Abstract: We focus on the problem of developing energy efficient controllers for quadrupedal robots. Animals can actively switch gaits at different speeds to lower their energy consumption. In this paper, we devise a hierarchical learning framework, in which distinctive locomotion gaits and natural gait transitions emerge automatically with a simple reward of energy minimization. We use evolutionary strategies (ES) to train a high-level gait policy that specifies gait patterns of each foot, while the low-level convex MPC controller optimizes the motor commands so that the robot can walk at a desired velocity using that gait pattern. We test our learning framework on a quadruped robot and demonstrate automatic gait transitions, from walking to trotting and to fly-trotting, as the robot increases its speed. We show that the learned hierarchical controller consumes much less energy across a wide range of locomotion speed than baseline controllers.

Keywords: Legged Locomotion, Hierarchical Control, Reinforcement Learning

1 Introduction

Fast and efficient locomotion is crucial for legged robots to accomplish tasks that traverse long distances. In the natural world, quadrupedal animals demonstrate a wide variety of distinctive locomotion patterns known as gaits [1], such as walking, trotting, bounding and galloping. Each gait is characterized by a unique foot contact schedule in a locomotion cycle. To lower their energy consumption, most quadrupedal animals switch to a preferred gait at each different speed range [1, 2]. While many locomotion gaits have been implemented on quadrupedal robots [3, 4], gait timing is often hand-engineered, and the switch between gaits is based on ad-hoc user commands. Can quadruped robots learn energy efficient gaits and natural gait transitions automatically?

In this work, we devise a learning framework in which energy-efficient locomotion controllers emerge automatically. The learned controllers naturally switch between different gaits at different speeds to maximize energy efficiency. Learning speed-adaptive locomotion gait controllers is challenging. Although reinforcement learning (RL) has been used to train policies end-to-end for a wide variety of continuous control tasks [5, 6, 7], these policies are often difficult to deploy safely on real robots without additional sim-to-real effort such as reward shaping [8], domain randomization [9, 10], or meta learning [11, 12]. Alternatively, optimal control based controllers have demonstrated robust performance on a number of quadruped robots [3, 13]. However, since gait patterns involve discrete contact events, it is difficult to optimize them together with other continuous forces. Therefore, most optimal control based controllers assume fixed, pre-selected gait timings.

To address the above challenges, we devise a hierarchical framework that combines the advantages of both RL and optimal control. This hierarchical framework consists of a high-level gait generator and a low-level convex MPC controller, which decouples the locomotion task into gait generation and motor control. Instead of directly outputting motor commands, the gait policy functions as part of the gait generator and specifies key gait parameters, which determines the contact schedule for each leg. Based on this contact schedule, the convex MPC controller then determines which legs are in contact, and computes the optimal motor command for each leg. We formulate the high-level gait policy learning as a Markov Decision Process (MDP), design a simple reward function based on velocity tracking and energy efficiency, and train the gait policy using evolutionary strategies (ES).
We formulate the low-level convex MPC controller using model-predictive control with simplified dynamics [3].

With this hierarchical framework and the simple reward function, the gait policy automatically learns distinctive gait patterns at different locomotion speeds, including slow walking, mid-speed trotting and fast fly-trotting. Moreover, the policy automatically transitions from one gait to another to generate the most efficient gait at all speeds. Thanks to the robustness of our hierarchical framework, the learned gait policy can be deployed successfully on a Unitree A1 robot [14] in various environments (e.g. carpet, grass, short obstacle) without additional data collection and fine-tuning.

The main contributions of this paper include:

- A hierarchical learning framework effectively combines RL with optimal control, which can automatically learn fast and efficient locomotion controllers;
- The learned controllers switch gaits across a wide range of locomotion speeds, similar to those demonstrated in the animal kingdom;
- The learned controller can be deployed directly to the real world, and performs robustly in various environments.

2 Related Work

Quadrupedal animals demonstrate a wide variety of gaits [15]. Hoyt and Taylor [1] showed empirically that horses minimize their energy consumption when using the preferred gait at each speed. Alexander and Jayes [2] generalized this result by providing a unifying theory of gait transitions for quadrupedal animals. A wide variety of these gaits have been implemented in quadrupedal robots, including walking [16], trotting [3], pacing [4], bounding [17] and galloping [18]. In these works, model-based controllers [3, 19] optimize for motor commands at a high frequency. These controllers usually assume a pre-defined contact sequence to keep the optimization problem tractable, which does not allow gait transitions. Alternatively, contact implicit optimization [20, 21, 22] optimizes contact forces and sequences together, but is not feasible for real-time use due to high computation cost. Using manually designed heuristics, Boussema et al. [23] achieved online gait transition by computing the Feasible Impulse Set for each leg, at a speed up to 0.6m/s, or 1 body length/s. Owaki and Ishiguro [24] also demonstrated online gait transition on a 2kg quadruped robot using foot-force heuristics. Compared to these approaches, our learning-based approach requires less manual tuning, achieves more agile motions (up to 2.5m/s, or 5 body length/s) on a larger robot (15kg).

Recently, reinforcement learning became a popular approach to learn locomotion policies for legged robots [9, 25, 26]. Since policies are often learned in simulation, extra effort is usually required to transfer the learned policies to the real robot, including building more accurate simulation [9, 25], dynamic randomization [9, 10], motion imitation [27, 28] and meta learning [11, 12]. Inspired by the periodicity of locomotion behaviors, several methods have been proposed to make the learned policy more predictable and safer for real robot deployment, such as cyclic trajectory generators [29], phase-functioned neural networks [30] and state machines [31]. In contrast to these previous works, our learned policy achieves zero-shot sim-to-real transfer, and the controller is robust in multiple real-world environments.

Compared to directly learning an end-to-end controller, hierarchical learning [32] can improve data efficiency, and achieve complex tasks. The low-level controller can be a learned policy [33, 34, 10], or a hand-tuned controller [35, 36, 37]. Li et al. [36] uses a learned policy to modulate objectives of the low-level MPC controller, with a fixed contact sequence. Recently, Da et al. [35] looked into learning hierarchical controllers for gait control in quadrupeds, where the low-level controller is model-based and high-level policy selects from a fixed set of gait primitives. We use a similar hierarchical setup as Da et al. [35]'s, but extend the high-level policy to search a continuous range of gaits with arbitrary gait changes, and achieve significantly faster walking.

3 A Hierarchical Framework for Gait Optimization

3.1 Overview

To learn fast and efficient locomotion, we build a hierarchical framework with a high-level gait generator and a low-level convex MPC controller (Fig. 1). The high-level gait generator includes a
learnable gait policy and a phase integrator. To generate a gait, the gait policy outputs gait parameters, such as frequency, to the phase integrator. Based on these parameters and the robot’s clock, the phase integrator increments the phase for each leg and determines its contact state. In each locomotion cycle, the phase progresses from 0 to 2π as the foot goes from liftoff to touchdown to the next liftoff. The low-level convex MPC controller consists of separate controllers for swing and stance legs, and controls each leg differently based on its contact state. Additionally, we implement a Kalman Filter-based state estimator for the torso velocity, which cannot be measured directly using onboard sensors and is used by both the gait generator and the convex MPC controller. We run the high-level gait generator at 20Hz to avoid abrupt changes of gait commands, and the low level controllers at 500Hz for fast replanning and stable torque control.

3.2 High-Level Gait Generation

A locomotion gait is determined by a contact schedule, the time and duration that each leg is in contact with the ground. To generate foot contact schedules, the phase integrator maintains a set of phase variables φ1,...,4, one for each leg. The phase φi ∈ [0, 2π) denotes the leg’s progress in its current gait cycle (Fig. 2). Each leg i starts with swing at the beginning of a gait cycle (φi = 0). As φi increases monotonically, it switches to stance after a threshold φi > φswing. After φi reaches 2π, it wraps back to zero, and starts a new gait cycle in the swing phase. The propagation of phase variables, as well as the transition from swing to stance, are controlled by three key parameters, including stepping frequency f, swing ratio pswing and phase offsets θ2, θ3, θ4, which are specified by the gait policy. We choose such parameterization because it is expressive enough to represent a rich set of locomotion gaits. We now describe these parameters in detail:

Stepping Frequency As a notable feature in locomotion, the stepping frequency is usually adjusted as a trade-off between speed and efficiency. While a high stepping frequency allows the robot
to run faster, stepping unnecessarily fast can cause additional energy consumption due to excessive leg swing. In our setup, the gait policy outputs the desired leg frequency $f \in (0 \text{Hz}, 4 \text{Hz}]$, which is used to increment the phase variable in the phase integrator. Specifically, at each control step, the phase is advanced by:

$$\phi[n] \leftarrow \phi[n-1] + 2\pi f \Delta t$$

(1)

where $\Delta t$ is the time step of low-level controller (0.002s).

**Swing Ratio**   Another important characteristic of gaits is the proportion of swing time in each gait cycle. For example, while a walking gait is usually characterized by spending less than 50% of a gait cycle in swing phase, a running gait typically requires a much longer swing time. To model this, we define another variable, $p_{\text{swing}} \in (0, 1)$, which controls the switching point in phase $\phi_{\text{swing}} = 2\pi p_{\text{swing}}$ between swing ($\phi < \phi_{\text{swing}}$) and stance ($\phi \geq \phi_{\text{swing}}$) in each gait cycle. Assuming that a leg moves at constant frequency, a larger $p_{\text{swing}}$ means that it will spend more time in air in a gait cycle, which usually results in a more dynamic gait.

**Phase Offsets**   Apart from careful design of individual gait cycles, careful coordination among legs is another critical component for efficient locomotion. While we use the same $f$ and $p_{\text{swing}}$ across all legs, we allow each individual leg to have a different phase offset. Let $\theta_i \in [0, 2\pi]$ denote the phase offset of leg $i$ compared to first leg (the front-right leg); then the phase of leg $i$ is $\phi_i = 2\pi p_{\text{swing}} + \theta_i$. Note that the order of legs is [front-right, front-left, rear-right, rear-left], or [FR, FL, RR, RL] for short. For example, setting $\theta_4 = 0$ would make the rear-left leg in sync with the front-right leg, which is frequently seen in trotting gaits.

### 3.3 Low-Level Convex MPC Control

The low-level convex MPC controller computes and applies torques for each actuated degree of freedom, given the leg phases from the high-level gait generator. Our low-level convex MPC controller is based on Di Carlo et al. [3]. We briefly describe the controller here for the completeness of the paper. Please refer to the Appendix A for more details.

**Stance Leg Control**   In the stance leg controller, we model the robot dynamics based on the Centroidal Dynamics Model [3], where the full robot is simplified as a rigid-body base with massless legs. Each stance leg can generate ground reaction force at the contact point, subject to torque limit and friction cone constraints. These ground reaction forces are solved as a short-horizon MPC problem whose objective is for the robot base to closely track a given reference trajectory. We generate the reference trajectory based on user-specified velocity commands. The optimized contact forces $f$ are then converted to motor torques using the Jacobian transpose method: $\tau = J^T f$. In our MPC setup, we re-optimize for ground reaction forces every time step (2ms), and only apply the first command in the optimized sequence.

**Swing Leg Control**   The swing leg controller calculates the swing foot trajectories and uses Proportional-Derivative (PD) controllers to track these trajectories. The swing trajectory is computed by fitting a quadratic polynomial over the lift-off, mid-air and landing position of each foot, where the lift-off position is the foot location at the beginning of the swing phase, the landing position is calculated using the Raibert Heuristics [38], and the mid-air position is set to ensure the minimum ground clearance. Please refer to Appendix A.2 for more details. Given the position in the swing trajectory, we convert it to the desired motor position using inverse kinematics, and apply motor torques using PD controllers.

### 4 Learning Gait Policies for Fast and Efficient Locomotion

Since locomotion gait involves discrete contact events, it is difficult to model and optimize them together with other continuous forces. Instead, we formulate a Markov Decision Process and apply Evolutionary Strategies (ES) to discover the most energy efficient gaits at different speeds.

**4.1 Preliminaries**

The reinforcement learning problem is represented as a Markov Decision Process (MDP), which includes the state space $S$, action space $A$, transition probability $p(s_{t+1}|s_t, a_t)$, reward function
\( r : S \times A \mapsto \mathbb{R} \), and initial state distribution \( p_0(s_0) \). We aim to learn a policy \( \pi : S \mapsto A \) that maximizes the expected cumulative reward over an episode of length \( T \), which is defined as:

\[
J(\pi) = E_{s_0 \sim p_0, s_{t+1} \sim p(s_t, \pi(s_t))} \sum_{t=0}^{T} r(s_t, a_t)
\]  

(2)

### 4.2 MDP Formulation

In our MDP formulation, we only learn the gait policy in the high-level gait generator, and consolidate the other components, including phase integrator, the convex MPC controller, and the robot dynamics, into the environment. At each step, the gait policy outputs gait parameters and receives a reward, which is based on energy consumption and speed-tracking performance.

**State and Action Space** Since we aim to optimize the gaits based on the current and desired speed, we only include the desired and actual linear velocity of the base in the state space \( s = [\bar{v}_{\text{base}}, v_{\text{base}}] \). We do not include proprioceptive information, such as joint angles and IMU readings, because the detailed control of balance and locomotion, which consumes these information, is delegated to the low-level controller. The action space is a 5-dimensional vector \( a = [f, p_{\text{swing}}, \theta_2, \theta_3, \theta_4] \), as defined in Section 3.2.

**Reward Design** We design the reward function as a linear combination of survival bonus, speed-tracking penalty, and energy penalty:

\[
r = c - w_v \frac{||\bar{v}_{\text{base}} - v_{\text{base}}||^2}{v_{\text{base}}} - w_c \sum_{i=1}^{12} \max(\tau_i \omega_i + \alpha \tau_i^2, 0) \frac{m g \bar{v}_{\text{base}}}{mg} \tag{3}
\]

The survival bonus \( c \) prevents the learning algorithm from falling into the local minima of early termination. The speed penalty is the L2 norm of the relative error between the desired \((\bar{v}_{\text{base}})\) and actual speed \((v_{\text{base}})\) of the base. The energy penalty estimates the Cost of Transport (CoT), a standard metric for measuring the efficiency of locomotion [24, 39, 40]. The numerator estimates total power consumption in all 12 motors based on the angular velocity \((\omega_i)\) and torque \((\tau_i)\) of each motor, and the motor parameter \((\alpha = 0.3)\). (See Appendix B for details.) The denominator consists of the mass of the robot \((m = 15\text{kg})\), and gravity constant \((g = 9.8\text{m/s}^2)\). In each episode, the desired velocity \(\bar{v}_{\text{base}}\) starts at 0 m/s, increases linearly to 2.5 m/s at 1 m/s/s and stays at 2.5 m/s for the rest of the episode. We use the same weights \(c = 3, w_v = 1, w_c = 0.37\) for all of our experiments.

**Early Termination on Infeasible Gaits** Despite the robustness of low-level whole body controller, the robot can still lose balance if the gait is infeasible, such as standing with one leg for an extended amount of time. To avoid unnecessary exploration in suboptimal gaits, we terminate an episode early if the robot falls (i.e. orientation deviates significantly from the upright pose, or the robot’s height becomes too low).

### 4.3 Policy Representation and Training

We represent our policy as a neural network with one hidden layer of 256 units and tanh nonlinearities. We chose this network architecture because it is sufficiently expressive to learn different gaits, and structurally compact to be efficiently optimized by our learning algorithm. We train our policies using Covariance Matrix Adaptation Evolution Strategy (CMA-ES) [41], a simple, parallelizable evolutionary algorithm that has been successfully applied to locomotion tasks [42, 43, 44]. Compared to other RL algorithms, CMA-ES performs exploration in the policy parameter space and does not require accurate value function estimation at every step [45, 46], which is well-suited for our complex hierarchical system. See Appendix C.1 for details.

### 5 Results and Analysis

We design experiments to validate that our framework can learn fast and efficient locomotion controllers. Particularly, we aim to answer the following questions:
1. Does our framework enable the robot to learn energy-efficient locomotion controllers?
2. Does the gait switching behavior, which is widely observed in animals, emerge naturally in the learning process?
3. Can the gait policy learned in simulation be deployed on real robots?
4. What are the advantages of our hierarchical framework and what are important design decisions?

5.1 Experiment Setup

We use the Unitree A1 robot [14], a small-scale, 15kg quadruped robot with 12 degrees of freedom. We use PyBullet [47] to simulate the robot dynamics. We implement the state estimation and high-level policy inference in Python, and the low-level Centroidal Dynamics-based Convex MPC Controller in C++. We use a Mac-Mini with M1 processor as our on-board computer, which runs the high-level gait generator at 20Hz and low-level convex MPC controller at 500Hz.

5.2 Emergence of Energy-Efficient Gaits

To demonstrate that our framework can learn efficient locomotion controllers, we evaluate the learned gait policy under different speed commands, and compare the Cost of Transport (CoT) with four carefully-designed, animal-inspired gaits: Walk, Slow Trot, Rapid Trot and Fly Trot. To find the parameters of these gaits, we first choose the phase offsets and swing-ratio based on the characteristics of each gait, and then perform grid search on stepping frequency to maximize the reward (Eq. 3) at different speed ranges. The parameters of these manually-designed gaits are summarized in Table. 1. We plot the CoT of each manually-designed gait and our learned controller (averaged over 5 random seeds) in Fig. 4. Clearly, the learned policy consistently achieves the lowest energy consumption at most of the speeds.

A closer look at Fig. 4 reveals that walking gait is the most efficient when the speed is below 0.8m/s, the slow and rapid trotting gait are the most efficient between 0.8 and 2m/s, and the fly-trotting gait is the most efficient when the speed is above 2m/s. We execute the learned gait policy on an accelerating speed profile, and are glad to find that the policy switches gaits at similar boundaries (Fig. 3). At low speeds (less than 0.9m/s), the policy exhibits a four-beat walking gait by moving one leg at a time in the order of [RR, FL, RL, FR]. At intermediate speeds (between 0.9 and 1.8 m/s), the policy synchronizes the diagonal legs and exhibits a trotting gait. At the highest speeds...
(1.8m/s or above), the policy exhibits a fly-trotting gait, with noticeable “airborne-phases” when all legs lift from the ground (characterized by $p_{\text{swing}} > 0.5$).

Compared to gaits observed in quadrupedal animals, our gait policy discovered similar behaviors at low and mid-range speeds (walking and trotting). However, at high speeds, many animals would gallop. To understand why our method does not automatically learn galloping at higher speeds, we reproduced a galloping gait in our framework by limiting the range of phase offsets. However, we found the learned galloping gait to be actually 30% less efficient than the flying trot on our robot, in contrast to animals [1]. This difference between animals and robots has been noted in [39], and it was hypothesized that such difference could result from differences in morphology, kinematics limits and joint actuation.

### 5.3 Validation on the Real Robot

We deploy our hierarchical controller, including the learned gait policy and the low-level model-based controllers, to the real robot (Fig. 5). Please watch the accompanying video. In contrast to many RL works that focus on sim-to-real transfer [9, 11, 12], our gait policy, learned entirely in simulation with PyBullet, can be directly deployed to the real world without additional data collection or fine-tuning. Similar to the simulation results, as the robot accelerates, it dynamically switches between walking, trotting and fly-trotting gaits, and eventually reached the speed of 2.5m/s, or 5 body lengths per second.

We test the generalization of our learned controller in a number of novel scenarios that were not seen during training. Although the policy is only trained using a slowly accelerating desired speed profile, the robot remains stable with abrupt changes of the desired speed, such as sharp acceleration and braking (Fig. 6a). The learned controller also generalizes to new terrains, including walking over an 8-cm step (Fig. 6b) and on grass (Fig. 6c). This excellent generalization is attribute to our hierarchical setup with a robust low-level convex MPC controller, which has demonstrated proven robustness on a wide variety of robot systems [3, 48, 49].

### 5.4 Comparisons with Non-Hierarchical Policies

To demonstrate the importance of the hierarchical setup, we compare the performance of our hierarchical framework with two non-hierarchical baselines: E2E and PMTG. E2E is a fully-connected end-to-end policy that directly maps from state to motor actions. PMTG implements the Policies Modulating Trajectory Generator [29], which simplifies learning by incorporating cyclic motion priors, and is widely used in the locomotion learning literature [33, 50, 51]. Following the prior work [52], we expand the state space to include IMU readings and motor angles, and modify the action space to be desired motor positions. Additionally, we carefully tuned the reward function in each baseline for optimal performance. See Appendix C.2 for details. We train all policies using the same CMA-ES algorithm.
5.5 Comparisons with Different Learning Algorithms

Using Evolutionary Strategies (ES) to train our hierarchical controller is a critical design decision. To understand its importance, we compare CMA-ES with other state-of-the-art methods, including PPO [53], SAC [7] and ARS [5] in training the hierarchical controller. Since both PPO and SAC can benefit from more comprehensive state information, we also run these algorithms with an extended observation space, which includes IMU readings, motor angles and gait phases, in addition to current and desired velocities. Please refer to Appendix C.1 for setup details and additional results.

As shown in Table 2, algorithms based on Evolutionary Strategies (ES), CMA-ES and ARS, significantly outperforms other algorithms. When using the original observation space, both PPO and SAC fail to complete the task, which is likely due to the lack of sufficient information to accurately estimate the value function. With the extended observation space, SAC learns to walk forward, but fails to track the speed closely, and consumes more energy, compared to ES-based algorithms. We hypothesize that the poor performance of these two popular reinforcement learning algorithms is because the low-level convex MPC controller is a black box to the RL agent, which is not fully-observable and make the environment less Markovian.

| Algorithm      | Success? | CoT      | Avg Speed Tracking Error   |
|----------------|----------|----------|---------------------------|
| PPO            | No       | 2.29 ± 0.96 | 0.080 ± 0.092           |
| PPO (extended obs) | No | 3.60 ± 1.05 | 0.15 ± 0.17             |
| SAC            | No       | 2.22 ± 0.47 | 0.069 ± 0.025           |
| SAC (extended obs) | Yes | 1.19 ± 0.04 | 0.030 ± 0.025           |
| ARS            | Yes      | 0.87 ± 0.0073 | 0.0082 ± 0.00034       |
| CMA-ES (ours)  | Yes      | 0.84 ± 0.017 | 0.0083 ± 0.00075        |

Table 2: Cost of Transport (CoT) and speed tracking error (Eq. 3) for gait policies trained by different algorithms. Error bar shows 1 standard deviation.

6 Conclusion

We present a hierarchical learning framework that can automatically learn fast and efficient gaits for quadrupedal robots. Our framework combines a high-level gait generator with a low-level convex MPC controller, where a gait policy is trained using evolutionary strategies with a simple reward function. Through learning, distinctive gaits and natural transitions between gaits emerge automatically. More importantly, the policy learned in simulation can be successfully deployed to the real world, thanks to the hierarchical setup. Observations in our robotic experiments agree well with prior bio-mechanical studies, which showed that quadrupedal animals switch gaits at different speeds to lower their energy expenditure. Our hierarchical control framework is general, and can be extended to modulate not only the gait patterns, but also other parts of the low-level controller, such as foot placement positions and desired base pose, to enable more agile and versatile locomotion skills. We plan to further develop this hierarchical framework through the lens of bi-level optimization, and apply it to other robotic platforms.
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A Details of the Low-Level Convex MPC Controller

Figure 8: Our low-level convex MPC controller uses different controllers for stance (left) and swing (right) legs.

A.1 Stance Leg Controller

The stance leg controller optimizes for the ground reaction forces using Model Predictive Control (MPC) (Fig. 8a), where the objective is for the base to track a desired trajectory. The robot is modeled using the simplified centroidal dynamics model. We now describe our setup in detail:

Notation We represent the base pose of the robot in the world frame as \( x = [\Theta, p, \omega, \dot{p}] \in \mathbb{R}^{12} \). \( \Theta = [\phi, \theta, \psi] \) is the robot’s base orientation represented as Z-Y-X Euler angles, where \( \psi \) is the yaw, \( \theta \) is the pitch and \( \phi \) is the roll. \( p \in \mathbb{R}^3 \) is the Cartesian coordinate of the base position. \( \omega \) and \( \dot{p} \) are the linear and angular velocity of the base. \( r_{\text{foot}} = (r_1, r_2, r_3, r_4) \in \mathbb{R}^{12} \) represents the four foot positions relative to the robot base. MPC optimizes for the ground reaction force \( f_1, ..., f_4 \) at each foot, which we denote as \( u = (f_1, f_2, f_3, f_4) \in \mathbb{R}^{12} \). \( I \) denotes the \( n \times n \) identity matrix. \( \cdot \times \) converts a 3d vector into a skew-symmetric matrix, so that for \( a, b \in \mathbb{R}^3 \), \( a \times b = [a] \times b \).

Centroidal Dynamics Model Our centroidal dynamics model is based on [3] with a few modifications. We assume massless legs, and simplify the robot base to a rigid body with mass \( m \) and inertia \( I_{\text{base}} \) (in the body frame). The rigid body dynamics in world coordinates are given by:

\[
\frac{d}{dt}(I_{\text{world}}\dot{\omega}) = \sum_{i=1}^{4} r_i \times f_i \\
\dot{p} = \frac{\sum_{i=1}^{4} f_i}{m} + g
\]

where \( g = [0, 0, -9.8]^T \) is the gravity vector. To simplify Eq.4, note that when angular velocity is small, we can omit the centripetal forces and write the left hand side as:

\[
\frac{d}{dt}(I_{\text{world}}\dot{\omega}) = I_{\text{world}}\ddot{\omega} + \omega \times (I_{\text{world}}\dot{\omega}) \approx I_{\text{world}}\ddot{\omega}
\]

Given the robot the orientation matrix in the world frame \( R \in SO(3) \), the world-frame inertia is:

\[
I_{\text{world}} = RI_{\text{base}}R^T
\]

When the robot is close to upright (\( \theta, \phi \approx 0 \)), the relationship between the angular velocity and the change rates of Euler angles can be written as:

\[
\dot{\Theta} = \begin{bmatrix}
\dot{\phi} \\
\dot{\theta} \\
\dot{\psi}
\end{bmatrix} \approx \begin{bmatrix}
\cos(\psi) & \sin(\psi) & 0 \\
-\sin(\psi) & \cos(\psi) & 0 \\
0 & 0 & 1
\end{bmatrix} \omega = R_z(\psi)\dot{\omega}
\]
With the above simplifications, we get the linear, time-varying dynamics model:

\[
\frac{d}{dt} \begin{bmatrix} \Theta \\ p \\ \omega \\ \dot{\Theta} \\ \dot{p} \\ \dot{\omega} \end{bmatrix} = \begin{bmatrix} 0_3 & 0_3 & R_z(\psi) & 0_3 \\ 0_3 & 0_3 & 0_3 & 0_3 \\ 0_3 & 0_3 & 0_3 & 0_3 \\ \end{bmatrix} \begin{bmatrix} \Theta \\ p \\ \omega \\ \dot{\Theta} \\ \dot{p} \\ \dot{\omega} \end{bmatrix} + \begin{bmatrix} f_1 \\ f_2 \\ f_3 \\ g \\ \end{bmatrix}
\]

(9)

We then discretize the continuous time dynamics equation, which we use in our MPC formulation.

\[
x_{t+1} = A' x_t + B' u_t + g'
\]

(10)

where \(A', B', g'\) are the discrete time counterpart of \(A, B\) and \(g\) in Eq. (9).

**Reference Trajectory Generation** Given the desired linear velocity of the base \(\bar{v}_{\text{base}}\), we compute a desired trajectory \(\bar{x}_t\) for the next \(T\) timesteps, where \(T\) is the MPC planning horizon. In each reference state, we set \(\ddot{p}\) to \(\bar{v}_{\text{base}}\) and set \(\dot{p}\) to numerically integrate \(\bar{v}_{\text{base}}\) for speed-tracking, and set the desired orientation \(\Theta\) and angular velocity to \(\omega\) to 0 to ensure stable walking.

**MPC Formulation** Given the reference trajectory \(\bar{x}_{1:T}\), we solve for the ground reaction forces \(u_{1:T}\) by solving the following Quadratic Program (QP):

\[
\min_{u_{1:T}} \sum_{t=1}^{T} ||x_t - \bar{x}_t||_Q + ||u_t||_R \\
\text{subject to } x_{t+1} = A' x_t + B' u_t + g' \text{ Eq. (10)} \\
f_{i,t} = 0 \text{ if leg } i \text{ is a swing leg at } t \\
f_{\text{min}} \leq f_{i,t} \leq f_{\text{max}} \text{ if leg } i \text{ is a stance leg at } t \\
-\mu f_{\text{min}} \leq f_{i,z,t} \leq \mu f_{\text{max}} \forall i, t \\
-\mu f_{\text{min}} \leq f_{i,y,t} \leq \mu f_{\text{max}} \forall i, t
\]

(11)

where \(Q, R\) are diagonal weight matrices. The constraints include the centroidal dynamics, the contact schedule of each leg and the approximated friction cone conditions. The optimized contact forces are then converted to motor torques using Jacobian transpose: \(\tau = J^T f\).

### A.2 Swing Leg Control

The swing leg controller calculates the swing foot trajectories and uses Proportional-Derivative (PD) controllers to track these trajectories (Fig. 8b). To calculate a leg’s swing trajectory, we first find its lift-off, mid-air and landing positions \((p_{\text{lift-off}}, p_{\text{air}}, p_{\text{land}})\) (Fig. 8b). The lift-off position \(p_{\text{lift-off}}\) is the foot location at the beginning of the swing phase. The mid-air position \(p_{\text{air}} = p_{\text{ref}} + (0, 0, z_{\text{des}})\) is a fixed distance above the normal standing position \(p_{\text{ref}}\). We use the Raibert Heuristic [38] to estimate the desired foot landing position:

\[
p_{\text{land}} = p_{\text{ref}} + v_{\text{CoM}} T_{\text{stance}}/2
\]

(12)

where \(v_{\text{CoM}}\) is the projected robot’s CoM velocity onto the \(x - y\) plane, and \(T_{\text{stance}}\) is the expected duration of the next stance phase, which can be calculated using the stepping frequency and swing ratio from the gait policy (Section 3.2). Raibert’s heuristic ensures that the stance leg will have equal forward and backward movement in the next stance phase, and is commonly used in locomotion controllers [4, 3, 13].
Given these three key points, $p_{\text{lift-off}}, p_{\text{air}},$ and $p_{\text{land}}$, we fit a quadratic polynomial, and computes the foot’s desired position in the curve based on its progress in the current swing phase. Given the desired foot position, we then compute the desired motor position using inverse kinematics, and track it using a PD controller. We re-compute the desired foot position of the feet at every step (500Hz) based on the latest velocity estimation.

## B Modeling Motor Power Consumption

### B.1 DC Motor Model

![Figure 9: Schematic drawing of DC motor model.](image)

We model a DC motor circuit as in Fig. 9, which includes a motor with internal resistance $r$ and torque constant $k$. To apply a torque $\tau_m$, the motor controller applies a voltage $v$ to the motor, which generates a current $i$. As the motor rotates with angular velocity $\omega_m$, it also generates a back-emf voltage $v_{\text{emf}}$. We aim to express the battery power consumption $p = vi$ in terms of the motor velocity $\omega_m$ and applied motor torque $\tau_m$. If we ignore motor inductance and only consider steady-state behaviors, the circuit characteristic can be written as:

\[
\begin{align*}
\tau_m &= ki \\
v_{\text{emf}} &= k\omega_m \\
i &= \frac{v - v_{\text{emf}}}{r}
\end{align*}
\]

where Eq.13 and Eq.14 models steady-state motor behavior, and Eq.15 is derived from Ohm’s law. Solving for $v$ in terms of $\tau_m, \omega_m$ and motor constants $k, r$, we get:

\[
v = \frac{r}{k} \omega_m + \frac{\tau_m r}{k}
\]

The power supplied by the battery can be computed by:

\[
p = vi = \left(\frac{r}{k} \omega_m + \frac{\tau_m r}{k}\right) \frac{r}{k} \omega_m = \frac{r}{k} \omega_m + \frac{r^2 \tau_m^2}{k^2}
\]

Note that the first term is the mechanical power delivered by the motor, and the second term is the extra heat dissipation in the motor circuit. Since Unitree’s battery management system does not support regenerative braking, we lower-bound the power consumption by 0, and get:

\[
p_{\text{actual}} = \max\left(\tau_m \omega_m + \frac{r^2 \tau_m^2}{k^2}, 0\right)
\]

### B.2 Power Consumption of A1 motors

Based on the motor characteristic curve of A1 (Fig. 10), at $\tau_m = 4\text{Nm}$ and the output power is approximately 400w, with an efficiency of approximately 50%. Therefore, $\tau_m \omega_m \approx \frac{1}{25} \tau_m^2 \approx 400\text{w}$. We can then deduce that $\frac{r}{k^2} \approx 25$ and express power consumption as:

\[
p_{\text{actual}} \approx \max(\tau_m \omega_m + 25 \tau_m^2, 0)
\]

The motor of A1 have a gear reduction ratio of 9.1. Therefore the joint velocity and joint torque $(\tau, \omega)$ can be expressed in terms of motor velocity and motor torque $(\tau_m, \omega_m)$ as:

\[
\begin{align*}
\tau &= 9.1 \tau_m \\
\omega &= \frac{\omega_m}{9.1}
\end{align*}
\]
Substituting into Eq. 19, we can express the power consumption in terms of joint torque and velocity:

\[
p_{\text{actual}} \approx \max \left( \tau \omega + \frac{25}{9.1^2} \tau^2, 0 \right) \approx \max (\tau \omega + 0.3\tau^2, 0)
\]  

(20)

\section*{C Experiment Details}

\subsection*{C.1 Comparison with Different Learning Algorithms}

**CMA-ES Setup**  We obtain the CMA-ES implementation from Pycma [54]. We represented the policy using a fully connected neural network with 1 hidden layer of 256 units and tanh non-linearity. We initialize the algorithm with a mean of 0 and standard deviation of 0.03, and perform each update using a population size of 32.

**ARS Setup**  In ARS, we represented the policy using a fully connected neural network with 1 hidden layer of 256 units and tanh non-linearity. The policy parameter is initialized to be all 0 at the start of training. At each iteration, we estimate the gradient by sampling 16 policy perturbations with standard deviation of 0.03, and update the policy using a step size of 0.02.

**PPO and SAC Setup**  We obtain the PPO and SAC implementation from the Stable-baselines-3 [55] repo. For both algorithms, we represent the actor and the critic using a fully connected neural network with 2 hidden layers of 64 units each and tanh non-linearity. For PPO, we additionally normalize the observation and reward using a moving average filter, which increases the total reward by 3x. We list the hyperparameters used in each algorithm in Table 3 and 4.

| Parameter       | Value     |
|-----------------|-----------|
| Learning rate   | 0.0003    |
| # env steps per update | 800 |
| Batch size      | 64        |
| # epochs per update | 10    |
| Discount factor | 0.99      |
| GAE \( \lambda \) | 0.95      |

Table 3: Hyperparameters used for PPO.

| Parameter       | Value     |
|-----------------|-----------|
| Learning rate   | 0.0003    |
| Replay buffer size | \(10^6\) |
| Batch size      | 256       |
| Discount factor | 0.99      |
| Entropy coefficient | Auto learned |
| # env steps per update | 10 |
| # gradient steps per update | 1 |

Table 4: Hyperparameters used for SAC.

**Parallel Rollouts to Reduce Training Time**  Since the low-level controller involves solving MPC problems, data collection in our environment is computationally heavy, and takes up a significant portion of the training time. To speed up training, we use multi-processing to parallelize rollouts whenever possible. For CMA-ES and ARS, we parallelize rollouts across 32 cpu cores, and collect 1
 episode (400 steps) from each core per training iteration. For PPO, we parallelize rollouts across 32 cpu cores, and collect 25 steps from each core per training iteration. We do not parallelize rollouts for SAC since the algorithm does not benefit significantly from parallel data collection.

Parallelized data collection greatly reduces the wall-clock training time, as CMA-ES (2 hours), ARS (2 hours) and PPO (12 hours) take significantly less time to reach 1.5 million environment steps compared to SAC (40 hours). In addition, ES-based algorithms (CMA-ES and ARS) update their policies less frequently and do not require back-propagation for policy update, which explains their wall-clock efficiency compared to PPO.

**Learning Curves** We plot the learning curves for different algorithms in Fig. 12. CMA-ES and ARS consistently out-performed other algorithms. When using the original observation space, which contains only the desired and current velocity, both PPO and SAC fail to complete the task, and show high variance in their learning curves. This is likely due to the lack of sufficient information to accurately estimate the value function. With the extended observation space, SAC learns to walk forward, but achieves a lower return compared to CMA-ES and ARS.

**C.2 Comparison with Non-Hierarchical Policies**

**Reward Function for TG Policy** We find the original reward function used in hierarchical environment (Eq. 3) to be ineffective in training the TG policy. Specifically, the TG policy usually incurs a significantly higher cost-of-transport compared to the hierarchical policy, especially in early stages of training. As a result, the reward (Eq. 3) is mostly negative, and CMA-ES learns to maximize return by terminating each episode early. Therefore, we reduce the energy penalty weight ($w_e$ in Eq. 3) from 0.37 to 0.037 to ensure that the reward stays positive.

**Reward Function for E2E Policy** In addition to reducing the energy penalty weight, we found it necessary to perform further reward shaping for the E2E policy. Without the cyclic trajectory priors defined by TG, the E2E policy struggles to maintain balance and often walks forward in unstable, tilted pose. To encourage stable, up-right walking, we include additional terms based on the height and orientation of the robot, which is similar to the cost function used in the low-level convex MPC controller (Eq. 11). We end up with the following reward function:

$$r = c - w_e \left( \frac{\bar{v}_{base}}{v_{base}} \right)^2 - w_e \sum_{i=1}^{12} \max(\tau_i \omega_i + \alpha \tau_i^2, 0) - w_o (\text{roll}^2 + \text{pitch}^2) - w_h (\bar{h} - h)^2$$

where the speed penalty and energy penalty is the same as defined in Eq. 3. The orientation penalty penalizes the robot’s deviation from an upright posture based on the IMU reading. The height

![Figure 11: Learning curve for hierarchical policies trained by different algorithms. Results show average over 5 random seeds. Error bar indicates 1 standard deviation.](image)
penalty penalizes the robot’s deviation from a desired walking height, where $\hat{h}$ and $h$ are the desired and actual height of the robot’s center of mass.

We set $\hat{h} = 0.26$, which is the same as the reference height in the low-level convex MPC controller in the hierarchical setting (Section A.1). We use the same weight for the alive bonus $c = 3$ and speed penalty $\omega_v = 1$ as in the hierarchical setup (Eq. 3, reduced $\omega_c$ from 0.37 to 0.037, and set $\omega_\alpha = 10, \omega_h = 200$ for E2E experiments.

**Policy Representation and Training**  
To train the non-hierarchical policies, we followed the same setup as the hierarchical policy (Section 4.3). We represent each policy using a neural network with 256 units and tanh non-linearity, and trained the policy using the same CMA-ES algorithm.

**Learning Curves**  
We plot the learning curves of non-hierarchical policies in Fig. 12. As noted in section 5.4, E2E only learns to stand for the entire episode, and the learning curve eventually becomes unstable. Although TG policy slowly learns to walk, the resulting gait is jaggy and only uses 3 legs.

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**Figure 12**: Learning curves for non-hierarchical policies. Results are averaged over 5 random seeds. Error bar shows 1 standard deviation.