Assessing the effect of soil parameterization in land use change impact modeling

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Abstract. This study addresses the importance of integrating the effect of land use on soil infiltration rate into land use change impact modeling. Based on a validated version 9.05.04 of the Water balance Simulation Model-WaSiM (statistical quality measures > 0.7), and field measurement of the infiltration rate under cropland and fallow, sixteen model simulations were performed. The impact of land use change is computed comparing LULC status of years 1990 and 2013. The effect of soil parameterization is computed using a refined soil map integrating land use change impact of soil infiltration rate and a classic soil map not considering this interaction. The results show differences in model results as an effect of soil parameterization approaches, indicating that the model is sensitive to the integration of LULC related effects on soil hydraulic conductivity. These differences are more pronounced with increasing modeling time steps (24 and 28 h). The signal-to-noise-ratio indicates that, results achieved in LULC impact assessment with a classic and a refined soil parameterization are very comparable except for interflow.

1 Introduction

Land use change impact is a major research topic in hydrology (Wagner et al., 2017). By affecting the partitioning of precipitation and influencing many hydrological process, land use and land cover (LULC) changes strongly affect the quality and quantity of water resources (Aghsaei et al., 2020). However, quantifying the net effect of LULC change impact on water resources remains challenging, as this effect is multifactorial (Yira et al., 2016), and includes a modeling approach component (Beven, 2012). Besides the modeling objective, a modeling approach often heavily relies on data availability.

Field evidences, by Yira and Bossa (2019), of land use impacts on soil infiltration rate provide the opportunity to assess the importance of considering land use dependent soil properties in the hydrological impact assessment of LULC change on water resources in the Dano catchment. A modeling exercise incorporating knowledge gained from field investigations with regards to land use impacts on soil infiltration rate may require additional parameterization effort, but the method has proven to improve hydrological processes representation (Hölzel and Diekkrüger, 2010).
The current study addresses the importance of integrating the influence of land use on soil infiltration rate into land use change impact assessment. It aims to analyze how soil parameterization and modeling time step could affect the results in land use change impact assessment. It has the following specific objectives: (i) assess the sensitivity of the hydrological simulation model to land use effect on soil infiltration rate, (ii) assess the consequences of integrating land use effect on soil infiltration rate in LULC impact assessment, and (iii) to evaluate whether the importance of integrating land use related effect on soil infiltration rate in the modeling exercise depend on the modeling time step.

2 Materials and methods

2.1 Study area

The study was carried out in the Dano catchment (Fig. 1). The catchment is located in the Sudanese climate zone of Burkina Faso and covers an area of 195 km². It is characterized by an alternation of two seasons including a dry season of 6 to 7 months (November to April) and a rainy season of 5 months spanning from May to October (Yira et al., 2016). The natural vegetation of the catchment is of Sudanian region. Average monthly temperatures and annual rainfall range between 24 and 32 °C, and 800 to 1200 mm yr⁻¹, respectively (Yira et al., 2016).

2.2 Land use change

The land use and land cover maps after Forkour (2014) and Landmann et al. (2007) corresponding to LULC status for the years 2013 and 1990 respectively, were used for LULC change impact assessment (Table 1). The reclassified version of both maps (Yira et al., 2016) was used, and the year 1990 was considered as baseline.

2.3 Infiltration measurement

A hood infiltrometer (Schwärzel and Punzel, 2007) was used to perform infiltration ($K_s$) tests on adjacent croplands and fallow areas. Measurements showed on average (1.16-fold) higher $K_s$ under fallow compared to cropland (Yira and Bossa, 2019).

2.4 Soil map refinement

Soil infiltration rate is parameterized in WaSiM through the soil map and soil classes’ characteristics, while no infiltration rate dependent parameter is associated with this parameterization. Following the infiltration test, the Eq. (1) by Hözel and Diekkrüger (2010) was adopted to integrate land use influence on $K_s$ into the soil parameterisation.

$$K_{s_{ref}} = K_{s_{map}} \cdot \frac{\hat{K}_{meas}}{K_{s_{meas}}}$$

where $\hat{K}_{s}$ is the mean of the infiltration rate, $x$ refers to all samples, $x_i$ is the samples of the specific area (cropland or savannah), “ref” refers the refined values, “meas” refers to measured values, and “map” indicates the initial values given by the classic soil map.

The reference basis for $K_s$ was provided by the $K_s$ values from the classic soil map (CS), which were derived from laboratory measurements for each soil type and different soil horizons following Saxton and Rawls (2006).

2.5 Modeling approach and simulation experiment

Version 9.05.04 of WaSiM, after Yira et al. (2016) and Schulla (2015), calibrated and validated (Fig. 2) at a daily time step using a classic soil parameterization and the LULC map of 2013 was the starting point of the study.

Table 1. Percentage of the catchment area per land use class in 1990 and 2013.

| Land use class | 1990 | 2013 |
|---------------|------|------|
| Cropland (%)  | 11.6 | 38   |
| Savannah (%)  | 87   | 58   |
| Water (%)     | 0.05 | 0.05 |
| Urban area (%)| 1    | 3    |
Figure 2. Daily observed and simulated discharges for the calibration (2013) and validation (2014) years at the outlet of the Dano catchment.

Table 2. Combined land use scenarios, soil parameterizations and time scales experiments.

| Classic soil (CS) | Refined soil (RS) |
|------------------|-------------------|

| Land use status 2013 (LU2013) | CS_LU2013_8h | CS_LU2013_12h | CS_LU2013_24h | CS_LU2013_48h |
|------------------------------|--------------|---------------|---------------|---------------|
| Refined soil (RS)            | RS_LU2013_8h | RS_LU2013_12h | RS_LU2013_24h | RS_LU2013_48h |

| Land use status 1990 (LU1990) | CS_LU1990_8h | CS_LU1990_12h | CS_LU1990_24h | CS_LU1990_48h |
|------------------------------|--------------|---------------|---------------|---------------|
| Refined soil (RS)            | RS_LU1990_8h | RS_LU1990_12h | RS_LU1990_24h | RS_LU1990_48h |

Step on this interaction (8, 12, 24, and 48 h time steps). Overall, 16 model configurations were set up combining these two factors and LULC status (Table 2). The fitted calibrated parameters of the initial model (Yira et al., 2016) were kept constant for all the simulations experiments.

2.6 Comparison of land use and soil parameterization effects

The “signal-to-noise-ratio” (SNR) (Bormann et al., 2009) was adapted to compare LULC change impacts with soil parameterizations effects (Eq. 2). In this study, the “noise” is represented by soil parameterization effect, and “signal” is represented by land use change impact. Positive SNR values indicate that land use change impacts are larger than soil parameterization effects and Negative SNR values imply the opposite.

\[
SNR = \left( \frac{|X_{CS,LU1990} - X_{CS,LU2013}|}{|X_{CS,LU1990} - X_{RS,LU1990}|} \right) - 1
\] (2)

where SNR is the “signal-to-noise-ratio”, X is the simulated variable (discharge, ETa, etc.).

3 Results and discussion

3.1 Modeling time step and model performance

The initial model, calibrated and validated at a daily time step using a classic soil parameterization and the LULC of 2013 (CS_LULC2013_24h), and the other seven model setups using the same LULC map but different soil parameterizations and time steps (see Table 2) are compared to the observed discharge in order to relate change in model performance to soil parameterization and time step (Fig. 3). The annual variation of discharge appears well reproduced by each model setup, although difference in simulated peak discharges can be noticed.

Soil refinement appears beneficial to all simulations performed at 8, 12 and 48 h time steps irrespective of the considered model statistical quality measure; this may suggest that refined \(K_s\) is more effective than classic \(K_s\). However, at the 24 h time step, classic soil (CS) outscores refined soil (RS) for Pearson product-moment-correlation-coefficient.

3.2 Modeling time step and water balance

Time step effects on water balance components are shown in Fig. 4. Change in water balance components with increasing modeling time step comparing land use status of 2013 and 1990 are very similar: (i) an increase of actual evapotranspiration, (ii) a decrease in total discharge, (iii) a decrease in surface runoff, (iv) an increase in baseflow, (v) a decrease in interception, and (vi) an increase followed by a decrease for interflow.

The comparison of RS and CS histograms for the same time step shows the effect of soil parameterization on dis-
Figure 3. Model performance using different modeling time steps and soil parameterization approaches. Period of January 2013 to December 2014. Performance is calculated using mean monthly discharges.

Furthermore, the difference in surface runoff between RS and CS decreases with the modeling time step. Simulated change in total discharge, baseflow and interflow following LULC change are lower with the refined soil compared to the classic soil.

It can be noted from Fig. 5c that irrespective of modeling time step, a LULC change impact assessments performed with a RS and CS parameterization do not yield the same water balance. Differences range from 0.2 to 18 mm yr\(^{-1}\) depending on water balance components. Figure 5 further indicates that simulated changes in water balance due to LULC change are larger than the change due to soil parameterization, suggesting that soil refinement might have a marginal impact in LULC impact assessment.

The SNR is calculated to test whether the LULC change effect (Table 3) is significantly larger than the soil refinement effect. Table 3 shows both positive and negative SNR. Except interflow, all water balance components show positive SNR, indicating that LULC change impact is larger than soil refinement, meaning the noise created by soil refinement does not affect LULC change signal. In other words, results achieved in LULC impact assessment with both soil parameterizations (CS and RS) are very comparable except for interflow. Noise is larger than signal only for simulations performed at 24 and 48 h, even though this noise is low. Therefore, for a LULC impact assessment focusing on discharge components it is necessary to use a refined soil as omitting this information produced an effect higher than LULC change effect. However, LULC change impact appears larger than soil refinement effect for the water balance, as confirmed by positive SNR indices. It is noteworthy that for interflow, soil refinement effect was larger than the LULC change impact for some modeling time steps, implying that a consistent assessment of LULC change impact on interflow (and consequently, on discharge components) should integrate LULC related effects into soil properties.
**Figure 4.** Annual water balance components for different modeling time steps and soil parameterization approaches for the period of January 2013 to December 2014.
Figure 5. Change in water balance as a result of LULC change, modeling time step and soil parameterization. Part (a) compares LULC1990 to LULC2013 using a classic soil-CS, part (b) compares LULC1990 to LULC2013 using a refined soil-RS, and (c) shows the difference between soil parametrization approaches (a, b).

Table 3. Signal-to-noise ratio for different modeling time steps. Signal refers to LULC change effect, and noise is soil refinement effect.

| Modeling time step (h) | Signal | Total discharge | Surface runoff | Interflow | Baseflow |
|-----------------------|--------|-----------------|----------------|-----------|----------|
| 8                     | 22.91  | 39.83           | 5.94           | 0.82      | 9.61     |
| 12                    | 69.76  | 9.35            | 27.51          | 0.42      | 6.20     |
| 24                    | 17.18  | 0.20            | 0.07           | -0.52     | 2.63     |
| 48                    | 8.13   | 0.81            | 1.34           | -0.58     | 2.86     |

4 Conclusion

In this study, land use change related effects on soil infiltration rate was integrated in the modeling of LULC change impact on the Dano catchment hydrology. Previous field investigation showed that soil surface hydraulic conductivity was significantly affected by land use. This additional information was integrated in the modeling as refined soil, and was compared to a simulation ignoring this information. Modelling time step was further considered as a potential factor affecting the model outputs. Several models were then set up combining soil parameterization, modeling time step, and LULC change.

The results show that trends in water balance and discharge components following LULC change was similar for classic and refined soil parameterization irrespective of the modeling time step. However, differences in model results could be observed between soil parameterization approaches, indicating that the model is sensitive to the integration of LULC related effects on soil hydraulic conductivity. This supports the idea that integrated land use related effects on soil properties renders LULC change scenarios more plausible.

Code availability. WaSIM code is not publicly accessible. The applied Richards version of the software is available for download at http://www.wasim.ch/en/products/wasim_richards.htm (last access: 7 October 2021) (WaSiM-ETH, 2021).
Data availability. The applied data are available on the WASCAL Geoportal (https://wascal-dataportal.org/geonetwork/apps/search?east_collapsed=true&s_search=&s_timeType=true&s_scaleOn=false&s_E_hitsperpage=20, last access: 7 October 2021) (WASCAL Geoportal, 2021).

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