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Numerical investigation of wave-plus-current induced scour beneath two submarine pipelines in tandem

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\textbf{ARTICLE INFO}

\textbf{ABSTRACT}

Two-dimensional (2D) local scour beneath two submarine pipelines in tandem under wave-plus-current conditions is investigated numerically. A fully-coupled hydrodynamic and morphologic model based on unsteady Reynolds-averaged Navier-Stokes (URANS) equations with the $k-\omega$ turbulence closure is applied. The model is validated against existing experimental measurements involving live-bed scour beneath a single pipeline and beneath two pipelines in tandem, respectively. The model is then employed to simulate scour beneath two tandem pipelines under wave-plus-current conditions for a variety of Keulegan-Carpenter ($KC$) numbers and relative current strengths. Horizontal gap ratios (the horizontal gap distance between two pipelines divided by the pipeline diameter) ranging from 1 to 4 are modelled. It is found that for conditions involving waves plus a low-strength current, the scour pattern beneath two pipelines behaves like that in the pure-wave condition. Conversely, when the current has equal strength to the wave-induced flow, the scour pattern beneath two pipelines resembles that in the pure-current condition. It is also observed that in the pure-wave condition the equilibrium scour depth beneath each pipeline is affected by both $KC$ and the horizontal gap ratio, except for $KC = 5.6$. For such a small $KC$, the horizontal gap ratio has insignificant influence on the equilibrium scour depth, since vortex shedding does not occur. When the current strength relative to the waves is low, the scour development beneath the upstream and the downstream pipelines are similar. However, when the current has equal strength to the waves, the scour development beneath the downstream pipeline has a different pattern to that upstream. Namely, smaller horizontal gap ratios result in delayed scour beneath the downstream pipeline.

1. Introduction

In the submarine environment hydrodynamic loads from waves and currents can act on submarine pipeline systems simultaneously. Once pipelines are installed on the seabed, the local flow patterns will be changed and the sediment transport capability can be increased. Significant local scour has been observed during surveys of submarine pipelines in service. The development of scour beneath such pipelines can cause free spanning of the pipeline, which can increase structural fatigue and damage. To predict the local scour under pipelines, research has been conducted mainly in three forms: (1) empirical models based on experimental data, e.g., Mao (1986), Sumer and Fredsøe (1990, 1996), (2) numerical models based on potential flow theory, e.g., Chao and Hennessy (1972), Chiew (1991), Li and Cheng (1999), and (3) numerical models capable of describing turbulent flows, e.g., Brørs (1999), Li and Cheng (2000), Liang et al. (2005), Fuhrman et al. (2014) and Larsen et al. (2016).

Mao (1986) performed a series of experiments involving scour beneath pipelines under a variety of flow conditions. It was found that the equilibrium scour depth divided by the pipeline diameter $S_e/D$ is a weakly varying function of the Shields parameters $\theta$. An empirical formula for the equilibrium scour depth in the live-bed regime based on Mao (1986)’s experimental measurement was established by Sumer and Fredsøe (2002). In the clear-water regime, the variation in scour depth with $\theta$ was large, and therefore no simple formula exists. For scour in waves, Sumer and Fredsøe (1990) investigated the variation of the scour depth with the Keulegan–Carpenter number ($KC$) and found that $S_e/D$ is a function of $\sqrt{KC}$ in the live-bed regime. In the case of combined waves and currents, Sumer and Fredsøe (1996) conducted experiments covering a wide range of wave-plus-current conditions. It was found that the scour depth may increase or decrease in wave-plus-current conditions relative to pure-wave conditions, depending on both $KC$ and the current velocity relative to the wave-induced near-bed orbital velocity.

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In addition to experimental studies, early attempts on numerically modelling the scour beneath pipelines were based on potential flow theory, according to Sumer (2007) and Sumer (2014). The studies of Chao and Hennessy (1972), Chiew (1991) and Li and Cheng (1999) could predict the maximum scour depth and the upstream slope. However, the potential flow theory cannot capture the flow separation and formation of lee-wake vortices, which are responsible for a more gentle downstream slope (Sumer and Fredsøe, 2002).

More recent attempts at the numerical modelling of scour beneath submarine pipelines have been based on the complete Navier-Stokes equations, with turbulence modelling in the form of either Reynolds-averaged Navier-Stokes (RANS) equations and established a fully-coupled hydrodynamic and morphologic model based on RANS equations coupled with the turbulence model for closure. The same turbulence models have been successfully used in previous scour studies of Fuhrman et al. (2014), Baykal et al. (2015), Larsen et al. (2016), and Zhao et al. (2015) performed numerical studies involving the local scour around two pipelines in tandem in steady currents. In their work, the numerical model was validated against experiments. Specifically, horizontal gap ratios (defined as the horizontal gap distance separating the two pipelines) ranging from 0 to 5.9. They found that for horizontal gap ratios between 0.5 and 2.5, the equilibrium scour depth beneath the downstream pipeline is slightly smaller than that for the upstream pipeline. However, for larger gap ratios between 3 and 5.9, the equilibrium scour depth beneath the downstream pipeline is slightly smaller than that upstream. Their results also showed that the time scale of scour beneath the downstream pipeline is generally larger (by up to a factor 4) than that for the upstream pipeline.

The present work focuses on the numerical investigation of local scour beneath two tandem pipelines subject to wave-plus-current conditions, which has not been previously studied in a detailed manner. A fully-coupled hydrodynamic and morphologic model based on RANS equations coupled with the $k$ $\omega$ turbulence closure is applied. The same turbulence models have been successfully used in previous scour studies of Fuhrman et al. (2014), Baykal et al. (2015), Larsen et al.

### Nomenclature

- $a$: Non-dimensional coefficient for bed load particle moving velocity
- $b$: Reference level of suspended sediment concentration
- $c$: Suspended sediment concentration
- $c_d$: Drag coefficient
- $d$: Median grain diameter
- $D$: Pipeline diameter
- $D_s$: Sediment deposition rate
- $E_t$: Erosion rate
- $F_i$: External body force driving the flow
- $h$: Computational domain height
- $h_b$: Bed height
- $k$: Kinetic energy of turbulent fluctuations per unit mass
- $m$: Relative current strength
- $n$: Porosity
- $q_b$: Bed load transport rate
- $R$: Reynolds number
- $S_0$: Initial scour hole depth
- $S_s$: Equilibrium scour depth
- $S_0$: Mean strain rate tensor
- $t$: Time in second
- $T_w$: Wave period
- $u_i$: Mean velocities in $x_1, x_2, x_3$ directions
- $U_b$: Bed load particle moving velocity
- $U_f$: Friction velocity
- $U_{fc}$: Friction velocity of the pure-current flow
- $U_m$: Near-bed orbital velocity amplitude of the oscillating flow
- $w_i$: Settling velocity
- $\chi$: Cartesian coordinates
- $\alpha, \beta, \gamma, \delta, \sigma, \sigma', \sigma_{0}, C_{lim}$: Constant coefficients for the present $k$ $\omega$ model
- $\beta_i$: Ratio factor for sediment particle diffusivity and eddy viscosity
- $\gamma$: Slope angle of the bed
- $\mu_d$: Dynamic friction coefficient
- $\mu_s$: Static friction coefficient
- $\nu$: Fluid kinematic viscosity
- $\nu_T$: Eddy viscosity
- $\omega$: Specific dissipation rate
- $\omega_s$: Sediment settling velocity
- $\rho$: Density of the fluid
- $\rho_i$: Density of the sediment grains
- $\tau_{ij}$: Reynolds stress tensor
- $\theta$: Shields parameter
- $\theta_c$: Critical Shields parameter for a slope bed
- $\theta_{0c}$: Critical Shields parameter for a horizontal bed
- $\theta_{w}$: Far-field Shields parameter for the wave-plus-current flow
- $\theta_m$: Mean Shields parameter for the wave-plus-current flow
- $\theta_{w}$: Maximum Shields parameter for the oscillating flow
The present numerical model solves the incompressible unsteady Reynolds-averaged Navier-Stokes (URANS) equations with the \( k - \omega \) turbulence model (Wilcox, 2006, 2008) as the closure. The equations governing the flow in the Cartesian coordinate system include a continuity equation and incompressible URANS equations:

\[
\frac{\partial \rho}{\partial t} + \frac{\partial (\rho u_j)}{\partial x_j} = 0
\]  

\[
\frac{\partial \rho u_j}{\partial t} + \frac{\partial (\rho u_i u_j)}{\partial x_i} = -\frac{\partial p}{\partial x_j} + \frac{\partial}{\partial x_i} \left[ \tau_{ij} - \rho \beta \frac{\partial \omega}{\partial x_j} \right] + F_i
\]

where \( u_i \) are the mean velocities, \( x_i \) are the Cartesian coordinates, \( \rho = 1000 \text{ kg/m}^3 \) is the fluid density, \( p \) is the pressure, \( \nu = 10^{-6} \text{ m}^2/\text{s} \) is the fluid kinematic viscosity, \( F_i \) is the external body force used to drive the flow, \( S_{ij} \) is the mean-strain-rate tensor defined as

\[
S_{ij} = \frac{1}{2} \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)
\]

\[
\tau_{ij} = -\rho \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) + 2 \nu \delta_{ij}
\]

\[
\delta_{ij} \text{ is the Kronecker delta, } k \text{ is the turbulent kinetic energy density expressed as}
\]

\[
k = \frac{1}{2} \rho u_i u_i
\]

\[\nu_T = \frac{k}{\omega} \]

\[\omega = \max \left\{ \omega, C_{in} \sqrt{\frac{2\kappa S}{\rho}} \right\}, \ C_{in} = \frac{7}{8}
\]

The two-equation \( k - \omega \) turbulence model is used in the present study as a closure for the URANS equations. The model includes the transport equation of the turbulent kinetic energy \( k \) and the specific dissipation rate \( \omega \) (Wilcox, 2006):

\[
\frac{\partial k}{\partial t} + \frac{\partial (k u_i)}{\partial x_i} = \frac{\partial}{\partial x_i} \left[ \nu + \frac{k}{\alpha} \frac{\partial k}{\partial x_i} \right]
\]

\[
\frac{\partial \omega}{\partial t} + \frac{\partial (\omega u_i)}{\partial x_i} = C_{in} \frac{\partial (\kappa S)}{\partial x_i} - \nu_T \frac{k}{\omega} + \frac{\partial}{\partial x_i} \left[ \left( \nu + \frac{k}{\alpha} \right) \frac{\partial \omega}{\partial x_i} \right]
\]

\[\alpha = H \left( \frac{\partial k}{\partial x_i} \right)^2 \frac{\sigma}{\partial x_i}
\]

where \( H (\cdot) \) denotes the Heaviside step function, which takes value 1 if the argument is positive and takes 0 otherwise. The standard closure coefficients are: \( \alpha = 0.52, \beta = 0.0708 \) (constant for two-dimensional problems), \( \beta^* = 0.09, \sigma = 0.5, \sigma^* = 0.6, \sigma_{in} = 0.125 \).

In Eqn. (2), the body force \( F_i \) is implemented to drive the flow. In the present work, preliminary one-dimensional vertical (1DV) pure flow simulations driven by the body force without morphology are carried out, in order to achieve a fully developed wave-plus-current boundary inlet. The one-dimensional body force of combined waves and current is given by (Larsen et al., 2016):

\[
F_i = \frac{2 \pi \cos \left( \frac{2 \pi}{T_w} \right) + U_m}{h}
\]

where \( U_m \) is the near-bed orbital velocity amplitude of the oscillating flow, \( T_w \) is the wave period, \( U_m \) is the desired friction velocity of the pure-current, and \( h \) is the domain height. After the 1DV flow simulation reaches the equilibrium state, the velocity field, \( k \) and \( \omega \) at the inlet boundary are applied as the boundary inlet for the scour simulations. The body force is then set to zero in the scour simulations as the flow will be driven by the Dirichlet condition at the inlet.

2.2. Sediment transport and morphological models

2.2.1. Bed load transport

The present sediment transport model consists of a bed load transport model and a suspended load transport model. A full description and numerical implementation of the model can be found in Jacobsen (2011) and Jacobsen and Fredsoe (2014). The bed load transport model is based on the work of Rouland et al. (2005) which is a generalized three-dimensional extension of the transport formulation by Engelund and Fredsoe (1976). The bed load sediment transport rate \( q_b \) can be written as (Fredsoe and Deigaard, 1992):

\[
q_b = \frac{\pi d^2 \rho_b \mu_f \gamma}{6} U_b
\]

where \( d \) is the median grain diameter, \( U_b \) is the bed load particle moving velocity, for which the detailed derivation can be found in Fredsoe and Deigaard (1992) and Rouland et al. (2005). In the present two-dimensional context, the expression for \( U_b \) is given by

\[
U_b = a U_f \left( 1 - 0.7 \frac{\partial \theta}{\partial x} \left( \cos \gamma \right) - \frac{1}{\mu_d} \sin \gamma \right)
\]

where \( a \approx 10 \) is a non-dimensional coefficient and \( U_f \) is the friction velocity, such that \( a U_f \) denotes the flow velocity at a distance of the order of magnitude \( d \) from the bottom (Fredsoe and Deigaard, 1992). \( \gamma \) is the slope angle; \( \mu_f \) is the percentage of particles in motion in the surface layer of the bed, expressed by Engelund and Fredsoe (1976):

\[
\mu_f = \left[ 1 + \left( \frac{2 \pi d \rho_b}{\theta - \theta_0} \right) \right]^{-1/4}
\]

where \( \theta_0 \) is the dynamic friction coefficient. In the present work, the value of \( \mu_f \) is specified as 0.7, following Fuhrman et al. (2014) and Larsen et al. (2016). The Shields parameter \( \theta \) is defined by

\[
\theta = \frac{U_f^2}{(s-1)gd}
\]

where \( s = \rho_s/\rho \) is the specific gravity of the sediment grains, with \( \rho_s \)
being the density of the sediment grains. The critical Shields parameter \( \theta_c \) for the incipient motion of the particles is taken as (appropriate for two-dimensional problems):

\[
\theta_c = \theta_{c,0} \left( \cos(\gamma) - \frac{1}{\mu_s} \sin(\gamma) \right) \tag{16}
\]

where \( \theta_{c,0} \) is the critical Shields parameter for a horizontal bed and \( \mu_s \) is the static friction coefficient. In the present study, \( \theta_{c,0} = 0.045 \) and \( \mu_s = 0.65 \) are utilized, as in Larsen et al. (2016).

### 2.2.2. Suspended load transport

The suspended load is computed by solving a turbulent-diffusion equation based on the continuity of the concentration (Fredsøe and Deigaard, 1992; Jacobsen, 2011).

\[
\frac{\partial c}{\partial t} + (u - w_s \delta_3) \frac{\partial c}{\partial x_j} = \frac{\partial}{\partial x_j} \left[ (\nu + \beta_s \omega) \frac{\partial c}{\partial x_j} \right] \tag{17}
\]

where \( c \) is the suspended sediment concentration, \( w_s \) is the settling velocity, \( \beta_s \) is the factor that is dependent on the grain size and level of turbulence which describes the ratio between sediment particle diffusivity and the eddy viscosity (Rijn, 1984). \( \beta_s = 1 \) is used in the present study, the same as that in Fuhrman et al. (2014).

A reference concentration \( c_b \) is utilized as the reference level \( b \). In the present work, \( b = 3.5d \) is used following Fuhrman et al. (2014). For \( c_b \), the formulation proposed by Engelund and Fredsøe (1976) is utilized:

\[
c_b = \left( 1 + \alpha c \right)^{- \lambda} \tag{18}
\]

where \( \alpha c = 0.65 \) is the maximum value for volumetric concentration, and \( \lambda \) is the linear concentration expressed by

\[
\lambda = \left( \frac{0.013a^2}{k^2} \right) \left( \theta - \theta_e - \frac{\pi}{6} \rho D u \right) \tag{19}
\]

The settling velocity \( w_s \) is calculated according to Fredsøe and Deigaard (1992):

\[
w_s = \sqrt{\frac{4(s-1)gd}{3\rho}} \tag{20}
\]

where the drag coefficient is \( c_D = 1.4 + 36/R \), and the settling Reynolds number is defined by \( R = \frac{wd}{v} \).

### 2.2.3. Morphology

The morphological model is based on the sediment continuity (Exner) equation:

\[
\frac{\partial h_i}{\partial t} = \frac{1}{1-n} \left[ - \frac{\partial h_i}{\partial x_j} + D_i + E_i \right], \quad i = 1, 2 \tag{21}
\]

where \( h_0 \) is the bed height, \( n \) is the porosity which take 0.4 in the present study, \( D_i \) is the deposition and \( E_i \) is the erosion:

\[
D_i = (w_i - v) c_i \tag{22}
\]

\[
E_i = \left( \nu + \beta_s \omega \right) \frac{\partial c_i}{\partial x_j}, \quad j = b \tag{23}
\]

In the present simulations, the morphological time step is the same as the hydrodynamic time step i.e. no morphological acceleration of any kind is utilized. To prevent the excess steepness of the bed, the sand slide model of Niemann et al. (2010) in two-dimensional is incorporated in the present study with the angle of repose of 32°. The sand slide model uses a geometrical approach (Marieu et al., 2008; Niemann et al., 2010) to prevent the un-physical steepening of the scour shape. The implementation of the sand slide model is described in Jacobsen (2011).

### 2.3. Boundary conditions

The hydrodynamic boundary conditions are specified as follows.

- At the seabed and pipeline surfaces, no-slip boundary conditions are used, i.e., the velocities at the walls are zero. The seabed is modelled as a hydraulically rough wall where the friction velocity \( U_f \) is determined by the tangential velocity at the nearest cell center based on an assumed logarithmic velocity distribution, as described in Fuhrman et al. (2014). The pipeline surface is modelled as a hydraulically smooth wall where the friction velocity \( U_f \) is determined based on the profile proposed by Cebeci and Chang (1978). The generalized wall functions for \( k \) and \( \omega \) are presented in Fuhrman et al. (2014).
- At the top boundary, a frictionless lid is modelled at which the vertical velocity is zero and the horizontal velocities and other hydrodynamic quantities have zero normal gradients.
- At the inlet boundary, a Dirichlet boundary is specified with time-varying \( u \) and \( \omega \), taken from the preliminary 1D simulations. The outlet boundary is specified by a Neumann condition with zero normal velocity gradient and zero pressure.

For the sediment transport model, the boundary conditions for the suspended sediment concentration \( c \) is specified as follows.

- At the top and pipeline boundaries, a zero-flux condition for \( c \) is specified.
- At the bottom seabed boundary, a reference concentration is specified, as presented in Eqn. (18). The reference concentration is not imposed at the bottom wall but is at a reference distance of 3.5d from the seabed.
- At the inlet and outlet boundaries, \( c \) is specified with a zero normal gradient.

### 3. Model validation

The present numerical model has been validated in Fuhrman et al. (2014) and Larsen et al. (2016). Fuhrman et al. (2014) validated the present model for scour around a pipeline in waves against the measurement of Sumer and Fredsøe (1990). Larsen et al. (2016) validated the present model for scour around a pipeline in the current against Mao (1986) and in the wave-plus-current condition against the experimental findings of Sumer and Fredsøe (1996). The present work uses the same model but with new mesh for the single pipeline case. Therefore, additional validations are conducted in the present study.

The computational meshes in the present study for a single pipeline and two pipelines in tandem are shown in Fig. 1 (sub-plots (a) and (b), respectively). A small initial scour hole \( S_0/D = 0.15 \) is needed to ensure that there are cells beneath the pipeline. First, the computational mesh setup for a single pipeline will be validated by reproducing the live-bed scour experiment of Mao (1986). The time series of the non-dimensional scour depth \( S/D \) development and the scour profiles at two time instants will be compared to the experimental data in section 3.1. Then, the computational mesh for a single pipeline is extended for two pipelines in tandem, as shown in Fig. 1a. For this purpose, the present model will be validated against the experiments of Zhao et al. (2015), involving live-bed scour around two tandem pipelines in a current. The bed profiles at the corresponding time instants will be compared in section 3.2. In all the cases, the smallest cells near the pipeline have a height of 0.003D and the smallest cells near the seabed have a height of 0.5d.

#### 3.1. Validation against the experiment of scour beneath a single pipeline

In this section the live-bed scour experiment in Mao (1986) is reproduced using the present model and mesh. The Shields parameter \( \theta \)
is 0.098 for both the experiment and the present simulation. The pipeline diameter and the grain size in \( \text{Mao (1986)} \) is \( D = 0.1 \text{ m} \) and \( d = 0.36 \text{ mm} \). In the present simulation, \( D = 0.03 \text{ m} \) and \( d = 0.19 \text{ mm} \). Following the arguments of \( \text{Larsen et al. (2016)} \), this is justifiable as non-dimensional comparison between the present numerical simulation and the experiment of \( \text{Mao (1986)} \) are performed in terms of \( S/D \) over the non-dimensional time \( t' \) which is expressed as

\[
t' = \sqrt{\frac{g(s - 1)v^3}{D^2}},
\]

where \( t \) is the physical time. It is ensured that the non-dimensional scour developments are comparable between two different scales once the Shields parameter is kept the same. The friction velocity \( U_f \) is calculated using Eqn. (15) and is equal to 0.017 m/s in the present simulation. The specific gravity of the sediment grains is \( s = 2.65 \) for both the experiment (\( \text{Mao, 1986} \)) and the present simulation. An initial hole of \( S_0/D = 0.15 \) is specified in the numerical simulation. Therefore, an approximation time that is used to develop the initial hole is added to compare the numerical time series to the corresponding experimental results of \( \text{Mao (1986)} \). The approximation time is calculated by \( t_0 = \frac{\Delta t}{\Delta t} \), \( \frac{dS}{dt} \) is the initial scour rate calculated by the scour depth growth between the initial two saved time instants divided by the saved time step. For the present validation case, the simulation results are saved every 3 s, corresponding to \( \Delta t' = 0.035 \). The non-dimensional scour depths \( S/D \) over the non-dimensional time \( t' \) from the present numerical simulation and the experiment of \( \text{Mao (1986)} \) are compared in Fig. 2a. It is shown in Fig. 2a that the present numerical results are in good agreement with the experimental measurement by \( \text{Mao (1986)} \). The final equilibrium scour depth reaches around 0.7\( D \) for both the numerical simulation and the experiment. As mentioned before, the expected equilibrium scour depth should be approximately constant (\( \text{Sumer and Fredsøe, 1990} \)) as \( \frac{S}{D} = 0.6 \pm 0.2 \). Fig. 2a compares the profiles between the numerical prediction and the experimental measurement. It shows that the predicted downstream shoulder is slightly smaller than the experiment at the first time instant (\( t' = 0.24 \)) and slightly larger than the experiment at the second time instant (\( t' = 4.86 \)). The predicted profiles are generally consistent with the experimental measurement and the scour depths beneath the pipeline are highly matched. Therefore, the present computational mesh setup and grid resolution for a single pipeline have been validated.

### 3.2. Validation against the experiment of scour beneath two pipeline in tandem

To further validate the present model, the experiments conducted by \( \text{Zhao et al. (2015)} \) will be considered, involving scour around two pipelines in a steady current. In \( \text{Zhao et al. (2015)} \), two laboratory tests were conducted with two identical pipelines having \( D = 0.15 \text{ m} \), having two different horizontal gap ratios \( G/D = 0.5 \) and 3. The sediment that was used in the model test has a median diameter of 0.24 mm and a specific gravity of \( s = 2.65 \). The incoming steady flow velocity is 0.65 m/s at a height of 0.15m above the sand bed surface, which corresponds to \( U_f = 0.029 \text{ m/s} \) and \( \theta = 0.218 \).
solved by the present numerical model are in a reasonable agreement with Zhao et al. (2015)’s experimental measurements. For the $G/D = 0.5$ case, the maximum scour depth is located in between the two pipelines. No ripples are observed between two pipelines after the test time of 5 min. For the $G/D = 3$ case, the numerical result of scour depth beneath the downstream pipeline is slightly smaller than the experimental data by Zhao et al. (2015) at $t = 6.4$ min. At $t = 96.3$ min, the berm in between the two pipelines from the numerical simulation is more obvious than that from the experiment. However, the final scour depths below the centers of two pipelines are generally in good agreement with the experimental data. Therefore, the present numerical model for predicting scour beneath two pipelines in tandem and the present grid resolution for two pipelines have been validated.

4. Model application

A sketch of the present numerical model of scour beneath two pipelines in tandem is shown in Fig. 4. The pipelines are placed on the seabed with the upstream pipeline’s bottom at the origin $(x, y) = (0, 0)$. The horizontal gap ratio, i.e., the horizontal gap distance between the two pipelines over the pipeline diameter $G/D$ takes the values of 1, 2, 3 and 4 in the present study. An initial hole with a depth of $S_0 = 0.15$ is set for both pipelines. In the present simulations, the pipeline diameter is $D = 0.03$ m and the grain size is $d = 0.19$ mm. The specific gravity of the sediment grains is $s = 2.65$.

The wave-plus-current conditions simulated in the present work are given in Table 1, with six different $KC$ ranging from 5.6 to 30, combined

---

**Fig. 3.** Comparison of the bed profiles between the present numerical simulations and the experimental measurement of Zhao et al. (2015). Left column: $G/D = 0.5$; Right column: $G/D = 3$.

**Fig. 4.** A sketch of the numerical layout for scour beneath two pipelines in tandem.
with three different current strengths for each KC. In Table 1, \( U_c \) is calculated while the relative current strength \( m \) is 0, 0.25 and 0.5, with \( m \) defined by

\[
m = \frac{U_c}{U_f + U_w}
\]

where \( U_w \) is the near-bed orbital velocity amplitude of the oscillating flow and \( U_f \) is the current velocity at the center of the pipeline. With this definition \( m = 0 \) corresponds to a pure-wave condition and \( m = 1 \) corresponds to a pure-current condition.

According to Sumer and Fredsøe (1996), when \( m > 0.7 \), (and similarly according to Larsen et al. (2016), when \( m \geq 0.5 \)), the current effect is dominant, and the scour depths are very similar to those in the pure-current conditions. The pure-current (\( m = 1 \)) induced scour beneath two tandem pipelines has been numerically simulated by Zhao et al. (2015) and experimentally investigated by Zhang et al. (2017). Therefore, the present work focuses on the range of \( m = 0 \) to 0.5, i.e., from pure-wave conditions (\( m = 0 \)) to an essentially equal strength of the wave and current (corresponding to \( m = 0.5 \)). Fig. 5 shows the time series of free stream velocity at the pipeline center with \( m = 0, 0.25 \) and 0.5, for cases having \( KC = 19.6 \), as an example.

The far-field Shields parameter \( \theta_w \) for the wave-plus-current flow is calculated as follows (Soulsby, 1995; Fuhrman et al., 2013; Larsen et al., 2016).

\[
\theta_w = \theta_w + \theta_m
\]

where \( \theta_m \) is the maximum Shields parameter of the oscillating flow. The maximum near-bed friction velocity induced by the oscillating flow is calculated by

\[
U_0 = \sqrt{0.5 \lambda} \cdot U_w
\]

Here, following e.g. Larsen et al. (2016), \( f_w \) is calculated by taking the maximum among the laminar, smooth-turbulent, and rough-turbulent wave friction factors: \( f_w^{lamin} \) \( f_w^{smooth} \) \( f_w^{rough} \).

\[
\begin{align*}
\begin{cases}
f_w^{lamin} &= \frac{2}{\sqrt{Re}} \\
f_w^{smooth} &= 0.035Re^{-0.16} \\
f_w^{rough} &= \exp \left[ 5.5 \left( \frac{u_c}{U_w} \right)^{0.16} - 6.7 \right]
\end{cases}
\end{align*}
\]

where \( Re = U_0 \lambda / \nu \) is the Reynolds number, \( \lambda = U_0T_w / (2 \pi) \) is the characteristic amplitude of free stream orbital motion, the \( f_w^{smooth} \) expression is from Fredsøe and Deigaard (1992), and the \( f_w^{rough} \) expression is from Fuhrman et al. (2013). The mean Shields parameter \( \theta_m \) is calculated by

\[
\theta_m = \theta_m \left[ 1 + 1.2 \left( \frac{\theta_m}{\theta_m + \theta_w} \right)^{1.2} \right]
\]

where \( \theta_m \) is the Shields parameter calculated from the pure current friction velocity \( U_c \). Table 1 shows that the far-field Shields parameters \( \theta_m \) of the present wave-plus-current cases are all larger than the critical Shields parameter \( \theta_0 = 0.045 \). Therefore, the present cases in wave-plus-current conditions are all in the live-bed regime. For all the simulated cases, a warm-up period (with morphology turned off) of \( t = 10T_w \) is applied.

5. Results and discussion

The discussion of the results will start from presenting the scour profile evolution and time series of scour depth development for representative cases with \( m = 0 \), \( m = 0.25 \) and \( m = 0.5 \), respectively. Then the equilibrium depths of all the cases will be summarized and discussed.

**Table 1**

Wave-plus-current conditions in the present study. Each \( KC \) and its corresponding \( T_w \) and \( U_w \) are taken from the references. The present study simulates wave-plus-current conditions by adding different levels of \( U_c \) to the pure-wave conditions. \( U_c \) is calculated while the relative current strength \( m \) is 0, 0.25 and 0.5.

| \( KC \) | Reference | \( T_w \) (s) | \( U_w \) (m/s) | \( U_c \) (m/s) | \( \theta_m \) |
|---|---|---|---|---|---|
| 5.6 | Fredsøe et al. (1991) | 1.1 | 0.153 | 0 | 0.051 | 0.019 | 0.125 | 0.161 |
| 11 | Sumer and Fredsøe (1990) | 1.22 | 0.24 | 0 | 0.080 | 0.177 | 0.191 | 0.269 |
| 15 | Sumer and Fredsøe (1990) | 2.5 | 0.177 | 0 | 0.059 | 0.177 | 0.091 | 0.099 | 0.141 |
| 19.6 | Fredsøe et al. (1991) | 3 | 0.196 | 0 | 0.065 | 0.196 | 0.092 | 0.102 | 0.150 |
| 25.3 | Fredsøe et al. (1991) | 3.51 | 0.216 | 0 | 0.072 | 0.216 | 0.094 | 0.105 | 0.161 |
| 30 | Fuhrman et al. (2014) | 3.5 | 0.257 | 0 | 0.086 | 0.257 | 0.120 | 0.136 | 0.212 |

![Fig. 5. Free stream velocity of wave-plus-current in a time series.](image-url)
5.1. Profile evolution and time series

5.1.1. Pure-wave conditions \( m = 0 \)

When \( m = 0 \), i.e. pure-wave conditions, the scour profile in the vicinity of the upstream and the downstream pipelines is generally symmetric. Fig. 6 shows the scour profiles in a pure-wave condition with \( KC = 30 \). It is seen that a small berm emerges between two pipelines at the initial time. For each \( G/D \), the berm in between two pipelines is gradually eroded over time and becomes less visible than that at the beginning. When the horizontal gap ratio is larger, the berm is more visible during the equilibrium stage. It is also noted that the maximum scour depths of the final scour profile are not located right below the center of the pipelines. The maximum scour depths gradually move towards the middle of the two pipelines during the development.

The time-averaged scour depth development with \( m = 0 \), \( KC = 30 \) can be seen in the left column of Fig. 7, which depicts time series of the scour beneath two pipelines in tandem for varying horizontal gap ratios. It is shown that the time-averaged scour depths beneath the upstream and the downstream pipelines are generally symmetric.

It is noted that the number of the berms that are formed in between the tandem pipelines is influenced by both \( G/D \) and \( KC \). As \( KC \) is proportional to the ratio of the amplitude of free stream orbital motion towards the middle of the two pipelines during the development.

When \( m = 0 \), since the lee-wake vortex shedding is largely suppressed in between the two pipelines. However, it appears that when the horizontal gap ratio increases to over 15, only one berm is observed between the tandem pipelines, as shown in Fig. 8 e.g. with \( KC = 25.3 \). It should be mentioned that the asymmetric form of the berms in \( KC = 15 \) is a momentary phenomenon, since the profile still changes cyclically during the equilibrium stage. The number of berms that are formed between the pipelines can be related to the natural length of vortex ripples. Following Broker (1985) and Fuhrman et al. (2014), the nature length of the vortex ripples is calculated by \( \lambda_r = 1.2/(2\pi) \cdot KC \). For \( KC = 5.6 \), \( \lambda_r/D \) is calculated as 1.07, meaning that we can expect three vortex ripples between the pipelines at \( G/D = 4 \). For \( KC = 15 \), \( \lambda_r/D \) is calculated as 2.86, so there is maximum two vortex ripples between the pipelines with \( G/D = 4 \). For \( KC = 25.3 \), \( \lambda_r/D \) is 4.83 so that only one vortex ripple can be formed between the pipelines with \( G/D = 4 \).

5.1.2. Waves with weak current \( m = 0.25 \)

We will now consider waves with a relatively weak current, corresponding specifically to the flows with \( m = 0.25 \). Fig. 9 presents a comparison of the scour profiles between the \( m = 0 \) and \( m = 0.25 \) cases with \( KC = 15, G/D = 2 \); \( KC = 25.3, G/D = 2 \) and \( KC = 25.3, G/D = 4 \). It is shown that with \( m = 0.25 \), the scour profiles resemble those under pure-wave conditions, but with slightly less symmetry. Especially, in Fig. 9c with \( KC = 25.3, m = 0.25, G/D = 4 \), the asymmetry of the scour profile is more apparent than those with \( m = 0.25 \) in Fig. 9a and b. Fig. 9 demonstrates that for these three cases the shoulders at the downstream are more eroded with \( m = 0.25 \) compared to \( m = 0 \). Fig. 9a and b present the scour profiles with the same \( G/D \) but different \( KC \). It is seen that the scour profile patterns (with \( m = 0.25 \) and \( m = 0.25 \), respectively) are similar with different \( KC \). With a larger \( KC \), the scour depth increases for both \( m = 0 \) and 0.25. Fig. 9b and c present the scour profiles with the same \( KC \) but different \( G/Ds \). It is shown that the scour depth also increases when \( G/D \) increases from 2 to 4 for both \( m = 0 \) and 0.25.

The scour time series with \( m = 0.25 \) are also compared with those with \( m = 0 \) in Figs. 7 and 10, respectively. It is generally observed that with \( m = 0.25 \), the scour depths at the equilibrium stage does not differ much from those with \( m = 0 \). The result is consistent with the findings in Larsen et al. (2016), who simulated the wave-plus-current induced scour beneath a single pipeline. They found that a low value of \( m \) leads to scour pattern quite close to pure-wave cases. It is seen that for the \( G/D = 1 \) cases, the scour time series with \( m = 0.25 \) are very close to those with \( m = 0 \), since the lee-wake vortex shedding is largely suppressed in between the two pipelines. However, it appears that when the horizontal gap ratio increases, the two pipelines eventually have different scour depths under the asymmetric effect of wave-plus-current conditions, although the difference is minor, as seen in Figs. 7 and 10 at \( G/D = 2, 3, \) and 4. Here, the downstream pipeline has a slightly larger scour depth than the upstream pipeline after reaching equilibrium.

5.1.3. Waves with strong current \( m = 0.5 \)

We will now consider waves with a strong current, corresponding specifically to the flows with \( m = 0.5 \). As shown before in Fig. 5, when \( m = 0.5 \), the undisturbed free stream velocity is \( \geq 0 \) at all times. This means that the undisturbed free stream flow behaves more like a uni-directional current flow with a fluctuating velocity from 0 to \( 2U_\infty \). Therefore, it is expected that with \( m = 0.5 \) the effect of the current should become more dominant compared to the effect of waves.

Fig. 11 presents the scour profile evolution and the time series with \( m = 0.5, G/D = 1 \) for the case having \( KC = 19.6 \) as an example. It is seen in Fig. 11a that the scour holes beneath the two tandem pipelines are merged into one large scour hole while reaching equilibrium. This profile shape is similar to that in the validation case involving a steady current, as shown in Fig. 3a. The same phenomenon is observed for \( m = 0.5 \).
0.5, G/D = 1 cases having all the KC except for KC = 5.6. Zhou and Yiu (2006) and Sumner (2010) investigated the flow around two pipelines in the pure current. They found that for G/D ≤ 1, the two pipelines behave effectively as a single extended body so that the one large scour hole is formed beneath the two tandem pipelines while reaching equilibrium.

It is noticed in Fig. 11 that the development of the scour profile with m = 0 is essentially different from that with m = 0.25. The scour hole beneath the downstream pipeline is slightly buried by the sediments transported from upstream. The scour depth beneath the downstream pipeline slightly decreases at this stage (e.g. \( t^* = 0.33 \) in Fig. 11a, stage (2) in Fig. 11b). The reduction of the scour hole beneath the downstream pipeline at the second stage is explained in Fig. 12 which shows the velocity field and the suspended sediment concentration at a time instant during this stage. As shown in Fig. 12a, the berm in the gap causes flow separation at its lee-side. The main flow is transported along the stoss-side of the berm towards the upper side of the downstream pipeline. Due to the low flow velocity and low shear
stress in the downstream tunnel, the small amount of sediments transported from the upstream are mainly trapped inside the tunnel while very little can be transported out. It is noted that for the present cases, both bed load transport and suspended sediment transport play important roles during the scour process. Fig. 12b shows the distribution of the suspended sediment concentration at the second stage. High suspended sediment concentration is observed at the lee-side of the berm. Suspended sediments are transported into the downstream tunnel. At the lee-side of the downstream pipeline, the suspended sediment concentration is relatively low, indicating that very few suspended sediments are transported out of the downstream tunnel, causing a decrease of the scour depth beneath the downstream pipeline. As the berm gradually migrates downstream until it comes to the vicinity of the downstream pipeline, the small gap between the downstream pipeline and the seabed triggers accelerated flow velocity and increased bed shear stress beneath the downstream pipeline. Therefore, the sediments beneath the downstream pipeline are transported out of the downstream scour hole. The height of the berm between the two pipelines is gradually decreased as the sediments formed the berm are washed downstream to the tandem pipelines.

At the third stage, the scour depths beneath the upstream and downstream pipelines are both increasing (e.g. \( t^* = 2.77 \) in Fig. 11a, stage (3) in Fig. 11b). Fig. 13 shows the velocity field and the suspended load concentration at this stage. With the disappearance of the berm in the gap, the main flow is passing beneath the downstream pipeline, causing high velocity and shear stress at the downstream slope. The depth and width beneath the downstream pipeline are gradually increasing. At this stage, the scour depth beneath the upstream pipeline reaches equilibrium first, while the scour depth beneath the downstream pipeline is still under development. The sediments are transported to the downstream of both pipelines because of the vortex shedding behind the downstream pipeline. At the final stage, the scour profile reaches equilibrium with minor cyclic fluctuations (e.g. \( t^* = 5.89 \) in Fig. 11a, stage (4) in Fig. 11b). The time series and the corresponding four stages of the scour development with \( KC = 19.6, m = 0.5, G/D = 1 \) are shown in Fig. 11b. The same phenomenon is seen at other \( KC \) except for \( KC = 5.6 \).

The final scour profile for \( KC = 5.6, m = 0.5, G/D = 1 \) is shown in Fig. 14. It is seen that the berm in between the two pipelines is not eroded due to the small stroke of the wave motion. Also, for such a low \( KC \), the \( T_w \) is also small so that the flow direction changes frequently with a small stroke of wave motion. Therefore, the scour depth does not develop much.

As the horizontal gap distance increases, two pipelines become more independent. Separate scour holes are formed beneath the two pipelines. Therefore, the berm in between the two pipelines will not disappear.

Fig. 8. The number of berms formed in between two pipelines varies with \( KC \) at \( G/D = 4 \).

Fig. 9. A comparison of scour profiles during equilibrium stage between \( m = 0 \) and \( m = 0.25 \). Left column: \( m = 0 \); Right column: \( m = 0.25 \).
even at the equilibrium stage. As shown in Fig. 15 and Fig. 16 (for $m = 0.5$ cases with $KC = 19.6$ and $KC = 25.3$, respectively), at the equilibrium stage, the berm is still present and is located close to the downstream pipelines. It is seen in Fig. 15 that as the horizontal gap distance increases from 2 to 4, the berm height becomes higher after reaching equilibrium. It is also seen that the width of the scour hole beneath the upstream pipeline becomes larger as the horizontal gap distance increases.

Fig. 17 and Fig. 18 present the scour time series with $KC = 15.6; m = 0.5$ and $KC = 30.6; m = 0.5$ at $G/D = 1, 2, 3,$ and $4$. It is observed that the time duration for the scour beneath the downstream pipeline to reach equilibrium is larger than that required for the upstream pipeline. It shows that with $G/D = 1$ the downstream pipeline experiences a greater delay of scour development compared to those with larger horizontal gap ratios. The same as the time series of $KC = 19.6; m = 0.5; G/D = 1$ in Fig. 11b, it is also shown in Figs. 17 and 18 that for $m = 0.5; G/D = 1$ at different $KC$, the downstream pipeline experiences an initial increase of the scour depth (stage 1) and then a decrease of the scour depth (stage 2) during the scour development process.
5.2. Equilibrium depths

For all the cases, the equilibrium scour depths beneath the centers of the upstream and downstream pipelines are shown in Figs. 19–21. For \( m = 0 \) (a pure-wave condition), the time-averaged scour depth development is symmetric below two pipelines. Therefore, only one \( S_e \) is shown in Fig. 19. Due to minor fluctuations of the scour depth at the equilibrium stage, \( S_e \) is calculated from \( \frac{S_1 + S_2}{2} \), where \( S_1 \) and \( S_2 \) are the average scour depths beneath the upstream and the downstream pipelines over ten wave periods after reaching equilibrium. For a single pipeline in pure-wave conditions, the equilibrium scour depth is a function of the \( KC \) number \( (\text{Sumer and Fredsøe, 1990}) \), \( S_e/D = f(KC) \), as expressed by the solid line in Fig. 19.

Figs. 20 and 21 present the equilibrium scour depths in combined waves and current with \( m = 0.25 \) and \( m = 0.5 \), where the reference lines in the figures correspond to the empirical expressions for the equilibrium scour depth for a single pipeline in combined waves and current given by Sumer and Fredsøe (1996):

\[
S_e = S_c F
\]

where \( S_c \) is the equilibrium scour depth in the pure current \( (S_c/D = 0.6 \pm 0.2) \). \( F \) is calculated by

\[
F = \begin{cases} 
\frac{5}{3}(KC)^m \exp(2.3b_m), & 0 \leq m \leq 0.7 \\
1, & m \geq 0.7 
\end{cases}
\]

where

Fig. 11. Scour profile development and time series of case \( KC = 19.6, m = 0.5, G/D = 1 \).

Fig. 12. Velocity field (unit: m/s) and suspended sediment concentration for case \( KC = 19.6, m = 0.5, G/D = 1 \). The time instant is \( t^* = 0.26 \), when the downstream pipeline experiences a decrease of the scour depth (corresponding to stage (2) in Fig. 11b).

Fig. 13. Velocity field (unit: m/s) and suspended sediment concentration for case \( KC = 19.6, m = 0.5, G/D = 1 \). The time instant is \( t^* = 1.52 \), when the downstream pipeline experiences an increase of the scour depth (corresponding to stage (3) in Fig. 11b).
5.2.1. Pure-wave conditions \( m = 0 \)

For a single pipeline in pure-wave conditions, the empirical equilibrium scour depth is a function of \( K_C \) in the live-bed regime, i.e., \( S_e = f\left( K_C, G/D \right) \) (Sumer and Fredsøe, 1990), while for two tandem pipelines in pure waves the equilibrium scour depth must also potentially depend on the horizontal gap ratio \( G/D \), i.e. such that:

\[
S_e = f\left( K_C, G/D \right) \tag{34}
\]

It is seen in Fig. 19 that when \( G/D = 1 \) and 2, the trend in which the equilibrium scour depth for two tandem pipelines varies with \( K_C \) is similar to that for single pipeline cases conducted by Larsen et al. (2016) but with a more significant drop in scour depth from \( K_C = 11 \) to \( K_C = 15 \). For \( G/D = 3 \) and 4, \( S_e/D \) increases with \( K_C \), which is in line with the trend of the empirical prediction for a single pipeline by Sumer and Fredsøe (1990).

For a given \( K_C \), the equilibrium scour depth generally increases with \( G/D \). A special case is \( K_C = 11 \), where the equilibrium scour depth with \( K_C = 11, G/D = 1 \) is much higher than that with other \( K_C \) at \( G/D = 1 \) and also higher than that with \( K_C = 11 \) at other horizontal gap ratios. Similar phenomena were observed for a single pipeline with \( K_C = 11 \) in simulations of Fuhrman et al. (2014) and Larsen et al. (2016). Fuhrman et al. (2014) explained the phenomenon as a resonance with the nature ripple length that is triggered within the model when \( K_C \) is around \( 10–11 \). The profile develops a ‘trough-to-trough’ wavelength beneath the pipeline which closely matches with the nature length of vortex ripples. Therefore, the scour depth at around \( K_C = 10–11 \) continually develops into a secondary stage and reached a final equilibrium. In Fig. 19, for \( K_C = 11 \) the two dots in grey from Larsen et al. (2016) are the scour depths beneath a single pipeline at the first temporary equilibrium stage and the secondary equilibrium stage, respectively. In the present simulations, the equilibrium depth of \( K_C = 11 \) at each horizontal gap ratio is dominated by the resonance phenomenon within the model so
that horizontal gap ratio has a relative small effect on $KC = 11$ compared to the other higher $KC$. It is worthwhile to mention that, in the present simulations, the equilibrium scour depths beneath two pipelines $S_1$ and $S_2$ are measured right below the center of the pipelines. The maximum scour depths in the scour hole may locate between two pipeline centers. Fig. 22 presents the scour profile with $KC = 11, G/D = 1, m = 0$. The averaged equilibrium scour depth $S_e/D$ is 0.48, while the averaged maximum scour depth $S_{max}/D$ is 0.625. In the study for a single pipeline in pure-waves by Larsen et al. (2016), the maximum scour depth locates right below the pipeline center, and the equilibrium scour depth is 0.62 at the secondary equilibrium stage. This explains why in Fig. 19, the $S_e/D$ with $KC = 11$ for two pipelines is lower than that for a single pipeline from Larsen et al. (2016) while the equilibrium scour status for this specific case is dominated by the resonance phenomenon. It is noted that the equilibrium scour depths for $KC = 5.6$ also varies insignificantly with $G/D$, which will be explained later. It is emphasized that, while the resonance phenomenon discussed above can occur in numerical models, it has yet to be observed in physical experiments, to the best of the authors’ knowledge.

For other $KC$ (except for $KC = 5.6$ and 11), the equilibrium scour depth generally increases with $G/D$. For $G/D = 1$, the equilibrium scour depth beneath both pipelines is generally smaller than the empirical
prediction and also the simulation results (Larsen et al., 2016) for a single pipeline. The reduction of the scour depth with \( G/D = 1 \) can be explained by the suppression of the vortex shedding behind the upstream pipeline. The small spacing between the pipelines partially inhibits the shedding and further reduces the effect of the lee wake on the scour depth. It can be seen in Fig. 23a that for \( KC = 19.6 \), \( G/D = 1 \), \( m = 0 \), no vortex shedding occurs between two pipelines. As \( G/D \) increases to 2, vortex shedding begins to occur in the gap between two pipelines. However, the suppression of the vortex shedding will not happen for the \( KC = 5.6 \) case at \( G/D = 1 \). It is found that when \( KC = 5.6 \), the vortex shedding does not occur and the vortices remain attached to the pipelines during the half cycle of oscillating flow motions. Fig. 24 presents the computed velocity field \( (U) \) in the x direction with \( KC = 5.6 \) and \( G/D = 1 \) during the scouring process. Snapshots at three time instants are presented: just after a change in flow direction at \( t/T = \frac{1}{4} \) and maximum velocity at \( t/T = \frac{3}{4} \), and during deceleration of the flow prior to changing direction at \( t/T = \frac{5}{4} \). These show that for \( KC = 5.6 \) the vortex at the lee-side of the upstream pipeline does not reach the downstream pipeline before the flow changes its direction. The vortex at the lee-side of the downstream pipeline remains attached to the pipeline during the first half of the wave cycle. Similar phenomenon was presented in Sumer and Fredsøe (2006), i.e., vortex shedding does not occur when \( KC = 4 \) in the oscillating flows. This explains the results shown in Fig. 19, where the equilibrium scour depth computed with \( KC = 5.6 \) varies insignificantly with \( G/D \) ranging from 1 to 4. The equilibrium scour depth with \( KC = 5.6 \) is higher than the empirical predictions for a single pipeline but is consistent with the simulated result for a single pipeline in Larsen et al. (2016).

When the horizontal gap ratio increases to \( G/D = 3 \) and 4, the effect of \( KC \) is dominant. The equilibrium scour depths beneath two tandem pipelines are increased with \( KC \) in a similar way to the empirical prediction of scour beneath a single pipeline. It is seen in Fig. 19 that the equilibrium scour depths for \( G/D = 3 \) and 4 beneath two pipelines are generally higher than that beneath a single pipeline in Larsen et al. (2016). This is because of the mutual interaction of the lee-wake erosion from the upstream and the downstream pipelines in the oscillating flow. As can be seen in Figs. 23c and d that for \( KC = 19.6 \), \( m = 0 \), \( G/D = 3 \) and 4, vortices are shed from the upstream pipeline and interact with the downstream pipeline.

5.2.2. Waves with weak current \( m = 0.25 \)

When the current of a relative strength \( m = 0.25 \) is added to the waves, the downstream pipeline can have a slightly higher equilibrium scour depth than the upstream pipeline, as shown in Fig. 20. The difference of the equilibrium scour depths between the upstream and the downstream pipelines is relatively obvious for \( G/D = 2 \) and 3. These differences can arise because the current-induced lee-wake vortex behind the upstream pipeline may influence the downstream pipeline, and this influence appears to be more apparent when \( G/D = 2 \) and 3. Detailed studies and reviews of the gap effect on the flow around two tandem cylinders in a current can be found in Zhou and Yiu (2006) and Sumner (2010). Zhou and Yiu (2006) have discussed that when the horizontal gap ratio between two cylinders is between 0 and 1, two cylinders in the current behave like a single ‘extended-body’ and no vortex shedding occurs in between. Once the gap between two pipelines exceeds a critical value of between 2 and 2.5 (Zhao et al., 2015), vortex shedding from the upstream cylinder will occur. The vortices shed from the pipeline will sweep the bed and amplify the shear stress and the sediment transport. Therefore, the scour depth at the downstream...
pipeline is enhanced at the intermediate horizontal gap ratios. When $G/D$ increases to 4, the influence from the vortex shedding behind the upstream pipeline on the downstream pipeline becomes less significant. The two pipelines then become more independent, so that at $G/D = 4$, the equilibrium scour depths beneath the upstream and downstream pipelines are very close to one another.

At each $G/D$, the trend of equilibrium scour depths varies with $K_C$ follows reasonably the empirical expression of Sumer and Fredsøe (1996). Furthermore, it is also worth noting that for $G/D = 1$ and 2, $m = 0.25$ in Fig. 20, the trend of equilibrium scour depths varies with $K_C$ is very similar to that for pure waves, i.e., $G/D = 1$ and 2, $m = 0$ in Fig. 19. Namely, a drop in scour depth from $K_C = 11$ to $K_C = 15$.

### 5.2.3. Waves with strong current $m = 0.5$

With $m = 0.5$, it appears in Fig. 21 that when $K_C$ is higher than 5.6, the equilibrium scour depth beneath the upstream pipeline is not affected by increases in $K_C$. The equilibrium scour depths are generally located within the range of $S_e/D = 0.85 \pm 0.1$. Similarly, it was found in the experimental study of Sumer and Fredsøe (1996) that when there is a strong current combined with waves ($m > 0.7$ in their study), the equilibrium scour depth $S_e/D$ is the same as in the current-alone case. As discussed before that when $m = 0.5$, the free stream flow behaves like a unidirectional current flow so that the results tend to be similar to those in pure-current conditions. Mao (1986) investigated the equilibrium scour depth versus Shields parameter in pure-current conditions, and it is found that when $\theta > 0.15$, the equilibrium scour depths are generally larger than those with $\theta < 0.15$ and are in the range of $S_e/D = 0.8 - 0.9$.

As presented in Table 1, the far-field Shields parameters $\theta_{cw}$ with $m = 0.5$ for each $K_C$ exceed 0.15 except for $K_C = 15$. The finding is consistent with the results in Larsen et al. (2016). Their simulation results of a single pipeline showed that for $K_C = 11 - 30$ and $m \geq 0.5$, the equilibrium scour depths were slightly larger than the empirical solutions predicted by Eqn. (30)-(33), being close to the equilibrium scour depth in pure-current conditions, i.e. with $m = 1$.

Fig. 21 shows that the equilibrium scour depth beneath the downstream pipeline is higher than that beneath the upstream pipeline at $G/D$.
At $G/D = 3$ and 4, the present work finds that the upstream and downstream pipelines have nearly equivalent scour depths, while the downstream pipeline does not always have a higher equilibrium scour depth than the upstream pipeline. The finding is similar to the results of the experimental study on the scour beneath two tandem pipelines in pure-currents of Zhang et al. (2017).

**6. Conclusions**

The present study has investigated the local scour beneath two pipelines in tandem in the wave-plus-current conditions. A fully-coupled hydrodynamic and morphologic numerical model based on unsteady Reynolds-averaged Navier-Stokes (URANS) equations with $k-\omega$ turbulence closure has been applied. The model has been validated against existing experimental measurements of live-bed scour beneath a single pipeline (Mao, 1986) and as well as against experimental data involving live-bed scour beneath two pipelines in tandem (Zhao et al., 2015).

The scour profiles, scour time series and the equilibrium scour depths have been studied for two pipelines in tandem, with horizontal gap ratios ranging from 1 to 4, coupled with various $KC$ and relative current strengths $m$. The following conclusions can be drawn from the present study.

- The effect of the Keulegan-Carpenter number, $KC$

The effect of $KC$ on the scour beneath two pipelines is dominant when the current strength is low ($m = 0$ and 0.25) and the horizontal gap ratio is high ($G/D \geq 3$). The present study found that in such conditions, the trend in which the equilibrium scour depths for two tandem pipelines varies with $KC$ is similar to that for a single pipeline: the equilibrium scour depth increases proportionally with $\sqrt{KC}$. When $KC$ is small, e.g. $KC = 5.6$, vortex shedding does not occur because the wave period is small and the flows change direction prior to vortices being shed. Therefore, the horizontal gap ratio has a less significant influence.
on the equilibrium scour depth. At a large horizontal gap ratio, i.e., \( G/D = 4 \) in the present study, \( K_C \) also affects the number of berms that formed in between two pipelines in pure-wave conditions. When \( K_C \leq 15 \), two or more berms are formed in the gap between two pipelines. With \( m = 0.5 \), \( K_C \) has insignificant effect on the scour depth and the results tend to be similar to those in the pure-current conditions.

- The effect of the relative current strength, \( m \)

It is generally seen that with \( m = 0 \) and 0.25, the scour pattern is more similar to that in pure-wave conditions. With \( m = 0.5 \), the scour pattern is very similar to that in the pure-current conditions. With \( m = 0 \), i.e. pure-wave conditions, the time-averaged scour depth development is symmetric below the two tandem pipelines. At a relative high \( K_C \) (\( K_C > 15 \) in the present study), one berm is formed in between the two pipelines and the height of the berm gradually reduces during the scour process. However, it is still visible after reaching equilibrium for each horizontal gap ratio considered. The maximum scour depth is located in the gap between the two pipelines rather than below either of their respective centers. At a low current strength, the scour profiles still resemble those under pure-wave conditions, but with less symmetry. The downstream shoulder tends to be more eroded compared to pure-wave conditions. In waves plus strong-strength currents \( (m = 0.5) \), the flows effectively behave like a unidirectional current flow with a fluctuating “pumping” velocity from 0 to \( 2U_m \). Therefore, the scour pattern resembles that in pure current conditions. The scour depths are generally located in the range of \( S_e/D = 0.85 \pm 0.1 \) for the present cases. The scour beneath the downstream pipeline is delayed due to shielding from the upstream pipeline.

- The effect of the horizontal gap ratio, \( G/D \)

The present study shows that in pure-waves, when \( G/D = 1 \) the vortex shedding behind the upstream pipeline is suppressed, except for \( K_C = 5.6 \), where vortex shedding does not occur. At a low relative current strength \( (m = 0.25) \), the scour depth beneath the downstream
pipeline is slightly higher than that upstream when \( G/D = 2 \) and 3, since that the current-induced lee-wake vortex behind the upstream pipeline will have the most effective influence on the downstream pipeline. At \( G/D = 4 \), the upstream pipeline and the downstream pipeline tend to have very similar equilibrium scour depths. Under strong currents (\( m = 0.5 \)), when the horizontal gap ratio is small, i.e. \( G/D = 1 \) in the present study, the scour hole below the tandem pipelines will eventually merge to one since the two pipelines effectively behave like a single extended body. As the horizontal gap ratio increases, the two pipelines become more independent and essentially separate scour holes are formed. The present study found that a smaller horizontal gap ratio, i.e., \( G/D = 1 \), can cause a greater delay of the scour beneath the downstream pipeline with \( m = 0.5 \). It is also seen that with \( m = 0.5 \) the width of the scour hole beneath the upstream pipeline becomes larger as the horizontal gap ratio increases.

Declaration of competing interest

No conflict of interest.

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