Assessment of Penetration Depth and Microleakage of Different Pit and Fissure Sealants Using Dye Penetration Method: An In Vitro Study

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ABSTRACT

Aim and objective: The aim of this study was to evaluate the depth of penetration as well as the microleakage of three different pit and fissure sealant materials employing the dye penetration method.

Materials and methods: Sixty healthy human mandibular premolar teeth without dental caries that were extracted for orthodontic treatment constituted the study samples. These 60 premolar samples were subjected to an equal division (20 in every group) into three groups. Group I: self-adhering flowable composite, group II: flowable nanocomposites, group III: classical pit and fissure sealants. Every sample tooth underwent thermocycling amid 4°C ± 2°C and 60°C ± 2°C for 1,000 cycles. The samples were placed in 1% methylene blue solution for 24 hours to permit diffusion of the dye into probable gaps in between the restoration and the tooth. The teeth were sectioned and evaluated below a stereomicroscope at 10x magnification with image analysis software.

Results: Flowable nanocomposites (3.69 ± 0.10) exhibited a slightly greater mean depth of penetration as compared to classical pit and fissure sealants (3.58 ± 0.16) and self-adhering flowable composites (3.51 ± 0.13) in that order. This difference between the three sealants was not significant statistical. Among the three sealant study groups, the lowest mean marginal microleakage was exhibited by the flowable nanocomposites (1.06 ± 0.03), followed by self-adhering flowable composites (1.98 ± 0.06), and classical pit and fissure sealants (2.74 ± 0.11). Analysis of variance revealed statistically significant differences among the three sealants that were studied.

Conclusion: This study concludes that flowable nanocomposites depicted enhanced penetration and reduced marginal leakage as compared to the self-adhering flowable composites and classical pit and fissure sealants.

Clinical significance: An efficient approach to preventing dental caries on the occlusal surfaces of teeth is the use of pit and fissure sealants. The efficiency of sealants chiefly depends on the morphological characteristics of the fissures and properties of dental materials used.

Keywords: Fissure morphology, Microleakage, Penetration, Sealants.

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INTRODUCTION

Although dental caries are amidst the frequent microbial diseases affecting mankind, their occurrence in children, as well as adolescents, has reduced in recent years, owing to several preventive steps that were sought in developing countries. Despite the benefit of caries preventing methods to smooth surfaces of teeth particularly the proximal surface, the high rate of dental caries affecting the occlusal surface of teeth still remains problematic. The chief reason for this setback is the complicated morphology of the pits and fissures present on the palatal, occlusal and buccal surface of the molars, which are vulnerable sites for the development of dental caries.¹

Techniques including sealing of the predisposed fissures using zinc phosphate cement, mechanically obliterating fissures, silver nitrate chemical management, and preventive odontology are among the various preventive methods that have been adopted to battle this issue.² Pit and fissure sealants are materials inserted in the pits and fissures on the occlusal surface of teeth prone to dental caries resulting in a layer of protection with a micromechanical bond that eliminates the entry of dental caries causing bacteria from their nutrition resources as described by Simonson.³

The two variants of the commercially available pit and fissure sealants these days are either glass-ionomer or resin-based. Depending on the manner of polymerization or their composition, the sealants which are resin-based are classified into various generations. Depending on the mechanism of curing, these sealants are categorized as chemically cured, light-activated, fluoride-
discharging, or self-curing. Filled and unfilled varieties of resin-based sealants are another classification based on the existence or lack of fillers. Microscopic glass beads, particles of quartz, and composite resin fillers constitute filled types of sealants.\(^1\)

The clinical efficiency of these sealants is dependent on their retention which is in turn related to the pit and fissure morphological characteristics, provision of appropriate isolation, traits of the materials, and the technique of application. The retention of fissure sealants may be enhanced by cleansing the occlusal surface before placing the sealant with prophylactic pumice, air abrasion, and polishing as well by mechanically preparing the fissures which are referred to as the invasive technique.\(^5\) An additional significant factor for a successful sealant is the marginal integrity that can be estimated by assessment of the microleakage. The seepage of bacteria and oral fluids in the space amid the restoration and tooth structure is defined as microleakage. Microleakage can cause progress of dental caries beneath the restoration in the absence of appropriate sealing.\(^6\)

Thus, the current study was performed to evaluate the depth of penetration as well as the microleakage of three different pit and fissure sealant materials employing the dye penetration method.

**Materials and Methods**

**Sample Selection**

The current in vitro study was performed in the department of public health dentistry, Vaidik Dental College and Research Centre, Daman, India. Sixty healthy human mandibular premolar teeth without dental caries that were extracted for orthodontic treatment constituted the study samples and were disinfected by 48 hours storage in 0.5% Chloramine-T solution (Merck, Darmstadt, Germany). Each tooth was assessed clinically employing standard lighting and an explorer to be declared free from dental caries. Every sample was subjected to cleansing to eliminate calculus and soft tissue debris with a hand scaler. About 0.9% NaCl consisting of 0.02% sodium azide was used to store the cleaned teeth at 4°C until they were utilized for the study. The premolars were organized for surface cleaning prophylaxis with pumice and Klint Paste* (Voco). These 60 premolar samples were subjected to an equal division (20 in every group) into three groups. The sealant application to the pits and fissures was performed in concordance with the recommendations of the manufacturer.

**Group I: Self-adhering Flowable Composite**

Dyad flow (Dyad flow; Kerr, Sybron dental specialties, USA) application was directly done to the sample teeth using the manufacturer-provided syringe. Surplus material was taken off with a brush given by the manufacturer. The sealant was then subjected to UV light curing for 20 seconds.

**Group II: Flowable Nanocomposite**

In each sample, the enamel of the occlusal surface was subjected to 37% phosphoric acid etching for 30 seconds. Following etching, the surface was subject to rinsing and drying with air. The Tetric N-Flow (Tetric N-Flow; Ivoclar Vivadent AG) sealant was applied on to the fissures in accordance with the guidelines of the manufacturer. In order to avoid air-inclusion and voids, tip of a periodontal probe (API) was passed through the fissure tenderly. A light-curing unit was then employed on the occlusal surface to achieve polymerization. A bonding agent application to the fissures was done with a microbrush and subjected to polymerization for 20 seconds before applying the sealant.

**Group III: Classical Pit and Fissure Sealant**

In each sample, the enamel of the occlusal surface was subjected to 37% phosphoric acid etching for 30 seconds. Following etching, the surface was subject to rinsing and drying with air. The Helioseal F (Helioseal F; Ivoclar Vivadent AG, Schaan, Liechtenstein) sealant was applied on to the fissures in accordance with the guidelines of the manufacturer. In order to avoid air-inclusion and voids, tip of a periodontal probe (API) was passed through the fissure tenderly. A light-curing unit was then employed on the occlusal surface to achieve polymerization for 20 seconds.

**Thermocycling and Dye Penetration Procedure**

Every sample tooth underwent thermocycling amid 4°C ± 2°C and 60°C ± 2°C for 1,000 cycles. The dwell span in every bath and the time gap at room temperature involving baths was 60 seconds. Following thermocycling, the tooth surfaces, excluding the restorations and 1.5 mm beyond the margins, were subjected to coating with dual layer of nail varnish. The samples that had been coated were placed in 1% methylene blue solution for 24 hours to permit diffusion of the dye into probable gaps in between the restoration and the tooth. After exposure to the dye, distilled water was used to wash and rinse the samples.

**Assessment of Microleakage**

The samples were cleansed with water to get rid of surplus dye and were then divided buccolingually in the course of the sealant by means of a high-speed straight handpiece, diamond disk, and water mist. These sectioned teeth were evaluated below a stereomicroscope at 10x magnification with image analysis software (SigmaScan, SPSS; Jandel Scientific, San Rafael, California, USA). Scores were allocated to every sample in agreement with the sealant penetration depth, and microleakage was expressed in millimeters and measured by two examiners.

Theodoridou-Pahini et al.\(^7\) microleakage scoring criteria were employed to evaluate the amount of dye penetration which is as under.

| Score | Description |
|-------|-------------|
| 4     | Penetration of the dye down the buccal or lingual wall |
| 3     | Penetration of the dye beneath the sealant and down the lingual or buccal wall |
| 2     | Penetration of the dye beneath the sealant |
| 1     | Shallow fissure with partial penetration |
| 0     | Absence of dye penetration |

Fracasso\(^8\) criteria as follows:

| Score | Description |
|-------|-------------|
| 0     | No penetration in shallow, medium, and deep fissures |
| 1     | Shallow fissure with partial penetration |
| 2     | Shallow fissure with total penetration and medium fissure with partial penetration |
| 3     | Medium fissure with total penetration and deep fissure with partial penetration |
| 4     | Deep fissure with total penetration |

**Statistical Analysis**

SPSS 20.0 was utilized for the data management and analysis. One-way analysis of variance (ANOVA) test was employed for penetration depth and microleakage comparison. Tukey’s post hoc examination was employed for various analogies. Statistical significance was ascertained with a p-value less than 0.05.
Results

Table 1 depicts the mean depth of sealant penetration into the pits and fissures. Flowable nanocomposites (3.69 ± 0.10) exhibited a slightly greater mean depth of penetration as compared to classical pit and fissure sealants (3.58 ± 0.16) and self-adhering flowable composites (3.51 ± 0.13) in that order. This difference between the three sealants was not significant statistically.

Table 2 shows the comparative assessment of the mean marginal microleakage among the three sealant study groups. The lowest mean marginal microleakage was exhibited by the flowable nanocomposites (1.06 ± 0.03), followed by self-adhering flowable composites (1.98 ± 0.06) and classical pit and fissure sealants (2.74 ± 0.11). ANOVA revealed statistically significant differences among the three sealants that were studied.

Table 3 denotes various comparisons of marginal microleakage among the three sealant groups that were studied using Turkey HSD. The difference between group II and group III was statistically significant while group I vs group II, as well as group I vs group III, depicted no statistically significant differences.

The inference of the present study indicates that the flowable nanocomposite group showed better penetration and less marginal leakage than self-adhering flowable composite group and classical pit and fissure sealant group.

| Pit and fissure sealant groups | Mean ± SD | F value | p value | Significance |
|-------------------------------|-----------|--------|--------|--------------|
| Group I: Self-adhering flowable composite | 3.51 ± 0.13 | 24.182 | 0.617 | NS |
| Group II: Flowable nanocomposite | 3.69 ± 0.10 | 23.642 | 0.001 | HS |
| Group III: Classical pit and fissure sealant | 3.58 ± 0.16 | 2.74 ± 0.11 | p < 0.05 | |

Discussion

Irrespective of the socioeconomic status and age, dental caries is a highly prevalent pathosis that affects almost every geographical region. Over the last decade, dental caries in the deciduous teeth that were not treated were categorized as the 10th most prevalent disease in the world while dental caries in the permanent teeth that were not treated remained the most prevalent disease. Although a multitude of advances in preventive strategies and dental material techniques are eminent, both the incidence and prevalence of dental caries in several countries have consistently stayed high. Dental decay is considered to be a “noncommunicable” and “behavioral” problem affecting the teeth. Dental caries initiation requires a net hard tissue demineralization to occur. This is a result of pH discrepancies and cariogenic bacteria that flourish in the acidic environment especially in the company of sugars that are fermentable.

One amid the highly successful method of prevention of dental caries is pit and fissure sealant materials. Fissure sealants provide swift protection of occlusal surfaces of teeth by physically blocking the fissures which are prone to decay, particularly in small children. The benefits obtained from these agents depend on their physical properties and are directly related to the retention rate they offer in the oral cavity. Sealants must be capable of staying intact and having a firm adherence to tooth structure in order to avoid microleakage. Numerous factors affect the tooth and sealant interface integrity. These include fissure anatomy, the oral environment, chemical and mechanical properties of the materials used, and the forces of mastication.

The sealant materials that have been developed off late are highly enhanced versions of those used before when considering the depth of penetration and their viscosity. The traditional composites were not regarded as efficient pit and fissure sealants owing to their greater viscosity. In contrast, novel composites like flowable composites and nanocomposites have lesser viscosity thereby offering an acceptable flow. This study thus had an aim to assess the efficiency of the recent new composites when employed as pit and fissure sealants. Stritikus et al. and Burrow et al. criteria were used to select the study samples in the current study. Healthy premolar teeth, not affected by caries were selected as these teeth present appropriate morphological traits of occlusal fissures. Additionally, they are frequently extracted for causes apart from dental caries leaving their occlusal fissure architecture preserved.

In this study, flowable nanocomposites exhibited slightly greater mean depth of penetration as compared to classical pit and fissure sealants and self-adhering flowable composites in that order. This difference amid the three sealants was not significant statistically (p > 0.05) when considering the penetration depth. These results are in agreement with Autio-Gold and Duangthip et al. which can be attributed to polymerization shrinkage of the supplies that are related to characteristics like the quality of adhesion, viscoelasticity, and their curing procedures.

In the current study, the lowest mean marginal microleakage was exhibited by the flowable nanocomposites, followed by self-adhering flowable composites and classical pit and fissure sealants. This study revealed that all study groups showed a certain degree of penetration of the dye which is in harmony with the study of Theodoridou-Pahini et al. and do Rego and de Araujo who acknowledged that microleakage may be anticipated in all materials used for restorative purposes. This can also result from the lower coefficient of thermal expansion of the teeth when compared to the
much higher coefficient of thermal expansion of fissure sealants. In this research, classical sealants showed higher microleakage as compared to flowable and self-adhering composites. This is in agreement with the study by Francescut et al., who did the depth of penetration and microleakage evaluation among flowable composites and conventional sealants.

Flowable composite sealants are basically the resin type of composites with less filler constitution and a higher portion of diluent monomers in their preparation. Owing to this, they present greater flow ability, better adaptation to the tooth surface, ease of insertion, and more elasticity. A combination of the composite resin technology as well as adhesives is the Dyad flow self-adhering flowable composite. This is achieved by the addition of the bonding agent that is the acidic adhesive monomer within the self-adhering flowable composite. The Dyad flow relies on the micromechanical as well as chemical relation amid the tooth surface or any other matter and the material.

This study also has certain limitations. Every pit and fissure sealant may act uniquely as it depends on the environment. Numerous factors like the morphology of the fissures and their preparation, manner of applying the adhesive, etched enamel with acid as well as presence or absence of fissure surface contamination. Hence, it is recommended that atherism including contamination with saliva be executed. Also more in vivo studies utilizing different flowable restoration supplies and other methodologies of preparation must be performed for more clarity on the clinical involvement of every variable. Keeping this in mind, other factors like longer adaptation and the shear bond strength of the sealant materials must be taken into consideration.

**Conclusion**

Despite the limitations of this study, it may be concluded that flowable nanocomposites depicted enhanced penetration and reduced marginal leakage as compared to the self-adhering flowable composites and classical pit and fissure sealants.

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