Research Article

Research on the Effect of Metal Electrode Coupling Voltage under Induced Electrostatic Discharge

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In this paper, the mechanism of electrostatic discharge induced by a strong electromagnetic field was studied through software simulation and test verification. By focusing on the effect mechanism of coupling voltage between metal electrodes to induce electrostatic discharge, we obtained the law of electrostatic discharge induced by the strong electromagnetic field. In the process of electrostatic discharge induced by the strong electromagnetic field, due to the antenna receiving effect of metal electrode structure, the strong electromagnetic field would form coupling induction voltage on the metal electrode, which acts on both ends of the discharge electrode structure and generates an electric field in the gap between the electrode structure, which superimposes on the original field; furthermore, it has an impact on the electrostatic discharge process, resulting in the formation of induced discharge with low charging voltage structure.

1. Introduction

Electrostatic discharge in an electromagnetic environment of spacecraft is a complex process, which is related to the space environment, spacecraft structure, size, and material performance [1–3]. For space equipment, electrostatic discharge induced by the strong electromagnetic field refers to the process of electrostatic discharge induced in the low charge potential area of spacecraft surface materials, cables, and some special structural components under the action of the external strong electromagnetic field [4–9]. In general, the electric field in the sensitive area of low charge potential on the surface of spacecraft is weak [10–15], the electron energy is lower than the ionization energy of molecules and atoms [16–23], and the probability of collision ionization is low [24, 25]. When subjected to a strong electromagnetic field, the low-pressure gas is excited to produce dense plasma [24–27], to reduce the discharge threshold and induce electrostatic charge discharge [28, 29]. It is of great significance to master the influence and mechanism of the strong electromagnetic field on electrostatic discharge process [30] and to study the law of electrostatic discharge induced by the strong electromagnetic field in space equipment [31].

In this paper, the needle-ball electrode was taken as the research object, and an ultra-wideband electromagnetic pulse was used to build a strong electromagnetic environment. The simulation model of the needle-ball electrode strong electromagnetic field coupling voltage was established by using CST software. The coupling voltage and gap electric field distribution of different lengths and sizes of metal electrodes were calculated, and the influence law of the polarization direction of strong electromagnetic field, the amplitude of field strength, and the size of metal electrode on the coupling voltage were studied. The experiment system of ultra-wideband electromagnetic pulse induced discharge with a needle-ball electrode was developed to study the influence of electrode size, amplitude of ultra-wideband electromagnetic pulse field, and polarization direction on the threshold value of induced discharge. The influence of the coupling voltage of metal electrode on induced discharge was analyzed by comprehensive simulation, calculation, and test results.
2. Establishment of the Simulation Model

2.1 Simulated Test Model. As shown in Figure 1, the simulation software CST microwave studio was used for modeling. The detailed parameter settings are as follows: the needle electrode was perpendicular to the surface of the ball electrode, the needle direction coincided with the z-axis direction, the electrode material was PEC, and the space was filled with vacuum. When the diameter of the spherical electrode was 15 cm, the coupling voltage and spatial electric field distribution were simulated by changing the electrode length or electrode spacing.

2.2 Parameter Settings. Figure 2 displays the ultra-wideband electromagnetic pulse signal that we simulated for irradiation. The excitation signal was a plane wave, whose working frequency was set between 0 GHz – 1 GHz, and the center frequency was set at 0.5 GHz. The polarization direction was linear polarization, and the propagation direction of the electromagnetic wave signal was vertical or horizontal to the direction of the needle. Simulation calculation was carried out by changing the electric field intensity of the excitation signal or the polarization direction of the excitation signal.

2.3 Measurement Settings. We placed a voltage monitor between the needle and the ball electrode to measure the change of the induced voltage between the needle and the ball; we also placed 5 electric field probes between the needle and the ball electrode, from 0.5 mm to 2.5 mm to the needle tip, to monitor the change of the induced field strength in the discharge channel.

3. Analysis of Simulation Results

Without changing other conditions, a single variable was changed to carry out the simulation calculation, and then, the relationship between the induced electric field and the variable was analyzed.

3.1 Influence of Polarization Direction of the External Electric Field. Under other conditions, unchanged, the relative polarization direction of the excitation signal and the needle electrode was changed to study the relationship between the direction of induced voltage or field strength between the poles and the polarization direction of the applied excitation signal.

The simulation parameters are set as follows: the needle electrode length was 30 cm; the radius of the ball electrode was 15 cm; the distance between the poles was 3 mm; the needle electrode was arranged vertically; a load resistance of 10 ohm and capacitance of 500 pF was added between the electrodes; the electric field probe was placed 0.5 mm away from the tip of the needle in the gap channel; the applied electric field was vertically polarized, and then, its peak value was constantly changed to facilitate the study of the peak value and induced voltage of the applied electric field and gap induced electric field.

The relationship between the peak value of the induced voltage of the metal electrode and the peak value of the applied electric field is shown in Figure 9, while the relationship between the peak value of the induced electric field and the peak value of the applied electric field at 0.5 mm of the tip of the gap channel is shown in Figure 10. Figures 9 and 10 show us that the peak field strength of the induced voltage between the metal electrodes and the peak field strength of the induced electric field at 0.5 mm of the tip of the gap channel is directly proportional to the peak value of the applied electric field. It also can be seen from Figure 10 that the induced field intensity is one order of magnitude larger than the peak value of the applied electric field, which has a greater impact on the discharge process of the gap channel than the applied electric field.
3.3. Influence of Electrode Size. The simulation parameters were set as follows: the distance between electrodes was 3 mm; the needle electrode was placed vertically; the peak value of the applied electric field was 100 kV/m; the applied electric field was polarized vertically; first, when the diameter of metal ball was 15 cm, we adjusted the needle electrode length, which was set as 10 mm, 40 mm, 80 mm, 120 mm, 150 mm, 300 mm, 450 mm, 600 mm, 750 mm, and 900 mm, respectively, to study the relationship between the induced voltage and the needle electrode length; then, we changed the size of the metal ball and readjusting the length of the electrode, for analysing the effect of the size of the ball electrode on the induced voltage.

Figure 11 displays the relationship between the induced peak voltage and the needle electrode length under different ball diameters, and Figure 12 shows the relationship between the induced peak voltage and the size of the ball electrode for different needle electrode lengths.

Figure 13 reveals the relationship between the frequency corresponding to the induced peak electric field and the electrode length for different ball diameters. The simulation results show that when the electrode size was very small, the peak field strength of the induced electric field was one order of magnitude lower than that of the external radiation field. Therefore, the external radiation field played a major role in the electrostatic discharge induction process; when the electrode size was large, the peak field strength of the induced electric field was one order of magnitude higher than that of the external radiation field; consequently, the induction field strength of the metal electrode played a major role in the electrostatic discharge induction process. Figure 11 displays that when the diameter of the ball was fixed, in a certain range, the induced peak voltage increased with the increase of the length of the needle electrode, but when it exceeded over a certain range, the induced peak voltage did not change anymore, and the maximum induced peak value increased with the increase of the diameter of the ball. Figure 12 shows that when the needle
Figure 3: The time-domain waveform of induced voltage signal in horizontal polarization of applied electric field.

Figure 4: The peak distribution of electric field components in the direction of gap channel at different positions during horizontal polarization.

Figure 5: The time-domain waveform of induced voltage signal in vertical polarization of applied electric field.
electrode length was fixed, the induced peak voltage increased with the increase of the diameter of the spherical electrode in a certain range, but when it exceeded over a certain range, the induced peak voltage did not increase anymore either. However, the maximum value of the induced voltage varied with the length of the needle electrode. Figure 13 reveals that the frequency corresponding to the peak value of the induced electric field would decrease gradually with the increase of the electrode size. And this conforms to the principle that the half-wave antenna has the strongest ability to receive electromagnetic waves.

3.4. Effect of Gap Size. The simulation parameters were set as follows: the length of needle electrode was 300 mm, the diameter of ball electrode was 15 cm, and the applied electric field was 100 kV/m. The direction of electric field was vertical polarization, and the electric field probe was placed at 0.5 mm from the gap channel to the needle tip. The distance between electrodes was adjusted to 1 mm, 2 mm, 3 mm, 6 mm, 12 mm, and 24 mm, respectively, to study the influence of gap size on the induced voltage and the induced electric field. The direction of the electric field is vertical polarization. The direction of the electric field was vertical polarization.

The relationship between the peak value of induced voltage and the peak value of induced electric field and the size of electrode gap distance is shown in Figures 14 and 15. It could be seen from Figure 14 that with the increase of electrode gap distance, the peak value of induced voltage would gradually increase, but the increment was relatively

Figure 6: The peak distribution of electric field components in different positions in the direction of gap channel, when the electric field was vertically polarized.

Figure 7: The distribution of induction field strength of needle ball electrode.
Figure 8: The relationship between the peak value of the induced electric field and the distance to the tip of the needle.

Figure 9: The relationship between induced peak voltage and peak value of applied electric field.

Figure 10: The relationship between peak field strength of induced electric field and peak value of applied electric field.
small. It could also be found out from Figure 15 that with the increase of the gap, when the electrode gap was 2 mm, the maximum induction field strength was 0.5 mm from the tip of the needle electrode; with the increase or decrease of the gap, the induction field strength would rapidly drop; however, when the gap distance exceeded over 5 mm, the peak value of the induction field at the needle electrode tip would gradually rose with the increase of the gap, which was caused by the gradual increase of the induction voltage.

4. Test Verification

To verify the effect of the metal-electrode coupling voltage on the induced electrostatic discharge, in this project, we have taken ultra-wideband electromagnetic pulse as the radiation source and needle ball electrode as the research object, and then, tested and verified the simulation results. The verification test consisted of two parts: one part was the verification test of induced voltage coupling law of the needle ball electrode under the action of the external radiation field; the other part was the verification of induced threshold law of different length electrode under the action of the external radiation field. Through the analysis of the test results, we obtained the law of the effect of the polarization direction of the electromagnetic field and the length of the electrode on the induced electrostatic discharge, to verify the correctness of the simulation conclusion of the influence of the coupling voltage of the metal electrode in the process of the induced electrostatic discharge.

In the test, the test parameters were set as follows: the needle discharge gap was set as 3 mm; the discharge needle length was set as 900 mm, 750 mm, 600 mm, 450 mm, 300 mm, 150 mm, or 100 mm, respectively; the needle electrode voltage was supplied by a GLOW28720 DC high-voltage source; the GW level UWB electromagnetic pulse radiation source was selected as the ultra-wide charged magnetic pulse source, which could provide the maximum vertical polarized electromagnetic pulse field of 80 kV/m; the induced current voltage and induced discharge current were collected by using a Tektronix TDS7404B oscilloscope through voltage and current probe (Tektronix RMS CAT, 5 mA/mV). During the test, the temperature was 26.9 ± 0.5°C; the humidity was 63.6%; the air pressure was 1 standard atmospheric pressure.
4.1. Measurement and Result Analysis of Induced Voltage of the Metal Electrode. As shown in the schematic diagram of the metal electrode induced voltage test in Figure 16, a high voltage probe was used for the induced voltage test. During the test, the test connecting wire should be shielded. At the moment of electromagnetic pulse irradiation, there would generate an induced coupling voltage of the transient electric field between the needle and the ball electrode, and it would be measured and recorded by the voltage probe and oscilloscope. Each group of experiments was repeated 5 times to ensure the repeatability and accuracy of the test data.

During the experiment, the metal needle electrode was placed in the horizontal direction or the vertical direction, respectively. Under the irradiation of ultra-wideband electromagnetic pulse, the induced voltage of different length metal electrodes was measured. The waveform fields shown in Figure 17 are, respectively, the coupling voltage of the test cable under GW level ultra-wideband electromagnetic pulse irradiation, with 100 mm, 600 mm, or 900 mm metal electrodes placed horizontally, or without metal electrodes. It can be seen from Figure 17 that the length of the discharge needle placed in the horizontal direction had little effect on the value of the induced voltage, and it was similar to the induced voltage on the test cable when no metal electrode is added. This was because the ultra-wideband was a vertically polarized electromagnetic wave, and its component in the horizontal direction was very small, so the value of the induced voltage in the horizontal direction did not change because of the length of the needle change.

Figure 18 shows the coupling voltage waveform between the metal electrodes of different lengths and the test cable without the metal electrode, under the irradiation of ultra-wideband electromagnetic pulse.
wide band electromagnetic pulse, when the metal electrode was placed vertically, that is, when the direction of the electrode was consistent with the polarization direction of the external ultra-wideband electromagnetic pulse.

It can be seen from Figure 18 that the induced voltage value of the needle with the length of less than 300 mm has no change. At the same time, compared with Figure 18(h), it is found that the induced voltage on the test cable without the metal electrode is greater than the induced voltage with the needle length of less than 300 mm, and the test cable has a great impact on the verification of the coupling voltage rule. According to the analysis of the induced voltage test data of the 450 mm–900 mm discharge needle, the induced voltage value is also increasing with the increasing of the length of the discharge needle. The relationship between the induced voltage and the length of different discharge needles is shown in Figure 19.

By comparing the induced voltage waveform of the discharge needle length of 900 mm in Figures 18 and 19, it can be seen that when the direction of the needle ball electrode was consistent with the polarization direction of the external ultra-wideband electromagnetic pulse, the induced voltage was greater than that when they were vertical. Therefore, the coupling voltage of the metal electrode had a great relationship with the polarization direction of the external electromagnetic field. When the direction of the metal electrode was the same as that of the external electromagnetic field, the induced discharge process of the electrode would be affected by the external electromagnetic field. When the direction of the metal electrode was perpendicular to the polarization direction of the external electromagnetic field, the influence of the metal electrode’s coupling voltage on the discharge process induced by the electromagnetic field could be ignored, which is consistent with the simulation results.

4.2. Measurement and Analysis of Induced Threshold of Different Lengths of Metal Electrodes. To further verify the influence of the different lengths of electrodes on the threshold of discharge induced by electromagnetic field, this project carried out the experimental research of the different lengths of electrodes induced discharge. The principle diagram of the induced discharge threshold test is shown in Figure 20, and the test site is shown in Figure 21. In this experiment, firstly, we had to find out the threshold value of spark...
Figure 17: Induced voltage of discharge needle with different length in horizontal direction. (a) 100 mm. (b) 600 mm. (c) 900 mm. (d) Without metal electrode.

Figure 18: Continued.
breakdown under the condition of DC voltage. Then, we figured out the threshold value of spark breakdown under the effect of external radiation field. And at last, we analyzed the relationship between the threshold value of spark breakdown induced under external radiation field and external field strength, electrode length by comparing the two.

During the test, we set the needle electrode in the same direction as the applied electric field. Without external electric field radiation, the threshold voltage of continuous spark breakdown was 4.9 kV. When the electrode could be induced to 100% electric breakdown under the effect of the external field irradiation, the voltage between the electrodes was taken as the threshold value of the induced discharge. When the electrode length was less than 300 mm, the uncertainty of the induced discharge threshold was larger than others. As shown in Table 1, we mainly list the test data with an electrode length of 300–900 mm. The relationship between induced discharge threshold and electrode length is shown in Figure 22.

It can be seen from Table 1 and Figure 22 that the threshold value of induced discharge between the same discharge electrodes would decrease gradually with the increase of the peak electric field under the irradiation of UWB electromagnetic pulse with different peak electric fields. And the threshold value would decrease gradually with the increase of the electrode length under the action of UWB with the same peak electric field. According to the test results of coupling voltage of the metal electrode, the longer the length of metal electrode is, the greater the coupling voltage is, the greater contribution it will make to the induced discharge process, and finally, it will reduce the threshold value of induced discharge, which verifies the correctness of the simulation results in this article.
Figure 20: The principle diagram of induced discharge threshold characteristic test.

Figure 21: The test connection diagram.

Table 1: The induced threshold of different discharge needle lengths when electrode spacing was 3 mm.

| The length of needle electrode (mm) | 87 (kV/m) | 72 (kV/m) | 65 (kV/m) | 53 (kV/m) |
|------------------------------------|-----------|-----------|-----------|-----------|
| 900                                | 4.0       | 4.1       | 4.4       | 4.5       |
| 750                                | 4.2       | 4.25      | 4.5       | 4.55      |
| 600                                | 4.3       | 4.4       | 4.58      | 4.6       |
| 450                                | 4.4       | 4.6       | 4.66      | 4.7       |
| 300                                | 4.5       | 4.7       | 4.72      | 4.8       |

The threshold without external field discharge is 4.9 kV.
Induced discharge threshold (kV)

Electric field intensity 87kV/m
Electric field intensity 72kV/m
Electric field intensity 65kV/m
Electric field intensity 53kV/m

The length of needle electrode (mm)

Figure 22: The relationship between induced discharge threshold and needle length.

5. Conclusions

The simulations’ result shows that when the direction of the applied electric field was perpendicular to the metal needle electrode, the coupling voltage and the electric field in the gap of the metal needle electrode were very small, and the influence on the electrostatic discharge induction process could be ignored. When the direction of the applied electric field was parallel to the needle electrode, the peak value of the electric field formed at the gap was one order of magnitude larger than the amplitude of the applied electric field, and the peak field strength of the induced voltage and the peak field strength of the gap channel was directly proportional to the peak value of the applied electric field.

When the electrode size was small, the peak field strength of the induced electric field was one order of magnitude lower than that of the external radiation field, so that the external radiation field played a major role in the electrostatic discharge induction process. However, when the electrode size was large, the peak field strength of the induced electric field was one order of magnitude higher than that of the external radiation field; therefore, the induced field of the metal electrode played a major role in the electrostatic discharge induction process.

When the diameter of the needle ball electrode’s ball was fixed, the peak of induction voltage increased with the increase of the length of the needle electrode in a certain range. However, when beyond the certain range, the peak of induced voltage did not change anymore, and the maximum peak of induction voltage increased with the increase of the diameter of the ball. When the needle electrode’s length was fixed, the peak of induction voltage increased with the increase of the diameter of the spherical electrode in a certain range; but when it exceeded over the certain range, the peak induction voltage did not change anymore either, and the maximum induced voltage varied with the length of the needle electrode. With the increase of the electrode size, the frequency corresponding to the peak of induction field would gradually decrease. And this is in accordance with the law that half-wave antenna has the strongest ability to receive electromagnetic waves.

It could be also seen from the verification test that the coupling voltage of the metal electrode had a great relationship with the polarization direction of the external electromagnetic field. When the direction of the metal electrode was parallel to the polarization direction of the external electromagnetic field, it would affect the electromagnetic field-induced discharge process. When the direction of the metal electrode was perpendicular to the polarization direction of the external electromagnetic field, the influence of metal coupling voltage on the process of electromagnetic field-induced discharge could be ignored, which was consistent with the simulation results.

For the same discharge electrode, the threshold value of induced discharge decreased with the increase of the peak value of the electric field under the irradiation of different peak electric fields of ultra-wideband electromagnetic pulse and decreased with the increase of electrode length under the action of ultra-wideband of the same peak electric field. According to the test results of coupling voltage of metal electrode, the longer the length of the metal electrode was, the greater the coupling voltage was; the greater the contribution of the metal electrode to the induced discharge process was, and the threshold value of induced discharge was reduced, which verifies the correctness of the simulation results.

Data Availability

The data used to support this study are obtained from the company’s internal business secrets. Data sharing can only be carried out after the patent period of the company has expired.

Conflicts of Interest

The authors declare that they have no conflicts of interest.

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