Mass conversion pathway during anaerobic digestion of wheat straw

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A material flow analysis (MFA) method was employed to investigate elemental flow direction during the anaerobic digestion (AD) of wheat straw (WS) pretreated with potassium hydroxide. A lab-scale batch AD experiment conducted at 35 ± 1 °C was investigated to realize carbon conversion in biogas, liquid and solid digestates. The results showed that the highest growth rate of carbon conversion in biogas was observed from the fourth day to the twenty-fourth day, which accounted for 70.64%. The cumulative biogas production of WS was 531 mL g−1 VS, along with a high volatile solids degradation rate (55.0%). The MFA results indicated that the flow mass fractions of carbon in biogas, liquid and solid digestates were 49.96%, 5.61% and 44.43%, respectively. The flow mass fraction of nitrogen in liquid and solid digestates was 45.65% and 54.35%, respectively. This study can provide a theoretical basis for elemental flow in each product from biogas projects.

1. Introduction

According to the United Nations Food and Agriculture Organization, the world wheat and wheat straw (WS) productions in 2018 were nearly 3.4 and 4.5 billion tons, respectively.1 The WS is rich in organic carbon, which could be utilized as an important raw material for the production of clean energy, rather than being discarded as waste.2 Anaerobic digestion (AD) is a mature and environmentally friendly organic waste treatment technology that plays a vital role in the harmless reduction of industrial wastewater and agricultural solid waste treatment.3 AD technology can convert agricultural solid waste materials such as WS into biogas, which is a clean energy source used to generate electricity without secondary pollution.4 To some extent, it has alleviated environmental pollution caused by the use of fossil fuels.5

The AD biochemical reactions of WS are the process of converting insoluble macromolecules into soluble small organic molecules, which in turn are converted to methane and carbon dioxide.6 Cellulose is hydrolyzed to glucose by extracellular enzymes, and cellubiose is an intermediate product. Hemicellulose is converted to galactose, mannose, arabinose, xylose and glucose by extracellular enzyme hydrolysis. These small molecular mass substances are firstly converted into volatile fatty acids by the action of fermenting bacteria, and then enter the acidification stage.7

Previous researchers have focused on the metabolism and transformation of determining the substances in the AD process. This is a matter of material conversion process by calculating the changes in the total solids (TS), volatile solids (VS) and lignocellulosic components before and after AD. For example, Liu et al. found that TS and VS bioconversion rates for the NaOH-pretreated group, respectively, with 1.0, 0.4, and 0.4 mg L−1 d of elements Fe, Co, and Ni group were 14–53% higher than the untreated group.8 Korai et al. found that the highest biogas production (570 mL g−1 VS) and hemicellulose reduction rate (9.6%) of WS was obtained by KOH and ultrasonic pretreatment.9

However, the flow distribution of materials and the mass conversion at the elemental level during the AD process of WS have not been clearly explained. The material flow analysis (MFA) is an overall method that allows the study of inflow and outflow of substances in a system.10 The main objective of MFA is to get the mass balance for the system, therefore, the sum of all system inputs and outputs must be equal.11 MFA can be used to estimate the generation of gas, liquid and solid materials from nine types of typical AD processes. For example, 30.8% of carbon in rice hull was converted into biogas during the anaerobic fermenting process, while 6.4% and 62.9% was left in liquid and solid digestate forms, respectively.12 Zhen et al. used the MFA method to analyze the flow direction of carbon and nitrogen elements in the AD process of hybrid wolf tail. They found that 33.1% and 8.0% of carbon in the raw material entered into biogas and liquid digestate forms, respectively, while 58.9% remained in the raw material. Regarding the
distribution of nitrogen, 69.4% was converted into liquid digestate, and 30.7% remained in the raw material.\textsuperscript{13}

In this study, MFA was used to analyze the process of using WS to produce biogas via mid-temperature batch AD. The flow distribution of materials, carbon and nitrogen were presented and discussed.

2. Methods and materials

2.1. Wheat straw and inoculum

The WS used in this study was obtained from the Daxing district of Beijing. It was naturally dried in open air and stored in a sheltered area between periods of use. To reduce its size and increase its surface area, the dried WS was shredded by a paper chopper (PC500, Staida Co., Tianjing, China) and then ground into the size of 20 meshes using a universal pulverizer (YSW-180, Yanshan Zhengde Co., Beijing, China). The raw WS had the original cellulose (43.52%), hemicellulose (24.87%), lignin content (10.21%), carbon (44.74%) and nitrogen percentage (0.52%) (Table 1).

The inoculum was collected from a biogas plant in Shunyi district of Beijing, which using pig manure and WS as the raw material. The biogas plant achieves continuously stable operation under mesophilic condition at 35 °C. The collected inoculum was initially concentrated by settling it for 48 h, then screened by a 1 mm sieve to prevent clogging problems and to remove impurities such as pig hair and twig before seeding in a reactor. The characteristics of WS and inoculum are listed in Table 1.

2.2. Pretreatment process

To enhance biodegradability and improve biogas production, potassium hydroxide (KOH) was used as a pretreatment reagent. Before being fed to reactors, the WS was pretreated for three days at an ambient temperature (25 ± 2 °C), based on a dry weight ratio of WS : KOH : H_2O = 1 : 0.04 : 6 (w/w/w).\textsuperscript{14}

2.3. Batch anaerobic digestion

Batch AD experiments were performed in 30 glass media bottles as the batch reactors, which were placed in mesophilic conditions (35 ± 1 °C). The total volume of each reactor was 1 L with a working volume of 0.8 L. An organic loading of 65 g TS per L pretreated WS was applied. The anaerobic inoculum seeded in each reactor was 20 g (mixed liquid suspended solid, MLSS) per L. The carbon-to-nitrogen ratio (C/N) and the pH value in each reactor were adjusted to the optimum level at the beginning of the anaerobic digestion process. The appropriate amount of urea was added to each bottle in order to adjust the C/N ratio to 25, which is believed to be optimal ratio for anaerobic bacterial growth and the pH value was adjusted to 7.0 ± 0.1 using calcium hydroxide solution.\textsuperscript{15}

The prepared reactors were carefully placed in a water bath incubated at mesophilic temperature (35 ± 1 °C) for 45 days to conduct the AD tests. Nitrogen gas was used to remove any oxygen residues from the bottles and all bottles were then capped and sealed to ensure the anaerobic conditions were produced.\textsuperscript{16}

All experiments were performed in triplicate, with the mean values used for reporting. Moreover, a blank AD was carried out, in which only the seeding sludge was added to know the background methane production as well as the carbon and nitrogen conversion changes.

The liquid digestate samples were periodically collected from the digesters every three days during AD process. They are denoted as R3, R6, R9, R12, R15, R18, R21, R24, R27, R30, R33, R36, R39, R42 and R45. Therefore, destructive sampling was taken from the digesters every three days during AD process. They are denoted as R3, R6, R9, R12, R15, R18, R21, R24, R27, R30, R33, R36, R39, R42 and R45. Therefore, destructive sampling was used, where the batch reactors were discarded after the samples were taken. Identical data analysis conducted for each sample: the TS, VS, total carbon (TC) and total nitrogen (TN) of every sample were measured.\textsuperscript{17} Lignin, cellulose, and hemicellulose contents were determined using an automatic fiber analyzer.\textsuperscript{18}

2.4. Analytic methods and data analysis

2.4.1 Analysis of biogas component. The daily biogas production (DBP) from each digester was recorded simultaneously using the water displacement method. The volume of biogas was converted to standard temperature (273.15 K) and pressure (101.325 kPa). Methane, carbon dioxide, nitrogen and hydrogen contents were measured by a gas chromatography (BeiFenRuiLi SP-2100, Beijing, China), which was equipped with a molecular sieve (TDX-01), packed with 2 m × 3 mm stainless-steel column and using a thermal conductivity detector (TCD). The temperature of oven, injector port, and TCD were 140, 150, and 150 °C, respectively. Argon was used as the carrier gas in the gas chromatograph, where its flow rate was 30 mL min\textsuperscript{-1}. The daily carbon dioxide and methane contents were calculated on the basis of the biogas composition. Subsequently, the corresponding cumulative methane, carbon dioxide and biogas production were calculated.

2.4.2 Chemical composition analysis. TC and TN were determined using Vario EL/micro cube elemental analyzer (Elementar, Germany). The pH value was tested by pH meter (3-Star, Thermo Scientific Orion, U.S.A.). The samples for volatile

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**Table 1** Characteristics of wheat straw and inoculum\textsuperscript{a}

| Parameter                | Value (%) | 
|--------------------------|-----------|
|                          | Wheat     | Inoculum |
| Total solids (TS, %)     | 96.63 ± 0.02 | 14.14 ± 0.04 |
| Volatile solids (VS, %)  | 82.34 ± 0.03 | 7.34 ± 0.02 |
| MLSS (g L\textsuperscript{-1}) | ND | 105.84 ± 1.28 |
| Total carbon (C, %)      | 44.74 ± 0.03 | 29.83 ± 0.04 |
| Total nitrogen (N, %)    | 0.52 ± 0.03 | 3.14 ± 0.02 |
| Total hydrogen (H, %)    | 5.61 ± 0.01 | 3.62 ± 0.01 |
| Total sulphur (S, %)     | 0.05 ± 0.02 | 0.70 ± 0.12 |
| VS/TS                    | 0.85     | 0.52     |
| Cellulose                | 43.52     | —        |
| Hemicellulose            | 24.87     | —        |
| Lignin                   | 10.21     | —        |
| C/N                      | 86.04 ± 2.56 | 9.5 ± 0.01 |

\textsuperscript{a} Values are means ± SD (n = 3); ND: not determined; MLSS: mixed liquid suspended solids.
fatty acids (VFAs) and ethanol were first centrifuged at 10 000 rpm for 5 min, the supernatants were then filtered through a filter with 0.22 mm diameter pore size, and the filtrates were collected in sample vials for analyses. The VFAs yields were calculated as the sum of the measured acetic (HAc), propionic (HPr), n-butyric (n-HBu), iso-butyric (iso-HBu), n-valeric (n-HVa) and isovaleric (iso-HVa) acids. The content of each VFA was determined using gas chromatography (GC2014, Shimadzu, Japan) equipped with a flame ionization detector and a DB-WAX123-7032 capillary column. Nitrogen was used as the carrier gas. The operational temperatures of the injector and detector were maintained at 250 ℃, while the temperature of column was increased from 100 to 180 ℃ at a rate of 5 ℃ min⁻¹.

2.4.3 Material flow analysis. The MFA is a tool to quantify the flows of materials in a complex systems.¹⁹

The MFA method used in this study was to estimate the generation of materials from gas, liquid and solid phases of AD processes. The conversion efficiency of carbon and nitrogen in the AD process of WS was studied by the methods of MFA. MFA analysis software (STAN 2.5) was applied to establish the MFA model, and the graphical rendering of MFA results were prepared using the E! Sankey 4.5 flow chart designer.

2.4.4 Data analyses. The ambient temperature throughout the AD process is assumed to 25 ℃ and it is kept constant for the volume of biogas during MFA. The mass of each biogas component in the AD process can be calculated by the actual gas state equation (van der Waals equation) as shown in eqn (1):²⁰

\[ \left( P + \frac{n^2}{V^2} \right) (V - nb) = nRT \]  

where \( P \) is the pressure of the gas; \( V \), the volume of the gas; \( n \), the amount of gas substance; \( R \), the ideal gas constant; \( T \), the temperature of the gas; further, \( a \) is related to the attraction between molecules; and \( b \) to the volume of molecules.

Eqn (2) was used to calculate the carbon content of each component in the total VFA concentration, so as to obtain the carbon content in the liquid digestate in different stages of the AD system.

\[ Y_{MC} = \frac{2 \times M_C}{2 \times M_C + M_O + M_H} \times 100\% \]  

where \( Y_{MC} \) is the carbon fraction of an individual acid in the VFA; \( M_C \) represents the mass of carbon; \( M_O \) represents the mass of oxygen; and \( M_H \) represent the mass of hydrogen in the VFAs.

3. Results and discussion

3.1. Biogas properties during the AD process

In this study, the effect of KOH pretreatment during biogas production from WS and the yields of biogas components such as methane and carbon dioxide contents were evaluated.

3.1.1 Daily biogas production performance. The DBP trend of the KOH pretreated WS is illustrated in Fig. 1. There were three biogas peaks across the entire AD period. The DBP trends for every reactor essentially resembled each other in each period. The first small DBP peak of WS was achieved on the fourth day, and then rapidly increased from 9 mL per g VS per day to the highest value of 34 mL per g VS per day at the second peak. It can be seen from the Fig. 2 that the pH value of R3 on the 3rd day was less than 6.5, indicating that the anaerobic fermentation condition was under acidification stage. This could be due to the sample WS was hydrolyzed and fermented into VFAs under anaerobic conditions.¹⁴ As a result, the excess concentration of VFAs caused high levels of acids accumulation, which lowered the pH of the digester and thus inhibited methanogenic activity and decreased biogas production.²¹
The pH of the system showed a slight increment with time-lapse which gradually increased the activities of methanogens that could have led to high methane production. This was due to the weakened acclimation of microorganisms caused by the digestion conditions in the reactors. The pH value of the second batch (R6) was in between 7 and 7.2 (Fig. 2), indicating that the 65 g TS per L organic loading could quickly cause a return to the optimum pH range for fermentation.\(^22\)

Furthermore, from day 19 to 21 day, the DBP then rapidly increased to achieve the last biogas production peak. Finally, the biogas production of each reaction system was below 200 mL from the start of the 29th day, and gradually decreased to zero at by end of the digestion time.

### 3.1.2 Cumulative biogas production

Three key parameters, namely cumulative methane production (CMP), cumulative carbon dioxide production (CCP) and cumulative biogas production (CBP) were used to evaluate AD performance for each reactor. The CBP, CMP and CCP of WS from AD process were shown in Fig. 3a. The CBP, CMP and CCP reached to 531, 318 and 162 mL g\(^{-1}\) VS, respectively, by the end of hydraulic retention time of AD process. More specifically, during the first 25 days of AD, the CBP reached 90% of the total biogas yield. In the remaining 20 days, the biogas production only accounted for 10%.

![Fig. 3 Cumulative biogas (CBP), methane (CMP) and CO\(_2\) (CCP) production (a) and cumulative carbon quantity of biogas (CQB), methane (CQM) and carbon dioxide (CQC) (b) of WS in batch experiments.](image)

The biodegradability and digestion efficiency of the substrate was also analyzed by measuring \(T_{90}\), where \(T_{90}\) is defined as the time required for achieving 90% of the total biogas production.\(^23\) The \(T_{90}\) in this study was achieved at 25 days (Fig. 2a). This shows that the biogas production during the AD period was mainly from the second and third peaks, which produced more methane in a relatively short period of time. Therefore, it could be confirmed that biogas production was mostly high in the second and third peaks of the methane production stage, \(i.e.\), between day 4 and day 25 of AD process.

### 3.2 Mass conversion during AD process

#### 3.2.1 TS and VS changes

AD is a substrate converted to methane and carbon dioxide by microbial consumption process, which resulting in a gradual decrease in TS and VS.\(^{23,24}\)

According to the change in the absolute mass of the substrate before and after AD, the whole TS and VS of WS can be calculated. Moreover, the degradation rate of TS and VS in AD stage are important indicators with which to evaluate the status of AD system.\(^{25}\) The TS and VS changes in the AD of WS in this study were shown in Fig. 4. During the 45 days of AD process, the final TS and VS degradation rates were 44.9% and 55.0%, respectively. From day 1 to day 24 day, that is, up to the end of the third biogas production peak, the TS and VS degradation rates gradually increased from 0% to 40.24% and 50.13%, respectively, accounting for 89.5% and 91.1% of the total degradation rates, respectively. This indicated that 90% of the biodegradable organic matter in the WS was degraded in the early and middle stages of AD. In the late stage of AD (\(i.e.\), the last 20 days), only 10% of the organic matter was degraded.

#### 3.2.2 Lignocellulosic components changes

Biomethane production potential and suitability of the specific biomass can be characterized on the basis of its relative lignocellulosic (LCH) contents. The LCH changes of WS was shown in Fig. 5a, in which the contents of lignin, cellulose and hemicellulose had different variation trend during the AD process. More specifically, the contents of cellulose and hemicellulose were decreased gradually, while the content of lignin increased from 10% to 14%. That is, in the AD process of WS, methane and
carbon dioxide were derived from the hydrolysis of cellulose and hemicellulose. Finally, lignin, cellulose and hemicellulose accounted for 14.83%, 22.65%, and 15.81% of the WS, respectively.

After 45 days of anaerobic fermentation, 64.72% of the cellulose and 62.11% of the hemicellulose in the WS were converted during the AD process compared with that found in the raw material. Conversely, the percentage of lignin did not show significant change after AD, indicating that a large amount of the organic matter remained in the solid digestate. This was consistent with the study by Weiland et al., in which 30–50% of the unused organic matter remained in the WS residue after AD.

3.3. Carbon conversion pathway in AD

3.3.1 Carbon conversion in biogas. It is known that the forms of carbon in biogas are methane (CH₄) and carbon dioxide (CO₂). The mass of carbon produced from CH₄ or CO₂ during the AD process can be calculated by CMP or CCP, as well as the corresponding proportion of carbon converted into these two substances. The van der Waals constant of methane and carbon dioxide are listed in Table 2. According to eqn (1), the

![Graph](image)

**Fig. 5** The composition analysis of LCH (a) and carbon quantity from LCH (b) during AD process.

| Gas    | a (Pa m⁶ mol⁻¹) | b (10⁵ m³ mol⁻¹) |
|--------|----------------|-----------------|
| CH₄    | 0.2283         | 4.278           |
| CO₂    | 0.3640         | 4.267           |

3.3.2 Carbon conversion in liquid digestate. In the early stage of the AD process, the products were primarily ethanol and VFAs, which are the main carbon sources for anaerobic microorganisms. Moreover, VFAs are considered as the most important intermediate product in the AD process and an indicator parameter to measure the stability of the AD system. Fig. 6a shows the different quantities of ethanol and VFAs produced in the whole AD process. After inoculation, both individual VFA and ethanol production increased significantly. After the ninth day, the content decreased rapidly, because in the methanogenic stage, the methanogens converted individual VFAs into methane.

In the anaerobic fermentation reactor, the process of biogas production occurs simultaneously with VFAs production. Therefore, the form of carbon in liquid digestate is VFAs. The mass of carbon produced from VFAs during AD process can be

![Graph](image)

**Fig. 6** The effect of different digestion time on individual VFA (a) and carbon quantity from total VFAs (b) during AD process.
calculated using individual VFA concentration and eqn (1) as shown in Fig. 6b. This indicated that the carbon quantity from VFAs increased quickly during the first ninth days, when the highest value of 23.8 g was found. Then, the value of carbon quantity slowly decreased from day 9 to day 21. Finally, as digestion time prolonged to 45 day, the carbon quantity from VFAs obtained its lowest value of 0.5 g. This was because more VFAs was converted to CH$_4$, which caused carbon to appear in the form of biogas. This was also consistent with that described in Section 3.1.2 and Fig. 3a.

3.3.3 Carbon conversion in solid digestate. The carbon that remained in the solid digestate was mainly that which was not utilized by microorganisms in the AD process. Moreover, the unused carbon is still mainly concentrated in lignin, cellulose and hemicellulose parts. In the AD process, the bacteria are unable to hydrolyze macromolecular compounds into small molecule substances, and hence, the complex LCH compounds cannot be used by methanogens.

As shown in Fig. 5b, the change in carbon content of the solid digestate in different periods during AD process was gradually reduced. The carbon quantity of the solid digestate before anaerobic fermentation was 26.6 g.

In the first 21 days of AD, the amount of carbon in the solid digestate decreased to 15.6 g, which indicated that carbon was converted into methane and carbon dioxide. The unused carbon in WS can be as much as 11.0 g. It is also obvious that a high proportion of carbon (41.4%) remained in the raw WS materials.

3.3.4 Carbon and nitrogen changes in control group. The blank AD for seeding sludge is carried out, which search for knowing the background methane production as well as the carbon and nitrogen content changes before and after AD. The cumulative methane production, carbon and nitrogen quantity changes of blank group for inoculum before and after AD was shown in Table 3.

The CBP of inoculum was 6 mL g$^{-1}$ VS after AD. Besides, before AD, the carbon quantity of inoculum (3.58 g) was far lower than that of WS (26.2 g). This was because the organic loading of inoculum was 20 g TS per L, which along with a relative low TS content. Moreover, the carbon quantity of inoculum remained in solid residue after AD was 2.94 g, which showed no obvious changes. The majority of N element in the inoculum after AD was recovered from the liquid digestate. The liquid digestate with high content of N element could be used as inoculum a showed no obvious changes. The majority of N element in the inoculum before AD was recovered from the liquid digestate. The output and input of substances in a system.

As shown in Table 3, the carbon quantity from the inoculum before and after AD was recovered from the liquid digestate. The output and input of substances in a system.

3.4. Element flow analysis in AD

3.4.1 Establishment of the material flow model. The E! Sankey 4.5 software was used to establish a model for the material flow of the AD. Anaerobic fermentation is a very complex process in which substances transform from one form to another in different phases: gas, liquid, and solid. Based on the law of conservation of mass, MFA can be used to quantify the input and output of substances in a system. This model can also be used for the establishment of material flow accounts for optimizing material management. This study focused on material conversion in the anaerobic fermentation process, where WS, inoculum and water as the input stream material of the anaerobic fermentation system shown in Fig. 7. The output stream material of the anaerobic fermentation system comprises the biogas (including methane, carbon dioxide and hydrogen) and the fermentation materials (including VFAs and residue).

3.4.2 Distribution characteristics of carbon and nitrogen. The distribution of carbon and nitrogen elements in the gas, liquid and solid phases during the AD process of WS was shown in Fig. 8. With the prolonging of AD time, the proportion of carbon in the gas phase increased, while it becomes less and less in the solid and liquid phases. This was because more biogas converted from the raw materials and VFAs. In the early and middle stages of AD, the distribution points of carbon and nitrogen elements showed dispersion in the Fig. 8, which was due to the relatively high hydrolysis acidification and methanogenesis rates. Correspondingly, the carbon element distribution in the gas phase showed increment during these stages. In the first 24 days of AD, nitrogen element in the liquid phase fluctuated between 36.53% and 57.73%. During this time, the proportion of carbon in the biogas phase increased from 1.67% to 39.39%. The carbon content in the solid phase was reduced to 50.29%. Further, at this time, the proportion of nitrogen in the solid phase decreased from 87.31% to 50.72%.

However, at the later 21 days, the proportion of carbon in the gas phase increased by only 10%, and the carbon element in the solid phase decreased for 6%. This is because in the later stage of AD, as the microbial activity decreased, the hydrolysis

| Inoculum | Before AD | After AD |
|----------|-----------|----------|
| CMP      | —         | 6 mL g$^{-1}$ VS |
| C        | —         | 0.53 g   |
| Liquid digestate | —         | 0.11 g   |
| Solid digestate | 3.58 g   | 2.94 g   |
| N        | —         | —        |
| Biogas   | —         | —        |
| Liquid digestate | —         | 0.23 g   |
| Solid digestate | 0.38 g   | 0.15 g   |

Table 3 Cumulative biogas production, carbon and nitrogen quantity changes of inoculum before and after AD

![Fig. 7 The system model for MFA of fermentation process.](image-url)
acidification and methanogenesis rates also gradually decreased, which resulted the distribution points in Fig. 8 more concentrated. Besides, the nitrogenous substance had not emerged in the biogas phase, but was focused on the liquid and the solid phases, since the red points are presented at the binary boundary line as shown in Fig. 8.

3.4.3 Carbon and nitrogen flow in anaerobic fermentation.
The MFA analysis of WS during AD followed the law of conservation of mass at all level\textsuperscript{12}. The Sankey diagram presents the changes in the AD process and the whole material analysis data in AD system was shown in Fig. 7 and Table 4. The analysis including WS, inoculum, biogas and residues, and microscopic elemental analysis of carbon and nitrogen.

Fig. 9a represents the overall mass balance of the system before and after AD. The total quantities of carbon (29.6 g) and nitrogen (1.38 g) in the system before AD is equal to the carbon quality after AD. The remaining mass, which included the urea and water was 851.31 g, did not affect the balance of carbon and nitrogen.

According to Fig. 9b, before AD, the quantities of carbon that remained in WS, water + urea and inoculum were 25.71, 0.31 and 3.58 g, respectively. After AD, carbon quantity remained in biogas, liquid and solid digestates were 14.79, 1.66 and 13.15 g, respectively. This suggested that 49.96% of the carbon element in the AD process was converted to biogas. However, the remaining carbon that existed in the liquid and solid digestates accounted for 5.61% and 44.43%, respectively. In summary,

### Table 4 Material data for MFA before and after anaerobic digestion of wheat straw

| Material          | Element | Mass (g) | Content (%) |
|-------------------|---------|----------|-------------|
| Wheat straw       | C       | 25.71    | 86.86       |
|                   | N       | 0.28     | 20.29       |
|                   | Others  | 29.46    | 95.60       |
| Urea and water    | C       | 0.31     | 1.05        |
|                   | N       | 0.72     | 52.17       |
|                   | Others  | 815.09   | 95.60       |
| Inoculum          | C       | 3.58     | 12.09       |
|                   | N       | 0.38     | 27.54       |
|                   | Others  | 8.04     | 95.60       |

| Material          | Element | Mass (g) | Content (%) |
|-------------------|---------|----------|-------------|
| Biogas            | C       | 14.79    | 49.96       |
|                   | N       | —        | —           |
| Liquid digestate  | C       | 1.66     | 5.61        |
|                   | N       | 0.63     | 46.65       |
|                   | Others  | 816.18   | 95.73       |
| Solid digestate   | C       | 13.15    | 44.43       |
|                   | N       | 0.75     | 54.35       |
|                   | Others  | 23.45    | 2.75        |
during the process of biogas production from WS anaerobic fermentation, the utilization of carbon to methane was 50.04%.

Similarly, before AD, the quantities of nitrogen remained in WS, water + urea and inoculum were 0.28, 0.72 and 0.38 g, respectively. After AD, nitrogen remained in biogas, liquid and solid digestates were 0.00, 0.63 and 0.75 g, respectively (Fig. 9c). This indicated that the nitrogen element remaining in the biogas and the liquid digestate, accounting for 0% and 45.65%, respectively. At the same time, 54.35% of the nitrogen element was remained in the solid digestate.

These results demonstrated that half of organic matters mainly in WS was not fully utilized. In order to strengthen the use of organic matters, either enhance the productivity of biogas or increase the use of organic fertilizers.22 In other words, the rational development of fermentation residues for solid and liquid organic fertilizers may improve the material conversion efficiency of resources, and it also decrease environmental pollution.

4. Conclusions

During the AD process of KOH pretreated WS, carbon conversion is primarily derived from biogas, VFAs and LCH. The results showed that the highest carbon conversion rate in biogas was achieved at day 24, which accounted for 70.64% of carbon. Simultaneously, the carbon quantity from VFAs showed the highest and lowest values of 23.8 g and 0.5 g at day 9 and day 45, respectively. The material conversion efficiency of WS during anaerobic fermentation process was 49.97% and the methane conversion rate was 40.24%. The MFA results indicated that the flow mass fraction of carbon in biogas, solid and liquid digestates were 49.96%, 44.43% and 5.61%, respectively. Therefore, this study could provide a theoretical basis for elemental flow and contents of each product from the biogas production of WS.

Conflicts of interest

There are no conflicts to declare.

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References

1 Food and Agriculture Organization of the United Nations, http://www.fao.org/home/en/, 2018.
2 C. M. Liu, A. C. Wachemo, H. R. Yuan, D. X. Zou, Y. P. Liu and L. Zhang, Renewable Energy, 2018, 116, 224–233.
3 J. J. Xie, Y. L. Luo, C. X. Zheng, Y. U. Xiong, H. T. Jia and C. L. Wang, China Cattle Sci., 2010, 36, 36–40.
4 J. Li, A. C. Wachemo, H. Yuan, X. Zuo and X. Li, Bioresour. Technol., 2019, 288, 121518.
5 B. S. Padam, H. S. Tin, F. Y. Chye and M. I. Abdullah, J. Food Sci. Technol., 2014, 51, 3527–3545.
6 C. C. Garcia, L. D. Mirquez and M. Hernandez, Environ. Technol. Innov., 2018, 10, 215–222.
7 S. C. Huang, T. T. Liu, B. Y. Peng and A. L. Geng, Bioprocess Biosyst. Eng., 2019, 42, 883–896.
8 C. M. Liu, H. R. Yuan and D. X. Zou, BioMed Res. Int., 2015, 12, 1–9.
9 M. Korai, A. C. Wachemo, L. Yue, M. Jaffar and X. Li, RSC Adv., 2020, 10, 9290–9298.
10 P. H. Brunner and H. Rechberger, Practical Handbook of Material Flow Analysis, Lewis Publishers, Boca Raton, FL, London, 2004.
11 A. Allesch and H. P. Brunner, Environ. Sci. Technol., 2017, 51, 540–551.
12 H. Z. Niu, X. Y. Kong and L. H. Li, CIESC J., 2015, 2, 723–729.
13 F. Zhen, Y. M. Sun and X. Y. Kong, Trans. Chin. Soc. Agric. Eng., 2017, 10, 236–241.
14 M. Jaffar, Y. Pang, H. Yuan, D. Zou, Y. Liu, B. Zhu, R. M. Korai and X. Li, Chin. J. Chem. Eng., 2016, 24, 404–409.
15 R. Zhang and Z. Zhang, Bioresour. Technol., 1999, 68, 235–245.
16 Y. Wei, X. Li, L. Yu, D. Zou and H. Yuan, Bioresour. Technol., 2015, 198, 431–436.
17 P. J. Van Soest, J. B. Robertson and B. A. Lewis, J. Dairy Sci., 1991, 74, 3583–3597.
18 J. Li, A. C. Wachemo, G. Yu and X. Li, J. Cleaner Prod., 2019, 119112.
19 F. G. Ran, M. Z. Hauschild, E. Tomas, G. Jeroen, H. Reinout, H. Stefanie, K. Annette, P. David and S. Sangwon, J. Environ. Manage., 2010, 91, 1–21.
20 F. Pennini and A. Plastino, Phys. A, 2016, 458, 239–247.
21 S. N. Misi and C. F. Forster, Bioresour. Technol., 2001, 80, 19–28.
22 H. Bouallagui, Y. Touhami, R. B. Cheikh and M. Hamdi, J. Cheminf., 2005, 36, 989–995.
23 H. R Yuan, R. P. Li and Y. T. Zhang, Biosyst. Eng., 2015, 129, 142–148.
24 J. Li, A. C. Wachemo, H. Yuan, X. Zuo and X. Li, Waste Manage., 2019, 97, 52–62.
25 H. R. Yuan, Y. Y. Lan and J. L. Zhu, Chin. J. Chem. Eng., 2019, 27, 200–207.
26 I. Angelidaki and B. K. Ahring, Appl. Microbiol. Biotechnol., 1993, 38, 560–564.
27 Y. Wang, Y. Zhang, L. Meng, J. Wang and W. Zhang, Biomass Bioenergy, 2009, 33, 1131–1138.
28 S. K. Khanal, M. Rasmussen, P. Shrestha, H. J. Van Leeuwen, C. Visvanathan and H. Liu, Water Environ. Res., 2008, 80, 1625–1647.
29 P. Weiland, Appl. Microbiol. Biotechnol., 2010, 85, 849.
30 G. Wang, H. N. Gavala, I. V. Skiadas and B. K. Ahring, Waste Manage., 2009, 29, 2830–2835.
31 M. Berni, I. Dorileo, G. Nathia, T. Forster-Carneiro and B. G. M. Santos, Int. J. Chem. Eng., 2014, 1, 1–8.
32 T. Forster-Carneiro, M. D. Berni, D. Lachos-Perez, I. L. Dorileo and M. A. Rostagno, Int. J. Environ. Sci. Technol., 2017, 14, 2077–2092.