A perovskite oxide with high conductivities in both air and reducing atmosphere for use as electrode for solid oxide fuel cells

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Electrode materials which exhibit high conductivities in both oxidising and reducing atmospheres are in high demand for solid oxide fuel cells (SOFCs) and solid oxide electrolytic cells (SOECs). In this paper, we investigated Cu-doped SrFe0.8Nb0.2O3−δ finding that the primitive perovskite oxide SrFe0.8Cu0.2Nb0.2O3−δ (SFCN) exhibits a conductivity of 63 Scm−1 and 60 Scm−1 at 415 °C in air and 5%H2/Ar respectively. It is believed that the high conductivity in 5%H2/Ar is related to the exsolved Fe (or FeCu alloy) on exposure to a reducing atmosphere. To the best of our knowledge, the conductivity of SrFe0.8Cu0.2Nb0.2O3−δ in a reducing atmosphere is the highest of all reported oxides which also exhibit a high conductivity in air.

For reversible SOFCs, the use of a symmetrical electrode such as (La0.75Sr0.25)Cr0.5Mn0.5O3−δ (LSCM) exhibits a conductivity of 63 Scm−1 and 60 Scm−1 at 415 °C in air and 5%H2/Ar respectively. It is believed that the high conductivity in 5%H2/Ar is related to the exsolved Fe (or FeCu alloy) on exposure to a reducing atmosphere. To the best of our knowledge, the conductivity of SrFe0.8Cu0.2Nb0.2O3−δ in a reducing atmosphere is the highest of all reported oxides which also exhibit a high conductivity in air. Fuel cell performance using SrFe0.8Cu0.2Nb0.2O3−δ as the anode, (Y2O3)0.06(ZrO2)0.94 as the electrolyte and La0.9Sr0.1FeO3−δ as the cathode achieved a power density of 423 mWcm−2 at 700 °C indicating that SFCN is a promising anode for SOFCs.

Solid oxide fuel cells (SOFCs) are electrochemical devices used to convert chemical energy into electricity with a very high efficiency1. Symmetrical fuel cells have the potential application to be used as reversible SOFCs, which can operate in both fuel cell and electrolyser modes. In a recent report, it was found that a much better stability of SFMO under the SOFC anode environment is not very high thus further improvements are required13. On the other hand, a promising family of redox stable anodes for SOFCs is B-site doped SrFeO3−δ (SFMO), was demonstrated to be a good electrode for symmetrical SOFCs12,13. However, the conductivity of SFMO under the SOFC anode environment is not very high thus further improvements are required13. On the other hand, a promising family of redox stable anodes for SOFCs is B-site doped SrFeO3−δ (SFMO), was demonstrated to be a good electrode for symmetrical SOFCs12,13. However, the conductivity of SFMO under the SOFC anode environment is not very high thus further improvements are required13.

There are plenty oxide materials which exhibit high conductivity in air. The real challenge is to identify a good stable oxide anode material exhibiting high conductivity in a reducing atmosphere2−4. Several redox stable mixed oxide-ion electronic conductors have been developed as ceramic anode materials for SOFCs, such as (La0.75Sr0.25)Cr1−xMnxO3−δ (LSCM)7, Sr2MgMoO6−δ (SMMO)8, LaSrTi1−xMnxGa0.5O3−δ (LSTM)9, La0.33Sr0.67Ti0.33Mn0.67O3−δ (LSTM)10, La0.5Ca0.5CrO3−δ (LSCM)11, SrFe1−xCuxMoO3−δ (SFCN)12, SrFe1−xCuxMoO3−δ (SFCN)12, PrBaMn2O514, Pr0.8Sr1.2(Co,Fe)0.8Nb0.2O4 (CMF-LSFM)17. All of these oxides or composite anodes are redox stable or redox reversible. However, except for La-doped SrTiO3, the conductivity at the anode is typically below 30 Scm−1. The anode conductivity needs to be further improved, particularly for tubular SOFCs with a long pathway for electrons. The conductivity of La-doped SrTiO3 in a reducing atmosphere is high if pre-reduced at a high temperature. However, the conductivity of doped SrTiO3 in air is generally less than 0.1 S/cm6,8,18. In reported perovskite oxides, besides LSCM, The double perovskite SrFe1−xTixO3−δ (SFMO), was demonstrated to be a good electrode for symmetrical SOFCs12−13. However, the conductivity of SFMO under the SOFC anode environment is not very high thus further improvements are required13. On the other hand, a promising family of redox stable anodes for SOFCs is B-site doped SrFeO3−δ. It has been reported that SrFe1−xTixO3−δ where x = 0.3, 0.4 combined with Ce0.9Gd0.1O2−δ performs well as an anode for SOFCs19. It was found that SrFe0.9Tb0.1O3−δ is redox stable with a conductivity of 2.53 S/cm at 600 °C in a reducing atmosphere20. 

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Anikina et al. investigated the conductivity of SrFe$_{1-x}$Nb$_x$O$_{3-\delta}$, where $x = 0.05, 0.1, 0.2, 0.3, 0.4$ and it was found SrFe$_{0.9}$Nb$_{0.1}$O$_{3-\delta}$ exhibits the highest conductivity in a reducing atmosphere. However, the conductivity is still below 1 S/cm at temperatures below 800 °C$^{21}$. In this study, we re-investigated the conductivity of SrFe$_{0.9}$Nb$_{0.1}$O$_{3-\delta}$ finding that its conductivity in a reducing atmosphere was ~30 S/cm which is much higher than the reported values. It was also found that partial replacement of Fe by Cu in SrFe$_{0.9}$Nb$_{0.1}$O$_{3-\delta}$ can further increase the conductivity in a reducing atmosphere. The perovskite oxide SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-\delta}$ (SFCN) exhibits a conductivity of 63 Scm$^{-1}$ and 60 Scm$^{-1}$ at 415 °C in air and 5%H$_2$/Ar respectively. To the best of our knowledge, the conductivity of SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-\delta}$ in a reducing atmosphere is the highest among reported oxide anodes for SOFCs which also exhibit a high conductivity in air. A SOFC using SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-\delta}$ as the anode and La$_{0.8}$Sr$_{0.2}$FeO$_{3-\delta}$ as the cathode has been fabricated with a good performance in hydrogen achieved at temperatures below 700 °C.

**Structure of New Oxides SrFe$_{0.9-x}$Cu$_x$Nb$_{0.1}$O$_{3-\delta}$ ($x = 0–0.4$)**

X-ray diffraction of SrFe$_{0.9-x}$Cu$_x$Nb$_{0.1}$O$_{3-\delta}$ ($x = 0–0.4$) showed that it exhibited a single phase cubic perovskite structure (SG: Pm-3m) for all compounds (Figure S1). The XRD pattern of the SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-\delta}$ sample is shown in Fig. 1A. The increase in the copper content significantly reduced the sintering temperature of the material, with the formation of a single phase perovskite structure that was not observed for SrFe$_{0.4}$Cu$_{0.5}$Nb$_{0.1}$O$_{3-\delta}$. Rietveld refinement of the structure using GSAS$^{22}$ demonstrated a pseudo-linear increase in the lattice parameters with increased copper doping up to SrFe$_{0.6}$Cu$_{0.3}$Nb$_{0.1}$O$_{3-\delta}$ (Figure S3 and Table S2). The increase in lattice parameters with increasing copper content can be attributed to the larger ionic radius of copper compared to iron (Cu$^{2+}$ 0.73 Å, Fe$^{3+}$ 0.645 Å, Fe$^{4+}$ 0.585 Å)$^{23}$. Samples SrFe$_{0.6}$Cu$_{0.3}$Nb$_{0.1}$O$_{3-\delta}$ and SrFe$_{0.5}$Cu$_{0.4}$Nb$_{0.1}$O$_{3-\delta}$ exhibit similar lattice parameters whilst no impurity peaks can be observed on the XRD patterns, this is thought to be due to the proximity of the solid solution limit. Therefore the limit for achieving single phase in the SrFe$_{0.9-x}$Cu$_x$Nb$_{0.1}$O$_{3-\delta}$ series lies at $x \leq 0.5$. The SEM picture of SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-\delta}$ prepared by the solid state reaction method is shown in Fig. 2A.

Thermogravimetric analysis of SrFe$_{0.9-x}$Cu$_x$Nb$_{0.1}$O$_{3-\delta}$ ($x = 0–0.4$) in air showed a minor total loss in weight for all compounds, between 0.2 wt% and 0.5 wt%, with no observable trend on increasing the dopant level, (Figure S3A). Accelerated weight loss was observed for all compounds on heating between 500 and 800 °C, with the weight loss noted to be reversible upon cooling. This acceleration in weight loss is likely to be the result of oxygen loss.

**Figure 1.** Room temperature X-ray diffraction patterns of SrFe$_{0.9-x}$Cu$_x$Nb$_{0.1}$O$_{3-\delta}$ ($x = 0–0.4$) ($x = 0–0.4$) after obtained in air (A) and after further reduction in 5%H$_2$/Ar at 700 °C for 10 hours (B).
through high temperature reduction. Differential scanning calorimetry, Figure S3B, exhibits a reversible transition for all copper doped compounds, between 600 °C and 670 °C on heating and between 670 °C and 590 °C on cooling which could be related to high temperature phase transition.

Conductivity of New Oxides \(\text{SrFe}_{0.9-x}\text{Cu}_x\text{Nb}_{0.1}\text{O}_{3-\delta}\) (\(x=0–0.4\)) in Air

The conductivity of the electrode materials is a key parameter to consider when evaluating their use in SOFCs. Whilst minimal copper doping, forming \(\text{SrFe}_{0.8}\text{Cu}_0.1\text{Nb}_{0.1}\text{O}_{3-\delta}\), elicits a significant increase in conductivity in air over \(\text{SrFe}_{0.9}\text{Nb}_{0.1}\text{O}_{3-\delta}\), additional copper doping is observed to reduce the conductivity of the materials, although increasing dopant levels do not elicit a linear response in the reduction in conductivity (Fig. 3A). The introduction of \(\text{Cu}^{2+}\) dopant is expected to increase the average charge of iron in the sample with the proportion of \(\text{Fe}^{4+}\) ions, increasing the number of charge carriers and thus, in theory, increasing the conductivity. Assuming that the copper dopant does not directly contribute to electronic conduction, the increase in the charge carrier concentration is only proportional to the iron content of the compound, which reduces with increasing \(\text{Cu}^{2+}\) dopant concentration. Thus at higher \(\text{Cu}^{2+}\) dopant concentrations the increase in charge carriers through the average charge of iron increasing is outweighed by the reduction in charge carriers through the reduction of the iron content leading to reduced conductivity. On the conductivity curves, a semiconductor-metal transition was observed for all compounds, with an increase in the transition temperature noted with increasing copper dopant levels (Fig. 3A). This transition has been observed previously for strontium ferrites, with Poulsen et al. suggesting that compound reduction at high temperature, resulting in a reduction in the charge carriers, was the cause of the transition. A pseudo-linear reduction in the oxygen content of strontium ferrite in air above 400 °C with increasing temperature, which would appear to confirm compound reduction at these temperatures, was observed previously. The increase in the conductivity with increasing temperature was determined by Patrakeev et al. to be offset by the reduction in charge carrier concentration, causing an overall reduction in the electronic conductivity with increasing temperature, resulting in the pseudo-metallic behaviour.

Stability of New Oxides \(\text{SrFe}_{0.9-x}\text{Cu}_x\text{Nb}_{0.1}\text{O}_{3-\delta}\) (\(x=0–0.4\))

In order to investigate the stability of \(\text{SrFe}_{0.9-x}\text{Cu}_x\text{Nb}_{0.1}\text{O}_{3-\delta}\) (\(x=0–0.4\)) in a reducing atmosphere, STA analyses in 5%H2/Ar was carried out on the samples. The observed weight loss upon reduction of \(\text{SrFe}_{0.9-x}\text{Cu}_x\text{Nb}_{0.1}\text{O}_{3-\delta}\) (\(x=0–0.4\)) varies between 2.6% and 3.3%, with no observed trend with increasing dopant concentration (Figure S4A). Differential scanning calorimetry exhibits non-reversible transitions on heating for all compounds between 600 °C and 670 °C, associated with cationic reduction (Figure S4B)20. With the increase of copper dopant, the exothermic peaks happened at lower temperature indicating the reduction at lower temperature thus they are likely less stable, this has been confirmed by the XRD study (Fig. 1B). After reducing in 5%H2/Ar at 700 °C for 10 hours, it was found that the Cu-free sample \(\text{SrFe}_{0.9}\text{Nb}_{0.1}\text{O}_{3-\delta}\) was redox stable. For sample \(\text{SrFe}_{0.8}\text{Cu}_0.1\text{Nb}_{0.1}\text{O}_{3-\delta}\), the majority of the phase is perovskite whilst an extra peak at ~45 degree was observed which belongs to the strongest (110) peak of \(\alpha\)-Fe (PDF: 6–696) after the reduction at 700 °C29. The formation of a Fe-rich FeCu alloy cannot be ruled out but the Cu content must be very low otherwise the peak should shift to a higher d-spacing. The exsolution of metal particles is further confirmed by SEM observation where a small particle of iron was exsolved on the surface after the reduction (Fig. 2B). The very weak peak at ~32.5° could be a peak for a solid solution based on \(\text{Sr}_2\text{Fe}_2\text{O}_5\) parent phase30. When x is increased to 0.2, the majority of sample \(\text{SrFe}_{0.7}\text{Cu}_0.2\text{Nb}_{0.1}\text{O}_{3-\delta}\) is possibly \(\alpha\)-Fe solid solution while an extra peak at ~43° was observed which could be the strongest peak.
of Cu (Fm-3m)\(^{31}\). Again, formation of a Cu-rich FeCu alloy is also possible with the presence of Fe at the B-site of the perovskite phase. At \(x = 0.3, 0.4\), Sr, Fe\(_2\)O\(_5\)+\(\delta\) based solid solution is the major phase with the Fe or Fe-rich alloy also present. The exsolution of metal seems strongly related to the composition, which will require further investigation. To exam whether the exsolution of metal is reversible, the reduced SrFe\(_{0.8}\)Cu\(_{0.1}\)Nb\(_{0.1}\)O\(_{3-\delta}\) sample was re-oxidised in air at 1300 °C for 15 hours then further reducing in 5%H\(_2\)/Ar at 700 °C for 10 hours and stop at the re-oxidation stage after 3 cycles. It was observed that the exsolved metal was ‘adsorbed’ back after re-oxidation ii air at high temperature (Fig. 2C) while it was exsolved out after further reduction in 5%H\(_2\)/Ar at 700 °C for 10 hours (Fig. 2D). This indicate the process for exsolved metal is reversible as observed in other oxides\(^{32,33}\).

Figure 3. Conductivity of SrFe\(_{0.9-x}\)Cu\(_x\)Nb\(_{0.1}\)O\(_{3-\delta}\) (\(x = 0–0.4\)) in air (A) 5% H\(_2\)/Ar (B) and comparison of conductivities of reported anode materials in H\(_2\) or 5%H\(_2\) (C).
Conductivity of New Oxides SrFe$_{0.9-x}$Cu$_x$Nb$_{0.1}$O$_{3-δ}$ (x = 0–0.4) in 5%H$_2$/Ar

To measure the conductivity in a reducing atmosphere, the SrFe$_{0.9-x}$Cu$_x$Nb$_{0.1}$O$_{3-δ}$ pellets were coated with silver electrodes on both sides then reduced in 5%H$_2$/Ar at 700°C for 10 hours (Fig. 3B). The conductivity was measured in 5%H$_2$/Ar on cooling. The highest conductivity for the samples measured was found to be for the SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ sample with a conductivity of about 30–60 S/cm, in a reduced atmosphere. This is possibly due to the presence of exsolved Fe particles leading to increased electronic conductivity thus the total conductivity was also high. The lowest conductivity was observed for sample SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ due to the SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ based solid solution being the major phase. This indicates that the conductivity of SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ based solid solution is lower than the primitive perovskite oxide based on SrFeO$_{3-δ}$. When x increased to 0.3 and 0.4, the intensity of the peak at ~45° which the compound SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ (Fig. 1B) even though the major phase was the SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ based solid solution. The conductivity of SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ is comparable to that for the Cu-free sample SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ whilst the conductivity of sample SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ is slightly higher (Fig. 3B) due to a higher concentration of exsolved Fe (or Fe-rich alloy). In the investigated oxides, in terms of both redox stability and conductivity, sample SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ is the best.

For comparison, the conductivity of sample SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ in a reducing atmosphere is plotted together with the reported best oxide anodes for SOFCs (Fig. 3C). It is the highest among the reported materials with reasonably high conductivity in air and a conductivity two times greater than that of the Pr$_{0.8}$Sr$_{1.2}$(Co,Fe)$_{0.8}$Nb$_{0.2}$O$_{4-δ}$/CoFe alloy. The characteristics of all other reported oxide anode materials in a reducing atmosphere are lower than 30 S/cm. This is clearly shown when the conductivity is plotted at absolute value (Figure S5). High conductivity is very important for SOFCs due to some designs involving long pathways for electrons at the electrode. Both SOFC and Pro SOFC (CoFe)$_{0.8}$Nb$_{0.2}$O$_{4-δ}$/CoFe alloy have exsolved metal under reduction indicating that designing a material with exsolved metal under reduction will help to achieve a high conductivity in a reducing atmosphere. The exsolved metal may also improve the catalytic activity under the fuel cell operating conditions.

Fuel Cell Performance when SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ Was Used as the Anode

Solid oxide fuel cells with a SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ anode, YSZ electrolyte and La$_{0.8}$Sr$_{0.2}$FeO$_{3-δ}$ cathode were fabricated. The performance and the corresponding A.C. impedance spectra of hydrogen/air fuel cell at different temperatures are shown in Fig. 4A,B. Good fuel cell performance with a power density of 423 mW/cm$^2$ was observed at 700°C. The total polaronic resistance of the electrode at 700°C was only 0.25 Ω cm$^2$ indicating SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ performs well as an anode for SOFCs. However, a small amount of Ru/CoO was introduced to improve the catalytic activity. For comparison, a SOFC with the same electrolyte and cathode was assembled with the Cu-free anode SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ used instead of the Cu doped anode. As shown in Fig. 4C,D, the highest power density at 700°C was 372 mW/cm$^2$ which was slightly lower than that for a SOFC with SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ anode. The total polaronic resistance was 0.30 Ω cm$^2$ at 700°C. The series resistance was 0.54 Ω cm$^2$ which is also slightly higher than that of the cell where the SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ anode was used (0.50 Ω cm$^2$) (Fig. 4B,D). This indicates that the high conductivity of SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ reduces both series and electrode polaronic resistances leading to high fuel cell performance. It should be noted that the exsolved Fe (or Fe-rich FeCu alloy) at the SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ anode may also improve the anode catalytic activity resulting in lower electrode polaronic resistances. The Arrhenius plot area-specific resistances (ASRs) for non-ohmic resistance of SrFe$_{0.8}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ and SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ anodes are shown in Figure S6. At 600°C, the ASR for the two oxide anodes are similar but the ASR for SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ is much lower at 650 and 700°C indicating better catalytic activity. Copper, copper alloy and iron alloy has been widely studied as excellent anode catalysts in SOFCs. In an early reported, it was found that FeCo alloy was exsolved from Pr$_{0.8}$Sr$_{0.2}$Co$_{0.8}$Fe$_{0.2}$Nb$_{0.2}$O$_{4-δ}$/CoFe alloy while excellent fuel cell performance has been achieved although the conductivity of this material was not presented.

Conclusions

In this work, a conductive perovskite oxide SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ has been identified which exhibits the highest conductivity in a reducing atmosphere for oxides which also exhibit a high conductivity in air. This high conductivity is probably related to the exsolution of Fe (or Fe-rich FeCu alloy) during the high temperature reduction process. After the reduction, besides the exsolved metal, the major phase is that of the perovskite. Good performance at intermediate temperatures in solid oxide fuel cells using the SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ based anode indicates that it is a promising anode for SOFCs. This study indicates that the conductivity of the oxides with exsolved metal is significantly high. This provides a strategy to identify a good material with high conductivity in both air and reducing atmospheres, i.e., starting from an oxide material with high conductivity in air, followed by introducing transition elements such as Fe, Co, Ni, Cu in the lattice which may be exsolved from the lattice on reduction therefore resulting in high conductivity in a reducing atmosphere.

Methods

Synthesis of oxides. SrFe$_{0.9}$Cu$_{0.1}$Nb$_{0.1}$O$_{3-δ}$ (x = 0–0.4) were synthesized by a sol–gel process, similar to previously reported processes. A stoichiometric amount of C$_2$H$_5$NNbO$_2$+xH$_2$O (99.9%, Sigma Aldrich) was dissolved in distilled water. H$_2$O was added to the niobium solution until a colour change was elicited. Citric acid (99%, Alfa Aesar), in a 2:1 molar ratio to the metal ions in the final product, was added and heated till a solution was formed. Stoichiometric amounts of Sr(NO$_3$)$_2$ (98%, Alfa Aesar), Fe(NO$_3$)$_3$·9H$_2$O (98%, Alfa Aesar) and Cu(NO$_3$)$_2$·2.5 H$_2$O (ACS grade, Alfa Aesar) were dissolved in distilled water. The solutions were mixed first then heated until gelation. The resultant gel formed was fired at 600°C for 2 hours and further fired at 1200–1300°C for 4–24 hours. The as-prepared powders were uniaxially pressed at 221 MPa in to pellets (ø 13 mm x 2 mm) and subsequently sintered in air at 1200°C–1450°C for 4–10 hours. The details are listed in Table S1.
Analytical Procedures. X-ray data was collected on a PANalyticalX’Pert Pro in the Bragg-Brentano
reflection geometry with a Ni-filtered Cu Kα source (1.5405 Å), fitted with a X'Celerator detector and an
Empyrean CuLFF xrd tube. Absolute scans in the 2θ range of 5–100° with step sizes of 0.0167° were used during
data collection. GSAS2 software was used to perform a least squares refinement of the lattice parameters of all
the samples.

Thermal analysis was conducted using a Stanton Redcroft STA 1500 Thermal Analyser on heating from room
temperature to 800 °C and on cooling from 800 °C to room temperature in air, with a heating/cooling rate of
10 °C/min, and in 5% H2/Ar, again with a heating/cooling rate of 10 °C min⁻¹, and with a flow rate of 5% H2/Ar
of 50 mL min⁻¹.

Scanning electron microscopy (SEM) measurements were carried out on a ZEISS SUPRA 55-VP Field
Emission Scanning Electron Microscope. The densities of the pellets were determined from the measured mass
and volume. Theoretical densities were calculated using experimental lattice parameters and the chemical for-
mula SrFe₀.9−ₓCuₓNb₀.1O₃−δ (x = 0–0.4). The relative density of the pellets was 80–90% for all compounds.

Conductivity Testing. The pellets (ø ≈ 13 mm × 2 mm) were coated on opposing sides using silver paste for
all samples. The conductivity of the samples was measured primarily in air between 300 °C to 700 °C. Secondary
measurements over the same temperature range were conducted in 5% H2/Ar following an equilibration step of
10 hours at 700 °C in 5% H2/Ar. Measurements were conducted using a pseudo four-terminal DC method using a
SolartronCell 1470E electrochemical interface controlled by CellTest software with an applied current of 1 - 0.1 A.

Fuel Cell Fabrication and Testing. The electrolyte support cell used in this study was prepared through a
tape casting process, with the outer two layers having pore formers. A dense YSZ powder with methyl ethyl ketone and ethanol, and along with binders (polypinvyl butyral and polyelelyene Glycol). Porous YSZ was prepared by adding YSZ powder with methyl ethyl ketone and ethanol, binders (polypinvyl butyral and polyelelyene Glycol) and graphite (UCP-2 grade, Alfa Aesar) sequentially. The resultant two slurries were tape-casted separately. The porous–dense–porous YSZ structure was prepared by laminating three green tapes, followed by sintering at 1500 °C for 4 h, after which the porosity was approximately 65%. The final thicknesses of the dense electrolyte and porous electrode were ~100μm and 45μm, respectively. The diameter of

Figure 4. Fuel cell performance. Current-voltage curves (A,C) and impedance spectra (B,D) of solid oxide
fuel cells with SrFe₀.8Cu₀.1Nb₀.1O₃−δ (A,B) and SrFe₀.9Nb₀.1O₃−δ (C,D) anode.
the porous YSZ region was 0.67 cm. To prepare composites of SFN-YSZ and SFCuN-YSZ electrolyte supported cell, the precursor solutions were firstly prepared by dissolving nitrate salts of Sr, Fe, Cu, and Nb in distilled water with the addition of quantitative amounts of citric acid. The SFCuN-YSZ anode was prepared by infiltrating the precursor aqueous solution into the anode side of the three-layered YSZ backbone. SFCuN was infiltrated into the porous YSZ backbone by a multi-step process followed by heating at 450 °C to decompose nitrates and citric acid. The infiltration process was repeated until 40 wt% loading of the oxide was achieved. Finally, SFCuN-YSZ anode wafers were calcined in air at 1000 °C. The LSF (La0.8Sr0.2FeO3−δ)–YSZ cathode was fabricated by infiltration using an aqueous solution of nitrate salts of La, Sr and Fe on a porous YSZ backbone opposite the anode layer. This was then calcined in air at 850 °C. 2 wt% Ru and 10 wt% ceria were also infiltrated into the anode and heated in air at 450 °C. For fuel cell performance tests, the cells were mounted on alumina tubes with ceramic adhesives (Ceramabond 525, Arcemco). Ag paste and Ag wire were used for the electrical connections to both the anode and the cathode. The entire cell was placed inside a furnace and heated to the desired temperature. V–I polarization curves were measured using a Potentiostat in the temperature range of 700–600 °C. The fuel cell performance was measured by a Solartron 1470e Electrochemical Interface coupled with a Solartron 1455 controlled by electrochemical software Solartron CellTest. The a.c. impedance was measured in the frequency range between 1 MHz and 0.01 Hz at the amplitude of the a.c. signal 20 mV.

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Author Contributions
S.T. conceptualized the study. R.L.P.I.C. and S.T. wrote the paper and all other authors provided feedback. P.I.C. synthesised the materials and measured the conductivity and performed XRD analyses. R.L. collect the SEM pictures and assisted XRD phase analyses. S.S. collected the fuel cell performance data.

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