurement on the light field [7]. Some of these aspects have been recently studied also in the spatial domain [8].

On the other hand, the use of feedback to control the noise in optical system has been long used. Classical theory is often adequate to describe such feedback. However, the advent of nonclassical light (in particular squeezed light), required a more accurate treatment. A number of useful approaches exist, using linearized quantum Langevin equations [9,10] and, more recently, exact quantum trajectories as well [11]. In particular, it has been shown that it is possible to use QND-mediated feedback to get squeezing, both extracavity [12] and intracavity [13].

Along this line, here we investigate the possibility of controlling the light statistics via optomechanical coupling and a consequent feedback action.

The paper is organized as follows: in Section II we present the measurement model, in Section III we study the light field dynamics, and the spectra are shown in Section IV. Then, in Section V we introduce the feedback action and show its influence on the light statistics. Section VI concludes with a numerical result.

II. THE MEASUREMENT MODEL

The system we wish to study consists of a Fabry-Perot cavity with a partially transmitting mirror on one side and a perfectly reflecting, and oscillating, mirror on the other side. We imagine the latter coated on the surface of a piezoelectric crystal and then we shall adopt the model of Ref. [13]. In such a case the variation of the crystal length can be measured by an electric circuit. Hence, in reality, the system is composed of three different coupled subsystems, the light, the crystal and the electric circuit. The light field is coupled to the crystal length by the radiation pressure force, while the crystal and the electric circuit are coupled by piezoelectric effect.

Concerning the light field, the system is equivalent to the usual Fabry-Perot cavity except that the cavity detuning may vary because of the crystal elasticity. The dynamics of the intracavity field $a$ in a rotating frame is described by

$$\frac{da(t)}{dt} = -\left[\gamma - i\tau^{-1}\Psi(t)\right]a(t) + \sqrt{2\gamma}a_{in}(t), \quad (1)$$

where $\tau$ is the cavity round trip time and $\gamma$ is the amplitude damping rate of the cavity (equal to the transmissivity of the fixed mirror divided by $\tau$). Furthermore, $a_{in}$ is the incoming field, and it is related to the intracavity and outgoing ones by the input-output relation

$$a_{out}(t) = \sqrt{2\gamma}a(t) - a_{in}(t). \quad (2)$$
The cavity detuning $\Psi/\tau$ depends linearly on the variation $x(t)$ of the crystal length

$$\Psi(t) = \tau \Delta + 2k_0 x(t),$$

and couples the mechanical motion of the crystal to the field. Here, $k_0 = \omega_0/c$ is the incoming field wave number, while $\Delta$ is the cavity detuning in the absence of the mirror’s motion.

The mechanical response of the crystal is described by the variation $x(t)$ of the crystal length. For small displacements, the linear response theory \cite{14} can be invoked

$$x(\omega) = \chi_0(\omega) \left[ F_R(\omega) + \zeta Q(\omega) + F_T(\omega) \right],$$

where $\chi_0(\omega)$ is the mechanical susceptibility

$$\chi_0(\omega) = \frac{1/m}{\omega_m^2 - \omega^2 - i\omega\gamma_m},$$

of the (movable mirror) crystal which has mass $m$, oscillates at frequency $\omega_m$, and it is damped at rate $\gamma_m$.

The first force acting on the mirror, $F_R$, is the radiation pressure force given by

$$F_R = 2\hbar k_0 a^\dagger a/\tau.$$

This has the simple interpretation of the momentum change of a photon under reflection, times the number of photons, divided by the round-trip time.

The electric circuit induces the presence of an electric charge $Q$ on one side of the crystal and $-Q$ on the other side (the current $I$ being the time derivative of $Q$, i.e. $I(\omega) = -i\omega Q(\omega)$). These charges generate a variation of the crystal length proportional to $Q$. This effect is equivalent to a force applied on both sides of the crystal, with opposite sign and absolute value $\zeta Q$, where $\zeta$ is a constant depending on the crystal characteristics \cite{15}.

Finally, $F_T$ corresponds to the Langevin force describing the coupling of the mechanical motion with a thermal bath. Its spectrum \cite{16} is given by

$$S_{F_T} = 2m\gamma_m k_B T,$$

where $T$ is the temperature of the thermal bath and $k_B$ the Boltzmann constant. This relation is valid when $T$ is such that $k_B T \gg \hbar \omega_m$. Otherwise, one should bring some corrections to the dynamics of the mechanical oscillator \cite{17}.

Now, the piezoelectric crystal is equivalent to a capacitance $C$ and a voltage generator in series. A length variation induces a polarization inside the crystal which generates a potential difference between the two sides of the crystal. This voltage is proportional to the length variation ($V = -\zeta x$) and thus, a measurement of this voltage allows one to monitor the crystal motion, and to measure the amplitude quadrature of the intracavity field (or equivalently the radiation pressure force).

The measured signal is the current $I^{\text{out}}$ going out of the system by a coaxial line; a counterpropagating current $I^{\text{in}}$ enters the system by the same line. This latter corresponds to the Nyquist noise of the characteristic resistance $R$ of the line. The input-output relation for the current is \cite{18}

$$I = I^{\text{in}} + I^{\text{out}},$$

and the noise spectrum of the current $I^{\text{in}}$ entering the system is given by

$$S_{I^{\text{in}}} = \frac{k_B T}{2R}.$$

The voltage at the entrance of the circuit is related to the currents by two equations, one for the line and one for the circuit

$$V(\omega) = R \left[ I^{\text{in}}(\omega) - I^{\text{out}}(\omega) \right],$$
$$V(\omega) = Z_0(\omega) I(\omega) - \zeta x(\omega),$$

where $Z_0$ is the (purely imaginary) impedance of the circuit including the capacitance $C$ of the crystal, and $-\zeta x$ is the voltage generated by the piezoelectric effect.

From Eqs.\cite{8}, \cite{10}, \cite{11}, and with the aid of Eq.\cite{8} it is possible to get the output, measured current as
\[ I_{\text{out}}(\omega) = \frac{R - Z(\omega)}{R + Z(\omega)} I_{\text{in}}(\omega) + \frac{\zeta \chi_0(\omega)}{R + Z(\omega)} [F_T(\omega) + F_R(\omega)], \]  

where \( Z(\omega) \) is an effective impedance

\[ Z(\omega) = Z_0(\omega) - i\frac{\zeta^2}{\omega} \chi_0(\omega). \]  

We see that the measured current provides information about the radiation pressure force.

### III. THE LIGHT FIELD DYNAMICS

Following Ref. [13], to study the light field dynamics we exploit the linearisation procedure. The equation for the mean field, which follows from Eq. (1), is

\[ 0 = -\left[ \gamma - i\psi/\tau \right] \alpha + \sqrt{2\gamma} \alpha_{\text{in}}, \]  

where \( \psi \) represents the steady state detuning. The solution reads

\[ \alpha = \frac{\sqrt{2\gamma}}{\gamma - i\psi/\tau} \alpha_{\text{in}}. \]  

For the sake of simplicity, we shall assume, from now on, \( \alpha_{\text{in}} \) to be real. After linearisation, we get the equation for the quantum fluctuations

\[ \frac{d}{dt} \delta \alpha(t) = -\left[ \gamma - i\tau^{-1}\psi \right] \delta \alpha(t) + i\alpha \delta \Psi(t)/\tau + \sqrt{2\gamma} \delta \alpha_{\text{in}}(t). \]  

Now, by defining the generic quadrature

\[ X_\theta = (ae^{-i\theta} + a^\dagger e^{i\theta}), \]  

the radiation pressure force (13) becomes

\[ F_R = 2\hbar k_0 \tau^{-1} \left[ |\alpha|^2 + \alpha \delta a^\dagger + \alpha^* \delta a \right] = 2\hbar k_0 \tau^{-1} |\alpha| (|\alpha| + \delta X_{\text{arg} \alpha}), \]  

so, it is proportional to the fluctuations of a quadrature determined by the stationary value of the intracavity field.

The equation of motion (16), can be rewritten as

\[ \frac{d}{dt} \delta X_\theta(t) = -\gamma \delta X_\theta(t) - \tau^{-1} \psi \delta X_{\theta + \pi/2}(t) + 2|\alpha|\tau^{-1} \sin (\theta - \text{arg} \alpha) \delta \Psi(t) + \sqrt{2\gamma} \delta X_{\text{in}}^\theta(t), \]  

where the spectrum of the input fluctuations is \( S_{X_{\text{in}}^\theta} = 1 \) for coherent light. We immediately see that the measured quadrature \( \theta = \text{arg} \alpha \) is not affected by the measurement process (i.e. being a QND observable) provided to have \( \psi = 0 \). So, from now on we assume such a condition, which also implies \( \alpha \) to be real (i.e. \( \text{arg} \alpha = 0 \)). Thus, in the frequency domain, the solution of Eq. (19) reads

\[ \delta X_\theta(\omega) = \frac{2\alpha \sin \theta}{(\gamma - i\omega)\tau} \delta \Psi(\omega) + \frac{\sqrt{2\gamma}}{(\gamma - i\omega)} \delta X_{\text{in}}^\theta(\omega). \]  

Any real measurement device must give a read-out and in this case it is the current \( I_{\text{out}} \). Hence the fluctuations of this current is directly related to the fluctuations of the quadrature \( X_\theta \). Specifically, by using Eqs. (12), and (18), we have

\[ \delta I_{\text{out}}(\omega) = \alpha_{\text{in}} G(\omega) \delta X_{\text{in}}^\theta(\omega) + I_T(\omega), \]  

where the gain \( G \), and the thermal current \( I_T \), are given by

\[ G(\omega) = 2\hbar k_0 \frac{1}{(\gamma - i\omega)\tau} \frac{\zeta \chi_0(\omega)}{R + Z(\omega)}, \]  

\[ I_T(\omega) = \frac{\zeta \chi_0(\omega)}{R + Z(\omega)}. \]
by means of Eqs.(9), (7), and (13), and the result

\[ I_T(\omega) = \frac{R - Z(\omega)}{R + Z(\omega)} I^{\text{in}}(\omega) + \frac{\zeta \chi_0(\omega)}{R + Z(\omega)} F_T(\omega). \]  

(23)

In the case of equal mechanical and electric temperatures, the spectrum of the thermal current can be easily calculated by means of Eqs.(9), (7), and (13), and the result

\[ S_{I_T} = \frac{k_B T}{2R}, \]  

(24)

as required for thermal equilibrium.

IV. THE LIGHT SPECTRUM

In order to derive the light spectra we first calculate the spectrum \( S_\Psi \) and the correlations \( C_\Psi X^{\mu
u}, C_\Psi I_T \). To this end, we remind that the current \( I \) is the time derivative of the charge \( Q \) (i.e. \( I(\omega) = -i \omega Q(\omega) \)) appearing in Eq.(9), and then we eliminate the electric variable in Eqs.(4), and (11), obtaining

\[ x(\omega) = \chi(\omega) \left[ F_R(\omega) + F_T(\omega) + i \frac{\zeta}{\omega} \frac{2R}{R + Z_0(\omega)} I^{\text{in}}(\omega) \right] \]  

(25)

where

\[ \frac{1}{\chi(\omega)} = \frac{1}{\chi_0(\omega)} - i \frac{\zeta^2}{\omega R + Z_0(\omega)}. \]  

(26)

This means that the mechanical response to the radiation pressure is modified by the coupling. As a consequence it will be

\[ \delta \Psi(\omega) = 2k_0 \chi(\omega) \left[ 2\hbar k_0 \tau^{-1} |\alpha| \delta X_0(\omega) + F_T(\omega) + i \frac{\zeta}{\omega} \frac{2R}{R + Z_0(\omega)} I^{\text{in}}(\omega) \right]. \]  

(27)

Now by considering Eqs.(27), (23), (20), (11), and (10) we can calculate the desired quantities

\[ S_\Psi(\omega) = 4k_0^2 |\chi(\omega)|^2 \left[ 4\hbar^2 k_0^2 |\alpha|^2 \frac{2\gamma}{(\gamma^2 + \omega^2) \tau^2} + 2m \gamma \omega k_B T + \frac{\zeta^2}{\omega^2} \left( \frac{2R}{R + Z_0(\omega)} \right)^2 k_B T \right], \]  

(28)

\[ C_\Psi X^{\mu
u} = 4\hbar k_0^2 |\alpha| \chi(\omega) \frac{\sqrt{2\gamma}}{(\gamma - i\omega) \tau} e^{i\theta}, \]  

(29)

and

\[ C_\Psi I_T = 2k_0 \chi(\omega) \left[ \frac{\zeta \chi_0(\omega)}{R + Z(\omega)} 2m \gamma \omega + i \frac{\zeta}{\omega} \frac{1}{R + Z_0(\omega)} \frac{R - Z^*(\omega)}{R + Z^*(\omega)} k_B T \right]. \]  

(30)

Now, from Eq. (29) the intracavity spectrum can be written as

\[ S_{X_\Psi} = \frac{4\alpha^2 \sin^2 \theta}{(\gamma^2 + \omega^2) \tau^2} S_\Psi(\omega) + \frac{2\gamma}{\tau^2 \gamma^2 + \omega^2} \]  

\[ + \frac{2\sqrt{2\gamma} \alpha \sin \theta}{(\gamma^2 + \omega^2) \tau} 2 \text{Re} \left\{ C_\Psi X^{\mu
u} \right\}. \]  

(31)

Finally, the output spectrum can be derived by using the input-output relation (3). The result is

\[ S_{X^{\mu
u}_{\Psi}} = \frac{8\gamma \alpha^2 \sin^2 \theta}{(\gamma^2 + \omega^2) \tau^2} S_\Psi(\omega) + 1 \]  

\[ + \frac{2\sqrt{2\gamma} \alpha \sin \theta}{(\gamma^2 + \omega^2) \tau} 2 \text{Re} \left\{ (\gamma + i\omega) C_\Psi X^{\mu
u} \right\}. \]  

(32)

It is immediately apparent that the output spectrum \( S_{X^{\mu
u}_{\Psi}} \) remains equal to one for \( \theta = 0 \) [a fact obvious from Eq. (24) and used in Eq. (28)], while it takes its maximum value for \( \theta = \pi/2 \). This is due to the back action of the mirror noise, which in the regime we consider is dominated by thermal noise. Furthermore, calculating Eq.(32) we neglected the thermal photons generated by the mirror motion. This is reasonable at optical frequencies (\( \omega_0 \)) since the mechanical frequency (\( \omega_m \)) is much smaller (3).

Notice, that in addition to Ref. (13) we explicitly calculated the spectrum for the detuning and for a generic quadrature.
We now assume that the cavity mode is controlled by modulating the input field linearly with the measured current. This can be achieved by using electro-optic modulators [20]. To model this feedback mechanism, we use the quantum Langevin approach rather than the quantum trajectory approach [21]. Moreover, to simplify the problem, we assume that the feedback is Markovian, that is the response function of the feedback loop is approximately flat from zero to a frequency much larger than that of the mirror or of the electric circuit. This is not unreasonable, as electronic and electro-optic devices can respond on time scales much shorter than $10^{-6}$s. Hence, the feedback can be modeled by changing the input beam according to the following rule

$$a_{\text{in}}(t) = a_{\text{in}} + \delta a_{\text{in}}(t) \rightarrow \tilde{a}_{\text{in}}(t) = a_{\text{in}} + \delta a_{\text{in}}(t) - \lambda \delta f^\text{out}(t).$$

In terms of the quadrature fluctuation operator

$$\delta X_\theta^\text{in}(t) \rightarrow \delta \tilde{X}_\theta^\text{in}(t) = \delta X_\theta^\text{in}(t) - \left( \lambda e^{-i\theta} + \lambda^* e^{i\theta} \right) \delta f^\text{out}(t).$$

Here, the value of $\lambda$ is related to the practical way of realize the feedback action, i.e., to the electro-optics modulators capabilities.

With the choice of $\lambda$ real, the quadrature Eq. (34) is modified as follows

$$\delta \tilde{X}_\theta(\omega) = \frac{2\alpha \sin \theta}{(\gamma - i\omega)\tau} \delta \Psi(\omega) + \frac{\sqrt{2}\gamma}{(\gamma - i\omega)} \delta X_\theta^\text{in}(\omega)$$

$$- 2\lambda \frac{\sqrt{2}\gamma}{\gamma - i\omega} \left[ \cos \theta + f(\omega) \sin \theta \right] \left[ \alpha_{\text{in}} G(\omega) \delta X_\theta^\text{in}(\omega) + I_T(\omega) \right].$$

where

$$f(\omega) = 8\hbar k^2 \frac{\alpha^2 \chi(\omega)}{(\gamma - i\omega)\tau^2},$$

is the feedback term coming from the modified detuning fluctuations, i.e. the term proportional to $\lambda$ when the replacement (34) is made in Eq. (27).

The intracavity spectrum then becomes

$$S_{\tilde{X}_\theta} = S_{X_\theta} - 4\lambda \frac{2\gamma}{\gamma^2 + \omega^2} \text{Re} \left\{ \alpha_{\text{in}} G^*(\omega) e^{-i\theta} \left[ \cos \theta + f^*(\omega) \sin \theta \right] \right\}$$

$$- 4\lambda \frac{\sqrt{2}\gamma}{(\gamma + \omega^2)\tau} \text{Re} \left\{ \left[ \sin(2\theta) + 2f^*(\omega) \sin^2 \theta \right] \left[ \alpha_{\text{in}} G^*(\omega) C_\Psi X_{\theta^*}(\omega) + C_\Psi I_T(\omega) \right] \right\}$$

$$+ 4\lambda^2 \frac{2\gamma}{\gamma^2 + \omega^2} \left[ \alpha_{\text{in}}^2 \left| G(\omega) \right|^2 + \frac{k_B T}{2R} \right] \left[ \cos \theta + f(\omega) \sin \theta \right]^2.$$

In view of Eqs. (34), (35), the input-output relation (2) gives

$$\delta \tilde{X}_\theta^\text{out} = \delta X_\theta^\text{out} - 2\lambda \frac{\gamma + i\omega}{\gamma - i\omega} \cos \theta + \frac{2\gamma f(\omega)}{\gamma - i\omega} \sin \theta \left[ \alpha_{\text{in}} G(\omega) \delta X_\theta^\text{in}(\omega) + I_T(\omega) \right].$$

Finally, the output spectrum in the presence of feedback action is

$$S_{\tilde{X}_\theta^\text{out}} = S_{X_\theta^\text{out}} - 4\lambda \text{Re} \left\{ \alpha_{\text{in}} G^*(\omega) e^{-i\theta} \left[ \cos \theta + 2f^*(\omega) \sin \theta \right] \right\}$$

$$- 4\lambda \text{Re} \left\{ \frac{\sqrt{2}\gamma}{\gamma + i\omega} \left[ \sin(2\theta) + 2f^*(\omega) \sin^2 \theta \right] \right\} \left[ \alpha_{\text{in}} G^*(\omega) C_\Psi X_{\theta^*}(\omega) + C_\Psi I_T(\omega) \right]$$

$$+ 4\lambda^2 \left[ \alpha_{\text{in}}^2 \left| G(\omega) \right|^2 + \frac{k_B T}{2R} \right] \left[ \frac{\gamma + i\omega}{\gamma - i\omega} \cos \theta + \frac{2\gamma f(\omega)}{\gamma - i\omega} \sin \theta \right]^2.$$

For the quadrature $X_0$ the above expression reduces to
\[ S_{X_0}^\ast = 1 - 2\alpha_{in}\lambda G(\omega) + 4\lambda^2 \frac{k_B T}{2R}. \]  

(40)

For any given frequency \( \omega \), it is possible to choose some value of feedback strength \( \lambda \) such that this expression will be less than one, providing the real part of \( G(\omega) \) is positive. That is, the feedback enables one to produce a sub-shot-noise output. The optimum value for the feedback parameter results

\[ \lambda_{\text{opt}} = \frac{\alpha_{in}\text{Re}[G(\omega)]}{2\alpha_{in}^2 |G(\omega)|^2 + \frac{k_B T}{2R}}. \]

(41)

For the amount of squeezing to be significant it is necessary for the measurement gain to be mostly positive and also large compared to the thermal noise:

\[ \alpha_{in}|G(\omega)| \gg \sqrt{\frac{k_B T}{2R}}. \]

(42)

The same conditions hold for the intracavity noise as can be seen from Eq.(37).

VI. CONCLUSION

The main result, obtained in the preceding section, is that using an electro-optic feedback mechanism it is possible to reduce the quantum fluctuations of a field quadrature below the shot-noise limit. The amount of noise reduction depends on the value of the feedback parameter \( \lambda \) as well as on the frequency \( \omega \) determining the gain in the measurement process. The best squeezing is obtained in the amplitude quadrature (with respect to the input field) for which a perfect QND measurement is achievable. On the other hand a rotation of the ellipse of fluctuations [22] could be devised at the output. It is also worth noting that in the model we have elaborated, the added thermal noise (Eq.(40)) can be controlled by means of the electric components (e.g. the resistance), contrary to the case of Refs. [5,6], where thermal fluctuations lead to unavoidable detrimental effects.

To better show the potentialities of our model, we consider a realistic experimental situation. First of all, to enhance the measurement efficiency, we imagine we have a resonant electric circuit. With self-induction of impedance \( L \) the electric resonance frequency \( \omega_e \) is given by

\[ LC\omega_e^2 = 1, \]

(43)

and we choose this to be almost equal to \( \omega_m \). The noncoupled electric impedance \( Z_0 \) is

\[ Z_0(\omega) = i \left( \frac{1}{C\omega} - L\omega \right). \]

(44)

Then, it is possible to define the electric damping and the piezoelectric coupling frequency

\[ \gamma_e = R/L, \quad \Omega_e = \zeta \sqrt{C/m}. \]

(45)

Now, we take for granted the values of parameters in Ref. [13]. The mirror parameters are: mass \( m = 10^{-3} \) g (this value should be intended as an effective value coming from the acoustic modes of the mirror [23]), resonance frequency \( \omega_m = 10^6 \) s\(^{-1}\), quality factor \( Q_m = \omega_m/\gamma_m = 10^6 \), and piezoelectric coupling frequency \( \Omega_e \approx 10^3 \) s\(^{-1}\). The cavity parameters are: bandwidth \( \gamma = 10^6 \) s\(^{-1}\), round trip time \( \tau = 10^{-11} \) s, field wavelength 0.5 \( \mu \)m, and incident power \( P^m = \hbar \omega_0 \alpha_m^2 = 100 \) mW. The transmissivity of the fixed mirror should be the smallest possible since the gain factor [23] is inversely proportional to it. Finally the electric quality factor \( Q_e = \omega_e/\gamma_e \approx 10^6 \).

In Fig.1 we display the spectrum of Eq.(40) for different values of temperature. We see that the noise reduction occurs in proximity of the mechanical resonance frequency, where the response of the meter is maximum. It is worth noting that the squeezing bandwidth is approximately proportional to the meter bandwidth \( \gamma_m \), and whenever it is increased the squeezing phenomenon becomes more sensible to the thermal noise since the mechanical quality factor \( Q_m \) decreases.

Finally, we would briefly discuss about the quantum mechanical consistency of our treatment. For the QND variable \( X_0 \), and its conjugate \( X_{\pi/2} \) the commutation relations are preserved from the input to the output. The same is not true in general for \( X_\theta \) and \( X_{\theta+\pi/2} \) with \( \theta \neq 0 \), due to the fact that the mirror introduces a frequency
dependent phase shift, an additional frequency-dependent damping \[I_2\]. Hence, the canonical commutation relation \([X_0^{\text{out}}(t), X_{\pi/2}^{\text{out}}(t')] = 2i\delta(t - t')\) holds, and it leads to the uncertainty relation
\[
S_{X_0^{\text{out}}}(\omega)S_{X_{\pi/2}^{\text{out}}}(\omega) \geq 1, \quad (46)
\]
for all \(\omega\). In reality, since there is a second output from our system, the current \(I^{\text{out}}\), which measures \(X_0^{\text{out}}\), we can demand a stronger inequality,
\[
S_{X_0^{\text{out}}(t)}(\omega)S_{X_{\pi/2}^{\text{out}}}(\omega) \geq 1. \quad (47)
\]
Here the first quantity is the spectrum of fluctuations in the \(\theta = 0\) quadrature conditioned upon the measured current \(I^{\text{out}}\). For Gaussian statistics, which hold in the linearized regime we are considering, this conditioned spectrum can be evaluated as
\[
S_{X_0^{\text{out}}(t)}(\omega) = S_{X_0^{\text{out}}}(\omega) - \left| C_{X_0^{\text{out}}(t)}(\omega) \right|^2 / S_{I^{\text{out}}}(\omega). \quad (48)
\]
We have checked the relation \((47)\) numerically for the regimes of interest, both with and without feedback, and find that it is always satisfied.

In conclusion, we have presented a realistic model, based on optomechanical coupling, for an active control of the quantum noise of a radiation field. The theory has been developed by using a semiclassical approach, which nevertheless guarantees quantum mechanical consistency for realistic situations. Of course in a real situation minor detrimental effects could appear; we mention for example the non-perfect reflectivity of the rear mirror (which decreases the gain factor), or the absorption and diffraction losses in the input coupler (which introduce excess noise). However, we think that the up-to-date technology is mature enough to envisage experimentally an optomechanical tailoring of quantum fluctuations; this could be useful in cavity based experiments, or to produce nonclassical light; among other possible interesting applications we cite the reduction of the radiation pressure noise in gravitational interferometers \[24\].

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FIG. 1. The quantity $S_{\chi_{\text{out}}}$ is plotted vs $\omega$ for different values of temperature. From top to bottom, the curves correspond to $T = 300$ K, $T = 70$ K, and $T = 4$ K. The values of the other parameters are set in the text, and $\lambda$ is chosen according to Eq. (41).
Fig. 1 Optomechanical ............
S. Mancini and H.M. Wiseman