Nonlinear Optical Signal Generation Mediated by a Plasmonic Azimuthally Chirped Grating

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ABSTRACT: Plasmonic gratings are simple and effective platforms for nonlinear signal generation since they provide a well-defined momentum for photon−plasmon coupling and local hot spots for frequency conversion. Here, a plasmonic azimuthally chirped grating (ACG), which provides spatially resolved broadband momentum for photon−plasmon coupling, was exploited to investigate the plasmonic enhancement effect in two nonlinear optical processes, namely two-photon photoluminescence (TPPL) and second harmonic generation (SHG). The spatial distributions of the nonlinear signals were determined experimentally by hyperspectral mapping with ultrashort pulsed excitation. The experimental spatial distributions of nonlinear signals agree very well with the analytical prediction based on photon−plasmon coupling with the momentum of the ACG, revealing the “antenna” function of the grating in plasmonic nonlinear signal generation. This work highlights the importance of the antenna effect of the gratings for nonlinear signal generation and provides insight into the enhancement mechanism of plasmonic gratings in addition to local hot spot engineering.

KEYWORDS: plasmonic grating, azimuthally chirped grating, second harmonic generation, two-photon photoluminescence, plasmonic nanoantennas, nonlinear signal generation

Nonlinear effects in light−matter interaction arise from the higher-order corrections to the susceptibility of matter.1 The nonlinear dependence of the induced polarization on the incident electric field has been used extensively for frequency conversion, which leads to a broad range of applications,2,3 including telecommunication,4 optical signal processing,5 all-optical switching,6 optical microscopy,7 optical tomography,8 and biosensing.9 To facilitate such nonlinear processes, rationally designed nanostructures have been exploited for the engineering of both near and far optical fields related to nonlinear optical processes.10−13 The success of nanostructure-assisted nonlinear signal generation lies in well-engineered overlapping and coupling of electromagnetic fields at multiple frequencies in both far- and near-field regimes. In general, the energy of far-field excitation at the fundamental frequency needs to be effectively concentrated in the near-field region, where the hot spot promotes the frequency conversion, and the locally generated nonlinear signals, possibly at multiple frequencies, need to be sent to the far-field region with high efficiency. Although the process is more complex than conventional nonlinear signal generation in bulk nonlinear crystals without nanostructures, it is the use of nanostructures that enables design-based enhancement of nonlinear signal generation.14,15

Plasmonic gratings are simple but effective nanostructures for enhancing nonlinear signal generation.16 There are three key steps for plasmonic grating-based nonlinear signal generation (Figure 1a). In the first step, the plasmonic grating should be designed such that it functions as an effective “receiving antenna” for the far-field excitation to generate near-field hot spots. This is typically done by choosing the right grating periodicity to provide the correct momentum for photon−plasmon coupling at the desired frequencies. In the second step, the hot spots should provide extreme spatial confinement and intensity enhancement of the optical near field at the input and output frequencies for the nonlinear optical processes. The spatial distribution of the hot spots at the input and output frequencies should overlap in space to provide maximal efficiency.17−26 Because the hot spots are extremely confined in space, they provide broad spatial frequency bandwidth to facilitate the phase matching required for the frequency conversion.

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Among various nonlinear signals, TPPL and SHG are two nonlinear processes that commonly occur in plasmonic nanostructures. While both nonlinear signals exhibit a quadratic dependence on the excitation power, the underlying mechanisms are quite different. TPPL is a third-order nonlinear process involving the sequential absorption of two photons as input and the emission of a blue-shifted single photon as output.17,27–29 The first photon absorption results in an intraband transition of an electron in the conductive sp-band. The second photon sequentially brings about an interband transition of a second electron from the d-band to fill the hole created by the first photon in the sp-band (Figure 1a).17,27,28 For the intraband transition in the first step, momentum conservation can only be fulfilled with the broadband momentum provided by the plasmonic hot spots.17,18,27,28

The recombination of the electron from the first transition with the hole in the d-band occurs through a radiative relaxation into broadband TPPL with shorter wavelengths than the excitation. On the other hand, SHG is a second-order nonlinear process marked by output at the SH of the fundamental excitation frequency. SHG requires the potential profile of the oscillating electrons to be symmetry broken.3 It is inherently weak and constrained by the phase-matching conditions. Therefore, the SHG of materials with central symmetry, such as metals, is usually weak under typical excitation by plane waves in the far field. However, SHG can be significantly enhanced by the hot spots of resonant plasmonic nanostructures due to field enhancement and localization. As explained previously, the field enhancement compensates for the weak nonlinearity of high-order harmonic generation, and the extreme field localization provides broadband momentum necessary for the required phase-matching condition.30 To promote nonlinear signal generation, plasmonic nanostructures need to be carefully designed.

In this work, the enhancement effects of a plasmonic ACG in TPPL and SHG were investigated and compared. Hyperspectral mapping on the ACG was performed to obtain simultaneously TPPL and SHG maps. This ensures a fair comparison since the two nonlinear signals were generated on the same structure with the same excitation condition. The spatial distribution of the two nonlinear signals is analyzed to show the antenna role of the plasmonic grating. The difference in the spatial distribution is also discussed.

The ACG is designed in a way that the trajectory of the nth circular groove can be described as12,31

$$ (x - nd)^2 + y^2 = (n\Delta r)^2 $$

(1)

where $d$ is the displacement of the center of the circular grooves and $\Delta r$ is the increment in radius. The grating periodicity ($P$) at a certain in-plane azimuthal angle ($\varphi$) is given by

$$ P_{\Delta r,\varphi} = ld \cos \varphi \pm \sqrt{(d^2 \cos 2\varphi + 2\Delta r^2 - d^2)/21} $$

(2)

As the in-plane azimuthal angle increases from 0° to 180°, the periodicity of ACG varies continuously from $\Delta r + d$ to $\Delta r - d$, as illustrated in Figure 2a. By choosing suitable $\Delta r$ and $d$, the range of grating periodicities can be easily designed for any desired application.12,31 In this work, the $\Delta r$ and $d$ were chosen to be 0.7 and 0.4 μm, respectively, corresponding to the minimum and maximum grating periodicities of 0.3 and 1.1 μm. A graphical
The error bar represents the standard deviation of the mean spectrum obtained from all points along the 45° in-plane azimuthal angle within the area of the ACG.

Figure 2. (a) The upper panel shows the design of ACG in the top view with the tilted view of the cross section. The lower panel shows one of the SEM images of the gold ACG structures used in this work with Δr = 700 nm, and d = 400 nm. Scale bar = 10 μm. (b) Mean spectrum showing simultaneously the SH peak and TPPL signal from ACG at an azimuthal angle of 45°. The inset shows the TPPL part of the spectrum. The error bar represents the standard deviation of the mean spectrum obtained from all points along the 45° in-plane azimuthal angle within the area of the ACG.

representation of this azimuthal angle-dependent periodicity is given in the Supporting Information (Figure S1). With the azimuthal angle-dependent periodicity and the photon-plasmon phase-matching condition, an azimuthal angle-dependent resonance wavelength (λ₀) can be determined by

\[
\lambda_0 = \frac{l d \cos \varphi \pm \sqrt{(d^2 \cos 2\varphi + 2\Delta r^2 - d^2)/2}}{m} \times \left(\frac{e_m n_i^2}{e_m + n_i^2} - n_i \sin \theta \right)
\]

where \(m\) is the order of resonance, \(\varphi\) is the angle of incidence, \(e_m\) is the permittivity of the metal, and \(n_i\) is the index of the dielectric surrounding. The designed ACG was fabricated by using a gallium focused-ion beam (FEI Helios NanoLab 600i) to mill selective areas of chemically synthesized gold flake. The thickness of the flakes is estimated to be ~200 nm. The target milling depth is 150 nm, and the width of the grooves is around 50 nm. The ACG used for the investigation of TPPL and SHG consists of 20 rings starting from the smallest ring with a zero radius. Outside of the grating area of the ACG, two pairs of horizontal and vertical slits are fabricated for position alignment. Figure 2a shows the schematic design of a typical ACG and the SEM image of the ACG used for TPPL and SHG investigation in this work.

For the investigation of SHG and TPPL generation from the plasmonic ACG, the wavelength-tunable (990–1100 nm) signal beam of an optical parametric oscillator (PP-OPO Automatic, Angewandte Physik & Elektronik GmbH Berlin) pumped by a Ti:sapphire oscillator (Mira HP, Coherent) has been used. The laser emits pulses of ~150 fs duration, an average power of ~200 mW, and a 76 MHz repetition rate for fundamental excitation. Inhomogeneous intensity distribution is indicated in the analytically calculated sector range for the excitation beam, the allowed angle ranges fulfilling the momentum matching condition without providing any information about the field intensity because the latter also depends on the impedance laser conditions. Our excitation beams have a Gaussian beam profile, most of the excitation power passes through the central area of the objective, corresponding to an effectively smaller NA than the specification of the objective. Therefore, most of the excitation power is delivered to the ACG within a small incident angle range. As a result, within the allowed in-coupling sector range for the excitation beam, the incident power is inhomogeneous with a gradient from the largest power on the right boundary at \(\varphi = 35^\circ\) to the weakest power on the left boundary at \(\varphi = 78^\circ\) (Figure 3a). The inhomogeneous intensity profile corresponds to an azimuthal angle \(\varphi = 62^\circ\). This angle was calculated by considering the radius of the cross-sectional area within the FWHM of the Gaussian beam intensity profile. The FWHM radius corresponds to an incident angle \(\theta = 14.5^\circ\). Inserting this incident angle into eq 3, we obtain the azimuthal angle \(\varphi = 62^\circ\) corresponding to the FWHM of the excitation power distribution. Details of the effect of the Gaussian beam...
We first focus on TPPL. Figure 3a shows the calculated sector areas for the in-coupling of an excitation wavelength (λex) at 1000 nm. (b) Azimuthal distribution of the emitted TPPL signal (ΔTPPL) at 595 nm for different grating orders (m). (c) Overlapping areas of the sectors shown in (a) for TPPL excited at 1000 nm and emission at 595 nm (b). (d) Experimentally observed TPPL signal at 595 nm from the ACG. Scale bar = 10 μm and color bar represents signal photon counts per second (Cts./s). (e) Azimuthal distribution of emitted SHG signal at 500 nm for different orders. (f) Overlapping area of the sectors shown in (a) and (e) for SHG excited at 1000 nm and emission at 500 nm, respectively. (g) Experimentally observed spatial distribution of the SHG signal from ACG. Scale bar = 10 μm.

Next, we focus on SHG. The sector areas for the in-coupling of the excitation are the same as that for TPPL (Figure 3a), and the emission is at the SHG wavelength. The calculated grating areas for SHG emission out-coupling via grating orders m = −1, −2, and −3 are depicted in Figure 3e with the consequent overlapping areas shown in Figure 3f and the experimental intensity distribution displayed in Figure 3g. A strong SHG signal is observed within the analytically calculated sector areas between 35° and 55°, which is suitable for an excitation in-coupling at λex = 1000 nm via an m = −1 grating order and the emission out-coupling at λSHG = 500 nm via an m = −3 order. Another analytically predicted enhancement sector area between 63° and 78°, where the out-coupling of the emission at λSHG is enhanced via an m = −2 grating mode, does not show a strong SHG signal in the experiment. The signal is not strong since the excitation beam has a Gaussian profile, and the power within the excitation sector (Figure 3a) decays to the FWHM of the Gaussian intensity profile at about φ = 62°. Therefore, the sector area between 63° and 78° is receiving relatively weak excitation power. Because SHG is quadratically dependent on the excitation power, the signal decays even faster than the excitation power gradient, leading to a rather dim SHG signal. Overall, the maximum SHG conversion efficiency obtained in this work is about 3.3 × 10^-10. Because of the fact that our SHG wavelength (500 nm) falls within the absorption range of gold due to interband transition, our conversion efficiency is 1–2 orders of magnitude smaller compared to the values reported in previous works using doubly resonant plasmonic gold nano-antennas or silver gratings. Details of the estimation of the conversion efficiency can be found in the Supporting Information. We note that the intensity distribution of the nonlinear signal shows some inhomogeneity along the radial direction even at the same azimuthal angle (e.g., Figure 3g). This is mainly due to two reasons. First, the effective grating area of the sector decreases with a reducing radius. As a result, the SHG signal intensity is lower at positions closer to the ACG center, where the effective sector area is smaller than the excitation spot size. Second, the ACG was fabricated by milling circular slits on a gold flake with the focused-ion beam. As the ring radius decreases, the uncertainty of the ring pattern and the redeposition contamination become more severe. Therefore, the intensity along the same azimuthal angle is not perfectly homogeneous. Nevertheless, this issue can be avoided by discarding the data from the central area of an ACG.

An intriguing difference between TPPL and SHG can be seen in the low azimuthal angle range between φ = 0° and φ = 35°. While TPPL is almost undetectable in this range, SHG shows detectable intensity like that from the unpatterned area. Within this angle range, the ACG does not provide the momentum needed for the photon-plasmon coupling at the excitation wavelength. Therefore, no excitation enhancement is expected for TPPL or SHG. This difference in the intensity of TPPL and
SHG in this angle range stems from the different nonlinear mechanisms and selection rules responsible for TPPL and SHG. As discussed previously, TPPL from gold is a nonlinear process involving the "sequential" absorption of two photons. The first photon triggers an intraband transition of electrons in the sp-band and leaves an sp-hole with a lifetime of about 1 ps. The intraband transition relies on the broadband momentum of the plasmonic hot spots. Therefore, TPPL is undetectable on the unpatterned ultrasmooth gold flake surface due to the absence of plasmonic hot spots. In contrast, SHG is a second-order nonlinear process that requires a broken symmetry of the oscillator or the modes responsible for the nonlinear signal generation. In principle, gold is not suitable for SHG because it is a centrosymmetric material. However, symmetry breaking is enforced at the gold surface. Therefore, SHG from the unpatterned gold surface is allowed. In the lower azimuthal angles range (particularly between $\varphi = 0^\circ$ and $\varphi = 35^\circ$), the grating periodicity (1100–989 nm) is comparable to or larger than the size of the laser focal spot (diameter $\sim$1000 nm). This means that the excitation beam does not see the grating but a flat gold surface. As a result, the efficiency of TPPL and SHG in this regime is very similar to that in the unpatterned gold surface area. This can be clearly seen in Figures 3d and 3g, where the signal from the low angle range is like that of the unpatterned surface. This difference reveals the different fundamental mechanisms responsible for the TPPL and SHG processes.

In summary, we investigated the enhancement effect of a plasmonic ACG in surface-enhanced TPPL and SHG. The ACG serves as a spatially and spectrally resolved antenna that mediates the far and near optical fields of multiple input and output beams at different frequencies. The intensity distribution maps of the two nonlinear processes are investigated as a function of the varying periodicity of the ACG. TPPL and SHG signals were simultaneously generated by efficiently coupling both fundamental excitation and emission at a shorter wavelength on a single ACG nanostructure. This study demonstrates that resonant plasmonic gratings serve as optical antennas to mediate the far and near optical fields. The difference in the spatial distributions of SHG and TPPL is revealed and linked to the responsible mechanisms. This work provides valuable information for the design of effective plasmonic nanostructures for nonlinear optical processes.

**ASSOCIATED CONTENT**

**Supporting Information**
The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acs.nanolett.2c03348.

Azimuthal angle-dependent periodicity, experimental setup, FWHM of the excitation and corresponding angles, estimation of the nonlinear signal conversion efficiency (PDF)

Video of TPPL and SHG intensity mapping (AVI)

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**Notes**
The authors declare no competing financial interest.

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**ABBREVIATIONS**
ACG, azimuthally chirped grating; SHG, second harmonic generation; TPPL, two-photon photoluminescence.

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